



## **LOT 1, STERLING RECYCLING SUBDIVISION**

DRAINAGE LETTER

PCD FILE NO: PPR2524

ALL TERRAIN ENGINEERING PROJECT NO: 25005

SEPTEMBER 2025

PREPARED FOR:

RHETORIC, LLC

CONTACT: ERIC HOWARD

20 BOULDER CRESCENT STREET, SUITE 200

COLORADO SPRINGS, CO 80903

PREPARED BY:

ALL TERRAIN ENGINEERING LLC

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## ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



09/11/2025

\_\_\_\_\_  
Nicholas Q. Jokerst, PE

\_\_\_\_\_  
Date

State of Colorado No. 59273

For and on behalf of All Terrain Engineering LLC

## DEVELOPER'S STATEMENT

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

09/11/2025

\_\_\_\_\_  
Eric Howard

\_\_\_\_\_  
Date

Rhetoric, LLC

20 Boulder Crescent Street, Suite 200, Colorado Springs, CO 80903

## EL PASO COUNTY ONLY

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

\_\_\_\_\_  
Joshua Palmer, P.E.

\_\_\_\_\_  
Date

County Engineer/ECM Administrator

Conditions:



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## I. General Purpose, Location & Description

### a. Purpose

The purpose of this Drainage Letter for LOT 1, STERLING RECYCLING SUBDIVISION is to demonstrate conformance with the approved *Final Drainage Report for Sterling Ranch Recycling Facility* (PCD File No: PPR2341 & SF2325). The *Final Drainage Report for Sterling Ranch Recycling Facility (FDRSRRF)* was completed with the final plat for the Sterling Recycling Subdivision and it described the site's onsite and offsite drainage patterns, existing and proposed storm infrastructure, and methods to safely route developed stormwater to adequate outfalls.

### b. Location

LOT 1, STERLING RECYCLING SUBDIVISION, referred to as 'the site' herein, is in the northwest quarter of the northwest quarter of Section 4 and the north half of Section 5, Township 13 South, Range 65 West of the 6th P.M., El Paso County, Colorado. The site was platted in El Paso County as Lot 1 of Sterling Recycling Subdivision on October 14, 2024. The site is bound by Marksheffel Road to the east and north, Lot 2 Sterling Recycling Subdivision to the west and unplatted parcels to the south. A vicinity map is presented in Appendix A.

### c. Description of Property

The site is approximately 4.74 acres of undeveloped land. The site is currently used as an asphalt and concrete recycling facility. The site has sparse vegetation around its perimeter but otherwise is compacted dirt and gravel. The approximate disturbed area is 9.15 acres. The additional disturbance beyond the site acreage is for improvements to Sterling Ranch Road, Marksheffel Road and the construction of Pond A, located in Tract A. In general, the site slopes southerly towards an existing 8' berm along the site's southern boundary. Onsite elevations range from 6,977' – 6,987' with slopes ranging 1 – 50%. Per a NRCS soil survey, the site is made up of Type A Blakeland loamy sand and Type A Columbine gravelly sandy loam. The NRCS soil survey is presented in Appendix A.

There are no major drainageways or irrigation facilities that traverse the site nor does the site fall within the Streamside Overlay Zone. The ultimate receiving waters for the site are Sand Creek. Existing, on-site utilities are limited to an 8" water line located within Sterling Ranch Road. An existing, off-site storm sewer system parallels the site's northern boundary along Marksheffel Road.

### d. Floodplain Statement

Based on FEMA Firm map 08041C0533G dated December 7, 2018, the site is Zone X. Zone X is defined as area outside the Special Flood Hazard Zone (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood.

## II. Drainage Basins

### a. Major Basin Description

The site is located within the upper Sand Creek Drainage Basin per the "Sand Creek Drainage Basin Planning Study" completed by Kiowa Engineering Corporation in January 1993, revised March 1996.

### b. Existing Subbasin Description

The site's existing drainage patterns are unchanged from those identified in the *FDRSRRF*. The site is contained within Basin EXE and Basin EXF. Basins EXE and EXF are captured at DP7.1 and DP9.1, respectively. Both basins concentrate offsite to the east in an existing natural stream section and discharge to Sand Creek. The existing drainage map is presented in Appendix F. The existing basin descriptions are presented in Appendix E.

### c. Proposed Subbasin Description

The *FDRSRRF* analyzed the site for an interim and ultimate condition. In the interim condition, the site was analyzed as a recycling facility. In the ultimate condition, the site was analyzed as heavy industrial (90%) impervious. The interim condition was used to size swales and inlets. However, the ultimate condition was used for the sizing of Pond A and the outfall infrastructure. Therefore, the outlet structure orifice plate will be sized & installed for the ultimate condition. The basin descriptions below will verify the sizing of swales and inlets per the revised ultimate condition of the site. Additionally, the basin descriptions will verify that the revised hydrologic parameters are in conformance the original Pond A design from *FDRSRRF*. The site's proposed grading and proposed drainage patterns are unchanged from those identified in the *FDRSRRF*. The site is contained within Basin E and Basin D.

Basin D is 2.16 acres of asphalt, self-storage units and landscaping. Basin D has a composite percent impervious of 73%, which is less than the assumed 90% from *FDRSRRF*. Therefore, Basin D is in conformance with the design of Pond A and will receive the required full spectrum water quality and detention therein. Runoff from this basin sheet flows overland southeast to a proposed swale that directs flow to DP5 ( $Q_5 = 5.8$  cfs  $Q_{100} = 11.5$  cfs). Runoff from DP5 is combined at the proposed Type C sump inlet at DP7.1 ( $Q_5 = 7.8$  cfs  $Q_{100} = 18.3$  cfs). Compared to the *FDRSRRF*, Basin D flow has increased (Original:  $Q_5 = 0.5$  cfs  $Q_{100} = 3.7$  cfs, Revised:  $Q_5 = 5.8$  cfs  $Q_{100} = 11.5$  cfs). The increase in flow can be attributed to the interim v. ultimate conditions analysis. The original hydrologic calculations were performed on the interim condition. The hydrologic analysis present in this report reflects the ultimate condition. For this reason, swale and inlet capacity calculations are provided in Appendix C to demonstrate the increased flow can be conveyed & captured by the swale and Type C inlet proposed by *FDRSRRF*. The DP5 swale conveys Basin D flow at 2.85 ft/s, a subcritical Froude number of 0.47 and with 0.84' of freeboard. The inlet capacity of the DP7.1 Type C inlet is  $Q_5 = 15.7$  cfs and  $Q_{100} = 18.4$ , cfs which exceeds the site's design flow at DP7.1.

Basin E is 3.10 acres of asphalt roadway, gravel, self-storage units and landscaping. Basin E has a composite percent impervious of 32%, which is less than the assumed 90% from *FDRSRRF*. Therefore, Basin E is in conformance with the design of Pond A and will receive the required full spectrum water quality and detention therein. Runoff from this basin sheet flows overland southeast to a proposed swale that directs flow to DP6 ( $Q_5 = 3.1$  cfs  $Q_{100} = 8.6$  cfs). Runoff from DP6 is combined at the proposed Type C sump inlet at DP7.1 ( $Q_5 = 7.8$  cfs  $Q_{100} = 18.3$  cfs). Compared to the *FDRSRRF*, Basin E flow has increased (Original:  $Q_5 = 2.2$  cfs  $Q_{100} = 7.1$  cfs, Revised:  $Q_5 = 3.1$  cfs  $Q_{100} = 8.6$  cfs). The increase in flow can be attributed to the interim v. ultimate conditions analysis. The original hydrologic calculations were performed on the interim condition. The hydrologic analysis present in this report reflects the ultimate condition. For this reason, swale and inlet capacity calculations are provided in Appendix C to demonstrate the increased flow can be conveyed &

captured by the swale and Type C inlet proposed by *FDRSRRF*. The DP6 swale conveys Basin D flow at 2.60 ft/s, a subcritical Froude number of 0.45 and with 0.95' of freeboard. The inlet capacity of the DP7.1 Type C inlet is  $Q_5 = 15.7$  cfs and  $Q_{100} = 18.4$ , cfs which exceeds the site's design flow at DP7.1.

Basin OS2 is 0.36 acres of offsite, undeveloped area. Basin OS2 is unchanged from the *FDRSRRF* and is shown to accurately quantify the flow at DP7.1. Basin OS2 stormwater ( $Q_5 = 0.1$  cfs  $Q_{100} = 0.8$  cfs) flows to DP7.1 and is captured by the Type C sump inlet.

In the event of inlet failure, the Type C sump inlet at DP7.1 would overtop the Pond A berm and overland flow directly into Pond A.

### III. Drainage Design Criteria

#### a. Development Criteria Reference

The drainage analysis follows the criteria from the "Drainage Criteria Manual County of El Paso, Colorado" Volumes 1 and 2," as amended.

#### b. Hydrologic Criteria

Hydrologic data was obtained from the "City of Colorado Springs Drainage Criteria Manual – Chapter 6 Hydrology" adopted by El Paso County.

#### d. Hydraulic Criteria

Hydraulic criteria for open channel analysis are obtained from EPCDCM Chapter 9 – Culvert Design & Chapter 10 - Open Channels and Structures.

### IV. Drainage Facility Design

#### a. General Concept

Onsite stormwater will be conveyed via grass lined swales to a Type C sump inlet. Captured stormwater will be piped to and detained in Pond A; a private, full spectrum water quality and detention pond. The ultimate receiving waters for the site are Sand Creek.

#### b. Water Quality & Detention

Water quality and detention for Basins D, E & OS2 are provided in Pond A. The approved design of Pond A accounted for Basin D and E at 90% impervious and Basin OS2 at 2% composite impervious. Based upon the proposed site plan for the Rhetoric Self Storage site, Basin D, E and OS2 have composite impervious values of 58.3%, 29.8% and 2%, respectively. Therefore, Basin D, E and OS2 are in conformance with the approved Pond A design. The approved, ultimate condition pond design calculations from *FDRSRRF* are presented in Appendix D.

#### c. Operations & Maintenance

The Stormwater Management Facility Operation and Maintenance Plan was approved with the Sterling Recycling Subdivision final plat and can be accessed under PCD File No: PPR2341 & SF2325.



d. **Grading & Erosion Control Plan**

The Sterling Recycling Facility Grading and Erosion Control Plan was approved on May 3, 2024, and includes all disturbed area associated with this Drainage Letter. Proposed grading and drainage patterns are unchanged from the approved Sterling Recycling Facility Grading and Erosion Control Plan.

e. **Drainage Basin & Bridge Fees**

Drainage and bridge fees were paid with the plat recordation of Sterling Recycling Subdivision.

f. **Engineer's Opinion of Probable Cost**

An engineer's opinion of probable cost was approved with the *Final Drainage Report for Sterling Ranch Recycling Facility* (PCD File No: PPR2341 & SF2325. There are no proposed changes to the approved OPC.

## V. Summary

LOT 1, STERLING RECYCLING SUBDIVISION remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements. The proposed development will not adversely affect downstream stormwater infrastructure or surrounding developments. This report meets the latest El Paso County Drainage criteria and is in conformance with the *Final Drainage Report for Sterling Ranch Recycling Facility* (PCD File No: PPR2341 & SF2325).

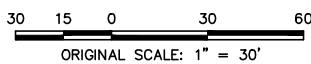
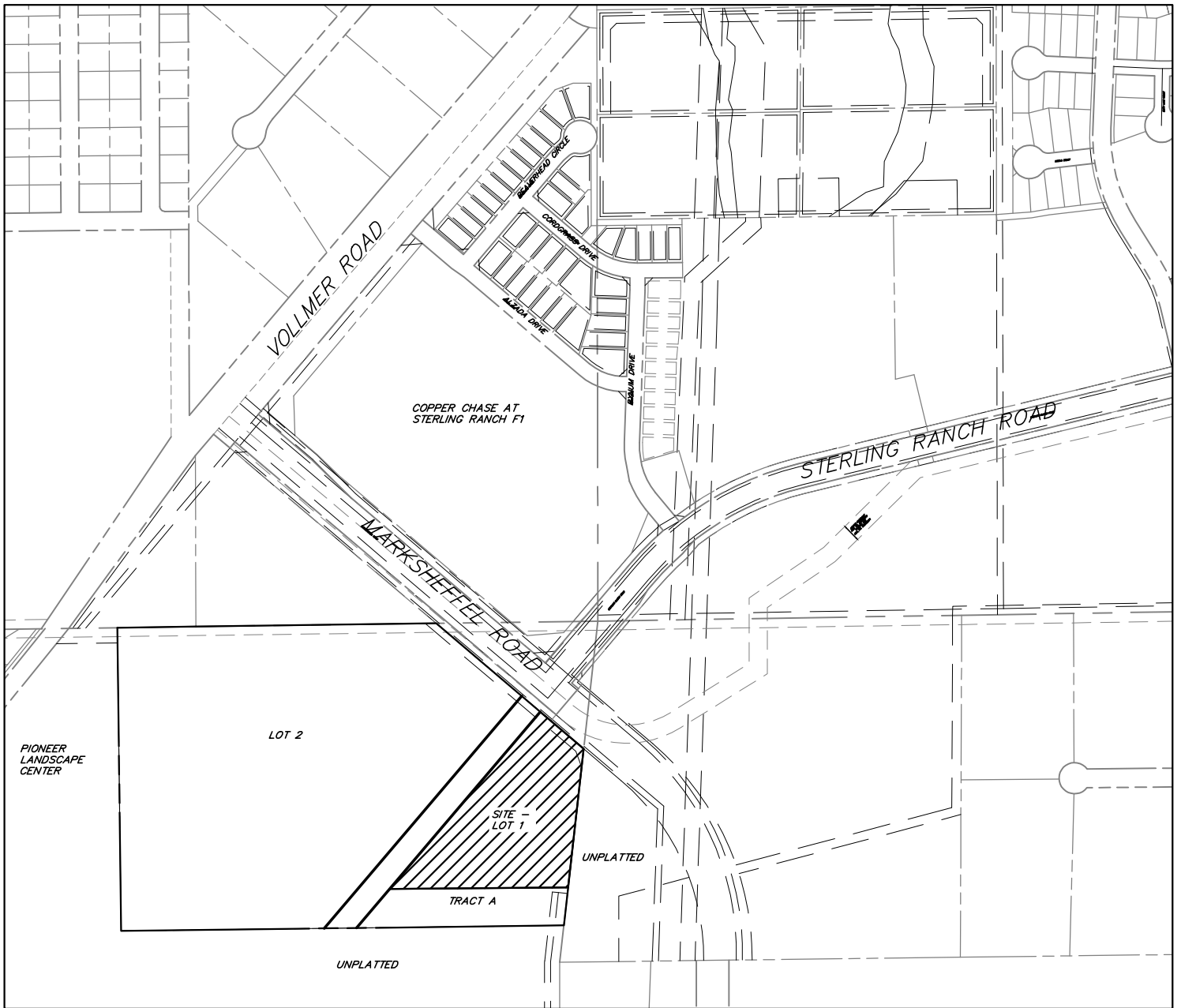
## VI. References


1. Drainage Criteria Manual of El Paso County, Revised October 2018.
2. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
3. Final Drainage Report for Sterling Ranch Recycling Facility, July 2014, JR Engineering, LLC.
4. Web Soil Survey, Natural Resources Conservation Service - <https://websoilsurvey.nrcs.usda.gov/app/>



## **APPENDIX A – VICINITY MAP & NRCS WEB SOIL SURVEY**

# LOT 1, STERLING RECYCLING SUBDIVISION VICINITY MAP

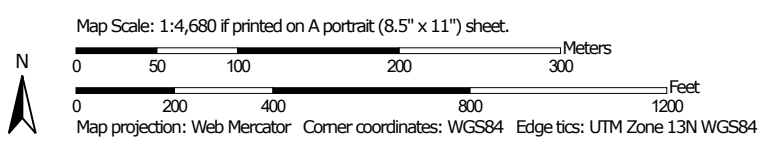


VICINITY MAP		 <b>ALL TERRAIN</b> ENGINEERING 1004 WEST VAN BUREN STREET COLORADO SPRINGS, CO 80907
LOT 1, STERLING RECYCLING SUBDIVISION		
JOB NO. 25005		
LOCATION: EPC	SHEET	
07/15/2025	SHEET: 1	

Hydrologic Soil Group—El Paso County Area, Colorado




Soil Map may not be valid at this scale.



### MAP LEGEND

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**

-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	46.2	51.5%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	43.6	48.5%
<b>Totals for Area of Interest</b>			<b>89.8</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



## **APPENDIX B – HYDROLOGIC CALCULATIONS**

**Subdivision:** Rhetoric Self Storage  
**Location:** El Paso County  
**Project Name:** Rhetoric Self Storage  
**Project Number:** 25005  
**Calculated By:** NQJ  
**Checked By:** REB  
**Date:** 7/21/2025

PROPOSED CALCS - BASIN SUMMARY TABLE							
Tributary Sub-basin	Area (acres)	Percent Impervious	C <sub>5</sub>	C <sub>100</sub>	t <sub>c</sub> (min)	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
D	2.16	73%	0.68	0.79	10.9	5.8	11.5
E	3.10	32%	0.32	0.53	19.4	3.1	8.6
OS2	0.36	2%	0.09	0.36	15.1	0.1	0.8

DESIGN POINT SUMMARY TABLE		
DP#	Q <sub>5-YR</sub>	Q <sub>100-YR</sub>
5	5.8	11.5
6	3.1	8.6
7	0.1	0.8
7.1	7.8	18.3

### COMPOSITE % IMPERVIOUS CALCULATIONS - PROPOSED CONDITIONS

Subdivision: Rhetoric Self Storage  
 Location: El Paso County

Project Name: Rhetoric Self Storage  
 Project No.: 25005.00  
 Calculated By: NQJ  
 Checked By: REB  
 Date: 7/21/25

Basin ID	Total Area (ac)	Gravel Drives				Paved				Roofs				Landscaped				Weighted C <sub>5</sub> & C <sub>100</sub>		Basins Total Weighted % Imp.
		C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	
D	2.16	0.59	0.70	0.00	80.0%	0.90	0.96	1.56	100.0%	0.73	0.81	0.00	90.0%	0.09	0.36	0.60	2.0%	0.68	0.79	72.8%
E	3.10	0.59	0.70	0.31	80.0%	0.90	0.96	0.69	100.0%	0.73	0.81	0.00	90.0%	0.09	0.36	2.10	2.0%	0.32	0.53	31.6%
OS2	0.36	0.59	0.70	0.00	80.0%	0.90	0.96	0.00	100.0%	0.73	0.81	0.00	90.0%	0.09	0.36	0.36	2.0%	0.09	0.36	2.0%
<b>Total</b>	<b>5.62</b>																			<b>45.5%</b>

## STANDARD FORM SF-2 - PROPOSED CONDITIONS TIME OF CONCENTRATION

Subdivision: Rhetoric Self Storage  
Location: El Paso County

Project Name: Rhetoric Self Storage  
Project No.: 25005.00  
Calculated By: NQJ  
Checked By: REB  
Date: 7/21/25

SUB-BASIN DATA					INITIAL/OVERLAND (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )					t <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Weighted C <sub>s</sub>	Impervious (%)	L (ft)	S <sub>o</sub> (%)	t <sub>i</sub> (min)	L <sub>t</sub> (ft)	S <sub>t</sub> (%)	K	VEL. (ft/s)	t <sub>t</sub> (min)	COMP. t <sub>c</sub> (min)	TOTAL LENGTH (ft)	Urbanized t <sub>c</sub> (min)	t <sub>c</sub> (min)
D	2.16	A	0.68	72.8%	215	3.0%	7.8	400	1.2%	20.0	2.1	3.1	10.9	615.0	16.9	10.9
E	3.10	A	0.32	31.6%	100	1.2%	13.3	910	1.5%	20.0	2.4	6.2	19.4	1010.0	29.8	19.4
OS2	0.36	A	0.09	2.0%	115	3.0%	13.6	300	3.0%	20.0	3.5	1.4	15.1	415.0	28.8	15.1

**NOTES:**

$$t_c = t_i + t_t$$

Where:

t<sub>c</sub> = computed time of concentration (minutes)

t<sub>i</sub> = overland (initial) flow time (minutes)

t<sub>t</sub> = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

t<sub>t</sub> = channelized flow time (travel time, min)

L<sub>t</sub> = waterway length (ft)

S<sub>o</sub> = waterway slope (ft/ft)

V<sub>t</sub> = travel time velocity (ft/sec) = K√S<sub>o</sub>

K = NRCS conveyance factor (see Table 6-2).

$$\text{Eq } t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_o^{0.33}}$$

Where:

t<sub>i</sub> = overland (initial) flow time (minutes)

C<sub>s</sub> = runoff coefficient for 5-year frequency (from Table 6-4)

L<sub>i</sub> = length of overland flow (ft)

S<sub>o</sub> = average slope along the overland flow path (ft/ft).

$$\text{Equation 6-4 } t_c = 1.49 S_o^{-1.48} L^{0.76} + \frac{L_t}{60(14i + 9)\sqrt{S_o}}$$

Where:

t<sub>c</sub> = minimum time of concentration for first design point when less than t<sub>c</sub> from Equation 6-1.

L<sub>t</sub> = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S<sub>o</sub> = slope of the channelized flow path (ft/ft).

Equation 6-3

Equation 6-5

**Table 6-2. NRCS Conveyance factors, K**

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Use a minimum t<sub>c</sub> value of 5 minutes for urbanized areas and a minimum t<sub>c</sub> value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

**STANDARD FORM SF-3 - PROPOSED CONDITIONS**  
**STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Rhetoric Self Storage

Location: El Paso County

Design Storm: 5-Year

Project Name: Rhetoric Self Storage

Project No.: 25005.00

Calculated By: NQJ

Checked By: REB

Date: 7/21/25

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS	
		Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t <sub>c</sub> (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)		t <sub>t</sub> (min)
	5	D	2.16	0.68	10.9	1.46	3.99	5.8															BASIN D FLOW CAPTURED IN DP5 SWALE, CAPTURED BY TYPE C INLET @ DP7.1, PIPE TO FULL SPECTRUM POND A
	6	E	3.10	0.32	19.4	0.99	3.13	3.1															BASIN E FLOW CAPTURED IN DP6 SWALE, CAPTURED BY TYPE C INLET @ DP7.1, PIPE TO FULL SPECTRUM POND A
	7	OS2	0.36	0.09	15.1	0.03	3.52	0.1															BASIN E FLOW CAPTURED IN DP6 SWALE, CAPTURED BY TYPE C INLET @ DP7.1, PIPE TO FULL SPECTRUM POND A
	7.1								19.4	2.48	3.13	7.8											TOTAL FLOW FROM BASIN D, E & OS2, PIPE TO FULL SPECTRUM POND A

**Notes:**  
Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

IDF Equations
$I_{100} = -2.52 \ln(D) + 12.735$
$I_{50} = -2.25 \ln(D) + 11.375$
$I_{25} = -2.00 \ln(D) + 10.111$
$I_{10} = -1.75 \ln(D) + 8.847$
$I_5 = -1.50 \ln(D) + 7.583$
$I_2 = -1.19 \ln(D) + 6.035$
<small>Note: Values calculated by equations may not precisely duplicate values read from figure.</small>

**STANDARD FORM SF-3 - PROPOSED CONDITIONS**  
**STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Rhetoric Self Storage  
Location: El Paso County  
Design Storm: 100-Year

Project Name: Rhetoric Self Storage  
Project No.: 25005.00  
Calculated By: NQJ  
Checked By: REB  
Date: 7/21/25

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	$t_c$ (min)	C*A (ac)	$I$ (in/hr)	$Q_i$ (cfs)	$t_c$ (min)	C*A (ac)	$I$ (in/hr)	$Q_i$ (cfs)	$Q_{street}$ (cfs)	C*A (ac)	Slope (%)	$Q_{pipe}$ (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_r$ (min)	
	5	D	2.16	0.79	10.9	1.71	6.71	11.5															BASIN D FLOW CAPTURED IN DP5 SWALE, CAPTURED BY TYPE C INLET @ DP7.1, PIPE TO FULL SPECTRUM POND A
	6	E	3.10	0.53	19.4	1.64	5.26	8.6															BASIN E FLOW CAPTURED IN DP6 SWALE, CAPTURED BY TYPE C INLET @ DP7.1, PIPE TO FULL SPECTRUM POND A
	7	OS2	0.36	0.36	15.1	0.13	5.90	0.8															BASIN E FLOW CAPTURED IN DP6 SWALE, CAPTURED BY TYPE C INLET @ DP7.1, PIPE TO FULL SPECTRUM POND A
	7.1								19.4	3.48	5.26	18.3											TOTAL FLOW FROM BASIN D, E & OS2, PIPE TO FULL SPECTRUM POND A

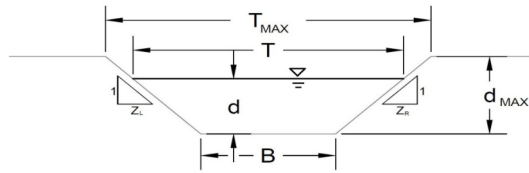
**Notes:**  
Street and Pipe C\*A values are determined by  $Q/i$  using the catchment's intensity value.



## **APPENDIX C – HYDRAULIC CALCULATIONS**

## AREA INLET IN A SWALE

**Rhetoric Self Storage**  
**DP7.1**



This worksheet uses the NRCS vegetat retardance method to determine Manning's n for grass-lined channels.

An override Manning's n can be entered for other channel materials.

Analysis of Trapezoidal Channel (Grass-Lined uses SCS Method)			A, B, C, D, or E =	
NRCS Vegetal Retardance (A, B, C, D, or E)			n =	0.030
Manning's n (Leave cell D16 blank to manually enter an n value)			S <sub>0</sub> =	0.0100 ft/ft
Channel Invert Slope			B =	0.00 ft
Bottom Width			Z1 =	3.00 ft/ft
Left Side Slope			Z2 =	3.00 ft/ft
Right Side Sloe			Choose One:	
Check one of the following soil types:			<input checked="" type="checkbox"/> Non-Cohesive <input type="checkbox"/> Cohesive <input type="checkbox"/> Paved	
Soil Type:	Max. Velocity (V <sub>MAX</sub> )	Max Froude No. (F <sub>MAX</sub> )		
Non-Cohesive	5.0 fps	0.60		
Cohesive	7.0 fps	0.80		
Paved	N/A	N/A		
Maximum Allowable Top Width of Channel for Minor & Major Storm			T <sub>MAX</sub> =	
Maximum Allowable Water Depth in Channel for Minor & Major Storm			d <sub>MAX</sub> =	
			Minor Storm	Major Storm
			9.00	12.00
			1.50	2.00
			ft	
			ft	
Allowable Channel Capacity Based On Channel Geometry				
MINOR STORM Allowable Capacity is based on Depth Criterion			Minor Storm	Major Storm
MAJOR STORM Allowable Capacity is based on Depth Criterion			26.7	57.5
			1.50	2.00
			cfs	
			ft	
Water Depth in Channel Based On Design Peak Flow				
Design Peak Flow			Q <sub>o</sub> =	
Water Depth			d =	
			7.8	18.3
			0.95	1.30
			cfs	
			ft	
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'				
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'				

## AREA INLET IN A SWALE

**Rhetoric Self Storage**  
**DP7.1**

Inlet Design Information (Input)																					
Type of Inlet <span style="float: right;">CDOT Type C</span>	Inlet Type = <span style="float: right;">CDOT Type C</span>																				
Angle of Inclined Grate (must be <= 30 degrees)	$\theta = 0.00$ degrees																				
Width of Grate	$W = 3.00$ ft																				
Length of Grate	$L = 3.00$ ft																				
Open Area Ratio	$A_{RATIO} = 0.70$																				
Height of Inclined Grate	$H_B = 0.00$ ft																				
Clogging Factor	$C_f = 0.50$																				
Grate Discharge Coefficient	$C_d = 0.96$																				
Orifice Coefficient	$C_o = 0.64$																				
Weir Coefficient	$C_w = 2.05$																				
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <th></th> </tr> </thead> <tbody> <tr> <td><math>d =</math></td> <td style="text-align: center;">0.95</td> <td style="text-align: center;">1.30</td> <td></td> </tr> <tr> <td><math>Q_a =</math></td> <td style="text-align: center;"><b>15.7</b></td> <td style="text-align: center;"><b>18.4</b></td> <td style="text-align: right;">cfs</td> </tr> <tr> <td><math>Q_b =</math></td> <td style="text-align: center;"><b>0.0</b></td> <td style="text-align: center;"><b>0.0</b></td> <td style="text-align: right;">cfs</td> </tr> <tr> <td><math>C\% =</math></td> <td style="text-align: center;"><b>100</b></td> <td style="text-align: center;"><b>100</b></td> <td style="text-align: right;">%</td> </tr> </tbody> </table>		MINOR	MAJOR		$d =$	0.95	1.30		$Q_a =$	<b>15.7</b>	<b>18.4</b>	cfs	$Q_b =$	<b>0.0</b>	<b>0.0</b>	cfs	$C\% =$	<b>100</b>	<b>100</b>	%
	MINOR	MAJOR																			
$d =$	0.95	1.30																			
$Q_a =$	<b>15.7</b>	<b>18.4</b>	cfs																		
$Q_b =$	<b>0.0</b>	<b>0.0</b>	cfs																		
$C\% =$	<b>100</b>	<b>100</b>	%																		
Total Inlet Interception Capacity (assumes clogged condition)																					
Bypassed Flow																					
Capture Percentage = $Q_a/Q_o$																					

**Warning 04: Froude No. exceeds USDCM Volume I recommendation.**

# Channel Report

## Swale DP5 (Q100 = Basin D = 11.5 cfs)

### Triangular

Side Slopes (z:1) = 3.00, 3.00

Total Depth (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.035

### Calculations

Compute by: Known Q

Known Q (cfs) = 11.50

### Highlighted

Depth (ft) = 1.16

Q (cfs) = 11.50

Area (sqft) = 4.04

Velocity (ft/s) = 2.85

Wetted Perim (ft) = 7.34

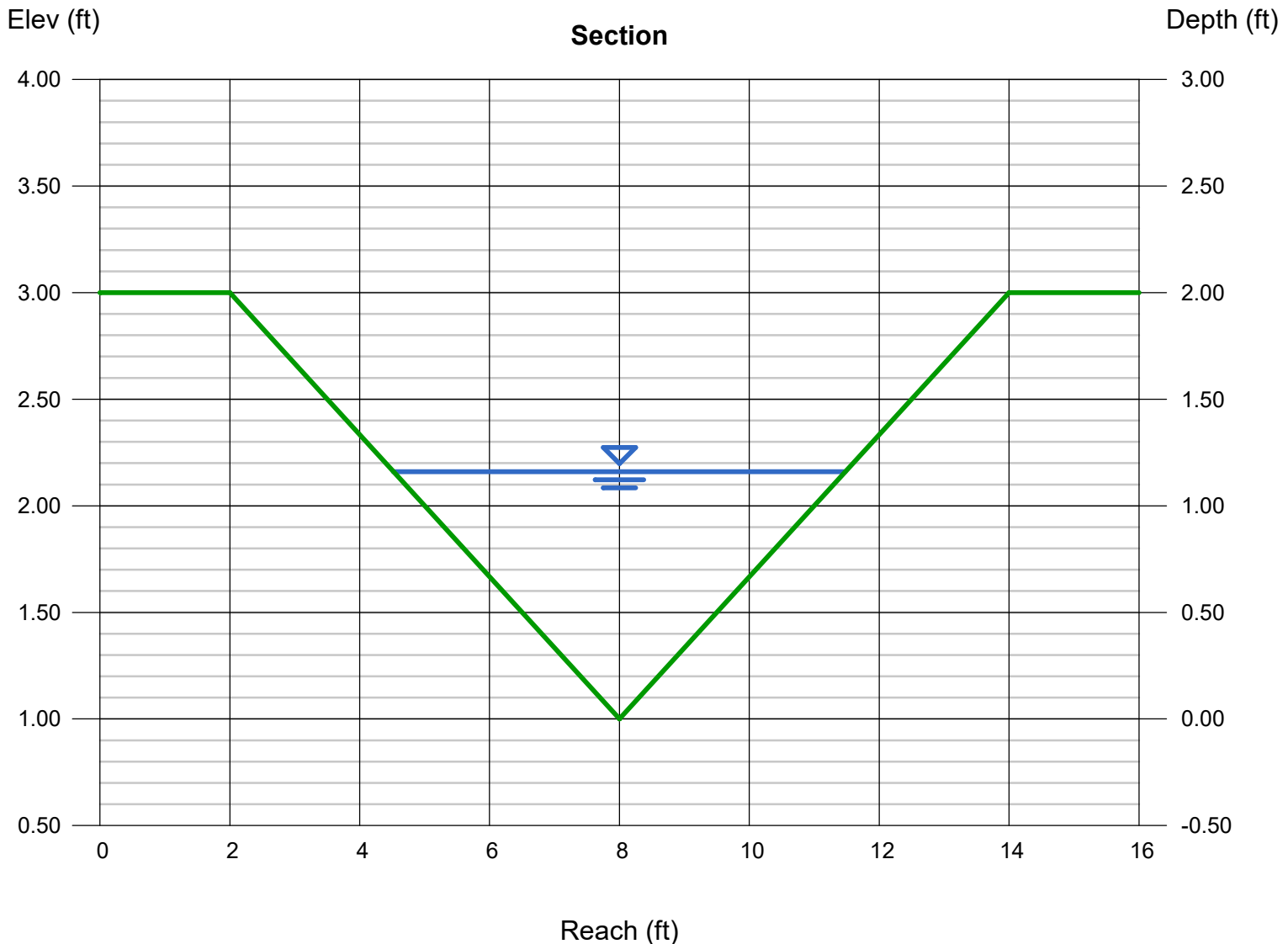
Crit Depth, Yc (ft) = 0.99

Top Width (ft) = 6.96

EGL (ft) = 1.29

$$\text{Froude} = v / \sqrt{g*d}$$

$$= 2.85 / \sqrt{32.2 * 1.16} = 0.47 \rightarrow \text{subcritical}$$



# Channel Report

## Swale DP6 (Q100 = Basin E = 8.6 cfs)

### Triangular

Side Slopes (z:1) = 3.00, 3.00

Total Depth (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.035

### Calculations

Compute by: Known Q

Known Q (cfs) = 8.60

### Highlighted

Depth (ft) = 1.05

Q (cfs) = 8.600

Area (sqft) = 3.31

Velocity (ft/s) = 2.60

Wetted Perim (ft) = 6.64

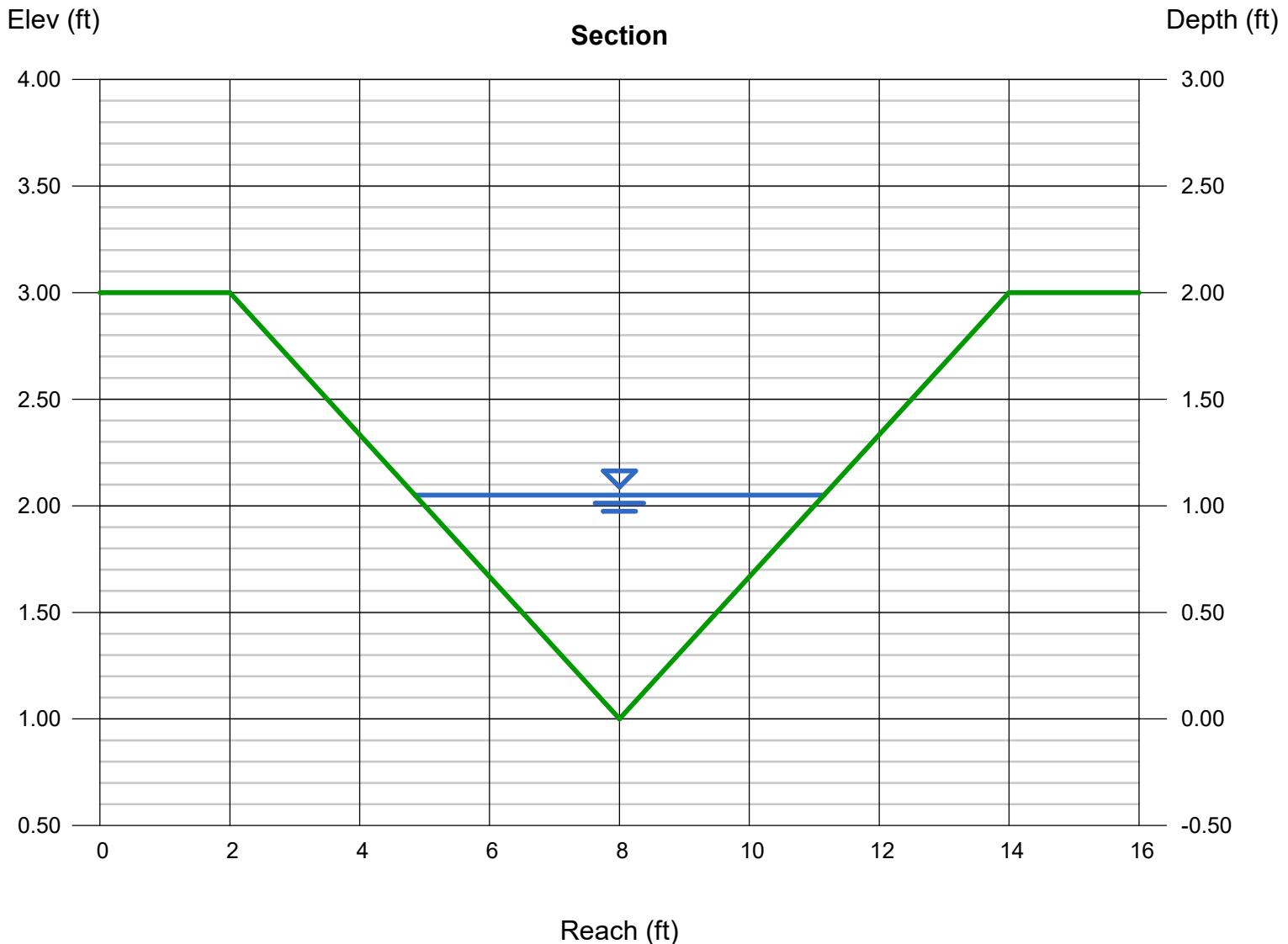
Crit Depth, Yc (ft) = 0.88

Top Width (ft) = 6.30

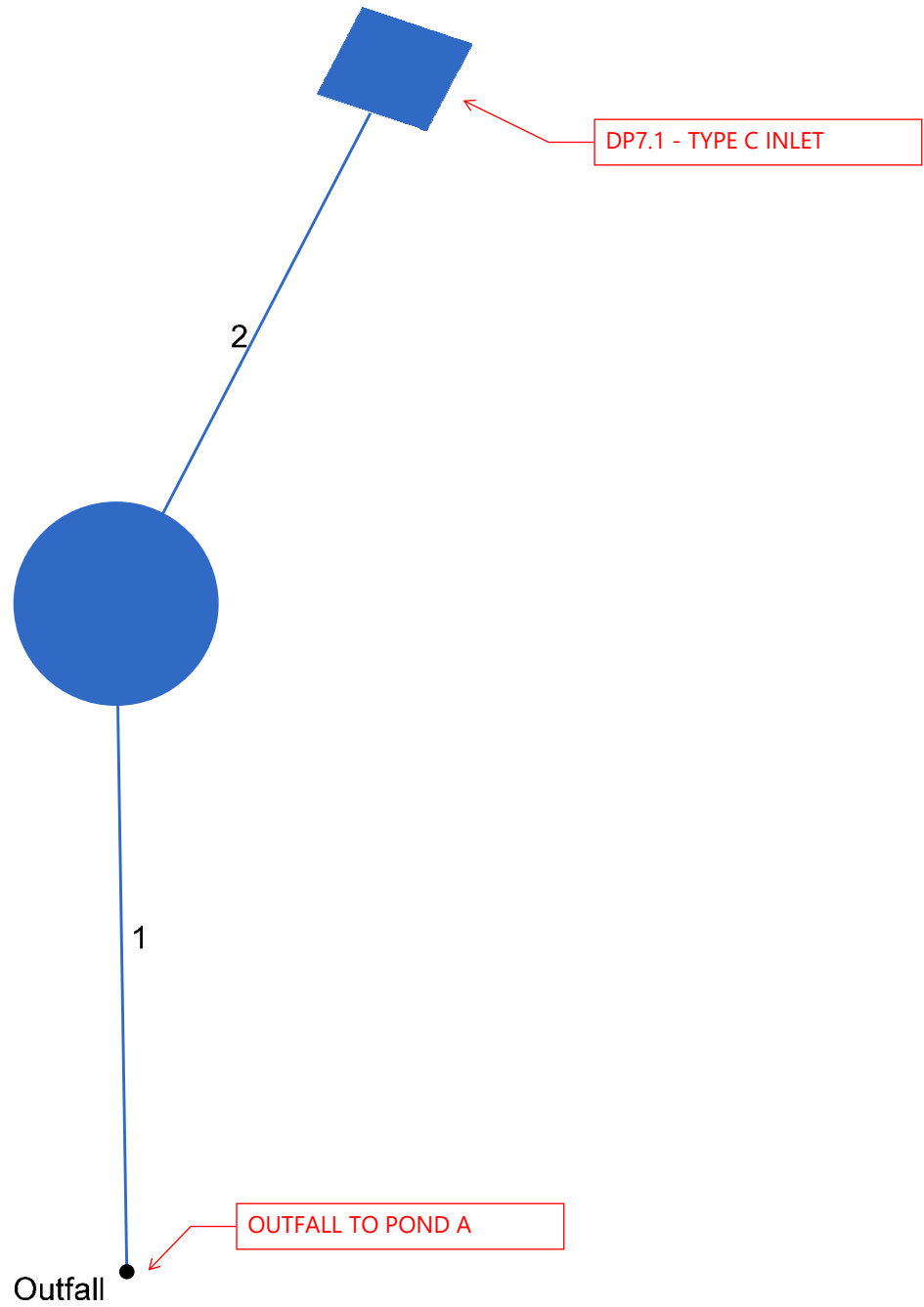
EGL (ft) = 1.16

$$\text{Froude} = v / \sqrt{g*d}$$

$$= 2.60 / \sqrt{32.2 * 1.05} = 0.45 \rightarrow \text{subcritical}$$



# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan

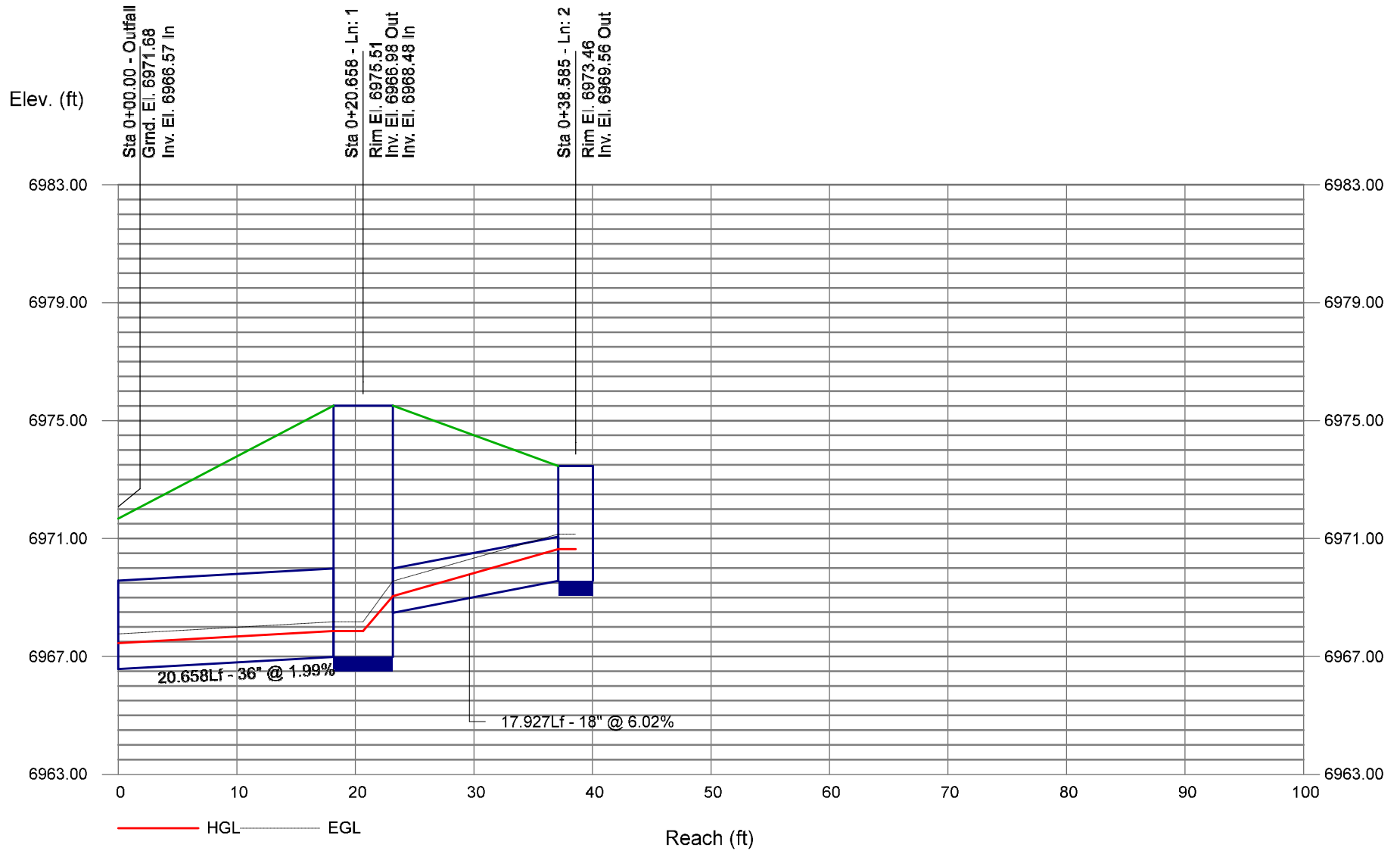


Line No.	Vel Ave (ft/s)	Flow Rate (cfs)	Line Size (in)	Line Length (ft)	Invert Up (ft)	Invert Dn (ft)	Line Slope (%)	HGL Up (ft)	HGL Dn (ft)	n-val Pipe	J-Loss Coeff	
1	4.52	7.80	36	20.658	6966.98	6966.57	1.99	6967.86	6967.45	0.013	0.45 z	
2	9.25	7.80	18	17.927	6969.56	6968.48	6.02	6970.64	6969.05	0.013	1.00 z	

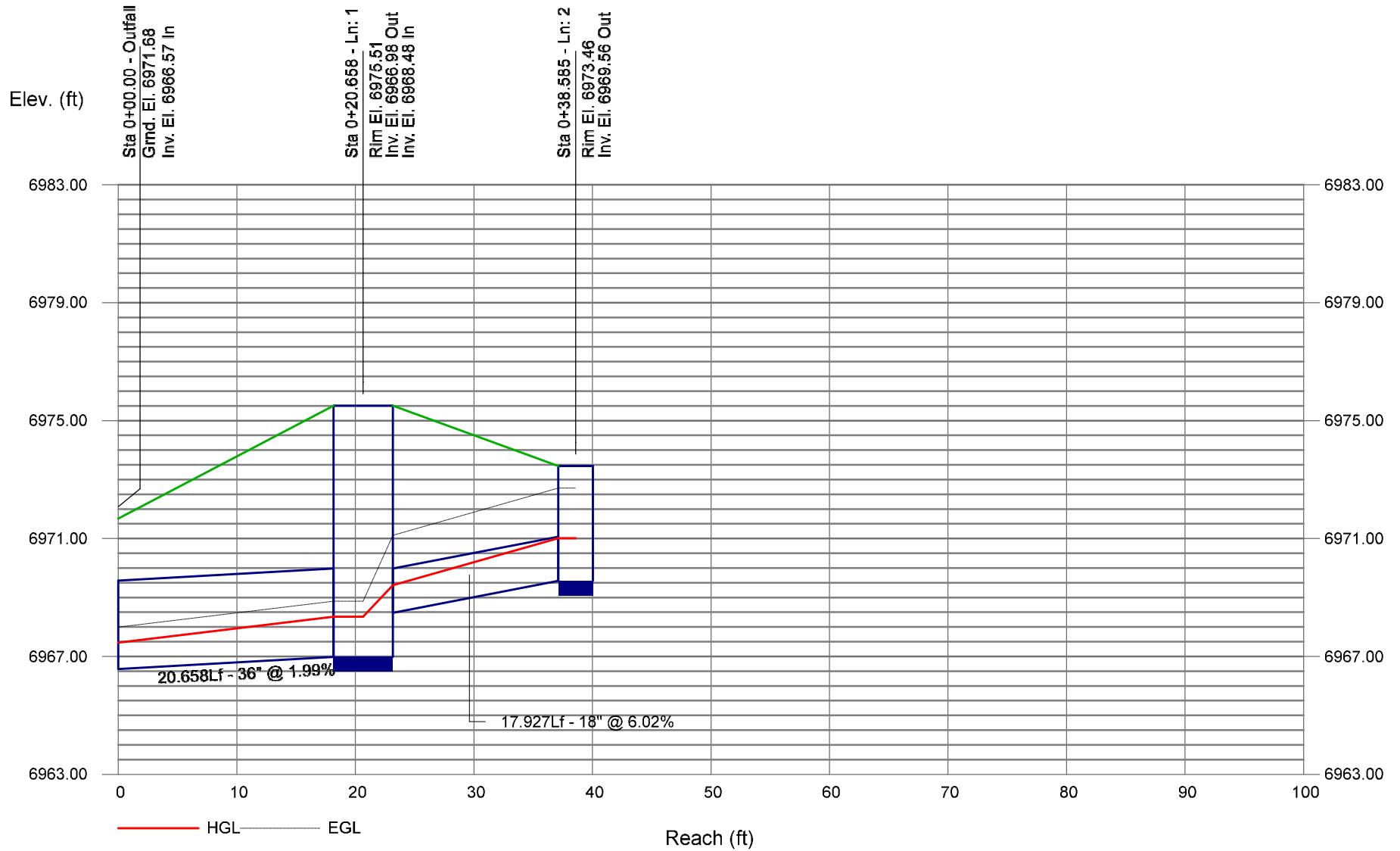
Project File: New.stm	Number of lines: 2	Date: 7/22/2025
-----------------------	--------------------	-----------------

NOTES: \*\* Critical depth

# Storm Sewer Profile



# Storm Sewer Profile



Line No.	Vel Ave (ft/s)	Flow Rate (cfs)	Line Size (in)	Line Length (ft)	Invert Up (ft)	Invert Dn (ft)	Line Slope (%)	HGL Up (ft)	HGL Dn (ft)	n-val Pipe	J-Loss Coeff	
1	8.06	18.30	36	20.658	6966.98	6966.57	1.99	6968.35	6967.47	0.013	0.45 z	
2	13.13	18.30	18	17.927	6969.56	6968.48	6.02	6971.01	6969.41	0.013	1.00 z	

Project File: New.stm	Number of lines: 2	Date: 7/22/2025
-----------------------	--------------------	-----------------

NOTES: \*\* Critical depth

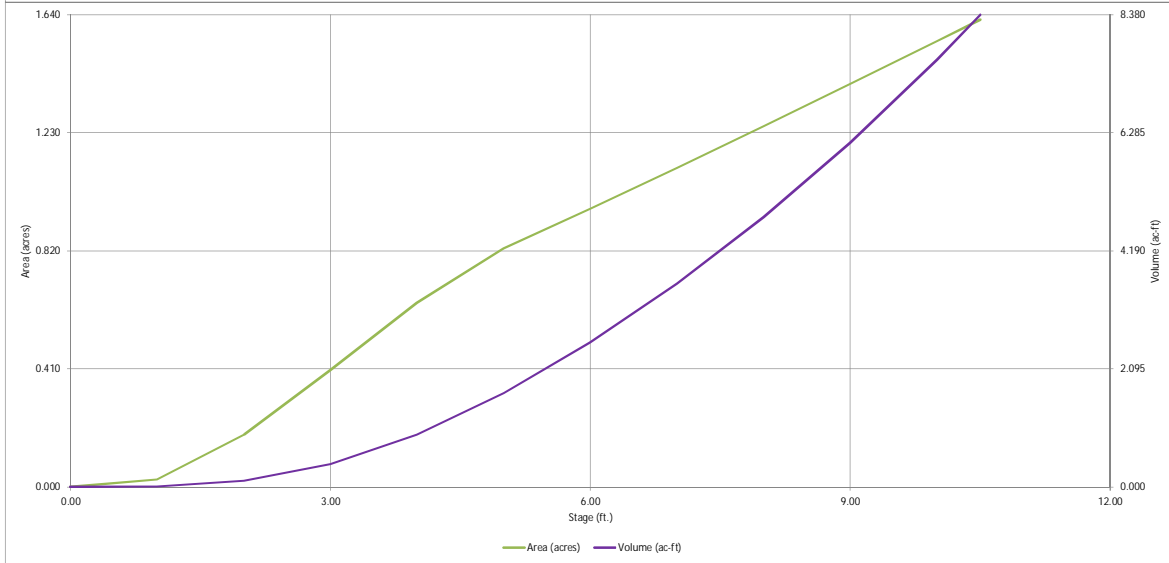
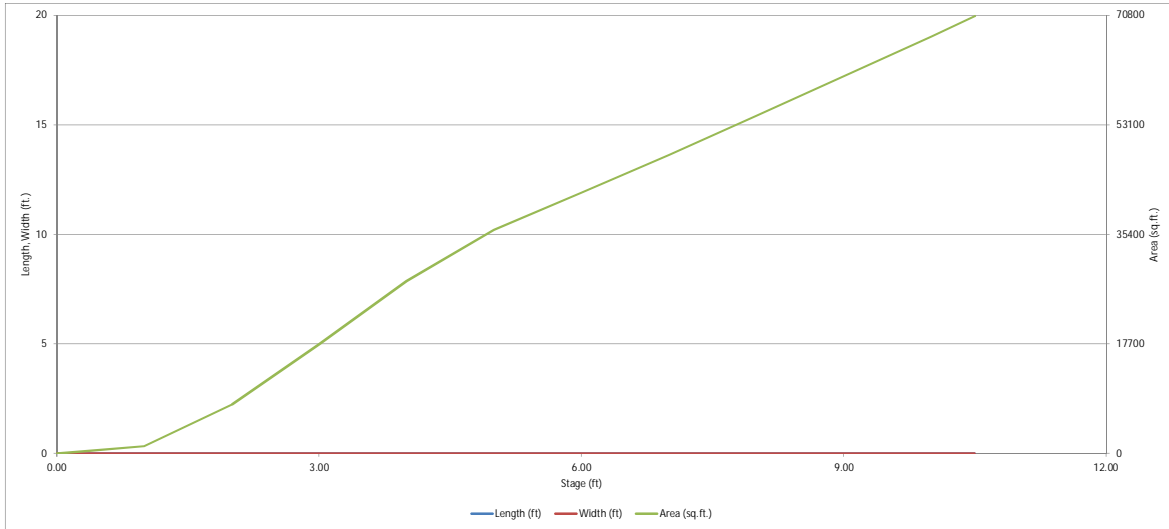


## **APPENDIX D – WATER QUALITY & DETENTION**



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

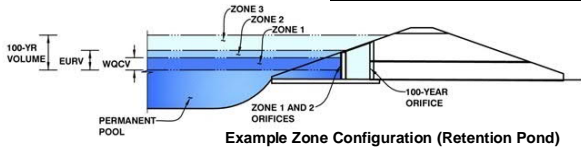
MHFD-Defention, Version 4.06 (July 2022)



**DETENTION BASIN OUTLET STRUCTURE DESIGN**

MHFD-Detention, Version 4.06 (July 2022)

Project: Sterling Ranch Recycling Facility  
Basin ID: Pond A-Ultimate



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WOCV)	4.16	1.037	Orifice Plate
Zone 2 (EURV)	7.38	2.987	Circular Orifice
Zone 3 (100-year)	8.83	1.839	Weir&Pipe (Restrict)
Total (all zones)		5.864	

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	4.16	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

Calculated Parameters for Plate

WO Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.35	2.77					
Orifice Area (sq. inches)	2.80	2.80	2.80					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	4.16	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	7.38	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	4.30	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.10	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.18	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	7.90	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Type =	Close Mesh Gate	N/A	
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>1</sub> =	7.90	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	9.01	N/A	
Overflow Gate Open Area w/o Debris =	12.66	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	6.33	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	11.00	N/A	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.40	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.53	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.49	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	9.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	120.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.48	feet
Stage at Top of Freeboard =	10.48	feet
Basin Area at Top of Freeboard =	1.62	acres
Basin Volume at Top of Freeboard =	8.34	acre-ft

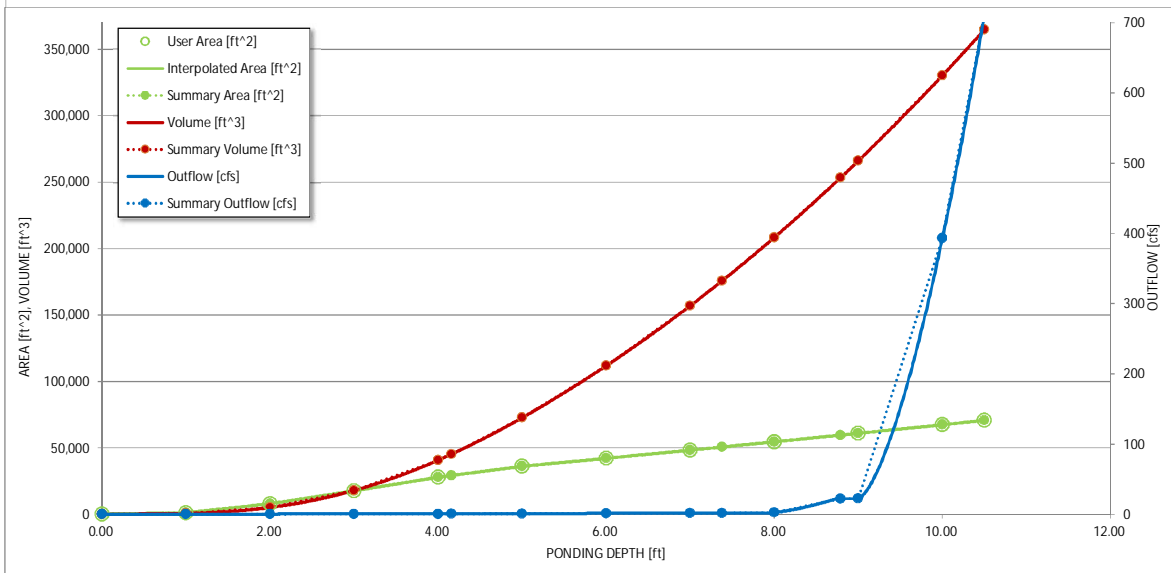
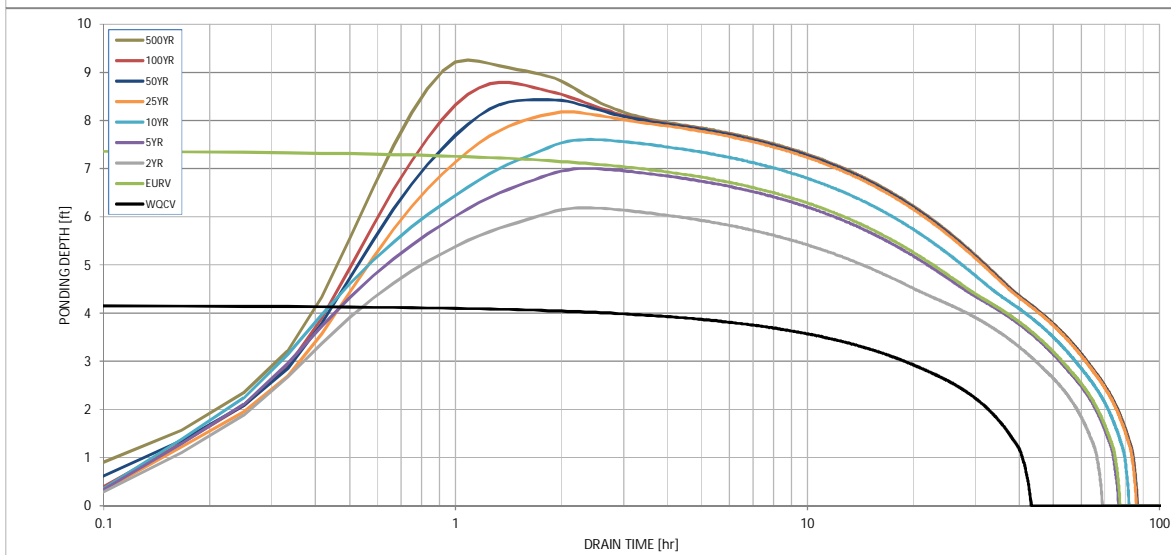
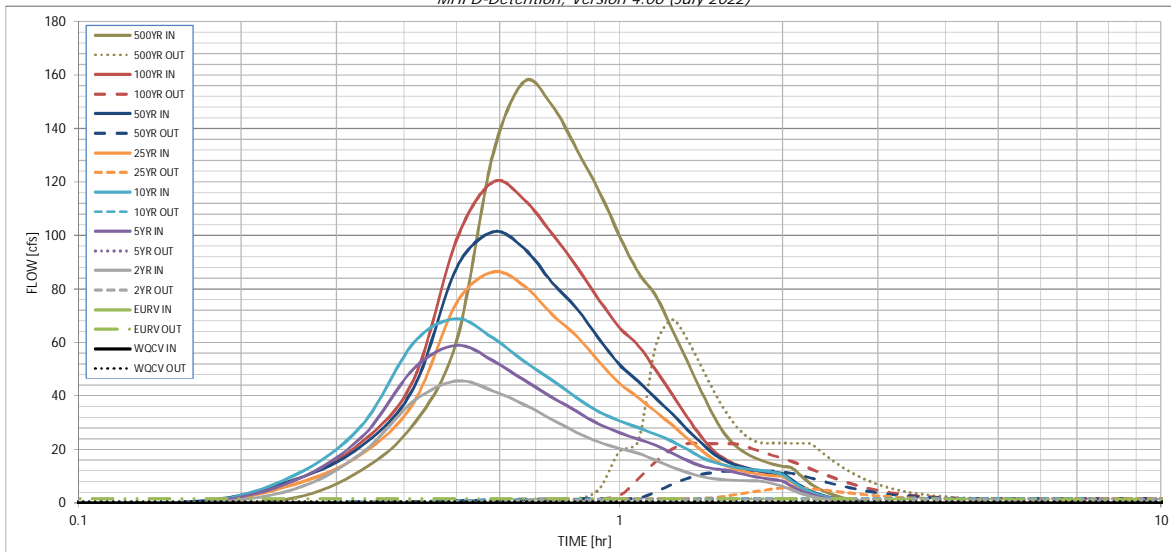
**Routed Hydrograph Results**

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WOCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	1.037	4.024	2.942	3.836	4.555	5.444	6.314	7.348	9.622
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.942	3.836	4.555	5.444	6.314	7.348	9.622
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.3	0.5	0.7	6.7	13.4	22.5	40.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.31	0.51	0.93
Peak Inflow Q (cfs) =	N/A	N/A	45.5	58.9	68.8	86.3	101.3	120.0	157.6
Peak Outflow Q (cfs) =	0.5	1.5	1.3	1.5	1.6	5.6	12.1	22.2	68.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.7	2.1	0.8	0.9	1.0	1.7
Structure Controlling Flow =	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.3	0.8	1.6	1.6
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	67	60	66	71	73	72	71	68
Time to Drain 99% of Inflow Volume (hours) =	41	72	65	71	76	80	79	79	78
Maximum Ponding Depth (ft) =	4.16	7.38	6.19	7.00	7.61	8.18	8.43	8.79	9.25
Area at Maximum Ponding Depth (acres) =	0.67	1.16	0.99	1.11	1.19	1.28	1.32	1.37	1.44
Maximum Volume Stored (acre-ft) =	1.039	4.036	2.743	3.604	4.295	5.012	5.336	5.819	6.464

### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

**DETENTION BASIN OUTLET STRUCTURE DESIGN**

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

**Inflow Hydrographs**

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.57	0.06	1.83
	0:15:00	0.00	0.00	5.05	8.22	10.18	6.84	8.59	8.34	12.16
	0:20:00	0.00	0.00	18.49	24.39	28.72	18.15	21.18	22.63	29.51
	0:25:00	0.00	0.00	38.05	50.12	59.86	37.51	43.02	46.17	60.49
	0:30:00	0.00	0.00	45.54	58.87	68.83	74.78	87.92	98.38	130.15
	0:35:00	0.00	0.00	41.90	53.26	61.67	86.30	101.33	119.99	157.58
	0:40:00	0.00	0.00	36.74	45.86	52.97	81.13	95.11	113.39	148.64
	0:45:00	0.00	0.00	31.21	39.50	45.91	70.58	82.55	100.68	132.31
	0:50:00	0.00	0.00	26.39	34.22	39.33	62.32	72.70	88.45	116.56
	0:55:00	0.00	0.00	22.70	29.43	33.99	52.82	61.36	75.91	99.84
	1:00:00	0.00	0.00	20.32	26.23	30.69	44.70	51.70	65.52	86.12
	1:05:00	0.00	0.00	18.51	23.80	28.11	39.37	45.45	58.85	77.48
	1:10:00	0.00	0.00	15.95	21.50	25.59	34.05	39.18	49.59	64.99
	1:15:00	0.00	0.00	13.45	18.71	23.09	29.16	33.43	40.80	53.16
	1:20:00	0.00	0.00	11.32	15.89	20.06	24.06	27.48	32.11	41.61
	1:25:00	0.00	0.00	9.80	13.80	16.95	19.69	22.38	24.67	31.79
	1:30:00	0.00	0.00	8.99	12.73	15.05	15.90	17.99	19.07	24.43
	1:35:00	0.00	0.00	8.58	12.15	13.89	13.59	15.33	15.79	20.11
	1:40:00	0.00	0.00	8.35	11.01	13.06	12.15	13.69	13.82	17.52
	1:45:00	0.00	0.00	8.20	10.02	12.46	11.21	12.62	12.47	15.72
	1:50:00	0.00	0.00	8.08	9.31	12.04	10.55	11.88	11.56	14.50
	1:55:00	0.00	0.00	7.16	8.78	11.48	10.11	11.38	10.90	13.63
	2:00:00	0.00	0.00	6.26	8.16	10.49	9.80	11.03	10.45	13.03
	2:05:00	0.00	0.00	4.79	6.27	8.01	7.59	8.53	8.03	10.00
	2:10:00	0.00	0.00	3.51	4.55	5.79	5.49	6.17	5.81	7.23
	2:15:00	0.00	0.00	2.55	3.31	4.20	3.98	4.47	4.23	5.27
	2:20:00	0.00	0.00	1.84	2.38	3.04	2.89	3.25	3.10	3.85
	2:25:00	0.00	0.00	1.31	1.66	2.15	2.04	2.29	2.19	2.72
	2:30:00	0.00	0.00	0.90	1.13	1.50	1.43	1.60	1.53	1.90
	2:35:00	0.00	0.00	0.60	0.78	1.04	1.01	1.13	1.08	1.34
	2:40:00	0.00	0.00	0.37	0.51	0.66	0.66	0.74	0.70	0.87
	2:45:00	0.00	0.00	0.19	0.30	0.37	0.39	0.43	0.41	0.50
	2:50:00	0.00	0.00	0.08	0.14	0.17	0.18	0.20	0.19	0.24
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	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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## **APPENDIX E – REFERENCE MATERIAL**

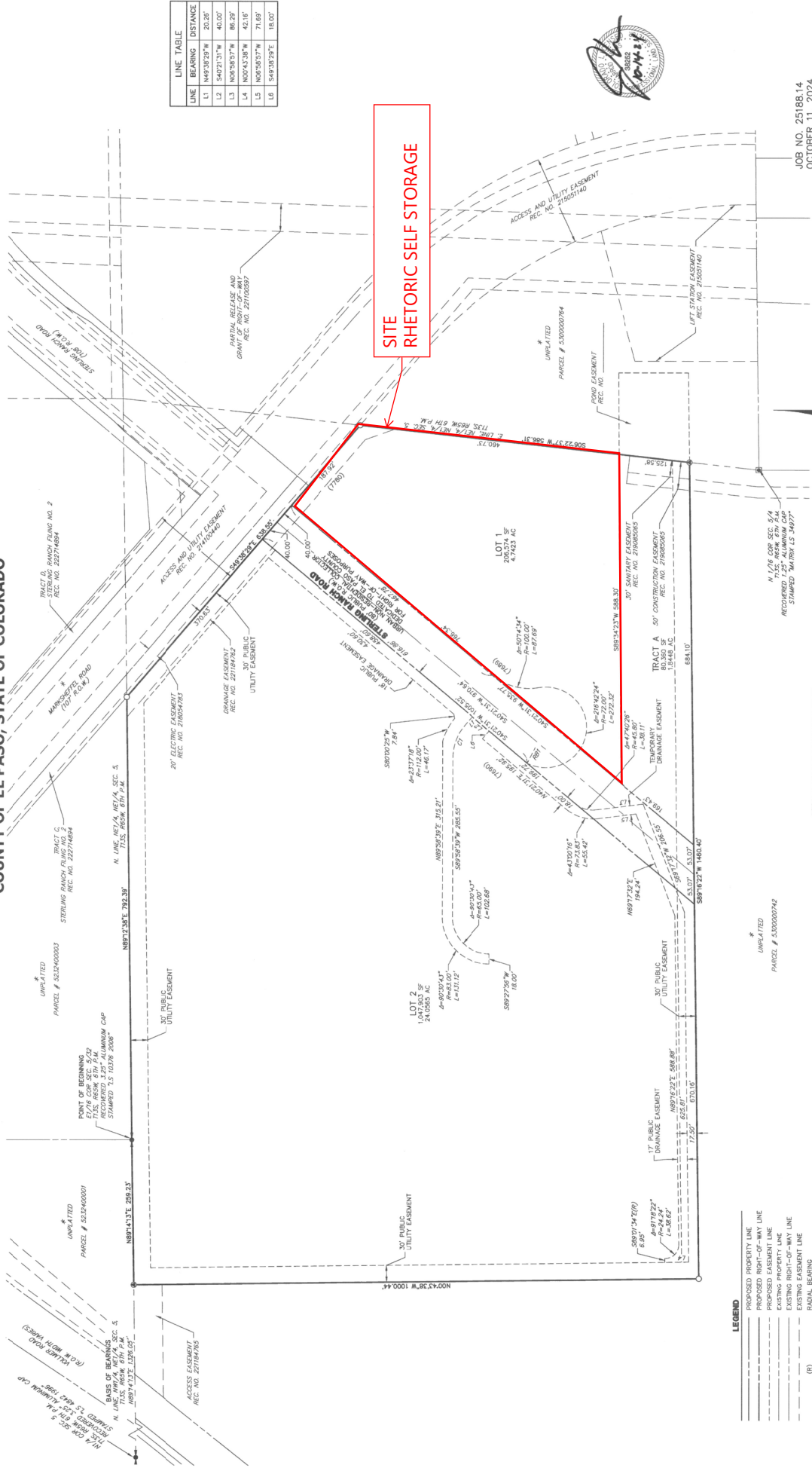




15466

# STERLING RECYCLING SUBDIVISION

LOCATED IN THE NW1/4 OF THE NW1/4 OF SECTION 4 & THE N1/2 OF SECTION 5,  
BOTH IN TOWNSHIP 13 SOUTH, RANGE 65 WEST OF THE 6TH PRINCIPAL MERIDIAN  
COUNTY OF EL PASO, STATE OF COLORADO



LINE	BEARING	DISTANCE
L1	N49°33'59"W	20.20'
L2	S40°21'51"W	40.00'
L3	N05°55'57"W	88.23'
L4	N07°43'38"W	42.16'
L5	N05°38'57"W	71.89'
L6	S49°35'59"E	18.00'



JOB NO. 2518814  
DATE: OCTOBER 11, 2024  
SHEET 3 OF 3

**J.R. ENGINEERING**  
A Western Company  
Colorado: 303.345.0800 • Colorado Springs: 719.589.5858  
Fax: 303.345.0800 • www.jrengineering.com



RADIAL BEARING TABLE

LINE	BEARING
R1	S83°10'39"E

CURVE TABLE

CURVE	DELTA	RADIUS	LENGTH
C1	40°22'52"	30.00'	15.43'

- LEGEND**
- PROPOSED PROPERTY LINE
  - PROPOSED RIGHT-OF-WAY LINE
  - PROPOSED EASEMENT LINE
  - EXISTING PROPERTY LINE
  - EXISTING RIGHT-OF-WAY LINE
  - EXISTING EASEMENT LINE
  - RADIAL BEARING LINE
  - PROPOSED ADDRESS
  - NOT PART OF THIS SUBDIVISION
  - RECOVERED 1.25" PINK PLASTIC CAP
  - STAMPED "S 3822" 1/4" ALUMINUM CAP
  - STAMPED "R 618 US 3822"

FILE NO. SF-2325

ORIGINAL SCALE: 1" = 60'

**FINAL DRAINAGE REPORT  
FOR  
STERLING RANCH RECYCLING FACILITY**

**Prepared For:**

**Colorado Concrete Crushing, LLC  
20 Boulder Crescent, Suite 200  
Colorado Springs, CO 80903  
(719) 491-3024**

**July 2024**

**Project No. 25188.14**

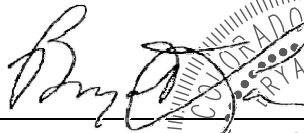
**PCD Filing No: PPR2341 & SF2325**

**Prepared By:**

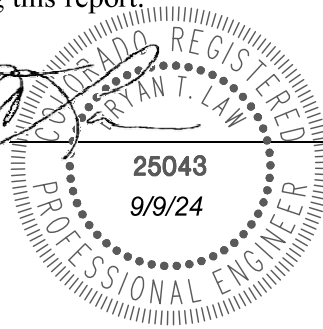
**JR Engineering, LLC  
5475 Tech Center Drive, Suite 235  
Colorado Springs, CO 80919  
719-593-2593**

**ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage letter has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.



Bryan T. Law, Colorado P.E. 25043  
For and On Behalf of JR Engineering, LLC



**DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Colorado Concrete Crushing, LLC

By: 

Title: M. Anderson

Address: 20 Boulder Crescent, Suite 200  
Colorado Springs, CO 80903

**El Paso County:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Gilbert LaForce, P.E.   
Digitally signed by Gilbert LaForce, P.E.  
Reason: Authorized signatory as County Engineer designee  
Date: 2024.11.07 09:20:04-07'00'

11/7/2024

County Engineer/ ECM Administrator



than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. Refer to the FIRM Map in Appendix A for additional information.

## EXISTING DRAINAGE CONDITIONS

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### MAJOR BASIN DESCRIPTIONS

The site lies within the upper Sand Creek Drainage Basin based on the “Sand Creek Drainage Basin Planning Study” (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into 7 major sub-basins. The site is within the respective upper basin Sand Creek sub-basin as shown in Appendix D. Sand Creek ultimately enters Fountain Creek about two miles upstream of the Academy Boulevard bridge over Fountain Creek.

The site generally drains from north to southwest. Sand Creek is located to the east of the site and runs from north to south. This reach of drainage conveyance does not currently have any improvements. As of the date of this report, Kiowa is performing studies and plans to address Sand Creek stabilization adjacent to the site.

### EXISTING SUB-BASIN DRAINAGE

The existing condition analyzes the parcel at the latest time of sale in 2021. The existing condition of the site was broken into nine sub-basins including six on-site basins and three off-site basins. The basin delineation is shown in the existing drainage map in Appendix E and is described as follows:

Basin EXA ( $Q_5=1.1$  cfs,  $Q_{100}=5.4$  cfs) is 2.68 acres with an 8 percent impervious and is located on the northwestern portion of the site. This basin is comprised of part of an existing paved access road, existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest onto the adjacent property to the west at design point (DP) 1. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin EXB ( $Q_5=0.6$  cfs,  $Q_{100}=4.3$  cfs) is 2.60 acres with a 2 percent impervious and is located on the western portion of the site. This basin is comprised of existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest onto the adjacent property to the west at DP2. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin EXC ( $Q_5=1.0$  cfs,  $Q_{100}=4.3$  cfs) is 2.11 acres with a 14 percent impervious and is located on the southwest portion of the site. This basin is comprised of several existing gravel roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest to DP3 located along the existing 8' berm. Runoff from DP3 infiltrates the ground along the berm's toe of slope.



Basin EXD ( $Q_5=7.6$  cfs,  $Q_{100}=28.1$  cfs) is 13.44 acres with a 17 percent impervious and is located on the western central portion of the site. This basin is comprised of part of an existing paved access road, several existing gravel roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows south to DP4 located along the existing 8' berm. Runoff from DP4 flows south across the existing berm via an existing 12" PVC pipe. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin OS1 ( $Q_5=1.4$  cfs,  $Q_{100}=9.2$  cfs) is 8.74 acres with a 2 percent impervious and is located to the north of the site. This basin is comprised of off-site undeveloped area tributary to the site. Runoff from this basin sheet flows south and then east along the existing off-site berm to DP5. Runoff from DP5 flows south entering into Basin EXE. Runoff follows historical drainage patterns within Basin EXE and combines at DP7.1.

Basin OS3 ( $Q_5=0.2$  cfs,  $Q_{100}=0.9$  cfs) is 0.29 acres with a 2 percent impervious and is located to the south of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows north to DP6 entering into Basin EXE. Runoff follows historical drainage patterns within Basin EXE and combines at DP7.1.

Basin EXE ( $Q_5=2.0$  cfs,  $Q_{100}=13.4$  cfs) is 8.51 acres with a 2 percent impervious and is located on the eastern central portion of the site. This basin is comprised of part of several existing dirt access roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows south and then east to DP6 located along the existing 8' berm. Runoff from DP5, DP6, and DP7 combine at DP7.1 ( $Q_5=2.8$  cfs,  $Q_{100}=18.3$  cfs). Runoff from DP7.1 continues to flow southeast through the neighboring property to the south. Flow becomes concentrated off-site in a natural stream section that ultimately follows the historical drainage patterns into Sand Creek.

Basin OS2 ( $Q_5=0.2$  cfs,  $Q_{100}=1.1$  cfs) is 0.53 acres with a 2 percent impervious and is located to the east of the site. Runoff from this basin sheet flows west to DP8 entering into Basin EXF. Runoff follows historical drainage patterns within Basin EXE and combines at DP9.1.

Basin EXF ( $Q_5=0.8$  cfs,  $Q_{100}=5.2$  cfs) is 3.09 acres with a 2 percent impervious and is located on the eastern portion of the site. This basin is comprised of part of an existing dirt access road and undeveloped area. Runoff from this basin sheet flows southeast to DP9 located along the eastern side of the site. Runoff from DP8 and DP9 combine at DP9.1 ( $Q_5=0.9$  cfs,  $Q_{100}=6.1$  cfs). Runoff from DP9.1 continues to flow south through the neighboring sanitary lift station property to the east. Flow becomes concentrated off-site in a natural stream section that ultimately follows the historical drainage patterns into Sand Creek.



## PROPOSED DRAINAGE CONDITIONS

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### PROPOSED CONVEYANCE

In general, developed flows are collected in proposed swales, which convey water to the proposed water quality and detention area. Proposed swale sections were designed to ensure they are stable and have required capacity to satisfy criteria. A swale is considered stable with a velocity of 5 ft/s or less. Where swale Froude numbers exceed 0.8, swales will be reinforced with the specified SC250 VMax TRM (turf reinforcement mat) product (or approved equivalent) shown in Appendix C. Specific locations where the TRM is required in swale sections is shown in the Grading and Erosion Control Construction Documents. To ensure capacity, swales will have a minimum of 1 ft. of freeboard over the water surface for flows anticipated in a 100-year storm event. In addition to the swales, a proposed culvert also conveys flows under the access roadway. The culvert was sized to not overtop the roadways with flows from a 100-year storm event. Detailed swale calculations, sections, and culvert calculations are located in Appendix C.

### PROPOSED SUB-BASIN DRAINAGE

The proposed condition analyzes the parcel for the interim use of a recycling facility. The Rational Method produced flows that were used to design the proposed interim swales, culverts, storm sewer, and pond forebays. The proposed site was broken into eight basins including six on-site basins and two off-site basins. The proposed basin delineation is shown on the drainage basin map within Appendix E and is described as follows:

Basin A ( $Q_5=0.3$  cfs,  $Q_{100}=1.6$  cfs) is 0.50 acres with a 2% impervious and is located on the western and a portion of the southern property line of the site. This basin is comprised of proposed area to remain undeveloped and therefore follows the historic drainage pattern flowing off-site to the west and south undetained or treated. This is in accordance with Section I.7.1.B.7 of the ECM Stormwater Quality Policy and Procedure. Runoff from this basin sheet flows southwest to DP1 and then off-site to the adjacent property to the west. Runoff then follows historical drainage patterns sheet flowing off-site and outfalls to Sand Creek.

Basin B ( $Q_5=7.4$  cfs,  $Q_{100}=25.1$  cfs) is 14.03 acres with a 19 percent impervious and is located on the western central portion of the site. This basin is comprised of part of a paved roadway, raw concrete stockpile, raw concrete with rebar stockpile, asphalt stockpile, weighing station, mobile crusher, fence, part of temporary gravel road, swales and undeveloped land. Runoff from this basin sheet flows overland south to a proposed swale that directs flows east to DP2. Runoff from DP2 is combined at the proposed 54" FES at DP4.2. Runoff from this basin is captured and treated within proposed Pond A.

Basin OS1 ( $Q_5=1.4$  cfs,  $Q_{100}=9.2$  cfs) is 8.74 acres with a 2 percent impervious and is located to the north of the site. This basin is comprised of off-site undeveloped area tributary to the site. Runoff



from this basin sheet flows south and then east along the existing off-site berm to DP3. Runoff from DP3 flows south entering into Basin C. Runoff follows the drainage patterns within Basin C and combines at the proposed 24" RCP culvert at DP4.1.

Basin C ( $Q_5=3.4$  cfs,  $Q_{100}=17.7$  cfs) is 10.70 acres with a 6 percent impervious and is located on the eastern central portion of the site. This basin is comprised of a part of proposed Sterling Ranch Road, asphalt access roads, swales and undeveloped land. Runoff from this basin flows along proposed curb and gutter as well as sheet flows overland south to proposed swales that directs flows east to DP4. Runoff from DP4 is combined with flows from DP3 at the proposed 24" RCP culvert at DP4.1 ( $Q_5=3.7$  cfs,  $Q_{100}=21.1$  cfs). Runoff from DP4.1 enters the proposed culvert into Basin B and a proposed swale directs flows to the proposed 54" FES at DP4.2 ( $Q_5=9.3$  cfs,  $Q_{100}=40.1$  cfs). DP4.2 flows are piped to the west forebay within the pond and combine at DP9.1. Runoff from this basin is captured and treated within proposed Pond A.

Basin D ( $Q_5=0.5$  cfs,  $Q_{100}=3.7$  cfs) is 2.16 acres with a 2 percent impervious and is located on the eastern boundary of the site. This basin is comprised of undeveloped land. Runoff from this basin sheet flows overland southeast to a proposed swale that directs flows south to DP5. Runoff from DP5 is combined at the proposed Type C sump inlet at DP7.1 within Basin E. Runoff from this basin is captured and treated within proposed Pond A.

Basin E ( $Q_5=2.2$  cfs,  $Q_{100}=7.1$  cfs) is 3.10 acres with a 22 percent impervious and is located on the eastern portion of the site. This basin is comprised of a part of proposed Sterling Ranch Road, part of a temporary gravel road, asphalt access road, swale and undeveloped land. Runoff from this basin flows along proposed curb and gutter and then sheet flows overland southeast to a proposed swale that directs flows east to DP6. Runoff from DP6 is combined at the proposed Type C sump inlet at DP7.1. Runoff from this basin is captured and treated within proposed Pond A.

Basin OS2 ( $Q_5=0.1$  cfs,  $Q_{100}=0.7$  cfs) is 0.36 acres with a 2 percent impervious and is located to the east of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows west and then south along the property boundary to DP7. Runoff from DP7 is combined with DP5 and DP6 flows at the proposed Type C sump inlet at DP7.1 ( $Q_5=2.8$  cfs,  $Q_{100}=11.2$  cfs). DP7.1 flows are piped to the north forebay within the pond and combine at DP9.1.

Basin OS3 ( $Q_5=0.2$  cfs,  $Q_{100}=1.0$  cfs) is 0.30 acres with a 2 percent impervious and is located to the south of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows north to DP8. Runoff from DP8 combines with DP4.2, DP7.1, and DP6 flows at the proposed outlet structure at DP9.1.

Basin F ( $Q_5=0.6$  cfs,  $Q_{100}=4.4$  cfs) is 2.27 acres with a 2 percent impervious and is located on the southeast portion of the site. This basin is comprised of a proposed full-spectrum extended detention



adversely affect downstream infrastructure. See the ultimate section below for more information on the existing downstream infrastructure.

2. Flows from Basin G leave the site uncaptured and untreated at DP10 ( $Q_5=0.2$  cfs,  $Q_{100}=0.4$  cfs) and combine with OS4 flows at DP11 ( $Q_5=6.7$  cfs,  $Q_{100}=12.8$  cfs) at the existing 15' Type R on-grade inlet at DP11.1 ( $Q_5=6.9$  cfs,  $Q_{100}=13.1$  cfs). The existing inlet was constructed as part of Sterling Ranch Filing No. 2 (see applicable excerpts in Appendix D). The Filing 2 report Basin A10 (Basin OS4) has a total flow to the 15' Type R on-grade inlet of  $Q_5=9.2$  cfs,  $Q_{100}=17.3$  cfs. Compared to the existing flows, DP11.1 flows are less than historic and will not adversely affect downstream infrastructure.

### ULTIMATE SUB-BASIN DRAINAGE

The ultimate condition analyzes the parcel and tributary properties for the future development based on the land use in order to design the ultimate full-spectrum EDB and spillway overflow path. The ultimate site was broken into five land uses. The land uses are shown on the proposed drainage map within Appendix E and is described as follows.

- Lot 1 is 4.74 acres and is zoned as Heavy Industrial Area (90% impervious)
- Urban Non-Residential Collector Roadway (80' R.O.W.) is 1.78 acres (100% impervious for roadway, curb & gutter, and sidewalk width, 2% impervious for other areas)
- Lot 2 is 24.05 acres and is zoned as Residential-1/8 Acre or Less (65% impervious)
- Tract A is 1.85 acres and is used as detention pond area (2% impervious)
- Off-site vacant land to the north is 8.74 acres and is zoned as Commercial Area (95% impervious)
- Off-site Tract/ Lift Station land to the east is 1.87 acres and is zoned as Heavy Industrial Area (90% impervious)
- Off-site land to the east is 0.44 acres and is used as detention pond area (2% impervious)
- Off-site land to the south is 0.30 acres and flows to detention pond area (2% impervious)
- Total Area = 43.77 acres with 71.6% impervious (used 72% for design)

The ultimate condition was used overall to size the full-spectrum EDB and ensure it will operate for future developments.

In the ultimate condition, there is one location where flows leave the site.

2. Ultimate released flows from the pond outlet structure ( $Q_5=1.5$  cfs,  $Q_{100}=22.2$  cfs) are released into the existing storm infrastructure located adjacent to the site. Flows from existing design points DP7.1 and 9.1 flow off-site to the south for a total flow of  $Q_5=3.7$  cfs,  $Q_{100}=24.4$  cfs. The existing downstream 66" RCP that the outfall ties into was designed and approved as part of the Sterling Ranch Filing 2 development. The pipe shall be installed by June 2024 and for the purposes of this report, considered as existing. The existing 66" RCP was designed for Filing 2 DP4.7 flows ( $Q_5=58.4$  cfs,  $Q_{100}=248.6$  cfs) and the ultimate



condition flows ( $Q_5=32.2$  cfs,  $Q_{100}=255.6$  cfs) will result in an increase in flows in the major storm. The StormCAD analysis in Appendix C shows that the existing storm system was designed deep enough to have the capacity for the increase in flow. There are also no adverse affects from the increase in flow in the minor storm shown in the MHFD Detention spreadsheet as the existing storm system was designed to handle the peak 100-year flows which greatly surpass the 5-year flow rates. See Appendix C for the StormCAD analysis and calculations. The existing storm system the proposed site ties continues to travel east and south about 1,800 feet before ultimately releasing directly into Sand Creek.

## DRAINAGE DESIGN CRITERIA

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### DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the “*City of Colorado Springs/El Paso County Drainage Criteria Manual*” Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the “*Urban Storm Drainage Criteria Manual*” Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the “*Colorado Springs Drainage Criteria Manual*” (CSDCM), dated May 2014, as adopted by El Paso County.

### HYDROLOGIC CRITERIA

All hydrologic data was obtained from the “*El Paso Drainage Criteria Manual*” Volumes 1 and 2, and the “*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*” Volumes 1, 2, and 3. On-site drainage improvements were designed based on the 5-year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One-hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

**Table 1: 1-hr Point Rainfall Data**

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52



# COMPOSITE % IMPERVIOUS & COMPOSITE EXISTING RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 1/18/24

Basin ID	Total Area (ac)	Streets-Paved (100% Impervious)				Streets-Gravel (80% Impervious)				Historical Analysis (2% Impervious)				Basins Total Weighted C Values		Basins Total Weighted % Imp.
		C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	
EXA	2.68	0.90	0.96	0.16	6.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.52	1.9%	0.14	0.40	7.9%
EXB	2.60	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.60	2.0%	0.09	0.36	2.0%
EXC	2.11	0.90	0.96	0.00	0.0%	0.59	0.70	0.33	12.5%	0.09	0.36	1.78	1.7%	0.17	0.41	14.2%
EXD	13.44	0.90	0.96	0.86	6.4%	0.59	0.70	1.48	8.8%	0.09	0.36	11.10	1.7%	0.20	0.44	16.9%
EXE	8.51	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	8.51	2.0%	0.09	0.36	2.0%
EXF	3.09	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	3.09	2.0%	0.09	0.36	2.0%
OS1	8.74	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	8.74	2.0%	0.09	0.36	2.0%
OS2	0.53	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.53	2.0%	0.09	0.36	2.0%
OS3	0.29	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.29	2.0%	0.09	0.36	2.0%
<b>TOTAL</b>	<b>41.99</b>															<b>7.7%</b>

**EXISTING  
STANDARD FORM SF-2  
TIME OF CONCENTRATION**

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By: \_\_\_\_\_  
Date: 1/18/24

SUB-BASIN DATA				INITIAL/OVERLAND (T)				TRAVEL TIME (T)				t <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL		
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C <sub>s</sub>	C <sub>100</sub>	L (ft)	S <sub>o</sub> (%)	t <sub>i</sub> (min)	L <sub>r</sub> (ft)	S <sub>r</sub> (%)	K	VEL. (ft/s)	t <sub>r</sub> (min)	COMP. t <sub>c</sub> (min)	TOTAL LENGTH (ft)	Urbanized t <sub>c</sub> (min)	t <sub>c</sub> (min)
EXA	2.68	A	8%	0.14	0.40	300	4.0%	19.0	190	2.3%	10.0	1.5	2.1	21.1	490.0	26.7	21.1
EXB	2.60	A	2%	0.09	0.36	300	2.5%	23.3	240	2.5%	10.0	1.6	2.5	25.9	540.0	28.4	25.9
EXC	2.11	A	14%	0.17	0.41	300	2.6%	21.3	135	1.7%	15.0	2.0	1.2	22.4	435.0	25.2	22.4
EXD	13.44	A	17%	0.20	0.44	300	3.6%	18.5	810	3.4%	15.0	2.8	4.9	23.4	1110.0	29.6	23.4
EXE	8.51	A	2%	0.09	0.36	300	4.0%	20.0	800	3.0%	10.0	1.7	7.7	27.7	1100.0	34.0	27.7
EXF	3.09	A	2%	0.09	0.36	300	3.5%	20.9	400	4.3%	10.0	2.1	3.2	24.1	700.0	29.1	24.1
OS1	8.74	A	2%	0.09	0.36	150	2.0%	17.8	850	0.2%	10.0	0.4	31.7	49.4	1000.0	59.8	49.4
OS2	0.53	A	2%	0.09	0.36	155	3.0%	15.8	0	0.0%	10.0	0.0	0.0	15.8	155.0	25.7	15.8
OS3	0.29	A	2%	0.09	0.36	35	15.0%	4.4	0	0.0%	10.0	0.0	0.0	4.4	35.0	25.7	5.0

NOTES:

$t_c = t_i + t_r$  Equation 6-2

Where:  $t_c$  = computed time of concentration (minutes)

$t_i$  = overland (initial) flow time (minutes)

$t_r$  = channelized flow time (minutes)

$t_i = \frac{0.395(1 - C_s) \sqrt{L}}{S_o^{0.33}}$  Equation 6-3

Where:  $t_i$  = overland (initial) flow time (minutes)

$C_s$  = runoff coefficient for 5-year frequency (from Table 6-4)

$L_i$  = length of overland flow (ft)

$S_o$  = average slope along the overland flow path (ft/ft)

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$t_r = \frac{L_r}{60K \sqrt{S_r}} - \frac{L_r}{60F_r}$

Where:  $t_r$  = channelized flow time (traveled time; min)

$L_r$  = waterway length (ft)

$S_o$  = waterway slope (ft/ft)

$F_r$  = travel time velocity (ft/sec) - K<sup>0.8</sup> $S_o$

$K$  = NRCS conveyance factor (see Table c-2)

Equation 6-4  $t_c = (26 - 17I) + \frac{L_c}{60(0.44 + 9)\sqrt{S_c}}$

Where:  $t_c$  = minimum time of concentration for first design point when less than  $t_c$  from Equation 6-1.

$L_c$  = length of channelized flow path (ft)

$I$  = imperviousness (expressed as a decimal)

$S_c$  = slope of the channelized flow path (ft/ft)

Table 6.2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

**STANDARD FORM SF-3 - EXISTING**  
**STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County  
Design Storm: 5-Year

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By:  
Date: 1/18/24

STREET	Design Point	Basin ID	Area (Ac)	DIRECT RUNOFF						TOTAL RUNOFF			STREET/SWALE			PIPE		TRAVEL TIME			REMARKS	
				Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t <sub>c</sub> (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)		Velocity (fps)
	1	EXA	2.68	0.14	21.1	0.37	3.01	1.1														Sheet flows overlant to DP1 Flows off-site to the west
	2	EXB	2.60	0.09	25.9	0.23	2.70	0.6														Sheet flows overlant to DP2 Flows off-site to the west
	3	EXC	2.11	0.17	22.4	0.35	2.92	1.0														Sheet flows overlant and along berm to DP3 Flows off-site to the south
	4	EXD	13.44	0.20	23.4	2.65	2.85	7.6														Sheet flows overlant and along berm to DP4 Flows off-site to the south
	5	OS1	8.74	0.09	49.4	0.79	1.73	1.4														Sheet flows overlant and along berm to DP5 Flows on-site and combines at DP7.1
	6	OS3	0.29	0.09	5.0	0.03	5.17	0.2														Flows on-site and combines at DP7.1
	7	EXE	8.51	0.09	27.7	0.77	2.60	2.0														Sheet flows overlant and along berm to DP7 Combines flows at DP7.1
	7.1								49.4	1.59	1.73	2.8										Combines the flows from DP5, DP6, and DP7 Flows off-site to the south
	8	OS2	0.53	0.09	15.8	0.05	3.44	0.2														Sheet flows overlant to DP8 Combines flows at DP9.1
	9	EXF	3.09	0.09	24.1	0.28	2.81	0.8														Sheet flows overlant to DP9 Combines flows at DP9.1
	9.1								24.1	0.33	2.81	0.9										Combines the flows from DP8 and DP9 Flows off-site to the east

**Notes:**  
Street and Pipe C\*A values are determined by Q/I using the catchment's intensity value.  
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

**STANDARD FORM SF-3 - EXISTING**  
**STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County  
Design Storm: 100-Year

Project Name: Sterling Ranch  
Project No.: 25188.14  
Calculated By: GAG  
Checked By:  
Date: 1/18/24

Description	Design Point	DIRECT RUNOFF						TOTAL RUNOFF			STREET/SWALE			PIPE			TRAVEL TIME		REMARKS				
		Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	I (in/hr)	Q (cfs)	tc (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)		Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)
	1	EXA	2.68	0.40	21.1	1.06	5.05	5.4															Sheet flows overlaid to DP1 Flows off-site to the west
	2	EXB	2.60	0.36	25.9	0.94	4.54	4.3															Sheet flows overlaid to DP2 Flows off-site to the west
	3	EXC	2.11	0.41	22.4	0.87	4.90	4.3															Sheet flows overlaid and along berm to DP3 Flows off-site to the south
	4	EXD	13.44	0.44	23.4	5.86	4.79	28.1															Sheet flows overlaid and along berm to DP4 Flows off-site to the south
	5	OS1	8.74	0.36	49.4	3.15	2.90	9.2															Sheet flows overlaid and along berm to DP5 Flows on-site and combines at DP7.1
	6	OS3	0.29	0.36	5.0	0.10	8.68	0.9															Flows on-site and combines at DP7.1
	7	EXE	8.51	0.36	27.7	3.06	4.37	13.4															Sheet flows overlaid and along berm to DP7 Combines flows at DP7.1
	7.1																						Combines the flows from DP5, DP6, and DP7 Flows off-site to the south
	8	OS2	0.53	0.36	15.8	0.19	5.78	1.1															Sheet flows overlaid to DP8 Combines flows at DP9.1
	9	EXF	3.09	0.36	24.1	1.11	4.72	5.2															Sheet flows overlaid to DP9 Combines flows at DP9.1
	9.1																						Combines the flows from DP8 and DP9 Flows off-site to the east

**Notes:**  
Street and Pipe C\*A values are determined by Q/I using the catchment's intensity value.  
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

# COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By:  
 Date: 1/24/24

PROPOSED CONDITION ANALYSIS FOR SIZING OF SWALES & INLETS.

Basin ID	Total Area (ac)	Streets-Paved (100% Impervious)				Streets-Gravel (80% Impervious)				Historical Analysis (2% Impervious)				Basins Total Weighted C Values		Basins Total Weighted % Imp.	
		C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>		
A	0.50	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.50	2.0%	0.09	0.36	2.0%	
B	14.03	0.90	0.96	2.45	17.5%	0.59	0.70	0.00	0.0%	0.09	0.36	11.58	1.7%	0.23	0.46	19.1%	
C	10.70	0.90	0.96	0.47	4.4%	0.59	0.70	0.00	0.0%	0.09	0.36	10.23	1.9%	0.13	0.39	6.3%	
D	2.16	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.16	2.0%	0.09	0.36	2.0%	
E	3.10	0.90	0.96	0.40	12.9%	0.59	0.70	0.31	8.0%	0.09	0.36	2.39	1.5%	0.24	0.47	22.4%	
F	2.27	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.27	2.0%	0.09	0.36	2.0%	
G	0.06	0.90	0.96	0.04	66.7%	0.59	0.70	0.00	0.0%	0.09	0.36	0.02	0.7%	0.63	0.76	67.3%	
OS1	8.74	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	8.74	2.0%	0.09	0.36	2.0%	
OS2	0.36	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.36	2.0%	0.09	0.36	2.0%	
OS3	0.30	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.30	2.0%	0.09	0.36	2.0%	
OS4	2.08	0.90	0.96	1.70	81.7%	0.59	0.70	0.00	0.0%	0.09	0.36	0.38	0.4%	0.75	0.85	82.1%	
Total W. Forebay (Basins B, C, OS1)																10.5%	
Total N. Forebay (Basins D, E, OS2)																13.3%	
Total Pond A (Basins B-F, OS1-3)																10.4%	

# PROPOSED STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Recycling Facility  
Location: El Paso County

Project Name: Sterling Ranch  
Project No.: 25188\_14  
Calculated By: GAG  
Checked By:  
Date: 1/24/24

DATA	SUB-BASIN					INITIAL/OVERLAND (T <sub>1</sub> )					TRAVEL TIME (T <sub>2</sub> )					tc CHECK (URBANIZED BASINS)		FINAL t <sub>c</sub> (min)
	BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C <sub>s</sub>	C <sub>100</sub>	L (ft)	S <sub>o</sub> (%)	t <sub>f</sub> (min)	L <sub>t</sub> (ft)	S <sub>t</sub> (%)	K	VEL. (ft/s)	t <sub>r</sub> (min)	COMP. t <sub>c</sub> (min)	TOTAL LENGTH (ft)	Urbanized t <sub>c</sub> (min)	
A	0.50	A	A	2%	0.09	0.36	20	33.0%	2.6	0	0.0%	10.0	0.0	0.0	2.6	20.0	25.7	5.0
B	14.03	A	A	19%	0.23	0.46	300	2.7%	19.6	1600	1.5%	15.0	1.8	14.5	34.1	1900.0	41.4	34.1
C	10.70	A	A	6%	0.13	0.39	300	2.7%	22.0	735	1.5%	15.0	1.8	6.7	28.6	1035.0	35.0	28.6
D	2.16	A	A	2%	0.09	0.36	215	3.0%	18.6	400	1.5%	10.0	1.2	5.4	24.1	615.0	31.5	24.1
E	3.10	A	A	22%	0.24	0.47	100	1.2%	14.5	910	1.5%	15.0	1.8	8.3	22.8	1010.0	32.4	22.8
F	2.27	A	A	2%	0.09	0.36	40	25.0%	4.0	615	0.5%	10.0	0.7	14.5	18.5	655.0	41.3	18.5
G	0.06	A	A	67%	0.63	0.76	54	2.0%	5.0	35	1.0%	20.0	2.0	0.3	5.3	89.0	14.9	5.3
OS1	8.74	A	A	2%	0.09	0.36	150	2.0%	17.8	850	0.2%	10.0	0.4	31.7	49.4	1000.0	59.8	49.4
OS2	0.36	A	A	2%	0.09	0.36	115	3.0%	13.6	300	3.0%	10.0	1.7	2.9	16.5	415.0	28.8	16.5
OS3	0.30	A	A	2%	0.09	0.36	35	15.0%	4.4	0	0.0%	10.0	0.0	0.0	4.4	35.0	25.7	5.0
OS4	2.08	A	A	82%	0.75	0.85	15	2.0%	1.9	1335	2.5%	20.0	3.2	7.0	9.0	1350.0	18.9	9.0

NOTES:  $t_c = t_1 + t_2$  Equation 6-2  $t_c = 0.395(L_1 - C_2) \sqrt{L_2} / S_o^{0.33}$  Equation 6-3

Where:  
 $t_c$  – computed time of concentration (minutes)  
 $t_1$  – overland (initial) flow time (minutes)  
 $t_2$  – channelized flow time (minutes)

Where:  
 $t_1$  = overland (initial) flow time (minutes)  
 $C_2$  = runoff coefficient for 5 year frequency (from Table 6-4)  
 $L_1$  = length of overland flow (ft)  
 $S_o$  = average slope along the overland flow path (ft/ft)

Where:  
 $t_2$  = minimum time of concentration for first design point when less than  $t_1$  from Equation 6-1  
 $L_2$  = length of channelized flow path (ft)  
 $S_2$  = slope of the channelized flow path (ft/ft)

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Equation 6-4  $t_c = (26 - 1/t) + \frac{L_c}{60K\sqrt{S_o}}$

Equation 6-5  $t_c = (26 - 1/t) + \frac{L_c}{60(Q_4 + 9)\sqrt{S_2}}$

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

**STANDARD FORM SF-3 - PROPOSED  
STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County  
 Design Storm: 5-Year

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By:  
 Date: 1/24/24

STREET	Design Point	Basin ID	DIRECT RUNOFF						TOTAL RUNOFF			STREET/SWALE			PIPE		TRAVEL TIME		REMARKS					
			Area (Ac)	Runoff Coeff.	$t_c$ (min)	C*A (Ac)	I (in/hr)	Q (cfs)	$t_c$ (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)		Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	
	1	A	0.50	0.09	5.0	0.05	5.17	0.3																Flows overland along the western site boundary to DP1 Flows off-site to the west
	2	B	14.03	0.23	34.1	3.25	2.29	7.4																Sheet flows overland to swale and then to DP2 Combines flow at FES at DP4.2
	3	OS1	8.74	0.09	49.4	0.79	1.73	1.4																Sheet flows overland and along berm to DP3 Flows on-site and combines at culvert at DP4.1
	4	C	10.70	0.13	28.6	1.34	2.55	3.4																Sheet flows overland to swale and then to DP4 Combines flow at culvert at DP4.1
	4.1								49.4	2.13	1.73	3.7												Combined flow of DP3 and DP4 within culvert Swale to FES at DP4.2
	4.2								49.4	5.38	1.73	9.3												Combined flow of DP2 and DP4.1 at sump inlet Piped to pond forebay, combines flow at DP9.1
	5	D	2.16	0.09	24.1	0.19	2.81	0.5																Sheet flows overland to swale and then to DP5 Combines flow at sump inlet at DP7.1
	6	E	3.10	0.24	22.8	0.76	2.89	2.2																Sheet flows overland to swale and then to DP6 Combines flow at sump inlet at DP7.1
	7	OS2	0.36	0.09	16.5	0.03	3.38	0.1																Sheet flows overland to DP7 Combines flow at sump inlet at DP7.1
	7.1								24.1	0.98	2.81	2.8												Combined flow of DP5, DP6, and DP7 at sump inlet Piped to pond forebay, combines flow at DP9.1
	8	OS3	0.30	0.09	5.0	0.03	5.17	0.2																Sheet flows overland to DP8 Combines flow at DP9.1
	9	F	2.27	0.09	18.5	0.20	3.21	0.6																Flows along trickle channel to DP9 at outlet structure Combines flow at DP9.1
	9.1								49.4	6.59	1.73	11.4												Combined flow of DP4.2, DP7.1, DP8 and DP9. Total interim pond inflow. Released through pond outlet structure at DP9.2
	9.2											0.1												Released flow through interim outlet structure from MHFD_Detention Piped to existing junction box and storm infrastructure
	10	G	0.06	0.63	5.3	0.04	5.09	0.2																Flows along prop. Sterling Ranch Rd. c&g to DP10 to Marksheffel Rd. Combines at existing Marksheffel Rd. existing 15" Type R inlet.
	11	OS4	2.08	0.75	9.0	1.56	4.29	6.7																Off-site work along existing Marksheffel Rd. c&g to ex. 15" Type R inlet. Combines at existing Marksheffel Rd. existing 15" Type R inlet.
	11.1								9.0	1.60	4.29	6.9												Combined flow of DP 10 and DP11 within existing 15" Type R inlet. Captured flow continues off-site southeast along Marksheffel Rd. storm

**Notes:**  
 Street and Pipe C\*A values are determined by Q/I using the catchment's intensity value.  
 All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

PROPOSED CONDITION  
ANALYSIS FOR SIZING OF  
SWALES & INLETS.

**STANDARD FORM SF-3 - PROPOSED  
STORM DRAINAGE SYSTEM DESIGN**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County  
 Design Storm: 100-Year

Project Name: Sterling Ranch  
 Project No.: 25188.14  
 Calculated By: GAG  
 Checked By:  
 Date: 1/24/24

Description	Design Point	Basin ID	DIRECT RUNOFF					TOTAL RUNOFF			STREET/SWALE			PIPE		TRAVEL TIME		REMARKS					
			Area (ac)	Runoff Coeff.	$t_c$ (min)	C*A (ac)	I (in/hr)	Q (cfs)	$t_c$ (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)		Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_r$ (min)
	1	A	0.50	0.36	5.0	0.18	8.68	1.6															Flows overlain along the western site boundary to DP1 Flows off-site to the west
	2	B	14.03	0.46	34.1	6.52	3.84	25.1															Sheet flows overlain to swale and then to DP2 Combines flow at FES at DP4.2
	3	OS1	8.74	0.36	49.4	3.15	2.90	9.2															Sheet flows overlain and along berm to DP3 Flows on-site and combines at culvert at DP4.1
	4	C	10.70	0.39	28.6	4.13	4.28	17.7															Sheet flows overlain to swale and then to DP4 Combines flow at culvert at DP4.1
	4.1								49.4	7.28	2.90	21.1											Combined flow of DP3 and DP4 within culvert Swale to FES at DP4.2
	4.2								49.4	13.80	2.90	40.1											Combined flow of DP2 and DP4.1 at sump inlet Piped to pond forebay, combines flow at DP9.1
	5	D	2.16	0.36	24.1	0.78	4.72	3.7															Sheet flows overlain to swale and then to DP5 Combines flow at sump inlet at DP7.1
	6	E	3.10	0.47	22.8	1.46	4.86	7.1															Sheet flows overlain to swale and then to DP6 Combines flow at sump inlet at DP7.1
	7	OS2	0.36	0.36	16.5	0.13	5.67	0.7															Sheet flows overlain to DP7 Combines flow at sump inlet at DP7.1
	7.1								24.1	2.37	4.72	11.2											Combined flow of DP5, DP6, and DP7 at sump inlet Piped to pond forebay, combines flow at DP9.1
	8	OS3	0.30	0.36	5.0	0.11	8.68	1.0															Sheet flows overlain to DP8 Combines flow at DP9.1
	9	F	2.27	0.36	18.5	0.82	5.38	4.4															Flows along trickle channel to DP9 at outlet structure Combines flow at DP9.1
	9.1								49.4	16.99	2.90	49.4											Combined flow of DP4.2, DP7.1, DP8 and DP9. Total Interim pond inflow. Released through pond outlet structure at DP9.2
	9.2											8.3											Released flow through interim outlet structure from M/HFD Detention Piped to existing junction box and storm infrastructure
	10	G	0.06	0.76	5.3	0.05	8.56	0.4															Flows along prop. Sterling Ranch Rd. c&g to DP10 to Markshffel Rd. Combines at existing Markshffel Rd. existing 15" Type R inlet.
	11	OS4	2.08	0.85	9.0	1.77	7.21	12.8															Off-site work along existing Markshffel Rd. c&g to ex. 15" Type R inlet. Combines at existing Markshffel Rd. existing 15" Type R inlet.
	11.1								9.0	1.82	7.21	13.1											Combined flow of DP 10 and DP11 within existing 15" Type R inlet. Captured flow continues off-site southeast along Markshffel Rd. storm

**Notes:**  
 Street and Pipe C\*A values are determined by Q/I using the catchment's intensity value.  
 All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

PROPOSED CONDITION  
ANALYSIS FOR SIZING OF  
SWALES & INLETS.

## COMPOSITE % IMPERVIOUS & COMPOSITE ULTIMATE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility  
 Location: El Paso County

Project Name: Sterling Ranch  
 Project No.: 2518814  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 2/8/24

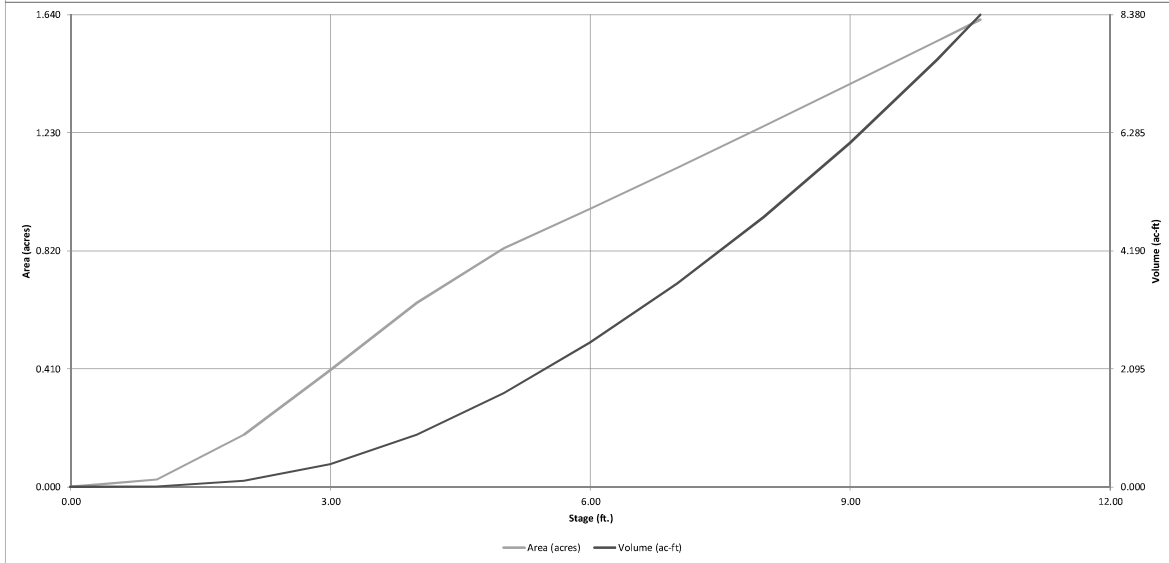
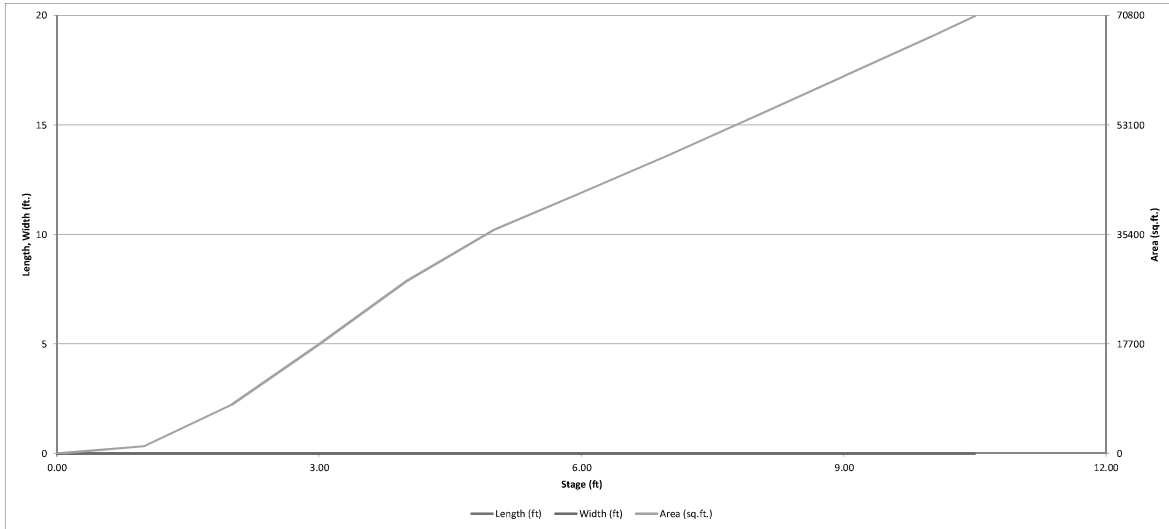
ULTIMATE CONDITION FOR POND SIZING FOR LOT 1

Basin ID	Total Area (ac)	Industrial-Heavy Areas (90% Impervious)			Business-Commercial Areas (95% Impervious)			Residential-1/8 Acre or Less (65% Impervious)			Streets-Paved (100% Impervious)			Historical Analysis (2% Impervious)			Basins Total Values		Basins Total Weighted % Imp.						
		C <sub>s</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>s</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>s</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>s</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>s</sub>		C <sub>100</sub>					
Lot 1 Heavy Industrial	4.74	0.73	0.81	4.74	90.0%	0.81	0.88	0.00	0.0%	0.45	0.59	0.00	0.0%	0.90	0.96	0.00	0.0%	0.09	0.36	0.00	0.0%	0.73	0.81	90.0%	
Urban Non-Residential Collector Roadway (R.O.W.)	1.78	0.73	0.81	0.00	0.0%	0.81	0.88	0.00	0.0%	0.45	0.59	0.00	0.0%	0.90	0.96	1.40	78.7%	0.09	0.36	0.38	0.4%	0.73	0.83	79.1%	
Lot 2 Residential-1/8 Acre or Less	24.05	0.73	0.81	0.00	0.0%	0.81	0.88	0.00	0.0%	0.45	0.59	24.05	65.0%	0.90	0.96	0.00	0.0%	0.09	0.36	0.00	0.0%	0.45	0.59	65.0%	
Tract A Detention Pond	1.85	0.73	0.81	0.00	0.0%	0.81	0.88	0.00	0.0%	0.45	0.59	0.00	0.0%	0.90	0.96	0.00	0.0%	0.09	0.36	1.85	2.0%	0.09	0.36	2.0%	
Future Commercial (Off-site to north)	8.74	0.73	0.81	0.00	0.0%	0.81	0.88	8.74	95.0%	0.45	0.59	0.00	0.0%	0.90	0.96	0.00	0.0%	0.09	0.36	0.00	0.0%	0.81	0.88	95.0%	
Future Heavy Industrial (Off-site to east)	1.87	0.73	0.81	1.87	90.0%	0.81	0.88	0.00	0.0%	0.45	0.59	0.00	0.0%	0.90	0.96	0.00	0.0%	0.09	0.36	0.00	0.0%	0.73	0.81	90.0%	
Detention Pond (Off-site to east)	0.44	0.73	0.81	0.00	0.0%	0.81	0.88	0.00	0.0%	0.45	0.59	0.00	0.0%	0.90	0.96	0.00	0.0%	0.09	0.36	0.44	2.0%	0.09	0.36	2.0%	
Detention Pond (Off-site to south)	0.30	0.73	0.81	0.00	0.0%	0.81	0.88	0.00	0.0%	0.45	0.59	0.00	0.0%	0.90	0.96	0.00	0.0%	0.09	0.36	0.30	2.0%	0.09	0.36	2.0%	
<b>Total Pond A</b>	<b>43.77</b>																							<b>71.6%</b>	
<b>Total W. Forebay (North Commercial, Lot 2, R.O.W.)</b>	<b>34.57</b>																						<b>0.56</b>	<b>0.68</b>	<b>73.3%</b>
<b>Total N. Forebay (Lot 1, East Heavy Industrial)</b>	<b>6.61</b>																						<b>0.73</b>	<b>0.81</b>	<b>90.0%</b>



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

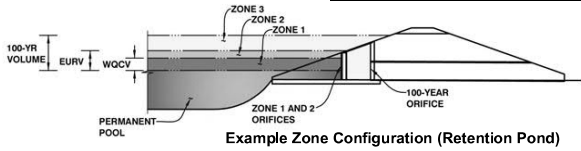
*MHFD-Detention, Version 4.06 (July 2022)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*

**Project: Sterling Ranch Recycling Facility**  
**Basin ID: Pond A-Ultimate**



**Example Zone Configuration (Retention Pond)**

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.16	1.037	Orifice Plate
Zone 2 (EURV)	7.38	2.987	Circular Orifice
Zone 3 (100-year)	8.83	1.839	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>5.864</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	4.16	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.35	2.77					
Orifice Area (sq. inches)	2.80	2.80	2.80					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	4.16	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	7.38	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	4.30	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.10	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.18	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)**

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	7.90	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	4.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Type =	Close Mesh Gate	N/A	
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>1</sub> =	7.90	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	9.01	N/A	
Overflow Gate Open Area w/o Debris =	12.66	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	6.33	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	11.00	N/A	inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.40	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.53	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.49	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage =	9.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	120.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.48	feet
Stage at Top of Freeboard =	10.48	feet
Basin Area at Top of Freeboard =	1.62	acres
Basin Volume at Top of Freeboard =	8.34	acre-ft

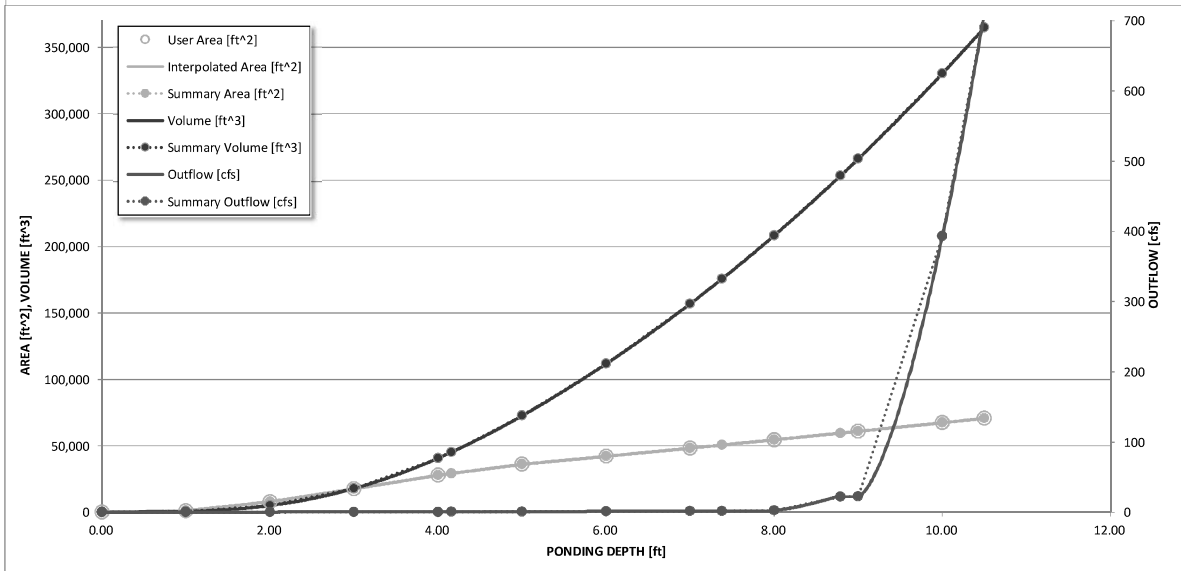
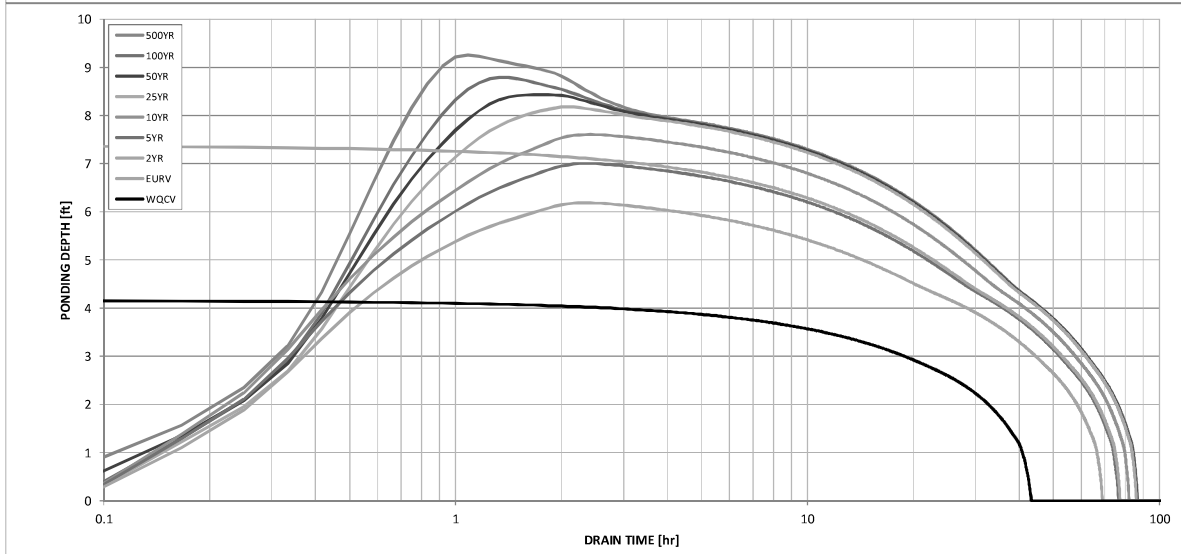
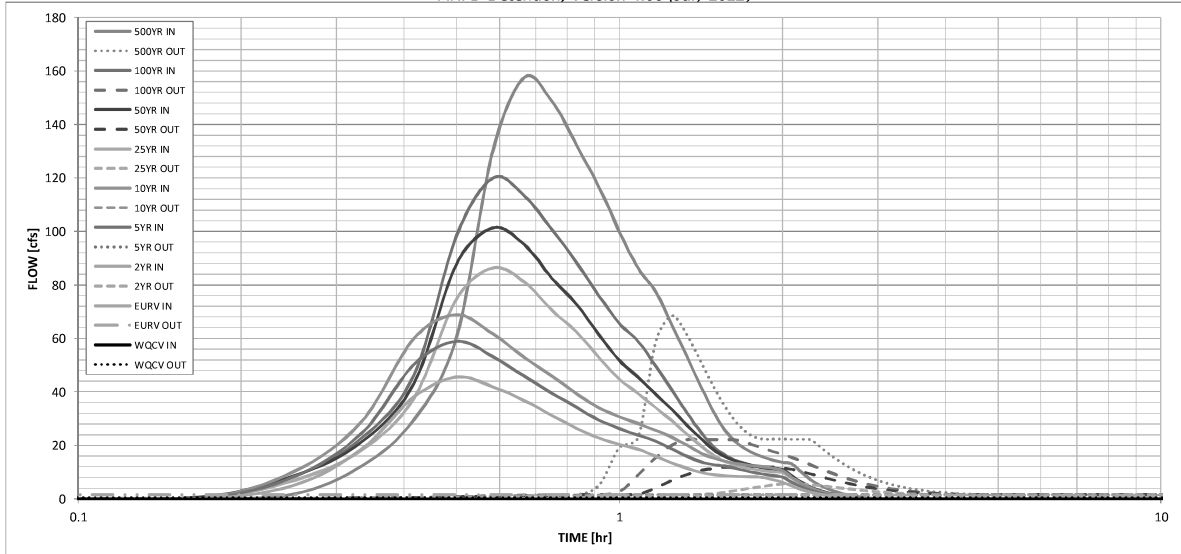
**Routed Hydrograph Results**

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	1.037	4.024	2.942	3.836	4.555	5.444	6.314	7.348	9.622
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.942	3.836	4.555	5.444	6.314	7.348	9.622
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.3	0.5	0.7	6.7	13.4	22.5	40.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.31	0.51	0.93
Peak Inflow Q (cfs) =	N/A	N/A	45.5	58.9	68.8	86.3	101.3	120.0	157.6
Peak Outflow Q (cfs) =	0.5	1.5	1.3	1.5	1.6	5.6	12.1	22.2	68.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.7	2.1	0.8	0.9	1.0	1.7
Structure Controlling Flow =	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.3	0.8	1.6	1.6
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hrs) =	39	67	60	66	71	73	72	71	68
Time to Drain 99% of Inflow Volume (hours) =	<b>41</b>	72	65	71	76	80	79	79	78
Maximum Ponding Depth (ft) =	4.16	7.38	6.19	7.00	7.61	8.18	8.43	8.79	9.25
Area at Maximum Ponding Depth (acres) =	0.67	1.16	0.99	1.11	1.19	1.28	1.32	1.37	1.44
Maximum Volume Stored (acre-ft) =	1.039	4.036	2.743	3.604	4.295	5.012	5.336	5.819	6.464

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

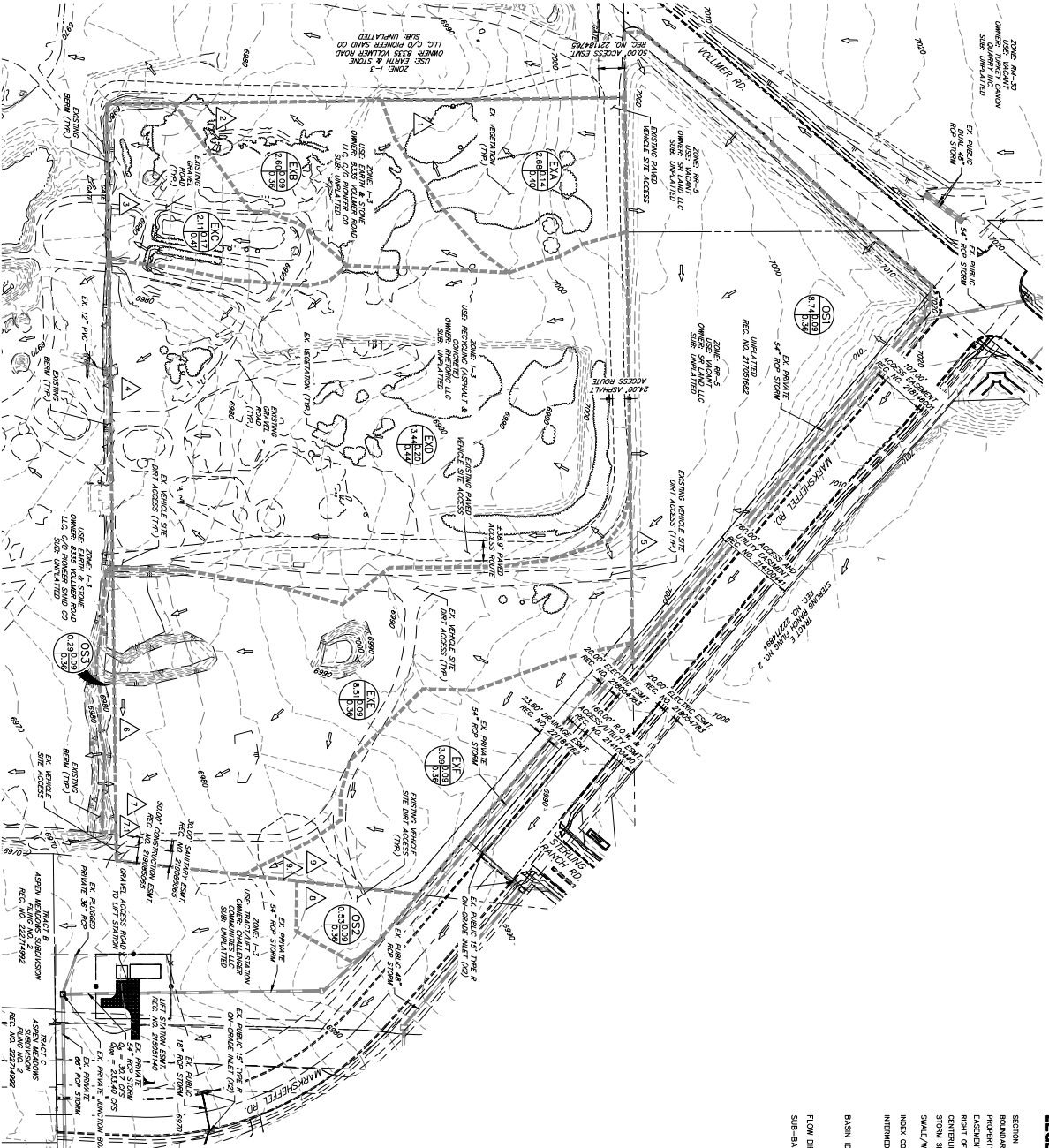
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5:00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.57	0.06	1.83
	0:15:00	0.00	0.00	5.05	8.22	10.18	6.84	8.59	8.34	12.16
	0:20:00	0.00	0.00	18.49	24.39	28.72	18.15	21.18	22.63	29.51
	0:25:00	0.00	0.00	38.05	50.12	59.86	37.51	43.02	46.17	60.49
	0:30:00	0.00	0.00	45.54	58.87	68.83	74.78	87.92	98.38	130.15
	0:35:00	0.00	0.00	41.90	53.26	61.67	86.30	101.33	119.99	157.58
	0:40:00	0.00	0.00	36.74	45.86	52.97	81.13	95.11	113.39	148.64
	0:45:00	0.00	0.00	31.21	39.50	45.91	70.58	82.55	100.68	132.31
	0:50:00	0.00	0.00	26.39	34.22	39.33	62.32	72.70	88.45	116.56
	0:55:00	0.00	0.00	22.70	29.43	33.99	52.82	61.36	75.91	99.84
	1:00:00	0.00	0.00	20.32	26.23	30.69	44.70	51.70	65.52	86.12
	1:05:00	0.00	0.00	18.51	23.80	28.11	39.37	45.45	58.85	77.48
	1:10:00	0.00	0.00	15.95	21.50	25.59	34.05	39.18	49.59	64.99
	1:15:00	0.00	0.00	13.45	18.71	23.09	29.16	33.43	40.80	53.16
	1:20:00	0.00	0.00	11.32	15.89	20.06	24.06	27.48	32.11	41.61
	1:25:00	0.00	0.00	9.80	13.80	16.95	19.69	22.38	24.67	31.79
	1:30:00	0.00	0.00	8.99	12.73	15.05	15.90	17.99	19.07	24.43
	1:35:00	0.00	0.00	8.58	12.15	13.89	13.59	15.33	15.79	20.11
	1:40:00	0.00	0.00	8.35	11.01	13.06	12.15	13.69	13.82	17.52
	1:45:00	0.00	0.00	8.20	10.02	12.46	11.21	12.62	12.47	15.72
	1:50:00	0.00	0.00	8.08	9.31	12.04	10.55	11.88	11.56	14.50
	1:55:00	0.00	0.00	7.16	8.78	11.48	10.11	11.38	10.90	13.63
	2:00:00	0.00	0.00	6.26	8.16	10.49	9.80	11.03	10.45	13.03
	2:05:00	0.00	0.00	4.79	6.27	8.01	7.59	8.53	8.03	10.00
	2:10:00	0.00	0.00	3.51	4.55	5.79	5.49	6.17	5.81	7.23
	2:15:00	0.00	0.00	2.55	3.31	4.20	3.98	4.47	4.23	5.27
	2:20:00	0.00	0.00	1.84	2.38	3.04	2.89	3.25	3.10	3.85
	2:25:00	0.00	0.00	1.31	1.66	2.15	2.04	2.29	2.19	2.72
	2:30:00	0.00	0.00	0.90	1.13	1.50	1.43	1.60	1.53	1.90
	2:35:00	0.00	0.00	0.60	0.78	1.04	1.01	1.13	1.08	1.34
	2:40:00	0.00	0.00	0.37	0.51	0.66	0.66	0.74	0.70	0.87
	2:45:00	0.00	0.00	0.19	0.30	0.37	0.39	0.43	0.41	0.50
	2:50:00	0.00	0.00	0.08	0.14	0.17	0.18	0.20	0.19	0.24
	2:55:00	0.00	0.00	0.03	0.04	0.05	0.06	0.06	0.06	0.07
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

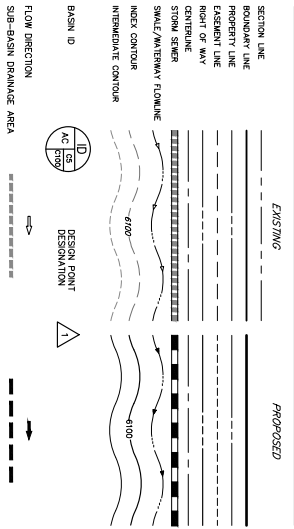


# STERLING RANCH RECYCLING FACILITY

## EXISTING DRAINAGE MAP

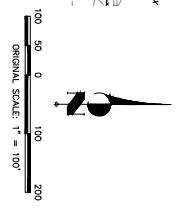


### LEGEND



Subbasin	Area (ac)	Impervious (%)	C <sub>1</sub>	C <sub>2</sub>	T <sub>1</sub> (min)	T <sub>2</sub> (min)	Q <sub>1</sub> (cfs)	Q <sub>2</sub> (cfs)
B3A	3.68	86%	0.34	0.40	21.1	1.1	5.4	
B3B	3.00	2%	0.09	0.36	25.9	0.6	4.3	
B3C	2.11	34%	0.17	0.41	22.4	1.0	4.3	
B3D	13.44	17%	0.20	0.44	23.4	7.6	28.1	
B3E	8.51	2%	0.09	0.36	27.7	3.0	13.4	
B3F	3.09	2%	0.09	0.36	24.1	0.8	5.2	
B3G	8.74	2%	0.09	0.36	40.4	1.4	8.2	
B3H	15.3	2%	0.09	0.36	15.8	0.7	4.1	
B3I	0.73	2%	0.09	0.36	5.0	0.2	0.9	

DP	CG	Q <sub>100</sub>
1	1.1	5.4
2	0.6	4.3
3	1.0	4.3
4	7.6	28.1
5	3.4	9.2
6	0.7	0.9
7	2.9	13.4
8	0.2	1.1
9	0.8	5.2
9.1	0.9	6.1



POD FILE NO. PFR2341 & SF2325  
 STERLING RANCH RECYCLING FACILITY  
 EXISTING DRAINAGE MAP  
 JOB NO. 251984.14  
 01/19/2024  
 SHEET 1 OF 1

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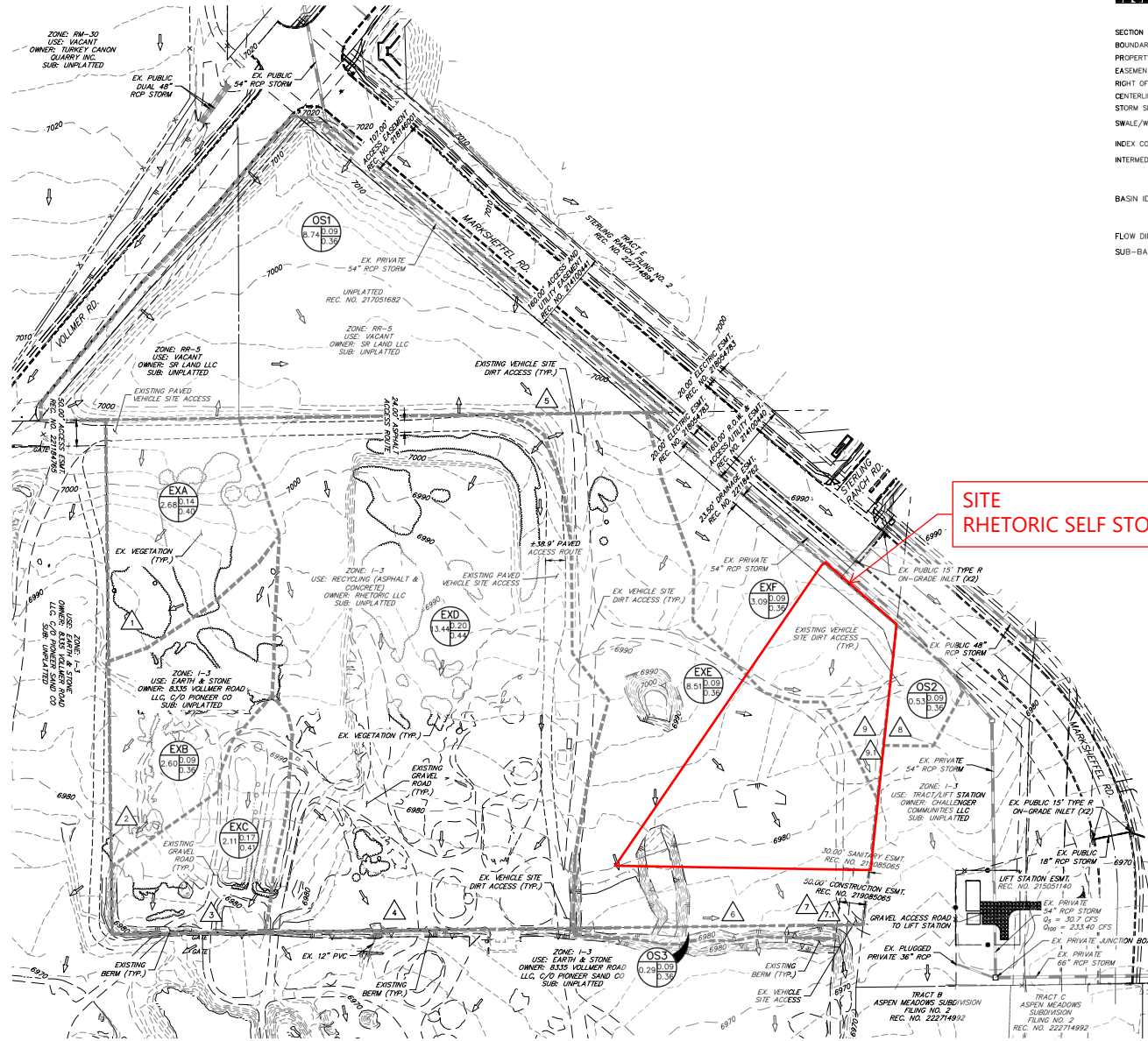




## **APPENDIX F – DRAINAGE MAPS**

# STERLING RANCH RECYCLING FACILITY

## EXISTING DRAINAGE MAP



### LEGEND

	EXISTING	PROPOSED
SECTION LINE	---	---
BOUNDARY LINE	---	---
PROPERTY LINE	---	---
EASEMENT LINE	---	---
RIGHT OF WAY	---	---
CENTERLINE	---	---
STORM SEWER	---	---
SWALE/WATERWAY FLOWLINE	---	---
INDEX CONTOUR	---	---
INTERMEDIATE CONTOUR	---	---
BASIN ID	⊙ ID AC CS STW	⊙
DESIGN POINT DESIGNATION	△	△
FLOW DIRECTION	→	→
SUB-BASIN DRAINAGE AREA	---	---

#### BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C <sub>s</sub>	C <sub>100</sub>	t <sub>s</sub> (min)	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
EVA	2.68	8%	0.14	0.40	21.1	1.1	5.4
EXB	2.60	2%	0.09	0.36	25.9	0.6	4.3
EXC	2.11	14%	0.17	0.41	22.4	1.0	4.3
EXD	13.44	17%	0.20	0.44	23.4	7.6	28.1
EXE	8.51	2%	0.09	0.36	27.7	2.0	13.4
EXF	3.09	2%	0.09	0.36	24.1	0.8	5.2
OS1	8.74	2%	0.09	0.36	49.4	1.4	9.2
OS2	0.53	2%	0.09	0.36	15.8	0.2	1.1
OS3	0.29	2%	0.09	0.36	5.0	0.2	0.9

#### DESIGN POINT

DP	QS	Q100
1	1.1	5.4
2	0.6	4.3
3	1.0	4.3
4	7.6	28.1
5	1.4	9.2
6	0.2	0.9
7	2.0	13.4
7.1	2.9	18.3
8	0.2	1.1
9	0.8	5.2
9.1	0.9	6.1

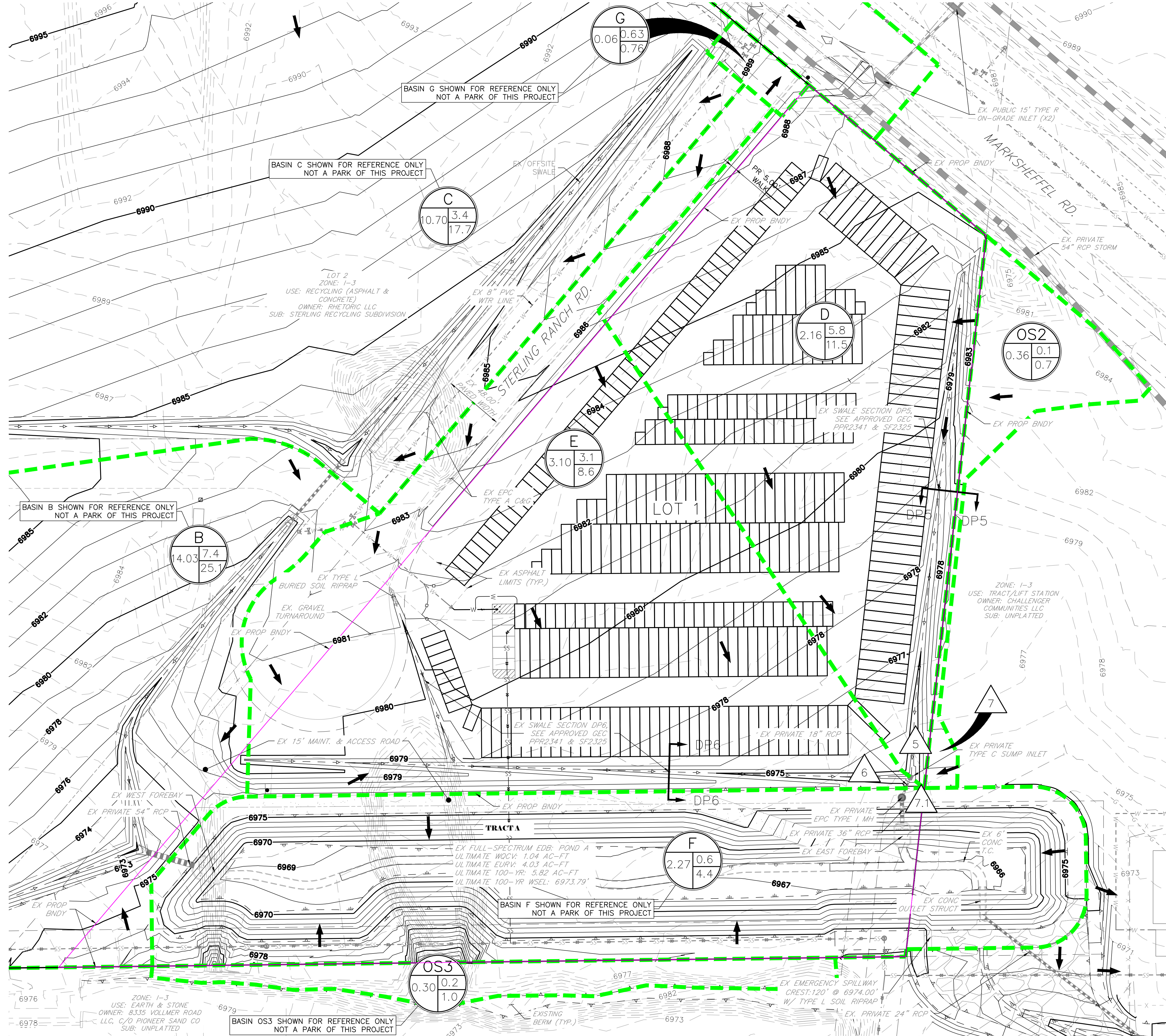
**SITE RHETORIC SELF STORAGE**

PCD FILE NO. PPR2341 & SF2325  
 STERLING RANCH RECYCLING FACILITY  
 EXISTING DRAINAGE MAP  
 JOB NO. 25188.14  
 01/19/2024  
 SHEET 1 OF 1



100 50 0 100 200  
 ORIGINAL SCALE: 1" = 100'

# RHETORIC SELF STORAGE PROPOSED DRAINAGE MAP



## LEGEND

	EXISTING	PROPOSED
SECTION LINE	---	---
BOUNDARY LINE	---	---
LOT 1 BOUNDARY LINE	---	---
PROPERTY LINE	---	---
EASEMENT LINE	---	---
RIGHT OF WAY	---	---
CENTERLINE	---	---
STORM SEWER	---	---
SWALE/WATERWAY FLOWLINE	---	---
INDEX CONTOUR	---	---
INTERMEDIATE CONTOUR	---	---
100-YEAR FLOODPLAIN	---	---
FLOW DIRECTION	---	---
BASIN ID	AC 05 0100	AC 05 0100
DESIGN POINT DESIGNATION	---	---
SUB-BASIN DRAINAGE AREA	---	---

## PROPOSED CALCS - BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C <sub>s</sub>	C <sub>100</sub>	t <sub>c</sub> (min)	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
D	2.16	73%	0.68	0.79	10.9	5.8	11.5
E	3.10	32%	0.32	0.53	19.4	3.1	8.6
OS2	0.36	2%	0.09	0.36	15.1	0.1	0.8

## DESIGN POINT SUMMARY TABLE

DP#	Q <sub>s</sub> -YR	Q <sub>100</sub> -YR
5	5.8	11.5
6	3.1	8.6
7	0.1	0.8
7.1	7.8	18.3

## PROPOSED DRAINAGE MAP NOTES:

- PROPOSED GRADING ON THIS DRAINAGE MAP WAS APPROVED WITH PCD FILE NO.: PPR2341 & SF2325. GRADING OPERATIONS HAVE ALREADY COMMENCED ON THE SITE & THE APPROVED GRADING IS SHOWN HERE FOR REFERENCE & IS UNCHANGED FROM THE ORIGINAL PROJECT.

PROPOSED DRAINAGE MAP  
RHETORIC SELF STORAGE  
JOB NO. 25005  
LOCATION: EPC  
07/21/2025

SHEET  
1

**ALL TERRAIN**  
ENGINEERING

