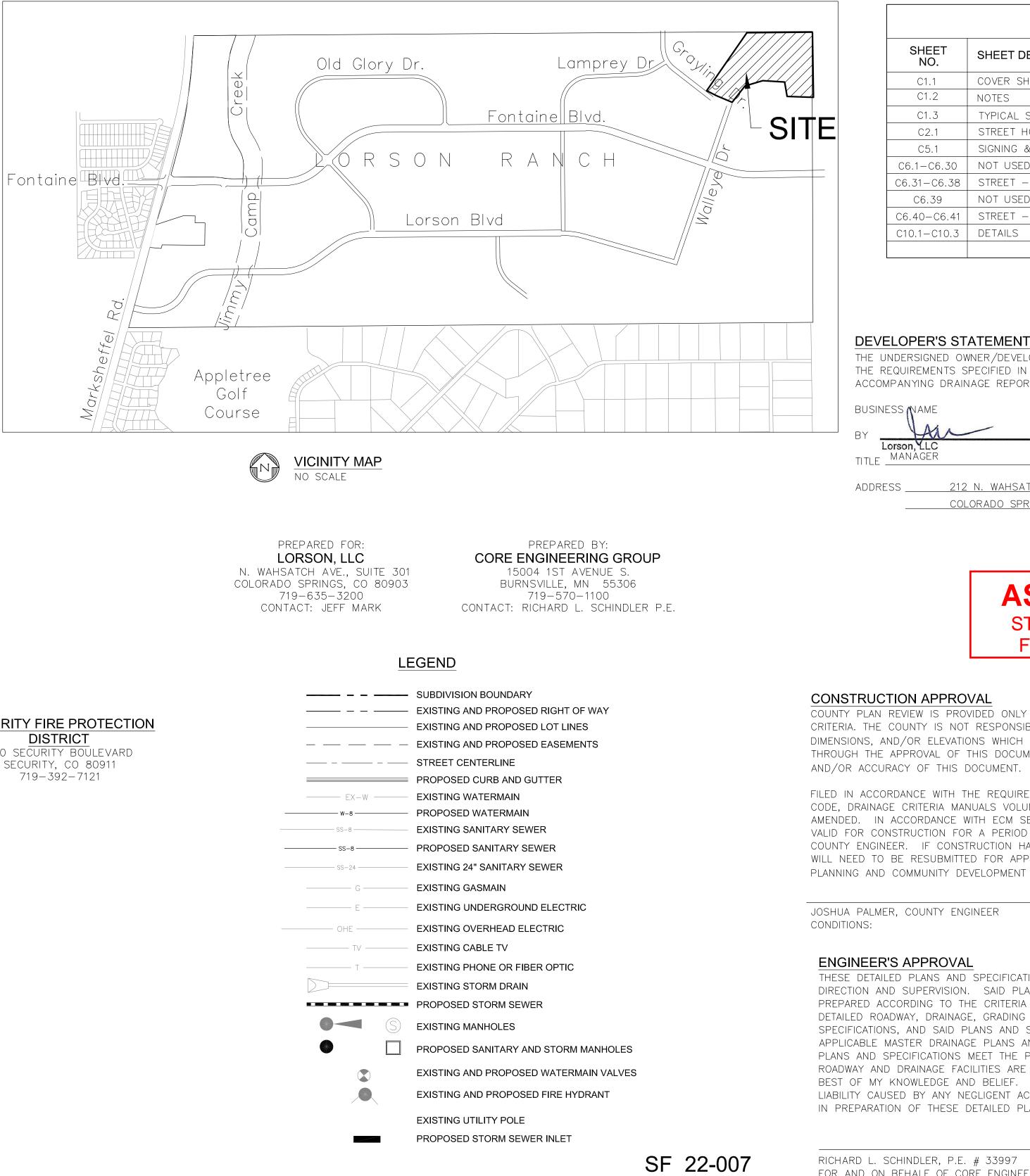


DĀNIS

<u> TASONS RIDGE WAY</u>





## TELEPHONE

CENTURYLINK 7925 INDUSTRY ROAD COLORADO SPRINGS, CO 80939 719-278-4651

GAS BLACK HILLS ENERGY 7060 ALLEGRE ST. FOUNTAIN, CO 80817 719-393-6639

CABLE

COMCAST

P.O. BOX 173838

DENVER, CO 80217

970-641-4774

KEY MAP

NO SCALE

ELECTRIC MOUNTAIN VIEW ELECTRIC 11140 E. WOODMEN RD. COLORADO SPRINGS, CO 80831 719-495-2283

EL PASO COUNTY

PLANNING AND COMMUNITY

DEVELOPMENT

2880 INTERNATIONAL CIRCLE

COLORADO SPRINGS, CO 80910

719-520-6300

SECURITY FIRE PROTECTION DISTRICT 400 SECURITY BOULEVARD SECURITY, CO 80911 719-392-7121

**BASIS OF BEARING** 

BEARINGS ARE BASED ON THE SOUTH LINE OF THE NORTH HALF OF SECTION 23, TOWNSHIP 15 SOUTH, RANGE 65 WEST OF THE 6TH PRINCIPAL MERIDIAN AS BEING SOUTH 8941'52" WEST. THE EAST QUARTER CORNER OF SAID SECTION 23 IS A FOUND 3-1/2" ALUMINUM CAP MONUMENT AND THE WEST QUARTER CORNER OF SAID SECTION 23 IS A FOUND 2-1/2" ALUMINUM CAP MONUMENT

### BENCHMARK

FIMS MONUMENT F204 LOCATED AT THE NORTHWEST CORNER OF FONTAINE BLVD AND COTTONWOOD GROVE DR. ELEVATION 5724.072 (N.G.V.D. 29)

### TRAFFIC CONTROL NOTE

THE CONTRACTOR SHALL PROVIDE ALL TRAFFIC CONTROL DEVICES AND MONITORING NECESSARY TO SAFELY COMPLETE THE WORK SHOWN IN THESE CONSTRUCTION DOCUMENTS IN CONFORMANCE WITH M.U.T.C.D. GUIDELINES. THE CONTRACTOR SHALL COMPLETE ALL NECESSARY WORK FOR PLAN REVIEW, PERMITS AND PROCESSING. TRAFFIC CONTROL WILL NOT BE PAID SEPARATELY BUT IS INCLUDED IN THE COST OF THE PROJECT.

## CONSTRUCTION PLANS FOR THE RIDGE AT LORSON RANCH FILING NO. 3

STREET & STORM SEWER CONSTRUCTION PLANS



CALL 2-BUSINESS DAYS IN ADVANCE BEFORE YOU DIG, GRADE OR EXCAVATE FOR THE MARKING OF UNDERGROUND MEMBER UTILITIES

|         | SHEET INDEX                      |
|---------|----------------------------------|
| ET<br>· | SHEET DESCRIPTION                |
|         | COVER SHEET                      |
| 2       | NOTES                            |
| 3       | TYPICAL SECTIONS                 |
| 1       | STREET HORIZONTAL CONTROL        |
| 1       | SIGNING & STRIPING PLAN          |
| 6.30    | NOT USED !!!1                    |
| 6.38    | STREET – STORM PLAN AND PROFILES |
| 9       | NOT USED !!!1                    |
| C6.41   | STREET – STORM PLAN AND PROFILES |
| 210.3   | DETAILS                          |
|         |                                  |

THE UNDERSIGNED OWNER/DEVELOPER HAS READ AND WILL COMPLY WITH ALL THE REQUIREMENTS SPECIFIED IN THESE CONSTRUCTION PLANS AND THE ACCOMPANYING DRAINAGE REPORT.

AUG 2, 2022

ADDRESS \_\_\_\_\_ 212 N. WAHSATCH AVE. SUITE 301 COLORADO SPRINGS, CO 80903



COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH COUNTY DESIGN CRITERIA. THE COUNTY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONSIBILITY FOR COMPLETENESS

FILED IN ACCORDANCE WITH THE REQUIREMENTS OF THE EL PASO COUNTY LAND DEVELOPMENT CODE, DRAINAGE CRITERIA MANUALS VOLUME 1 AND 2, AND ENGINEERING CRITERIA MANUAL AS AMENDED. IN ACCORDANCE WITH ECM SECTION 1.12, THESE CONSTRUCTION DOCUMENTS WILL BE VALID FOR CONSTRUCTION FOR A PERIOD OF 2 YEARS FROM THE DATE SIGNED BY THE EL PASO COUNTY ENGINEER. IF CONSTRUCTION HAS NOT STARTED WITHIN THOSE TWO YEARS THE PLANS WILL NEED TO BE RESUBMITTED FOR APPROVAL, INCLUDING PAYMENT OF REVIEW FEES AT THE PLANNING AND COMMUNITY DEVELOPMENT DIRECTOR'S DISCRETION



THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR DETAILED ROADWAY, DRAINAGE, GRADING AND EROSION CONTROL PLANS AND SPECIFICATIONS, AND SAID PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH APPLICABLE MASTER DRAINAGE PLANS AND MASTER TRANSPORTATION PLANS. SAID PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR ROADWAY AND DRAINAGE FACILITIES ARE DESIGNED AND ARE CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THESE DETAILED PLANS AND SPECIFICATIONS

33997

-8-2-2022

FOR AND ON BEHALF OF CORE ENGINEERING GROUP

|             | CORE   | ENGINEERING GROUP | 15004 1ST AVENUE S. | PUCKNS VILLE, MN 33308<br>PH: 719.570.1100 |  |                                      |
|-------------|--|-------------------|---------------------|--|--|--------------------------------------|
| DATE        |  |                   |                     | LORSON, LLC                                | 212 N. WAHSATCH AVE, SUITE 301<br>COLORADO SPRINGS, COLORADO 80903 | (719) 635-3200<br>Contact: Jeff Mark |
| DESCRIPTION |  |                   | PREPAREI            |  |  |                                      |
| D           |  |                   | ECT:                | THE RIDGE AT LORSO                         | RANCH FIL. NO. 3   | COLORADO SPRINGS, COLORADO           |
| DE          | RAWN:<br>ESIGNEI<br>HECKEE   |                   | -S                  |  |  |                                      |
|             | <b>NCH FIL NO. 3</b>   |                   |                     |  | PLANS  |                                      |
|             | THE RIDGE AT LORSON RANCH FIL NO. 3  |                   | VIREEL & VIORIN     |  | CONSTRUCTION PLANS   |                                      |
|             | Contraction of the second seco | 10 0 3 2 SION     | NAL                 | GALLAND TO A ENGLAND                       | A COLORIDA STATE   |                                      |

TOTAL SHEETS: 18

### CONSTRUCTION NOTES

- 1. ALL WORK SHALL COMPLY WITH THE CODES AND POLICIES FOR EL PASO COUNTY.
- 2. EXISTING TOPOGRAPHIC INFORMATION SHOWN ON THIS GRADING PLAN WAS OBTAINED FROM DREXEL, BARRELL & CO., JULY, 2005. SUPPLEMENTAL SURVEY DATA WAS OBTAINED FOR MARKSHEFFEL ROAD FROM M&S CIVIL GROUP IN NOVEMBER, 2016. THE CONTRACTOR SHALL BE RESPONSIBLE TO EXAMINE THE SITE AND BE FAMILIAR WITH THE EXISTING CONDITIONS.
- 3. DEPTH OF MOISTURE-DENSITY CONTROL FOR THIS PROJECT SHALL BE AS FOLLOWS: BASE OF ALL CUTS AND FILLS - 12 INCHES, FULL DEPTH OF ALL EMBANKMENTS
- 4. THE CONTRACTOR IS RESPONSIBLE FOR THE RE-ESTABLISHMENT OF ALL SURVEY MONUMENTS DISTURBED WITHIN THE PROJECT LIMITS.
- 5. THE CONTRACTOR SHALL PROTECT ALL WORK AREAS AND FACILITIES FROM FLOODING AT ALL TIMES. AREAS AND FACILITIES SUBJECTED TO FLOODING, REGARDLESS OF THE SOURCE OF WATER, SHALL BE PROMPTLY DEWATERED AND RESTORED.
- 6. PRIOR TO PAVING OPERATIONS, THE ENTIRE SUBGRADE SHALL BE PROOF-ROLLED WITH A LOADED 988 FRONT-END LOADER OR SIMILAR HEAVY RUBBER TIRED VEHICLE (GVW OF 50,000 POUNDS WITH 18 KIP PER AXLE AT TIRE PRESSURES OF 90 PSI) TO DETECT ANY SOFT OR LOOSE AREAS. IN AREAS WHERE SOFT OR LOOSE SOILS, PUMPING OR EXCESSIVE MOVEMENT IS OBSERVED, THE EXPOSED MATERIALS SHALL BE OVER-EXCAVATED TO A MINIMUM DEPTH OF TWO FEET BELOW PROPOSED FINAL GRADE OR TO A DEPTH AT WHICH SOILS ARE STABLE. AFTER THIS HAS BEEN COMPLETED, THE EXPOSED MATERIALS SHALL BE SCARIFIED TO A DEPTH OF 12 INCHES AND MOISTURE CONDITIONED. THE SUBGRADE SHALL THEN BE UNIFORMLY COMPACTED TO A MINIMUM OF 95% OF STANDARD PROCTOR DENSITY (ASTMM D-698) AT 0 TO +4.0% OF OPTIMUM MOISTURE CONTENT FOR A-6 AND A-7-6 SOILS ENCOUNTERED. OTHER SUBGRADE TYPES SHALL BE UNIFORMLY COMPACTED TO A MINIMUM OF 95% OF MODIFIED PROCTOR DENSITY (ASTM D-1557) AT PLUS OR MINUS 2.0% OF OPTIMUM MOISTURE CONTENT. AREAS WHERE STABLE NATURAL SOILS ARE ENCOUNTERED AT PROPOSED SUBGRADE ELEVATION SHALL ALSO BE SCARIFIED (18 INCHES FOR A-7-6 SOILS BELOW FULL-DEPTH ASPHALT CONCRETE) AND COMPACTED AS OUTLINED ABOVE PRIOR TO PAVING OPERATIONS. SUBGRADE FILL SHALL BE PLACED IN SIX-INCH LIFTS AND UNIFORMLY COMPACTED, MEETING THE REQUIREMENTS AS PREVIOUSLY DESCRIBED.
- 7. SUBGRADE MATERIALS DEEMED UNSUITABLE BY THE ENGINEER SHALL BE EXCAVATED, DISPOSED OF AND REPLACED WITH APPROVED MATERIALS.
- 8. FILL SHALL BE PLACED IN 8-INCH MAXIMUM LOOSE LIFTS AND SHALL BE COMPACTED PRIOR TO SUCCESSIVE LIFTS.
- 9. THE CONTRACTOR IS RESPONSIBLE FOR PREVENTING AND CONTROLLING EROSION DURING CONSTRUCTION ACTIVITIES AT ALL TIMES DURING GRADING AND CONSTRUCTION. THE CONTRACTOR SHALL PROVIDE THE FOLLOWING EROSION AND SEDIMENT CONTROL MEASURES:
  - HAY BALE BARRIERS WHERE NEEDED AND/OR AS DIRECTED BY THE ENGINEER.
  - SILT FENCE WHERE NEEDED AND/OR AS DIRECTED BY THE ENGINEER.
  - TEMPORARY SEDIMENTATION BASINS WHERE NEEDED AND/OR AS DIRECTED BY THE ENGINEER.
  - MULCHING AND SEEDING OF EXCESSIVE SLOPED AREAS AS NEEDED OR AS DIRECTED BY THE ENGINEER.
  - TEMPORARY VEHICLE TRACKING CONTROL AS NEEDED AND/OR DIRECTED BY THE ENGINEER.
  - CONCRETE WASH AREAS.

- INLET PROTECTION.

THESE AND ALL EROSION CONTROL BEST MANAGEMENT PRACTICES AS SHOWN IN THE GRADING AND EROSION CONTROL PLANS SHALL BE STRICTLY ADHERED TO.

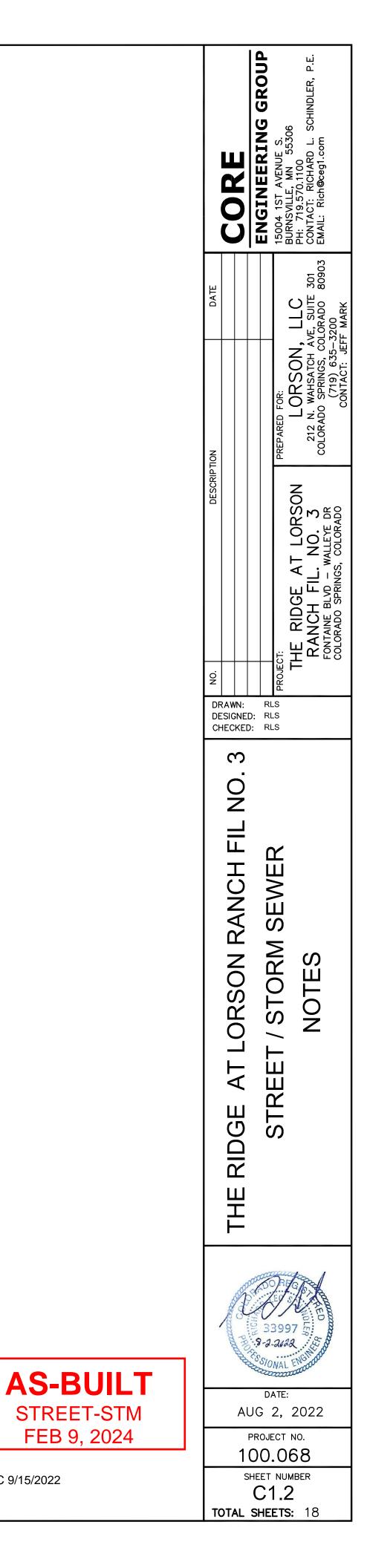
10. FINISHED CONTOURS/SPOT ELEVATIONS SHOWN HEREON REPRESENT FINISHED GRADES. ALL PAVEMENT SUBGRADES ARE BASED ON THE COMPOSITE ASPHALT PAVEMENT RECOMMENDATIONS MADE IN THE "GEOTECHNICAL STUDY" FOR LORSON RANCH.

### EL PASO COUNTY STANDARD CONSTRUCTION NOTES:

- ALL DRAINAGE AND ROADWAY CONSTRUCTION SHALL MEET THE STANDARDS AND SPECIFICATIONS OF THE CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2, AND THE EL PASO COUNTY ENGINEERING CRITERIA MANUAL.
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE NOTIFICATION AND FIELD NOTIFICATION OF ALL EXISTING UTILITIES, WHETHER SHOWN ON THE PLANS OR NOT, BEFORE BEGINNING CONSTRUCTION. LOCATION OF EXISTING UTILITIES SHALL BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. CALL 811 TO CONTACT THE UTILITY NOTIFICATION CENTER OF COLORADO (UNCC).
- 3. CONTRACTOR SHALL KEEP A COPY OF THESE APPROVED PLANS, THE GRADING AND EROSION CONTROL PLAN, THE STORMWATER MANAGEMENT PLAN (SWMP), THE SOILS AND GEOTECHNICAL REPORT, AND THE APPROPRIATE DESIGN AND CONSTRUCTION STANDARDS AND SPECIFICATIONS AT THE JOB SITE AT ALL TIMES, INCLUDING THE FOLLOWING:
  - a. EL PASO COUNTY ENGINEERING CRITERIA MANUAL (ECM)
  - b. CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2 c. COLORADO DEPARTMENT OF TRANSPORTATION (CDOT) STANDARD SPECIFICATIONS FOR ROAD AND
- BRIDGE CONSTRUCTION
- d. CDOT M & S STANDARDS
- 4. NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION, ALL DESIGN AND CONSTRUCTION RELATED TO ROADS, STORM DRAINAGE AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS, INCLUDING THE LAND DEVELOPMENT CODE, THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING. ANY MODIFICATIONS NECESSARY TO MEET CRITERIA AFTER-THE-FACT WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY.
- 5. IT IS THE DESIGN ENGINEER'S RESPONSIBILITY TO ACCURATELY SHOW EXISTING CONDITIONS, BOTH ONSITE AND OFFSITE, ON THE CONSTRUCTION PLANS. ANY MODIFICATIONS NECESSARY DUE TO CONFLICTS, OMISSIONS, OR CHANGED CONDITIONS WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY.
- 6. CONTRACTOR SHALL SCHEDULE A PRE-CONSTRUCTION MEETING WITH PLANNING AND COMMUNITY DEVELOPMENT (PCD) - INSPECTIONS, PRIOR TO STARTING CONSTRUCTION.
- 7. IT IS THE CONTRACTOR'S RESPONSIBILITY TO UNDERSTAND THE REQUIREMENTS OF ALL JURISDICTIONAL AGENCIES AND TO OBTAIN ALL REQUIRED PERMITS, INCLUDING BUT NOT LIMITED TO EL PASO COUNTY EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP), REGIONAL BUILDING FLOODPLAIN DEVELOPMENT PERMIT, U.S. ARMY CORPS OF ENGINEERS-ISSUED 401 AND/OR 404 PERMITS, AND COUNTY AND STATE FUGITIVE DUST PERMITS.
- CONTRACTOR SHALL NOT DEVIATE FROM THE PLANS WITHOUT FIRST OBTAINING WRITTEN APPROVAL FROM THE DESIGN ENGINEER AND PCD. CONTRACTOR SHALL NOTIFY THE DESIGN ENGINEER IMMEDIATELY UPON DISCOVERY OF ANY ERRORS OR INCONSISTENCIES.
- 9. ALL STORM DRAIN PIPE SHALL BE CLASS III RCP UNLESS OTHERWISE NOTED AND APPROVED BY PCD.
- CONTRACTOR SHALL COORDINATE GEOTECHNICAL TESTING PER ECM STANDARDS. PAVEMENT DESIGN SHALL 10. BE APPROVED BY EL PASO COUNTY PCD PRIOR TO PLACEMENT OF CURB AND GUTTER AND PAVEMENT.
- 11. ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE AT APPROVED CONSTRUCTION ACCESS POINTS.
- 12. SIGHT VISIBILITY TRIANGLES AS IDENTIFIED IN THE PLANS SHALL BE PROVIDED AT ALL INTERSECTIONS. OBSTRUCTIONS GREATER THAN 18 INCHES ABOVE FLOWLINE ARE NOT ALLOWED WITHIN SIGHT TRIANGLES.
- 13. SIGNING AND STRIPING SHALL COMPLY WITH EL PASO COUNTY PUBLIC WORKS DEPARTMENT AND MUTCD CRITERIA.
- 14. CONTRACTOR SHALL OBTAIN ANY PERMITS REQUIRED BY EL PASO COUNTY PUBLIC WORKS DEPARTMENT, INCLUDING WORK WITHIN THE RIGHT-OF-WAY AND SPECIAL TRANSPORT PERMITS.
- 15. THE LIMITS OF CONSTRUCTION SHALL REMAIN WITHIN THE PROPERTY LINE UNLESS OTHERWISE NOTED. THE OWNER/DEVELOPER SHALL OBTAIN WRITTEN PERMISSION AND EASEMENTS, WHERE REQUIRED, FROM ADJOINING PROPERTY OWNER(S) PRIOR TO ANY OFF-SITE DISTURBANCE, GRADING, OR CONSTRUCTION.

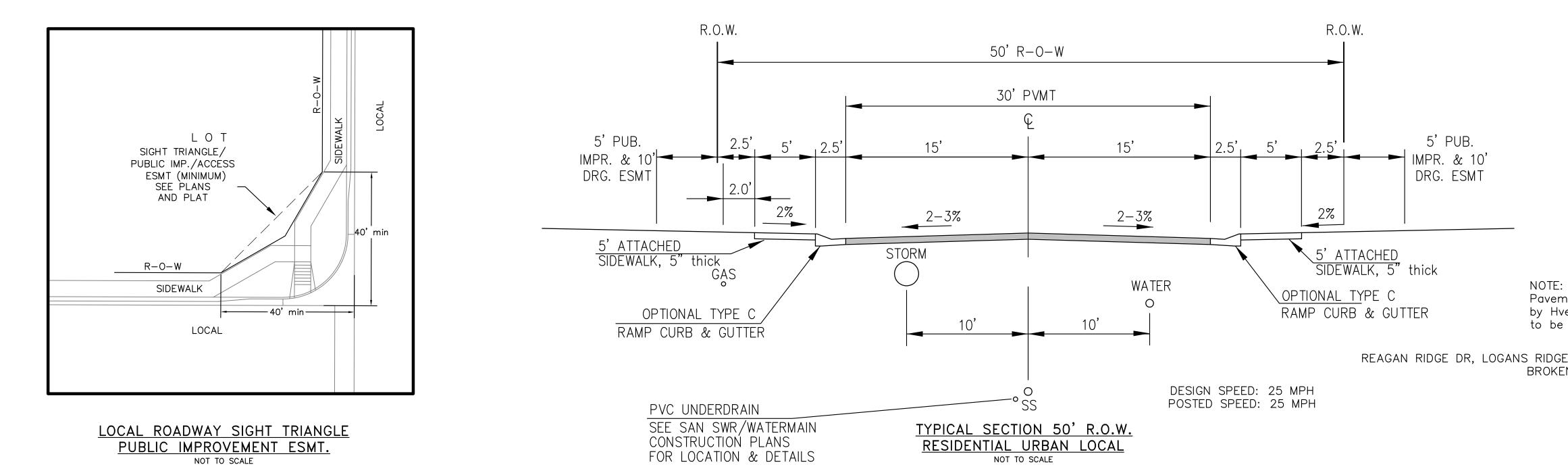
### STORM SEWER NOTES:

1. CONTRACTOR SHALL USE "TYLOX SUPER SEAL" OR APPROVED EQUL JOINT GASKET FOR ALL RCP STORM SEWER JOINTS

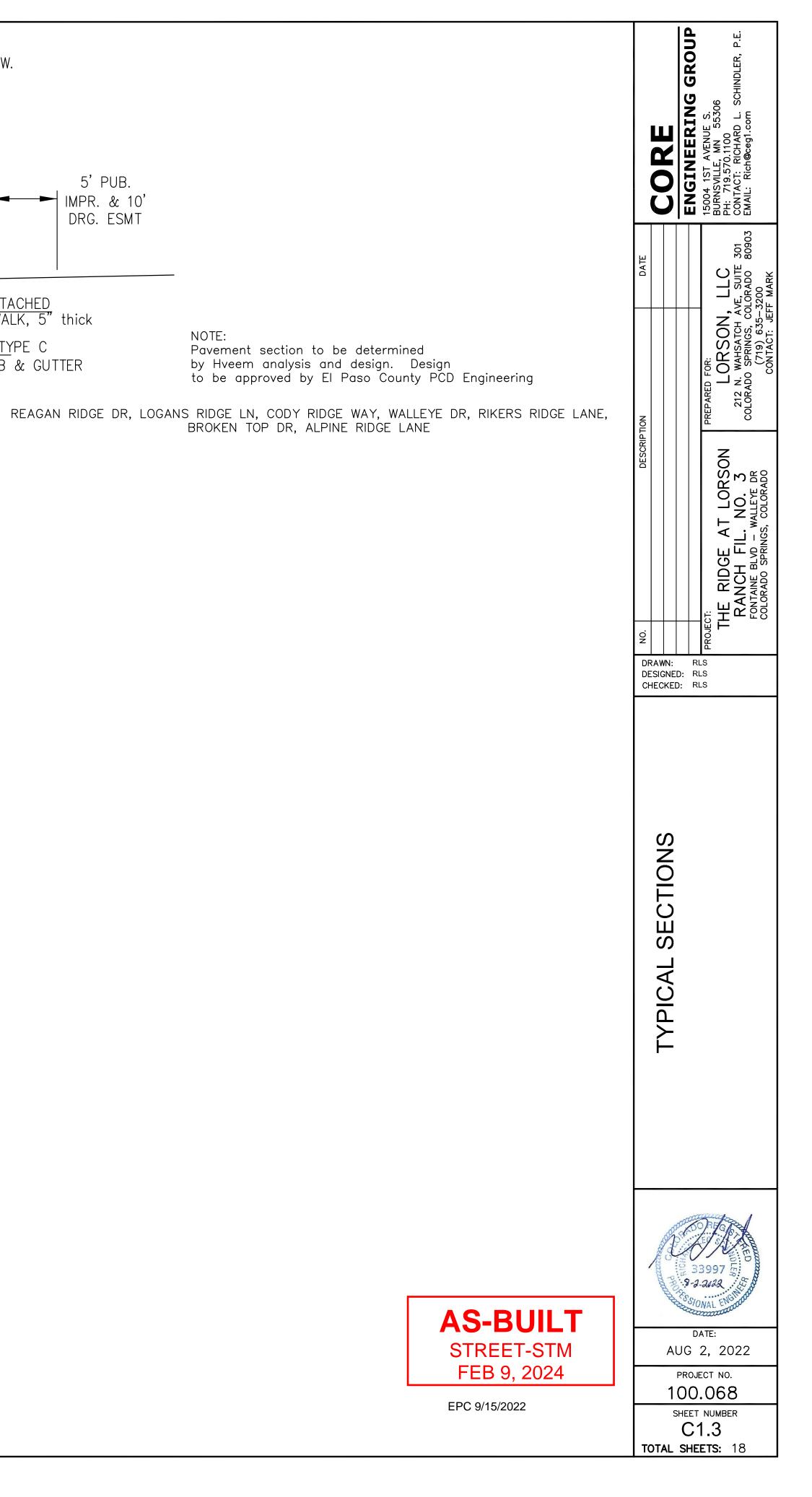


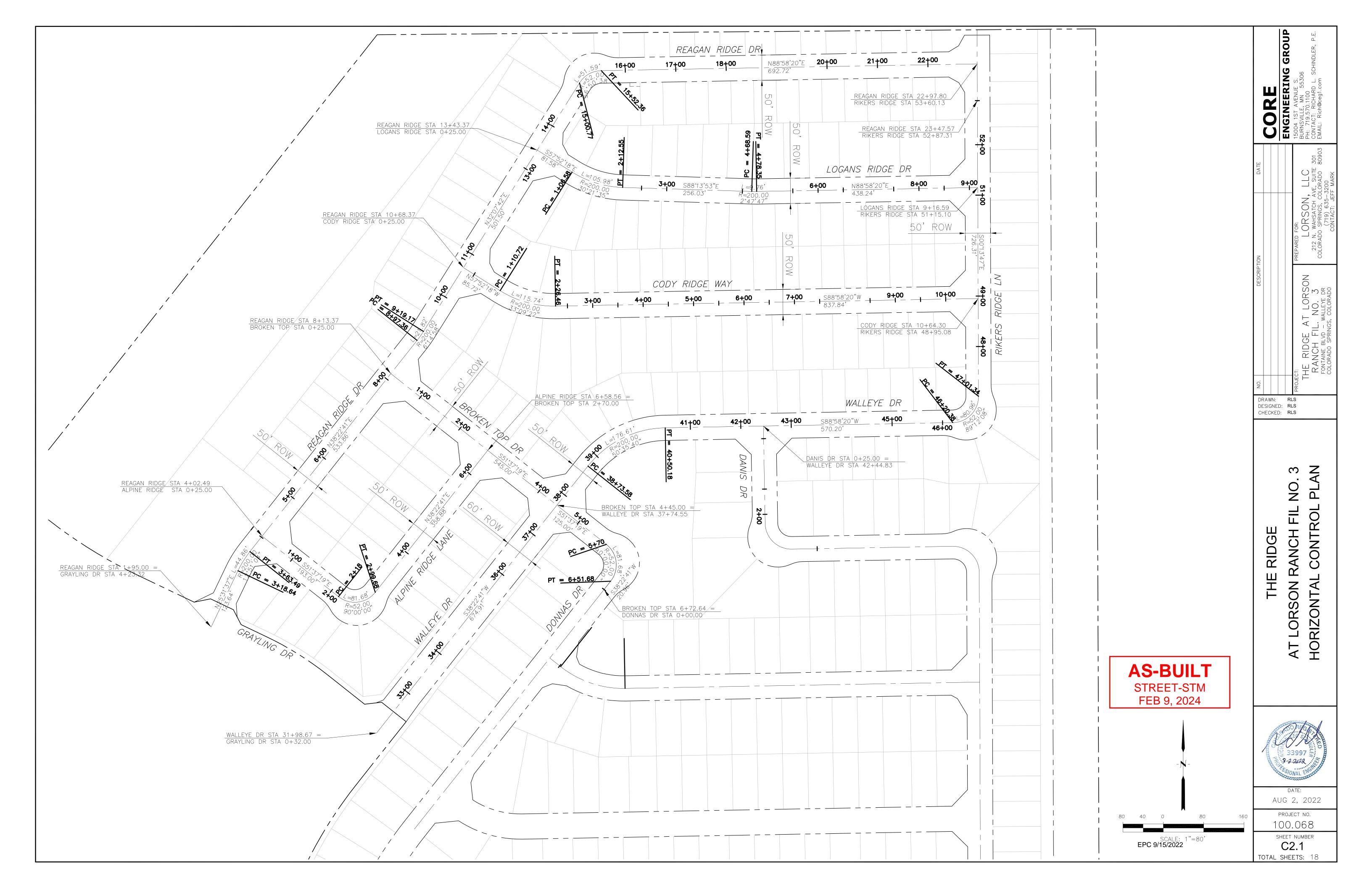
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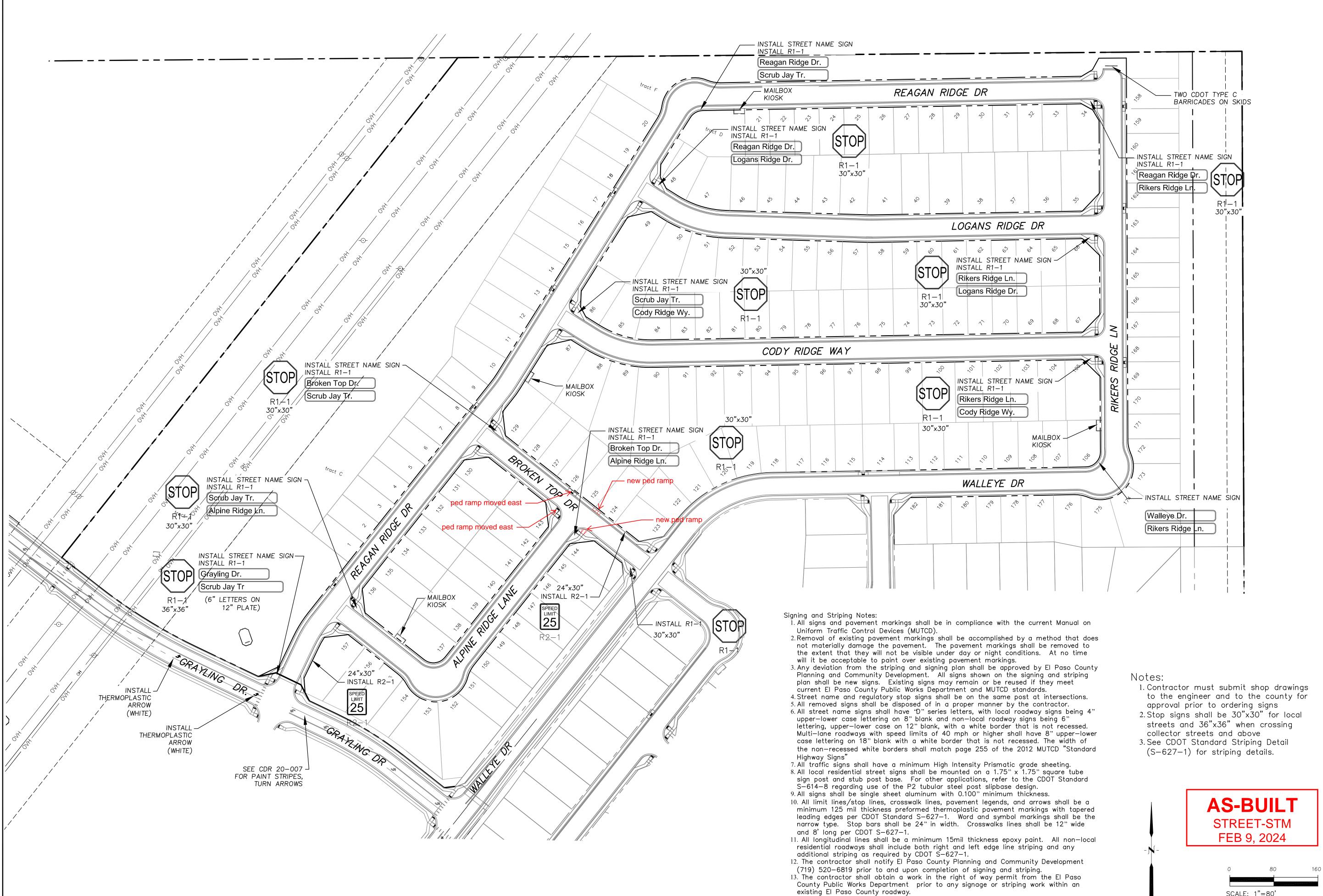
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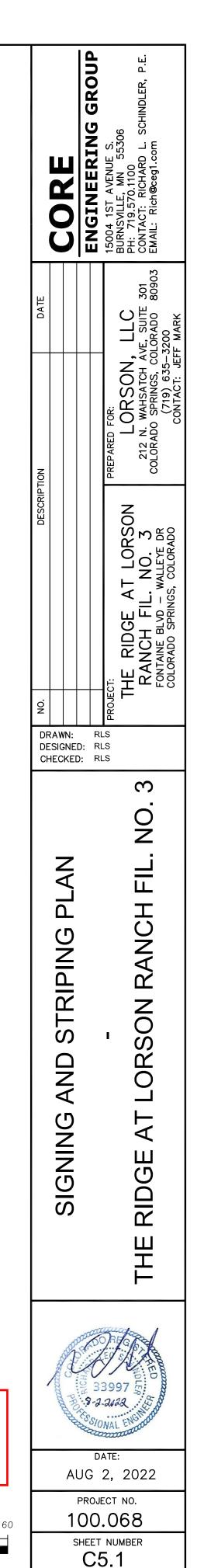


NOTE: ADDITIONAL PUBLIC IMPROVEMENT EASEMENTS ARE REQUIRED WHERE SIDEWALK ENCROACHES INTO THE PRIVATE LOTS. SEE CONSTRUCTION DRAWINGS AND THE FINAL PLAT. SEE CONSTRUCTION DRAWINGS AND PLAT FOR SIGHT TRIANGLES





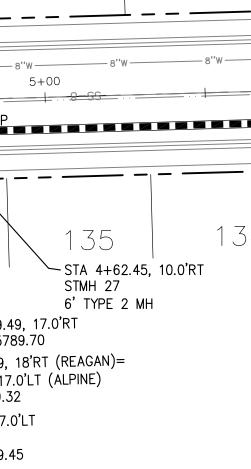


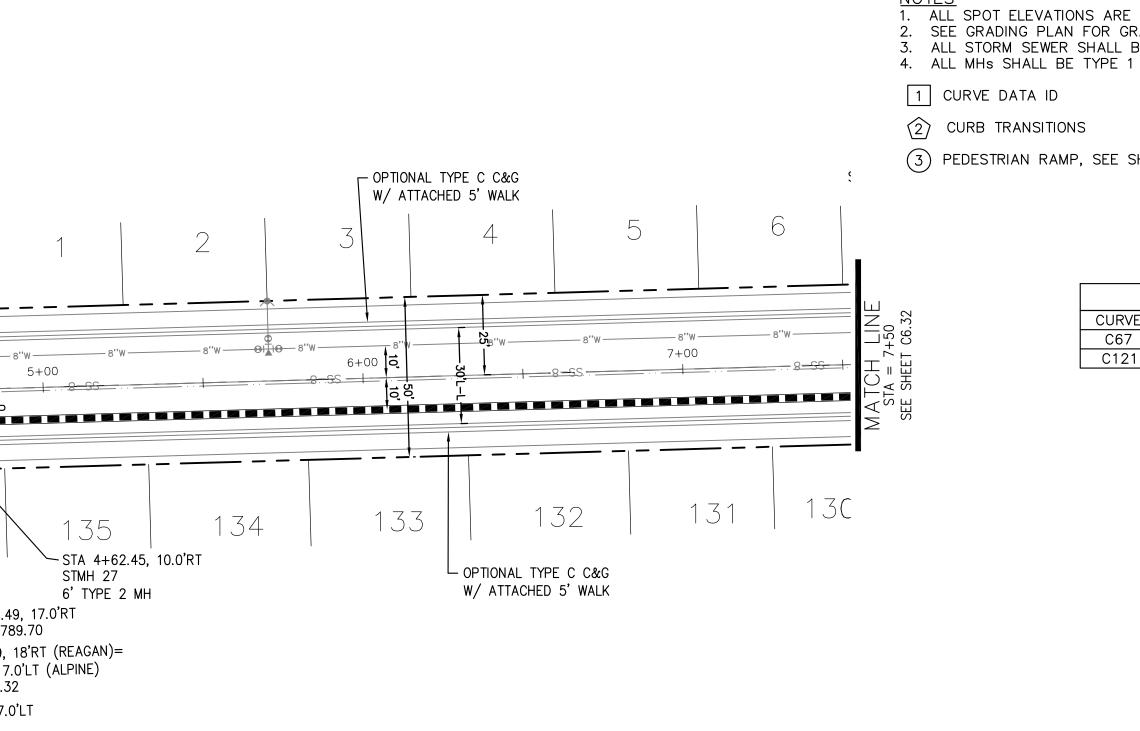


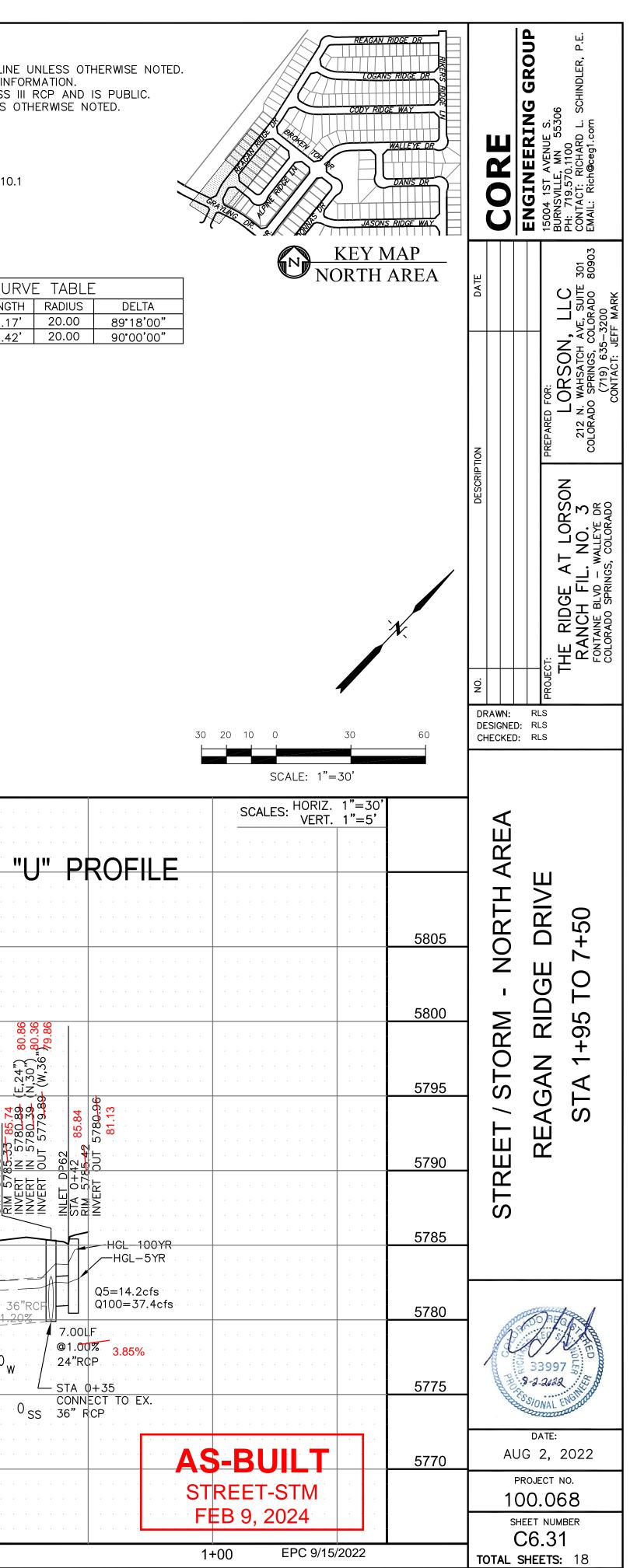
TOTAL SHEETS: 18

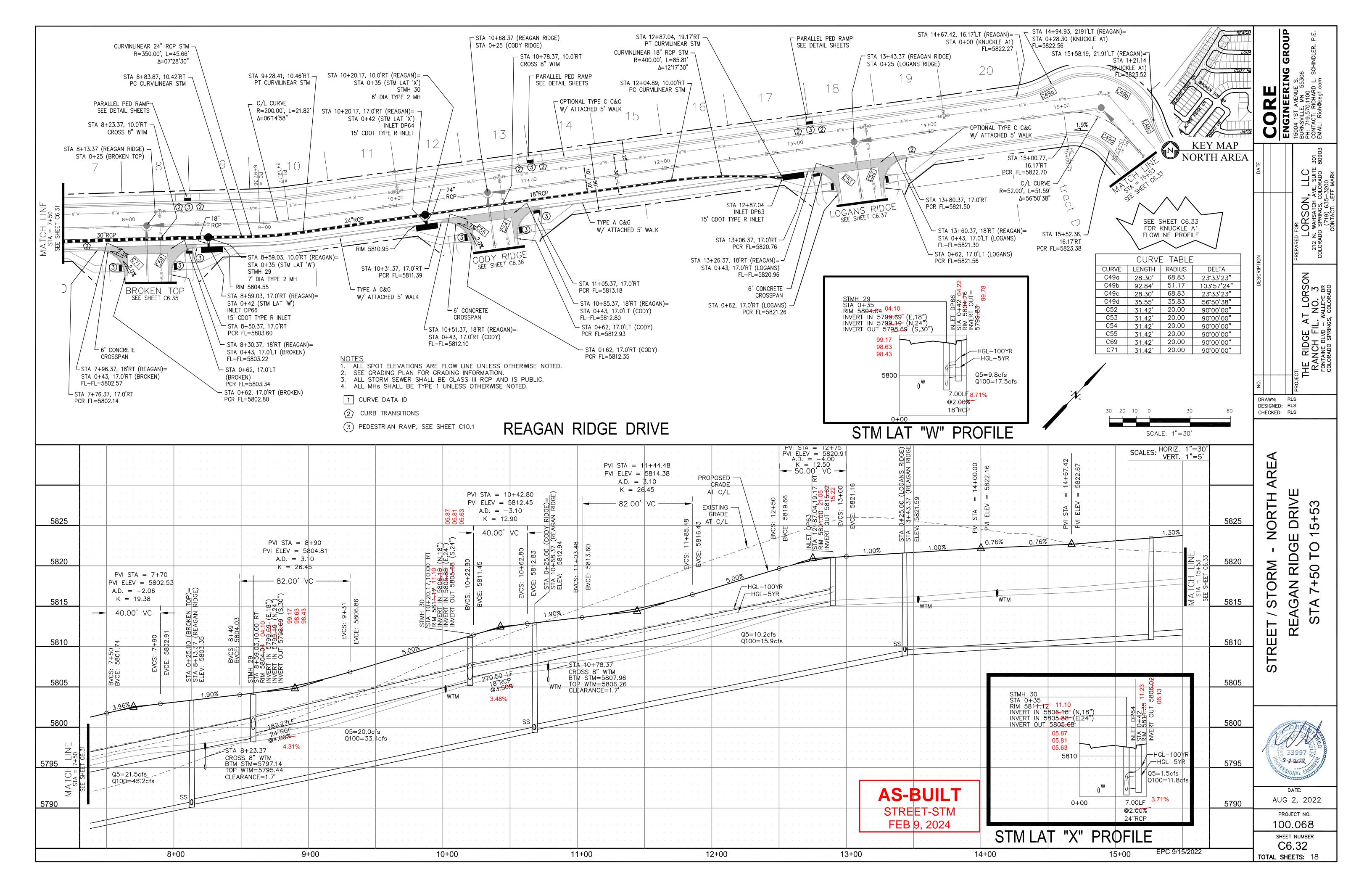
# SCALE: 1"=80' EPC 9/15/2022

| 5790<br>5785<br>5780<br>5775<br>5770                        |  |  | · · · · · · · · ·               |   | · · · · · · · · ·  |                                       | .     . <th>.     .<th></th><th>6+00</th><th>· · · · · · · · ·</th><th></th><th></th><th></th><th>· · · · · · · · · · ·</th></th> | .     . <th></th> <th>6+00</th> <th>· · · · · · · · ·</th> <th></th> <th></th> <th></th> <th>· · · · · · · · · · ·</th> |                | 6+00                        | · · · · · · · · ·                |                             |  |  | · · · · · · · · · · ·  |
|---|--|--|---------------------------------|---|--|---------------------------------------|---|---|----------------|-----------------------------|----------------------------------|-----------------------------|--|--|--|
| 5785<br>5780<br>5775  |  | · · · · · · · · · · · · · · · · · · ·  |                                 | · · · · · · · · · · · ·   | · · · · · · · · ·  | · · · · · · · · · ·                   | · · · · · · · · · · · · · · · · · · ·   |   |                |                             |                                  |                             |  |  |  |
| 5785<br>5780<br>5775  |  | 0  |                                 |   |  |                                       |   |   |                |                             |                                  |                             |  |  |  |
| <u>5785</u><br>5780   |  | · · · · · · · · · · · · · · · · · · ·  | STM                             |   |  |                                       |   |   |                |                             |                                  |                             |  |  |  |
| 5785  |  | · · · · · · · · · · · · · · · · · · ·  | STM                             |   |  | · · · · · · · · · · ·                 | SS 0  |   |                |                             | · · · · · · · · · ·              | · · · · · · · · · · ·       |  |  | Q5=33.0cfs 0<br>Q100=76.5cfs V   |
|   |  | · · · · · · · · · · ·  |                                 | 211 LF 1.9<br>30"RCP<br>@2. <del>00%</del>  | 97%  | Q5=21.5cfs<br>Q100=45.2cfs            | WTM CLEARANCE=1   | 82.92<br>81.22<br>1.7'  |                |                             |                                  |                             | · · · · · · · · · · ·  |  | EX 3   |
|   |  |  |                                 |   |  |                                       | CROSS 8" WT<br>BTM STM=578<br>TOP WTM=578   | 03.50%  | <b>5</b>       |                             |                                  | · · · · · · · · · · · ·     |  | · · · · · ·                              |  |
| 5790  |  | م می می ا  | -2.00%                          |   | 2.56%  |                                       |   | 396.83LF  |                |                             | <i></i>                          |                             |  |  | STA<br>RIM<br>STA<br>RIM<br>RIM<br>RIM   |
| 1   |  | PVI STA<br>PVI ELEV<br>FA 4+23.<br>FA 1+95.  |                                 | NI ELEV =   | · · · · · · · · · ·  |                                       | 1.90%   |   |                |                             |                                  |                             | 21.5cfs<br>=45.2cfs  | · · · · · ·                              | INLET<br>5785.43<br>RT IN 57<br>RT OUT 5<br>AH 27<br>(0+35<br>5785.33                                  |
|   |  | = 5785.<br>= 5785.<br>32 (GRAY<br>00 (REAG   |                                 | = 2+42<br>= 5785.35<br>HH 27<br>2+49.06,1<br>5785.33<br>5785.33<br>5786.33<br>5786.1<br>5780<br>ERT IN 5780<br>ERT IN 5780<br>ERT IN 5780 | · · · · · · · · ·  | · · · · · · · · · ·                   | -A 0+25.0<br>-A 4+02.4<br>-PM ELEV  | BVC<br>STMH 2<br>STA 4+<br>RIM 57<br>INVERT<br>INVERT   |                |                             |                                  | 05=                         | 21.5cfs  | MA<br>SEE                                | 79.52<br>5779.02   |
| 5795  |  | .7<br>93<br>JAN RIDGE  |                                 | 0.00 R<br>85.74<br>79.89 (E<br>79.89  | 000<br>000<br>000<br>000<br>000<br>000<br>000<br>000   | · ·   · · · · · · ·                   | 00 (ALPIN<br>49 (REAG,<br>1 = 5789.   | CS: 4+45<br>E: 5790.2<br>8<br>62.45,10.<br>30.45 90.<br>IN 5784.6<br>0UT 5784.6   | EVCE: 5        | EXISTING<br>GRADE<br>AT C/L | 3.96%                            |                             | HGL-100YR<br>HGL-5YR   | TCH L TA = 7+5C SHEET C6.                |  |
| 5800  |  |  | · · · · · · · · · · ·           | T<br>3.24")<br>(W, 36")   | 8<br>8<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9   | · · · · · · · · · · · · · · · · · · · | AN RIDGE)=<br>46  | 27<br>27<br>27<br>28<br>26<br>27<br>27<br>28<br>29<br>27<br>20<br>27<br>20<br>27<br>20<br>27<br>20<br>27<br>20<br>27<br>20<br>27<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  | 5+05<br>792.03 | PROPOSED<br>GRADE<br>AT C/L | · · · · · · · · · · ·            | · · · · · · · · · · · · · · |  | 33<br>37 NE                              | · · · · · · · · · · · · · · · · · · ·  |
| 5805  |  | · · · · · · · · · ·  |                                 | · · · · · · · · · · · · · · · · · · ·   |  | · · · · · · · · · ·                   |   | A.D. = $2.06$<br>K = $29.07$<br>60.00' VC -   |                |                             | · · · · · · · · ·                |                             |  |  |  |
|   |  | · · · · · · · · · · ·  |                                 |   | · · · · · · · · · ·  |                                       | · · ·   · · · · · · · · · · · · · · · ·   | PVI STA = 4+75<br>PVI ELEV = 5790.8<br>A.D. = 2.06  |                |                             | · · · · · · · · · ·              | · · · · · · · · · · · ·     |  |  |  |
|   |  |  |                                 | · · · · · · · · · · · · · · ·   | · · · · · · · · ·  | · · · · · · · · · · · · · · · · · · · | · · · · · · · · · · · · · · · · · · ·   | · · · · · · · · · · · · · ·   |                |                             |                                  |                             | · · · · · · · · · · · ·  |  | TMLAT  |
| ST  | STA 2<br>P<br>CONN<br>TA 2+49.06,<br>STA 0 | SIDEWALK<br>2+40.00, 17.0'RT<br>CR TBC=5784.93<br>NECT TO EX. C/G<br>17.0'RT (REAGAN)=<br>+42 (STM LAT 'U')<br>INLET DP62<br>CDOT TYPE R INLET | / _ STA 2+7<br>RIM=578          | 71.36, 17.0'RT<br>6.14  | (<br>PCR FL=   | 5788.79                               |   |   | RE             | AGAN RID                    | GE DRI\                          | /E                          |  |  |  |
| STA 2+4   | STA 0+35 (S                                | T (REGAN)=<br>TM LAT 'U')<br>STMH 27<br>TYPE 1 MH<br>TO EXISTING   |                                 | W-16<br>3+00<br>C/L CURVE -<br>R=200.00', L=44.86'<br>Δ=12'51'04"<br>STA 3+65.73, 17<br>PCR FL=578<br>STA 3+85.49, 1<br>STA 0+43,         | 7.0'RT<br>88.06<br>18'RT (REAGAN)=<br>17.0'RT (ALPINE)<br>FL-FL=5788.52<br>6' CONCRETE<br>CROSSPAN<br>STA 0+62.  | ALPINE<br>SEE SHEET C6.3              | 3<br>3<br>4<br>4<br>5<br>5<br>7<br>4<br>5<br>7<br>4<br>4<br>5<br>7<br>6<br>4<br>4<br>5<br>7<br>6<br>4<br>4<br>5<br>7<br>6<br>4<br>4<br>5<br>7<br>6<br>7<br>6<br>7<br>7<br>6<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7   | RCP<br>1 35<br>STA 4+62.45, 10.<br>STMH 27<br>6' TYPE 2 MH<br>39.49, 17.0'RT<br>=5789.70<br>.49, 18'RT (REAGAN)=<br>, 17.0'LT (ALPINE)<br>89.32<br>17.0'LT<br>'89.45  | 134<br>.0'RT   | 133<br>OPTIONAL<br>W/ATTAC  | 132<br>TYPE C C&G<br>HED 5' WALK | 131 1                       | JAN<br>JAN<br>JAN<br>JAN<br>JAN<br>JAN<br>JAN<br>JAN<br>JAN<br>JAN                                 |  |  |
| STA 2+<br>PCR<br>CONNEC<br>CONSTRUC<br>E<br>GRAYL<br>SEE CD | 49.06, 10.0'R<br>STA 0+35 (S               | WALK<br>T<br>G<br>R<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T                                       | STA PC<br>STA 2+66<br>EX. RIM=S | W-16<br>3+00<br>C/L CURVE<br>R=200.00', L=44.86'<br>Δ=12'51'04"<br>STA 3+65.73, 17<br>PCR FL=578<br>STA 3+85.49, 1<br>STA 0+43,           | $\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$<br>$\frac{M}{9}$ | ALPINE<br>SEE SHEET C6.3              | A 4+02.49 (REAGAN RIDGE)<br>A 0+25 (ALPINE)<br>PARALLEL PED RAMF<br>SEE DETAIL SHEETS   | 2<br>1<br>8''W<br>5+00<br>1 35<br>CCP<br>1 35<br>STA 4+62.45, 10.<br>STMH 27<br>6' TYPE 2 MH<br>39.49, 17.0'RT<br>=5789.70<br>49, 18'RT (REAGAN)=<br>, 17.0'LT (ALPINE)<br>89.32<br>17.0'LT   |                |                             | TYPE C C&G                       | 6<br>                       | 4. ALL N<br>1 CUR<br>2 CUR<br>3 PEDI<br>3 EE SHEET C0.32<br>3 SEE SHEET C0.32<br>3 SEE SHEET C0.32 | HS SHALL BE<br>VE DATA ID<br>B TRANSITIO | R SHALL BE CLASS<br>E TYPE 1 UNLESS<br>ONS<br>AP, SEE SHEET C10<br>CURVE LENG<br>C67 31.1<br>C121 31.4 |

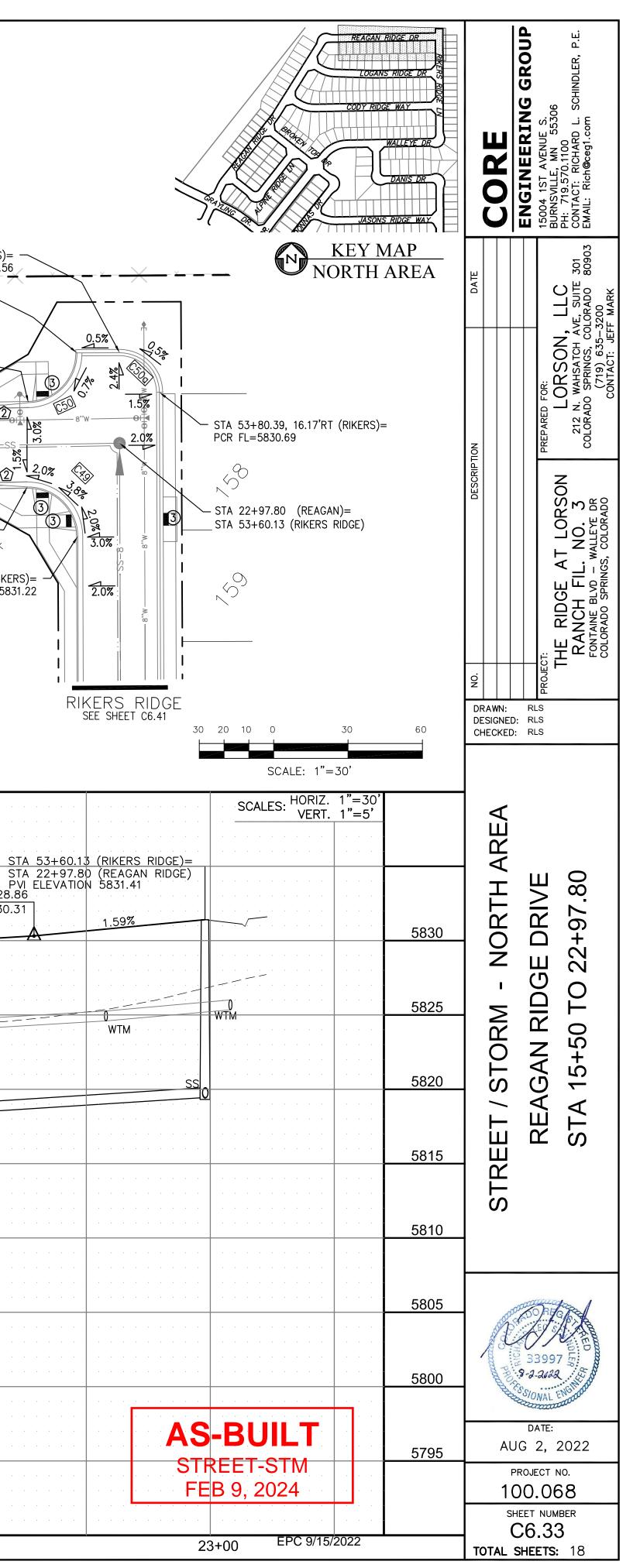




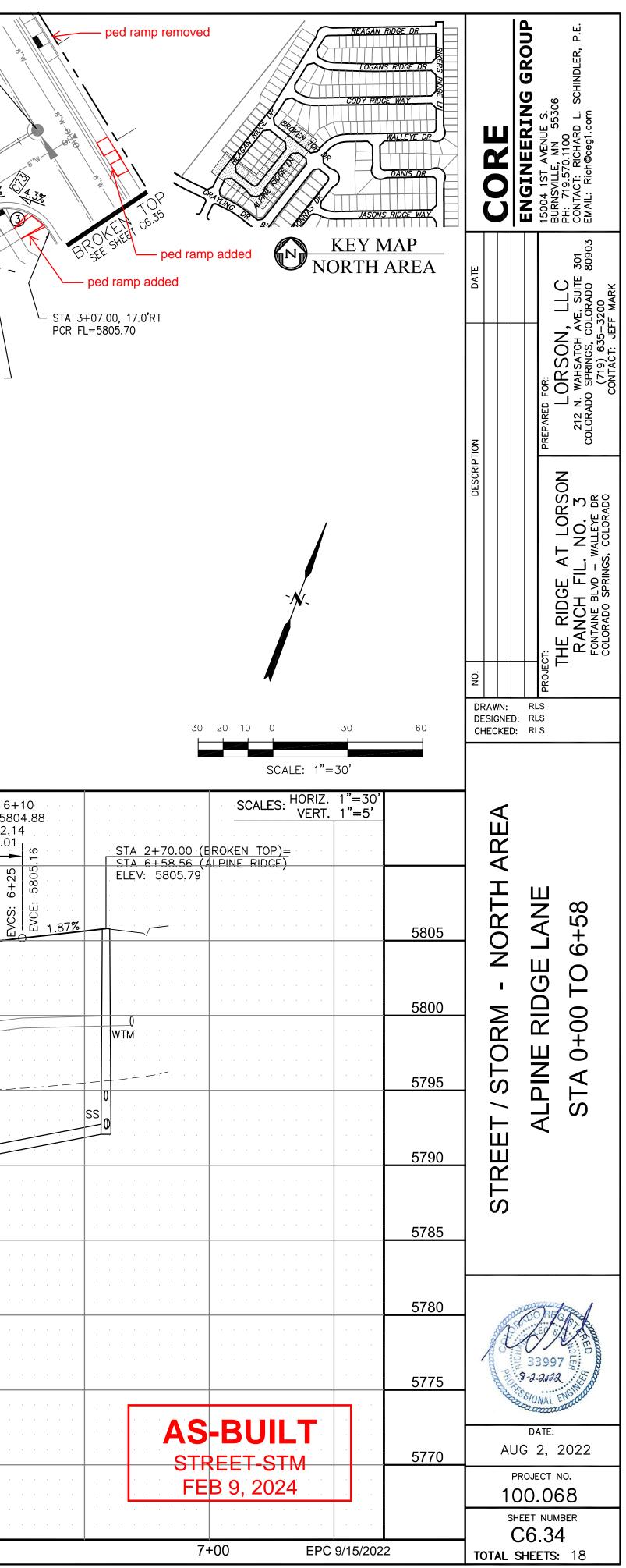


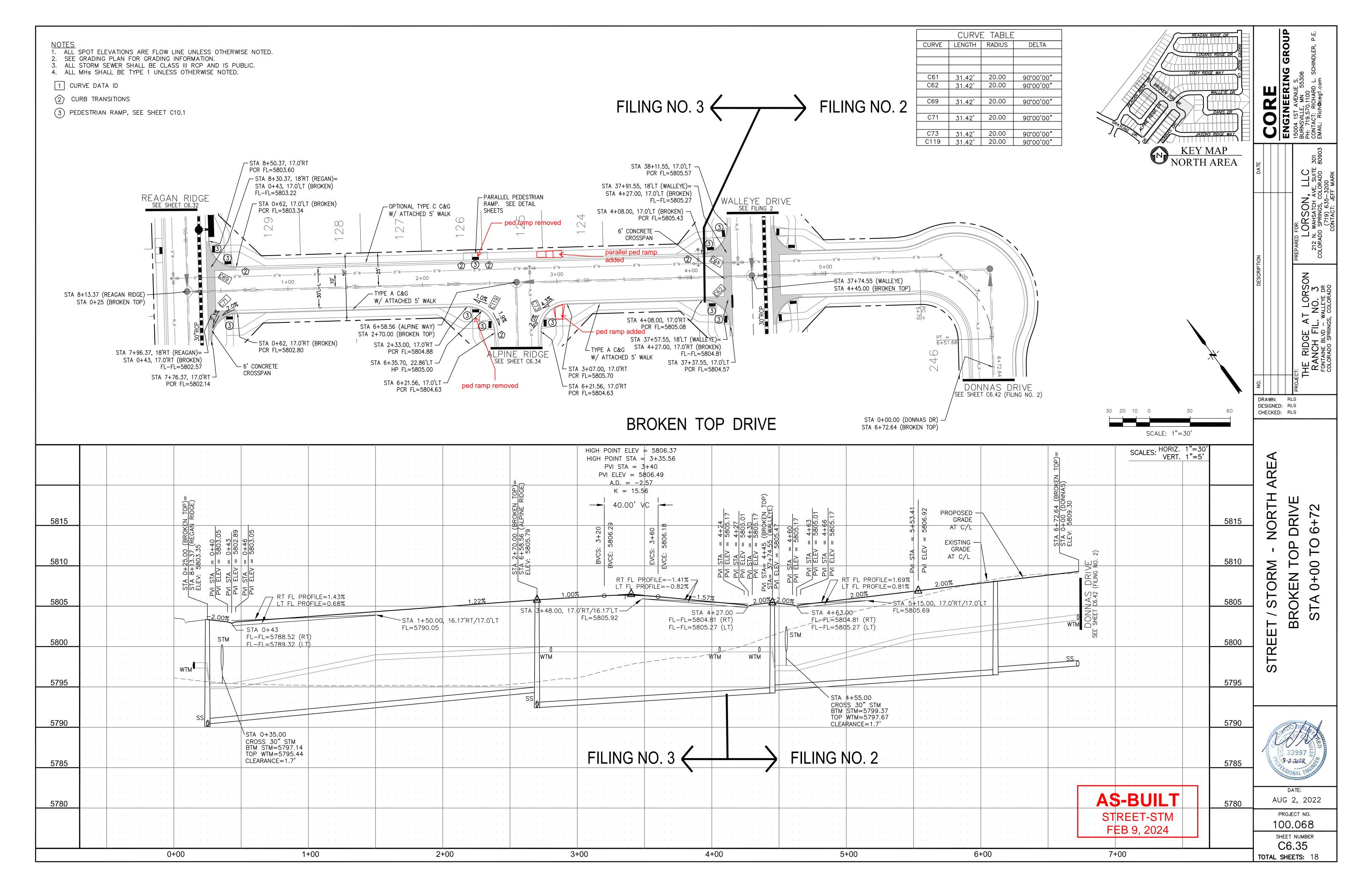


| 2. SEE<br>3. ALL<br>4. ALL                   | GRADING<br>STORM SE             | VATIONS ARE FLOW L<br>PLAN FOR GRADING<br>EWER SHALL BE CLAS<br>LL BE TYPE 1 UNLES<br>ID  | NFORMATION.<br>S III RCP AND IS F | PUBLIC.   |  |  | 5825 S   | TA 0+00 (KNUCKLE A1<br>TA 14+67.42 (REAGAN)<br>VI ELEVATION 5822.27<br>1. | ) <u>STA 1+49.44 (KNU</u><br>STA 15+85.70 (RE<br>PVI ELEVATION 58<br>03% | JCKLE_A1)<br>TAGAN)<br>23.81  |   |          |                   |   |   |
|--|---------------------------------|---|-----------------------------------|---|--|--|--|---|--|---|---|----------|-------------------|---|---|
| 2 CL   | JRB TRAN                        |   | 0.1                               | CURVE LENG<br>C49 31.6<br>C50 31.1<br>C50a 25.1 | 9' 20.00 90'47<br>4' 20.00 89'12         | .'52"<br>.'08"                               | 5820<br>0+00<br>KNU                            | ICKLE "A1"  | <sup>1+00</sup><br>FL PROFI  | LE  |   |          |                   |   |   |
|  |                                 | ~×  | X                                 | ××  |  | <del>`````````````````````````````````</del> | — <u>*                                    </u> |   | <u>X</u>   | - <u>×</u> - <del>×</del>   | XX  | <u> </u> |                   | STA 53+96.62, 0.17'RT<br>PCR FL<br>3+96.62, 17.00'LT (RIKERS)=<br>PCR FL=5830.44  | L=5830.56                                 |
|  |                                 | STA 15+85.70, 16<br>STA 1+49.44 (KN<br>FL=5823.81   | J¢KLE A1)<br>OPTION               | AL TYPE C C&G                                   |  |  |  |   |  |   |   |          |                   | 17.00'LT (REAGAN)=<br>PCR FL=5830.22  | $\searrow$                                |
|  | 8"W                             | 8''W 8''W 8   | W/ ATT                            | ACHED 5' WALK                                   | 8"W8                                     | ""w 8"W                                      |  | -8"W  |  |   | 8''W  |          | 8"W8. <u></u>     | 8''W 8''W | 8"W 200                                   |
| MATCH LINL<br>STA = 15+50<br>SEE SHEET C6.32 |                                 |   |                                   | OPTIONAL TYPE C<br>W/ ATTACHED 5'               | ۲ – ۲<br>• C&G                           |  | Ý Ý  |   | P.   | $\mathcal{P}$   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~   | 3        | STA 22+60.28, 17. | 00'RT (REAGAN)=<br>PCR FL=5830.44<br>STA 53+22.61, 17.00<br>P(  | 0'LT (RIKERS<br>CR FL=5831                |
|  |                                 |   |                                   |   |  |  |  |   | RE   | agan Rie  | DGE DRI   | VE       |                   |   |   |
|  | · · · · ·                       | · · · · · · · · · ·   |                                   |   |  |  |  |   | · · · · · · · · · · ·  | · · · · · · · · · · ·   | · · · · · · · · · · · ·   |          |                   | · · · · · · · · · · ·   |   |
| 5830   | · · · ·                         | = 15+85.70<br>= 5824.21   |                                   |   |  |  |  |   | · · · · · · · · · · ·  |   | EXISTING  | PROPOSED |                   | PVI STA =<br>PVI ELEV   | ST,<br>ST,<br>PV<br>22+28.86<br>= 5830.31 |
| 5825   |                                 | PVI STA<br>PVI ELEV   | · · · · · · · · · · ·             | 0.80%   | PVI STA = 17+50.00<br>PVI ELEV = 5825.52 | 1.00%  |  |   |  | · · · · · · · · · · ·   |   |          |                   |   | · · · · ·                                 |
| 5820   | MATC<br>STA<br>SEE SH           | 1.30%   | · · · · · · · · · · · · ·         |   | · · · · · · · · · · · ·                  |  |  |   |  |   |   |          |                   |   |   |
| 5815   | H LINE<br>= 15+50<br>HEET C6.32 | .     .     .     .     .     .     .       .     .     .     .     .     .     .       .     .     .     .     .     .     .       .     .     .     .     .     .     .   |                                   |   |  |  |  |   |  |   | · · · · · · · · · · · · ·   |          |                   |   | · · · · ·                                 |
| 5810   |                                 | · · · · · · · · · · ·   | · · · · · · · · · · ·             |   |  |  |  |   | · · · · · · · · · · ·  | .       .       .       .       .       .       .       .         .       .       .       .       .       .       .       .         .       .       .       .       .       .       .       .         .       .       .       .       .       .       .       .         .       .       .       .       .       .       .       .         .       .       .       .       .       .       .       . | .       . |          |                   | · · · · · · · · · ·   | · · · · ·                                 |
| 5805   |                                 | · · · · · · · · · ·   |                                   |   |  |  |  |   |  |   | · · · · · · · · · · ·   |          |                   |   | · · · ·                                   |
| -  |                                 | · · · · · · · · · · ·   | · · · · · · · · · ·               |   |  |  |  |   | · · · · · · · · · · ·  | · · · · · · · · · · ·   |   |          |                   | · · · · · · · · · · ·   |   |
| 5800   |                                 |   |                                   |   |  |  |  |   |  |   |   |          |                   |   |   |
| <u>5800</u><br>5795                          |                                 | .       . |                                   |   |  |  |  |   |  |   | · · · · · · · · · · ·   |          |                   |   |   |

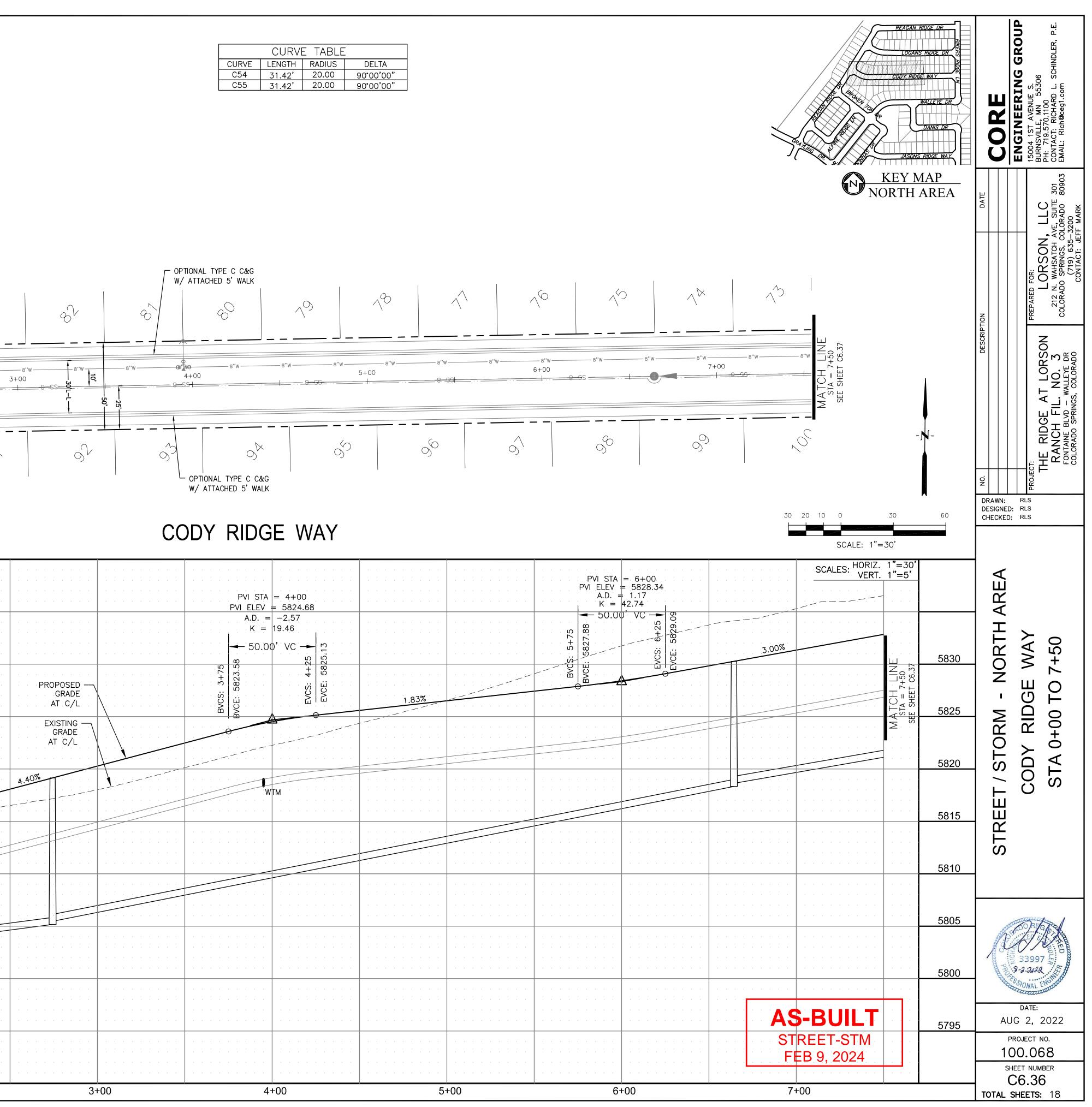


| 2. SEE<br>3. ALL<br>4. ALL<br>1 CUF<br>2 CU   | GRADING<br>STORM S<br>MHs SHA<br>RVE DATA<br>RB TRAN<br>DESTRIAN<br>CUR<br>LENGTI<br>22.02<br>22.02 | PLAN FO<br>EWER SH<br>LL BE T<br>A ID<br>SITIONS<br>RAMP, S<br>RAMP, S<br>CVE TA<br>H RADI<br>A 48.8<br>A 48.8 | IUS DE<br>83 25°5<br>83 25°5             | CIO.1<br>CIO.1<br>CIO.1<br>CIO.1<br>CIO.1 | ION.<br>AND IS PL                 | JBLIC.                    | 2.49 (REAGAN<br>STA 0+25 (<br>STA 3+65.        | (ALPINE)<br>73, 17.0'RT  |   | 2.9% 677<br>3 2  | 20 RCP                              | AND BOGE                              | PCR FL<br>STA 4+<br>STA 0+<br>FL-FL=<br>STA 0+<br>(ALPINE | 43, 17.0'LT (<br>5789.32<br>·62, 17.0'LT | (REAGAN)=       |   |                        |      |  |   |   | TYPE C C&C<br>CHED 5' WALF  | PCR<br>STA 6+35<br>HI<br>STA 6+<br>PC<br>G<br>K | STA 6+58.<br>STA 2+70.0<br>3.00, 17.0'RT<br>FL=5804.88<br>5.70, 22.86'LT<br>FL=5805.00<br>-21.56, 17.0'L<br>CR FL=5804.6  |             | WAY)<br>TOP) |                              | 2.0%<br>2.0%<br>3<br>2<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3 |
|---|---|--|--|---|-----------------------------------|---------------------------|--|--|---|--|-------------------------------------|---------------------------------------|---|--|-----------------|---|------------------------|------|--|---|---|---|---|---|-------------|--------------|------------------------------|---|
| C48<br>C67<br>C73<br>C119<br>C120<br>C121<br>C121<br>C121<br>C121<br>C121<br>C121<br>C121 | 126.54<br>31.17<br>31.42<br>56.28<br>31.42  | , 20.0<br>, 20.0<br>, 20.0<br>, 35.8   | 00 89*1<br>00 90*0<br>00 90*0<br>83 90*0 | <u>41'02"</u><br><u>1.48%</u>             | 0                                 | STA 3-<br>ST/             | +85.49, 18'RT<br>A 0+43, 17.0'I<br>FL-<br>6' ( | RT (ALPINE<br>FL=5788.52<br>CONCRETE -<br>CROSSPAN<br>STA 0<br>PCR | =^<br>2<br>2<br>9+62, 17.0'RT<br>(ALPINE)<br>2 FL=5788.79<br>STA 2+01.4   | 41, 16.17'RT<br>TA 0+00 (KN<br>21.34, ———<br>'INE)=<br>22.02 | (ALPINE)=<br>NUCKLE A)<br>_=5790.78 | a.                                    |   | TYPE A C&G                               | D 5' WALK       | A 2+18.00, 1<br>R FL=5791.15<br>TA 2+99.68,<br>CR FL=5792.<br>$12^{+}$ $3^{+}$ $3^{+}$<br>$-12^{+}$ $3^{+}$ $3^{+}$ | 5                      |      | 578-58-<br>578-58-<br>578-58-<br>578-58-<br>578-58-<br>574-5793-31<br>574-2+96.34, | 4+00<br>8"<br>4<br>4<br>4<br>8"<br>4<br>4<br>9<br>4<br>9  | LPINE)=   |   | -OPTIONAL T<br>W/ ATTACH                        | TYPE C C&G  | 46          | 7,45<br>STA  | A 6+21.56,<br>PCR FL=5       | 17.0'RT   |
|   | K   | NUC  | KLE                                      | "A" Fl                                    | _ PRC                             | OFILE                     | =  |  |   |  |                                     | R=52.00', L                           | CURVE   | 53 /                                     | 15              | ,2  |                        | (    | ALPINE)=   | (KNUCKLE A)   | ļ   | <b>L</b> PIN  | IE R  | IDGE  | LAN         | E            |                              |   |
|   | · · · · ·   | · · · · ·  | · · · · · · ·                            | · · · · ·                                 | · · · · · ·                       | · · · ·                   | · · · · · · ·                                  | · · · ·  |   | <br><br>   | · · · · · ·                         | <br><br>                              | · · · · · · ·   |  | · · · · · · · · | · · · · ·   | PVI STA<br>PVI ELEV    |      | · · · · ·  | <br>  | <br><br>  | <br>  | · · · · ·                                       | <br>  | · · · · ·   | 30.00'       | PVI S<br>PVI ELI<br>A.D<br>K | STA = 6+<br>EV = 580<br>C = -2.14<br>= 14.01  |
| 5805  |   |  | · · · · · · · ·                          |   | · · · · · · ·                     |                           | · · · · · · · ·                                |  | .         .         .         .         .           .         .         .         .         .           .         .         .         .         .           .         .         .         .         . |  | <br><br>                            |                                       | · · · · · · · ·   |  |                 |   | A.D. =<br>K =<br>80.00 |      | 90<br>9.05<br>9.05   | .       .       .       .       .         .       .       .       .       .         .       .       .       .       .         .       .       .       .       .         .       .       .       .       .         .       .       .       .       .         .       .       .       .       .         .       .       .       .       . | .     .     .     .       .     .     .     .       .     .     .     .       .     .     .     .       .     .     .     . | .         .         .         .         .           .         .         .         .         .           .         .         .         .         .           .         .         .         .         .           .         .         .         .         . | · · · · ·                                       | .         .         .         .         .           .         .         .         .         .           .         .         .         .         .           .         .         .         .         .           .         .         .         .         . | · · · · · · |              | BVCS: 5+95<br>BVCE: 5804.28  | EVCS: 6+25  |
| 5800  | · · · ·   | · · · · ·  |  |   | 16<br>16                          | <u>16</u>                 | · · · · · · ·                                  |  | · · · · · ·   | · · · · ·  | · · · · · ·                         | 91.18                                 | PROPOSED<br>GRADE<br>AT C/L                               |  | · · · · · · ·   | 5: 3+10<br>5793.57  |                        |      | EVCS: 3+<br>EVCE: 579  | · · · · · ·   | · · · · ·   | · · · · · · ·   | 4.01%   | · · · · · ·   | · · · · · · |              | · · · · ·                    | · · · · ·   |
| 5795  | · · · ·   | · · · · ·  | · · · · · · ·                            | 0+25.00 (ALPI                             | 146<br>9.46<br>778<br>9.46<br>789 | V = 5789.0<br>V = 5789.0  | · · · · · · ·                                  |  | · · · · · ·   | · · · · ·  | · · · · · ·                         | STA = 2                               | EXISTING<br>GRADE<br>AT C/L                               |  |                 | BVCS:   | · · · · · ·            |      |  |   |   |   | · · · · ·                                       |   |             |              |                              |   |
| E700  | · · · · ·   | · · · · ·  | · · · · · · · ·                          | STA 0+0                                   |                                   | PVI ELE                   | - RT FL PI                                     | ROFILE=1.<br>ROFILE=0.   | 43%<br>68%<br>.30%  | · · · · ·  | · · · · · ·                         |                                       | · · · · · · · · ·   | 2.20%                                    |                 |   |                        |      | · · · · ·  |   |   |   |   | · · · · · · · · · · · · · · · · · · ·   |             | · · · · · ·  | · · · · ·                    | · · · · ·   |
| 5790  |   | · · · · ·  |  |   |                                   | - STA 0<br>FL-FL<br>FL-FL | +43<br>=5788.52 (F<br>=5789.32 (L              |  |   |  | STA 1+50<br>FL=5790.0               | 00, 16.17'                            | RT/17.0'LT  |  | · · · · · · ·   | · · · · ·   |                        | WT.M | · · · · ·  | · · · · · ·   | · · · · ·   | · · · · · ·   |   |   | · · · · ·   |              |                              |   |
| 5785  |   |  | · · · · · · ·                            | wtm()                                     | STM                               |                           | · · · · · · · · ·                              |  | · · · · · ·   |  | · · · · · ·                         |                                       | · · · · · · · ·   |  | · · · · · · ·   | · · · · ·   |                        |      |  |   |   | · · · · · · ·   | · · · · ·                                       | · · · · · ·   | · · · · ·   | · · · · · ·  |                              | · · · · ·   |
| 5780<br>5775  |   |  | · · · · · · ·                            | · · · · · ·                               |                                   |                           |  |  | · · · · · ·   |  | · · · · · ·                         | · · · · · · · · · · · · · · · · · · · |   |  |                 |   |                        |      |  | · · · · ·   | · · · · ·   | · · · · · ·   | · · · · ·                                       | · · · · · ·   | · · · · ·   | · · · · · ·  | · · · · ·                    | · · · ·   |
| 5770  | · · · ·   |  | · · · · · · · ·                          |   | · · · · · ·                       |                           | <br>   |  | <ul> <li></li> <li></li> <li></li> </ul>  |  |                                     |                                       | · · · · · · ·   |  | · · · · · · · · |   |                        |      |  | <br>  |   |   |   | <br>  |             | <br>         |                              | · · · · ·   |
|   |   |  |  |   |                                   |                           | · · · · · · · ·                                |  | · · · · · ·   |  |                                     | · · · ·                               | · · · · · · ·   |  | 3               | +00   |                        |      | · · · · ·  | 00  |   |   |   | 00  |             | · · · · · ·  |                              | · · · · · ·   |



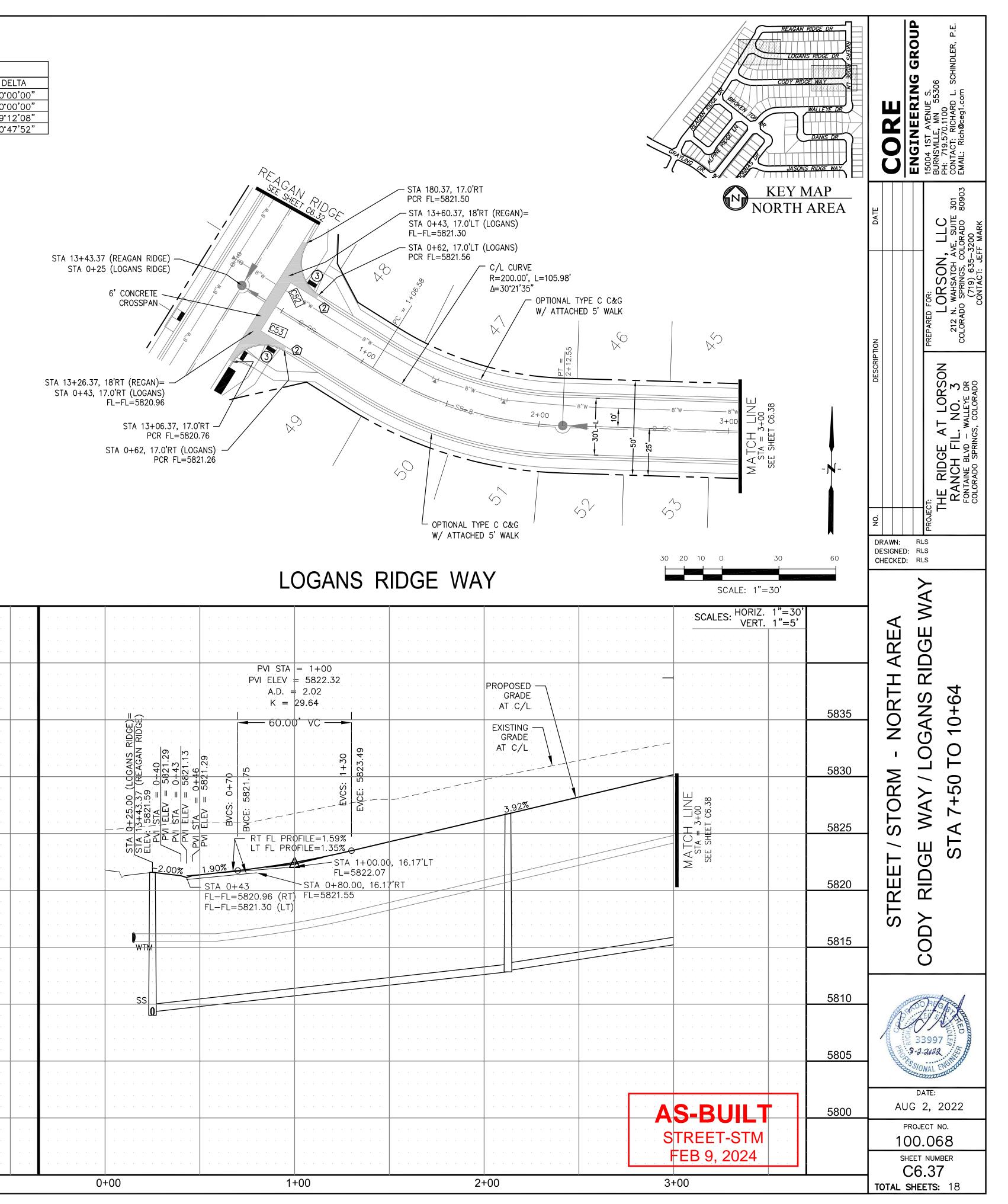


| 2. SEE<br>3. ALL<br>4. ALL<br>1 CUI | GRADING<br>STORM<br>MHS SH<br>RVE DA <sup>-</sup><br>IRB TRA | G PLAN FO<br>SEWER SH<br>ALL BE T<br>TA ID<br>NSITIONS  | OR GRADINO<br>IALL BE CL | G INFORMAT<br>ASS III RCP<br>ISS OTHERV            | SS OTHERWI<br>ION.<br>AND IS PUI<br>VISE NOTED.   | SE NOTED.<br>BLIC.                 |   |  |                                 |                               |                   |               |             |                                       |                               |       |                   |  | C54                 |                                 | RADIUS<br>20.00                       | DELTA<br>90°00'00"<br>90°00'00" |             |           |             |   |   |  |
|-------------------------------------|--|---|--------------------------|--|---|------------------------------------|---|--|---------------------------------|-------------------------------|-------------------|---------------|-------------|---------------------------------------|-------------------------------|-------|-------------------|--|---------------------|---------------------------------|---------------------------------------|---------------------------------|-------------|-----------|-------------|---|---|--|
| STA 10+6<br>STA<br>STA 10<br>S      | 0+51.37,<br>TA 0+43,   | GAN RIDGE)<br>ODY RIDGE)<br>18'RT (REG.<br>17.0'RT (C<br>FL-FL=58<br>0+31.37, 17<br>PCR FL=58 | AN)=                     | 3.1% C55<br>3.1% C55<br>3                          | AN RID GE<br>CE 32 GE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>3 CE<br>5 M CO<br>NCRETE<br>SPAN                 | 8°W 1400                           | STA 0+43,<br>FL-FL=5812<br>- STA 0+62,<br>PCR FL=58 | 37, 17.0'RT<br>13.18<br>37, 18'RT (RI<br>17.0'LT (COD<br>2.80<br>17.0'LT (COD<br>12.93 |                                 | Δ=33°0                        | .00', L=115.      | 74'           | 8''W        | 8''W                                  |                               |       | -8"W              | PTIONAL TYP<br>/ ATTACHED<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/ | 2E C C&G<br>5' WALK | 8''W                            | )<br>                                 |                                 |             |           |             | <ul> <li>√○</li> <li>8''W</li> <li>6+00</li> <li>1 · · · · · 8</li> </ul> |   | )<br>  |
|                                     |  |   | STA U-                   | ⊦62, 17.0'RT<br>PCR FL=5                           | 5812.35   |                                    | ~~~ /   |  |                                 |                               | 90                |               | O<br>N      |                                       | 57                            |       | 3                 | - OPTIONAL<br>W/ ATTA  | TYPE C C&G          |                                 | <u>م</u> ک                            |                                 | 50          |           | 5           |   | 50  |  |
|                                     |  |   |                          |  |   |                                    |   |  |                                 |                               |                   |               |             |                                       |                               |       | CC                | DDY  | RIDO                | GE W                            | /AY                                   |                                 |             |           |             |   |   |  |
|                                     |  |   |                          |  | · · · · · ·   |                                    | · · · · ·   | · · · · · ·  | · · · · ·                       |                               | · · · · ·         |               | · · · · · · | <br><br>                              | · · · · · · · ·               | · · · | · · · · · · · · · |  | PVI ELEV            | A = 4+00<br>= 5824.6<br>= −2.57 |                                       |                                 | · · · · · · |           | · · · · · · |   | PVI STA<br>PVI ELEV =<br>A.D. =<br>K =<br>50.00 | = 6+00<br>= 5828.34<br>1.17<br>42.74<br>) VC |
| 5830                                |  |   | · · · · · · ·            |  | · · · · · ·   |                                    | · · · · ·   | · · · · · ·  | PVI STA<br>PVI ELEV #<br>A.D. # | = 1+50<br>= 5813.68<br>= 3.40 | · · · · ·         | · · ·         | · · · · · · | · · · · ·                             | · · · · · · ·                 | · · · | · · · · · · · · · |  |                     | 19.46                           | 325.13                                |                                 | · · · · · · |           | · · · · · · | o\$: 5+75   | E: \5827.88                                     | EVCS: 6+25                                   |
| 5825                                | · · · · ·  |   | · · · · · · · ·          | RIDGE)=<br>SAN RIDGE)                              | 14 m  |                                    | · · · · ·   | · · · · · ·  |                                 | 29.41                         | · · · · ·         |               | · · · · · · | <br><br>                              | PROPOSED                      |       | · · · · · · · · · |  | 3VCE: 5823.         | FVCS- 44                        |                                       |                                 | 1.83%       |           |             |   | BAC   | <b>5</b>                                     |
| 5820                                |  |   |                          | 0+ <u>25.00 (CODY</u><br>10+68.37 (REA(<br>5812.94 | $\begin{array}{rrrr} A & = & 0+40 \\ LEV & = & 5812.6 \\ A & = & 0+43 \\ LEV & = & 5812.4 \\ = & 0+46 \\ = & 0+46 \\ A & = & 5812.64 \end{array}$ |                                    | · · · · · ·   | 5813.18<br>· · · · · ·   | · · · · ·                       |                               | EVCS: 2+00        | EVCE: 5815.88 | · · · · · · | · · · · · · · · · · · · · · · · · · · | EXISTING —<br>GRADE<br>AT C/L |       |                   |  |                     |                                 | · · · · · · · · · · · · · · · · · · · |                                 | · · · · · · | · · · · · | · · · · · · |   | · · · · · ·                                     |  |
| 5815                                |  |   |                          | STA 1<br>ELEV:                                     | PVI SI<br>PVI E<br>PVI E<br>PVI ELEN  |                                    | RT FL PRO   | )<br>FILE=1.30%<br>FILF=0.67%  |                                 | STA 1+40<br>FL=5813.4         | 0.00, 16.17<br>45 |               |             | 4.40%                                 |                               |       |                   |  |                     | WTM                             | · · · · · · ·                         |                                 | · · · · · · |           | · · · · · · |   |   |  |
| 5810                                |  |   | · · · · · · ·            |  | 2.00%   | - STA 0+43<br>FL-FL=58<br>FL-FL=58 |   | STA 0+80<br>FL=5812.   | 0.00, 16.17<br>58               | 7'RT                          |                   |               |             |                                       |                               | · · · | · · · · · · · · · |  | · · · · · ·         |                                 |                                       |                                 |             |           |             |   | · · · · · ·                                     |  |
| 5805                                | · · · · ·  | · · · ·   | · · · · · · · ·          | WTM  |   |                                    | · · · · · ·   | · · · · · ·  | · · · · ·                       |                               |                   |               | <br>        | · · · · ·                             |                               |       |                   |  |                     |                                 | <br>                                  |                                 | <br>        |           | <br><br>    |   | · · · · · ·                                     | <br>   |
| 5800                                |  |   | <br>                     |  |   |                                    |   |  |                                 |                               |                   |               |             |                                       | · · · · · · ·                 | · · · | · · · · · · · ·   |  | <br>                |                                 | · · · · · ·                           |                                 | · · · · · · |           | · · · · · · |   |   |  |
| 5795                                |  |   |                          |  |   |                                    |   |  |                                 |                               |                   |               |             |                                       |                               |       | · · · · · · · · · |  |                     |                                 |                                       |                                 |             |           |             |   | · · · · · ·                                     |  |
| 5780                                |  |   |                          |  |   |                                    |   |  |                                 |                               |                   |               |             |                                       |                               |       |                   |  |                     |                                 |                                       |                                 |             |           |             |   |   |  |
|                                     | 1  |   |                          | )+00   |   |                                    |   | -00  |                                 |                               |                   | +00           |             |                                       |                               | 3+00  |                   |  |                     | 1+00                            |                                       |                                 |             | +00       |             | ]   |   | +00  |

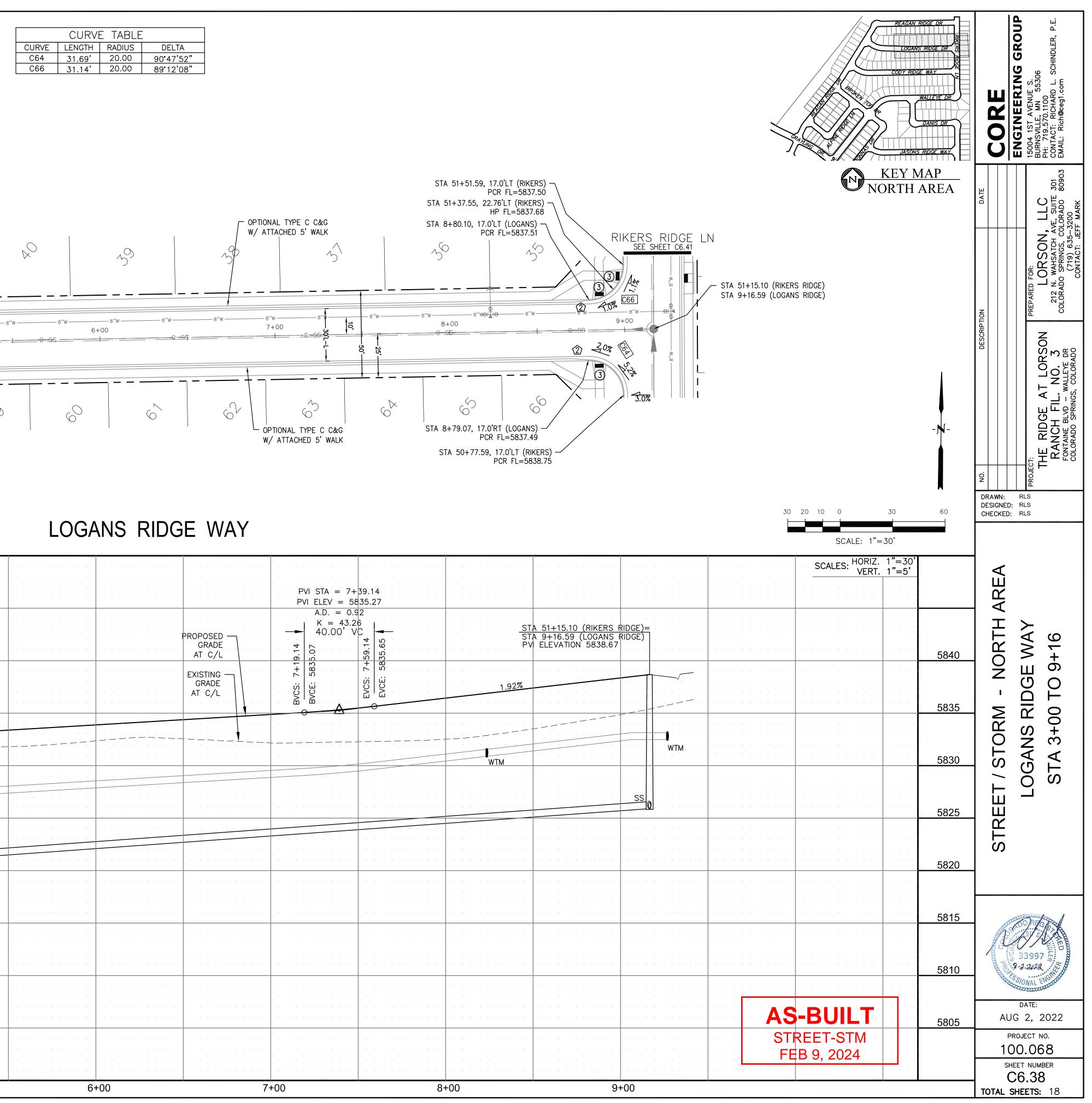


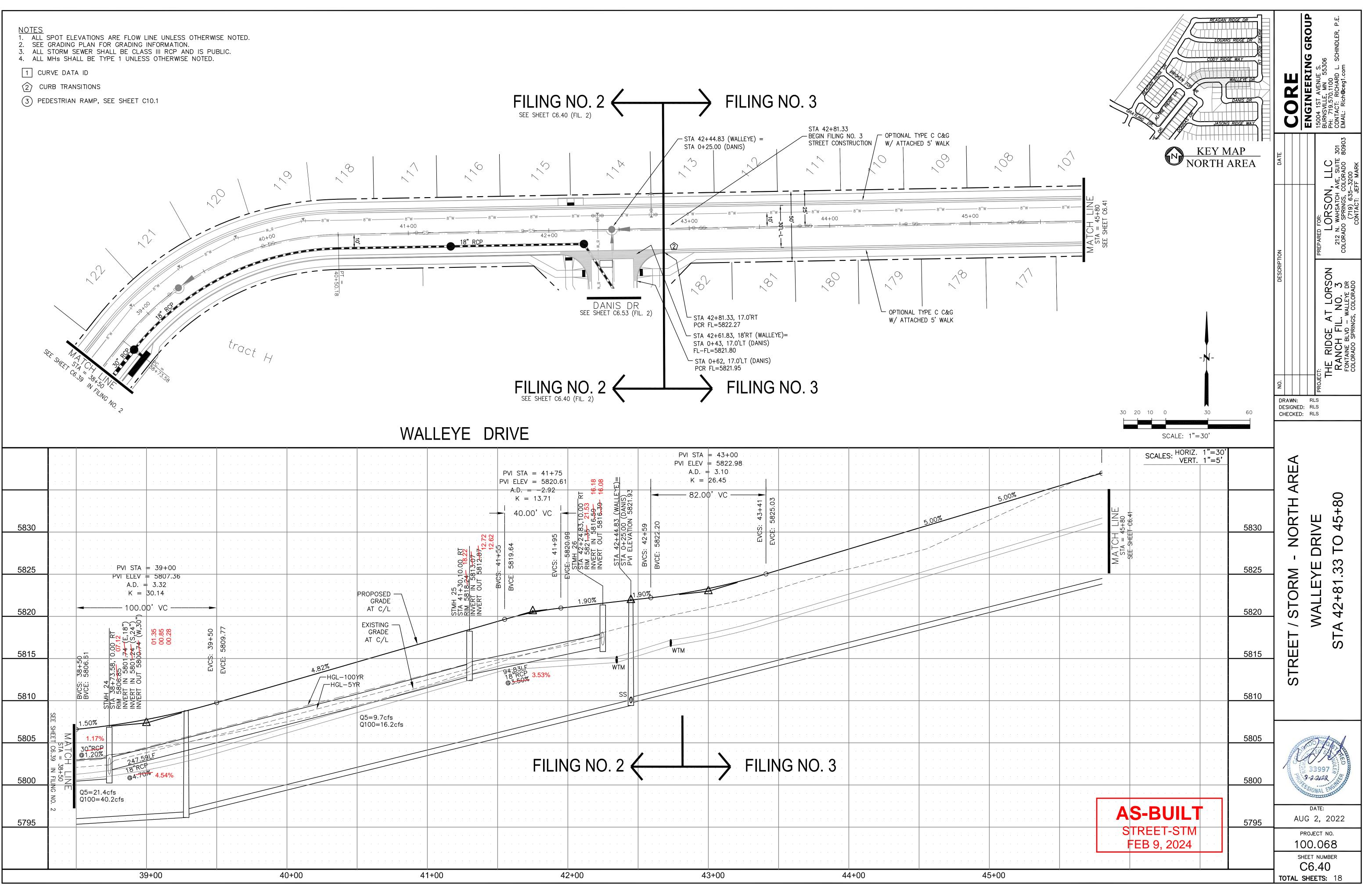
| 2. SEE<br>3. ALL<br>4. ALL<br>1 CL<br>2 CL | SPOT EL<br>GRADING<br>STORM<br>MHs SH<br>JRVE DAT<br>JRB TRA | G PLAN FOR GRADING<br>SEWER SHALL BE CLA<br>ALL BE TYPE 1 UNLE | LINE UNLESS OTHERN<br>INFORMATION.<br>ASS III RCP AND IS P<br>SS OTHERWISE NOTED | WISE NOTED.<br>UBLIC.<br>).   |   |   | CURVE         LE           C52         3           C53         3           C58         3 | 1.42'20.00901.42'20.00901.14'20.0080  | DELTA<br>0°00'00"<br>0°00'00"<br>9°12'08"<br>0°47'52" |   |   |  |   |
|--|--|--|--|---|---|---|--|---|---|---|---|--|---|
| MATCH LINESTA = 7+50SEE SHEET C6.36        |  |  | ED 5' WALK   | STA<br>STA<br>STA<br>STA<br>STA<br>STA<br>STA<br>STA  | 49+31.57, 17.0'LT (RIKERS)<br>PCR FL=5840.90<br>A 10+27.81, 17.0'LT (CODY)<br>PCR FL=5840.52<br>8''W<br>8''W<br>10+00<br>22<br>A 10+25<br>B''W<br>10+00<br>C<br>PCR FL=5840.50<br>A 48+57.56, 17.0'LT (RIKERS)<br>PCR FL=5840.98  | RIKERS F<br>SEE SHER<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3   | Bi <sup>™</sup> B''W   | 5.08 (RIKERS RIDGE)<br>.30 (CODY RIDGE)   | STA 0+<br>STA 13+26.37                                | 37 (REAGAN RIDGE)<br>25 (LOGANS RIDGE)<br>6' CONCRETE<br>CROSSPAN<br>7, 18'RT (REGAN)=<br>17.0'RT (LOGANS)<br>FL-FL=5820.96<br>STA 13+06.37, 17.0<br>PCR FL=5820<br>STA 0+62, 17.0'RT (LOG<br>PCR FL=5820   | ста<br>СБЗ<br>СБЗ<br>СБЗ<br>СБЗ<br>СБЗ<br>СБЗ<br>ССБЗ<br>ССБЗ<br>ССБЗ   | Control Contro | - STA 180.37, 17.0'RT<br>PCR FL=5821.50<br>- STA 13+60.37, 18'RT (REGAN)=<br>STA 0+43, 17.0'LT (LOGANS)<br>FL-FL=5821.30<br>- STA 0+62, 17.0'LT (LOGANS)<br>PCR FL=5821.56<br>- C/L CURV<br>R=200.00<br>Δ=30'21'3<br>- SS 8<br>- SS 8<br>- OPTIONAL TYPE C C&G<br>W/ ATTACHED 5' WALK   |
|  |  |  | CO   | DY RIDGE WA   | Y   |   |  |   |   |   | LC  | GANS RI  | DGE WAY   |
|  | · · · · ·  |  |  | .       . | .       . | .       . |  | .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .       .     .     .     .     .     .     . |   | .     .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .     .   | .       . | .        | .       . |
| 5855                                       | · · · · ·  |  |  |   | · · · · · · PVI E   | STA = 10+10<br>LEV = 5840.64<br>D. = -1.08  |  | .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .       .     .     .     .     .     .     . | · · · · · · · · · · ·                                 |   | A.D. =<br>K = 2   | = 1+00<br>5822.32<br>2.02<br>9.64  | PROPOSE<br>GRAD   |
| 5850                                       |  |  |  | .       . | · · · · · ·   · · · · · · · · · · · · ·   | K = 37.14<br>40.00' VC  | 48+95 08 (RIKERS<br>10+64.30 (CODY RI<br>/ATION 5841.68                                  |   |   | 06ANS RIDGE<br>REAGAN RIDG<br>40<br>821.29<br>321.13<br>46  | 00.09<br>   | 5823.49  | EXISTING<br>GRADE<br>AT C/L   |
| 5845                                       |  |  |  | PROPOSEI<br>GRADE<br>AT C/I   |   | EVCS: 10+   | STA 48+<br>STA 10+(<br>ELEVATIO  |   |   | 0+25.00<br>0+25.00<br>113+43.37<br>13+43.37<br>13+43.37<br>13+43.37<br>13+43.37<br>13+43.37<br>13+43.37<br>13+43.37<br>13+43<br>13+43<br>13+43<br>13+43<br>13+43<br>13+43<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13<br>13+13+13<br>13+13<br>13+13+13<br>13+13+13<br>13+13+13+13+13+13+13+13+13+13+13+13+13+1 |   | S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S   | 3.927   |
| 5840                                       |  |  |  | EXISTING<br>GRADE<br>AT C/L   |   | <u> </u>  | 2%   |   |   |   | 1.90% 0<br>5TA 0+43   | STA 1+00.00,<br>FL=5822.07<br>STA 0+80.00, 16.17'R<br>FL=5821.55   |   |
| 5835                                       |  | 3.00%  |  |   |   |   | · · · · · · · · · · · · · · · · · · ·  |   |   | · · · · · · · · · · · · · · · · · · ·   | FL-FL=5820.96 (RT)<br>FL-FL=5821.30 (LT)  |  |   |
| <u>5830</u><br>5825                        | ATCH LINE<br>STA = 7+50<br>SEE SHEET C6.36                   |  | WTM · · · · · · · · · · ·  |   |   |   | · · · · · · · · · · · · · · · · · · ·  |   |   | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$  |   | ·        |   |
| 5820                                       |  |  |  |   |   |   |  | · · · · · · · · · · ·   |   | · · · · · · · · · · · ·   |   | .        |   |
|  |  |  |  |   | · · · · · · · · · · · · · · · · · · ·   |   |  |   |   | .     .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .     .       .     .     .     .     .     .     .     .     .   |   |  |   |
|  | -  |  | 3+00   | 9+00  | · · · · · · · · · · · · · · · · · · ·   | 0+00  | ·  | · ·   |   | 0+00  | 1+(   | 00   | 2+00  |



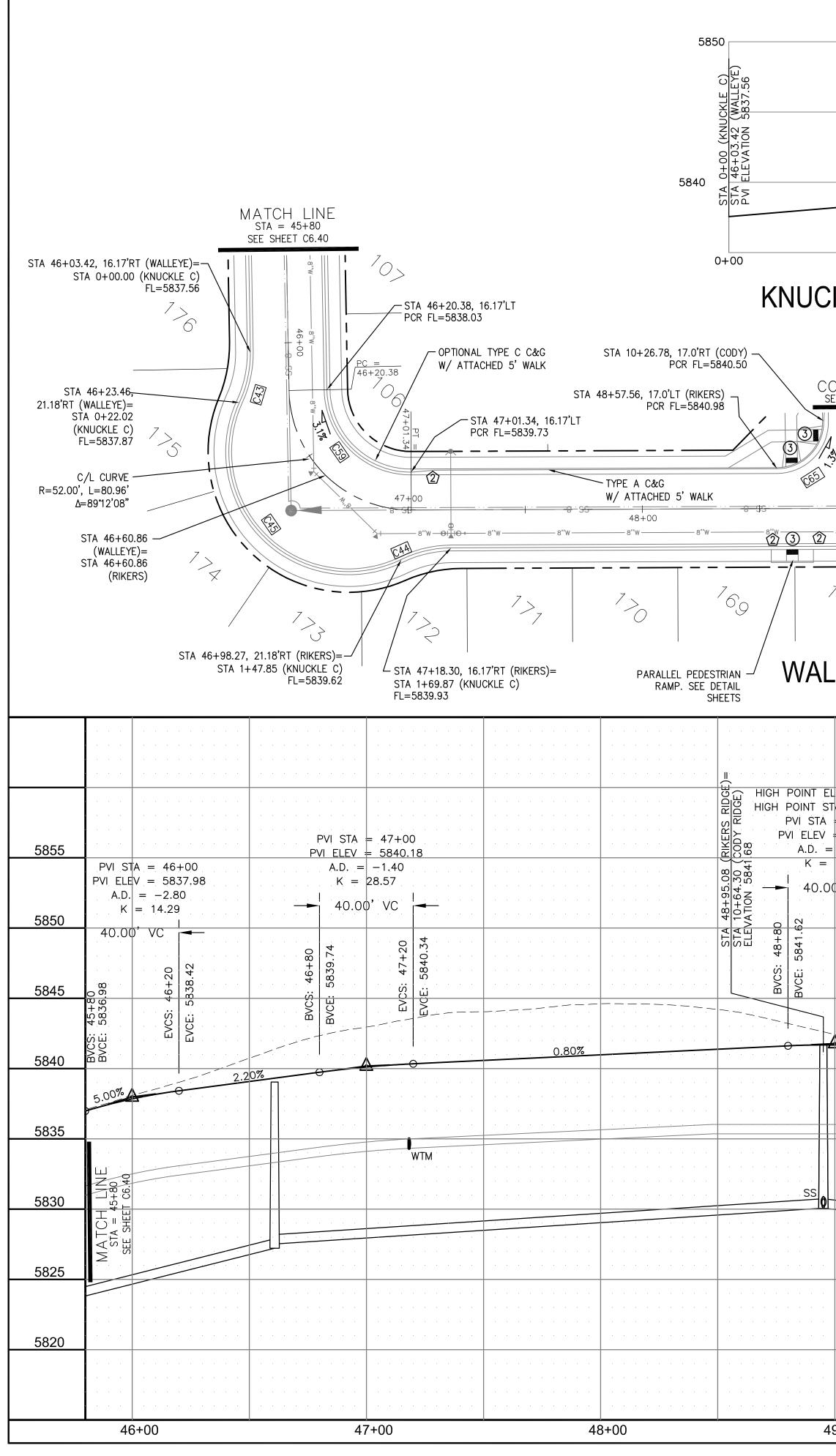


| 2. SEE 0<br>3. ALL 5<br>4. ALL M<br>1 CUR<br>2 CUP | GRADING PLA<br>STORM SEWE<br>MHS SHALL<br>RVE DATA ID<br>RB TRANSITI | AN FOR GRADING<br>ER SHALL BE CLA<br>BE TYPE 1 UNLES<br>) | SS III RCP AND IS PUSS OTHERWISE NOTED.  | JBLIC.      |                   |                   |                 |           |             |           | CURVE LEN<br>C64 31. | JRVE TAB<br>GTH RADIU<br>69' 20.00<br>14' 20.00 | S DEI<br>D 90°4 <sup>-</sup> |                             |           |                         |                                   |                        |                                       |  |   |   |                   |
|--|--|---|--|-------------|-------------------|-------------------|-----------------|-----------|-------------|-----------|----------------------|---|------------------------------|-----------------------------|-----------|-------------------------|-----------------------------------|------------------------|---------------------------------------|--|---|---|-------------------|
|  |  | MATCH LINE<br>STA = 3+00<br>SEE SHEET C6.37               | )<br>  |             | 8''W<br>4+00      |                   |                 | = 4+78.35 | 47"<br>     |           | N                    |   |                              | w/                          | ATTACHED  | E C C&G<br>5' WALK      |                                   | STA<br>STA<br>STA<br>% | 8+80.10, 17.0<br>PCF                  | .76'LT (RIKERS<br>HP FL=5837.6<br>'LT (LOGANS)<br>R FL=5837.51 |   | RIKEF<br>3<br>7.0% C66<br>9+00<br>9+00<br>5.2% C67<br>5.2%  |                   |
|  |  |   |  |             |                   |                   |                 |           |             |           | LOC                  | GANS  | RID                          | GE WAY                      |           |                         |                                   |                        |                                       |  |   |   |                   |
|  | · · · · ·  |   |  |             | · · · · · · · ·   | <br>              | · · · · · · · · | · · · · · | <br>        | <br><br>  | · · · · · · · · ·    | · · · · ·                                       | <br>                         | · · · · · · · · · · · · ·   |           | PVI STA =<br>PVI ELEV = |                                   | · · · · · · ·          | · · · · · ·                           | · · · · ·  | <br>  | · · · · · ·   | · ·               |
| 5840   | · · · · · · · · · · · · · · · · · · ·                                | · · · · · · · · · ·                                       | PVI STA = $3+25$<br>PVI ELEV = $5831.15$<br>A.D. = $-2.93$   | 5           | · · · · · · · · · | · · · · · · · · · | · · · · · · · · | · · · · · | · · · · · · | · · · · · | · · · · · · · · ·    | · · · · ·                                       | · · · · · ·                  | PROPOSED                    |           | A.D. =                  | 0.92<br>3.26<br>VC 71<br>0.92<br> |                        |                                       | STA<br>STA<br>PVI  | <u>51+15.10 (RIKE</u><br>9+16.59 (LOGA<br>ELEVATION 583 | ERS RIDGE<br>ANS RIDGE<br>88.67   | $\frac{1}{2} = 1$ |
| 5835   | · · · · · · · · · · · · · · · · · · ·                                | · · · · · · · · · · · · · · · · · · ·                     | K = 13.66 $40.00' VC$ $920' + 100'$ |             | · · · · · · · · · | · · · · · · · · · | · · · · · · · · | · · · · · | · · · · · · | · · · · · | · · · · · · · · ·    | · · · · · · · · · · · · · · · · · · ·           | · · · · · ·                  | EXISTING<br>GRADE<br>AT C/L |           | BVCE: 5835              | EVCS: 7+5<br>D EVCE: 583          | · · · · · · ·          | · · · · · ·                           | 1.92%  | · · · · · · · · ·                                       | · · · · · ·   |                   |
| 5830   | · · · · · · · · · · · · · · · · · · ·                                | · · · · · · · · · ·                                       |  |             |                   |                   | · · · · · · · · | · · · · · | <br>        | 00%       | · · · · · · · · · ·  |   | · · · · · ·                  |                             | · · · ·   | · · · · · · · · · ·     |                                   | · · · · · · · ·        |                                       |  | · · · · · · · · · · · · · · · · · · ·                   |   |                   |
| 5825   | · · · · · ·  | LINE<br>3+00<br>1 C6.37                                   |  |             |                   | 0 <b>1</b>        |                 | · · · · · |             | · · · ·   | · · · · · · · · ·    | · · · ·   | · · · · · ·                  |                             | · · · · · | · · · · · · ·           | · · · · ·                         | · · · · · · · ·        | · · · · · · · · · · · · · · · · · · · |  | · · · · · · · · ·                                       |   | s o               |
| 5820   | · · · · · ·  | MATCH<br>SEE SHEE   |  |             | · · · · · · · · · | · · · · · · · · · | · · · · · · ·   |           |             | · · · · · | · · · · · · · · ·    |   | · · · · · ·                  | · · · · · · · · · · ·       |           | · · · · · · ·           | · · · ·                           | · · · · · · · ·        |                                       |  | · · · · · · · · ·                                       | .     .     .     .       .     .     .     .       .     .     .     .       .     .     .     . | · · ·             |
| 5815   |  |   |  | · · · · · · |                   |                   |                 |           | · · · · · · | · · · · · | · · · · · · · · ·    | · · · · ·                                       | · · · · · ·                  | · · · · · · · · · · · · ·   | · · · ·   | · · · · · · · ·         | · · · · ·                         | · · · · · · · ·        |                                       |  | · · · · · · · · ·                                       | · · · · · · · · · · · · · · · · · · ·   | · · ·             |
|  | · · · · · ·  |   |  |             |                   | <br>              |                 | · · · · · | <br>        | · · · · · | · · · · · · · · ·    | · · · · ·                                       | · · · · · ·                  | · · · · · · · · · · · ·     | · · · ·   | · · · · · · ·           | · · · · ·                         | · · · · · · ·          |                                       |  | · · · · · · · ·   | .     .     .     .       .     .     .     .       .     .     .     .       .     .     .     . | · · ·             |
| 5810   |  |   |  |             |                   |                   |                 |           |             |           |                      |   |                              | · · · · · · · · · · · ·     |           |                         |                                   |                        |                                       |  |   |   |                   |
| 5805   | · · · · · ·  | · · · · · · · · · ·                                       |  |             | · · · · · · · ·   |                   | · · · · · · · · | · · · · · | · · · · · · | · · · · · | · · · · · · · · ·    | · · · · ·                                       | · · · · · ·                  | · · · · · · · · · · · ·     | · · · · · | · · · · · · ·           | · · · · ·                         | · · · · · · ·          |                                       | · · · · ·  | · · · · · · · ·   | · · · · · ·   | · · ·             |
| - I I  |  |   |  | `           |                   |                   |                 |           |             |           |                      |   |                              |                             |           | -                       |                                   |                        |                                       |  |   | 9+00  |                   |

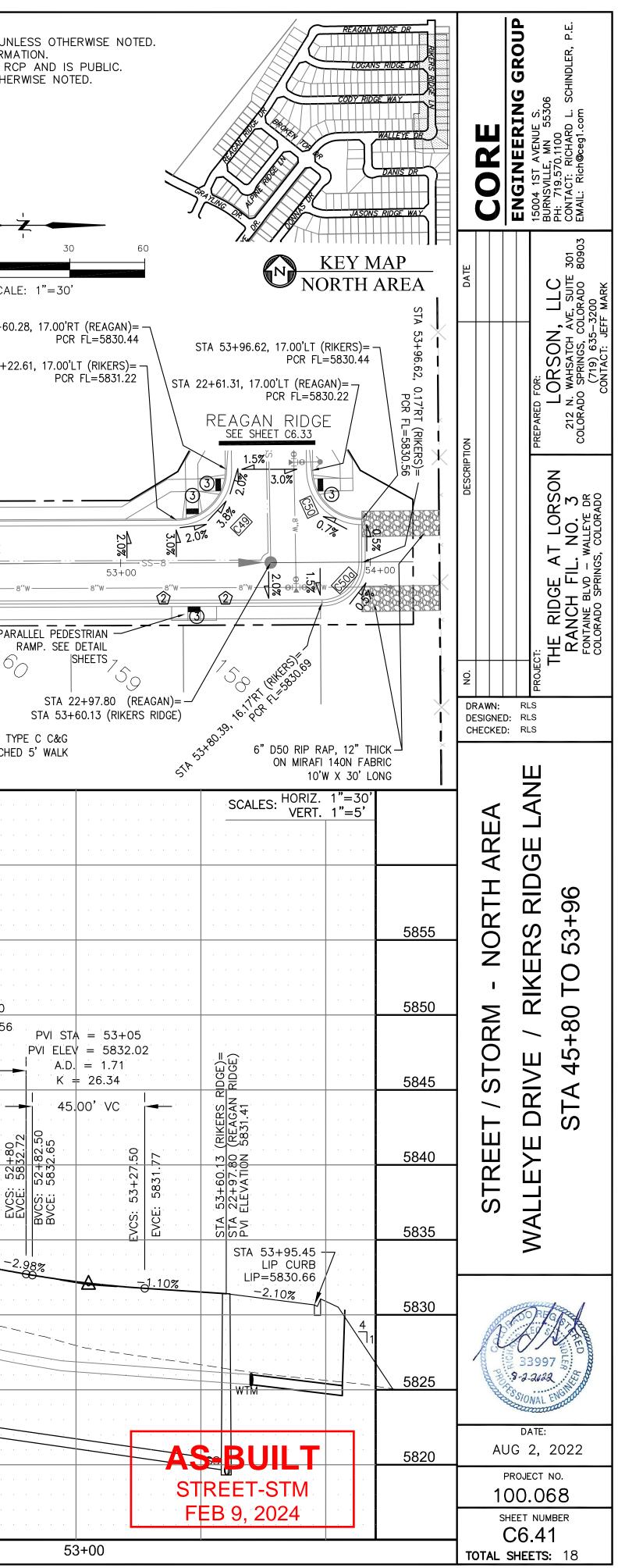


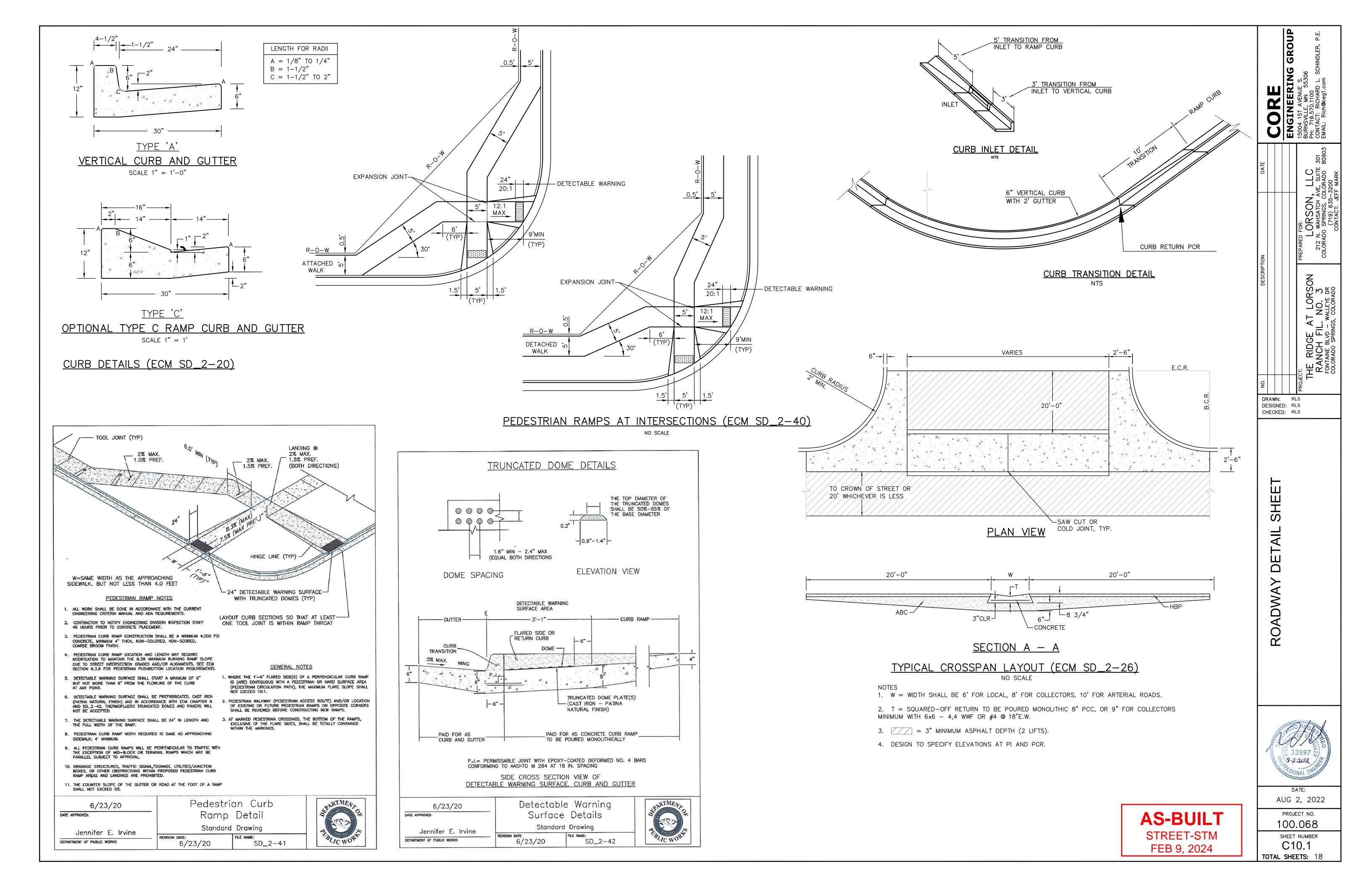


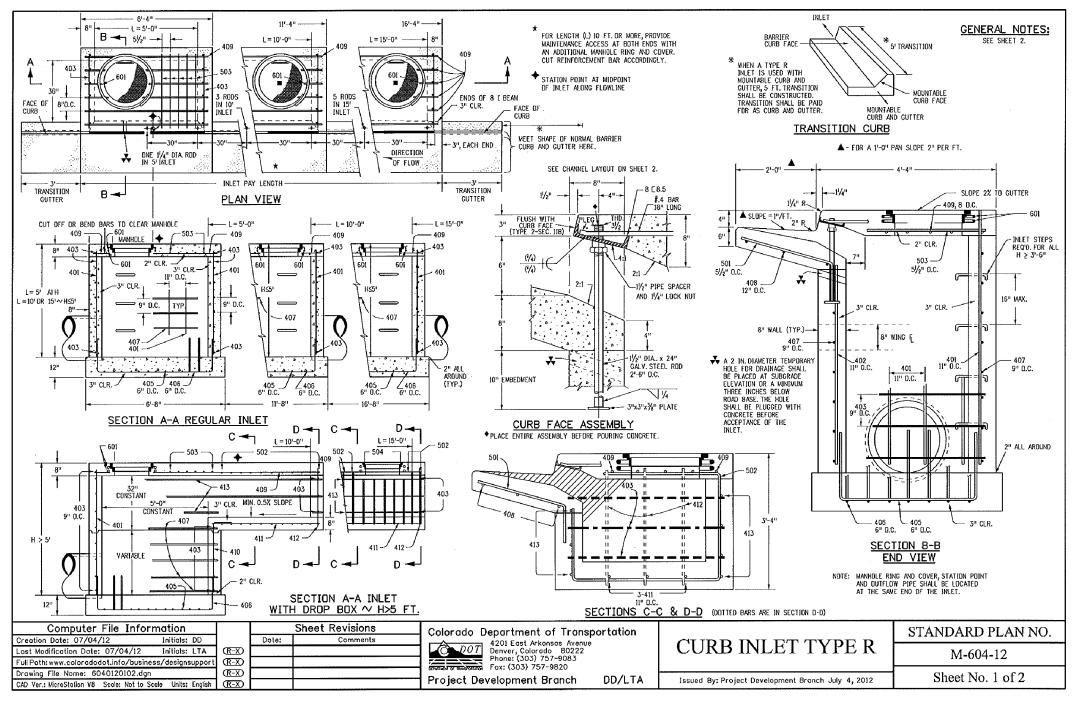
|              | 42  | 2+00   | 4                       | 3+00                |        | 44      | 1+00  | 4   | 5+00      |
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|              |   |  |                         |                     |        |         |   |   |           |
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|              | FILIN   | IG NO. 2 🗲   |                         | $\rightarrow$ Filli | NG NO. | 3       | .       . | .       . | · · · · · |
|              |   |  |                         |                     |        |         |   |   |           |
|              |   |  | · · · · · · · · · · · · |                     |        |         |   |   |           |
|              | .@  | SS   |                         |                     |        |         | · · · · · · · · · ·   |   |           |
|              | 94.83LF<br>18"RCP 3.53%<br>@ <del>3.50%</del> | · · · · · · · · · · · · · · · · · ·  |                         |                     |        |         |   |   |           |
|              |   |  | WTM                     |                     |        |         |   |   |           |
| -            |   |  | · · · · · · · · · · ·   |                     |        |         |   |   |           |
|              |   | 1.90%  |                         |                     |        |         | · · · · · · · · · · ·   |   |           |
| RVCS<br>BVCS |   |  | .90%                    |                     |        |         |   |   |           |
| 4            | 581   | TANK AND   | BVCS:<br>BVCE:          |                     |        | · · · · |   |   |           |
| 12.62<br>+55 | 9.64  | A220.05<br>H 26<br>42+24<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5821.3<br>5755 |                         |                     |        |         |   |   |           |
|              |   | 21.35 21.5<br>21.35 21.5<br>1N 5816.59<br>0UT 5816.3<br>0UT 5816.3<br>0UT 5816.3<br>0UT 5816.3<br>0UT 5816.3<br>0UT 5816.3   | 42+59<br>5822.20        | i i i               |        |         |   | 5.00%   |           |
|              | K = 13.71<br>40.00' VC                        | A2+24.83,10.00 RT<br>42+24.83,10.00 RT<br>5821. <del>35</del> 21.53<br>RT IN 5816.59 16.<br>RT OUT 5816.59 16.<br>RT OUT 5816.39 16.<br>A 42+44.83 (WALLEYE<br>A 0+25.00 (DANIS)<br>C 0+25.00 (DANIS)  |                         |                     |        |         |   |   | 5.00%     |
|              | PVI ELEV = 5820.61<br>A.D. = $-2.92$          | □ 100<br>□  | K =                     | 26.45               |        |         |   |   |           |
|              | PVI STA = 41+75                               |  | PVI ELEV                | = 5822.98<br>= 3.10 |        |         | · · · · · · · · · ·   |   |           |
|              |   |  | A A A A PVI ELEV        |                     |        |         |   |   |           |



|                          |   |                                       |  | 1+69.87 (KNUCKLE C)<br>47+18.30 (RIKERS RIDGE)<br>ELEVATION 5839.93 |   |  |  | 2. SEE GRAD<br>3. ALL STORN<br>4. ALL MHs S<br>1 CURVE D<br>2 CURB TH  | ING PLAN FOR (<br>M SEWER SHALL<br>SHALL BE TYPE   | E FLOW LINE UNI<br>GRADING INFORMA<br>BE CLASS III RC<br>1 UNLESS OTHEF<br>SHEET C10.1 |
|--------------------------|---|---------------------------------------|--|---|---|--|--|--|--|--|
| Cł                       | <u>1.40%</u>  | 1+00                                  | FILE   | STA<br>STA<br>PVI   | .0'RT (LOGANS) —  | CURVE<br>C43<br>C44<br>C45<br>C49<br>C50<br>C50<br>C50<br>C50<br>C58<br>C59<br>C64<br>C65<br>C66 | CURVE<br>LENGTH<br>22.02'<br>125.82'<br>31.69'<br>31.14'<br>25.13'<br>31.14'<br>55.78'<br>31.69'<br>31.69'<br>31.69'<br>31.14'   | RADIUS       D         48.83       25°         48.83       25°         51.17       140         20.00       90°         20.00       89°         16.00       90°         20.00       89°         35.83       89°         20.00       90°         20.00       90°         20.00       90°         20.00       90°   | DELTA<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>3<br>50'31"<br>3<br>50'31"<br>3<br>50'31"<br>3<br>50'31"<br>3<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'31"<br>50'53'09"<br>50'53'09"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50'00"<br>50 | 0 20 10 0<br>SCAL<br>STA 22+60.<br>STA 53+22   |
| SEE<br>SEE               | E SHEET C6.37   | PCR FL                                | +31.57, 17.0'LT (<br>=5840.90                                  |   | 7.0'LT (RIKERS)<br>CR FL=5838.75  | LOGANS<br>SEE SHEET  | RIDGE<br>$C6.38$ $1^{10}$ $C66$ $1.76$ $R^{10}$  | ST<br>HF<br>P(   | STA 8+80.10, 17.0'<br>PCR FL=5837.51<br>TA 51+37.55, 22.76<br>P FL=5837.68<br>TA 51+51.59, 17.0'<br>CR FL=5837.50<br>TYPE A<br>W/ AT<br>52+00<br>8''W  | 6'LT (RIKERS)<br>'LT (RIKERS)  |
|                          | U STA 48+95   | RIVE /                                |  | Tog<br>S RIDG   | STA 51+15.10 (RIKER<br>STA 9+16.59 (LOGAN<br>ELANE  | S RIDGE)<br>PARALLE  | PEDESTRIAN<br>P. SEE DETAIL<br>SHEETS  |  |  | OPTIONAL TY<br>W/ ATTACHE  |
| ST4<br>A =<br>V =<br>= 1 | EV = 5841.68<br>A = 48+95.07<br>= 49+00<br>= 5841.78  |                                       |  | · · · · · · ·   |   |  | · · · · · · ·  | · · · · · · ·  |  |  |
|                          | -2.12<br>18.84<br>)' VC<br>-2.12<br>18.84<br>)' VC<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12 |                                       |  | PVI<br>· · · · · · · · · · · · · · · · · · ·                        | 'I STA = $50+70$<br>ELEV = $5839.53$<br>A.D. = $-0.58$<br>K = $104.08$<br>60.00' VC   | 5<br>(ERS RIDGE)=<br>38.67<br>1<br>1   | PV STA =<br>PVI ELEV =<br>A.D. =<br>K = 1<br>+   | - 5837.73<br>- 3.00<br>3.33  | PVI .[   | STA = 52+50<br>ELEV = 5833.56<br>A.D. = 2.09   |
|                          | -2.12<br>18.84<br>)' VC<br>-2.12<br>18.84<br>)' VC<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2.12<br>-2  | · · · · · · · · · · · · · · · · · · · | DPOSED<br>GRADE<br>AT C/L<br>(ISTING<br>GRADE<br>AT C/L<br>32% | PVI   | $\frac{\text{ELEV} = 5839.53}{\text{A.D.} = -0.58}$ $\text{K} = 104.08$   | E: 5838.96<br>15.10 (RIKERS<br>6.59 (LOGANS<br>ATION 5838.67                                     | BVCS: 51+45<br>= V3L3<br>K = 1<br>K = 1<br>- V3L3<br>- V | - 5837.73<br>- 3.00<br>3.33  |  | ELEV = 5833.56   |
|                          | -2.12<br>18.84<br>)' VC<br>+ 6<br>+ 6<br>+ 6<br>+ 6<br>+ 6<br>+ 6<br>+ 6<br>+ 6<br>+ 6<br>+ 6   |                                       | GRADE<br>AT C/L<br>KISTING<br>GRADE<br>AT C/L                  | 5839.93<br>5839.93  | $\begin{array}{rcl} \text{ELEV} &=& 5839.53\\ \text{A.D.} &=& -0.58\\ \text{K} &=& 104.08\\ & & & & & & & \\ 60.00' & \text{VC} & & & & \\ & & & & & & \\ & & & & & & & $ | EVCE: 5838.96<br>STA 51+15.10 (RIKERS<br>STA 9+16.59 (LOGANS<br>PVI ELEVATION 5838.67            | BVCS: 51+45<br>= V3L3<br>K = 1<br>K = 1<br>- V3L3<br>- V | -5837.73<br>-3.00<br>3.33<br>VC<br>-5.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-3.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5.00<br>-5. | BVCS: 52+20<br>BVCE: 5835.03<br>BVCE: 5835.03  | ELEV = 5833.56<br>A.D. = 2.09<br>K = 28.69<br>60.00' VC                                |







BW

6'-4"

6'-10"

OD + 16"

11/10

