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Final Drainage Report

Arvidson Subdivision

Project No. 61049

June 12, 2017

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ADD: all three project numbers to the bottom of this report (MS. P, ADR)

Final Drainage Report

for

Arvidson Subdivision

Project No. 61049

June 12, 2017

prepared for

Matthew and Jenna Arvidson 2310 Wakonda Way Monument, CO 80132 970.381.

prepared by

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5 MARS Anvigs and Minor Subdivision PAIR Figure Destroys Report par

Statements and Acknowledgments

Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are
correct to the best of my knowledge and belief. Said drainage report has been prepared according
to the criteria established by the County for drainage reports and said report is in conformity with the
applicable master plan of the drainage basin. I accept responsibility for any liability caused by any
negligent acts, errors or omissions on my part in preparing this report.
applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

David R. Gorman, P.E. For and on Behalf of MVE, Inc.	Colorado No. 3	31672 D	ate	
Developer's Statement	الأسماد الأساد المسادر	ith all of the requi	iroments specified in	this
I, the owner/developer have rea drainage report and plan.	id and will comply w	nur all of the requ	merinente apcoince in	
Matthew Arvidson	Date	Jenna Arvidson	Date	
Owner 2310 Wakonda Way Monument, CO 80132		Owner 2310 Wakonda W Monument, CO 80		
El Paso County				
Filed in accordance with the rec Paso County Engineering Criteria	quirements of the Dra Manual and Land De	ainage Criteria Man evelopment Code as	ual, Volumes 1 and 2 s amended.	2, El
Jennifer Irvine, P.E.,			Date	
County Engineer / ECM Administ	rator			

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Final Drainage Report

The purpose of this Final Drainage Report is to identify drainage patterns and quantities within and affecting the proposed Arvidson Subdivision . This plat is the subdivision of a 5.45± Acre parcel into two lots. The report will "identify specific solutions to problems on-site and off-site resulting from the proposed project.¹ The report and included maps present results of hydrologic and drainage facilities analyses. The report will discuss the recommended drainage improvements to the site and identify drainage requirements relative to the proposed project. This report has been prepared and submitted in accordance with the requirements of the El Paso County Final Plat approval process. An Appendix is included with this report with pertinent calculations and graphs used in the facility design and drainage analyses.

1 General Location and Description

1.1 Location

The proposed Arvidson Subdivision site is located within the southeast one-quarter of Section 3, Township 11 South, Range 67 west of the 6th principal meridian in El Paso County, Colorado. The 5.45± acre site is situated on the north side of Wakonda Way, west of Beacon Lite Rd and east of Aries Dr. The proposed site has never been platted. A **Vicinity Map** is included in the **Appendix**.

The property to the south is part of platted subdivision: Tract 33, Wakonda Hills, Subdivision, No.1. The property to the east, west, and north are not platted. The properties to the south are zoned RR-.5 (Residential Rural) and are used as single family residencies and vacant residential lots. The property to the southeast is zoned as I-2 (Limited Industrial) and is used as a warehouse/storage facility. The property to the east is zoned as RR-2.5 (Rural Residential) and is used as a single family residence. The property to the northeast is zoned C-1 (Commercial Obsolete) and is used for single family residencies. The property to the north is zoned at RR-5 (Rural Residential) and is used as a single family residence.

1.2 Description of Property

Arvidson Subdivision contains 5.45± acres zoned RR-5 (Rural Residential). The property contains one existing residence, gravel drive, and auxiliary structures. The property is planned to be rezoned RR-2.5 (Rural Residential).

The southeast portion of the site is grass meadow and the northwest portion is wooded hillside. The ground cover, which is in good condition, consists of native grasses and trees. The existing site topography slopes to the southwest with grades that range from 2% to 10% towards of Wakonda Way.

According to the National Resource Conservation Service, the dominant soil in the immediate area of the Arvidson Subdivision site is Kettle gravelly loam (map unit 41). The Kettle gravelly loam is typically deep and well drained. Permeability is rapid, surface runoff is medium, and the hazard of erosion is moderate. Kettle gravelly loam is classified as being part of Hydrologic Soil Group B. A

¹ DCM, 4-6

Please describe proposed condition and show any hazards Drainage Basins and Sub-Basins as described in the geologic report.

Existing off site sub-basin OSA1 is north and east of the site. These flows enter sub-basin A2 and travelwesterly into a V ditch along Beacon Lite Rd before flowing southerly to Point of Interest 1. The combined flows of OSA1 and A2 drain toward Point of Interest 2, a low point on Wakonda Way, where flows from OSA1, A2, and A3 combine.

ditch and

please show Please elaborate where the flow

3 Drainage Design Criteria

POI's on plan.

goes next.

3.1 Development Criteria Reference

This Final Drainage Report for Arvidson Subdivision has been prepared according to the report guidelines presented in the latest edition of El Paso County Drainage Criteria Manual (DCM)5. The hydrologic analysis is based on a collection of data from the DCM, the NCSS Web Soil Survey⁶, and proposed lot layout by M.V.E., Inc.

3.2 Hydrologic Criteria

For this Final Drainage Report, the Rational Method as described in the Drainage Criteria Manual has been used for all Storm Runoff calculations, as the development and all sub-basins are less than 130 acres in area. "Colorado Springs Rainfall Intensity Duration Frequency" curves, Figure 6-5 in the DCM, was used to obtain the design rainfall values; a copy is included in the Appendix. The "Overland (Initial) Flow Equation" (Eq. 6-8) in the DCM, and Manning's equation with estimated depths were used in time of concentration calculations. "Runoff Coefficients for Rational Method", Table 6-6 in the DCM, was utilized as a guide in estimating runoff coefficient and Percent Impervious values; a copy is included in the Appendix. Peak runoff discharges were calculated for each drainage sub-basin for both the 5-year storm event and the 100-year storm event with the Rational Method formula, (Eq. 6-5) in the DCM.⁷

No other drainage reports for any of the adjacent properties are available for review during the course of preparing this drainage report.

4 Drainage Facility Design

4.1 General Concept

The intent of the drainage concept presented in this Final Drainage Report is to maintain the existing drainage patterns & quantities on the site. Major and minor storm flows will continue to be safely conveyed through the site and downstream.

The existing and proposed drainage hydrologic conditions are described in more detail below. Input data and results for all calculations are included in the Appendix. Drainage maps for the hydrology are also included in the Appendix.

4.2 Specific Details

4.2.1 Existing Hydrologic Conditions

The off-site drainage area north and east of the site, Basin OSA 1, contains 9.76 acres draining to the site. Discharges of $Q_5 = 4$ cfs and $Q_{100} = 22.5$ cfs (existing flows) flow on site into Basin A2.

Existing sub-basin A2 (0.54 acres) is comprised of a portion of Wakonda Way, a portion of Beacon Lite Rd, and a portion of the land east of Beacon Lite Rd. The discharges generated by A2 are Q₅ = 1.4 cfs and $Q_{100} = 2.9$ cfs (existing flow), which drains southerly along Beacon Lite Rd via V ditch and continues to flow westerly along the northern edge of Wakonda Way to a low point as described in Section 2.2 above. The combined flows at Point of Interest 1 for OSA1 and A2 are Q₅ = 5.0 cfs and $Q_{100} = 24.2$ cfs (existing flows).

DCM Section 4,3 and Section 4.4

DCM

4.3 Downstream Facilities

The existing 24" Corrugated Metal Pipe (CMP) pipe culvert located at the low point on the north side of Wakonda Way will continue to be utilized for draining the flows from sub-basins OSA1, A2 and A3 from the north side of Wakonda Way to the property to the south as in the existing conditions. The proposed subdivision has negligible effects on stormwater flows from the property.

5 Drainage and Bridge Fees

The site is located in the Palmer Lake Major Drainage Basin. Development in this basin carries Drainage Fees of \$11,276.00 per impervious acre. The impervious area does not consider the Right of Way from Wakonda Way or from Beacon Lite Rd. The Drainage Fees for the subdivision are calculated below:

Arvidson Subdivision

Drainage Fees:

Drainage Fees = Platted Area x %imperviousness x \$11,276.00

Drainage Fees = $4.82 \text{ Ac} \times 0.081 \times \$11,276.00 = \$4,402.38$

These Drainage Fees will be paid by the Developer at the filing of the plat-

6 Conclusion

This Final Drainage Report presents existing and proposed drainage conditions for the proposed subdivision. The subdivision development will have negligible and inconsequential effects on the existing site drainage and drainage conditions downstream. The proposed project will not, with respect to stormwater runoff, negatively impact the adjacent properties and downstream properties.

Please show on plan, as well if there is a driveway culvert.

Please add a statement as to why there is no water quality required for this site.

References

City of Colorado Springs/El Paso County Drainage Criteria Manual. City of Colorado Springs, Department of Public Works, Engineering Division; HDR Infrastructure, Inc.; El Paso County, Department of Public Works, Engineering Division (Colorado Springs: City of Colorado Springs, Revised November 1991).

Drainage Area Identification Study. Muller Engineering Company, Inc. (Lakewood, CO: , 1986).

Flood Insurance Rate Map. Federal Emergency Management Agency, National Flood Insurance Program (Washington D.C.: FEMA, March 17, 1997).

Flood Insurance Study for El Paso County, Colorado and incorporated Areas. Federal Emergency Management Agency (Washington D.C.: FEMA, March 17, 1997).

NCSS Web Soil Survey. United States Department of Agriculture, Natural Resources Conservation Service ("http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx", accessed May 1, 2008).

City of Colorado Springs Drainage Criteria Manual Volume 1. City of Colorado Springs Engineering Division with Matrix Design Group and Wright Water Engineers (Colorado Springs, Colorado: , May 2014).

References

City of Colorado Springs/El Paso County Drainage Criteria Manual. City of Colorado Springs, Department of Public Works, Engineering Division; HDR Infrastructure, Inc.; El Paso County, Department of Public Works, Engineering Division (Colorado Springs: City of Colorado Springs, Revised November 1991).

Drainage Area Identification Study. Muller Engineering Company, Inc. (Lakewood, CO: , 1986).

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NCSS Web Soil Survey. United States Department of Agriculture, Natural Resources Conservation Service ("http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx", accessed May 1, 2008).

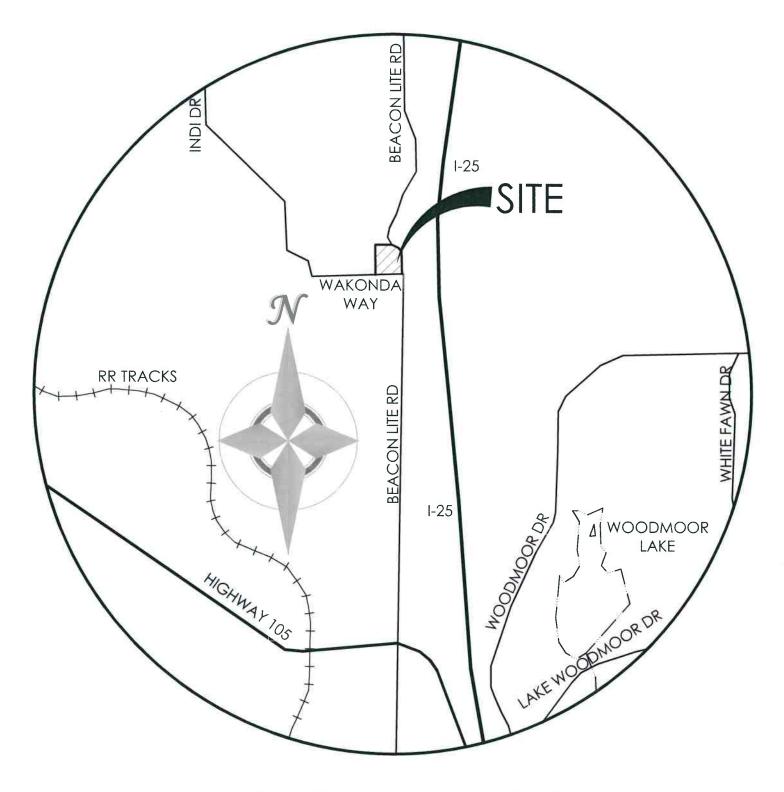
City of Colorado Springs Drainage Criteria Manual Volume 1. City of Colorado Springs Engineering Division with Matrix Design Group and Wright Water Engineers (Colorado Springs, Colorado: , May 2014).

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Appendices

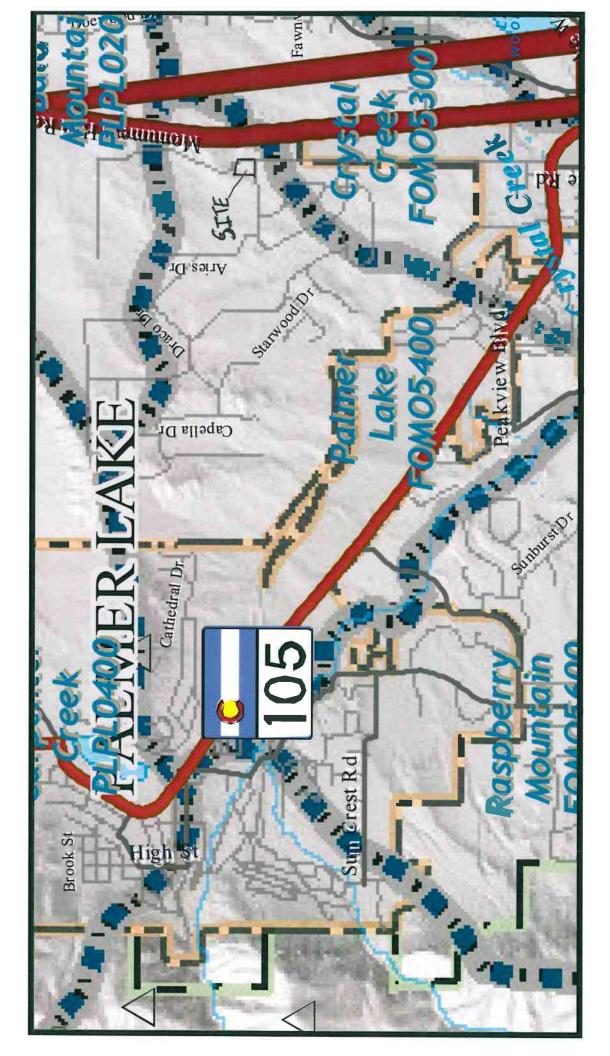
1 General Maps and Supporting Data

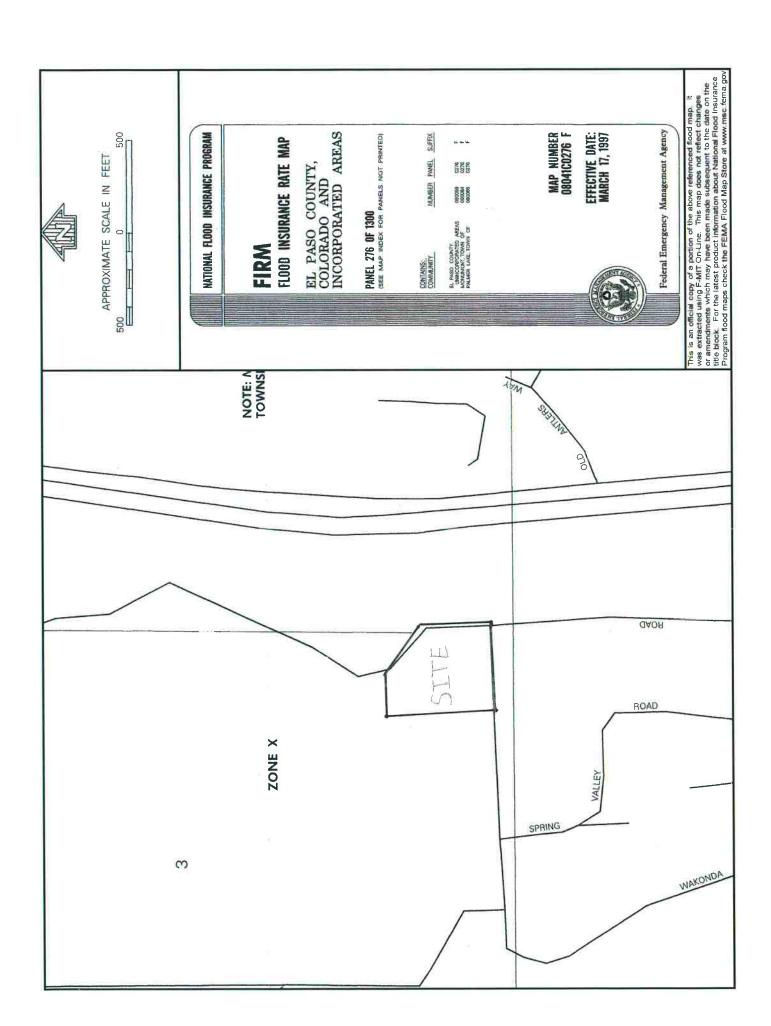
Vicinity Map Portion of Flood Insurance Rate Map Soil Type map and Tables Official Soil Series Descriptions Hydrologic Soil Group Map and Tables



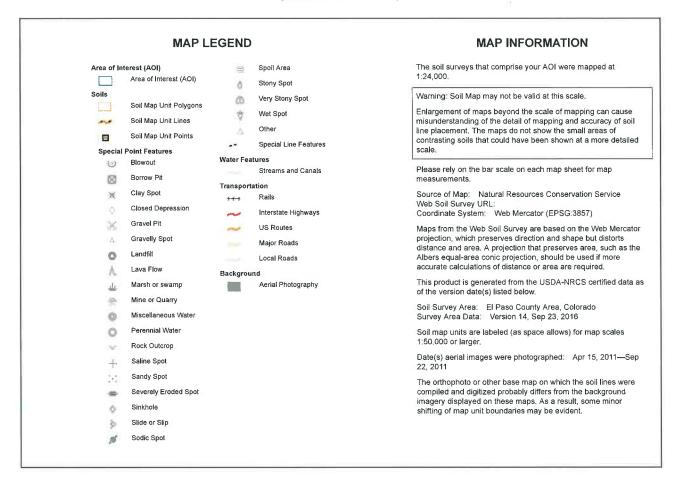
VICINITY MAP

NOT TO SCALE









Map Unit Legend

	El Paso County Area, C	Colorado (CO625)	
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Alamosa loam, 1 to 3 percent slopes	0.1	0.8%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	7.6	98.5%
92	Tomah-Crowfoot loamy sands, 3 to 8 percent slopes	0.1	0.7%
Totals for Area of Interest		7.7	100.0%

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cludes some of each of the two or more dominant soils, and the pattern and proportion are somewhat similar in all areas. Elbeth-Pring complex, 5 to 30 percent slopes, is an example.

An undifferentiated group is made up of two or more soils that could be mapped individually but are mapped as one unit because there is little value in separating them. The pattern and proportion of the soils are not uniform. An area shown on the map has at least one of the dominant (named) soils or may have all of them. Olney and Vona soils, eroded, is an undifferentiated group in this survey area.

Most map units include small, scattered areas of soils other than those that appear in the name of the map unit. Some of these soils have properties that differ substantially from those of the dominant soil or soils and thus could significantly affect use and management of the map unit. These soils are described in the description of each map unit. Some of the more unusual or strongly contrasting soils that are included are identified by a special symbol on the soil map.

Most mapped areas include places that have little or no soil material and support little or no vegetation. Such places are called *miscellaneous areas*; they are delineated on the soil map and given descriptive names. Pits, gravel is an example. Some of these areas are too small to be delineated and are identified by a special symbol on the soil map.

The military impact area described in some map units consists of a large area on the Fort Carson Military Reservation. It is used as an artillery and bombing target area. This area has not been surveyed, but most of the soils mapped adjacent to the area are in the Heldt, Kim, Midway, Razor, and Wiley series. It is estimated that most of the impact area is Razor-Midway complex.

The acreage and proportionate extent of each map unit are given in table 4, and additional information on properties, limitations, capabilities, and potentials for many soil uses is given for each kind of soil in other tables in this survey. (See "Summary of tables.") Many of the terms used in describing soils are defined in the Glossary.

Soil descriptions

1—Alamosa loam, 1 to 3 percent slopes. This deep, poorly drained soil formed in alluvium on flood plains and fans. Elevation ranges from 7,200 to 7,700 feet. The average annual precipitation is about 18 inches, the average annual air temperature is about 42 degrees F, and the average frost-free period is about 120 days.

Typically, the surface layer is dark gray loam about 6 inches thick. The subsoil is clay loam about 27 inches thick; it is very dark gray in the upper part and gray in the lower part. The substratum is dark greenish gray and light gray sandy clay loam and sandy loam. Mottles are common in the subsoil and substratum.

Included with this soil in mapping are small areas of Ellicott loamy coarse sand, 0 to 5 percent slopes;

Cruckton sandy loam, 1 to 9 percent slopes; Peyton sandy loam, 1 to 5 percent slopes; and Pring coarse sandy loam, 3 to 8 percent slopes.

Permeability of this Alamosa soil is moderately slow. Effective rooting depth is 60 inches or more. Available water capacity is high. Organic matter content of the surface layer is high. This soil has a high water table, usually between May and October. Surface runoff is slow, and the hazard of erosion is slight.

This soil is used mostly for native hay or pasture.

The potential plant community is mainly slender wheatgrass, Baltic rush, Nebraska sedge, timothy, and reedgrasses. Willows are a part of the plant community.

If the range has deteriorated, it consists mostly of Kentucky bluegrass and willows. If overgrazing is severe, denuding of the soil and gullying are possible and reestablishment of a good plant cover is very difficult. Where seeding is practical, smooth brome, orchardgrass, Garrison creeping foxtail, or reed canarygrass should be used.

Wet areas of this soil are well suited to shallow water developments, which encourage wetland wildlife such as waterfowl and a number of shore birds. Because of the availability of moisture, this soil provides excellent waterfowl nesting cover. Rangeland wildlife, such as deer and cottontail, use the areas where excellent cover is provided by willows, rushes, and other wetland vegetation. Wildlife on this soil can best be aided by using proper livestock grazing practices and allowing natural vegetation, such as willows and cattails, to grow.

This soil has poor potential for homesites. The main limitations for this use are a high water table and the hazard of flooding. Capability subclass Vw.

2—Ascalon sandy loam, 1 to 3 percent slopes. This deep, well drained soil formed in mixed alluvium and wind-laid material on uplands. Elevation ranges from 5,500 to 6,500 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 48 degrees F, and the average frost-free period is about 140 days.

Typically, the surface layer is brown sandy loam about 8 inches thick. The subsoil is brown, yellowish brown, and pale brown sandy clay loam about 22 inches thick. The substratum is calcareous, very pale brown sandy loam and loamy sand.

Included with this soil in mapping are small areas of Bresser sandy loam, 0 to 3 percent slopes; Olney sandy loam, 0 to 3 percent slopes; Vona sandy loam, 1 to 3 percent slopes; and Fort Collins loam, 0 to 3 percent slopes.

Permeability of this Ascalon soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Organic matter content of the surface layer is medium. Surface runoff is slow, and the hazards of erosion and soil blowing are moderate.

This soil is used mainly as cropland.

A typical rotation is wheat and summer fallow. Summer fallow is necessary because rainfall is insufficient for yearly cropping. Feed grains such as millet are used as a pricklypear occur. Ample amounts of litter and forage should be left on the soil because of the high hazard of soil blowing.

Windbreaks and environmental plantings are generally well suited to this soil. Summer fallow a year prior to planting and continued cultivation for weed control are needed to insure establishment and survival of plantings. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, Siberian peashrub, and American plum.

Depending on land use, this soil can produce habitat that is suitable for either rangeland wildlife, such as antelope, or for openland wildlife, such as pheasant, cottontail, and mourning dove. Availability of irrigation water largely determines the land use. Where no irrigation water is available, this soil is mainly used as rangeland, a use that favors rangeland wildlife. If this soil is used as rangeland, fences, livestock water developments, and proper livestock grazing use are practices that enhance habitat for rangeland wildlife. Production of crops such as wheat, corn, and alfalfa provides suitable habitat for openland wildlife, especially pheasant. Among the practices that increase openland wildlife populations are planting trees and shrubs and providing undisturbed nesting cover.

The main limitation of this soil for urban use is shrinkswell potential. Buildings and roads need to be designed to overcome this limitation. Roads need to be designed to minimize frost-heave damage. Capability subclasses IVe, nonirrigated, and IIe, irrigated.

40—Kettle gravelly loamy sand, 3 to 8 percent slopes. This deep, well drained soil formed in sandy arkosic deposits on uplands. Elevation ranges from 7,000 to 7,700 feet. The average annual precipitation is about 18 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 120 days.

Typically, the surface layer is gray gravelly loamy sand about 3 inches thick. The subsurface layer is light gray gravelly loamy sand about 13 inches thick. The subsoil is very pale brown gravelly sandy loam about 24 inches thick. It consists of a matrix of loamy coarse sand that has thin bands of coarse sandy loam or sandy clay loam. The substratum to a depth of 60 inches or more is light yellowish brown extremely gravelly loamy sand.

Included with this soil in mapping are small areas of Alamosa loam, 1 to 3 percent slopes; Elbeth sandy loam, 3 to 8 percent slopes; Pring coarse sandy loam, 3 to 8 percent slopes; Tomah-Crowfoot loamy sands, 3 to 8 percent slopes; and a few rock outcrops.

Permeability of this Kettle soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Surface runoff is slow, and the hazard of erosion is slight to moderate. A few gullies have formed in drainageways.

This soil is used for woodland, livestock grazing, wildlife habitat, recreation, and homesites.

This soil is suited to the production of ponderosa pine. It is capable of producing about 2,240 cubic feet or 4,900 board feet (International rule), of merchantable timber per acre from a fully stocked, even-aged stand of 80-year-old trees. The main limitation for the production or harvesting of timber is the low available water capacity. The low available water capacity also influences seedling survival, especially in areas where understory plants are plentiful. Erosion must be kept to a minimum when harvesting timber.

This soil has good potential for mule deer, tree squirrels, cottontail rabbit, and wild turkey. These animals obtain their food and shelter from pine trees, shrubs, and ground cover, which provide browse, forbs, fruit, and seeds. The presence of ponderosa pine and Gambel oak should encourage wild turkey populations; however, where water is not naturally present, wildlife watering facilities must be provided to attract and maintain wild turkey and other wildlife species. Livestock grazing management is vital on this soil if wildlife populations are to be maintained.

This soil has good potential for use as homesites. Plans for homesite development on this soil should provide for the preservation of as many trees as possible in order to maintain the esthetic value of the sites. During seasons of low precipitation, fire may become a hazard to homesites. This hazard can be minimized by installing firebreaks and reducing the amount of litter on the forest floor. Capability subclass VIe.

41—Kettle gravelly loamy sand, 8 to 40 percent slopes. This deep, well drained soil formed in sandy arkosic deposits on uplands. Elevation ranges from 7,000 to 7,700 feet. The average annual precipitation is about 18 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 120 days.

Typically, the surface layer is gray gravelly loamy sand about 3 inches thick. The subsurface layer is light gray gravelly loamy sand about 13 inches thick. The subsoil is very pale brown gravelly sandy loam about 24 inches thick. It consists of a matrix of loamy coarse sand that has thin bands of coarse sandy loam or sandy clay loam. The substratum to a depth of 60 inches or more is light yellowish brown extremely gravelly loamy sand.

Included with this soil in mapping are small areas of Elbeth sandy loam, 8 to 15 percent slopes; Pring coarse sandy loam, 8 to 15 percent slopes; Tomah-Crowfoot loamy sands, 8 to 15 percent slopes; and a few rock outcrops.

Permeability of this Kettle soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Surface runoff is medium, and the hazard of erosion is moderate. Some gullies have formed in drainageways.

The soil is used for woodland, livestock grazing, wildlife habitat, recreation, and homesites.

This soil is suited to the production of ponderosa pine. It is capable of producing 2,240 cubic feet, or 4,900 board

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feet (International rule), of merchantable timber per acre from a fully stocked, even-aged stand of 80-year-old trees. The main limitation for this use is the moderate hazard of erosion. Measures must be taken to reduce erosion when harvesting timber, especially on the steeper slopes. The low to moderate available water capacity also influences seedling survival, especially in areas where understory plants are plentiful.

This soil has good potential for mule deer, tree squirrel, cottontail, and wild turkey. These animals obtain their food and shelter from pine trees, shrubs, and ground cover, which provide browse, forbs, fruit, and seeds. The presence of ponderosa pine and Gambel oak should encourage wild turkey populations; however, where water is not naturally present, wildlife watering facilities must be provided to attract and maintain wild turkey and other wildlife species. Livestock grazing management is vital on this soil if wildlife populations are to be maintained.

The moderately sloping to steep slopes limit the suitability of this soil for homesites. Special practices must be provided to minimize surface runoff and thus keep erosion to a minimum. This soil requires special site or building designs because of the slope. Deep cuts, to provide essentially level building sites, may expose bedrock. Access roads must be designed to provide adequate cut-slope grade, and drains must be used to control surface runoff and keep soil losses to a minimum. During seasons of low precipitation, fire may become a hazard to homesites. This hazard can be minimized by installing firebreaks and reducing the amount of litter on the forest floor. Capability subclass VIe.

42—Kettle-Rock outcrop complex. This gently rolling to very steep complex, is mostly on the side slopes of uplands. Slopes range from 8 to 60 percent. Elevation ranges from 6,800 to 7,700 feet. The average annual precipitation is about 18 inches, and average annual air temperature is about 43 degrees F.

The Kettle soil makes up about 60 percent of the complex, Rock outcrop about 20 percent, and other soils about 20 percent.

Included with this complex in mapping are areas of Peyton-Pring complex, 8 to 15 percent slopes; Elbeth sandy loam, 8 to 15 percent slopes; and Elbeth-Pring complex, 5 to 50 percent slopes.

The Kettle soil is deep and well drained. It formed in sandy arkosic deposits, mostly on the lower slopes of the complex. Slope is commonly less than 20 percent. Typically, the surface layer is gray, medium acid or slightly acid gravelly loamy sand about 3 inches thick. The subsurface layer is light gray, medium acid gravelly loamy sand about 13 inches thick. The subsoil is very pale brown, medium acid or slightly acid gravelly sandy loam about 24 inches thick. It consists of loamy coarse sand that has thin bands of coarse sandy loam or sandy clay loam. The substratum to a depth of 60 inches or more is light yellowish brown extremely gravelly loamy sand.

Permeability of the Kettle soil is rapid. Effective rooting depth is more than 60 inches. Available water capaci-

ty is low to moderate. Surface runoff is medium to rapid, and the hazard of erosion is slight to high. Soil slippage and deep gullies are common.

Rock outcrop is mostly in the form of vertical cliffs. Large stones are common on the lower slopes of this complex.

This complex is suited to the production of ponderosa pine. It is capable of producing 2,240 cubic feet, or 4,900 board feet (International rule), of merchantable timber per acre from a fully stocked, even-aged stand of 80-year-old trees. The main limitation of this complex for this use is the presence of Rock outcrop and the moderate hazard of erosion on the Kettle soil. Measures must be taken to minimize erosion when harvesting timber, especially on the steeper slopes. The low to moderate available water capacity also influences seedling survival, especially where understory plants are plentiful.

This complex has good potential for producing habitat for mule deer, tree squirrels, cottontail, and wild turkey. These animals obtain their food and shelter from pine trees, shrubs, and ground cover, which provide browse, forbs, fruit, and seeds. The presence of ponderosa pine and Gambel oak should encourage wild turkey populations; however, where water is not naturally present, wildlife watering facilities must be provided to attract and maintain wild turkey and other wildlife species. Livestock grazing management is vital on this soil if wildlife populations are to be maintained.

The moderate to very steep slopes limit the potential of this complex for homesites. Special practices must be provided to minimize surface runoff and thus keep erosion to a minimum. Special site or building designs are required because of the slope. Deep cuts, to provide essentially level building sites, can expose bedrock. The limitation of large stones on the soil surface can be overcome through the use of heavy equipment when preparing building sites. Access roads must be designed to provide adequate cut-slope grade, and drains must be used to control surface runoff and thus keep soil losses to a minimum. Deep cuts along the uphill side of the roads can expose the bedrock. Capability subclass VIIe.

43—Kim loam, 1 to 8 percent slopes. This deep, well drained soil formed in calcareous loamy sediment on fans and uplands. Elevation ranges from 5,300 to 5,600. The average annual precipitation is about 13 inches, the average annual temperature is about 49 degrees F, and the average frost-free period is about 145 days.

Typically, the surface layer is brown loam about 4 inches thick. The substratum is very pale brown loam to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Fort Collins loam, 3 to 8 percent slopes; Midway clay loam, 3 to 25 percent slopes, and Wiley silt loam, 3 to 9 percent slopes.

Permeability of this Kim soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is high. Surface runoff is medium, and the hazard of erosion is moderate.

Almost all areas of this soil are used as rangeland.

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strength. Special designs for buildings and roads are required to offset these limitations. Methods of sewage disposal other than septic tank absorption fields are needed because of the limited depth to bedrock. Capability subclass VIe.

92—Tomah-Crowfoot loamy sands, 3 to 8 percent slopes. These gently sloping to moderately sloping soils are on alluvial fans, hills, and ridges in the uplands. Elevation ranges from about 7,300 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 42 degrees F, and the average frost-free period is about 120 days.

The Tomah soil makes up about 50 percent of the complex, the Crowfoot soil about 30 percent, and other soils about 20 percent.

Included with these soils in mapping are areas of Elbeth sandy loam, 3 to 8 percent slopes; Kettle gravelly loamy sand, 3 to 8 percent slopes; and Pring coarse sandy loam, 3 to 8 percent slopes.

The Tomah soil is deep and well drained. It formed in alluvium or residuum derived from arkose beds. Typically, the surface layer is dark grayish brown loamy sand about 10 inches thick. The subsurface layer is very pale brown coarse sand about 12 inches thick. The subsoil, about 26 inches thick, is a matrix of very pale brown coarse sand in which are embedded many thin bands and lamellae of pale brown coarse sandy clay loam. The substratum is very pale brown coarse sand to a depth of 60 inches or more.

Permeability of the Tomah soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazard of erosion is slight to moderate.

The Crowfoot soil is deep and well drained. It formed in sediment weathered from arkosic sandstone. Typically, the surface layer is grayish brown loamy sand about 12 inches thick. The subsurface layer is very pale brown sand about 11 inches thick. The subsoil is light yellowish brown sandy clay loam about 13 inches thick. The substratum is very pale brown coarse sand to a depth of about 68 inches.

Permeability of the Crowfoot soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazard of erosion is slight to moderate.

This complex is used as rangeland, for wildlife habitat, and as homesites.

Native vegetation is mainly mountain muhly, bluestem, mountain brome, needleandthread, and blue grama. These soils are subject to invasion by Kentucky bluegrass and Gambel oak. Noticeable forbs are hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat.

Properly locating livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to protect the plant cover.

Windbreaks and environmental plantings are fairly well suited to these soils. Blowing sand and moderate available water capacity are the principal limitations for the

establishment of trees and shrubs. The soils are so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

These soils are best suited to habitat for openland wildlife such as pronghorn antelope and sharp-tailed grouse. Although sharp-tailed grouse are not plentiful, they could be encouraged on these soils, especially where brush species are interspersed with grasses and forbs. If these soils are used as rangeland, wildlife production can be increased by managing livestock grazing to preclude overuse of the more desirable grass species and depletion of the various brush species.

These soils have good potential for use as homesites. The main limitation of the Crowfoot soil is frost-action potential. Roads and streets need to be designed to minimize frost-heave damage. Maintaining the existing vegetation on building sites during construction helps to control erosion. Capability subclass IVe.

93—Tomah-Crowfoot loamy sands, 8 to 15 percent slopes. These moderately sloping to strongly sloping soils are on alluvial fans, hills, and ridges in the uplands. Elevation ranges from about 7,300 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 42 degrees F, and the average frost-free period is about 120 days.

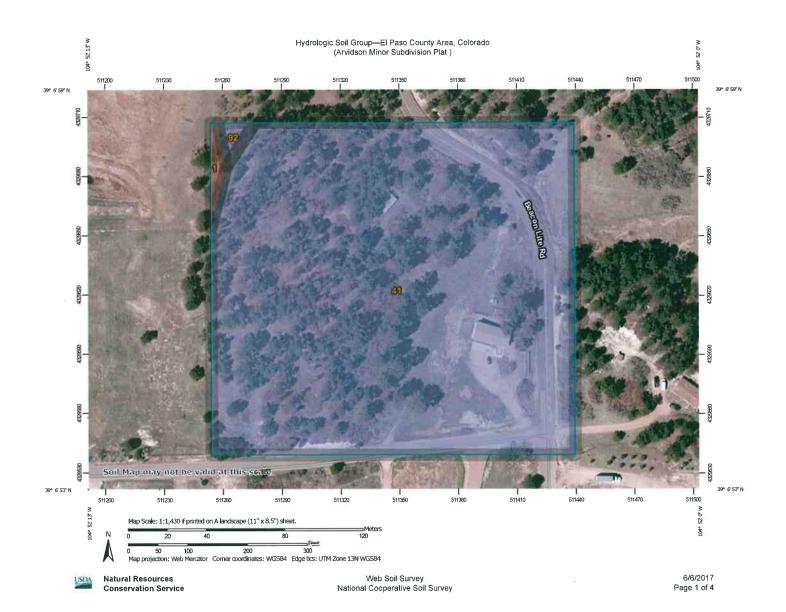
The Tomah soil makes up about 50 percent of the complex, the Crowfoot soil about 30 percent, and other soils about 20 percent.

Included with these soils in mapping are areas of Elbeth sandy loam, 8 to 15 percent slopes; Peyton-Pring complex, 8 to 15 percent slopes; and Kettle gravelly loamy sand, 8 to 40 percent slopes.

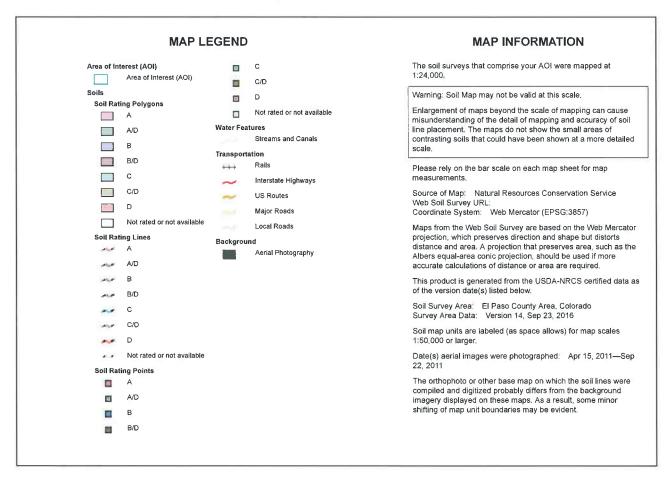
The Tomah soil is deep and well drained. It formed in alluvium or residuum derived from arkose beds. Typically, the surface layer is dark grayish brown loamy sand about 10 inches thick. The subsurface layer is very pale brown coarse sand about 12 inches thick. The subsoil, about 26 inches thick, consists of a matrix of very pale brown coarse sandy clay loam. The substratum is very pale brown coarse sand to a depth of 60 inches or more.

Permeability of the Tomah soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is medium, and the hazard of erosion is moderate. Some gullies are present in some drainageways and along stock trails.

The Crowfoot soil is deep and well drained. It formed in sediment weathered from arkosic sandstone. Typically, the surface layer is grayish brown loamy sand about 12 inches thick. The subsurface layer is very pale brown sand about 11 inches thick. The subsoil is light yellowish brown sandy clay loam about 13 inches thick. The substratum is very pale brown coarse sand to a depth of about 68 inches.



Hydrologic Soil Group—El Paso County Area, Colorado (Arvidson Minor Subdivision Plat)





Hydrologic Soil Group

OI AOI	Perce	Pe	Acres in AOI	Rating	Map unit name	Map unit symbol
0.8%		0.1	0.1	D	Alamosa loam, 1 to 3 percent slopes	1
98.5%		7.6	7.6	В	Kettle gravelly loamy sand, 8 to 40 percent slopes	41
0.7%		0.1	0.1	В	Tomah-Crowfoot loamy sands, 3 to 8 percent slopes	92
		7.7	7.7		slopes	Totals for Area of Inter

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher

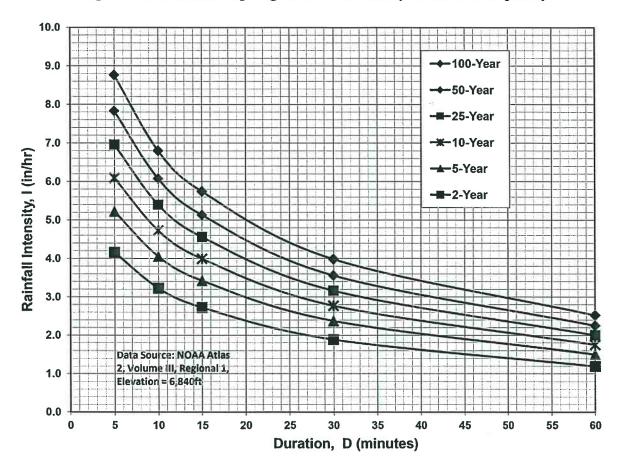


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

Higheritor Higheritor Higheritor Higheritor	Land Use or Surface	Percent						Runoff Co	Runoff Coefficients					
ess mmercial Areas ghborhood Areas To 0.45 0.80 0.81 ential ential Acre or less	Characteristics	Impervious	2-y	ear	7.4	ear	10,	10-year	25-3	25-year	50-	50-year	100	100-year
ess mmercial Areas pertial Acre or less			HSG A&B	-	(HSG A&B)	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HGGCRD	UCC A 9.D	400 000		1
nmercial Areas 95 0.79 0.80 0.81 ghborhood Areas 70 0.45 0.49 0.49 ential Acre or less 65 0.41 0.45 0.45 Acre or less 65 0.41 0.45 0.45 0.45 Acre or less 65 0.41 0.45 0.20 0.20 Acre 30 0.18 0.22 0.25 0.25 0.25 Acre 20 0.13 0.20 0.25 0.20 0.25 0.26 0.23 0.25 0.26 0.23 0.25 0.26 0.23 0.26 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 </td <td>Susiness</td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td>_</td> <td>2000</td> <td>TISO COL</td> <td>חאם אמם</td> <td>HSG C&D</td> <td>HSG A&B</td> <td>HSG C&D</td>	Susiness			_				_	2000	TISO COL	חאם אמם	HSG C&D	HSG A&B	HSG C&D
## Out of the Figure 100 of th	Commercial Areas	95	0.79	0.80	0.81	0.82	0,83	0.84	0.85	0.87	780	0000	000	8
Acre or less 65 0.41 0.45 0.45 Acre or less 65 0.41 0.45 0.45 Acre or less 65 0.41 0.45 0.45 Acre or less 65 0.41 0.45 0.30 Acre or less 0.30 0.12 Acre or less 0.30 0.12 Acre or less 0.30 0.12 Acre or less 0.30 0.13 0.15 Acre or less 0.30 0.12 Acre or less 0.30 0.30 Acre or less 0.30 Ac	Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0 50	300	200	00.0	0.00	0.89
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Acre or less 65 0.41 0.45 0.45 Acre 40 0.23 0.28 0.30 Acre 30 0.18 0.22 0.25 Acre 25 0.15 0.20 0.25 Acre 20 0.12 0.07 0.02 0.25 Ital 20 0.12 0.07 0.05 0.05 0.05 Ital 80 0.71 0.73 0.05 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0	Residential													
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Acre 30 0.18 0.22 0.25 Cre 25 0.15 0.20 0.22 Cre 20 0.12 0.17 0.20 Itial It Areas By 0.57 0.60 0.59 It Areas By 0.57 0.60 0.59 It Areas By 0.57 0.60 0.59 It Areas It Areas By 0.57 0.60 0.59 It Areas It Areas It Areas It Areas It Areas By 0.57 0.60 0.59 It Areas It A	1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.43	5 6	0.33	0.57	0.62	0.59	0.65
Acre 25 0.15 0.20 0.22 rial it Areas it Are	1/3 Acre	30	0.18	0.22	0.25	0.30	032	250	0.20	8.50	0.40	47.0	0.50	0.58
rial It Areas	1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.35	0.47	0.43	0.52	0.47	0.57
rial It Areas	1 Acre	20	0.12	0.17	0.20	35.0	0.27	72.0	100	2	0.41	10.01	0.46	0.56
irial 80 0.57 0.60 0.59 it Areas 80 0.57 0.60 0.59 it Areas 90 0.71 0.73 0.73 and Cemeteries 7 0.05 0.09 0.12 ounds 13 0.07 0.13 0.16 and Vard Areas 40 0.23 0.28 0.30 ieloped Areas 40 0.23 0.28 0.30 ieloped Areas 2 0.03 0.05 0.09 celoped Areas 0 0.02 0.04 0.08 celoped Areas 0 0.02 0.04 0.08 celoped Areas 0 0.02 0.04 0.08 celoped Areas 100 0.89 0.89 0.90 celoped Rock 100 0.89 0.89 0.90 celoped Rock 100 0.89 0.89 0.90 celoped Rock 100 0.89 0.89 0.90 celoped Roc						27.5	0.27	500	0.33	0.44	0.40	0.50	0.44	0.55
It Areas 80 0.57 0.60 0.59 Iny Areas 90 0.71 0.73 0.73 and Cemeteries 7 0.05 0.09 0.12 and Vard Areas 13 0.07 0.13 0.16 and Vard Areas 40 0.23 0.28 0.30 and Vard Areas 40 0.23 0.28 0.30 and Vard Areas 40 0.23 0.08 0.30 and Vard Areas 2 0.03 0.05 0.09 celoped Areas 2 0.03 0.05 0.09 celoped Areas 0 0.02 0.04 0.08 celoped Areas 0 0.02 0.04 0.08 celoped Areas 100 0.02 0.04 0.08 celoped Rock 100 0.02 0.04 0.08 celoped Rock 100 0.26 0.31 0.32 celoped Rock 100 0.26 0.31 0.32	ndustrial													
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and Cemeteries 7 0.05 0.09 0.12 ounds ad Yard Areas 40 0.23 0.28 0.30 eloped Areas oric Flow Analysis enbelts, Agriculture oric Flow Analysis (when ite Flow									2	2000	0.00	70.0	U.81	0.83
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ad Yard Areas 40 0.23 0.28 0.30 eloped Areas coric Flow Analysis enbelts, Agriculture coric Flow Analysis (when the Flow	laygrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.33	70.0
eloped Areas coric Flow Analysis enbelts, Agriculture enbelts, Agriculture ture/Meadow sst 0 0.03 0.05 0.09 0.002 0.004 0.08 sst 0 0.002 0.04 0.08 sst 0 0.02 0.04 0.08 osed Rock 100 0.89 0.89 0.90 ed 100 0.89 0.89 0.90 ed nd Walks 100 0.89 0.89 0.90 osed	ailroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.40	0 50	200		14.0	100
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ite Flow Analysis (when the Fl	Cornet Constant		70.0	20.0	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
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luse is undefined) luse is undefined) ed 100 0.26 0.31 0.32 0.36 0.30 ed 100 0.89 0.89 0.90 nd Walks 100 0.89 0.89 0.90 100 0.89 0.73 0.73	Official Flam A series	OOT	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	96.0	0.96
red 100 0.89 0.89 0.90 80 0.89 0.90 0.89 0.90 0.89 0.90 0.89 0.89	Unsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	44.	0.44	0.51	0.48	7.	2	9
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nd Walks 100 0.89 0.89 0.90 90 0.71 0.73 0.73	Gravel	80	0.57	09.0	0.59	0.63	0.63	0.66	0.66	6,0	890	25.00	0.30	0.70
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	oofs	06	0.71	0.73	0.73	0.75	0.75	0.77	0.78	80	080	660	200	00.00
0 0.02 0.04 0.08	Lawns	0	0.02	9.0	0.08	0.15	0.15	0.75	0.25	0.37	2000	70.07	10.0	20.00

61049 Job No.: Project:

Arvidson Minor Subdivision Plat

Calcs By: Date:

6/16/2017 9:03

A. Orrego

Checked By:

14.8 8.6 14.7 12.1 14.8 8.6 15.0 12.5 (min) 4 4 4 4 2 2 2 2 4 4 4 4 2 2 2 2 (min) t_c Check 847 658 614 233 847 658 614 233 (min) __ 2.7 2.7 1.4 2.1 0.0 (min) ب 3.4 4.4 2.5 0.0 3.4 4.4 0.0 0.0 (ft/s) Channelized V0c 0.059 0.047 0.070 0.000 0.059 0.047 0.070 0.000 S_{0c} (ft/ft) 547 358 314 0 358 314 0 **≟** Time of Concentration (Modified from Standard Form SF-1) 0.000 0.0 (min) ڻه Shallow Channel 0.0 0.0 (ft/s) Vosc 0.000 0.000 (ft/ft) Š 0000 0000 j E 12.1 7.3 12.9 12.5 12.1 7.3 12.6 12.1 (min) سخني Overland 17% 10% 13% 12% 17% 10% 13% 12% °S (%) 300 300 300 233 300 300 300 233 # 11% 64% 7% 0% 11% 64% 10% 5% Imp. % 0.40 0.74 0.39 0.35 0.40 0.74 0.40 0.37 C100/CN Sub-Basin Data 0.12 0.61 0.13 0.08 0.12 0.61 0.15 0.11 \mathcal{C}_{5} 9.8 0.5 3.6 1.3 9.8 0.5 3.6 1.3 (Acres) Area Basin -qns EX-OSA1 EX-A2 EX-A3 EX-B1 PP-OSA1 PP-A2 PP-A3 PP-B1

Arvidson Minor Subdivision Plat

5-Year Storm
UDFCD Job No.: Project: Design Storm: Jurisdiction:

(20% Probability)

Sub-Basin and Combined Flows (Modified from Standard Form SF-2)

6/26/2017 16:27

A. Orrego

Date: Calcs By: Checked By:

Ф	ىد	(min)								
Travel Time	Vosc	(ft/s)								
Ĭ	Length	(ft)								
	DPipe	(in)								
	Length	(ft)								
Pipe Flow	Mnngs Length	L								
	Slope	(%)								
	a	(cfs)								
>	ø	(cfs)								
Streetflow	Slope Length	(#)								
	Slope	(%)								
	Q5	(cfs)		5.0	9,9			r.	9.9	
Runoff	15	(in/hr)		3.35	3.35			3 35	3.35	
Combined Runoff	CA	(Acres)		1.50	1,97			150	2.04	
	+0	(min)		15.5	15.5			15.6	15.6	
	Q5	(cts)	0. 4	1.6 4.0		0.4	1.9	0.5		
nnoff	15	(in/hr)	3.43	3.70		3.43	3.43	3.75		
Direct Runoff	C.A.	(Acres)	1.17	0.10		1.17	0.54	0.14		
	۰	(min)	14.8	15.0		14.8	14.7	12.1		
		C5	0.12	0.13	0.14	0.12	0.15	0.11	0.15	
	Area	(Acres)	9.76	3.61 1.30 10.30	13.90	9.76	3.61	1.30	13.90	
	-qnS	Basin	EX-OSA1 EX-A2	EX-A3 EX-B1	<u>و</u>	PP-OSA1	PP-A3	PP-B1	(3	
		DP		EX OSA1+A2	EX OSA1+A2+A3			DD 0001+00	PP 0SA1+A2+A3	

Rainfall Intensity: 1 = (28.5 * P1) / (10 + tc)^0.786 P1 1.5

Arvidson Minor Subdivision Plat

100-Year Storm (
UDFCD Job No.: Project: Design Storm: Jurisdiction:

(1% Probability)

6/26/2017 16:27

A. Orrego

Date: Calcs By: Checked By:

Jurisdiction:		UDFCD				Sub-Ba	isin and	Combine	d Flows	Sub-Basin and Combined Flows (Modified from Standard Form SF-2)	om Standa	rd Form	SF-2)									
					Direct Runoff	Runoff			Combined Runoff	d Runoff			Streetflow			<u>a</u>	Pipe Flow		L	Trave	Travel Time	П
	-qnS	Area		٠٠	CA	1100	Q100	ور	CA	1100	Q100	Slope	Length	Ø	ø	Slope	Mnngs Length	_	D _{Pipe} Ler	Length v _c	Vosc	.و.
DP	Basin	(Acres)	C100	(min)	(Acres)	(in/hr)	(cts)	(min)	(Acres)	(in/hr)	(cfs)	(%)	(L)	(cts)	(cts)	(%)	n (ff)	一		(ff) (ff	(t/vs) (r	(min)
	EX-OSA1	9.76				97.6	22.5															
	EX-A2	0.54				7.20	2.9												_			
	EX-A3	3.61		15.0	1.39	5.72	8.0												_			_
	EX-B1	1,30				6.21	2.8															_
EX OCA1+A2		10.30						15.5		5 63	24.2											
EX OSA1+A2+A3	e	13.90	0.41					15.5	5.69	5.63	32.0								_			
																				_		
	PP-OSA1	9.76		14.8		5.76	22.5												_			
	DD_A2	0.54		00	0.40	7.20	2.0															_
	77			2 1																		
	PP-A3	3.61		14.7		2.77	8.3															
	PP-81	1,30		12.1		6.29	3.0															
PP OSA1+A2		10.30	0.42				3	15.6	4.30	5.62	24.2											
DD 0001+02+02	c	13.90						25.0	5.75	5 62	32.3											
1000	2	2)	-)												
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Rainfall Intensity: $I = (28.5 * P1) / (10 + tc)^{A}0.786$ P1; 2.52

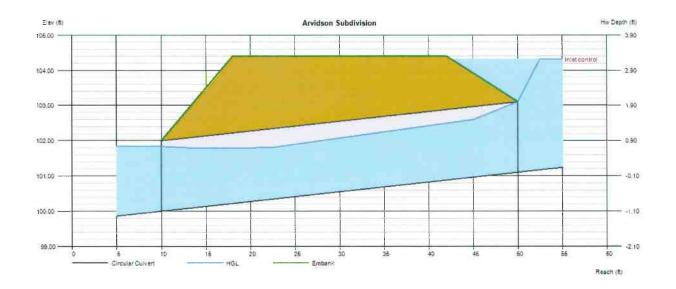
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Jun 19 2017

Arvidson Subdivision

Invert Elev Dn (ft)	= 100.00	Calculations	
Pipe Length (ft)	= 40.00	Qmin (cfs)	= 5.00
Slope (%)	= 2.75	Qmax (cfs)	= 24.20
Invert Elev Up (ft)	= 101.10	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 22.00
No. Barrels	= 1	Qpipe (cfs)	= 22.00
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 7.28
Culvert Entrance	= Headwall	Veloc Up (ft/s)	= 7.84
Coeff. K,M,c,Y,k	= 0.0078, 2, 0.0379, 0.69, 0.5	HGL Dn (ft)	= 101.84
		HGL Up (ft)	= 102.77
Embankment		Hw Elev (ft)	= 104.31
Top Elevation (ft)	= 104.40	Hw/D (ft)	= 1.61
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		





ARVIDSON MINOR PLAT **OFFSITE** DRAINAGE BASIN MAP

JUNE, 2017 61049-Offsite-DR-Map

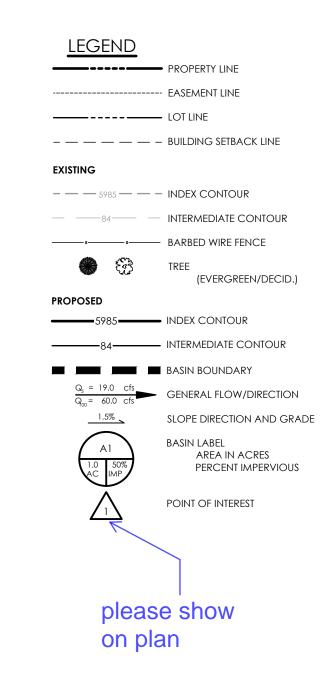
suite 200 co 80909 1903 leiaray street colorado springs 719.635.5736

www.mvecivil.com



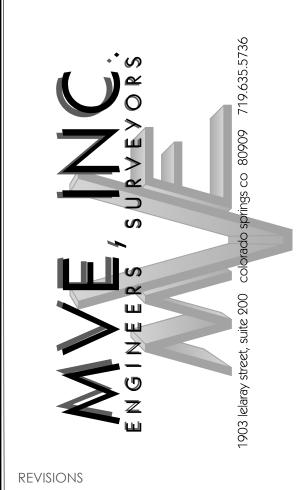
SCALE: 1"=500'





FLOODPLAIN STATEMENT:

NO PORTION OF THE SUBJECT PROPERTY IS LOCATED WITHIN A FEMA DESIGNATED SPECIAL FLOOD HAZARD AREA (SFHA) AS INDICATED ON THE FLOOD INSURANCE RATE MAP (FIRM) FOR EL PASO COUNTY, COLORADO AND INCORPORATED AREAS - MAP NUMBER 08041C0276 F, EFFECTIVE MARCH 17, 1997.



1" = 50' 1:600

VICINITY MAP

BENCHMARK

EXISTIN	G DRAINAGE	E SUMM <i>A</i>	ARY TABLE		
INTE	nt of erest/ in(s)	AREA (AC)	TC (MIN.)	RUN Q5 (CFS)	Q100 (CFS)
	OSA1	9.76	14.8	4.0	22.5
	A2	.54	8.6	1.4	2.9
	A3	3.61	15.0	1.6	8.0
	B1	1.30	12.5	0.4	2.8
POI 1	OSA1, A2	10.30	15.5	5.0	24.2

DESIGNED BY
DRAWN BY
CHECKED BY
AS-BUILTS BY
CHECKED BY _____

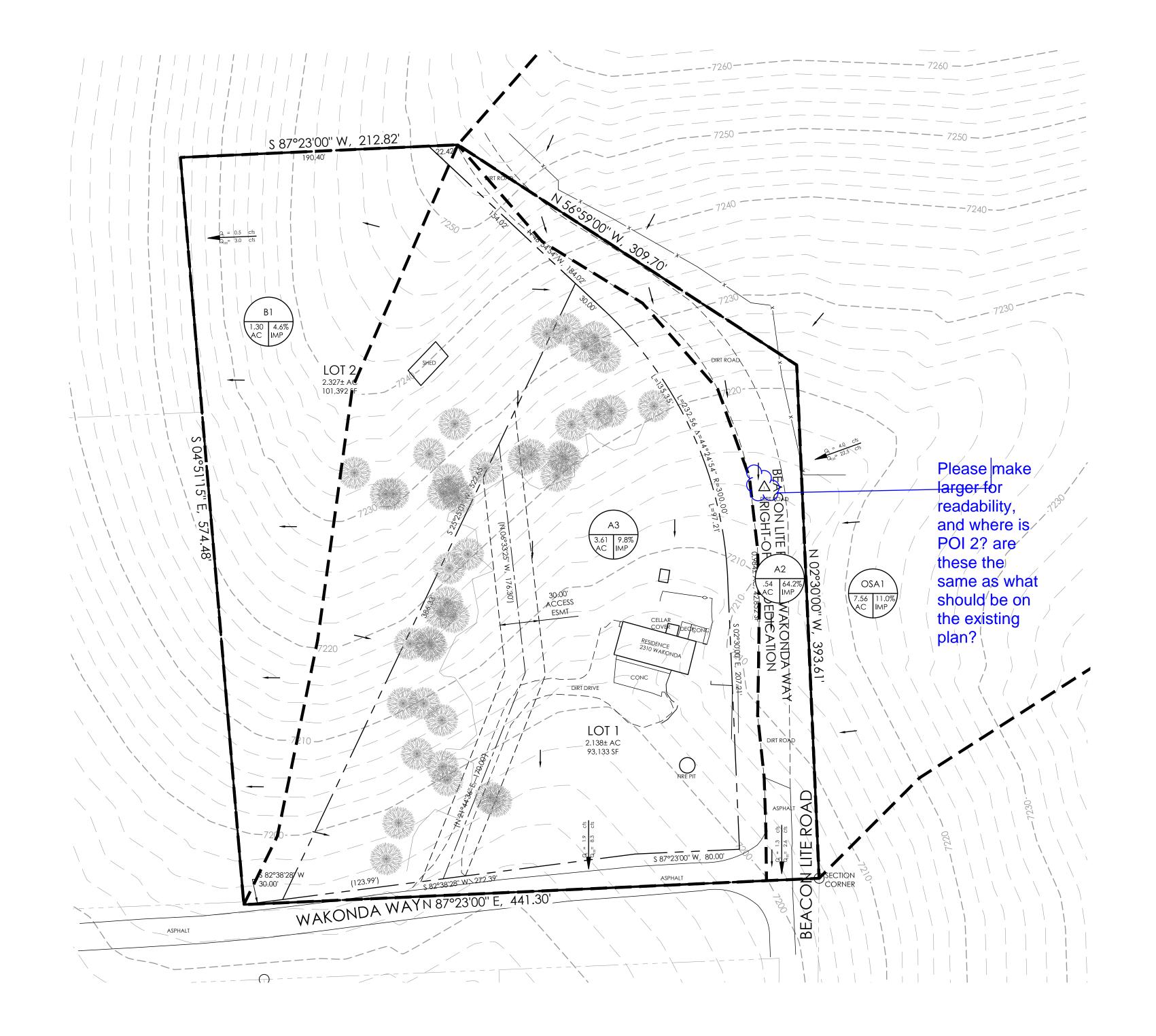
ARVIDSON MINOR SUBDIVISION PLAT

EXISTING DRAINAGE MAP

MVE PROJECT 61049

MVE DRAWING 61049-EX-DR-MAP

JUNE 08, 2017 SHEET 1 OF 2



<u>LEGEND</u>

FLOODPLAIN STATEMENT:

NO PORTION OF THE SUBJECT PROPERTY IS LOCATED WITHIN A FEMA DESIGNATED SPECIAL FLOOD HAZARD AREA (SFHA) AS INDICATED ON THE FLOOD INSURANCE RATE MAP (FIRM) FOR EL PASO COUNTY, COLORADO AND INCORPORATED AREAS - MAP NUMBER 08041C0276 F, EFFECTIVE MARCH 17, 1997.

PROPERTY LINE
------ EASEMENT LINE
LOT LINE

- — — — — — BUILDING SETBACK LINE

EXISTING

- - - 5985 - - INDEX CONTOUR

- 84 - INTERMEDIATE CONTOUR

- x BARBED WIRE FENCE

දිදීදී TREE (EVERGREEN/DECID.)

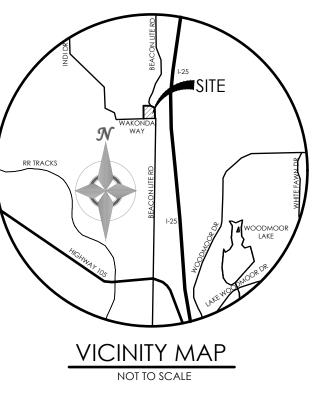
5985 INDEX CONTOUR

84 INTERMEDIATE CONTOUR

BASIN BOUNDARY

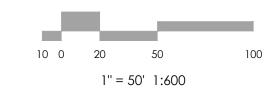
 $\begin{array}{c} \underline{Q_{g} = 19.0 \quad \text{cfs}} \\ \underline{Q_{gg} = 60.0 \quad \text{cfs}} \end{array} \qquad \begin{array}{c} \text{GENERAL FLOW/DIRECTION} \\ \underline{1.5\%} \qquad \qquad \text{SLOPE DIRECTION AND GRADE} \\ \\ \underline{A1} \\ \underline{A1} \\ \underline{AC} \\$

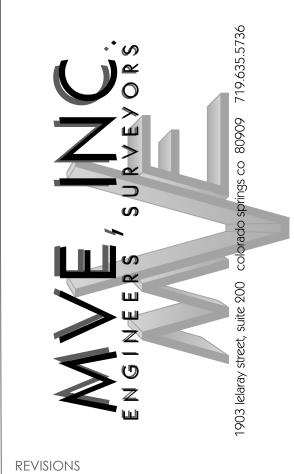
POINT OF INTEREST



BENCHMARK







DRAINAG	ANNNII2 F	RYTARIF

POI	NT OF	AREA	Тс	RUN	IOFF
	erest/ In(s)	(AC)	(MIN.)	Q5 (CFS)	Q100 (CFS)
	OSA1	9.76	14.8	4.0	22.5
	A2	.54	8.6	1.4	2.9
А3		3.61	14.7	1.9	8.3
	B1	1.30	12.1	0.5	3.0
POI 1	O\$A1, A2	10.30	15.6	5.0	24.2

ARVIDSON MINOR SUBDIVISION PLAT

PROPOSED DRAINAGE MAP

MVE PROJECT 61049

MVE DRAWING 61049-PP-DR-MAP

JUNE 08, 2017 SHEET 2 OF 2

Markup Summary

dsdnijkamp (9)		
ADD: all three project numbers to the bottom of this report (MS. P, ADR)	Subject: Text Box Page Label: 1 Lock: Locked Author: dsdnijkamp	ADD: all three project numbers to the bottom of this report (MS. P, ADR)
Change flaste and factors and the same flast of	Subject: Callout Page Label: 6 Lock: Locked Author: dsdnijkamp	please show ditch and POI's on plan.
Please describe proceed confidence and those are the proceeding the procedure of the proced	Subject: Cloud+ Page Label: 6 Lock: Locked Author: dsdnijkamp	Please describe proposed condition and show any hazards as described in the geologic report.
Compare forms and the desired of the compare of the	Subject: Callout Page Label: 6 Lock: Locked Author: dsdnijkamp	Please elaborate where the flow goes next.
State of the control	Subject: Callout Page Label: 7 Lock: Locked Author: dsdnijkamp	Please show on plan, as well if there is a driveway culvert.
Please add a statement as to why there is no water quality required for this site.	Subject: Text Box Page Label: 7 Lock: Locked Author: dsdnijkamp	Please add a statement as to why there is no water quality required for this site.
indian from attention of course of the cours	Subject: Callout Page Label: 32 Lock: Locked Author: dsdnijkamp	please show ditch as called out on page 3 of report.
please show on plan	Subject: Callout Page Label: 32 Lock: Locked Author: dsdnijkamp	please show on plan
Primary Andrews (1997)	Subject: Cloud+ Page Label: 33 Lock: Locked Author: dsdnijkamp	Please make larger for readability, and where is POI 2? are these the same as what should be on the existing plan?

dsdruiz (1)

duplicate page

Subject: Text Box Page Label: 9 Lock: Locked Author: dsdruiz

duplicate page