

**FINAL DRAINAGE REPORT
FOR
ABTR STORAGE
UNPLATTED
415 N FRANCEVILLE COAL MINE ROAD
COLORADO SPRINGS, COLORADO**

MARCH 2023

Prepared For:
FLYING HORSE REALTY
2748 North Gate Blvd
Colorado Springs, CO 80921
719.235.8195

Prepared By:
TERRA NOVA ENGINEERING, INC.
721 S. 23RD Street
Colorado Springs, CO 80904
719.635.6422

TNE Job No. 2309.00
County Job No. ###

FINAL DRAINAGE REPORT FOR ABTR STORAGE

TABLE OF CONTENTS

Engineer's Statement	Page 3
Purpose	Page 4
General Description	Page 4
Existing Drainage Conditions	Page 5
Proposed Drainage Conditions	Page 6
Hydrologic Calculations	Page 9
Hydraulic Calculations	Page 9
Floodplain Statement	Page 10
Water Quality	Page 10
Construction Cost Opinion	Page 10
Drainage Fees	Page 10
Maintenance	Page 10
Summary	Page 11
Bibliography	Page 11

APPENDICIES

VICINITY MAP

S.C.S. SOILS MAP

FEMA FIRM MAP

HYDROLOGIC CALCULATIONS

HYDRAULIC CALCULATIONS

DETENTION CALCULATIONS

DRAINAGE PLAN

**FINAL DRAINAGE REPORT
FOR
ABTR STORAGE**

DESIGN ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Dane Frank, P.E. 50207
On behalf of Terra Nova Engineering, Inc.

Date

OWNER/DEVELOPER'S STATEMENT:

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

Authorized Signature

Date

Printed Name, Title

Business Name

Address

EL PASO COUNTY:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine, P.E.
County Engineer / ECM Administrator

Date

Conditions:

FINAL DRAINAGE REPORT FOR ABTR STORAGE

PURPOSE

The purpose of this Final Drainage Report (FDR) is to identify and analyze the proposed drainage patterns, determine proposed runoff quantities, size drainage structures for conveyance of developed runoff, and present solutions to drainage impacts on-site and off-site resulting from this development. The site has not been previously platted or studied.

GENERAL DESCRIPTION

This FDR is an analysis of approximately 38.5 acres of undeveloped land located at 415 n Franceville Coal Mine Road. A portion of this site is being developed as vehicle/trailer parking. The site is in the northeast quarter of Section 18, Township 14 South, Range 65 West and the northwest quarter of Section 17, Township 14 South, Range 65 West of the 6th Principal Meridian within El Paso County. The parcel is bounded to the north by Highway 94, to the east and south by unplatted land, and to the west by North Franceville Coal Mine Road (See vicinity map in appendix).

The site lies within the Jimmy Camp Creek Basin, with storm runoff surface draining from the east to the west, with most of the runoff flowing onto North Franceville Coal Mine Road and some runoff flowing off the site to the south. There is one culvert on the west side of the site that crosses North Franceville Coal Mine Road and drains to the neighboring property to the west.

Soils for this project are delineated by the map in the appendix as Nelson-Tassel fine sandy loams, 3 to 18 percent slopes (56). Soils in the study area are shown as mapped by S.C.S. in the “Soils Survey of El Paso County Area” and contains soils of Hydrologic Group B.

The site is largely undeveloped with mostly grass and dirt surfaces, and occasional shrubs/trees. There is one building with a fence and gravel yard in the northwest corner that is owned by Cherokee Metro District. The site drains to the southeast, with an average slope of 3.8%.

EXISTING DRAINAGE CONDITIONS

There are six drainage basins, three of which are offsite. See attached Existing Drainage Map (in appendix).

Basin OS-X is 7.12 acres and drains to Design Point X on the east side of the site. This basin is offsite and runoff from this basin flows onto the site and into basin EX-A. Basin OS-X has flows of $Q_5 = 2.1$ cfs and $Q_{100} = 13.4$ cfs.

Basin OS-Y is 21.4 acres and drains to Design Point Y at the east side of the site. This basin is offsite and runoff from this basin flows onto the site and into basin EX-C. Basin OS-Y has flows of $Q_5 = 7.7$ cfs and $Q_{100} = 34.5$ cfs.

Basin OS-Z is 1.84 acres and drains to Design Point Z at the north side of the site. This basin is offsite and runoff from this basin flows onto the site and into basin EX-C. Basin OS-Z has flows of $Q_5 = 3.1$ cfs and $Q_{100} = 7.8$ cfs.

Basin EX-A is 13.4 acres and drains to Design Point A near the southwest corner of the site. Runoff flows off the site and onto the adjacent property. Basin EX-A has flows of $Q_5 = 3.1$ cfs and $Q_{100} = 19.1$ cfs. Design Point A has combined flows of $Q_5 = 5.2$ cfs and $Q_{100} = 32.5$ cfs from basins OS-X and EX-A.

Basin EX-B is 1.96 acres and drains to Design Point B at the west side of the site. Runoff flows off the site and onto North Franceville Coal Mine Road. Basin EX-B has flows of $Q_5 = 0.6$ cfs and $Q_{100} = 4.0$ cfs.

Basin EX-C is 23.2 acres and drains to Design Point C at the west side of the site. Runoff flows into a 54" CMP culvert, under North Franceville Coal Mine Road, and onto the neighboring property to the west. Basin EX-C has flows of $Q_5 = 5.0$ cfs and $Q_{100} = 30.2$ cfs. Design Point C has combined flows of $Q_5 = 15.8$ cfs and $Q_{100} = 72.5$ cfs from basins OS-z, OS-Y, and EX-C.

Note: After the culvert crosses the road and ends, there is a retaining wall that appears to have a RCP pipe opening of similar size that continues west. No plans or reports containing this pipe have been found and the discharge point is not known. Based on historic aerial photos, this pipe may discharge approximately 500 feet west-southwest of the retaining wall, but this has not been confirmed.

PROPOSED DRAINAGE CONDITIONS

Runoff in the developed conditions consists of 11 basins; one existing basin, seven onsite basins, and three offsite basins. Below is a description of the runoff in the developed conditions and how it will be safely routed, treated and detained. See appendix for calculations.

Existing Basins

Basin EX-B is 1.96 acres and drains to Design Point B at the west side of the site. Runoff flows off the site and onto North Franceville Coal Mine Road. Basin EX-B has flows of $Q_5 = 0.6$ cfs and $Q_{100} = 4.0$ cfs.

Offsite Basins

Basin OS-X is 7.12 acres and drains to Design Point X on the east side of the site. This basin is offsite and runoff from this basin flows onto the site and into basin EX-A. Basin OS-X has flows of $Q_5 = 2.1$ cfs and $Q_{100} = 13.4$ cfs.

Basin OS-Y is 21.4 acres and drains to Design Point Y at the east side of the site. This basin is offsite and runoff from this basin flows onto the site and into basin EX-C. Basin OS-Y has flows of $Q_5 = 7.7$ cfs and $Q_{100} = 34.5$ cfs.

Basin OS-Z is 1.84 acres and drains to Design Point Z at the north side of the site. This basin is offsite and runoff from this basin flows onto the site and into basin EX-C. Basin OS-Z has flows of $Q_5 = 3.1$ cfs and $Q_{100} = 7.8$ cfs.

Onsite Basins

Basin PR-1 is 9.92 acres and drains to Design Point 1 at the southwest EDB. Basin PR-1 is the

southern portion of the asphalt millings parking area. Basin PR-1 has flows of $Q_5 = 11.4$ cfs and $Q_{100} = 27.3$ cfs.

Basin PR-2 is 9.30 acres and drains to Design Point 2 at the northeast corner of the asphalt millings parking area. Basin PR-2 has flows of $Q_5 = 10.6$ cfs and $Q_{100} = 25.6$ cfs.

Basin PR-3 is 8.78 acres and drains to Design Point 3 at the west end of the basin. Basin PR-3 has flows of $Q_5 = 32.9$ cfs and $Q_{100} = 62.8$ cfs. This basin has been calculated with the future commercial development runoff, which has also been used to determine the volume of the northwest EDB.

Basin PR-4 is 3.27 acres and drains to Design Point 4 at the northwest EDB. Basin PR-4 has flows of $Q_5 = 1.1$ cfs and $Q_{100} = 7.1$ cfs. Design Point 4 has combined flows of $Q_5 = 44.7$ cfs and $Q_{100} = 95.5$ cfs from basins PR-4, PR-3, and PR-2.

Basin PR-5 is 1.78 acres and drains to Design Point 5 at the west edge of the site. This basin is mostly undeveloped area, plus the Cherokee Metro District facility, that includes the culvert that drains the north portion of the site across N Franceville Coal Mine Road. Basin PR-5 has flows of $Q_5 = 1.0$ cfs and $Q_{100} = 4.5$ cfs. Design Point 5 has combined flows of $Q_5 = 4.6$ cfs and $Q_{100} = 34.4$ cfs from basins PR-5 and the pond outlet.

Basin PR-6 is 0.42 acres and drains to Design Point 6 on the south edge of the site. This basin is a landscaping area that flows offsite to the south. Basin PR-6 has flows of $Q_5 = 0.2$ cfs and $Q_{100} = 1.1$ cfs.

Basin PR-7 is 3.03 acres and drains to Design Point 7 at the south edge of the site. This basin is landscaping area, driveway, and the portion of the asphalt millings parking area that is below the southwest EDB. Basin PR-7 has flows of $Q_5 = 1.9$ cfs and $Q_{100} = 8.1$ cfs. Water quality treatment for this basin is provided by the landscaping area south of the driveway and parking area (runoff reduction by grass buffer).

At Design Point 1 the runoff from basin PR-1 will be captured in a 0.794 acre-foot Southwest EDB. Runoff sheet flows into the EDB from three sides. Two 117 cu-ft concrete lined forebays with 1.5 feet high concrete cutoff walls have been placed in the east corners of the EDB where most of the flow will enter. A 3 inch notch in the wall drains the flow to a 1' concrete trickle channel, then the runoff is routed to the 3.0' deep micropool which has a 6" deep initial surcharge area. The 9.92 acres tributary to the EDB are 40% impervious. Based upon this we need a WQCV of 0.149 ac-ft, an EURV volume of 0.268 ac-ft and 100-year volume of 0.377 ac-ft, for a total volume needed of 0.794 ac-ft. The bottom of the micropool elevation is at 6233.00 while the top of the ISV elevation is at 6236.00. The WQCV orifice plate has four rows of 1 inch diameter holes spaced irregularly. A 4'x4' outlet structure is set at 6238.75. The 100-year elevation tops out at 6239.63. A 18" HDPE outlet with a restrictor plate will release $Q_5=1.7$ cfs and $Q_{100}=14.2$ cfs discharge south, to a riprap settling basin near that south property line that will provide energy dissipation and allow smaller flows to infiltrate. Larger flows will overtop the settling basin and follow the existing drainage path south of the site.

At Design Point 4 the runoff from basins PR-2, PR-3, and PR-4 will be captured in a 2.293 acre-foot Northwest EDB. This EDB has been sized for the volume from the future commercial development of basing PR-3, while the proposed structures (such as forebay and outlet structure) have been sized based on the currently proposed design. Runoff sheet flows into the EDB from three sides. A 300 cu-ft concrete lined forebay with 1.5 feet high concrete cutoff walls has been placed in the southeast corner of the EDB where most of the proposed flow will enter (another forebay will be required for the future commercial development). A 3 inch notch in the wall drains the flow to a 2' concrete trickle channel, then the runoff is routed to the 3.0' deep micropool which has a 6" deep initial surcharge area. The 21.4 acres tributary to the EDB are 20% impervious (not including the future commercial development). Based upon this we need a WQCV of 0.206 ac-ft, an EURV volume of 0.219 ac-ft and 100-year volume of 0.697 ac-ft, for a total volume needed of 1.122 ac-ft. The bottom of the micropool elevation is at 6219.00 while the top of the ISV elevation is at 6222.00. The WQCV orifice plate has three rows of 15/16 inch diameter holes spaced irregularly. A 4'x5' outlet structure is set at 6224.05. The 100-year elevation tops out at 6225.19. A 24" HDPE outlet with a restrictor plate will release $Q_5=4.8$ cfs and $Q_{100}=27.0$ cfs discharge west, to an outfall point near the existing culvert under N Franceville Coal Mine Road.

In an effort to protect receiving water and as part of the “four-step process to minimize adverse impacts of urbanization” this site was analyzed in the following manner:

1. Reduce Runoff- The proposed impervious areas on the site are surrounded by landscaping and green space areas. Also, the proposed parking area is being surface with asphalt millings, which slow runoff and allow for infiltration compared to pavement. Additionally, the new improvements and impervious areas on the site are being routed to proposed EDBs. These items will reduce the volume of runoff using ponding and infiltration.
2. Stabilize Drainageways- There are no existing drainageways onsite. The proposed swales have been designed to be stable.
3. Provide Water Quality Capture Volume (WQCV)- The EDBs has been sized and designed to sufficiently capture the required WQCV and slowly release it though the orifice plate, thereby allowing solids and contaminants to settle out.
4. Consider Need for Industrial and Commercial BMPs- The proposed development is a vehicle/trailer parking lot; therefore, no Industrial and Commercial BMPs have been proposed.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County Storm Drainage Design Criteria Manual - Volumes 1 & 2, latest editions. The Rational Method was used to estimate storm water runoff anticipated from design storms with 5-year and 100-year recurrence intervals. The Urban Drainage Criteria Manual was used to calculate the detention and water quality volume.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning’s Formula and the methods described in the El Paso County Storm Drainage Design Criteria Manual – Volumes 1 & 2, latest editions. The pertinent data sheets are included in the appendix of this report.

The existing culvert under N Franceville Coal Mine Road has been evaluated for capacity. The calculation have been included in the appendix.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain, as determined by Flood Insurance Rate Map No. 08041C0780 G, dated December 7, 2018 (see appendix).

WATER QUALITY

The proposed EDBs provides water quality treatment for most of the proposed development.

Runoff from the impervious areas in basin PR-7 is being treated by the landscaping areas to the south (runoff reduction from grass buffers).

CONSTRUCTION COST OPINION

Public Reimbursable

None

Public Non-Reimbursable

None

Private Non-Reimbursable

1. 18" HDPE	120 LF	\$ 60	\$ 7,200
2. 24" HDPE	1605 LF	\$ 70	\$ 112,350
3. CDOT Type C Area Inlet	2 EA	\$ 5,000	\$ 10,000
4. 5' Manhole	2 EA	\$ 7,700	\$ 15,400
5. EDB	2 EA	\$ 75,000	<u>\$ 150,000</u>
			Total \$ 294,950

DRAINAGE FEES

This drainage report is part of a site development application; therefore, no drainage fees are due.

MAINTENANCE

The Extended Detention Basins are private and will be maintained by the property owner. The proposed storm sewers and swales are private and will be maintained by the property owner.

SUMMARY

Development of this site will not adversely affect the surrounding development. This report is in general conformance with the previous reports which included this site. Site runoff and storm drain appurtenances from the development will not adversely affect the downstream and surrounding developments and will be safely routed to the proposed extended detention basins and runoff reduced to the allowable pre-developed rates while slowly treating the water quality capture volume. Runoff leaving the proposed extended detention basins is then routed to the existing drainage paths.

PREPARED BY:
TERRA NOVA ENGINEERING, INC.

Dane Frank, P.E.
Project Engineer

Jobs/2309.00/Drainage/230900 FDR.doc

BIBLIOGRAPHY

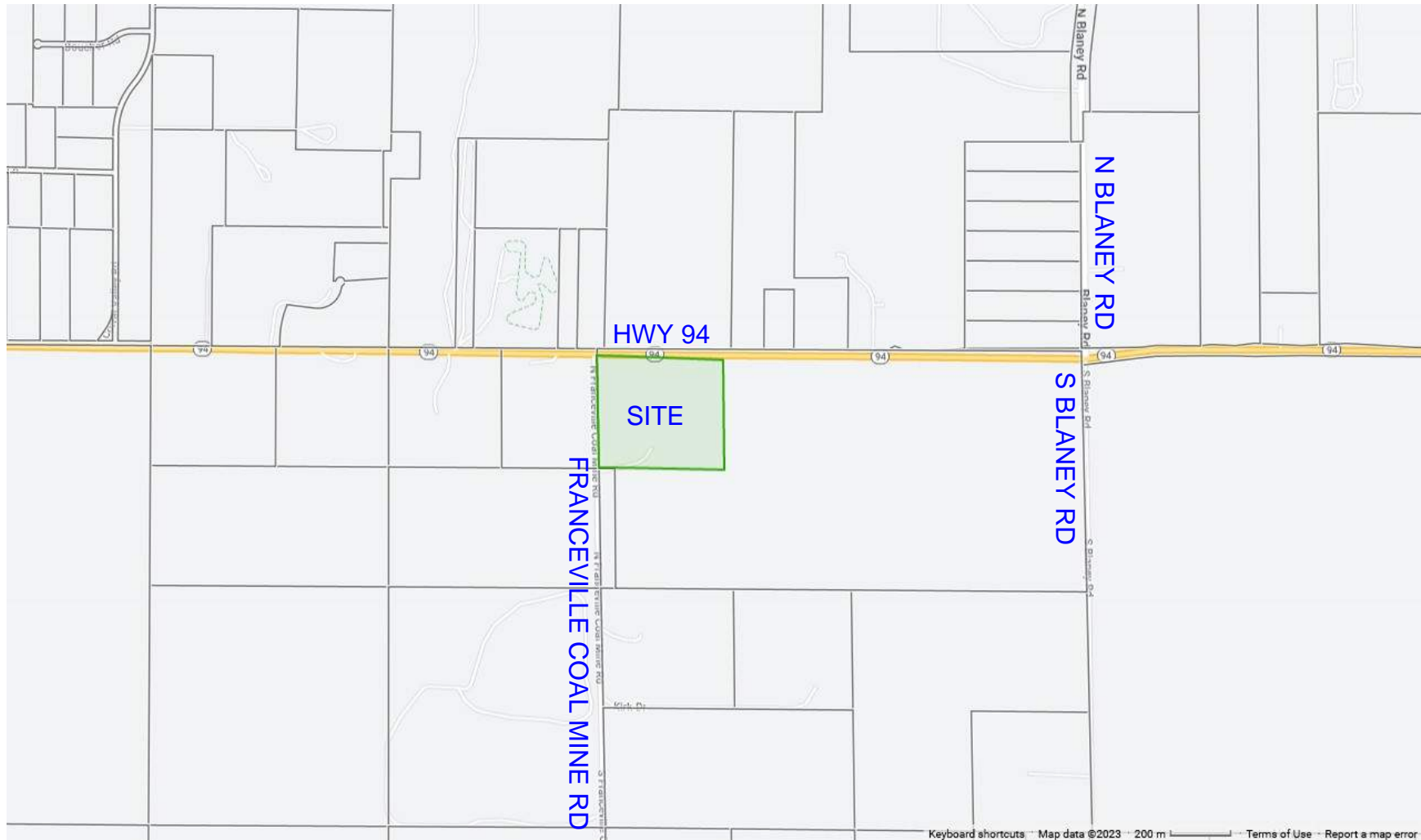
El Paso County Drainage Criteria Manual-Volumes 1 & 2, latest edition

El Paso County Board Resolution No 15-042 (Adoption of Chapter 6 and Section 3.2.1 Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014, Hydrology and Full Spectrum Detention)

VICINITY MAP

El Paso County - Community: Property Search
Schedule Number: 4400000565

2309.00 ABTR Storage
Vicinity Map



North is up 

ABTR - Storage - Location Map

Image Dated Oct 2019

All Auto Recyclers

94

SITE

N Franceville Coal Mine Rd

Google Earth

N

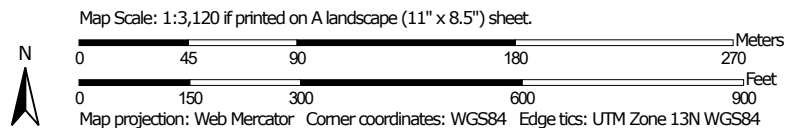
900 ft

S.C.S. SOILS MAP

Soil Map—El Paso County Area, Colorado (BTR Storage)



Soil Map may not be valid at this scale.



**Natural Resources
Conservation Service**

Web Soil Survey
National Cooperative Soil Survey

2/15/2023
Page 1 of 3

MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils



Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 20, Sep 2, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Oct 20, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	38.7	100.0%
Totals for Area of Interest		38.7	100.0%

El Paso County Area, Colorado

56—Nelson-Tassel fine sandy loams, 3 to 18 percent slopes

Map Unit Setting

National map unit symbol: 3690

Elevation: 5,600 to 6,400 feet

Mean annual precipitation: 12 to 14 inches

Mean annual air temperature: 48 to 52 degrees F

Frost-free period: 135 to 155 days

Farmland classification: Not prime farmland

Map Unit Composition

Nelson and similar soils: 55 percent

Tassel and similar soils: 40 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Nelson

Setting

Landform: Hills

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Calcareous residuum weathered from interbedded sedimentary rock

Typical profile

A - 0 to 5 inches: fine sandy loam

Ck - 5 to 23 inches: fine sandy loam

Cr - 23 to 27 inches: weathered bedrock

Properties and qualities

Slope: 3 to 12 percent

Depth to restrictive feature: 20 to 40 inches to paralithic bedrock

Drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water

(Ksat): Moderately low to high (0.06 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 10 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Very low (about 2.8 inches)

Interpretive groups

Land capability classification (irrigated): 4e

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: B

Ecological site: R067BY045CO - Shaly Plains

Other vegetative classification: SHALY PLAINS (069AY046CO)

Hydric soil rating: No

Description of Tassel

Setting

Landform: Hills

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Calcareous slope alluvium over residuum
weathered from sandstone

Typical profile

A - 0 to 4 inches: fine sandy loam

C - 4 to 10 inches: fine sandy loam

Cr - 10 to 14 inches: weathered bedrock

Properties and qualities

Slope: 3 to 18 percent

Depth to restrictive feature: 6 to 20 inches to paralithic bedrock

Drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water

(Ksat): Moderately high (0.20 to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 10 percent

Available water supply, 0 to 60 inches: Very low (about 1.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: R067BY045CO - Shaly Plains

Other vegetative classification: SHALY PLAINS (069AY046CO)

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 4 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent

Landform: Depressions

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 20, Sep 2, 2022

FEMA FIRM MAP

HYDROLOGIC CALCULATIONS

ABTR STORAGE
AREA RUNOFF COEFFICIENT (C) SUMMARY

EXISTING

		<i>DEVELOPED / IMPERVIOUS</i>			<i>UNDEVELOPED / NON-IMPERVIOUS</i>			<i>WEIGHTED</i>		<i>WEIGHTED CA</i>	
BASIN	TOTAL AREA	AREA	C5	C100	AREA	C5	C100	C5	C100	CA5	CA100
	<i>(Acres)</i>	<i>(Acres)</i>			<i>(Acres)</i>						
<i>OS-X</i>	7.12	0.14	0.90	0.96	6.98	0.08	0.35	0.10	0.36	0.68	2.58
<i>OS-Y</i>	21.40	1.71	0.90	0.96	19.69	0.08	0.35	0.15	0.40	3.11	8.53
<i>OS-Z</i>	1.84	0.74	0.90	0.96	1.10	0.08	0.35	0.41	0.60	0.75	1.10
<i>EX-A</i>	13.40	0.27	0.90	0.96	13.13	0.08	0.35	0.10	0.36	1.29	4.85
<i>EX-B</i>	1.96	0.04	0.90	0.96	1.92	0.08	0.35	0.10	0.36	0.19	0.71
<i>EX-C</i>	23.20	0.46	0.90	0.96	22.74	0.08	0.35	0.10	0.36	2.23	8.40

DEVELOPED

		<i>DEVELOPED / IMPERVIOUS</i>			<i>UNDEVELOPED / NON-IMPERVIOUS</i>			<i>WEIGHTED</i>		<i>WEIGHTED CA</i>	
BASIN	TOTAL AREA	AREA	C5	C100	AREA	C5	C100	C5	C100	CA5	CA100
	<i>(Acres)</i>	<i>(Acres)</i>			<i>(Acres)</i>						
<i>EX-B</i>	1.96	0.04	0.90	0.96	1.92	0.08	0.35	0.10	0.36	0.19	0.71
<i>PR-1</i>	9.92	3.97	0.90	0.96	5.95	0.08	0.35	0.41	0.59	4.05	5.89
<i>PR-2</i>	9.30	3.72	0.90	0.96	5.58	0.08	0.35	0.41	0.59	3.79	5.52
<i>PR-3</i>	8.78	8.34	0.90	0.96	0.44	0.08	0.35	0.86	0.93	7.54	8.16
<i>PR-4</i>	3.27	0.07	0.90	0.96	3.20	0.08	0.35	0.10	0.36	0.32	1.19
<i>PR-5</i>	1.78	0.18	0.90	0.96	1.60	0.08	0.35	0.16	0.41	0.29	0.73
<i>PR-6</i>	0.42	0.01	0.90	0.96	0.41	0.08	0.35	0.10	0.36	0.04	0.15
<i>PR-7</i>	3.03	0.30	0.90	0.96	2.73	0.08	0.35	0.16	0.41	0.49	1.24

Calculated by: DLF
Date: 2/20/2023
Checked by: _____

ABTR STORAGE RUNOFF SUMMARY

EXISTING

BASIN	AREA TOTAL (Acres)	WEIGHTED		OVERLAND				STREET / CHANNEL FLOW				T _c	INTENSITY		TOTAL FLOWS	
		C ₅	C ₁₀₀	C ₅	Length	Slope	T _t	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀
		* For Calcs See Runoff Summary			(ft)	(ft/ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
<i>OS-X</i>	7.12	0.10	0.36	0.10	300	0.08	15.8	300	8%	1.4	3.5	19.3	3.1	5.2	2.1	13.4
<i>OS-Y</i>	21.40	0.15	0.40	0.15	300	0.06	16.5	1000	6%	1.2	13.6	30.1	2.5	4.0	7.7	34.5
<i>OS-Z</i>	1.84	0.41	0.60	0.41	30	0.10	3.2	400	4%	1.0	6.7	9.9	4.1	7.1	3.1	7.8
<i>EX-A</i>	13.40	0.10	0.36	0.10	300	0.04	19.9	700	4%	1.0	11.7	31.5	2.4	3.9	3.1	19.1
<i>EX-B</i>	1.96	0.10	0.36	0.10	300	0.07	16.5	0	7%	1.3	0.0	16.5	3.3	5.6	0.6	4.0
<i>EX-C</i>	23.20	0.10	0.36	0.10	300	0.04	19.9	1000	4%	1.0	16.7	36.5	2.2	3.6	5.0	30.2

DEVELOPED

BASIN	AREA TOTAL (Acres)	WEIGHTED		OVERLAND				STREET / CHANNEL FLOW				T _c	INTENSITY		TOTAL FLOWS	
		C ₅	C ₁₀₀	C ₅	Length	Slope	T _t	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀
		* For Calcs See Runoff Summary			(ft)	(ft/ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
<i>OS-X</i>	7.12	0.10	0.36	0.10	300	0.08	15.8	300	8%	1.4	3.5	19.3	3.1	5.2	2.1	13.4
<i>OS-Y</i>	21.40	0.15	0.40	0.15	300	0.06	16.5	1000	6%	1.2	13.6	30.1	2.5	4.0	7.7	34.5
<i>OS-Z</i>	1.84	0.41	0.60	0.41	30	0.10	3.2	400	4%	1.0	6.7	9.9	4.1	7.1	3.1	7.8
<i>EX-B</i>	1.96	0.10	0.36	0.10	300	0.07	16.5	0	7%	1.3	0.0	16.5	3.3	5.6	0.6	4.0
<i>PR-1</i>	9.92	0.41	0.59	0.41	300	0.04	13.7	600	4.0%	1.0	10.0	23.7	2.8	4.6	11.4	27.3
<i>PR-2</i>	9.30	0.41	0.59	0.41	300	0.04	13.7	600	4.0%	1.0	10.0	23.7	2.8	4.6	10.6	25.6
<i>PR-3</i>	8.78	0.86	0.93	0.86	300	0.04	4.8	800	4.0%	4.0	3.3	8.1	4.4	7.7	32.9	62.8
<i>PR-4</i>	3.27	0.10	0.36	0.10	300	0.10	14.7	0	10.0%	1.6	0.0	14.7	3.5	6.0	1.1	7.1
<i>PR-5</i>	1.78	0.16	0.41	0.16	300	0.10	13.7	0	10.0%	1.6	0.0	13.7	3.6	6.2	1.0	4.5
<i>PR-6</i>	0.42	0.10	0.36	0.10	20	0.05	4.7	400	5.0%	1.1	6.0	10.7	4.0	6.9	0.2	1.1
<i>PR-7</i>	3.03	0.16	0.41	0.16	200	0.08	12.1	0	8.0%	1.4	0.0	12.1	3.8	6.5	1.9	8.1

Note: Basin PR-3 is shown for the future commercial conditions.

Calculated by: DLF

Date: 2/20/2023

Checked by: _____

ABTR STORAGE SURFACE ROUTING SUMMARY

<i>Design Point(s)</i>	<i>Contributing Basins</i>	<i>Area (ac)</i>	<i>Flow (cfs)</i>	
			<i>Q₅</i>	<i>Q₁₀₀</i>
A	EX-A, OS-X	20.52	5.2	32.4
B	EX-B	1.96	0.6	4.0
C	EX-C, OS-Y	44.60	12.7	64.7
1	PR-1	9.92	11.4	27.3
2	PR-2	9.30	10.6	25.6
3	PR-3	8.78	32.9	62.8
4	PR-4, PR-3, PR-2	21.35	44.7	95.5
5	PR-5, NW EDB Outfall	1.78	4.6	34.4
6	PR-6	0.42	0.2	1.1
7	PR-7	3.03	1.9	8.1
51	PR-5, NW EDB Outfall, OS-Y, OS-Z	25.02	15.4	76.7
52	PR-6, OS-X	7.54	2.3	14.4

Calculated by: DLF

Date: 2/20/2023

Checked by: _____

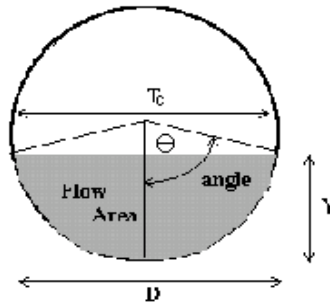
HYDRAULIC CALCULATIONS

CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

MHFD-Culvert, Version 4.00 (May 2020)

Project: **ABTR Storage**

Pipe ID: **Existing Road Culvert**



Design Information (Input)		
Pipe Invert Slope	So =	0.0270 ft/ft
Pipe Manning's n-value	n =	0.0220 *
Pipe Diameter	D =	54.00 inches
Design discharge	Q =	68.90 cfs
Full-Flow Capacity (Calculated)		
Full-flow area	Af =	15.90 sq ft
Full-flow wetted perimeter	Pf =	14.14 ft
Half Central Angle	Theta =	3.14 radians
Full-flow capacity	Qf =	191.45 cfs
Calculation of Normal Flow Condition		
Half Central Angle ($0 < \theta < 3.14$)	Theta =	1.40 radians
Flow area	An =	6.23 sq ft
Top width	Tn =	4.43 ft
Wetted perimeter	Pn =	6.30 ft
Flow depth	Yn =	1.87 ft
Flow velocity	Vn =	11.05 fps
Discharge	Qn =	68.90 cfs
Percent of Full Flow	Flow =	36.0% of full flow
Normal Depth Froude Number	Fr _n =	1.64 supercritical
Calculation of Critical Flow Condition		
Half Central Angle ($0 < \theta < 3.14$)	Theta-c =	1.65 radians
Critical flow area	Ac =	8.71 sq ft
Critical top width	Tc =	4.49 ft
Critical flow depth	Yc =	2.42 ft
Critical flow velocity	Vc =	7.91 fps
Critical Depth Froude Number	Fr _c =	1.00

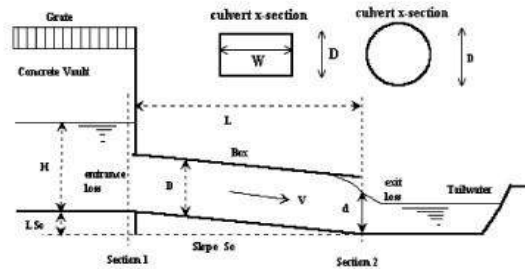
* Unexpected value for Manning's n

CULVERT SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

MHFD-Culvert, Version 4.00 (May 2020)

Project: **ABTR Storage**

ID: **Existing Road Culvert**



Design Information (Input):

Circular Culvert: Barrel Diameter in Inches
Inlet Edge Type (Choose from pull-down list)

D = 54 inches
Grooved Edge Projecting

OR:

Box Culvert: Barrel Height (Rise) in Feet
Barrel Width (Span) in Feet
Inlet Edge Type (Choose from pull-down list)

H (Rise) = ft
W (Span) = ft

Number of Barrels
Inlet Elevation at Culvert Invert
Outlet Elevation **OR** Slope
Culvert Length
Manning's Roughness
Bend Loss Coefficient
Exit Loss Coefficient

Barrels = 1
Elev IN = 6218 ft
Elev OUT = 6216 ft
L = 75 ft
n = 0.022 **For concrete, typically <= 0.016**
K_b = 0
K_e = 1

Design Information (calculated):

Entrance Loss Coefficient
Friction Loss Coefficient
Sum of All Loss Coefficients
Minimum Energy Condition Coefficient
Orifice Inlet Condition Coefficient

K_e = 0.20
K_f = 0.90
K_s = 2.10
K_{E_{low}} = -0.0693
C_d = 0.67

Calculations of Culvert Capacity (output):

Backwater calculations required to obtain Outlet Control Flowrate when H_{W0} < 0.75 * Culvert Rise

Headwater Surface Elevation (ft)	Tailwater Surface Elevation (ft)	Inlet Control Equation Used	Inlet Control Flowrate (cfs)	Outlet Control Flowrate (cfs)	Controlling Culvert Flowrate (cfs)	Flow Control Used
6218.00		No Flow (WS < inlet)	0.00	0.00	0.00	N/A
6218.25		Min. Energy. Eqn.	0.41	#N/A	#N/A	#N/A
6218.50		Min. Energy. Eqn.	1.52	#N/A	#N/A	#N/A
6218.75		Min. Energy. Eqn.	3.55	#N/A	#N/A	#N/A
6219.00		Min. Energy. Eqn.	7.24	#N/A	#N/A	#N/A
6219.25		Min. Energy. Eqn.	11.16	#N/A	#N/A	#N/A
6219.50		Min. Energy. Eqn.	15.84	#N/A	#N/A	#N/A
6219.75		Min. Energy. Eqn.	21.23	#N/A	#N/A	#N/A
6220.00		Min. Energy. Eqn.	27.31	#N/A	#N/A	#N/A
6220.25		Min. Energy. Eqn.	34.02	#N/A	#N/A	#N/A
6220.50		Regression Eqn.	40.41	#N/A	#N/A	#N/A
6220.75		Regression Eqn.	47.34	#N/A	#N/A	#N/A
6221.00		Regression Eqn.	54.87	#N/A	#N/A	#N/A
6221.25		Regression Eqn.	62.98	#N/A	#N/A	#N/A
6221.50		Regression Eqn.	71.61	114.16	71.61	INLET
6221.75		Regression Eqn.	80.56	120.86	80.56	INLET
6222.00		Regression Eqn.	89.71	127.33	89.71	INLET
6222.25		Regression Eqn.	98.82	133.62	98.82	INLET
6222.50		Regression Eqn.	107.74	139.65	107.74	INLET
6222.75		Regression Eqn.	116.35	145.52	116.35	INLET
6223.00		Regression Eqn.	124.61	151.24	124.61	INLET
6223.25		Regression Eqn.	132.42	156.80	132.42	INLET
6223.50		Regression Eqn.	139.91	162.22	139.91	INLET
6223.75		Regression Eqn.	147.01	167.47	147.01	INLET
6224.00		Regression Eqn.	153.74	172.63	153.74	INLET
6224.25		Regression Eqn.	160.21	177.69	160.21	INLET
6224.50		Regression Eqn.	166.41	182.59	166.41	INLET
6224.75		Regression Eqn.	172.33	187.45	172.33	INLET
6225.00		Regression Eqn.	178.05	192.20	178.05	INLET
6225.25		Regression Eqn.	183.57	196.82	183.57	INLET

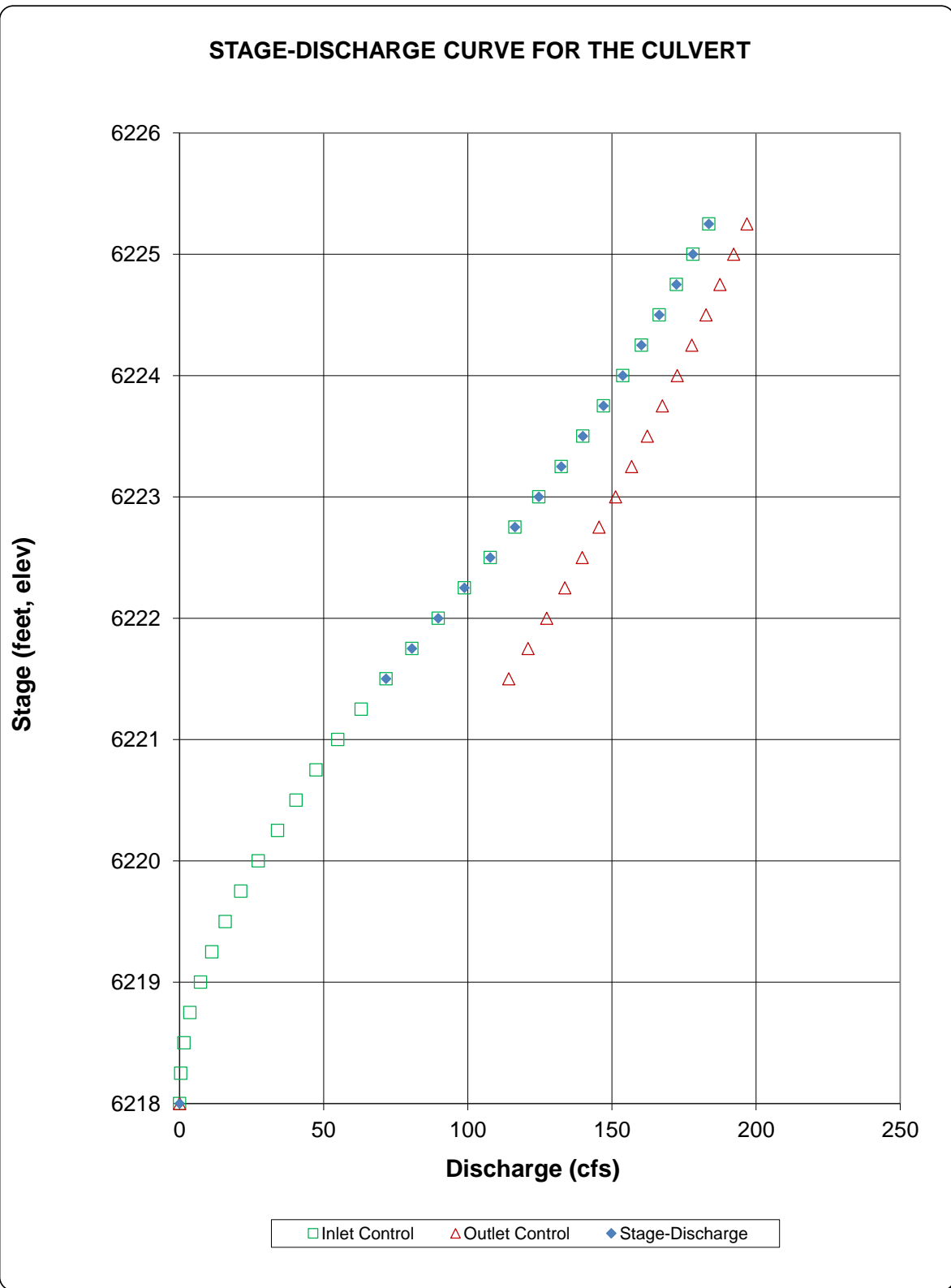
Processing Time: **00.30 Seconds**

CULVERT SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

MHFD-Culvert, Version 4.00 (May 2020)

Project: **ABTR Storage**

ID: **Existing Road Culvert**

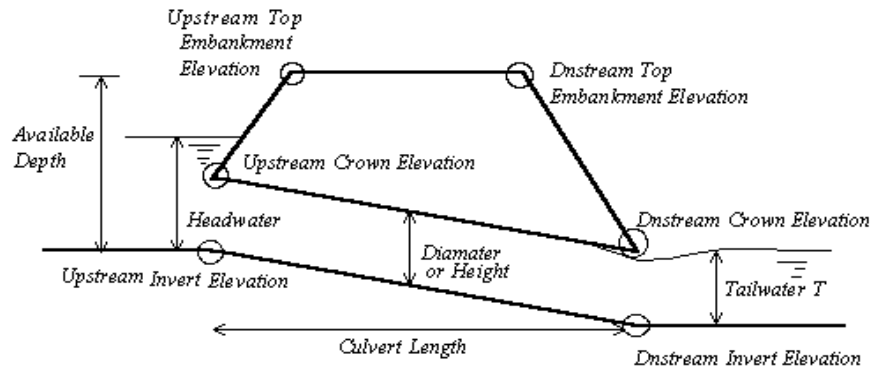


VERTICAL PROFILE FOR THE CULVERT

MHFD-Culvert, Version 4.00 (May 2020)

Project = **ABTR Storage**

ID = **Existing Road Culvert**



Culvert Information (Input)

Barrel Diameter or Height	D or H =	54.00	inches
Barrel Length	L =	75.00	ft
Barrel Invert Slope	So =	0.0270	ft/ft
Downstream Invert Elevation	EDI =	6216.00	ft
Downstream Top Embankment Elevation	EDT =	6225.00	ft
Upstream Top Embankment Elevation	EUT =	6225.00	ft
Design Headwater Depth (not elev.)	Hw =	4.00	ft
Tailwater Depth (not elev.)	Yt =	1.40	ft

Culvert Hydraulics (Calculated)

Available Headwater Depth	HW-a =	6.98	ft
Design Hw/D ratio	Hw/D =	0.89	

Culvert Vertical Profile

Upstream Invert Elevation	EUI =	6218.03	ft
Upstream Crown Elevation	EUC =	6222.53	ft
Upstream Soil Cover Depth	Upsoil =	2.48	ft
Downstream Crown Elevation	EDC =	6220.50	ft
Downstream Soil Cover Depth	Dnsoil =	4.50	ft

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **ABTR Storage**

Location: **SE Diversion Swale - E PL (need Q=13.4 cfs)**

By: **Dane Frank**

Date: **2/20/2023**

Chk By:

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

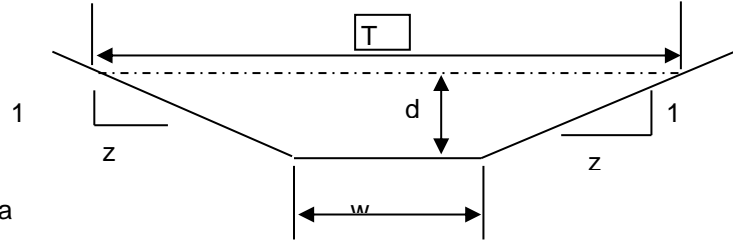
$$R = A/P$$

A = cross sectional area

P = wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 4
z (sideslope)= 4
b (btm width, ft)= 2
d (depth, ft)= 0.88
S (slope, ft/ft) 0.01
n low = 0.035
n high = 0.035

Clear Data
Entry Cells

		Low N		High N			
Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs
0.88	4.86	9.26	0.52	2.76218569	13.4176	2.762186	13.4176
				T =		9.04	
				Dm =		0.537	
				Sc low =		0.0226	
				Sc high =		0.0226	
				.7 Sc		1.3 Sc	
				0.0158		0.0294	

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: ABTR Storage **Location:** SE Conveyance Swale - S PL (need Q=13.4 cfs)
By: Dane Frank **Date:** 2/20/2023
Chk By: **Date:** version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

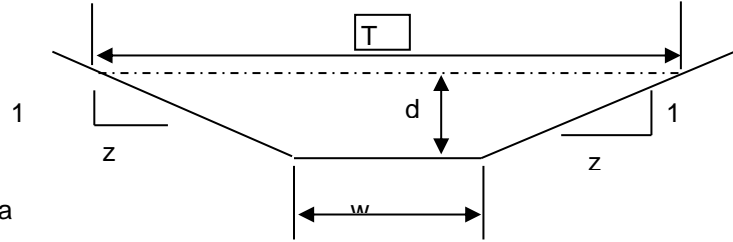
$$R = A/P$$

A = cross sectional area

P = wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 4
z (sideslope)= 4
b (btm width, ft)= 2
d (depth, ft)= 0.64
S (slope, ft/ft) 0.04
n low = 0.035
n high = 0.035

Clear Data
Entry Cells

		Low N		High N			
Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs
0.64	2.92	7.28	0.40	4.61749332	13.4757	4.617493	13.4757
				T =		7.12	
				Dm =		0.410	
				Sc low =		0.0247	
				Sc high =		0.0247	
				.7 Sc		1.3 Sc	
				0.0173		0.0321	

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: ABTR Storage

By: Dane Frank

Chk By:

Location: NE Diversion Swale - E PL (need Q=34.5 cfs)

Date: 2/20/2023

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

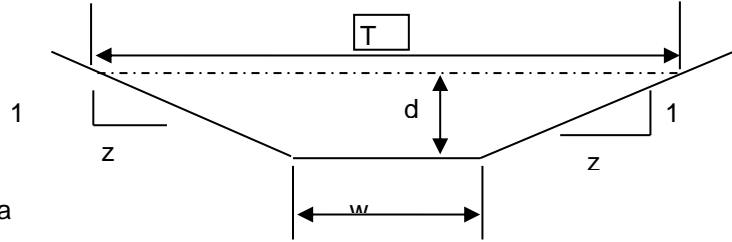
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 4
z (sideslope)= 4
b (btm width, ft)= 2
d (depth, ft)= 0.9
S (slope, ft/ft) 0.06
n low = 0.035
n high = 0.035

Clear Data
Entry Cells

				Low N		High N			
Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.9	5.04	9.42	0.53	6.85311816	34.5397	6.853118	34.5397	T =	9.2
				Sc low =		Sc high =		Dm =	0.548
				.7 Sc		.7 Sc			
				0.0158		0.0158			
				1.3 Sc		1.3 Sc			
				0.0293		0.0293			

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **ABTR Storage**

By: **Dane Frank**

Chk By:

Location: **Highway 94 Swale (need Q=7.8 cfs)**

Date: **2/20/2023**

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

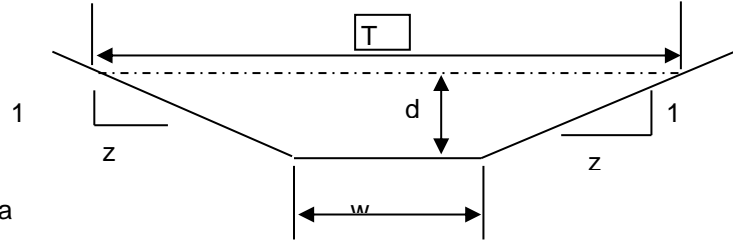
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 5
z (sideslope)= 5
b (btm width, ft)= 2
d (depth, ft)= 0.47
S (slope, ft/ft) 0.04
n low = 0.035
n high = 0.035

Clear Data
Entry Cells

		Low N		High N			
Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs
0.47	2.04	6.79	0.30	3.81338253	7.79646	3.813383	7.79646
				T =		6.7	
				Dm =		0.305	
				Sc low =		0.0270	
				Sc high =		0.0270	
				.7 Sc		1.3 Sc	
				0.0189		0.0351	

s_c = critical slope ft / ft

T = top width of the stream

d_m = a/T = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION FOR PIPE FLOW

Project: ABTR Storage Location: NE Div Swale Drain Pipe (need Q=34.5 cfs)
 By: dane Frank Date:
 Chk. By: Date: mdo version 12.8.00

Clear Data
Entry Cells

INPUT

D= 24 inches
 d= 24 inches
 n= 0.012 mannings coeff
 θ= 0.0 degrees
 S= 0.03 slope in/in

Mannings Formula

$$Q=(1.486/n)AR_h^{2/3}S^{1/2}$$

$$R=A/P$$

A=cross sectional area

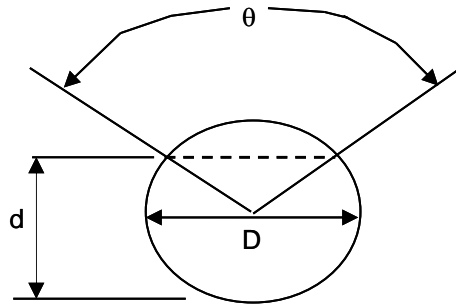
P=wetted perimeter

S=slope of channel

n=Manning's roughness coefficient

$$V=(1.49/n)R_h^{2/3}S^{1/2}$$

$$Q=V \times A$$



			Solution to Mannings Equation		Manning's n-values	
Area,ft ²	Wetted Perimeter, ft	Hydraulic Radius, ft	velocity ft/s	flow, cfs		
3.14	6.28	0.50	13.51	42.45	PVC	0.01
					PE (<9"dia)	0.015
					PE (>12"dia)	0.02
					PE(9-12"dia)	0.017
					CMP	0.025
					ADS N12	0.012
					HCMP	0.023
					Conc	0.013

Created by: Mike O'Shea

DETENTION CALCULATIONS

Design Procedure Form: Runoff Reduction

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 1

Designer: Dane Frank
Company: Terra Nova Engineering
Date: February 20, 2023
Project: ABTR Storage
Location: Southwest corner driveway and corner of parking area below SW EDB

SITE INFORMATION (User Input in Blue Cells)

WQCV Rainfall Depth 0.60 inches
 Depth of Average Runoff Producing Storm, d_6 = 0.43 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3)

Area Type	UIA:RPA												
Area ID	PR-7												
Downstream Design Point ID	7												
Downstream BMP Type	None												
DCIA (ft ²)	--												
UIA (ft ²)	910												
RPA (ft ²)	2,800												
SPA (ft ²)	--												
HSG A (%)	0%												
HSG B (%)	100%												
HSG C/D (%)	0%												
Average Slope of RPA (ft/ft)	0.030												
UIA:RPA Interface Width (ft)	1200.00												

CALCULATED RUNOFF RESULTS

Area ID	PR-7												
UIA:RPA Area (ft ²)	3,710												
L / W Ratio	0.06												
UIA / Area	0.2453												
Runoff (in)	0.00												
Runoff (ft ³)	0												
Runoff Reduction (ft ³)	38												

CALCULATED WQCV RESULTS

Area ID	PR-7												
WQCV (ft ³)	38												
WQCV Reduction (ft ³)	38												
WQCV Reduction (%)	100%												
Untreated WQCV (ft ³)	0												

CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID)

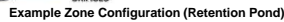
Downstream Design Point ID	7												
DCIA (ft ²)	0												
UIA (ft ²)	910												
RPA (ft ²)	2,800												
SPA (ft ²)	0												
Total Area (ft ²)	3,710												
Total Impervious Area (ft ²)	910												
WQCV (ft ³)	38												
WQCV Reduction (ft ³)	38												
WQCV Reduction (%)	100%												
Untreated WQCV (ft ³)	0												

CALCULATED SITE RESULTS (sums results from all columns in worksheet)

Total Area (ft ²)	3,710
Total Impervious Area (ft ²)	910
WQCV (ft ³)	38
WQCV Reduction (ft ³)	38
WQCV Reduction (%)	100%
Untreated WQCV (ft ³)	0

MHFD-Detention, Version 4.06 (July 2022)

Basin ID: Northwet EDB - North half of parking area + future commercial development along HWY 94



Initial Surcharge Area (A_{ISV}) =	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{TBD}) =	user	acre-feet

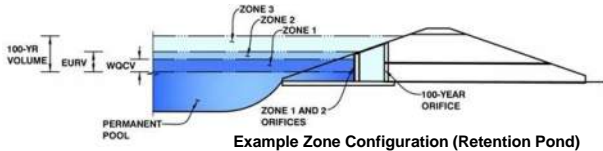
Optional User Overrides

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: **ABTR Storage**

Basin ID: **Northwet EDB - North half of parking area + future commercial development along HWY 94**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.54	0.421	Orifice Plate
Zone 2 (EURV)	5.04	0.972	Orifice Plate
Zone 3 (100-year)	6.86	0.901	Weir&Pipe (Restrict)
Total (all zones)		2.293	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-1/2 inches)

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	2.00	3.00	3.50			
Orifice Area (sq. inches)	1.74	1.74	1.74	1.74	1.74			

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, H_o = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Grate Slope = H:V
Horiz. Length of Weir Sides = feet
Overflow Grate Type = %
Debris Clogging % = %

Calculated Parameters for Overflow Weir
Height of Grate Upper Edge, H_u = feet
Overflow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area = ft²
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter = inches
Restrictor Plate Height Above Pipe Invert = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres
Basin Volume at Top of Freeboard = acre-ft

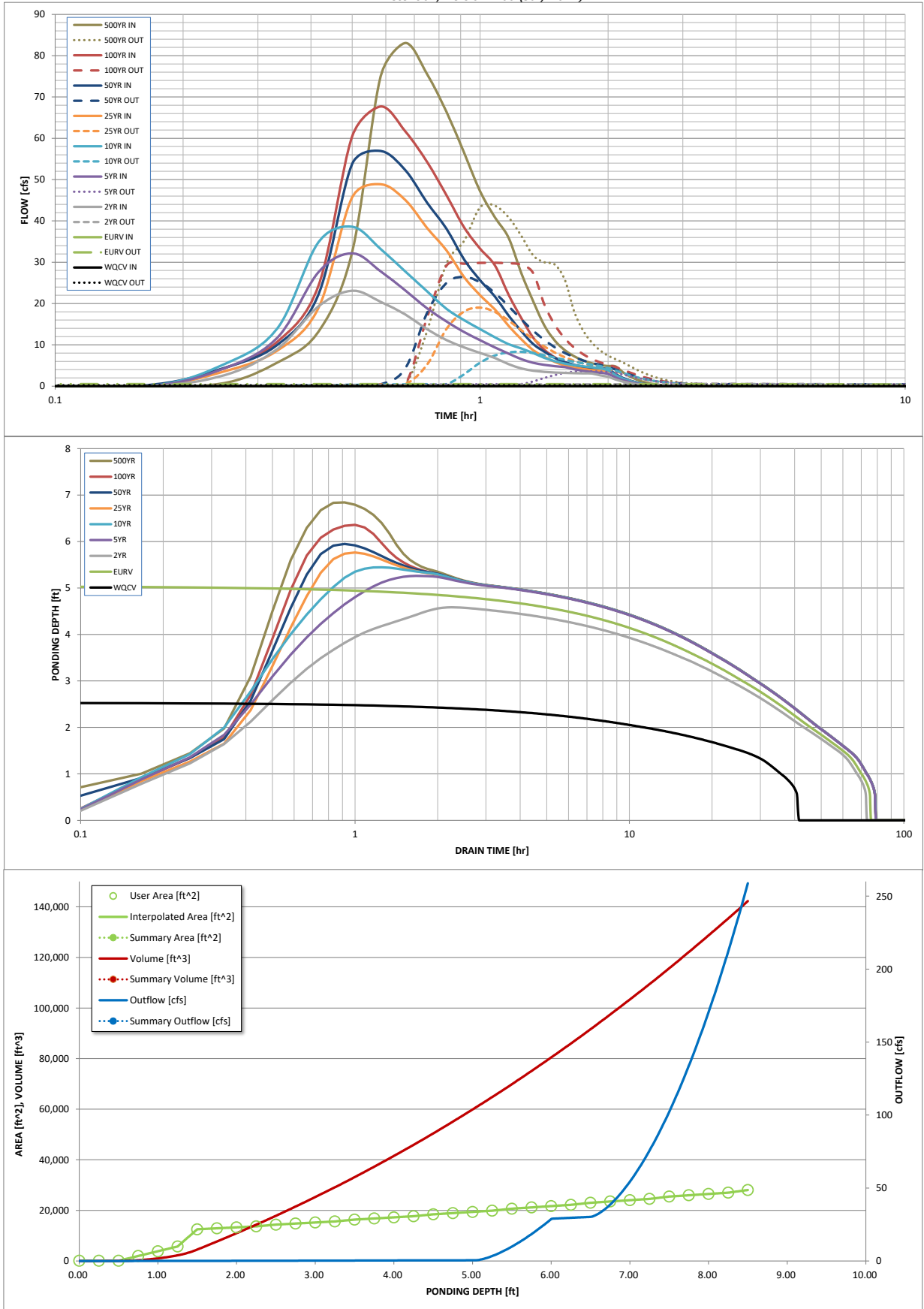
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.00
One-Hour Rainfall Depth (in) =	0.421	1.393	1.262	1.743	2.156	2.680	3.122	3.666	4.535
CUHP Runoff Volume (acre-ft) =	N/A	N/A	1.262	1.743	2.156	2.680	3.122	3.666	4.535
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.6	7.2	10.9	19.2	24.2	30.2	39.4
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.34	0.51	0.90	1.13	1.41	1.84
Peak Inflow Q (cfs) =	N/A	N/A	23.1	32.2	38.6	48.9	56.9	67.7	83.1
Peak Outflow Q (cfs) =	0.2	0.5	0.5	3.6	8.3	19.0	26.4	29.9	43.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.8	1.0	1.1	1.0	1.1
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	0.00	N/A	0.2	0.5	1.2	1.6	1.9	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	67	65	69	68	66	64	63	60
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	75	74	73	72	71	70
Maximum Ponding Depth (ft) =	2.54	5.05	4.58	5.26	5.45	5.76	5.95	6.36	6.84
Area at Maximum Ponding Depth (acres) =	0.33	0.45	0.43	0.46	0.47	0.49	0.50	0.52	0.54
Maximum Volume Stored (acre-ft) =	0.424	1.397	1.192	1.492	1.576	1.729	1.818	2.025	2.285

DETENTION BASIN OUTLET STRUCTURE DESIGN

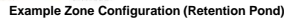
MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

MHFD-Detention, Version 4.06 (July 2022)

Basin ID: Northwet EDB - North half of parking area (no future commercial)



Initial Surcharge Area (A_{ISV}) =	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{TOTAL}) =	user	acre-feet

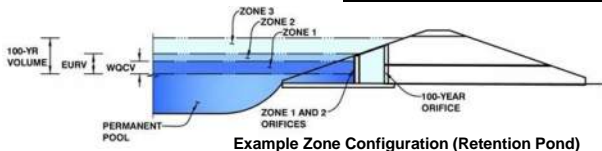
[illegible]

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: **ABTR Storage**

Basin ID: **Northwet EDB - North half of parking area (no future commercial)**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.85	0.206	Orifice Plate
Zone 2 (EURV)	2.55	0.219	Orifice Plate
Zone 3 (100-year)	4.42	0.697	Weir&Pipe (Restrict)
Total (all zones)		1.122	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 15/16 inch)

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	<input type="text" value="0.00"/>	<input type="text" value="0.50"/>	<input type="text" value="1.00"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
Orifice Area (sq. inches)	<input type="text" value="0.71"/>	<input type="text" value="0.71"/>	<input type="text" value="0.71"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
Orifice Area (sq. inches)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, H_o = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Grate Slope = H:V
Horiz. Length of Weir Sides = feet
Overflow Grate Type =
Debris Clogging % = %

Calculated Parameters for Overflow Weir
Height of Grate Upper Edge, H_u = feet
Overflow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area =
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter = inches
Restrictor Plate Height Above Pipe Invert = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres
Basin Volume at Top of Freeboard = acre-ft

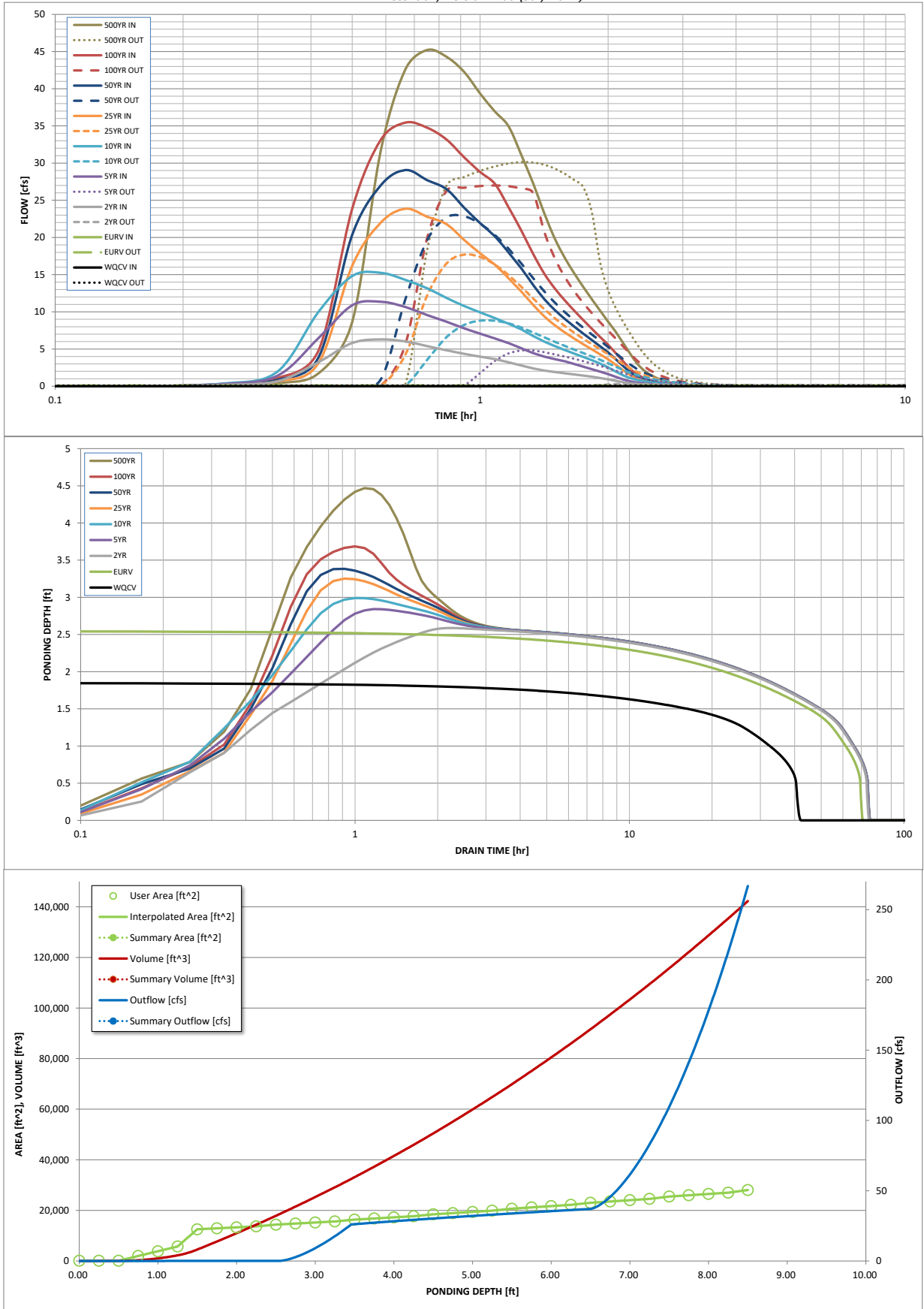
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.00
One-Hour Rainfall Depth (in) =	0.206	0.425	0.467	0.851	1.216	1.811	2.237	2.828	3.681
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.467	0.851	1.216	1.811	2.237	2.828	3.681
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.6	7.2	10.9	19.2	24.2	30.2	39.4
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.34	0.51	0.90	1.13	1.41	1.84
Peak Inflow Q (cfs) =	N/A	N/A	6.3	11.4	15.3	23.9	29.1	35.4	45.2
Peak Outflow Q (cfs) =	0.1	0.1	0.3	4.8	8.8	17.7	22.9	27.0	30.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.7	0.8	0.9	0.9	0.9	0.8
Structure Controlling Flow =	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	0.02	0.3	0.6	1.1	1.4	1.7	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	65	68	65	63	59	56	53	49
Time to Drain 99% of Inflow Volume (hours) =	40	68	72	71	69	68	66	65	63
Maximum Ponding Depth (ft) =	1.85	2.55	2.59	2.84	2.99	3.25	3.38	3.69	4.47
Area at Maximum Ponding Depth (acres) =	0.30	0.33	0.33	0.34	0.35	0.36	0.37	0.38	0.42
Maximum Volume Stored (acre-ft) =	0.207	0.427	0.437	0.525	0.573	0.669	0.716	0.829	1.141

DETENTION BASIN OUTLET STRUCTURE DESIGN

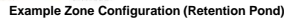
MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

MHFD-Detention, Version 4.06 (July 2022)

Basin ID: Southwest EDB (south half of parking area)



Initial Surcharge Area (A_{ISV})	=	user	ft ²
Surcharge Volume Length (L_{ISV})	=	user	ft
Surcharge Volume Width (W_{ISV})	=	user	ft
Depth of Basin Floor (H_{FLOOR})	=	user	ft
Length of Basin Floor (L_{FLOOR})	=	user	ft
Width of Basin Floor (W_{FLOOR})	=	user	ft
Area of Basin Floor (A_{FLOOR})	=	user	ft ²
Volume of Basin Floor (V_{FLOOR})	=	user	ft ³
Depth of Main Basin (H_{MAIN})	=	user	ft
Length of Main Basin (L_{MAIN})	=	user	ft
Width of Main Basin (W_{MAIN})	=	user	ft
Area of Main Basin (A_{MAIN})	=	user	ft ²
Volume of Main Basin (V_{MAIN})	=	user	ft ³
Calculated Total Basin Volume (V_{TOTAL})	=	user	acre-feet

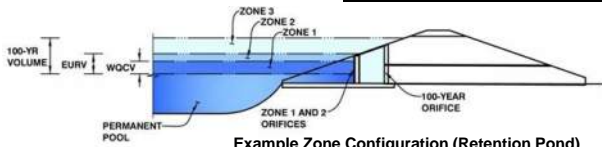
[illegible]

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: **ABTR Storage**

Basin ID: **Southwest EDB (south half of parking area)**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.83	0.149	Orifice Plate
Zone 2 (EURV)	3.11	0.268	Orifice Plate
Zone 3 (100-year)	4.55	0.377	Weir&Pipe (Restrict)
Total (all zones)		0.794	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1 inch)

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	2.00	2.50				
Orifice Area (sq. inches)	0.85	0.85	0.85	0.85				

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, H_o = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Grate Slope = H:V
Horiz. Length of Weir Sides = feet
Overflow Grate Type = %
Debris Clogging % = %

Calculated Parameters for Overflow Weir
Height of Grate Upper Edge, H_u = feet
Overflow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area = ft²
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter = inches
Restrictor Plate Height Above Pipe Invert = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres
Basin Volume at Top of Freeboard = acre-ft

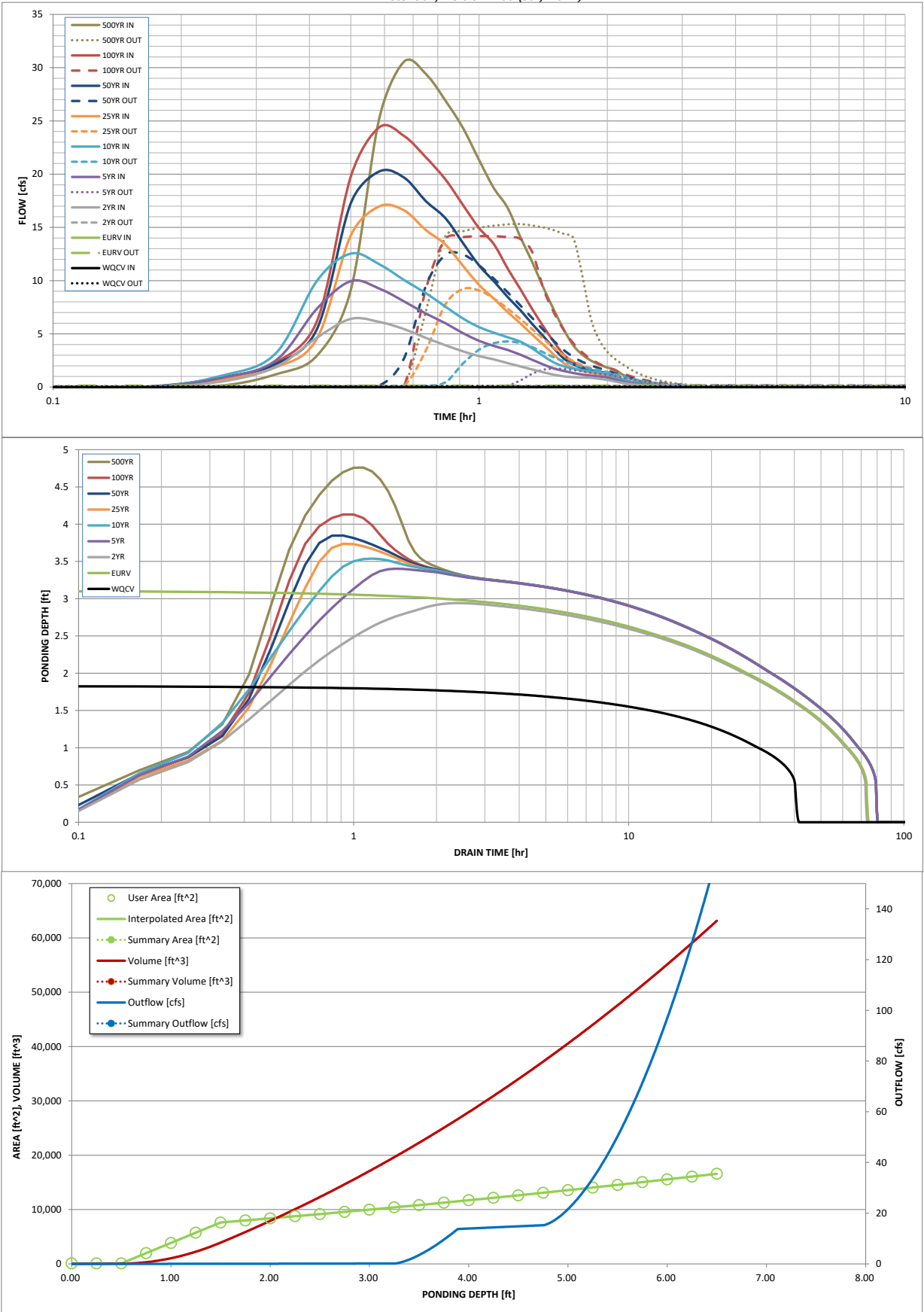
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.00
One-Hour Rainfall Depth (in) =	0.149	0.417	0.400	0.598	0.775	1.031	1.229	1.489	1.886
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.400	0.598	0.775	1.031	1.229	1.489	1.886
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.2	3.4	5.1	9.1	11.4	14.3	18.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.34	0.52	0.92	1.15	1.44	1.87
Peak Inflow Q (cfs) =	N/A	N/A	6.4	10.0	12.5	17.0	20.3	24.4	30.6
Peak Outflow Q (cfs) =	0.1	0.1	0.1	1.7	4.3	9.2	12.5	14.2	15.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.8	1.0	1.1	1.0	0.8
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.3	0.7	1.0	1.1	1.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	67	71	69	66	64	62	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	71	77	76	75	74	73	71
Maximum Ponding Depth (ft) =	1.83	3.11	2.94	3.40	3.54	3.74	3.85	4.13	4.76
Area at Maximum Ponding Depth (acres) =	0.19	0.23	0.23	0.24	0.25	0.26	0.26	0.27	0.30
Maximum Volume Stored (acre-ft) =	0.149	0.418	0.379	0.487	0.519	0.570	0.599	0.674	0.858

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

FORBAY VOLUMES

NW POND - SE FOREBAY - FORBAY VOLUME

Required Forbay Volume = Half of 3% of WQCV
WQCV = 0.421 ac-ft
WQCV = 18,339 cu-ft
Half of 3% of WQCV = 275 cu-ft

<i>ELEV</i>	<i>AREA</i>	<i>AREA AVG.</i>	<i>DELTA ELEV.</i>	<i>VOLUME</i>	<i>VOLUME TOTAL</i>
6223.00	200	200	1.50	300	
6224.50	200				300

Design Volume: 300 cu-ft
0.007 ac-ft

FORBAY VOLUMES

SW POND - FORBAY VOLUME

Required Forbay Volume = 2% of WQCV

WQCV = 0.149 ac-ft

WQCV = 6,490 cu-ft

2% of WQCV = 97 cu-ft

<i>ELEV</i>	<i>AREA</i>	<i>AREA AVG.</i>	<i>DELTA ELEV.</i>	<i>VOLUME</i>	<i>VOLUME TOTAL</i>
6237.00	157	157	1.50	236	
6238.50	157				236

Design Volume: 236 cu-ft
0.005 ac-ft

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **ABTR Storage**

By: **Dane Frank**

Chk By:

Location: **NW EDB - Forebay Notch - Q=35.4 cfs * 2% = 0.71 cfs**

Date: **2/22/2023**

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

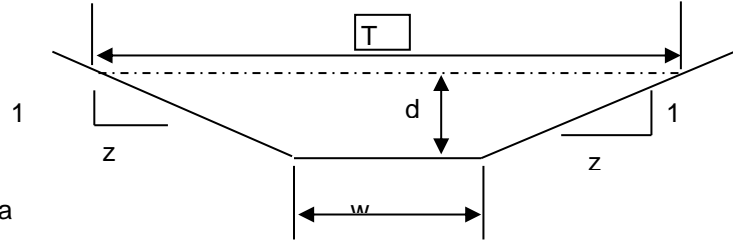
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
z (sideslope)= 0
b (btm width, ft)= 0.25
d (depth, ft)= 1.5
S (slope, ft/ft) 0.005
n low = 0.013
n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs	
1.5	0.38	3.25	0.12	1.91555431	0.71833	1.915554	0.71833	T = 0.25
				Sc low = 0.0657		Sc high = 0.0657		Dm = 1.500
				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc	
				0.0460	0.0854	0.0460	0.0854	

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **ABTR Storage**

By: **Dane Frank**

Chk By:

Location: **SW EDB Trickle Channels (need Q= 0.71 cfs)**

Date: **2/22/2023**

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

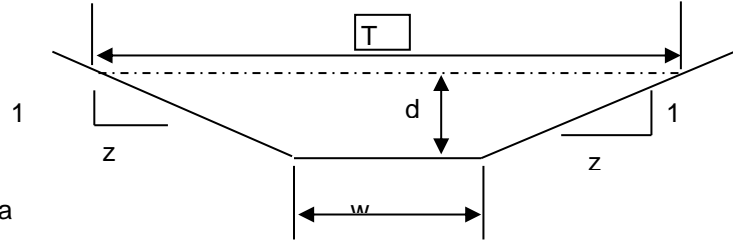
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
z (sideslope)= 0
b (btm width, ft)= 0.6
d (depth, ft)= 0.5
S (slope, ft/ft) 0.005
n low = 0.013
n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		T =	Dm =
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs		
0.5	0.30	1.60	0.19	2.64770995	0.79431	2.64771	0.79431	0.6	0.500
Sc low =				0.0115	Sc high =		0.0115		
s _c = critical slope				ft / ft					
T = top width of the stream				.7 Sc		1.3 Sc			
d _m = a/T = mean depth of flow				0.0080		0.0149			

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: ABTR Storage **Location:** SW EDB - Forebay Notch - $Q=22.4 \text{ cfs} \times 2\% = 0.45 \text{ cfs}$
By: Dane Frank **Date:** 2/22/2023
Chk By: **Date:** version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

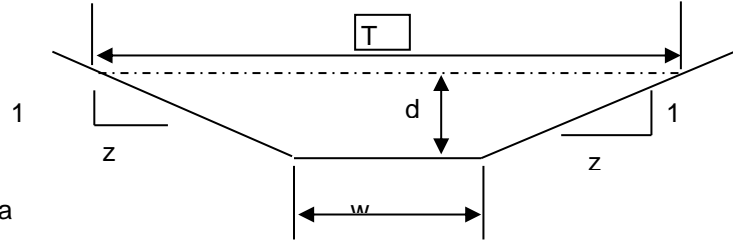
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
 z (sideslope)= 0
 b (btm width, ft)= 0.19
 d (depth, ft)= 1.5
 S (slope, ft/ft) 0.005
 n low = 0.013
 n high = 0.013

Clear Data
 Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs	
1.5	0.29	3.19	0.09	1.61520734	0.46033	1.615207	0.46033	T = 0.19
				Sc low = 0.0924		Sc high = 0.0924		Dm = 1.500
				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc	
				0.0647	0.1201	0.0647	0.1201	

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **ABTR Storage**

By: **Dane Frank**

Chk By:

Location: **SW EDB Trickle Channels (need Q= 0.45 cfs)**

Date: **2/22/2023**

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

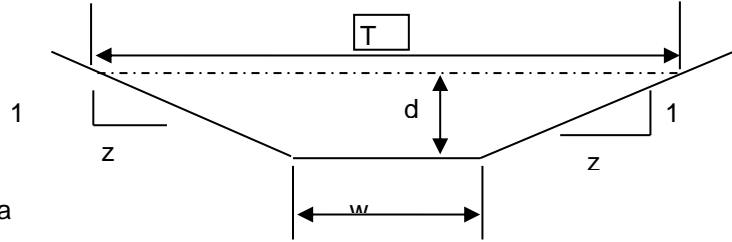
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
z (sideslope)= 0
b (btm width, ft)= 0.4
d (depth, ft)= 0.5
S (slope, ft/ft) 0.005
n low = 0.013
n high = 0.013

Clear Data
Entry Cells

Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Low N		High N		
				Velocity, fps	Flow, cfs	Velocity, fps	Flow, cfs	
0.5	0.20	1.40	0.14	2.20868406	0.44174	2.208684	0.44174	T = 0.4
				Sc low = 0.0165		Sc high = 0.0165		Dm = 0.500
				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc	
				0.0115	0.0214	0.0115	0.0214	

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

DRAINAGE MAPS

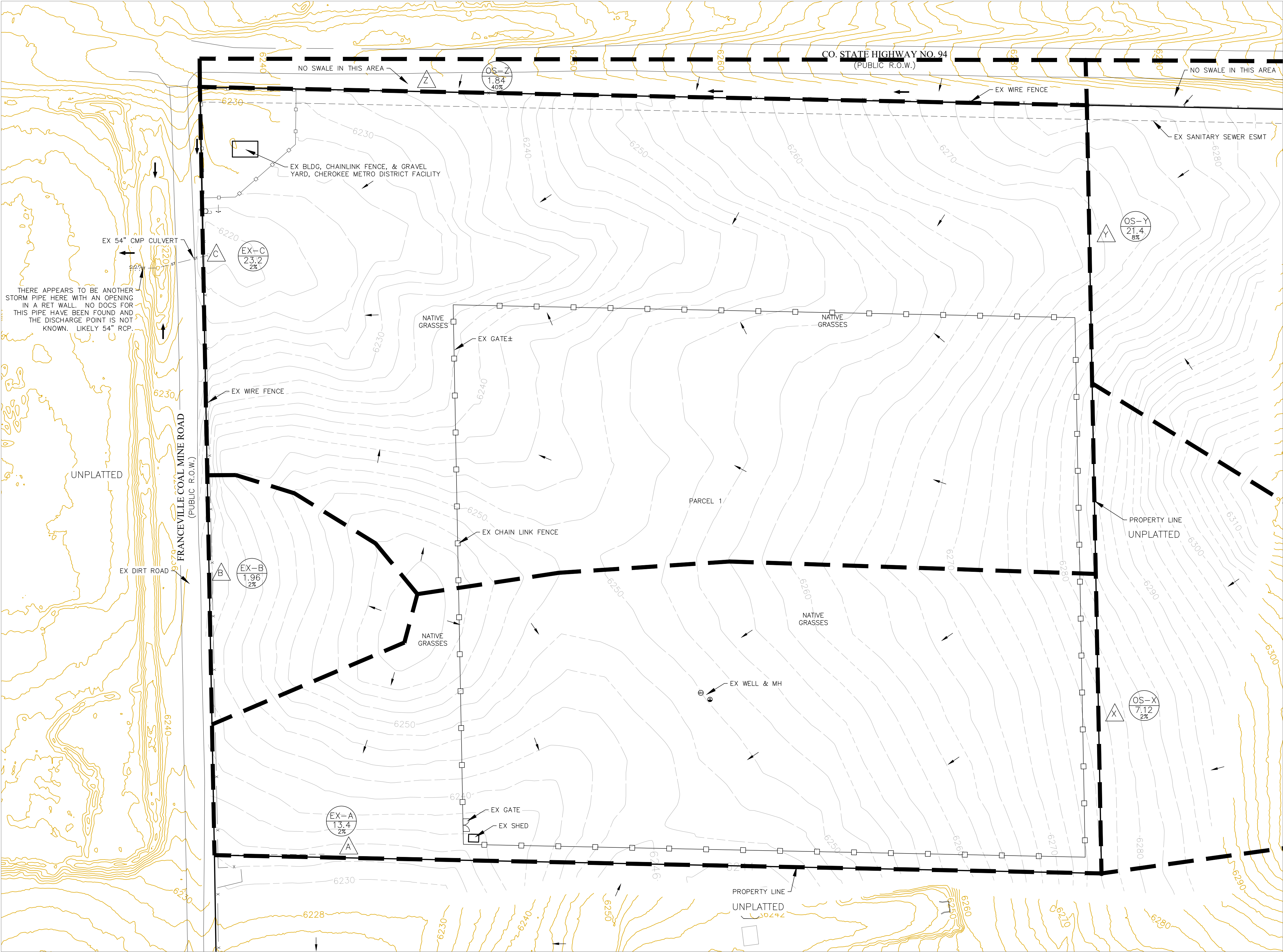
N:\jobs\2309.00\Drawings\230900 SDP.dwg, 3/8/2023 11:41:54 AM

ABTR STORAGE

SITE DEVELOPMENT PLAN

EXISTING DRAINAGE MAP

MARCH 2023



LEGEND

P-7

12.22

8%

12.22

8%

AREA IN BASIN (AC)

PERCENT IMPERVIOUS

D

DESIGN POINT

BASIN BOUNDARY

EXISTING 2' CONTOUR

GROUND SURFACE FLOW DIRECTION

ROAD AND DITCH FLOW DIRECTION

FENCE

EX

EXISTING

PR

PROPOSED

NOTES

1. ALL FEATURE SHOWN ARE EXISTING.
2. NO GRADING CHANGES ARE INCLUDED IN THIS PLAN.
3. BROWN GROUND SURFACE CONTOURS ARE LIDAR DATA DOWNLOADED FROM THE COLORADO HAZARD MAPPING & RISK MAP PORTAL. DATA SET: 2018 3DEP EAST CO EL PASO. THIS DATA IS APPROXIMATE. LIDAR DATA IS FROM 2018.

BASIN SUMMARY

BASIN	AREA TO TAL (acres)	TOTAL FLOWS	
		Qs (cfs)	Qout (cfs)
OS-X	7.12	2.1	13.4
OS-Y	21.40	7.7	34.5
OS-Z	1.84	3.1	7.8
EX-A	13.40	3.1	19.1
EX-B	1.96	0.6	4.0
EX-C	23.20	5.0	30.2

N

80'

0

80'

160'

SCALE: 1"=80'

DESIGNED BY DLF

DRAWN BY DLF

CHECKED BY LD

H-SCALE AS SHOWN

V-SCALE N/A

JOB NO. 2309.00

DATE ISSUED 03/07/23

SHEET NO. 1 OF 6

ABTR STORAGE

EXISTING DRAINAGE MAP

721 S. 23RD STREET

COLORADO SPRINGS, CO 80904

OFFICE: 719-635-6422

FAX: 719-635-6426

www.tnslinc.com

Terra Nova

Engineering, Inc.

Creative Civil Engineering

PREPARED FOR:

FLYING HORSE REALTY

ATTN: MIKE JACOBSON

2748 NORTH GATE BLVD

COLORADO SPRINGS, CO 80921

719.235.8195

UNITS SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE REVIEWING AGENCIES, TERRA NOVA ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT AND FOR THE PURPOSES SPECIFIED BY WRITTEN AUTHORIZATION.

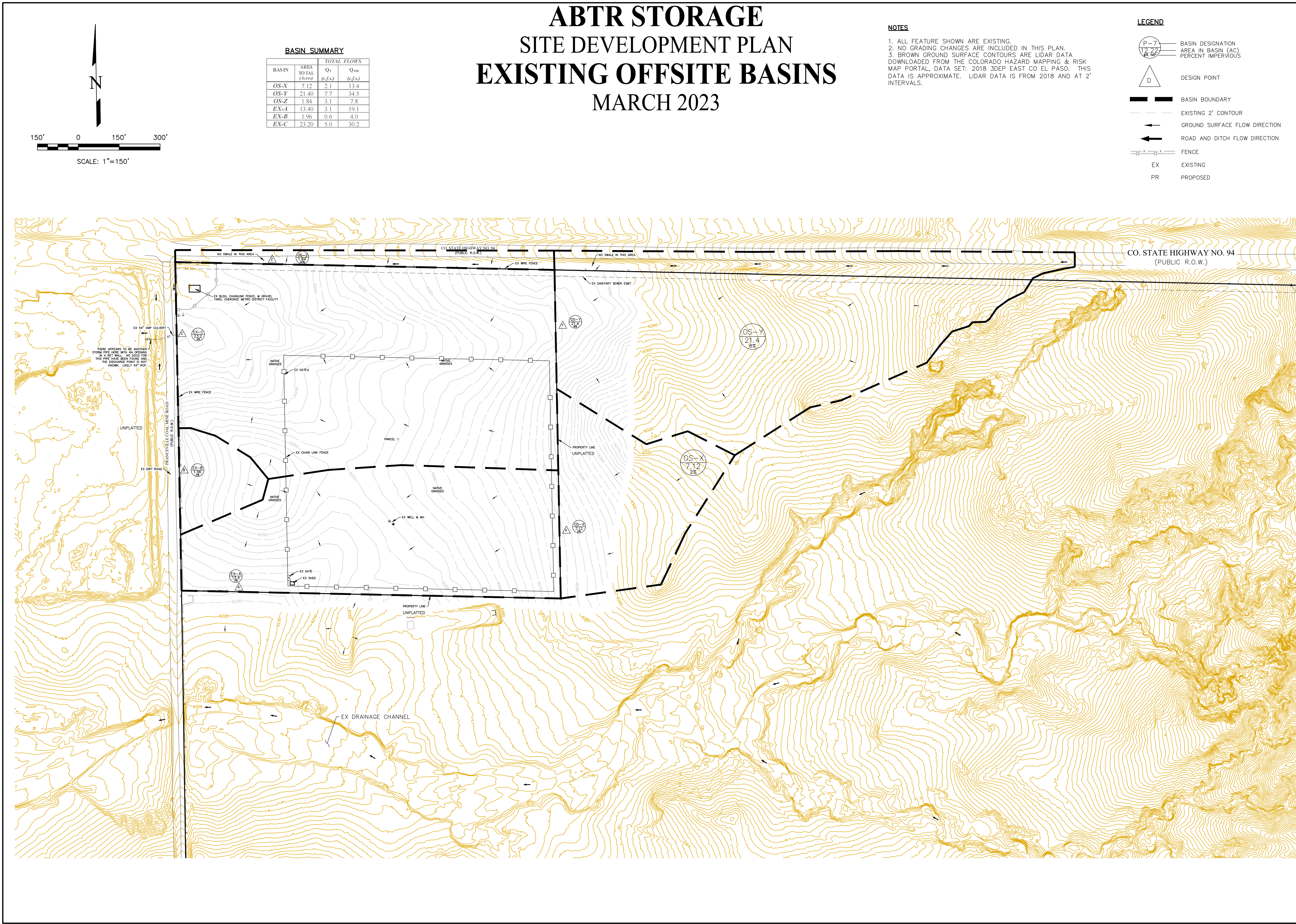
REVISIONS

NO.

DESCRIPTION

DATE

N:\jobs\2309.00\Drawings\230900 SDP.dwg, 3/8/2023 11:41:55 AM



REVISIONS	
NO.	DESCRIPTION

UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE COLORADO DEPARTMENT OF REVENUE ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT DESIGNATED BY THE PROJECT DESIGNER'S WRITTEN AUTHORIZATION.

PREPARED FOR:
FLYING HORSE REALTY
ATTN: MIKE JACOBSON
2748 NORTH GATE BLVD
COLORADO SPRINGS, CO 80921
719.235.8195

721 S. 23RD STREET
COLORADO SPRINGS, CO 80904
OFFICE: 719-635-6422
FAX: 719-635-6426
www.fhresinc.com

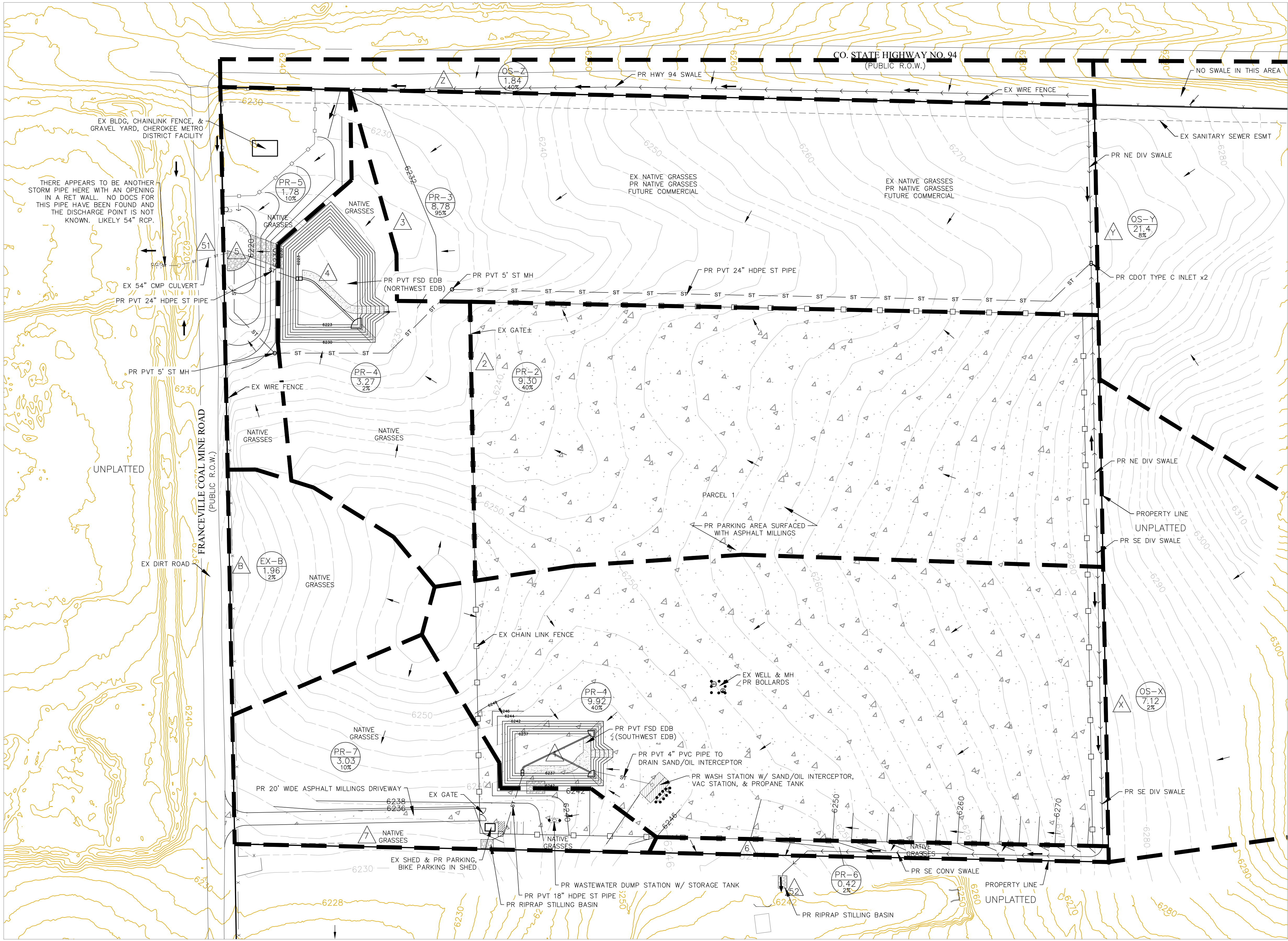
Terra Nova
Engineering, Inc.
Creative Civil Engineering

ABTR STORAGE

EXISTING OFFSITE BASINS

DESIGNED BY DLF
DRAWN BY DLF
CHECKED BY LD
H-SCALE AS SHOWN
V-SCALE N/A
JOB NO. 2309.00
DATE ISSUED 03/07/23
SHEET NO. 2 OF 6

ABTR STORAGE
SITE DEVELOPMENT PLAN
PROPOSED DRAINAGE MAP
MARCH 2023



LEGEND

- BASIN DESIGNATION
- AREA IN BASIN (AC)
- PERCENT IMPERVIOUS
- DESIGN POINT
- BASIN BOUNDARY
- EXISTING 2' CONTOUR
- GROUND SURFACE FLOW DIRECTION
- ROAD AND DITCH FLOW DIRECTION
- FENCE
- EX EXISTING
- PR PROPOSED

NOTES

1. BROWN GROUND SURFACE CONTOURS ARE LIDAR DATA DOWNLOADED FROM THE COLORADO HAZARD MAPPING & RISK MAP PORTAL, DATA SET: 2018 3DEP EAST CO EL PASO. THIS DATA IS APPROXIMATE. LIDAR DATA IS FROM 2018 AND AT 2' INTERVALS.

2. BASIN PR-3 PERCENT IMPERVIOUS IS BASED ON THE FUTURE COMMERCIAL DEVELOPED CONDITION SO THE NORTHWEST EDB COULD BE SIZED TO ACCOMMODATE THAT RUNOFF.

BASIN SUMMARY

BASIN	AREA TOTAL (Acres)	TOTAL FLOWS	
		Q _s (cfs)	Q ₁₀₀ (cfs)
OS-X	7.12	2.1	13.4
OS-Y	21.40	7.7	34.5
OS-Z	1.84	3.1	7.8
EX-B	1.96	0.6	4.0
PR-1	9.92	11.4	27.3
PR-2	9.30	10.6	25.6
PR-3	8.78	32.9	62.8
PR-4	3.27	1.1	7.1
PR-5	1.78	1.0	4.5
PR-6	0.42	0.2	1.1
PR-7	3.03	1.9	8.1

DESIGN POINT SUMMARY

Design Point(s)	Contributing Basins	Area (ac)	Flow (cfs)	
			Q _s	Q ₁₀₀
A	EX-A, OS-X	20.52	5.2	32.4
B	EX-B	1.96	0.6	4.0
C	EX-C, OS-Y	44.60	12.7	64.7
1	PR-1	9.92	11.4	27.3
2	PR-2	9.30	10.6	25.6
3	PR-3	8.78	32.9	62.8
4	PR-4, PR-3, PR-2	21.35	44.7	95.5
5	PR-5, NW EDB Outfall	1.78	4.6	34.4
6	PR-6	0.42	0.2	1.1
7	PR-7	3.03	1.9	8.1
51	PR-5, NW EDB Outfall, OS-Y, OS-Z	25.02	15.4	76.7
52	PR-6, OS-X	7.54	2.3	14.4

DATE

DESCRIPTION

REVISIONS

NO.

UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE REVIEWING AGENCIES, THE REVIEWING AGENCIES, TERRA NOVA ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT AND FOR THE DESIGNATED BY WRITTEN AUTHORIZATION.

PREPARED FOR:

FLYING HORSE REALTY

ATTN: MAKE JACOBSON

2748 NORTH GATE BLVD

COLORADO SPRINGS, CO 80921

719.235.8195

721 S. 23RD STREET

COLORADO SPRINGS, CO 80904

OFFICE: 719-635-6422

FAK: 719-635-6426

www.tnainc.com

DESIGNED BY DLF

DRAWN BY DLF

CHECKED BY LD

H-SCALE AS SHOWN

V-SCALE N/A

JOB NO. 2309.00

DATE ISSUED 03/07/23

SHEET NO. 3 OF 6

ABTR STORAGE

PROPOSED DRAINAGE MAP

N:\jobs\2309.00\Drawings\230900 SDP.dwg, 3/8/2023 11:41:59 AM

ABTR STORAGE

SITE DEVELOPMENT PLAN

PROPOSED DRAINAGE MAP

MARCH 2023

LEGEND

P-7

12.22

PR

MP

BASIN DESIGNATION
AREA IN BASIN (AC)
PERCENT IMPERVIOUS

D

DESIGN POINT

BASIN BOUNDARY

EXISTING 2' CONTOUR

GROUND SURFACE FLOW DIRECTION

ROAD AND DITCH FLOW DIRECTION

FENCE

EX

EXISTING

PR

PROPOSED

Q = 7.8 CFS
SLOPE = 4.0%
n VALUE = 0.035
DEPTH = 0.47'
VELOCITY = 3.81 FT/S

SWALE CROSS SECTION - HWY 94

Q = 34.5 CFS
SLOPE = 6.0%
n VALUE = 0.035
DEPTH = 0.90'
VELOCITY = 6.85 FT/S

SWALE CROSS SECTION - NE DIV

Q = 13.4 CFS
SLOPE = 4.0%
n VALUE = 0.035
DEPTH = 0.64'
VELOCITY = 4.62 FT/S

SWALE CROSS SECTION - SE CONV

Q = 13.4 CFS
SLOPE = 1.0%
n VALUE = 0.035
DEPTH = 0.88'
VELOCITY = 2.76 FT/S

SWALE CROSS SECTION - SE DIV

REVISIONS

NO.	DESCRIPTION	DATE

UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED FOR THE PROJECT BY THE FOLLOWING AGENCIES:

TERRA NOVA ENGINEERING, INC. APPROVES THEIR USE ONLY FOR THE PROJECT DESIGNATED BY THE PROJECT NUMBER AND WRITTEN AUTHORIZATION.

PREPARED FOR:

FLYING HORSE REALTY
ATTN: MAKE JACOBSON
2748 NORTH GATE BLVD
COLORADO SPRINGS, CO 80921
719.235.8195

721 S. Z3RD STREET
COLORADO SPRINGS, CO 80904

OFFICE: 719-635-6422
FAX: 719-635-6426
www.tnecinc.com

721 S. Z3RD STREET
COLORADO SPRINGS, CO 80904

OFFICE: 719-635-6422
FAX: 719-635-6426
www.tnecinc.com

ABTR STORAGE

PROPOSED DRAINAGE MAP

DESIGNED BY DLF

DRAWN BY DLF

CHECKED BY LD

H-SCALE AS SHOWN

V-SCALE N/A

JOB NO. 2309.00

DATE ISSUED 03/07/23

SHEET NO. 4 OF 6

