JOYFUL VIEW SUBDIVISION

FINAL DRAINAGE REPORT

PREPARED BY

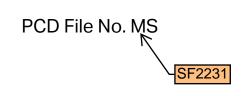
RESPEC 102 S Tejon St., Suite 1110 Colorado Springs, CO 80903 719-266-5212

PREPARED FOR

Kevin O'Neil PO Box 1385 Colorado Springs, CO 80901-1385 719-445-5050

SEPTEMBER 28, 2021

Project Number W008.1







ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my an ingressing this report.

Richard G. Gallegos, Jr., P.E. #36247

DEVELOPER'S STATEMENT:

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

•	Kevin O'Neil	
Title: Owne	r	
Address:	PO Box1385	
	Colorado Springs, CO 80901-13	385
Filed in acco	ordance the El Paso County Land	Development Code, Drainage Criteria Manual
Volumes 1 a	and 2, and the Engineering Criteri	ia Manual, as amended.
7		
County Engi	neer	Date
Conditions:		

Please add table of contents

FINAL DRAINAGE REPORT JOYFUL VIEW SUBDIVISION

Please indicate if there are any improvement identified in the DBPS that are required.

PROJECT DESCRIPTION

This drainage report is for the development of the Joyful View Subdivision. The currently vacant 70.18 acres site is located approximately 600 feet east of North Peyton Hwy and approximately 2.0 mile north of SH 94. It is currently part of the Grandview Subdivision, Tracts 2 and 3. It is further described as the southern portion of Section 33, Township 13 South, Range 63 West of the 6th Principal Meridian in El Paso County, Colorado.

All of this subdivision is located in the Haegler Ranch drainage basin. Flows from the site drain directly into the Haegler Channel which is tributary to the West Fork of Black Squirrel Creek.

SOILS

The soil on the site can be described as having a rapid permeability, medium-surface runoff, and moderate to high hazard of erosion. The soils within the site please revise this statement as lot 7

8 Blakeland Loamy Sand
 10 Blendon Sandy Loams
 Blendon Sandy Loams
 residential home have the floodplain going through their property

FLOODPLAIN STATEMENT

No portion of the developed site is located within a designated FEMA 100-year floodplain according to the information published in the Federal Emergency Management Agency Flood Plain Map No. 08041C0805G, dated December 7, 2018 and LOMR #20-08-0369P-080059 dated February 16, 2021. Detailed Base Flood Elevations (BFE) are delineated on the plans.

METHOD OF COMPUTATION

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual, Volumes 1*, dated May 2014. The Rational Method for computation of runoff was used for determining Sub-Basin flows.

Q = cia Where

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration

required for the runoff to become established

a = drainage basin size in acres

EXISTING DRAINAGE CONDITIONS

The existing 70.18 acre site is currently undeveloped. An existing gravel drive is located off of N. Peyton Hwy within the adjacent Tract 1 area to service an existing home within that Tract. A 60 ft. Access Easement is located along the north property line but currently no road exists within Tracts 2 and 3. Approximately 90% of the parcel is covered with rangeland grasses with slopes varying from 2% to 4%. Haegler Creek flows across the parcel from west to east in a southeasterly direction. According to the FEMS Study done in this area Haegler Creek carries a 100-yr flow of 1,862 cfs. The northern portion of the parcel generally slopes to the southeast toward Haegler Creek and the southern area drains to the northwest. No improvements will occur within the existing Floodplain.

per the drainage plan OS4 and OS5 both flow into the site

Two off-site basins flow into the area from the north and one basin flows into the parcel from Tract 1. Although the northwestern off-site basin does not flow into our site it is tributary to the existing culvert crossing at N. Peyton Hwy and Joyful View Road.

Sub-Basin OS1 contains 9.20 acres and drains the area along N. Peyton Hwy just north of Joyful View Road and Tract 1 of the Grandview Subdivision. It produces flows of 2.7 cfs for the 5-year storm and 15.0 cfs for the 100-year storm. These flows travel under Joyful View Road through a 23"x15" cmp arch. These ditch flows continue through Sub-Basin OS3 south along N. Peyton Per the above description of OS3, OS3 flows will be conveyed to OS5. Please also provide the cumulative flows of these two basins

Sub-Basin OS3 contains 0.90 acres and drains the area along N. Peyton Hwy just south of Joyful View Road and Tract 1 of the Grandview Subdivision. It produces flows of 0.8 cfs for the 5-year storm and 2.0 cfs for the 100-year storm. The combined ditch flows at DP3 are 2.6 cfs and 10.6 cfs respectively. These ditch flows continue to Sub-Basin OS5 and Heagler Creek.

Sub-Basin OS2 contains 45.00 acres and drains the area just north of Joyful View Road It produces flows of 6.8 cfs for the 5-year storm and 51.8 cfs for the 100-year storm. These flows travel under the dirt tracks within the Joyful View Road easement through an 18" cmp. These ditch flows continue into Sub-Basin A1ex.

Sub-Basin A1ex contains 11.70 acres and drains the northeastern area of the site. This area drains to the southeast and into Tract 4 of the Grandview Subdivision. It produces flows of 2.0 cfs for the 5-year storm and 14.3 cfs for the 100-year storm. They will combine with the flows from Sub-Basin OS2 at DP1 to produce flows into Tract 4 of 7.3 cfs for the 5-year storm and 55.9 cfs for the 100-year storm.

Sub-Basin OS4 contains 10.10 acres and is located east of Sub-Basin OS3 and south of the existing Joyful View Drive. It currently contains a gravel driveway and a single-family home. It will produce flows of 2.2 cfs and 151 cfs respectively. These flows continue southeast into Sub-Basin A2ex.

DP1 is on the east side of the property and

flows into Tract 4. Per the narrative, it
Sub-Basin A2ex contains 27.40 acres and drains the centrappears that flows from DP3. QS5 and OS6
the southeast and into Tract 4 of the Grandview Subdivis will combine at DP4f Revise accordingly
5-year storm and 26.1 cfs for the 100-year storm. They will combine with the flows from SubBasin OS4 at DP2 to produce flows into Tract 4 of 4.8 cfs for the 5-year storm and 36.0 cfs for
the 100-year storm.

Sub-Basin OS5 contains 10.60 acres and is located in the southwest portion of Tract 1 north of Heagler Creek. This undeveloped area sheet flows into Heagler Creek and produces flows of 2.0 cfs for the 5-year storm and 15.0 cfs for the 100-year storm.

Sub-Basin OS6 contains 13.90 acres and is located in the southwest corner of Tract 1 south of Heagler Creek. This undeveloped area sheet flows into Heagler Creek and produces flows of 3.5 cfs for the 5-year storm and 21.8 cfs for the 100-year storm. These flows will combine with the flows from DP1 and Sub-Basin OS5 at DP4 to produce flows into the Joyful View Subdivision of 5.1 cfs for the 5-year storm and 30.3 cfs for the 100-year storm.

Sub-Basin A3ex contains 20.50 acres and is located south of Sub-Basin A2ex and north of Heagler Creek. This undeveloped area sheet flows into Heagler Creek and produces flows of 3.7 cfs for the 5-year storm and 28.0 cfs for the 100-year storm.

Please see the above comment on basin OS6 and revise if necessary

DP5

Sub-Basin A4ex contains 10.60 acres and is located in the southern corner of the Joyful View Subdivision south of Heagler Creek. This undeveloped area sheet flows into Heagler Creek and produces flows of 2.0 cfs for the 5-year storm and 15.2 cfs for the 100-year storm. These flows will combine with the flows from DP4 and Sub-Basin A3ex at DP4 to produce flows into Tract 4 of the Grandview Subdivision of 7.4 cfs for the 5-year storm and 49.2 cfs for the 100-year storm.

The CD's identifies low grade pavement. Please design for the

DEVELOPED DRAINAGE CONDITIONS worst case.

The proposed subdivision will consist of nine (9) lots ranging from 5.05 acres to 18.2 acres. It will contain a private gravel road extending from Joyful View Drive to a proposed Cul-De-Sac. These new lots are assumed to be developed with 3000 sf homes and 12 ft gravel drives. No overlot grading will take place within the proposed subdivision. Ditches will only be provided along the north side of Joyful View Drive and the west side of Joyful View Circle.

Flows from Sub-Basins OS1, OS3, OS5 and OS6 will remain the same with flows of 5.1 cfs for the 5-year storm and 30.3 cfs for the 100-year storm entering Joyful View Subdivision within Heagler Creek. With a new culvert constructed at the intersection of N. Peyton Hwy consisting of two 23"x14" RCEP pipes to carry to total 100-year flow of 15.0 cfs.

Sub-Basin OS2 will be subdivided into several subbasins along Joyful View Drive to provide the required Runoff Reduction for the addition of gravel pavement. The subbasins along the proposed roadway have been further divided to calculate flows from the centerline of the roadway to the centerline of the proposed ditch and from the subbasin boundary to the centerline of the proposed ditch.

Sub-Basin OS2A1 contains 0.20 acres and is located just east of N. Peyton Hwy, along the north side of Joyful View Drive. This roadway area sheet flows into the ditch in Sub-Basin OS2A2 and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-Basin OS2A2 contains 0.80 acres and drains the area north of Joyful View Drive. This subbasin produces flows of 0.2 cfs for the 5-year storm and 1.7 cfs for the 100-year storm. These flows will combine with the flows from Sub-basin OS2A1at DP8 to produce flows of 0.5 cfs for the 5-year storm and 2.4 cfs for the 100-year storm. These flows continue east into Sub-Basin OS2B2.

Sub-Basin OS2B1 contains 0.20 acres and is located just east of Sub-Basin OS2A2 along the north side of Joyful View Drive. This roadway area sheet flows into the ditch in Sub-Basin OS2B2 and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-Basin OS2B2 contains 0.70 acres and drains the area north of Joyful View Drive. This sub-basin produces flows of 0.2 cfs for the 5-year storm and 1.5 cfs for the 100-year storm. These flows will combine with the flows from Sub-basin OS2B1and DP8 at DP9 to produce flows of 0.9 cfs for the 5-year storm and 4.1 cfs for the 100-year storm. These flows continue east into Sub-Basin OS2C2.

Sub-Basin OS2C1 contains 0.20 acres and is located just east of Sub-Basin OS2B2 along the north side of Joyful View Drive. This roadway area sheet flows into the ditch in Sub-Basin OS2B2 and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

This depth does not meet criteria for cross flow at the roadway. Please refer to DCMV1 Ch6 table 6-1 and revise accordingly.

Sub-Basin OS2C2 contains 0.50 acres and drains the area north of Joyful View Drive. This subbasin produces flows of 0.1 cfs for the 5-year storm and 1.0 cfs for the 100-year storm. These flows will combine with the flows from Sub-Basin OS2C1 and DP9 at DP10 to produce flows of 1.2 cfs for the 5-year storm and 5.3 cfs for the 100-year storm. These flows will then combine with the flows from Sub-Basin OS2D.

Sub-Basin OS2D contains 42.40 acres and drains the area just north of Joyful View Road. It produces flows of 6.4 cfs for the 5-year storm and 48.8 cfs for the 100-year storm. These flows will combine with the flows from DP10 at DP11 to produce flows of 7.2 cfs for the 5-year storm and 52.4 cfs for the 100-year storm. These flows continue south under Joyful View Drive through two proposed 30"x19" RECP pipes and into Sub-Basin A1. Due to the topography the culverts are designed to pick up approximately 42.4 cfs with the remaining 10.0 cfs flowing over the roadway at a depth of 0.68 '.

Sub-Basin A1 contains 15.00 acres and will drain the east half of the proposed gravel road and will also contain two single family homes. It will continue to drain to the southeast and into Tract 4 of the Grandview Subdivision. It produces flows of 2.1 cfs for the 5-year storm and 14.8 cfs for the 100-year storm. These flows will combine with the flows from DP11 at DP12 to produce flows of 7.5 cfs for the 5-year storm and 54.1 cfs for the 100-year storm. The existing flow from this area was 55.9 cfs for the 100-year storm.

A2 is 15 acres per the drainage plan. revise

Sub-Basin A2 contains 9.10 acres and will drain the east half accordinglyed gravel road and will also contain two single family homes. It will continue to drain to the southeast and into Tract 4 of the Grandview Subdivision. It produces flows of 3.1 cfs for the 5-year storm and 19.8 cfs for the 100-year storm. The existing flow from this area was 34.0 cfs for the 100-year storm.

36 per the drainage plan

Sub-Basin A3A1 contains 0.20 acres and is located just east of Joyful View Drive, along the west side of Joyful View Circle. This roadway area sheet flows into the ditch in Sub-Basin A3A2 and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-Basin A3A2 contains 2.60 acres and drains the area south of Joyful View Drive and west of Joyful View Circle. This sub-basin produces flows of 1.1 cfs for the 5-year storm and 5.6 cfs for the 100-year storm. These flows will combine with the flows from Sub-basin A3A1at DP3 to produce flows of 1.4 cfs for the 5-year storm and 6.3 cfs for the 100-year storm. These flows continue east into Sub-Basin A3B2.

Sub-Basin OS4A contains 2.50 acres and is located east of Sub-Basin OS3 and south of the existing Joyful View Drive and currently contains a gravel driveway. It will produce flows of 0.8 cfs and 4.5 cfs respectively. These flows continue southeast into Sub-Basin A3B2.

Sub-Basin A3B1 contains 0.20 acres and is located just east of Joyful View Drive, along the west side of Joyful View Circle. This roadway area sheet flows into the ditch in Sub-Basin A3B2 and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-Basin A3B2 contains 5.50 acres and drains the area south of Sub-Basin A3A2 and west of Joyful View Circle. This sub-basin produces flows of 1.6 cfs for the 5-year storm and 11.0 cfs for the 100-year storm. These flows will combine with the flows from Sub-Basin A3A1, Sub-Basin OS4A and DP3 at DP4 to produce flows of 3.1 cfs for the 5-year storm and 17.1 cfs for the 100-year storm. These flows continue east into Sub-Basin A3C2.

Sub-Basin OS4B contains 7.80 acres and is located east of Sub-Basin OS3 and south of the existing Joyful View Drive and currently contains a gravel driveway as well as a single-family home. It will produce flows of 1.7 cfs and 12.2 cfs respectively. These flows continue southeast into Sub-Basin A3C2.

Sub-Basin A3C1 contains 0.20 acres and is located just east of Joyful View Drive, along the west side of Joyful View Circle. This roadway area sheet flows into the ditch in Sub-Basin A3C2 and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-Basin A3C2 contains 5.40 acres and drains the area south of Sub-Basin A3B2 and west of Joyful View Circle. This sub-basin produces flows of 1.5 cfs for the 5-year storm and 10.4 cfs for the 100-year storm. These flows will combine with the flows from Sub-Basin A3C1, Sub-Basin OS4B and DP4 at DP5 to produce flows of 5.4 cfs for the 5-year storm and 32.8 cfs for the 100year storm. These flows continue east into Sub-Basin A3D2.

Sub-Basin A3D1 contains 0.20 acres and is located just east of Joyful View Drive, along the west side of Joyful View Circle. This roadway area sheet flows into the ditch in Sub-Basin A3D2 and produces flows of 0.3 cfs for the 5-year storm and 0.8 cfs for the 100-year storm.

Sub-Basin A3D2 contains 2.60 acres and drains the area south of Sub-Basin A3C2 and west of Joyful View Circle. This sub-basin produces flows of 0.8 cfs for the 5-year storm and 5.2 cfs for the 100-year storm. These flows will combine with the flows from Sub-Basin A3D1 and DP5 at DP6 to produce flows of 5.6 cfs for the 5-year storm and 34.0 cfs for the 100-year storm. These flows continue east into Sub-Basin A3E.

Sub-Basin A3E contains 18.7 acres and is located in the south of Joyful View Circle and north of Heagler Creek. This undeveloped area sheet flows into Heagler Creek and produces flows of 3.3 cfs for the 5-year storm and 25.6 cfs for the 100-year storm.

Sub-Basin A4 contains 10.6 acres and is located in the southeast corner of Joyful View Subdivision and Tract 1 south of Heagler Creek. This undeveloped area sheet flows into Heagler Creek and produces flows of 2.0 cfs for the 5-year storm and 15.2 cfs for the 100-year storm. These flows will combine with the flows from DP2, DP6 and Sub-Basin A3E at DP7 to produce flows of 10.7 cfs for the 5-year storm and 68.9 cfs for the 100-year storm. These flows travel east in Heagler Creek and into Tract 4 of the Grandview Subdivision. The existing site flows at this location were 49.2 cfs for the 100-year storm. The additional flows into the main channel of Heagler Creek were diverted from the area east of Joyful View Circle which previously flowed to the southeast and into Tract 4, further north of this main channel location. The total estimated flow in the main channel is approximately 1862 cfs as delineated in the FEMA report for the area west of N. Peyton Hwy. Note that per clarification from CDPHE, this

WATER QUALITY AND DETENTION

Water quality basins are not required for subdivisions containing lots greater than 5.0 acres per the Engineering Criteria Manual Section 1.7.1.B.5. Runoff Reduction calculations have been provided to eliminate the need for water quality basins. However temporary sedimentation basin will be added to mitigate sediment from the construction of the private access roads.

This is not correct. The above paragraph indicates an increase in flows from 49.2 to 68.9 cfs at DP7. The increase in flows must be mitigated. Justification for not providing detention has not been provided. Please revise accordingly.

exclusion only pertains to the lots and does not

include roadways, hence RR is needed.

Show on **GEC Plans** Include section on existing floodplain area and channel. Provide status of the channel condition and stability and if any improvement or stabilizations are needed.

Per DCMV1 Ch1.4.2:

DEVELOPERS IN AND ALONG A DRAINAGEWAY ARE REQUIRED TO IMPLEMENT THE PROPER MEASURES TO MAINTAIN OR CREATE STABLE CHARACTERISTICS OF THE DRAINAGEWAY. THE PRINCIPAL OBJECTIVE IS TO LIMIT EXCESSIVE EROSION IN AND ALONG THE CHANNEL. HISTORICAL CHANNEL RELOCATIONS/REALIGNMENTS SHALL NOT BE ALLOWED UNLESS ENGINEERING DESIGNS FOR STABLE SYSTEMS UNDER FLOOD FLOW CONDITIONS ARE ACHIEVED AND APPROVED.

DRAINAGE BASIN FEES

The proposed development is located within the Haegler Ranch Drainag

2022 Haegler Ranch Drainage Fees

Area Subject to Fees = 0.020 x 70.18 = 1.40 Acres

Haeglet Ranch Fee \$11,891 y Acre

Drainage Basin Fee = \$11,891 x 1.40 = \$16,647

2022 Haegler Ranch Bridge Fees
Impervious Coverage = 2.0%
Area Subject to Fees = 0.020 x 70.18 = 1.40 Acres
Haegler Ranch Fee = \$1,755 Acre
Bridge Fee = \$1,755 x 1.40 = \$2,457

CONCLUSION

The proposed development and subsequent lot developments follow the mandated by the EPA as follows:

Step 1: Employ runoff reduction practices

Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

- Impervious areas have been directed to the existing earth swales and ditches to encourage infiltration.
- A gravel roadway has been used for the upper portion of the project to reduce the impervious of the areas.

Step 2: Stabilize drainageways

All drainageways, ditches and channels have been stabilized by the following methods:

- Tributaries have been left in their relatively natural state where possible.
- New ditches have been stabilized with either riprap or erosion control fabric depending on the erosion potential.

 This does not match what calcs show:

Step 3: Provide water quality capture volume (WQCV)

Based on the Runoff Reduction calculations performed for the proposed development, the 2.2 acres for the asphalt and gravel roadway construction does not require any water quality basins, however a temporary sedimentation basin will be constructed.

Step 4: Consider need for industrial and commercial BMP's.

No industrial and commercial development is proposed for the site.

Based on longer times of concentration and minimal development, the proposed development flows of 57.5 cfs for the 100-year storm are below the historic levels of 63.5 cfs for the 100-year storm. Therefore, the proposed development will not adversely affect downstream or surrounding properties.

Include Joy View Rd in impervious calcs
Please correct fees

There is ~107Ksf of road for Tract A ~2.45ac. This needs to be broken out separate for fees

A 25% fee reduction applies for Low Density Lots (2.5 acres and greater lot sizes). Large lot reduction does not apply to bridge fee or roads.

Single Family 5ac parcels have a ~impervious area basis of 7% per ECM Ref Appdx L

Appendix L

a 0% reduction, which is not sufficient.

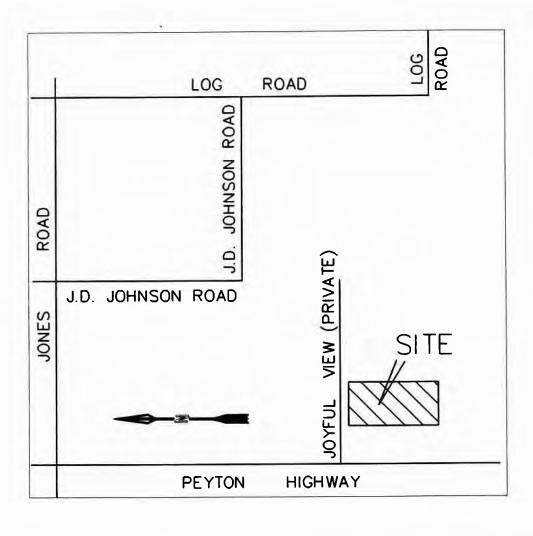
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REFERENCES

- 1. City of Colorado Springs and El Paso County (2014). *Drainage Criteria Manual Volume 1* (DCM).
- 2. City of Colorado Springs and El Paso County (2014)
- 3. Drainage Criteria Manual Volume II (DCM) as amended.
- 4. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
- 5. El Paso County (January 2016) Engineering Criteria Manual.
- 6. Urban Drainage and Flood Control District (June 2017). *Urban Storm Drainage Criteria Manual, Volume 1-3*.

APPENDIX A

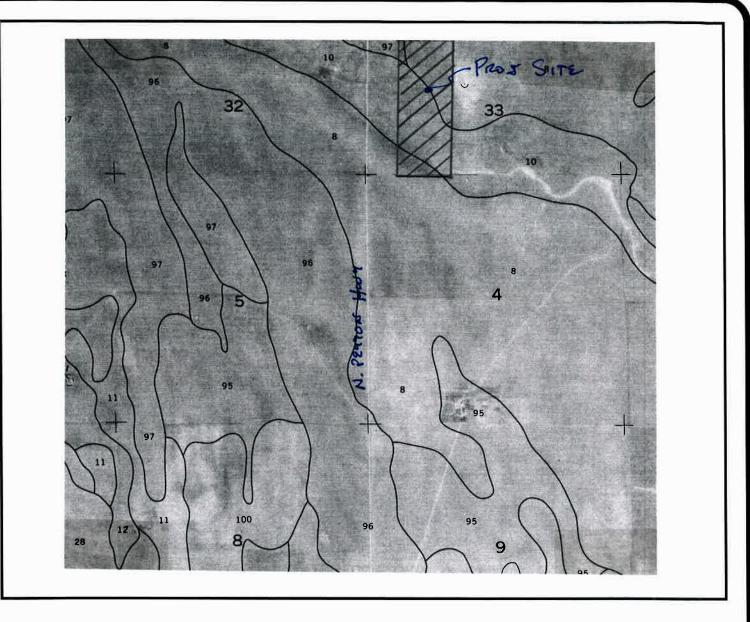
MAPS



VICINITY MAP



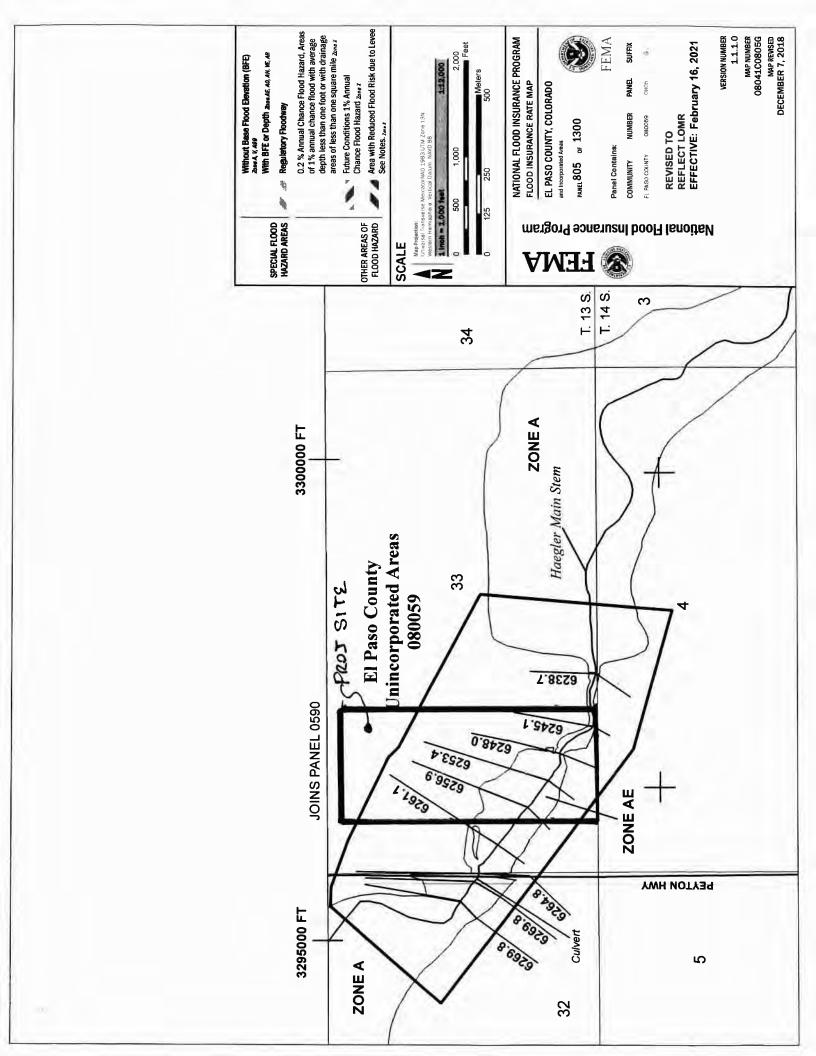
121 S Tejon St., Suite 1110 Colorado Springs, CO 80903 Phone: (719) 283-7671



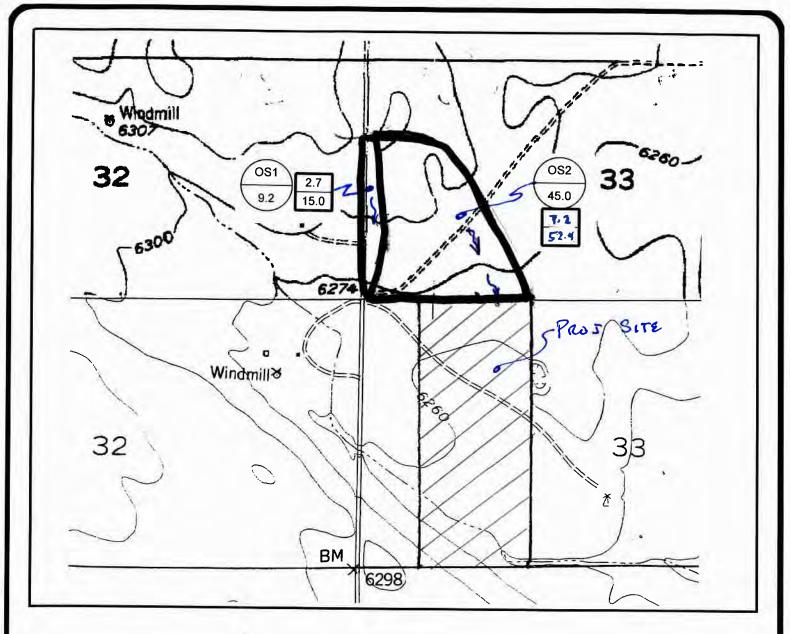




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APPENDIX B DESIGN CALCULATIONS







121 S Tejon St., Suite 1110 Colorado Springs, CO 80903 Phone: (719) 283-7671

JOYFUL VIEW	SUBDIVI	SION						
C FACTOR CAL								
EXISTING CON	NDITIONS							
RUNOFF COE	FICIENT							
TYPE A/B SOI	[LS							
LAND USE		Imperv %	5 YR	100 YR				
INDELL			0.00	0.05				
UNDEV		0						
GRAVEL ROAD		80	0.59					
ASPHALT ROAL)	100	0.9					
ROOFS		90	0.73	0.81				
	TOTAL	SURFACE CO	NDITION A	REAS		CALCULA	TED C	
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100	% IMPERVIOUS
DESIG.	(acre)		ROAD	ROAD		YR	YR	
A1ex	11.70	11.70	0.00	0.00	0.00	0.08	0.35	0.00
A2ex	27.40	27.40	0.00	0.00	0.00	0.08	0.35	0.00
A3ex	20.50	19.95	0.55	0.00	0.00	0.09	0.36	2.15
A4ex	10.60	10.24	0.00	0.36	0.00	0.11	0.37	3.40
OS1	9.20	8.73	0.00	0.47	0.00	0.12	0.38	5.11
OS2	45.00	45.00	0.00	0.00	0.00	0.08	0.35	0.00
OS3	0.90	0.51	0.00	0.39	0.00	0.44	0.61	43.33
OS4	10.10	9.91	0.14	0.00	0.05	0.09	0.36	1.55
OS5	10.60	10.60	0.00	0.00	0.00	0.08	0.35	0.00
OS6	13.90	13.62	0.00	0.28	0.00	0.10	0.36	2.01
Aex+B1ex+B2ex	59.60	59.05	0.55	0.36	0.00			
	0.8	0.00	0.44	0.36	0.00			
	Impervious	sness = (0.44)/	37.29 = 2.29	6				
DEVELOPED C		NS						
RUNOFF COEF								
TYPE A/B SOI	LS							
LAND USE		Imperv %	5 YR	100 YR				
UNDEV		0	0.08	0.35				
GRAVEL ROAD		80	0.08					
ASPHALT ROAD)	100	0.59					
ROOFS		90	0.73	0.81				

Developed C	onditions								
Developed C	TOTAL	SURFACE CO	NDITION A	REAS		CALCULA	TED C		
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5		% IMPERV	IOUS
DESIG.	(acre)	CIUDET	ROAD	ROAD	ROOFO	YR	YR	O Hell LIVE	1000
A1	9.20	8.97	0.16	0.00	0.07	0.09	0.36		2.08
A2	15.00	14.58	0.21	0.00	0.21	0.10	0.36		2.38
A3A1	0.20	0.05	0.15	0.00	0.00		0.61		60.00
A3A2	2.60	2.38	0.15	0.00	0.07		0.38		7.04
A3B1	0.20	0.05	0.15	0.00	0.00		0.61		60.00
A3B2	5.50	5.43	0.00	0.00	0.07		0.36		1.15
A3C1	0.20	0.05	0.15	0.00	0.00		0.61		60.00
A3C2	5.40	5.33	0.00	0.00	0.07	0.09	0.36		1.17
A3D1	0.30	0.11	0.19	0.00	0.00	0.41	0.58		51.73
A3D2	2.30	2.23	0.00	0.00	0.07	0.10	0.36		2.74
A3E	18.70	18.70	0.00	0.00	0.00	0.08	0.35		0.00
A4	10.60	10.60	0.00	0.00	0.00	0.08	0.35		0.00
	70.20	68.48	1.16	0.00	0.56	TOTAL SITE	E IMPERVIO	USNESS	2.04
OS1	9.20	8.73	0.00	0.47	0.00	0.12	0.38		5.11
OS2A1	0.20	0.05	0.15	0.00	0.00	0.46	0.61		60.00
OS2A2	0.80	0.80	0.00	0.00	0.00	0.08	0.35		0.00
OS2B1	0.20	0.05	0.15	0.00	0.00	0.46	0.61		60.00
OS2B2	0.70	0.70	0.00	0.00	0.00	0.08	0.35		0.00
OS2B1	0.20	0.05	0.15	0.00	0.00	0.46	0.61		60.00
OS2B2	0.50	0.50	0.00	0.00	0.00	0.08	0.35		0.00
OS2D	42.40	42.40	0.00	0.00	0.00	0.08	0.35		0.00
OS3	0.90	0.51	0.00	0.39	0.00	0.44	0.61		43.33
OS4A	2.50	2.35		0.00	0.00	0.11	0.37		4.80
OS4B	7.80	7.64	0.09	0.00	0.07	0.09	0.36		1.73
OS5	10.60	10.60	0.00	0.00	0.00	0.08	0.35		0.00
OS6	13.90	13.62	0.00	0.28	0.00	0.10	0.36		2.01

Please account for development of Lot 9 in this basin

Part			102220												i							
Market Enclotation Sheller Market Enclose	PROJ.W008.1	-																				
March Marc	DRAINAGE	CALCULATIC	N SHEET																			
Column C	07/16/21																					
No. Continue Con								Initial Tci			Travel Tir	Jue Tue		t					length	Ş.		
State Continue C	REA	AREA		C100	C5 X A	C100 X A		Slope	#		Slope	>	ij	ည	H	1100	92		_	>	¥	AREA
STING COMPITIONS X	ESIG.	(acre)		(100 yr)			L (ft)	(%)	(min)	L (ff)	(%)	(tps)				(Jyhr)	(cfs)	(cfs)	(feet)	(tps)	(min)	DESIG
1.170 1.01	XISTING	SNOITIONS																				
1177 1018 1019 1035 1034 1410 2000 2010 26204 1750 1750 1750 1040 2020 244 1750	25	45.00	80.0	0.35			300	2.00	26.28	1700	000	-	+	40.00	1 00	000	6 70	00 74	4450	7	77	000
10 10 10 10 10 10 10 10	A1ex	11.70	0.08	0.35			300	2.00	26.28	1230	1.70	-	-	38.34	00.0	3.49	1.87	14.28	00	1.70	17,71	7700
1010 0.000 0.38 0.39 0.39 0.39 0.39 0.30 0.300 0.302 0.430 14.50 14.	DP1	26.70												53.30	1.61	2.82	7.32	55.94				DP1
This column	75	10 10	000	0.36	-	364	150	000	10 40	750	500	-	-	C	0.01	7 7 0	077					
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	29.	27.40	800	0.00			200	2.00	0.40	7 700	00.	+	+	70.07	4.57	0 1 0	0 :	20.08				5.54
9 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 K	37.50	00.0	0.00	3.10	Ш	000	00.2	87.07	000	2	-	-	56.28	1.56	2.72	4 83	35.95				A2ex DP2
1010 1010	S1	9.20	0.12	0.38	1.10	3.50	100	2.00	14.58	1500	2.50	-	-	27.08	2.46	4 30	27.0	15.03	1350	0.70	22 14	00.4
10 10 10 10 10 10 10 10	93	0.90	0.44	0.61	0.40	0.55	20	2.00	4.39	1350	0.80	-	-	36.53	2.06	3.59	0.81	1.97	3	2	100	083
10.00 0.00 0.036 1.036 1.030	23	10.10			1.50	4.05						-		59.22	1.50	2.63	2.26	10.62	2007	1.25	9.33	DP3
13.89	35	10.60	0.08	0.35	0.85	3.71	150	1.30	21.42	650	1.40	1.25		30.09	2.31	4.04	1.96	15.00				085
A	98	13.90	0.10	0.36	1.39	2.00	300	4.00	20.50	800	4.60	2.20		26.56	2.49	4.35	3.46	21.76				980
Carrollo	4	34.60	000	0	3.74	12.76	C.	,	9, 99				-	58.56	1.36	2.38	5.09	30.32	1450	1.70	14.22	DP4
ELOPED CONDITIONS 1	ex ex	70.50	80.0	0.35	1.64	7.18	720	1.20	28.40	400	1.60	-	-	31.91	2.23	3.90	3.67	28.01				A3ex
ELOPED CONDITIONS ELOPE CONDITIONS ELOP	, č	10.80	00.0	0.50	0.00	23.64	2000	0.00	0.03	1300	07.1		4	29.38	2.35	01.4	1.99	15.21				A4ex
ELOPED CONDITIONS 1																		1				5
920 0.12 0.36 1.10 3.50 1.00 2.00 4.39 150 2.00 12.50 2.00 12.50 27.0 2.00 2.00 2.00 1.20 2.00 1.20 2.00 1.20 2.00 1.20 2.00 1.20 2.00 1.20 2.00 2.00 1.20 2.00 <th< td=""><td>EVELOPED</td><td>CONDITION</td><td>S</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	EVELOPED	CONDITION	S																			
090 044 0.64 0.65 20 2.00 4.39 1350 0.80 0.70 32.44 36.53 2.06 3.59 0.81 1.97 1.97 0.70 3.214 36.53 2.06 3.50 1.97 4.04 1.96 1.97 1.94 1.96 <th< td=""><td>7.5</td><td>9.20</td><td></td><td>0.38</td><td>1.10</td><td>3.50</td><td>100</td><td>2.00</td><td>14.58</td><td>1500</td><td>2.50</td><td></td><td></td><td>27.08</td><td>2.46</td><td>4.30</td><td>2.72</td><td>15.03</td><td>1350</td><td>0.70</td><td>32.14</td><td>081</td></th<>	7.5	9.20		0.38	1.10	3.50	100	2.00	14.58	1500	2.50			27.08	2.46	4.30	2.72	15.03	1350	0.70	32.14	081
10.10 10.00 0.008 0.35 0.45 0.40 0.008 0.35 0.45 0.40 0.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 1.50 0.40 0.50 0.40	33	06.0	0.44	0.61	0.40	0.55	20	2.00	4.39	1350	0.80			36.53	5.06	3.59	0.81	1.97				OS3
10,60 0.08 0.35 0.85 3.71 150 1.30 21,42 650 14,0 1.25 867 3.09 2.31 4.04 1.50 1.05 0.05 1.40 1.25 6.06 2.55 3.36 3.65 3.64 1.50 1.70 1.40 1.25 6.06 2.00 4.05 2.20 6.06 2.55 3.36 3.63 3.09 2.176 1.70 1.40 1.75 3.81 1.84 3.13 5.63 3.09 0.82 1.40 1.40 4.75 6.85 1.36 1.70 1.70 1.40 4.75 6.85 1.36 1.70 1.70 1.40 4.75 8.65 1.36 1.70 1.70 4.75 8.75 1.40 1.70 4.75 8.75 1.70 1.70 4.75 8.75 1.70 1.70 4.75 8.75 1.70 1.70 4.75 8.75 1.70 1.70 4.75 8.75 1.71 1.70 1.70 <th< td=""><td><u>-</u></td><td>10.10</td><td></td><td></td><td>1.50</td><td>4.05</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>59.22</td><td>1.50</td><td>2.63</td><td>2.26</td><td>10.62</td><td>700</td><td>1.25</td><td>9.33</td><td>DP1</td></th<>	<u>-</u>	10.10			1.50	4.05								59.22	1.50	2.63	2.26	10.62	700	1.25	9.33	DP1
13.50 0.10 0.30 3.00 4.00 4.00 4.20 6.00 4.30 4.35 3.46 21.06 2.00 4.86 4.00 2.00 4.86 4.00 2.00 4.80 4.00 2.00 4.86 4.00 3.00 1.76 3.81 6.85 4.13 7.19 6.38 6.30 1.70 4.12 7.10 1.70 4.12 7.10 1.70 4.10 4.76 6.85 4.13 7.19 6.38 6.30 1.70 1.70 4.70 6.85 4.12 7.19 6.30 1.70 4.70 4.76 6.85 4.13 7.19 6.38 6.80 1.70 4.70 <	, O	10.60	0.08	0.35	0.85	3.71	150	1.30	21.42	650	1.40	1.25	-	30.09	2.31	4.04	1.96	15.00				085
4.2. 6.0. <th< td=""><td>0 0</td><td>13.90</td><td>0.0</td><td>030</td><td>1.39</td><td>12.76</td><td>3000</td><td>9.4</td><td>70,50</td><td>200</td><td>09.4</td><td>7.20</td><td>-</td><td>26.56</td><td>2.49</td><td>35</td><td>3.46</td><td>21.76</td><td>7.400</td><td>1</td><td>27</td><td>980</td></th<>	0 0	13.90	0.0	030	1.39	12.76	3000	9.4	70,50	200	09.4	7.20	-	26.56	2.49	35	3.46	21.76	7.400	1	27	980
2 2.60 0.13 0.38 0.34 0.99 100 3.00 17.62 400 3.00 17.63 3.81 16.43 3.23 5.63 1.09 5.57 9 7 1 0.20 0.46 0.61 0.09 0.12 2.6 2.00 4.85 4.00 0.50 1.40 4.76 3.63 1.39 6.25 4.00 1.40 4.76 3.63 1.39 6.25 4.00 1.40 4.76 3.63 1.39 6.25 4.00 1.40 4.76 3.63 1.39 6.25 4.00 1.40 4.76 3.63 1.39 6.25 4.00 1.40 4.76 3.63 3.73 4.14 4.00 1.40 4.76 3.63 3.71 4.75 1.79 0.38 0.88 4.75 4.76 4.75 4.12 7.19 0.38 0.88 4.76 4.76 4.76 4.76 4.77 7.19 0.38 0.88 4.75 4.76	A1	0.20	0.46	0.61	60.0	0.12	26	2 00	4 85	400	0.50	1 40	-	00.00	05.7	7.19	0.09	20.02	004	0/-	14,22	DP2
2.80 0.43 1.11 2.80 4.85 4.00 0.50 1.40 4.76 9.62 4.12 7.19 0.38 6.25 4.00 1.40 4.76 9.62 4.12 7.19 0.38 0.88 4.00 4.86 2 5.50 0.046 0.61 0.09 0.12 2.6 2.00 4.85 4.00 1.75 3.81 16.95 3.17 5.55 1.57 10.98 0.88 0.89 0.70 4.85 4.00 1.30 1.20 4.71 2.20 2.75 4.81 10.98 0.71 0.88 0.88 0.88 0.89 0.71 0.70 0.70 0.71 0.70 0.	A2	2.60	0.13	0.38	0.34	0.99	100	3.00	12.62	400	3.00	1.75	-	6 43	3.23	563	1 09	5.57				A3A2
1 0.20 0.46 0.61 0.09 0.12 26 2.00 4.85 400 0.50 1.40 4.76 9.62 4.12 7.19 0.38 0.88<	23	2.80			0.43	1.1							-	16.43	3.23	5.63	1.39	6.25	400	1.40	4.76	DP3
2 5.50 0.09 0.36 0.50 1.98 100 3.00 13.14 400 3.00 1.75 3.81 16.95 3.17 5.55 1.57 10.98 9 9 9 9 1.20 1.71 4.17 2.20 2.75 4.81 0.76 4.45 700 1.75 6.67 A 1.100 3.00 1.20 4.17 2.20 2.75 4.81 0.76 4.45 700 1.75 6.67 1.100 3.00 0.04 0.05 0.04 0.05 0.04 0.70 4.85 400 0.50 4.76 4.76 2.75 4.14 3.06 1.71 4.76 4.76 3.06 4.14 4.70 4.76 4	1	0.20	0.46	0.61	0.09	0.12	56	2.00	4.85	400	0.50	1.40		9.62	Ц	7.19	0.38	0.88				A3B1
A 2.50 0.11 0.37 0.28 0.93 150 2.00 18.04 300 1.30 1.20 4.17 22.20 2.75 4.81 0.76 4.45 700 1.75 6.67 11.00 0.20 0.046 0.641 0.020 0.046 0.641 0.09 0.012 2.60 4.85 400 0.50 1.30 4.16 2.34 1.30 6.73 4.14 3.06 17.14 4.00 1.40 4.76 8.02 4.12 7.19 0.38 0.38 0.88 7.60 1.40 4.76 8.02 4.12 7.19 0.38 0.38 0.88 7.60 1.40 4.76 8.02 4.14 4.00 1.30 1.40 4.76 <td< td=""><td>B2</td><td>5.50</td><td>0.09</td><td>0.36</td><td>0.50</td><td>1.98</td><td>9</td><td>3.00</td><td>13.14</td><td>400</td><td>3.00</td><td>1.75</td><td>-</td><td>16.95</td><td>3.17</td><td>5.55</td><td>1.57</td><td>10.98</td><td></td><td>7</td><td></td><td>A3B2</td></td<>	B2	5.50	0.09	0.36	0.50	1.98	9	3.00	13.14	400	3.00	1.75	-	16.95	3.17	5.55	1.57	10.98		7		A3B2
11.00 0.40 0.414 4.04 4.14 4.06 1.29 4.14 4.06 1.29 4.14 4.06 1.20 4.16 4.16 2.88 ft 2.37 4.14 3.06 17.14 4.00 1.40 4.76 9.62 4.12 7.19 0.38 0.714 4.06 4.76 9.62 4.12 7.19 0.38 0.88 0.88 0.88 0.88 0.12 0.20 0.30 0.30 1.30 1.30 1.30 8.33 1.30 8.33 2.34 1.30 1.30 8.33 2.34 1.30 1.30 8.33 1.30 1.30 1.30 1.30 8.33 1.40 4.76 1.30 8.33 1.40 4.76 1.30 8.33 1.40 4.76 1.30 1.40 4.76 1.00 4.76 1.30 3.34 3.24 5.01 1.80 4.83 1 0.20 0.20 0.20 1.30 1.30 1.40 4.76 1.00 <t< td=""><td>94A</td><td>2.50</td><td>0.11</td><td>0.37</td><td>0.28</td><td>0.93</td><td>120</td><td>2.00</td><td>18.04</td><td>300</td><td>1.30</td><td>1.20</td><td>-</td><td>22.20</td><td>2.75</td><td>18.9</td><td>92.0</td><td>4.45</td><td>200</td><td>1.75</td><td>6.67</td><td>OS4A</td></t<>	94A	2.50	0.11	0.37	0.28	0.93	120	2.00	18.04	300	1.30	1.20	-	22.20	2.75	18.9	92.0	4.45	200	1.75	6.67	OS4A
1 0.20 0.45b 0.05 0	4 0	11.00	0		1.29	4.14	3	0				9	4	28.87	2.37	4.14	3.06	17.14	400	1.40	4.76	DP4
2 3.40 0.09 0.36 0.45 1.34 100 3.00 13.14 400 1.30 1.30 1.30 3.15 1.24 3.06 5.34 1.48 10.37 3.00 1.30 1.30 1.30 1.30 1.30 1.30 3.15 3.24 4.33 1.74 12.17 700 1.30 8.97 1 24.40 2.57 9.01 2.60 2.01 2.23 400 0.50 1.40 4.76 10.00 4.05 7.08 3.24 5.01 1.80 4.63 2 2.00 0.26 0.09 1.00 3.00 1.75 3.81 1.682 3.19 5.77 0.83 5.21 9.0 2 2.00 0.10 0.36 0.26 0.30 1.301 40.34 1.93 3.38 5.21 9.0 1.80 9.2 2 2.00 0.26 0.30 1.27 3.81 1.682 3.19 3.38 5.	2 6	0.20	0.40	000	90.0	2.0.12	07	2.00	60.4	400	0.50	04.	+	20.6	4.12	61.7	0.38	0.00				ASCI
24.40 0.20 0.41 0.58 0.08 0.12 26 2.00 6.523 400 0.50 1.40 4.76 1.00 4.05 7.08 0.33 0.82 9.01 1.80	24B	7.80	60.0	0.36	0.49	284	3 5	2000	18.40	920	05.	00.1	-	12.01	3.00	0.54	1.40	12.17	200	1 30	8 07	ASCZ
1 0.20 0.41 0.58 0.08 0.12 26 2.00 5.23 400 0.50 1.40 4.76 10.00 4.05 7.08 0.33 0.82 2 2.60 0.10 0.36 0.26 0.94 100 3.00 17.5 3.81 16.82 3.19 5.57 0.83 5.21 27.20 2.91 10.06 2.91 10.06 1.20 28.40 40.0 1.60 1.90 3.51 5.63 33.99 5.63 33.99 18.70 0.08 0.35 1.50 6.55 250 1.20 28.40 1.60 1.90 3.51 3.91 3.34 25.55 9	55.	24.40		3	2.57	9.01	3	S	2	3	3	3	-	35.71	L	3.64	5.37	32.84	2005	180	4 63	DP5
2 2.60 0.10 0.36 0.26 0.29 100 3.00 13.01 40.34 1.68 3.81 16.82 3.19 5.57 0.83 5.21 9.21 27.20 27.20 2.91 10.06 1.20 28.40 400 1.60 1.90 3.51 3.34 5.63 33.99 8 18.70 0.08 0.35 1.50 6.55 250 1.20 28.40 4.00 1.60 3.51 31.91 2.23 3.90 3.34 25.55	A3D1	0.20	0.41	0.58	0.08	0.12	56	2.00	5.23	400	0.50	1.40	-	0.00	L	7.08	0.33	0.82				A3D1
27.20 2.91 10.06 2.91 10.06 2.840 400 1.60 1.90 3.51 40.34 1.93 3.38 5.63 33.99 18.70 0.08 0.35 1.50 6.55 250 1.20 28.40 400 1.60 1.90 3.51 31.91 2.23 3.90 3.34 25.55 3.90	302	2.60	0.10	0.36	0.26	0.94	100	3.00	13.01	400	3 00	1.75		16.82		5.57	0.83	5.21				A3D2
18.70 0.08 0.35 1.50 6.55 250 1.20 28.40 400 1.60 1.90 3.51 31.91 2.23 3.90 3.34 25.55	90	27.20			2.91	10.06								10.34		3.38	5.63	33.99				DP6
	щ	18.70	0.08	0.35	1.50	6.55	250	1.20	28.40	400	1.60	-	-	31.91		3.90	3.34	25.55				A3E

DP/	08242	1.75 3.81 DP8	OS2B1	OS2B2	40 2.78		OS2C1	0S2C1 0S2C2	0S2C1 0S2C2 DP10	0S2C1 0S2C2 0P10 0S2D	0S2C1 0S2C2 DP10 0S2D 1.70 11.27 DP11	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27	11.27
		400 1.			400 2	i					-	· -					₹	-	₹	-		-	-	-							-
D	87		88	51																											
		53 2.40								`		745	7 27 - 27	7 40 7 40	75,55	70-0	7 2 7 2	(4) - u) -	(U) - U) -	4 2 4 2	4 2 4 2	70,70	70.0	7 0 - 0	7 0 - 0 -	7 0 1	4 0 1	7070			7 0 7 0
	L																														
	L	3.42 5.97	L	3.54 6.18																											
		ш							13.57 3.5 18.42 3.0 9.62 4.7 14.61 3.4 21.19 2.8																						
4 76 9	+	5	-		2.78 13														2.78 13 4.76 9 3.81 14 15.74 42.1 18.33 55 18.33 35	2.78 13 4.76 9 3.81 14, 21 15.74 42.2 9.80 24, 42.2 18.33 35 18.33 35	2.78 13 3.81 14 15.74 42 2.15.74 42 9.80 24.2 9.80 24.2 18.33 35 18.33 35	2.78 13 3.81 14 16.74 42 9.80 24.2 9.80 24.2 18.33 35 Hwy Ditch	2.78 13 3.81 14 16.74 42 9.80 24.2 9.80 24.2 53.3 35 Hwy Ditch	2.78 13 4.76 9 3.81 14 15.74 42 2.1 15.74 42 9.80 24, 4.42 5.33 35 Hwy Ditch Hwy Ditch	2.78 13 4.76 9 3.81 14 15.74 42 21 15.74 42 9.80 24 4.22 18.33 35 Hwy Ditch	2.78 13 4.76 9 3.81 14 15.74 42 21 15.74 42 23 33 35 18.33 35 Hwy Ditch	2.78 13 3.81 14, 76 9 3.81 14, 21, 14, 22, 21, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 24	2.78 13 3.81 14, 76 9 3.81 14, 21, 14, 22, 21, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 22, 24, 24	2.78 13 4.76 9.80 14.76 9.80 24.20.16.74 42.20.24.40.2	2.78 13 3.81 14,76 3.81 14, 21 15,74 422 9.80 24, 422 18,33 35, 33 18,33 35, 18, 18, 18, 18, 18	2.78 13 3.81 14,76 9 3.81 14, 221 15,74 422 18,33 35. 18,33 35.
	1.75		L			2.40													1.40 2.40 1.75 1.70 1.00 1.00	1.40 1.75 1.70 1.00 1	1.40 1.75 1.70 1.00 1.00 1.00 1.00 1	7 7 E E	1.40 1.40 1.75 1.70 1.00 1 1.00 Peyton F	1.40 1.40 1.75 1.70 1.00 1 N Peyton F	1.40 1.75 1.70 1.70 1.00 1 N Peyton I	1.40 1.75 1.80 1.70 1.70 1.00 1 N Peyton I	1.40 1.75 1.80 1.70 1.00 1.00 N Peyton I	1.40 1.75 1.70 1.70 1.00 1 N Peyton I	1.40 1.75 1.70 1.70 1.00 1 N Peyton I	1.40 1.75 1.70 1.70 1.00 1 N Peyton F	1.40 1.75 1.70 1.00 1 1.00 1 N Peyton F
0.50	080	2		0.50	0.50	0.50	0.50	0.50 1.40 0.50 0.80	0.50 0.50 0.80	0.50 0.50 0.80 2.00	0.50 0.50 0.80 2.00	0.50 0.80 0.80 2.00	0.50 0.50 0.80 2.00 1.70	0.50 0.50 0.80 2.00 1.70	0.50 0.50 0.80 0.80 1.70	0.50 0.50 0.80 0.80 1.70	0.50 0.50 0.80 0.80 1.70 1.20	α	0.50 1.40 0.50 0.80 2.00 1.70 1.20 Riprap Size	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing h	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 1.40 0.50 0.80 2.00 1.70 1.20 Riprap Size Existing N	0.50 1.40 0.50 0.80 2.00 1.70 1.20 Size Existing N	0.50 1.40 0.50 0.80 2.00 1.70 1.20 Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 Riprap Size Existing N	0.50 0.50 0.80 0.80 1.70 1.20 1.20 Existing N Existing N
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4 85	10.80	3	10.4	60.4	10.80	10.80	10.80	10.80 10.80 10.80	10.80 10.80 10.80	4.85 10.80 10.80 26.28	4.85 10.80 10.80 26.28	4.85 10.80 10.80 10.80 26.28 15.03	4.85 10.80 10.80 26.28 15.03	4.85 10.80 10.80 15.03 17.15	4.85 4.85 10.80 15.03 17.15	10.80 10.80 10.80 15.03 17.15	10.80 10.80 10.80 15.03 17.15														
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36	8	3	26		8	80	80	80 S0 80 80	80 80 80	300 80	300 80	80 26 80 300 100	26 80 80 300 100	26 80 300 300 100 100	30 8 80 30 00 100 100 100 100 100 100 100 100 10	300 880 880 100 100 100 100 100 100 100 1	300 880 80 100 100 100 100 100 100 100 10	W	6	W	W			W		" ⁻	,				
0.12	0.28	0.40	0.12	;	0.25	0.25	0.25	0.25	0.25 0.77 0.12 0.18	0.25 0.77 0.12 0.18 1.07	0.25 0.77 0.12 0.18 1.07 14.84	0.25 0.77 0.12 0.18 14.84 15.91 3.28	0.25 0.77 0.12 0.18 1.07 14.84 15.91 3.28 19.18	0.25 0.75 0.75 0.12 1.07 1.07 1.84 1.591 3.28 19.18	0.25 0.75 0.75 0.18 1.07 1.07 1.84 1.91 19.18	0.25 0.75 0.12 0.18 1.07 1.07 1.591 1.591 1.918 1.918 2.28 1.918	0.25 0.75 0.12 0.18 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07	0.7.0 1.0 1.0 1.0 3.2 3.2 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0													
0	900	0.16	60 0	225	0.06	0.00	0.00	0.00	0.00	0.00 0.00 0.00 0.04 0.04 3.39	0.00 0.00 0.00 0.04 0.04 0.04 3.39	0.00 0.00 0.00 0.04 0.44 0.44 0.82	0.00 0.00 0.03 0.04 0.04 0.04 0.04 0.04	0.00 0.00 0.00 0.04 0.04 0.04 0.08 3.39 3.39 4.65 0.05 0.06	0.00 0.00 0.00 0.00 0.04 0.04 0.04 0.082 0.082 0.082 0.082 0.082 0.082	0.00 0.00 0.00 0.04 0.44 0.82 3.39 4.65 4.65	0.00 0.00 0.04 0.44 0.44 0.82 0.82 4.65 1.50	0.00 0.00 0.00 0.04 0.44 0.82 3.39 4.65 4.65	0.00 0.00 0.04 0.44 0.82 0.82 4.65 4.65 7	0.00 0.00 0.04 0.04 0.04 0.82 0.82 4.65 1.50 0.00	0.00 0.00 0.00 0.04 0.04 0.04 0.04 0.04	0.00 0.00 0.00 0.04 0.04 0.04 0.04 0.04	0.00 0.00 0.00 0.04 0.04 0.04 0.082 0.082 0.082 0.09 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.04 0.04 0.082 0.082 0.00 0.00 0.00 0.00 0.00	8.3 3 3.39 9.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	B## B## 0.00 0.00 0.00 0.00 0.00 0.00 0.	B # # # # # # # # # # # # # # # # # # #
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0.46	800	3	0.46	5	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.00	0.08 0.08 0.09 0.09	0.08 0.08 0.09 0.09 0.09	0.08 0.08 0.09 0.09 0.09	0.00 0.08 0.09 0.09 0.09	0.08 0.08 0.09 0.09 0.10	0.08 0.08 0.09 0.09 0.10	0.08 0.08 0.08 0.09 0.10 0.10 Q100 cfs	0.08 0.08 0.09 0.09 0.10 0.10 0.10 0.10	0.08 0.08 0.08 0.09 0.10 0.10 0.10 15.0	0.08 0.08 0.08 0.09 0.09 0.10 0.10 15.0	0.08 0.08 0.08 0.09 0.10 0.10 0.10 15.0 16.6 30.3	0.08 0.08 0.08 0.09 0.10 0.10 0.10 15.0 15.0 16.3 6.3	0.08 0.08 0.08 0.09 0.09 0.10 0.10 0.10 15.0 17.2 8.3 32.8	0.08 0.08 0.08 0.09 0.09 0.10 0.10 15.0 17.2 32.8 34.0	0.08 0.08 0.09 0.09 0.10 0.10 15.0 17.2 32.8 34.0 68.9	0.08 0.08 0.09 0.09 0.09 0.10 0.10 15.0 17.2 32.8 34.0 68.9	0.08 0.08 0.09 0.09 0.09 0.10 0.10 15.0 16.3 17.2 32.8 34.0 63.9 6.3 4.1	C.10 0.08 0.08 0.09 0.09 0.10 0.10 15.0 15.0 16.3 17.2 32.8 34.0 63.9 2.4 4.1	CATION SHEE CA100 cfs 0.08 0.08 0.08 0.09 0.10 0.10 10.6 30.3 32.8 34.0 68.9 68.9 67.4 4.1 4.1
0.70	0.80	1.00		0.20	0.20	0.20 0.70 1.90	0.20 0.70 1.90 0.20	0.20 0.70 1.90 0.20 0.50	0.20 0.70 1.90 0.20 0.50 2.60	0.20 0.70 1.90 0.20 0.50 2.60	0.20 0.70 1.90 0.20 0.50 2.60 42.40	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 15.00	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 TY CALCUL	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 17 CALCUL	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 TY CALCUL 2.7 2.3 5.1	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 15.00 17. CALCUL	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 TY CALCUL 2.7 2.3 2.3 2.1 3.1	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 17. CALCUL Q5 cfs 2.7 2.7 2.3 2.7 2.3 3.1	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 15.00 15.00 15.00 15.00 17. CALCUL 2.7 2.3 2.7 2.3 3.1	0.20 0.70 1.90 0.70 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 15.00 17 CALCUL 2.3 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 3.1	0.20 0.70 1.90 0.70 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 15.00 17 CALCUL 2.3 2.3 2.3 2.4 3.1 10.7	0.20 0.70 1.90 0.70 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 17. CALCUL 2.3 2.7 2.3 2.7 2.3 2.7 2.3 2.7 2.3 2.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	0.20 0.70 1.90 0.20 0.50 2.60 42.40 45.00 9.10 54.10 15.00 17 CALCUL 0.5 2.3 2.3 2.7 2.3 2.1 1.4 3.1 3.1 6.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	0.20 0.70 1.90 0.50 2.60 42.40 45.00 9.10 9.10 54.10 15.00 17 CALCUL 7.2 2.3 3.1 1.4 3.1 1.2 6.5 6.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6
0.8284	OS2A2	DP8	06204	OSZBI	OS2B2	OS2B2 DP9	082B2 082B2 0P9 082C1	08282 08282 082C1 082C2	0.5282 0.5282 0.5267 0.5262 0.510	08282 08282 082C1 082C2 0810	08282 08282 08261 08262 0810	052B1 052B2 052C1 052C2 0710 0711	08282 08282 08261 08262 0810 0811	OS2B2 OS2B2 OS2C1 OS2C2 OS2C2 DP11 A1 DP12	0.5281 0.5282 0.5262 0.5262 0.520 0.520 0.520 0.520 0.520 0.520 0.520 0.520 0.520 0.520	05282 05282 05262 05262 0520 0510 071	05282 05282 05262 05262 0520 0520 0511 41	05282 05282 0599 052C1 052C2 052D 0511 41	052B1 052B2 052B2 052C1 052C2 052D 0511 41 42 42 42 42	DS2B2 DS2C1 DS2C2 DP10 DP11 A1 DP12 A2 Location OS1	052B2 052B2 052C1 052C2 051 0512 07CH CAPACI 051 051	DSZB1 0SZB2 0SZC1 0SZC2 0P10 0P11 0P12 0TCH CAPACI Location 0S1 0P2	DITCH CAPACI	05282 05282 05262 05262 0510 0511 0512 051 051 051 061 063	U A	0.52.0.1 0.52.0.2 0.52.0.2 0.52.0.2 0.52.0 0.52.0 0.51.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	DSZB1 0SZB2 0S2C1 0S2C2 0P10 0P11 A1 A1 A1 A1 DP12 DP12 DP12 DP1 DP1 DP2 DP3 DP3 DP3 DP3 DP3 DP3 DP3 DP3 DP3 DP3	DSZB1 0SZB2 0S2C1 0S2C2 0P10 0P11 A1 A1 A1 DP12 A2 A2 DP12 DP1 DP1 DP1 DP1 DP2 DP1 DP3 DP3 DP3 DP3 DP4 DP4 DP4 DP4 DP4 DP4 DP6 DP6	DS2B2 DS2B2 DS2C1 DS2C2 DP10 DP11 A1 A1 A1 DP12 DP12 DP2 DP3 DP3 DP3 DP3 DP3 DP3 DP3 DP3 DP3 DP3	DS2B2 DS2B2 DS2C1 DS2C2 DP10 DP11 A1 A1 A1 DP12 DP12 DP12 DP2 DP3 DP3 DP3 DP4 DP4 DP3 DP4 DP3 DP3 DP4 DP4 DP3 DP4 DP3 DP4 DP4 DP3 DP4 DP4 DP4 DP7 DP4 DP7 DP4 DP7 DP7 DP7 DP7 DP7 DP7 DP7 DP7 DP7 DP7	DITCH CAPACITO DP3 DITCH CAPACITO DP12 A2 Location DP2 DP3 DP4 DP7 DP7 DP7 DP7 DP7 DP7 DP7

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materials may be considered on a case-by-case basis. In either case, the protection shall be constructed to convey the 100-year developed condition flow from the upstream watershed without accounting for any flow attenuation within the detention facility.

The crest elevation of the emergency spillway shall be set at or above the calculated 100-year water surface elevation. A concrete wall shall be constructed at the emergency spillway crest extending at least to the bottom of the riprap and bedding layers located immediately downstream for regional and subregional ponds. On-site ponds do not require a concrete crest wall. The crest wall shall be extended at the sides up to 1 foot above the emergency spillway design water surface as shown in Figure 13-12c.

Riprap embankment protection shall be sized based on methodologies described in *Development of Riprap Testing in Flumes: Phase II Follow-up Investigations* (Apt et al. 1988) to determine the D₅₀ dimension. According to this method:

$$D_{50} = 5.23 \, S^{0.43} \, (1.35 \, \hat{C}_f \, q)^{0.56} \qquad = 5.94 \, ''$$

$$D_{50} = 5.23 \, S^{0.43} \, (1.35 \, \hat{C}_f \, q)^{0.56} \qquad = 5.94 \, ''$$

$$D_{50} = \text{median rock size (in)}$$

$$S = \text{longitudinal slope (ft/ft)}$$

$$C_f = \text{concentration factor (1.0 to 3.0) } 2$$

$$q = \text{unit discharge (cfs/ft)} \qquad l.59$$
When:
$$\eta \text{ (porosity)} = 0.0 \text{ (i.e., for buried soil riprap)}$$

The unit discharge shall be determined by dividing the design flow by the crest width, excluding the side slopes. According to this method, the types of riprap needed for typical embankment slopes and design flows are shown in Figure 13-12d. The riprap types shown were determined assuming that there is no interstitial flow (i.e., no flow between the rocks—soil riprap with filled voids and porosity = 0) and that the "concentration factor" (C_f) is equal to 2.0. For plain riprap with interstitial flow, the method requires an interactive process described in Apt et al. (1988). The range for each type shown is based on the D_{50} dimension at the midpoint between the D_{50} for adjacent types. Riprap characteristics such as rock size distributions, thickness, hardness, specific gravity, angle of repose, etc., shall be as required in the Major Drainage chapter of Volume 1 in the UDFCD Manual. For design conditions outside of the parameters or conditions represented in Figure 13-12d, the designer shall propose an appropriate alternative approach that may include grouted boulders or concrete protection. Alternative approaches must be submitted for approval prior to incorporation into designs.

The emergency spillway is also needed to control the location and direction of any overflows. The emergency spillway and the path of the emergency overflow downstream of the spillway and embankment shall be clearly depicted on the drainage plan. Structures shall not be permitted in the path of the emergency spillway or overflow. The emergency overflow water surface shall be shown on the detention facility construction drawings. When emergency overflows will pass over a roadway, the depth of flow shall not be greater than 1 foot over the street crown.

5.13 Retaining Walls

The use of retaining walls within detention basins is discouraged due to the potential increase in long-term maintenance costs and concerns regarding the safety of the general public and maintenance personnel. Retaining walls shall only be considered for on-site facilities. If retaining walls are proposed, footings shall be located above the WQCV or EURV. Wall heights not exceeding 30 inches are

DESIGN FORM	ROADWAY ELEVATION: 73.56 (11) (11) So: (11) So: (11) TW S=So-FALL/Lo Lo" Lo"	NOI	TE TO COMMENTS	OR. EFI HE	128 6.5		ER)		CULVERT BARREL SELECTED: SIZ E: SHAPE: MATERIAL: RETAR OF E:
1 15 1	ROADWAY ELEVATION: 75.5			0 E	12.8		(6) h TW or (dc+0/2)(WHICHEVER IS GREATER)		SIZE: SHAPE: MATERIAL: ENTNANCE:
CULVERT DESIGNER	AY ELEVAT			= 8	5.0		IICHEVER IS	7	
	S S S L		OUTLET CONTROL		2.0		(6) h _a = TW or (d _c +D/2)(WHIC		
	ROADW	SNO	TLET	23	1.3		140.0	H.	
	FAUL	CULAT	NO S		1001			(0) EL _{ho} EL _o ·H·h _o	
		ER CAI		9"	0.85		(6) h.	(6) EL,	
0	-(n) -(m)	HEADWATER CALCULATIONS	1	<u>:</u> (c)	1,5				
 z		물		() () () () ()	73.0		T OF	PTH IN	
STATION	EL _{bd} :-			316			ELN HW; EL; (INVERT OF INLET CONTROL SECTION)	TW BASED ON DOWN STREAM CONTROL OR FLOW DEPTH IN CHANNEL.	
0. 0,	8				1.4		HW; E	ISED ON 10L OR F NEL.	CUSSIC
11			= -	2/2	2.1		(4) ELN"	(5) TW BA CONTR CHAN	COMMENTS / DISCUSSION :
		FLOW			7.5		= =	ຽ	VENTS.
	STREAM SLOPE: 0.8% OTHER: TAILWATER 1 TW (II)	TOTAL	-	, 3	15.0			ARTS	CÓMI
PROJECT: JOYFUL VIEW SUR	HYDROLOGICAL DATA HYDROLOGICAL DATA B CHANNEL SHAPE: 4.2 STREAM SLU CHANNEL SHAPE: 4.1 3.1 CHANNEL SHAPE: 4.1 3.1 CHANNEL SHAPE: 4.1 3.1 M CHANTEL SHAPE: 4.1 3.1	CULVERT DESCRIPTION:	MATERIAL - SHAPE - SIZE - ENTRANCE		2-Reap - 23"X14" paos		TECHNICAL FOOTNOTES:	(2) HW ₁ /D = HW /D OR HW ₁ /D FROM DESIGN CHARTS (3) FALL = HW ₁ = (EL _{hd} = EL _{el}) , FALL IS ZERO FOR CLIVERTS ON GRADE	SUBSCRIPT DEFINITIONS: - APPROXIMATE I. CULVERT FACE NA. DESIGN NEADWATER NI. HEADWATER IN WILET CONTROL I. NILET CONTROL I. NILET CONTROL I. STREAMSED AT CRAVERT FACE II. TALL WATER

CULVERT DESIGN FORM	DESIGNER / DATE: //	:VATION : 62.23 (11)	L ₃ f ————————————————————————————————————	DED TW	S= S ₀ - FALL/L ₀ Let. S7.09(n)	NO	TROL	AEL OUT CON	2 62.12 62.58 8.0 0.68 FLOW		6) h TW or (d.+D/2)(WHICHEVER IS GREATER)	2/29		CULVERT BARREL SELECTED :	MATERIAL:
200	REV S	ROAD WAY ELEVATION		STREAM BED	8 8		劇	ΞE	2.1 2		- MHICHE	(7) H-[1+h4+ (29n2 L) / R133 V2/29			
		ROADW		CORIGINAL		2	OUTLET CONTROL	2° 3	1.46 0.2		10/2/	, (1) Zu(6		
			E. I.	FALL		HEADWATER CALCULATIONS	OUTL	2 2	1.46		- S &	P ber (25	(0) EL _{ho} * EL _o + H + h _o		
			17	1		R CALC	lt	۵ ₁	1.35			7) H-[-	19) EL.bo		
	_ OF_	(m)-	¥.	1		ADWATE	lt	¥ (5)	1.7			J			
z				25'25		HE		Et hi	8≤.29		- de	(NOIT:	TREAM EPTH IN		
STATION	SHEET	EL _{hd} :-		ELI				FALL	5.0		HW;+ EL;(INVERT OF	ET CONTROL SECTION)	TW BASED ON DOWN STREAM CONTROL OR FLOW DEPTH IN CHANNEL.		
-		*					INLET	I N	268		- HW;+ E	ET CONT	TW BASED ON CONTROL OR CHANNEL.	COMMENTS / DISCUSSION :	
			%0.					HW ₁ /D	121		(4) EL _k	INCE	(S) TW E CONI	TS / DI	
			-	i	(B) WT	FLOW		× =	27.72					MMEN	
S. 6		Y.	STREAM SLOPE;	ER:	4	TOTAL	10	e 🗓	52.4				CHARTS	8	
PROJECT: Joygou View S.		HYDROLOGICAL DATA	DRAINAGE AREA: 45:0 STR		R.I. (YEARS) FLOW(cds) S 7.2 100 52.4	CULVERT DESCRIPTION:	MATERIAL - SHAPE - SIZE - ENTRANCE		2- RCEP 30 XI9" PROS		TECHNICAL FOOTNOTES:	(I) USE Q/NB FOR BOX CULVERTS	(2) HW, /D . HW /D OR HW, /D FROM DESIGN CHARTS (3) FALL * HW, - (EL _{hd} - EL _{el}), FALL IS ZERO FOR CALVERTS ON GRADE	SUBSCRIPT DEFINITIONS: - APPROXIMATE (CULVENT FACE 14. DESIGN MEADWATER	AL REDUNTEN IN NUTLEI CONTROL. 1. HEADWATER IN OUTLET CONTROL. 2. OUTLET CONTROL SECTION 3. STREMBED AT CALVERT FACE 14. TAILWATER

			Desig	n Procedu	re Form: F	Runoff Red	luction					
		_		UD-BMP (Ve	ersion 3.07, Mai	rch 2018)						Sheet 1 of 1
Designer:	Mike Bartuse	k									•	
Company:	Respec											
Date:	September 23										•	
Project:	Joyful View S	Sub - Work She	et 1									
Location:	Joyful View R	Road										
												55.0
SITE INFORMATION (Use	er Input in Bl	lue Cells)								r MHFD D e Denver N		oage RR-8, on.
D # (A D		Rainfall Depth	0.60	inches <							opriate fo	r this site.
Depth of Average Ru	non Producin	ig Storm, a ₆ =	0.43	inches (for w	/atersheds Ou	itside of the L	Denver Region	1, Figure 3-1 i	n USDCM Vo	1. 3)		
Area Type	UIA:RPA	SPA	UIA:RPA	SPA	UIA:RPA	SPA	UIA:RPA	SPA	UIA:RPA	SPA	UIA:RPA	SPA
Area ID	OS2A1	OSA2A2	OS2B1	OS2B2	OS2C1	OS2C2	A3A1	A3A2	A3B1	A3B2	A3C1	A3C2
Downstream Design Point ID	2	2	4	4	9	9	9	10	6	6	11	
Downstream BMP Type												
DCIA (ft ²)									-			
UIA (ft²)	6,400	-	6,400		6,400	-	6,400		6,400		6,400	-
RPA (ft²)	4,000		4,000		4,000	-	4,000		4,000		4,000	
SPA (ft²)		34,850		30,500		21,800		113,250		348,500		57,500
HSG A (%)	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%
HSG B (%)	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%
HSG C/D (%)	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%
Average Slope of RPA (ft/ft)	0.250		0.250	-	0.250	-	0.250		0.250		0.250	
UIA:RPA Interface Width (ft)	400.00		400.00		400.00		400.00		400.00		400.00	
CALCULATED RUNOFF			00001	00000	00001				1001		1001	1000
Area ID	OS2A1	OSA2A2	OS2B1	OS2B2	OS2C1	OS2C2	A3A1	A3A2	A3B1	A3B2	A3C1	A3C2
UIA:RPA Area (ft²)	10,400		10,400		10,400		10,400		10,400		10,400	-
L / W Ratio	0.07		0.07	-	0.07	-	0.07		0.07	-	0.07	
UIA / Area	0.6154		0.6154		0.6154		0.6154		0.6154		0.6154	
Runoff (in)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Runoff (ft ³) Runoff Reduction (ft ³)	267	1743	267	1525	267	1090	267	5663	267	17425	267	2875
Runon Reduction (It.)	201	1743	201	1323	201	1090	201	3003	201	17423	201	2073
CALCULATED WQCV RE	SULTS											
Area ID	OS2A1	OSA2A2	OS2B1	OS2B2	OS2C1	OS2C2	A3A1	A3A2	A3B1	A3B2	A3C1	A3C2
WQCV (ft ³)	OOZATI	00/12/12	OOZDI	OOZDZ	00201	00202	710711	710712	7,001	71002	71001	71002
WQCV Reduction (ft ³)												
WQCV Reduction (%)												
Untreated WQCV (ft ³)												
Omeodica (11 do 1 (11)					Į							
CALCULATED DESIGN F	OINT RESUI	LTS (sums re	sults from a	ll columns w	ith the same	Downstream	n Design Poir	nt ID)				
CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID 2 2 4 4 9 9 Downstream Design Point ID 2 2 4 4 9 9 DCIA (ft²) 0 0 0 0 0 0 UIA (ft²) 6,400 6,400 6,400 12,800 12,800 12,800	9	10	6	6	11							
	0	0	0	0	0							
	12,800	0	6,400	6,400	6,400							
RPA (ft²)	4,000	4,000	4,000	4,000	8,000	8,000	8,000	0	4,000	4,000	4,000	
SPA (ft²)	34,850	34,850	30,500	30,500	21,800	21,800	21,800	113,250	348,500	348,500	0	
Total Area (ft ²)	45,250	45,250	40,900	40,900	42,600	42,600	42,600	113,250	358,900	358,900	10,400	
Total Impervious Area (ft ²)	6,400	6,400	6,400	6,400	12,800	12,800	12,800	0	6,400	6,400	6,400	
WQCV (ft ³)	0	0	0	0	0	0	0	0	0	0	0	
WQCV Reduction (ft ³)	0	0	0	0	0	0	0	0	0	0	0	
WQCV Reduction (%)	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	
Untreated WQCV (ft ³)	0	0	0	0	0	0	0	0	0	0	0	
CALCULATED SITE RES	III TS (eume	resulte from	all columns	in workshoo	.t)							
Total Area (ft²)		Tooung HOIII			*							
Total Impervious Area (ft²)	83,200	1	Per M	IS4 perm	nit page 2	29, this s	should be	e a				
WQCV (ft ³)	0	1			. Check							
WQCV (It*) WQCV Reduction (ft³)	0				et minim							
WQCV Reduction (%)	0%				nal/alter							
Untreated WQCV (ft ³)	0 %	1	with a	iii addiill	niai/ailei	nauve P	DIVIP.					
55alou 11401 (It)		j										

Provide a figure showing all proposed UIA and RPA areas to be utilized for runoff reduction. All RPA areas will need to be within a no build/drainage easement (add to Plat) and discussed in the maintenance agreement and O&M manual. Wetlands are not an acceptable RPA per the MS4 Permit and MHFD guidelines. Also make sure to show RPA limits on GEC Plans (not just FDR) so our SW inspectors and the QSM know that these areas are to remain pervious and vegetated post-construction.

I don't see the value of including SPA's in this spreadsheet as they don't actually contribute to treating any runoff from UIA's. Remove them unless you see value in having them on here and add a discuss of them to the report text above.

			Desig		ure Form: ersion 3.07, Ma	Runoff Red	duction					Sheet 1 of 1
Designer:	Mike Bartuse	k		OD-DIVIE (VE	5.51011 0.01, IVI							SHEEL I OI I
Company:	Respec										-	
Date:	September 23	3. 2022										
Project:		Sub - Work Shee	et 2								-	
Location:	Joyful View F										-	
Location.	Joylar View P										<u>. </u>	
SITE INFORMATION (Us	WQCV F	Rainfall Depth	0.60 0.43	inches inches (for W	/atersheds O	utside of the D	enver Regior	n, Figure 3-1 ir	n USDCM Vol	. 3)		
Area Type	UIA:RPA	SPA										
Area ID	A3D1	A3D2										
Downstream Design Point ID	2	2										
Downstream BMP Type												
DCIA (ft ²)	-											
UIA (ft ²)												
RPA (ft ²)												
SPA (ft²)		10,000										
HSG A (%)		0%										
HSG B (%)		100%						1				
HSG C/D (%)		0%				1	1	ļ				
Average Slope of RPA (ft/ft)								<u> </u>				
UIA:RPA Interface Width (ft)	455.00			<u> </u>			<u> </u>					
CALCULATED RUNOFF Area ID UIA:RPA Area (ft ²)	A3D1	A3D2 										
L / W Ratio												
UIA / Area	0.6402											
Runoff (in)		0.00										
Runoff (ft ³)		0		ļ			ļ					
Runoff Reduction (ft ³)	352	500										
CALCULATED WQCV RE	SULTS											
Area ID	A3D1	A3D2										
WQCV (ft ³)												
WQCV Reduction (ft ³)												
WQCV Reduction (%)												
Untreated WQCV (ft ³)												
CALCULATED DESIGN F	POINT RESUL	LTS (sums res	ults from al	l columns wi	th the same	Downstream	Design Poin	t ID)				
Downstream Design Point ID		2										
DCIA (ft ²)		0										
UIA (ft²)		8,450										
RPA (ft²)		4,750										
SPA (ft²)		10,000										
Total Area (ft ²)	23,200	23,200										
Total Impervious Area (ft ²)		8,450										
WQCV (ft ³)		0										
WQCV Reduction (ft ³)		0										
WQCV Reduction (%)		0%										
Untreated WQCV (ft ³)	0	0		<u> </u>		1	1					
CALCULATED SITE RES		results from a	all columns	in worksheet	:)							
Total Area (ft ²)	46,400]										
Total Impervious Area (ft²)]										
WQCV (ft ³)		1										
WQCV Reduction (ft ³)		1										
WQCV Reduction (%)]										
Untreated WQCV (ft ³)	0]										
WQCV Reduction (ft ³)	0 0%											

- Specify soil mixture on GEC Plans, like is done for seeding and mulching details. Look at Table RR-3 in MHFD Detail T-0 for specific soil characteristics.
- Specify in GEC Plans that RPA vegetation should be turf grass (from seed or sod)
- Specify in GEC Plans that turf grass vegetation should have a uniform density of at least 80%.
- In Drainage Report summarize (if already discussed at length in Soils Report) suitability of topsoil of RPA and steps for proper preparation of RPA soil per recommendations in MHFD detail T-0.
- Provide an O&M manual for the RPAs. See the City's template for grass buffers / grass swales to use as a starting point: https://coloradosprings.gov/stormwater-enterprise/page/operations-and-maintenance-permanent-bmps?mlid=6126
- Note on GEC Plans that irrigation (temp or permanent) is necessary to establish sufficient vegetation and not just weeds.

APPENDIX C

FEMA LOMR

Issue Date: October 2, 2020

Effective Date: February 16, 2021

Case No.: 20-08-0369P

LOMR-APP



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT

	COMMUNITY AND REVISION INFORMATION	PROJECT DESCRIPTION	BASIS OF REQUEST
COMMUNITY	El Paso County Colorado (Unincorporated Areas)	NO PROJECT	HYDRAULIC ANALYSIS HYDROLOGIC ANALYSIS UPDATED TOPOGRAPHIC DATA BASEMAP CHANGES
	COMMUNITY NO.: 080059		
IDENTIFIER	Joyful View Subdivision - Haegler	APPROXIMATE LATITUDE & LONGI SOURCE: USGS QUADRANGLE	
	ANNOTATED MAPPING ENCLOSURES	ANNOTATED S	TUDY ENCLOSURES
TYPE: FIRM*	NO.: 08041C0805G DATE: December 7, 2018	DATE OF EFFECTIVE FLOOD INSUF PROFILE: 451P SUMMARY OF DISCHARGE TAB	

Enclosures reflect changes to flooding sources affected by this revision

* FIRM - Flood Insurance Rate Map;

FLOODING SOURCE AND REVISED REACH

Haegler Main Stem - From approximately 3,330 feet downstream of Peyton Highway to approximately 1,750 feet upstream of Peyton Highway

	SUMMARY OF REVISION	IS		
Flooding Source	Effective Flooding	Revised Flooding	Increases	Decreases
Haegler Main Stem	No BFEs⁺ Zone A	BFEs Zone AE	YES YES	NONE YES
	Zone A	Zone A	YES	YES

* BFEs - Base Flood Elevations

DETERMINATION

This document provides the determination from the Department of Homeland Security's Federal Emergency Management Agency (FEMA) regarding a request for a Letter of Map Revision (LOMR) for the area described above. Using the information submitted, we have determined that a revision to the flood hazards depicted in the Flood Insurance Study (FIS) report and/or National Flood Insurance Program (NFIP) map is warranted. This document revises the effective NFIP map, as indicated in the attached documentation. Please use the enclosed annotated map panels revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals in your community.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.gov/flood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch

Federal Insurance and Mitigation Administration

20-08-0369P

102-I-A-C



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

COMMUNITY INFORMATION

APPLICABLE NFIP REGULATIONS/COMMUNITY OBLIGATION

We have made this determination pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (P.L. 93-234) and in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, P.L. 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65. Pursuant to Section 1361 of the National Flood Insurance Act of 1968, as amended, communities participating in the NFIP are required to adopt and enforce floodplain management regulations that meet or exceed NFIP criteria. These criteria, including adoption of the FIS report and FIRM, and the modifications made by this LOMR, are the minimum requirements for continued NFIP participation and do not supersede more stringent State/Commonwealth or local requirements to which the regulations apply.

COMMUNITY REMINDERS

We based this determination on the 1-percent-annual-chance discharges computed in the submitted hydrologic model. Future development of projects upstream could cause increased discharges, which could cause increased flood hazards. A comprehensive restudy of your community's flood hazards would consider the cumulative effects of development on discharges and could, therefore, indicate that greater flood hazards exist in this area.

Your community must regulate all proposed floodplain development and ensure that permits required by Federal and/or State/Commonwealth law have been obtained. State/Commonwealth or community officials, based on knowledge of local conditions and in the interest of safety, may set higher standards for construction or may limit development in floodplain areas. If your State/Commonwealth or community has adopted more restrictive or comprehensive floodplain management criteria, those criteria take precedence over the minimum NFIP requirements.

We will not print and distribute this LOMR to primary users, such as local insurance agents or mortgage lenders; instead, the community will serve as a repository for the new data. We encourage you to disseminate the information in this LOMR by preparing a news release for publication in your community's newspaper that describes the revision and explains how your community will provide the data and help interpret the NFIP maps. In that way, interested persons, such as property owners, insurance agents, and mortgage lenders, can benefit from the information.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426 Additional Information about the NFIP is available on our website at https://www.fema.gov/flood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

We have designated a Consultation Coordination Officer (CCO) to assist your community. The CCO will be the primary liaison between your community and FEMA. For information regarding your CCO, please contact:

Ms. Jeanine D. Petterson
Director, Mitigation Division
Federal Emergency Management Agency, Region VIII
Denver Federal Center, Building 710
P.O. Box 25267
Denver, CO 80225-0267
(303) 235-4830

STATUS OF THE COMMUNITY NFIP MAPS

We will not physically revise and republish the FIRM and FIS report for your community to reflect the modifications made by this LOMR at this time. When changes to the previously cited FIRM panel(s) and FIS report warrant physical revision and republication in the future, we will incorporate the modifications made by this LOMR at that time.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.gov/flood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

20-08-0369P

102-I-A-C

Case No.: 20-08-0369P



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

PUBLIC NOTIFICATION OF REVISION

A notice of changes will be published in the *Federal Register*. This information also will be published in your local newspaper on or about the dates listed below, and through FEMA's Flood Hazard Mapping website at https://www.floodmaps.fema.gov/fhm/bfe_status/bfe_main.asp

Name: The Gazette

Dates: October 12, 2020 and October 19, 2020

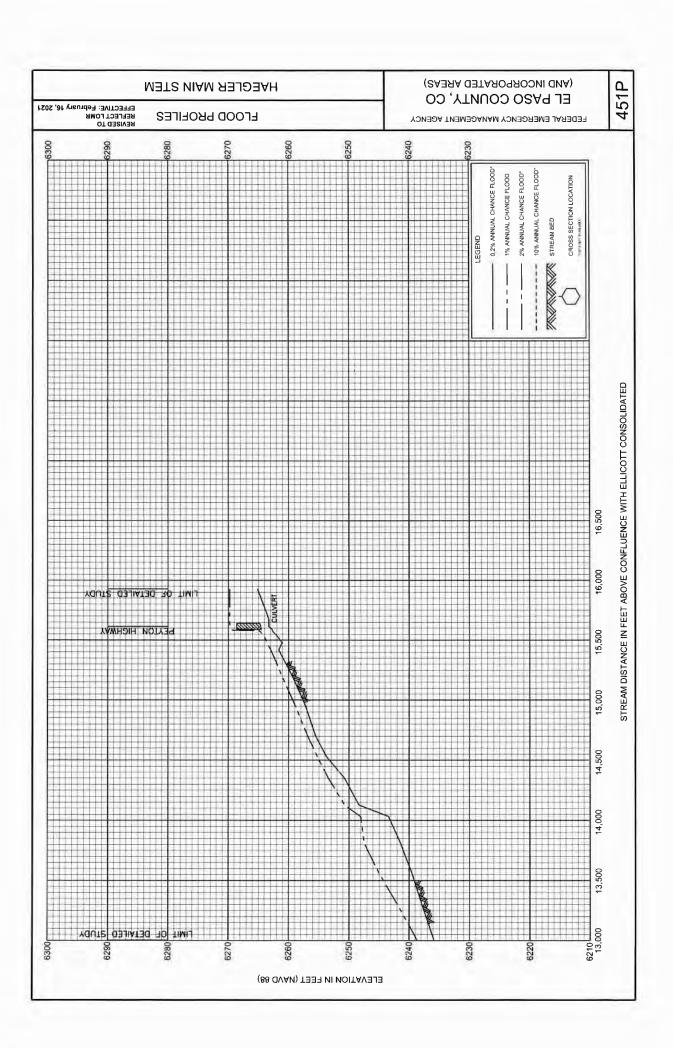
Within 90 days of the second publication in the local newspaper, any interested party may request that we reconsider this determination. Any request for reconsideration must be based on scientific or technical data. Therefore, this letter will be effective only after the 90-day appeal period has elapsed and we have resolved any appeals that we receive during this appeal period. Until this LOMR is effective, the revised flood hazard determination presented in this LOMR may be changed.

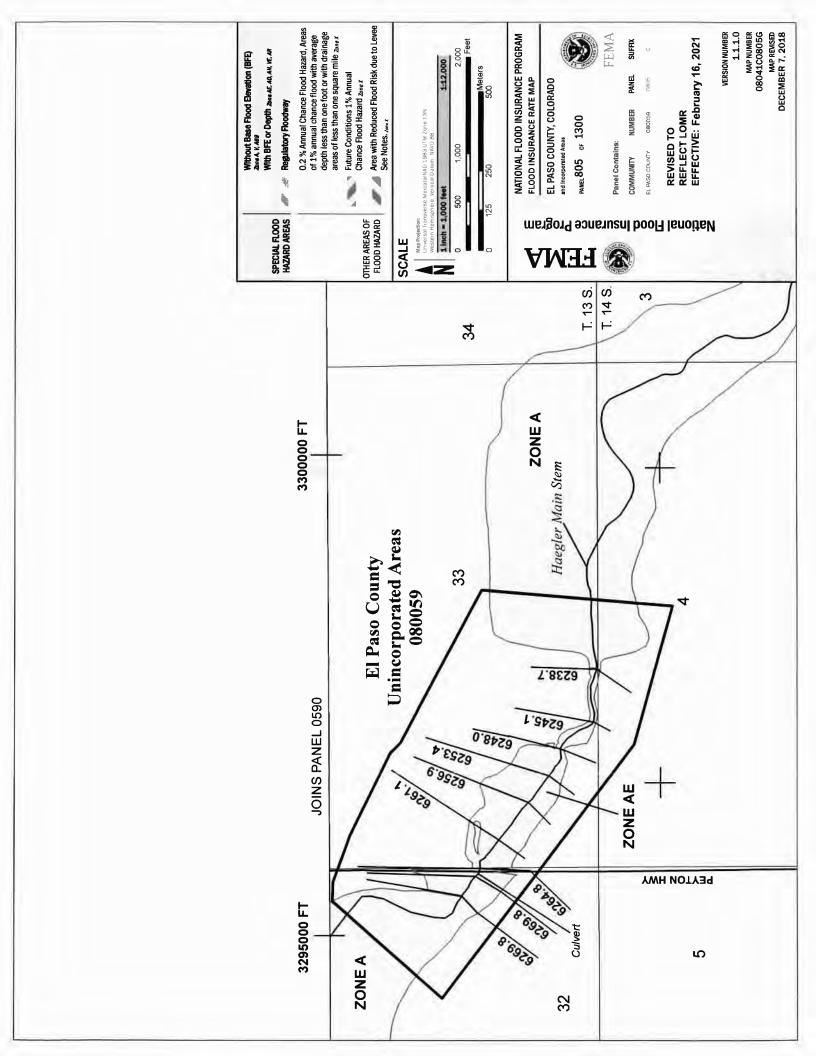
This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.gov/flood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

Table 4. Summary of Discharges (cont.)

Flooding Source and Location	Drainage Area (Square Miles)	-Year	ik Discharges (C	Peak Discharges (Cubic Feet Per Second) 50-Year 100-Year	ond) <u>500-Year</u>	
Fountain Creek Near Colorado Springs, CO At Colorado Springs, CO	103 392	1,300 7,900	2,800 14,300	3,700	6,500 29,400	
At Janitell, CO At Security, CO	413 495	11,800	18,800	22,400 25.800	32,200 39.500	
At Fountain, CO	681	14,700	29,900	39,400	71,300	
Near Pinon, CO	849	10,700	24,200	33,300	66,800	
Franceville Tributary to Jimmy Camp Creek At confluence with Jimmy Camp Creek	926	1,700	2.800	3,500	4,300	
Haegler Main Stem At Peyton Highway At approximately 3,200 feet downstream of Peyton Highway	10.67	17	11	1,862	77	
Haegler Ranch Tributary 1 At Eastonville Road	0.96	7	7	80	7,	1
REVISED Haegler Ranch Tributary 1A At Eastonville Road	0.07	7		70	٦	
Haegler Ranch Tributary 2 At Eastonville Road	96:0	7	٦	40		
Haegler Ranch Tributary 2 At confluence with Geick Ranch West Tributary	1.47	٦	٦	592	٦	
Haegler Ranch Tributary 3 At approximately 2,300 feet upstream of the confluence with Haegler Ranch Tributary 4	60:1	7	7	505	٦	
Haegler Ranch Tributary 4 At approximately 3,700 feet upstream of the confluence with Haegler Ranch Tributary 3	09:0	٦	7	130	Ē	
Jackson Creek At Assembly Road	2.44	7	٦	1,313	7	
¹ Data not available	32		REVISED TO REFLECT LC EFFECTIVE:	REVISED TO REFLECT LOMR EFFECTIVE: February 16, 2021	, 16, 2021	





APPENDIX D DESIGN CHARTS

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-уеаг		25-уеаг		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSGASB	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business								1					1
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0,53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0,22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0,34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas											-	-	
Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets							+						1
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44		0.50

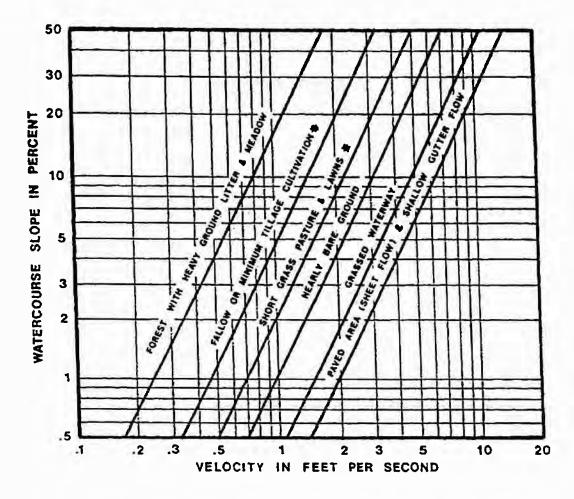


Figure 6-25. Estimate of Average Concentrated Shallow Flow

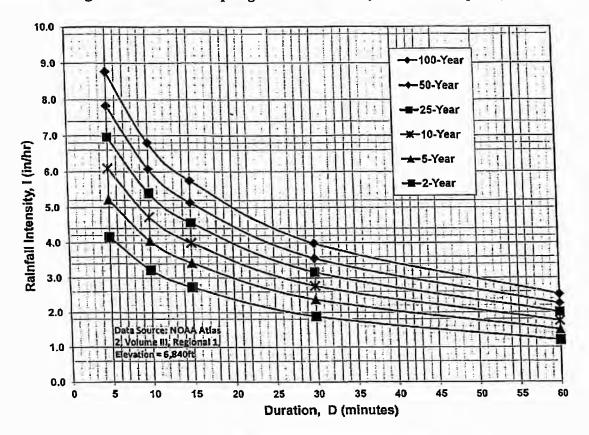


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \text{ ln}(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

