

December 15, 2023

Ms. Ashlyn Mathy  
El Paso County  
2880 International Circle, Suite 110,  
Colorado Springs, CO 80910

**Re: PCD File No. PPR2329  
The Rock Commerce Center, 2nd Review  
Response to Comments**

Dear Ms. Mathy,

Please accept this letter on behalf of Central Development, LLC, the applicant for The Rock Commerce Center. We received your comment letter dated December 8, 2023, regarding the application and we offer the following responses:

Site Plan

*Engineering and Planning Comments*

Sheet 5-6, Grading Plan – Responses were prepared by Redland

1. Wall will need drainage pan to direct flows around and not over wall. Refer to County detail SD\_3-44. Provide calculation for sizing of ditch section in drainage report.

**Response:** A drainage pan was added to direct flows around the walls and the County detail was added to the SDP set. An SF table and flow calculations were added to the Drainage Report for sizing of the drainage pan.

Public Improvement Plan Construction Documents

*Engineering Comments*

Sheet C3.0, Horizontal Control Plan – Responses were prepared by Redland

2. Riprap depth should be minimum of 12" (2xD50 of riprap size).

**Response:** The riprap was all updated to be 12" deep on all plans.

Sheet C4.0, Plan and Profile - Responses were prepared by Redland

3. Riprap depth should be minimum of 12" (2xD50 of riprap size).

**Response:** The riprap was all updated to be 12" deep on all plans.

4. Per DCM Section 8.3 include HGL.

**Response:** The 10-YR and 100-YR HGLs were added to this storm sewer profile and labeled.

Sheet C6.0, Erosion Control Plan - Responses were prepared by Redland

5. Riprap depth should be minimum of 12" (2xD50 of riprap size).

**Response:** The riprap was all updated to be 12" deep on all plans.

Grading and Erosion Control Plans

Engineering and EPC Stormwater Comments

Sheet 4, Grading Plan – Responses were prepared by Redland

6. Riprap depth should be minimum of 12" (2xD50 of riprap size).

**Response:** The riprap was all updated to be 12" deep on all plans.

Sheet 8, Interim Erosion Control Plan – Responses were prepared by Redland

7. Assign a name/number to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling throughout (example Pond A or Pond 1).

**Response:** The full spectrum detention pond was named Pond A and it was updated in all plans and reports.

8. Riprap depth should be minimum of 12" (2xD50 of riprap size).

**Response:** The riprap was all updated to be 12" deep on all plans.

Sheet 9, Final Erosion Control Plan – Responses were prepared by Redland

9. Call out type of riprap and size of pad. Provide a detail showing how the riprap will tie into the trickle channel without causing erosion or undermining at interface.

**Response:** The trickle channel was extended up to the flared end section and a splash wall was added where this trickle channel branch meets up with the main trickle channel to act as a energy dissipator as the flow is directed 90 degrees towards the outlet structure.

Sheet 10, Pond Details – Responses were prepared by Redland

10. Please submit a State Non-Jurisdictional Water Impoundment Structure Application for this pond.

**Response:** This application will be submitted as requested.

11. Provide a bolt at top and bottom of orifice plate to ensure a water tight seal.

**Response:** A bolt was added to the top and bottom of the orifice plate as requested.

12. Change rectangular to circular in the orifice opening note.

**Response:** This note was updated as requested.

13. Provide details for Outlet structure, Forebay, and Trickle Channel.

**Response:** These details were added as requested.

14. Verify all highlighted elevation. Heights and depths should be from micropool elevation which is 7134.00 per MHFD Detention spreadsheet in FDR.

**Response:** The MHFD spreadsheet was updated so that the micropool is at the correct elevation of 7134.23.

15. First orifice is set at micropool elevation, which per MHFD spreadsheet in Drainage report is 7134.00.

**Response:** The MHFD spreadsheet was updated so that the micropool is at the correct elevation of 7134.23.

16. Please revise the minimum access road width is 15'.

**Response:** These details were updated to reflect the 15' wide access road.

17. Provide a cross section detail of spillway.

**Response:** A cross section detail of the emergency spillway was added as requested.

18. Please label detail.

**Response:** The emergency spillway detail was labeled as requested.

Final Drainage Report – Responses were prepared by Redland

*Engineering and EPC Stormwater Comments*

19. *Change the Orifice area from 1.30 to 1.35.*

**Response:** This was updated on the MHFD spreadsheet.

20. Updated the debris clogging % from 0% to 50%.

**Response:** This was updated on the MHFD spreadsheet and the resulting changes were updated throughout the Report.

21. Riprap is not seen on the Plans at DP-C, please confirm location.

**Response:** The riprap at DP-C was covered by the major basin line, this was shifted so that the riprap is now visible.

Traffic Impact Study – Responses were prepared by Fox Tuttle Transportation Group

*Engineering Comments*

1. *State what the spacing is that is described in ECM Table 2-35.*

**Response:** Required spacing from ECM Table 2-35 has been listed specifically in the report text.

2. *Indicate if the applicant intends to pay the full-fee amount or use one the two PID options. Refer to Resolution 19-471(Copy attached in EDarp For Reference)*

**Response:** Clarification has been added that the owner intends to pay the full fee amount and does not plan to use either PID option.

If you have any questions regarding the above response to comments, please contact me at 720-283-6783 ext. 136 or at mcevaal@redland.com.

Sincerely,



Mark D. Cevaal, P.E.  
Sr. Project Manager

# THE ROCK COMMERCE CENTER

## SITE DEVELOPMENT PLAN

LOCATED IN THE SOUTHWEST QUARTER OF THE  
NORTHWEST QUARTER OF SECTION 11, TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
EL PASO COUNTY, STATE OF COLORADO.

### PROJECT TEAM

#### OWNER / DEVELOPER

CENTRAL DEVELOPMENT, LLC  
1600 S. ALBON ST., #200  
DENVER, CO 80222  
303.628.0200 voice  
CONTACT: JEREMY RECORDS

#### CIVIL ENGINEER

REDLAND  
1500 W. CANAL CT.  
LITTLETON, CO 80120  
720.283.6783 voice  
CONTACT: MARK CEVAAL, P.E.  
EMAIL: mcevaal@redland.com

#### ARCHITECT

INTERGROUP ARCHITECTS  
2000 W. LITTLETON BLVD.  
LITTLETON, CO 80120  
303.407.1157 voice  
CONTACT: BILL SMITH, AIA

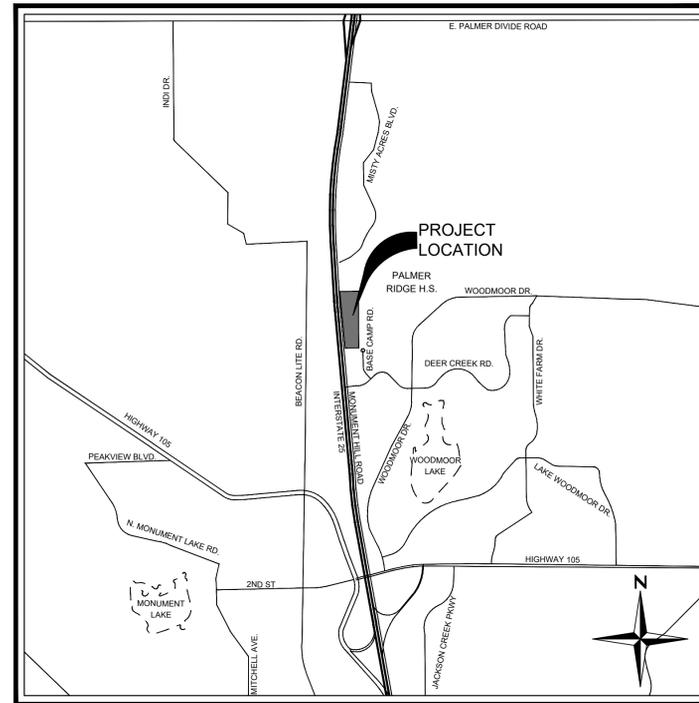
#### LANDSCAPE ARCHITECT

STACKLOT  
5366 S. CURTICE ST.  
LITTLETON, CO 80120  
303.808.4523 voice  
CONTACT: STEVE WIENS  
EMAIL: steve@stacklot.com

### LEGAL DESCRIPTION:

#### PARCEL B:

THAT PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11, TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE 6TH P.M. LYING EAST OF THE EAST LINE OF THAT TRACT CONVEYED TO THE STATE HIGHWAY DEPARTMENT BY QUITCLAIM DEED RECORDED SEPTEMBER 8, 1948 IN BOOK 1185, PAGE 458, ALSO DESCRIBED AS: THAT PART OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11, TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE P.M., COUNTY OF EL PASO, STATE OF COLORADO, MORE PARTICULARLY DESCRIBED AS FOLLOWS:  
COMMENCING AT THE SOUTHWEST CORNER OF SAID NORTHWEST QUARTER; THENCE EASTERLY ALONG THE SOUTHERLY LINE OF SAID NORTHWEST QUARTER A DISTANCE OF 996.04 FEET TO A POINT ON THE EASTERLY RIGHT-OF-WAY OF INTERSTATE HIGHWAY 25 DESCRIBED IN THAT DEED TO THE STATE HIGHWAY DEPARTMENT RECORDED SEPTEMBER 8, 1948 IN BOOK 1185 AT PAGE 458, WHICH POINT IS THE TRUE POINT OF THE BEGINNING OF THE PARCEL TO BE DESCRIBED; THENCE ON A DEFLECTION ANGLE TO THE LEFT 95°08'20" AND ALONG SAID EASTERLY RIGHT OF WAY LINE A DISTANCE OF 1334.24 FEET TO A POINT ON THE NORTHERLY LINE OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER; THENCE ON A DEFLECTION ANGLE TO THE RIGHT 95°00'36" AND ALONG SAID NORTHERLY LINE 441.95 FEET TO THE NORTHEAST CORNER OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER; THENCE ON A DEFLECTION ANGLE TO THE RIGHT 90°16'15" AND ALONG THE EASTERLY LINE OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER A DISTANCE OF 1329.88 FEET TO THE SOUTHEAST CORNER OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER; THENCE ON A DEFLECTION ANGLE TO THE RIGHT 89°51'29" AND ALONG THE SOUTHERLY LINE OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER A DISTANCE OF 319.15 FEET TO THE POINT OF BEGINNING.



VICINITY MAP  
SCALE: 1" = 2000'

#### BENCHMARK

NGS CONTROL POINT T 395 BEING A STANDARD NGS STEEL ROD IN A LOGO MONUMENT BOX LOCATED 20 MILES NORTH OF COLORADO SPRINGS ON THE EAST SIDE OF I-25, 1,200 FEET NORTH OF THE WEIGH STATION BUILDING, AND 20.5 FEET EAST OF THE EASTERLY EDGE OF OIL OF THE NORTHBOUND LANES OF I-25.

NAVD88. ELEV = 7111.32'

#### BASIS OF BEARINGS

BEARINGS SHOWN HEREON ARE REFERENCED TO THE SOUTHERLY BOUNDARY OF LOT 1, GREATER EUROPE MISSION SUBDIVISION FILING NO. 1, BEING MONUMENTED AS SHOWN HEREON, ASSUMED TO BEAR SOUTH 80°00'37" WEST, A DISTANCE OF 358.79 FEET.

Sheet List Table	
Sheet Number	Sheet Title
1 OF 20	COVER SHEET
2 OF 20	OVERALL SITE PLAN
3 OF 20	SITE PLAN
4 OF 20	SITE PLAN
5 OF 20	GRADING PLAN
6 OF 20	GRADING PLAN
7 OF 20	UTILITY PLAN
8 OF 20	UTILITY PLAN
9 OF 20	LANDSCAPE PLAN 'A'
10 OF 20	LANDSCAPE PLAN 'B'
11 OF 20	LANDSCAPE PLAN 'C'
12 OF 20	LANDSCAPE NOTES
13 OF 20	LANDSCAPE DETAILS
14 OF 20	EXTERIOR ELEVATIONS
15 OF 20	EXTERIOR ELEVATIONS
16 OF 20	EXTERIOR ELEVATIONS
17 OF 20	EXTERIOR PERSPECTIVES
18 OF 20	SITE DETAILS
19 OF 20	PHOTOMETRIC SITE PLAN
20 OF 20	PHOTOMETRIC DETAILS

**15 Redland**  
YEARS WHERE GREAT PLACES BEGIN

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009			
	08/08/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
COVER SHEET

SHEET

1 OF 20

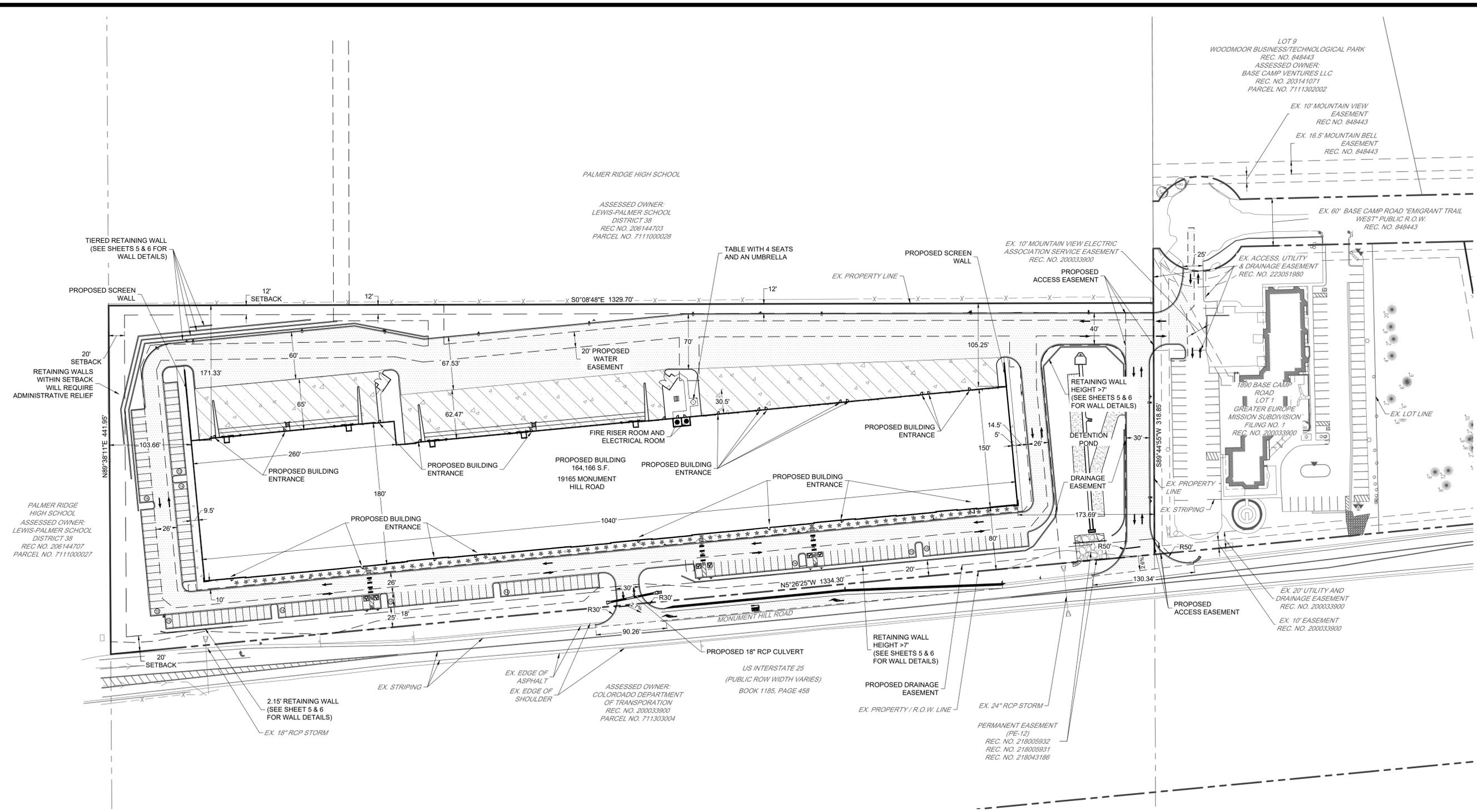
I:\2023\23009 - The Rock Commerce Center\CAAD\Sheet Sets\Site Plan\The Rock\23009\_Cover Sheet.dwg tab: 1 OF 24 COVER SHEET Nov 20, 2023 - 7:23am csalz

I:\2023\23009 - The Rock Commerce Center\CAD\Sheet Sets\Site Plan\The Rock\23009\_Overall Site Plan.dwg Tab: 2 OF 24 OVERALL SITE PLAN Nov 20, 2023 - 7:23am caoiz

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	DATE	NO.	NOTES
23009	08/08/2023	1	10/20/2023	2	1ST SUBMITTAL
		2	11/17/2023	3	2ND SUBMITTAL
		3			3RD SUBMITTAL

**THE ROCK COMMERCE CENTER  
 SITE DEVELOPMENT PLAN  
 OVERALL SITE PLAN**



- NOTE:
1. ANY WORK WITHIN EL PASO COUNTY RIGHT-OF-WAY REQUIRES A WORK IN RIGHT-OF-WAY PERMIT FROM EL PASO COUNTY DEPARTMENT OF PUBLIC WORKS.
  2. A BUILDING PERMIT FORM PIKES PEAK REGIONAL BUILDING DEPARTMENT IS REQUIRED FOR RETAINING WALLS GREAT THAN 4 FEET IN HEIGHT.

**PROPOSED LEGEND**

[Symbol]	EASEMENT
[Symbol]	CURB AND GUTTER
[Symbol]	SIDEWALK
[Symbol]	CONCRETE PAVEMENT
[Symbol]	ASPHALT PAVEMENT
[Symbol]	LIMITS OF CONSTRUCTION / SAWCUT
[Symbol]	PEDESTRIAN ACCESSIBLE ROUTE
[Symbol]	RETAINING WALL

**EXISTING LEGEND**

[Symbol]	PROPERTY LINE
[Symbol]	R.O.W.
[Symbol]	LOT LINE
[Symbol]	EASEMENT LINE
[Symbol]	SECTION LINE
[Symbol]	EDGE OF PAVEMENT
[Symbol]	CURB AND GUTTER
[Symbol]	CONCRETE
[Symbol]	FENCE
[Symbol]	SETBACK

**SITE DATA TABLE**

LOT 1, THE ROCK COMMERCE CENTER SUBDIVISION FILING NO. 1	REQUIRED	PROPOSED
ZONING	CS	CS
PARCEL AREA	11.61 AC. (505,680 S.F.)	11.61 AC. (505,680 S.F.)
BUILDING AREA	-	163,800 S.F.
BUILDING HEIGHT	40' MAX.	36'
STANDARD SPACES	*RETAIL = 28 SPACES *WAREHOUSE = 123 SPACES TOTAL = 151 SPACES	PROPOSED PARKING = 151 SPACES
ACCESSIBLE SPACES	6 ACCESSIBLE SPACES	6 ACCESSIBLE SPACES
VAN ACCESSIBLE	1 VAN ACCESSIBLE SPACE	1 VAN ACCESSIBLE SPACES
LANDSCAPE AREA	-	2.4 AC. (105,409.5 S.F. / 20.8%)
HARDSCAPE AREA	-	9.2 AC. (400,270.5 S.F. / 79.2%)

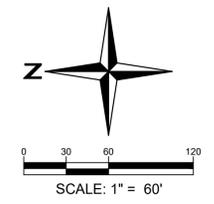
- \* RETAIL = 10% OF BLDG S.F. @ 1/600 S.F.
- \* WAREHOUSE = 90% OF BLDG S.F. @ 1/1200 S.F.
- \* AN ALTERNATIVE PARKING RATIO WILL BE REQUESTED TO CHANGE THE WAREHOUSE PARKING TO 1 SPACE PER 1,200 S.F. FROM 1 SPACE PER 1,000 S.F.
- \* THE TOTAL AMOUNT OF ACCESSIBLE SPACES WILL STILL FOLLOW THE ORIGINAL CODE.

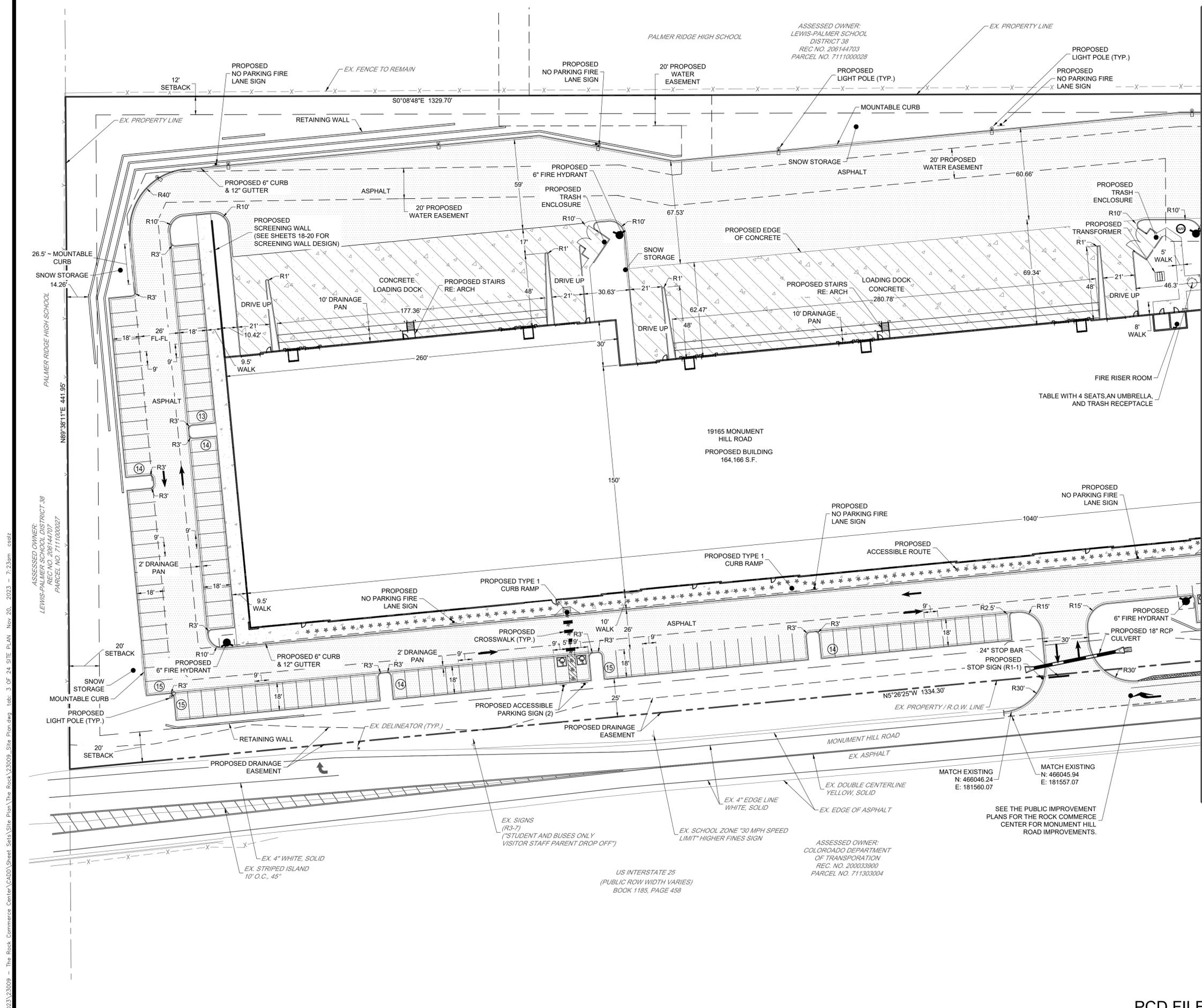
**SITE DATA TABLE**

LOT 1, GREATER EUROPE MISSION FILING NO. 1	
ZONING	CS
PARCEL AREA	3.59 AC. (156,422 S.F.)
BUILDING AREA	+11,784 S.F.
BUILDING HEIGHT	45' MAX.
STANDARD SPACES	REQUIRED = 59 SPACES EXISTING = 96 SPACES PROPOSED = 88 SPACES
ACCESSIBLE SPACES	3 ACCESSIBLE SPACES
VAN ACCESSIBLE	1 VAN ACCESSIBLE
LANDSCAPE AREA	(87,973.7 S.F. / 56.2%)
HARDSCAPE AREA	(68,448.3 S.F. / 43.8%)

NOTE:  
 THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.

PCD FILE NO. PPR2329





- PROPOSED LEGEND**
- EASEMENT
  - CURB AND GUTTER
  - SIDEWALK
  - CONCRETE PAVEMENT
  - ASPHALT PAVEMENT
  - LIMITS OF CONSTRUCTION / SAWCUT
  - \*\*\*\*\* PEDESTRIAN ACCESSIBLE ROUTE
  - RETAINING WALL
  - FIRE HYDRANT

- EXISTING LEGEND**
- PROPERTY LINE
  - R.O.W.
  - LOT LINE
  - EASEMENT LINE
  - SECTION LINE
  - EDGE OF PAVEMENT
  - CURB AND GUTTER
  - CONCRETE
  - FENCE
  - SETBACK

NOTE: THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.

MATCHLINE - SEE SHEET NO. 4 OF 20

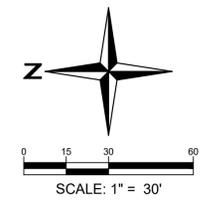
**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND, CO  
 • Land Planning • Landscape Architecture • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	08/08/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
 SITE PLAN

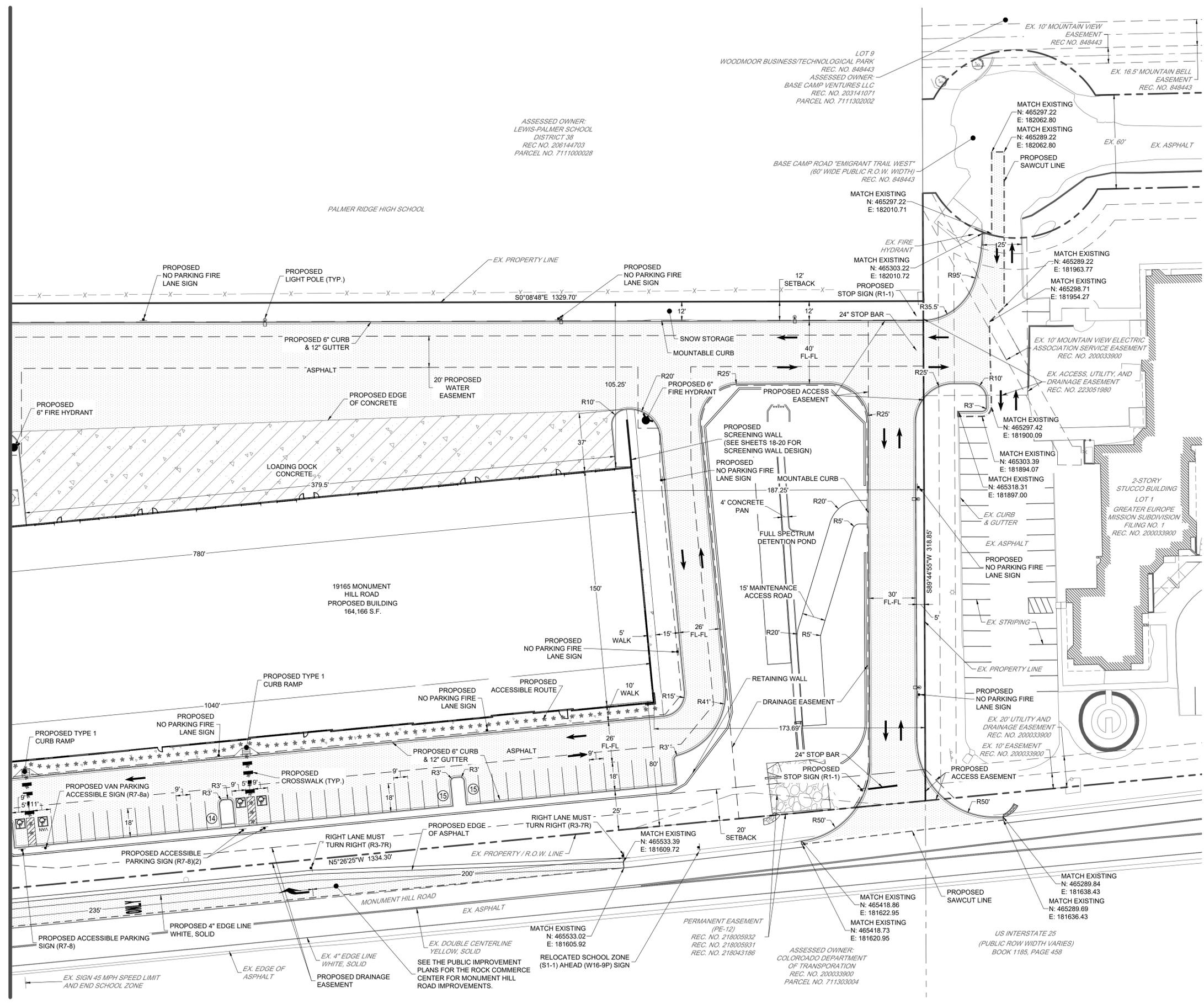
PCD FILE NO. PPR2329



I:\2023\23009 - The Rock Commerce Center\CAAD\Sheet Sets\Site Plan\The Rock\23009\_Site Plan.dwg tab: 3 OF 24 SITE PLAN Nov 20, 2023 -- 7:23am csalz  
 ASSESSED OWNER: LEWIS-PALMER SCHOOL DISTRICT 38  
 REC NO. 206144707  
 PARCEL NO. 7111000027  
 PALMER RIDGE HIGH SCHOOL  
 N89°38'11"E 441.95'  
 26.5' - MOUNTABLE CURB  
 SNOW STORAGE 14.26'  
 12' SETBACK  
 PROPOSED NO PARKING FIRE LANE SIGN  
 EX. FENCE TO REMAIN  
 S0°08'48"E 1329.70'  
 EX. PROPERTY LINE  
 RETAINING WALL  
 PROPOSED 6" FIRE HYDRANT  
 PROPOSED NO PARKING FIRE LANE SIGN  
 20' PROPOSED WATER EASEMENT  
 PROPOSED LIGHT POLE (TYP.)  
 EX. PROPERTY LINE  
 PROPOSED LIGHT POLE (TYP.)  
 PROPOSED NO PARKING FIRE LANE SIGN  
 20' PROPOSED WATER EASEMENT  
 MOUNTABLE CURB  
 SNOW STORAGE  
 20' PROPOSED WATER EASEMENT  
 60.66'  
 PROPOSED TRASH ENCLOSURE  
 PROPOSED TRASH ENCLOSURE  
 PROPOSED TRANSFORMER  
 R10'  
 R10'  
 5' WALK  
 R10'  
 46.3'  
 DRIVE UP  
 8' WALK  
 FIRE RISER ROOM  
 TABLE WITH 4 SEATS, AN UMBRELLA, AND TRASH RECEPTACLE  
 19165 MONUMENT HILL ROAD  
 PROPOSED BUILDING 164,166 S.F.  
 PROPOSED NO PARKING FIRE LANE SIGN  
 PROPOSED ACCESSIBLE ROUTE  
 PROPOSED TYPE 1 CURB RAMP  
 PROPOSED NO PARKING FIRE LANE SIGN  
 1040'  
 PROPOSED NO PARKING FIRE LANE SIGN  
 PROPOSED TYPE 1 CURB RAMP  
 PROPOSED CROSSWALK (TYP.)  
 10' WALK 26'  
 9'  
 R3'  
 R3'  
 18'  
 24" STOP BAR  
 PROPOSED STOP SIGN (R1-1)  
 R30'  
 PROPOSED 6" FIRE HYDRANT  
 PROPOSED 18" RCP CULVERT  
 R30'  
 20' SETBACK  
 SNOW STORAGE  
 MOUNTABLE CURB  
 PROPOSED LIGHT POLE (TYP.)  
 20' SETBACK  
 RETAINING WALL  
 EX. DELINEATOR (TYP.)  
 PROPOSED DRAINAGE EASEMENT  
 EX. 4" WHITE, SOLID  
 EX. STRIPED ISLAND 10' O.C., 45°  
 EX. SIGNS (R3-7) ("STUDENT AND BUSES ONLY VISITOR STAFF PARENT DROP OFF")  
 EX. SCHOOL ZONE "30 MPH SPEED LIMIT" HIGHER FINES SIGN  
 US INTERSTATE 25 (PUBLIC ROW WIDTH VARIES) BOOK 1185, PAGE 458  
 ASSESSED OWNER: COLORADO DEPARTMENT OF TRANSPORTATION REC. NO. 200033900 PARCEL NO. 711303004  
 MATCH EXISTING N: 466046.24 E: 181560.07  
 MATCH EXISTING N: 466045.94 E: 181557.07  
 SEE THE PUBLIC IMPROVEMENT PLANS FOR THE ROCK COMMERCE CENTER FOR MONUMENT HILL ROAD IMPROVEMENTS.  
 N5°26'25"W 1334.30'  
 EX. PROPERTY / R.O.W. LINE  
 MONUMENT HILL ROAD  
 EX. ASPHALT  
 EX. DOUBLE CENTERLINE YELLOW, SOLID  
 EX. EDGE OF ASPHALT  
 EX. 4" EDGE LINE WHITE, SOLID

I:\2023\23009 - The Rock Commerce Center\Sheet Sets\Site Plan\The Rock\23009\_Site Plan.dwg tab: 4 OF 24 SITE PLAN Nov 20, 2023 - 7:23am csalz

MATCHLINE - SEE SHEET NO. 3 OF 20



- PROPOSED LEGEND**
- EASEMENT
  - CURB AND GUTTER
  - SIDEWALK
  - CONCRETE PAVEMENT
  - ASPHALT PAVEMENT
  - LIMITS OF CONSTRUCTION / SAWCUT
  - PEDESTRIAN ACCESSIBLE ROUTE
  - RETAINING WALL
  - FIRE HYDRANT
- EXISTING LEGEND**
- PROPERTY LINE
  - R.O.W.
  - LOT LINE
  - EASEMENT LINE
  - SECTION LINE
  - EDGE OF PAVEMENT
  - CURB AND GUTTER
  - CONCRETE
  - FENCE
  - SETBACK

NOTE: THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.

**15 Redland YEARS**  
 WHERE GREAT PLACES BEGIN

720.283.6783  
 REDLAND.CO.VA

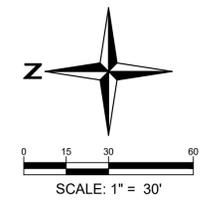
• Land Planning  
 • Landscape Architecture  
 • Civil Engineering  
 • Construction Management

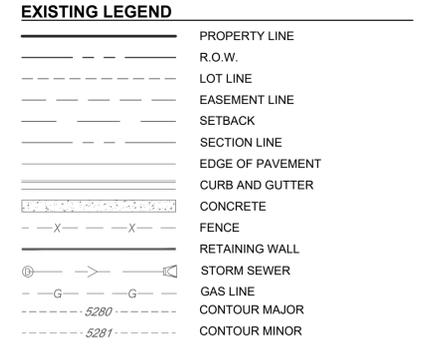
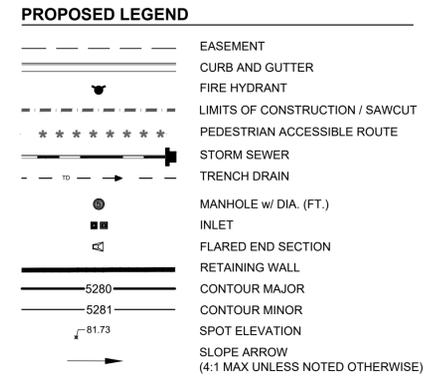
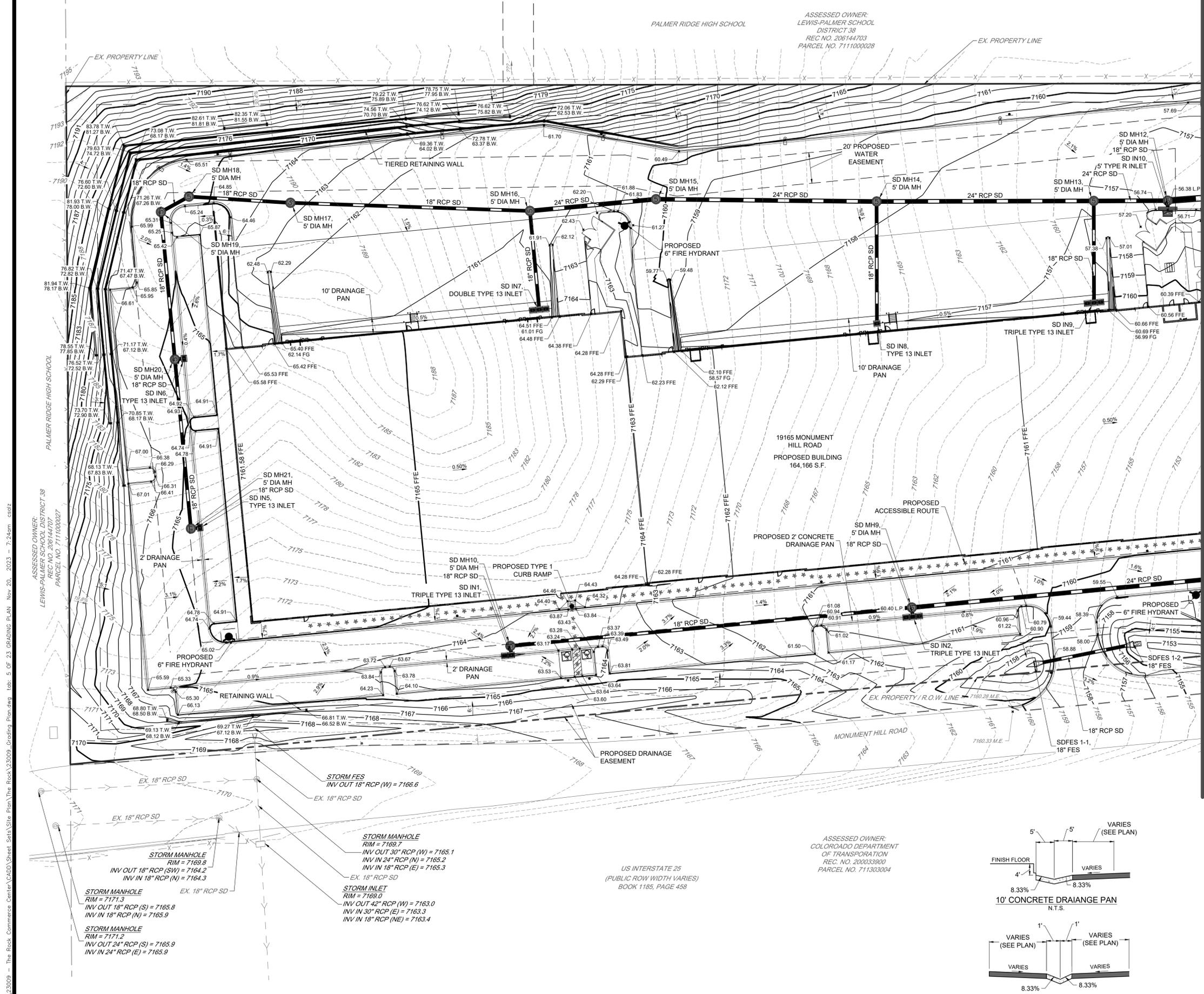
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	08/08/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

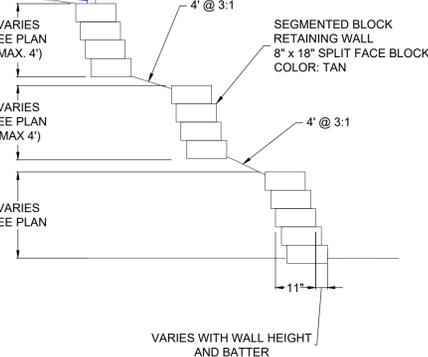
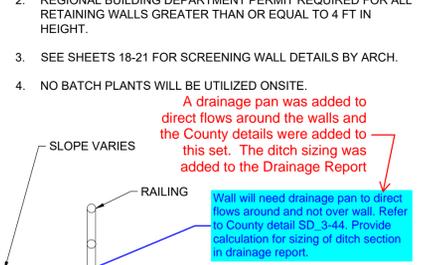
**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
 SITE PLAN

PCD FILE NO. PPR2329

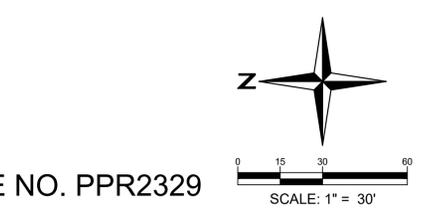




- NOTE:
- THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OR PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.
  - REGIONAL BUILDING DEPARTMENT PERMIT REQUIRED FOR ALL RETAINING WALLS GREATER THAN OR EQUAL TO 4 FT IN HEIGHT.
  - SEE SHEETS 18-21 FOR SCREENING WALL DETAILS BY ARCH.
  - NO BATCH PLANTS WILL BE UTILIZED ONSITE.



NOTE: RETAINING WALL WILL REQUIRE A SEPARATE BUILDING PERMIT



**15 Redland**  
WHERE GREAT PLACES BEGIN  
YEARS

720.283.6793  
REDLAND, CO • Landscape Architecture • Land Planning • Civil Engineering • Construction Management

**NOT FOR CONSTRUCTION**

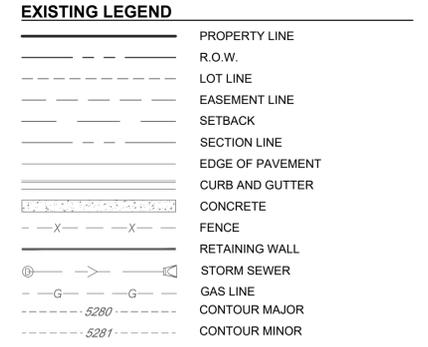
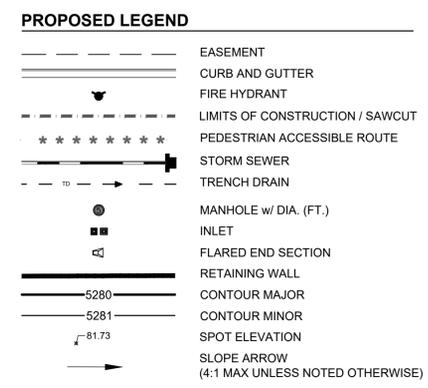
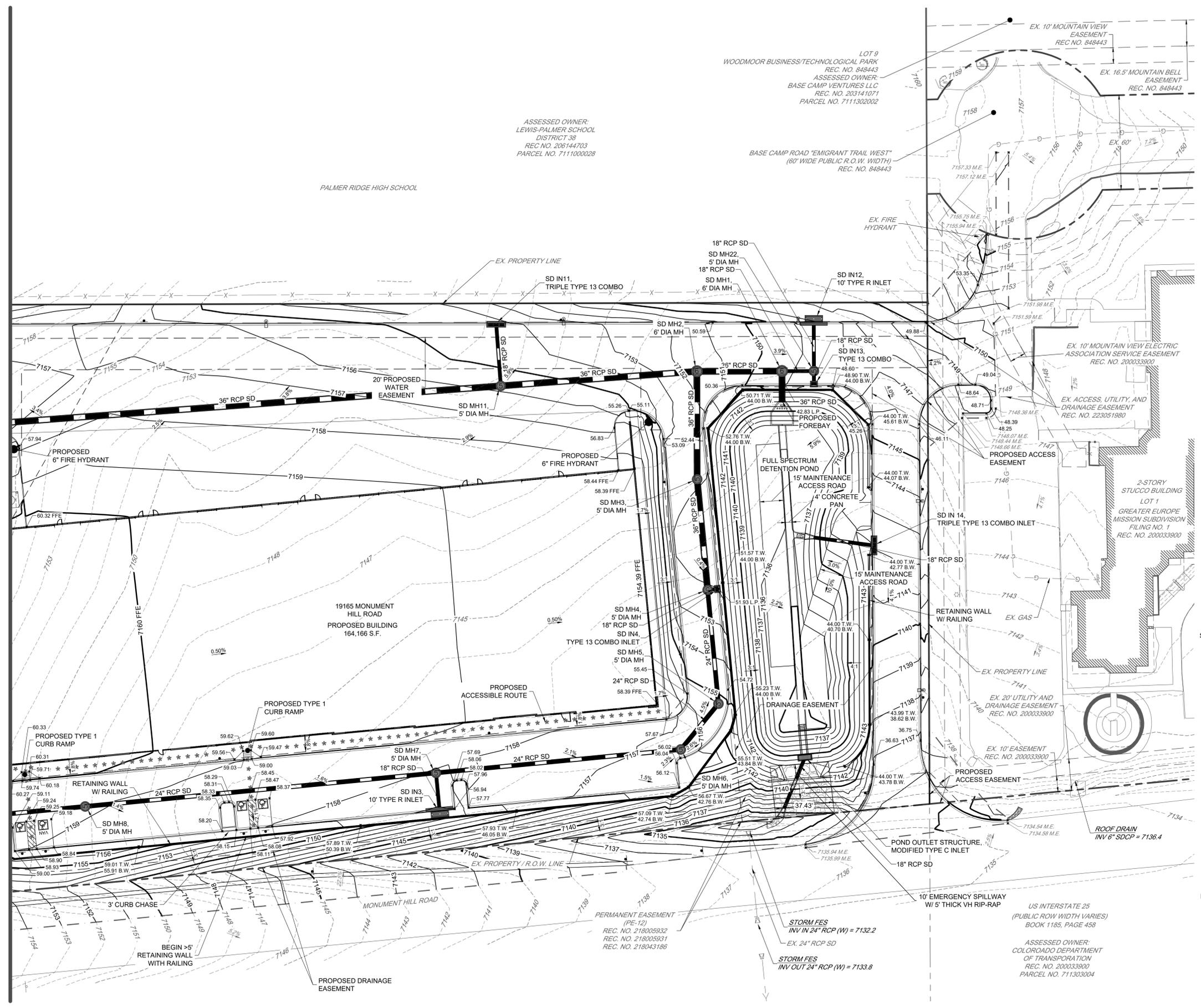
PROJECT NO.	DATE	NO.	NOTES
23009	08/08/2023	1	1ST SUBMITTAL
	10/02/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
GRADING PLAN

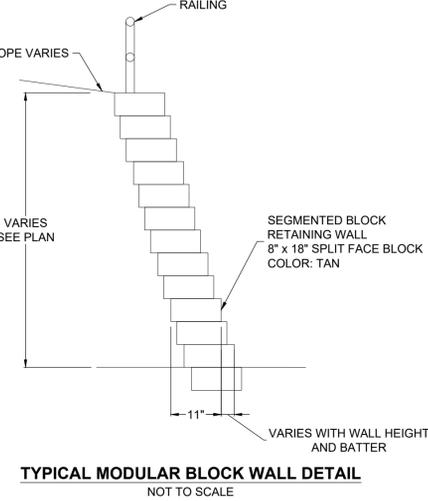
I:\2023\23009 - The Rock Commerce Center\CA00\Sheet\Set1\Site Plan\The Rock\23009\_Grading Plan.dwg tab: 5 OF 23 GRADING PLAN Nov 20, 2023 - 7:24am caalz

I:\2023\23009 - The Rock Commerce Center\Sheet Sets\Site Plan\The Rock\_V23009\_Grading Plan.dwg tab: 6 OF 22 GRADING PLAN Nov 20, 2023 - 7:24am casj

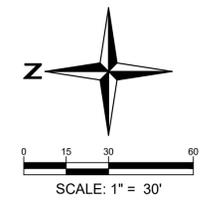
MATCHLINE - SEE SHEET NO. 5 OF 20



- NOTE:
1. THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.
  2. REGIONAL BUILDING DEPARTMENT PERMIT REQUIRED FOR ALL RETAINING WALLS GREATER THAN OR EQUAL TO 4 FT IN HEIGHT.
  3. SEE SHEETS 18-21 FOR SCREENING WALL DETAILS BY ARCH.
  4. NO BATCH PLANTS WILL BE UTILIZED ONSITE.



NOTE: RETAINING WALL WILL REQUIRE A SEPARATE BUILDING PERMIT



**15 Redland**  
 WHERE GREAT PLACES BEGIN  
 YEARS  
 720.283.6793  
 REDLAND, CO  
 • Land Planning  
 • Landscape Architecture  
 • Civil Engineering  
 • Construction Management

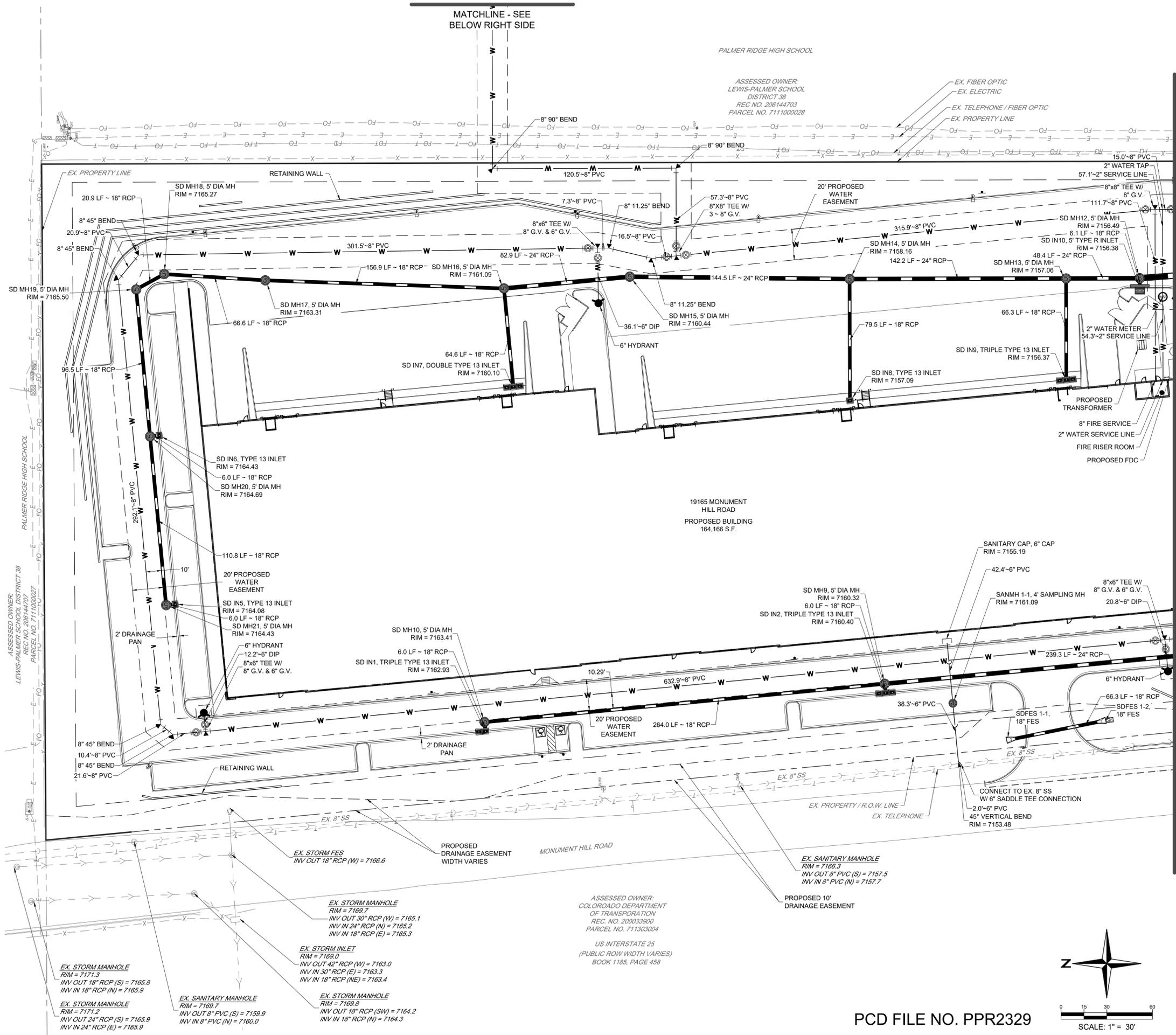
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	08/08/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
 GRADING PLAN

PCD FILE NO. PPR2329

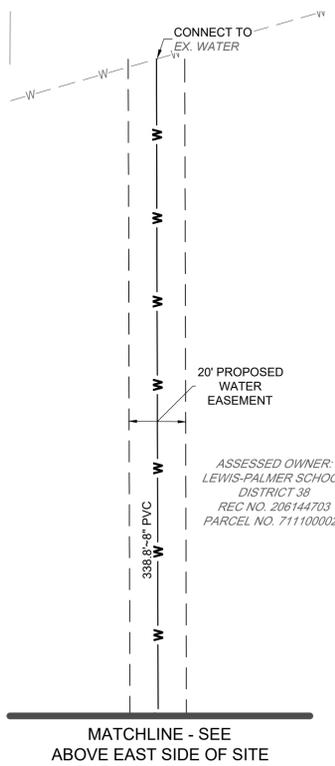
I:\2023\23009 - The Rock Commerce Center\CADD\Sheet Sets\Site Plan\The Rock\23009\_Utility Plan.dwg Tab: 11 OF 24 UTILITY PLAN Nov 20, 2023 - 7:24am caslz



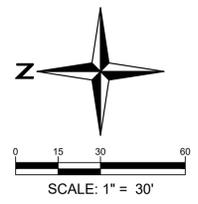
- PROPOSED LEGEND**
- EASEMENT
  - CURB AND GUTTER
  - LIMITS OF CONSTRUCTION / SAWCUT
  - FIRE HYDRANT
  - STORM SEWER
  - SANITARY SEWER
  - TRENCH DRAIN
  - W --- WATER LINE
  - IRR --- IRRIGATION LINE
  - NP --- NONPOTABLE WATER LINE
  - RW --- RAW WATER LINE
  - MANHOLE w/ DIA. (FT.)
  - INLET
  - FLARED END SECTION
  - WATER BEND
  - WATER CROSS
  - WATER TEE
  - WATER REDUCER
  - WATER VALVE
  - PLUG/CAP
  - RETAINING WALL
- EXISTING LEGEND**
- PROPERTY LINE
  - R.O.W.
  - LOT LINE
  - EASEMENT LINE
  - SECTION LINE
  - SETBACK
  - EDGE OF PAVEMENT
  - CURB AND GUTTER
  - FENCE
  - RETAINING WALL
  - WATER LINE
  - RAW WATER LINE
  - NP --- NON-POTABLE WATER LINE
  - IRR --- IRRIGATION LINE
  - SANITARY SEWER
  - STORM SEWER
  - ELECTRIC LINE
  - GAS LINE
  - TELEPHONE LINE
  - FO --- FIBER OPTICS LINE
  - OH --- OVERHEAD ELECTRIC LINE

MATCHLINE - SEE SHEET NO. 8 OF 20

NOTE: THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OR PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.



MATCHLINE - SEE ABOVE EAST SIDE OF SITE



PCD FILE NO. PPR2329

**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND, CO  
 • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

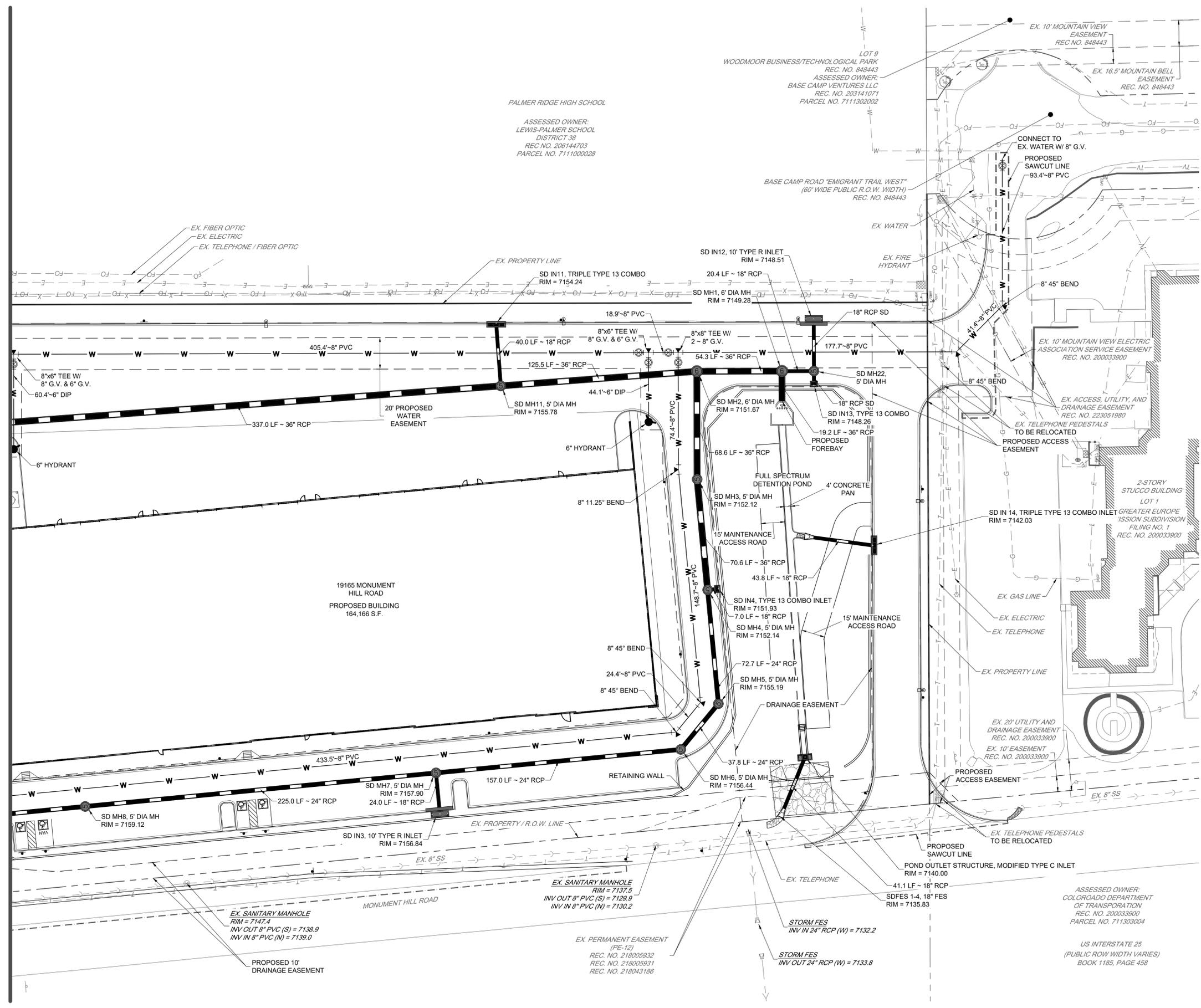
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	09/08/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
 UTILITY PLAN

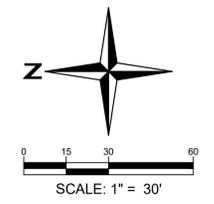
I:\2023\23009 - The Rock Commerce Center\Sheet Sets\Site Plan\The Rock\23009\_Utility Plan.dwg Tab: 12 OF 24 UTILITY PLAN Nov 20, 2023 - 7:24am csoiz

MATCHLINE - SEE SHEET NO. 7 OF 20



PROPOSED LEGEND	
	EASEMENT
	CURB AND GUTTER
	LIMITS OF CONSTRUCTION / SAWCUT
	FIRE HYDRANT
	STORM SEWER
	SANITARY SEWER
	TRENCH DRAIN
	WATER LINE
	IRRIGATION LINE
	NONPOTABLE WATER LINE
	RAW WATER LINE
	MANHOLE w/ DIA. (FT.)
	INLET
	FLARED END SECTION
	WATER BEND
	WATER CROSS
	WATER TEE
	WATER REDUCER
	WATER VALVE
	PLUG/CAP
	RETAINING WALL
EXISTING LEGEND	
	PROPERTY LINE
	R.O.W.
	LOT LINE
	EASEMENT LINE
	SECTION LINE
	SETBACK
	EDGE OF PAVEMENT
	CURB AND GUTTER
	FENCE
	RETAINING WALL
	WATER LINE
	RAW WATER LINE
	NON-POTABLE WATER LINE
	IRRIGATION LINE
	SANITARY SEWER
	STORM SEWER
	ELECTRIC LINE
	GAS LINE
	TELEPHONE LINE
	FIBER OPTICS LINE
	OVERHEAD ELECTRIC LINE

NOTE: THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.



PCD FILE NO. PPR2329

**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND.CO.WE  
 • Land Planning • Landscape Architecture • Construction Management

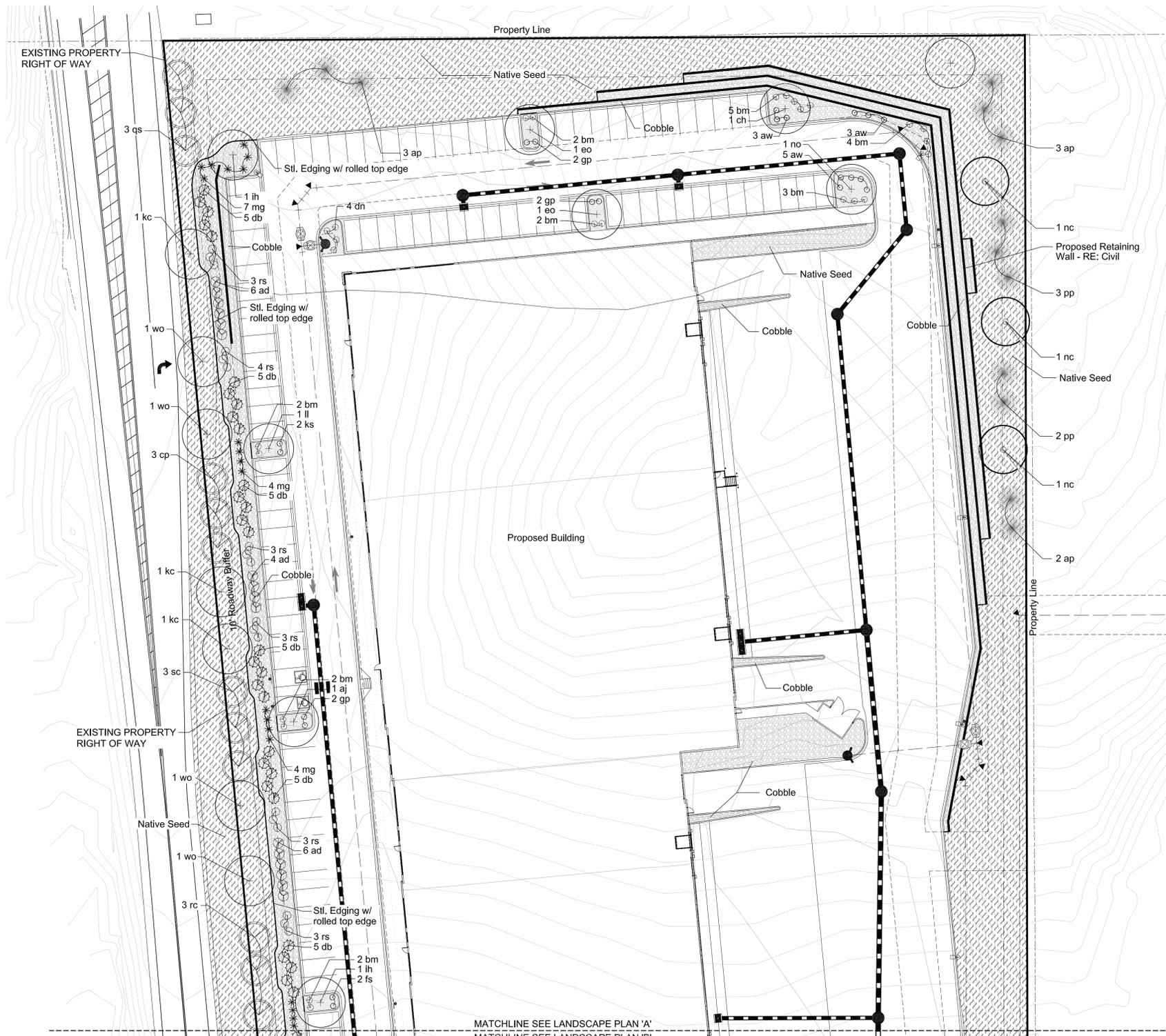
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	08/02/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**SITE DEVELOPMENT PLAN**  
 UTILITY PLAN

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



### LANDSCAPE LEGEND:

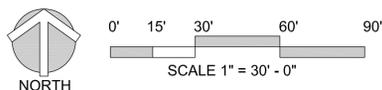
- DECIDUOUS TREE
- ORNAMENTAL TREE
- EVERGREEN TREE
- SHRUB
- ORNAMENTAL GRASS / PERENNIAL

NATIVE SEED MIX NON-IRRIGATED		% OF TOTAL	PLS PER ACRE
BLUE GRAMA	BOUTELOUA GRACILIS	25%	1.8 LBS.
SAND DROPSEED	SPOROBOLUS CRYPTANDRUS	20%	0.20 LBS.
SIDEOATS GRAMA	BOUTELOUA CURTIPENDULA	20%	6.3 LBS.
WESTERN WHEATGRASS	PASCOPYRUM SMITHII	15%	8.2 LBS.
BUFFALO GRASS	BOUTELOUA DACTYLOIDES	10%	10.7 LBS.
INLAND SALTGRASS	DISTICHLIS SPICATA	1%	0.60 LBS.
PASTURE SAGE	ARTEMISIA FRIGIDA	1%	0.01 LBS.
BLANKET FLOWER	GAILLARDIA ARTISTATA	1%	0.5 LBS.
PRAIRIE CONEFLOWER	RATIBIDA COLUMNIFERA	1%	0.1 LBS.
PURPLE PRAIRIECLOVER	DALEA PURPUREA	1%	0.3 LBS.
BLUE FLAX	LINUM LEWISII	1%	0.4 LBS.

DETENTION SEED MIX		% OF TOTAL	PLS PER ACRE
BLUE GRAMA	BOUTELOUA GRACILIS	20%	1.5 LBS.
SAND DROPSEED	SPOROBOLUS CRYPTANDRUS	20%	0.20 LBS.
SWITCHGRASS	PANICUM VIRGATUM	20%	3.2 LBS.
SIDEOATS GRAMA	BOUTELOUA CURTIPENDULA	15%	4.7 LBS.
WESTERN WHEATGRASS	PASCOPYRUM SMITHII	10%	5.5 LBS.
GREEN NEEDLEGRASS	NASELLA VIRIDULA	10%	3.3 LBS.

- 4"-8" ROUND COBBLE OVER FILTER FABRIC
- SHREDDED CEDAR MULCH
- STEEL EDGING w/ ROLLED TOP EDGE
- RETAINING WALL - RE: CIVIL

LANDSCAPE PLAN 'A'



**STACKlot**  
5639 SOUTH CURTICE STREET  
LITTLETON, COLORADO 80120  
phone. 303.808.4523

PCD FILE NO: PPR2329

REVISIONS	DATE	DESCRIPTION
BY	10/23/23	RESUBMITTAL
	11/16/23	RESUBMITTAL

DRAWN: sdw  
CHECKED: jah  
DESIGNED: sdw  
FILENAME:

SITE DEVELOPMENT PLAN  
THE ROCK COMMERCE CENTER  
LANDSCAPE PLAN 'A'

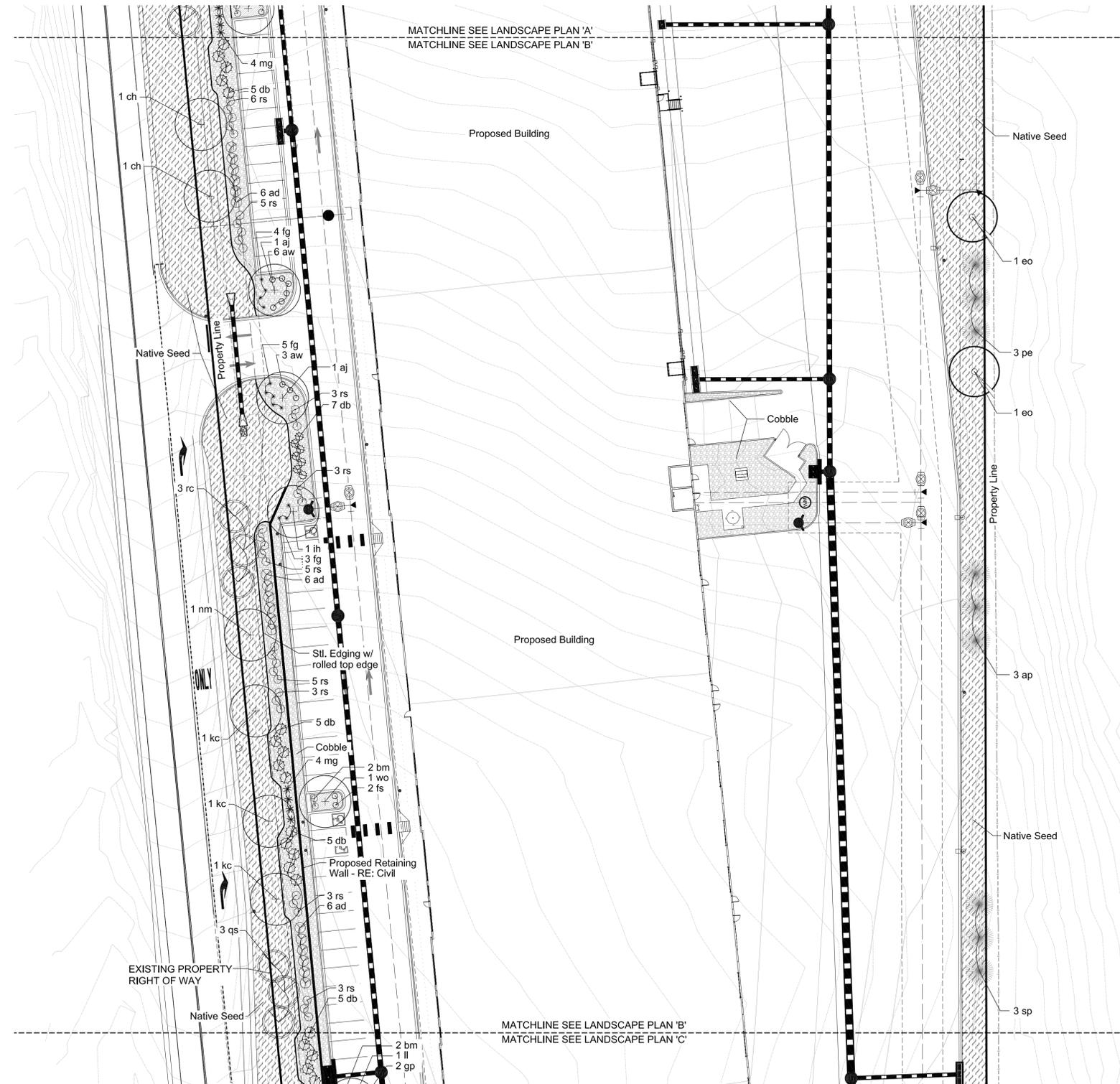


architecture  
planning  
interiors  
2000 West Littleton Blvd  
Littleton, Colorado 80120  
P: 303.758.8877 F: 303.758.2294  
www.igarch.com

JOB NO.  
SCALE: AS SHOWN  
DATE: 07/28/2023  
SHEETS: 20 SHEET: 9

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



### LANDSCAPE LEGEND:

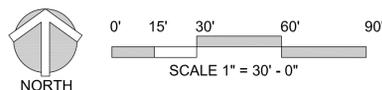
- DECIDUOUS TREE
- ORNAMENTAL TREE
- EVERGREEN TREE
- SHRUB
- ORNAMENTAL GRASS / PERENNIAL

NATIVE SEED MIX NON-IRRIGATED			
COMMON NAME	SCIENTIFIC NAME	% OF TOTAL	PLS PER ACRE
BLUE GRAMA	BOUTELOUA GRACILIS	25%	1.8 LBS.
SAND DROPSEED	SPOROBOLUS CRYPTANDRUS	20%	0.20 LBS.
SIDEOATS GRAMA	BOUTELOUA CURTIPENDULA	20%	6.3 LBS.
WESTERN WHEATGRASS	PASCOPYRUM SMITHII	15%	8.2 LBS.
BUFFALO GRASS	BOUTELOUA DACTYLOIDES	10%	10.7 LBS.
INLAND SALTGRASS	DISTICHLIS SPICATA	1%	0.60 LBS.
PASTURE SAGE	ARTEMISIA FRIGIDA	1%	0.01 LBS.
BLANKET FLOWER	GAILLARDIA ARTISTATA	1%	0.5 LBS.
PRAIRIE CONEFLOWER	RATIBIDA COLUMNIFERA	1%	0.1 LBS.
PURPLE PRAIRIECLOVER	DALEA PURPUREA	1%	0.3 LBS.
BLUE FLAX	LINUM LEWISII	1%	0.4 LBS.

DETENTION SEED MIX			
COMMON NAME	SCIENTIFIC NAME	% OF TOTAL	PLS PER ACRE
BLUE GRAMA	BOUTELOUA GRACILIS	20%	1.5 LBS.
SAND DROPSEED	SPOROBOLUS CYRPTANDRUS	20%	0.20 LBS.
SWITCHGRASS	PANICUM VIRGATUM	20%	3.2 LBS.
SIDEOATS GRAMA	BOUTELOUA CURIPENDULA	15%	4.7 LBS.
WESTERN WHEATGRASS	PASCOPYRUM SMITHII	10%	5.5 LBS.
GREEN NEEDLEGRASS	NASELLA VIRIDULA	10%	3.3 LBS.

- 4"-8" ROUND COBBLE OVER FILTER FABRIC
- SHREDDED CEDAR MULCH
- STEEL EDGING w/ ROLLED TOP EDGE
- RETAINING WALL - RE: CIVIL

LANDSCAPE PLAN 'A'



**STACKlot**  
5639 SOUTH CURTICE STREET  
LITTLETON, COLORADO 80120  
phone. 303.808.4523

PCD FILE NO: PPR2329

REVISIONS	DATE	DESCRIPTION
BY	10/23/23	RESUBMITTAL
	11/16/23	RESUBMITTAL

DRAWN: sdw  
CHECKED: jah  
DESIGNED: sdw  
FILENAME:

SITE DEVELOPMENT PLAN  
THE ROCK COMMERCE CENTER  
LANDSCAPE PLAN 'B'

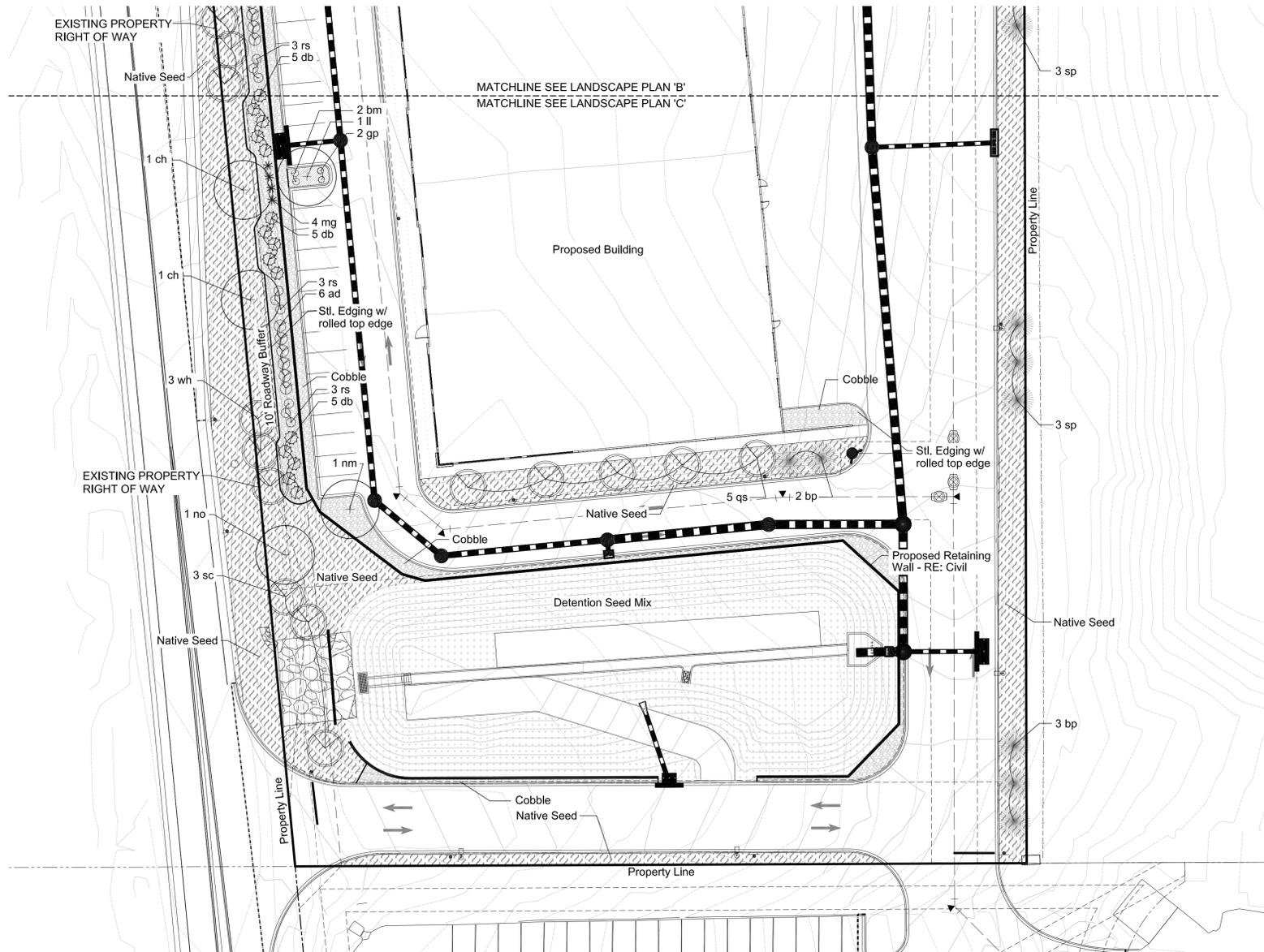


architecture  
planning  
interiors  
2000 West Littleton Blvd  
Littleton, Colorado 80120  
P: 303.758.8877 F: 303.758.2294  
www.igarch.com

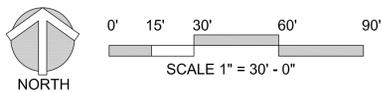
JOB NO.	
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	20
SHEET	10

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



LANDSCAPE PLAN 'A'



### LANDSCAPE LEGEND:

- DECIDUOUS TREE
- ORNAMENTAL TREE
- EVERGREEN TREE
- SHRUB
- ORNAMENTAL GRASS / PERENNIAL

NATIVE SEED MIX NON-IRRIGATED		% OF TOTAL	PLS PER ACRE
BLUE GRAMA	BOUTELOUA GRACILIS	25%	1.8 LBS.
SAND DROPSEED	SPOROBOLUS CRYPTANDRUS	20%	0.20 LBS.
SIDEOATS GRAMA	BOUTELOUA CURTIPENDULA	20%	6.3 LBS.
WESTERN WHEATGRASS	PASCOPYRUM SMITHII	15%	8.2 LBS.
BUFFALO GRASS	BOUTELOUA DACTYLOIDES	10%	10.7 LBS.
INLAND SALTGRASS	DISTICHLIS SPICATA	1%	0.60 LBS.
PASTURE SAGE	ARTEMISIA FRIGIDA	1%	0.01 LBS.
BLANKET FLOWER	GAILLARDIA ARTISTATA	1%	0.5 LBS.
PRAIRIE CONEFLOWER	RATIBIDA COLUMNIFERA	1%	0.1 LBS.
PURPLE PRAIRIECLOVER	DALEA PURPUREA	1%	0.3 LBS.
BLUE FLAX	LINUM LEWISII	1%	0.4 LBS.

DETENTION SEED MIX		% OF TOTAL	PLS PER ACRE
BLUE GRAMA	BOUTELOUA GRACILIS	20%	1.5 LBS.
SAND DROPSEED	SPOROBOLUS CYRPTANDRUS	20%	0.20 LBL.
SWITCHGRASS	PANICUM VIRGATUM	20%	3.2 LBS.
SIDEOATS GRAMA	BOUTELOUA CURIPENDULA	15%	4.7 LBS.
WESTERN WHEATGRASS	PASCOPYRUM SMITHII	10%	5.5 LBS.
GREEN NEEDLEGRASS	NASELLA VIRIDULA	10%	3.3 LBS.

- 4"-8" ROUND COBBLE OVER FILTER FABRIC
- SHREDDED CEDAR MULCH
- STEEL EDGING w/ ROLLED TOP EDGE
- RETAINING WALL - RE: CIVIL

REVISIONS	DATE	DESCRIPTION
BY	10/23/23	RESUBMITTAL
	11/16/23	RESUBMITTAL

DRAWN: sdw  
CHECKED: jah  
DESIGNED: sdw  
FILENAME:

SITE DEVELOPMENT PLAN  
THE ROCK COMMERCE CENTER  
LANDSCAPE PLAN 'C'



architecture  
planning  
interiors  
2000 West Littleton Blvd  
Littleton, Colorado 80120  
P: 303.758.8877 F: 303.758.2294  
www.igarch.com

**STACKlot**  
5639 SOUTH CURTICE STREET  
LITTLETON, COLORADO 80120  
phone. 303.808.4523

PCD FILE NO: PPR2329

JOB NO.	XX-XXXX
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	20
SHEET	11

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO

## GENERAL PLANTING NOTES:

- PRIOR TO BEGINNING ANY WORK ON THE SITE THE LANDSCAPE CONTRACTOR SHALL CONTACT THE OFFICE OF THE GENERAL CONTRACTOR AND LANDSCAPE ARCHITECT FOR SPECIFIC INSTRUCTIONS RELEVANT TO THE SEQUENCING OF WORK.
- LANDSCAPE CONTRACTOR SHALL PROVIDE ALL LABOR, MATERIALS AND SERVICE NECESSARY TO FURNISH AND INSTALL PLANTINGS AND MATERIALS AS SPECIFIED HEREIN AND AS SHOWN ON PLANS.
- NO MATERIAL SUBSTITUTIONS SHALL BE MADE WITHOUT THE LANDSCAPE ARCHITECTS APPROVAL IN WRITING. ALTERNATE MATERIALS OF SIMILAR SIZE AND CHARACTER MAY BE CONSIDERED IF SPECIFIED PLANT MATERIALS CANNOT BE OBTAINED.
- LANDSCAPE ARCHITECT RESERVES THE RIGHT TO REVISE PLANT MATERIAL LIST AS DEEMED NECESSARY.
- ALL PLANT LOCATIONS ARE APPROXIMATE. ADJUST AS NECESSARY TO AVOID CONFLICTS.
- QUANTITIES OF MATERIALS SHOWN ON THE PLANTING PLAN TAKE PRECEDENCE OVER QUANTITIES SHOWN ON THE PLANT MATERIAL SCHEDULE. THE LANDSCAPE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFY ALL QUANTITIES ON THE PLANTING PLAN(S).
- LANDSCAPE CONTRACTOR SHALL LOCATE ALL UTILITIES BEFORE COMMENCEMENT OF WORK. VERIFY EXACT LOCATION OF ALL UTILITIES BY CONTACTING APPROPRIATE UTILITY COMPANIES. LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR THE REPAIR / REPLACEMENT FOR ANY DAMAGE CAUSED TO UTILITIES.
- FINISH GRADE SHALL BE ADJUSTED FOR TURF THICKNESS.
- ALL PLANT MATERIALS SHALL HAVE BACKFILL, CAREFULLY PLACED AROUND BASE AND IDES OF BALL TO TWO-THIRDS (2/3) DEPTH OF BALL THEN THOROUGHLY SOAKED WITH WATER TO ALLOW SETTLEMENT. ALL WIRE, BURLAP FASTENERS, TOP ONE-THIRD (1/3) OF BURLAP AND LOOSE BURLAP SHALL BE REMOVED AT THIS TIME THE REMAINDER OF HE PIT SHALL THEN BE BACKFILLED, ALLOWING FOR THE DEPTH OF THE MULCH SAUCER AND SETTLEMENT OF BACKFILL. BACKFILL SHALL THEN BE THOROUGHLY WATERED ONCE AGAIN.
- AFTER PLANTING IS COMPLETED REPAIR INJURIES TO ALL PLANTS AS REQUIRED. LIMIT AMOUNT OF PRUNING TO A MINIMUM NECESSARY TO REMOVE DEAD OR INJURED TWIGS AND BRANCHES. PRUNE IN SUCH A MANNER AS NOT TO CHANGE THE NATURAL GROWING HABIT OR SHAPE OF THE PLANT. MAKE ALL CUTS FLUSH, LEAVING NO STUBS. CENTRAL LEADERS SHALL NOT BE REMOVED. IF THE CENTRAL LEADER OF A PLANT IS DEAD THE PLANT SHALL BE REPLACED.
- PLANT SPECIFIED GROUND COVERS WITHIN ONE FOOT OF TRUCK OF TREES AND SHRUBS PLANTED WITHIN THE AREA. PLANTING ARRANGEMENTS SHALL BE TRIANGULAR WITH PROPER SPACING BETWEEN PLANTS.
- COMMERCIAL GRADE 3/8 INCH BY 4" POWDER COATED STEEL EDGING SHALL BE USED TO SEPARATE ALL TURF AREAS FROM PLANTING BEDS. PLACE EDGING FLUSH WITH GRADE AND STAKE TO GROUND PER MANUFACTURES RECOMMENDATIONS.
- LANDSCAPE CONTRACTOR TO PROVIDE THE LANDSCAPE CONTRACTOR A SAMPLE OF PROPOSED STEEL EDGING FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.
- USE SHREDDED CEDAR MULCH IN ALL PLANTING BEDS AND TREE SAUCERS. LANDSCAPE CONTRACTOR SHALL PROVIDE A 1 CUBIC FOOT SAMPLE OF PROPOSED MULCH TO LANDSCAPE ARCHITECT FOR REVIEW AND APPROVAL.
- PLACE FOUR INCHES OF MULCH IN ALL SHRUB BEDS, PLACE FOUR INCHES OF MULCH IN ALL GROUND COVER, PERENNIAL BEDS AND PLACE 4 INCHES OF MULCH AT ALL TREE SAUCERS.
- PLANTING BEDS RECEIVING MULCH MULCH ARE TO BE FREE OF WEEDS AND GRASS. TREAT BEDS WITH A PRE-EMMERGENT HERBICIDE PRIOR TO PLANTING AND MULCH PLACEMENT. DO NOT APPLY HERBICIDE IN PERENNIAL OR ANNUAL BEDS.
- LANDSCAPE CONTRACTOR TO REMOVE TREE STAKES AND ALL DEAD WOOD ON TREES AND SHRUBS ONE YEAR AFTER SUBSTANTIAL COMPLETION IS GRANTED ON THE COMPLETE PROJECT.
- REPORT ANY DISCREPANCIES IN THE PLANTING PLAN TO THE LANDSCAPE ARCHITECT PRIOR TO STARTING CONSTRUCTION.
- ALL LANDSCAPE AREAS SHALL BE IRRIGATED BY AN UNDERGROUND AUTOMATIC UNDERGROUD IRRIGATION SYSTEM. WITH SEPARATE ZONES FOR TURF AND SHRUBS / TREES / GROUNDCOVER.
- IF TRANSFORMERS, GROUND MOUNTED HVAC EQUIPMENT, UTILITY PEDESTALS, ETC. ARE NOT SHOWN ON THE SITE IMPROVEMENT PLAN, ADDITIONAL LANDSCAPE/SCREENING MAY BE REQUIRED BASED UPON FIELD CONDITIONS DISCOVERED VIA THE SITE INSPECTION BY STAFF, MADE PRIOR TO THE ISSUANCE OF CERTIFICATE OF OCCUPANCY, OR FINAL INSPECTION AS APPLICABLE.

## SOIL ANALYSIS CONTRACTOR REQUIREMENT

"THE REQUIRED SOIL ANALYSIS REPORT IS REQUIRED TO BE SUBMITTED AND APPROVED WITH THE IRRIGATION PLAN SUBMITTAL AND BEFORE ANY LANDSCAPE CONSTRUCTION. THIS WOULD INCLUDE COMPLETING THE SOIL SAMPLING AND SUBMITTING THE SAMPLES TO A SOILS LAB FOR TESTING. A SEPARATE LAB TEST REPORT AND SOIL PREPARATION RECOMMENDATIONS (AMENDMENT/FERTILIZER AMOUNTS AND APPLICATION RATES) FOR EACH TYPE OF PROPOSED LANDSCAPING (SHRUB BEDS/SOD/NATIVE SEED) WILL NEED TO BE PROVIDED TO CITY STAFF FOR REVIEW AND APPROVAL."

## SOIL AMENDMENTS

PRIOR TO PLANTING, ALL SITES FOR PLANTINGS SHALL INCORPORATE SOIL AMENDMENTS AT A RATE OF 3 CUBIC YARDS PER 1000 SQUARE FEET TO A MINIMUM DEPTH OF 6". A LESSER AMOUNT SHALL BE ALLOWED IF A SOIL TEST SHOWS THAT 3 CUBIC YARDS PER 1000 SQUARE FEET IS NOT NECESSARY FOR WATER RETENTION AND DEEP ROOTING OF PLANT MATERIALS. IF THE SPECIFIED PLANT MATERIAL REQUIRES LESS FERTILE SOIL, THOSE AREAS MAY HAVE LESS SOIL AMENDMENTS INSTALLED IF APPROVED BY THE COMMUNITY DEVELOPMENT DIRECTOR. THESE AREAS SHALL BE IDENTIFIED ON THE LANDSCAPE PLAN. EXISTING TOPSOIL SHALL BE SALVAGED AND STOCKPILED FOR USE AS SOIL AMENDMENTS OR TOPSOIL. NO TOPSOIL SHALL BE REMOVED FROM THE SITE UNLESS THE CITY APPROVES THE TRANSFER OF TOPSOIL TO A CITY-OWNED PARK OR OPEN SPACE AREA. A NOTE SHALL BE PLACED ON THE LANDSCAPE PLAN REFLECTING THE ABOVE REQUIREMENTS REGARDING SOIL AMENDMENTS AND TOPSOIL. EXAMPLES OF ACCEPTABLE SOIL AMENDMENTS INCLUDE COMPOST AND AGED MANURE. MOUNTAIN PEAT AND INORGANIC MATERIALS SUCH AS SAND, GYPSUM AND LIME ARE PROHIBITED SOIL AMENDMENTS. ALL SITES ARE SUBJECT TO INSPECTION BY THE CITY FOR COMPLIANCE WITH SOIL AMENDMENT REQUIREMENTS.

## PLANT MATERIAL SCHEDULE:

SYMBOL	QTY.	I.D.	COMMON NAME	BOTANICAL NAME	SIZE	COND.
<b>SHADE TREES</b>						
	2	nm	NORWAY MAPLE	ACER PLATANOIDES	1 1/2" CAL.	B & B
	3	aj	AUTUMN BLAZE MAPLE	ACER X FREEMANII 'JEFFERSRED'	1 1/2" CAL.	B & B
	5	ch	COMMON HACKBERRY	CELTIS OCCIDENTALIS	1 1/2" CAL.	B & B
	3	ih	IMPERIAL HONEY LOCUST	GLEDITSIA TRIACANTHOS INERMIS 'IMPERIAL'	1 1/2" CAL.	B & B
	6	kc	KENTUCKY COFFEE TREE	GYMNOCLADUS DIOICUS	1 1/2" CAL.	B & B
	3	nc	NARROWLEAF COTTONWOOD	NARROWLEAF COTTONWOOD	1 1/2" CAL.	B & B
	5	wo	SWAMP WHITE OAK	QUERCUS BICOLOR	1 1/2" CAL.	B & B
	2	no	NORTHERN RED OAK	QUERCUS RUBRA	1 1/2" CAL.	B & B
	2	ll	LITTLELEAF LINDEN	TILIA CORDATA	1 1/2" CAL.	B & B
	4	eo	ENGLISH OAK	QUERCUS ROBUR	1 1/2" CAL.	B & B
<b>ORNAMENTAL TREES</b>						
	3	wh	WASHINGTON HAWTHORN	CRATAEGUS PHAENOPYRUM	1" CAL.	B & B
	6	rc	RADIANT CRABAPPLE	MALAU 'RADIANT'	1" CAL.	B & B
	6	sc	SPRING SNOW CRABAPPLE	MALUS 'SPRING SNOW'	1" CAL.	B & B
	3	cp	CHANTICLEER PEAR	PYRUS CALLERYANA	1" CAL.	B & B
	11	qs	CRIMSON SPIRE OAK	QUERCUS X BIMUNDORUM 'CRIMSCHMIDT'	1" CAL.	B & B
	<b>EVERGREEN TREES</b>					
	3	pe	PINON PINE	PINUS EDULIS	6' HT.	B & B
	11	ap	AUSTRIAN PINE	PINUS NIGRA	6' HT.	B & B
	5	pp	PONDEROSA PINE	PINUS PONDEROSA	6' HT.	B & B
	6	sp	SOUTHWESTERN WHITE PINE	PINUS STROBIFORMIS	6' HT.	B & B
	5	bp	BOSNIA PINE	PINUS HELDREICHII	6' HT.	B & B
	<b>SHRUBS</b>					
	2	ks	DARK KNIGHT SPIREA	CARYOPTERIS X CLANDONENSIS 'DARK KNIGHT'	5 GAL.	CONT.
	20	aw	ANOTHONY WATERER SPIREA	SPIREA JAPONICA 'ANTHONY WATER'	5 GAL.	CONT.
	4	fs	GOLD FLAME SPIREA	SPIREA JAPONICA 'GOLDFLAME'	5 GAL.	CONT.
	8	gp	GOLD DROP POTENTILLA	POTENTILLA FRUITICOSA 'GOLD DROP'	5 GAL.	CONT.
	26	bm	BLUE MIST SPIREA	CARYOPTERIS X CLANDONENSIS	5 GAL.	CONT.
	67	db	DWARF BURNING BUSH	EOUNYMUS ALATA 'DWARF NANA'	5 GAL.	CONT.
	61	rs	RUSSIAN SAGE	PEROVSKIA ATRIPLICIFOLIA	5 GAL.	CONT.
	40	ad	ARCTIC FIRE DOGWOOD	CORNUS STOLONIFERA 'FARROW'	5 GAL.	CONT.
	4	dn	DWARF NINEBARK	PHYSOCARPUS 'OPULIFOLIUS 'NANUS'	5 GAL.	CONT.
	<b>ORNAMENTAL GRASSES</b>					
	27	mg	MAIDEN GRASS	MISCANTHUS SINENSIS 'GRACILLIMUS'	1 GAL.	CONT.
	12	fg	MEXICAN FEATHER GRASS	NESSELLA TENUISSIMA	1 GAL.	CONT.

### Roadway Buffer

MONUMENT HILL ROAD NON-ARTERIAL	REQUIRED ROADWAY BUFFER	PROVIDED ROADWAY BUFFER	REQUIRED TREES 1 TREE / 30 LN.FT.	PROVIDED TREES
1,175 LN.FT.	10 FEET	10 FEET	40	40

### Internal Landscaping

SITE AREA	INTERNAL LANDSCAPE AREA REQUIRED - (5%)	INTERNAL LANDSCAPE AREA PROVIDED	REQUIRED TREES 1 TREE / 500 SF	PROVIDED TREES
505,679 SF.	25,284 SF.	115,434 SF.	51	54



5639 SOUTH CURTICE STREET  
LITTLETON, COLORADO 80120  
phone. 303.808.4523

PCD FILE NO: PPR2329

REVISIONS	DATE	DESCRIPTION
	10/23/23	RESUBMITTAL
	11/16/23	RESUBMITTAL

DRAWN  
sdw

CHECKED  
jah

DESIGNED  
sdw

FILENAME

SITE DEVELOPMENT PLAN  
THE ROCK COMMERCE CENTER

LANDSCAPE NOTES



INTERGROUP  
ARCHITECTS

architecture  
planning  
interiors  
2000 West Littleton Blvd  
Littleton, Colorado 80120  
P. 303.758.8877 F. 303.758.2294  
www.igarch.com

JOB NO. XX-XXXX

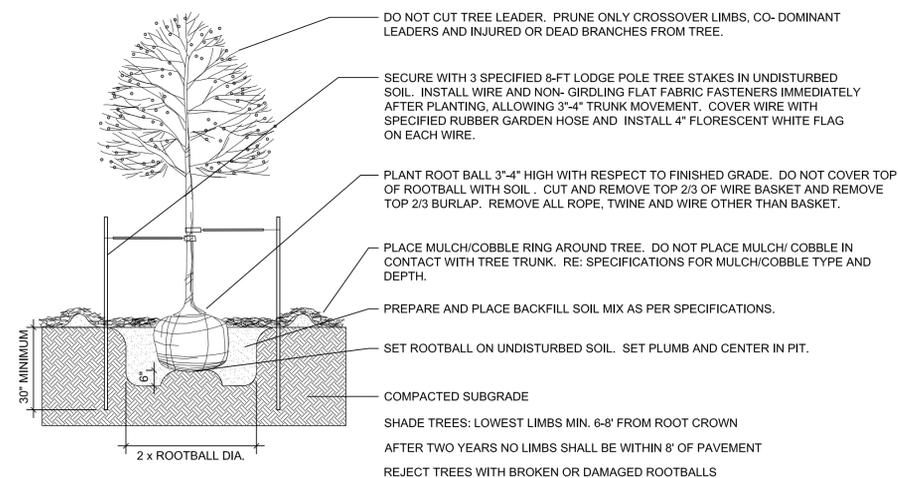
SCALE AS SHOWN

DATE 07/28/2023

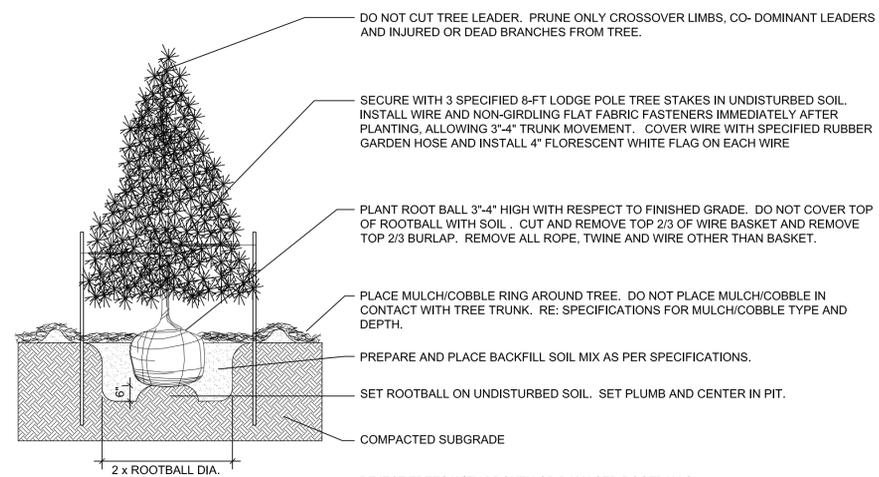
SHEETS SHEET  
20 12

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

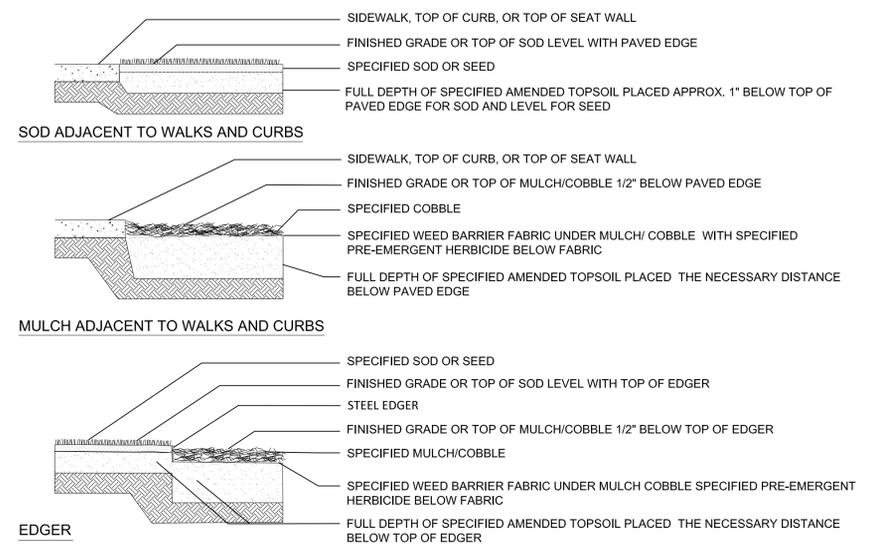
A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



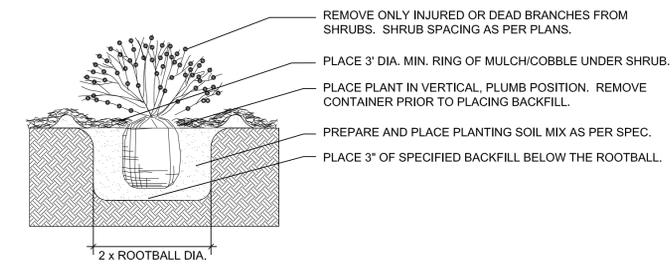
**1 DECIDUOUS TREE**  
NOT TO SCALE



**2 EVERGREEN TREE PLANTING**  
NOT TO SCALE



**3 EDGE TREATMENT**  
NOT TO SCALE



**4 SHRUB PLANTING**  
NOT TO SCALE

REVISIONS	DATE	DESCRIPTION
	10/23/23	RESUBMITTAL
	11/16/23	RESUBMITTAL

DRAWN: sdw  
CHECKED: jah  
DESIGNED: sdw  
FILENAME:

SITE DEVELOPMENT PLAN  
THE ROCK COMMERCE CENTER  
LANDSCAPE DETAILS



architecture  
planning  
interiors  
2000 West Littleton Blvd  
Littleton, Colorado 80120  
P: 303.758.8877 F: 303.758.2294  
www.igarch.com

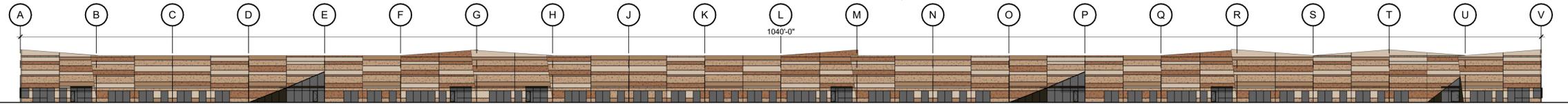
**STACKlot**  
5639 SOUTH CURTICE STREET  
LITTLETON, COLORADO 80120  
phone. 303.808.4523

PCD FILE NO: PPR2329

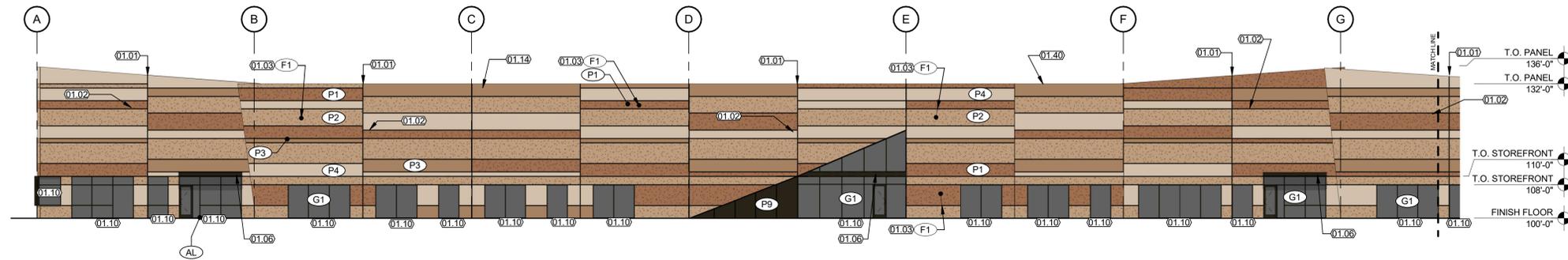
JOB NO.	XX-XXXX
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	20
SHEET	13

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

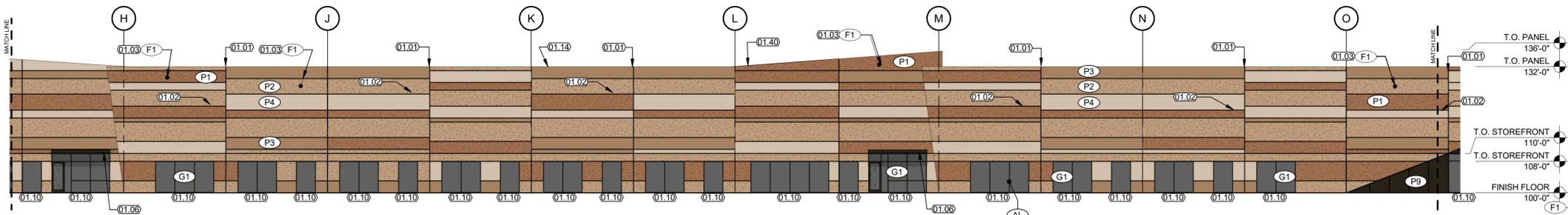
A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



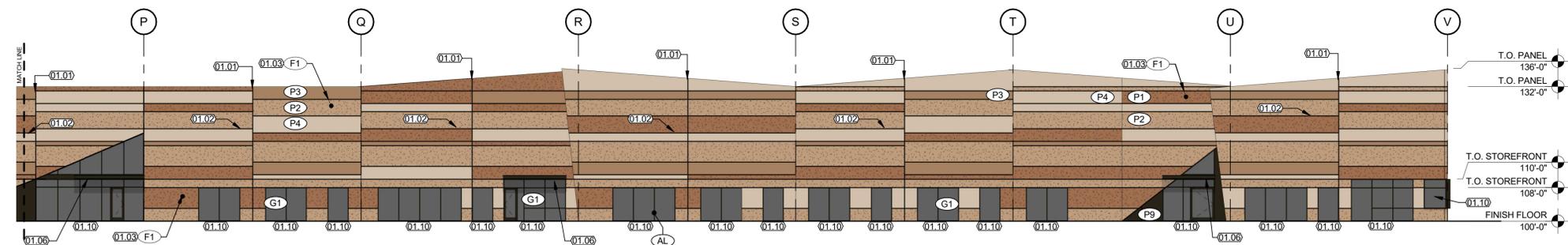
**1** OVERALL WEST ELEVATION  
SCALE: 1" = 40'-0"



**2** ENLARGED WEST ELEVATION - NORTH  
SCALE: 1/16" = 1'-0"



**3** ENLARGED WEST ELEVATION - MID  
SCALE: 1/16" = 1'-0"



**4** ENLARGED WEST ELEVATION - SOUTH  
SCALE: 1/16" = 1'-0"

### KEYNOTES:

- 01.01 CONCRETE PANEL JOINT WITH 3/4" CHAMFERED EDGES, BACKER ROD & SEALANT FULL LENGTH.
- 01.02 3/4" x 2 1/4" REVEAL, PAINTED.
- 01.03 US FORMLINER 2/156 STEINWALD.
- 01.06 STEEL CHANNEL ENTRY CANOPY TO ATTACH TO CONC. TILT-UP WALL WITH T.S. SUPPORTS, PAINTED.
- 01.10 INSULATED TINTED GLAZING IN ANODIZED ALUMINUM STOREFRONT SYSTEM, SEE FINISH LEGEND.
- 01.14 SITE CAST TILT-UP CONCRETE PANEL, PAINTED WITH MEDIUM TEXTURED PAINT. SEE EXTERIOR FINISH LEGEND FOR SPECIFIC COLORS.
- 01.40 PREFINISHED METAL CAP FLASHING, TYP @ ALL CONCRETE PANELS.

### EXTERIOR FINISH LEGEND

KEY	DESCRIPTION	IMAGE	MANUFACTURER	REMARKS / COMMENTS
P1	EXTERIOR PAINT		GLIDDEN #50YR 18/223 "SOFT COPPER"	MEDIUM TEXTURE @ CONC. PANEL
F1	CONCRETE TILT UP ACCENT		US FORMLINER	2/156 STEINWALD ROCK PATTERN
P2	EXTERIOR PAINT		GLIDDEN #10YY 41/175 "HIGHLAND PLAINS"	MEDIUM TEXTURE @ CONC. PANEL
P3	EXTERIOR PAINT		GLIDDEN #20YY 33/145 "DEACON'S BENCH"	MEDIUM TEXTURE @ CONC. PANEL
P4	EXTERIOR PAINT		GLIDDEN #20YY 51/098 "LEGEND TAN"	MEDIUM TEXTURE @ CONC. PANEL
P5	EXTERIOR PAINT		GLIDDEN #30YY 46/036 "ZEPELIN"	MEDIUM TEXTURE @ CONC. PANEL
F2	CONCRETE TILT UP ACCENT		US FORMLINER	2/75 KOCHER - HORIZONTAL
P6	EXTERIOR PAINT		GLIDDEN #30YY 33/047 "OLD MONTEREY"	MEDIUM TEXTURE @ CONC. PANEL
P7	EXTERIOR PAINT		GLIDDEN #30YY 20/029 "MANSARD STONE"	MEDIUM TEXTURE @ CONC. PANEL
P8	EXTERIOR PAINT		GLIDDEN #30YY 10/038 "FOREST BLACK"	MEDIUM TEXTURE @ CONC. PANEL
P9	EXTERIOR PAINT		GLIDDEN #30YY 05/044 "THE DARK SIDE"	MEDIUM TEXTURE @ CONC. PANEL
G1	GLAZING		VITRO GLASS - SOLARGRAY	
AL	STOREFRONT FRAME		DARK BRONZE	

REVISIONS	DATE	DESCRIPTION
BY	10/20/2023	RESUBMITTAL
	11/16/2023	RESUBMITTAL

DRAWN	CBW
CHECKED	BS
DESIGNED	KS
FILENAME	BS11530

**SITE DEVELOPMENT PLAN  
THE ROCK COMMERCE CENTER  
EXTERIOR ELEVATIONS**



architecture  
planning  
interiors

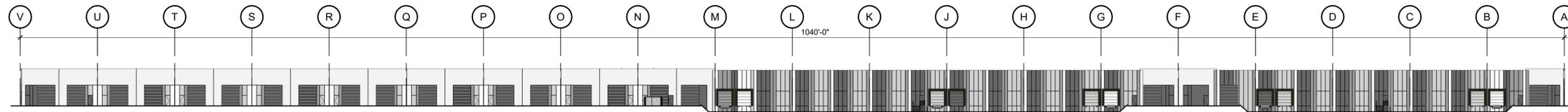
2000 West Littleton Blvd  
Littleton, Colorado 80120  
P. 303.756.8877 F. 303.756.2294  
www.igarch.com

JOB NO.	BS11530
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	20
SHEET	14

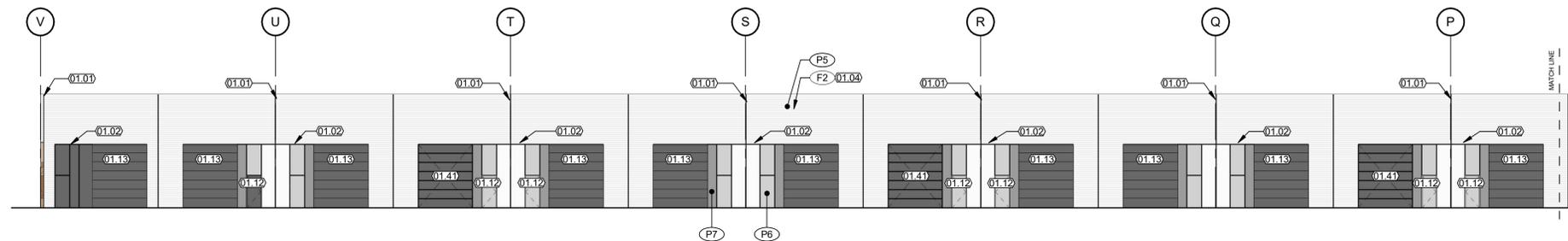
PCD FILE NO: PPR2329

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

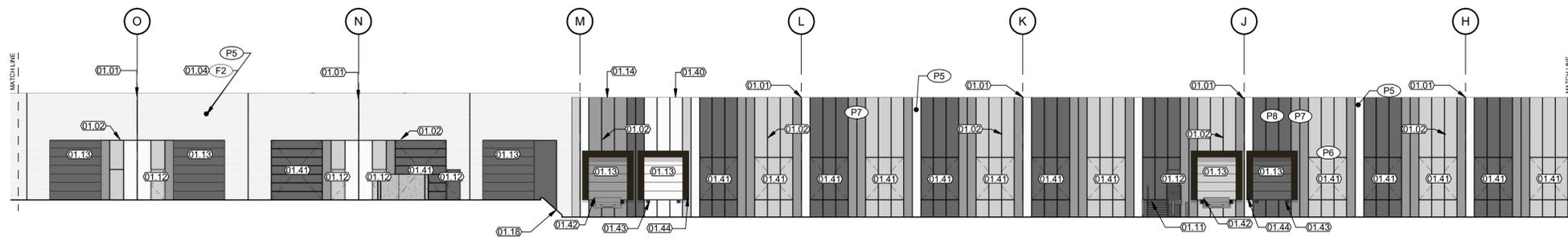
A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



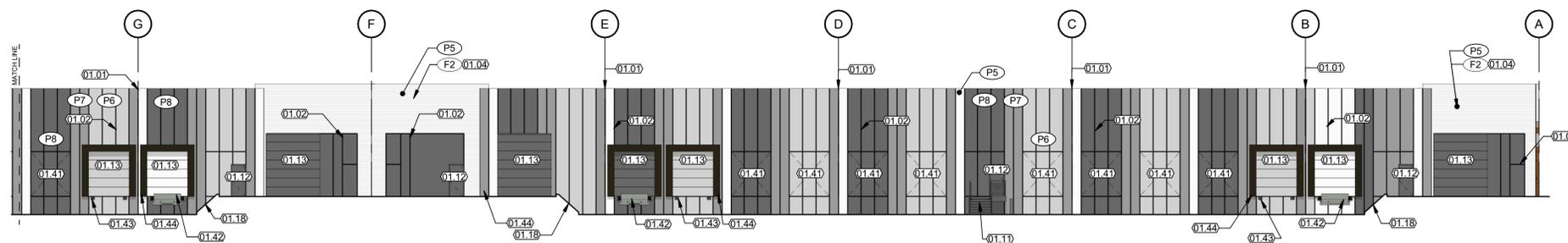
**1 OVERALL EAST ELEVATION**  
SCALE: 1" = 40'-0"



**2 ENLARGED EAST ELEVATION - SOUTH**  
SCALE: 1/16" = 1'-0"



**3 ENLARGED EAST ELEVATION - MID**  
SCALE: 1/16" = 1'-0"



**4 ENLARGED EAST ELEVATION - NORTH**  
SCALE: 1/16" = 1'-0"

### KEYNOTES:

- 01.01 CONCRETE PANEL JOINT WITH 3/4" CHAMFERED EDGES, BACKER ROD & SEALANT FULL LENGTH.
- 01.02 3/4" x 2 1/4" REVEAL, PAINTED.
- 01.04 US FORMLINER 2/75 KOCHER - ORIENTATION HORIZONTAL.
- 01.11 EXTERIOR STEEL STAIRS, LANDING, GUARDRAIL & HANDRAILS. TREAD & LANDING TO BE 1" DEEP OPEN GRATING WITH LONG DIM. PERP. TO PATH OF TRAVEL. GUARDRAIL TO BE 1 1/2"Ø x 42H. WITH 1 1/2"Ø x 34H. HARDRAIL, PAINTED.
- 01.12 INSULATED H.M. MAN DOOR, PAINT TO MATCH ADJACENT WALL SURFACE COLOR, U.N.O.
- 01.13 INSULATED STEEL O.H. DOOR, PAINTED - SEE FINISH LEGEND.
- 01.14 SITE CAST TILT-UP CONCRETE PANEL, PAINTED WITH MEDIUM TEXTURED PAINT. SEE EXTERIOR FINISH LEGEND FOR SPECIFIC COLORS.
- 01.18 SLOPING CONCRETE RETAINING WALL.
- 01.40 PREFINISHED METAL CAP FLASHING, TYP @ ALL CONCRETE PANELS.
- 01.41 AREA TO BE KNOCK-OUT FOR FUTURE DOCK DOOR, PROVIDE 1 1/2" DEEP RECESS. TYPICAL 3/4" x 2 1/4" REVEALS WITHIN RECESS TO PROVIDE THE O.H. DOOR APPEARANCE.
- 01.42 6' x 8' DOCK LEVELER
- 01.43 DOCK BUMPER, TYP. @ DOCK LEVELER
- 01.44 DOCK SEAL, TYP @ DOCK HEIGHT O.H. DOORS

### EXTERIOR FINISH LEGEND

KEY	DESCRIPTION	IMAGE	MANUFACTURER	REMARKS / COMMENTS
P1	EXTERIOR PAINT		GLIDDEN #50YR 18/223 "SOFT COPPER"	MEDIUM TEXTURE @ CONC. PANEL
F1	CONCRETE TILT UP ACCENT		US FORMLINER	2/156 STEINWALD ROCK PATTERN
P2	EXTERIOR PAINT		GLIDDEN #10YY 41/175 "HIGHLAND PLAINS"	MEDIUM TEXTURE @ CONC. PANEL
P3	EXTERIOR PAINT		GLIDDEN #20YY 33/145 "DEACON'S BENCH"	MEDIUM TEXTURE @ CONC. PANEL
P4	EXTERIOR PAINT		GLIDDEN #20YY 51/098 "LEGEND TAN"	MEDIUM TEXTURE @ CONC. PANEL
P5	EXTERIOR PAINT		GLIDDEN #30YY 46/036 "ZEPPELIN"	MEDIUM TEXTURE @ CONC. PANEL
F2	CONCRETE TILT UP ACCENT		US FORMLINER	2/75 KOCHER - HORIZONTAL
P6	EXTERIOR PAINT		GLIDDEN #30YY 33/047 "OLD MONTEREY"	MEDIUM TEXTURE @ CONC. PANEL
P7	EXTERIOR PAINT		GLIDDEN #30YY 20/029 "MANSARD STONE"	MEDIUM TEXTURE @ CONC. PANEL
P8	EXTERIOR PAINT		GLIDDEN #30YY 10/038 "FOREST BLACK"	MEDIUM TEXTURE @ CONC. PANEL
P9	EXTERIOR PAINT		GLIDDEN #30YY 05/044 "THE DARK SIDE"	MEDIUM TEXTURE @ CONC. PANEL
G1	GLAZING		VITRO GLASS - SOLARGRAY	
AL	STOREFRONT FRAME		DARK BRONZE	

PCD FILE NO: PPR2329

REVISIONS	DESCRIPTION
DATE	RESUBMITTAL
10/20/2023	RESUBMITTAL
11/16/2023	RESUBMITTAL
BY	

DRAWN	CBW
CHECKED	BS
DESIGNED	KS
FILENAME	BS11530

**SITE DEVELOPMENT PLAN**  
**THE ROCK COMMERCE CENTER**  
**EXTERIOR ELEVATIONS**



**architecture**  
**planning**  
**interiors**  
 2000 West Littleton Blvd  
 Littleton, Colorado 80120  
 P. 303.758.8877 F. 303.758.2294  
 www.igarch.com

JOB NO.	BS11530
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	SHEET
20	15

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO

REVISIONS	DATE	DESCRIPTION
	10/20/2023	RESUBMITTAL
	11/16/2023	RESUBMITTAL

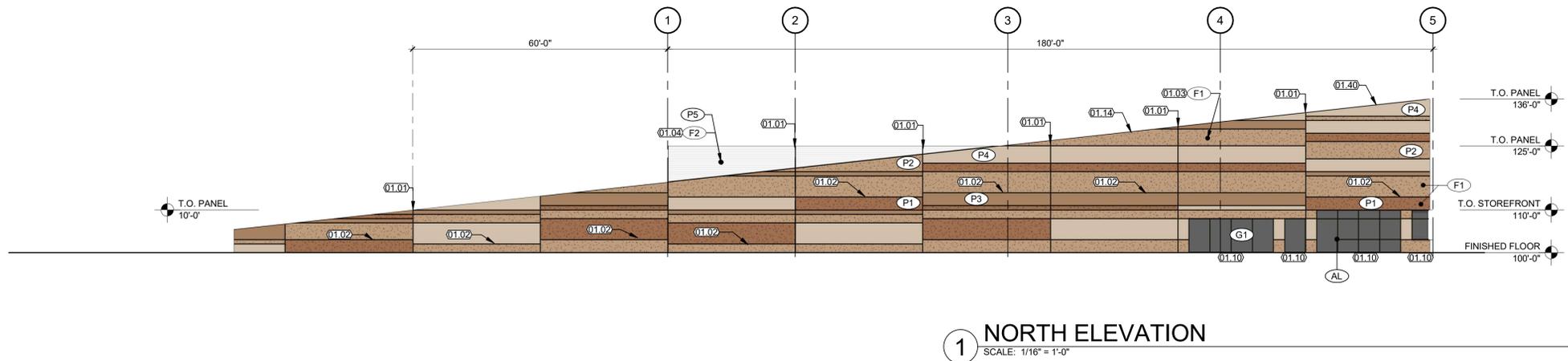
DRAWN	CBW
CHECKED	BS
DESIGNED	KS
FILENAME	BS11530

**SITE DEVELOPMENT PLAN**  
**THE ROCK COMMERCE CENTER**  
**EXTERIOR ELEVATIONS**



**architecture**  
**planning**  
**interiors**  
 2000 West Littleton Blvd  
 Littleton, Colorado 80120  
 P. 303.758.8877 F. 303.758.2294  
 www.igarch.com

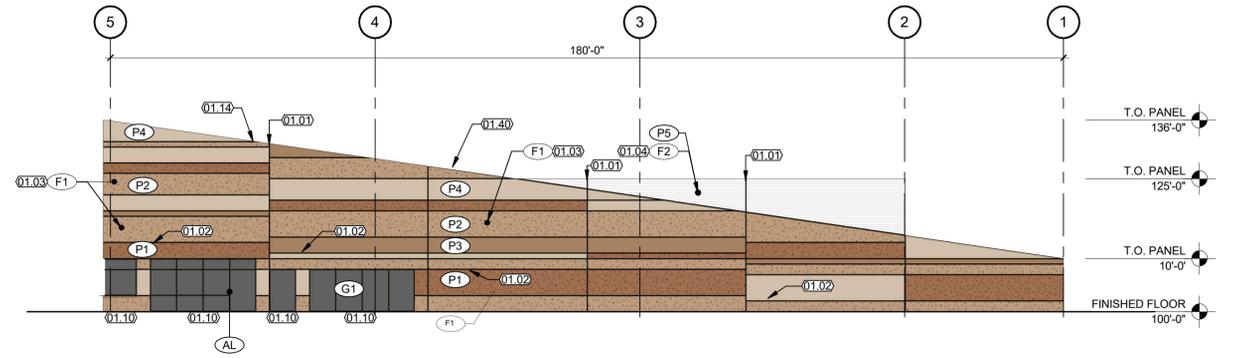
JOB NO. BS11530  
 SCALE AS SHOWN  
 DATE 07/28/2023  
 SHEETS 20 SHEET 16



**1 NORTH ELEVATION**  
SCALE: 1/16" = 1'-0"

**KEYNOTES:**

- 01.01 CONCRETE PANEL JOINT WITH 3/4" CHAMFERED EDGES, BACKER ROD & SEALANT FULL LENGTH.
- 01.02 3/4" x 2 1/4" REVEAL, PAINTED.
- 01.03 US FORMLINER 2/156 STEINWALD.
- 01.04 US FORMLINER 2/75 KOCHER - ORIENTATION HORIZONTAL.
- 01.10 INSULATED TINTED GLAZING IN ANODIZED ALUMINUM STOREFRONT SYSTEM. SEE FINISH LEGEND.
- 01.14 SITE CAST TILT-UP CONCRETE PANEL, PAINTED WITH MEDIUM TEXTURED PAINT. SEE EXTERIOR FINISH LEGEND FOR SPECIFIC COLORS.
- 01.40 PREFINISHED METAL CAP FLASHING, TYP @ ALL CONCRETE PANELS.



**2 SOUTH ELEVATION**  
SCALE: 1/16" = 1'-0"

**EXTERIOR FINISH LEGEND**

KEY	DESCRIPTION	IMAGE	MANUFACTURER	REMARKS / COMMENTS
(P1)	EXTERIOR PAINT		GLIDDEN #50YR 18/223 "SOFT COPPER"	MEDIUM TEXTURE @ CONC. PANEL
(F1)	CONCRETE TILT UP ACCENT		US FORMLINER	2/156 STEINWALD ROCK PATTERN
(P2)	EXTERIOR PAINT		GLIDDEN #10YY 41/175 "HIGHLAND PLAINS"	MEDIUM TEXTURE @ CONC. PANEL
(P3)	EXTERIOR PAINT		GLIDDEN #20YY 33/145 "DEACON'S BENCH"	MEDIUM TEXTURE @ CONC. PANEL
(P4)	EXTERIOR PAINT		GLIDDEN #20YY 51/098 "LEGEND TAN"	MEDIUM TEXTURE @ CONC. PANEL
(P5)	EXTERIOR PAINT		GLIDDEN #30YY 46/036 "ZEPPELIN"	MEDIUM TEXTURE @ CONC. PANEL
(F2)	CONCRETE TILT UP ACCENT		US FORMLINER	2/75 KOCHER - HORIZONTAL
(P6)	EXTERIOR PAINT		GLIDDEN #30YY 33/047 "OLD MONTEREY"	MEDIUM TEXTURE @ CONC. PANEL
(P7)	EXTERIOR PAINT		GLIDDEN #30YY 20/029 "MANSARD STONE"	MEDIUM TEXTURE @ CONC. PANEL
(P8)	EXTERIOR PAINT		GLIDDEN #30YY 10/038 "FOREST BLACK"	MEDIUM TEXTURE @ CONC. PANEL
(P9)	EXTERIOR PAINT		GLIDDEN #30YY 05/044 "THE DARK SIDE"	MEDIUM TEXTURE @ CONC. PANEL
(G1)	GLAZING		VITRO GLASS - SOLARGRAY	
(AL)	STOREFRONT FRAME		DARK BRONZE	

PCD FILE NO: PPR2329

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



1 NORTH END CAP PERSPECTIVE  
SCALE: 12" = 1'-0"



2 SOUTH TENANT PERSPECTIVE  
SCALE: 12" = 1'-0"

REVISIONS	DATE	DESCRIPTION
	10/20/2023	RESUBMITTAL
	11/16/2023	RESUBMITTAL

DRAWN	CBW
CHECKED	BS
DESIGNED	KS
FILENAME	BS11530

**SITE DEVELOPMENT PLAN**  
**THE ROCK COMMERCE CENTER**  
**EXTERIOR PERSPECTIVES**

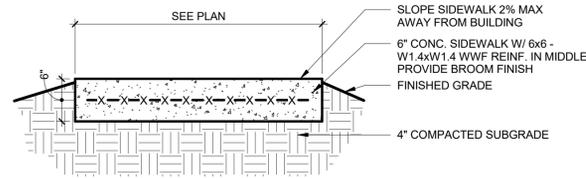


■ architecture  
 ■ planning  
 ■ interiors  
 2000 West Littleton Blvd  
 Littleton, Colorado 80120  
 P. 303.738.8877 F. 303.738.2294  
 www.igarch.com

JOB NO.	BS11530
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	20
SHEET	17

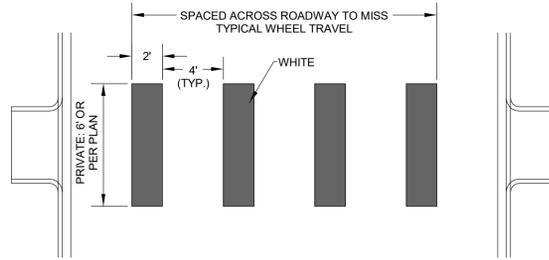
# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO

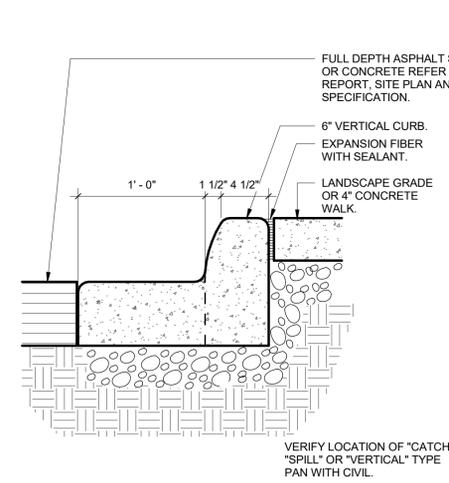


**NOTE:** PROVIDE HAND TOOLED TRANSVERSE & LONGITUDINAL CONTRACTION JOINTS @ 5'-0" O.C. MAX., 3/8" EXPANSION JOINTS @ 25'-0" O.C. MAX.

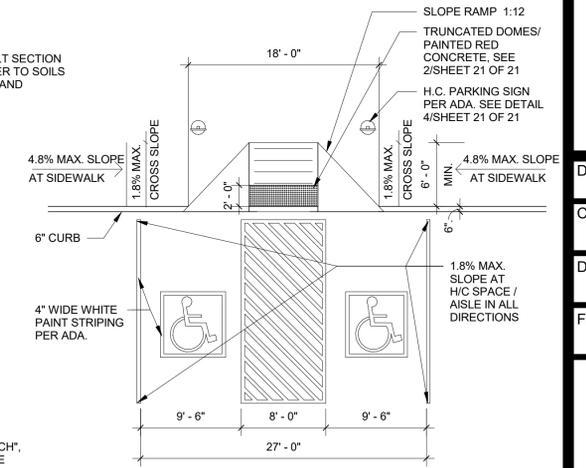
**12 EXTERIOR CONC. SIDEWALK**  
SCALE: 1" = 1'-0"



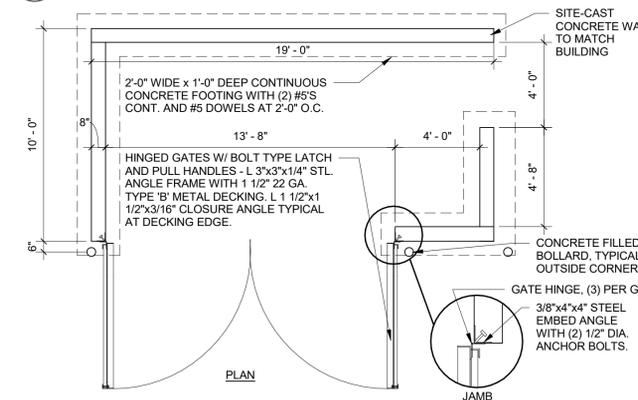
**9 CROSS WALK STRIPING DETAIL**  
SCALE: 12" = 1'-0"



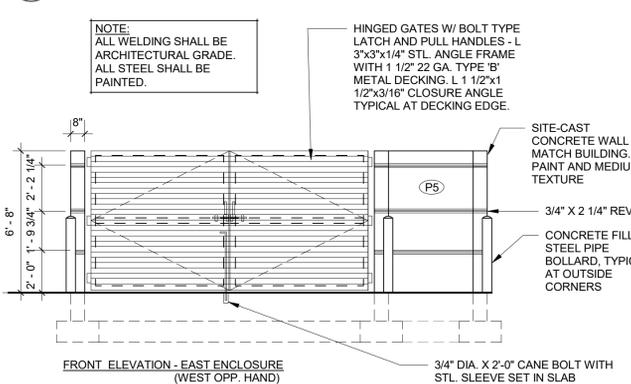
**6 CURB DETAIL**  
SCALE: 1 1/2" = 1'-0"



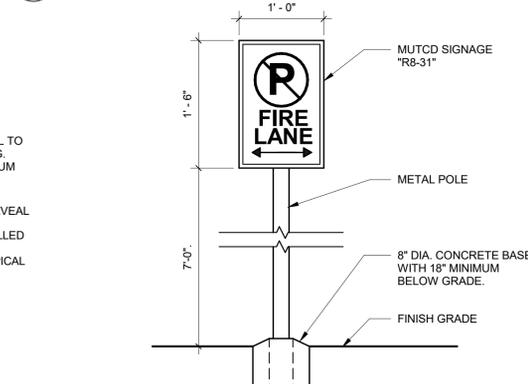
**3 ACCESSIBLE PARKING ENLARGED PLAN**  
SCALE: 1/8" = 1'-0"



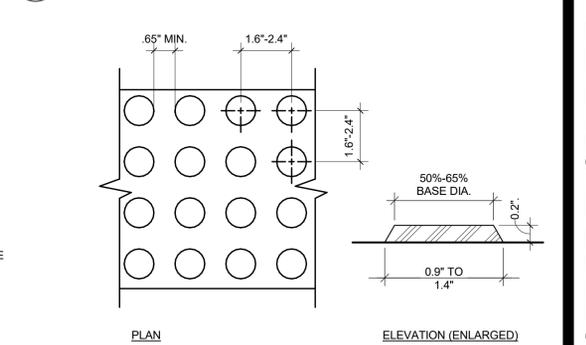
**11 TRASH ENCLOSURE DETAIL**  
SCALE: 1/4" = 1'-0"



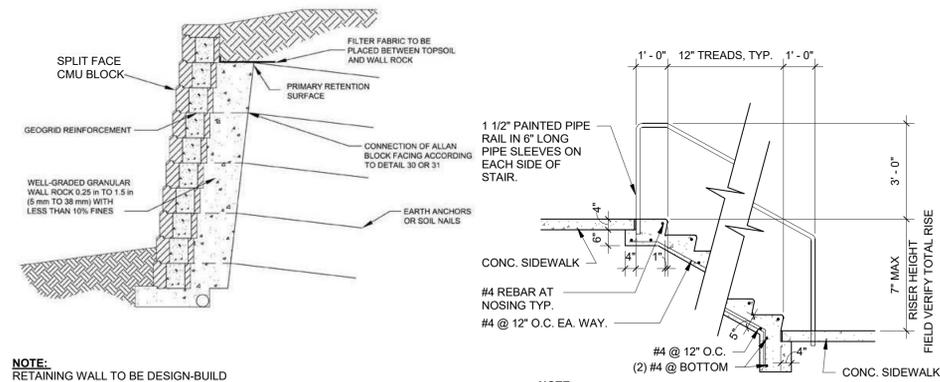
**FRONT ELEVATION - EAST ENCLOSURE (WEST OPP. HAND)**



**5 FIRE LANE SIGN DETAIL**  
SCALE: 1" = 1'-0"

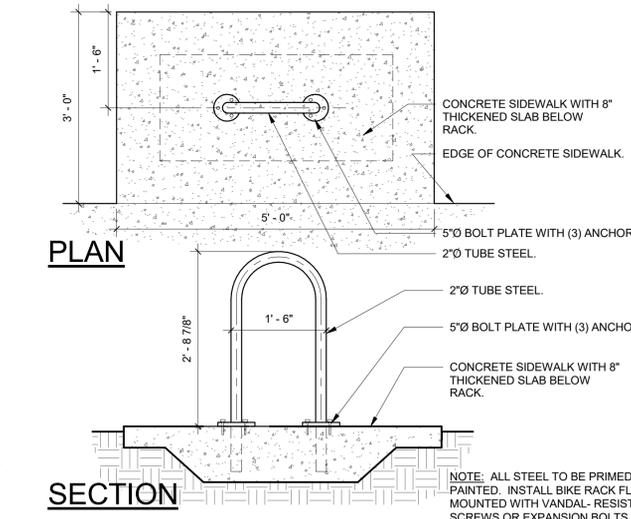


**2 TRUNCATED DOME SIZING & SPACING**  
SCALE: 3" = 1'-0"

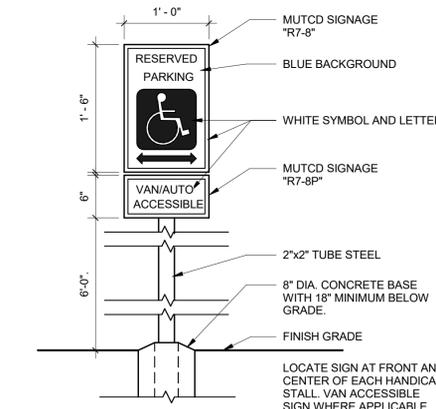


**13 SEGMENTED BLOCK RETAINING WALL**  
SCALE: 3/4" = 1'-0"

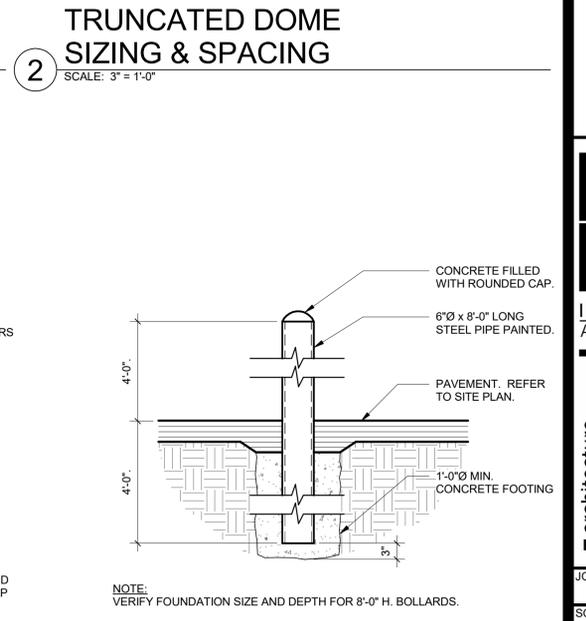
**10 LANDSCAPE STAIR DETAIL**  
SCALE: 3/8" = 1'-0"



**7 BIKE RACK DETAIL**  
SCALE: 3/4" = 1'-0"



**4 HC PARKING SIGN**  
SCALE: 1" = 1'-0"



**1 BOLLARD DETAIL**  
SCALE: 3/4" = 1'-0"

REVISIONS	DESCRIPTION
DATE	RESUBMITTAL
10/20/2023	RESUBMITTAL
11/16/2023	RESUBMITTAL

BY	
DRAWN	CBW
CHECKED	BS
DESIGNED	KS
FILENAME	BS11530

**SITE DEVELOPMENT PLAN**  
**THE ROCK COMMERCE CENTER**  
**SITE DETAILS**



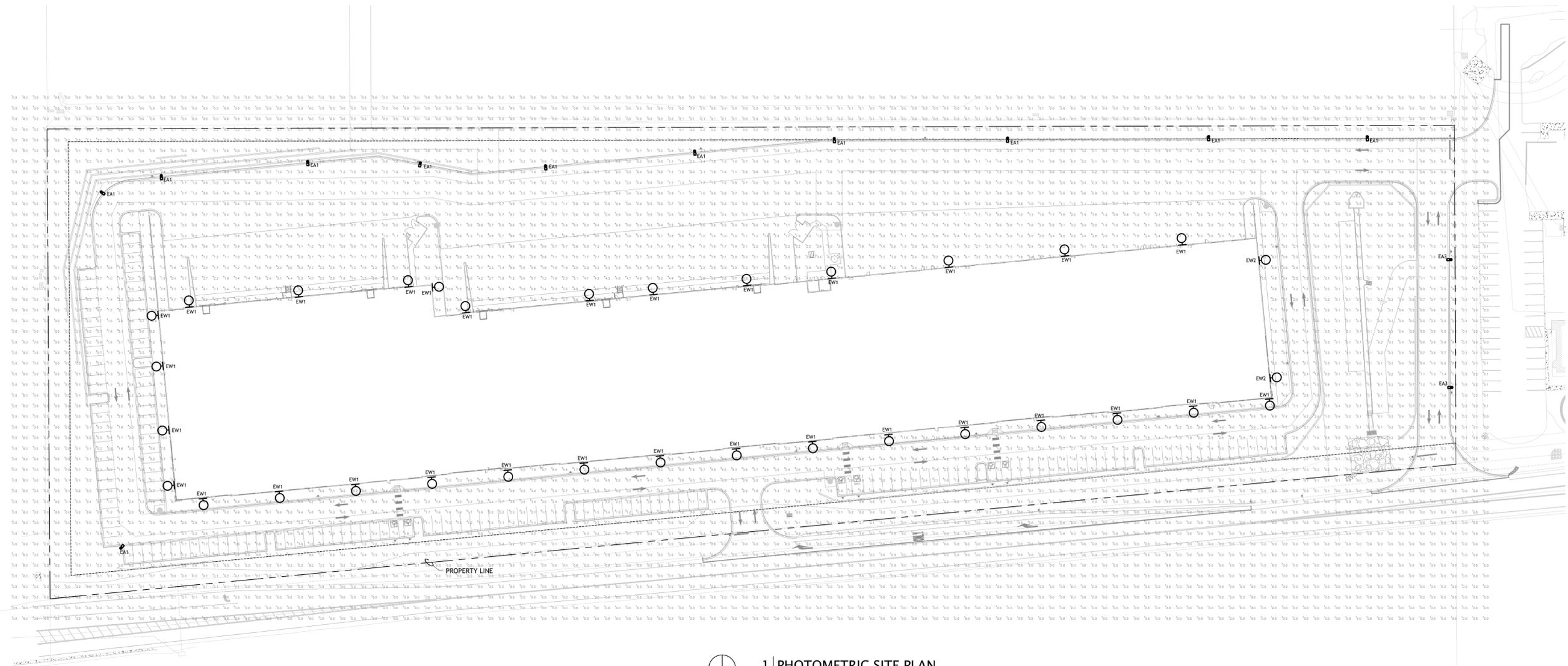
**architecture**  
**planning**  
**interiors**  
 2000 West Littleton Blvd  
 Littleton, Colorado 80120  
 P. 303.758.8877 F. 303.758.2294  
 www.igarch.com

JOB NO.	BS11530
SCALE	AS SHOWN
DATE	07/28/2023
SHEETS	SHEET
<b>20</b>	<b>18</b>

PCD FILE NO: PPR2329

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO



1 | PHOTOMETRIC SITE PLAN  
25 | SCALE: 1" = 50'

REVISIONS	DATE	DESCRIPTION
	10/20/23	2ND SUBMITTAL
	11/17/23	3RD SUBMITTAL

DRAWN  
HJ, HK

CHECKED  
EDR

DESIGNED  
HJ, HK

FILENAME  
PPR2329

**SITE DEVELOPMENT PLAN**  
**THE ROCK COMMERCE CENTER**  
**PHOTOMETRIC SITE PLAN**



**INTERGROUP  
ARCHITECTS**

**architecture**  
**planning**  
**interiors**  
 2000 West Littleton Blvd  
 Littleton, Colorado 80120  
 P: 303.758.8877 F: 303.758.2294  
[www.igarch.com](http://www.igarch.com)

JOB NO.  
6411.00

SCALE  
AS SHOWN

DATE  
07/28/2023

SHEETS  
**20**

SHEET  
**19**

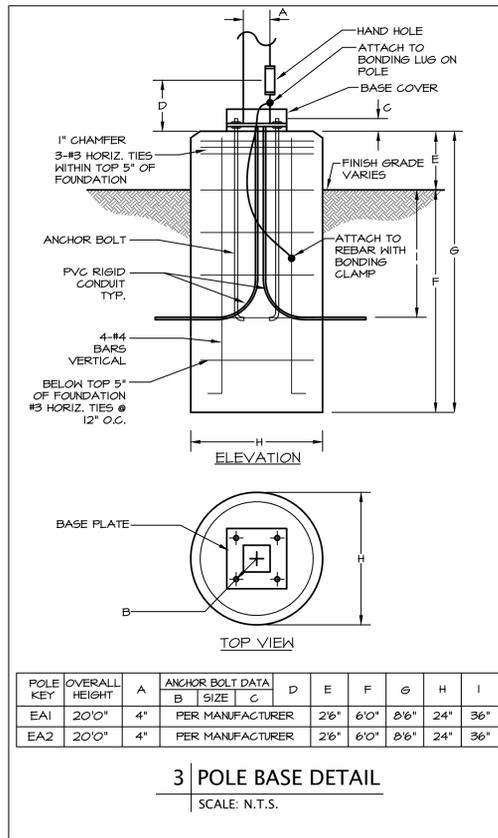
**AE DESIGN**  
 Integrated Lighting, Technology, and Electrical Solutions  
 1900 Wazee Street #205 | Denver, CO 80202 | 303.296.3034  
[aedesign-inc.com](http://aedesign-inc.com) Project #: 6411.00

PCD FILE NO: PPR2329

# SITE DEVELOPMENT PLAN THE ROCK COMMERCE CENTER

A PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11,  
TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
COUNTY OF EL PASO, STATE OF COLORADO

Description	Symbol	Avg	Max	Min	Max/Min	Avg/Min
EAST LOADING	X	2.6 fc	11.3 fc	0.1 fc	113.0:1	25.0:1
NORTH PARKING LOT	X	2.4 fc	8.8 fc	0.2 fc	44.0:1	12.0:1
PROPERTY LINE	+	0.1 fc	1.5 fc	0.0 fc	N/A	N/A
PROPERTY LINE + 20'	+	0.0 fc	0.1 fc	0.0 fc	N/A	N/A
SITE	+	1.1 fc	15.6 fc	0.0 fc	N/A	N/A
SOUTH PARKING LOT	X	3.0 fc	7.9 fc	0.9 fc	8.8:1	3.3:1
SOUTHEAST PARKING LOT	X	2.6 fc	8.2 fc	0.5 fc	16.4:1	5.2:1
WEST PARKING LOT	X	3.7 fc	15.6 fc	0.4 fc	39.0:1	9.3:1



### D-Series Size 1 LED Area Luminaire

**Specifications**

- EPA: 0.69 ft<sup>2</sup> (0.06m<sup>2</sup>)
- Length: 32.71" (831mm)
- Width: 14.26" (362mm)
- Height H1: 7.28" (185mm)
- Height H2: 2.23" (57mm)
- Weight: 34 lbs (15.4kg)

**Introduction**

The modern styling of the D-Series features a highly refined aesthetic that blends seamlessly with its environment. The D-Series offers the benefits of the latest in LED technology into a high performance, high efficacy, long-life luminaire.

The photometric performance results in sites with excellent uniformity, greater pole spacing and lower power density. D-Series outstanding photometry aids in reducing the number of poles required in area lighting applications with typical energy savings of 65% and expected service life of over 100,000 hours.

**Ordering Information**

EXAMPLE: DSX1 LED P7 40K 70CRI T3M MVOLT SPA NLAIR2 PIRH9 DBX0

Series	Optics	Color Temperature	Color Rendering Index	Distribution	Mounting	Shipping
DSX1 LED	Forward optics	(this section 70CRI only)	70CRI	A9	Automotive front row	T3M Type II medium
P7	P6	300K	3000K	T306	Type II (short)	T306 Type II low glare
P7	P7	400K	4000K	T308	Type II medium	T308 Type II medium
P7	P8	500K	5000K	T309	Type II medium	T309 Type II medium
P7	P9	(this section 80CRI only, extended lead times apply)	80CRI	T310	Type II (low glare)	T310 Type II low glare
P7	P10	300K	3000K	T311	Type II medium	T311 Type II medium
P7	P11	400K	4000K	T312	Type II low glare	T312 Type II low glare
P7	P12	500K	5000K	T313	Forward throw medium	T313 Forward throw medium

**Shipping included**

- WVOLT (100V-277V)
- WVOLT (147V-480V)
- WVOLT (277V-480V)
- SPA Suspension mounting (DBX only)
- RPA Round pole mounting (DBX only)
- SRM Square pole mounting (DBX only)
- SRM Square pole mounting #1 drilling
- SRM Square pole mounting #2 drilling
- SRM Square pole mounting #3 drilling
- SRM Square pole mounting #4 drilling
- SRM Square pole mounting #5 drilling
- SRM Square pole mounting #6 drilling
- SRM Square pole mounting #7 drilling
- SRM Square pole mounting #8 drilling
- SRM Square pole mounting #9 drilling
- SRM Square pole mounting #10 drilling
- SRM Square pole mounting #11 drilling
- SRM Square pole mounting #12 drilling
- SRM Square pole mounting #13 drilling
- SRM Square pole mounting #14 drilling
- SRM Square pole mounting #15 drilling
- SRM Square pole mounting #16 drilling
- SRM Square pole mounting #17 drilling
- SRM Square pole mounting #18 drilling
- SRM Square pole mounting #19 drilling
- SRM Square pole mounting #20 drilling
- SRM Square pole mounting #21 drilling
- SRM Square pole mounting #22 drilling
- SRM Square pole mounting #23 drilling
- SRM Square pole mounting #24 drilling
- SRM Square pole mounting #25 drilling
- SRM Square pole mounting #26 drilling
- SRM Square pole mounting #27 drilling
- SRM Square pole mounting #28 drilling
- SRM Square pole mounting #29 drilling
- SRM Square pole mounting #30 drilling
- SRM Square pole mounting #31 drilling
- SRM Square pole mounting #32 drilling
- SRM Square pole mounting #33 drilling
- SRM Square pole mounting #34 drilling
- SRM Square pole mounting #35 drilling
- SRM Square pole mounting #36 drilling
- SRM Square pole mounting #37 drilling
- SRM Square pole mounting #38 drilling
- SRM Square pole mounting #39 drilling
- SRM Square pole mounting #40 drilling
- SRM Square pole mounting #41 drilling
- SRM Square pole mounting #42 drilling
- SRM Square pole mounting #43 drilling
- SRM Square pole mounting #44 drilling
- SRM Square pole mounting #45 drilling
- SRM Square pole mounting #46 drilling
- SRM Square pole mounting #47 drilling
- SRM Square pole mounting #48 drilling
- SRM Square pole mounting #49 drilling
- SRM Square pole mounting #50 drilling
- SRM Square pole mounting #51 drilling
- SRM Square pole mounting #52 drilling
- SRM Square pole mounting #53 drilling
- SRM Square pole mounting #54 drilling
- SRM Square pole mounting #55 drilling
- SRM Square pole mounting #56 drilling
- SRM Square pole mounting #57 drilling
- SRM Square pole mounting #58 drilling
- SRM Square pole mounting #59 drilling
- SRM Square pole mounting #60 drilling
- SRM Square pole mounting #61 drilling
- SRM Square pole mounting #62 drilling
- SRM Square pole mounting #63 drilling
- SRM Square pole mounting #64 drilling
- SRM Square pole mounting #65 drilling
- SRM Square pole mounting #66 drilling
- SRM Square pole mounting #67 drilling
- SRM Square pole mounting #68 drilling
- SRM Square pole mounting #69 drilling
- SRM Square pole mounting #70 drilling
- SRM Square pole mounting #71 drilling
- SRM Square pole mounting #72 drilling
- SRM Square pole mounting #73 drilling
- SRM Square pole mounting #74 drilling
- SRM Square pole mounting #75 drilling
- SRM Square pole mounting #76 drilling
- SRM Square pole mounting #77 drilling
- SRM Square pole mounting #78 drilling
- SRM Square pole mounting #79 drilling
- SRM Square pole mounting #80 drilling
- SRM Square pole mounting #81 drilling
- SRM Square pole mounting #82 drilling
- SRM Square pole mounting #83 drilling
- SRM Square pole mounting #84 drilling
- SRM Square pole mounting #85 drilling
- SRM Square pole mounting #86 drilling
- SRM Square pole mounting #87 drilling
- SRM Square pole mounting #88 drilling
- SRM Square pole mounting #89 drilling
- SRM Square pole mounting #90 drilling
- SRM Square pole mounting #91 drilling
- SRM Square pole mounting #92 drilling
- SRM Square pole mounting #93 drilling
- SRM Square pole mounting #94 drilling
- SRM Square pole mounting #95 drilling
- SRM Square pole mounting #96 drilling
- SRM Square pole mounting #97 drilling
- SRM Square pole mounting #98 drilling
- SRM Square pole mounting #99 drilling
- SRM Square pole mounting #100 drilling

### WDGE4 LED Architectural Wall Sconce

**Specifications**

- Depth (D1): 10"
- Depth (D2): 2"
- Height: 9"
- Width: 25"
- Weight (without options): 30.5 lbs

**Introduction**

The WDGE4 LED family is designed to meet specifier's every wall-mounted lighting need in a widely accepted shape that blends with any architecture. The clean, rectangular design comes in four sizes with lumen packages ranging from 1,200 to 25,000 lumens, providing a true site-wide solution. Embedded with LightBulb AIR wireless controls, the WDGE4 family provides additional energy savings and code compliance.

WDGE4 has been designed to deliver up to 25,000 lumens through a precision refractive lens with wide distribution, perfect for augmenting the lighting from pole-mounted luminaires.

**WDGE4 LED Family Overview**

Luminaire	Standard LED, 9°C	Cold LED, 24°C	Series	P1	P2	P3	P4	P5	P6
WDGE4 LED	4W	—	—	1,200	2,000	—	—	—	—
WDGE4 LED	10W	10W	Standard / Height	1,200	2,000	3,000	4,500	6,000	—
WDGE4 LED	15W	15W	Standard / Height	7,500	8,500	10,000	12,000	—	—
WDGE4 LED	—	—	Standard / Height	12,000	14,000	16,000	20,000	22,000	25,000

**Ordering Information**

EXAMPLE: WDGE4 LED P3 40K 70CRI R3 MVOLT SRM DBX0

Series	Optics	Color Temperature	CR	Mounting	Shipping
WDGE4 LED	P1	P4	300K	3000K	R3 Type 2
P2	P5	400K	4000K	R3 Type 3	WVOLT
P3	P6	500K	5000K	R4 Type 4	WVOLT
				R7	Forward throw

**Shipping included**

- SRM Square pole mounting #1 drilling
- SRM Square pole mounting #2 drilling
- SRM Square pole mounting #3 drilling
- SRM Square pole mounting #4 drilling
- SRM Square pole mounting #5 drilling
- SRM Square pole mounting #6 drilling
- SRM Square pole mounting #7 drilling
- SRM Square pole mounting #8 drilling
- SRM Square pole mounting #9 drilling
- SRM Square pole mounting #10 drilling
- SRM Square pole mounting #11 drilling
- SRM Square pole mounting #12 drilling
- SRM Square pole mounting #13 drilling
- SRM Square pole mounting #14 drilling
- SRM Square pole mounting #15 drilling
- SRM Square pole mounting #16 drilling
- SRM Square pole mounting #17 drilling
- SRM Square pole mounting #18 drilling
- SRM Square pole mounting #19 drilling
- SRM Square pole mounting #20 drilling
- SRM Square pole mounting #21 drilling
- SRM Square pole mounting #22 drilling
- SRM Square pole mounting #23 drilling
- SRM Square pole mounting #24 drilling
- SRM Square pole mounting #25 drilling
- SRM Square pole mounting #26 drilling
- SRM Square pole mounting #27 drilling
- SRM Square pole mounting #28 drilling
- SRM Square pole mounting #29 drilling
- SRM Square pole mounting #30 drilling
- SRM Square pole mounting #31 drilling
- SRM Square pole mounting #32 drilling
- SRM Square pole mounting #33 drilling
- SRM Square pole mounting #34 drilling
- SRM Square pole mounting #35 drilling
- SRM Square pole mounting #36 drilling
- SRM Square pole mounting #37 drilling
- SRM Square pole mounting #38 drilling
- SRM Square pole mounting #39 drilling
- SRM Square pole mounting #40 drilling
- SRM Square pole mounting #41 drilling
- SRM Square pole mounting #42 drilling
- SRM Square pole mounting #43 drilling
- SRM Square pole mounting #44 drilling
- SRM Square pole mounting #45 drilling
- SRM Square pole mounting #46 drilling
- SRM Square pole mounting #47 drilling
- SRM Square pole mounting #48 drilling
- SRM Square pole mounting #49 drilling
- SRM Square pole mounting #50 drilling
- SRM Square pole mounting #51 drilling
- SRM Square pole mounting #52 drilling
- SRM Square pole mounting #53 drilling
- SRM Square pole mounting #54 drilling
- SRM Square pole mounting #55 drilling
- SRM Square pole mounting #56 drilling
- SRM Square pole mounting #57 drilling
- SRM Square pole mounting #58 drilling
- SRM Square pole mounting #59 drilling
- SRM Square pole mounting #60 drilling
- SRM Square pole mounting #61 drilling
- SRM Square pole mounting #62 drilling
- SRM Square pole mounting #63 drilling
- SRM Square pole mounting #64 drilling
- SRM Square pole mounting #65 drilling
- SRM Square pole mounting #66 drilling
- SRM Square pole mounting #67 drilling
- SRM Square pole mounting #68 drilling
- SRM Square pole mounting #69 drilling
- SRM Square pole mounting #70 drilling
- SRM Square pole mounting #71 drilling
- SRM Square pole mounting #72 drilling
- SRM Square pole mounting #73 drilling
- SRM Square pole mounting #74 drilling
- SRM Square pole mounting #75 drilling
- SRM Square pole mounting #76 drilling
- SRM Square pole mounting #77 drilling
- SRM Square pole mounting #78 drilling
- SRM Square pole mounting #79 drilling
- SRM Square pole mounting #80 drilling
- SRM Square pole mounting #81 drilling
- SRM Square pole mounting #82 drilling
- SRM Square pole mounting #83 drilling
- SRM Square pole mounting #84 drilling
- SRM Square pole mounting #85 drilling
- SRM Square pole mounting #86 drilling
- SRM Square pole mounting #87 drilling
- SRM Square pole mounting #88 drilling
- SRM Square pole mounting #89 drilling
- SRM Square pole mounting #90 drilling
- SRM Square pole mounting #91 drilling
- SRM Square pole mounting #92 drilling
- SRM Square pole mounting #93 drilling
- SRM Square pole mounting #94 drilling
- SRM Square pole mounting #95 drilling
- SRM Square pole mounting #96 drilling
- SRM Square pole mounting #97 drilling
- SRM Square pole mounting #98 drilling
- SRM Square pole mounting #99 drilling
- SRM Square pole mounting #100 drilling

1 | FIXTURE TYPE 'EA1', 'EA2', 'EA3'  
SCALE: N.T.S.

2 | FIXTURE TYPE 'EW1' & 'EW2'  
SCALE: N.T.S.

TYPE	DESCRIPTION	MANUFACTURER	CATALOG NUMBER	VOLTAGE	SOURCE		MAX WATTS	LUMEN OUTPUT	DIMMING	FIXTURE FINISH	MOUNTING INFORMATION	
					QTY	WATT					LOCATION	BOF/RFD/OFF
EA1	LED AREA LIGHT, POLE TOP, TYPE IV DISTRIBUTION, HOUSE SIDE SHIELD	LITHONIA	DSX1-P2-40K-70CRI-T4M-MVOLT-RPA-HS-DBLXD	277V	1	60	4000K 70+ CRI	9,909 LM	SWITCHING	BLACK	POLE TOP	20' - 0" BOF
EA2	LED AREA LIGHT, POLE TOP, TYPE III DISTRIBUTION, HOUSE SIDE SHIELD	LITHONIA	DSX1-P2-40K-70CRI-T3M-MVOLT-RPA-HS-DBLXD	277V	1	60	4000K 70+ CRI	9,763 LM	SWITCHING	BLACK	POLE TOP	20' - 0" BOF
EA3	LED AREA LIGHT, POLE TOP, TYPE IV DISTRIBUTION, LOWER OUTPUT, HOUSE SIDE SHIELD	LITHONIA	DSX1-P1-40K-70CRI-T4M-MVOLT-RPA-HS-DBLXD	277V	1	51	4000K 70+ CRI	7,107 LM	SWITCHING	BLACK	POLE TOP	20' - 0" BOF
EW1	SURFACE MOUNTED LED WALL PACK, TYPE IV DISTRIBUTION	LITHONIA	WDGE4-LED-P3-40K-70CRI-R4-MVOLT-SRM-DBLXD	277V	1	123	4000K 70+ CRI	18,524 LM	SWITCHING	BLACK	WALL SURFACE	20' - 0" BOF
EW2	SURFACE MOUNTED LED WALL PACK, TYPE III DISTRIBUTION	LITHONIA	WDGE4-LED-P3-40K-70CRI-R3-MVOLT-SRM-DBLXD	277V	1	123	4000K 70+ CRI	18,074 LM	SWITCHING	BLACK	WALL SURFACE	20' - 0" BOF

ABBREVIATIONS: BOF - BOTTOM OF FIXTURE, RFD - RECESSED FIXTURE DEPTH, OFF - OVERALL FIXTURE HEIGHT, AFF(AFO) - ABOVE FINISHED FLOOR (GRADE), WFD - WALL FIXTURE DEPTH

GENERAL NOTES:

- ALL REFLECTOR LAMPS SHALL BE PROVIDED AS WIDE FLOOD DISTRIBUTION, UON.
- LUMENS LISTED ARE DELIVERED LUMENS, NOT INITIAL.
- FOR ALL SPECIFIED LUMINAIRES, THE ELECTRICAL CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING ALL MOUNTING HARDWARE, ACCESSORIES, COMPONENTS, LEADER/JUMPER CABLES, WIRE FEED, CONNECTORS, END CAPS, REMOTE POWER SUPPLIES, AND ANY OTHER NECESSARY COMPONENT AS REQUIRED FOR INSTALLING A SECURE AND FULLY FUNCTIONAL SYSTEM.
- ALL FINISH SELECTIONS SHALL BE VERIFIED BY ARCHITECT/INTERIOR DESIGNER/OWNER AS PART OF THE SUBMITTAL PROCESS. UNLESS OTHERWISE NOTED, EC SHALL ASSUME STANDARD LUMINAIRE FINISH OPTION FOR PRICING.
- EC SHALL VERIFY ALL FIXTURE MOUNTING HEIGHTS WITH ARCHITECTURAL ELEVATIONS PRIOR TO ANY ROUGH-IN.
- EXTERIOR LUMINAIRES SHALL BE COLD WEATHER RATED FOR 0 DEG. F / -10 DEG. C, AND RATED FOR OUTDOOR USE.

REVISIONS	DATE	DESCRIPTION
	10/20/23	2ND SUBMITTAL
	11/17/23	3RD SUBMITTAL

DRAWN: HJ, HK  
CHECKED: EDR  
DESIGNED: HJ, HK  
FILENAME: PPR2329

SITE DEVELOPMENT PLAN  
 THE ROCK COMMERCE CENTER  
 PHOTOMETRIC DETAILS



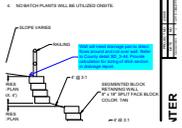
architecture  
planning  
interiors

2000 West Lithonia Blvd  
Lithonia, Colorado 80120  
P: 303.758.8977 F: 303.758.2294  
www.igarch.com

JOB NO: 6411.00  
SCALE: AS SHOWN  
DATE: 07/28/2023  
SHEETS: 20 SHEET: 20

# V3\_Site Development Plan Comments.pdf Markup Summary

CDurham (1)



**Subject:** Callout  
**Page Label:** [5] 5 OF 20 GRADING PLAN  
**Author:** CDurham  
**Date:** 12/5/2023 7:54:47 AM  
**Color:** ■

Wall will need drainage pan to direct flows around and not over wall. Refer to County detail SD\_3-44. Provide calculation for sizing of ditch section in drainage report.

# THE ROCK COMMERCE CENTER PUBLIC IMPROVEMENT PLAN CONSTRUCTION DOCUMENTS

LOCATED IN THE SOUTHWEST QUARTER OF THE  
NORTHWEST QUARTER OF SECTION 11, TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE SIXTH PRINCIPAL MERIDIAN,  
EL PASO COUNTY, STATE OF COLORADO.

## PROJECT TEAM

### OWNER / DEVELOPER

CENTRAL DEVELOPMENT, LLC  
1600 S. ALBION ST., #200  
DENVER, CO 80222  
303.628.0200 voice  
CONTACT: JEREMY RECORDS

### CIVIL ENGINEER

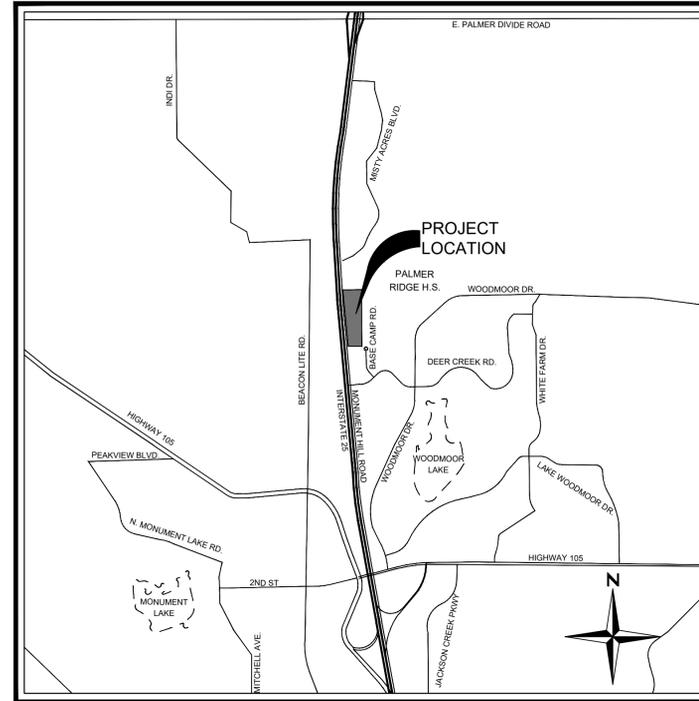
REDLAND  
1500 W. CANAL CT.  
LITTLETON, CO 80120  
720.283.6783 voice  
CONTACT: MARK CEVAAL, P.E.  
EMAIL: mcevaal@redland.com

### ARCHITECT

INTERGROUP ARCHITECTS  
2000 W. LITTLETON BLVD.  
LITTLETON, CO 80120  
303.407.1157 voice  
CONTACT: BILL SMITH, AIA

### LANDSCAPE ARCHITECT

STACKLOT  
5369 S. CURTICE ST.  
LITTLETON, CO 80120  
303.808.4523 voice  
CONTACT: STEVE WIENS  
EMAIL: steve@stacklot.com



VICINITY MAP  
SCALE: 1" = 2000'

### BENCHMARK

NGS CONTROL POINT T 395 BEING A STANDARD NGS STEEL ROD IN A LOGO MONUMENT BOX LOCATED 20 MILES NORTH OF COLORADO SPRINGS ON THE EAST SIDE OF I-25, 1,200 FEET NORTH OF THE WEIGH STATION BUILDING, AND 20.5 FEET EAST OF THE EASTERLY EDGE OF OIL OF THE NORTHBOUND LANES OF I-25.

NAVD88. ELEV = 7111.32'

### BASIS OF BEARINGS

BEARINGS SHOWN HEREON ARE REFERENCED TO THE SOUTHERLY BOUNDARY OF LOT 1, GREATER EUROPE MISSION SUBDIVISION FILING NO. 1, BEING MONUMENTED AS SHOWN HEREON, ASSUMED TO BEAR SOUTH 80°00'37" WEST, A DISTANCE OF 358.79 FEET.

### DESIGN ENGINEER'S STATEMENT

THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR DETAILED ROADWAY, DRAINAGE, GRADING, AND EROSION CONTROL PLANS AND SPECIFICATIONS, AND SAID PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH APPLICABLE MASTER DRAINAGE PLANS AND MASTER TRANSPORTATION PLANS. SAID PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR ROADWAY AND DRAINAGE FACILITIES ARE DESIGNED AND ARE CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THESE DETAILED PLANS AND SPECIFICATIONS

MARK D. CEVAAL, P.E. #33123

DATE

### OWNER/DEVELOPER'S STATEMENT

I, THE OWNER/DEVELOPER HAVE READ AND WILL COMPLY WITH THE REQUIREMENTS OF THE GRADING AND EROSION CONTROL PLAN.

JEREMY RECORDS  
CENTRAL DEVELOPMENT, LLC  
1600 S. ALBION ST #200,  
DENVER, CO 80222

DATE

Sheet List Table	
Sheet Number	Sheet Title
C1.0	COVER SHEET
C1.1	REDLAND GENERAL NOTES
C2.0	DEMOLITION PLAN
C3.0	HORIZONTAL CONTROL PLAN
C4.0	PLAN AND PROFILE
C5.0	GRADING PLAN
C6.0	EROSION CONTROL PLAN
C7.1	ROAD CROSS SECTIONS
C7.2	ROAD CROSS SECTIONS
C8.0	SIGNAGE AND STRIPING PLAN
C9.1	SITE DETAILS
C9.2	EROSION CONTROL DETAILS
C9.3	EROSION CONTROL DETAILS

### STANDARD NOTES FOR EL PASO COUNTY CONSTRUCTION PLANS:

- ALL DRAINAGE AND ROADWAY CONSTRUCTION SHALL MEET THE STANDARDS AND SPECIFICATIONS OF THE CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2, AND THE EL PASO COUNTY ENGINEERING CRITERIA MANUAL.
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE NOTIFICATION AND FIELD NOTIFICATION OF ALL EXISTING UTILITIES, WHETHER SHOWN ON THE PLANS OR NOT, BEFORE BEGINNING CONSTRUCTION. LOCATION OF EXISTING UTILITIES SHALL BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. CALL 811 TO CONTACT THE UTILITY NOTIFICATION CENTER OF COLORADO (UNCC).
- CONTRACTOR SHALL KEEP A COPY OF THESE APPROVED PLANS, THE GRADING AND EROSION CONTROL PLAN, THE STORMWATER MANAGEMENT PLAN (SWMP), THE SOILS AND GEOTECHNICAL REPORT, AND THE APPROPRIATE DESIGN AND CONSTRUCTION STANDARDS AND SPECIFICATIONS AT THE JOB SITE AT ALL TIMES, INCLUDING THE FOLLOWING:
  - EL PASO COUNTY ENGINEERING CRITERIA MANUAL (ECM)
  - CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2
  - COLORADO DEPARTMENT OF TRANSPORTATION (CDOT) STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION
  - CDOT M & S STANDARDS
- NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION, ALL DESIGN AND CONSTRUCTION RELATED TO ROADS, STORM DRAINAGE AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS, INCLUDING THE LAND DEVELOPMENT CODE, THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING. ANY MODIFICATIONS NECESSARY TO MEET CRITERIA AFTER-THE-FACT WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY.
- IT IS THE DESIGN ENGINEER'S RESPONSIBILITY TO ACCURATELY SHOW EXISTING CONDITIONS, BOTH ON-SITE AND OFF-SITE, ON THE CONSTRUCTION PLANS. ANY MODIFICATIONS NECESSARY DUE TO CONFLICTS, OMISSIONS, OR CHANGED CONDITIONS WILL BE ENTIRELY THE DEVELOPER'S RESPONSIBILITY TO RECTIFY. CONTRACTOR SHALL SCHEDULE A PRE-CONSTRUCTION MEETING WITH EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT (PCD) - INSPECTIONS, PRIOR TO STARTING CONSTRUCTION.
- IT IS THE CONTRACTOR'S RESPONSIBILITY TO UNDERSTAND THE REQUIREMENTS OF ALL JURISDICTIONAL AGENCIES AND TO OBTAIN ALL REQUIRED PERMITS, INCLUDING BUT NOT LIMITED TO EL PASO COUNTY EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP), REGIONAL BUILDING FLOODPLAIN DEVELOPMENT PERMIT, U.S. ARMY CORPS OF ENGINEERS-ISSUED 401 AND/OR 404 PERMITS, AND COUNTY AND STATE FUGITIVE DUST PERMITS.
- CONTRACTOR SHALL NOT DEVIATE FROM THE PLANS WITHOUT FIRST OBTAINING WRITTEN APPROVAL FROM THE DESIGN ENGINEER AND PCD. CONTRACTOR SHALL NOTIFY THE DESIGN ENGINEER IMMEDIATELY UPON DISCOVERY OF ANY ERRORS OR INCONSISTENCIES.
- ALL STORM DRAIN PIPE SHALL BE CLASS III RCP UNLESS OTHERWISE NOTED AND APPROVED BY PCD.
- CONTRACTOR SHALL COORDINATE GEOTECHNICAL TESTING PER ECM STANDARDS. PAVEMENT DESIGN SHALL BE APPROVED BY EL PASO COUNTY PCD PRIOR TO PLACEMENT OF CURB AND GUTTER AND PAVEMENT.
- ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE AT APPROVED CONSTRUCTION ACCESS POINTS.
- SIGHT VISIBILITY TRIANGLES AS IDENTIFIED IN THE PLANS SHALL BE PROVIDED AT ALL INTERSECTIONS. OBSTRUCTIONS GREATER THAN 18 INCHES ABOVE FLOWLINE ARE NOT ALLOWED WITHIN SIGHT TRIANGLES.
- SIGNING AND STRIPING SHALL COMPLY WITH EL PASO COUNTY DOT AND MUTCD CRITERIA. (IF APPLICABLE, ADDITIONAL SIGNING AND STRIPING NOTES WILL BE PROVIDED).
- CONTRACTOR SHALL OBTAIN ANY PERMITS REQUIRED BY EL PASO COUNTY DOT, INCLUDING WORK WITHIN THE RIGHT-OF-WAY AND SPECIAL TRANSPORT PERMITS.
- THE LIMITS OF CONSTRUCTION SHALL REMAIN WITHIN THE PROPERTY LINE UNLESS OTHERWISE NOTED. THE OWNER/DEVELOPER SHALL OBTAIN WRITTEN PERMISSION AND EASEMENTS, WHERE REQUIRED, FROM ADJOINING PROPERTY OWNER(S) PRIOR TO ANY OFF-SITE DISTURBANCE, GRADING, OR CONSTRUCTION

### EL PASO COUNTY

COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH COUNTY DESIGN CRITERIA. THE COUNTY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

FIELD IN ACCORDANCE WITH REQUIREMENTS OF THE EL PASO COUNTY LAND DEVELOPMENT CODE, DRAINAGE CRITERIA MANUAL, VOLUMES 1 AND 2, AND ENGINEERING CRITERIA MANUAL AS AMENDED. IN ACCORDANCE WITH ECM SECTION 1.12, THESE CONSTRUCTION DOCUMENTS WILL BE VALID FOR CONSTRUCTION FOR A PERIOD OF 2 YEARS FROM THE DATE SIGNED BY THE EL PASO COUNTY ENGINEER. IF CONSTRUCTION HAS NOT STARTED WITHIN THOSE 2 YEARS, THE PLANS WILL NEED TO BE RESUBMITTED FOR APPROVAL, INCLUDING PAYMENT OF REVIEW FEES AT THE PLANNING AND COMMUNITY DEVELOPMENT DIRECTORS DISCRETION.

JOSH PALMER, P.E.  
COUNTY ENGINEER/ECM ADMINISTRATOR

DATE

### LEGAL DESCRIPTION:

#### PARCEL B:

THAT PORTION OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11, TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE 6TH P.M. LYING EAST OF THE EAST LINE OF THAT TRACT CONVEYED TO THE STATE HIGHWAY DEPARTMENT BY QUITCLAIM DEED RECORDED SEPTEMBER 8, 1948 IN BOOK 1185, PAGE 458, ALSO DESCRIBED AS: THAT PART OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 11, TOWNSHIP 11 SOUTH, RANGE 67 WEST OF THE P.M., COUNTY OF EL PASO, STATE OF COLORADO, MORE PARTICULARLY DESCRIBED AS FOLLOWS:  
COMMENCING AT THE SOUTHWEST CORNER OF SAID NORTHWEST QUARTER; THENCE EASTERLY ALONG THE SOUTHERLY LINE OF SAID NORTHWEST QUARTER A DISTANCE OF 996.04 FEET TO A POINT ON THE EASTERLY RIGHT-OF-WAY OF INTERSTATE HIGHWAY 25 DESCRIBED IN THAT DEED TO THE STATE HIGHWAY DEPARTMENT RECORDED SEPTEMBER 8, 1948 IN BOOK 1185 AT PAGE 458, WHICH POINT IS THE TRUE POINT OF THE BEGINNING OF THE PARCEL TO BE DESCRIBED; THENCE ON A DEFLECTION ANGLE TO THE LEFT 95°08'20" AND ALONG SAID EASTERLY RIGHT OF WAY LINE A DISTANCE OF 1334.24 FEET TO A POINT ON THE NORTHERLY LINE OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER; THENCE ON A DEFLECTION ANGLE TO THE RIGHT 95°00'36" AND ALONG SAID NORTHERLY LINE 441.95 FEET TO THE NORTHEAST CORNER OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER; THENCE ON A DEFLECTION ANGLE TO THE RIGHT 90°16'15" AND ALONG THE EASTERLY LINE OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER A DISTANCE OF 1329.88 FEET TO THE SOUTHEAST CORNER OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER; THENCE ON A DEFLECTION ANGLE TO THE RIGHT 89°51'29" AND ALONG THE SOUTHERLY LINE OF SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER A DISTANCE OF 319.15 FEET TO THE POINT OF BEGINNING.

### SIGNING AND STRIPING NOTES:

- ALL SIGNS AND PAVEMENT MARKINGS SHALL BE IN COMPLIANCE WITH THE CURRENT MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (MUTCD).
- REMOVAL OF EXISTING PAVEMENT MARKINGS SHALL BE ACCOMPLISHED BY A METHOD THAT DOES NOT MATERIALLY DAMAGE THE PAVEMENT. THE PAVEMENT MARKINGS SHALL BE REMOVED TO THE EXTENT THAT THEY WILL NOT BE VISIBLE UNDER DAY OR NIGHT CONDITIONS. AT NO TIME WILL IT BE ACCEPTABLE TO PAINT OVER EXISTING PAVEMENT MARKINGS.
- ANY DEVIATION FROM THE STRIPING AND SIGNING PLAN SHALL BE APPROVED BY EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT.
- ALL SIGNS SHOWN ON THE SIGNING AND STRIPING PLAN SHALL BE NEW SIGNS. EXISTING SIGNS MAY REMAIN OR BE REUSED IF THEY MEET CURRENT EL PASO COUNTY AND MUTCD STANDARDS.
- STREET NAME AND REGULATORY STOP SIGNS SHALL BE ON THE SAME POST AT INTERSECTIONS.
- ALL REMOVED SIGNS SHALL BE DISPOSED OF IN A PROPER MANNER BY THE CONTRACTOR.
- ALL STREET NAME SIGNS SHALL HAVE "D" SERIES LETTERS, WITH LOCAL ROADWAY SIGNS BEING 4" UPPER-LOWER CASE LETTERING ON 8" BLANK AND NON-LOCAL ROADWAY SIGNS BEING 6" LETTERING, UPPER-LOWER CASE ON 12" BLANK, WITH A WHITE BORDER THAT IS NOT RECESSED. MULTI-LANE ROADWAYS WITH SPEED LIMITS OF 35 MPH OR HIGHER SHALL HAVE 8" UPPER-LOWER CASE LETTERING ON 12" BLANK WITH A WHITE BORDER THAT IS NOT RECESSED. THE WIDTH OF THE NON-RECESSED WHITE BORDERS SHALL MATCH PAGE 255 OF THE 2012 MUTCD "STANDARD HIGHWAY SIGNS". SIGNAL POLE MOUNTED AND OVERHEAD STREET NAME SIGNS SHALL BE PER MUTCD SIZE STANDARDS.
- ALL TRAFFIC SIGNS SHALL HAVE A MINIMUM HIGH INTENSITY PRISMATIC GRADE SHEETING.
- ALL LOCAL RESIDENTIAL STREET SIGNS SHALL BE MOUNTED ON A 1.75" X 1.75" SQUARE TUBE SIGN POST AND STUB POST BASE. FOR OTHER APPLICATIONS, REFER TO THE CDOT STANDARD S-614-8 REGARDING USE OF THE P2 TUBULAR STEEL POST SLIPBASE DESIGN.
- ALL SIGNS SHALL BE SINGLE SHEET ALUMINUM WITH 0.100" MINIMUM THICKNESS.
- ALL LIMIT LINES/STOP LINES, CROSSWALK LINES, PAVEMENT LEGENDS, AND ARROWS SHALL BE A MINIMUM 125 MIL THICKNESS PREFORMED THERMOPLASTIC PAVEMENT MARKINGS WITH TAPERED LEADING EDGES PER CDOT STANDARD S-627-1. STOP BARS SHALL BE 24" IN WIDTH. CROSSWALKS LINES SHALL BE 24" WIDE AND A MINIMUM OF 9' LONG.
- WORD AND SYMBOL MARKINGS SHALL BE THE NARROW TYPE.
- ALL LONGITUDINAL LINES SHALL BE A MINIMUM 15MIL THICKNESS EPOXY PAINT. ALL NON-LOCAL RESIDENTIAL ROADWAYS SHALL INCLUDE BOTH RIGHT AND LEFT EDGE LINE STRIPING AND ANY ADDITIONAL STRIPING AS REQUIRED BY CDOT S-627-1.
- THE CONTRACTOR SHALL NOTIFY EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT (719) 520-6819 PRIOR TO AND UPON COMPLETION OF SIGNING AND STRIPING.
- THE CONTRACTOR SHALL OBTAIN A WORK IN THE RIGHT OF WAY PERMIT FROM THE EL PASO COUNTY DEPARTMENT OF PUBLIC WORKS (DPW) PRIOR TO ANY SIGNAGE OR STRIPING WORK WITHIN AN EXISTING EL PASO COUNTY ROADWAY.

**15 Redland YEARS**  
WHERE GREAT PLACES BEGIN  
720.283.6783  
REDLAND.CO  
• Land Planning  
• Landscape Architecture  
• Civil Engineering  
• Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER  
PUBLIC IMPROVEMENTS PLAN  
CONSTRUCTION DOCUMENTS  
COVER SHEET**

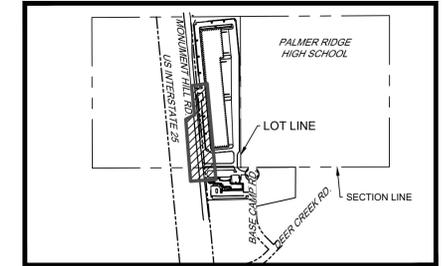
SHEET

PCD FILE NO. PPR2329

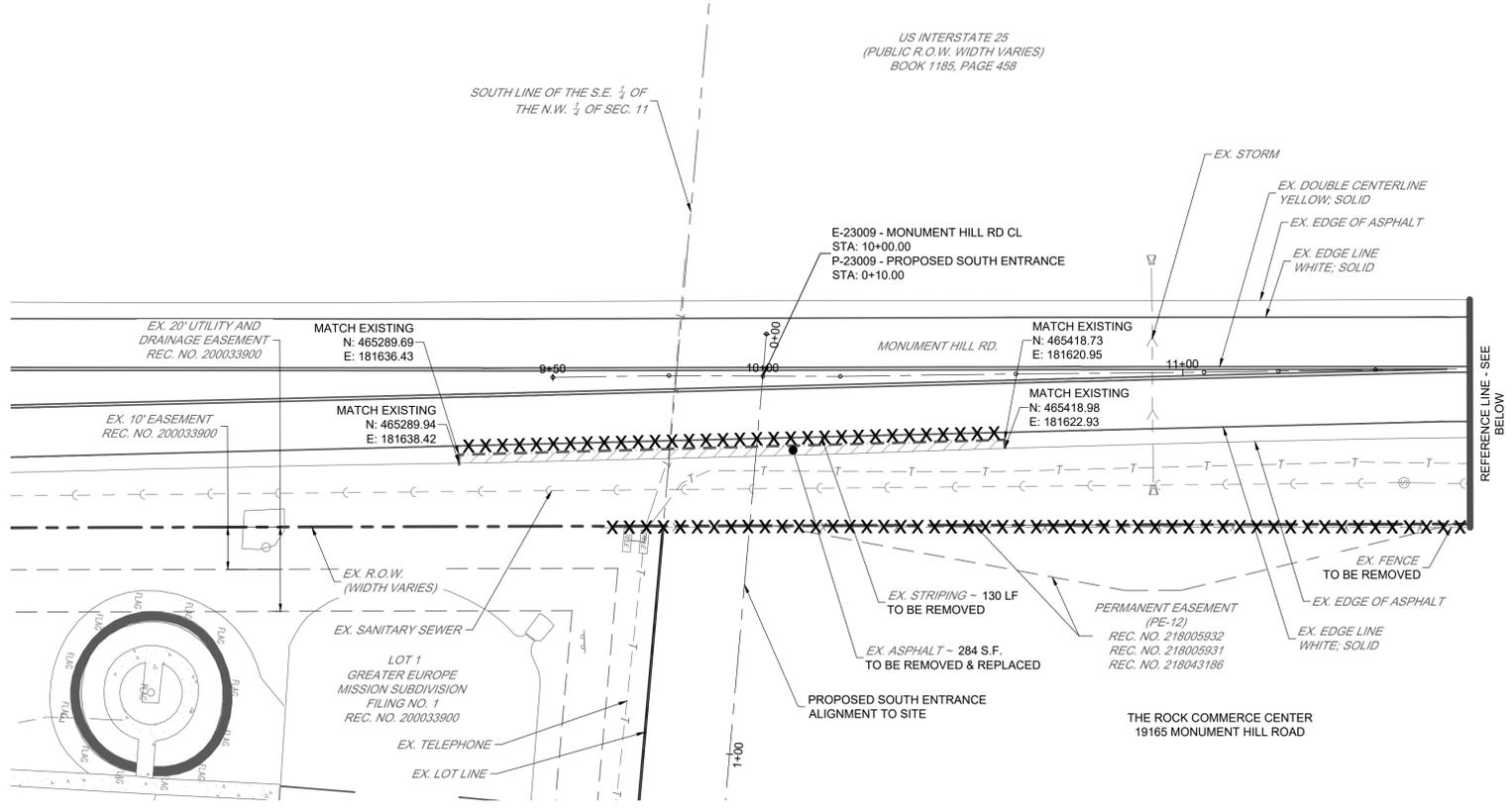
C1.0



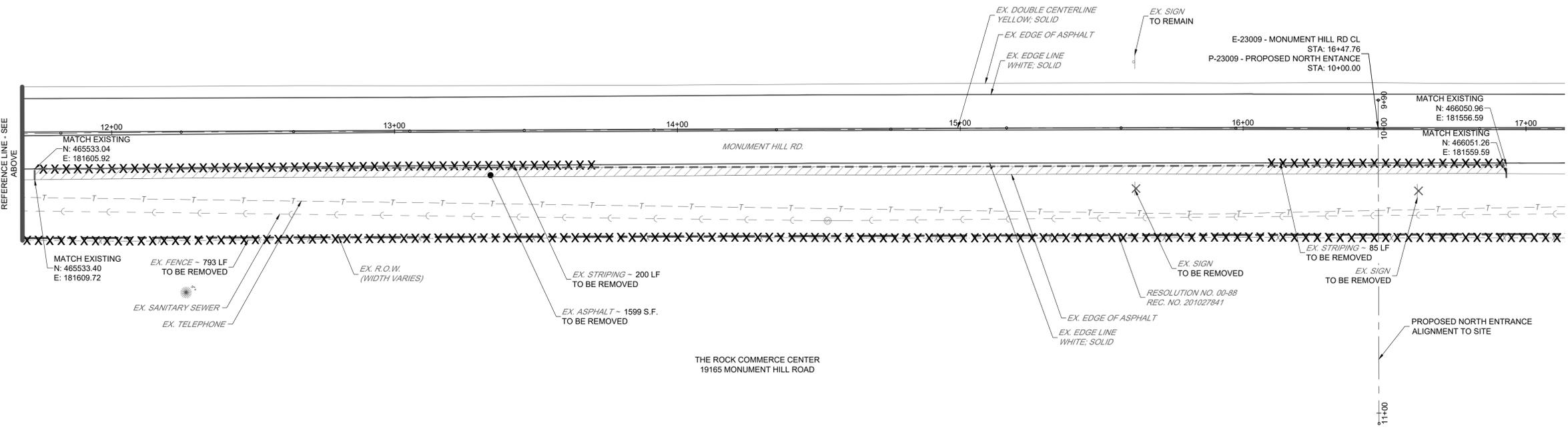
I:\2023\23009 - The Rock Commerce Center\Sheet Sets\CDs\PIP\23009\_Demo Plan.dwg tab: Demo Plan Nov 20, 2023 - 7:29am casz



KEYMAP  
SCALE = 1" = 750'



US INTERSTATE 25  
(PUBLIC R.O.W. WIDTH VARIES)  
BOOK 1185, PAGE 458



THE ROCK COMMERCE CENTER  
19165 MONUMENT HILL ROAD



Know what's below.  
Call before you dig.



SCALE: 1" = 20'

**15 Years**  
WHERE GREAT PLACES BEGIN

720.283.6783  
REDLAND.COM

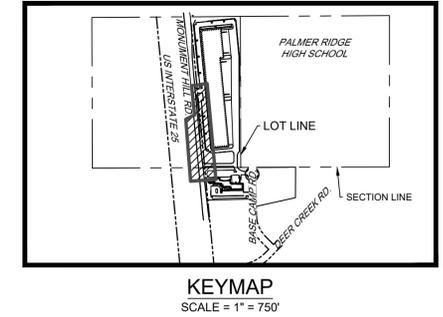
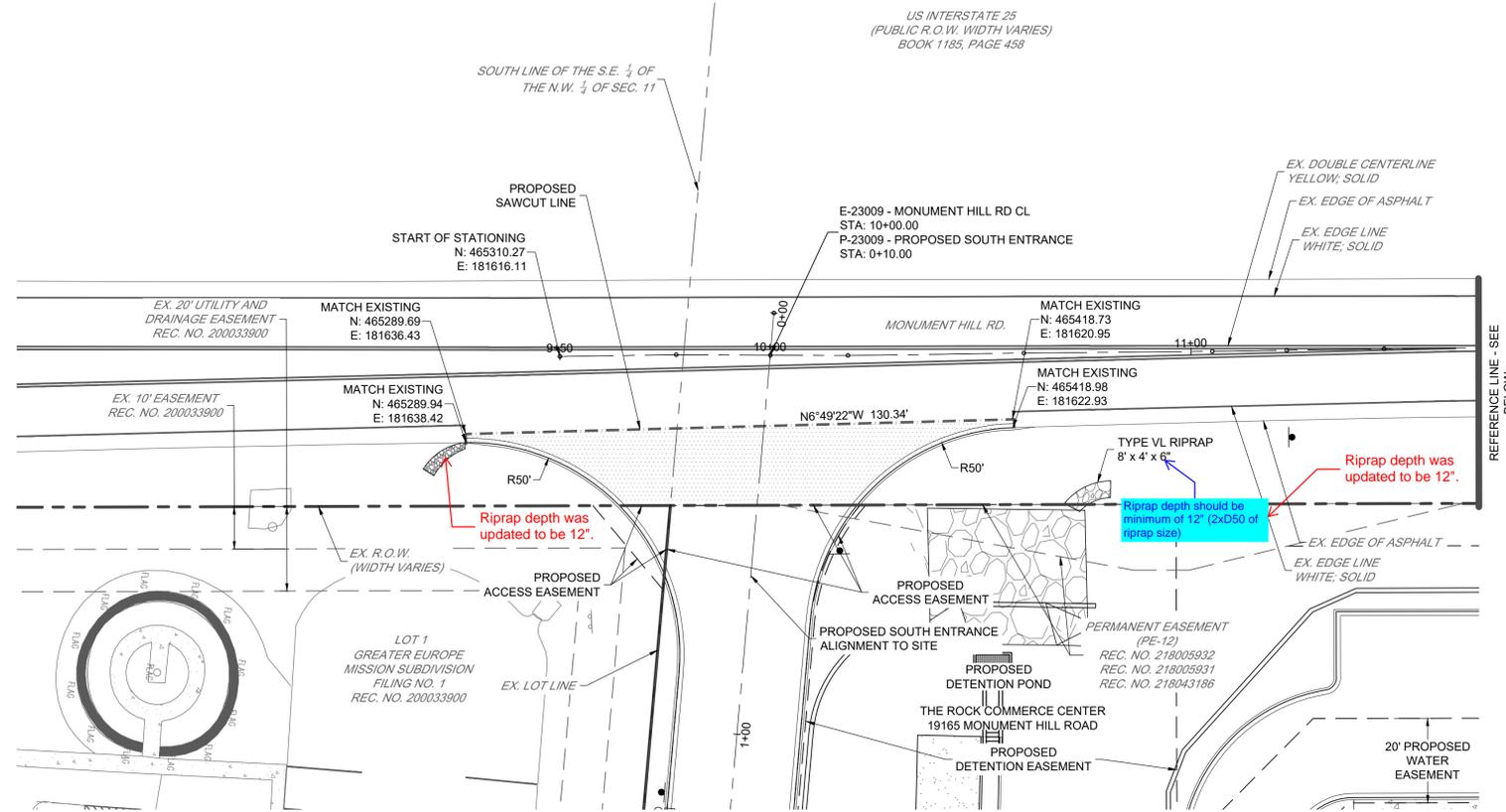
**NOT FOR CONSTRUCTION**

PROJECT NO.	NO.	DATE	NOTES
23009	1	07/28/2023	1ST SUBMITTAL
	2	10/20/2023	2ND SUBMITTAL
	3	11/17/2023	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DODUMENTS**  
DEMOLITION PLAN

SHEET  
**C2.0**

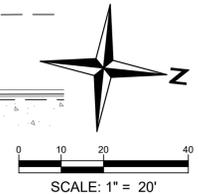
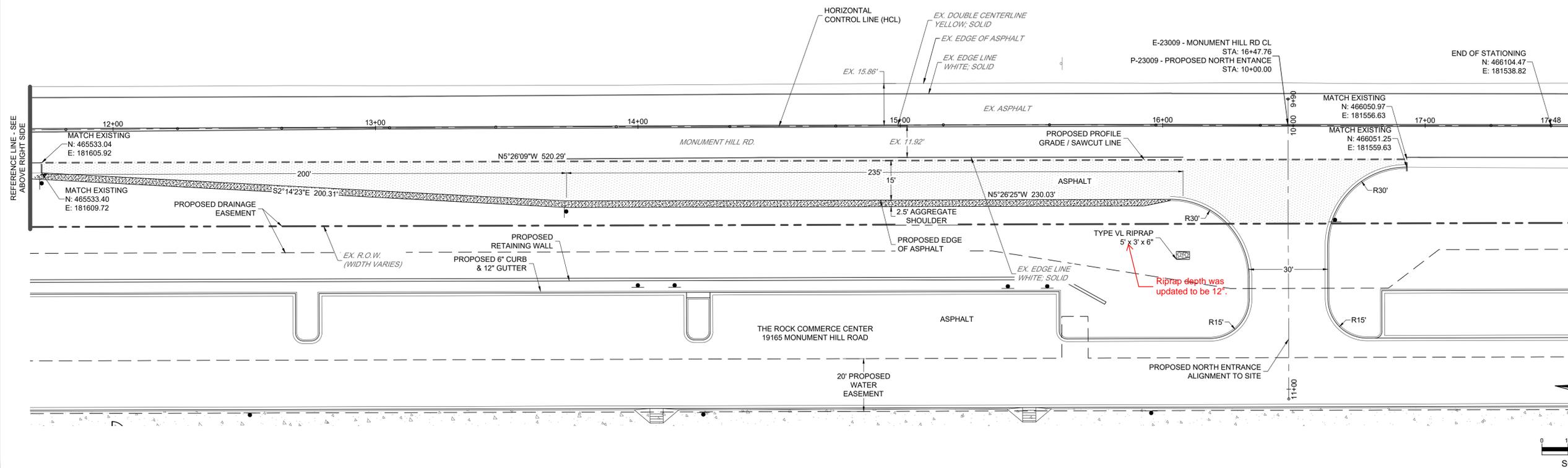
I:\2023\23009 - The Rock Commerce Center\CAAD\Sheet Sets\CDa\PIP\23009\_Horizontal Control Plan.dwg tab: Horizontal Control Plan Nov 20, 2023 -- 7:29am cszlj



PAVING LEGEND

	PROPOSED ASPHALT PAVEMENT 7.5-INCHES ASPHALT OVER 10-INCHES COMPACTED CLASS 6 AGGREGATE BASE COURSE.
	PROPOSED SHOULDER
	MATCH EXISTING

US INTERSTATE 25  
(PUBLIC R.O.W. WIDTH VARIES)  
BOOK 1185, PAGE 458



**15 YEARS**  
WHERE GREAT PLACES BEGIN

Redland  
720.283.6783  
REDLAND, CO, USA

• Land Planning  
• Landscape Architecture  
• Civil Engineering  
• Construction Management

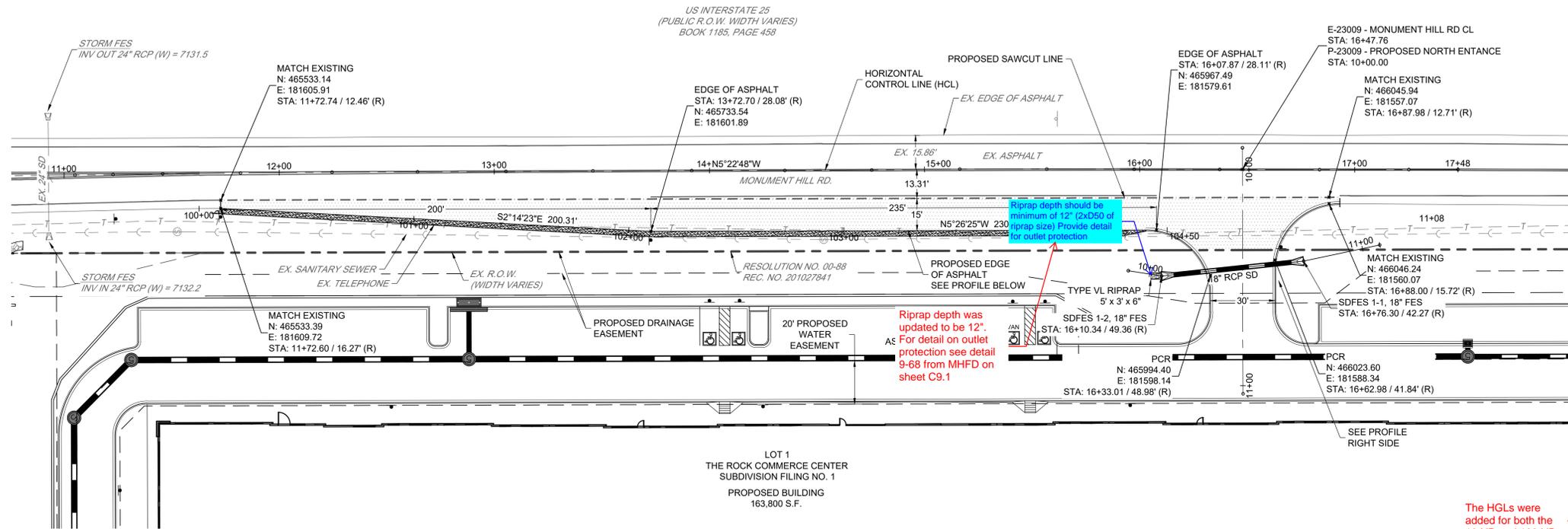
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

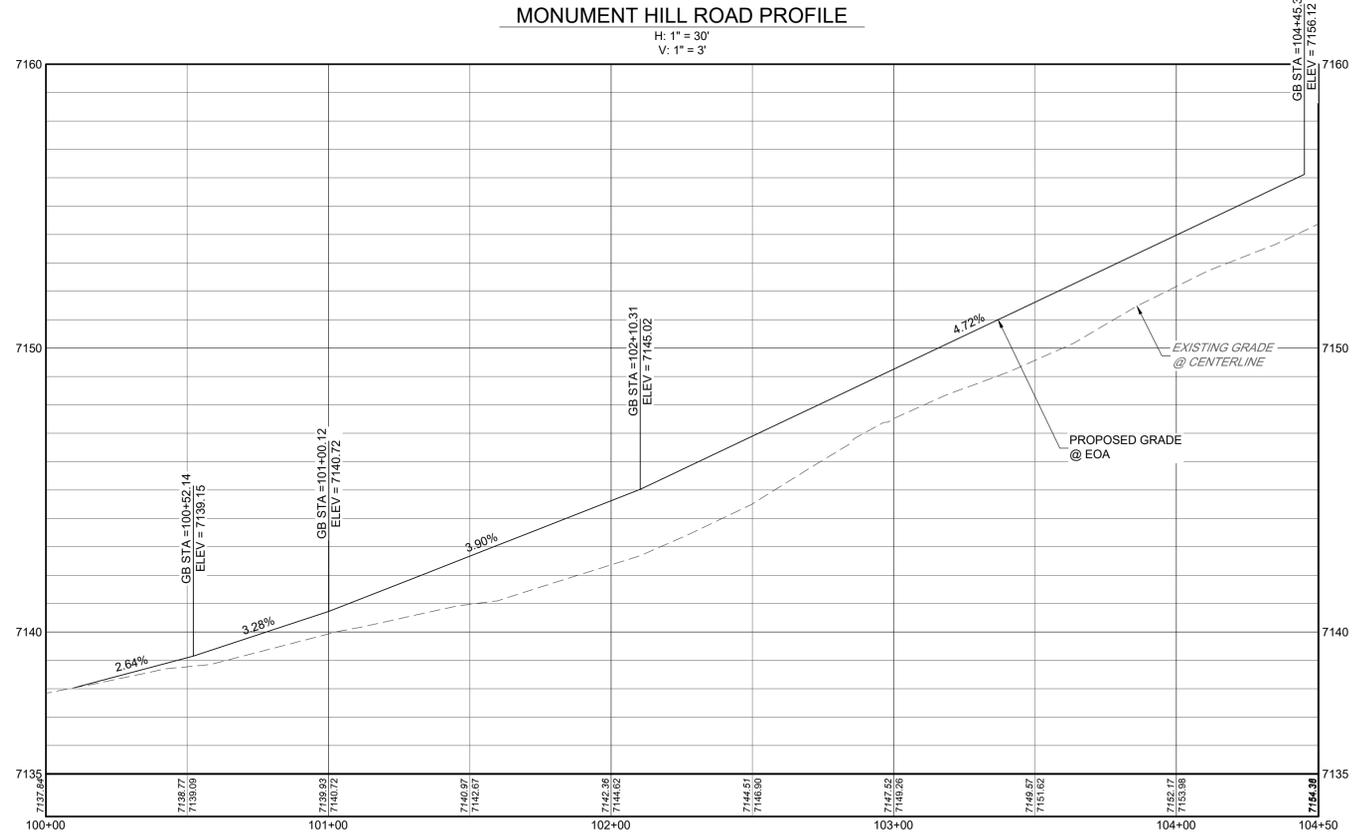
**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DOCUMENTS**  
HORIZONTAL CONTROL PLAN

SHEET  
**C3.0**

I:\2023\23009 - The Rock Commerce Center\Sheet Sets\CDs\PIP\23009\_Monument Hill Plan & Profile Nov 20, 2023 - 7:30am csaz



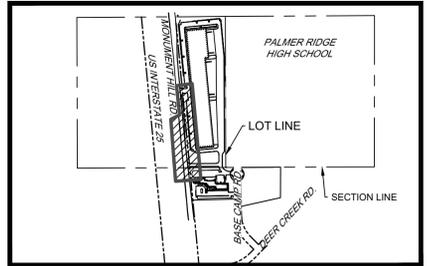
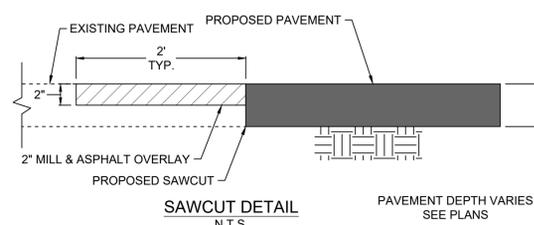
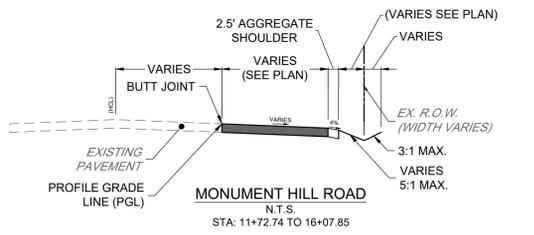
**MONUMENT HILL ROAD PLAN**  
SCALE: 1" = 30'



**MONUMENT HILL ROAD PROFILE**  
H: 1" = 30'  
V: 1" = 3'

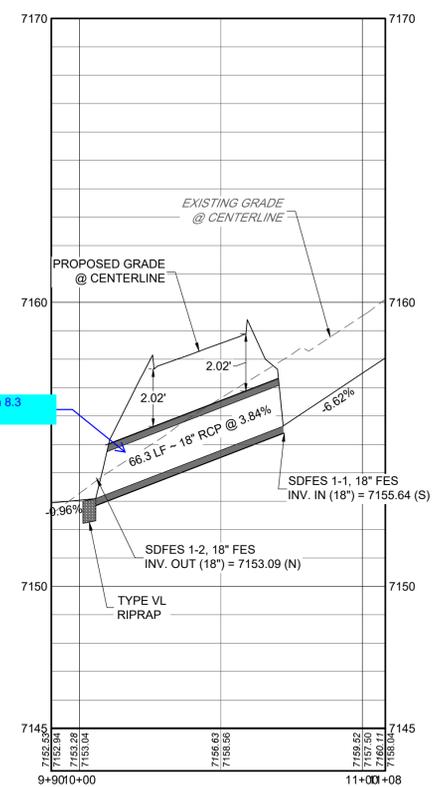
**PAVING LEGEND**

- PROPOSED ASPHALT PAVEMENT  
7.5-INCHES ASPHALT OVER 10-INCHES COMPACTED CLASS 6 AGGREGATE BASE COURSE.  
\*THIS MAY BE USED FOR BIDDING PURPOSES ONLY. HOWEVER, THE ACTUAL PAVEMENT DESIGN IS SUBJECT TO CHANGE PENDING PAVEMENT DESIGN REPORT SUBMITTAL.
- PROPOSED SHOULDER  
MATCH EXISTING



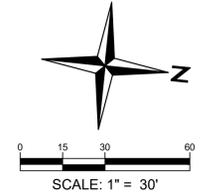
**KEYMAP**  
SCALE = 1" = 750'

**NORTH ENTRANCE CULVERT PROFILE**  
H: 1" = 30'  
V: 1" = 3'



The HGLs were added for both the 10-YR and 100-YR.

Per DCM Section 8.3 include HGL.



**15 Years** WHERE GREAT PLACES BEGIN

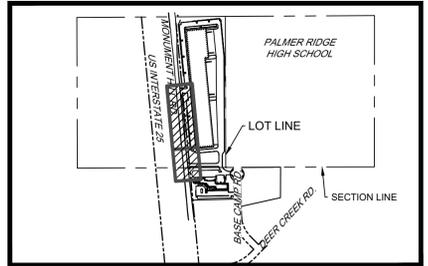
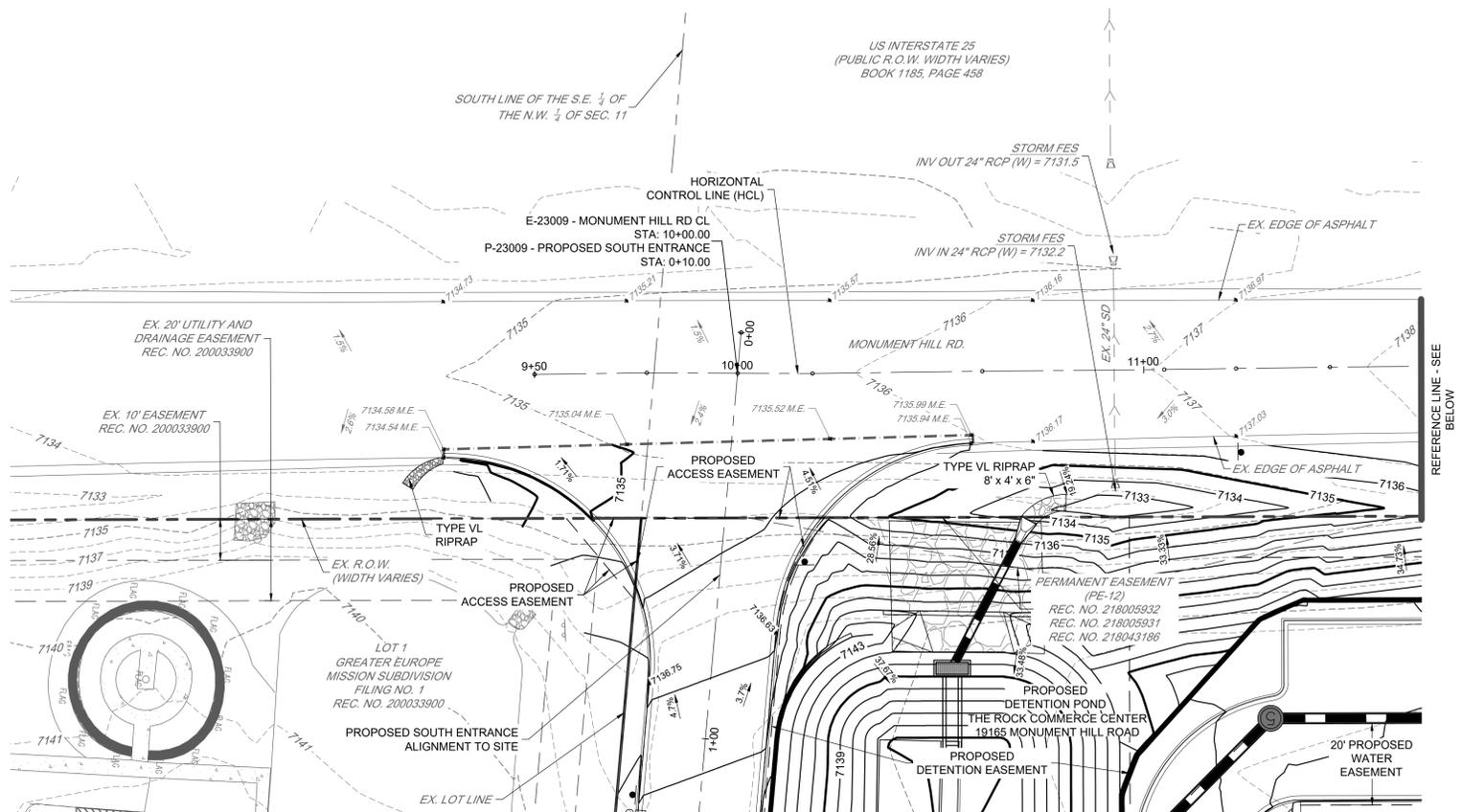
720.283.6793  
REDLAND.CO.VA

• Land Planning  
• Landscape Architecture  
• Civil Engineering  
• Construction Management

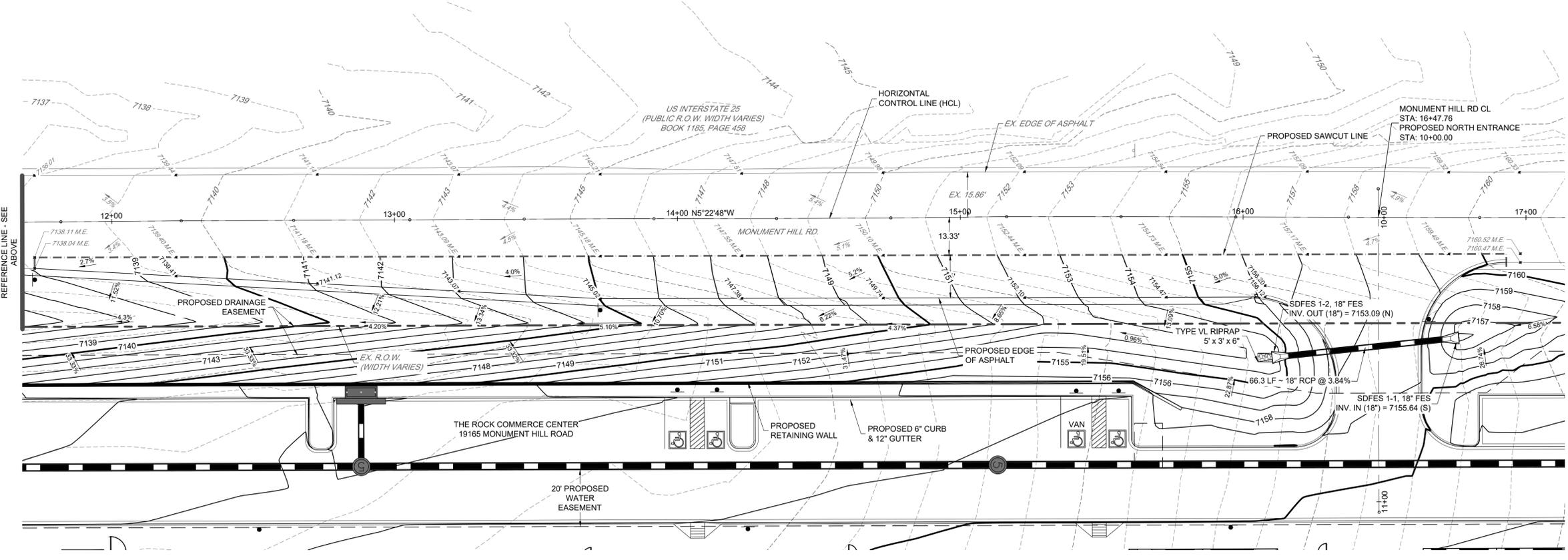
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DOCUMENTS**  
PLAN AND PROFILE



KEYMAP  
SCALE = 1" = 750'



Know what's below.  
Call before you dig.



SCALE: 1" = 20'

**15 Years**  
WHERE GREAT PLACES BEGIN

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

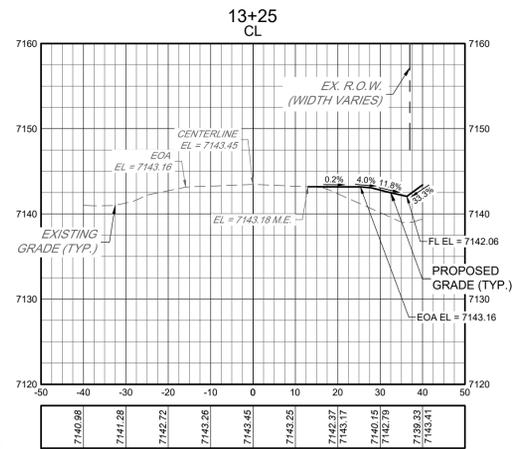
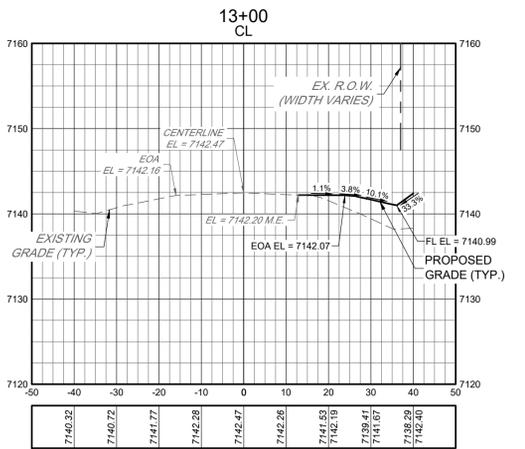
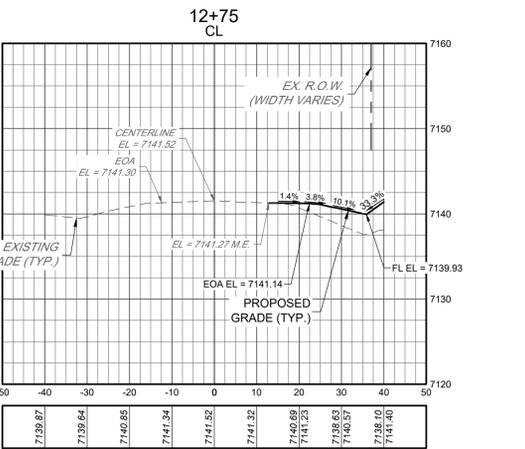
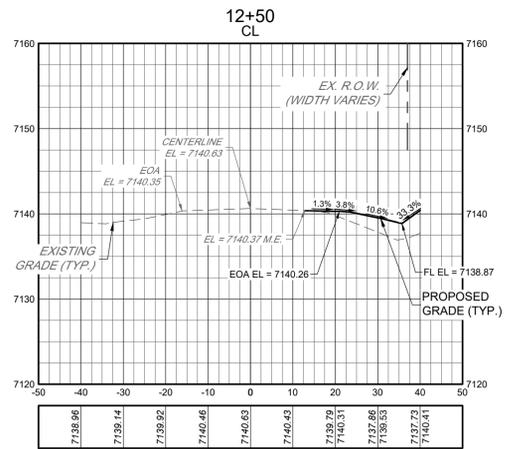
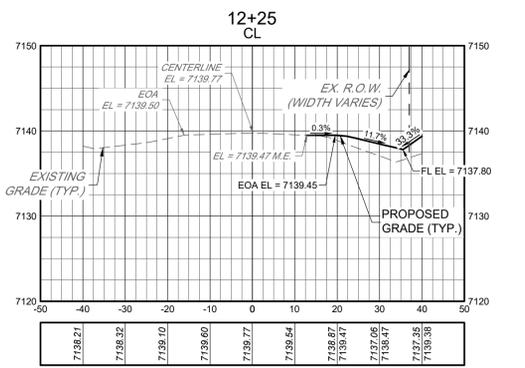
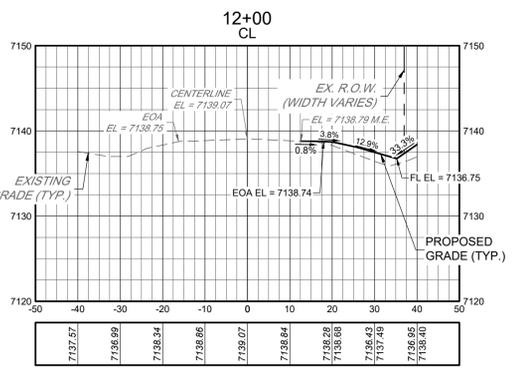
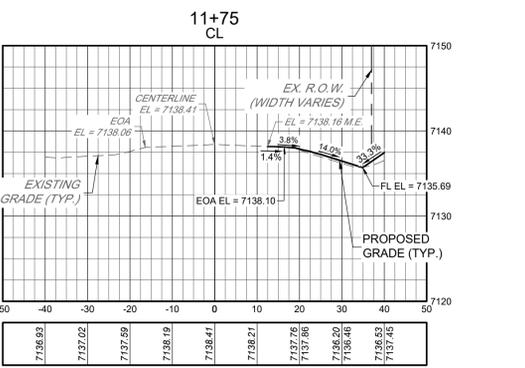
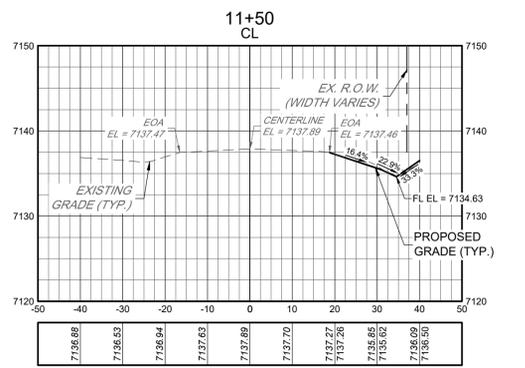
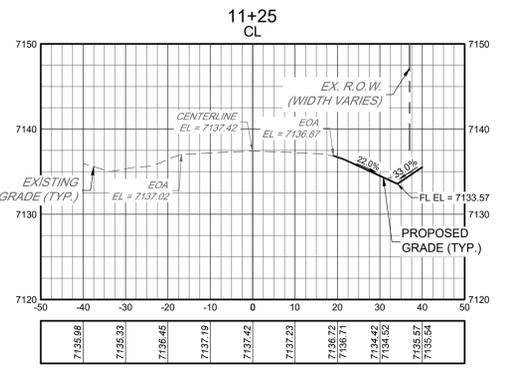
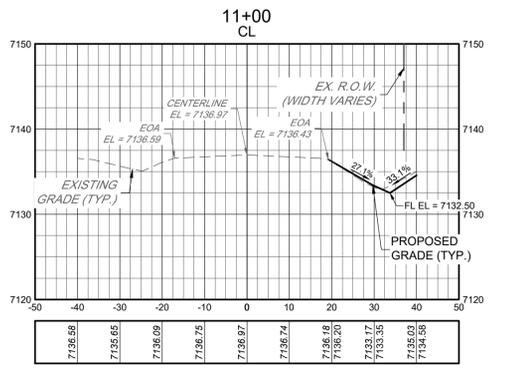
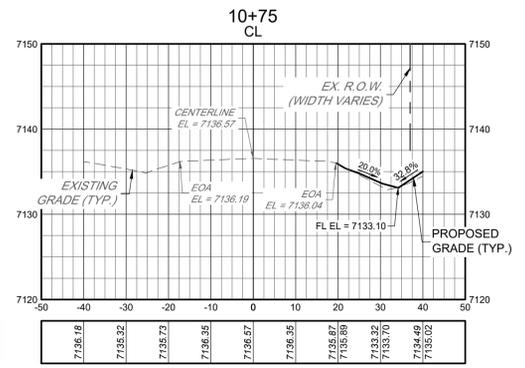
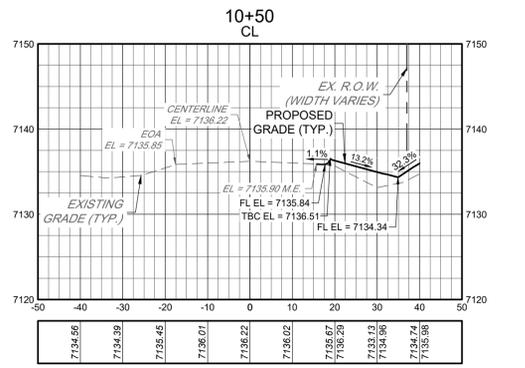
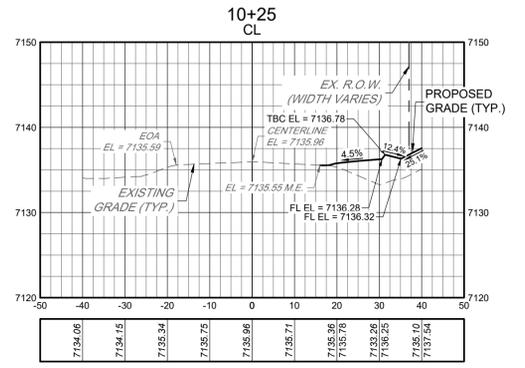
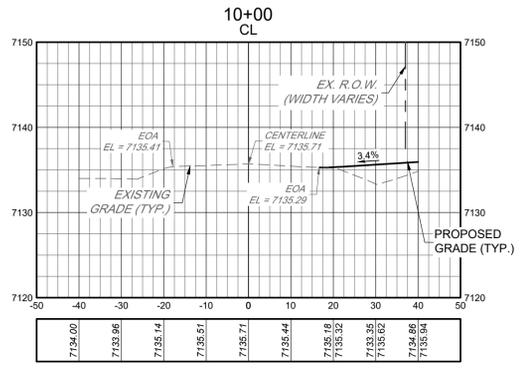
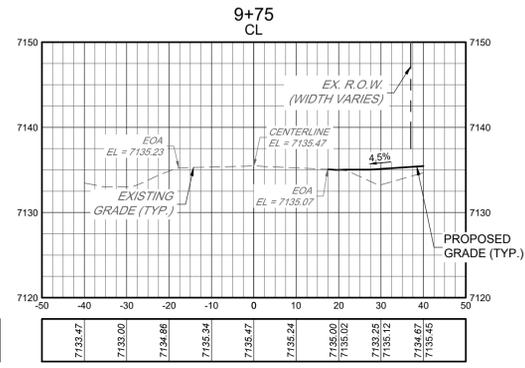
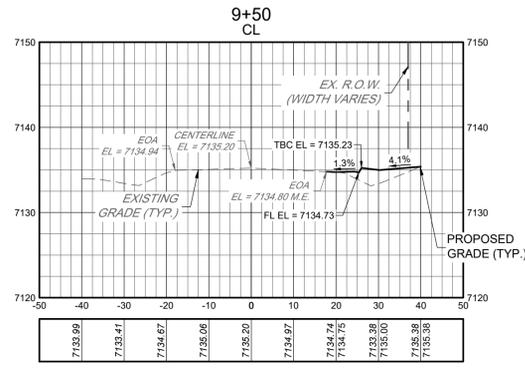
**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DODUMENTS**  
GRADING PLAN

SHEET  
**C5.0**

I:\2023\23009 - The Rock Commerce Center\CA00\Sheet Sets\CDs\PIP\23009\_Grading\_Plan.dwg Lab: Grading Plan Nov 20, 2023 - 7:30am cseaz



I:\2023\23009 - The Rock Commerce Center\Sheet Sets\GDA\PIP\23009\_Cross Sections.dwg tab: Cross Sections-1 Nov 20, 2023 7:30am csolz



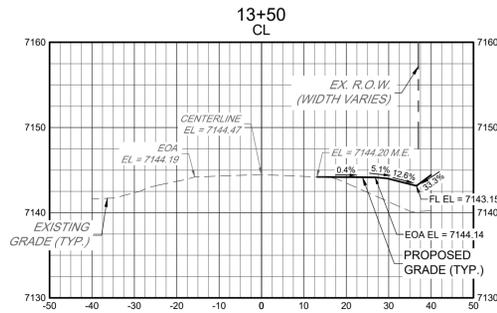
SECTION VIEWS  
 H: 1" = 20'  
 V: 1" = 10'  
 SCALE: 1" = 20'

**15 Redland YEARS**  
 WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND, CO. • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

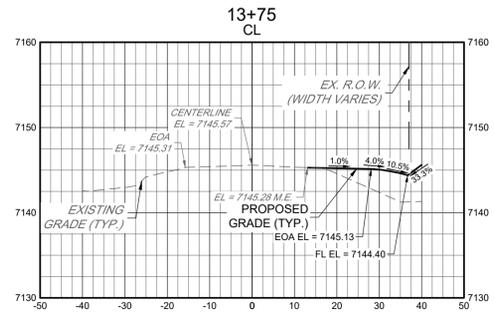
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

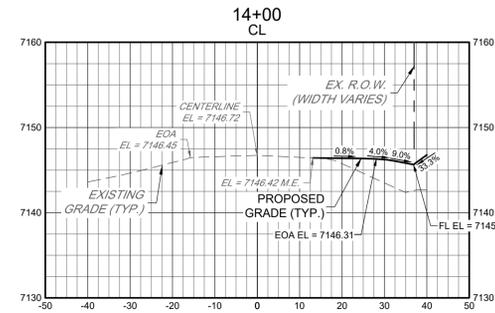
**THE ROCK COMMERCE CENTER**  
 PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DOCUMENTS**  
 ROAD CROSS SECTIONS



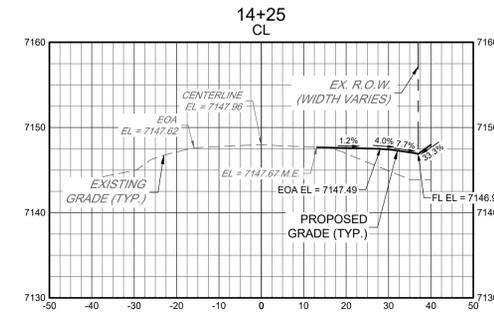
SECTION DATA
7144.66
7142.93
7148.67
7144.29
7144.47
7144.26
7149.47
7144.16
7141.27
7143.97
7140.27
7144.42



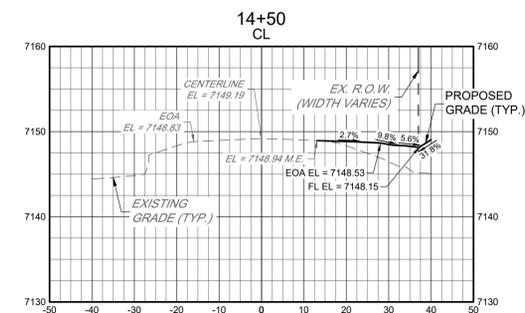
SECTION DATA
7142.96
7148.86
7144.79
7145.40
7146.97
7146.34
7144.57
7145.22
7145.05
7144.33
7145.91



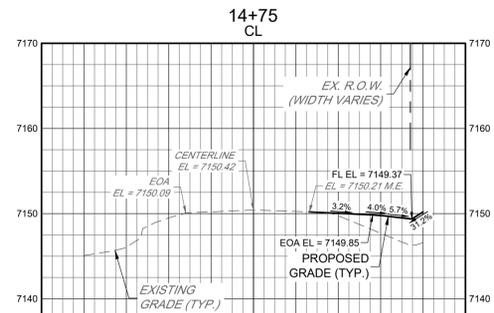
SECTION DATA
7149.59
7146.64
7146.88
7146.97
7146.72
7146.49
7145.74
7146.36
7146.48
7146.23
7146.68
7146.78



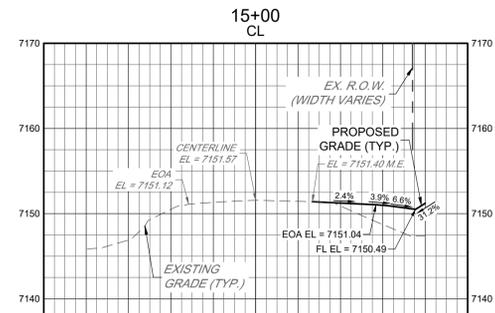
SECTION DATA
7144.00
7144.94
7147.12
7147.76
7147.96
7147.74
7146.93
7147.59
7144.90
7147.41
7148.87
7147.86



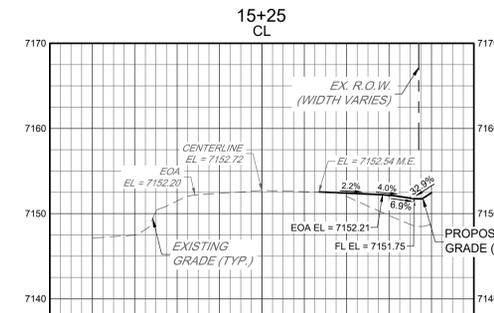
SECTION DATA
7144.45
7144.85
7148.33
7148.95
7149.19
7149.07
7148.34
7148.85
7148.44
7148.19
7145.09
7149.05



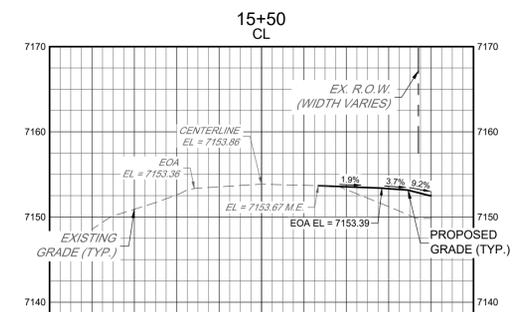
SECTION DATA
7145.06
7146.06
7149.48
7150.21
7150.42
7150.26
7148.78
7150.61
7147.70
7149.78
7146.54
7150.19



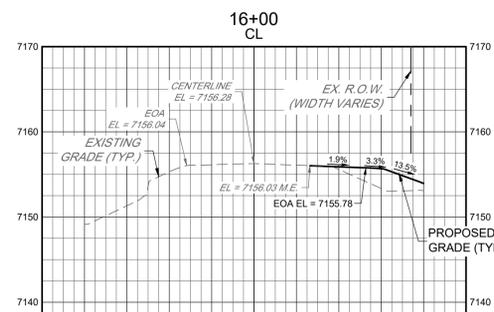
SECTION DATA
7146.91
7150.51
7151.32
7151.67
7151.45
7150.99
7151.64
7148.71
7150.88
7147.40
7151.22



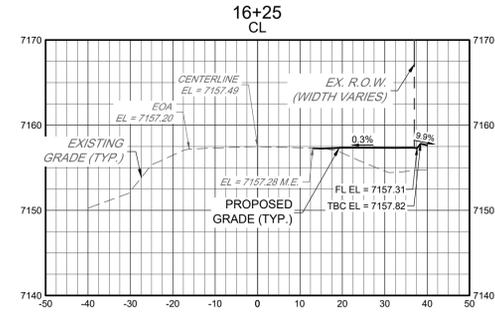
SECTION DATA
7147.13
7147.48
7151.49
7152.39
7152.72
7152.59
7152.41
7149.78
7152.15
7148.74
7152.45



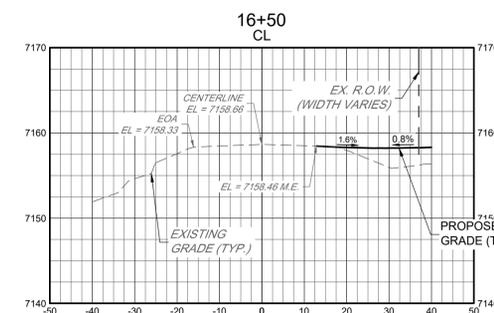
SECTION DATA
7148.55
7150.91
7152.61
7153.54
7153.86
7153.72
7153.21
7153.54
7151.32
7153.32
7149.84
7152.51



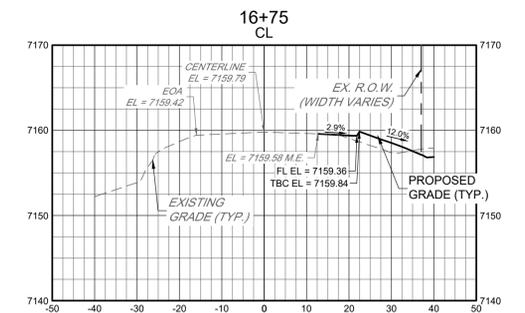
SECTION DATA
7149.15
7151.31
7155.31
7155.13
7156.28
7156.09
7155.89
7155.99
7153.35
7155.67
7153.11
7155.95



SECTION DATA
7150.25
7152.24
7156.47
7157.32
7157.49
7157.34
7156.72
7157.35
7154.62
7157.34
7154.74
7157.64



SECTION DATA
7157.91
7154.62
7157.96
7158.46
7158.66
7158.50
7157.95
7158.30
7155.96
7158.22
7158.34
7158.31

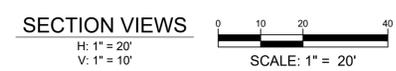


SECTION DATA
7152.21
7153.87
7158.67
7159.56
7159.79
7159.63
7159.05
7159.37
7157.24
7158.61
7157.92
7156.87

**NOT FOR CONSTRUCTION**

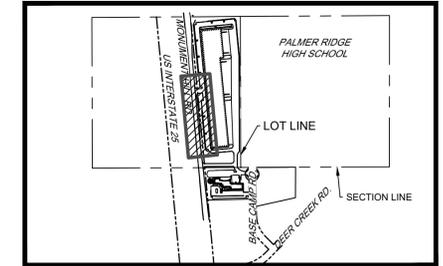
PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

SHEET

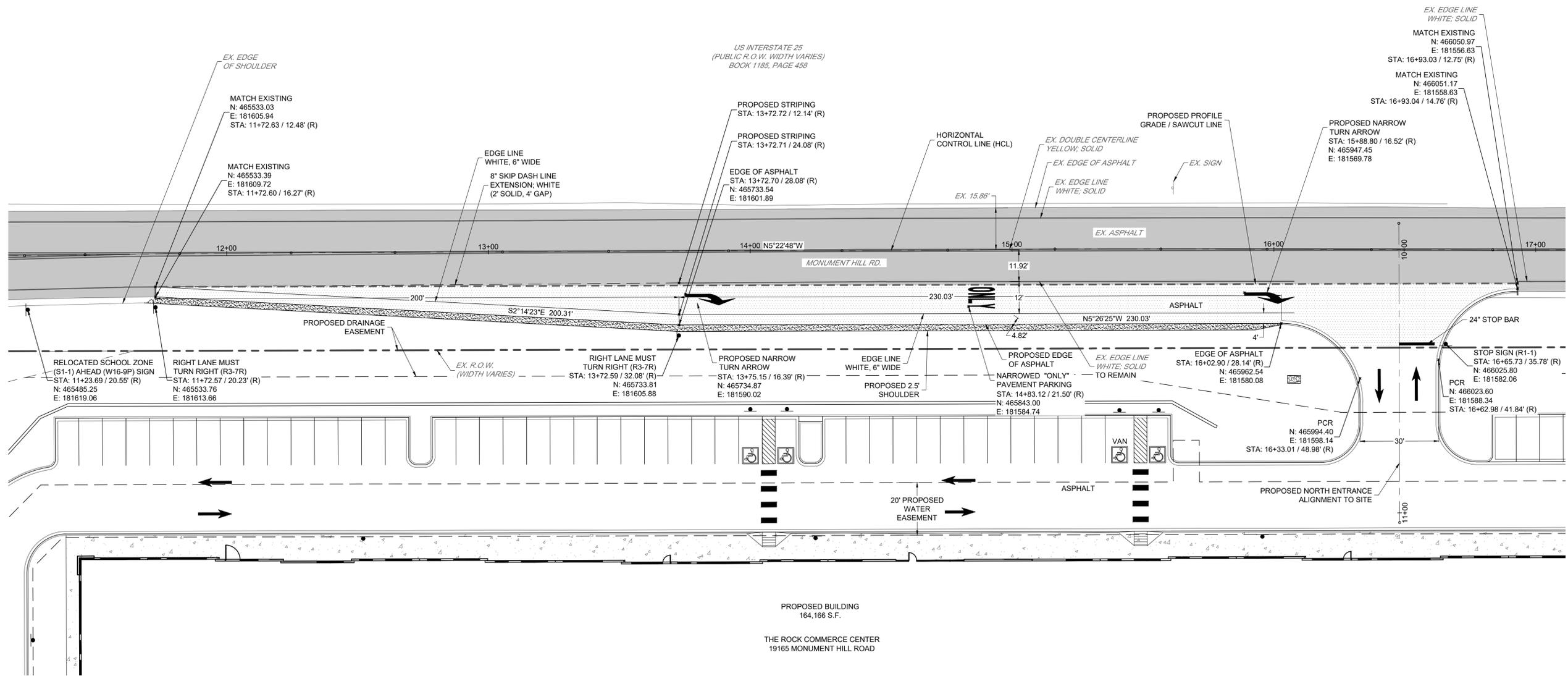


I:\2023\23009 - The Rock Commerce Center\ADD Sheet Sets\CDA\PIP\23009\_Cross Sections.dwg Job: Cross Sections-2, Nov. 20, 2023 - 7:30am csaiz

I:\2023\23009 - The Rock Commerce Center\Sheet Sets\CDs\PIP\23009\_Signage & Striping Plan.dwg tab: Striping & Signage Nov 20, 2023 - 7:31am casaz



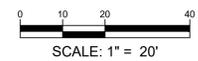
KEYMAP  
SCALE = 1" = 750'



PROPOSED BUILDING  
164,166 S.F.  
THE ROCK COMMERCE CENTER  
19165 MONUMENT HILL ROAD



Know what's below.  
Call before you dig.



**15 YEARS**  
WHERE GREAT PLACES BEGIN

720.283.6783  
REDLAND.COM

• Land Planning  
• Landscape Architecture  
• Civil Engineering  
• Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DODUMENTS**  
SIGNAGE AND STRIPING PLAN

SHEET  
**C8.0**

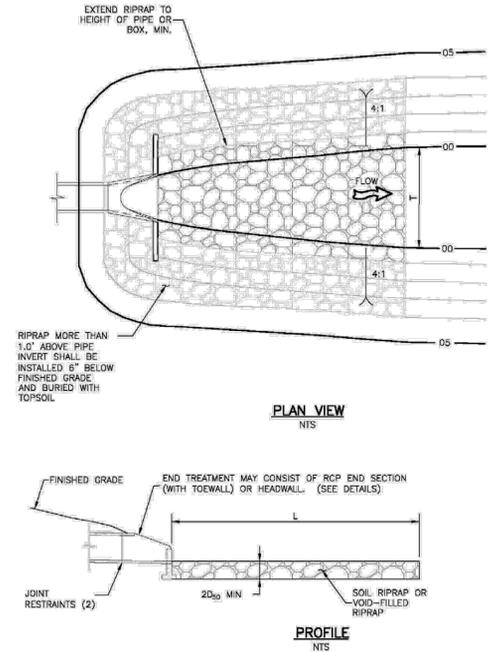
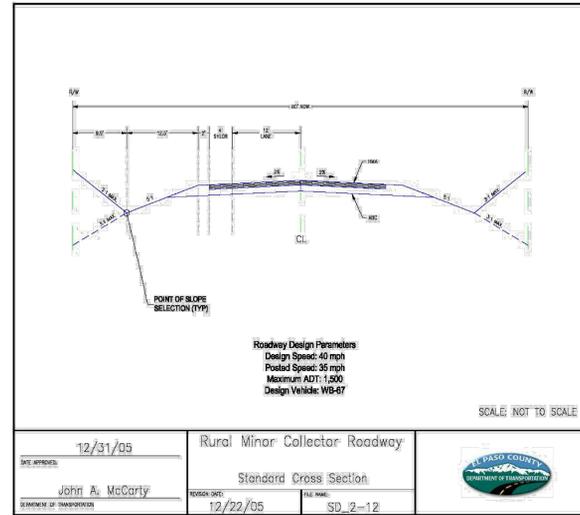
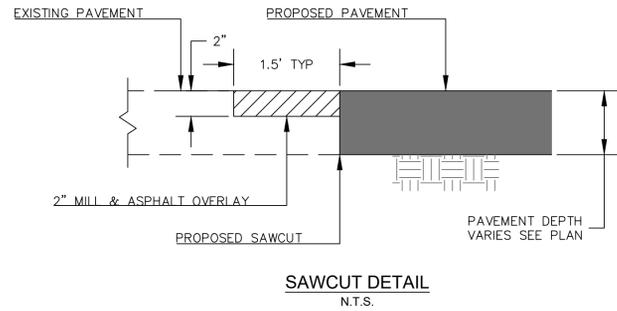
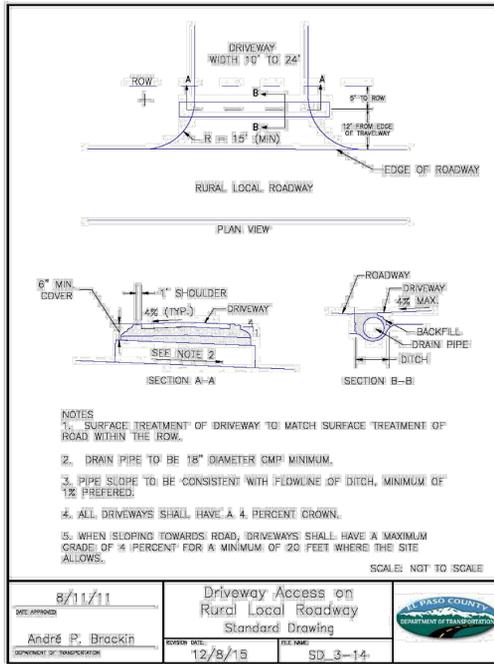


Figure 9-34. Riprap apron detail for culverts in-line with the channel

**GENERAL NOTES**

- DIMENSIONS OF END SECTIONS MAY VARY SLIGHTLY FROM THOSE SHOWN ON THE TABLES DUE TO DIFFERENT MANUFACTURERS' CONFIGURATIONS.
- CONCRETE END SECTIONS SHALL BE FINISHED WITH TONGUE OR GROOVE AS REQUIRED.
- DESIGN LENGTH OF PIPE OR SIDE DRAIN IS BASED ON LENGTH OF END SECTION SHOWN IN TABLE. ANY ADDITIONAL PIPE REQUIRED TO PROVIDE THE DESIGN LENGTH SHALL BE FURNISHED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE PROJECT.
- THE INSIDE CONFIGURATION AND THE JOINT OF CONCRETE END SECTION AND PIPE SHALL MATCH ON THE PLANS.
- END SECTIONS FOR CMP ARCH PIPE SHALL MATCH THE DIMENSIONS OF THE PIPE SHOWN ON THE PLANS.
- GALVANIZED TOE PLATE AS SHOWN IS REQUIRED ON END SECTIONS FOR CORRUGATED STEEL PIPE AND SHALL BE THE SAME THICKNESS AS END SECTIONS. TOE PLATE SHALL BE FIELD-BOLTED TO END SECTION WITH 3/8" IN. GALVANIZED BOLTS, NUTS AND WASHERS.
- GALVANIZED STEEL SHALL CONFORM TO AASHTO M 111, M 218 OR M 232.
- CONCRETE PIPE JOINT FASTENERS, WHERE SHOWN ON PLANS, SHALL BE INSTALLED SO THAT A MINIMUM OF 15 LINEAR FEET OF THE BULLET END OF THE PIPE ARE MECHANICALLY LOCKED TOGETHER. END SECTION LENGTHS WHEN USED, SHALL BE INCLUDED IN THE 15 LF REQUIREMENT.
- CONNECTIONS OF METAL END SECTIONS TO PLASTIC PIPE SHALL BE APPROVED BY THE ENGINEER. PLASTIC END SECTIONS SHALL NOT BE USED.
- THE END SECTION STYLE, EITHER REGULAR OR SAFETY, SHALL BE AS SHOWN ON THE PLANS.
- AT THE OPTION OF THE CONTRACTOR AND APPROVAL OF THE GOOD PROJECT ENGINEER, REINFORCED CONCRETE END SECTIONS MAY BE MADE WITH SYNTHETIC FIBERS INSTEAD OF STEEL FOR PIPES 36 INCHES IN DIAMETER AND SMALLER, AND CONFORM TO AASHTO M 86 AND SUBSECTION 601.03.

**PIPE ARCH**

PIPE DIA. x RISE	THICKNESS	DIMENSIONS					
		A (41°)	B (MAX.)	H (41.5°)	L (42°)	W	T
21 x 15	0.064	7	10	6	23	36	46
24 x 18	0.064	8	12	6	28	42	52
28 x 20	0.064	9	14	6	32	48	58
35 x 24	0.079	10	16	6	39	60	70
42 x 29	0.079	12	18	8	46	75	85
48 x 33	0.109	13	21	9	53	85	103
57 x 38	0.109	18	26	12	63	90	108
64 x 43	0.109	18	30	12	70	102	120
71 x 47	0.109	18	33	12	77	114	132

**FLEXIBLE PIPE ARCH**

**END SECTION AND CONNECTION DETAILS FOR ROUND AND ARCH METAL PIPES**

**REINFORCED CONCRETE CIRCULAR PIPE**

PIPE DIA.	DIMENSIONS			
	A	C	L	E
18	10	48	78	36
24	10	48	78	48
30	14	36	96	60
36	18	36	96	72
42	24	36	96	78
48	28	24	96	84
54	30	36	96	90
60	36	36	96	96
72	42	36	96	108

**STEEL END SECTION FOR CONCRETE CIRCULAR PIPE**

D	Z (MIN)
18 - 24	12
30 AND 36	16
42 AND LARGER	24

**CONCRETE AND METAL END SECTIONS**

STANDARD PLAN NO. M-603-10

Standard Sheet No. 1 of 1

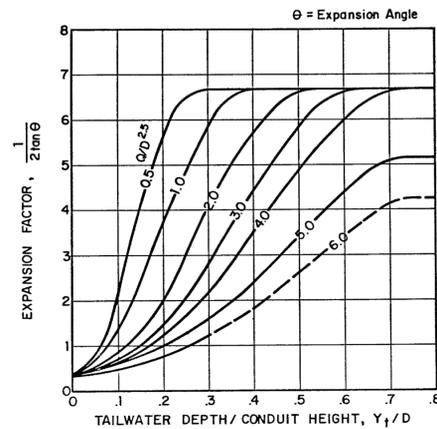


Figure 9-35. Expansion factor for circular conduits

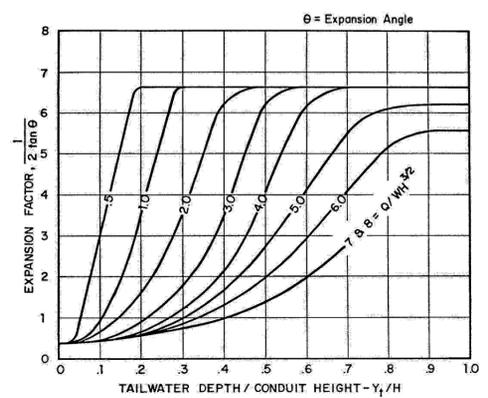


Figure 9-36. Expansion factor for rectangular conduits

**15 Redland YEARS**  
WHERE GREAT PLACES BEGIN

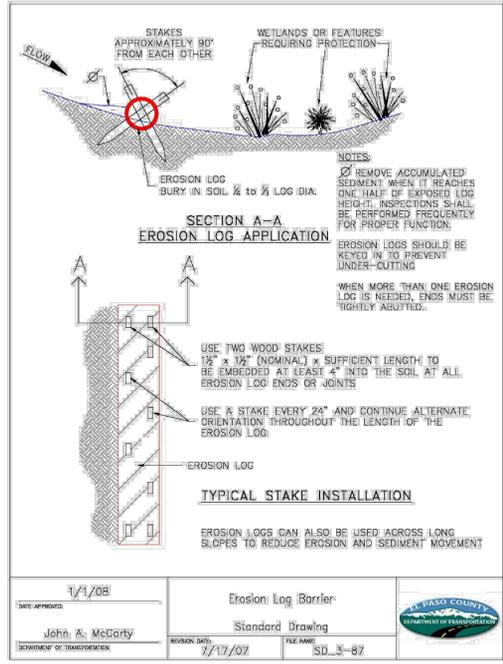
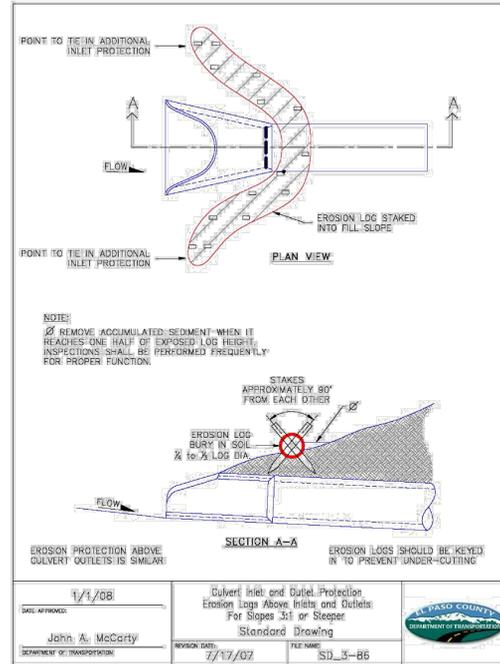
220.283.6783  
REDLAND, CO, USA

• Land Planning  
• Landscape Architecture  
• Civil Engineering  
• Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	DESCRIPTION
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DOCUMENTS**  
SITE DETAILS



**Inlet Protection (IP)**

SC-6

**Description**

Inlet protection consists of permeable barriers installed around an inlet to filter runoff and remove sediment prior to entering a storm drain inlet. Inlet protection can be constructed from rock socks, sediment control logs, silt fence, block and rock socks, or other materials approved by the local jurisdiction. Area inlets can also be protected by over-excavating around the inlet to form a sediment trap.



Photograph IP-1. Inlet protection for a curb opening inlet.

**Appropriate Uses**

Install protection at storm sewer inlets that are operable during construction. Consider the potential for tracked-out sediment or temporary stockpile areas to contribute sediment to inlets when determining which inlets must be protected. This may include inlets in the general proximity of the construction area, not limited to downgradient inlets. Inlet protection is not a stand-alone BMP and should be used in conjunction with other upgradient BMPs.

**Design and Installation**

To function effectively, inlet protection measures must be installed to ensure that flows do not bypass the inlet protection and enter the storm drain without treatment. However, designs must also enable the inlet to function without completely blocking flows into the inlet in a manner that causes localized flooding. When selecting the type of inlet protection, consider factors such as type of inlet (e.g., curb or area, sump or on-grade conditions), traffic, anticipated flows, ability to secure the BMP properly, safety and other site-specific conditions. For example, block and rock socks will be better suited to a curb and gutter along a roadway, as opposed to silt fence or sediment control logs, which cannot be properly secured in a curb and gutter setting, but are effective area inlet protection measures.

Several inlet protection designs are provided in the Design Details. Additionally, a variety of proprietary products are available for inlet protection that may be approved for use by local governments. If proprietary products are used, design details and installation procedures from the manufacturer must be followed. Regardless of the type of inlet protection selected, inlet protection is most effective when combined with other BMPs such as curb socks and check dams. Inlet protection is often the last barrier before runoff enters the storm sewer or receiving water.

Design details with notes are provided for these forms of inlet protection:

- IP-1. Block and Rock Sock Inlet Protection for Sump or On-grade Inlets
- IP-2. Curb (Rock) Socks Upstream of Inlet Protection, On-grade Inlets

Inlet Protection (various forms)	
Erosion Control	No
Sediment Control	Yes
Site/Material Management	No

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-1

**SC-6**

**Inlet Protection (IP)**

- IP-3. Rock Sock Inlet Protection for Sump/Area Inlet
- IP-4. Silt Fence Inlet Protection for Sump/Area Inlet
- IP-5. Over-excavation Inlet Protection
- IP-6. Straw Bale Inlet Protection for Sump/Area Inlet
- CIP-1. Culvert Inlet Protection

Proprietary inlet protection devices should be installed in accordance with manufacturer specifications. More information is provided below on selecting inlet protection for sump and on-grade locations.

**Inlets Located in a Sump**

When applying inlet protection in sump conditions, it is important that the inlet continue to function during larger runoff events. For curb inlets, the maximum height of the protective barrier should be lower than the top of the curb opening to allow overflow into the inlet during larger storms without excessive localized flooding. If the inlet protection height is greater than the curb elevation, particularly if the filter becomes clogged with sediment, runoff will not enter the inlet and may bypass it, possibly causing localized flooding, public safety issues, and downstream erosion and damage from bypassed flows.

Area inlets located in a sump setting can be protected through the use of silt fence, concrete block and rock socks (on paved surfaces), sediment control logs/straw wattles embedded in the adjacent soil and stacked around the area inlet (on pervious surfaces), over-excavating around the inlet, and proprietary products providing equivalent functions.

**Inlets Located on a Slope**

For curb and gutter inlets on paved sloping streets, block and rock sock inlet protection is recommended in conjunction with curb socks in the gutter leading to the inlet. For inlets located along unpaved roads, also see the Check Dam Fact Sheet.

**Maintenance and Removal**

Inspect inlet protection frequently. Inspection and maintenance guidance includes:

- Inspect for tears that can result in sediment directly entering the inlet, as well as result in the contents of the BMP (e.g., gravel) washing into the inlet.
- Check for improper installation resulting in untreated flows bypassing the BMP and directly entering the inlet or bypassing to an unprotected downstream inlet. For example, silt fence that has not been properly trenched around the inlet can result in flows under the silt fence and directly into the inlet.
- Look for displaced BMPs that are no longer protecting the inlet. Displacement may occur following larger storm events that wash away or reposition the inlet protection. Traffic or equipment may also crush or displace the BMP.
- Monitor sediment accumulation upgradient of the inlet protection.

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-2

**Inlet Protection (IP)**

SC-6

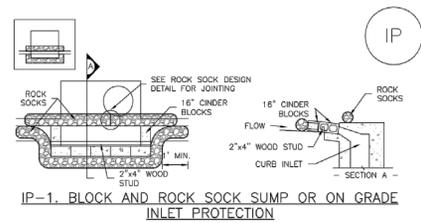
- Remove sediment accumulation from the area upstream of the inlet protection, as needed to maintain BMP effectiveness, typically when it reaches no more than half the storage capacity of the inlet protection. For silt fence, remove sediment when it accumulates to a depth of no more than 6 inches. Remove sediment accumulation from the area upstream of the inlet protection as needed to maintain the functionality of the BMP.

- Proprietary inlet protection devices should be inspected and maintained in accordance with manufacturer specifications. If proprietary inlet insert devices are used, sediment should be removed in a timely manner to prevent devices from breaking and spilling sediment into the storm drain.

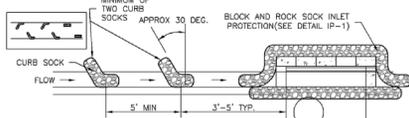
Inlet protection must be removed and properly disposed of when the drainage area for the inlet has reached final stabilization.

SC-6

**Inlet Protection (IP)**



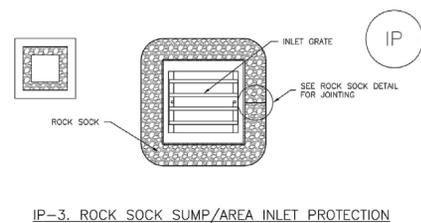
- BLOCK AND CURB SOCK INLET PROTECTION INSTALLATION NOTES**
- SEE ROCK SOCK DESIGN DETAIL FOR INSTALLATION REQUIREMENTS.
  - CONCRETE "CINDER" BLOCKS SHALL BE LAID ON THEIR SIDES AROUND THE INLET IN A SINGLE ROW, ABUTTING ONE ANOTHER WITH THE OPEN END FACING AWAY FROM THE CURB.
  - GRAVEL BAGS SHALL BE PLACED AROUND CONCRETE BLOCKS, CLOSELY ABUTTING ONE ANOTHER AND JOINTED TOGETHER IN ACCORDANCE WITH ROCK SOCK DESIGN DETAIL.



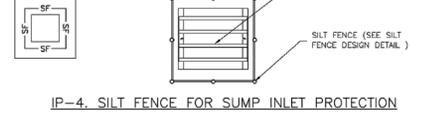
- CURB ROCK SOCK INLET PROTECTION INSTALLATION NOTES**
- SEE ROCK SOCK DESIGN DETAIL FOR INSTALLATION REQUIREMENTS.
  - PLACEMENT OF THE SOCK SHALL BE APPROXIMATELY 30 DEGREES FROM PERPENDICULAR IN THE OPPOSITE DIRECTION OF FLOW.
  - SOCKS ARE TO BE FLUSH WITH THE CURB AND SPACED A MINIMUM OF 5 FEET APART.
  - AT LEAST TWO CURB SOCKS IN SERIES ARE REQUIRED UPSTREAM OF ON-GRADE INLETS.

**Inlet Protection (IP)**

SC-6



- ROCK SOCK SUMP/AREA INLET PROTECTION INSTALLATION NOTES**
- SEE ROCK SOCK DESIGN DETAIL FOR INSTALLATION REQUIREMENTS.
  - STRAW WATTLES/SEDIMENT CONTROL LOGS MAY BE USED IN PLACE OF ROCK SOCKS FOR INLETS IN PERVIOUS AREAS. INSTALL PER SEDIMENT CONTROL LOG DETAIL.



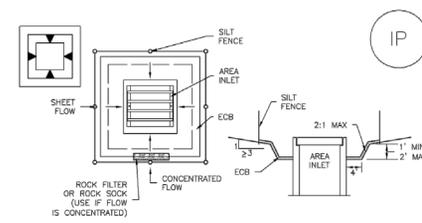
- SILT FENCE INLET PROTECTION INSTALLATION NOTES**
- SEE SILT FENCE DESIGN DETAIL FOR INSTALLATION REQUIREMENTS.
  - POSTS SHALL BE PLACED AT EACH CORNER OF THE INLET AND AROUND THE EDGES AT A MAXIMUM SPACING OF 3 FEET.
  - STRAW WATTLES/SEDIMENT CONTROL LOGS MAY BE USED IN PLACE OF SILT FENCE FOR INLETS IN PERVIOUS AREAS. INSTALL PER SEDIMENT CONTROL LOG DETAIL.

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

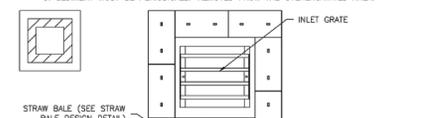
IP-3

SC-6

**Inlet Protection (IP)**



- OVEREXCAVATION INLET PROTECTION INSTALLATION NOTES**
- THIS FORM OF INLET PROTECTION IS PRIMARILY APPLICABLE FOR SITES THAT HAVE NOT YET REACHED FINAL GRADE AND SHOULD BE USED ONLY FOR INLETS WITH A RELATIVELY SMALL CONTRIBUTING DRAINAGE AREA.
  - WHEN USING FOR CONCENTRATED FLOWS, SHAPE BASIN IN 2:1 RATIO WITH LENGTH ORIENTED TOWARDS DIRECTION OF FLOW.
  - SEDIMENT MUST BE PERIODICALLY REMOVED FROM THE OVEREXCAVATED AREA.



- STRAW BALE BARRIER INLET PROTECTION INSTALLATION NOTES**
- SEE STRAW BALE DESIGN DETAIL FOR INSTALLATION REQUIREMENTS.
  - BALES SHALL BE PLACED IN A SINGLE ROW AROUND THE INLET WITH ENDS OF BALES TIGHTLY ABUTTING ONE ANOTHER.

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-5

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-4

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-6

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-5

August 2013 Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

IP-6

**15 Redland YEARS**  
WHERE GREAT PLACES BEGIN  
Land Planning • Landscape Architecture  
Civil Engineering • Construction Management  
720.283.6793  
REDLAND, COLO.

**NOT FOR CONSTRUCTION**

PROJECT NO.	NO.	DATE	NOTES
23009	1	07/28/2023	1ST SUBMITTAL
	2	10/20/2023	2ND SUBMITTAL
	3	11/17/2023	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DOCUMENTS**  
EROSION CONTROL DETAILS

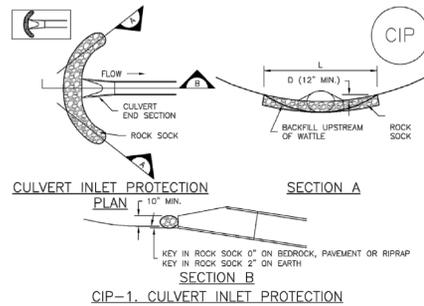
SHEET  
**C9.2**

**Inlet Protection (IP)**

SC-6

SC-6

**Inlet Protection (IP)**



CIP-1. CULVERT INLET PROTECTION

**CULVERT INLET PROTECTION INSTALLATION NOTES**

- SEE PLAN VIEW FOR:
  - LOCATION OF INLET PROTECTION.
  - TYPE OF INLET PROTECTION (IP-1, IP-2, IP-3, IP-4, IP-5, IP-6)
- INLET PROTECTION SHALL BE INSTALLED PROMPTLY AFTER INLET CONSTRUCTION OR PAVING IS COMPLETE (TYPICALLY WITHIN 48 HOURS), IF A RAINFALL/RUNOFF EVENT IS FORECAST. INSTALL INLET PROTECTION PRIOR TO ONSET OF EVENT.
- MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

**INLET PROTECTION MAINTENANCE NOTES**

- INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.
- FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
- WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.
- SEDIMENT ACCUMULATED UPSTREAM OF INLET PROTECTION SHALL BE REMOVED AS NECESSARY TO MAINTAIN BMP EFFECTIVENESS, TYPICALLY WHEN STORAGE VOLUME REACHES 50% OF CAPACITY, A DEPTH OF 6" WHEN SILT FENCE IS USED, OR 1/3 OF THE HEIGHT FOR STRAW BALES.
- INLET PROTECTION IS TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS PERMANENTLY STABILIZED, UNLESS THE LOCAL JURISDICTION APPROVES EARLIER REMOVAL OF INLET PROTECTION IN STREETS.
- WHEN INLET PROTECTION AT AREA INLETS IS REMOVED, THE DISTURBED AREA SHALL BE COVERED WITH TOP SOIL, SEEDED AND MULCHED, OR OTHERWISE STABILIZED IN A MANNER APPROVED BY THE LOCAL JURISDICTION.

(DETAILS ADAPTED FROM TOWN OF PARKER, COLORADO AND CITY OF AURORA, COLORADO, NOT AVAILABLE IN AUTOCAD)

**NOTE:** MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

August 2013 Urban Drainage and Flood Control District IP-7  
Urban Storm Drainage Criteria Manual Volume 3

IP-8 Urban Drainage and Flood Control District  
Urban Storm Drainage Criteria Manual Volume 3 August 2013

**Temporary Outlet Protection (TOP)**

EC-8

**Description**

Outlet protection helps to reduce erosion immediately downstream of a pipe, culvert, slope drain, runoff or other conveyance with concentrated, high-velocity flows. Typical outlet protection consists of riprap or rock aprons at the conveyance outlet.



Photograph TOP-1. Riprap outlet protection.

**Appropriate Uses**

Outlet protection should be used at a conveyance discharges onto a disturbed area where there is potential for accelerated erosion due to concentrated flow. Outlet protection should be provided where the velocity at the culvert outlet exceeds the maximum permissible velocity of the material in the receiving channel.

Note: This Fact Sheet and detail are for temporary outlet protection, outlets that are intended to be used for less than 2 years. For permanent, long-term outlet protection, see the *Major Drainage* chapter of Volume 1.

**Design and Installation**

Design outlet protection to handle runoff from the largest drainage area that may be contributing runoff during construction (the drainage area may change as a result of grading). Key in rock, around the entire perimeter of the apron, to a minimum depth of 6 inches for stability. Extend riprap to the height of the culvert or the normal flow depth of the downstream channel, whichever is less. Additional erosion control measures such as vegetative lining, turf reinforcement mat and/or other channel lining methods may be required downstream of the outlet protection if the channel is susceptible to erosion. See Design Detail OP-1 for additional information.

**Maintenance and Removal**

Inspect apron for damage and displaced rocks. If rocks are missing or significantly displaced, repair or replace as necessary. If rocks are continuously missing or displaced, consider increasing the size of the riprap or deeper keying of the perimeter.

Remove sediment accumulated at the outlet before the outlet protection becomes buried and ineffective. When sediment accumulation is noted, check that upgradient BMPs, including inlet protection, are in effective operating condition.

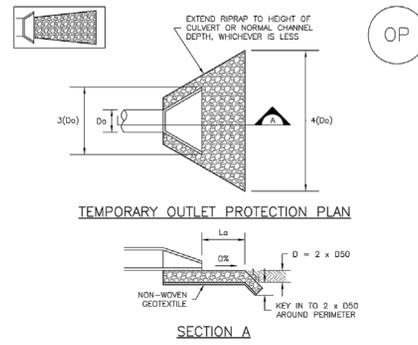
Outlet protection may be removed once the pipe is no longer draining an upstream area, or once the downstream area has been sufficiently stabilized. If the drainage pipe is permanent, outlet protection can be left in place; however, permanent outlet protection should be designed and constructed in accordance with the requirements of the *Major Drainage* chapter of Volume 2.

Outlet Protection	
Erosion Control	Yes
Sediment Control	Moderate
Site/Material Management	No

November 2010 Urban Drainage and Flood Control District TOP-1  
Urban Storm Drainage Criteria Manual Volume 3

EC-8

**Temporary Outlet Protection (TOP)**



TEMPORARY OUTLET PROTECTION PLAN

SECTION A

PIPE DIAMETER, D <sub>p</sub> (INCHES)	DISCHARGE, Q (CFS)	APRON LENGTH, L <sub>a</sub> (FT)	RRIPRAP D50 DIAMETER MIN (INCHES)
8	2.5	5	4
	5	10	6
12	5	10	4
	10	13	6
	10	10	6
18	25	18	9
	30	23	12
	40	26	16
24	30	16	9
	40	26	9
	50	28	12
	60	30	16

OP-1. TEMPORARY OUTLET PROTECTION

TOP-2 Urban Drainage and Flood Control District  
Urban Storm Drainage Criteria Manual Volume 3 November 2010

**Temporary Outlet Protection (TOP)**

EC-8

**TEMPORARY OUTLET PROTECTION INSTALLATION NOTES**

- SEE PLAN VIEW FOR:
    - LOCATION OF OUTLET PROTECTION.
    - DIMENSIONS OF OUTLET PROTECTION.
  - DETAIL IS INTENDED FOR PIPES WITH SLOPE  $\leq$  10% ADDITIONAL EVALUATION OF RRIPRAP SIZES AND OUTLET PROTECTION DIMENSIONS REQUIRED FOR STEEPER SLOPES.
  - TEMPORARY OUTLET PROTECTION INFORMATION IS FOR OUTLETS INTENDED TO BE UTILIZED LESS THAN 2 YEARS.
- TEMPORARY OUTLET PROTECTION INSPECTION AND MAINTENANCE NOTES**
- INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.
  - FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
  - WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.
- (DETAILS ADAPTED FROM AURORA, COLORADO AND PREVIOUS VERSION OF VOLUME 3, NOT AVAILABLE IN AUTOCAD)

November 2010 Urban Drainage and Flood Control District TOP-3  
Urban Storm Drainage Criteria Manual Volume 3

**Rock Sock (RS)**

SC-5

SC-5

**Rock Sock (RS)**

**Rock Sock (RS)**

SC-5

**Description**

A rock sock is constructed of gravel that has been wrapped by wire mesh or a geotextile to form an elongated cylindrical filter. Rock socks are typically used either as a perimeter control or as part of inlet protection. When placed at angles in the curb line, rock socks are typically referred to as curb socks. Rock socks are intended to trap sediment from stormwater runoff that flows onto roadways as a result of construction activities.



Photograph RS-1. Rock socks placed at regular intervals in a curb line can help reduce sediment loading to storm sewer inlets. Rock socks can also be used as perimeter controls.

**Appropriate Uses**

Rock socks can be used at the perimeter of a disturbed area to control localized sediment loading. A benefit of rock socks as opposed to other perimeter controls is that they do not have to be trenched or staked into the ground; therefore, they are often used on roadway construction projects where paved surfaces are present.

Use rock socks in inlet protection applications when the construction of a roadway is substantially complete and the roadway has been directly connected to a receiving storm system.

**Design and Installation**

When rock socks are used as perimeter controls, the maximum recommended tributary drainage area per 100 lineal feet of rock socks is approximately 0.25 acres with disturbed slope length of up to 150 feet and a tributary slope gradient no steeper than 3:1. A rock sock design detail and notes are provided in Detail RS-1. Also see the Inlet Protection Fact Sheet for design and installation guidance when rock socks are used for inlet protection and in the curb line.

When placed in the gutter adjacent to a curb, rock socks should protrude no more than two feet from the curb in order for traffic to pass safely. If located in a high traffic area, place construction markers to alert drivers and street maintenance workers of their presence.

**Maintenance and Removal**

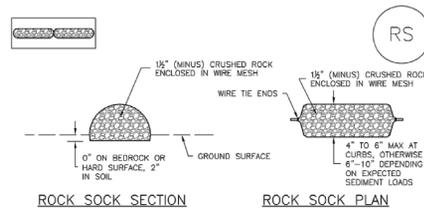
Rock socks are susceptible to displacement and breaking due to vehicle traffic. Inspect rock socks for damage and repair or replace as necessary. Remove sediment by sweeping or vacuuming as needed to maintain the functionality of the BMP, typically when sediment has accumulated behind the rock sock to one-half of the sock's height.

Rock Sock	
Erosion Control	No
Sediment Control	Yes
Site/Material Management	No

November 2010 Urban Drainage and Flood Control District RS-1  
Urban Storm Drainage Criteria Manual Volume 3

SC-5

**Rock Sock (RS)**



ROCK SOCK SECTION

ROCK SOCK PLAN

ANY GAP AT JOINT SHALL BE FILLED WITH AN ADEQUATE AMOUNT OF 1/2" (MINUS) CRUSHED ROCK AND WRAPPED WITH ADDITIONAL WIRE MESH SECURED TO ENDS OF ROCK REINFORCED SOCK, AS AN ALTERNATIVE TO FILLING JOINTS BETWEEN ADJOINING ROCK SOCKS WITH CRUSHED ROCK AND ADDITIONAL WIRE WRAPPING, ROCK SOCKS CAN BE OVERLAPPED (TYPICALLY 12-INCH OVERLAP) TO AVOID GAPS.



ROCK SOCK JOINTING

SIEVE SIZE	MASS PERCENT PASSING SQUARE MESH SIEVES
NO. 4	100
2"	90 - 100
1 1/2"	20 - 55
3/4"	0 - 15
3/8"	0 - 5

**ROCK SOCK INSTALLATION NOTES**

- SEE PLAN VIEW FOR:
  - LOCATION(S) OF ROCK SOCKS.
- CRUSHED ROCK SHALL BE 1/2" (MINUS) IN SIZE WITH A FRACTURED FACE (ALL SIDES) AND SHALL COMPLY WITH GRADATION SHOWN ON THIS SHEET (1/2" MINUS).
- WIRE MESH SHALL BE FABRICATED OF 10 GAGE POULTRY MESH, OR EQUIVALENT, WITH A MAXIMUM OPENING OF 1/2", RECOMMENDED MINIMUM ROLL WIDTH OF 48"
- WIRE MESH SHALL BE SECURED USING "HOG RINGS" OR WIRE TIES AT 6" CENTERS ALONG ALL JOINTS AND AT 2' CENTERS ON ENDS OF SOCKS.
- SOME MUNICIPALITIES MAY ALLOW THE USE OF FILTER FABRIC AS AN ALTERNATIVE TO WIRE MESH FOR THE ROCK ENCLASURE.

RS-1. ROCK SOCK PERIMETER CONTROL

RS-2 Urban Drainage and Flood Control District  
Urban Storm Drainage Criteria Manual Volume 3 November 2010

**Street Sweeping and Cleaning**

S-11

S-11

**Street Sweeping and Cleaning**

**Description**

Street sweeping uses mechanical pavement cleaning practices to reduce sediment, litter and other debris washed into storm sewers by runoff. This can reduce pollutant loading to receiving waters and in some cases reduce clogging of storm sewers and prolong the life of infiltration oriented BMPs and reduce clogging of outlet structures in detention BMPs.



Photograph SSC-1. Monthly street sweeping from April through November removed nearly 40,690 cubic yards of sediment/debris from Denver streets in 2009. Photo courtesy of Denver Public Works.

Different designs are available with typical sweepers categorized as a broom and conveyor belt sweeper, wet or dry vacuum-assisted sweepers, and regenerative-air sweepers. The effectiveness of street sweeping is dependent upon particle loadings in the area being swept, street texture, moisture conditions, parked car management, equipment operating conditions and frequency of cleaning (Pitt et al. 2004).

**Appropriate Uses**

Street sweeping is an appropriate technique in urban areas where sediment and litter accumulation on streets is of concern for aesthetic, sanitary, water quality, and air quality reasons. From a pollutant loading perspective, street cleaning equipment can be most effective in areas where the surface to be cleaned is the major source of contaminants. These areas include freeways, large commercial parking lots, and paved storage areas (Pitt et al. 2004). Where significant sediment accumulation occurs on pervious surfaces tributary to infiltration BMPs, street sweeping may help to reduce clogging of infiltration media. In areas where construction activity is occurring, street sweeping should occur as part of construction site stormwater management plans. Vacuuming of permeable pavement systems is also considered a basic routine maintenance practice to maintain the BMP in effective operating condition. See the maintenance chapter for more information on permeable pavement systems. Not all sweepers are appropriate for this application.

**Practice Guidelines<sup>1</sup>**

- Post street sweeping schedules with signs and on local government websites so that cars are not parked on the street during designated sweeping days.
- Sweeping frequency is dependent on local government budget, staffing, and equipment availability, but monthly sweeping during non-winter months is a common approach in the metro Denver urban

<sup>1</sup> Practice guidelines adapted from CASQA (2003) *California Stormwater BMP Handbook*, Practice SC-70 Road and Street Maintenance.

November 2010 Urban Drainage and Flood Control District SWC-1  
Urban Storm Drainage Criteria Manual Volume 3

**Changes in Street Sweeper Technology** (Source: Center for Watershed Protection 2002)

- Consider increasing sweeping frequency based on factors such as traffic volume, land use, field observations of sediment and trash accumulation, proximity to watercourses, etc. For example:
  - Increase the sweeping frequency for streets with high pollutant loadings, especially in high traffic and industrial areas.
  - Conduct street sweeping prior to wetter seasons to remove accumulated sediments.
  - Increase the sweeping frequency for streets in special problem areas such as special events, high litter or erosion zones.
- Perform street cleaning during dry weather if possible.
- Avoid wet cleaning the street; instead, utilize dry methods where possible.
- Maintain cleaning equipment in good working condition and purchase replacement equipment as needed. Old sweepers should be replaced with more technologically advanced sweepers (preferably regenerative air sweepers) that maximize pollutant removal.
- Operate sweepers at manufacturer recommended optimal speed levels to increase effectiveness.
- Regularly inspect vehicles and equipment for leaks and repair promptly.
- Keep accurate logs of the number of curb-miles swept and the amount of waste collected.
- Dispose of street sweeping debris and dirt at a landfill.
- Do not store swept material along the side of the street or near a storm drain inlet.

**At one time, street sweepers were thought to have great potential to remove stormwater pollutants from urban street surfaces and were widely touted as a stormwater treatment practice in many communities. Street sweeping gradually fell out of favor, largely as a result of performance monitoring conducted as part of the National Urban Runoff Program (NURP). These studies generally concluded that street sweepers were not very effective in reducing pollutant loads (USEPA, 1983). The primary reason for the mediocre performance was that mechanical sweepers of that era were unable to pick up fine-grained sediment particles that carry a substantial portion of the stormwater pollutant load. In addition, the performance of sweepers is constrained by that portion of a street's stormwater pollutant load delivered from outside street pavements (e.g., pollutants that wash onto the street from adjacent areas or are directly deposited on the street by rainfall). Street sweeping technology, however, has evolved considerably since the days of the NURP testing. Today, communities have a choice in three basic sweeping technologies to clean their urban streets: traditional mechanical sweepers that utilize a broom and conveyor belt, vacuum-assisted sweepers, and regenerative-air sweepers (those that blast air onto the pavement to loosen sediment particles and vacuum them into a hopper).**

For more information, see [http://www.cwp.org/Resource\\_Library/Center\\_Docs/PWP/ELC\\_PWP121.pdf](http://www.cwp.org/Resource_Library/Center_Docs/PWP/ELC_PWP121.pdf)

SWC-2 Urban Drainage and Flood Control District  
Urban Storm Drainage Criteria Manual Volume 3 November 2010

**15 Redland YEARS** WHERE GREAT PLACES BEGIN

**NOT FOR CONSTRUCTION**

PROJECT NO.	NO.	DATE	NO.	NOTES
07282023	1			1ST SUBMITTAL
10202023	2			2ND SUBMITTAL
11172023	3			3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
PUBLIC IMPROVEMENTS PLAN  
**CONSTRUCTION DOCUMENTS**  
EROSION CONTROL DETAILS

SHEET

C9.3

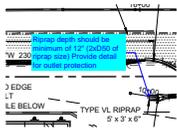
# V3\_Public Improvement Plan Comments.pdf Markup Summary

CDurham (5)



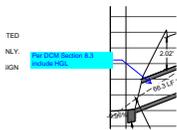
**Subject:** Callout  
**Page Label:** [4] C3.0 HORIZONTAL CONTROL PLAN  
**Author:** CDurham  
**Date:** 12/5/2023 9:26:17 AM  
**Color:** ■

Riprap depth should be minimum of 12" (2xD50 of riprap size)



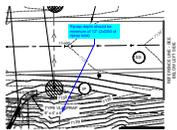
**Subject:** Callout  
**Page Label:** [5] C4.0 PLAN AND PROFILE  
**Author:** CDurham  
**Date:** 12/5/2023 4:20:55 PM  
**Color:** ■

Riprap depth should be minimum of 12" (2xD50 of riprap size) Provide detail for outlet protection



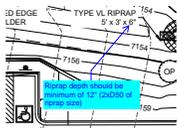
**Subject:** Callout  
**Page Label:** [5] C4.0 PLAN AND PROFILE  
**Author:** CDurham  
**Date:** 12/5/2023 10:53:03 AM  
**Color:** ■

Per DCM Section 8.3 include HGL



**Subject:** Callout  
**Page Label:** [7] C6.0 EROSION CONTROL PLAN  
**Author:** CDurham  
**Date:** 12/5/2023 10:54:12 AM  
**Color:** ■

Riprap depth should be minimum of 12" (2xD50 of riprap size)



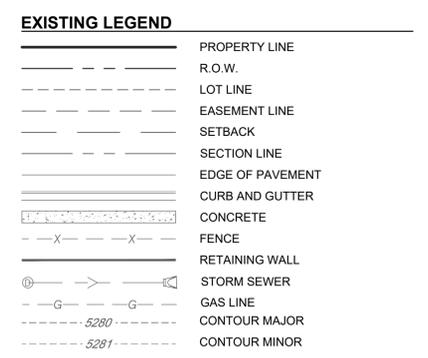
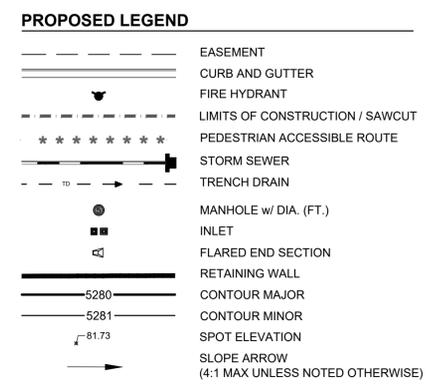
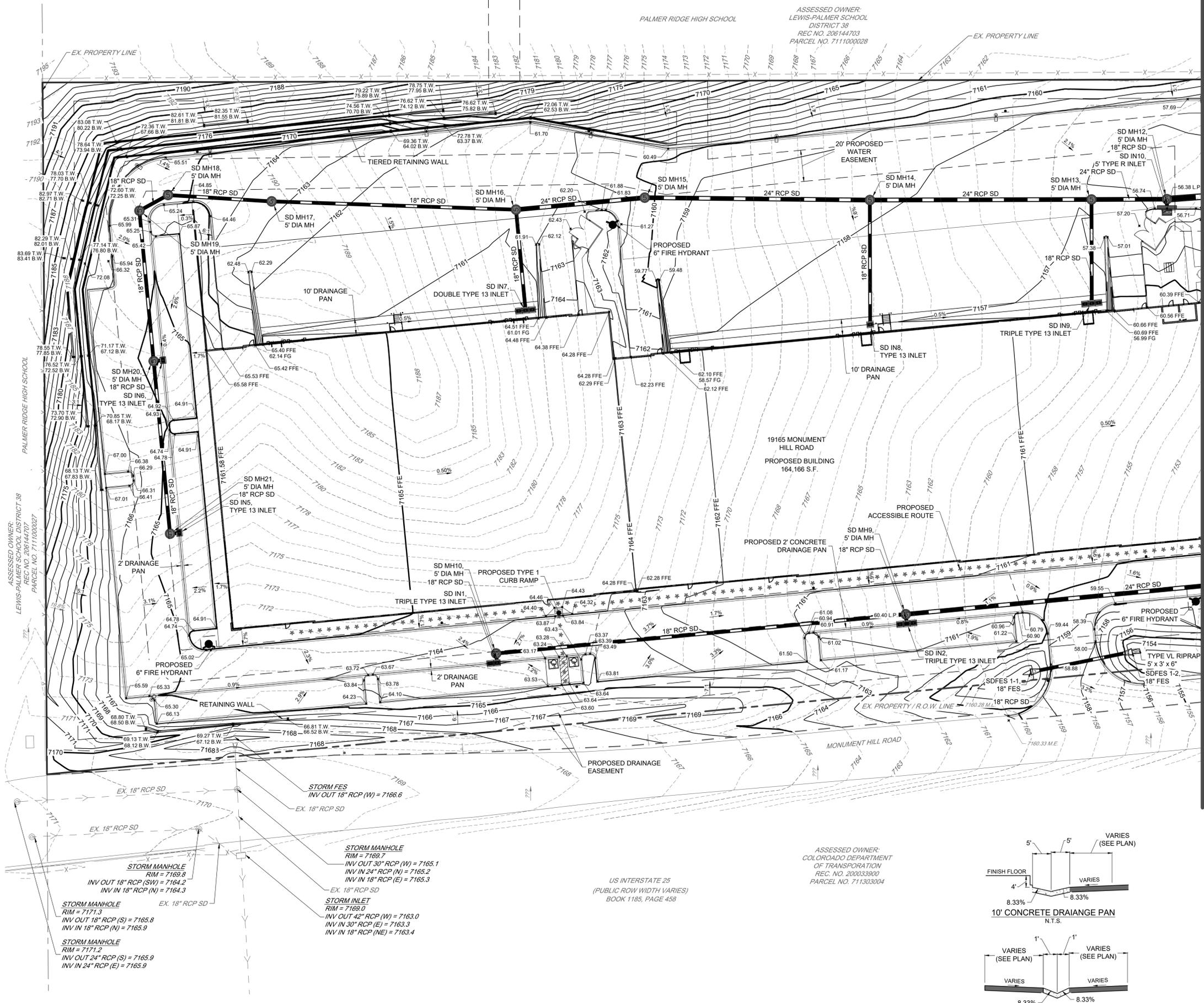
**Subject:** Callout  
**Page Label:** [7] C6.0 EROSION CONTROL PLAN  
**Author:** CDurham  
**Date:** 12/5/2023 10:54:35 AM  
**Color:** ■

Riprap depth should be minimum of 12" (2xD50 of riprap size)



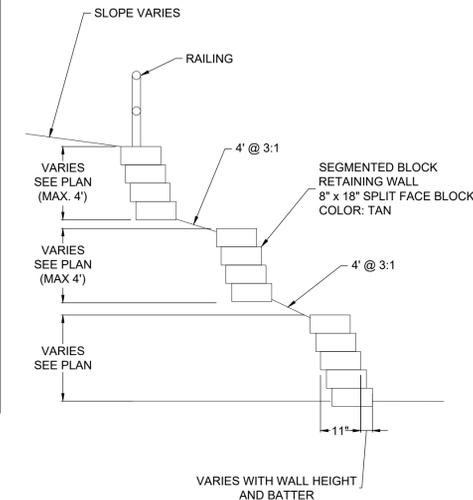


I:\2023\23009 - The Rock Commerce Center\CAADD\Sheet Sets\CECC\The Rock\23009\_Grading Plan.dwg Lab. 5 OF 23 GRADING PLAN Nov 20, 2023 - 7:34am ccsz

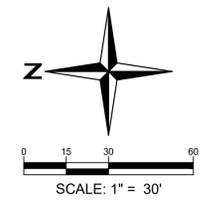
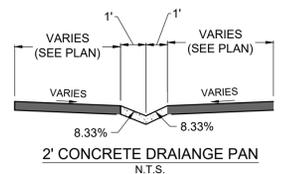
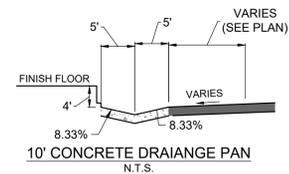


- NOTE:
- THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.
  - REGIONAL BUILDING DEPARTMENT PERMIT REQUIRED FOR ALL RETAINING WALLS GREATER THAN OR EQUAL TO 4 FT IN HEIGHT.
  - SEE SITE DEVELOPMENT PLAN FOR SCREENING WALL DETAILS BY ARCH.
  - NO BATCH PLANTS WILL BE UTILIZED ONSITE.

MATCHLINE - SEE SHEET NO. EC2.2



NOTE: RETAINING WALL WILL REQUIRE A SEPARATE BUILDING PERMIT



**15 Redland**  
WHERE GREAT PLACES BEGIN  
YEARS  
720.283.6793  
REDLAND, CO  
Landscape Architecture  
Civil Engineering  
Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL		
	10/20/2023	2	2ND SUBMITTAL		
	11/17/2023	3	3RD SUBMITTAL		

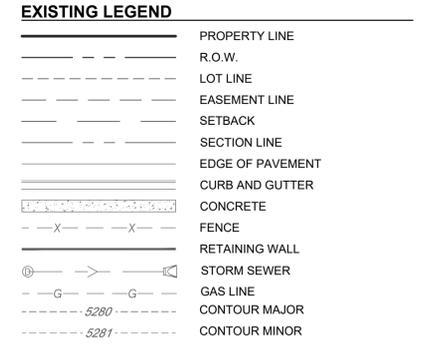
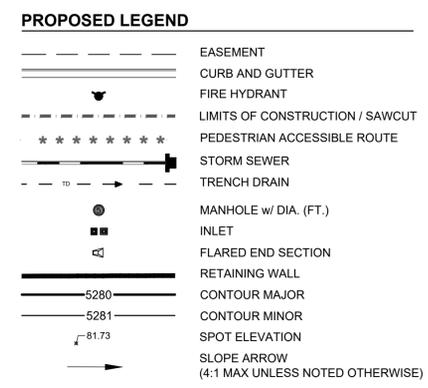
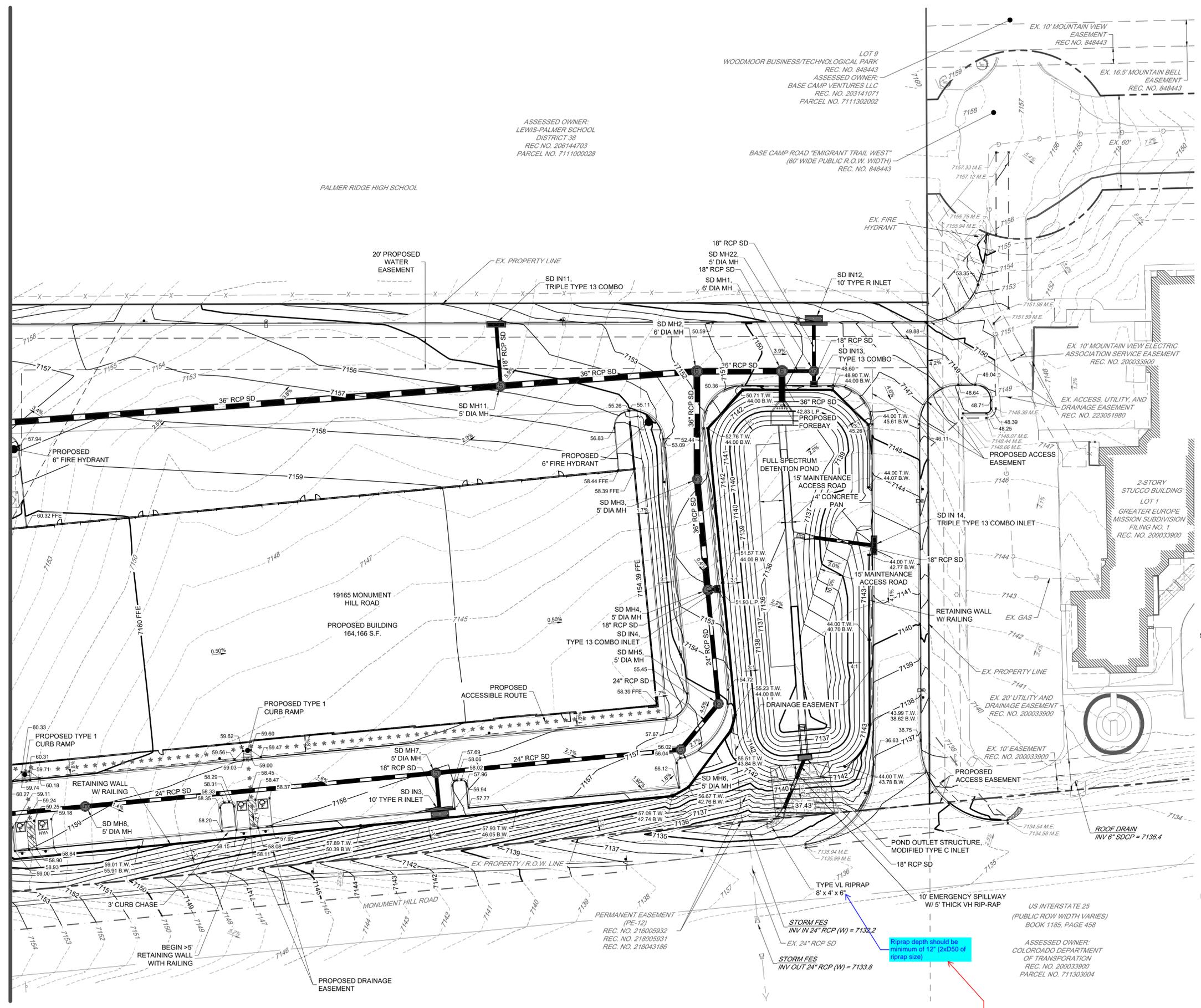
**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
GRADING PLAN

SHEET  
**EC2.1**

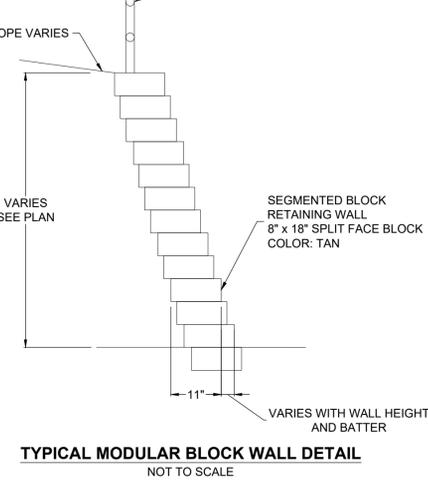
PCD FILE NO. PPR2329

I:\2023\23009 - The Rock Commerce Center\CADD\Sheet Sets\GCC\The Rock\23009\_Grading Plan.dwg Lab: 6 OF 22 GRADING PLAN Nov 20, 2023 - 7:35am ccsz

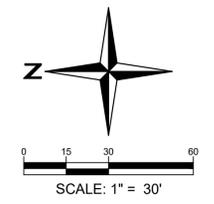
MATCHLINE - SEE SHEET NO. EC2.1



- NOTE:
1. THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATION AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OF GUIDELINES ENACTED OF PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.
  2. REGIONAL BUILDING DEPARTMENT PERMIT REQUIRED FOR ALL RETAINING WALLS GREATER THAN OR EQUAL TO 4 FT IN HEIGHT.
  3. SEE SITE DEVELOPMENT PLAN FOR SCREENING WALL DETAILS BY ARCH.
  4. NO BATCH PLANTS WILL BE UTILIZED ONSITE.



NOTE: RETAINING WALL WILL REQUIRE A SEPARATE BUILDING PERMIT



PCD FILE NO. PPR2329

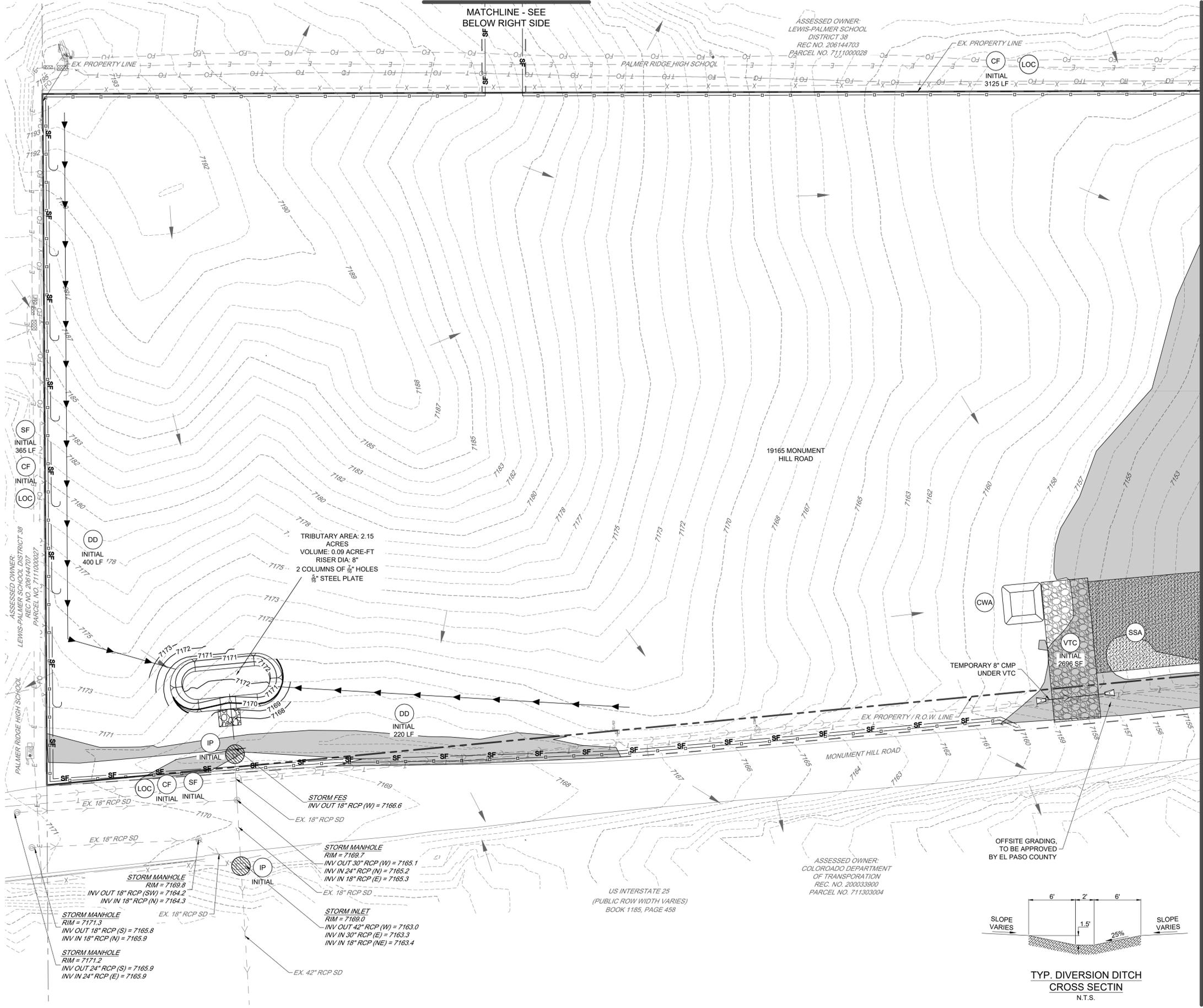
**15 Redland**  
 WHERE GREAT PLACES BEGIN  
 YEARS  
 720.283.6793  
 REDLAND, CO  
 • Land Planning  
 • Landscape Architecture  
 • Civil Engineering  
 • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
 GRADING PLAN

I:\2023\23009 - The Rock Commerce Center\Sheet Sets\CECC\The Rock\23009\_Initial Erosion Control Plan.dwg tab: 7 OF 24 INITIAL EROSION CONTROL PLAN Nov. 20, 2023 - 7:35am csalz

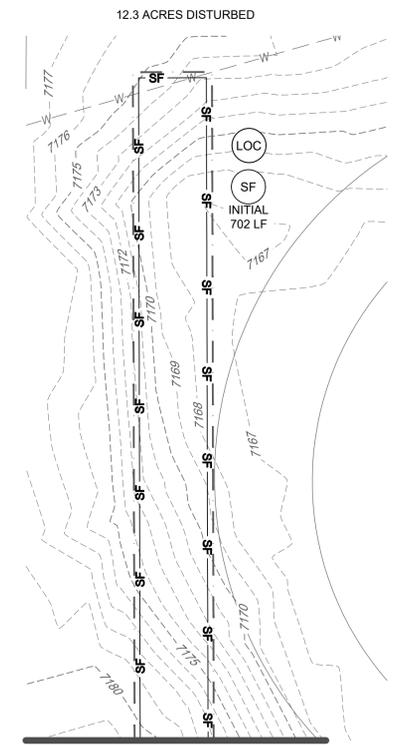


MATCHLINE - SEE BELOW RIGHT SIDE

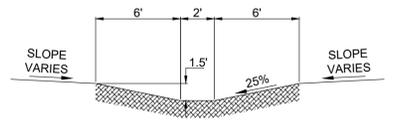
**LEGEND**

- CWA CONCRETE WASHOUT AREA
- CF CONSTRUCTION FENCE
- DD DIVERSION DITCH
- IP INLET PROTECTION
- OP OUTLET PROTECTION
- SB SEDIMENT BASIN
- SF SILT FENCE
- SCL SEDIMENT CONTROL LOG
- SSA STABILIZED STAGING AREA
- VTC VEHICLE TRACKING CONTROL
- ECB EROSION CONTROL BLANKET
- LOC LIMITS OF CONSTRUCTION
- ST SEDIMENT TRAP
- FLOW ARROW
- CS CURB SOCK
- SM SEEDING AND MULCHING
- REMOVE INDICATED BMP
- AREA OF CUT
- AREA OF FILL

MATCHLINE - SEE SHEET NO. EC3.2



MATCHLINE - SEE ABOVE EAST SIDE OF SITE



TYP. DIVERSION DITCH CROSS SECTION  
N.T.S.



SCALE: 1" = 30'

**15 Redland**  
YEARS WHERE GREAT PLACES BEGIN  
720.283.6793  
REDLAND, CO, USA  
• Land Planning • Landscape Architecture  
• Civil Engineering • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
INITIAL EROSION CONTROL PLAN

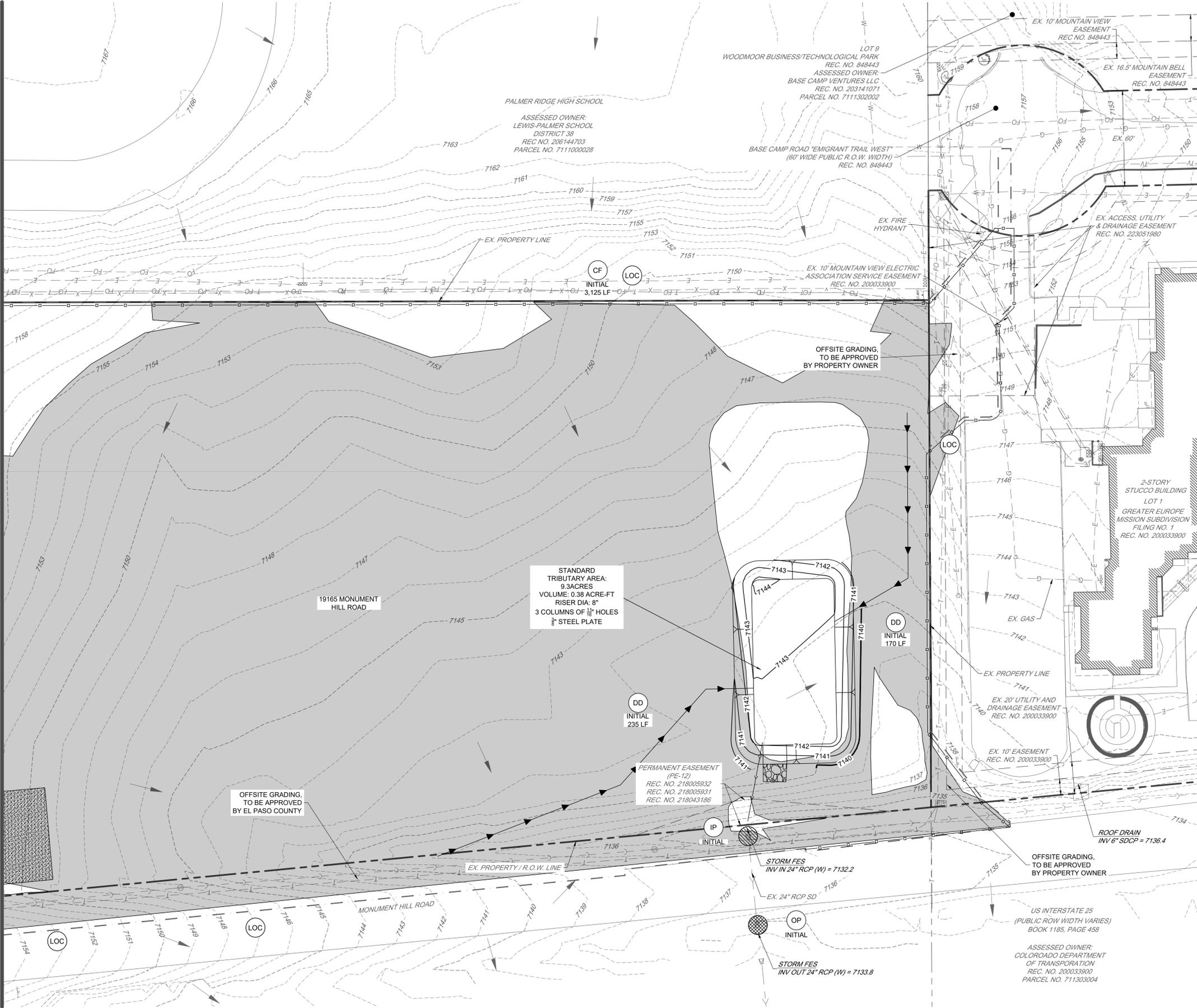
SHEET

EC3.1

PCD FILE NO. PPR2329

I:\2023\23009 - The Rock Commerce Center\CADD\Sheet Sets\GEC\The Rock\23009\_Initial Erosion Control Plan.dwg tab: 8 OF 24 INITIAL EROSION CONTROL PLAN Nov. 20, 2023 - 7:35am csalz

MATCHLINE - SEE SHEET NO. EC3.1



### LEGEND

	(CWA)	CONCRETE WASHOUT AREA
	(CF)	CONSTRUCTION FENCE
	(DD)	DIVERSION DITCH
	(IP)	INLET PROTECTION
	(OP)	OUTLET PROTECTION
	(SB)	SEDIMENT BASIN
	(SF)	SILT FENCE
	(SCL)	SEDIMENT CONTROL LOG
	(SSA)	STABILIZED STAGING AREA
	(VTC)	VEHICLE TRACKING CONTROL
	(ECB)	EROSION CONTROL BLANKET
	(LOC)	LIMITS OF CONSTRUCTION
	(ST)	SEDIMENT TRAP
		FLOW ARROW
	(CS)	CURB SOCK
	(SM)	SEEDING AND MULCHING
	(X)	REMOVE INDICATED BMP
		AREA OF CUT
		AREA OF FILL
		12.3 ACRES DISTURBED

**TYP. DIVERSION DITCH CROSS SECTION**  
N.T.S.

**15 Redland**  
YEARS WHERE GREAT PLACES BEGIN

720.283.6793  
REDLAND.CO.VA

• Land Planning  
• Landscape Architecture  
• Civil Engineering  
• Construction Management

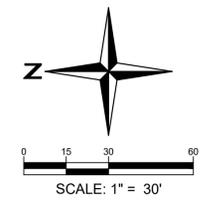
**NOT FOR CONSTRUCTION**

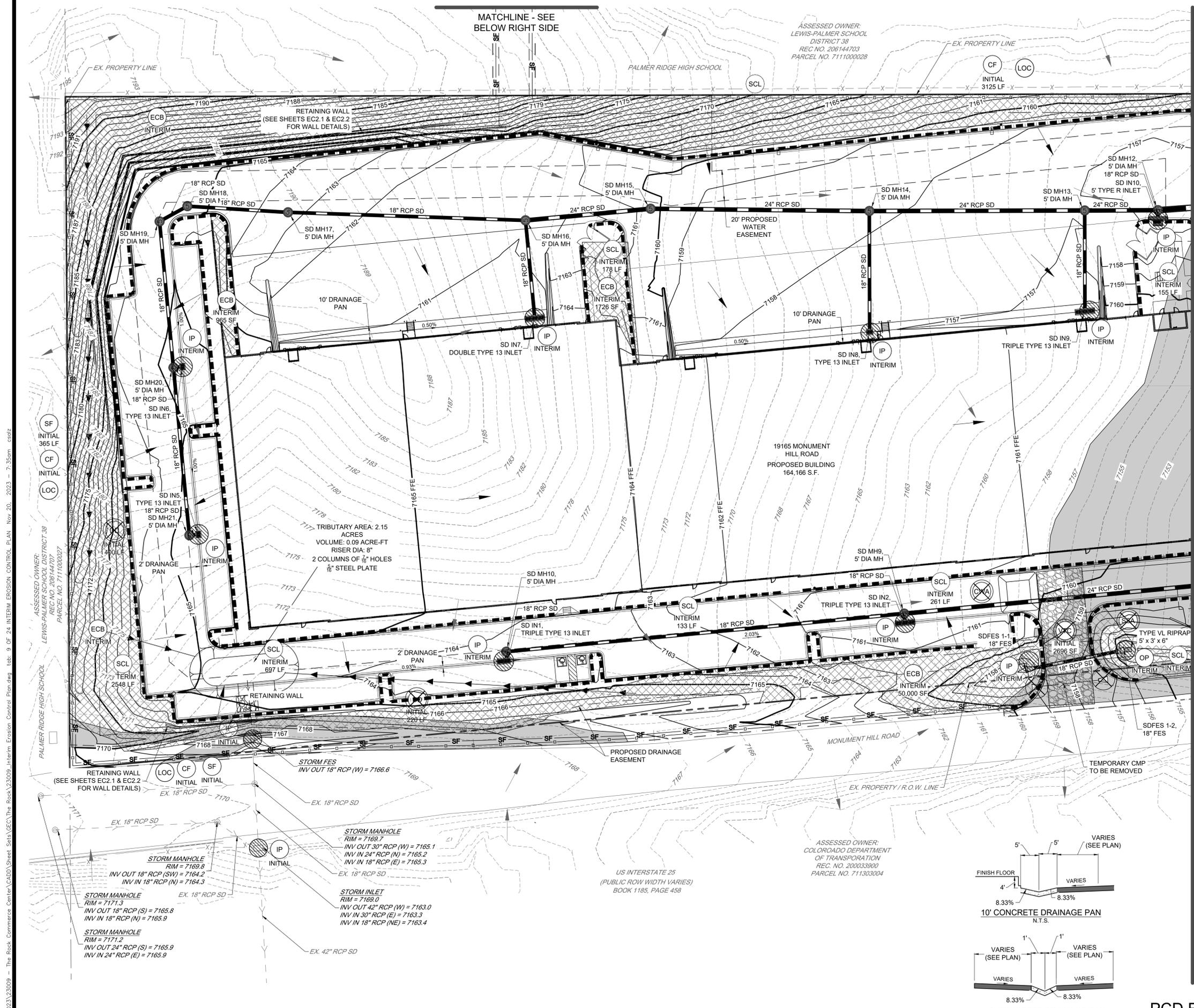
PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
INITIAL EROSION CONTROL PLAN

SHEET  
**EC3.2**

PCD FILE NO. PPR2329

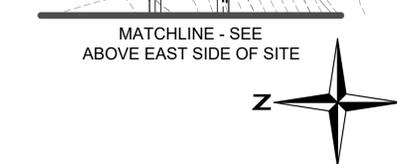
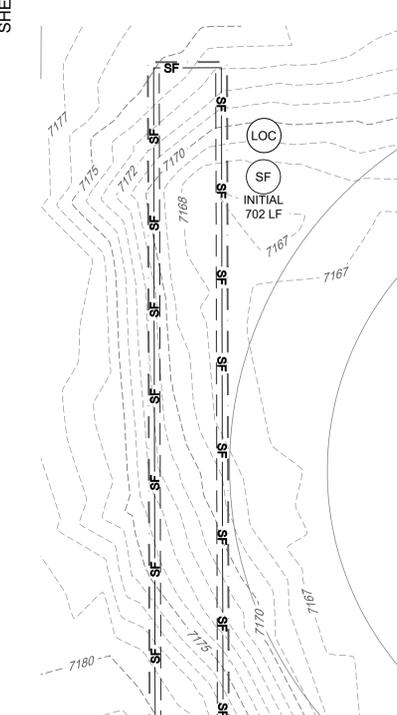




**LEGEND**

- CWA CONCRETE WASHOUT AREA
- CF CONSTRUCTION FENCE
- DD DIVERSION DITCH
- IP INLET PROTECTION
- OP OUTLET PROTECTION
- SB SEDIMENT BASIN
- SF SILT FENCE
- SCL SEDIMENT CONTROL LOG
- SSA STABILIZED STAGING AREA
- VTC VEHICLE TRACKING CONTROL
- ECB EROSION CONTROL BLANKET
- LOC LIMITS OF CONSTRUCTION
- ST SEDIMENT TRAP
- FLOW ARROW
- CS CURB SOCK
- SM SEEDING AND MULCHING
- REMOVE INDICATED BMP
- AREA OF CUT
- AREA OF FILL

MATCHLINE - SEE SHEET NO. EC3.4



PCD FILE NO. PPR2329

**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 LANDSCAPE ARCHITECTURE  
 CIVIL ENGINEERING  
 CONSTRUCTION MANAGEMENT

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

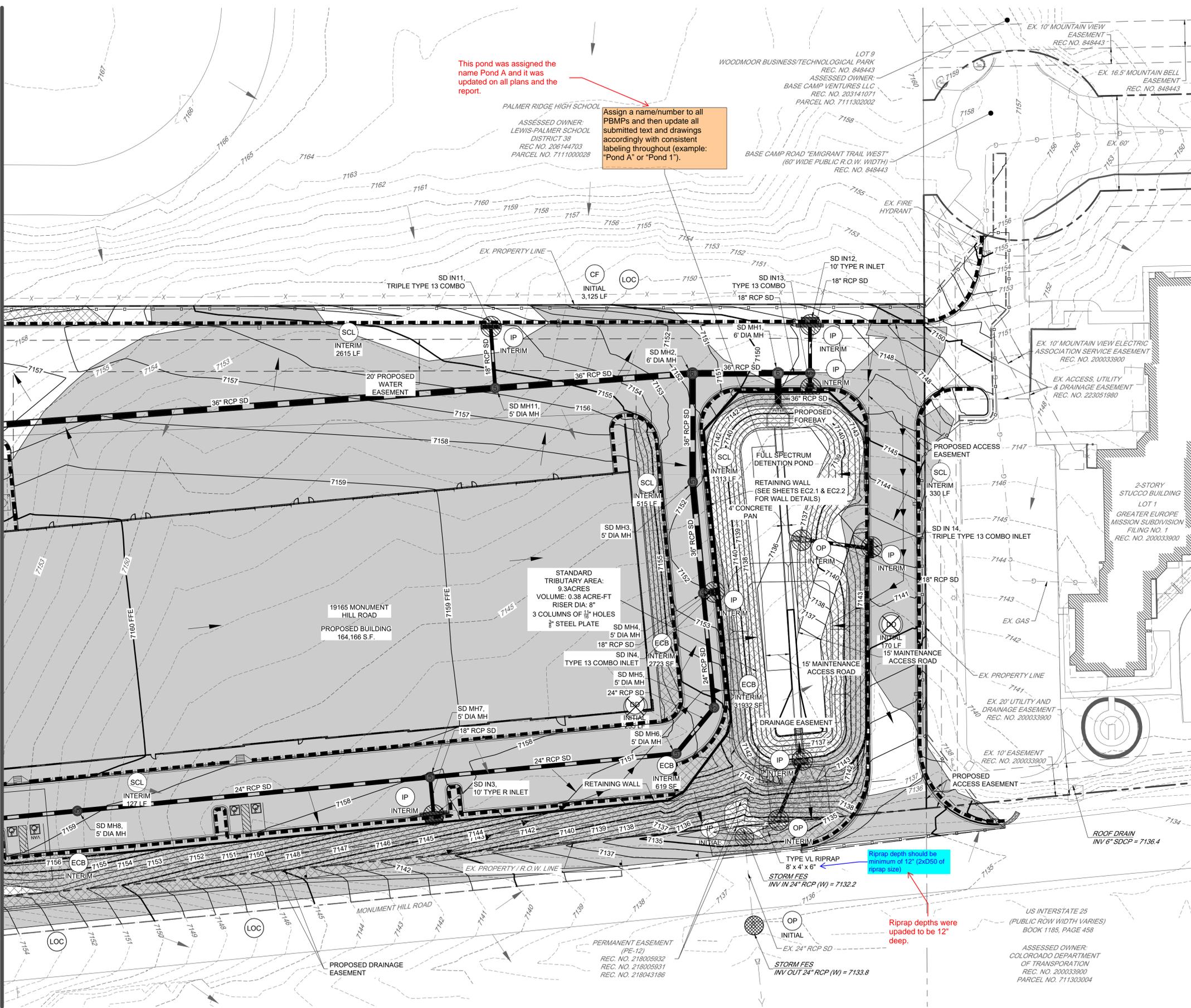
**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
 INTERIM EROSION CONTROL PLAN

SHEET  
**EC3.3**

I:\2023\23009 - The Rock Commerce Center\CAD\Sheet Sets\GECC\The Rock\23009\_Interim Erosion Control Plan.dwg Tab: 9 OF 24 INTERIM EROSION CONTROL PLAN Nov 20, 2023 - 7:35am csolz

I:\2023\23009 - The Rock Commerce Center\CADD\Sheet Sets\GECC\The Rock\23009\_Interim Erosion Control Plan.dwg Tab: 10 OF 24 INTERIM EROSION CONTROL PLAN Nov 20, 2023 - 7:36am caabz

MATCHLINE - SEE SHEET NO. EC3.3



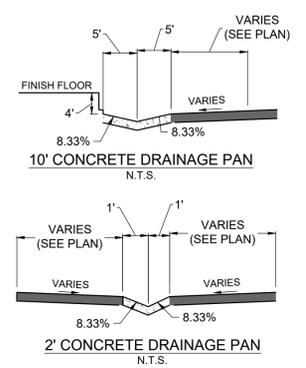
This pond was assigned the name Pond A and it was updated on all plans and the report.

Assign a name/number to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling throughout (example: "Pond A" or "Pond 1").

LEGEND

- CWA CONCRETE WASHOUT AREA
- CF CONSTRUCTION FENCE
- DD DIVERSION DITCH
- IP INLET PROTECTION
- OP OUTLET PROTECTION
- SB SEDIMENT BASIN
- SF SILT FENCE
- SCL SEDIMENT CONTROL LOG
- SSA STABILIZED STAGING AREA
- VTC VEHICLE TRACKING CONTROL
- ECB EROSION CONTROL BLANKET
- LOC LIMITS OF CONSTRUCTION
- ST SEDIMENT TRAP
- FLOW ARROW
- CS CURB SOCK
- SM SEEDING AND MULCHING
- REMOVE INDICATED BMP
- AREA OF CUT
- AREA OF FILL

FULL SPECTRUM POND SUMMARY		
ZONE	VOLUME (AC-FT)	WATER ELEV.
WQCV	0.294	7137.55
EURV	0.675	7140.11
100-YEAR	0.518	7141.64



Riprap depth should be minimum of 12" (2xD50 of riprap size)

Riprap depths were updated to be 12" deep.

**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND.CO  
 Land Planning  
 Landscape Architecture  
 Civil Engineering  
 Construction Management

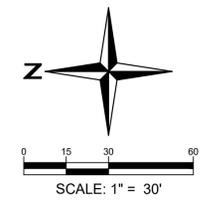
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

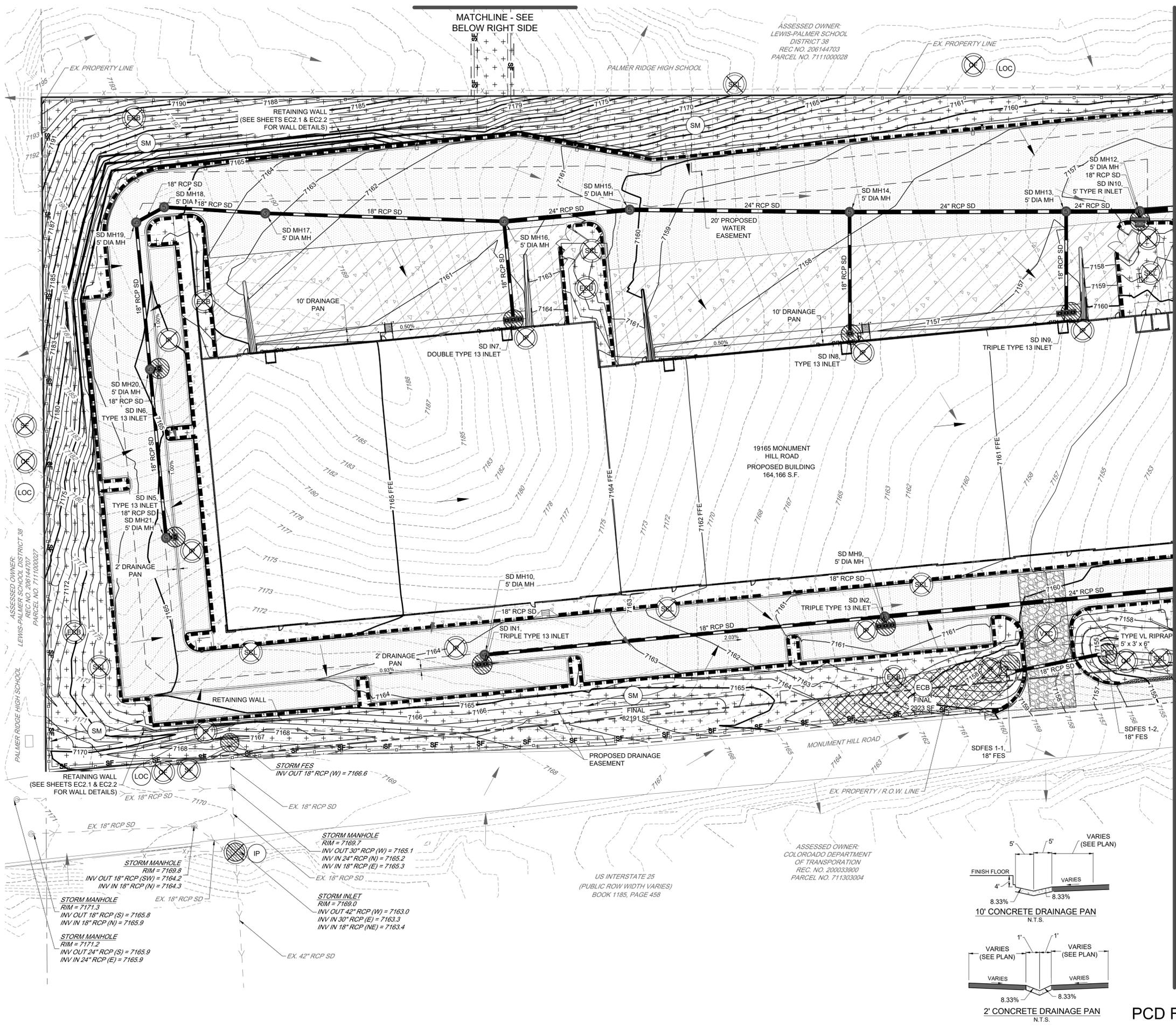
**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
 INTERIM EROSION CONTROL PLAN

SHEET  
**EC3.4**

PCD FILE NO. PPR2329



I:\2023\23009 - The Rock Commerce Center\Sheet Sets\GECC\The Rock\23009\_Final Erosion Control Plan.dwg tab: 9 OF 24 FINAL EROSION CONTROL PLAN Nov 20, 2023 - 7:36am esatz

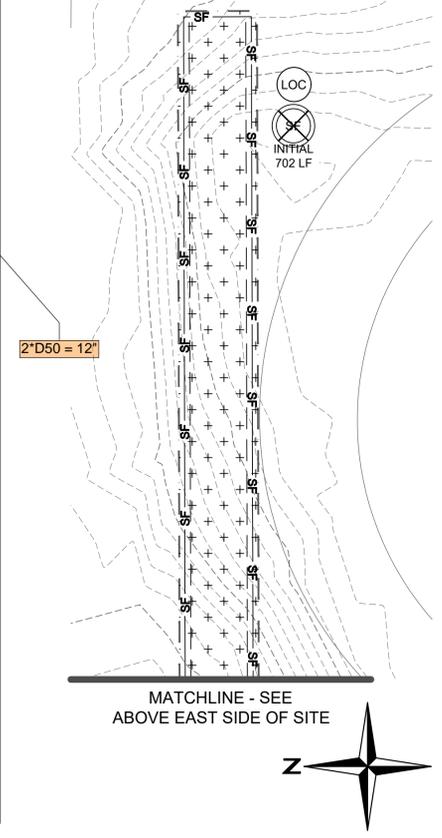


### LEGEND

	(CWA)	CONCRETE WASHOUT AREA
	(CF)	CONSTRUCTION FENCE
	(DD)	DIVERSION DITCH
	(IP)	INLET PROTECTION
	(OP)	OUTLET PROTECTION
	(SB)	SEDIMENT BASIN
	(SF)	SILT FENCE
	(SCL)	SEDIMENT CONTROL LOG
	(SSA)	STABILIZED STAGING AREA
	(VTC)	VEHICLE TRACKING CONTROL
	(ECB)	EROSION CONTROL BLANKET
	(LOC)	LIMITS OF CONSTRUCTION
	(ST)	SEDIMENT TRAP
		FLOW ARROW
	(CS)	CURB SOCK
	(SM)	SEEDING AND MULCHING
	(X)	REMOVE INDICATED BMP

SEEDING AND MULCHING = 124,089 SF  
 PERMANENT EROSION CONTROL BLANKET = 16,058 SF

MATCHLINE - SEE SHEET NO. EC3.6



MATCHLINE - SEE ABOVE EAST SIDE OF SITE

MATCHLINE - SEE BELOW RIGHT SIDE

ASSESSED OWNER:  
LEWIS-PALMER SCHOOL  
DISTRICT 38  
REC NO. 206144703  
PARCEL NO. 7111000028

EX. PROPERTY LINE  
EX. PROPERTY LINE  
EX. PROPERTY LINE

US INTERSTATE 25  
(PUBLIC ROW WIDTH VARIES)  
BOOK 1185, PAGE 458

ASSESSED OWNER:  
COLORADO DEPARTMENT  
OF TRANSPORTATION  
REC. NO. 2000339004  
PARCEL NO. 711303004

ASSESSED OWNER:  
LEWIS-PALMER SCHOOL DISTRICT 38  
REC NO. 206144707  
PARCEL NO. 7111000027

PALMER RIDGE HIGH SCHOOL

19165 MONUMENT HILL ROAD  
PROPOSED BUILDING  
164,166 S.F.

**15 Redland**  
 WHERE GREAT PLACES BEGIN  
 YEARS

720.283.6793  
 LANDSCAPE ARCHITECTURE  
 REDLAND, CO • Civil Engineering • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

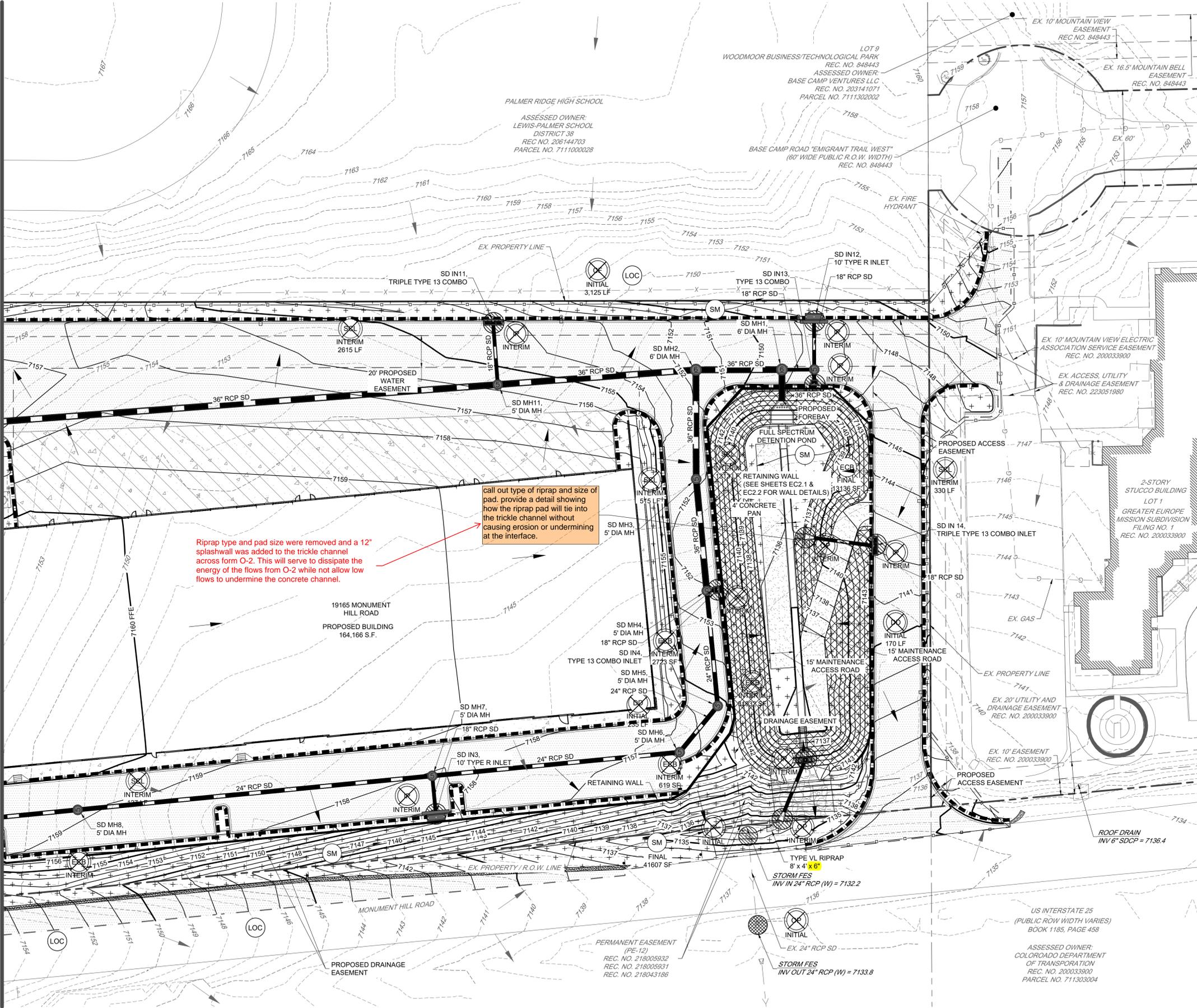
**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
 FINAL EROSION CONTROL PLAN

SHEET  
**EC3.5**

PCD FILE NO. PPR2329

I:\2023\23009 - The Rock Commerce Center\CADD\Sheet Sets\EC\The Rock\23009\_Final Erosion Control Plan.dwg tab: 10 OF 24 FINAL EROSION CONTROL PLAN Nov 20, 2023 - 7:36am cslz

MATCHLINE - SEE SHEET NO. EC3.5



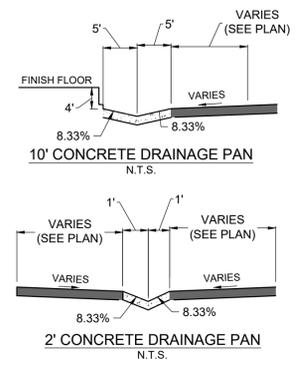
Riprap type and pad size were removed and a 12" splashwall was added to the trickle channel across form O-2. This will serve to dissipate the energy of the flows from O-2 while not allow low flows to undermine the concrete channel.

call out type of riprap and size of pad, provide a detail showing how the riprap pad will tie into the trickle channel without causing erosion or undermining at the interface.

### LEGEND

- CWA CONCRETE WASHOUT AREA
- CF CONSTRUCTION FENCE
- DD DIVERSION DITCH
- IP INLET PROTECTION
- OP OUTLET PROTECTION
- SB SEDIMENT BASIN
- SF SILT FENCE
- SCL SEDIMENT CONTROL LOG
- SSA STABILIZED STAGING AREA
- VTC VEHICLE TRACKING CONTROL
- ECB EROSION CONTROL BLANKET
- LOC LIMITS OF CONSTRUCTION
- ST SEDIMENT TRAP
- FLOW ARROW
- CS CURB SOCK
- SM SEEDING AND MULCHING
- REMOVE INDICATED BMP

FULL SPECTRUM POND SUMMARY		
ZONE	VOLUME (AC-FT)	WATER ELEV.
WQCV	0.294	7137.55
EURV	0.675	7140.11
100-YEAR	0.518	7141.64



**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND.CO.VO • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

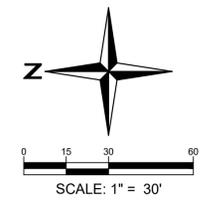
**NOT FOR CONSTRUCTION**

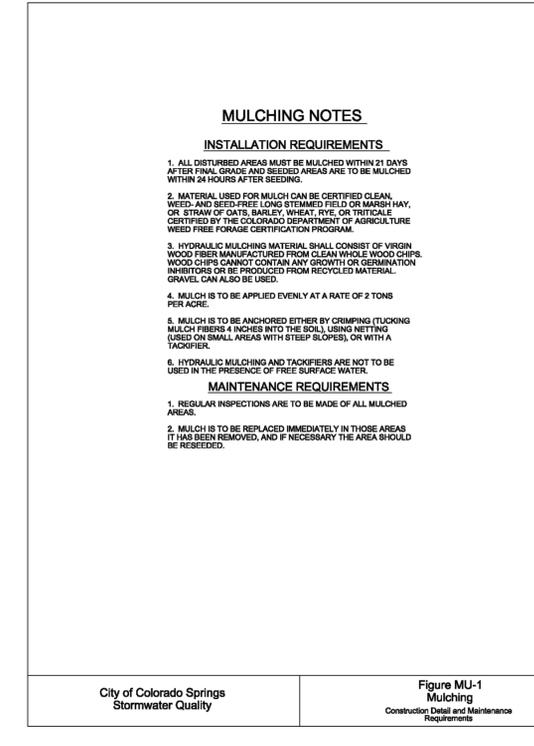
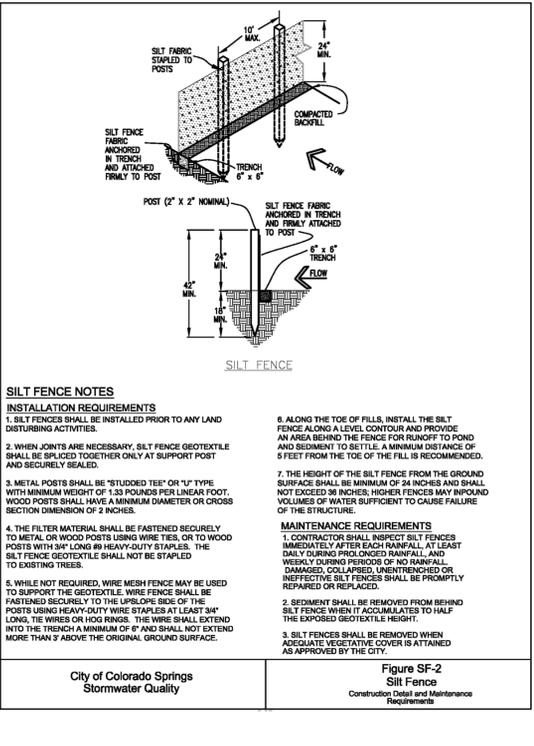
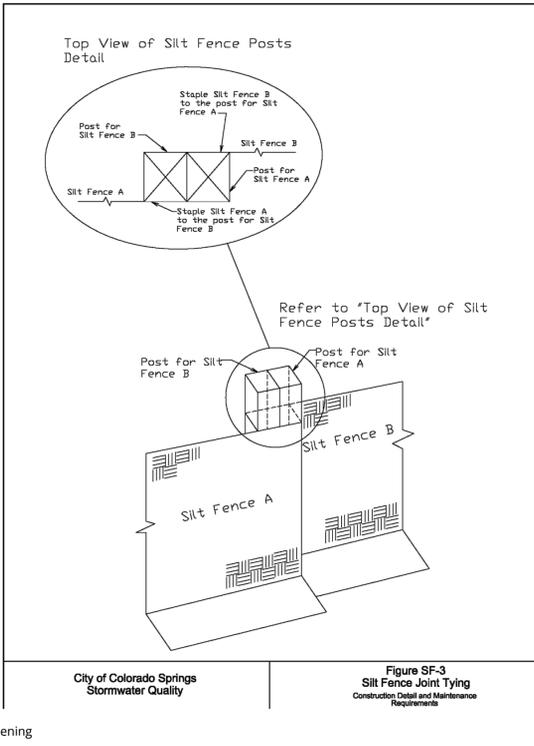
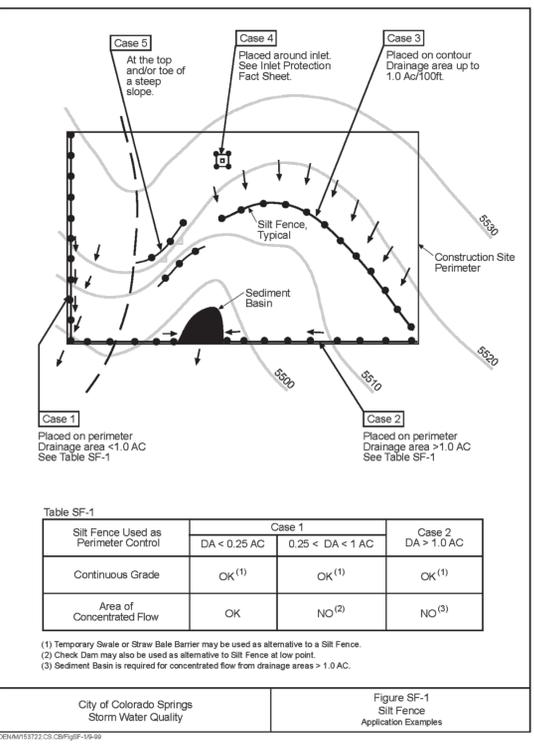
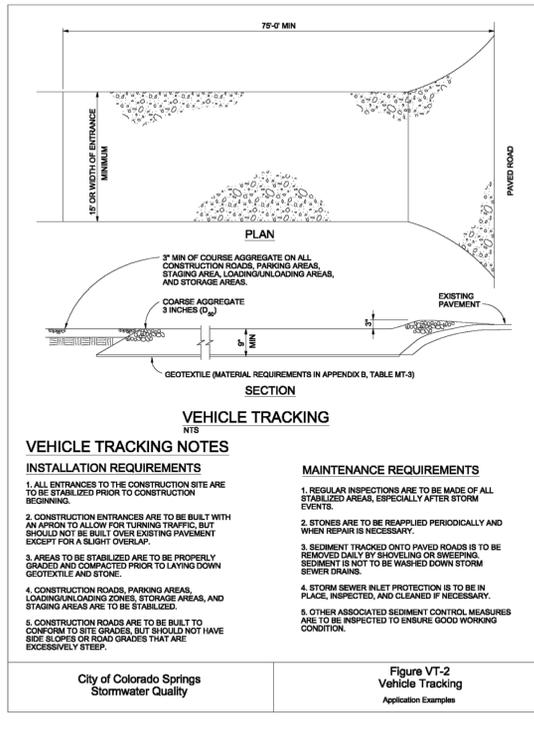
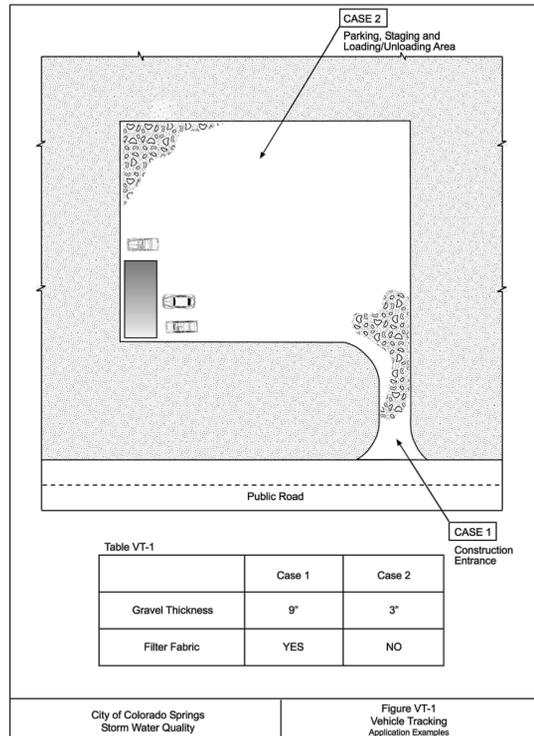
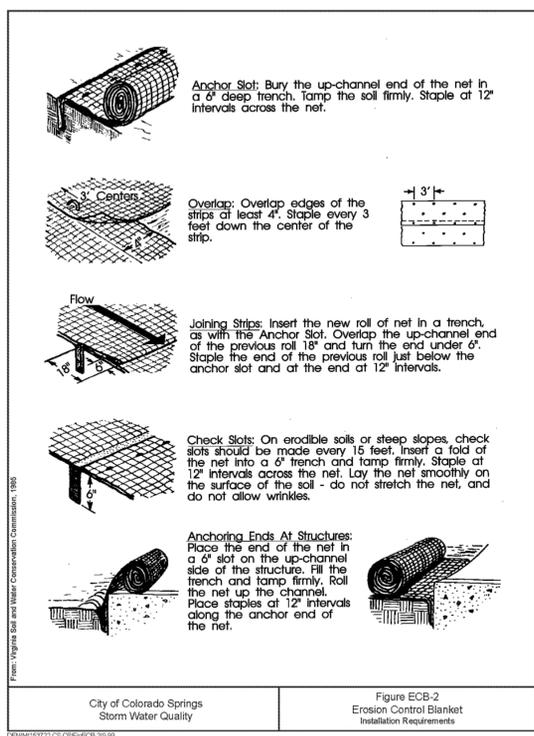
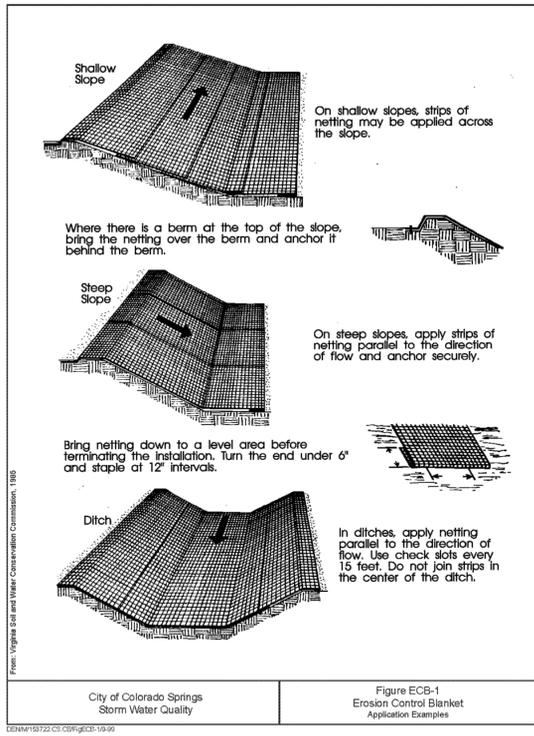
PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
 FINAL EROSION CONTROL PLAN

SHEET  
**EC3.6**

PCD FILE NO. PPR2329





**15 Years** WHERE GREAT PLACES BEGIN

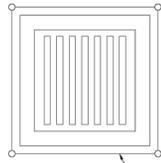
720.283.6793  
REDLAND.CO.VO • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.: 23009

DATE	NO.	NOTES
07/28/2023	1	1ST SUBMITTAL
10/20/2023	2	2ND SUBMITTAL
11/17/2023	3	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
GEC DETAILS



**FILTER FABRIC INLET PROTECTION**  
NTS

**FILTER FABRIC INLET PROTECTION NOTES**

**INSTALLATION REQUIREMENTS**

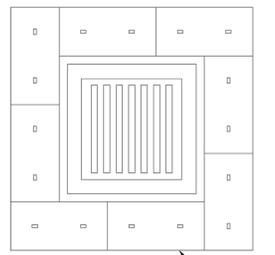
1. INLET PROTECTION SHALL BE INSTALLED IMMEDIATELY AFTER CONSTRUCTION OF INLET.
2. SEE S&T FIGURE SB-2 FOR INSTALLATION REQUIREMENTS.
3. PORTS ARE TO BE PLACED AT EACH CORNER OF THE INLET AND AROUND THE EDGES AT A MAXIMUM SPACING OF 3 FEET.

**MAINTENANCE REQUIREMENTS**

1. CONTRACTOR SHALL INSPECT INLET PROTECTION IMMEDIATELY AFTER EACH RAINFALL, AT LEAST DAILY DURING PROLONGED RAINFALL, AND WEEKLY DURING PERIODS NO RAINFALL.
2. DAMAGED OR COLLAPSED UNFENCED OR UNSUPPORTED INLET PROTECTION SHALL BE PROMPTLY REPAIRED OR REPLACED.
3. SEDIMENT SHALL BE REMOVED FROM BEHIND FILTER FABRIC WHEN IT ACCUMULATES TO HALF THE EXPOSED GEOTEXTILE HEIGHT.
4. FILTER FABRIC PROTECTION SHALL BE REMOVED WHEN ADEQUATE VEGETATIVE COVER IS ATTAINED IN THE DRAINAGE AREA AS APPROVED BY THE CITY.

City of Colorado Springs  
Stormwater Quality

Figure IP-1  
Filter Fabric Inlet Protection  
Construction Detail and Maintenance  
Requirements



**STRAW BALE INLET PROTECTION**  
NTS

**STRAW BALE INLET PROTECTION NOTES**

**INSTALLATION REQUIREMENTS**

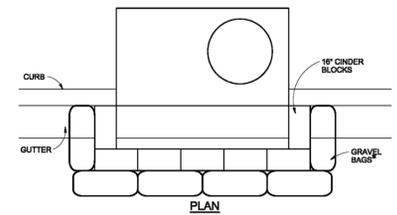
1. INLET PROTECTION SHALL BE INSTALLED IMMEDIATELY AFTER CONSTRUCTION OF INLET.
2. BALES ARE TO BE PLACED IN A SINGLE ROW AROUND THE INLET WITH THE END OF THE BALES TIGHTLY ABUTTING ONE ANOTHER.
3. SEE STRAW BALE BARRIER FIGURE SB8-2 FOR INSTALLATION REQUIREMENTS.

**MAINTENANCE REQUIREMENTS**

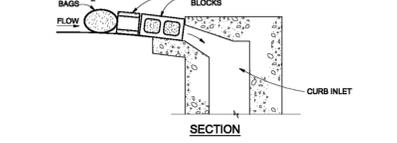
1. CONTRACTOR SHALL INSPECT STRAW BALE INLET PROTECTION IMMEDIATELY AFTER EACH RAINFALL, AT LEAST DAILY DURING PROLONGED RAINFALL, AND WEEKLY DURING PERIODS NO RAINFALL.
2. DAMAGED OR INEFFECTIVE INLET PROTECTION SHALL PROMPTLY BE REPAIRED. REPLACING BALES IF NECESSARY, AND UNFENCED BALES NEED TO BE REPAIRED WITH COMPACTED BACKFILL MATERIAL.
3. SEDIMENT SHALL BE REMOVED FROM BEHIND STRAW BALES WHEN IT ACCUMULATES TO APPROXIMATELY 1/2 THE HEIGHT OF THE BARRIER.
4. INLET PROTECTION SHALL BE REMOVED WHEN ADEQUATE VEGETATIVE COVER IS ATTAINED WITHIN THE DRAINAGE AREA AS APPROVED BY THE CITY.

City of Colorado Springs  
Stormwater Quality

Figure IP-2  
Straw Bale Inlet Protection  
Construction Detail and Maintenance  
Requirements



**PLAN**



**SECTION**

**BLOCK AND GRAVEL BAG CURB INLET PROTECTION**  
NTS

**BLOCK AND GRAVEL BAG CURB INLET PROTECTION NOTES**

**INSTALLATION REQUIREMENTS**

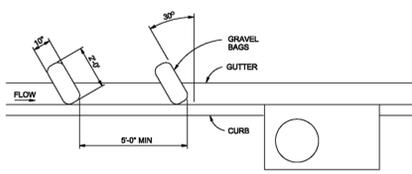
1. INLET PROTECTION SHALL BE INSTALLED IMMEDIATELY AFTER CONSTRUCTION OF INLET.
2. CONCRETE BLOCKS ARE TO BE LAID AROUND THE INLET IN A SINGLE ROW ON THEIR SIDES, ABUTTING ONE ANOTHER WITH THE OPEN END OF THE BLOCK FACING OUTWARD.
3. GRAVEL BAGS ARE TO BE PLACED AROUND THE CONCRETE BLOCKS CLOSELY ABUTTING ONE ANOTHER SO THERE ARE NO GAPS.
4. GRAVEL BAGS ARE TO CONTAIN WASHED SAND OR GRAVEL, APPROXIMATELY 3/4 INCH IN DIAMETER.
5. BAGS ARE TO BE MADE OF 1/4" INCH WIRE MESH (USED WITH GRAVEL ONLY) OR GEOTEXTILE.

**MAINTENANCE REQUIREMENTS**

1. CONTRACTOR SHALL INSPECT INLET PROTECTION IMMEDIATELY AFTER EACH RAINFALL, AT LEAST DAILY DURING PROLONGED RAINFALL, AND WEEKLY DURING PERIODS NO RAINFALL.
2. DAMAGED OR INEFFECTIVE INLET PROTECTION SHALL PROMPTLY BE REPAIRED OR REPLACED.
3. SEDIMENT SHALL BE REMOVED WHEN SEDIMENT HAS ACCUMULATED TO APPROXIMATELY 1/2 THE DEPTH OF THE TRAP.
4. INLET PROTECTION SHALL BE REMOVED WHEN ADEQUATE VEGETATIVE COVER IS ATTAINED WITHIN THE DRAINAGE AREA AS APPROVED BY THE CITY.

City of Colorado Springs  
Stormwater Quality

Figure IP-3  
Block & Gravel Bag Curb Inlet Protection  
Construction Detail and Maintenance  
Requirements



**CURB SOCK INLET PROTECTION**  
NTS

**CURB SOCK INLET PROTECTION NOTES**

**INSTALLATION REQUIREMENTS**

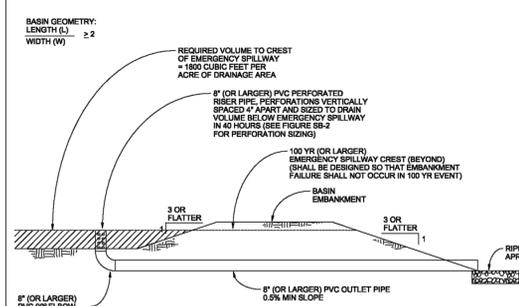
1. INLET PROTECTION SHALL BE INSTALLED IMMEDIATELY AFTER CONSTRUCTION OF INLET.
2. SOCK IS TO BE MADE OF 1/4 INCH WIRE MESH (USED WITH GRAVEL ONLY) OR GEOTEXTILE.
3. WASHED SAND OR GRAVEL 3/4 INCH TO 4 INCHES IN DIAMETER IS PLACED INSIDE THE SOCK.
4. PLACEMENT OF THE SOCK IS TO BE 30 DEGREES FROM PERPENDICULAR IN THE OPPOSITE DIRECTION OF FLOW.
5. SOCKS ARE TO BE FLUSH WITH THE CURB AND SPACED AT A MINIMUM 3 FEET APART.
6. AT LEAST 2 CURB SOCKS IN SERIES IS REQUIRED.

**MAINTENANCE REQUIREMENTS**

1. CONTRACTOR SHALL INSPECT INLET PROTECTION IMMEDIATELY AFTER EACH RAINFALL, AT LEAST DAILY DURING PROLONGED RAINFALL, AND WEEKLY DURING PERIODS NO RAINFALL.
2. DAMAGED OR INEFFECTIVE INLET PROTECTION SHALL PROMPTLY BE REPAIRED OR REPLACED.
3. SEDIMENT SHALL BE REMOVED FROM BEHIND THE SOCK WHEN GUTTER WIDTH IS FILLED.
4. INLET PROTECTION SHALL BE REMOVED WHEN ADEQUATE VEGETATIVE COVER IS ATTAINED WITHIN THE DRAINAGE AREA AS APPROVED BY THE CITY.

City of Colorado Springs  
Stormwater Quality

Figure IP-4  
Curb Sock Inlet Protection  
Construction Detail and Maintenance  
Requirements



**SEDIMENT BASIN**  
NTS

**SEDIMENT BASIN NOTES**

**INSTALLATION REQUIREMENTS**

1. SEDIMENT BASINS SHALL BE INSTALLED BEFORE ANY CLEARING AND/OR GRADING IS UNDERTAKEN.
2. THE AREA UNDER WHICH THE EMBANKMENT IS TO BE INSTALLED SHALL BE CLEARED, GRUBBED, AND STRIPPED OF ALL VEGETATION AND ROOT MAT.
3. THE OUTLET OF THE BASIN SHALL BE DESIGNED TO DRAIN ITS VOLUME IN 40 HOURS.
4. THE OUTLET IS TO BE LOCATED AT THE FURTHEST DISTANCE FROM THE INLET OF THE BASIN. Baffles MAY BE NEEDED TO INCREASE THE FLOW LENGTH AND SETTLING TIME.
5. EMBANKMENT MATERIAL SHALL CONSIST OF SOIL WITH A MINIMUM OF 15% PASSING A #200 SIEVE. EXCAVATED SOIL CAN BE USED IF IT MEETS THIS REQUIREMENT.
6. EMBANKMENT IS TO BE COMPACTED TO AT LEAST 80% OF MAXIMUM DENSITY AND WITHIN 2% OF OPTIMUM MOISTURE CONTENT ACCORDING TO ASTM D 698.
7. WHEN A BASIN IS INSTALLED NEAR A RESIDENTIAL AREA, FOR SAFETY REASONS, A SIGN SHALL BE POSTED AND THE AREA SECURED WITH A FENCE.

**MAINTENANCE REQUIREMENTS**

1. CONTRACTOR SHALL INSPECT SEDIMENT BASINS AFTER EACH RAINFALL, AT LEAST DAILY DURING PROLONGED RAINFALL, AND WEEKLY DURING PERIODS NO RAINFALL.
2. SEDIMENT BASINS SHALL BE CLEANED OUT BEFORE SEDIMENT HAS FILLED HALF THE VOLUME OF THE BASIN.
3. SEDIMENT BASINS SHALL REMAIN OPERATIONAL AND PROPERLY MAINTAINED UNTIL THE SITE AREA IS PERMANENTLY STABILIZED WITH ADEQUATE VEGETATIVE COVER AND/OR OTHER PERMANENT STRUCTURE AS APPROVED BY THE CITY.

City of Colorado Springs  
Stormwater Quality

Figure SB-1  
Sediment Basin  
Construction Detail and Maintenance  
Requirements

Design Volume (cubic feet)	Required Area per Row (sq ft)							
	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
2	15.04	17.71	5.10	3.76	2.95	2.41	2.02	1.73
1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87
0.8	4.81	2.31	1.63	1.13	0.89	0.72	0.61	0.52
0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35
0.2	1.50	0.77	0.51	0.38	0.30	0.24	0.20	0.17
0.1	0.75	0.39	0.26	0.19	0.15	0.12	0.10	0.09
0.08	0.45	0.23	0.15	0.11	0.09	0.07	0.06	0.05
0.04	0.30	0.16	0.10	0.08	0.06	0.05	0.04	0.03
0.02	0.15	0.08	0.05	0.04	0.03	0.02	0.02	0.02
0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01

**TABLE SB-1**

Hole Diameter (in)	Hole Diameter (in)	Area per Row (sq ft)		
		n = 1	n = 2	n = 3
1/4	0.250	0.05	0.10	0.15
5/16	0.313	0.08	0.15	0.23
3/8	0.375	0.11	0.22	0.33
7/16	0.438	0.15	0.30	0.45
1/2	0.500	0.20	0.39	0.59
9/16	0.563	0.25	0.50	0.75
5/8	0.625	0.31	0.61	0.92
11/16	0.688	0.37	0.74	1.11
3/4	0.750	0.44	0.88	1.33
7/8	0.875	0.60	1.20	1.80
1	1.000	0.79	1.57	2.36
1 1/8	1.125	0.99	1.99	2.98
1 1/4	1.250	1.23	2.45	3.68
1 3/8	1.375	1.48	2.97	4.45
1 1/2	1.500	1.77	3.53	5.30
1 5/8	1.625	2.07	4.15	6.22
1 3/4	1.750	2.41	4.81	7.22
1 7/8	1.875	2.78	5.52	8.29
2	2.000	3.14	6.28	9.42

**TABLE SB-2**

City of Colorado Springs  
Stormwater Quality

Figure SB-2  
Outlet Sizing  
Application Techniques and Maintenance  
Requirements

SPECIES (COMMON NAME)	GROWTH SEASON	SEEDING DATE	POUNDS OF PURE LIVE SEED (PLS) (PL/SQ YD)	PLANTING DEPTH (INCHES)
2. SPRING WHEAT	COOL	MARCH 16 - APRIL 30	25-35	1-2
3. SPRING BARLEY	COOL	MARCH 16 - APRIL 30	25-35	1-2
4. ANNUAL KYRGASS	COOL	MARCH 16 - JUNE 30	10-15	1/2
5. MILLET	WARM	MAY 16 - JULY 15	3-15	1/2-3/4
6. BLUINGRASS	WARM	MAY 16 - JULY 15	5-10	1/2-3/4
7. SORGHAM	WARM	MAY 16 - JULY 15	5-10	1/2-3/4
8. WINTER WHEAT	COOL	SEPTEMBER 1 - 30	20-35	1-2
9. WINTER BARLEY	COOL	SEPTEMBER 1 - 30	20-35	1-2
10. WINTER RYE	COOL	SEPTEMBER 1 - 30	20-35	1-2
11. TRITICALE	COOL	SEPTEMBER 1 - 30	25-40	1-2

**TABLE TS-1**

**TEMPORARY SEEDING NOTES**

**INSTALLATION REQUIREMENTS**

1. DISTURBED AREAS ARE TO BE SEEDS WITHIN 21 DAYS AFTER CONSTRUCTION ACTIVITY OR GRADING ENDS IF SEASON ALLOWS.
2. IF NECESSARY, SOIL IS TO BE CONDITIONED FOR PLANT GROWTH BY APPLYING TOPSOIL, FERTILIZER, OR LIMES.
3. SOIL IS TO BE TILLED IMMEDIATELY PRIOR TO APPLYING SEEDS. CONTACT SOILS ESPECIALLY NEED TO BE LOOSENED.
4. SEEDBED DEPTH IS TO BE 4 INCHES FOR SLOPES FLATTER THAN 2:1, AND 1 INCH FOR SLOPES STEEPER THAN 2:1.
5. ANNUAL GRASSES LISTED IN TABLE TS-1 ARE TO BE USED FOR TEMPORARY SEEDING. SEEDS ARE NOT TO CONTAIN ANY NOXIOUS WEED SEEDS INCLUDING RUSSIAN OR CANADIAN THISTLE, KNAPWEED, PURPLE LOOSESTRIKE, EUROPEAN BIRNWEED, JOHNSON GRASS, AND LEAFY SPURGE.
6. TABLE TS-1 ALSO PROVIDES REQUIREMENTS FOR SEEDING RATES, SEEDING DATES, AND PLANTING DEPTHS FOR THE APPROVED TYPES OF ANNUAL GRASSES.
7. SEEDING IS TO BE APPLIED USING MECHANICAL TYPE DRILLS EXCEPT WHERE SLOPES ARE STEEP OR ACCESS IS LIMITED THEN HYDRAULIC SEEDING MAY BE USED.
8. ALL SEEDS ARE TO BE MULCHED (SEE FACTSHEET ON MULCHING).
9. IF HYDRAULIC SEEDING IS USED THEN HYDRAULIC MULCHING SHALL BE DONE SEPARATELY TO AVOID SEEDS BECOMING ENCAPSULATED IN THE MULCH.

**MAINTENANCE REQUIREMENTS**

1. REGULAR INSPECTIONS ARE TO BE MADE OF ALL SEEDS AREAS TO ENSURE GROWTH.
2. AREAS WHERE GROWTH IS NOT OCCURRING QUICKLY OR THE MULCH HAS BEEN REMOVED SHALL BE RE-SEEDS AS SOON AS POSSIBLE AND RE-MULCHED IF NEEDED.
3. SEEDS AREAS ARE NOT TO BE DRIVEN OVER WITH CONSTRUCTION EQUIPMENT OR VEHICLES.

City of Colorado Springs  
Stormwater Quality

Figure TS-1  
Temporary Seeding  
Construction Detail and Maintenance  
Requirements

**15 Redland YEARS**  
WHERE GREAT PLACES BEGIN  
720.283.6793  
REDLAND.CO.VO • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/2023	1	1ST SUBMITTAL
	10/20/2023	2	2ND SUBMITTAL
	11/17/2023	3	3RD SUBMITTAL

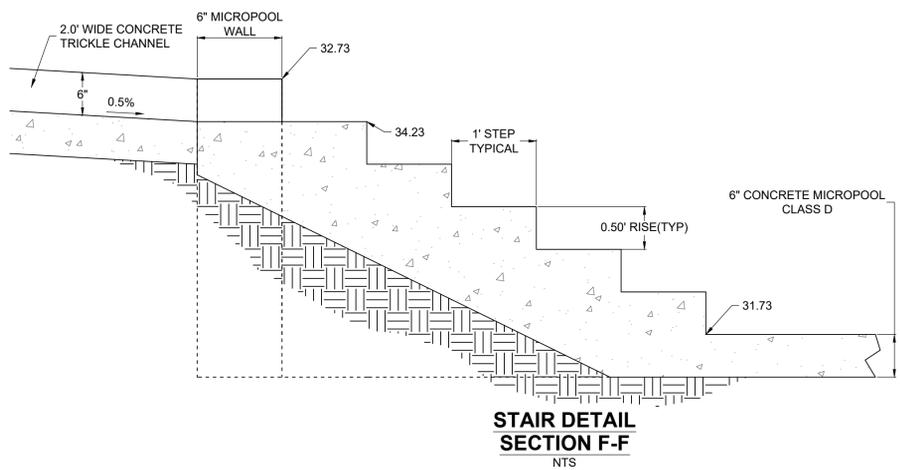
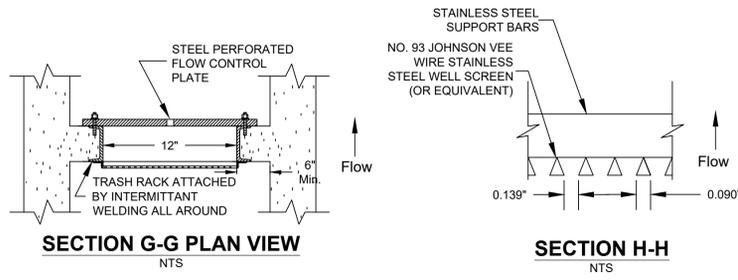
**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
GEC DETAILS

SHEET

Please submit a State Non-Jurisdictional Water Impoundment Structure Application for this pond

This application will be submitted as requested.

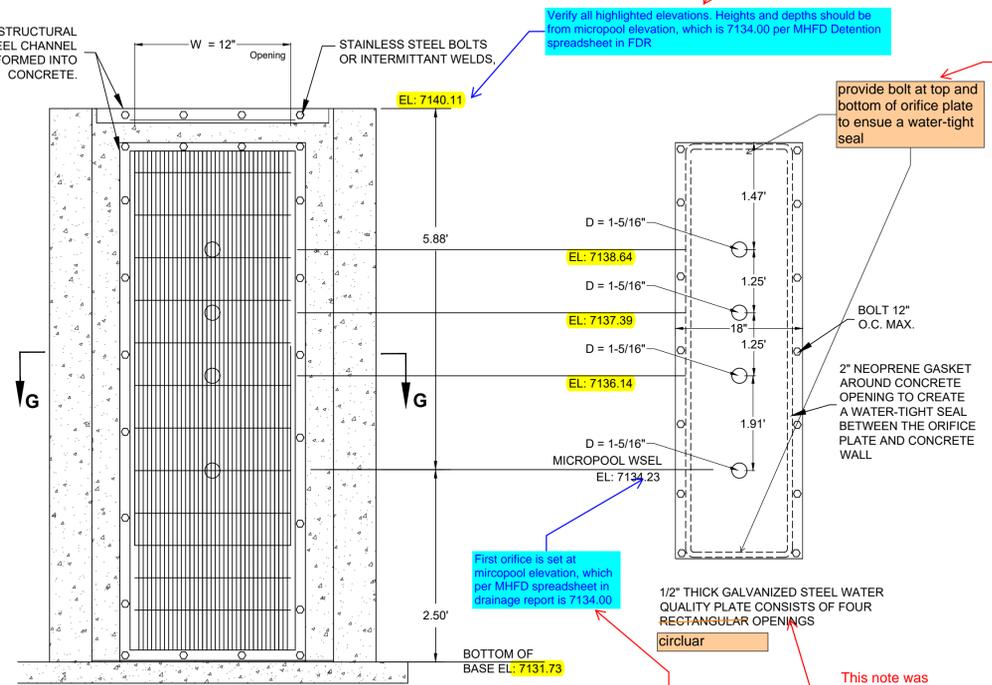
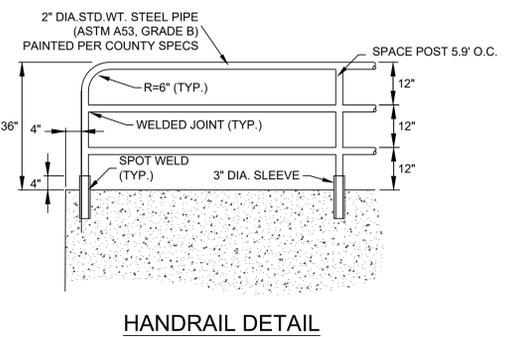
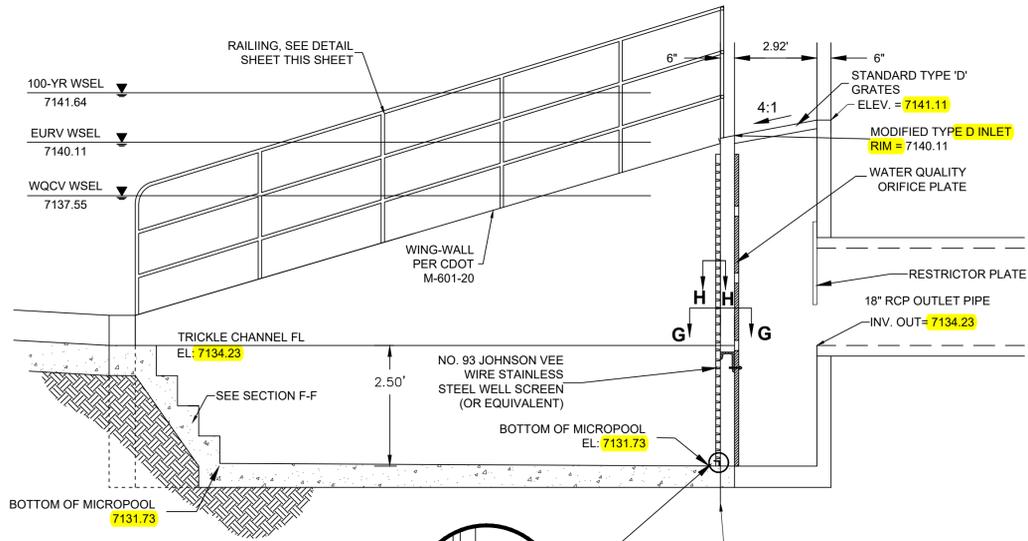
NOTES:  
 1) ALL STRUCTURES SHALL CONSIST OF CDOT CLASS D CONCRETE.  
 2) CONTRACTOR TO SUPPLY STRUCTURAL SHOP DRAWINGS FOR ALL STRUCTURES PRIOR TO CONSTRUCTION.



Provide details for:  
 - Outlet Structure  
 - Forebay  
 - Trickle Channel

These details have been added as requested.

The MHFD Detention Spread sheet was updated so that the micropool elevation is now 7134.23.



Verify all highlighted elevations. Heights and depths should be from micropool elevation, which is 7134.00 per MHFD Detention spreadsheet in FDR.

A bolt was added to the top and bottom of the orifice plate.

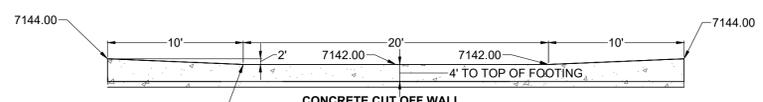
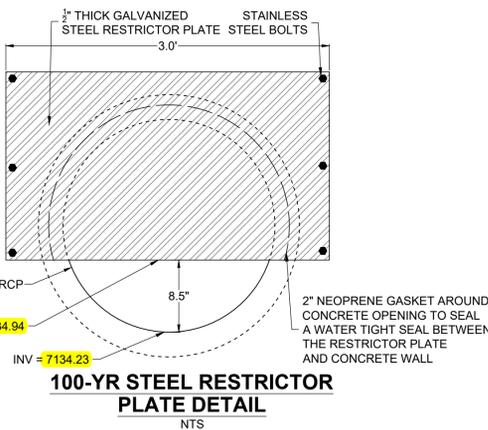
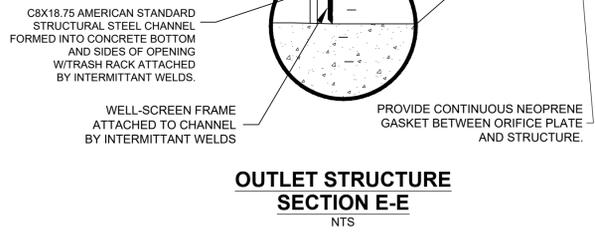
provide bolt at top and bottom of orifice plate to ensure a water-tight seal

First orifice is set at micropool elevation, which per MHFD spreadsheet in drainage report is 7134.00

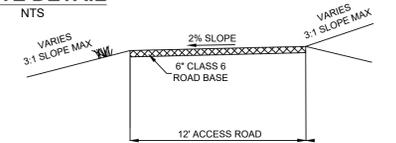
1/2" THICK GALVANIZED STEEL WATER QUALITY PLATE CONSISTS OF FOUR RECTANGULAR OPENINGS

The MHFD Detention Spread sheet was updated so that the micropool elevation is now 7134.23.

This note was updated as requested.

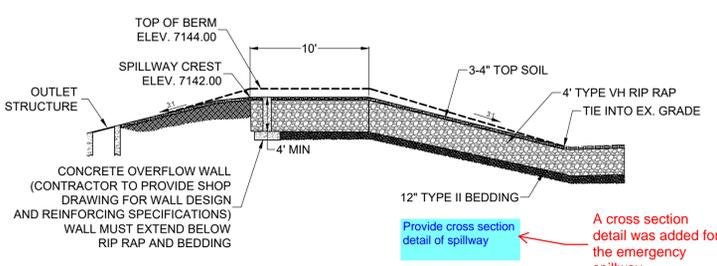


NOTE: CONTRACTOR TO PROVIDE STRUCTURAL SHOP DRAWINGS FOR CUT-OFF WALL



These details were updated to reflect the 15' access road.

Please revise the minimum access road width is 15'.



A cross section detail was added for the emergency spillway.

This detail is now labeled as requested.

**15 Redland YEARS**  
 WHERE GREAT PLACES BEGIN  
 720.283.6783  
 REDLAND, CO  
 • Land Planning  
 • Landscape Architecture  
 • Civil Engineering  
 • Construction Management

**NOT FOR CONSTRUCTION**

PROJECT NO.	NO.	DATE	NOTES
23009	1	07/28/2023	1ST SUBMITTAL
	2	10/20/2023	2ND SUBMITTAL
	3	11/17/2023	3RD SUBMITTAL

**THE ROCK COMMERCE CENTER**  
**GRADING AND EROSION CONTROL PLANS**  
 POND DETAILS



Know what's below. Call before you dig.

PCD FILE NO. PPR2329

EC4.3

I:\2023\23009 - The Rock Commerce Center\CADD\Sheet Sets\GCC\The Rock\23009\_POND\_Details.dwg Lab: POND DETAILS Nov 20, 2023 - 7:36am caslz

# V3\_Grading and Erosion Control Plan.pdf Markup Summary

Carlos (2)



**Subject:** Callout  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** Carlos  
**Date:** 11/29/2023 11:31:02 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Please revise the minimum access road width is 15'.

Please label detail

**Subject:** Text Box  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** Carlos  
**Date:** 11/29/2023 11:32:51 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

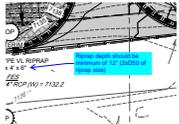
Please label detail

CDurham (20)



**Subject:** Callout  
**Page Label:** [4] EC2.2 GRADING PLAN  
**Author:** CDurham  
**Date:** 12/5/2023 1:34:50 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Riprap depth should be minimum of 12" (2xD50 of riprap size)



**Subject:** Callout  
**Page Label:** [8] EC3.4 INTERIM EROSION CONTROL PLAN  
**Author:** CDurham  
**Date:** 12/5/2023 1:37:00 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Riprap depth should be minimum of 12" (2xD50 of riprap size)

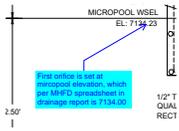
PE VL RIF  
4' x 6"  
ECS

**Subject:** Highlight  
**Page Label:** [10] EC3.6 FINAL EROSION CONTROL PLAN x 6"  
**Author:** CDurham  
**Date:** 12/5/2023 3:45:24 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Provide details for:  
- Outlet Structure  
- Forebay  
- Trickle Channel

**Subject:** Text Box  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:22:19 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Provide details for:  
- Outlet Structure  
- Forebay  
- Trickle Channel



**Subject:** Callout  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:23:02 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

First orifice is set at micropool elevation, which per MHFD spreadsheet in drainage report is 7134.00

D = 1-5/16"  
 EL: 7136.14

**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:23:08 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

EL: 7136.14

D = 1-5/16"  
 EL: 7137.39

**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:23:11 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

EL: 7137.39

D = 1-5/16"  
 EL: 7138.64

**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:23:13 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

EL: 7138.64

EL: 7131.73

**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:23:18 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

: 7131.73

EL: 7140.11

**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:23:30 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

EL: 7140.11

Subject: Highlight  
Page Label: [13] EC4.3 POND DETAILS 7134.94  
E = 7134.94  
Author: CDurham  
Date: 12/5/2023 4:25:37 PM  
Status:  
Color:   
Layer:  
Space:

Subject: Highlight  
Page Label: [13] EC4.3 POND DETAILS 7134.23  
IV = 7134.23  
Author: CDurham  
Date: 12/5/2023 4:25:38 PM  
**100-YI**  
Status:  
Color:   
Layer:  
Space:

Subject: Highlight  
Page Label: [13] EC4.3 POND DETAILS 7134.23  
TRICKLE CHAN  
EL: 7134.23  
Author: CDurham  
Date: 12/5/2023 4:25:46 PM  
1  
Status:  
Color:   
Layer:  
Space:

Subject: Highlight  
Page Label: [13] EC4.3 POND DETAILS 7131.73  
ICROPOOL  
7131.73  
Author: CDurham  
Date: 12/5/2023 4:25:50 PM  
Status:  
Color:   
Layer:  
Space:

Subject: Highlight  
Page Label: [13] EC4.3 POND DETAILS 7131.73  
ICROPOOL  
EL: 7131.73  
Author: CDurham  
Date: 12/5/2023 4:25:53 PM  
Status:  
Color:   
Layer:  
Space:

Subject: Highlight  
Page Label: [13] EC4.3 POND DETAILS 7141.11  
DARD TYPE D  
ES  
7141.11  
Author: CDurham  
Date: 12/5/2023 4:26:05 PM  
MODIFIED TYPE I  
Status:  
Color:   
Layer:  
Space:

- STANDARD TYPE 'D'  
GRATES
- ELEV. = 7141.11
- MODIFIED TYPE 'D' INLET  
RIM = 7140.11
- WATER QUALITY  
ORIFICE PLATE

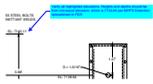
**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:26:08 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

E D INLET  
RIM =

' OUTLET PIPE  
JT= 7134.23

**Subject:** Highlight  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:26:14 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

7134.23



**Subject:** Callout  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:27:14 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Verify all highlighted elevations. Heights and depths should be from micropool elevation, which is 7134.00 per MHFD Detention spreadsheet in FDR

12" TYPE II BEDDING  
Provide cross section detail of spillway

**Subject:** Text Box  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** CDurham  
**Date:** 12/5/2023 4:27:48 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Provide cross section detail of spillway

Christina Prete (8)

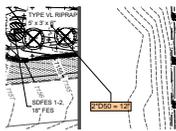


**Subject:** Stormwater Comments Color  
**Page Label:** [1] EC1.0 COVER SHEET  
**Author:** Christina Prete  
**Date:** 12/6/2023 5:24:45 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**



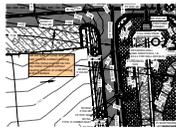
**Subject:** Contractor  
**Page Label:** [8] EC3.4 INTERIM EROSION CONTROL PLAN  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:24:13 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Assign a name/number to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling throughout (example: "Pond A" or "Pond 1").



---

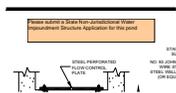
**Subject:** Contractor  
**Page Label:** [9] EC3.5 FINAL EROSION CONTROL PLAN 2\*D50 = 12"  
**Author:** Christina Prete  
**Date:** 12/6/2023 5:06:49 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**



---

**Subject:** Contractor  
**Page Label:** [10] EC3.6 FINAL EROSION CONTROL PLAN  
**Author:** Christina Prete  
**Date:** 12/6/2023 5:03:41 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

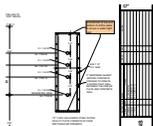
call out type of riprap and size of pad. provide a detail showing how the riprap pad will tie into the trickle channel without causing erosion or undermining at the interface.



---

**Subject:** Contractor  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:26:03 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

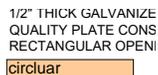
Please submit a State Non-Jurisdictional Water Impoundment Structure Application for this pond



---

**Subject:** Contractor  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:31:35 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

provide bolt at top and bottom of orifice plate to ensure a water-tight seal

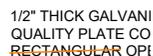


---

**Subject:** Contractor  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:32:09 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

1/2" THICK GALVANIZE QUALITY PLATE CONS RECTANGULAR OPENING  
circular

circular



---

**Subject:** Line  
**Page Label:** [13] EC4.3 POND DETAILS  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:32:12 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

1/2" THICK GALVANIZED QUALITY PLATE CONS RECTANGULAR OPENING

# Final Drainage Report The Rock Commerce Center

Prepared for:

**Central Development LLC**  
1660 S Albion St, Suite 200  
Denver, CO 80222  
(303) 628-0200 voice

Prepared by:

**Redland**  
1500 W Canal Court  
Littleton, Colorado 80120  
(720) 283-6783 voice  
Mark D. Cevaal, P.E.

PCD File No. PPR2329

July 28, 2023  
October 20, 2023  
November 17, 2023  
Project No. 23009.001

**Signature Page**

**The Rock Commerce Center**

**Design Engineer’s Statement**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

SIGNATURE (Affix Seal) : \_\_\_\_\_  
Colorado P.E. No. 33123

10/20/23  
Date

**Developer’s Statement**

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
[Jeremy Records, Principal]  
[Central Development LLC]  
[1660 S Albion St, Suite 200  
Denver, CO 80222]

\_\_\_\_\_  
Date

**El Paso County**

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

\_\_\_\_\_  
Joshua Palmer, P.E.  
County Engineer / ECM Administrator

\_\_\_\_\_  
Date

Conditions:

## Table of Contents

Table of Contents.....	3
General Location and Description .....	4
Introduction .....	4
Site Location .....	4
Description of Property .....	4
Drainage Basins and Subbasins.....	5
Existing Major Basin Description.....	5
Existing Subbasin Description .....	5
Drainage Design Criteria.....	7
Runoff/Proposed Basin Description .....	7
Major Basins.....	7
Sub-Basins.....	8
Stormwater Detention and Water Quality Design .....	21
Drainage Fees.....	23
Erosion Control Plan.....	23
Construction Cost Estimate .....	23
Conclusion.....	24
References .....	25

Appendix A – Vicinity Map, Soils Map, FIRM Map

Appendix B – Hydrologic Calculations

Appendix C – Hydraulic Calculations

Appendix D – Reference Documents

Appendix E – Drainage Maps

## General Location and Description

### Introduction

The purpose of this Final Drainage Report is to identify on-site and off-site drainage patterns, storm sewer, inlet locations, areas tributary to the site, and to safely route the developed flows to the proposed full spectrum pond. Analyses for the proposed drainage patterns and requirements for the proposed The Rock Commerce Center development, hereafter referred to as the Site, are presented in the appendices of this Report.

### Site Location

The Site is located on unplatted land in the Northwest Quarter of Section 11, Township 11 South, Range 67 West of the 6th Principal Meridian, El Paso County, Colorado. The site is bordered on the west side by Monument Hill Road and I-25, Palmer Ridge High School to the north and west, and 18950 Base Camp Road to the south, see Appendix A. The site will have two connections onto Monument Hill Road and one connection to the southeast to Base Camp Road.

### Description of Property

The Site encompasses approximately 11.61 acres and is currently undeveloped. The project area was determined by an ALTA/NSPS Land Title Survey conducted by Aztec Consultants Inc. dated 02/23/2023. This survey can be seen in Appendix A of this report. Native grasses and weeds currently cover the site with a few small trees. The site generally falls north to south but has a ridge running diagonally from the northwest corner toward Monument Hill Road splitting the site north and south. The northern section of site slopes at about 12% from west to east. The middle of the site slopes at about 4% from the northeast to the southwest. The southern section of site slopes at about 4% from the west to east.

The property is proposed to include a 164,166 SF commercial warehouse/showroom with associated parking, sidewalks, drive aisles, and landscaping. The building will be located in the middle of the site running north to south parallel to Monument Hill Road. The total disturbed area is 12.30 acres. The disturbed area is greater than the project area due to offsite improvements and grading required for Monument Hill Road. There will also be some offsite improvements required to create an access to Base Camp Road.

The Site is located within the Crystal Creek Drainage Basin which outfalls to Monument Lake per the *El Paso County Drainage Basin Map (DBMP), prepared by the Board of Commissioners, El Paso County, dated 2005.*

There are no existing irrigation facilities on the Site.

There is an existing 18" RCP storm sewer located near the northwest corner of the Site located in a roadside swale next to Monument Hill Road This storm sewer crosses Monument Hill Road and ties into a 42" storm sewer which flows under I-25 to outfall west of I-25. An existing

and outfalls into the I-25 right of way where it then enters another storm sewer that outfalls to the west of I-25.

The property lies within the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) panel 08041C0276G dated December 18, 2018. Based on a review of the FIRM panel, the Site is located within Flood Zone X which is designated as an area determined to be outside the 0.2% (500-year) annual chance floodplain (see Appendix A).

The NRCS soil survey indicates that the soil on site is primarily Tomah-Crowfoot loamy sands and Tomah-Crowfoot complex, whose hydrologic soil group is Type B. A soil map has been included in the appendix for reference.

## Drainage Basins and Subbasins

### Existing Major Basin Description

The Site is located within the Crystal Creek Drainage Basin. The Crystal Creek Basin outfalls to Monument Lake. The Site is included in the *Dirty Woman Creek and Crystal Creek Drainage Basin Planning Study, prepared by Kiowa Engineering Corporation, dated September 1993. The Final Drainage Report for Palmer Ridge High School, prepared by Tetra Tech, dated July 3, 2007* (PRHS Report) also includes a small portion of the site. Both of these previous drainage reports focus primarily on the flows entering and flowing through Crystal Creek. The flows from the site flow west crossing under I-25 before flowing southwest in an undefined channel towards Crystal Creek and eventually Monument Lake.

### Existing Subbasin Description

The Site currently is made up of three existing basins that are all part of the Crystal Creek Drainage Basin. Basin A is the north basin that is 2.35 acres and drains east to west to an existing 18" storm sewer at Design Point A that eventually outfalls west of I-25. Basin A has a total surface runoff of 1.5 cfs in the 10-year event and 4.6 cfs in the 100-year event at Design Point A. These flows are the total basin flows from Basin A, not the routed flows at Design Point A. Basin B is the largest existing basin with 7.40 acres flowing northeast to southwest into an existing 24" storm sewer at Design Point B. This existing storm sewer outfalls on the west side of Monument Hill Road where the flow enters another storm sewer to eventually outfall west of I-25. Basin B has a total surface runoff of 3.7 cfs in the 10-year event and 11.4 cfs in the 100-year event at Design Point B. These flows are the total basin flows from Basin B, not the routed flows at Design Point B. Both Basin A and B flow in an undefined channel on the west side of I-25 to the southwest until eventually making it to Monument Lake. Basin C is the south basin on the site with 1.86 acres flowing east to southwest. Basin C has a total surface runoff of 1.1 cfs in the 10-year event and 3.4 cfs in the 100-year event at Design Point C. These flows are the total basin flows from Basin C, not the routed flows at Design Point C. The runoff from this basin currently enters a roadside ditch on the east side of Monument Hill Road where it flows south away from the site to eventually enter Crystal Creek. An Existing Conditions Map is included in Appendix E.

There are four existing off-site basins that currently flow onto the site or into the Monument Hill Road swale adjacent to the Site. Basin OSA1 is a west portion of the Palmer Ridge High School that includes the school's west entrance and a detention pond. Basin OSA1 is 0.75 acres and flows northeast to southwest where it enters the existing 24" storm sewer at Design Point A. The flow from Basin OSA1 at Design Point A is 2.0 cfs in the 10-year event and 3.4 cfs in the 100-year event. These flows are the total basin flows from Basin OSA1, not the routed flows at Design Point A. Basin EP1 represents Detention Pond B from the PRHS Report. According to the PRHS Report the 100-year release rate from the existing pond is 35.33 cfs at Design Point A. Basin OSB1 is a southwest portion of the Palmer Ridge High School that includes field, lawn, and parts of the school's track. Basin OSB1 is 1.14 acres and flows east to west on to the Site. The runoff then flows through Basin B until it reaches the existing 24" storm sewer at Design Point B. The flow generated from Basin OSB1 at Design Point B is 0.8 cfs in the 10-year event and 2.5 cfs in the 100-year event. These flows are the total basin flows from Basin OSB1, not the routed flows at Design Point B. Basin OSB2 is the east half section of Monument Hill Road and its road side ditch. Basin OSB2 is 0.76 acres and flows east to west into the road side ditch then south towards Design Point B. The runoff then flows through the existing 24" storm sewer at Design Point B. The flow generated from Basin OSB2 at Design Point B is 1.5 cfs in the 10-year event and 2.6 cfs in the 100-year event. These flows are the total basin flows from Basin OSB2, not the routed flows at Design Point B. The largest existing offsite basin is Basin OSC1 at 1.91 acres. Basin OSC1 is the southwest corner of the Palmer Ridge High School and includes field, lawn, and parts of the school's track. Basin OSC1 flows northeast to southwest flowing through Basin C until it reaches the roadside ditch next to Monument Hill Road at Design Point C. The flow generated from Basin OSC1 is 1.0 cfs in the 10-year event and 3.0 cfs in the 100-year event. These flows are the total basin flows from Basin OSC1, not the routed flows at Design Point C.

After routing flows from off-site and on-site basins through the Standard SF form for the 10-year and 100-year storm events the existing drainage values were found:

Design Point A has a combined 3.07 cfs for the 10-year event from Basins A1 and Basin OSA1. Design Point A has a combined 7.27 cfs for the 100-year event from Basins A1 and Basin OSA1. The Existing Pond B from the Lewis Palmer Ridge High School Drainage Report has an emergency overflow that is tributary to Design Point A. Assuming the outlet structure is completely clogged Design Point A would receive an extra 35.33 cfs.

Design Point B has a combined 5.53 cfs for the 10-year event from Basins B1 and Basin OSB1. Design Point B has a combined 15.26 cfs for the 100-year event from Basins B1 and Basin OSB1.

Design Point C has a combined 1.97 cfs for the 10-year event from Basins C1 and Basin OSC1. Design Point C has a combined 6.02 cfs for the 100-year event from Basins C1 and Basin OSC1.

## Drainage Design Criteria

This Report has been prepared in accordance with the *El Paso County Drainage Criteria Manual Volume 1 & 2 October 2018*. Supplemental information is taken from the *Mile High Flood District Urban Storm Drainage Criteria Manual Volumes 1, 2 and 3*.

Water Quality is required to be provided on the site and the developed 100-year release rate is 90% of the predeveloped flow from the Site. Existing storm sewers are located in the northwest and southwest corners of the site within drainage easements. The pond sizing and outlet design was done through the Mile High Flood District Detention v4-06 spreadsheet. A tributary area table is provided in Appendix B. The table shows that the area on-site the is tributary to the pond is 10.98 acres at 77% imperviousness. The Full Spectrum Pond will also accept water from 5 off-site basins for a total of 3.2 acres. The Full Spectrum Pond was sized for the full site of 11.38 acres. The Full Spectrum Pond is over detaining runoff to offset the runoff not detained on-site. The pond is not sized to detain the additional runoff from the off-site basins but the emergency overflow is sized to be able to pass the developed 100-year runoff plus the additional off-site runoff. The outlet of the proposed full spectrum pond is planned to discharge into the existing roadside ditch and enter the existing 24” storm sewer near the southwest of the Site. The full spectrum pond will be designed so the release of the 100-year runoff will be restricted to a release rate equal to or less than 90% of the predeveloped runoff. It was estimated that the predeveloped 10-year runoff to be 4.0 cfs and the 100-year runoff to be 11.7 cfs. For the purpose of this Report, the 100-year storm event will be released from the pond at a rate of 10.4 cfs. The release rate of 10.4 cfs was chosen since it is 88.9% of the predeveloped runoff.

The hydrologic design was computed using the Rational Method as defined by El Paso County Drainage Criteria Manual. The 10-year storm was used as the minor storm event, while the 100-year storm was used as the major event. The one-hour point rainfall depth used for the 10-year storm was 1.75 inches and 2.52 inches for the 100-year event. The Rational Method was used to analyze fully developed conditions. Hydraulic grade lines were calculated using Haestad’s StormCadd and are attached in the appendices. On-site detention includes a full spectrum detention pond with water quality control volume, excess urban runoff volume, and the 100-year flood volume. The 100-year release is required to be less than 10.4 cfs. Inlets were sized using the UD-Inlet\_V4.06 spreadsheet. The full spectrum pond was sized using the MHFD-Detention\_v4.06 spreadsheet.

## Runoff/Proposed Basin Description

### Major Basins

The Site in its development condition includes 3 primary Basins described as Basins A, B, and C. The Proposed Drainage Map in included in Appendix E. Basin B is the largest basin with 10.58 acres on-site plus an additional 3.88 acres of an off-site basin tributary to it. Basin B consists of 30 on-site basins and 8 off-site basins. The on-site basins are numbered B1 through B30 and the off-site basins are numbered OSB1 through OSB8. Basin A has 0.12

acres on-site plus an additional 0.71 acres of an off-site tributary to it. Basin C has 0.11 acres on-site and no off-site basins.

### Sub-Basins

#### Basin A1 (0.09 Acres):

Basin A1 represents the northwest edge of the Site and includes the portion of the roadside ditch along Monument Hill Road that is located on the site. Basin A1 is tributary to the existing 18” storm sewer located in the northwest of the Site and discharges under Monument Hill Road and to the west side of I-25. This Basin has an overall imperviousness of 0%. This Basin it not tributary to the proposed full spectrum pond. Water quality is not required for this basin because under exclusion I.7.1.B.7 the land is undeveloped and will remain undeveloped.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 0.1 \text{ CFS} \quad Q_{100} = 0.2 \text{ CFS}$$

#### Basin OSA1 (0.71 Acres)

Basin OSA1 consists of a portion of the Palmer Ridge High School site and the east half section of Monument Hill Road. This basin all flows to the road side ditch and is tributary to the northwest existing storm sewer. This Basin has an overall imperviousness of 63%.

$$C_{10} = 0.64 \quad C_{100} = 0.74$$

$$Q_{10} = 2.4 \text{ CFS} \quad Q_{100} = 4.0 \text{ CFS}$$

The combined Basin A 100-year overland routed runoff of 3.51 CFS discharges to the existing 18” storm sewer at Design Point A and will not be routed through the proposed full spectrum pond.

## Basin B1 (0.53 Acres)

Basin B1 consists of parking lot, sidewalk, and landscape islands located to the west of proposed Building. It will also receive the water from a portion of the roof in basin B16. The grades of this Basin generally slope at 3% and 4%. Runoff will sheet flow to a 2-foot concrete drainage pan where the concentrated flow will be collected in a Triple Type 13 Inlet at Design Point 1 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 64%. Emergency overflow from this Basin will route to the next downstream Sub-basin, B2.

$$C_{10} = 0.64 \quad C_{100} = 0.74$$

$$Q_{10} = 2.0 \text{ CFS} \quad Q_{100} = 3.4 \text{ CFS}$$

## Basin B2 (0.48 Acres)

Basin B2 consists of parking lot, sidewalk, and landscape islands located to the west of proposed Building B. It will also receive the water from a portion of the roof in basins B17 and B18. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a 2-foot concrete drainage pan where the concentrated flow will be collected in a Triple Type 13 Inlet at Design Point 2 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 73%.

$$C_{10} = 0.71 \quad C_{100} = 0.80$$

$$Q_{10} = 2.0 \text{ CFS} \quad Q_{100} = 3.2 \text{ CFS}$$

## Basin B3 (0.30 Acres)

Basin B3 consists of parking lot, sidewalk, and landscape islands located to the west of the proposed building. This basin also includes the north entrance into the site. It will also receive the water from a portion of the roof in basin B19 and the off-site basin OSB7. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow away from the proposed building to the curb and gutter on the west side. The concentrated flow will be then be conveyed through a curb chase at Design Point 3 and conveyed to the next downstream basin, B4. This Basin has an overall imperviousness of 95%.

$$C_{10} = 0.88 \quad C_{100} = 0.93$$

$$Q_{10} = 1.6 \text{ CFS} \quad Q_{100} = 2.4 \text{ CFS}$$

## Basin B4 (0.19 Acres)

Basin B4 consists of parking lot, sidewalk, and landscape islands located to the west of the proposed building. It will also receive the water from a portion of the roof in basin B20. The grades of this Basin generally slope at 3%. Runoff will sheet flow away from the proposed building to the curb and gutter on the west side. The concentrated flow will be then be conveyed to a 10' Type R Inlet at Design Point 4 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 100%.

$$C_{10} = 0.92 \quad C_{100} = 0.96$$

$$Q_{10} = 1.0 \text{ CFS} \quad Q_{100} = 1.5 \text{ CFS}$$

## Basin B5 (0.40 Acres)

Basin B5 consists of parking lot, sidewalk, and landscape islands located to the west and south of the proposed building. It will also receive the water from a portion of the roof in basin B21. The grades of this Basin generally slope at 3% and 7%. Runoff will sheet flow away from the proposed building to the curb and gutter on the west side. The concentrated flow will be then be conveyed to a Single Type 13 Combo Inlet at Design Point 5 and conveyed to the proposed Full spectrum pond via storm sewer. This Basin has an overall imperviousness of 82%. Emergency overflow from this Basin will overtop of curb and enter the proposed full spectrum pond.

$$C_{10} = 0.78 \quad C_{100} = 0.85$$

$$Q_{10} = 1.8 \text{ CFS} \quad Q_{100} = 2.9 \text{ CFS}$$

## Basin B6 (0.31 Acres)

Basin B6 consists of parking lot, sidewalk, landscape islands, and landscape buffer located to the north of proposed Building. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a 2-foot concrete drainage pan where the concentrated flow will be collected in a Single Type 13 Inlet at Design Point 6 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 68%.

$$C_{10} = 0.68 \quad C_{100} = 0.77$$

$$Q_{10} = 1.2 \text{ CFS} \quad Q_{100} = 2.0 \text{ CFS}$$

## Basin B7 (0.40 Acres)

Basin B7 consists of parking lot, sidewalk, landscape islands, and landscape buffer located to the north of proposed Building. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a 2-foot concrete drainage pan where the concentrated flow will be collected in a Single Type 13 Inlet at Design Point 7 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 58%. Emergency overflow from this Basin will route to the next downstream Basin, B6.

$$C_{10} = 0.60 \quad C_{100} = 0.70$$

$$Q_{10} = 1.4 \text{ CFS} \quad Q_{100} = 2.4 \text{ CFS}$$

## Basin B8 (0.98 Acres)

Basin B8 consists of loading dock and landscape islands located to the east of proposed Building. It will also receive the water from a portion of the roof in basin B22. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a 10-foot concrete drainage pan where the concentrated flow will be collected in a Double Type 13 Inlet at Design Point 8 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 68%.

$$C_{10} = 0.68 \quad C_{100} = 0.77$$

$$Q_{10} = 3.9 \text{ CFS} \quad Q_{100} = 6.4 \text{ CFS}$$

## Basin B9 (0.59 Acres)

Basin B9 consists of loading dock and landscape islands located to the east of proposed Building. It will also receive the water from a portion of the roof in basin B23. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a 10-foot concrete drainage pan where the concentrated flow will be collected in a on grade Single Type 13 Inlet at Design Point 9 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 71%. Emergency overflow from this Basin will route to the next downstream Basin, B10.

$$C_{10} = 0.70 \quad C_{100} = 0.78$$

$$Q_{10} = 2.4 \text{ CFS} \quad Q_{100} = 3.9 \text{ CFS}$$

## Basin B10 (0.67 Acres)

Basin B10 consists of loading dock located to the east of proposed Building. It will also receive the water from the offsite basin OSB1 and a portion of the roof in basin B24. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a 10-foot concrete drainage pan where the concentrated flow will be collected in a Triple Type 13 Inlet at Design Point 10 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 83%.

$$C_{10} = 0.79 \quad C_{100} = 0.85$$

$$Q_{10} = 3.1 \text{ CFS} \quad Q_{100} = 4.9 \text{ CFS}$$

## Basin B11 (0.37 Acres)

Basin B11 consists of loading dock and landscape islands located to the east of proposed Building. It will also receive the water from the off-site basin OSB2 and a portion of the roof in basin B25. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a curb and gutter on the west side of the drive aisle where the concentrated flow will be collected in a 5' Type R Inlet at Design Point 11 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 74%.

$$C_{10} = 0.72 \quad C_{100} = 0.80$$

$$Q_{10} = 1.6 \text{ CFS} \quad Q_{100} = 2.5 \text{ CFS}$$

## Basin B12 (0.75 Acres)

Basin B12 consists of loading dock located to the east of proposed Building. It will also receive the water from the off-site basin OSB3 and a portion of the roof in basin B26. The grades of this Basin generally slope between 3% to 5%. Runoff will sheet flow to a curb and gutter on the east side of the drive aisle where the concentrated flow will be collected in an on-grade Triple Type 13 Combo Inlet at Design Point 12 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 89%. Emergency overflow from this Basin will route to the next downstream Basin, B13.

$$C_{10} = 0.83 \quad C_{100} = 0.89$$

$$Q_{10} = 3.6 \text{ CFS} \quad Q_{100} = 5.6 \text{ CFS}$$

## Basin B13 (0.43 Acres)

Basin B13 consists of loading dock and landscaping located to the east and south of proposed Building. It will also receive the water from the off-site basin OSB4 and a portion of the roof in basin B27. The grades of this Basin generally slope between 3% to 7%. Runoff will sheet flow to a curb and gutter on the west side of the drive aisle where the concentrated flow will be collected in a 10' Type R Inlet at Design Point 13 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 81%. Emergency overflow from this Basin will route to the next downstream Basin, B14.

$$C_{10} = 0.77 \quad C_{100} = 0.84$$

$$Q_{10} = 2.0 \text{ CFS} \quad Q_{100} = 3.1 \text{ CFS}$$

## Basin B14 (0.08 Acres)

Basin B14 consists of drive aisle and landscape islands located to the south of proposed Building. The grades of this Basin generally slope between 3% to 7%. Runoff will sheet flow to a curb and gutter where the concentrated flow will be collected in a Single Type 13 Combo Inlet at Design Point 14 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 87%.

$$C_{10} = 0.82 \quad C_{100} = 0.88$$

$$Q_{10} = 0.4 \text{ CFS} \quad Q_{100} = 0.6 \text{ CFS}$$

## Basin B15 (0.11 Acres)

Basin B15 consists of a loading dock area and landscape islands located to the east of proposed Building. It will also receive the water from the off-site basin OSB5. The grades of this Basin generally slope between 4% to 8%. Runoff will sheet flow to a curb and gutter on the north side of the entrance drive where the concentrated flow will be collected in a on grade Triple Type 13 Combo Inlet at Design Point 15 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 97%.

$$C_{10} = 0.90 \quad C_{100} = 0.94$$

$$Q_{10} = 0.6 \text{ CFS} \quad Q_{100} = 0.9 \text{ CFS}$$

## Basin B16 (0.30 Acres)

Basin B16 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to grade through a drainage chase located on the west side of proposed Building into Basin B1. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B17 (0.30 Acres)

Basin B17 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to grade through a drainage chase located on the west side of proposed Building into Basin B2. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B18 (0.30 Acres)

Basin B18 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to grade through a drainage chase located on the west side of proposed Building into Basin B2. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B19 (0.30 Acres)

Basin B19 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to grade through a drainage chase located on the west side of proposed Building into Basin B3. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B20 (0.30 Acres)

Basin B20 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to grade through a drainage chase located on the west side of proposed Building into Basin B4. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B21 (0.30 Acres)

Basin B21 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to grade through a drainage chase located on the west side of proposed Building into Basin B5. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B22 (0.42 Acres)

Basin B22 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to the east side of proposed Building into Basin B8. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.8 \text{ CFS} \quad Q_{100} = 2.9 \text{ CFS}$$

## Basin B23 (0.36 Acres)

Basin B23 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to the east side of proposed Building into Basin B9. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.6 \text{ CFS} \quad Q_{100} = 2.5 \text{ CFS}$$

## Basin B24 (0.30 Acres)

Basin B24 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to the east side of proposed Building into Basin B10. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.0 \text{ CFS}$$

## Basin B25 (0.30 Acres)

Basin B25 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to the east side of proposed Building into Basin B11. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.84$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B26 (0.30 Acres)

Basin B26 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to the east side of proposed Building into Basin B12. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B27 (0.30 Acres)

Basin B27 consists of a portion of the proposed roof. The slope of the rooftop is 2.5% and runoff will sheet flow to a roof drain. Runoff will then discharge to the east side of proposed Building into Basin B13. This Basin has an overall imperviousness of 90%.

$$C_{10} = 0.75 \quad C_{100} = 0.81$$

$$Q_{10} = 1.3 \text{ CFS} \quad Q_{100} = 2.1 \text{ CFS}$$

## Basin B28 (0.06 Acres)

Basin B28 consists of a portion of the roadside ditch next to Monument Hill Road that is on site. The grades of this Basin generally slope between 4% to 15%. Runoff will sheet flow to roadside ditch where the concentrated flow will be conveyed under the north entrance to the south half of the roadside ditch via an 18" culvert at design point RC1. This Basin has an overall imperviousness of 0%. This Basin it not tributary to the proposed full spectrum pond. Water quality is not required for this basin because under exclusion I.7.1.B.7 the land is undeveloped and will remain undeveloped.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 0.0 \text{ CFS} \quad Q_{100} = 0.1 \text{ CFS}$$

## Basin B29 (0.38 Acres)

Basin B29 consists of a portion of the roadside ditch next to Monument Hill Road and landscaping. The grades of this Basin generally slope between 4% to 33%. Runoff will sheet flow to the Monument Hill Road roadside ditch where the concentrated flow will be collected by the existing southwest 24" storm sewer at design point B. It will then be conveyed to the west side of I-25 via the existing storm sewer. This Basin has an overall imperviousness of 0%. This Basin it not tributary to the proposed full spectrum pond. Water quality is not required for this basin because under exclusion I.7.1.B.7 the land is undeveloped and will remain undeveloped.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 0.2 \text{ CFS} \quad Q_{100} = 0.8 \text{ CFS}$$

## Basin B30 (0.61 Acres)

Basin B30 consists of the proposed full spectrum pond that include lawn and the gravel access road. The sides of the full spectrum pond will be 33% except for the access road that is a max of 10%. The runoff will sheet flow down to the trickle channel where the concentrated flow will then flow west to the outlet structure. This basin has an overall imperviousness of 3%.

$$C_{10} = 0.08 \quad C_{100} = 0.44$$

$$Q_{10} = 0.3 \text{ CFS} \quad Q_{100} = 1.9 \text{ CFS}$$

## Basin B31 (0.02 Acres)

Basin B31 consists of road at the central entrance of the site along Monument Hill Road. The basin will drain northeast to southwest into the curb at the south side of the entrance. The concentrated gutter flow will then discharge into the road side ditch and flow to Design Point B. This basin has an overall imperviousness of 100%. This Basin is not tributary to the proposed full spectrum pond. Water quality is not required for this basin because under exclusion I.7.1.C.1 that allows for 20%, not to exceed 1 acre, of the development to not be captured for water quality.

$$C_{10} = 0.87 \quad C_{100} = 0.90$$

$$Q_{10} = 0.1 \text{ CFS} \quad Q_{100} = 0.1 \text{ CFS}$$

## Basin OSB1 (0.08 Acres)

Basin OSB1 consists of lawn and field on the west edge of the Palmer Ridge School Site. The grades of this Basin generally slope between 6% to 8%. Runoff will sheet flow to the southwest onto the site and enter the curb and gutter in basin B10. Where the concentrated flow will be collected in a Triple Type 13 Inlet at Design Point 10 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 0%.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 0.1 \text{ CFS} \quad Q_{100} = 0.2 \text{ CFS}$$

## Basin OSB2 (0.34 Acres)

Basin OSB2 consists of lawn, field, and a portion of the school's track on the west edge of the Palmer Ridge School Site. The grades of this Basin generally slope between 1% to 12%. Runoff will sheet flow to the west onto the site and enter the curb and gutter in basin B11. Where the concentrated flow will be collected in a 5' Type R Inlet at Design Point 11 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 0%.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 0.2 \text{ CFS} \quad Q_{100} = 0.8 \text{ CFS}$$

## Basin OSB3 (0.78 Acres)

Basin OSB3 consists of lawn, field, and a portion of the school's track on the west edge of the Palmer Ridge School Site. The grades of this Basin generally slope between 1% to 25%. Runoff will sheet flow to the west onto the site and enter the curb and gutter in basin B12. Where the concentrated flow will be collected in a Triple Type 13 Combo Inlet at Design Point 12 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 0%.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 0.6 \text{ CFS} \quad Q_{100} = 1.9 \text{ CFS}$$

## Basin OSB4 (1.88 Acres)

Basin OSB4 consists of lawn, field, and a portion of the school's track on the west edge of the Palmer Ridge School Site. The grades of this Basin generally slope between 1% to 25%. Runoff will sheet flow to the west onto the site and enter the curb and gutter in basin B13. Where the concentrated flow will be collected in a 10' Type R Inlet at Design Point 13 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 0%.

$$C_{10} = 0.15 \quad C_{100} = 0.35$$

$$Q_{10} = 1.1 \text{ CFS} \quad Q_{100} = 3.7 \text{ CFS}$$

## Basin OSB5 (0.06 Acres)

Basin OSB5 consists of landscaping, parking lot, and drive aisle between the site and Case Camp Road to the southeast. The grades of this Basin generally slope between 3% to 7%. Runoff will sheet flow to the northwest onto the site and enter the curb and gutter in basin B15. Where the concentrated flow will be collected in a 5' Type R Inlet at Design Point 15 and conveyed to the proposed full spectrum pond via storm sewer. This Basin has an overall imperviousness of 71%.

$$C_{10} = 0.70 \quad C_{100} = 0.78$$

$$Q_{10} = 0.2 \text{ CFS} \quad Q_{100} = 0.4 \text{ CFS}$$

## Basin OSB6 (0.21 Acres)

Basin OSB6 consists of a half section of Monument Hill Road and a portion of the roadside ditch to the west of the site. The grades of this Basin generally slope between 2% to 20%. Runoff will sheet flow to the southeast and enter the roadside ditch. Where the concentrated flow will be conveyed under the north entrance of the site to the south half of the roadside ditch, via an 18” culvert at Design Point RC1. This Basin has an overall imperviousness of 49%. This basin it not tributary to the proposed full spectrum pond.

$$C_{10} = 0.53 \quad C_{100} = 0.65$$

$$Q_{10} = 0.6 \text{ CFS} \quad Q_{100} = 1.0 \text{ CFS}$$

## Basin OSB7 (0.05 Acres)

Basin OSB7 consists of a half section of Monument Hill Road and the north connection to the site. The grades of this Basin generally slope between 2% to 4%. Runoff will sheet flow to the southeast enter the site through the north entrance. The sheet flow will be collected in the curb and gutter in Basin B3. This Basin has an overall imperviousness of 100%.

$$C_{10} = 0.92 \quad C_{100} = 0.96$$

$$Q_{10} = 0.3 \text{ CFS} \quad Q_{100} = 0.4 \text{ CFS}$$

## Basin OSB8 (0.47 Acres)

Basin OSB8 consists of a half section of Monument Hill Road and a portion of the roadside ditch to the west of the site. The grades of this Basin generally slope between 2% to 33%. Runoff will sheet flow to the southeast and enter the roadside ditch. Where the concentrated flow will be collected by the existing southwest 24” storm sewer at design point B. It will then be conveyed to the west side of I-25 via the existing storm sewer. This Basin has an overall imperviousness of 65%. This Basin it not tributary to the proposed full spectrum pond.

$$C_{10} = 0.65 \quad C_{100} = 0.75$$

$$Q_{10} = 1.6 \text{ CFS} \quad Q_{100} = 2.7 \text{ CFS}$$

The combined Basin B 100-year runoff of 54.14 cfs that discharges to the proposed full spectrum pond at Design Point O-1 and 1.31 cfs at Design Point O-2. Basins B28 and B29 combine with Basins OSB6 and OSB8 in the roadside ditch adjacent to Monument Hill Road to discharge into the existing 24” storm sewer at Design Point B. The previously mentioned basins have a combined 100-year runoff of 4.29 cfs that enters the roadside ditch without being routed through the full spectrum pond. This flow of 4.29 cfs then combines with the

100-year release from the full spectrum pond of 10.4 cfs and enters the 24” existing storm sewer at Design Point B. Since, the full spectrum pond delays the release on the 100-year event, the peak flow at Design Point B is 10.4 cfs.

Basin C1 (0.22 Acres):

Basin C1 represents the southwest edge of the site and includes the south entrance road. Basin C1 will sheet flow south to enter the Monument Hill Road roadside ditch that runs south from the site. This Basin has an overall imperviousness of 80%. Water quality is not required for this basin because under exclusion I.7.1.C.1 that allows for 20%, not to exceed 1 acres, of the development to not be captured for water quality.

$$C_{10} = 0.76 \quad C_{100} = 0.84$$

$$Q_{10} = 1.0 \text{ CFS} \quad Q_{100} = 1.6 \text{ CFS}$$

Basin C has a total 100-year runoff of 1.6 cfs that discharges to the existing roadside ditch next to Monument Hill Road without being routed through the proposed full spectrum pond.

Under exclusion I.7.1.B.7 the project is allowed to have 20%, not to exceed 1 acre of development to not be captured and treated for water quality. There are 5 on-site basin that are not captured and treated that sum to 0.77 acres. These basins are Basins A1, B28, B29, B31, and C1.

The proposed drainage design will decrease 100-year flows going to the existing storm sewer at Design Point A from 7.27 cfs to 3.51 cfs. With the restriction of the outflows from the proposed full spectrum pond, the 100-year flows at Design Point B will decrease from 15.26 cfs to 10.4 cfs. It will decrease the 100-year flows entering the roadside ditch next to Monument Hill Road at Design Point C from 6.02 cfs to 1.6 cfs. These values and calculations can be found in Appendix B in the Existing and Developed SF Form Tables. The proposed Site will not have an adverse impact on existing downstream conveyance systems.

### **Stormwater Detention and Water Quality Design**

Runoff from the Site will surface flow and be piped to a full spectrum pond located near the southwest corner of the Site. The full spectrum pond has been sized using the MHFD-Detention\_v4.06 spreadsheet to meet the El Paso County Drainage Criteria Manual Standards. The full spectrum pond has been sized to provide Water Quality Control Volume (WQCV), Excess Urban Runoff Volume (EURV) and 100-year flood protection for the developed Site. The full spectrum pond has been sized for 11.4 acres with a watershed imperviousness of 77%. The area that is tributary to the pond is 10.98 acres however, 11.4 acres was used to size the pond to over detain stormwater on the site. This was done offset the stormwater that is not being detained on-site. The full spectrum pond is approximately 80 feet by 230 feet in size. Runoff enters the full spectrum pond via a forebay at the east end of the pond, Forebay O-1, and an 18” FES at about the midpoint of the south side of the pond, Design Point O-2. Forebay O-1 notch was calculated at 5.7 inches wide to release at 1.08 cfs. The calculation

for Forebay O-1 were made using the UD-BMP v3.07 from Mile High Flood District. The required WQCV is 0.294 ac-ft. The micropool water surface elevation and outlet pipe are at a water surface elevation of 7134.23. The WQCV provided is 0.294 ac-ft at an elevation of 7137.55. The WQCV is drained through an orifice plate that has four 1-1/4" diameter with 23" between the bottom two holes and 15" spacing for the top two holes. The 99% drain time for the WQCV is 40 hours. The EURV storage provided by the full spectrum pond is 0.675 ac-ft at an elevation of 7140.11. The EURV will be drained from the full spectrum pond through the same orifice plate as the WQCV. In the 100-year storm event, runoff overtops the overflow weir and is released through an 18" storm sewer with a restrictor plate. The restrictor plate will be 8.5 inches above the invert of the 18" pipe. An additional 0.518 ac-ft volume is provided in the full spectrum pond for the release of the 100-year runoff. The 100-year runoff will pond to an elevation of 7141.64 and will discharge at a maximum of 10.4 cfs into the roadside ditch next to Monument Hill Road. The 99% drain time of the 100-year volume is 76 hours. A concrete emergency spillway is provided on the west side of the full spectrum pond. The spillway crest length is 20 feet with an invert elevation of 7142.00. The spillway end slopes are 5H:1V. The emergency spillway discharges into the roadside ditch next to Monument Hill Road. The spillway was over sized to allow the flows from offsite to be bypassed over the spillway in the 100-year event. The full spectrum pond calculations are included in Appendix C.

A 15' wide maintenance access road is provided to the outlet structure of the proposed full spectrum pond.

The County of El Paso requires the UDFCD Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the WQCV, stabilizing drainageways, and implementing long-term source controls. The four steps and how they are implemented into the proposed design is below:

- 1) Step one is Employ Runoff Reduction Practices.
  - The existing roadside ditch on the west side of the site are being conserved and landscaping islands are being used. With the grades on site, there are no more opportunities to implement Runoff Reduction Practices.
- 2) Step two is Stabilize Drainage Ways.
  - No stream is located within the vicinity of this project so step three does not apply. Stormwater runoff from the Site is being provided water quality treatment and discharged into a storm sewer system rather than flowing directly into the Monument Hill Road roadside ditch. The Monument Hill Road roadside ditch is located on the west property line. This project will benefit the Monument Hill Road roadside ditch by reducing the amount of sediment tributary to the ditch from the Site and by improving the embankment and running slope of the ditch.
- 3) Step three is Provide a Water Quality Capture Volume.
  - Water Quality Capture Volume is provided in the full spectrum pond and is released over a period of 40 hours. Which lowers the peak flow at the existing storm sewer in the Monument Hill Road roadside ditch.

- 4) Step four is Identify Best Management Practices to be used to control industrial and commercial pollutants.
  - All parking, driving aisle, and loading docks drain to the proposed storm sewer system and are discharged into the full spectrum pond. This will remove pollutants from the commercial runoff.

### Drainage Fees

The Site will require \$23,078 per Impervious Acre for the 2023 Drainage Fee and an additional \$1,262 per Impervious Acre for the 2023 Bridge Fee. With 9.04 acres of impervious area, the Site will require a Drainage Fee of \$208,625.12. With 9.04 acres of impervious area, the Site will require a Bridge Fee of \$11,408.48. The impervious area was determined by add all on-site areas on the SF form that include roof, drive/walk, and gravel road. This calculation can be seen in the table called Impervious Area Table in Appendix B.

$$\begin{aligned} \$23,078 \text{ per Impervious Acre} &= \$23,078 * 9.04 = \$208,625.12 \\ \$1,262 \text{ per Impervious Acre} &= \$1,262 * 9.04 = \$11,408.48 \end{aligned}$$

### Erosion Control Plan

A Grading and Erosion Control Plan will be submitted to the County for review and approval prior to construction.

### Construction Cost Estimate

Storm sewer and water quality are required for the Site. All drainage and detention facilities are private and non-reimbursable. The storm infrastructure includes RCP storm sewer, inlets and manholes. The full spectrum pond includes an outlet structure and spillway. Below is a cost estimate for the private storm facilities and the full spectrum pond.

	QUANTITY	UNIT	UNIT PRICE	TOTAL COST
<b>Strom Sewer</b>				
18" RCP (0-8' depth)	1,150	LF	\$50.00	\$57,500
24" RCP (0-8' depth)	1,150	LF	\$65.00	\$74,750
36" RCP (0-8' depth)	654	LF	\$100.00	\$65,400
5' Dia. Manhole	20	EA	\$4,500.00	\$90,000
5' Type 'R' Inlet	2	EA	\$4,750.00	\$9,500
6' Dia. Manhole	2	EA	\$6,000.00	\$12,000
10' Type 'R' Inlet	1	EA	\$6,500.00	\$6,500
18" Flared End Section	4	EA	\$1,350.00	\$5,400
Type '13' Inlet	22	EA	\$3,500.00	\$77,000
Type 'VL' Rip Rap	1,270	CY	\$110.00	\$139,700
Type 'VH' Rip Rap - Spillway	2,400	CY	\$100.00	\$240,000
Concrete Drainage Pan	1,255	LF	\$5.00	\$6,275
Cutoff Wall - Spillway	10	CY	\$1,250.00	\$12,500
Pond Gravel Access Road	4,385	SY	\$10.00	\$43,850
Forebay (36"-42" Inlet)	1	EA	\$15,000.00	\$15,000
Pond Outlet Structure	1	EA	\$15,000.00	\$15,000
Trickle Channel	200	LF	\$90.00	\$18,000
			<b>Subtotal</b>	<b>\$888,375</b>
			<b>15% Contingency</b>	<b>\$133,256</b>
			<b>TOTAL COST</b>	<b>\$1,021,631</b>

## Other Government Agency Requirements

The proposed drainage improvements on The Rock Commerce Center will not require any other agency approval. It is not with the FEMA floodplain so will not require further review or floodplain map revisions. The full spectrum pond's spillway will not need review by the State Engineer's office since it is less than 10' in height at the centerline of the spillway

## Conclusion

The proposed drainage improvements on The Rock Commerce Center will have no adverse effects to the surrounding properties, downstream storm conveyance system, or regional drainage facilities. The Site was designed in compliance with the El Paso County Stormwater Criteria. The Site development proposed is in conformance with the approved land use and zoning. This Report and its findings are in conformance with all pertinent studies related to this site. The existing roadside ditches along Monument Hill Road are in stable condition currently. The existing ditch will require new erosion control measures during and post construction. This project will require the regrading of the road side ditches so their current state will be improved. The culvert within the road side ditch running under the proposed access drive will require type VL riprap at its outlet. There will be erosion control blanket placed in the road side ditch north of the culvert but no riprap is required for protection. In the 100-year event the velocity is 1.15 fps within the road side ditch. This velocity is less than the velocities stated in table 10-4. The subcritical flow value is also less than the riprap requirements listed in table 10-6. The two culverts under I-25 currently have permanent inlet protection and new permanent inlet protection is being installed with the public improvement plans submitted with this project. The existing culverts will also be receiving less flow than in the current conditions and the flow capacity calculations are included in Appendix B of this Report.

## References

### **REFERENCES**

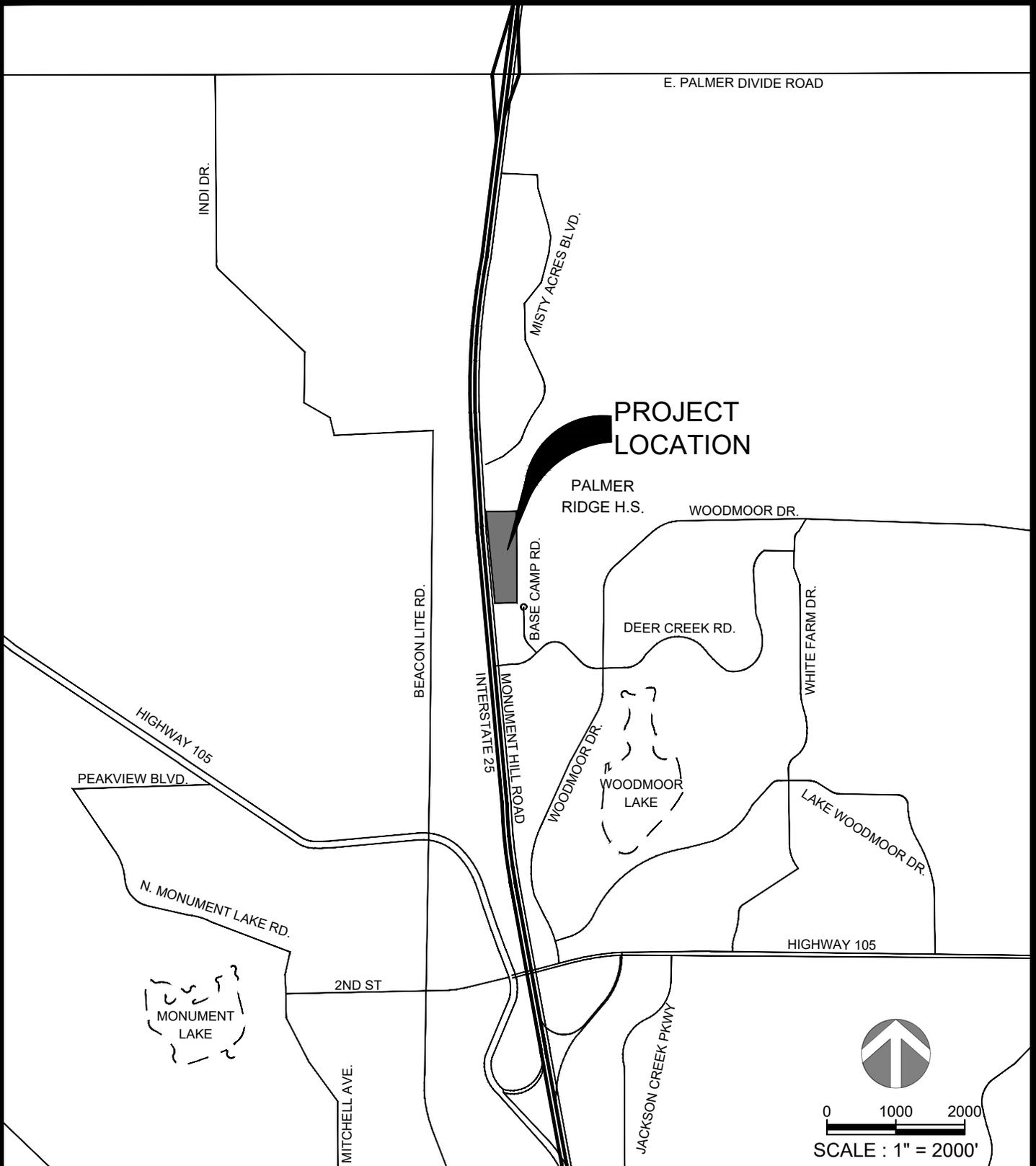
1. *Drainage Criteria Manual Volumes 1 & 2, El Paso County. October 2018.*
2. *Mile High and Flood District, Denver, Colorado, Urban Storm Drainage Criteria Manual, Volume 1-3, latest online addition.*
3. *The El Paso County Drainage Basin Map (DBMP), El Paso County Board of Commissioners, 2005*
4. *Final Drainage Report for Palmer Ridge High School, Monument, Colorado, Tetra Tech, July 3, 2007*



720.283.6783 Office  
1500 West Canal Court  
Littleton, Colorado 80120  
[REDLAND.COM](http://REDLAND.COM)

Appendix A - Vicinity Map, FIRM Map, Soils Map

C:\Users\csalzi\appdata\local\temp\AcPublish\_22880\23009\_Vicinity\_Map.dwg tab: Layout1 Jul 27, 2023 - 4:26pm csalzi



**PROJECT  
LOCATION**



0 1000 2000  
SCALE : 1" = 2000'

# THE ROCK LOT 1 FILING NO. 1

## VICINITY MAP EXHIBIT

**15 YEARS** **Redland**  
WHERE GREAT PLACES BEGIN

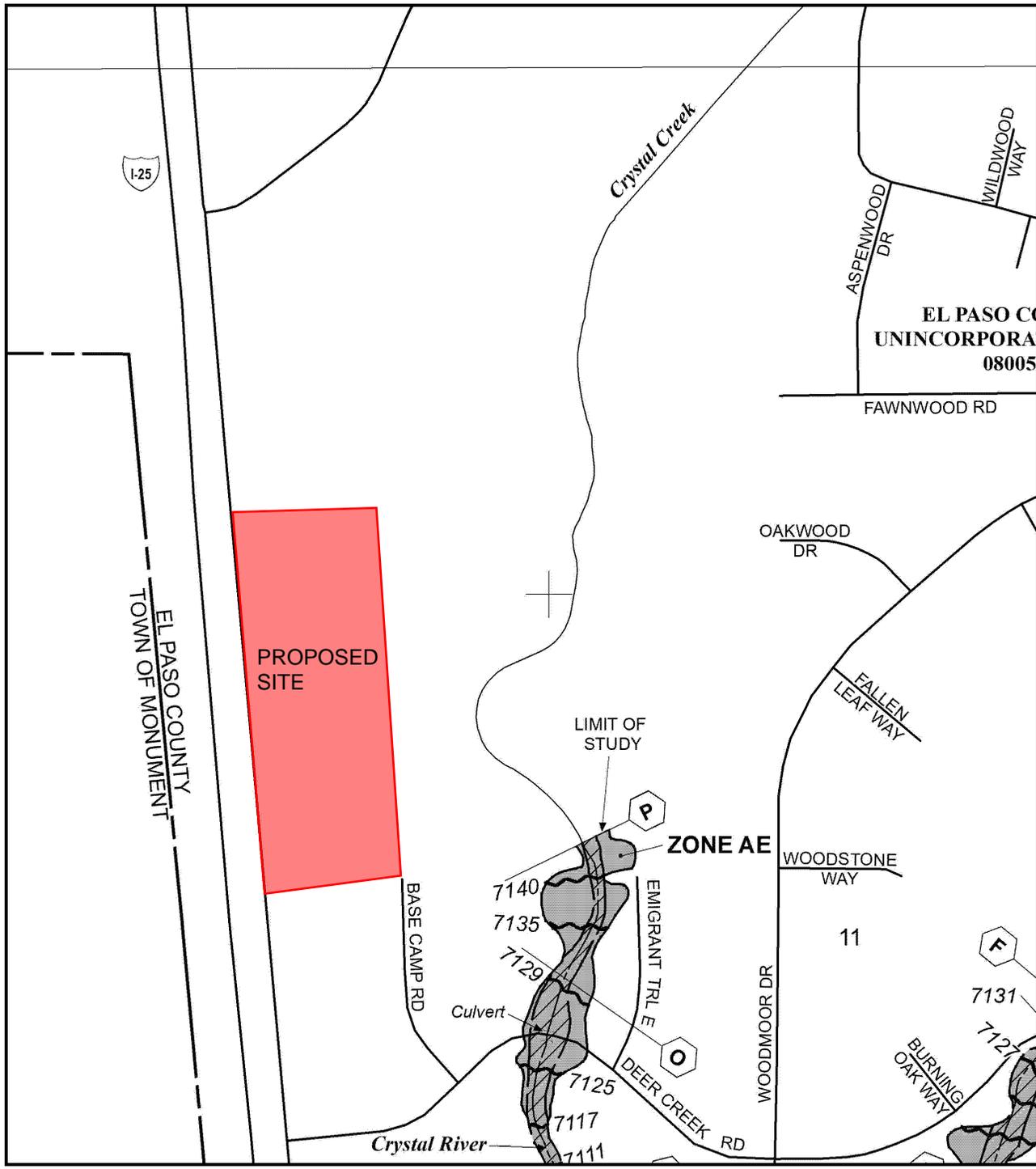
720.283.6783 ■ Land Planning ■ Landscape Architecture  
REDLAND.COM ■ Civil Engineering ■ Construction Management

PROJECT NO: 23009.001

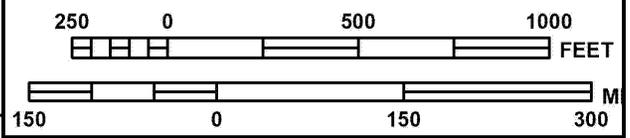
DATE: 07/28/2023

DRAWING NO:

1 OF 1



MAP SCALE 1" = 500'



PANEL 0276G

NATIONAL FLOOD INSURANCE PROGRAM

**FIRM**  
**FLOOD INSURANCE RATE MAP**  
**EL PASO COUNTY,**  
**COLORADO**  
**AND INCORPORATED AREAS**

**PANEL 276 OF 1300**  
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
EL PASO COUNTY	080059	0276	G
MONUMENT, TOWN OF	080064	0276	G
PALMER LAKE, TOWN OF	080065	0276	G

Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the Notice-to-User Letter that accompanied this correction for details.

Notice to User: The **Map Number** shown below should be used when placing map orders; the **Community Number** shown above should be used on insurance applications for the subject community.



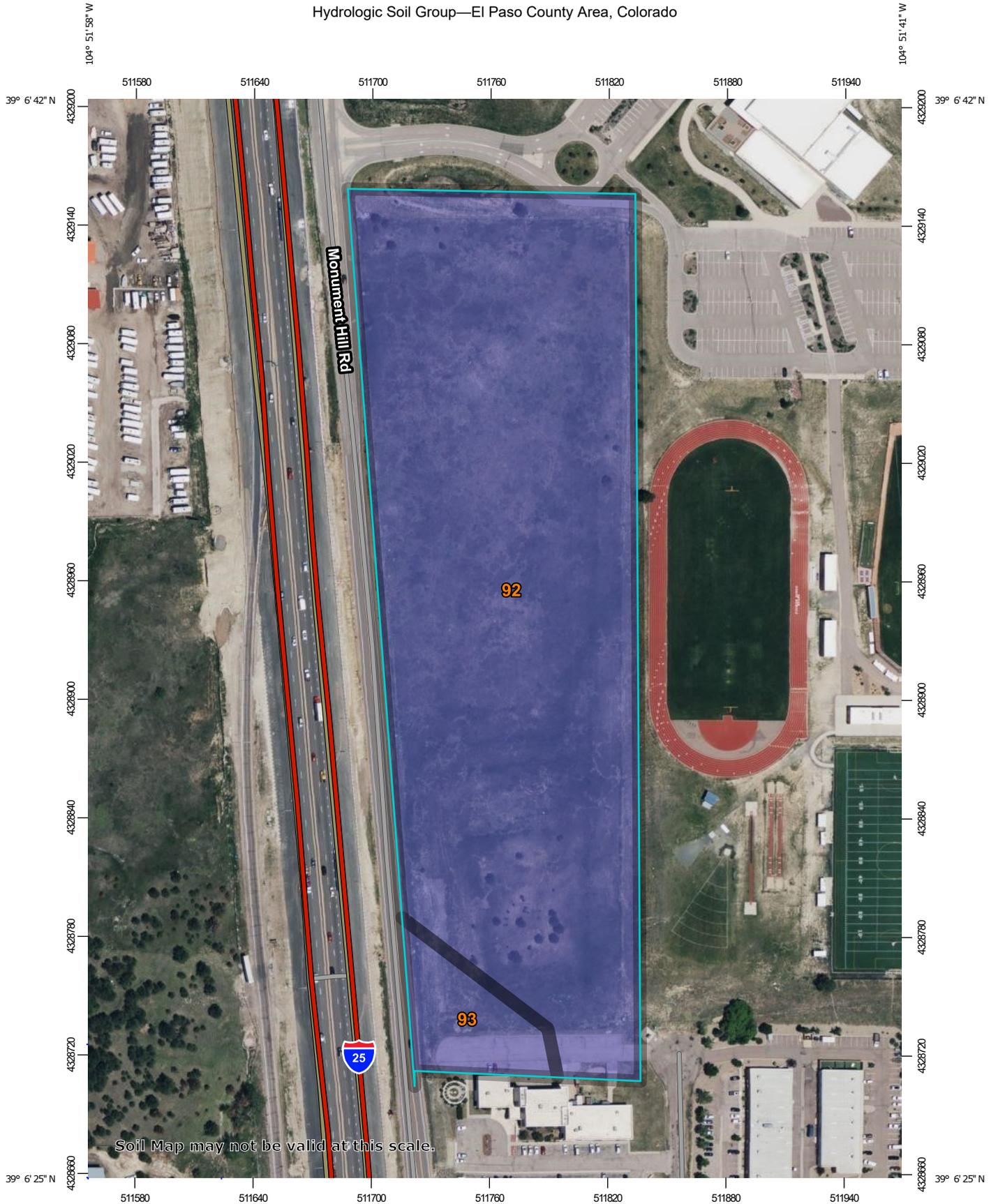
**MAP NUMBER**  
**08041C0276G**

**MAP REVISED**  
**DECEMBER 7, 2018**

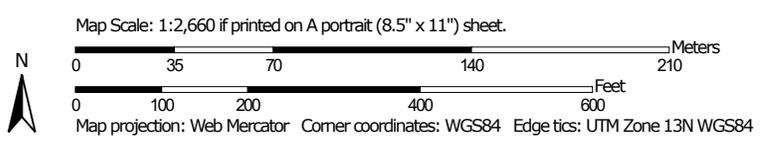
Federal Emergency Management Agency

This is an official FIRMette showing a portion of the above-referenced flood map created from the MSC FIRMette Web tool. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For additional information about how to make sure the map is current, please see the Flood Hazard Mapping Updates Overview Fact Sheet available on the FEMA Flood Map Service Center home page at <https://msc.fema.gov>.

Hydrologic Soil Group—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



### MAP LEGEND

**Area of Interest (AOI)**

 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**

-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available

**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 20, Sep 2, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 9, 2021—Jun 12, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
92	Tomah-Crowfoot loamy sands, 3 to 8 percent slopes	B	13.6	93.8%
93	Tomah-Crowfoot complex, 8 to 15 percent slopes	B	0.9	6.2%
<b>Totals for Area of Interest</b>			<b>14.5</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher



720.283.6783 Office  
1500 West Canal Court  
Littleton, Colorado 80120  
[REDLAND.COM](http://REDLAND.COM)

## Appendix B - Hydrologic Calculation

TOTAL IMPERVIOUS AREA TABLE			
BASIN	DRIVE/WALK (AC)	ROOF (AC)	GRAVEL (AC)
B16	0.00	0.30	0.00
B1	0.34	0.00	0.00
B17	0.00	0.30	0.00
B18	0.00	0.30	0.00
B2	0.35	0.00	0.00
B19	0.00	0.30	0.00
B3	0.29	0.00	0.00
B20	0.00	0.30	0.00
B4	0.19	0.00	0.00
B21	0.00	0.30	0.00
B5	0.33	0.00	0.00
B27	0.00	0.30	0.00
B7	0.23	0.00	0.00
B6	0.21	0.00	0.00
B8	0.67	0.00	0.00
B22	0.00	0.42	0.00
B9	0.42	0.00	0.00
B23	0.00	0.36	0.00
B24	0.00	0.30	0.00
B10	0.56	0.00	0.00
B25	0.00	0.30	0.00
B26	0.00	0.30	0.00
B11	0.27	0.00	0.00
B12	0.66	0.00	0.00
B13	0.35	0.00	0.00
B14	0.07	0.00	0.00
B15	0.11	0.00	0.00
C1	0.18	0.00	0.00
A1	0.00	0.00	0.00
B28	0.00	0.00	0.00
B29	0.00	0.00	0.00
B30	0.00	0.00	0.05
B31	0.02	0.00	0.00
TOTAL	5.23	3.76	0.05
TOTAL IMPERVIOUS AREA:		9.04	



**STANDARD FORM SF-1 - UNDEVELOPED  
RUNOFF COEFFICIENTS**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/19/2023  
 JURISDICTION: El Paso

LAND USE:	Drive/Walk	Roof	Lawn	Undeveloped Land	Gravel Road
IMPERVIOUSNESS	100%	90%	0%	2%	40%
C10 VALUES	0.92	0.75	0.15	0.17	0.63
C100 VALUES	0.96	0.81	0.35	0.36	0.7

NRCS SOIL TYPE: TYPE B

**OVERALL SITE STUDY AREA**

DESIGN BASIN	DESIGN POINT	Drive/Walk (AC)	Roof (AC)	Lawn (AC)	Undeveloped Land (AC)	Gravel Road (AC)	TOTAL AREA (AC)	C <sub>d</sub> (10)	C <sub>d</sub> (100)	Imp (%)
A1	A	0.00	0.00	0.00	2.35	0.00	<b>2.35</b>	0.17	0.36	2%
OSA1	A	0.40	0.00	0.00	0.35	0.00	<b>0.75</b>	0.57	0.68	54%
BASIN A		<b>0.40</b>			<b>2.71</b>		<b>3.10</b>			<b>14%</b>
		<b>12.7%</b>			<b>87.3%</b>		<b>100.0%</b>			
B1	B	0.00	0.00	0.00	7.40	0.00	<b>7.40</b>	0.17	0.36	2%
OSB1	B	0.00	0.00	0.00	1.14	0.00	<b>1.14</b>	0.17	0.36	2%
OSB2	B	0.38	0.00	0.00	0.38	0.00	<b>0.76</b>	0.55	0.66	51%
BASIN B		<b>0.38</b>			<b>8.92</b>		<b>9.29</b>			<b>6%</b>
		<b>4.1%</b>			<b>95.9%</b>		<b>100.0%</b>			
C1	C	0.00	0.00	0.00	1.86	0.00	<b>1.86</b>	0.17	0.36	2%
OSC1	C	0.00	0.00	0.00	1.91	0.00	<b>1.91</b>	0.17	0.36	2%
BASIN C					<b>3.77</b>		<b>3.77</b>			<b>2%</b>
					<b>100.0%</b>		<b>100.0%</b>			



**STANDARD FORM SF-2 - UNDEVELOPED  
TIME OF CONCENTRATION**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/16/2023  
 JURISDICTION: El Paso

SUB-BASIN DATA			INITIAL TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )						t <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL T <sub>c</sub>	RUNOFF COEFFICIENT	
DESIGN BASIN (1)	AREA (AC) (2)	C <sub>10</sub> (3)	LENGTH* (FT) (4)	SLOPE (%) (5)	T <sub>i</sub> (MINUTES) (6)	LENGTH (FT) (7)	SLOPE (%) (8)	C <sub>v</sub> (9)	Land Surface (10)	VEL (FPS) (11)	T <sub>t</sub> (MINUTES) (12)	COMP. t <sub>c</sub> (13)	TOTAL LENGTH (14)	REGIONAL t <sub>c</sub> (15)	Min. t <sub>c</sub>	C <sub>10</sub>	C <sub>100</sub>
A1	2.35	0.17	110	5.0%	10	445	5.0%	5.0	Tillage/Field	1.1	6.6	17.1	555	25.9	17.1	0.17	0.36
OSA1	0.75	0.57	128	3.5%	7.3	192	4.3%	5.0	Tillage/Field	1.0	3.1	10.4	320	17.0	10.4	0.57	0.68
B1	7.40	0.17	197	4.0%	15.1	962	4.4%	5.0	Tillage/Field	1.0	15.3	30.4	1159	26.3	26.3	0.17	0.36
OSB1	1.14	0.17	85	2.0%	12.5	104	16.0%	5.0	Tillage/Field	2.0	0.9	13.3	189	25.7	13.3	0.17	0.36
OSB2	0.76	0.55	100	2.0%	8.1	750	4.1%	5.0	Tillage/Field	1.0	12.3	20.4	850	17.8	17.8	0.55	0.66
C1	1.86	0.17	155	5.0%	12.4	385	3.3%	5.0	Tillage/Field	0.9	7.1	19.5	540	25.9	19.5	0.17	0.36
OSC1	1.91	0.17	165	1.0%	21.9	210	7.0%	5.0	Tillage/Field	1.3	2.6	24.5	375	25.8	24.5	0.17	0.36



**STANDARD FORM SF-3 - UNDEVELOPED  
STORM DRAINAGE DESIGN - RATIONAL METHOD 10 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 1.75

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE		TRAVEL TIME			
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{10}$	$t_c$ (minutes)	$C^*A$ (ac)	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C^*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	$t_t$ (minutes)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
	A	A1	2.4	0.17	17.1	0.4	3.73	1.5	17.09	0.82	3.73	3.07								
	A	OSA1	0.7	0.57	10.4	0.4	4.66	2.0	17.09	0.82	3.73	3.07								
	B	B1	7.4	0.17	26.3	1.3	2.97	3.7	26.27	1.86	2.97	5.53								
	B	OSB1	1.1	0.17	13.3	0.2	4.19	0.8	26.27	1.86	2.97	5.53								
	B	OSB2	0.8	0.55	17.8	0.4	3.66	1.5	26.27	1.86	2.97	5.53								
	C	C1	1.9	0.17	19.5	0.3	3.49	1.1	24.55	0.64	3.08	1.97								
	C	OSC1	1.9	0.17	24.5	0.3	3.08	1.0	24.55	0.64	3.08	1.97								



**STANDARD FORM SF-3 - UNDEVELOPED  
STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/16/2023  
 JURISDICTION: El Paso  
 $P_1$  (1-Hour Rainfall) = 2.52

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{100}$	$t_c$ (minutes)	$C*A$ (ac)	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	$t_t$ (minutes)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	A	A1	2.4	0.36	17.1	0.8	5.37	4.6	17.09	1.35	5.37	7.27									
	A	OSA1	0.7	0.68	10.4	0.5	6.71	3.4	17.09	1.35	5.37	7.27									
	B	B1	7.4	0.36	26.3	2.7	4.27	11.4	26.27	3.57	4.27	15.26									
	B	OSB1	1.1	0.36	13.3	0.4	6.04	2.5	26.27	3.57	4.27	15.26									
	B	OSB2	0.8	0.66	17.8	0.5	5.27	2.6	26.27	3.57	4.27	15.26									
	C	C1	1.9	0.36	19.5	0.7	5.03	3.4	24.55	1.36	4.44	6.02									
	C	OSC1	1.9	0.36	24.5	0.7	4.44	3.0	24.55	1.36	4.44	6.02									

**BASIN SUMMARY - UNDEVELOPED**



PROJECT NAME: The Rock Commerce Center      DATE: 10/16/2023  
 PROJECT NUMBER: 23009.000      JURISDICTION: El Paso  
 CALCULATED BY: CJS  
 CHECKED BY: MC

**Basin Summary Table**

Basin	Area (AC)	Runoff Coefficients		I (%)	Peak Flows (cfs)	
		C <sub>10</sub>	C <sub>100</sub>		Q <sub>10</sub>	Q <sub>100</sub>
A1	2.35	0.17	0.36	2%	1.5	4.6
OSA1	0.75	0.57	0.68	54%	2.0	3.4
B1	7.40	0.17	0.36	2%	3.7	11.4
OSB1	1.14	0.17	0.36	2%	0.8	2.5
OSB2	0.76	0.41	0.66	51%	1.5	2.6
C1	1.86	0.17	0.36	2%	1.1	3.4
OSC1	1.91	0.17	0.36	2%	1.0	3.0



**STANDARD FORM SF-1 - DEVELOPED  
RUNOFF COEFFICIENTS**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/19/2023  
 JURISDICTION: El Paso

LAND USE:	Drive/Walk	Roof	Lawn	Undeveloped Land	Gravel Road
<b>IMPERVIOUSNESS</b>	100%	90%	0%	2%	40%
<b>C10 VALUES</b>	0.92	0.75	0.15	0.17	0.63
<b>C100 VALUES</b>	0.96	0.81	0.35	0.36	0.7

NRCS SOIL TYPE: TYPE B

**OVERALL SITE STUDY AREA**

DESIGN BASIN	DESIGN POINT	Drive/Walk (AC)	Roof (AC)	Lawn (AC)	Undeveloped Land (AC)	Gravel Road (AC)	TOTAL AREA (AC)	C <sub>d</sub> (10)	C <sub>d</sub> (100)	Imp (%)
B16	1	0.00	0.30	0.00			0.30	0.75	0.81	90%
B1	1	0.34	0.00	0.19			0.53	0.64	0.74	64%
B17	2	0.00	0.30	0.00			0.30	0.75	0.81	90%
B18	2	0.00	0.30	0.00			0.30	0.75	0.81	90%
B2	2	0.35	0.00	0.13			0.48	0.71	0.80	73%
B19	3	0.00	0.30	0.00			0.30	0.75	0.81	90%
B3	3	0.29	0.00	0.02			0.30	0.88	0.93	95%
B20	4	0.00	0.30	0.00			0.30	0.75	0.81	90%
B4	4	0.19	0.00	0.00			0.19	0.92	0.96	100%
B21	5	0.00	0.30	0.00			0.30	0.75	0.81	90%
B5	5	0.33	0.00	0.07			0.40	0.78	0.85	82%
B27	13	0.00	0.30	0.00			0.30	0.75	0.81	90%
B7	7	0.23	0.00	0.17			0.40	0.60	0.70	58%
B6	6	0.21	0.00	0.10			0.31	0.68	0.77	68%
B8	8	0.67	0.00	0.31			0.98	0.68	0.77	68%
B22	8	0.00	0.42	0.00			0.42	0.75	0.81	90%
B9	9	0.42	0.00	0.17			0.59	0.70	0.78	71%
B23	9	0.00	0.36	0.00			0.36	0.75	0.81	90%
B24	10	0.00	0.30	0.00			0.30	0.75	0.81	90%
B10	10	0.56	0.00	0.12			0.67	0.79	0.85	83%
B25	11	0.00	0.30	0.00			0.30	0.75	0.81	90%
B26	12	0.00	0.30	0.00			0.30	0.75	0.81	90%
B11	11	0.27	0.00	0.09			0.37	0.72	0.80	74%
B12	12	0.66	0.00	0.08			0.75	0.83	0.89	89%
B13	13	0.35	0.00	0.08			0.43	0.77	0.84	81%
B14	14	0.07	0.00	0.01			0.08	0.82	0.88	87%
B15	15	0.11	0.00	0.00			0.11	0.90	0.94	97%
C1	C	0.18	0.00	0.05			0.22	0.76	0.84	80%
A1	A	0.00	0.00	0.09			0.09	0.15	0.35	0%



**STANDARD FORM SF-1 - DEVELOPED  
RUNOFF COEFFICIENTS**

PROJECT NAME: The Rock Commerce Center

DATE: 10/19/2023

PROJECT NUMBER: 23009

JURISDICTION: El Paso

CALCULATED BY: CJS

CHECKED BY: MC

B28	RC1	0.00	0.00	0.06			<b>0.06</b>	0.15	0.35	0%
B29	B	0.00	0.00	0.36			<b>0.36</b>	0.15	0.35	0%
OSB1	10	0.00	0.00	0.08			<b>0.08</b>	0.15	0.35	0%
OSB2	11	0.00	0.00	0.34			<b>0.34</b>	0.15	0.35	0%
OSB3	12	0.00	0.00	0.78			<b>0.78</b>	0.15	0.35	0%
OSB4	13	0.00	0.00	1.88			<b>1.88</b>	0.15	0.35	0%
OSA1	A	0.45	0.00	0.26			<b>0.71</b>	0.64	0.74	63%
OSB6	RC1	0.10	0.00	0.11			<b>0.21</b>	0.53	0.65	49%
OSB7	4	0.05	0.00	0.00			<b>0.05</b>	0.92	0.96	100%
OSB8	B	0.31	0.00	0.16			<b>0.47</b>	0.65	0.75	65%
OSB5	15	0.04	0.00	0.02			<b>0.06</b>	0.70	0.78	71%
B30	16	0.00	0.00	0.56		0.05	<b>0.61</b>	0.08	0.44	3%
B31	B	0.02					<b>0.02</b>	0.87	0.90	100%



**STANDARD FORM SF-2 - DEVELOPED  
TIME OF CONCENTRATION**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/16/2023  
 JURISDICTION: El Paso

SUB-BASIN DATA			INITIAL TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )						t <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL T <sub>c</sub>	RUNOFF COEFFICIENT	
DESIGN BASIN (1)	AREA (AC) (2)	C <sub>10</sub> (3)	LENGTH* (FT) (4)	SLOPE (%) (5)	T <sub>i</sub> (MINUTES) (6)	LENGTH (FT) (7)	SLOPE (%) (8)	C <sub>v</sub> (9)	Land Surface (10)	VEL (FPS) (11)	T <sub>t</sub> (MINUTES) (12)	COMP. t <sub>c</sub> (13)	TOTAL LENGTH (14)	REGIONAL t <sub>c</sub> (15)	Min. t <sub>c</sub>	C <sub>10</sub>	C <sub>100</sub>
B16	0.30	0.75	50	2.5%	3	210	2.5%	20.0	Paved Areas	3.2	1.1	4.5	260	10.9	5.0	0.75	0.81
B1	0.53	0.64	77	30.0%	2.4	228	0.8%	20.0	Paved Areas	1.7	2.2	4.6	305	15.4	5.0	0.64	0.74
B17	0.30	0.75	100	2.5%	4.7	200	2.0%	20.0	Paved Areas	2.8	1.2	5.9	300	10.9	5.9	0.75	0.81
B18	0.30	0.75	50	2.5%	3.3	210	2.5%	20.0	Paved Areas	3.2	1.1	4.5	260	10.9	5.0	0.75	0.81
B2	0.48	0.71	70	5.0%	3.5	189	75.0%	20.0	Paved Areas	17.3	0.2	3.6	259	13.6	5.0	0.71	0.80
B19	0.30	0.75	50	2.5%	3.3	375	1.5%	20.0	Paved Areas	2.4	2.6	5.9	425	11.1	5.9	0.75	0.81
B3	0.30	0.88	40	2.5%	1.9	230	1.0%	20.0	Paved Areas	2.0	1.9	3.8	270	10.2	5.0	0.88	0.93
B20	0.30	0.75	50	2.5%	3.3	210	2.5%	20.0	Paved Areas	3.2	1.1	4.5	260	10.9	5.0	0.75	0.81
B4	0.19	0.92	65	3.0%	1.8	115	1.0%	20.0	Paved Areas	2.0	1.0	2.8	180	9.1	5.0	0.92	0.96
B21	0.30	0.75	50	2.5%	3.3	265	2.5%	20.0	Paved Areas	3.2	1.4	4.7	315	10.9	5.0	0.75	0.81
B5	0.40	0.78	60	3.0%	3.1	275	3.5%	20.0	Paved Areas	3.7	1.2	4.4	335	12.2	5.0	0.78	0.85
B27	0.30	0.75	50	2.5%	3.3	300	2.5%	20.0	Paved Areas	3.2	1.6	4.9	350	10.9	5.0	0.75	0.81
B7	0.40	0.60	90	30.0%	2.8	45	1.0%	20.0	Paved Areas	2.0	0.4	3.2	135	16.2	5.0	0.60	0.70
B6	0.31	0.68	90	25.0%	2.5	66	1.0%	20.0	Paved Areas	2.0	0.6	3.1	156	14.5	5.0	0.68	0.77
B8	0.98	0.68	65	33.0%	2.0	324	2.5%	20.0	Paved Areas	3.2	1.7	3.7	389	14.6	5.0	0.68	0.77
B22	0.42	0.75	75	2.0%	4.4	120	2.0%	20.0	Paved Areas	2.8	0.7	5.1	195	10.8	5.1	0.75	0.81
B9	0.59	0.70	100	18.0%	2.8	175	1.2%	20.0	Paved Areas	2.2	1.3	4.2	275	14.1	5.0	0.70	0.78
B23	0.36	0.75	50	2.5%	3.3	250	2.0%	20.0	Paved Areas	2.8	1.5	4.8	300	10.9	5.0	0.75	0.81
B24	0.30	0.75	50	2.5%	3.3	200	0.5%	20.0	Paved Areas	1.4	2.4	5.7	250	11.0	5.7	0.75	0.81
B10	0.67	0.79	100	18.0%	2.2	250	0.5%	20.0	Paved Areas	1.4	2.9	5.1	350	12.4	5.1	0.79	0.85



**STANDARD FORM SF-2 - DEVELOPED  
TIME OF CONCENTRATION**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/16/2023  
 JURISDICTION: El Paso

SUB-BASIN DATA			INITIAL TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )						t <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL T <sub>c</sub>	RUNOFF COEFFICIENT	
DESIGN BASIN (1)	AREA (AC) (2)	C <sub>10</sub> (3)	LENGTH* (FT) (4)	SLOPE (%) (5)	T <sub>i</sub> (MINUTES) (6)	LENGTH (FT) (7)	SLOPE (%) (8)	C <sub>v</sub> (9)	Land Surface (10)	VEL (FPS) (11)	T <sub>t</sub> (MINUTES) (12)	COMP. t <sub>c</sub> (13)	TOTAL LENGTH (14)	REGIONAL t <sub>c</sub> (15)	Min. t <sub>c</sub>	C <sub>10</sub>	C <sub>100</sub>
B25	0.30	0.75	50	2.5%	3.3	120	2.5%	20.0	Paved Areas	3.2	0.6	4.0	170	10.8	5.0	0.75	0.81
B26	0.30	0.75	50	2.5%	3.3	280	2.5%	20.0	Paved Areas	3.2	1.5	4.8	330	10.9	5.0	0.75	0.81
B11	0.37	0.72	100	6.5%	3.7	10	1.0%	20.0	Paved Areas	2.0	0.1	3.8	110	13.4	5.0	0.72	0.80
B12	0.75	0.83	100	3.0%	3.4	290	1.7%	20.0	Paved Areas	2.6	1.9	5.2	390	11.2	5.2	0.83	0.89
B13	0.43	0.77	100	3.0%	4.2	175	4.0%	20.0	Paved Areas	4.0	0.7	4.9	275	12.4	5.0	0.77	0.84
B14	0.08	0.82	85	7.0%	2.5	47	4.2%	20.0	Paved Areas	4.1	0.2	2.6	132	11.2	5.0	0.82	0.88
B15	0.11	0.90	70	3.0%	2.2	70	4.0%	20.0	Paved Areas	4.0	0.3	2.5	140	9.6	5.0	0.90	0.94
C1	0.22	0.76	50	2.5%	3.2	125	2.0%	20.0	Paved Areas	2.8	0.7	4.0	175	12.6	5.0	0.76	0.84
A1	0.09	0.15	60	3.3%	9.0	215	3.0%	7.0	Short Pasture/Lawn	1.2	3.0	12.0	275	26.2	12.0	0.15	0.35
B28	0.06	0.15	40	5.0%	6.4	200	7.5%	7.0	Short Pasture/Lawn	1.9	1.7	8.2	240	26.1	8.2	0.15	0.35
B29	0.36	0.15	40	5.0%	6.4	470	4.0%	7.0	Short Pasture/Lawn	1.4	5.6	12.0	510	26.3	12.0	0.15	0.35
OSB1	0.08	0.15	75	7.4%	7.7	180	4.0%	20.0	Paved Areas	4.0	0.8	8.5	255	26.1	8.5	0.15	0.35
OSB2	0.34	0.15	100	3.9%	11.1	165	3.5%	20.0	Paved Areas	3.7	0.7	11.8	265	26.1	11.8	0.15	0.35
OSB3	0.78	0.15	100	7.2%	9.0	230	10.9%	20.0	Paved Areas	6.6	0.6	9.6	330	26.1	9.6	0.15	0.35
OSB4	1.88	0.15	100	2.3%	13.2	350	14.3%	7.0	Short Pasture/Lawn	2.6	2.2	15.4	450	26.1	15.4	0.15	0.35
OSA1	0.71	0.64	100	2.5%	6.2	250	3.5%	20.0	Paved Areas	3.7	1.1	7.3	350	15.4	7.3	0.64	0.74
OSB6	0.21	0.53	75	2.5%	6.7	200	7.5%	20.0	Paved Areas	5.5	0.6	7.3	275	17.7	7.3	0.53	0.65
OSB7	0.05	0.92	84	4.0%	1.9	0	1.0%	20.0	Paved Areas	2.0	0.0	1.9	84	9.0	5.0	0.92	0.96
OSB8	0.47	0.65	90	2.5%	5.7	470	4.0%	20.0	Paved Areas	4.0	2.0	7.7	560	15.2	7.7	0.65	0.75
OSB5	0.06	0.70	60	7.0%	3.0	120	1.0%	20.0	Paved Areas	2.0	1.0	4.0	180	14.0	5.0	0.70	0.78



**STANDARD FORM SF-2 - DEVELOPED  
TIME OF CONCENTRATION**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

DATE: 10/16/2023  
 JURISDICTION: El Paso

SUB-BASIN DATA			INITIAL TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )						t <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL T <sub>c</sub>	RUNOFF COEFFICIENT	
DESIGN BASIN (1)	AREA (AC) (2)	C <sub>10</sub> (3)	LENGTH* (FT) (4)	SLOPE (%) (5)	T <sub>i</sub> (MINUTES) (6)	LENGTH (FT) (7)	SLOPE (%) (8)	C <sub>v</sub> (9)	Land Surface (10)	VEL (FPS) (11)	T <sub>t</sub> (MINUTES) (12)	COMP. t <sub>c</sub> (13)	TOTAL LENGTH (14)	REGIONAL t <sub>c</sub> (15)	Min. t <sub>c</sub>	C <sub>10</sub>	C <sub>100</sub>
B30	0.61	0.08	50	33.0%	4.1	200	1.0%	7.0	Short Pasture/Lawn	0.7	4.8	8.9	250	25.7	8.9	0.08	0.44
B31	0.02	0.87	100	7.0%	2.2	475	4.6%	7.0	Short Pasture/Lawn	1.5	5.3	7.5	575	9.3	7.5	0.87	0.90



**STANDARD FORM SF-3 - DEVELOPED**  
**STORM DRAINAGE DESIGN - RATIONAL METHOD 10 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 1.75

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{10}$	$t_c$ (minutes)	$C*A$ (ac)	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	$t_t$ (minutes)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	1	B16	0.3	0.75	5.0	0.2	5.94	1.3	5.00	0.56	5.94	3.35									
	1	B1	0.5	0.64	5.0	0.3	5.94	2.0	5.00	0.56	5.94	3.35									
	2	B17	0.3	0.75	5.9	0.2	5.67	1.3	5.91	0.79	5.67	4.46									
	2	B18	0.3	0.75	5.0	0.2	5.94	1.3	5.91	0.79	5.67	4.46									
	2	B2	0.5	0.71	5.0	0.3	5.94	2.0	5.91	0.79	5.67	4.46									
	3	B19	0.3	0.75	5.9	0.2	5.67	1.3	5.89	0.49	5.67	2.78									
	3	B3	0.3	0.88	5.0	0.3	5.94	1.6	5.89	0.49	5.67	2.78									
	4	B20	0.3	0.75	5.0	0.2	5.94	1.3	5.00	0.44	5.94	2.63									
	4	B4	0.2	0.92	5.0	0.2	5.94	1.0	5.00	0.44	5.94	2.63									
	5	B21	0.3	0.75	5.0	0.2	5.94	1.3	5.00	0.54	5.94	3.19									
	5	B5	0.4	0.78	5.0	0.3	5.94	1.8	5.00	0.54	5.94	3.19									
	13	B27	0.3	0.75	5.0	0.2	5.94	1.3	15.40	0.84	3.92	3.30									
	7	B7	0.4	0.60	5.0	0.2	5.94	1.4	5.00	0.24	5.94	1.40									
	6	B6	0.3	0.68	5.0	0.2	5.94	1.2	5.00	0.21	5.94	1.24									
	8	B8	1.0	0.68	5.0	0.7	5.94	3.9	5.12	0.98	5.90	5.76									
	8	B22	0.4	0.75	5.1	0.3	5.90	1.8	5.12	0.98	5.90	5.76									
	9	B9	0.6	0.70	5.0	0.4	5.94	2.4	5.00	0.68	5.94	4.03									
	9	B23	0.4	0.75	5.0	0.3	5.94	1.6	5.00	0.68	5.94	4.03									
	10	B24	0.3	0.75	5.7	0.2	5.73	1.3	8.49	0.76	5.04	3.85									
	10	B10	0.7	0.79	5.1	0.5	5.89	3.1	8.49	0.76	5.04	3.85									



**STANDARD FORM SF-3 - DEVELOPED**  
**STORM DRAINAGE DESIGN - RATIONAL METHOD 10 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 1.75

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{10}$	$t_c$ (minutes)	$C*A$ (ac)	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	$t_t$ (minutes)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	11	B25	0.3	0.75	5.0	0.2	5.94	1.3	11.80	0.54	4.42	2.39									
	12	B26	0.3	0.75	5.0	0.2	5.94	1.3	9.60	0.96	4.81	4.63									
	11	B11	0.4	0.72	5.0	0.3	5.94	1.6	11.80	0.54	4.42	2.39									
	12	B12	0.7	0.83	5.2	0.6	5.86	3.6	9.60	0.96	4.81	4.63									
	13	B13	0.4	0.77	5.0	0.3	5.94	2.0	15.40	0.84	3.92	3.30									
	14	B14	0.1	0.82	5.0	0.1	5.94	0.4	5.00	0.06	5.94	0.38									
	15	B15	0.1	0.90	5.0	0.1	5.94	0.6	5.00	0.14	5.94	0.85									
	C	C1	0.2	0.76	5.0	0.2	5.94	1.0	5.00	0.17	5.94	1.01									
	A	A1	0.1	0.15	12.0	0.0	4.39	0.1	11.99	0.47	4.39	2.05									
	RC1	B28	0.1	0.15	8.2	0.0	5.10	0.0	8.18	0.12	5.10	0.61									
	B	B29	0.4	0.15	12.0	0.1	4.39	0.2	12.04	0.38	4.39	1.66									
	10	OSB1	0.1	0.15	8.5	0.0	5.04	0.1	8.49	0.76	5.04	3.85									
	11	OSB2	0.3	0.15	11.8	0.1	4.42	0.2	11.80	0.54	4.42	2.39									
	12	OSB3	0.8	0.15	9.6	0.1	4.81	0.6	9.60	0.96	4.81	4.63									
	13	OSB4	1.9	0.15	15.4	0.3	3.92	1.1	15.40	0.84	3.92	3.30									
	A	OSA1	0.7	0.64	7.3	0.5	5.29	2.4	11.99	0.47	4.39	2.05									
	RC1	OSB6	0.2	0.53	7.3	0.1	5.31	0.6	8.18	0.12	5.10	0.61									
	4	OSB7	0.1	0.92	5.0	0.0	5.94	0.3	5.00	0.44	5.94	2.63									
	B	OSB8	0.5	0.65	7.7	0.3	5.21	1.6	12.04	0.38	4.39	1.66									
	15	OSB5	0.1	0.70	5.0	0.0	5.94	0.2	5.00	0.14	5.94	0.85									



**STANDARD FORM SF-3 - DEVELOPED  
STORM DRAINAGE DESIGN - RATIONAL METHOD 10 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 1.75

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{10}$	$t_c$ (minutes)	$C*A$ (ac)	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	$t_t$ (minutes)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	16	B30	0.6	0.08	8.9	0.1	4.96	0.3	8.87	0.05	4.96	0.26									
	B	B31	0.0	0.87	7.5	0.0	5.26	0.1	12.04	0.38	4.39	1.66									



**STANDARD FORM SF-3 - DEVELOPED**  
**STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 2.52

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF C <sub>100</sub>	t <sub>c</sub> (minutes)	C*A(ac)	I (in/hr)	Q (cfs)	t <sub>c</sub> (minutes)	S(C*A) (ac)	I (in/hr)	Q (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	t <sub>t</sub> (minutes)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	1	B16	0.3	0.81	5.0	0.2	8.55	2.1	5.00	0.63	8.55	5.42									
	1	B1	0.5	0.74	5.0	0.4	8.55	3.4	5.00	0.63	8.55	5.42									
	2	B17	0.3	0.81	5.9	0.2	8.16	2.0	5.91	0.86	8.16	7.04									
	2	B18	0.3	0.81	5.0	0.2	8.55	2.1	5.91	0.86	8.16	7.04									
	2	B2	0.5	0.80	5.0	0.4	8.55	3.2	5.91	0.86	8.16	7.04									
	3	B19	0.3	0.81	5.9	0.2	8.17	2.0	5.89	0.52	8.17	4.28									
	3	B3	0.3	0.93	5.0	0.3	8.55	2.4	5.89	0.52	8.17	4.28									
	4	B20	0.3	0.81	5.0	0.2	8.55	2.1	5.00	0.47	8.55	4.03									
	4	B4	0.2	0.96	5.0	0.2	8.55	1.5	5.00	0.47	8.55	4.03									
	5	B21	0.3	0.81	5.0	0.2	8.55	2.1	5.00	0.58	8.55	4.98									
	5	B5	0.4	0.85	5.0	0.3	8.55	2.9	5.00	0.58	8.55	4.98									
	13	B27	0.3	0.81	5.0	0.2	8.55	2.1	15.40	1.27	5.65	7.16									
	7	B7	0.4	0.70	5.0	0.3	8.55	2.4	5.00	0.28	8.55	2.39									
	6	B6	0.3	0.77	5.0	0.2	8.55	2.0	5.00	0.24	8.55	2.02									
	8	B8	1.0	0.77	5.0	0.8	8.55	6.4	5.12	1.09	8.50	9.26									
	8	B22	0.4	0.81	5.1	0.3	8.50	2.9	5.12	1.09	8.50	9.26									
	9	B9	0.6	0.78	5.0	0.5	8.55	3.9	5.00	0.75	8.55	6.42									
	9	B23	0.4	0.81	5.0	0.3	8.55	2.5	5.00	0.75	8.55	6.42									
	10	B24	0.3	0.81	5.7	0.2	8.25	2.0	8.49	0.84	7.25	6.13									
	10	B10	0.7	0.85	5.1	0.6	8.49	4.9	8.49	0.84	7.25	6.13									



**STANDARD FORM SF-3 - DEVELOPED**  
**STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 2.52

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{100}$	$t_c$ (minutes)	$C*A(ac)$	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	$t_t$ (minutes)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	11	B25	0.3	0.81	5.0	0.2	8.55	2.1	11.80	0.66	6.37	4.18									
	12	B26	0.3	0.81	5.0	0.2	8.55	2.1	9.60	1.18	6.93	8.16									
	11	B11	0.4	0.80	5.0	0.3	8.55	2.5	11.80	0.66	6.37	4.18									
	12	B12	0.7	0.89	5.2	0.7	8.44	5.6	9.60	1.18	6.93	8.16									
	13	B13	0.4	0.84	5.0	0.4	8.55	3.1	15.40	1.27	5.65	7.16									
	14	B14	0.1	0.88	5.0	0.1	8.55	0.6	5.00	0.07	8.55	0.58									
	15	B15	0.1	0.94	5.0	0.1	8.55	0.9	5.00	0.15	8.55	1.31									
	C	C1	0.2	0.84	5.0	0.2	8.55	1.6	5.00	0.19	8.55	1.60									
	A	A1	0.1	0.35	12.0	0.0	6.33	0.2	11.99	0.55	6.33	3.51									
	RC1	B28	0.1	0.35	8.2	0.0	7.35	0.1	8.18	0.16	7.35	1.15									
	B	B29	0.4	0.35	12.0	0.1	6.32	0.8	12.04	0.50	6.32	3.14									
	10	OSB1	0.1	0.35	8.5	0.0	7.25	0.2	8.49	0.84	7.25	6.13									
	11	OSB2	0.3	0.35	11.8	0.1	6.37	0.8	11.80	0.66	6.37	4.18									
	12	OSB3	0.8	0.35	9.6	0.3	6.93	1.9	9.60	1.18	6.93	8.16									
	13	OSB4	1.9	0.35	15.4	0.7	5.65	3.7	15.40	1.27	5.65	7.16									
	A	OSA1	0.7	0.74	7.3	0.5	7.62	4.0	11.99	0.55	6.33	3.51									
	RC1	OSB6	0.2	0.65	7.3	0.1	7.64	1.0	8.18	0.16	7.35	1.15									
	4	OSB7	0.1	0.96	5.0	0.1	8.55	0.4	5.00	0.47	8.55	4.03									
	B	OSB8	0.5	0.75	7.7	0.4	7.51	2.7	12.04	0.50	6.32	3.14									
	15	OSB5	0.1	0.78	5.0	0.0	8.55	0.4	5.00	0.15	8.55	1.31									



**STANDARD FORM SF-3 - DEVELOPED  
STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT**

PROJECT NAME: The Rock Commerce Center  
 PROJECT NUMBER: 23009  
 CALCULATED BY: CJS  
 CHECKED BY: MC

$P_1$  (1-Hour Rainfall) = 2.52

DATE: 10/16/2023  
 JURISDICTION: El Paso

STORM LINE	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE		TRAVEL TIME			REMARKS	
		DESIGN BASIN	AREA (AC)	RUNOFF COEFF $C_{100}$	$t_c$ (minutes)	$C*A$ (ac)	$I$ (in/hr)	$Q$ (cfs)	$t_c$ (minutes)	$S(C*A)$ (ac)	$I$ (in/hr)	$Q$ (cfs)	SLOPE (%)	STREET FLOW(cfs)	DESIGN FLOW(cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)		$t_t$ (minutes)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
	16	B30	0.6	0.44	8.9	0.3	7.14	1.9	8.87	0.27	7.14	1.92									
	B	B31	0.0	0.90	7.5	0.0	7.57	0.1	12.04	0.50	6.32	3.14									

**BASIN SUMMARY - DEVELOPED**



PROJECT NAME: The Rock Commerce Center      DATE: 10/16/2023  
 PROJECT NUMBER: 23009.000      JURISDICTION: El Paso  
 CALCULATED BY: CJS  
 CHECKED BY: 0

**Basin Summary Table**

Basin	Area (AC)	Runoff Coefficients		I (%)	Peak Flows (cfs)	
		C <sub>10</sub>	C <sub>100</sub>		Q <sub>10</sub>	Q <sub>100</sub>
B16	0.30	0.75	0.81	90%	1.3	2.1
B1	0.53	0.64	0.74	64%	2.0	3.4
B17	0.30	0.75	0.81	90%	1.3	2.0
B18	0.30	0.75	0.81	90%	1.3	2.1
B2	0.48	0.71	0.80	73%	2.0	3.2
B19	0.30	0.75	0.81	90%	1.3	2.0
B3	0.30	0.88	0.93	95%	1.6	2.4
B20	0.30	0.75	0.81	90%	1.3	2.1
B4	0.19	0.92	0.96	100%	1.0	1.5
B21	0.30	0.75	0.81	90%	1.3	2.1
B5	0.40	0.78	0.85	82%	1.8	2.9
B27	0.30	0.75	0.81	90%	1.3	2.1
B7	0.40	0.60	0.70	58%	1.4	2.4
B6	0.31	0.68	0.77	68%	1.2	2.0
B8	0.98	0.68	0.77	68%	3.9	6.4
B22	0.42	0.75	0.81	90%	1.8	2.9
B9	0.59	0.70	0.78	71%	2.4	3.9
B23	0.36	0.75	0.81	90%	1.6	2.5
B24	0.30	0.75	0.81	90%	1.3	2.0
B10	0.67	0.79	0.85	83%	3.1	4.9
B25	0.30	0.75	0.81	90%	1.3	2.1
B26	0.30	0.75	0.81	90%	1.3	2.1
B11	0.37	0.72	0.80	74%	1.6	2.5
B12	0.75	0.83	0.89	89%	3.6	5.6
B13	0.43	0.77	0.84	81%	2.0	3.1
B14	0.08	0.82	0.88	87%	0.4	0.6
B15	0.11	0.90	0.94	97%	0.6	0.9
C1	0.22	0.76	0.84	80%	1.0	1.6
A1	0.09	0.15	0.35	0%	0.1	0.2
B28	0.06	0.15	0.35	0%	0.0	0.1
B29	0.36	0.15	0.35	0%	0.2	0.8
OSB1	0.08	0.15	0.35	0%	0.1	0.2
OSB2	0.34	0.15	0.35	0%	0.2	0.8
OSB3	0.78	0.15	0.35	0%	0.6	1.9
OSB4	1.88	0.15	0.35	0%	1.1	3.7
OSA1	0.71	0.64	0.74	63%	2.4	4.0
OSB6	0.21	0.53	0.65	49%	0.6	1.0
OSB7	0.05	0.92	0.96	100%	0.3	0.4
OSB8	0.47	0.65	0.75	65%	1.6	2.7
OSB5	0.06	0.70	0.78	71%	0.2	0.4
B30	0.61	0.08	0.44	3%	0.3	1.9
B31	0.02	0.87	0.90	100%	0.1	0.1



720.283.6783 Office  
1500 West Canal Court  
Littleton, Colorado 80120  
**REDLAND.COM**

## Appendix C - Hydraulic Calculations

**BASINS TRIBUTARY TO POND**

<b>BASIN</b>	<b>AREA</b>	<b>% IMPERVIOUS</b>
B1	0.53	64%
B2	0.48	73%
B3	0.3	95%
B4	0.19	100%
B5	0.4	82%
B6	0.31	68%
B7	0.4	58%
B8	0.98	68%
B9	0.59	71%
B10	0.67	83%
B11	0.37	74%
B12	0.75	89%
B13	0.43	81%
B14	0.08	87%
B15	0.11	97%
B16	0.3	90%
B17	0.3	90%
B18	0.3	90%
B19	0.3	90%
B20	0.3	90%
B21	0.3	90%
B22	0.42	90%
B23	0.36	90%
B24	0.3	90%
B25	0.3	90%
B26	0.3	90%
B27	0.3	90%
B30	0.61	3%
<b>TOTAL:</b>	<b>10.98</b>	<b>77%</b>

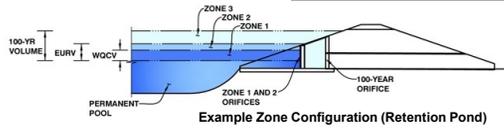


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: **23009 - The Rock Lot 1 Filing No. 1**

Basin ID: **Basin B**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.32	0.294	Orifice Plate
Zone 2 (EURV)	5.88	0.675	Orifice Plate
Zone 3 (100-year)	7.41	0.518	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>1.488</b>	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =  ft<sup>2</sup>  
 Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
 Orifice Plate: Orifice Vertical Spacing =  inches  
 Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 1-1/4 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row =  ft<sup>2</sup>  
 Elliptical Half-Width =  feet  
 Elliptical Slot Centroid =  feet  
 Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.91	3.16	4.41				
Orifice Area (sq. inches)	1.30	1.30	1.30	1.30				
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

change to 1.35

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
 Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area =  ft<sup>2</sup>  
 Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, H <sub>o</sub>	5.88	N/A
Overflow Weir Front Edge Length	3.00	N/A
Overflow Weir Gate Slope	4.00	N/A
Horiz. Length of Weir Sides	4.00	N/A
Overflow Gate Type	Type C Gate	N/A
Debris Clogging %	0%	N/A

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected
Height of Gate Upper Edge, H <sub>t</sub>	6.88	N/A
Overflow Weir Slope Length	4.12	N/A
Grate Open Area / 100-yr Orifice Area	10.48	N/A
Overflow Grate Open Area w/o Debris	8.61	N/A
Overflow Grate Open Area w/ Debris	8.61	N/A

assume 50%

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe	0.00	N/A
Outlet Pipe Diameter	18.00	N/A
Restrictor Plate Height Above Pipe Invert	8.50	

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected
Outlet Orifice Area	0.82	N/A
Outlet Orifice Centroid	0.41	N/A
Half-Central Angle of Restrictor Plate on Pipe	1.52	N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
 Spillway Crest Length =  feet  
 Spillway End Slopes =  H:V  
 Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =  feet  
 Stage at Top of Freeboard =  feet  
 Basin Area at Top of Freeboard =  acres  
 Basin Volume at Top of Freeboard =  acre-ft

## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

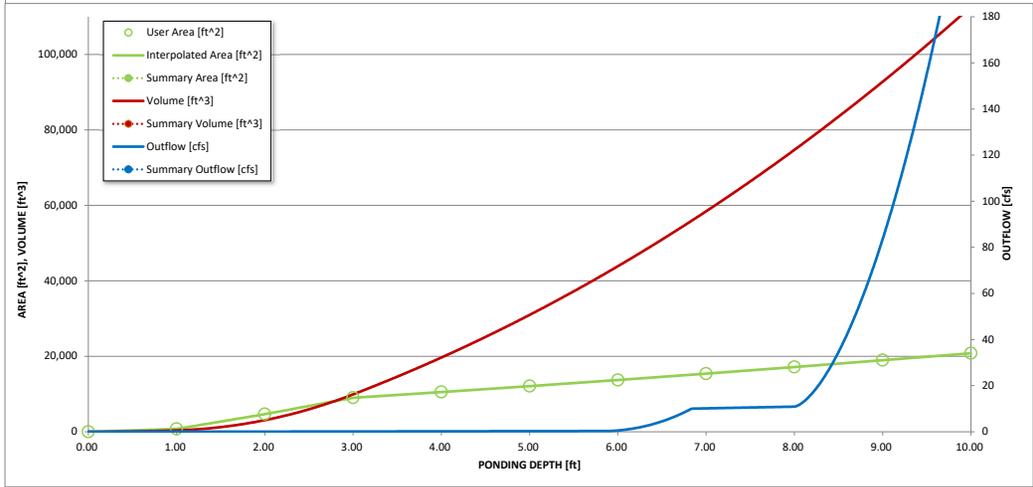
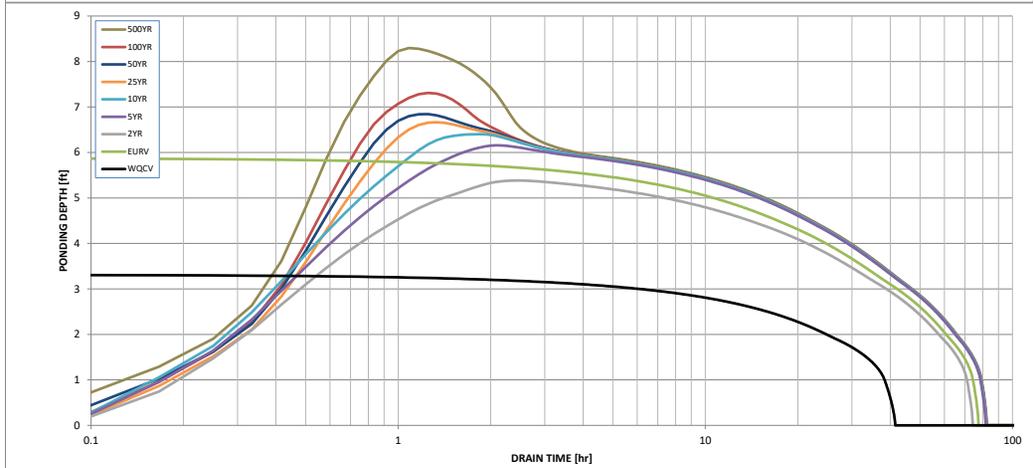
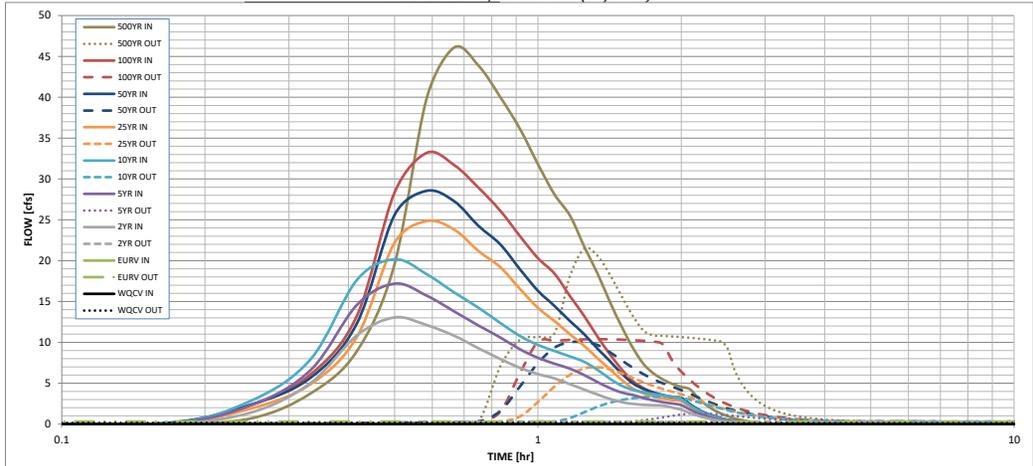
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.39
One-Hour Rainfall Depth (in)	N/A	N/A	0.867	1.153	1.392	1.660	1.907	2.192	3.067
CUHP Runoff Volume (acre-ft)	0.294	0.969	0.867	1.153	1.392	1.660	1.907	2.192	3.067
Inflow Hydrograph Volume (acre-ft)	N/A	N/A	0.867	1.153	1.392	1.660	1.907	2.192	3.067
CUHP Predevelopment Peak Q (cfs)	N/A	N/A	0.9	2.6	4.0	7.3	9.2	11.7	18.4
OPTIONAL Override Predevelopment Peak Q (cfs)	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre)	N/A	N/A	0.08	0.23	0.35	0.64	0.80	1.03	1.61
Peak Inflow Q (cfs)	N/A	N/A	13.1	17.2	20.2	24.9	28.6	33.2	46.1
Peak Outflow Q (cfs)	0.1	0.3	0.3	1.3	3.4	7.0	10.0	10.4	21.5
Ratio Peak Outflow to Predevelopment Q	N/A	N/A	N/A	0.5	0.8	1.0	1.1	0.9	1.2
Structure Controlling Flow	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps)	N/A	N/A	N/A	0.1	0.3	0.8	1.1	1.2	1.2
Max Velocity through Gate 2 (fps)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours)	38	69	67	72	71	69	68	66	63
Time to Drain 99% of Inflow Volume (hours)	40	74	71	78	78	77	76	76	74
Maximum Ponding Depth (ft)	3.32	5.88	5.39	6.16	6.40	6.67	6.84	7.31	8.30
Area at Maximum Ponding Depth (acres)	0.22	0.31	0.29	0.32	0.33	0.34	0.35	0.37	0.41
Maximum Volume Stored (acre-ft)	0.295	0.970	0.819	1.055	1.136	1.224	1.285	1.453	1.831

This was updated to be 1.35 on final calculations.

This was updated to be 50% on final calculations.

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention\_Version 4.06 (July 2022)



S-A-V-D Chart Axis Override  
 minimum bound X-axis Left Y-Axis Right Y-Axis

# INLET MANAGEMENT

Worksheet Protected

<b>INLET NAME</b>	<a href="#">SD IN1</a>	<a href="#">SD IN2</a>	<a href="#">SD IN3</a>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT/Denver 13 Valley Grate	CDOT/Denver 13 Valley Grate	CDOT Type R Curb Opening

## USER-DEFINED INPUT

### User-Defined Design Flows

Minor $Q_{known}$ (cfs)	3.4	4.5	5.4
Major $Q_{known}$ (cfs)	5.4	7.0	8.3

### Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.

Receive Bypass Flow from:	No Bypass Flow Received	User-Defined	No Bypass Flow Received
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0

### Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

### Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

### Minor Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

### Major Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

## CALCULATED OUTPUT

<b>Minor Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>3.4</b>	<b>4.5</b>	<b>5.4</b>
<b>Major Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>5.4</b>	<b>7.0</b>	<b>8.3</b>
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	N/A	N/A

# INLET MANAGEMENT

Worksheet Protected

<b>INLET NAME</b>	<a href="#">SD IN4</a>	<a href="#">SD IN5</a>	<a href="#">SD IN6</a>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT/Denver 13 Combination	CDOT/Denver 13 Valley Grate	CDOT/Denver 13 Valley Grate

## USER-DEFINED INPUT

### User-Defined Design Flows

Minor $Q_{known}$ (cfs)	3.2	1.2	1.4
Major $Q_{known}$ (cfs)	5.0	2.0	2.4

### Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0

### Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

### Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

### Minor Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

### Major Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

## CALCULATED OUTPUT

<b>Minor Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>3.2</b>	<b>1.2</b>	<b>1.4</b>
<b>Major Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>5.0</b>	<b>2.0</b>	<b>2.4</b>
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	N/A	N/A

# INLET MANAGEMENT

Worksheet Protected

<b>INLET NAME</b>	<a href="#">SD IN7</a>	<a href="#">SD IN8</a>	<a href="#">SD IN9</a>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	On Grade	In Sump
Inlet Type	CDOT/Denver 13 Valley Grate	CDOT/Denver 13 Valley Grate	CDOT/Denver 13 Valley Grate

## USER-DEFINED INPUT

### User-Defined Design Flows

Minor $Q_{known}$ (cfs)	5.8	4.0	3.9
Major $Q_{known}$ (cfs)	9.3	6.4	6.1

### Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	User-Defined
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	2.1
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	3.7

### Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

### Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

### Minor Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

### Major Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

## CALCULATED OUTPUT

<b>Minor Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>5.8</b>	<b>4.0</b>	<b>6.0</b>
<b>Major Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>9.3</b>	<b>6.4</b>	<b>9.8</b>
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	2.1	N/A
Major Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	3.7	N/A

# INLET MANAGEMENT

Worksheet Protected

<b>INLET NAME</b>	<a href="#">SD IN10</a>	<a href="#">SD IN11</a>	<a href="#">SD IN12</a>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	On Grade	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT/Denver 13 Combination	CDOT Type R Curb Opening

## USER-DEFINED INPUT

### User-Defined Design Flows

Minor $Q_{known}$ (cfs)	2.4	4.6	3.3
Major $Q_{known}$ (cfs)	4.2	8.2	7.2

### Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	User-Defined
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.2
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	1.0

### Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

### Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

### Minor Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

### Major Storm Rainfall Input

Design Storm Return Period, $T_r$ (years)			
One-Hour Precipitation, $P_1$ (inches)			

## CALCULATED OUTPUT

<b>Minor Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>2.4</b>	<b>4.6</b>	<b>3.5</b>
<b>Major Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>4.2</b>	<b>8.2</b>	<b>8.2</b>
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	0.2	N/A
Major Flow Bypassed Downstream, $Q_b$ (cfs)	N/A	1.0	N/A

# INLET MANAGEMENT

Worksheet Protected

<b>INLET NAME</b>	<a href="#">SD IN13</a>	<a href="#">SD IN14</a>
Site Type (Urban or Rural)	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET
Hydraulic Condition	On Grade	On Grade
Inlet Type	CDOT/Denver 13 Combination	CDOT/Denver 13 Combination

## USER-DEFINED INPUT

<b>User-Defined Design Flows</b>		
Minor $Q_{known}$ (cfs)	0.4	0.9
Major $Q_{known}$ (cfs)	0.6	1.3
<b>Bypass (Carry-Over) Flow from Upstream</b>		
Receive Bypass Flow from:	User-Defined	User-Defined
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.1
<b>Watershed Characteristics</b>		
Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		
<b>Watershed Profile</b>		
Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		
<b>Minor Storm Rainfall Input</b>		
Design Storm Return Period, $T_r$ (years)		
One-Hour Precipitation, $P_1$ (inches)		
<b>Major Storm Rainfall Input</b>		
Design Storm Return Period, $T_r$ (years)		
One-Hour Precipitation, $P_1$ (inches)		

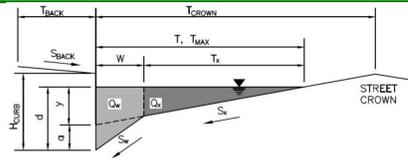
## CALCULATED OUTPUT

<b>Minor Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>0.4</b>	<b>0.9</b>
<b>Major Total Design Peak Flow, <math>Q</math> (cfs)</b>	<b>0.6</b>	<b>1.4</b>
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	0.0	0.0
Major Flow Bypassed Downstream, $Q_b$ (cfs)	0.1	0.0

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

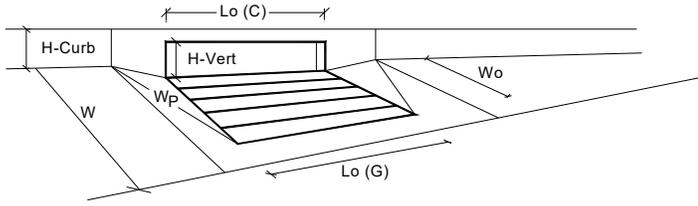
Inlet ID: **SD IN1**



<b>Gutter Geometry:</b>													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 0.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.050$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 14.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 18.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.035$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.000$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>T_{MAX}</math></td> <td>18.0</td> <td>18.0</td> <td>ft</td> </tr> <tr> <td><math>d_{MAX}</math></td> <td>6.0</td> <td>14.0</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX}$	18.0	18.0	ft	$d_{MAX}$	6.0	14.0	inches
	Minor Storm	Major Storm											
$T_{MAX}$	18.0	18.0	ft										
$d_{MAX}$	6.0	14.0	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>												
<b>MINOR STORM Allowable Capacity is not applicable to Sump Condition</b>													
<b>MAJOR STORM Allowable Capacity is not applicable to Sump Condition</b>													
<b>Q<sub>allow</sub></b>	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><b>Q<sub>allow</sub></b></td> <td><b>SUMP</b></td> <td><b>SUMP</b></td> <td><b>cfs</b></td> </tr> </table>		Minor Storm	Major Storm		<b>Q<sub>allow</sub></b>	<b>SUMP</b>	<b>SUMP</b>	<b>cfs</b>				
	Minor Storm	Major Storm											
<b>Q<sub>allow</sub></b>	<b>SUMP</b>	<b>SUMP</b>	<b>cfs</b>										

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

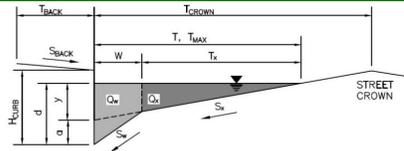


		MINOR	MAJOR	
<b>Design Information (Input)</b>				
Type of Inlet	CDOT/Denver 13 Valley Grate			
Local Depression (additional to continuous gutter depression 'a' from above)		2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)		3	3	
Water Depth at Flowline (outside of local depression)		6.0	6.8	inches
<b>Grate Information</b>				
Length of a Unit Grate		3.00	3.00	feet
Width of a Unit Grate		1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)		0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)		3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		0.60	0.60	
<b>Curb Opening Information</b>				
Length of a Unit Curb Opening		N/A	N/A	feet
Height of Vertical Curb Opening in Inches		N/A	N/A	inches
Height of Curb Orifice Throat in Inches		N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)		N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>				
Depth for Grate Midwidth		0.52	0.59	ft
Depth for Curb Opening Weir Equation		N/A	N/A	ft
Grated Inlet Performance Reduction Factor for Long Inlets		0.57	0.64	
Curb Opening Performance Reduction Factor for Long Inlets		N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets		N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>				
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>		4.4	5.9	cfs
Q PEAK REQUIRED		3.4	5.4	cfs

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:**  
**Inlet ID: SD IN2**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK}$	0.0	ft
$S_{BACK}$	0.000	ft/ft
$n_{BACK}$	0.020	
$H_{CURB}$	14.00	inches
$T_{CROWN}$	18.0	ft
$W$	2.00	ft
$S_x$	0.030	ft/ft
$S_w$	0.083	ft/ft
$S_0$	0.000	ft/ft
$n_{STREET}$	0.020	
$T_{MAX}$	Minor Storm: 18.0, Major Storm: 18.0	ft
$d_{MAX}$	Minor Storm: 6.0, Major Storm: 12.0	inches
	<input type="checkbox"/> <input type="checkbox"/>	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

**Maximum Capacity for 1/2 Street based On Allowable Spread**

Water Depth without Gutter Depression ( $T * S_x * 12$ )  
 Vertical Depth between Gutter Lip and Gutter Flowline ( $W * S_w * 12$ )  
 Gutter Depression ( $d_c - (W * S_x * 12)$ )  
 Water Depth at Gutter Flowline ( $y + a$ )  
 Allowable Spread for Discharge outside the Gutter Section ( $T - W$ )  
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. 7-7)  
 Discharge outside the Gutter Section, carried in Section  $T_x$   
 Discharge within the Gutter Section ( $Q_T - Q_x - Q_{BACK}$ )  
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)  
 Maximum Flow Based On Allowable Spread  
 Flow Velocity within the Gutter Section  
 $V*d$  Product: Flow Velocity times Gutter Flowline Depth

	Minor Storm	Major Storm	
$y$	6.48	6.48	inches
$d_c$	2.0	2.0	inches
$a$	1.27	1.27	inches
$d$	7.75	7.75	inches
$T_x$	16.0	16.0	ft
$E_0$	0.304	0.304	
$Q_x$	0.0	0.0	cfs
$Q_w$	0.0	0.0	cfs
$Q_{BACK}$	0.0	0.0	cfs
$Q_T$	SUMP	SUMP	cfs
$V$	0.0	0.0	fps
$V*d$	0.0	0.0	

**Maximum Capacity for 1/2 Street based on Allowable Depth**

Theoretical Water Spread  
 Theoretical Spread for Discharge outside the Gutter Section ( $T - W$ )  
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. 7-7)  
 Theoretical Discharge outside the Gutter Section, carried in Section  $T_{X,TH}$   
 Actual Discharge outside the Gutter Section, (limited by distance  $T_{CROWN}$ )  
 Discharge within the Gutter Section ( $Q_d - Q_x$ )  
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)  
 Total Discharge for Major & Minor Storm (Pre-Safety Factor)  
 Average Flow Velocity Within the Gutter Section  
 $V*d$  Product: Flow Velocity Times Gutter Flowline Depth  
 Slope-Based Safety Factor for Minor/Major Storm depth reduction,  $d \geq 6"$   
 Max Flow based on Allowable Depth (Safety Factor Applied)  
 Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)  
 Resultant Flow Depth at Street Crown (Safety Factor Applied)

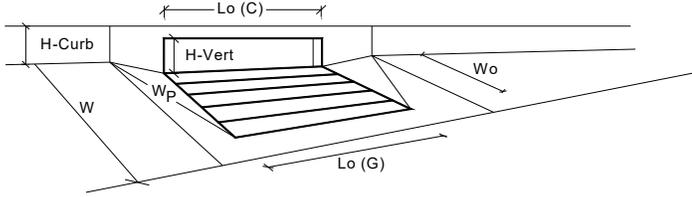
	Minor Storm	Major Storm	
$T_{TH}$	13.1	29.8	ft
$T_{X,TH}$	11.1	27.8	ft
$E_0$	0.411	0.184	
$Q_{X,TH}$	0.0	0.0	cfs
$Q_x$	0.0	0.0	cfs
$Q_w$	0.0	0.0	cfs
$Q_{BACK}$	0.0	0.0	cfs
$Q$	SUMP	SUMP	cfs
$V$	0.0	0.0	fps
$V*d$	0.0	0.0	
$R$	SUMP	SUMP	
$Q_d$	SUMP	SUMP	cfs
$d$			inches
$d_{CROWN}$			inches

MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

$Q_{allow}$	Minor Storm: SUMP, Major Storm: SUMP	cfs
-------------	--------------------------------------	-----

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

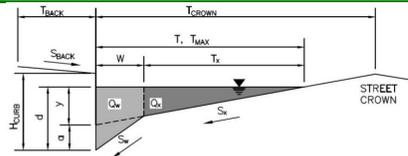


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Valley Grate		
Local Depression (additional to continuous gutter depression 'a' from above)	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	3	3	
Water Depth at Flowline (outside of local depression)	6.5	8.2	inches
<b>Grate Information</b>			
Length of a Unit Grate	3.00	3.00	feet
Width of a Unit Grate	1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	0.60	0.60	
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening	N/A	N/A	feet
Height of Vertical Curb Opening in Inches	N/A	N/A	inches
Height of Curb Orifice Throat in Inches	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth	0.56	0.70	ft
Depth for Curb Opening Weir Equation	N/A	N/A	ft
Grated Inlet Performance Reduction Factor for Long Inlets	0.61	0.77	
Curb Opening Performance Reduction Factor for Long Inlets	N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	<b>5.3</b>	<b>9.2</b>	cfs
Q PEAK REQUIRED =	4.5	7.0	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

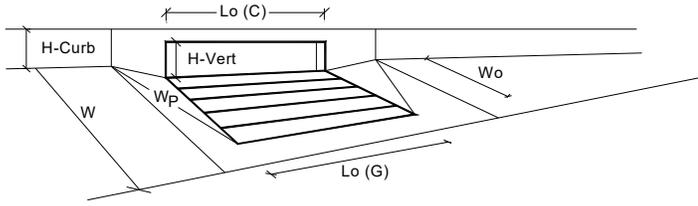
Inlet ID: **SD IN3**



<b>Gutter Geometry:</b>													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 4.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.010$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 18.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.040$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.000$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>T_{MAX}</math></td> <td>18.0</td> <td>18.0</td> <td>ft</td> </tr> <tr> <td><math>d_{MAX}</math></td> <td>6.0</td> <td>6.3</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX}$	18.0	18.0	ft	$d_{MAX}$	6.0	6.3	inches
	Minor Storm	Major Storm											
$T_{MAX}$	18.0	18.0	ft										
$d_{MAX}$	6.0	6.3	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>d_{MAX}</math></td> <td>6.0</td> <td>6.3</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$d_{MAX}$	6.0	6.3	inches				
	Minor Storm	Major Storm											
$d_{MAX}$	6.0	6.3	inches										
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>												
MINOR STORM Allowable Capacity is not applicable to Sump Condition													
MAJOR STORM Allowable Capacity is not applicable to Sump Condition													
<b>Q<sub>allow</sub></b>	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><b>Q<sub>allow</sub></b></td> <td><b>SUMP</b></td> <td><b>SUMP</b></td> <td><b>cfs</b></td> </tr> </table>		Minor Storm	Major Storm		<b>Q<sub>allow</sub></b>	<b>SUMP</b>	<b>SUMP</b>	<b>cfs</b>				
	Minor Storm	Major Storm											
<b>Q<sub>allow</sub></b>	<b>SUMP</b>	<b>SUMP</b>	<b>cfs</b>										

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

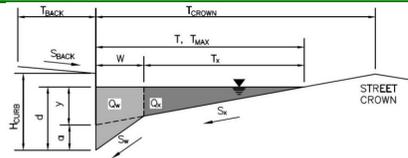


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	2	2	
Water Depth at Flowline (outside of local depression)	6.0	6.3	inches
<b>Grate Information</b>			
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.35	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	0.93	0.95	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	8.3	9.2	cfs
Q PEAK REQUIRED	5.4	8.3	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Inlet ID: **SD IN4**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$	0.0	ft
$S_{BACK}$	0.000	ft/ft
$n_{BACK}$	0.012	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$	6.00	inches
$T_{CROWN}$	13.0	ft
$W$	2.00	ft
$S_x$	0.030	ft/ft
$S_w$	0.083	ft/ft
$S_o$	0.000	ft/ft
$n_{STREET}$	0.020	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

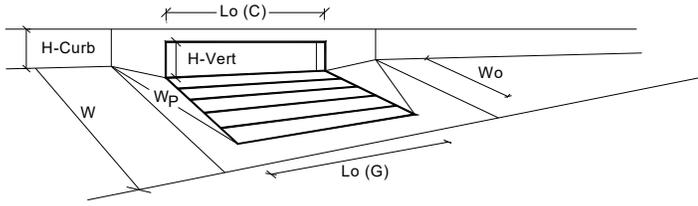
	Minor Storm	Major Storm	
$T_{MAX}$	13.0	13.0	ft
$d_{MAX}$	6.0	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

	Minor Storm	Major Storm	
$Q_{allow}$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

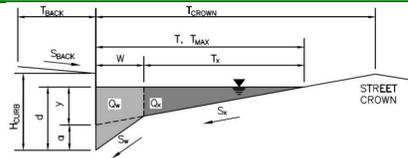


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Combination		
Local Depression (additional to continuous gutter depression 'a' from above)	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
<b>Grate Information</b>			
Length of a Unit Grate	3.00	3.00	feet
Width of a Unit Grate	1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	0.60	0.60	
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening	3.00	3.00	feet
Height of Vertical Curb Opening in Inches	6.50	6.50	inches
Height of Curb Orifice Throat in Inches	5.25	5.25	inches
Angle of Throat (see USDCM Figure ST-5)	0.00	0.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.70	3.70	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.66	0.66	
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth	0.52	0.52	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	0.94	0.94	
Curb Opening Performance Reduction Factor for Long Inlets	N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets	0.94	0.94	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	<b>5.1</b>	<b>5.1</b>	<b>cfs</b>
Q PEAK REQUIRED =	3.2	5.0	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

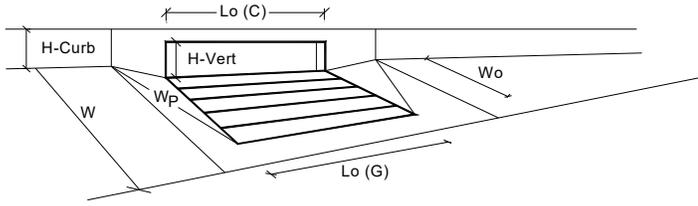
Inlet ID: **SD IN5**



<b>Gutter Geometry:</b>													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 0.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.000$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 12.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 18.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.040$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.000$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>T_{MAX}</math></td> <td>18.0</td> <td>18.0</td> <td>ft</td> </tr> <tr> <td><math>d_{MAX}</math></td> <td>7.9</td> <td>7.9</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX}$	18.0	18.0	ft	$d_{MAX}$	7.9	7.9	inches
	Minor Storm	Major Storm											
$T_{MAX}$	18.0	18.0	ft										
$d_{MAX}$	7.9	7.9	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>d_{MAX}</math></td> <td>7.9</td> <td>7.9</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$d_{MAX}$	7.9	7.9	inches				
	Minor Storm	Major Storm											
$d_{MAX}$	7.9	7.9	inches										
Check boxes are not applicable in SUMP conditions	<table border="1"> <tr> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> </tr> </table>	<input type="checkbox"/>	<input type="checkbox"/>										
<input type="checkbox"/>	<input type="checkbox"/>												
MINOR STORM Allowable Capacity is not applicable to Sump Condition													
MAJOR STORM Allowable Capacity is not applicable to Sump Condition													
Allowable Capacity	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>Q_{allow}</math></td> <td>SUMP</td> <td>SUMP</td> <td>cfs</td> </tr> </table>		Minor Storm	Major Storm		$Q_{allow}$	SUMP	SUMP	cfs				
	Minor Storm	Major Storm											
$Q_{allow}$	SUMP	SUMP	cfs										

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

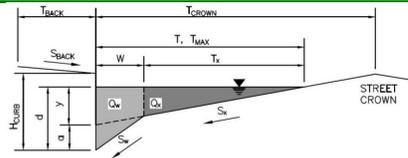


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Valley Grate		
Local Depression (additional to continuous gutter depression 'a' from above)	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	7.9	7.9	inches
<input type="checkbox"/> Override Depths			
<b>Grate Information</b>			
Length of a Unit Grate	3.00	3.00	feet
Width of a Unit Grate	1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	0.60	0.60	
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening	N/A	N/A	feet
Height of Vertical Curb Opening in Inches	N/A	N/A	inches
Height of Curb Orifice Throat in Inches	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth	0.68	0.68	ft
Depth for Curb Opening Weir Equation	N/A	N/A	ft
Grated Inlet Performance Reduction Factor for Long Inlets	1.00	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	<b>4.0</b>	<b>4.0</b>	<b>cfs</b>
Q PEAK REQUIRED	1.2	2.0	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Inlet ID: **SD IN6**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T<sub>BACK</sub> = 0.0 ft  
 S<sub>BACK</sub> = 0.000 ft/ft  
 n<sub>BACK</sub> = 0.020

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H<sub>CURB</sub> = 12.00 inches  
 T<sub>CROWN</sub> = 18.0 ft  
 W = 2.00 ft  
 S<sub>x</sub> = 0.040 ft/ft  
 S<sub>w</sub> = 0.083 ft/ft  
 S<sub>0</sub> = 0.000 ft/ft  
 n<sub>STREET</sub> = 0.020

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
T <sub>MAX</sub>	18.0	18.0	ft
d <sub>MAX</sub>	6.0	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

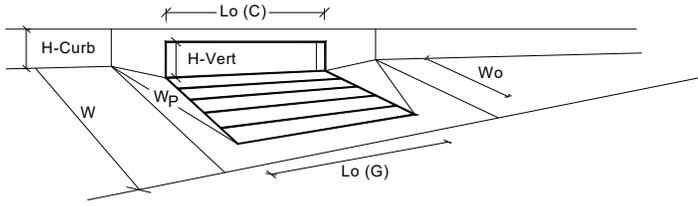
MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

Q<sub>allow</sub> = 

Minor Storm	Major Storm	
SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)



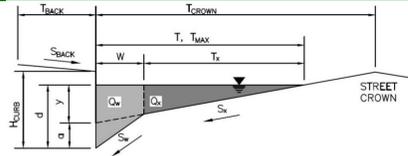
Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Valley Grate		
Local Depression (additional to continuous gutter depression 'a' from above)	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
<input type="checkbox"/> Override Depths			
<b>Grate Information</b>			
Length of a Unit Grate	3.00	3.00	feet
Width of a Unit Grate	1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	0.60	0.60	
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening	N/A	N/A	feet
Height of Vertical Curb Opening in Inches	N/A	N/A	inches
Height of Curb Orifice Throat in Inches	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth	0.52	0.52	ft
Depth for Curb Opening Weir Equation	N/A	N/A	ft
Grated Inlet Performance Reduction Factor for Long Inlets	0.94	0.94	
Curb Opening Performance Reduction Factor for Long Inlets	N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	<b>2.6</b>	<b>2.6</b>	<b>cfs</b>
Q PEAK REQUIRED =	1.4	2.4	cfs

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Inlet ID: **SD IN7**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK}$	0.0	ft
$S_{BACK}$	0.000	ft/ft
$n_{BACK}$	0.020	

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB}$	11.00	inches
$T_{CROWN}$	25.0	ft
$W$	5.00	ft
$S_X$	0.040	ft/ft
$S_W$	0.083	ft/ft
$S_0$	0.000	ft/ft
$n_{STREET}$	0.020	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX}$	12.5	18.0	ft
$d_{MAX}$	8.8	8.8	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

**Maximum Capacity for 1/2 Street based On Allowable Spread**

Water Depth without Gutter Depression ( $T * S_x * 12$ )  
 Vertical Depth between Gutter Lip and Gutter Flowline ( $W * S_w * 12$ )  
 Gutter Depression ( $d_c - (W * S_x * 12)$ )  
 Water Depth at Gutter Flowline ( $y + a$ )  
 Allowable Spread for Discharge outside the Gutter Section ( $T - W$ )  
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. 7-7)  
 Discharge outside the Gutter Section, carried in Section  $T_X$   
 Discharge within the Gutter Section ( $Q_T - Q_X - Q_{BACK}$ )  
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)  
 Maximum Flow Based On Allowable Spread  
 Flow Velocity within the Gutter Section  
 $V*d$  Product: Flow Velocity times Gutter Flowline Depth

	Minor Storm	Major Storm	
$y$	6.00	8.64	inches
$d_c$	5.0	5.0	inches
$a$	2.58	2.58	inches
$d$	8.58	11.22	inches
$T_X$	7.5	13.0	ft
$E_0$	0.815	0.646	
$Q_X$	0.0	0.0	cfs
$Q_W$	0.0	0.0	cfs
$Q_{BACK}$	0.0	#DIV/0!	cfs
$Q_T$	SUMP	SUMP	cfs
$V$	0.0	0.0	fps
$V*d$	0.0	0.0	

**Maximum Capacity for 1/2 Street based on Allowable Depth**

Theoretical Water Spread  
 Theoretical Spread for Discharge outside the Gutter Section ( $T - W$ )  
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. 7-7)  
 Theoretical Discharge outside the Gutter Section, carried in Section  $T_{X,TH}$   
 Actual Discharge outside the Gutter Section, (limited by distance  $T_{CROWN}$ )  
 Discharge within the Gutter Section ( $Q_d - Q_X$ )  
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)  
 Total Discharge for Major & Minor Storm (Pre-Safety Factor)  
 Average Flow Velocity Within the Gutter Section  
 $V*d$  Product: Flow Velocity Times Gutter Flowline Depth  
 Slope-Based Safety Factor for Minor/Major Storm depth reduction,  $d \geq 6"$   
 Max Flow based on Allowable Depth (Safety Factor Applied)  
 Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)  
 Resultant Flow Depth at Street Crown (Safety Factor Applied)

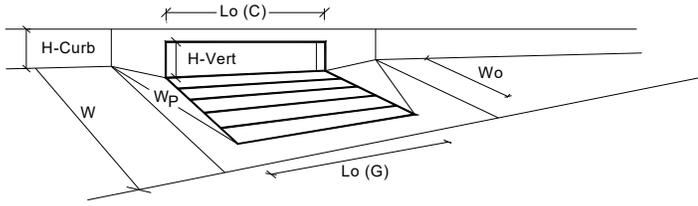
	Minor Storm	Major Storm	
$T_{TH}$	12.9	12.9	ft
$T_{X,TH}$	7.9	7.9	ft
$E_0$	0.803	0.803	
$Q_{X,TH}$	0.0	0.0	cfs
$Q_X$	0.0	0.0	cfs
$Q_W$	0.0	0.0	cfs
$Q_{BACK}$	0.0	0.0	cfs
$Q$	SUMP	SUMP	cfs
$V$	0.0	0.0	fps
$V*d$	0.0	0.0	
$R$	SUMP	SUMP	
$Q_d$	SUMP	SUMP	cfs
$d$			inches
$d_{CROWN}$			inches

MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

	Minor Storm	Major Storm	
$Q_{allow}$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

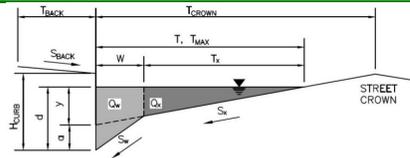


		MINOR	MAJOR	
<b>Design Information (Input)</b>				
Type of Inlet	CDOT/Denver 13 Valley Grate			
Local Depression (additional to continuous gutter depression 'a' from above)		2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)		2	2	
Water Depth at Flowline (outside of local depression)		8.6	8.8	inches
<b>Grate Information</b>				
Length of a Unit Grate		3.00	3.00	feet
Width of a Unit Grate		1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)		0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)		3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		0.60	0.60	
<b>Curb Opening Information</b>				
Length of a Unit Curb Opening		N/A	N/A	feet
Height of Vertical Curb Opening in Inches		N/A	N/A	inches
Height of Curb Orifice Throat in Inches		N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)		N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>				
Depth for Grate Midwidth		0.78	0.80	ft
Depth for Curb Opening Weir Equation		N/A	N/A	ft
Grated Inlet Performance Reduction Factor for Long Inlets		1.00	1.00	
Curb Opening Performance Reduction Factor for Long Inlets		N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets		N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>				
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>		9.4	9.7	cfs
Q PEAK REQUIRED		5.8	9.3	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

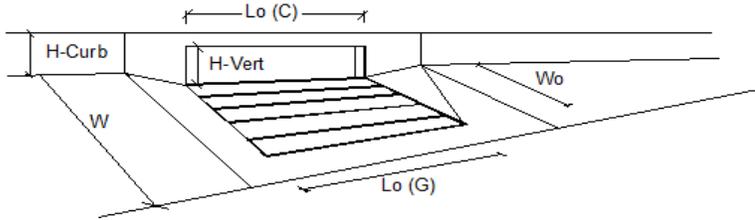
Inlet ID: **SD IN8**



<b>Gutter Geometry:</b>	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 0.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.000$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$
Height of Curb at Gutter Flow Line	$H_{CURB} = 11.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 18.0$ ft
Gutter Width	$W = 5.00$ ft
Street Transverse Slope	$S_x = 0.040$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.005$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 12.5 & 12.5 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 8.0 & 8.0 \end{matrix}$ inches
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<input type="checkbox"/> <input type="checkbox"/>
<a href="#">MINOR STORM Allowable Capacity is based on Depth Criterion</a>	
<a href="#">MAJOR STORM Allowable Capacity is based on Depth Criterion</a>	
<b>Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.03 cfs on sheet 'Inlet Management'</b>	$Q_{allow} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 8.7 & 8.7 \end{matrix}$ cfs
<b>Major storm max. allowable capacity GOOD - greater than the design peak flow of 6.42 cfs on sheet 'Inlet Management'</b>	

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

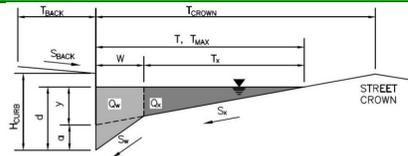


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Valley Gate		
Local Depression (additional to continuous gutter depression 'a')	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	3.00	3.00	ft
Width of a Single Unit Inlet (Grate or Curb Opening)	1.73	1.73	ft
Clogging Factor for a Single Unit Inlet (typical min. value = 0.5)	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	2.0	2.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	2.1	3.7	cfs
Capture Percentage = $Q_i/Q_o$	49	43	%

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Inlet ID: **SD IN9**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} =$   ft  
 $S_{BACK} =$   ft/ft  
 $n_{BACK} =$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} =$   inches  
 $T_{CROWN} =$   ft  
 $W =$   ft  
 $S_x =$   ft/ft  
 $S_w =$   ft/ft  
 $S_o =$   ft/ft  
 $n_{STREET} =$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	<input type="text" value="12.5"/>	<input type="text" value="12.5"/>	ft
$d_{MAX} =$	<input type="text" value="10.0"/>	<input type="text" value="10.0"/>	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

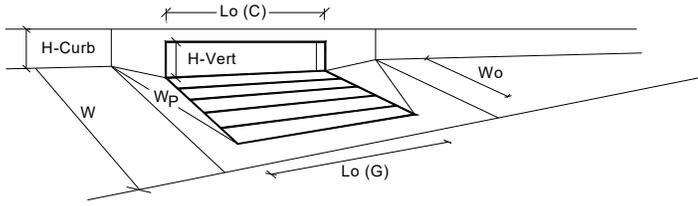
MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

$Q_{allow} =$ 

Minor Storm	Major Storm	
<input type="text" value="SUMP"/>	<input type="text" value="SUMP"/>	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.02 (August 2022)

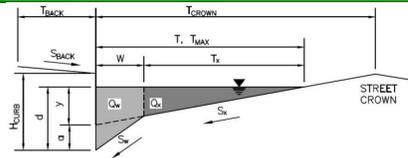


		MINOR	MAJOR	
<b>Design Information (Input)</b>				
Type of Inlet	CDOT/Denver 13 Valley Grate			
Local Depression (additional to continuous gutter depression 'a' from above)		2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)		3	3	
Water Depth at Flowline (outside of local depression)		8.6	8.6	inches
<b>Grate Information</b>				
Length of a Unit Grate		3.00	3.00	feet
Width of a Unit Grate		1.73	1.73	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)		0.43	0.43	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)		3.30	3.30	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		0.60	0.60	
<b>Curb Opening Information</b>				
Length of a Unit Curb Opening		N/A	N/A	feet
Height of Vertical Curb Opening in Inches		N/A	N/A	inches
Height of Curb Orifice Throat in Inches		N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)		N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>				
Depth for Grate Midwidth		0.78	0.78	ft
Depth for Curb Opening Weir Equation		N/A	N/A	ft
Grated Inlet Performance Reduction Factor for Long Inlets		0.81	0.81	
Curb Opening Performance Reduction Factor for Long Inlets		N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets		N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>				
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>		11.4	11.4	cfs
Q PEAK REQUIRED		6.0	9.8	cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

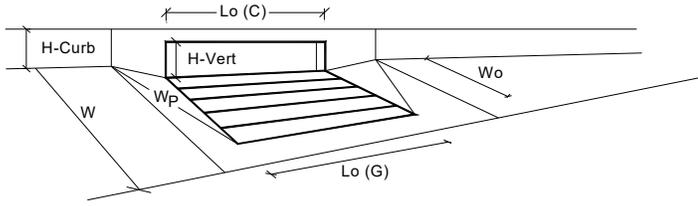
Inlet ID: **SD IN10**



<b>Gutter Geometry:</b>	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 2.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.070$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 30.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_x = 0.040$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.000$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 20.0 & 20.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 6.0 & 6.0 \end{matrix}$ inches
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>
<b>MINOR STORM Allowable Capacity is not applicable to Sump Condition</b>	
<b>MAJOR STORM Allowable Capacity is not applicable to Sump Condition</b>	
<b>Q<sub>allow</sub> =</b>	<b>SUMP SUMP cfs</b>

# INLET IN A SUMP OR SAG LOCATION

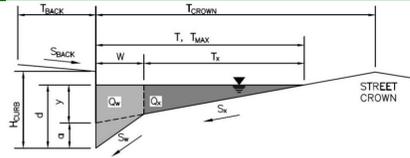
MHFD-Inlet, Version 5.02 (August 2022)



Design Information (Input)	MINOR      MAJOR	
Type of Inlet <span style="float: right;">CDOT Type R Curb Opening</span>	Type = <b>CDOT Type R Curb Opening</b>	
Local Depression (additional to continuous gutter depression 'a' from above)	$a_{local} = 3.00$	3.00 inches
Number of Unit Inlets (Grate or Curb Opening)	No = 1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth = 6.0	6.0 inches
<b>Grate Information</b>	<input type="checkbox"/> Override Depths	
Length of a Unit Grate	$L_o(G) = N/A$	N/A feet
Width of a Unit Grate	$W_o = N/A$	N/A feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} = N/A$	N/A
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) = N/A$	N/A
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) = N/A$	N/A
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = N/A$	N/A
<b>Curb Opening Information</b>	MINOR      MAJOR	
Length of a Unit Curb Opening	$L_o(C) = 5.00$	5.00 feet
Height of Vertical Curb Opening in Inches	$H_{vert} = 6.00$	6.00 inches
Height of Curb Orifice Throat in Inches	$H_{throat} = 6.00$	6.00 inches
Angle of Throat (see USDCM Figure ST-5)	Theta = 63.40	63.40 degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = 2.00$	2.00 feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) = 0.10$	0.10
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) = 3.60$	3.60
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = 0.67$	0.67
<b>Low Head Performance Reduction (Calculated)</b>	MINOR      MAJOR	
Depth for Grate Midwidth	$d_{Grate} = N/A$	N/A ft
Depth for Curb Opening Weir Equation	$d_{Curb} = 0.33$	0.33 ft
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} = N/A$	N/A
Curb Opening Performance Reduction Factor for Long Inlets	$RF_{Curb} = 1.00$	1.00
Combination Inlet Performance Reduction Factor for Long Inlets	$RF_{combination} = N/A$	N/A
Total Inlet Interception Capacity (assumes clogged condition)	MINOR      MAJOR	
<b>Inlet Capacity IS GOOD for Minor and Major Storms (&gt;Q Peak)</b>	$Q_a = 5.4$	5.4 cfs
Q PEAK REQUIRED	2.4	4.2 cfs

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

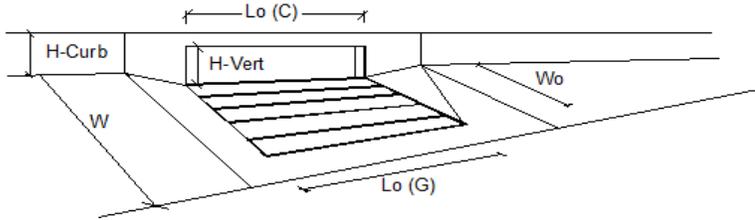
Project:  
 Inlet ID: **SD IN11**



<b>Gutter Geometry:</b>									
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 0.1$ ft								
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.100$ ft/ft								
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$								
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches								
Distance from Curb Face to Street Crown	$T_{CROWN} = 54.0$ ft								
Gutter Width	$W = 2.00$ ft								
Street Transverse Slope	$S_x = 0.040$ ft/ft								
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft								
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.014$ ft/ft								
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$								
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>T_{MAX}</math></td> <td>15.0</td> <td>15.0</td> <td>ft</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX}$	15.0	15.0	ft
	Minor Storm	Major Storm							
$T_{MAX}$	15.0	15.0	ft						
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>d_{MAX}</math></td> <td>6.0</td> <td>6.0</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$d_{MAX}$	6.0	6.0	inches
	Minor Storm	Major Storm							
$d_{MAX}$	6.0	6.0	inches						
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> </tr> <tr> <td></td> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> </tr> </table>		Minor Storm	Major Storm		<input type="checkbox"/>	<input type="checkbox"/>		
	Minor Storm	Major Storm							
	<input type="checkbox"/>	<input type="checkbox"/>							
MINOR STORM Allowable Capacity is based on Depth Criterion									
MAJOR STORM Allowable Capacity is based on Depth Criterion									
Minor storm max. allowable capacity GOOD - greater than the design peak flow of 4.63 cfs on sheet 'Inlet Management'	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>Q_{allow}</math></td> <td>8.5</td> <td>8.5</td> <td>cfs</td> </tr> </table>		Minor Storm	Major Storm		$Q_{allow}$	8.5	8.5	cfs
	Minor Storm	Major Storm							
$Q_{allow}$	8.5	8.5	cfs						
Major storm max. allowable capacity GOOD - greater than the design peak flow of 8.16 cfs on sheet 'Inlet Management'									

# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)

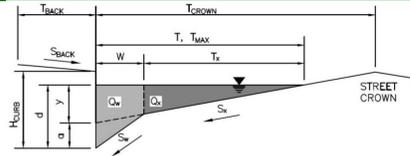


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Combination		
Local Depression (additional to continuous gutter depression 'a')	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	3.00	3.00	ft
Width of a Single Unit Inlet (Grate or Curb Opening)	1.73	1.73	ft
Clogging Factor for a Single Unit Inlet (typical min. value = 0.5)	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	4.4	7.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.2	1.0	cfs
Capture Percentage = $Q_i/Q_o$	96	88	%

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Inlet ID: **SD IN12**



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 2.0$  ft  
 $S_{BACK} = 0.040$  ft/ft  
 $n_{BACK} = 0.012$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 20.0$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.020$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

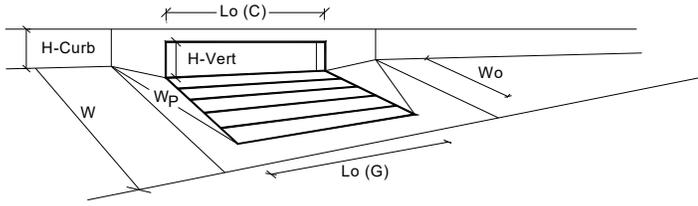
MINOR STORM Allowable Capacity is not applicable to Sump Condition  
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

$Q_{allow} =$ 

Minor Storm	Major Storm	
SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

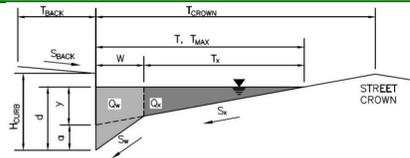
MHFD-Inlet, Version 5.02 (August 2022)



<b>Design Information (Input)</b>		<table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> <th></th> </tr> </thead> <tbody> <tr> <td>Type =</td> <td>CDOT Type R Curb Opening</td> <td></td> <td></td> </tr> <tr> <td><math>a_{local}</math> =</td> <td>3.00</td> <td>3.00</td> <td>inches</td> </tr> <tr> <td>No =</td> <td>2</td> <td>2</td> <td></td> </tr> <tr> <td>Ponding Depth =</td> <td>6.0</td> <td>6.3</td> <td>inches</td> </tr> <tr> <td></td> <td>MINOR</td> <td>MAJOR</td> <td><input type="checkbox"/> Override Depths</td> </tr> <tr> <td><math>L_o</math> (G) =</td> <td>N/A</td> <td>N/A</td> <td>feet</td> </tr> <tr> <td><math>W_o</math> =</td> <td>N/A</td> <td>N/A</td> <td>feet</td> </tr> <tr> <td><math>A_{ratio}</math> =</td> <td>N/A</td> <td>N/A</td> <td></td> </tr> <tr> <td><math>C_f</math> (G) =</td> <td>N/A</td> <td>N/A</td> <td></td> </tr> <tr> <td><math>C_w</math> (G) =</td> <td>N/A</td> <td>N/A</td> <td></td> </tr> <tr> <td><math>C_o</math> (G) =</td> <td>N/A</td> <td>N/A</td> <td></td> </tr> <tr> <td></td> <td>MINOR</td> <td>MAJOR</td> <td></td> </tr> <tr> <td><math>L_o</math> (C) =</td> <td>5.00</td> <td>5.00</td> <td>feet</td> </tr> <tr> <td><math>H_{vert}</math> =</td> <td>6.00</td> <td>6.00</td> <td>inches</td> </tr> <tr> <td><math>H_{throat}</math> =</td> <td>6.00</td> <td>6.00</td> <td>inches</td> </tr> <tr> <td>Theta =</td> <td>63.40</td> <td>63.40</td> <td>degrees</td> </tr> <tr> <td><math>W_p</math> =</td> <td>2.00</td> <td>2.00</td> <td>feet</td> </tr> <tr> <td><math>C_f</math> (C) =</td> <td>0.10</td> <td>0.10</td> <td></td> </tr> <tr> <td><math>C_w</math> (C) =</td> <td>3.60</td> <td>3.60</td> <td></td> </tr> <tr> <td><math>C_o</math> (C) =</td> <td>0.67</td> <td>0.67</td> <td></td> </tr> <tr> <td></td> <td>MINOR</td> <td>MAJOR</td> <td></td> </tr> <tr> <td><math>d_{Grate}</math> =</td> <td>N/A</td> <td>N/A</td> <td>ft</td> </tr> <tr> <td><math>d_{Curb}</math> =</td> <td>0.33</td> <td>0.36</td> <td>ft</td> </tr> <tr> <td><math>RF_{Grate}</math> =</td> <td>N/A</td> <td>N/A</td> <td></td> </tr> <tr> <td><math>RF_{Curb}</math> =</td> <td>0.93</td> <td>0.95</td> <td></td> </tr> <tr> <td><math>RF_{combination}</math> =</td> <td>N/A</td> <td>N/A</td> <td></td> </tr> <tr> <td></td> <td>MINOR</td> <td>MAJOR</td> <td></td> </tr> <tr> <td><math>Q_a</math> =</td> <td>8.3</td> <td>9.4</td> <td>cfs</td> </tr> <tr> <td><math>Q_{PEAK REQUIRED}</math> =</td> <td>3.5</td> <td>8.2</td> <td>cfs</td> </tr> </tbody> </table>			MINOR	MAJOR		Type =	CDOT Type R Curb Opening			$a_{local}$ =	3.00	3.00	inches	No =	2	2		Ponding Depth =	6.0	6.3	inches		MINOR	MAJOR	<input type="checkbox"/> Override Depths	$L_o$ (G) =	N/A	N/A	feet	$W_o$ =	N/A	N/A	feet	$A_{ratio}$ =	N/A	N/A		$C_f$ (G) =	N/A	N/A		$C_w$ (G) =	N/A	N/A		$C_o$ (G) =	N/A	N/A			MINOR	MAJOR		$L_o$ (C) =	5.00	5.00	feet	$H_{vert}$ =	6.00	6.00	inches	$H_{throat}$ =	6.00	6.00	inches	Theta =	63.40	63.40	degrees	$W_p$ =	2.00	2.00	feet	$C_f$ (C) =	0.10	0.10		$C_w$ (C) =	3.60	3.60		$C_o$ (C) =	0.67	0.67			MINOR	MAJOR		$d_{Grate}$ =	N/A	N/A	ft	$d_{Curb}$ =	0.33	0.36	ft	$RF_{Grate}$ =	N/A	N/A		$RF_{Curb}$ =	0.93	0.95		$RF_{combination}$ =	N/A	N/A			MINOR	MAJOR		$Q_a$ =	8.3	9.4	cfs	$Q_{PEAK REQUIRED}$ =	3.5	8.2	cfs
	MINOR	MAJOR																																																																																																																									
Type =	CDOT Type R Curb Opening																																																																																																																										
$a_{local}$ =	3.00	3.00	inches																																																																																																																								
No =	2	2																																																																																																																									
Ponding Depth =	6.0	6.3	inches																																																																																																																								
	MINOR	MAJOR	<input type="checkbox"/> Override Depths																																																																																																																								
$L_o$ (G) =	N/A	N/A	feet																																																																																																																								
$W_o$ =	N/A	N/A	feet																																																																																																																								
$A_{ratio}$ =	N/A	N/A																																																																																																																									
$C_f$ (G) =	N/A	N/A																																																																																																																									
$C_w$ (G) =	N/A	N/A																																																																																																																									
$C_o$ (G) =	N/A	N/A																																																																																																																									
	MINOR	MAJOR																																																																																																																									
$L_o$ (C) =	5.00	5.00	feet																																																																																																																								
$H_{vert}$ =	6.00	6.00	inches																																																																																																																								
$H_{throat}$ =	6.00	6.00	inches																																																																																																																								
Theta =	63.40	63.40	degrees																																																																																																																								
$W_p$ =	2.00	2.00	feet																																																																																																																								
$C_f$ (C) =	0.10	0.10																																																																																																																									
$C_w$ (C) =	3.60	3.60																																																																																																																									
$C_o$ (C) =	0.67	0.67																																																																																																																									
	MINOR	MAJOR																																																																																																																									
$d_{Grate}$ =	N/A	N/A	ft																																																																																																																								
$d_{Curb}$ =	0.33	0.36	ft																																																																																																																								
$RF_{Grate}$ =	N/A	N/A																																																																																																																									
$RF_{Curb}$ =	0.93	0.95																																																																																																																									
$RF_{combination}$ =	N/A	N/A																																																																																																																									
	MINOR	MAJOR																																																																																																																									
$Q_a$ =	8.3	9.4	cfs																																																																																																																								
$Q_{PEAK REQUIRED}$ =	3.5	8.2	cfs																																																																																																																								
Type of Inlet	CDOT Type R Curb Opening																																																																																																																										
Local Depression (additional to continuous gutter depression 'a' from above)																																																																																																																											
Number of Unit Inlets (Grate or Curb Opening)																																																																																																																											
Water Depth at Flowline (outside of local depression)																																																																																																																											
<b>Grate Information</b>																																																																																																																											
Length of a Unit Grate																																																																																																																											
Width of a Unit Grate																																																																																																																											
Open Area Ratio for a Grate (typical values 0.15-0.90)																																																																																																																											
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)																																																																																																																											
Grate Weir Coefficient (typical value 2.15 - 3.60)																																																																																																																											
Grate Orifice Coefficient (typical value 0.60 - 0.80)																																																																																																																											
<b>Curb Opening Information</b>																																																																																																																											
Length of a Unit Curb Opening																																																																																																																											
Height of Vertical Curb Opening in Inches																																																																																																																											
Height of Curb Orifice Throat in Inches																																																																																																																											
Angle of Throat (see USDCM Figure ST-5)																																																																																																																											
Side Width for Depression Pan (typically the gutter width of 2 feet)																																																																																																																											
Clogging Factor for a Single Curb Opening (typical value 0.10)																																																																																																																											
Curb Opening Weir Coefficient (typical value 2.3-3.7)																																																																																																																											
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)																																																																																																																											
<b>Low Head Performance Reduction (Calculated)</b>																																																																																																																											
Depth for Grate Midwidth																																																																																																																											
Depth for Curb Opening Weir Equation																																																																																																																											
Grated Inlet Performance Reduction Factor for Long Inlets																																																																																																																											
Curb Opening Performance Reduction Factor for Long Inlets																																																																																																																											
Combination Inlet Performance Reduction Factor for Long Inlets																																																																																																																											
Total Inlet Interception Capacity (assumes clogged condition)																																																																																																																											
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)																																																																																																																											

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

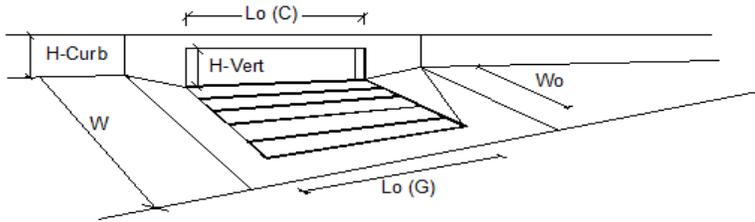
Project:  
 Inlet ID: **SD IN13**



<b>Gutter Geometry:</b>													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 0.1$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.100$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 20.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.040$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>T_{MAX} =</math></td> <td>20.0</td> <td>20.0</td> <td>ft</td> </tr> <tr> <td><math>d_{MAX} =</math></td> <td>6.0</td> <td>6.0</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX} =$	20.0	20.0	ft	$d_{MAX} =$	6.0	6.0	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	20.0	20.0	ft										
$d_{MAX} =$	6.0	6.0	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> </tr> <tr> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> </tr> </table>		Minor Storm	Major Storm	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>						
	Minor Storm	Major Storm											
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>											
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design peak flow of 0.38 cfs on sheet 'Inlet Management'	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>Q_{allow} =</math></td> <td>13.0</td> <td>13.0</td> <td>cfs</td> </tr> </table>		Minor Storm	Major Storm		$Q_{allow} =$	13.0	13.0	cfs				
	Minor Storm	Major Storm											
$Q_{allow} =$	13.0	13.0	cfs										
Major storm max. allowable capacity GOOD - greater than the design peak flow of 0.58 cfs on sheet 'Inlet Management'													

# INLET ON A CONTINUOUS GRADE

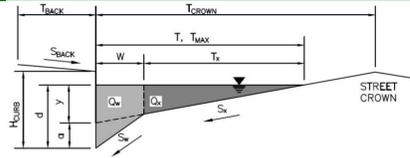
MHFD-Inlet, Version 5.02 (August 2022)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Combination		
Local Depression (additional to continuous gutter depression 'a')	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	0.4	0.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.0	0.1	cfs
Capture Percentage = $Q_i/Q_o$	94	90	%

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

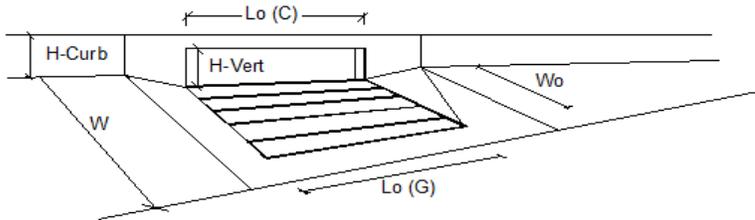
Project:  
 Inlet ID: **SD IN14**



<b>Gutter Geometry:</b>													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 0.1$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.100$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 24.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.040$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.020$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>T_{MAX}</math></td> <td>18.0</td> <td>18.0</td> <td>ft</td> </tr> <tr> <td><math>d_{MAX}</math></td> <td>6.0</td> <td>6.0</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX}$	18.0	18.0	ft	$d_{MAX}$	6.0	6.0	inches
	Minor Storm	Major Storm											
$T_{MAX}$	18.0	18.0	ft										
$d_{MAX}$	6.0	6.0	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> </tr> <tr> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> </tr> </table>		Minor Storm	Major Storm	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>						
	Minor Storm	Major Storm											
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>											
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design peak flow of 0.85 cfs on sheet 'Inlet Management'	<table border="1"> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> <tr> <td><math>Q_{allow}</math></td> <td>13.0</td> <td>13.0</td> <td>cfs</td> </tr> </table>		Minor Storm	Major Storm		$Q_{allow}$	13.0	13.0	cfs				
	Minor Storm	Major Storm											
$Q_{allow}$	13.0	13.0	cfs										
Major storm max. allowable capacity GOOD - greater than the design peak flow of 1.41 cfs on sheet 'Inlet Management'													

## INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.02 (August 2022)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Combination		
Local Depression (additional to continuous gutter depression 'a')	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	3.00	3.00	ft
Width of a Single Unit Inlet (Grate or Curb Opening)	1.73	1.73	ft
Clogging Factor for a Single Unit Inlet (typical min. value = 0.5)	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	<b>Q</b> = 0.9	<b>Q</b> = 1.4	<b>cfs</b>
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q<sub>b</sub></b> = 0.0	<b>Q<sub>b</sub></b> = 0.0	<b>cfs</b>
Capture Percentage = $Q_i/Q_o$	<b>C%</b> = 104	<b>C%</b> = 97	<b>%</b>

# Channel Report

## Drainage Pan @ Design Point 1 - 10yr

### User-defined

Invert Elev (ft) = 7163.15  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

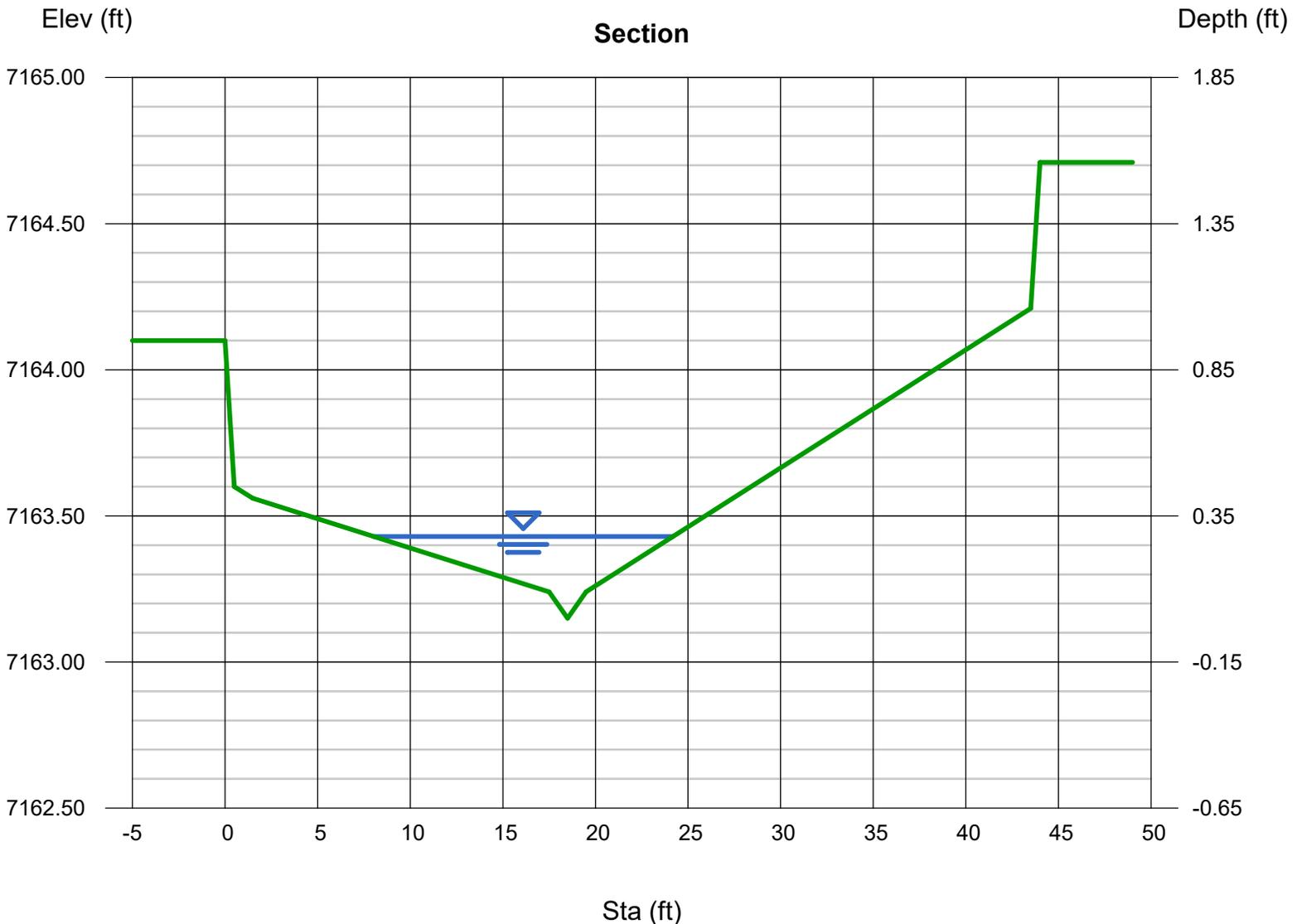
Depth (ft) = 0.28  
Q (cfs) = 3.400  
Area (sqft) = 1.81  
Velocity (ft/s) = 1.88  
Wetted Perim (ft) = 16.18  
Crit Depth, Yc (ft) = 0.28  
Top Width (ft) = 16.17  
EGL (ft) = 0.33

### Calculations

Compute by: Known Q  
Known Q (cfs) = 3.40

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7164.10)-(0.50, 7163.60, 0.013)-(1.50, 7163.56, 0.013)-(17.50, 7163.24, 0.013)-(18.50, 7163.15, 0.013)-(19.50, 7163.24, 0.013)-(43.50, 7164.21, 0.013)  
-(44.00, 7164.71, 0.013)



# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Sunday, Oct 15 2023

## Drainage Pan @ Design Point 1 - 100yr

### User-defined

Invert Elev (ft) = 7163.15  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

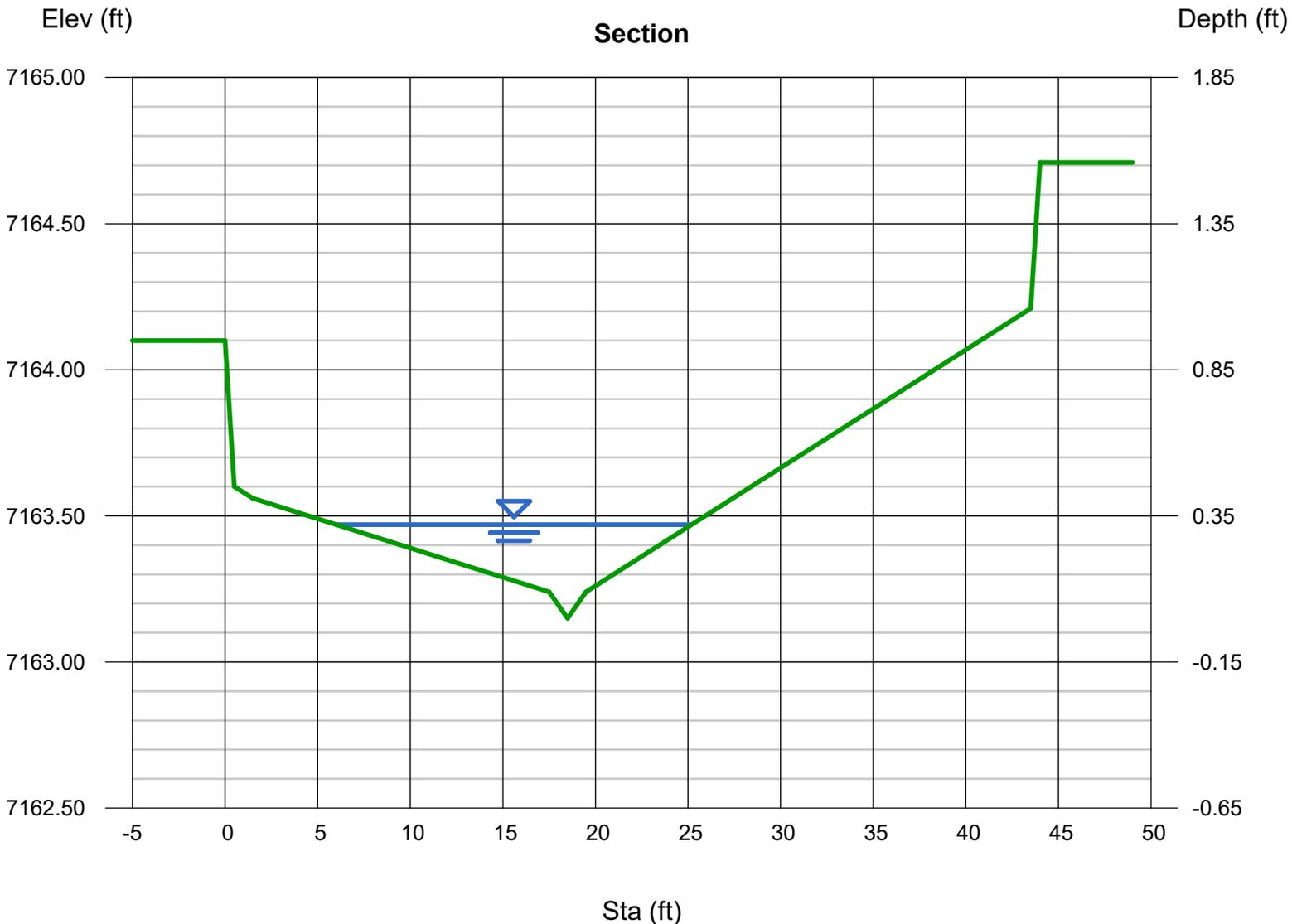
Depth (ft) = 0.32  
Q (cfs) = 5.400  
Area (sqft) = 2.52  
Velocity (ft/s) = 2.14  
Wetted Perim (ft) = 19.18  
Crit Depth, Yc (ft) = 0.33  
Top Width (ft) = 19.16  
EGL (ft) = 0.39

### Calculations

Compute by: Known Q  
Known Q (cfs) = 5.40

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7164.10)-(0.50, 7163.60, 0.013)-(1.50, 7163.56, 0.013)-(17.50, 7163.24, 0.013)-(18.50, 7163.15, 0.013)-(19.50, 7163.24, 0.013)-(43.50, 7164.21, 0.013)  
-(44.00, 7164.71, 0.013)



# Channel Report

## Drainage Pan @ Design Point 2 - 10yr

### User-defined

Invert Elev (ft) = 7160.59  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

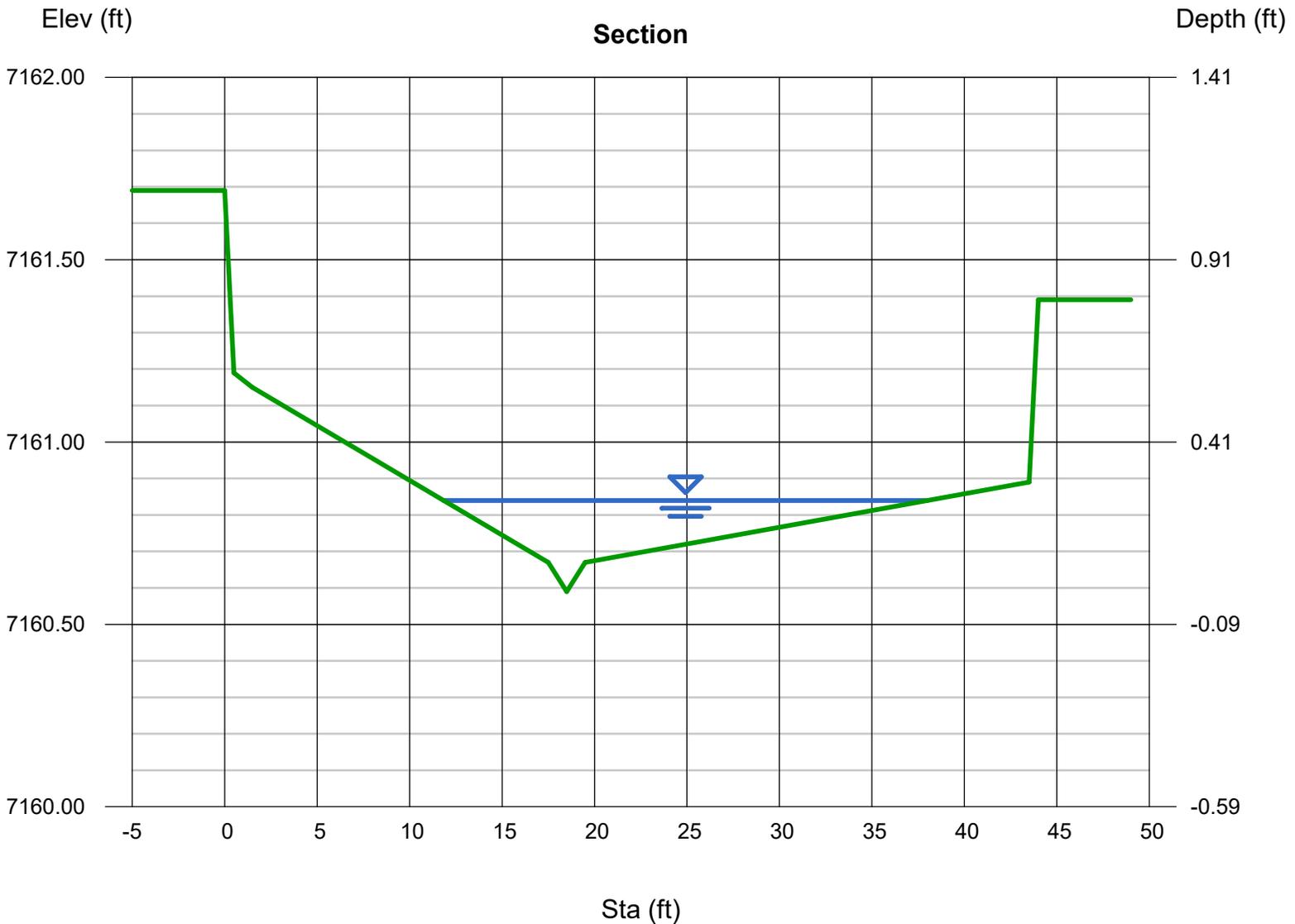
Depth (ft) = 0.25  
Q (cfs) = 4.500  
Area (sqft) = 2.47  
Velocity (ft/s) = 1.82  
Wetted Perim (ft) = 26.19  
Crit Depth, Yc (ft) = 0.26  
Top Width (ft) = 26.18  
EGL (ft) = 0.30

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.50

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7161.69)-(0.50, 7161.19, 0.013)-(1.50, 7161.15, 0.013)-(17.50, 7160.67, 0.013)-(18.50, 7160.59, 0.013)-(19.50, 7160.67, 0.013)-(43.50, 7160.89, 0.013)  
-(44.00, 7161.39, 0.013)



# Channel Report

## Drainage Pan @ Design Point 2 - 100yr

### User-defined

Invert Elev (ft) = 7160.59  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

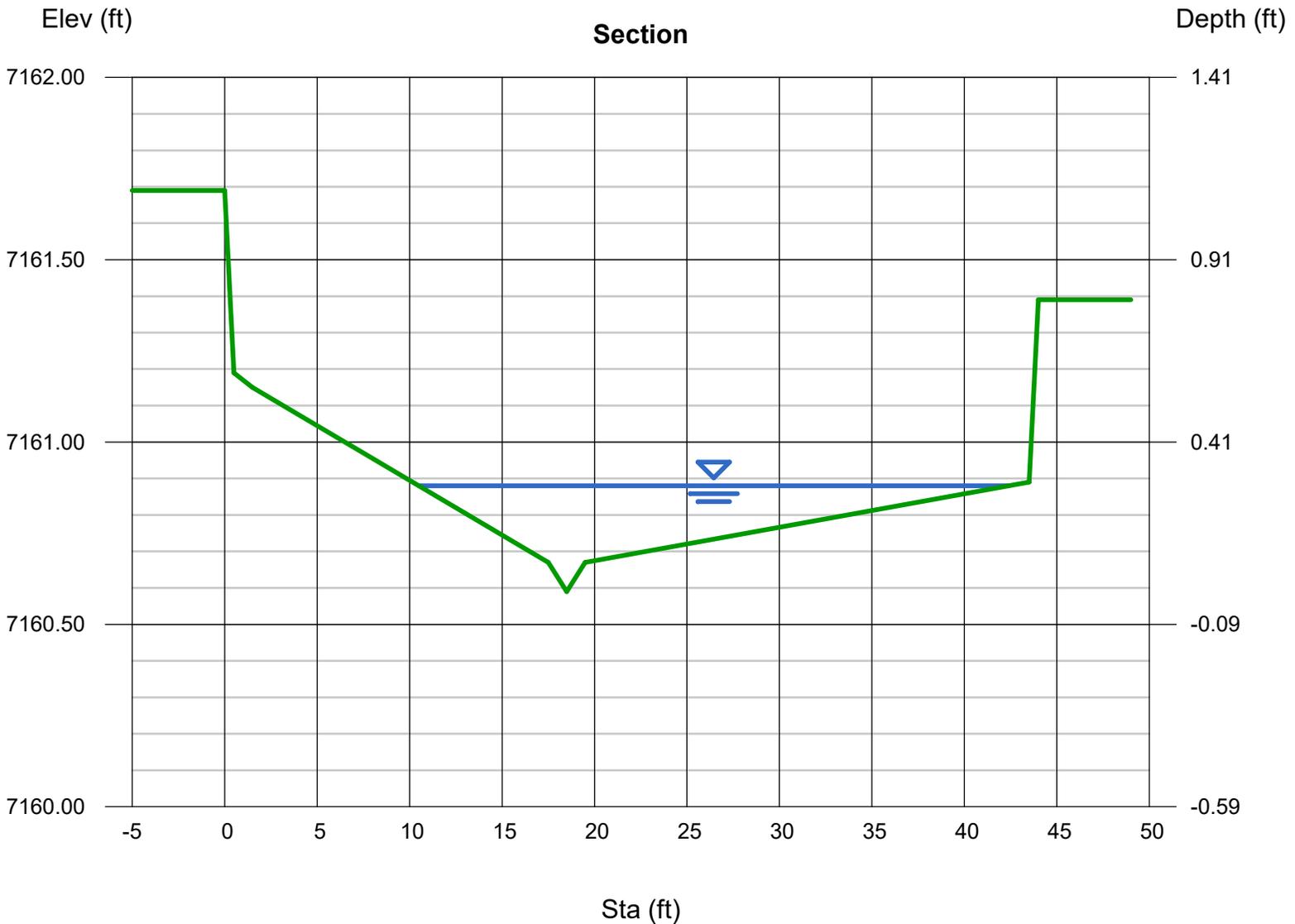
Depth (ft) = 0.29  
Q (cfs) = 7.000  
Area (sqft) = 3.64  
Velocity (ft/s) = 1.92  
Wetted Perim (ft) = 31.89  
Crit Depth, Yc (ft) = 0.30  
Top Width (ft) = 31.88  
EGL (ft) = 0.35

### Calculations

Compute by: Known Q  
Known Q (cfs) = 7.00

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7161.69)-(0.50, 7161.19, 0.013)-(1.50, 7161.15, 0.013)-(17.50, 7160.67, 0.013)-(18.50, 7160.59, 0.013)-(19.50, 7160.67, 0.013)-(43.50, 7160.89, 0.013)  
-(44.00, 7161.39, 0.013)



# Channel Report

## Drainage Pan @ Design Point 6 - 10yr

### User-defined

Invert Elev (ft) = 7164.30  
Slope (%) = 1.00  
N-Value = 0.013

### Highlighted

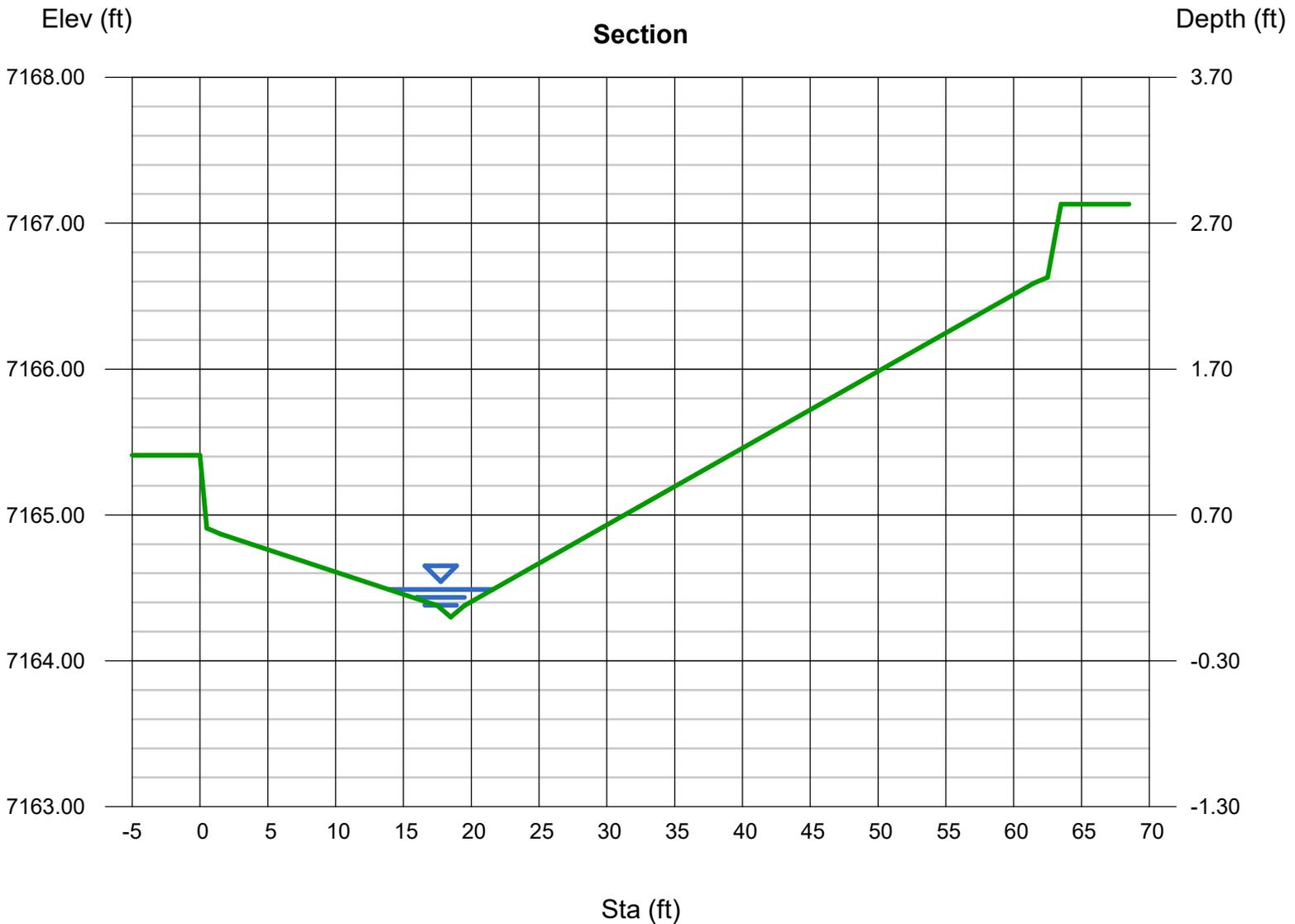
Depth (ft) = 0.19  
Q (cfs) = 1.200  
Area (sqft) = 0.61  
Velocity (ft/s) = 1.96  
Wetted Perim (ft) = 7.68  
Crit Depth, Yc (ft) = 0.21  
Top Width (ft) = 7.67  
EGL (ft) = 0.25

### Calculations

Compute by: Known Q  
Known Q (cfs) = 1.20

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7165.41)-(0.50, 7164.91, 0.013)-(1.50, 7164.87, 0.013)-(17.50, 7164.38, 0.013)-(18.50, 7164.30, 0.013)-(19.50, 7164.38, 0.013)-(61.50, 7166.59, 0.013)  
-(62.50, 7166.63, 0.013)-(63.50, 7167.13, 0.013)



# Channel Report

## Drainage Pan @ Design Point 6 - 100yr

### User-defined

Invert Elev (ft) = 7164.30  
Slope (%) = 1.00  
N-Value = 0.013

### Highlighted

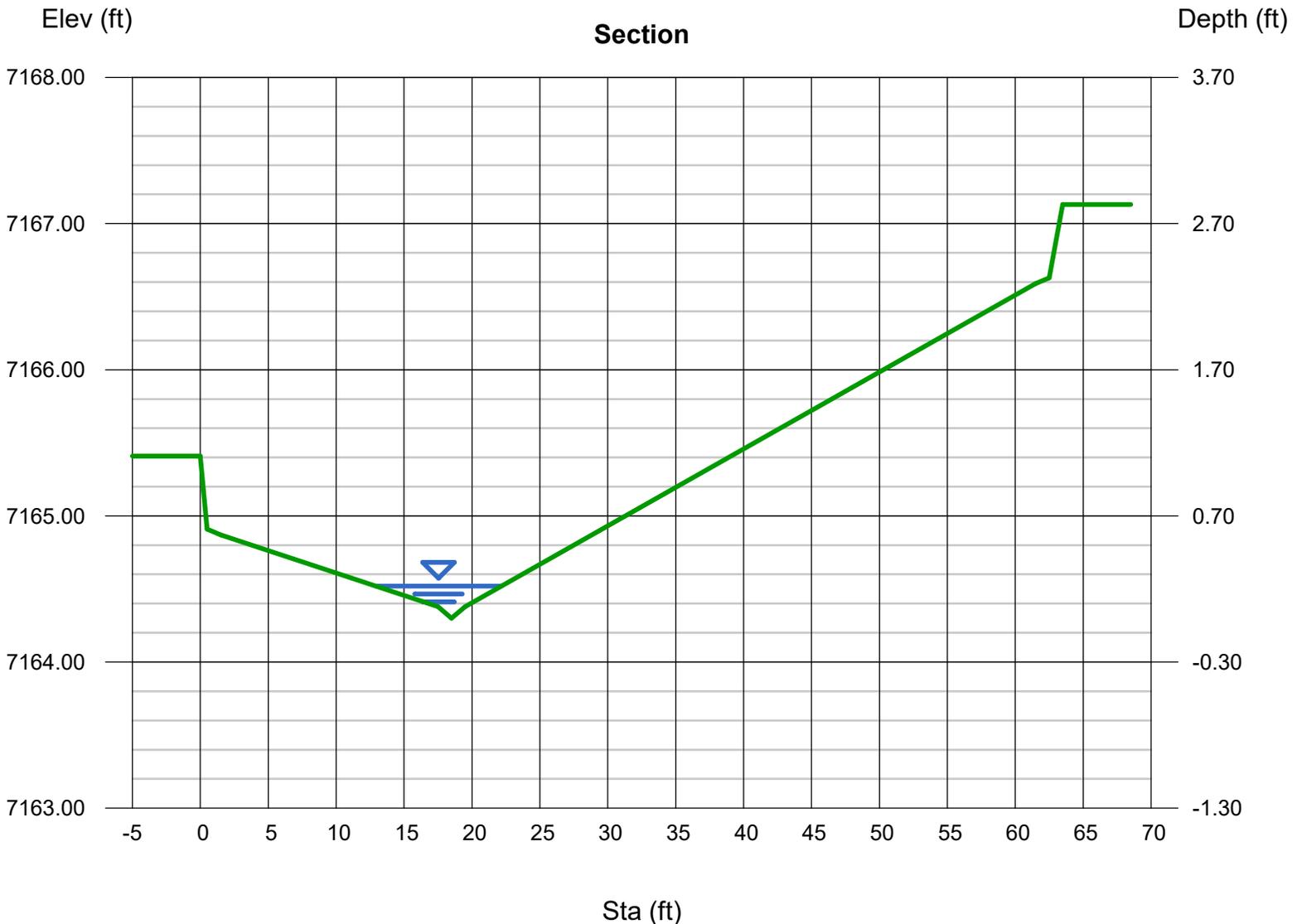
Depth (ft) = 0.22  
Q (cfs) = 2.000  
Area (sqft) = 0.87  
Velocity (ft/s) = 2.31  
Wetted Perim (ft) = 9.25  
Crit Depth, Yc (ft) = 0.25  
Top Width (ft) = 9.24  
EGL (ft) = 0.30

### Calculations

Compute by: Known Q  
Known Q (cfs) = 2.00

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7165.41)-(0.50, 7164.91, 0.013)-(1.50, 7164.87, 0.013)-(17.50, 7164.38, 0.013)-(18.50, 7164.30, 0.013)-(19.50, 7164.38, 0.013)-(61.50, 7166.59, 0.013)  
-(62.50, 7166.63, 0.013)-(63.50, 7167.13, 0.013)



# Channel Report

## Drainage Pan @ Design Point 7 - 10yr

### User-defined

Invert Elev (ft) = 7164.50  
Slope (%) = 1.00  
N-Value = 0.013

### Highlighted

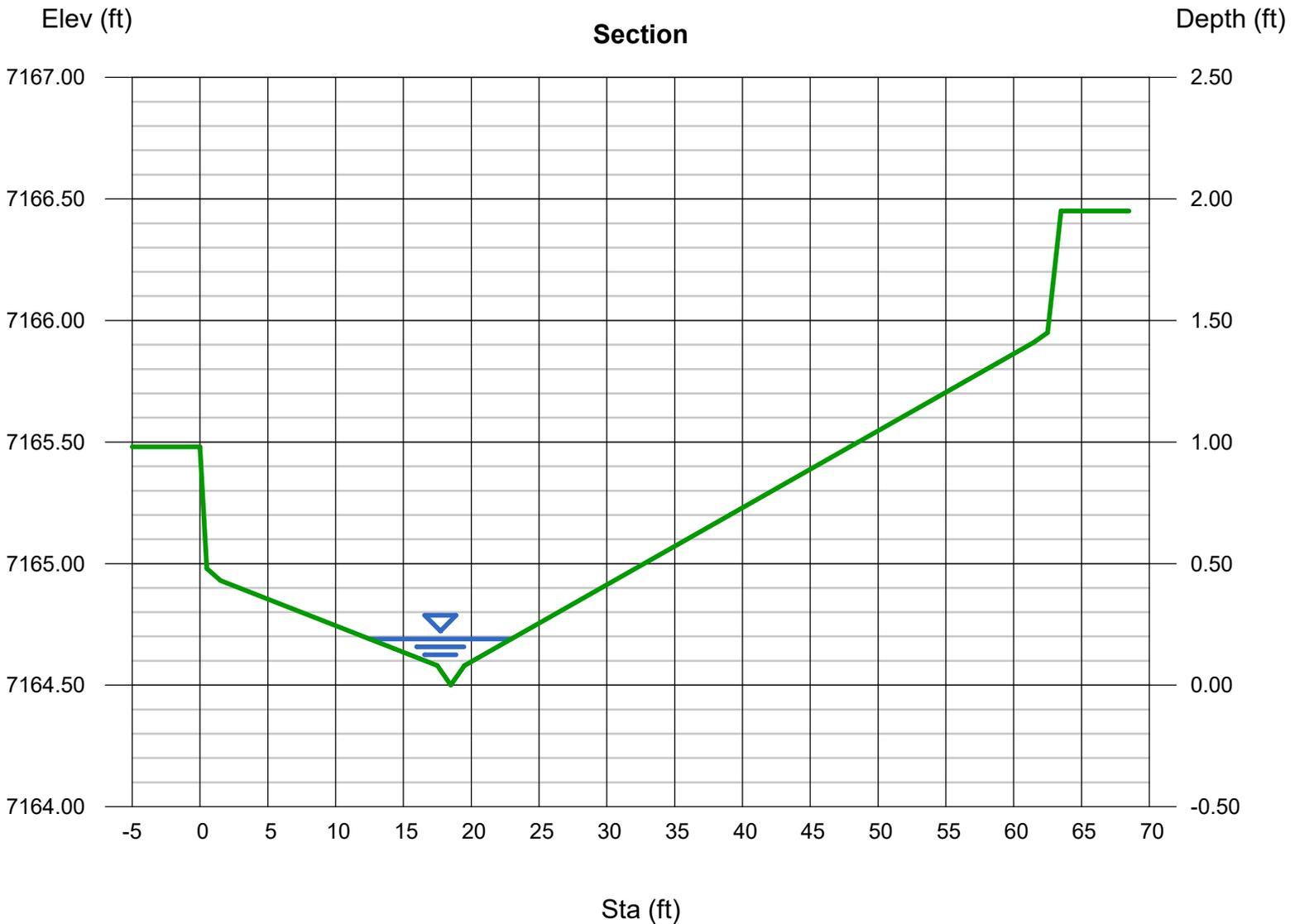
Depth (ft) = 0.19  
Q (cfs) = 1.400  
Area (sqft) = 0.77  
Velocity (ft/s) = 1.83  
Wetted Perim (ft) = 10.50  
Crit Depth, Yc (ft) = 0.21  
Top Width (ft) = 10.49  
EGL (ft) = 0.24

### Calculations

Compute by: Known Q  
Known Q (cfs) = 1.40

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7165.48)-(0.50, 7164.98, 0.013)-(1.50, 7164.93, 0.013)-(17.50, 7164.58, 0.013)-(18.50, 7164.50, 0.013)-(19.50, 7164.58, 0.013)-(61.50, 7165.91, 0.013)  
-(62.50, 7165.95, 0.013)-(63.50, 7166.45, 0.013)



# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Sunday, Oct 15 2023

## Drainage Pan @ Design Point 7 - 100yr

### User-defined

Invert Elev (ft) = 7164.50  
Slope (%) = 1.00  
N-Value = 0.013

### Highlighted

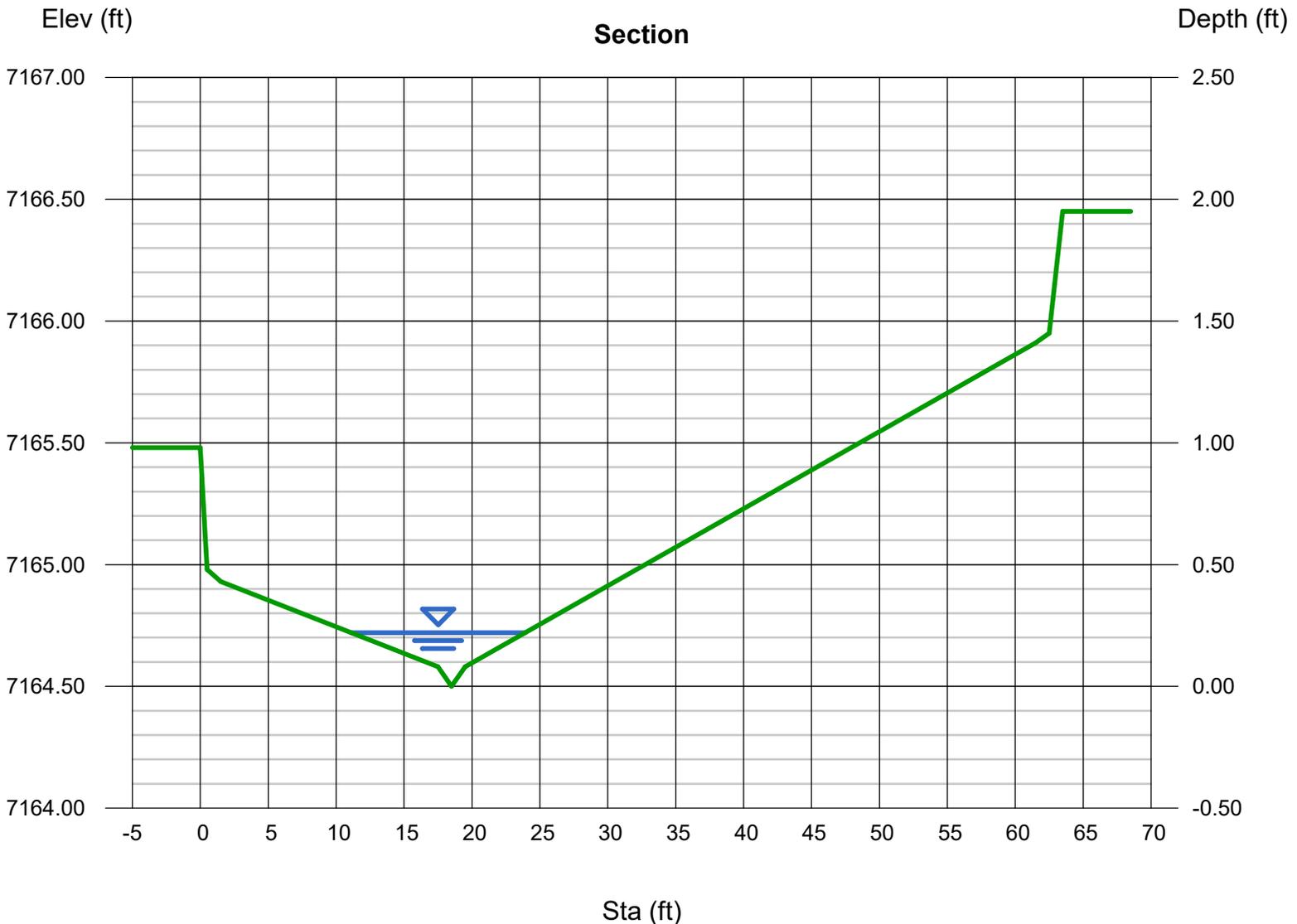
Depth (ft) = 0.22  
Q (cfs) = 2.400  
Area (sqft) = 1.12  
Velocity (ft/s) = 2.14  
Wetted Perim (ft) = 12.84  
Crit Depth, Yc (ft) = 0.24  
Top Width (ft) = 12.83  
EGL (ft) = 0.29

### Calculations

Compute by: Known Q  
Known Q (cfs) = 2.40

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7165.48)-(0.50, 7164.98, 0.013)-(1.50, 7164.93, 0.013)-(17.50, 7164.58, 0.013)-(18.50, 7164.50, 0.013)-(19.50, 7164.58, 0.013)-(61.50, 7165.91, 0.013)  
-(62.50, 7165.95, 0.013)-(63.50, 7166.45, 0.013)



# Channel Report

## Drainage Pan @ Design Point 8 - 10yr

### User-defined

Invert Elev (ft) = 7160.15  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

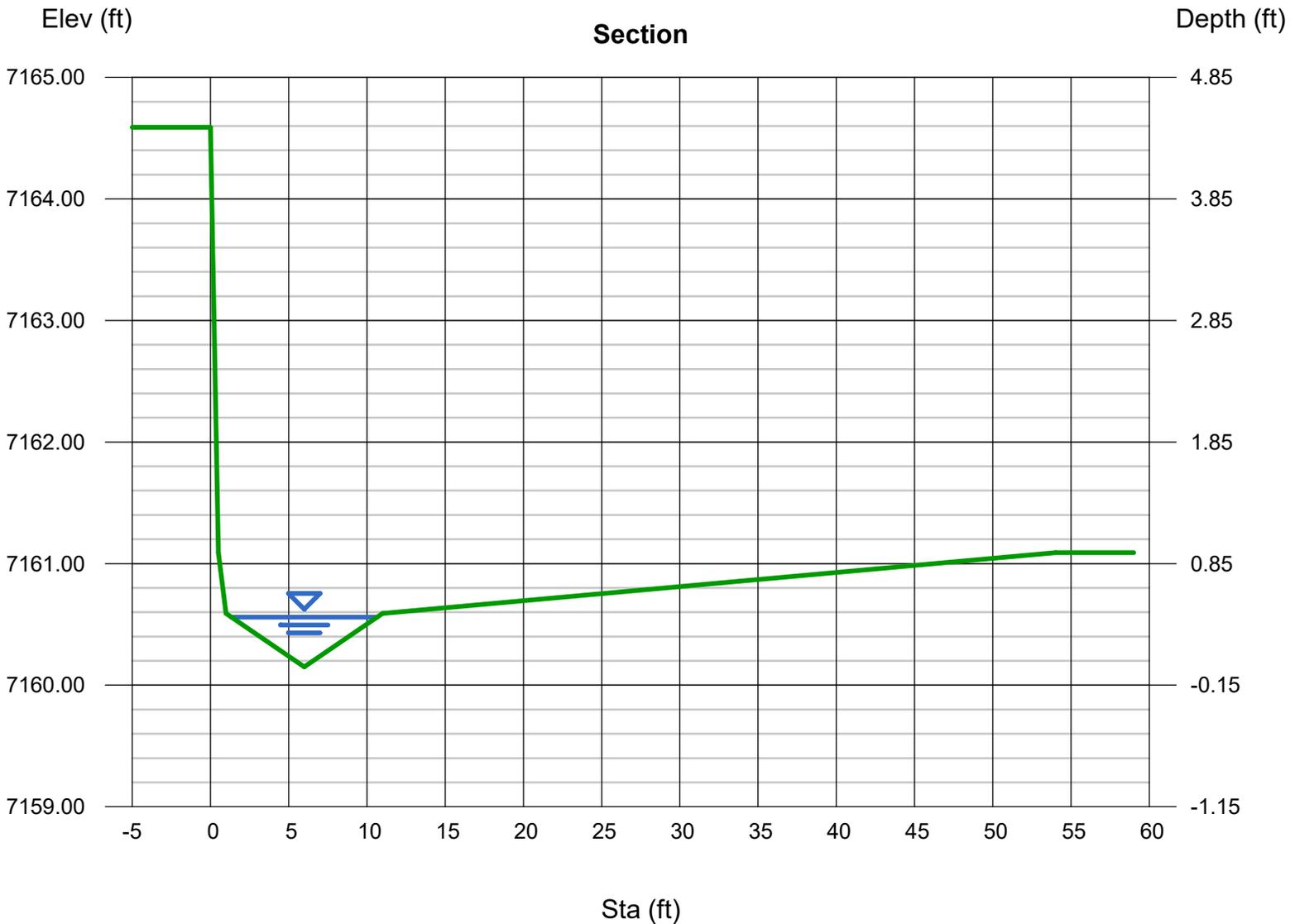
Depth (ft) = 0.41  
Q (cfs) = 5.800  
Area (sqft) = 1.91  
Velocity (ft/s) = 3.03  
Wetted Perim (ft) = 9.36  
Crit Depth, Yc (ft) = 0.44  
Top Width (ft) = 9.32  
EGL (ft) = 0.55

### Calculations

Compute by: Known Q  
Known Q (cfs) = 5.80

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7164.59)-(0.50, 7161.09, 0.013)-(1.00, 7160.59, 0.013)-(6.00, 7160.15, 0.013)-(11.00, 7160.59, 0.013)-(54.00, 7161.09, 0.013)



# Channel Report

## Drainage Pan @ Design Point 8 - 100yr

### User-defined

Invert Elev (ft) = 7160.15  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

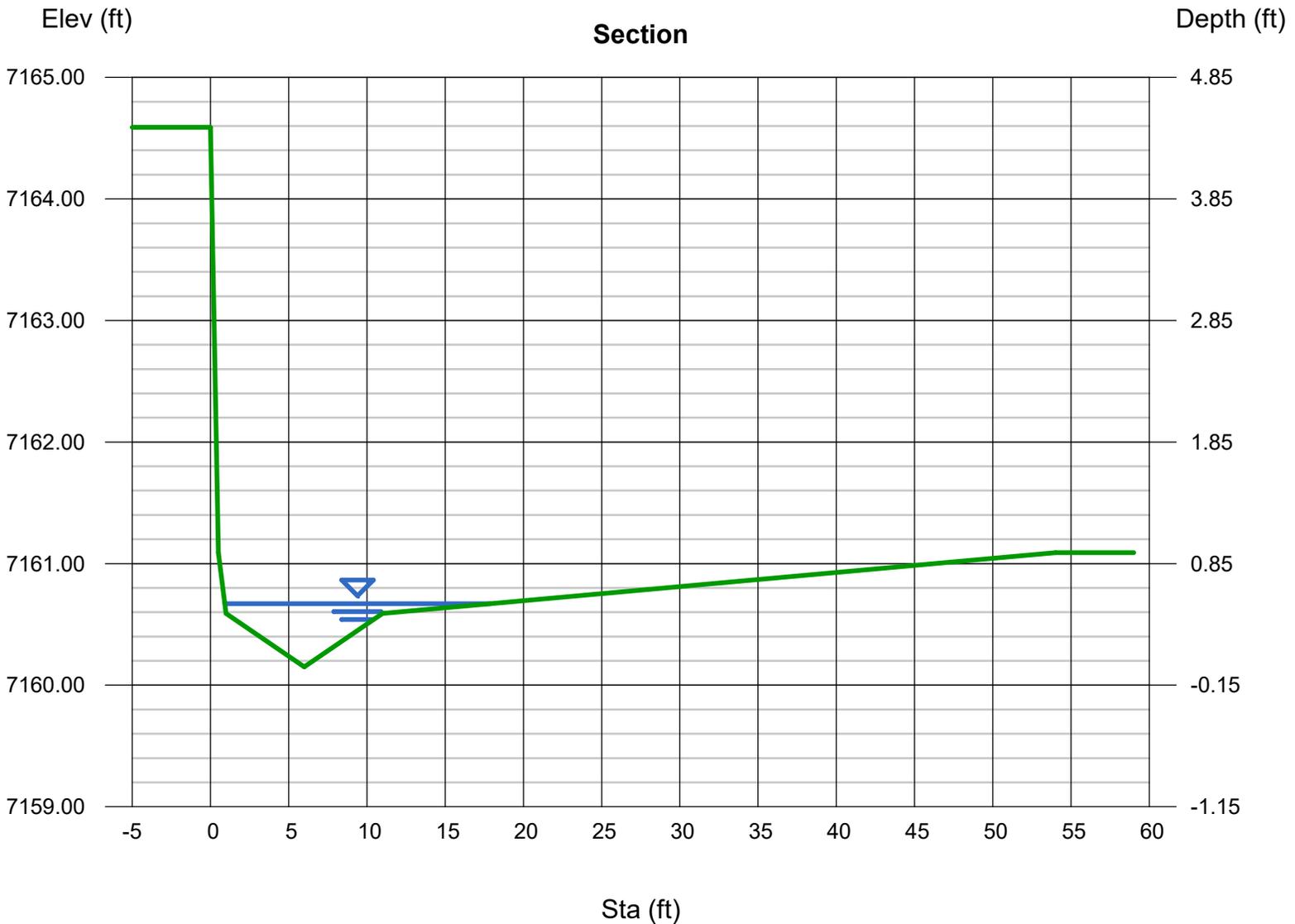
Depth (ft) = 0.52  
Q (cfs) = 9.300  
Area (sqft) = 3.28  
Velocity (ft/s) = 2.84  
Wetted Perim (ft) = 17.04  
Crit Depth, Yc (ft) = 0.55  
Top Width (ft) = 16.97  
EGL (ft) = 0.65

### Calculations

Compute by: Known Q  
Known Q (cfs) = 9.30

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7164.59)-(0.50, 7161.09, 0.013)-(1.00, 7160.59, 0.013)-(6.00, 7160.15, 0.013)-(11.00, 7160.59, 0.013)-(54.00, 7161.09, 0.013)



# Channel Report

## Drainage Pan @ Design Point 10 - 10yr

### User-defined

Invert Elev (ft) = 7156.46  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

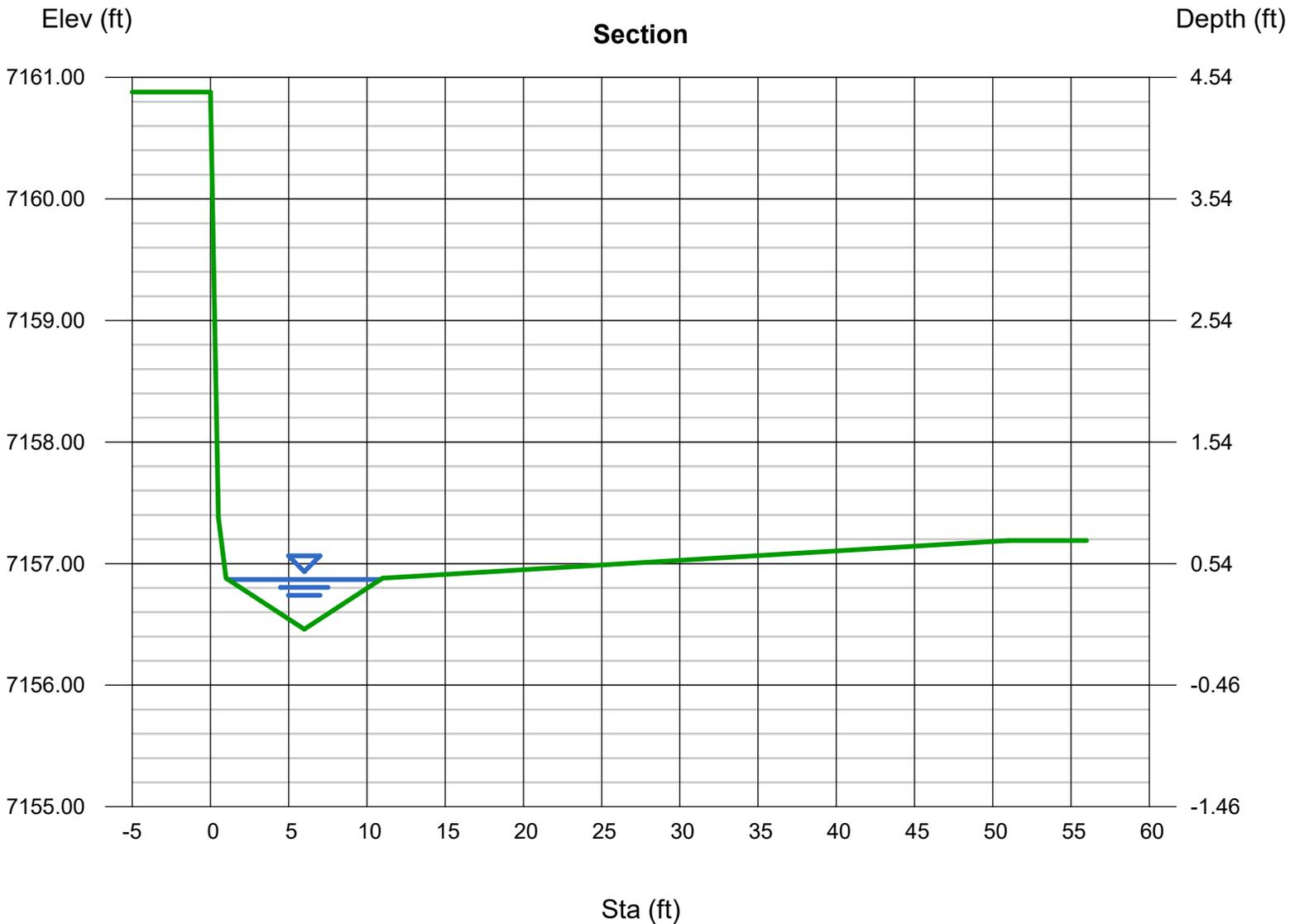
Depth (ft) = 0.41  
Q (cfs) = 6.000  
Area (sqft) = 2.00  
Velocity (ft/s) = 3.00  
Wetted Perim (ft) = 9.80  
Crit Depth, Yc (ft) = 0.46  
Top Width (ft) = 9.77  
EGL (ft) = 0.55

### Calculations

Compute by: Known Q  
Known Q (cfs) = 6.00

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7160.88)-(0.50, 7157.38, 0.013)-(1.00, 7156.88, 0.013)-(6.00, 7156.46, 0.013)-(11.00, 7156.88, 0.013)-(51.00, 7157.19, 0.013)



# Channel Report

## Drainage Pan @ Design Point 10 - 100yr

### User-defined

Invert Elev (ft) = 7156.46  
Slope (%) = 0.60  
N-Value = 0.013

### Highlighted

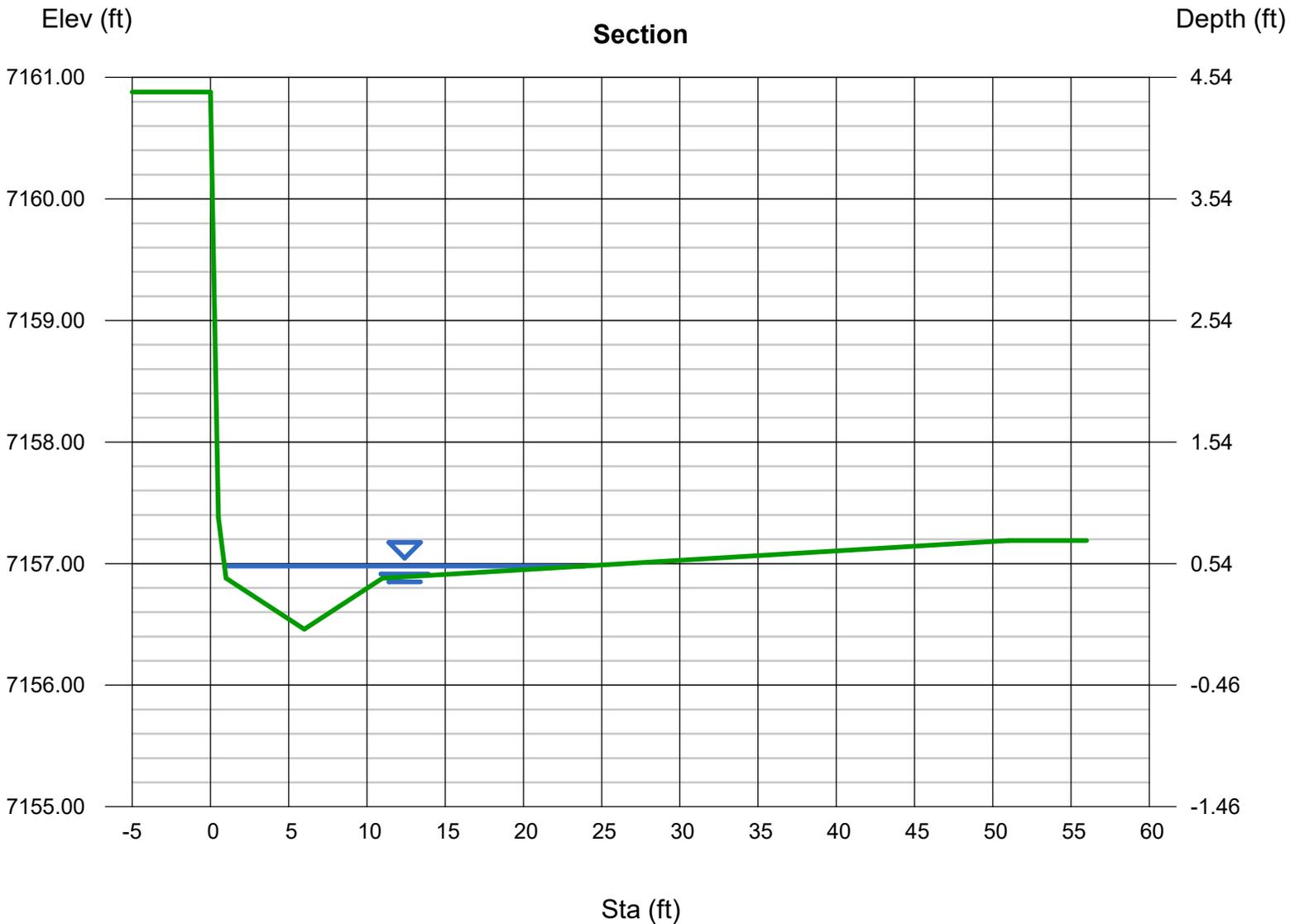
Depth (ft) = 0.52  
Q (cfs) = 9.800  
Area (sqft) = 3.75  
Velocity (ft/s) = 2.61  
Wetted Perim (ft) = 23.09  
Crit Depth, Yc (ft) = 0.55  
Top Width (ft) = 23.01  
EGL (ft) = 0.63

### Calculations

Compute by: Known Q  
Known Q (cfs) = 9.80

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7160.88)-(0.50, 7157.38, 0.013)-(1.00, 7156.88, 0.013)-(6.00, 7156.46, 0.013)-(11.00, 7156.88, 0.013)-(51.00, 7157.19, 0.013)



# Culvert Report

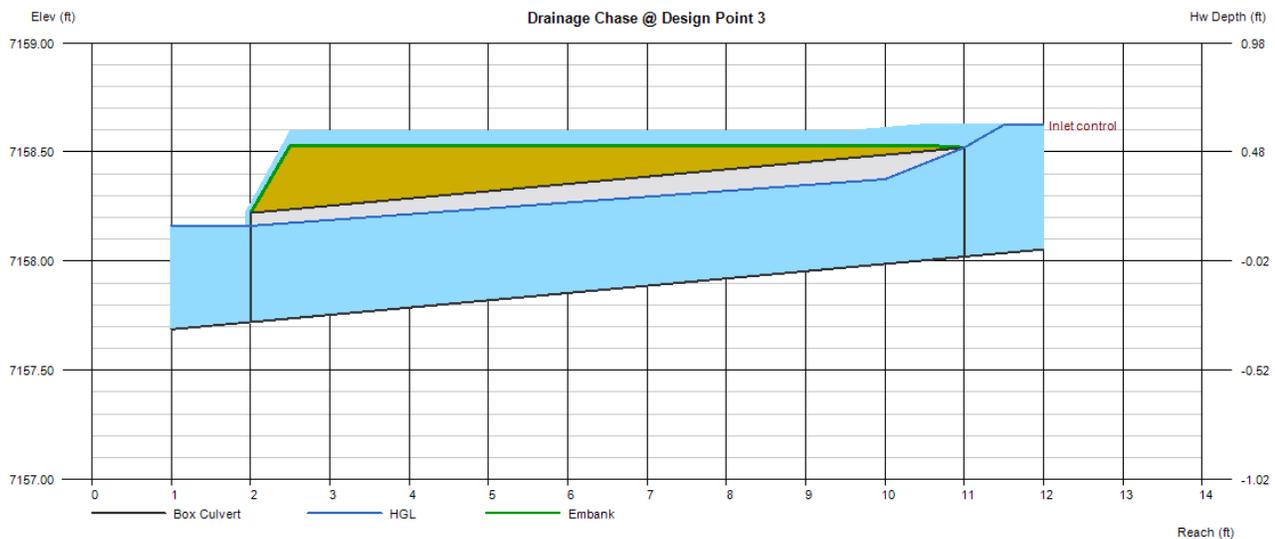
## Drainage Chase @ Design Point 3

Invert Elev Dn (ft)	= 7157.72
Pipe Length (ft)	= 9.00
Slope (%)	= 3.33
Invert Elev Up (ft)	= 7158.02
Rise (in)	= 6.0
Shape	= Box
Span (in)	= 36.0
No. Barrels	= 1
n-Value	= 0.013
Culvert Type	= Rectangular Concrete
Culvert Entrance	= Tapered inlet throat
Coeff. K,M,c,Y,k	= 0.475, 0.667, 0.0179, 0.97, 0.2

<b>Embankment</b>	
Top Elevation (ft)	= 7158.53
Top Width (ft)	= 8.00
Crest Width (ft)	= 3.00

<b>Calculations</b>	
Qmin (cfs)	= 2.78
Qmax (cfs)	= 4.28
Tailwater Elev (ft)	= (dc+D)/2

<b>Highlighted</b>	
Qtotal (cfs)	= 4.24
Qpipe (cfs)	= 4.01
Qovertop (cfs)	= 0.23
Veloc Dn (ft/s)	= 3.03
Veloc Up (ft/s)	= 3.50
HGL Dn (ft)	= 7158.16
HGL Up (ft)	= 7158.40
Hw Elev (ft)	= 7158.63
Hw/D (ft)	= 1.21
Flow Regime	= Inlet Control



# Channel Report

## Detention Pond Trickle Channel

### Rectangular

Bottom Width (ft) = 4.00

Total Depth (ft) = 0.50

Invert Elev (ft) = 50.00

Slope (%) = 1.00

N-Value = 0.013

### Calculations

Compute by: Known Q

Known Q (cfs) = 5.20

### Highlighted

Depth (ft) = 0.29

Q (cfs) = 5.200

Area (sqft) = 1.16

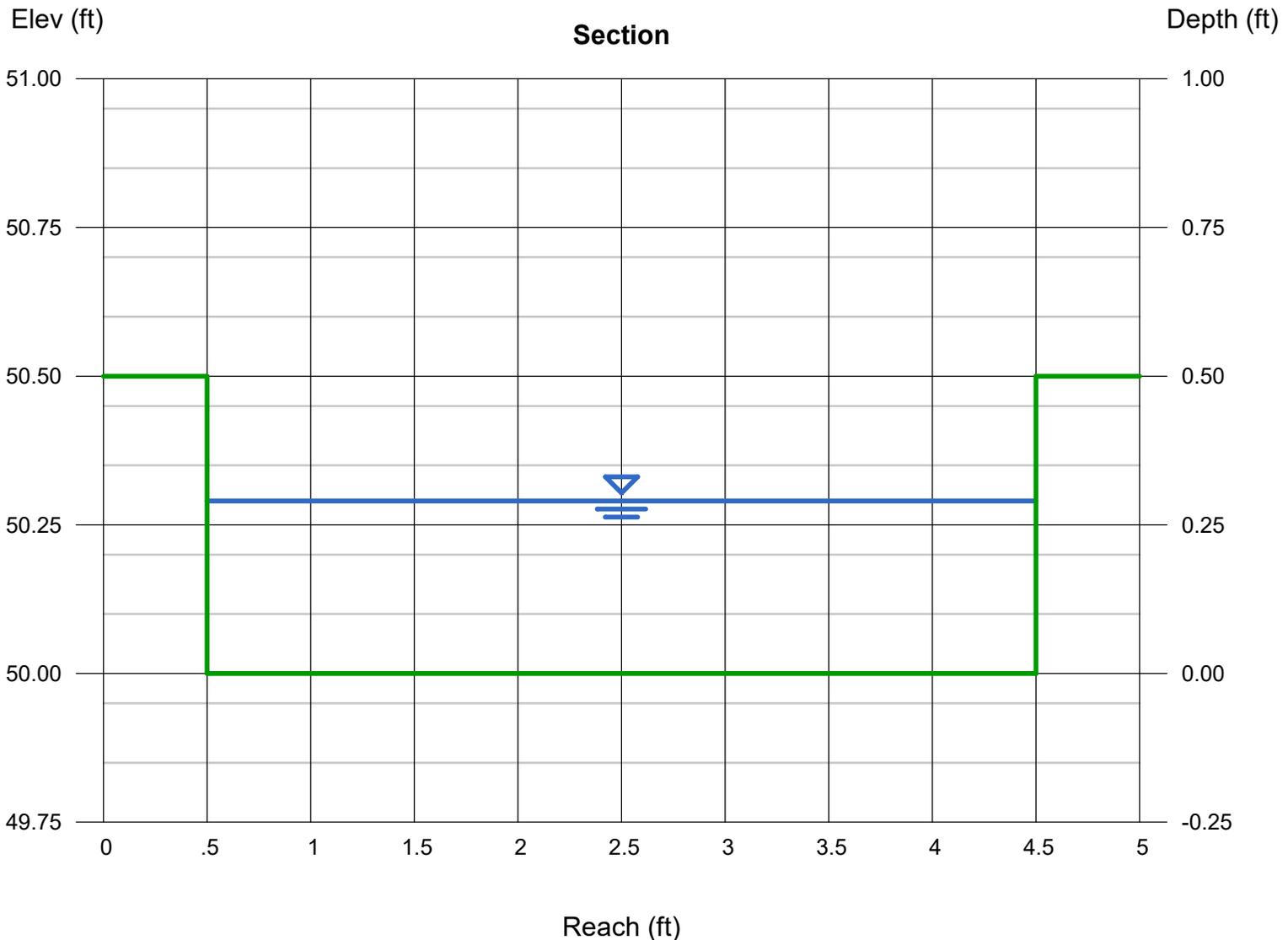
Velocity (ft/s) = 4.48

Wetted Perim (ft) = 4.58

Crit Depth, Yc (ft) = 0.38

Top Width (ft) = 4.00

EGL (ft) = 0.60



## Design Procedure Form: Grass Swale (GS)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 1

**Designer:** Cameron Salz  
**Company:** Redland Consultants  
**Date:** November 15, 2023  
**Project:** The Rock Commerce Center  
**Location:** Monument Hill Road - Road Side Ditch

1. Design Discharge for 2-Year Return Period	$Q_2 = $ <input style="width: 50px;" type="text" value="0.20"/> cfs
2. Hydraulic Residence Time A) : Length of Grass Swale B) Calculated Residence Time (based on design velocity below)	$L_S = $ <input style="width: 50px;" type="text" value="100.0"/> ft $T_{HR} = $ <input style="width: 50px;" type="text" value="2.5"/> minutes
3. Longitudinal Slope (vertical distance per unit horizontal) A) Available Slope (based on site constraints) B) Design Slope	$S_{avail} = $ <input style="width: 50px;" type="text" value="0.070"/> ft / ft $S_D = $ <input style="width: 50px;" type="text" value="0.070"/> ft / ft
4. Swale Geometry A) Channel Side Slopes (Z = 4 min., horiz. distance per unit vertical) B) Bottom Width of Swale (enter 0 for triangular section)	$Z = $ <input style="width: 50px;" type="text" value="25.00"/> ft / ft $W_B = $ <input style="width: 50px;" type="text" value="0.00"/> ft
5. Vegetation A) Type of Planting (seed vs. sod, affects vegetal retardance factor)	Choose One <input type="checkbox"/> <input checked="" type="radio"/> Grass From Seed <input type="checkbox"/> Grass From Sod
6. Design Velocity (0.333 ft / s maximum for desirable 5-minute residence time)	$V_2 = $ <input style="width: 50px;" type="text" value="0.66"/> ft / s
7. Design Flow Depth (1 foot maximum) A) Flow Area B) Top Width of Swale C) Froude Number (0.50 maximum) D) Hydraulic Radius E) Velocity-Hydraulic Radius Product for Vegetal Retardance F) Manning's n (based on SCS vegetal retardance curve E for seeded grass) G) Cumulative Height of Grade Control Structures Required	$D_2 = $ <input style="width: 50px;" type="text" value="0.11"/> ft $A_2 = $ <input style="width: 50px;" type="text" value="0.3"/> sq ft $W_T = $ <input style="width: 50px;" type="text" value="5.5"/> ft $F = $ <input style="width: 50px;" type="text" value="0.50"/> $R_H = $ <input style="width: 50px;" type="text" value="0.05"/> $VR = $ <input style="width: 50px;" type="text" value="0.04"/> $n = $ <input style="width: 50px;" type="text" value="0.080"/> $H_D = $ <input style="width: 50px;" type="text" value="0.00"/> ft
8. Underdrain (Is an underdrain necessary?)	Choose One <input type="radio"/> YES <input checked="" type="radio"/> NO
9. Soil Preparation (Describe soil amendment)	_____ _____ _____
10. Irrigation	Choose One <input checked="" type="radio"/> Temporary <input type="radio"/> Permanent

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

# Culvert Report

## DRAINAGE CHASE FOR ROOF DRAIN (TYP.)

Invert Elev Dn (ft) = 7157.72  
 Pipe Length (ft) = 9.00  
 Slope (%) = 2.00  
 Invert Elev Up (ft) = 7157.90  
 Rise (in) = 6.0  
 Shape = Box  
 Span (in) = 24.0  
 No. Barrels = 1  
 n-Value = 0.013  
 Culvert Type = 90D Headwall,  
 Chamfered or Beveled Inlet Edges

Culvert Entrance = 90D headwall w/3/4-in chamfers  
 Coeff. K,M,c,Y,k = 0.515, 0.667, 0.0375, 0.79, 0.2

### Embankment

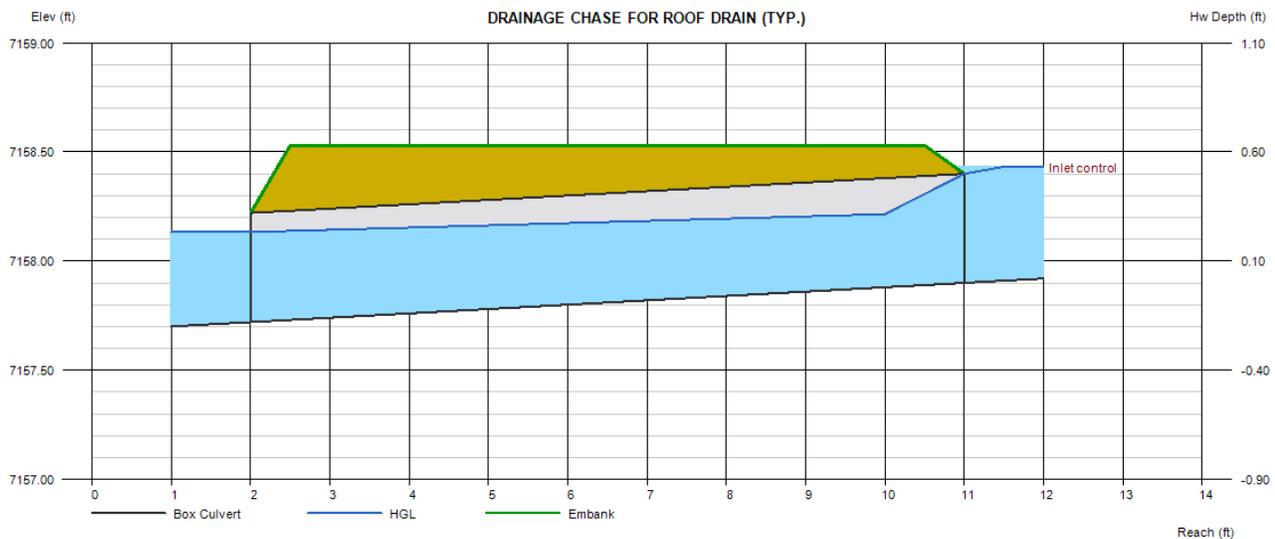
Top Elevation (ft) = 7158.53  
 Top Width (ft) = 8.00  
 Crest Width (ft) = 2.00

### Calculations

Qmin (cfs) = 1.30  
 Qmax (cfs) = 2.10  
 Tailwater Elev (ft) = (dc+D)/2

### Highlighted

Qtotal (cfs) = 2.10  
 Qpipe (cfs) = 2.10  
 Qovertop (cfs) = 0.00  
 Veloc Dn (ft/s) = 2.54  
 Veloc Up (ft/s) = 3.23  
 HGL Dn (ft) = 7158.13  
 HGL Up (ft) = 7158.23  
 Hw Elev (ft) = 7158.43  
 Hw/D (ft) = 1.06  
 Flow Regime = Inlet Control



# Culvert Report

## Existing Culvert @ Design Point A

Invert Elev Dn (ft)	= 7165.30
Pipe Length (ft)	= 30.00
Slope (%)	= 4.67
Invert Elev Up (ft)	= 7166.70
Rise (in)	= 18.0
Shape	= Circular
Span (in)	= 18.0
No. Barrels	= 1
n-Value	= 0.013
Culvert Type	= Circular Concrete
Culvert Entrance	= Groove end projecting (C)
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2

### Embankment

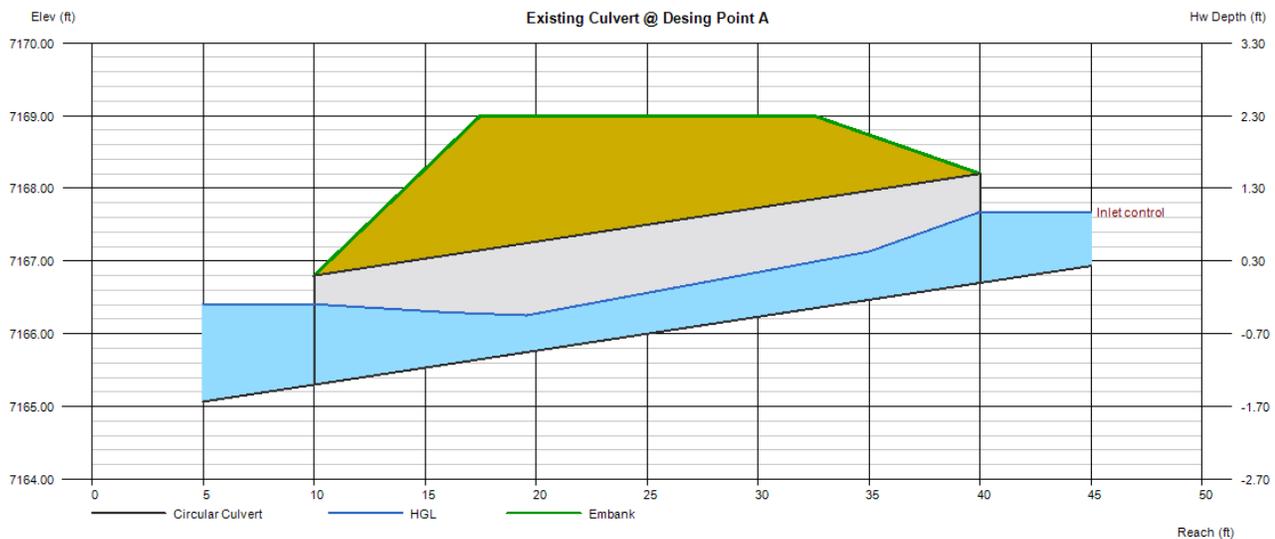
Top Elevation (ft)	= 7169.00
Top Width (ft)	= 15.00
Crest Width (ft)	= 15.00

### Calculations

Qmin (cfs)	= 2.05
Qmax (cfs)	= 3.51
Tailwater Elev (ft)	= (dc+D)/2

### Highlighted

Qtotal (cfs)	= 3.51
Qpipe (cfs)	= 3.51
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 2.51
Veloc Up (ft/s)	= 4.23
HGL Dn (ft)	= 7166.41
HGL Up (ft)	= 7167.42
Hw Elev (ft)	= 7167.68
Hw/D (ft)	= 0.65
Flow Regime	= Inlet Control



# Culvert Report

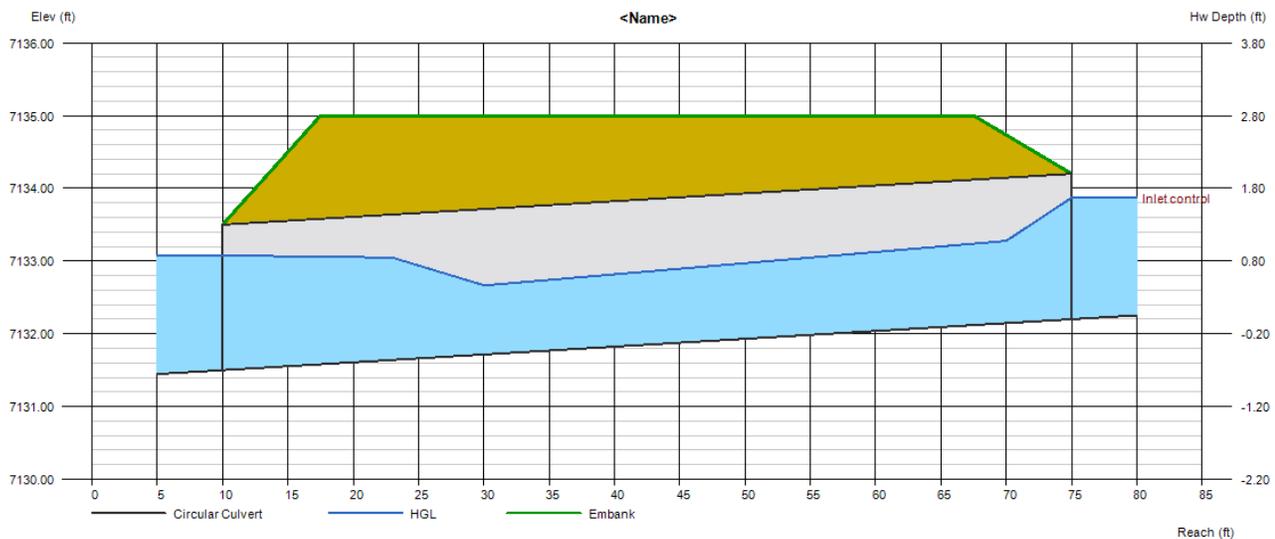
## Existing Culvert @ Design Point B

Invert Elev Dn (ft)	= 7131.50
Pipe Length (ft)	= 65.00
Slope (%)	= 1.08
Invert Elev Up (ft)	= 7132.20
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.013
Culvert Type	= Circular Concrete
Culvert Entrance	= Groove end projecting (C)
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2

<b>Embankment</b>	
Top Elevation (ft)	= 7135.00
Top Width (ft)	= 50.00
Crest Width (ft)	= 20.00

<b>Calculations</b>	
Qmin (cfs)	= 3.40
Qmax (cfs)	= 10.40
Tailwater Elev (ft)	= (dc+D)/2

<b>Highlighted</b>	
Qtotal (cfs)	= 10.40
Qpipe (cfs)	= 10.40
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 3.91
Veloc Up (ft/s)	= 5.54
HGL Dn (ft)	= 7133.08
HGL Up (ft)	= 7133.35
Hw Elev (ft)	= 7133.87
Hw/D (ft)	= 0.83
Flow Regime	= Inlet Control

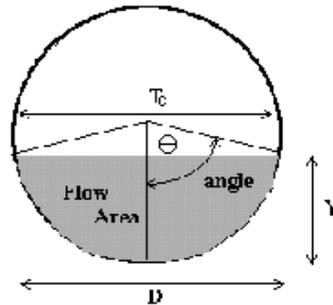


# CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

*MHFD-Culvert, Version 4.00 (May 2020)*

**Project: P-23009 The Rock Commerce Center**

**Pipe ID: Pipe at Design Point O-2**



<u>Design Information (Input)</u>	
Pipe Invert Slope	So = <input style="width: 100px;" type="text" value="0.0059"/> ft/ft
Pipe Manning's n-value	n = <input style="width: 100px;" type="text" value="0.0130"/>
Pipe Diameter	D = <input style="width: 100px;" type="text" value="18.00"/> inches
Design discharge	Q = <input style="width: 100px;" type="text" value="1.31"/> cfs
<u>Full-Flow Capacity (Calculated)</u>	
Full-flow area	Af = <input style="width: 100px;" type="text" value="1.77"/> sq ft
Full-flow wetted perimeter	Pf = <input style="width: 100px;" type="text" value="4.71"/> ft
Half Central Angle	Theta = <input style="width: 100px;" type="text" value="3.14"/> radians
Full-flow capacity	Qf = <input style="width: 100px;" type="text" value="8.09"/> cfs
<u>Calculation of Normal Flow Condition</u>	
Half Central Angle ( $0 < \text{Theta} < 3.14$ )	Theta = <input style="width: 100px;" type="text" value="1.10"/> radians
Flow area	An = <input style="width: 100px;" type="text" value="0.39"/> sq ft
Top width	Tn = <input style="width: 100px;" type="text" value="1.34"/> ft
Wetted perimeter	Pn = <input style="width: 100px;" type="text" value="1.65"/> ft
Flow depth	Yn = <input style="width: 100px;" type="text" value="0.41"/> ft
Flow velocity	Vn = <input style="width: 100px;" type="text" value="3.37"/> fps
Discharge	Qn = <input style="width: 100px;" type="text" value="1.31"/> cfs
Percent of Full Flow	Flow = <input style="width: 100px;" type="text" value="16.2%"/> of full flow
Normal Depth Froude Number	Fr <sub>n</sub> = <input style="width: 100px;" type="text" value="1.10"/> supercritical
<u>Calculation of Critical Flow Condition</u>	
Half Central Angle ( $0 < \text{Theta-c} < 3.14$ )	Theta-c = <input style="width: 100px;" type="text" value="1.13"/> radians
Critical flow area	Ac = <input style="width: 100px;" type="text" value="0.42"/> sq ft
Critical top width	Tc = <input style="width: 100px;" type="text" value="1.36"/> ft
Critical flow depth	Yc = <input style="width: 100px;" type="text" value="0.43"/> ft
Critical flow velocity	Vc = <input style="width: 100px;" type="text" value="3.15"/> fps
Critical Depth Froude Number	Fr <sub>c</sub> = <input style="width: 100px;" type="text" value="1.00"/>

## Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

**Designer:** Cameron Salz  
**Company:** Redland  
**Date:** October 16, 2023  
**Project:** The Rock Commerce Center  
**Location:** El Paso County

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math></p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Contributing Watershed Area</p> <p>D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>E) Design Concept (Select EURV when also designing for flood control)</p> <p>F) Design Volume (WQCV) Based on 40-hour Drain Time (<math>V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area)</math>)</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume (<math>V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))</math>)</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p> <p>I) NRCS Hydrologic Soil Groups of Tributary Watershed                      i) Percentage of Watershed consisting of Type A Soils                      ii) Percentage of Watershed consisting of Type B Soils                      iii) Percentage of Watershed consisting of Type C/D Soils</p> <p>J) Excess Urban Runoff Volume (EURV) Design Volume                      For HSG A: <math>EURV_A = 1.68 * i^{1.28}</math>                      For HSG B: <math>EURV_B = 1.36 * i^{1.08}</math>                      For HSG C/D: <math>EURV_{C/D} = 1.20 * i^{1.08}</math></p> <p>K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired)</p>	<p><math>I_a =</math> <input type="text" value="77.0"/> %</p> <p><math>i =</math> <input type="text" value="0.770"/></p> <p>Area = <input type="text" value="11.380"/> ac</p> <p><math>d_6 =</math> <input type="text" value=""/></p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input type="radio"/> Water Quality Capture Volume (WQCV)</p> <p><input checked="" type="radio"/> Excess Urban Runoff Volume (EURV)</p> </div> <p><math>V_{DESIGN} =</math> <input type="text" value="0.294"/> ac-ft</p> <p><math>V_{DESIGN\ OTHER} =</math> <input type="text" value=""/> ac-ft</p> <p><math>V_{DESIGN\ USER} =</math> <input type="text" value=""/> ac-ft</p> <p>HSG <math>A =</math> <input type="text" value="0"/> %                      HSG <math>B =</math> <input type="text" value="100"/> %                      HSG <math>C/D =</math> <input type="text" value="0"/> %</p> <p>EURV<math>_{DESIGN} =</math> <input type="text" value="0.973"/> ac-ft</p> <p>EURV<math>_{DESIGN\ USER} =</math> <input type="text" value=""/> ac-ft</p>
<p>2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.)</p>	<p>L : W = <input type="text" value="2.0"/> : 1</p>
<p>3. Basin Side Slopes</p> <p>A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>Z = <input type="text" value="3.00"/> ft / ft</p> <p style="color: red; font-weight: bold;">DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE</p>
<p>4. Inlet</p> <p>A) Describe means of providing energy dissipation at concentrated inflow locations:</p>	<p>_____</p> <p>_____</p> <p>_____</p>
<p>5. Forebay</p> <p>A) Minimum Forebay Volume (<math>V_{FMN} =</math> <input type="text" value="3%"/> of the WQCV)</p> <p>B) Actual Forebay Volume</p> <p>C) Forebay Depth (<math>D_F =</math> <input type="text" value="18"/> inch maximum)</p> <p>D) Forebay Discharge</p> <p>i) Undetained 100-year Peak Discharge</p> <p>ii) Forebay Discharge Design Flow (<math>Q_F = 0.02 * Q_{100}</math>)</p> <p>E) Forebay Discharge Design</p> <p>F) Discharge Pipe Size (minimum 8-inches)</p> <p>G) Rectangular Notch Width</p>	<p><math>V_{FMN} =</math> <input type="text" value="0.009"/> ac-ft</p> <p><math>V_F =</math> <input type="text" value="0.020"/> ac-ft</p> <p><math>D_F =</math> <input type="text" value="18.0"/> in</p> <p><math>Q_{100} =</math> <input type="text" value="54.14"/> cfs</p> <p><math>Q_F =</math> <input type="text" value="1.08"/> cfs</p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input type="radio"/> Berm With Pipe</p> <p><input checked="" type="radio"/> Wall with Rect. Notch</p> <p><input type="radio"/> Wall with V-Notch Weir</p> </div> <p style="color: blue; font-weight: bold;">Flow too small for berm w/ pipe</p> <p>Calculated <math>D_P =</math> <input type="text" value=""/> in</p> <p>Calculated <math>W_N =</math> <input type="text" value="5.7"/> in</p>

**Design Procedure Form: Extended Detention Basin (EDB)**

**Designer:** Cameron Salz  
**Company:** Redland  
**Date:** October 16, 2023  
**Project:** The Rock Commerce Center  
**Location:** El Paso County

<p>6. Trickle Channel</p> <p>A) Type of Trickle Channel</p> <p>F) Slope of Trickle Channel</p>	<p>Choose One</p> <p><input checked="" type="radio"/> Concrete</p> <p><input type="radio"/> Soft Bottom</p> <p>S = <input type="text" value="0.0100"/> ft / ft</p>
<p>7. Micropool and Outlet Structure</p> <p>A) Depth of Micropool (2.5-foot minimum)</p> <p>B) Surface Area of Micropool (10 ft<sup>2</sup> minimum)</p> <p>C) Outlet Type</p> <p>D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)</p> <p>E) Total Outlet Area</p>	<p>D<sub>M</sub> = <input type="text" value="2.5"/> ft</p> <p>A<sub>M</sub> = <input type="text" value="10"/> sq ft</p> <p>Choose One</p> <p><input checked="" type="radio"/> Orifice Plate</p> <p><input type="radio"/> Other (Describe):</p> <hr/> <hr/> <p>D<sub>orifice</sub> = <input type="text" value="1.36"/> inches</p> <p>A<sub>orifice</sub> = <input type="text" value="0.85"/> square inches</p>
<p>8. Initial Surcharge Volume</p> <p>A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)</p> <p>B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)</p> <p>C) Initial Surcharge Provided Above Micropool</p>	<p>D<sub>IS</sub> = <input type="text" value="4"/> in</p> <p>V<sub>IS</sub> = <input type="text" value="38"/> cu ft</p> <p>V<sub>s</sub> = <input type="text" value="3.3"/> cu ft</p>
<p>9. Trash Rack</p> <p>A) Water Quality Screen Open Area: <math>A_t = A_{ot} * 38.5 * (e^{-0.095D})</math></p> <p>B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open area to the total screen area for the material specified.)</p> <p style="text-align: center;">Other (Y/N): <input type="text" value="N"/></p> <p>C) Ratio of Total Open Area to Total Area (only for type 'Other')</p> <p>D) Total Water Quality Screen Area (based on screen type)</p> <p>E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)</p> <p>F) Height of Water Quality Screen (H<sub>TR</sub>)</p> <p>G) Width of Water Quality Screen Opening (W<sub>opening</sub>) (Minimum of 12 inches is recommended)</p>	<p>A<sub>t</sub> = <input type="text" value="29"/> square inches</p> <p><input o.c."="" type="text" value="Aluminum Amico-Klemp SR Series with Cross Rods 2"/></p> <hr/> <hr/> <p>User Ratio = <input type="text"/></p> <p>A<sub>total</sub> = <input type="text" value="41"/> sq. in.</p> <p>H = <input type="text" value="6.06"/> feet</p> <p>H<sub>TR</sub> = <input type="text" value="100.72"/> inches</p> <p>W<sub>opening</sub> = <input type="text" value="12.0"/> inches <span style="color: red; font-weight: bold;">VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.</span></p>

Design Procedure Form: Extended Detention Basin (EDB)

Designer: Cameron Salz  
Company: Redland  
Date: October 16, 2023  
Project: The Rock Commerce Center  
Location: El Paso County

<p>10. Overflow Embankment</p> <p>A) Describe embankment protection for 100-year and greater overtopping:</p> <p>B) Slope of Overflow Embankment (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>_____</p> <p>_____</p> <p>_____</p> <p>Ze = <input type="text" value="4.00"/> ft / ft</p>
---	--

<p>11. Vegetation</p>	<p>Choose One</p> <p><input type="radio"/> Irrigated</p> <p><input checked="" type="radio"/> Not Irrigated</p>
-----------------------	--

<p>12. Access</p> <p>A) Describe Sediment Removal Procedures</p>	<p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p>
--	--

Notes: \_\_\_\_\_

\_\_\_\_\_

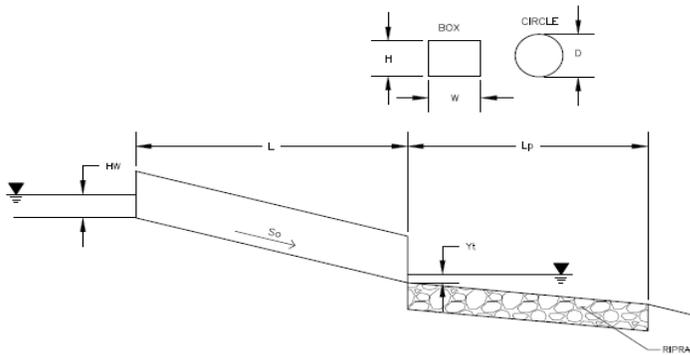
\_\_\_\_\_

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

*MHFD-Culvert, Version 4.00 (May 2020)*

**Project: P-23009 The Rock Commerce Center**

**ID: Pond Invert O-2**



**Soil Type:**

Choose One:

- Sandy  
 Non-Sandy

**Supercritical Flow! Using Adjusted Diameter to calculate protection type.**

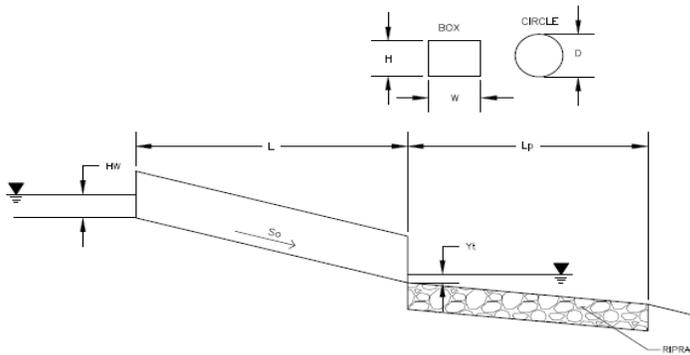
Design Information:	
Design Discharge	Q = <input type="text" value="1.31"/> cfs
<b>Circular Culvert:</b>	
Barrel Diameter in Inches	D = <input type="text" value="18"/> inches
Inlet Edge Type (Choose from pull-down list)	Grooved Edge Projecting
<b>OR:</b>	
<b>Box Culvert:</b>	
Barrel Height (Rise) in Feet	H (Rise) = <input type="text"/> ft
Barrel Width (Span) in Feet	W (Span) = <input type="text"/> ft
Inlet Edge Type (Choose from pull-down list)	
Number of Barrels	# Barrels = <input type="text" value="1"/>
Inlet Elevation	Elev IN = <input type="text" value="7137.26"/> ft
Outlet Elevation <b>OR</b> Slope	Elev OUT = <input type="text" value="7137"/> ft
Culvert Length	L = <input type="text" value="32"/> ft
Manning's Roughness	n = <input type="text" value="0.012"/>
Bend Loss Coefficient	k <sub>b</sub> = <input type="text" value="0"/>
Exit Loss Coefficient	k <sub>x</sub> = <input type="text" value="1"/>
Tailwater Surface Elevation	Y <sub>t</sub> , Elevation = <input type="text" value="7137.61"/> ft
Max Allowable Channel Velocity	V = <input type="text" value="7"/> ft/s
Calculated Results:	
Culvert Cross Sectional Area Available	A = <input type="text" value="1.77"/> ft <sup>2</sup>
Culvert Normal Depth	Y <sub>n</sub> = <input type="text" value="0.36"/> ft
Culvert Critical Depth	Y <sub>c</sub> = <input type="text" value="0.43"/> ft
Froude Number	Fr = <input type="text" value="1.39"/> <span style="color: red;">Supercritical!</span>
Entrance Loss Coefficient	k <sub>e</sub> = <input type="text" value="0.20"/>
Friction Loss Coefficient	k <sub>f</sub> = <input type="text" value="0.49"/>
Sum of All Loss Coefficients	k <sub>s</sub> = <input type="text" value="1.69"/> ft
<b>Headwater:</b>	
Inlet Control Headwater	HW <sub>I</sub> = <input type="text" value="0.58"/> ft
Outlet Control Headwater	HW <sub>O</sub> = <input type="text" value="N/A"/> ft
<b>Design Headwater Elevation</b>	<b>HW = <input type="text" value="N/A"/> ft</b>
<b>Headwater/Diameter OR Headwater/Rise Ratio</b>	<b>HW/D = <input type="text" value="N/A"/></b>
<b>Outlet Control Headwater Approximation Method Inaccurate for Low Flow - Backwater Calculations Required</b>	
<b>Outlet Protection:</b>	
Flow/(Diameter <sup>2.5</sup> )	Q/D <sup>2.5</sup> = <input type="text" value="0.48"/> ft <sup>0.5</sup> /s
Tailwater Surface Height	Y <sub>t</sub> = <input type="text" value="0.61"/> ft
Tailwater/Diameter	Y <sub>t</sub> /D = <input type="text" value="0.41"/>
Expansion Factor	1/(2*tan(Θ)) = <input type="text" value="6.70"/>
Flow Area at Max Channel Velocity	A <sub>t</sub> = <input type="text" value="0.19"/> ft <sup>2</sup>
Width of Equivalent Conduit for Multiple Barrels	W <sub>eq</sub> = <input type="text" value="-"/> ft
<b>Length of Riprap Protection</b>	<b>L<sub>p</sub> = <input type="text" value="5"/> ft</b>
<b>Width of Riprap Protection at Downstream End</b>	<b>T = <input type="text" value="3"/> ft</b>
Adjusted Diameter for Supercritical Flow	Da = <input type="text" value="0.93"/> ft
Minimum Theoretical Riprap Size	d <sub>50 min</sub> = <input type="text" value="1"/> in
Nominal Riprap Size	d <sub>50 nominal</sub> = <input type="text" value="6"/> in
<b>MHFD Riprap Type</b>	<b>Type = <input type="text" value="VL"/></b>

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

*MHFD-Culvert, Version 4.00 (May 2020)*

**Project: P-23009 The Rock Commerce Center**

**ID: Culvert at Design Point O-3**



**Soil Type:**

Choose One:

- Sandy  
 Non-Sandy

**Supercritical Flow! Using Adjusted Diameter to calculate protection type.**

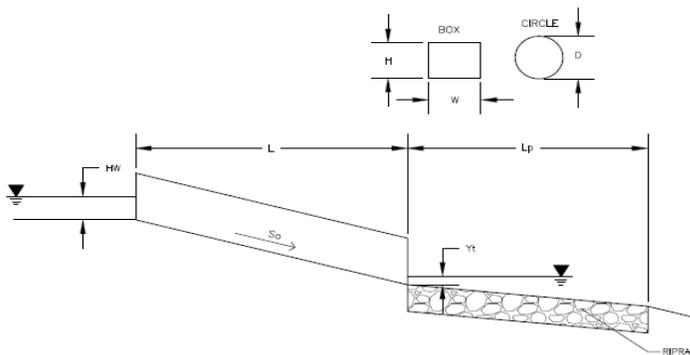
Design Information:	
Design Discharge	Q = <input type="text" value="1.15"/> cfs
Circular Culvert:	
Barrel Diameter in Inches	D = <input type="text" value="18"/> inches
Inlet Edge Type (Choose from pull-down list)	Beveled Edge (1:1)
<b>OR:</b>	
Box Culvert:	
Barrel Height (Rise) in Feet	H (Rise) = <input type="text"/> ft
Barrel Width (Span) in Feet	W (Span) = <input type="text"/> ft
Inlet Edge Type (Choose from pull-down list)	
Number of Barrels	# Barrels = <input type="text" value="1"/>
Inlet Elevation	Elev IN = <input type="text" value="7156.62"/> ft
Outlet Elevation <b>OR</b> Slope	Elev OUT = <input type="text" value="7153.87"/> ft
Culvert Length	L = <input type="text" value="65.4"/> ft
Manning's Roughness	n = <input type="text" value="0.012"/>
Bend Loss Coefficient	k <sub>b</sub> = <input type="text" value="0"/>
Exit Loss Coefficient	k <sub>x</sub> = <input type="text" value="1"/>
Tailwater Surface Elevation	Y <sub>t</sub> , Elevation = <input type="text"/> ft
Max Allowable Channel Velocity	V = <input type="text" value="7"/> ft/s
Calculated Results:	
Culvert Cross Sectional Area Available	A = <input type="text" value="1.77"/> ft <sup>2</sup>
Culvert Normal Depth	Y <sub>n</sub> = <input type="text" value="0.23"/> ft
Culvert Critical Depth	Y <sub>c</sub> = <input type="text" value="0.40"/> ft
Froude Number	Fr = <input type="text" value="3.06"/> <span style="color: red; font-weight: bold;">Supercritical!</span>
Entrance Loss Coefficient	k <sub>e</sub> = <input type="text" value="0.20"/>
Friction Loss Coefficient	k <sub>f</sub> = <input type="text" value="1.01"/>
Sum of All Loss Coefficients	k <sub>s</sub> = <input type="text" value="2.21"/> ft
Headwater:	
Inlet Control Headwater	HW <sub>I</sub> = <input type="text" value="0.53"/> ft
Outlet Control Headwater	HW <sub>O</sub> = <input type="text" value="N/A"/> ft
<b>Design Headwater Elevation</b>	<b>HW = <input type="text" value="N/A"/> ft</b>
<b>Headwater/Diameter <b>OR</b> Headwater/Rise Ratio</b>	<b>HW/D = <input type="text" value="N/A"/></b>
Outlet Control Headwater Approximation Method Inaccurate for Low Flow - Backwater Calculations Required	
Outlet Protection:	
Flow/(Diameter <sup>2.5</sup> )	Q/D <sup>2.5</sup> = <input type="text" value="0.42"/> ft <sup>0.5</sup> /s
Tailwater Surface Height	Y <sub>t</sub> = <input type="text" value="0.60"/> ft
Tailwater/Diameter	Y <sub>t</sub> /D = <input type="text" value="0.40"/>
Expansion Factor	1/(2*tan(Θ)) = <input type="text" value="6.70"/>
Flow Area at Max Channel Velocity	A <sub>t</sub> = <input type="text" value="0.16"/> ft <sup>2</sup>
Width of Equivalent Conduit for Multiple Barrels	W <sub>eq</sub> = <input type="text" value="-"/> ft
<b>Length of Riprap Protection</b>	<b>L<sub>p</sub> = <input type="text" value="5"/> ft</b>
<b>Width of Riprap Protection at Downstream End</b>	<b>T = <input type="text" value="3"/> ft</b>
Adjusted Diameter for Supercritical Flow	Da = <input type="text" value="0.86"/> ft
Minimum Theoretical Riprap Size	d <sub>50</sub> min = <input type="text" value="1"/> in
Nominal Riprap Size	d <sub>50</sub> nominal = <input type="text" value="6"/> in
<b>MHFD Riprap Type</b>	<b>Type = <input type="text" value="VL"/></b>

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

*MHFD-Culvert, Version 4.00 (May 2020)*

**Project: P-23009 The Rock Commerce Center**

**ID: Pond Outlet @ Design Point O-4**



**Soil Type:**

Choose One:

- Sandy  
 Non-Sandy

**Design Information:**

Design Discharge	Q = <input type="text" value="10.4"/> cfs
<b>Circular Culvert:</b>	
Barrel Diameter in Inches	D = <input type="text" value="18"/> inches
Inlet Edge Type (Choose from pull-down list)	Grooved Edge Projecting
<b>OR:</b>	
<b>Box Culvert:</b>	
Barrel Height (Rise) in Feet	H (Rise) = <input type="text"/> ft
Barrel Width (Span) in Feet	W (Span) = <input type="text"/> ft
Inlet Edge Type (Choose from pull-down list)	
<b>OR:</b>	
Number of Barrels	# Barrels = <input type="text" value="1"/>
Inlet Elevation	Elev IN = <input type="text" value="7134.29"/> ft
Outlet Elevation <b>OR</b> Slope	Elev OUT = <input type="text" value="7134"/> ft
Culvert Length	L = <input type="text" value="41.25"/> ft
Manning's Roughness	n = <input type="text" value="0.013"/>
Bend Loss Coefficient	k <sub>b</sub> = <input type="text" value="0"/>
Exit Loss Coefficient	k <sub>x</sub> = <input type="text" value="1"/>
Tailwater Surface Elevation	Y <sub>t</sub> , Elevation = <input type="text"/> ft
Max Allowable Channel Velocity	V = <input type="text" value="5"/> ft/s

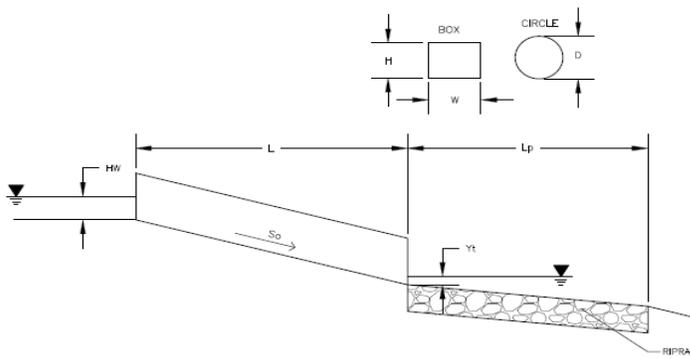
**Calculated Results:**

Culvert Cross Sectional Area Available	A = <input type="text" value="1.77"/> ft <sup>2</sup>
Culvert Normal Depth	Y <sub>n</sub> = <input type="text" value="1.50"/> ft
Culvert Critical Depth	Y <sub>c</sub> = <input type="text" value="1.24"/> ft
Froude Number	Fr = <input type="text" value="-"/> <b>Pressure flow!</b>
Entrance Loss Coefficient	k <sub>e</sub> = <input type="text" value="0.20"/>
Friction Loss Coefficient	k <sub>f</sub> = <input type="text" value="0.75"/>
Sum of All Loss Coefficients	k <sub>s</sub> = <input type="text" value="1.95"/> ft
<b>Headwater:</b>	
Inlet Control Headwater	HW <sub>I</sub> = <input type="text" value="2.12"/> ft
Outlet Control Headwater	HW <sub>O</sub> = <input type="text" value="2.13"/> ft
<b>Design Headwater Elevation</b>	<b>HW = <input type="text" value="7136.42"/> ft</b>
<b>Headwater/Diameter OR Headwater/Rise Ratio</b>	<b>HW/D = <input type="text" value="1.42"/></b>
<b>Outlet Protection:</b>	
Flow/(Diameter <sup>2.5</sup> )	Q/D <sup>2.5</sup> = <input type="text" value="3.77"/> ft <sup>0.5</sup> /s
Tailwater Surface Height	Y <sub>t</sub> = <input type="text" value="0.60"/> ft
Tailwater/Diameter	Y <sub>t</sub> /D = <input type="text" value="0.40"/>
Expansion Factor	1/(2*tan(Θ)) = <input type="text" value="3.70"/>
Flow Area at Max Channel Velocity	A <sub>t</sub> = <input type="text" value="2.08"/> ft <sup>2</sup>
Width of Equivalent Conduit for Multiple Barrels	W <sub>eq</sub> = <input type="text" value="-"/> ft
<b>Length of Riprap Protection</b>	<b>L<sub>p</sub> = <input type="text" value="8"/> ft</b>
<b>Width of Riprap Protection at Downstream End</b>	<b>T = <input type="text" value="4"/> ft</b>
<b>Adjusted Diameter for Supercritical Flow</b>	
Minimum Theoretical Riprap Size	Da = <input type="text" value="-"/> ft
Nominal Riprap Size	d <sub>50</sub> min = <input type="text" value="5"/> in
<b>MHFD Riprap Type</b>	d <sub>50</sub> nominal = <input type="text" value="6"/> in
	<b>Type = <input type="text" value="VL"/></b>

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

*MHFD-Culvert, Version 4.00 (May 2020)*

**Project:** P-23009 The Rock Commerce Center  
**ID:** Design Point C Run Down



i dont see riprap at DP-C on the Plans. Please confirm location

The riprap was covered by the basin boundary line, it has been adjusted so it can now be seen.

**Soil Type:**  
 Choose One:  
 Sandy  
 Non-Sandy

**Supercritical Flow! Using Adjusted Diameter to calculate protection type.**

Design Information:	
Design Discharge	Q = <input type="text" value="1.6"/> cfs
<b>Circular Culvert:</b>	
Barrel Diameter in Inches	D = <input type="text" value="18"/> inches
Inlet Edge Type (Choose from pull-down list)	Grooved Edge Projecting
<b>OR:</b>	
<b>Box Culvert:</b>	
Barrel Height (Rise) in Feet	H (Rise) = <input type="text"/> ft
Barrel Width (Span) in Feet	W (Span) = <input type="text"/> ft
Inlet Edge Type (Choose from pull-down list)	
Number of Barrels	# Barrels = <input type="text" value="1"/>
Inlet Elevation	Elev IN = <input type="text" value="7134.54"/> ft
Outlet Elevation <b>OR</b> Slope	Elev OUT = <input type="text" value="7133.19"/> ft
Culvert Length	L = <input type="text" value="15"/> ft
Manning's Roughness	n = <input type="text" value="0.012"/>
Bend Loss Coefficient	k <sub>b</sub> = <input type="text" value="0"/>
Exit Loss Coefficient	k <sub>x</sub> = <input type="text" value="1"/>
Tailwater Surface Elevation	Y <sub>t</sub> , Elevation = <input type="text"/> ft
Max Allowable Channel Velocity	V = <input type="text" value="7"/> ft/s
Calculated Results:	
Culvert Cross Sectional Area Available	A = <input type="text" value="1.77"/> ft <sup>2</sup>
Culvert Normal Depth	Y <sub>n</sub> = <input type="text" value="0.40"/> ft
Culvert Critical Depth	Y <sub>c</sub> = <input type="text" value="0.48"/> ft
Froude Number	Fr = <input type="text" value="1.40"/> <b>Supercritical!</b>
Entrance Loss Coefficient	k <sub>e</sub> = <input type="text" value="0.20"/>
Friction Loss Coefficient	k <sub>f</sub> = <input type="text" value="0.23"/>
Sum of All Loss Coefficients	k <sub>s</sub> = <input type="text" value="1.43"/> ft
<b>Headwater:</b>	
Inlet Control Headwater	HW <sub>I</sub> = <input type="text" value="0.65"/> ft
Outlet Control Headwater	HW <sub>O</sub> = <input type="text" value="N/A"/> ft
<b>Design Headwater Elevation</b>	<b>HW = <input type="text" value="N/A"/> ft</b>
<b>Headwater/Diameter OR Headwater/Rise Ratio</b>	<b>HW/D = <input type="text" value="N/A"/></b>
<b>Outlet Control Headwater Approximation Method Inaccurate for Low Flow - Backwater Calculations Required</b>	
<b>Outlet Protection:</b>	
Flow/(Diameter <sup>2.5</sup> )	Q/D <sup>2.5</sup> = <input type="text" value="0.58"/> ft <sup>0.5</sup> /s
Tailwater Surface Height	Y <sub>t</sub> = <input type="text" value="0.60"/> ft
Tailwater/Diameter	Y <sub>t</sub> /D = <input type="text" value="0.40"/>
Expansion Factor	1/(2*tan(θ)) = <input type="text" value="6.70"/>
Flow Area at Max Channel Velocity	A <sub>t</sub> = <input type="text" value="0.23"/> ft <sup>2</sup>
Width of Equivalent Conduit for Multiple Barrels	W <sub>eq</sub> = <input type="text" value="-"/> ft
<b>Length of Riprap Protection</b>	<b>L<sub>p</sub> = <input type="text" value="5"/> ft</b>
<b>Width of Riprap Protection at Downstream End</b>	<b>T = <input type="text" value="3"/> ft</b>
Adjusted Diameter for Supercritical Flow	Da = <input type="text" value="0.95"/> ft
Minimum Theoretical Riprap Size	d <sub>50 min</sub> = <input type="text" value="1"/> in
Nominal Riprap Size	d <sub>50 nominal</sub> = <input type="text" value="6"/> in
<b>MHFD Riprap Type</b>	<b>Type = <input type="text" value="VL"/></b>

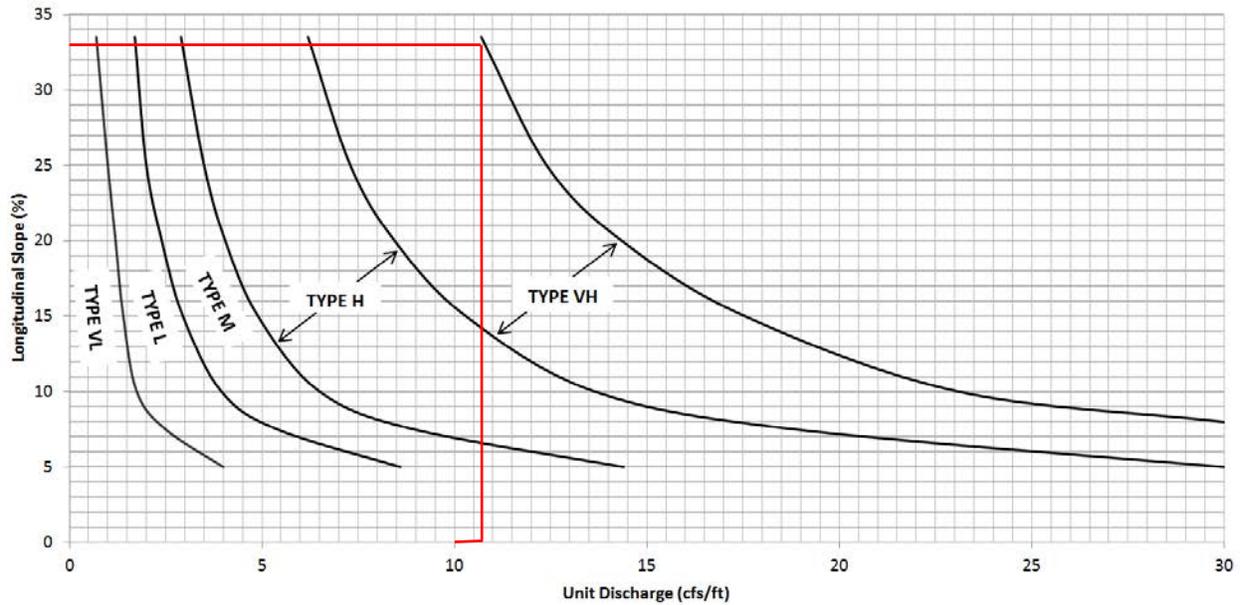
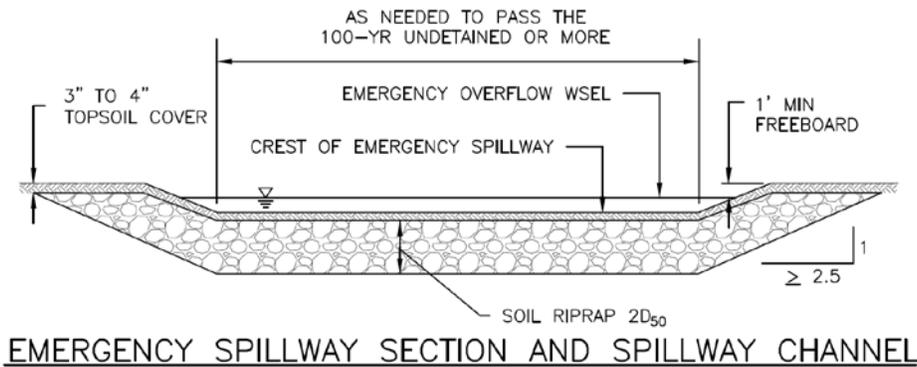
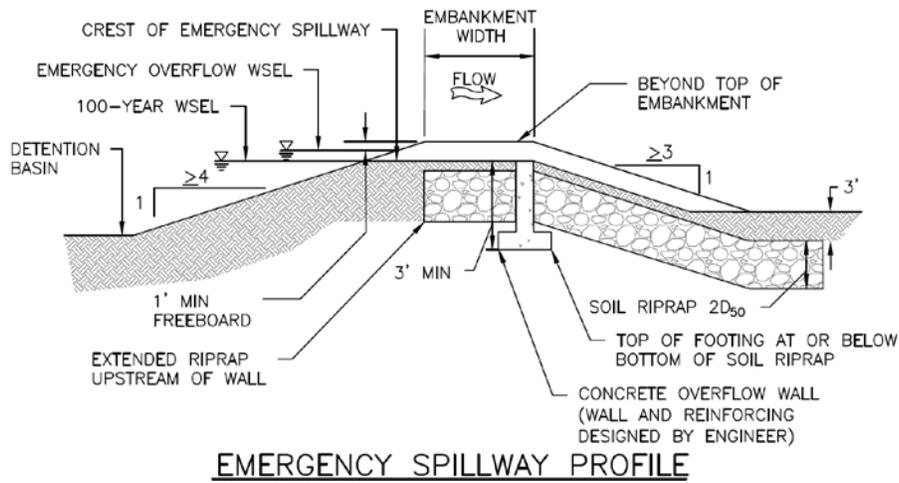
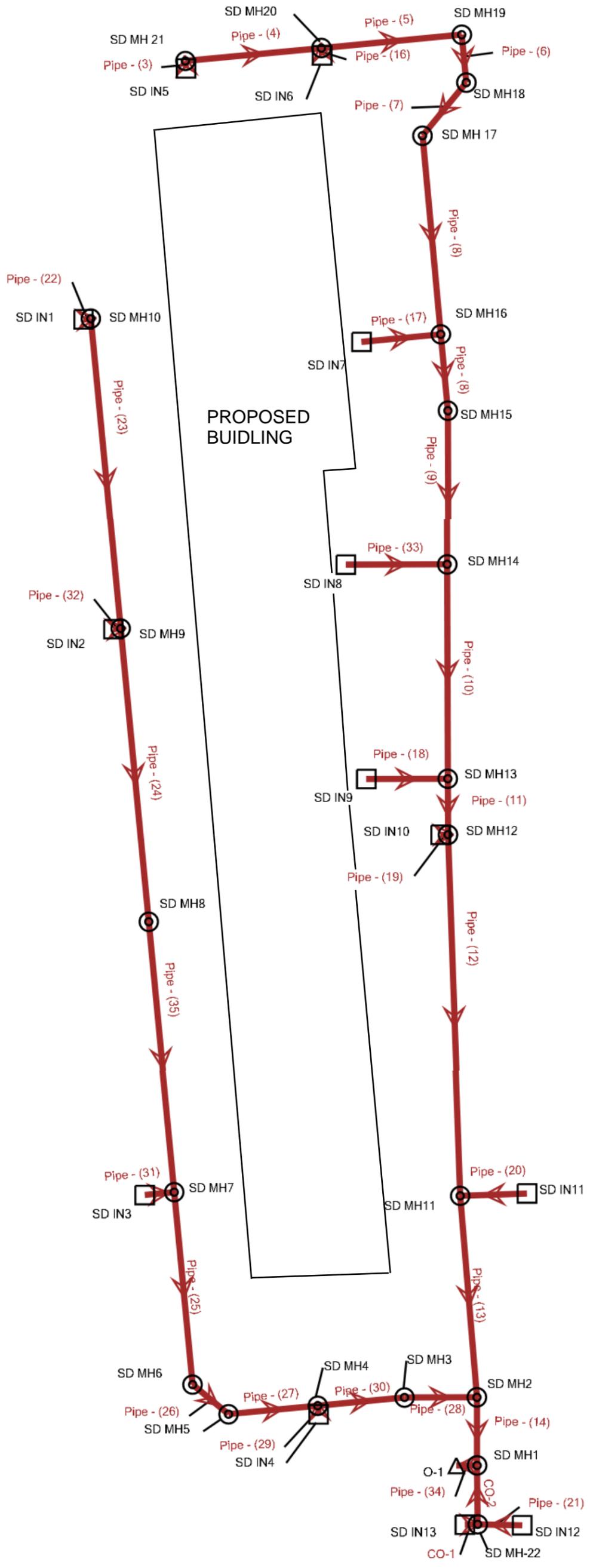


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

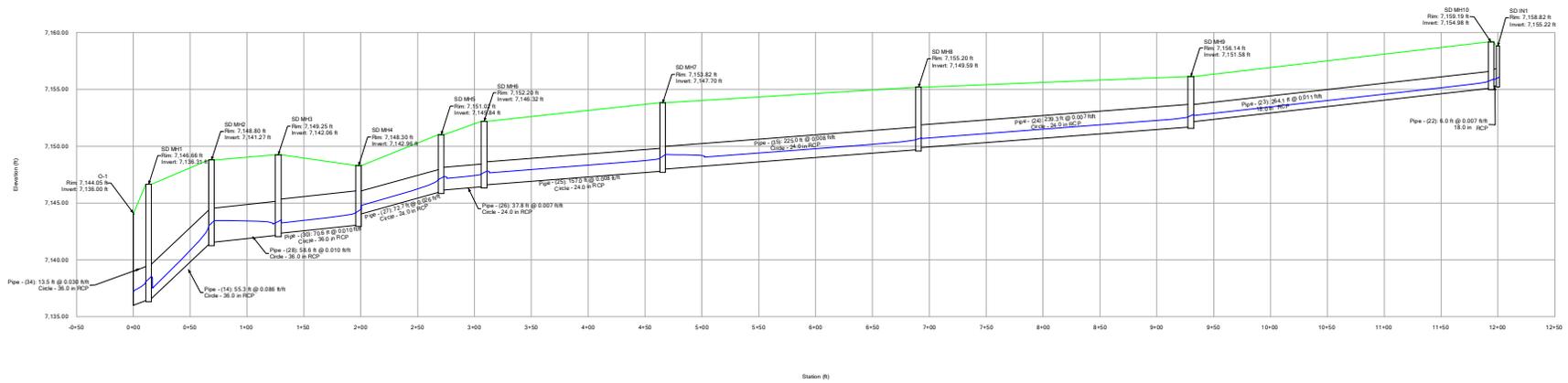
STORMCAD NETWORK PREVIEW FOR THE ROCK COMMERCE CENTER



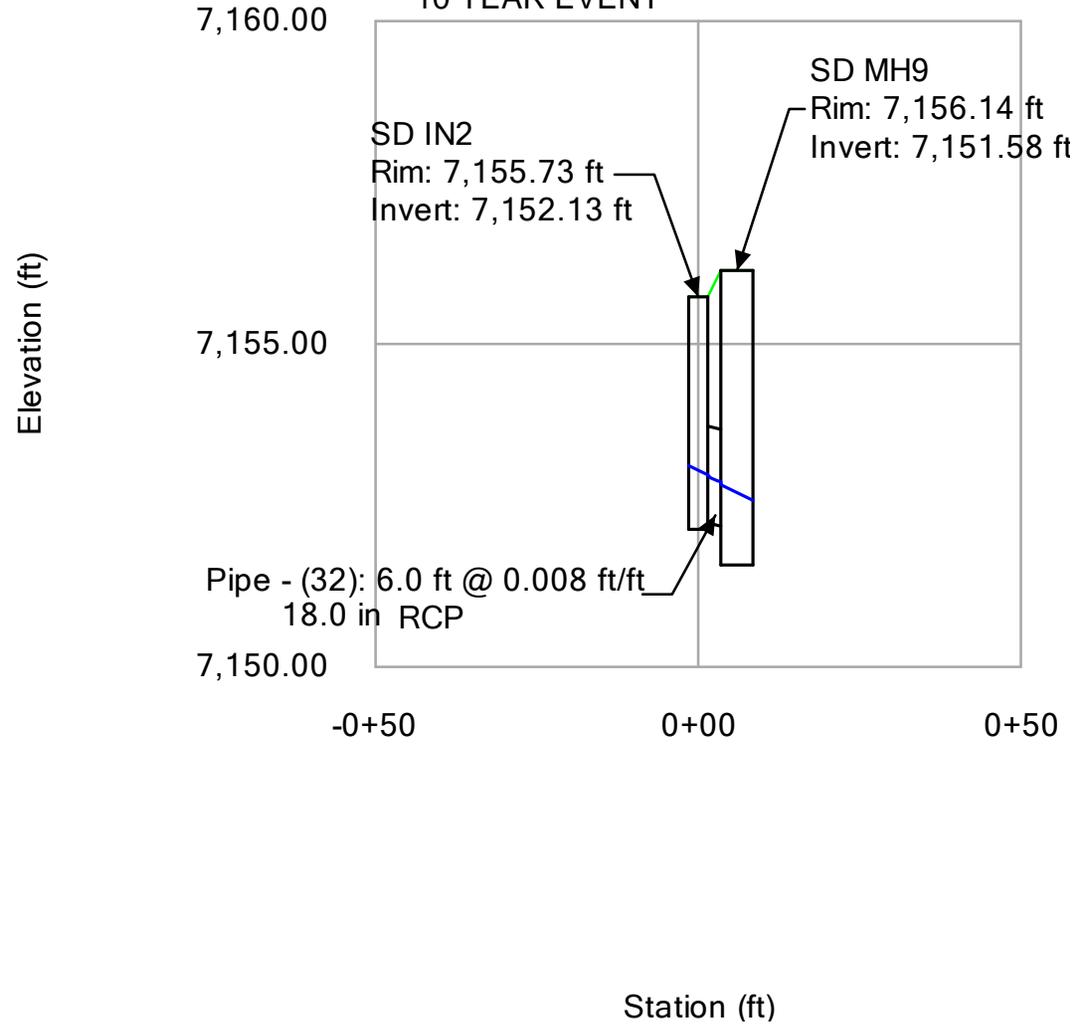
# Profile Report

## Engineering Profile - O-1 to SD IN1 (Proposed Strom.stsw)

### 10 YEAR EVENT

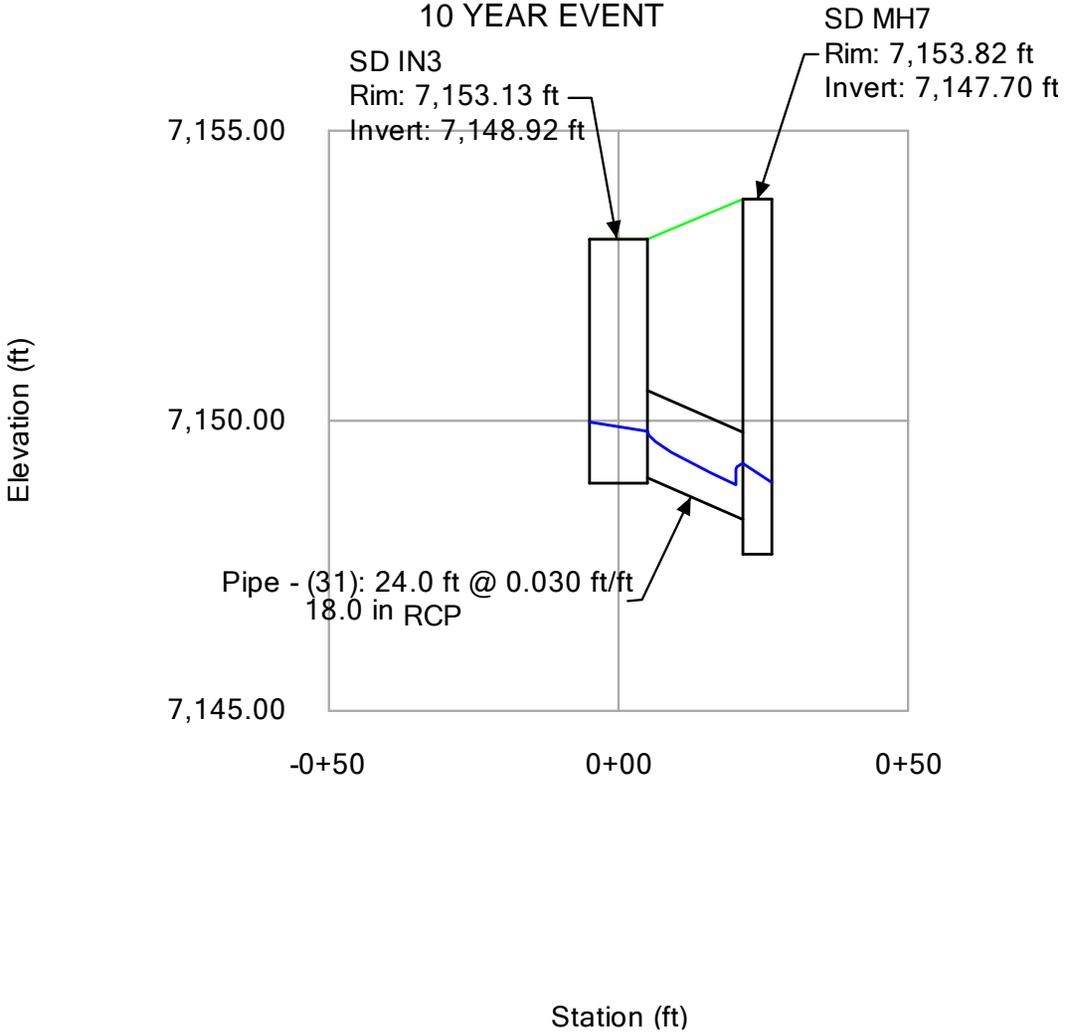


**Profile Report**  
**Engineering Profile - SD IN2 to SD MH9 (Proposed Strom.stsw)**  
10 YEAR EVENT



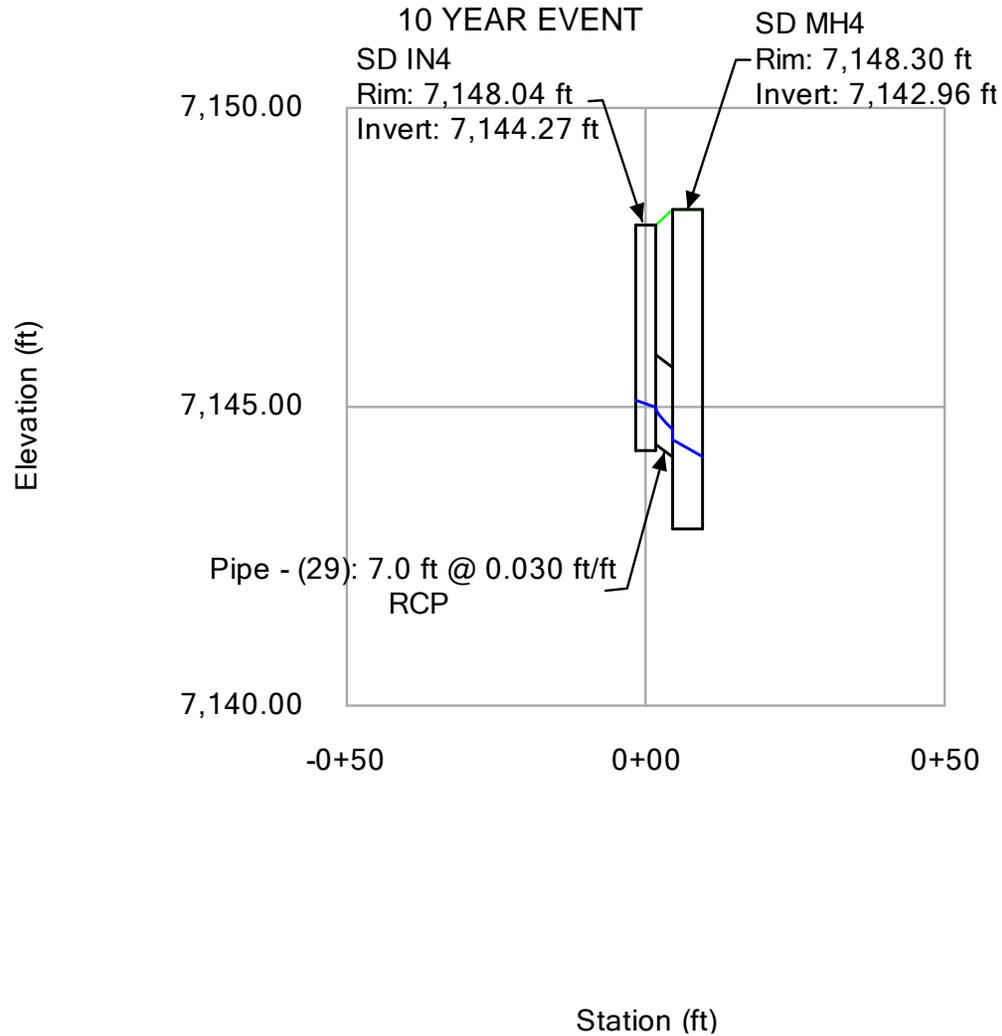
# Profile Report

## Engineering Profile - SDIN3 to SD MH7 (Proposed Strom.stsw)



# Profile Report

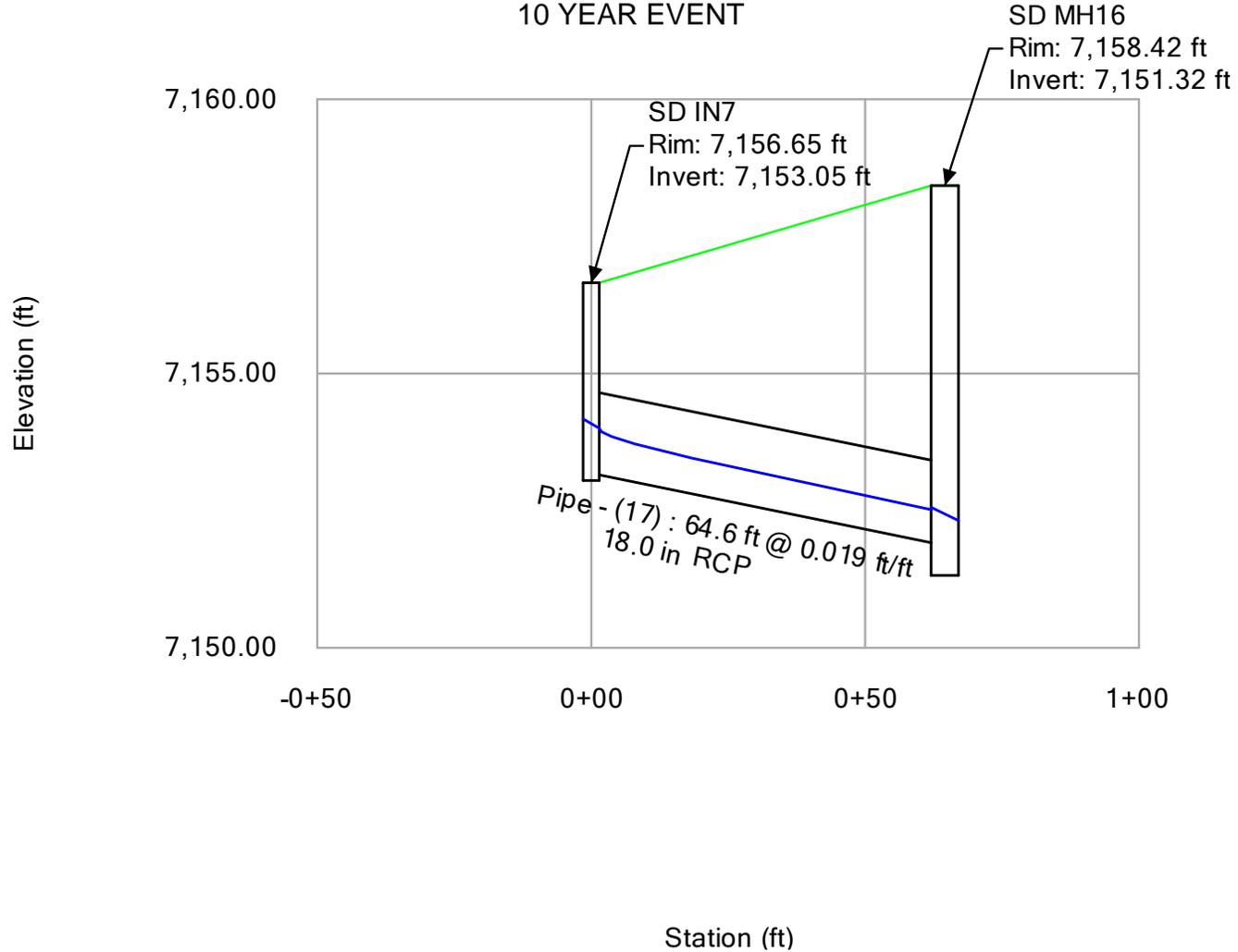
## Engineering Profile - SD IN4 to SD MH4 (Proposed Strom.stsw)



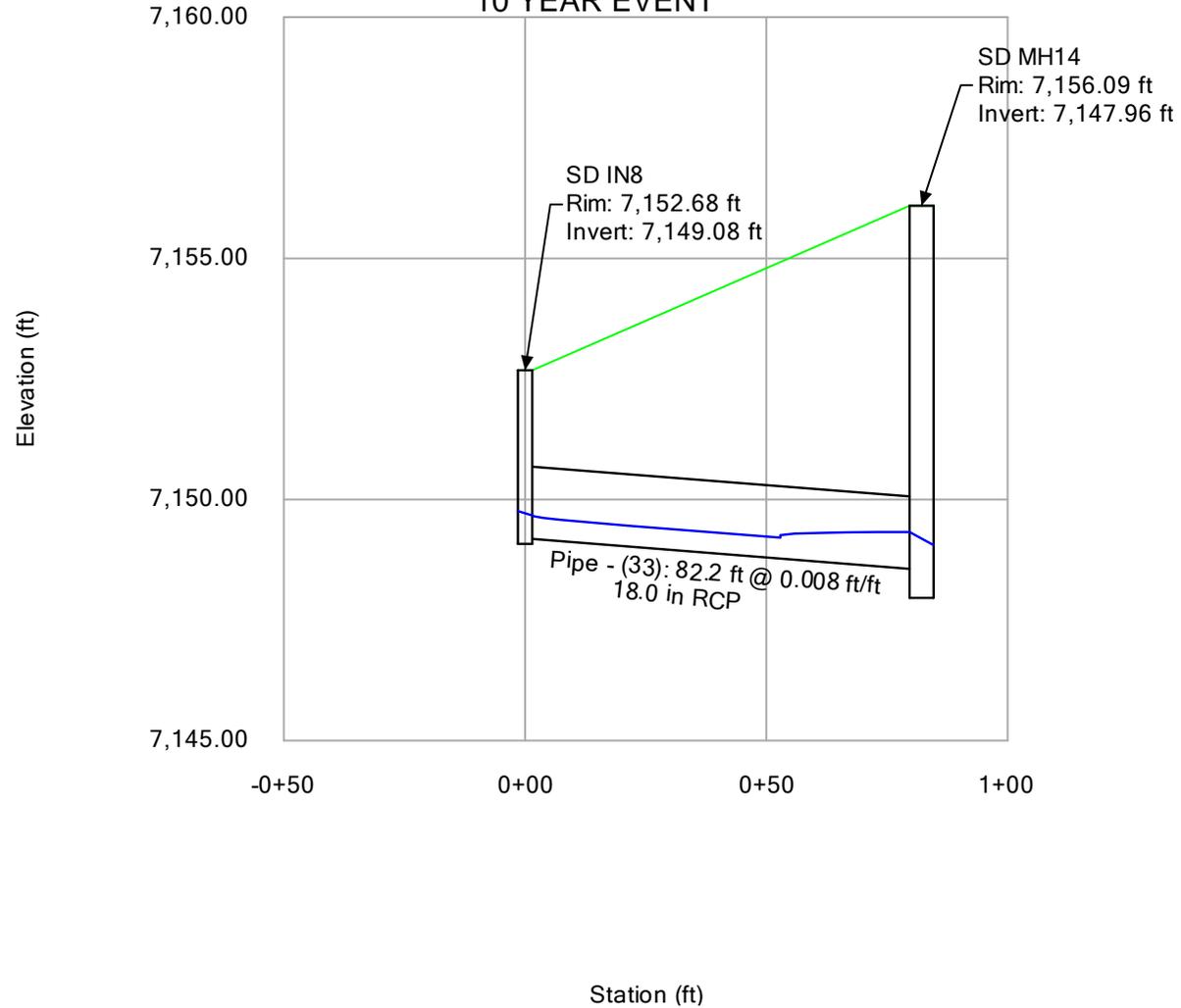
# Profile Report

## Engineering Profile - SD IN7 to SD MH16 (Proposed Strom.stsw)

10 YEAR EVENT



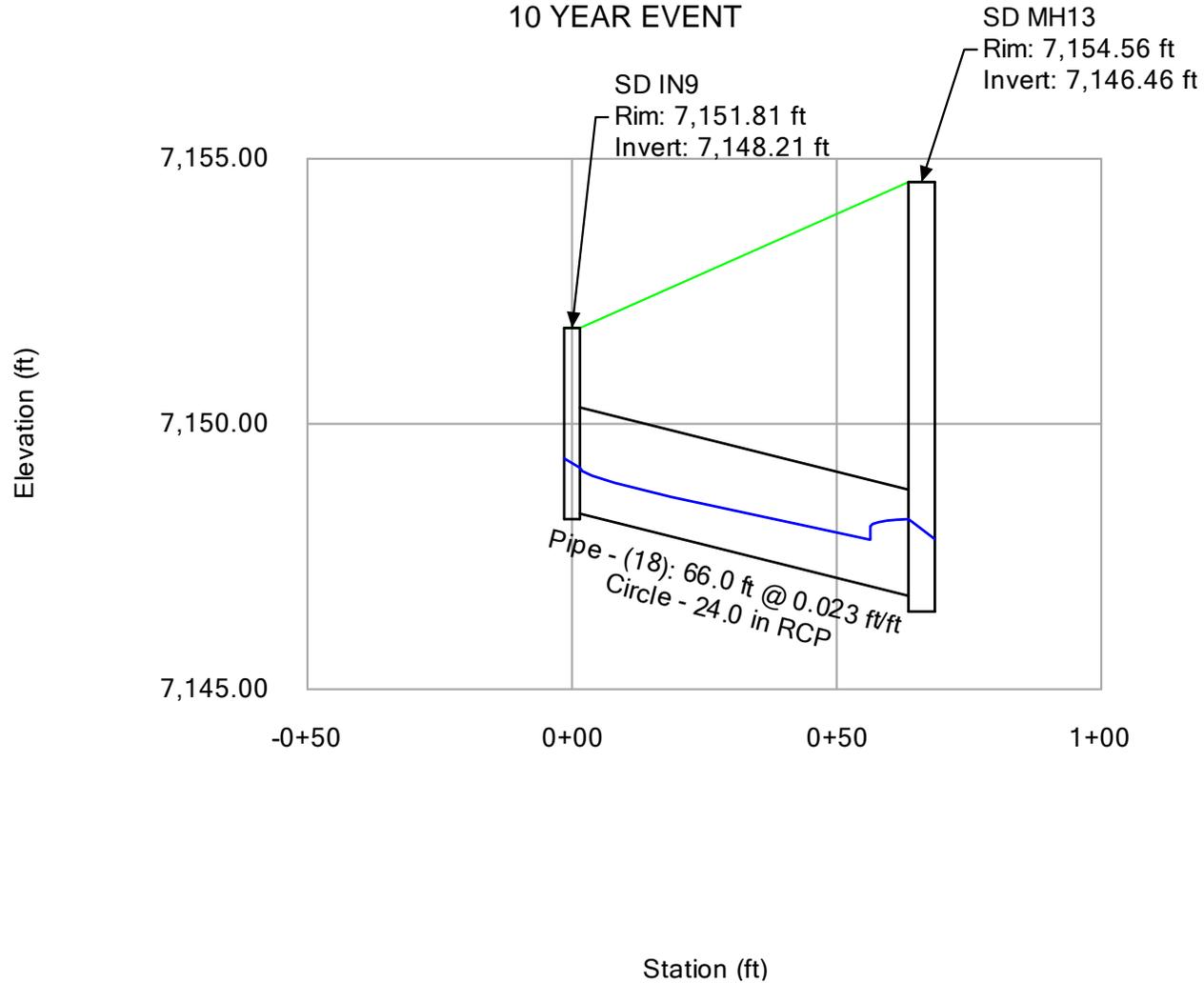
**Profile Report**  
**Engineering Profile - SD IN8 to SD MH14 (Proposed Strom.stsw)**  
10 YEAR EVENT



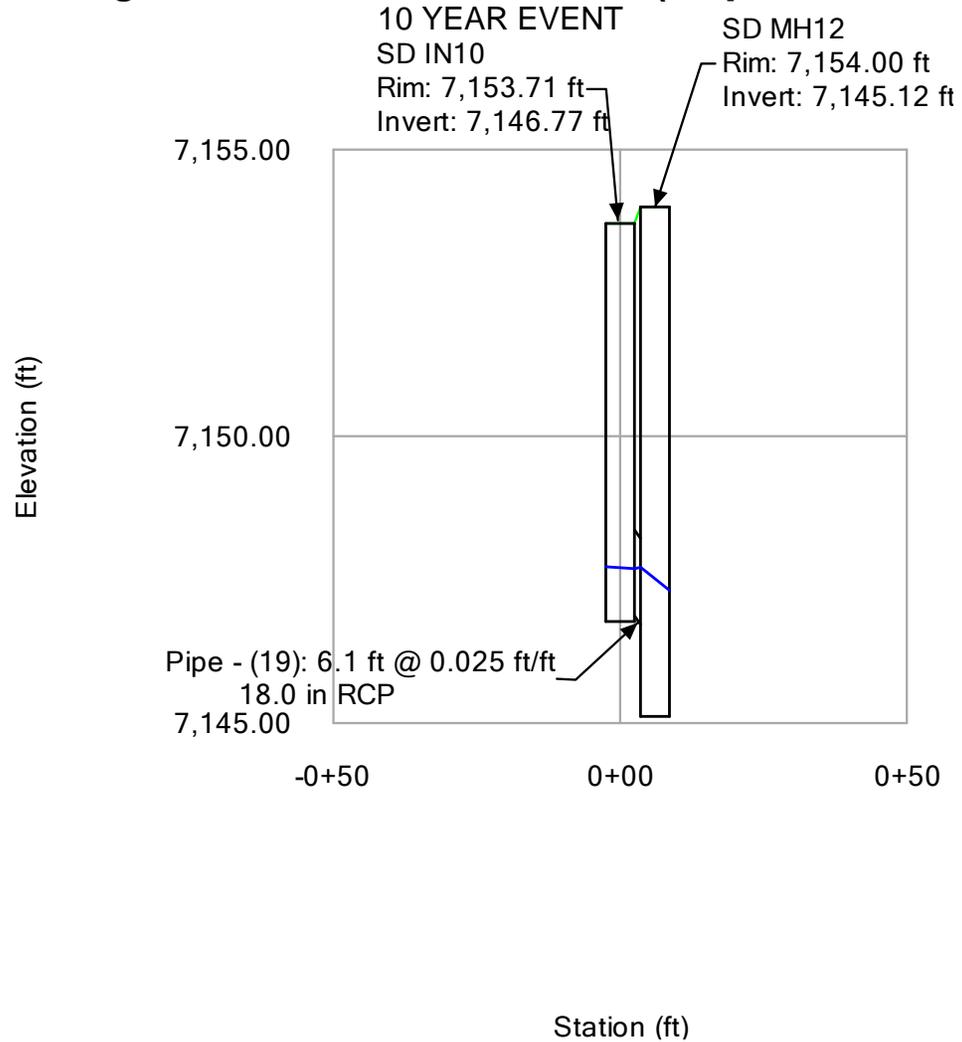
# Profile Report

## Engineering Profile - SD IN9 to SD MH13 (Proposed Strom.stsw)

10 YEAR EVENT



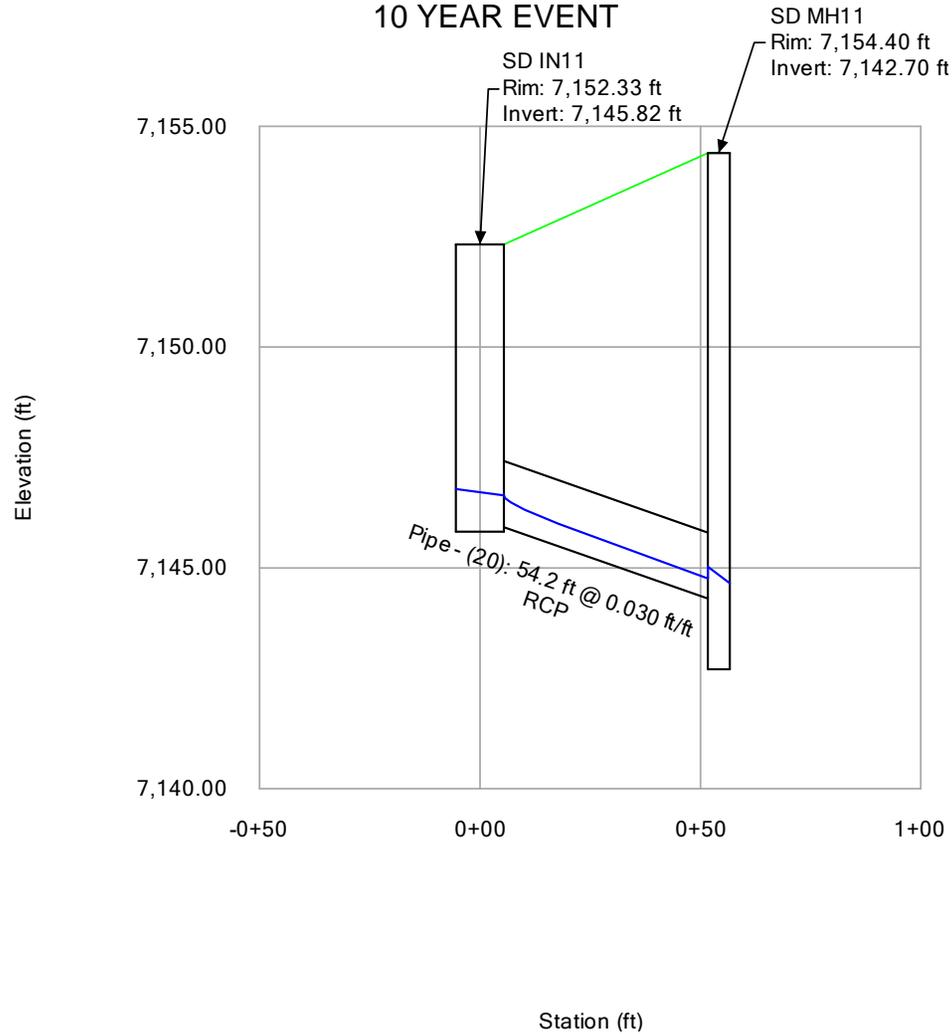
**Profile Report**  
**Engineering Profile - SD IN10 to SD MH12 (Proposed Strom.stsw)**



# Profile Report

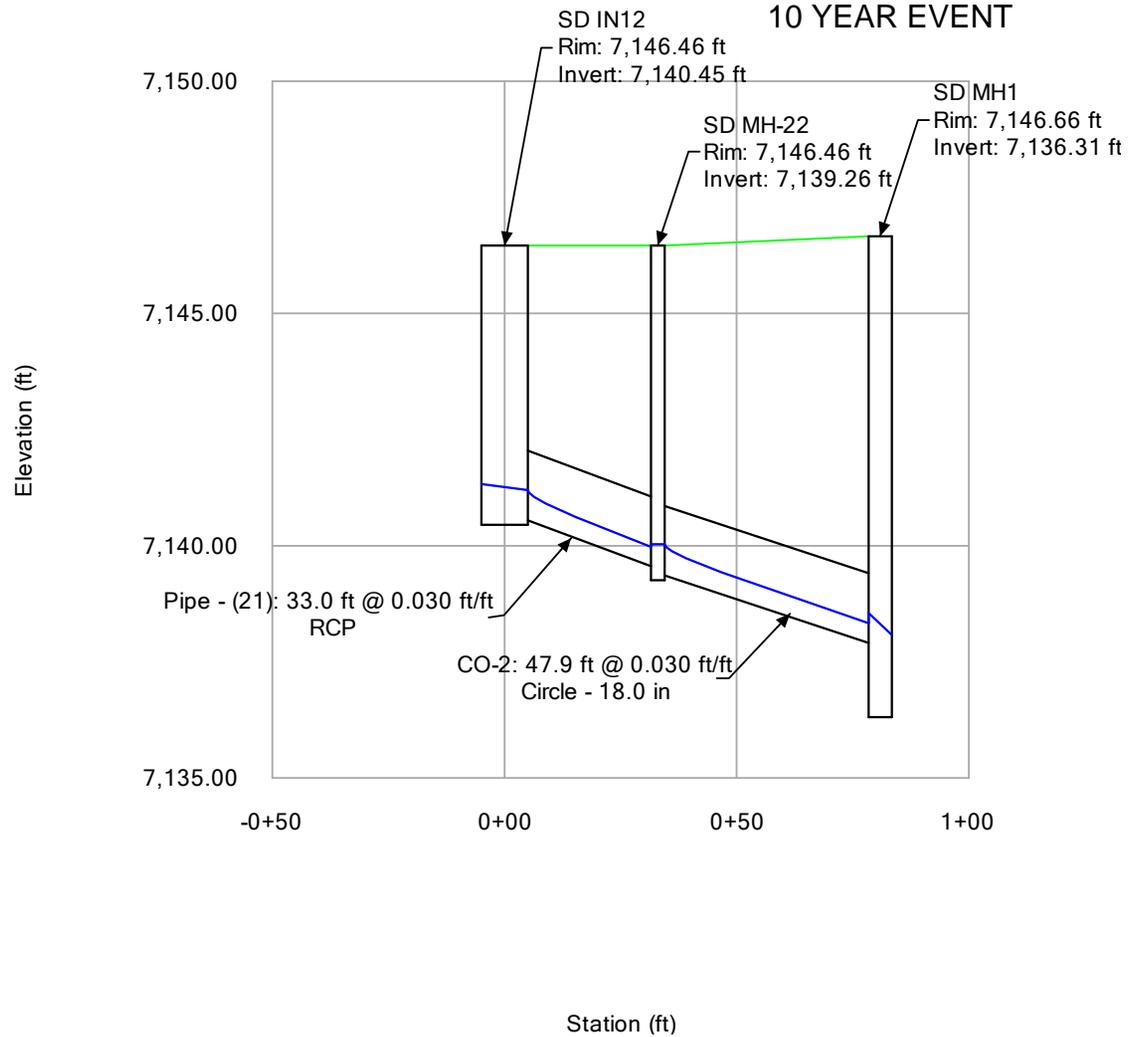
## Engineering Profile - SD IN11 to SD MH11 (Proposed Strom.stsw)

10 YEAR EVENT



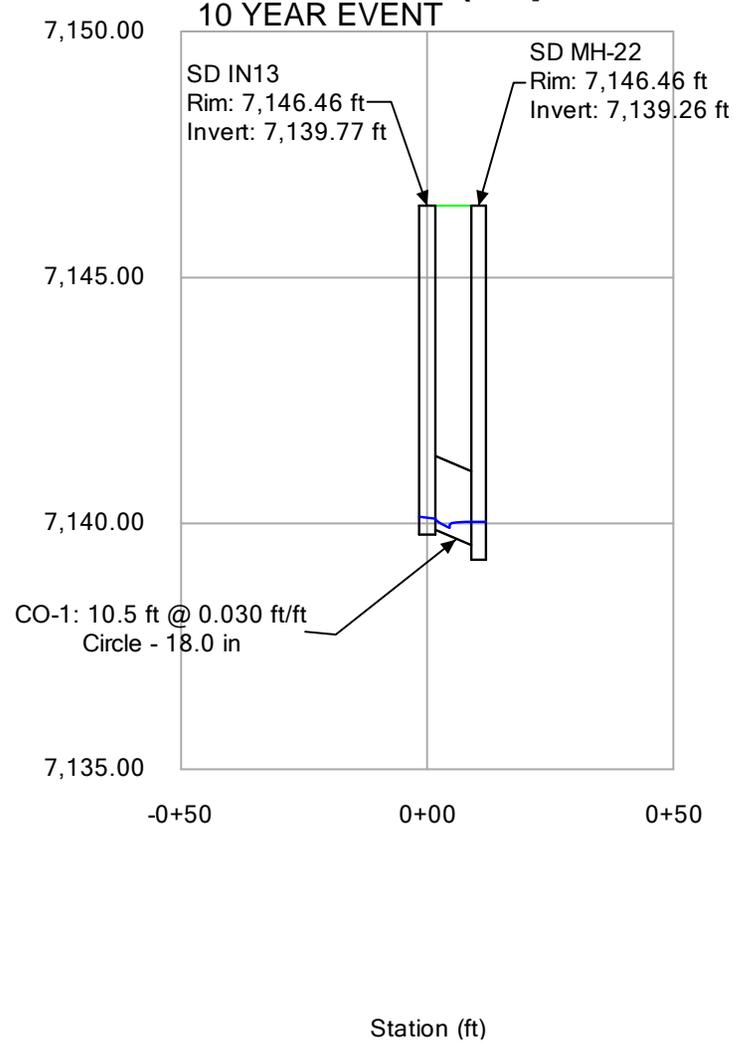
# Profile Report

## Engineering Profile - SD IN12 to SD MH1 (Proposed Strom.stsw)



# Profile Report

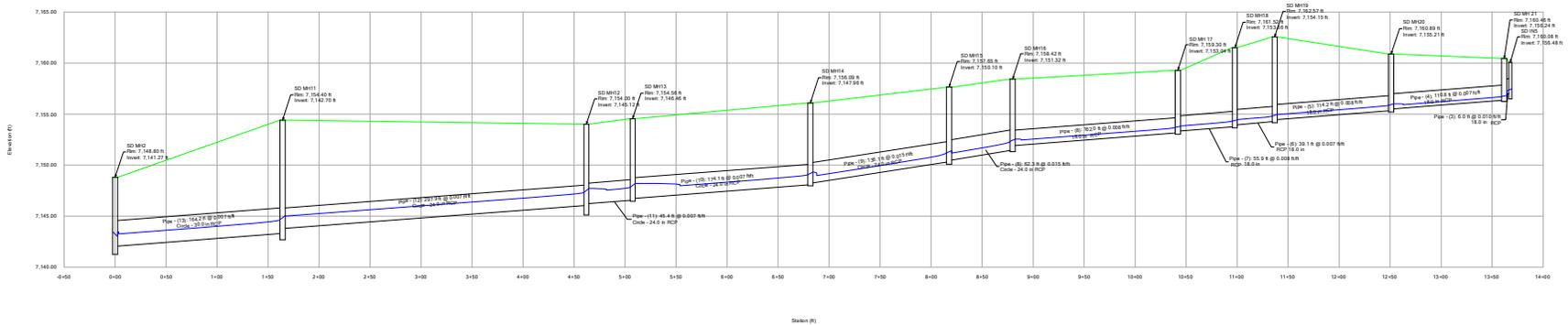
## Engineering Profile - SDIN 13 to MH22 (Proposed Strom.stsw)



# Profile Report

## Engineering Profile - SD MH2 to SD IN5 (Proposed Strom.stsw)

### 10 YEAR EVENT



**FlexTable: Catch Basin Table - 10 YEAR EVENT**

Label	Notes	Elevation (Ground) (ft)	Headloss Method	Headloss Coefficient (Standard)	Headloss (ft)
SD IN11	CDOT Type 13 Combo	7,152.33	Standard	0.500	0.14
SD IN13	CDOT Type 13 Combo	7,146.46	Standard	0.500	0.01
SD IN12	CDOT Type R	7,146.46	Standard	0.500	0.12
SD IN4	CDOT Type 13 Combo	7,148.04	Standard	0.500	0.12
SD IN3	CDOT Type R	7,153.13	Standard	0.500	0.16
SD IN10	CDOT Type R	7,153.71	Standard	0.500	0.03
SD IN9	CDOT Type 13	7,151.81	Standard	0.500	0.15
SD IN8	CDOT Type 13	7,152.68	Standard	0.500	0.09
SD IN7	CDOT Type 13	7,156.65	Standard	0.500	0.17
SD IN6	CDOT Type 13	7,160.43	Standard	0.500	0.07
SD IN5	CDOT Type 13	7,160.08	Standard	0.500	0.07
SD IN1	CDOT Type 13	7,158.82	Standard	0.500	0.12
SD IN2	CDOT Type 13	7,155.73	Standard	0.500	0.15

### FlexTable: Manhole Table - 10 YEAR EVENT

Label	Notes	Elevation (Rim) (ft)	Headloss Method	Headloss Coefficient (Standard)	Headloss (ft)
SD MH19	5' DIA MH	7,162.57	Standard	0.800	0.16
SD MH18	5' DIA MH	7,161.52	Standard	0.600	0.12
SD MH20	5' DIA MH	7,160.89	Standard	0.700	0.14
SD MH 21	5' DIA MH	7,160.46	Standard	0.800	0.11
SD MH 17	5' DIA MH	7,159.30	Standard	0.600	0.12
SD MH10	5' DIA MH	7,159.19	Standard	0.800	0.19
SD MH16	5' DIA MH	7,158.42	Standard	0.700	0.24
SD MH15	5' DIA MH	7,157.65	Standard	0.600	0.21
SD MH9	5' DIA MH	7,156.14	Standard	0.700	0.24
SD MH14	5' DIA MH	7,156.09	Standard	0.700	0.27
SD MH8	5' DIA MH	7,155.20	Standard	0.500	0.17
SD MH13	5' DIA MH	7,154.56	Standard	0.700	0.38
SD MH11	5' DIA MH	7,154.40	Standard	0.700	0.38
SD MH12	5' DIA MH	7,154.00	Standard	0.700	0.40
SD MH7	5' DIA MH	7,153.82	Standard	0.700	0.33
SD MH6	5' DIA MH	7,152.20	Standard	0.600	0.28
SD MH5	5' DIA MH	7,151.02	Standard	0.600	0.27
SD MH3	5' DIA MH	7,149.25	Standard	0.600	0.24
SD MH2	6' DIA MH	7,148.80	Standard	0.700	0.46
SD MH4	5' DIA MH	7,148.30	Standard	0.700	0.29
SD MH1	6' DIA MH	7,146.66	Standard	0.700	0.47
SD MH-22	5' DIA MH	7,146.46	Standard	0.700	0.18

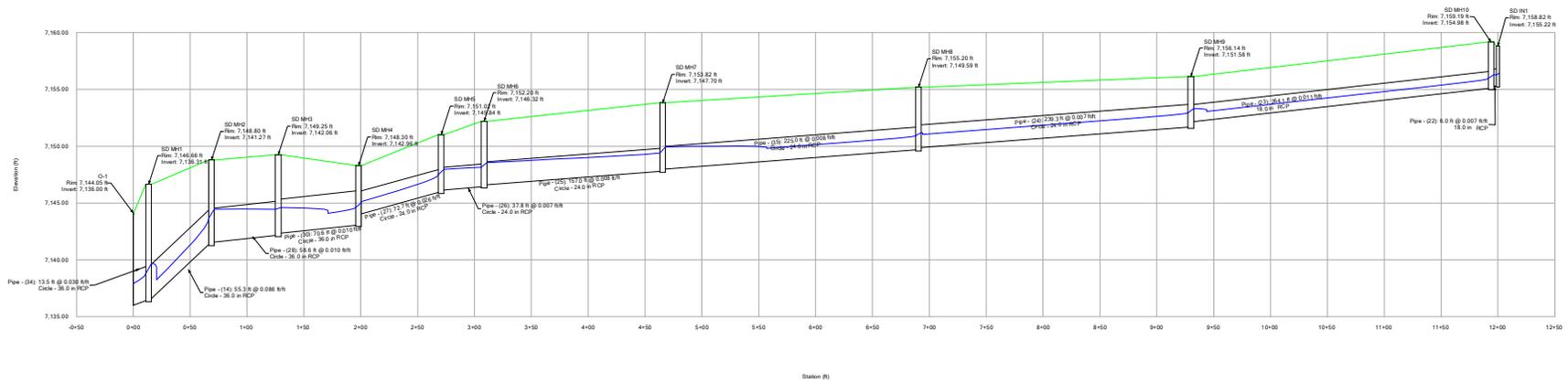
**FlexTable: Conduit Table - 10 YEAR EVENT**

Label	Diameter (in)	Slope (Calculated) (ft/ft)	Velocity (ft/s)	Invert (Start) (ft)	Invert (Stop) (ft)	Manning's n	Flow (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Froude Number (Normal)
Pipe - (5)	18.0	0.008	4.23	7,155.31	7,154.45	0.013	2.18	7,155.87	7,154.95	7,156.07	7,155.23	1.236
Pipe - (6)	18.0	0.007	4.19	7,154.25	7,153.96	0.013	2.13	7,154.80	7,154.46	7,155.01	7,154.73	1.229
Pipe - (7)	18.0	0.008	4.20	7,153.76	7,153.34	0.013	2.12	7,154.31	7,153.83	7,154.51	7,154.11	1.237
Pipe - (4)	18.0	0.007	3.43	7,156.34	7,155.51	0.013	1.05	7,156.72	7,156.01	7,156.86	7,156.08	1.228
Pipe - (16)	18.0	0.010	3.95	7,155.80	7,155.74	0.013	1.20	7,156.21	7,156.10	7,156.36	7,156.31	1.418
Pipe - (3)	18.0	0.010	3.80	7,157.00	7,156.94	0.013	1.05	7,157.38	7,157.27	7,157.52	7,157.47	1.414
Pipe - (8)	18.0	0.008	4.19	7,153.14	7,151.92	0.013	2.09	7,153.69	7,152.56	7,153.89	7,152.69	1.239
Pipe - (22)	18.0	0.007	4.34	7,155.32	7,155.28	0.013	2.80	7,155.95	7,155.88	7,156.19	7,156.16	1.154
Pipe - (23)	18.0	0.011	5.20	7,155.08	7,152.18	0.013	2.79	7,155.71	7,152.82	7,155.95	7,153.05	1.493
Pipe - (8)	24.0	0.015	7.15	7,151.42	7,150.50	0.013	6.46	7,152.32	7,151.40	7,152.67	7,151.74	1.819
Pipe - (17)	18.0	0.019	7.39	7,153.15	7,151.92	0.013	4.86	7,154.00	7,152.52	7,154.34	7,153.37	1.948
Pipe - (9)	24.0	0.015	7.18	7,150.30	7,148.26	0.013	6.42	7,151.20	7,149.33	7,151.54	7,149.55	1.833
Pipe - (24)	24.0	0.007	5.58	7,151.68	7,149.89	0.013	6.43	7,152.58	7,150.68	7,152.92	7,151.16	1.282
Pipe - (32)	18.0	0.008	5.10	7,152.23	7,152.18	0.013	3.77	7,152.97	7,152.86	7,153.26	7,153.22	1.275
Pipe - (10)	24.0	0.007	5.87	7,148.06	7,146.76	0.013	7.81	7,149.05	7,148.21	7,149.44	7,148.37	1.265
Pipe - (33)	18.0	0.008	3.94	7,149.18	7,148.56	0.013	1.68	7,149.67	7,149.33	7,149.84	7,149.38	1.240
Pipe - (35)	24.0	0.008	5.54	7,149.69	7,148.00	0.013	6.21	7,150.57	7,149.26	7,150.91	7,149.40	1.286
Pipe - (11)	24.0	0.007	6.60	7,146.56	7,146.22	0.013	12.45	7,147.83	7,147.71	7,148.37	7,148.09	1.190
Pipe - (18)	24.0	0.023	7.86	7,148.31	7,146.76	0.013	5.04	7,149.10	7,148.21	7,149.40	7,148.28	2.290
Pipe - (12)	24.0	0.007	6.65	7,146.02	7,143.80	0.013	13.00	7,147.32	7,144.99	7,147.88	7,145.68	1.175
Pipe - (13)	30.0	0.007	7.03	7,143.30	7,142.07	0.013	15.90	7,144.65	7,143.47	7,145.19	7,143.96	1.303
Pipe - (20)	18.0	0.030	8.01	7,145.92	7,144.30	0.013	3.61	7,146.65	7,144.75	7,146.93	7,145.75	2.469
Pipe - (19)	18.0	0.025	6.33	7,146.87	7,146.72	0.013	2.01	7,147.70	7,147.71	7,147.76	7,147.75	2.234
Pipe - (25)	24.0	0.008	6.29	7,147.80	7,146.62	0.013	10.07	7,148.94	7,147.82	7,149.40	7,148.23	1.238
Pipe - (31)	18.0	0.030	8.44	7,149.02	7,148.30	0.013	4.33	7,149.82	7,149.26	7,150.14	7,149.47	2.467
Pipe - (26)	24.0	0.007	6.23	7,146.42	7,146.14	0.013	9.88	7,147.54	7,147.34	7,148.00	7,147.73	1.232
Pipe - (27)	24.0	0.026	9.84	7,145.94	7,144.06	0.013	9.84	7,147.06	7,144.78	7,147.52	7,146.22	2.400
Pipe - (30)	36.0	0.010	7.15	7,143.06	7,142.36	0.013	12.13	7,144.17	7,143.51	7,144.57	7,143.88	1.596
Pipe - (28)	36.0	0.010	7.17	7,142.16	7,141.57	0.013	12.04	7,143.26	7,143.47	7,143.67	7,143.57	1.608
Pipe - (14)	36.0	0.086	19.16	7,141.37	7,136.61	0.013	25.69	7,143.01	7,138.56	7,143.67	7,138.99	4.684
Pipe - (29)	18.0	0.030	7.38	7,144.37	7,144.16	0.013	2.70	7,144.99	7,144.62	7,145.23	7,145.15	2.470
Pipe - (21)	18.0	0.030	7.57	7,140.55	7,139.56	0.013	2.95	7,141.20	7,140.21	7,141.45	7,140.46	2.472
Pipe - (34)	36.0	0.030	13.35	7,136.41	7,136.00	0.013	26.72	7,138.08	7,137.27	7,138.76	7,138.64	2.790
CO-1	18.0	0.030	3.83	7,139.87	7,139.56	0.013	0.30	7,140.20	7,140.21	7,140.22	7,140.22	2.236
CO-2	18.0	0.030	7.74	7,139.36	7,137.91	0.013	3.14	7,140.03	7,138.33	7,140.29	7,139.25	2.486

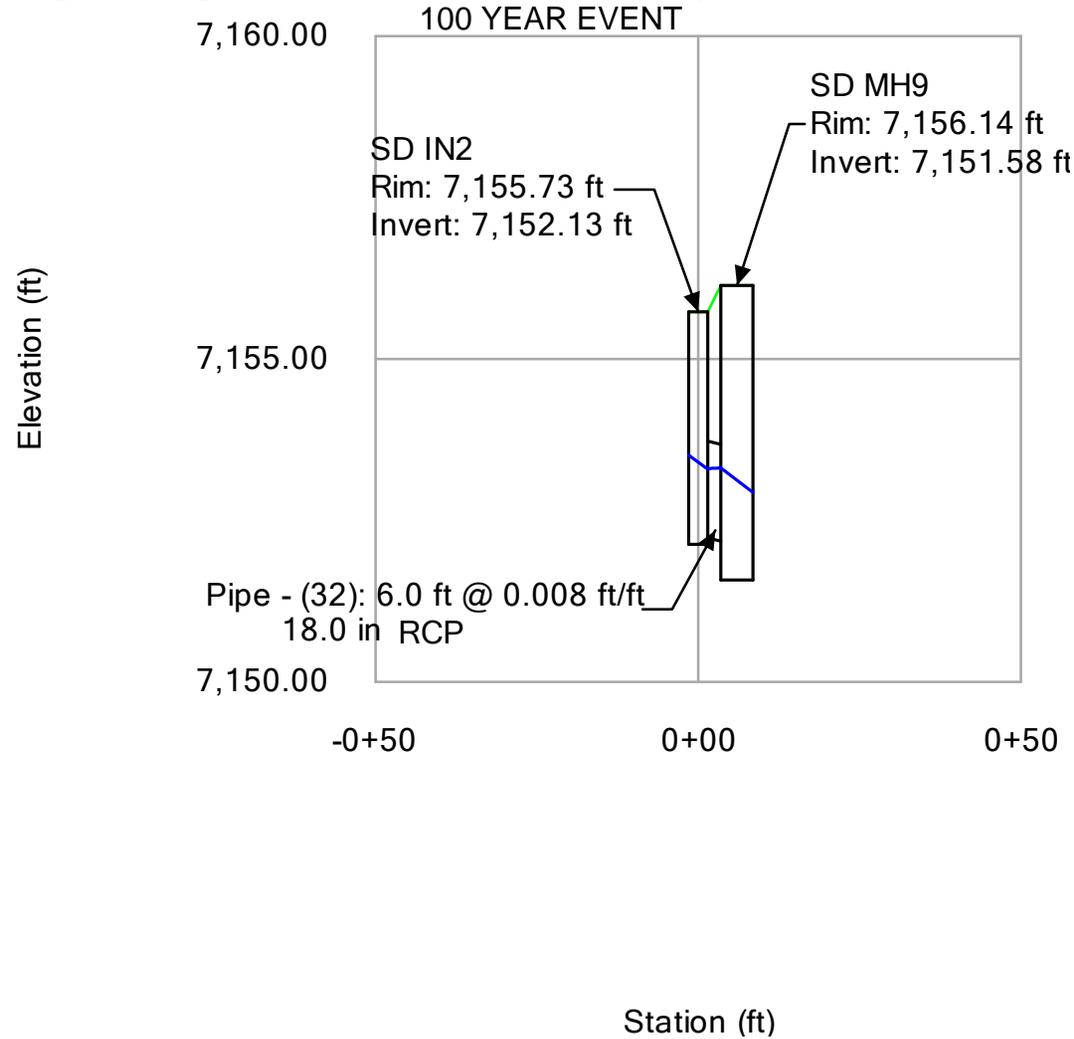
# Profile Report

## Engineering Profile - O-1 to SD IN1 (Proposed Strom.stsw)

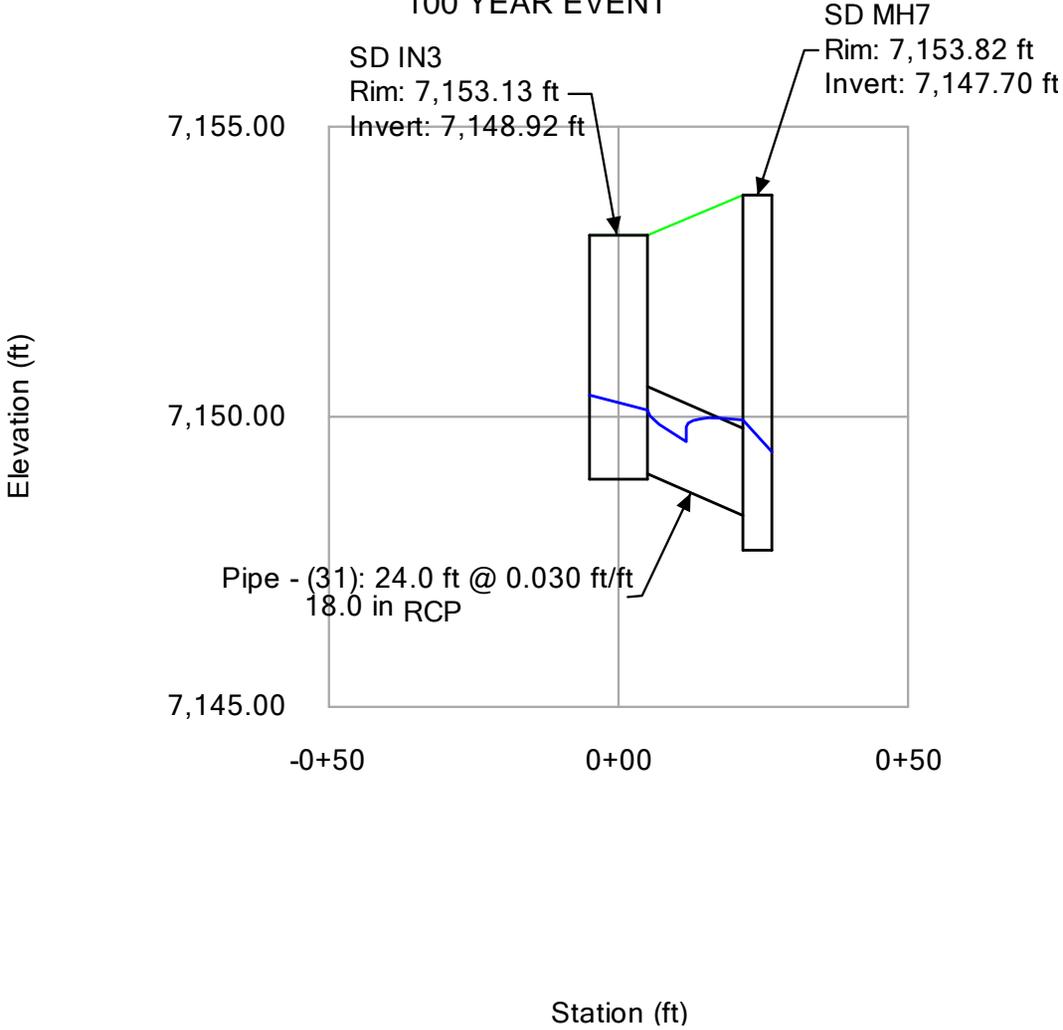
### 100 YEAR EVENT



**Profile Report**  
**Engineering Profile - SD IN2 to SD MH9 (Proposed Strom.stsw)**

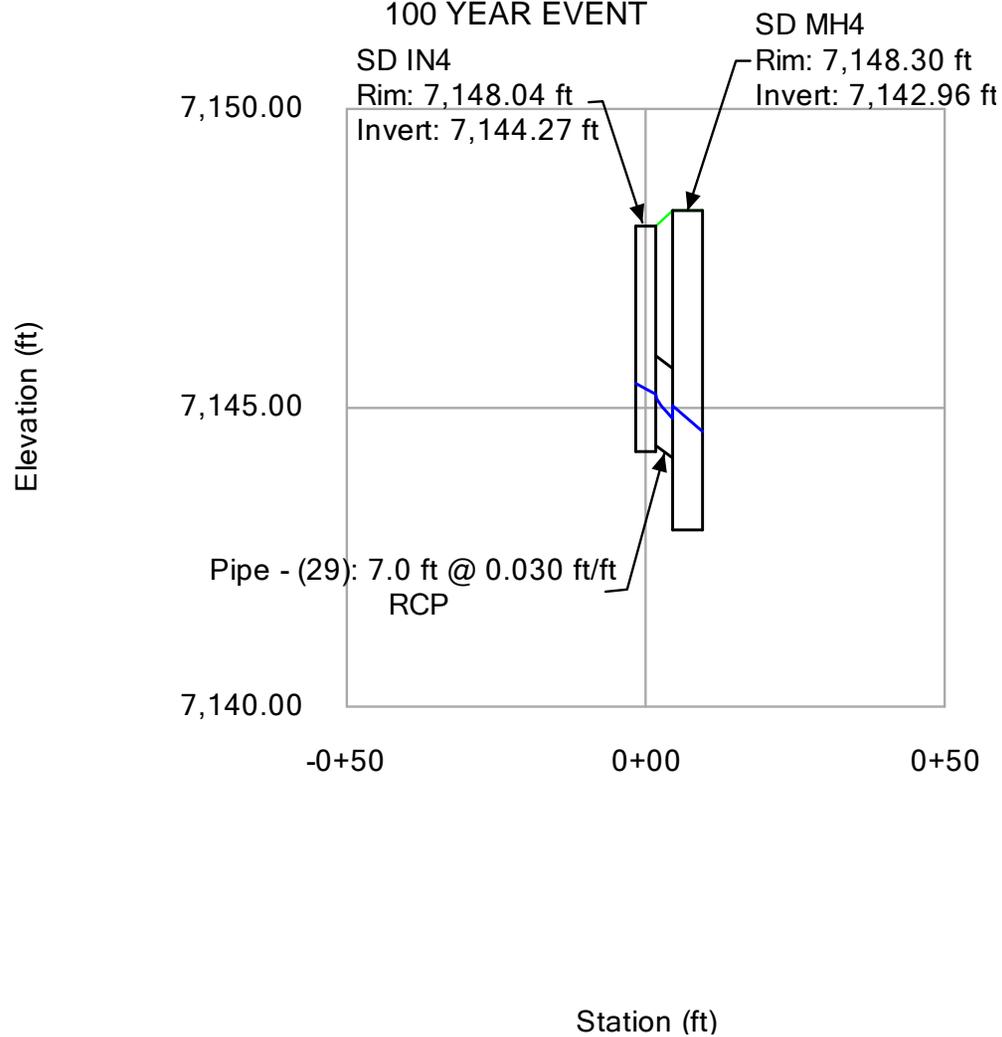


**Profile Report**  
**Engineering Profile - SDIN3 to SD MH7 (Proposed Strom.stsw)**  
 100 YEAR EVENT

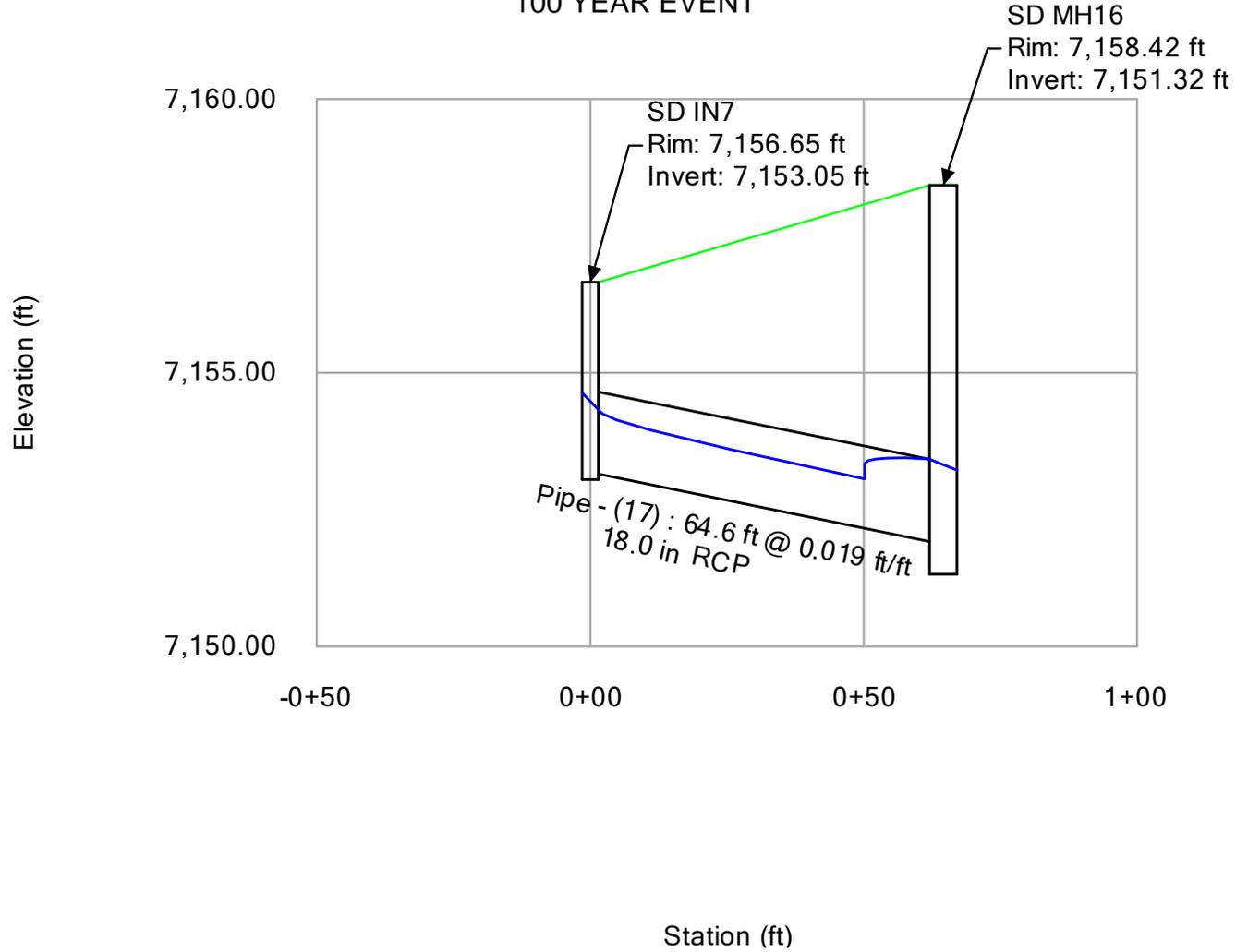


# Profile Report

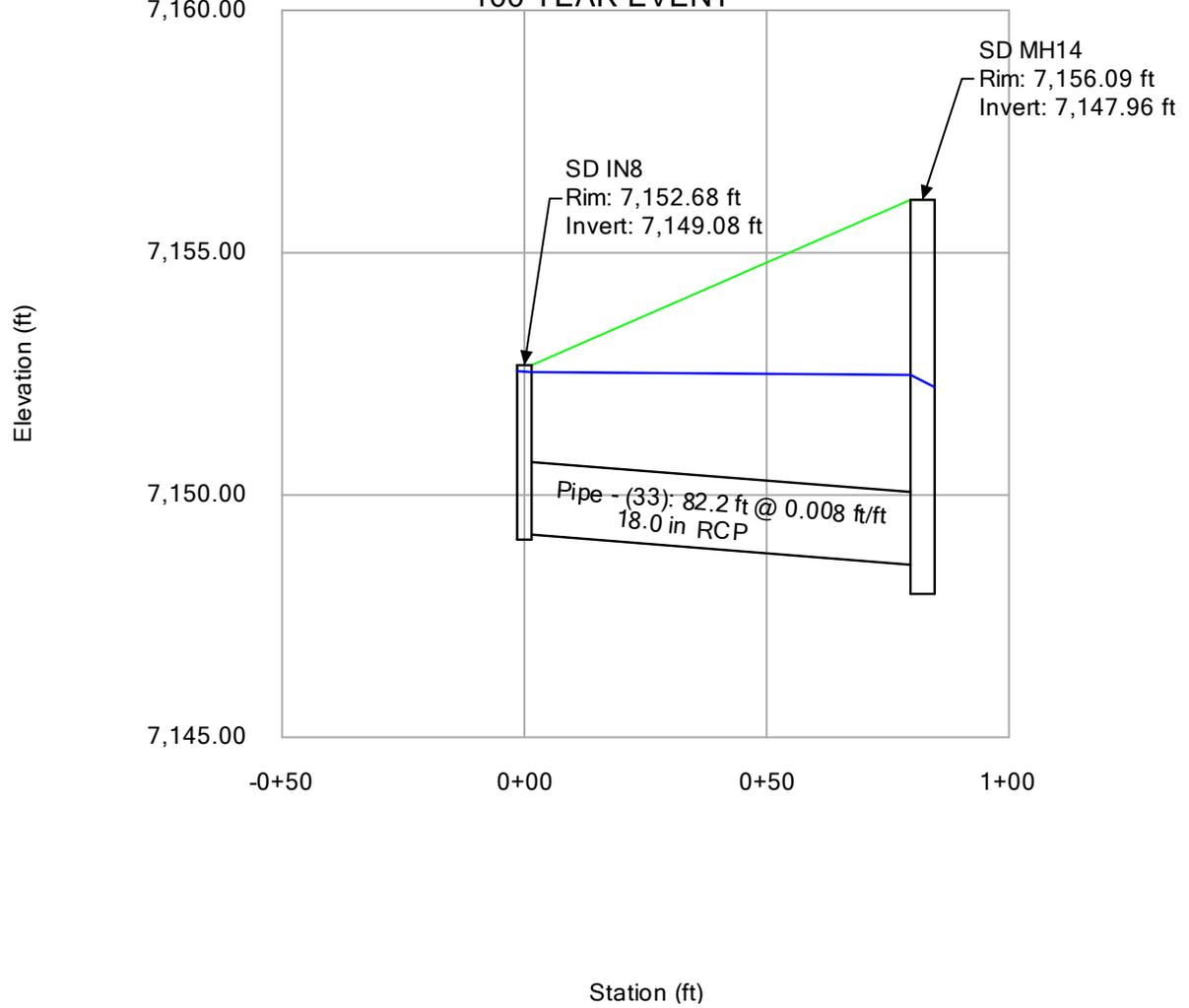
## Engineering Profile - SD IN4 to SD MH4 (Proposed Strom.stsw)



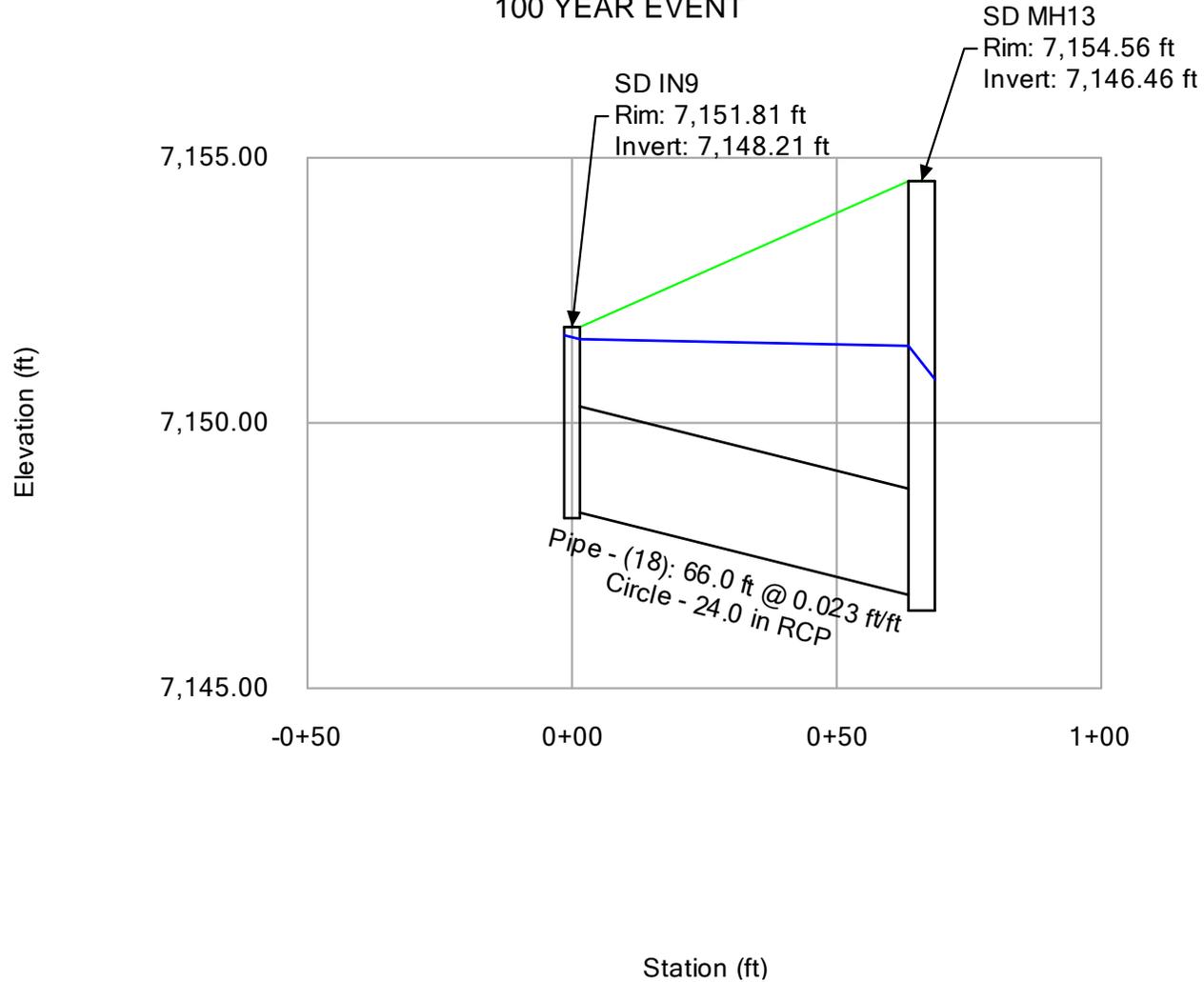
**Profile Report**  
**Engineering Profile - SD IN7 to SD MH16 (Proposed Strom.stsw)**  
100 YEAR EVENT



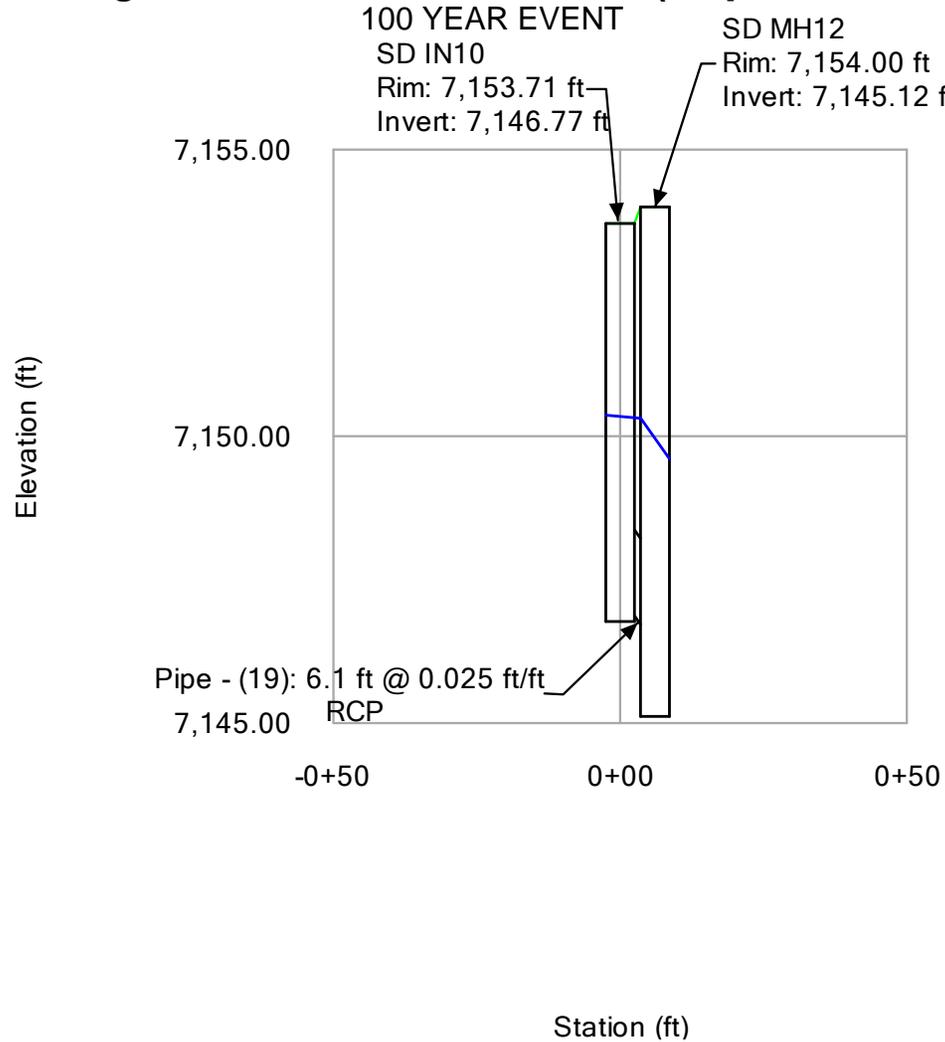
**Profile Report**  
**Engineering Profile - SD IN8 to SD MH14 (Proposed Strom.stsw)**  
**100 YEAR EVENT**



**Profile Report**  
**Engineering Profile - SD IN9 to SD MH13 (Proposed Strom.stsw)**  
 100 YEAR EVENT



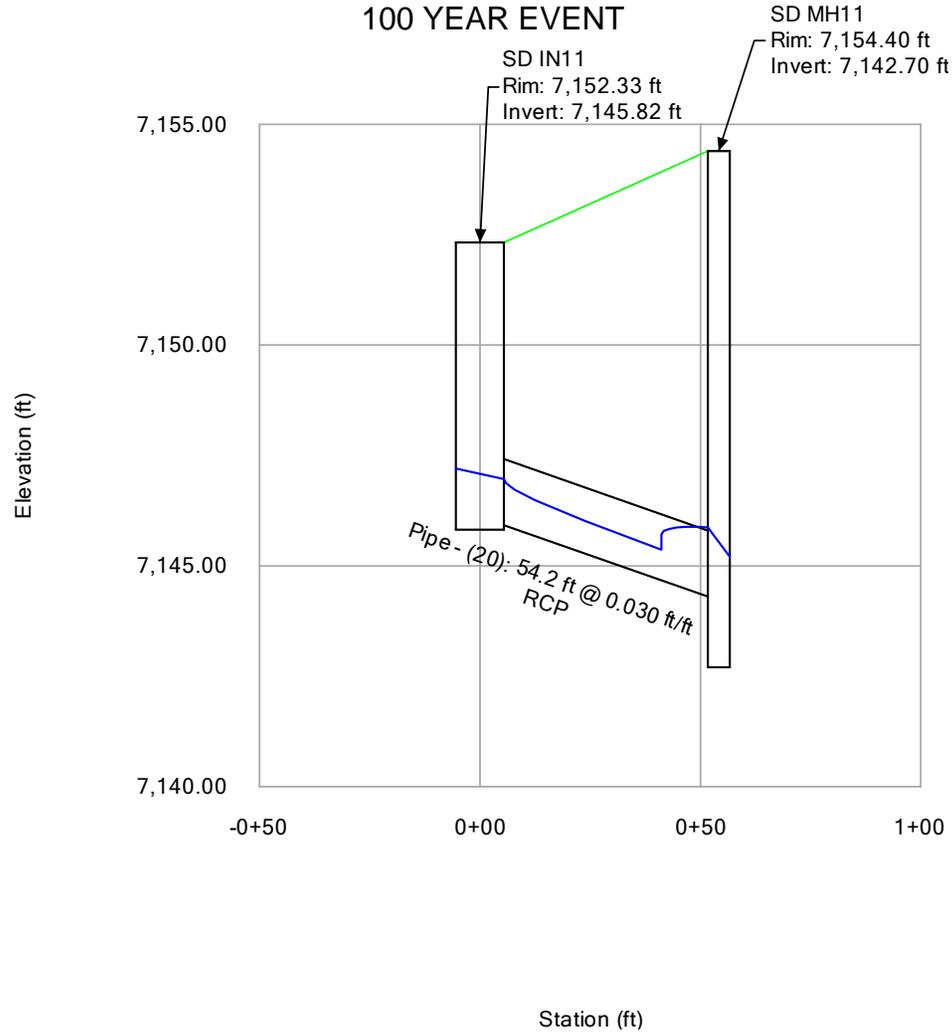
**Profile Report**  
**Engineering Profile - SD IN10 to SD MH12 (Proposed Strom.stsw)**



# Profile Report

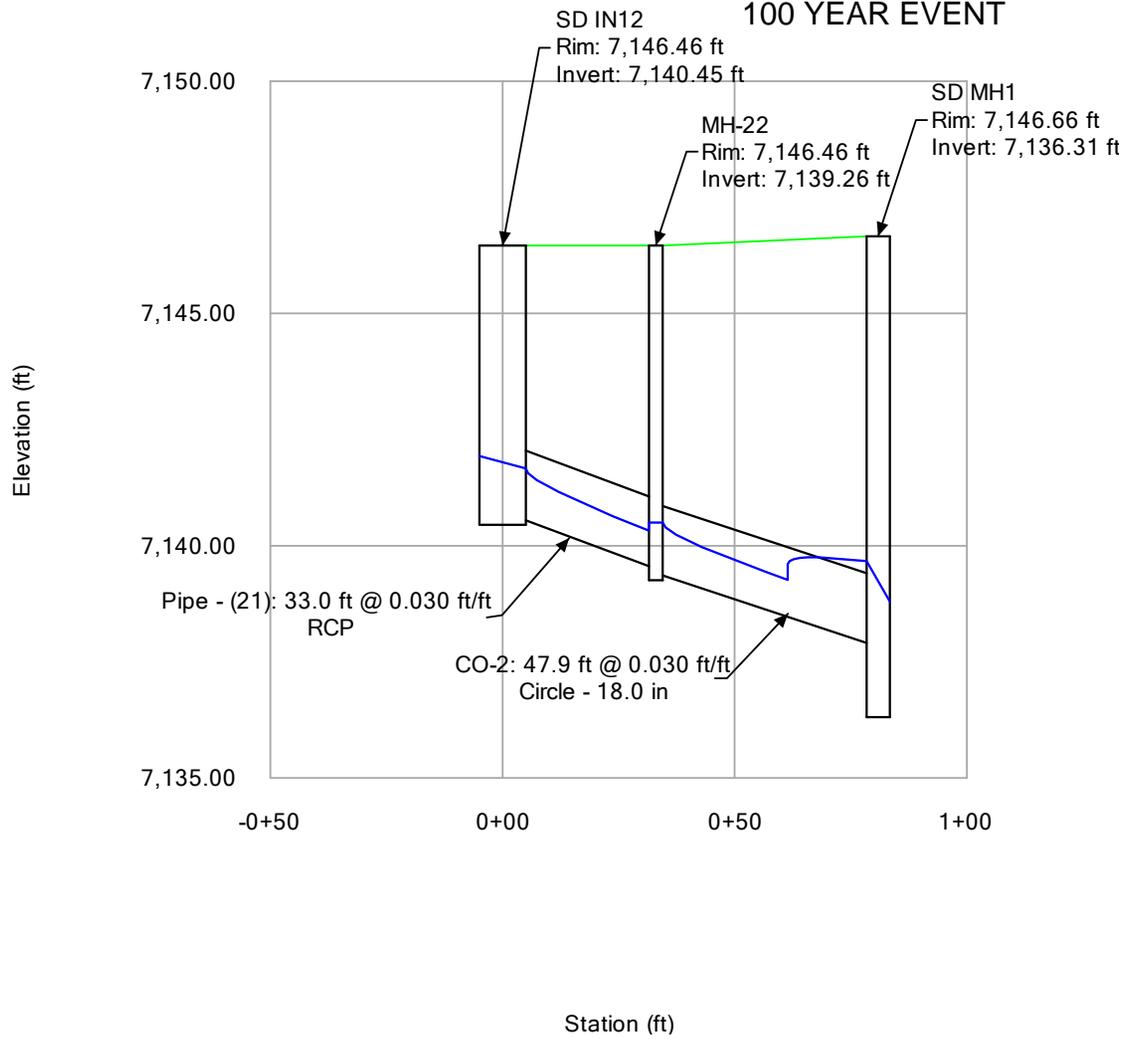
## Engineering Profile - SD IN11 to SD MH11 (Proposed Strom.stsw)

100 YEAR EVENT



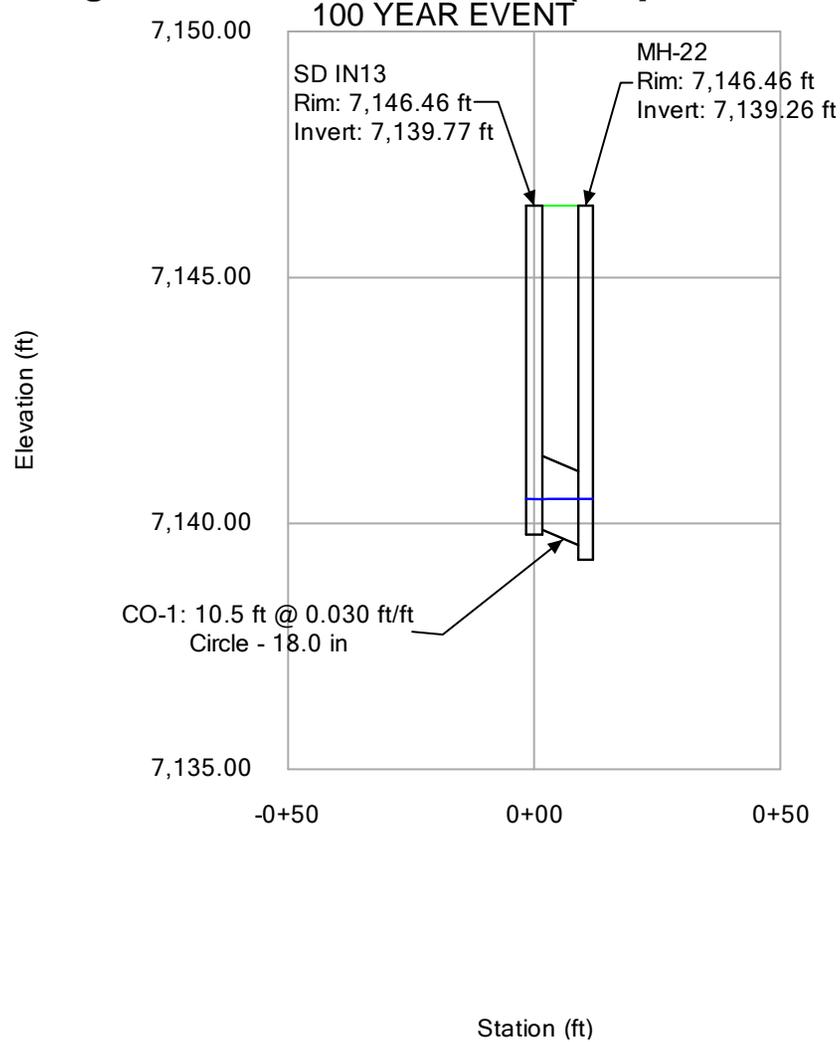
# Profile Report

## Engineering Profile - SD IN12 to SD MH1 (Proposed Strom.stsw)



# Profile Report

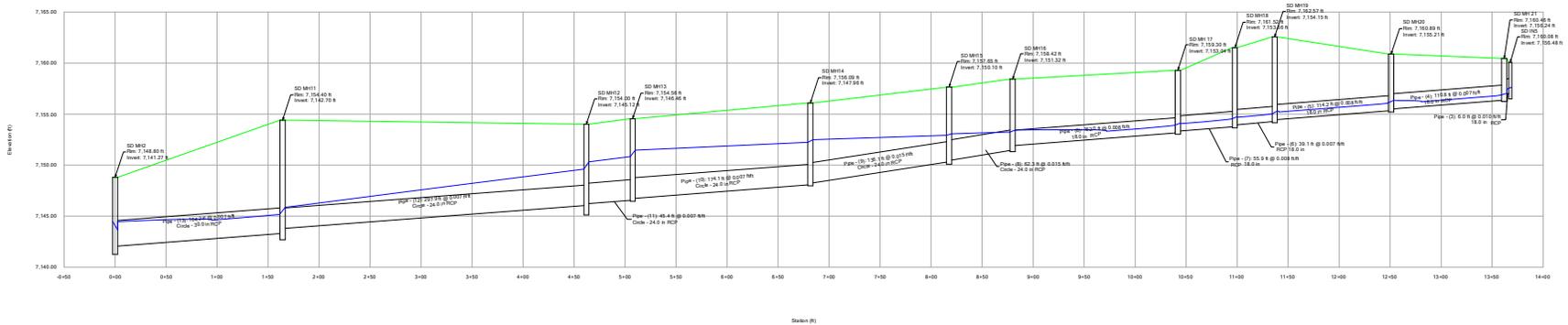
## Engineering Profile - SDIN 13 to MH22 (Proposed Strom.stsw)



# Profile Report

## Engineering Profile - SD MH2 to SD IN5 (Proposed Strom.stsw)

### 100 YEAR EVENT



### FlexTable: Catch Basin Table - 100 YEAR EVENT

Label	Notes	Elevation (Ground) (ft)	Headloss Method	Headloss Coefficient (Standard)	Headloss (ft)
SD IN11	CDOT Type 13 Combo	7,152.33	Standard	0.500	0.24
SD IN13	CDOT Type 13 Combo	7,146.46	Standard	0.500	0.01
SD IN12	CDOT Type R	7,146.46	Standard	0.500	0.27
SD IN4	CDOT Type 13 Combo	7,148.04	Standard	0.500	0.18
SD IN3	CDOT Type R	7,153.13	Standard	0.500	0.26
SD IN10	CDOT Type R	7,153.71	Standard	0.500	0.04
SD IN9	CDOT Type 13	7,151.81	Standard	0.500	0.08
SD IN8	CDOT Type 13	7,152.68	Standard	0.500	0.02
SD IN7	CDOT Type 13	7,156.65	Standard	0.500	0.30
SD IN6	CDOT Type 13	7,160.43	Standard	0.500	0.11
SD IN5	CDOT Type 13	7,160.08	Standard	0.500	0.10
SD IN1	CDOT Type 13	7,158.82	Standard	0.500	0.16
SD IN2	CDOT Type 13	7,155.73	Standard	0.500	0.22

### FlexTable: Manhole Table - 100 YEAR EVENT

Label	Notes	Elevation (Rim) (ft)	Headloss Method	Headloss Coefficient (Standard)	Headloss (ft)
SD MH19	5' DIA MH	7,162.57	Standard	0.800	0.25
SD MH18	5' DIA MH	7,161.52	Standard	0.600	0.19
SD MH20	5' DIA MH	7,160.89	Standard	0.700	0.22
SD MH 21	5' DIA MH	7,160.46	Standard	0.800	0.16
SD MH 17	5' DIA MH	7,159.30	Standard	0.600	0.19
SD MH10	5' DIA MH	7,159.19	Standard	0.800	0.30
SD MH16	5' DIA MH	7,158.42	Standard	0.700	0.20
SD MH15	5' DIA MH	7,157.65	Standard	0.600	0.15
SD MH9	5' DIA MH	7,156.14	Standard	0.700	0.38
SD MH14	5' DIA MH	7,156.09	Standard	0.700	0.25
SD MH8	5' DIA MH	7,155.20	Standard	0.500	0.26
SD MH13	5' DIA MH	7,154.56	Standard	0.700	0.63
SD MH11	5' DIA MH	7,154.40	Standard	0.700	0.66
SD MH12	5' DIA MH	7,154.00	Standard	0.700	0.71
SD MH7	5' DIA MH	7,153.82	Standard	0.700	0.55
SD MH6	5' DIA MH	7,152.20	Standard	0.600	0.40
SD MH5	5' DIA MH	7,151.02	Standard	0.600	0.47
SD MH3	5' DIA MH	7,149.25	Standard	0.600	0.14
SD MH2	6' DIA MH	7,148.80	Standard	0.700	0.80
SD MH4	5' DIA MH	7,148.30	Standard	0.700	0.43
SD MH1	6' DIA MH	7,146.66	Standard	0.700	0.88
SD MH-22	5' DIA MH	7,146.46	Standard	0.700	0.39

**FlexTable: Conduit Table - 100 YEAR EVENT**

Label	Diameter (in)	Slope (Calculated) (ft/ft)	Velocity (ft/s)	Invert (Start) (ft)	Invert (Stop) (ft)	Manning's n	Flow (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Froude Number (Normal)
Pipe - (5)	18.0	0.008	5.11	7,155.31	7,154.45	0.013	4.37	7,156.11	7,155.30	7,156.43	7,155.58	1.191
Pipe - (6)	18.0	0.007	5.06	7,154.25	7,153.96	0.013	4.29	7,155.04	7,154.69	7,155.36	7,155.08	1.184
Pipe - (7)	18.0	0.008	5.07	7,153.76	7,153.34	0.013	4.27	7,154.55	7,154.06	7,154.87	7,154.46	1.193
Pipe - (4)	18.0	0.007	4.16	7,156.34	7,155.51	0.013	2.07	7,156.88	7,156.34	7,157.08	7,156.40	1.234
Pipe - (16)	18.0	0.010	4.83	7,155.80	7,155.74	0.013	2.41	7,156.39	7,156.34	7,156.61	7,156.55	1.428
Pipe - (3)	18.0	0.010	4.62	7,157.00	7,156.94	0.013	2.07	7,157.54	7,157.42	7,157.74	7,157.70	1.428
Pipe - (8)	18.0	0.008	5.06	7,153.14	7,151.92	0.013	4.23	7,153.93	7,153.42	7,154.24	7,153.51	1.196
Pipe - (22)	18.0	0.007	5.14	7,155.32	7,155.28	0.013	5.43	7,156.27	7,156.28	7,156.60	7,156.57	1.072
Pipe - (23)	18.0	0.011	6.21	7,155.08	7,152.18	0.013	5.42	7,155.98	7,153.31	7,156.35	7,153.54	1.434
Pipe - (8)	24.0	0.015	8.59	7,151.42	7,150.50	0.013	12.76	7,153.23	7,153.06	7,153.51	7,153.32	1.757
Pipe - (17)	18.0	0.019	8.71	7,153.15	7,151.92	0.013	9.33	7,154.33	7,153.42	7,154.94	7,153.86	1.805
Pipe - (9)	24.0	0.015	8.62	7,150.30	7,148.26	0.013	12.69	7,152.91	7,152.48	7,153.16	7,152.73	1.772
Pipe - (24)	24.0	0.007	6.57	7,151.68	7,149.89	0.013	12.23	7,152.94	7,151.19	7,153.47	7,151.69	1.194
Pipe - (32)	18.0	0.008	5.93	7,152.23	7,152.18	0.013	7.06	7,153.29	7,153.31	7,153.73	7,153.69	1.152
Pipe - (10)	24.0	0.007	6.87	7,148.06	7,146.76	0.013	15.08	7,152.23	7,151.46	7,152.59	7,151.81	1.125
Pipe - (33)	18.0	0.008	4.55	7,149.18	7,148.56	0.013	2.82	7,152.54	7,152.48	7,152.58	7,152.52	1.229
Pipe - (35)	24.0	0.008	6.54	7,149.69	7,148.00	0.013	11.87	7,150.93	7,149.94	7,151.45	7,150.17	1.205
Pipe - (11)	24.0	0.007	7.61	7,146.56	7,146.22	0.013	23.92	7,150.82	7,150.32	7,151.73	7,151.22	0.949
Pipe - (18)	24.0	0.023	9.51	7,148.31	7,146.76	0.013	9.88	7,151.58	7,151.46	7,151.73	7,151.61	2.283
Pipe - (12)	24.0	0.007	8.07	7,146.02	7,143.80	0.013	25.35	7,149.61	7,145.87	7,150.62	7,146.88	1.006
Pipe - (13)	30.0	0.007	8.16	7,143.30	7,142.07	0.013	31.32	7,145.21	7,144.47	7,146.15	7,145.12	1.095
Pipe - (20)	18.0	0.030	9.70	7,145.92	7,144.30	0.013	7.25	7,146.96	7,145.87	7,147.44	7,146.13	2.413
Pipe - (19)	18.0	0.025	7.82	7,146.87	7,146.72	0.013	4.24	7,150.33	7,150.32	7,150.42	7,150.41	2.238
Pipe - (25)	24.0	0.008	7.11	7,147.80	7,146.62	0.013	19.09	7,149.39	7,148.54	7,150.18	7,149.13	0.971
Pipe - (31)	18.0	0.030	9.96	7,149.02	7,148.30	0.013	7.99	7,150.12	7,149.94	7,150.63	7,150.26	2.399
Pipe - (26)	24.0	0.007	7.06	7,146.42	7,146.14	0.013	18.78	7,148.15	7,147.97	7,148.81	7,148.57	0.976
Pipe - (27)	24.0	0.026	11.66	7,145.94	7,144.06	0.013	18.70	7,147.50	7,145.12	7,148.29	7,147.02	2.296
Pipe - (30)	36.0	0.010	8.54	7,143.06	7,142.36	0.013	23.00	7,144.60	7,144.60	7,145.22	7,144.86	1.575
Pipe - (28)	36.0	0.010	8.57	7,142.16	7,141.57	0.013	22.86	7,144.46	7,144.47	7,144.70	7,144.63	1.587
Pipe - (14)	36.0	0.086	23.13	7,141.37	7,136.61	0.013	49.84	7,143.67	7,139.68	7,144.81	7,140.45	4.689
Pipe - (29)	18.0	0.030	8.78	7,144.37	7,144.16	0.013	5.00	7,145.23	7,145.03	7,145.58	7,145.37	2.462
Pipe - (21)	18.0	0.030	10.05	7,140.55	7,139.56	0.013	8.27	7,141.66	7,140.32	7,142.20	7,141.62	2.391
Pipe - (34)	36.0	0.030	16.15	7,136.41	7,136.00	0.013	54.16	7,138.80	7,137.92	7,140.05	7,139.92	2.692
CO-1	18.0	0.030	4.73	7,139.87	7,139.56	0.013	0.60	7,140.49	7,140.50	7,140.50	7,140.50	2.329
CO-2	18.0	0.030	10.20	7,139.36	7,137.91	0.013	8.65	7,140.50	7,139.68	7,141.06	7,140.05	2.393

## Appendix D - Reference Documents

## 2.1. - Rainfall Depths

Rainfall depths must be determined based on the duration and return period of the design storm and the size of the drainage basin being evaluated. Depths can be derived by the methods described in the NOAA Atlas. The depths reported in the NOAA Atlas represent probable total depths for each duration and return period at a point on the ground. An extensive evaluation of available rain gage data was completed with the Carlton Study. While some increase in recorded depths was noted from the airport gage data, the other long-term gage locations showed that depths consistent with the NOAA Atlas can be expected. Since the NOAA Atlas is in the process of being updated, it was determined that the published atlas should continue to be used as the source of rainfall depths until this publication is revised or replaced.

The methods described in this Manual require only that the 1-hour, 6-hour and 24-hours depths be used as input. The storm return periods required for the application of methods in this Manual are the 2-, 5-, 10-, 25-, 50- and 100-year events. The 6-hour and 24-hour depths for these return periods can be read directly from Figures 6-6 through 6-17 at the end of this chapter. The 1-hour depth for return periods can be calculated for all design return periods following this procedure:

Step 1: Calculate 2-year, 1-hour rainfall based on 2-year, 6-hour and 24-hour values.

$$Y_2 = 0.218 + 0.709 \cdot (X_1 \cdot X_1 / X_2) \quad (\text{Eq. 6-1})$$

Where:

$Y_2$  = 2-year, 1-hour rainfall (in)

$X_1$  = 2-year, 6-hour rainfall (in) from Figure 6-6

$X_2$  = 2-year, 24-hour rainfall (in) from Figure 6-12

Step 2: Calculate 100-year, 1-hour rainfall based on 2-year 6-hour and 24-hour values

$$Y_{100} = 1.897 + 0.439 \cdot (X_3 \cdot X_3 / X_4) - 0.008Z \quad (\text{Eq. 6-2})$$

Where:

$Y_{100}$  = 100-year, 1-hour rainfall (in)

$X_3$  = 100-year, 6-hour rainfall (in) from Figure 6-11

$X_4$  = 100-year, 24-hour rainfall (in) from Figure 6-17

Z = Elevation in hundreds of feet above sea level

### 3.0. - RATIONAL METHOD

The Rational Method is used to determine runoff peak discharges for drainage basins up to and including 130 acres in size and when hydrologic routing is relatively simple. However, the drainage area should be divided into sub-basins that represent homogeneous land uses, soil types or land cover. The Rational Method is most typically applied for inlet and storm drain sizing.

The Rational Method is based on the direct relationship between rainfall and runoff, and is expressed by the following equation:

$$Q = C \cdot I \cdot A \quad (\text{Eq. 6-5})$$

In which:

Q = the maximum rate of runoff (cubic feet per second [cfs])

C = the runoff coefficient that is the ratio between the runoff volume from an area and the average rainfall depth over a given duration for that area

I = the average intensity of rainfall for a duration equal to the time of concentration (in/hr)

A = drainage basin area (acres)

The assumptions and limitations of the Rational Method are described in the UDFCD Manual, Volume 1, Runoff chapter. Standard Form 1 (SF-1) and Standard Form 2 (SF-2) are provided at the end of this chapter as Figure 6-23 and Figure 6-24, respectively to provide a standard format for Rational Method calculations. The SF-1 Form is used for calculating the time of concentration, and the SF-2 form is used to estimate accumulated peak discharges from multiple basins as storm runoff flows downstream in a channel or pipe. Results from the Rational Method calculations shall be included with the drainage report submittal. As an alternative to SF-1 and SF-2, the UD-Rational spreadsheet can be used to document basin parameters and calculations or other spreadsheets or programs can be used as long as the information and format is the similar to that shown in these standard forms.

#### 3.1. - Rational Method Runoff Coefficient (C)

The runoff coefficient represents the integrated effects of infiltration, detention storage, evaporation, retention, flow routing, and interception, all of which affect the time distribution and peak rate of runoff. Runoff coefficients are based on the imperviousness of a particular land use and the hydrologic soil type of the area and are to be selected in accordance with Table 6-6.

The procedure for determining the runoff coefficient includes these steps:

1. Categorize the site area into one or more similar land uses, each with a representative imperviousness, according to the information in Table 6-6.
2. Based on the dominant hydrologic soil type in the area, use Table 6-6 to estimate the runoff coefficient for the particular land use category for the design storms of interest.
3. Calculate an area-weighted average runoff coefficient for the site based on the runoff coefficients from individual land use areas of the site.

When analyzing an area for design purposes, urbanization of the full watershed, including both on-site and off-site areas, shall be assumed.

Gravel parking areas, storage areas, and access drives proposed on Site Improvement Plans shall be analyzed based on an imperviousness of 80%. This is due to the potential for gravel areas being paved over time by property owners and the resulting adverse impacts on the stormwater management facilities and adjacent properties.

There are some circumstances where the selection of impervious percentage values may require additional investigation due to unique land characteristics (e.g., recent burn areas). When these circumstances arise, it is the designer's responsibility to verify that the correct land use assumptions are made.

When multiple sub-basins are delineated, the composite C value calculation is:

$$C_c = (C_1 A_1 + C_2 A_2 + C_3 A_3 + \dots + C_i A_i) / A_t \quad (\text{Eq. 6-6})$$

Where:

$C_c$  = composite runoff coefficient for total area

$C_i$  = runoff coefficient for subarea corresponding to surface type or land use

$A_i$  = area of surface type corresponding to  $C_i$  (units must be the same as those used for total area)

$A_t$  = total area of all subareas for which composite runoff coefficient applies

$i$  = number of surface types in the drainage area

**Table 6-6. Runoff Coefficients for Rational Method**  
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/2 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57

½ Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96

Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

### 3.2. - Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration ( $t_c$ ) consists of an initial time or overland flow time ( $t_i$ ) plus the travel time ( $t_t$ ) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time ( $t_i$ ) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion ( $t_t$ ) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

$$t_c = t_i + t_t \quad (\text{Eq. 6-7})$$

Where:

$t_c$  = time of concentration (min)

$t_i$  = overland (initial) flow time (min)

$t_t$  = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

The overland flow time,  $t_i$ , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \quad (\text{Eq. 6-8})$$

Where:

$t_i$  = overland (initial) flow time (min)

$C_5$  = runoff coefficient for 5-year frequency (see Table 6-6)

$L$  = length of overland flow (300 ft maximum for non-urban land uses, 100 ft maximum for urban land uses)

$S$  = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time,  $t_t$ , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time,  $t_t$ , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_v S_w^{0.5} \quad (\text{Eq. 6-9})$$

Where:

$V$  = velocity (ft/s)

$C_v$  = conveyance coefficient (from Table 6-7)

$S_w$  = watercourse slope (ft/ft)

**Table 6-7. Conveyance Coefficient,  $C_v$**

Type of Land Surface	$C_v$
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried) *	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20
* For buried riprap, select $C_v$ value based on type of vegetative cover.	

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration ( $t_c$ ) is then the sum of the overland flow time ( $t_i$ ) and the travel time ( $t_t$ ) per Equation 6-7.

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = L / 180 + 10 \quad (\text{Eq. 6-10})$$

## 2.1. - DESIGN STORM WATER RUNOFF DETERMINATION

The City/County drainage policy permits the Rational Method and the Soil Conservation Service (SCS) Hydrograph Method as models to be used by designers in estimating storm water runoff for project purposes. The Rational Method is required for drainage basins of 100 acres or less. The SCS Hydrograph Method is required for drainage basins greater than 100 acres. For large complex Drainage Basin Planning Studies, computer models may be utilized following approval by City/County. Necessary data requirements, assumptions and detailed procedures for using models are discussed Section II. All drainage systems must be planned, designed and constructed to handle runoff from both the initial and major design storms. The initial design storm shall be the 10 year event. The major design storm shall be the 100-year event.

Normally in a roadway section, the initial drainage system should convey a substantial portion of the minor storm flows with the more intense or major storm flows conveyed by the available street capacity. Out of roadway sections, storm drain systems combined with overflow swales or drainageway or channel sections must be of adequate capacity to convey both design storms and protect adjacent properties.



**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Monument, Colorado, USA\***  
**Latitude: 39.1092°, Longitude: -104.864°**  
**Elevation: 7156 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps\\_&\\_aerials](#)

**PF tabular**

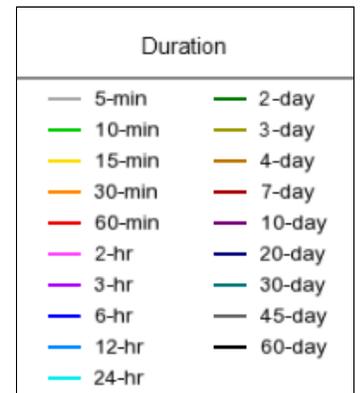
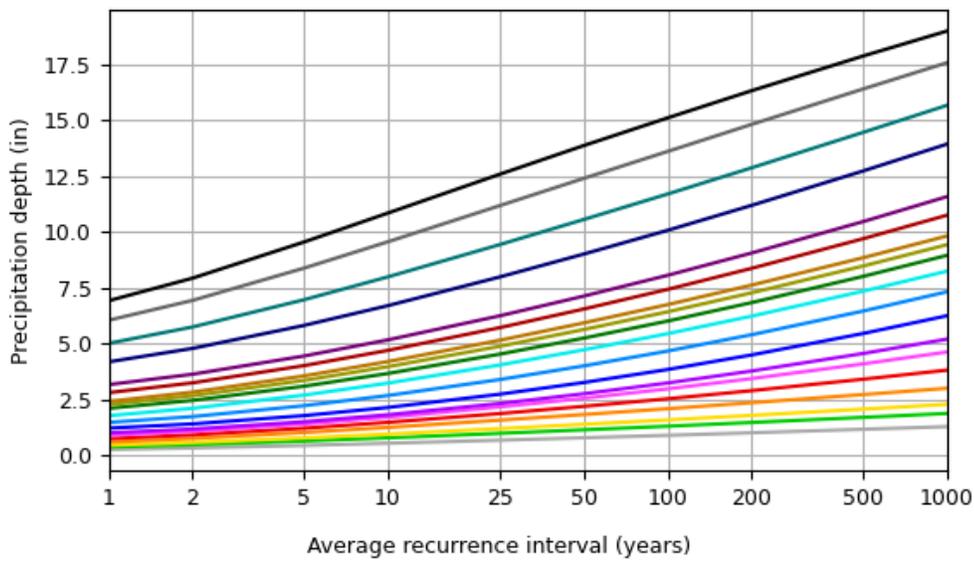
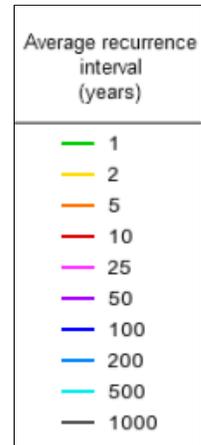
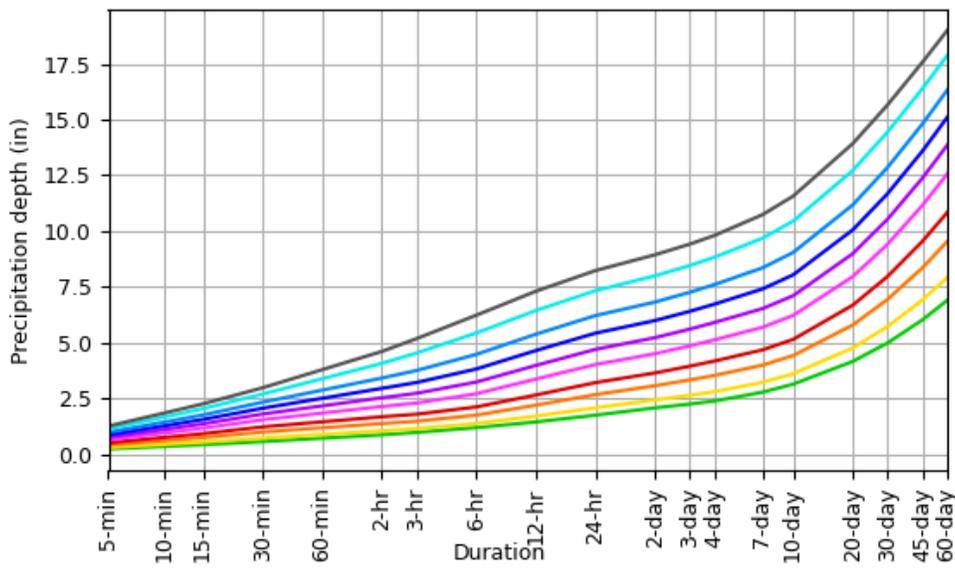
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.244</b> (0.200-0.297)	<b>0.312</b> (0.256-0.379)	<b>0.426</b> (0.348-0.518)	<b>0.523</b> (0.424-0.638)	<b>0.659</b> (0.517-0.830)	<b>0.768</b> (0.587-0.974)	<b>0.878</b> (0.648-1.14)	<b>0.993</b> (0.702-1.31)	<b>1.15</b> (0.780-1.55)	<b>1.27</b> (0.839-1.73)
<b>10-min</b>	<b>0.358</b> (0.293-0.434)	<b>0.457</b> (0.375-0.555)	<b>0.624</b> (0.509-0.759)	<b>0.765</b> (0.621-0.934)	<b>0.966</b> (0.757-1.22)	<b>1.12</b> (0.859-1.43)	<b>1.29</b> (0.949-1.66)	<b>1.45</b> (1.03-1.92)	<b>1.68</b> (1.14-2.27)	<b>1.86</b> (1.23-2.53)
<b>15-min</b>	<b>0.436</b> (0.358-0.530)	<b>0.558</b> (0.457-0.677)	<b>0.761</b> (0.621-0.926)	<b>0.933</b> (0.757-1.14)	<b>1.18</b> (0.923-1.48)	<b>1.37</b> (1.05-1.74)	<b>1.57</b> (1.16-2.03)	<b>1.77</b> (1.25-2.34)	<b>2.05</b> (1.39-2.76)	<b>2.27</b> (1.50-3.09)
<b>30-min</b>	<b>0.575</b> (0.471-0.698)	<b>0.736</b> (0.603-0.894)	<b>1.00</b> (0.820-1.22)	<b>1.23</b> (1.00-1.51)	<b>1.56</b> (1.22-1.96)	<b>1.81</b> (1.38-2.30)	<b>2.07</b> (1.53-2.68)	<b>2.34</b> (1.65-3.09)	<b>2.70</b> (1.84-3.64)	<b>2.99</b> (1.97-4.06)
<b>60-min</b>	<b>0.727</b> (0.596-0.882)	<b>0.897</b> (0.735-1.09)	<b>1.20</b> (0.975-1.45)	<b>1.46</b> (1.18-1.78)	<b>1.85</b> (1.46-2.35)	<b>2.17</b> (1.67-2.78)	<b>2.52</b> (1.86-3.27)	<b>2.88</b> (2.04-3.82)	<b>3.39</b> (2.31-4.59)	<b>3.80</b> (2.51-5.17)
<b>2-hr</b>	<b>0.878</b> (0.725-1.06)	<b>1.06</b> (0.872-1.27)	<b>1.38</b> (1.14-1.67)	<b>1.69</b> (1.38-2.04)	<b>2.15</b> (1.71-2.72)	<b>2.54</b> (1.97-3.23)	<b>2.96</b> (2.21-3.84)	<b>3.42</b> (2.45-4.52)	<b>4.08</b> (2.80-5.50)	<b>4.61</b> (3.07-6.24)
<b>3-hr</b>	<b>0.987</b> (0.818-1.18)	<b>1.16</b> (0.958-1.39)	<b>1.48</b> (1.22-1.78)	<b>1.80</b> (1.48-2.17)	<b>2.30</b> (1.85-2.92)	<b>2.74</b> (2.14-3.49)	<b>3.22</b> (2.42-4.18)	<b>3.76</b> (2.71-4.97)	<b>4.54</b> (3.14-6.12)	<b>5.19</b> (3.46-6.99)
<b>6-hr</b>	<b>1.20</b> (1.00-1.42)	<b>1.39</b> (1.16-1.65)	<b>1.76</b> (1.46-2.09)	<b>2.13</b> (1.75-2.54)	<b>2.72</b> (2.21-3.43)	<b>3.24</b> (2.55-4.10)	<b>3.83</b> (2.90-4.93)	<b>4.48</b> (3.25-5.89)	<b>5.44</b> (3.78-7.29)	<b>6.24</b> (4.19-8.35)
<b>12-hr</b>	<b>1.46</b> (1.22-1.71)	<b>1.72</b> (1.44-2.02)	<b>2.20</b> (1.84-2.60)	<b>2.66</b> (2.21-3.15)	<b>3.37</b> (2.74-4.19)	<b>3.98</b> (3.14-4.98)	<b>4.65</b> (3.54-5.92)	<b>5.39</b> (3.92-7.00)	<b>6.44</b> (4.50-8.55)	<b>7.31</b> (4.94-9.72)
<b>24-hr</b>	<b>1.76</b> (1.48-2.05)	<b>2.09</b> (1.76-2.44)	<b>2.68</b> (2.25-3.13)	<b>3.22</b> (2.69-3.77)	<b>4.02</b> (3.28-4.93)	<b>4.70</b> (3.73-5.80)	<b>5.43</b> (4.15-6.83)	<b>6.22</b> (4.55-8.00)	<b>7.33</b> (5.15-9.64)	<b>8.23</b> (5.61-10.9)
<b>2-day</b>	<b>2.09</b> (1.77-2.41)	<b>2.44</b> (2.07-2.82)	<b>3.08</b> (2.60-3.56)	<b>3.65</b> (3.07-4.24)	<b>4.51</b> (3.69-5.47)	<b>5.23</b> (4.17-6.39)	<b>6.00</b> (4.61-7.48)	<b>6.82</b> (5.02-8.70)	<b>8.00</b> (5.65-10.4)	<b>8.94</b> (6.13-11.7)
<b>3-day</b>	<b>2.26</b> (1.92-2.59)	<b>2.65</b> (2.26-3.05)	<b>3.34</b> (2.83-3.85)	<b>3.95</b> (3.33-4.57)	<b>4.86</b> (3.99-5.85)	<b>5.61</b> (4.49-6.82)	<b>6.41</b> (4.94-7.95)	<b>7.26</b> (5.36-9.21)	<b>8.46</b> (6.00-11.0)	<b>9.42</b> (6.48-12.3)
<b>4-day</b>	<b>2.39</b> (2.05-2.74)	<b>2.81</b> (2.40-3.22)	<b>3.54</b> (3.01-4.06)	<b>4.18</b> (3.54-4.82)	<b>5.13</b> (4.22-6.14)	<b>5.91</b> (4.74-7.15)	<b>6.73</b> (5.20-8.31)	<b>7.61</b> (5.63-9.61)	<b>8.83</b> (6.28-11.4)	<b>9.81</b> (6.77-12.8)
<b>7-day</b>	<b>2.79</b> (2.40-3.17)	<b>3.23</b> (2.77-3.67)	<b>4.00</b> (3.42-4.56)	<b>4.68</b> (3.98-5.36)	<b>5.70</b> (4.71-6.77)	<b>6.53</b> (5.26-7.84)	<b>7.42</b> (5.76-9.10)	<b>8.36</b> (6.22-10.5)	<b>9.68</b> (6.92-12.5)	<b>10.7</b> (7.45-13.9)
<b>10-day</b>	<b>3.15</b> (2.72-3.56)	<b>3.62</b> (3.11-4.09)	<b>4.43</b> (3.80-5.02)	<b>5.15</b> (4.40-5.87)	<b>6.23</b> (5.17-7.37)	<b>7.11</b> (5.75-8.50)	<b>8.05</b> (6.28-9.83)	<b>9.05</b> (6.76-11.3)	<b>10.5</b> (7.50-13.4)	<b>11.6</b> (8.06-15.0)
<b>20-day</b>	<b>4.17</b> (3.62-4.67)	<b>4.77</b> (4.14-5.35)	<b>5.80</b> (5.01-6.52)	<b>6.69</b> (5.74-7.55)	<b>7.97</b> (6.63-9.30)	<b>8.99</b> (7.30-10.6)	<b>10.1</b> (7.88-12.1)	<b>11.2</b> (8.39-13.8)	<b>12.7</b> (9.17-16.1)	<b>13.9</b> (9.76-17.9)
<b>30-day</b>	<b>5.00</b> (4.35-5.57)	<b>5.73</b> (4.99-6.39)	<b>6.95</b> (6.03-7.77)	<b>7.98</b> (6.88-8.96)	<b>9.42</b> (7.85-10.9)	<b>10.5</b> (8.58-12.3)	<b>11.7</b> (9.18-14.0)	<b>12.9</b> (9.68-15.8)	<b>14.4</b> (10.4-18.2)	<b>15.7</b> (11.0-20.0)
<b>45-day</b>	<b>6.03</b> (5.28-6.68)	<b>6.92</b> (6.05-7.68)	<b>8.36</b> (7.28-9.30)	<b>9.55</b> (8.27-10.7)	<b>11.2</b> (9.31-12.8)	<b>12.4</b> (10.1-14.4)	<b>13.6</b> (10.7-16.2)	<b>14.8</b> (11.2-18.0)	<b>16.4</b> (11.9-20.5)	<b>17.6</b> (12.4-22.4)
<b>60-day</b>	<b>6.90</b> (6.06-7.62)	<b>7.92</b> (6.94-8.75)	<b>9.54</b> (8.33-10.6)	<b>10.8</b> (9.41-12.1)	<b>12.6</b> (10.5-14.3)	<b>13.9</b> (11.3-16.0)	<b>15.1</b> (11.9-17.8)	<b>16.3</b> (12.3-19.8)	<b>17.9</b> (13.0-22.2)	<b>19.0</b> (13.5-24.1)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

**PF graphical**

PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 39.1092°, Longitude: -104.8640°



[Back to Top](#)

**Maps & aeriels**

**Small scale terrain**

$V S^{0.17} / (S_s - 1)^{0.66} * (ft^{1/2}/sec)$	Rock Type***
1.4 to 3.2	VL
3.3 to 3.9	L
4.0 to 4.5	M
4.6 to 5.5	H
5.6 to 6.4	VH

\*where:

V = mean channel flow velocity, in fps;

S = longitudinal channel slope, in feet per foot (ft/ft); and

$S_s$  = specific gravity of stone (minimum  $S_s = 2.50$ )

\*\* Table valid only for Froude number of 0.8 or less and side slopes no steeper than 2h:1v.

\*\*\* Type VL and L riprap may be buried after placement to reduce vandalism.

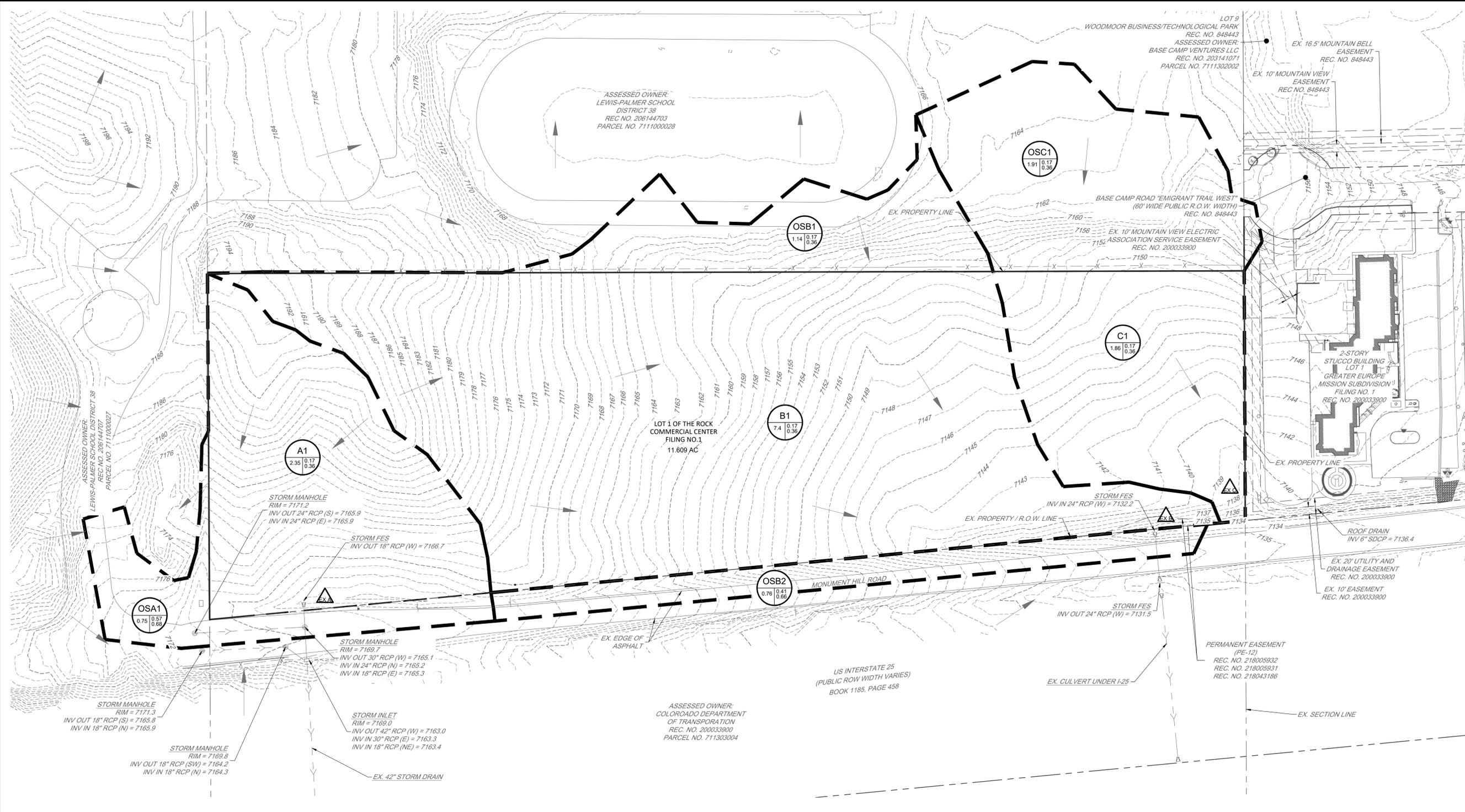
Channel Slope	Lining	Permissible Mean Channel Velocity* (ft/sec)	
0 - 5%	Sodded grass	7	
	Bermudagrass	6	
	Reed canarygrass	5	
	Tall fescue	5	
	Kentucky bluegrass	5	
	Grass-legume mixture	4	
	Red fescue	2.5	
	Redtop	2.5	
	Sericea lespedeza	2.5	
	Annual lespedeza	2.5	
	Small grains (temporary)	2.5	
	5 - 10%	Sodded grass	6
		Bermudagrass	5
Reed canarygrass		4	
Tall fescue		4	
Kentucky bluegrass		4	
Grass-legume mixture		3	
Greater than 10%		Sodded grass	5
	Bermudagrass	4	
	Reed canarygrass	3	
	Tall fescue	3	
	Kentucky bluegrass	3	

\*For highly erodible soils, decrease permissible velocities by 25%.

\*Grass lined channels are dependent upon assurances of continuous growth and maintenance of grass.

## Appendix E - Drainage Maps

I:\2023\23009 - The Rock Commerce Center\cadd\Sheet Sets\Drainage\The Rock\23009 - Existing Drainage Map.dwg tab: Proposed Drainage Map Nov 15, 2023 1:53pm esatz

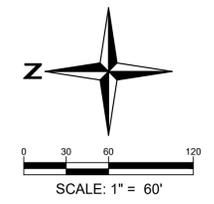


**DRAINAGE LEGEND**

- EXISTING MINOR CONTOUR
- EXISTING MAJOR CONTOUR
- EXISTING STORM SEWER LINE
- FEMA 100-YEAR FLOOD PLAIN
- FEMA ZONE X
- SUB-BASIN BOUNDARY
- MAJOR BASIN BOUNDARY
- PROPERTY LINE
- EXISTING BASIN ID
- EXISTING 10 YEAR RUNOFF COEFFICIENT
- EXISTING 100 YEAR RUNOFF COEFFICIENT
- BASIN AREA (ACRES)
- EXISTING GRADE FLOW ARROW
- EXISTING DESIGN POINT

BASIN PEAK FLOW SUMMARY		
BASIN	Q10	Q100
A1	1.5	4.6
OSA1	2.0	3.4
B1	3.7	11.4
OSB1	0.8	2.5
OSB2	1.5	2.6
C1	1.1	3.4
OSC1	1.0	3.0

DESIGN POINT FLOW SUMMARY		
DESIGN POINT	Q10	Q100
A	3.07	7.27
B	5.53	15.26
C	1.97	6.02



PCD FILE NO. PPR2329

**15 Redland**  
 YEARS WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND.CO.VA • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

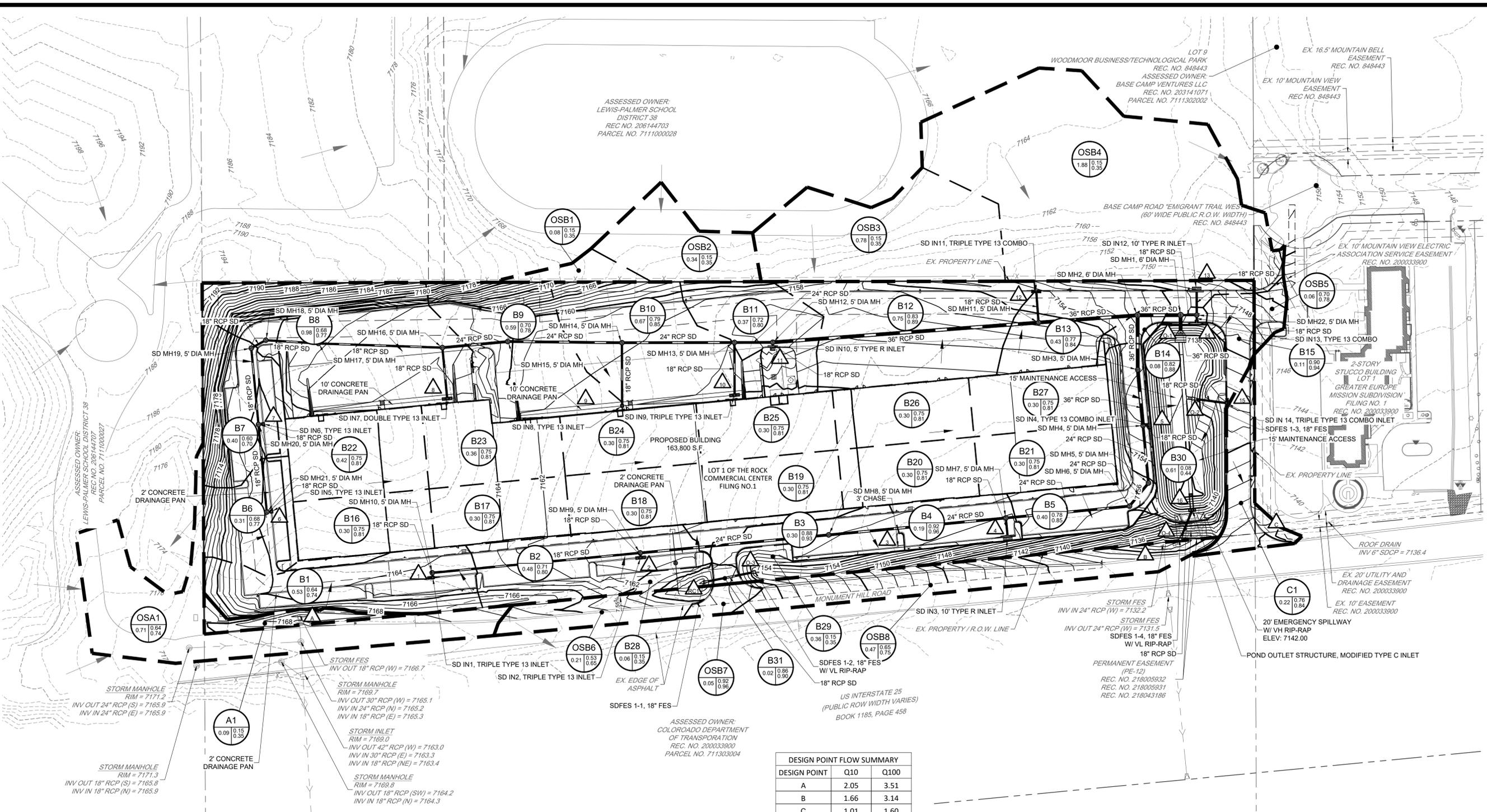
**NOT FOR CONSTRUCTION**

PROJECT NO.	DATE	NO.	NOTES
23009	07/28/23	1	1ST SUBMITTAL
	10/20/23	2	2ND SUBMITTAL
	11/17/23	3	3RD SUBMITTAL

LOT 1 OF THE ROCK COMMERCE CENTER FILING NO. 1  
**DRAINAGE MAPS**  
 EXISTING DRAINAGE MAP

SHEET  
**DNG-1**

I:\2023\23009 - The Rock Commerce Center\Sheet Sets\Drainage\The Rock\23009 - Proposed Drainage Map.dwg Lab: Proposed Drainage Map.dwg Nov 15, 2023 1:52pm csaiz



**DRAINAGE LEGEND**

- 5282--- EXISTING MINOR CONTOUR
  - 5280--- EXISTING MAJOR CONTOUR
  - 5281--- PROPOSED MINOR CONTOUR
  - 5280--- PROPOSED MAJOR CONTOUR
  - PHASE 2 CONSTRUCTION BOUNDARY
  - EXISTING STORM SEWER LINE
  - PROPOSED STORM SEWER LINE
  - PROPOSED MANHOLE
  - EXISTING INLET
  - PROPOSED INLET
  - PROPOSED FLARED END SECTION
  - SUB-BASIN BOUNDARY
  - MAJOR BASIN BOUNDARY
  - PROPERTY LINE
- 
- A1** --- BASIN ID
  - 0.000 0.00 0.00 --- 10 YEAR RUNOFF COEFFICIENT
  - 0.000 0.00 0.00 --- 100 YEAR RUNOFF COEFFICIENT
  - BASIN AREA (ACRES)
  - PROPOSED DESIGN POINT**
  - EX-1** --- EXISTING BASIN ID
  - 0.00 0.00 0.00 --- EXISTING 10 YEAR RUNOFF COEFFICIENT
  - 0.00 0.00 0.00 --- EXISTING 100 YEAR RUNOFF COEFFICIENT
  - BASIN AREA (ACRES)
  - EXISTING DESIGN POINT**
  - EXISTING GRADE FLOW ARROW
  - PROPOSED GRADE FLOW ARROW

**BASIN PEAK FLOW SUMMARY**

BASIN	Q10	Q100
B1	2.0	3.4
B2	2.0	3.2
B3	1.6	2.4
B4	1.0	1.5
B5	1.8	2.9
B6	1.2	2.0
B7	1.4	2.4
B8	3.9	6.4
B9	2.4	3.9
B10	3.1	4.9
B11	1.6	2.5
B12	3.6	5.6
B13	2.0	3.1
B14	0.4	0.6
B15	0.6	0.9
B16	1.3	2.1
B17	1.3	2.0
B18	1.3	2.1
B19	1.3	2.0
B20	1.3	2.1
B21	1.3	2.1

**BASIN PEAK FLOW SUMMARY**

BASIN	Q10	Q100
B22	1.8	2.9
B23	1.6	2.5
B24	1.3	2.0
B25	1.3	2.1
B26	1.3	2.1
B27	1.3	2.1
B28	0.0	0.1
B29	0.2	0.8
B30	0.3	1.9
B31	0.1	0.1
OSB1	0.1	0.2
OSB2	0.2	0.8
OSB3	0.6	1.9
OSB4	1.1	3.7
OSB5	0.2	0.4
OSB6	0.6	1.0
OSB7	0.3	0.4
OSB8	1.6	2.7
A1	0.1	0.2
OSA1	2.4	4.0
C1	1.0	1.6

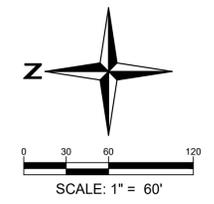
**DESIGN POINT FLOW SUMMARY**

DESIGN POINT	Q10	Q100
A	2.05	3.51
B	1.66	3.14
C	1.01	1.60
O-1	26.71	54.14
O-2	0.85	1.31
O-3	0.61	1.15
O-4	3.4	10.4
RC1	0.61	1.15
1	3.35	5.42
2	4.46	7.04
3	2.78	4.28
4	2.63	4.03
5	3.19	4.98
6	1.24	2.02
7	1.40	2.39
8	5.76	9.26
9	4.03	6.42
10	3.85	6.13
11	2.39	4.18
12	4.63	8.16
13	3.30	7.16
14	0.38	0.58
15	0.85	1.31
16	0.26	1.92

**FULL SPECTRUM POND SUMMARY**

ZONE	VOLUME (AC-FT)	WATER ELEV.
WQCV	0.294	7137.55
EURV	0.675	7140.11
100-YEAR	0.518	7141.64

PCD FILE NO. PPR2329



**15 Redland YEARS**  
 WHERE GREAT PLACES BEGIN  
 720.283.6793  
 REDLAND.CO.VA • Land Planning • Landscape Architecture • Civil Engineering • Construction Management

**NOT FOR CONSTRUCTION**

**NOTES**

NO.	DATE	NOTES
1	07/28/23	1ST SUBMITTAL
2	10/20/23	2ND SUBMITTAL
3	11/17/23	3RD SUBMITTAL

**LOT 1 OF THE ROCK COMMERCE CENTER FILING NO. 1**  
**DRAINAGE MAPS**  
 PROPOSED DRAINAGE MAP  
 SHEET  
**DNG-2**

# V3\_Drainage Report - Final.pdf Markup Summary

Christina Prete (6)



**Subject:** Stormwater Comments Color  
**Page Label:** 1  
**Author:** Christina Prete  
**Date:** 12/6/2023 5:24:54 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

User Input: Stage and Total An

change to 1.35

Stage of f  
Orific

**Subject:** Contractor  
**Page Label:** 55  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:42:42 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:** change to 1.35

Flow	Velocity	Depth	Area	Perimeter	Wetted Perimeter	Hydraulic Radius	Velocity	Discharge
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
2.00	2.00	2.00	4.00	4.00	2.00	2.00	4.00	
3.00	3.00	3.00	9.00	6.00	3.00	3.00	9.00	
4.00	4.00	4.00	16.00	8.00	4.00	4.00	16.00	

**Subject:** Highlight  
**Page Label:** 55  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:42:47 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:** 1.30 1.30 1.30 1.30

Overflow W  
Horiz. Length  
Overfl  
Deb

assume 50%

User Input: Outlet Pipe w/ Flow

Depth to Invert

**Subject:** Contractor  
**Page Label:** 55  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:45:15 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:** assume 50%

Type C Grate

0%

**Subject:** Highlight  
**Page Label:** 55  
**Author:** Christina Prete  
**Date:** 12/6/2023 4:45:11 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:** 0%

AND OUTLET PROTECTION

rip rap

**Subject:** Contractor  
**Page Label:** 115  
**Author:** Christina Prete  
**Date:** 12/6/2023 5:15:24 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:** i dont see riprap at DP-C on the Plans. Please confirm location