



505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

September 15, 2020

FLRD #5 2138 Flying Horse Club Drive Colorado Springs, Colorado 80921

Attn: Mark Sherwood

Re: Pavement Recommendations

Forest Lakes Filing No. 5 El Paso County, Colorado APPROVED
Engineering Department

09/22/2020 12:18:45 PM dsdnijkamp EPC Planning & Community Development Department

SF 1915

Dear Mr. Sherwood:

As requested, Entech Engineering, Inc. has obtained samples of the pavement subgrade soils from the roadways in the Forest Lakes, Filing No. 5 subdivision in El Paso County, Colorado. This letter presents the results of the laboratory testing and pavement recommendations for the roadways.

Project Description

The roadways for this project consist of sections of, Mesa Top Road and Forest Lakes Drive. A Subsurface Soil Investigation and laboratory testing was performed in order to determine the pavement support characteristics of the soils. The general layout of the site is presented in the Test Boring Location Map in Figure 1.

Subgrade Conditions

Sixteen test borings were drilled along the roadways to depths of approximately 5 and 10 feet below the existing subgrade surface. The soils at the roadway subgrade depth consisted of silty to clayey sand fill (Soil Type 1), native silty sand (Soil Type 1A), very silty sand fill (Soil Type 2). and native very silty to very clayey sand (Soil Type 2A). The Type 1 soils were encountered in all of the borings with the exception of Test Boring Nos. 11-14, and 16, in which Soil Types 1, 1A, and 2A were encountered at subgrade depth. The Type 3 soils were not encountered in the subgrade influence zone. Groundwater was not encountered in the test borings. The Test Boring Logs are presented in Appendix A. Sieve Analyses and Atterberg Limit testing were performed on soil samples obtained from the test borings for the purpose of classification. The Type 1 soils percent passing the No. 200 sieve ranged from approximately 23 to 34 percent and classified as A-2-4 and A-1-b soils, using the AASHTO classification system. The Type 1A, 2, and 2A soils percent passing the No. 200 sieve ranged from approximately 35 to 40 percent and classified as A-2-4 and A-4 soils, using the AASHTO classification system. One general subgrade soil type was determined for pavement evaluation based on the laboratory testing (Type 1). The Type 1A, 2, and 2A soils will be grouped with the Type 1 soils due the limited areas in which they were encountered and their similar characteristics. Water-soluble sulfate tests results indicated that the soils exhibit a negligible potential for sulfate attack.

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Swell/Consolidation Testing was not required on the site soils due to their plastic indexes. Mitigation of expansive soils on this site is not required. Laboratory test results are presented in Appendix B and are summarized on Table 1.

California Bearing Ratio (CBR) testing was performed on a representative sample to determine the support characteristics of the subgrade soils for the roadway section. The results of the CBR testing, are presented in Appendix B and summarized as follows:

Soil Type 1 – Silty Sand Fill CBR 1 R @ 90% = 12.0 R @ 95% = 71.0 Use R = 50.0 for design

Classification Testing	
Liquid Limit	NV
Plasticity Index	NP
Percent Passing 200	27.3
AASHTO Classification	A-2-4
Group Index	0
Unified Soils Classification	SM

Pavement Design

CBR testing was used to determine pavement sections for the roadways. Pavement sections were determined utilizing El Paso County Engineering Criteria Manual. The roadways classify as urban residential collectors, which used an 18k ESAL value of 821,000 for design purposes. Alternative pavement sections were determined for asphalt supported on aggregate basecourse, and asphalt on cement stabilized subgrade.

Design parameters used in the pavement analysis for the roadways are as follows:

Reliability	
Urban Residential Collector	85%
Standard Deviation	0.45
Δpsi	2.2
"R" Value Subgrade	50
Resilient Modulus	13,168 psi
Hot Bituminous Pavement	0.44
Aggregate Basecourse	0.11
Cement Stabilized Subgrade	0.12

The pavement design calculations are presented in Appendix C. Pavement section alternatives for the roadway sections are presented as follows. Any additional grading may result in subgrade soils with different support characteristics. The following pavement sections should be re-evaluated if additional grading is performed.

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Pavement Sections - Soil Type 1

<u>Ur</u> ban Reside	ential Collector	s - ESAL = 821,00	0
<u>Alternative</u>	Asphalt••	Basecourse	Cement Stabilized
	<u>(in)</u>	<u>(in)</u>	Subgrade (in.)
 Asphalt Over Basecourse 	4.0*	8.0*	••
2. Cement Stabilized Subgrade	4.0*		10.0

^{*}Minimum sections required per the El Paso County Engineering Criteria Manual.

Roadway Construction - Full Depth Asphalt and Asphalt on Aggregate Basecourse Alternatives

Prior to placement of the asphalt, the subgrade should be proofrolled and compacted to a minimum of 95 percent of the soils maximum Modified Proctor Dry Density, ASTM D-1557 at \pm 2 percent of optimum moisture content. Any loose or soft areas should be removed and replaced with suitable materials. Basecourse materials should be compacted to a minimum of 95 percent of its maximum Modified Proctor Dry Density, ASTM D-1557 at \pm 2 percent of optimum moisture content. Special attention should be given to areas adjacent to manholes, inlet structures and valves.

Roadway Construction - Cement Stabilized Subgrade Alternative

Prior to placement of the asphalt, the subgrade shall be stabilized by addition of cement to a depth of at least 10 inches. The amount of cement applied shall be 2.0 percent (by weight) of the subgrade's maximum dry density as determined by the Modified Proctor Test (ASTM D-1557) based on laboratory cement stabilization testing. The cement should be spread evenly on the subgrade surface and be thoroughly mixed into the subgrade over a 10 inches depth such that a uniform blend of soil and cement is achieved. Prior to application or mixing of the cement, the upper 10 inches of subgrade should be thoroughly moisture conditioned to the soil's optimum water content or as much as 2 percent more than the optimum water content as necessary to provide a compactable soil condition. Densification of the cement-stabilized subgrade should be completed to obtain a compaction of at least 95 percent of the subgrade maximum dry density as determined by the Modified Proctor Test (ASTM D-1557). Satisfactory compaction of the subgrade shall occur within 90 minutes from the time of mixing the cement into the subgrade.

The following conditions shall be observed as part of the subgrade stabilization:

- Type I/II cement as supplied, a local supplier shall be used. All cement used for stabilization should come from the same source. If cement sources are changed a new laboratory mix design should be completed.
- Moisture conditioning of the subgrade and/or mixing of the cement into the subgrade shall not occur when soil temperatures are below 40 °F. Cement treated subgrades should be maintained at a temperature of 40 °F or greater until the subgrade has been compacted as required.

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 Cement placement, cement mixing and compaction of the cement treated subgrade should be observed by a Soils Engineer. The Soils Engineer should complete in situ compaction tests and construct representative compacted specimens of the treated subgrade material for subsequent laboratory quality assurance testing.

If significant grading is performed, the soils at subgrade may change. Modification to the pavement sections should be evaluated after site grading is completed.

In addition to the above guidance, the asphalt, cement, subgrade conditions, compaction of materials and roadway construction methods shall meet the El Paso County specifications.

We trust that this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Daniel P. Stegman

DPS/bs

Entech Job No. 201782 AAprojects/2020/201782 - pr Reviewed by:

Mark H. Hauschild, P.E. Senior Engineer

TABLE

TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

FLRD #2 FOREST LAKES, FILING 5 201782 CLIENT PROJECT JOB NO.

	SOIL DESCRIPTION	FILL, SAND, SILTY	FILL, SAND, CLAYEY	FILL, SAND, SILTY	FILL, SAND, CLAYEY	FILL, SAND, SILTY	FILL, SAND, SILTY	FILL, SAND, SILTY	SAND, SILTY	FILL, SAND, VERY SILTY	FILL, SAND, VERY SILTY	SAND, VERY SILTY	SAND, VERY CLAYEY	SANDSTONE, SILTY					
	UNIFIED	SM	SC	SM	SM	WS	SM	SM	SM	SC	SM	SM	SM	SM	SM	SM	SM	SC	SM
, i Live	SWELL/ CONSOL (%)																		
	AASHTO CLASS.	A-2-4	A-2-4	A-1-b	A-2-4	A-2-4	A-2-4	A-2-4	A-1-b	A-2-4	A-2-4	A-2-4	A-1-b	A-2-4	A-4	A-4	A-4	A-4	A-2-4
	SULFATE (WT %)			<0.01			<0.01			<0.01				<0.01		0.03			
C A	INDEX (%)	ď	10	NP	NP	NP	NP	NP	NP	8	NP	NP	NP	NP	NP	NP	ЧN	6	NP
2	LIMIT (%)	N N	28	NV	N	NV		N<	N<	26		N	NV	NN	NV	N	N<	24	N/
040	NO. 200 SIEVE (%)	27.3	26.0	25.1	29.4	33.7	31.5	29.5	24.0	29.2	32.3	30.6	22.9	34.8	40.4	39.4	38.0	39.9	27.5
2	DENSITY (PCF)																		
	WATER (%)																		
	DEPTH (FT)	0-3	1-2	1-2	1-2	1.2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	10
FOUL	BORING NO.	7	1	2	3	4	2	9	7	8	6	10	15	11	13	14	12	16	0
	SOIL	1, CBR	1	-	-	-	-	-	-	-	-	-	-	1A	2	2	2A	2A	3

FIGURE



TEST BORING LOCATION MAP FOREST LAKES FILING #5 EL PASO COUNTY, CO FOR: FLRD #5





APPENDIX A: Test Boring Logs

TEST BORING NO. TEST BORING NO. DATE DRILLED 8/26/2020 DATE DRILLED 8/26/2020 Job# 201782 **CLIENT** FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Soil Type Depth (ft) Soil Type Samples Samples Symbol Symbol DRY TO 10', 8/26/20 DRY TO 5', 8/26/20 FILL O-10', SAND, CLAYEY TO FILL O-5', SAND, SILTY, FINE TO SILTY, FINE TO COARSE GRAINED. 24 7.7 COARSE GRAINED, RED BROWN, 17 6.4 1 RED BROWN, MEDIUM DENSE, MEDIUM DENSE TO LOOSE, MOIST MOIST 5 7 15 4.5 1 9 1 6.4 10 41.1 32 4.9 1 10 15 20



	Ti	EST BORING L	OG
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JOB NO.: 201782 FIG NO.: A- 1

TEST BORING NO. 3 TEST BORING NO. DATE DRILLED 8/26/2020 DATE DRILLED 8/26/2020 Job# 201782 **CLIENT** FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Watercontent % Blows per foot foot Watercontent Soil Type Blows per Depth (ft) Soil Type Samples Depth (ft) Samples Symbol Symbol DRY TO 5', 8/26/20 DRY TO 10', 8/26/20 FILL O-5', SAND, SILTY, FINE TO FILL 0-10', SAND, SILTY, FINE TO COARSE GRAINED, RED BROWN, 15 4.6 COARSE GRAINED, RED BROWN, 13 9.7 1 MEDIUM DENSE, MOIST MEDIUM DENSE TO LOOSE, MOIST 5 20 6.0 1 14 7.6 1 10 10 9 7.7 1 15 15 20 20



	TEST BORING LOG			
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JOB NO.: 201782 FIG NO.: A- 2

TEST BORING NO. TEST BORING NO. DATE DRILLED 8/26/2020 DATE DRILLED 8/26/2020 Job# 201782 CLIENT FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Blows per foot Watercontent Blows per foot Watercontent Depth (ft) Samples Samples Symbol Symbol DRY TO 5', 8/26/20 DRY TO 5', 8/26/20 FILL 0-5', SAND, SILTY, FINE TO FILL O-5', SAND, SILTY, FINE TO COARSE GRAINED, RED BROWN, 10 5.6 COARSE GRAINED, RED BROWN, 9 5.6 1 MEDIUM DENSE, MOIST LOOSE, MOIST 5 111 10 4.8 1 5 4.8 1 10 15 15 20 20



	TES	T BORING LOG	
DRAWN	DATE:	CHECKED	9/11/20

201782 FIG NO. A- 3

TEST BORING NO. 7 TEST BORING NO. DATE DRILLED 8/26/2020 DATE DRILLED 8/27/2020 Job# 201782 CLIENT FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Soil Type Depth (ft) Soil Type Depth (ft) Samples Symbol Symbol DRY TO 10', 8/26/20 DRY TO 5', 8/27/20 FILL 0-6', SAND, SILTY, FINE TO FILL O-5', SAND, CLAYEY, FINE 33 COARSE GRAINED, RED BROWN, 4.2 TO COARSE GRAINED, BROWN, 25 7.8 1 DENSE TO MEDIUM DENSE. MEDIUM DENSE, MOIST MOIST 5 28 4.8 1 21 8.0 1 SAND, SILTY, FINE TO COARSE GRAINED, BROWN, MEDIUM DENSE, MOIST 10 28 3.5 1A 10 15 15 20 20



	•	TEST BORING LOG
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JOB NO.: 201782 FIG NO.: A- 4

TEST BORING NO. 9 TEST BORING NO. 10 DATE DRILLED 8/27/2020 DATE DRILLED 8/27/2020 Job# 201782 CLIENT FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Blows per foot Watercontent Blows per foot Watercontent Soil Type Depth (ft) Soil Type Samples Depth (ft) Samples Symbol Symbol DRY TO 5', 8/27/20 DRY TO 10', 8/27/20 POSS. FILL O-5', SAND, SILTY, P055. FILL 0-4', SAND, SILTY. FINE TO COARSE GRAINED, 7.9 23 1 FINE TO COARSE GRAINED. 19 8.4 1 BROWN, MEDIUM DENSE, MOIST TAN, MEDIUM DENSE, MOIST 5 21 8.6 SAND, SILTY, FINE TO COARSE 17 7.2 1A GRAINED, RED BROWN, MEDIUM DENSE, MOIST SANDSTONE, SILTY, FINE TO 10 COARSE GRAINED, RED BROWN, 10 <u>50</u> 4.5 3 VERY DENSE, MOIST 4" 15 15 20 20



	TEST	FBORING LOC	9
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JOB NO.: 201782 FIG NO.: A- 5

TEST BORING NO. 11 TEST BORING NO. 12 DATE DRILLED 8/27/2020 DATE DRILLED 8/27/2020 Job# 201782 CLIENT FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Watercontent Blows per foot Watercontent Blows per Samples Depth (ft) Samples Depth (ft) Symbol Symbol DRY TO 5', 8/27/20 DRY TO 5', 8/27/20 SAND, SILTY, FINE TO COARSE SAND, VERY SILTY, FINE TO GRAINED, BROWN, MEDIUM 16 8.5 1A COARSE GRAINED, BROWN, 21 7.6 2A DENSE TO DENSE, MOIST MEDIUM DENSE, MOIST WEATHERED SANDSTONE, SILTY, 5 3 40 6.4 20 7.4 2A FINE TO COARSE GRAINED, RED BROWN, DENSE, MOIST 10 10 15 15 20 20



	TEST	FBORING LOG	à
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JOB NO. 201782 FIG NO. A- 6

TEST BORING NO. 13 TEST BORING NO. 14 DATE DRILLED 8/27/2020 DATE DRILLED 8/27/2020 Job# 201782 CLIENT FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Watercontent % Blows per foot foot Watercontent Blows per Depth (ft) Samples Soil Type Depth (ft) Samples Symbol Symbol Soil DRY TO 10', 8/27/20 DRY TO 5', 8/27/20 FILL 0-10, SAND, VERY SILTY, FILL O-5', SAND, VERY SILTY, FINE TO COARSE GRAINED. 28 7.4 2 FINE TO COARSE GRAINED, RED 2 37 5.9 BROWN TO RED BROWN, MEDIUM BROWN, MEDIUM DENSE TO DENSE TO DENSE, MOIST DENSE, MOIST 34 5.8 2 26 4.5 2 10 24 4.8 2 10 15 15 20 20



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201782 FIG NO.: A- 7

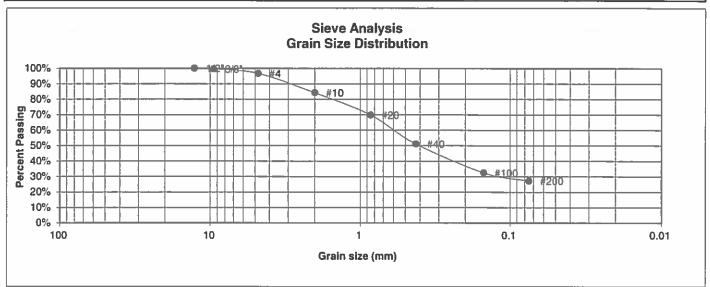
TEST BORING NO. 15 TEST BORING NO. 16 DATE DRILLED 8/27/2020 DATE DRILLED 8/27/2020 Job# 201782 CLIENT FLRD #2 LOCATION FOREST LAKES, FILING 5 REMARKS REMARKS Blows per foot Watercontent Natercontent Blows per Depth (ft) Soil Type Samples Depth (ft) Samples Symbol Symbol Soil. DRY TO 5', 8/27/20 DRY TO 10', 8/27/20 FILL 0-5', SAND, SILTY WITH SAND, VERY CLAYEY, FINE 36 5.5 ORGANICS, FINE TO COARSE 1 GRAINED, RED BROWN, DENSE, 39 5.7 2A GRAINED, DARK BROWN, DENSE MOIST TO MEDIUM DENSE, MOIST 5 27 7.3 1 39 4.3 2A 10 10 31 5.8 2A 15 15 20 20



,	TES	ST BORING LOG	
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JOB NO.: 201782 FIG NO.: A- 8 **APPENDIX B: Laboratory Test Results**

UNIFIED CLASSIFICATION CLIENT SM FLRD #2 1, CBR SOIL TYPE # **PROJECT** FOREST LAKES, FILING 5 TEST BORING # 7 JOB NO. 201782 DEPTH (FT) 0-3 **TEST BY** BL **GROUP INDEX 0** AASHTO CLASSIFICATION A-2-4



U.S. Sieve # 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
1/2"	100.0%	
3/8"	99.6%	
4	96.7%	<u>Swell</u>
10	84.2%	Moisture at start
20	69.8%	Moisture at finish
40	51.1%	Moisture increase
100	32.4%	Initial dry density (pcf)
200	27.3%	Swell (psf)

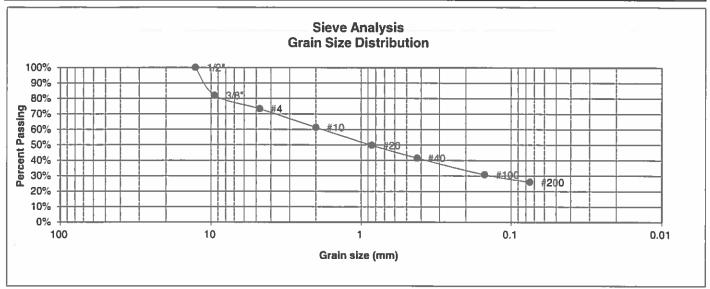


	LABORATORY TEST RESULTS DATE: CHECKED:			
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JOB NO.: 201782 FIG NO.:

BY

UNIFIED CLASSIFICATION SC CLIENT FLRD #2 SOIL TYPE # **PROJECT** 1 FOREST LAKES, FILING 5 **TEST BORING #** JOB NO. 1 201782 DEPTH (FT) 1-2 **TEST BY** BL**AASHTO CLASSIFICATION** A-2-4 **GROUP INDEX** 0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 17 Liquid Limit 28 Plastic Index 10
1/2" 3/8" 4 10	100.0% 82.0% 73.3% 61.3%	Swell Moisture at start
20 40 100 200	49.8% 41.5% 30.8% 26.0%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)

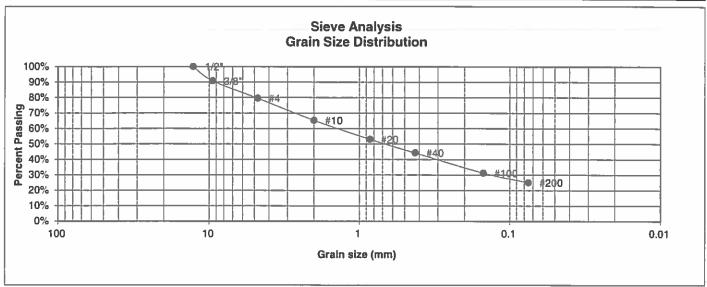


	LABORATORY TEST RESULTS DATE: CHECKED: DATE: 9/11/20			
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FIG NO

UNIFIED CLASSIFICATION SM CLIENT FLRD #2 **SOIL TYPE # PROJECT** 1 FOREST LAKES, FILING 5 **TEST BORING #** 2 JOB NO. 201782 DEPTH (FT) 1-2 **TEST BY** BLAASHTO CLASSIFICATION A-1-b **GROUP INDEX 0**



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 90.7%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	79.6% 65.3%	<u>Swell</u> Moisture at start
20	53.1%	Moisture at finish
40	44.3%	Moisture increase
100	31.2%	Initial dry density (pcf)
200	25.1%	Swell (psf)

DRAWN:



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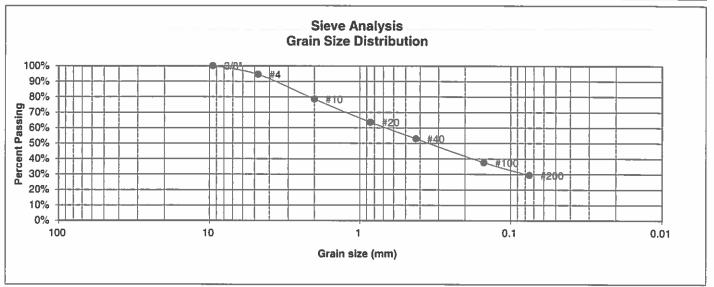
JOB NO.

201782

FIG NO

Bろ

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	1	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	3	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3* 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	94.5% 78.6%	<u>Swell</u> Moisture at start
20 40	63.6% 52.9%	Moisture at start Moisture at finish Moisture increase
100 200	37.6% 29.4%	Initial dry density (pcf) Swell (psf)

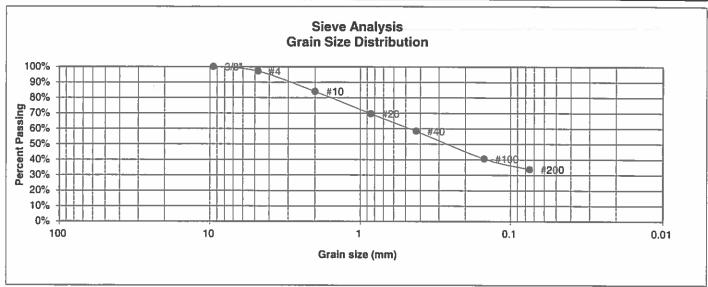


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JOB NO:

FIG NO.

UNIFIED CLASSIFICATION SM CLIENT FLRD #2 SOIL TYPE # **PROJECT** 1 FOREST LAKES, FILING 5 TEST BORING # JOB NO. 4 201782 DEPTH (FT) 1-2 **TEST BY** BLAASHTO CLASSIFICATION A-2-4 **GROUP INDEX 0**



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	97.2%	<u>Swell</u>
10	84.0%	Moisture at start
20	69.6%	Moisture at finish
40	58.3%	Moisture increase
100 200	40.5% 33.7%	Initial dry density (pcf) Swell (psf)

DRAWN:

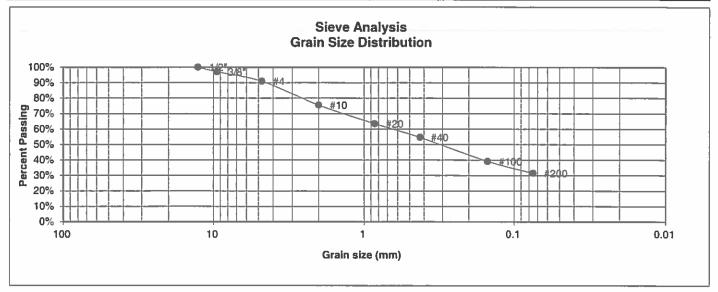


LABORATORY TEST RESULTS			
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JOB NO.:

FIGNO:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	1	<u>PROJECT</u>	FOREST LAKES, FILING 5
TEST BORING #	5	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0% 97.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP	
4	91.0% 75.5%	<u>Swell</u> Moisture at start	
20	63.5%	Moisture at finish	
40	54.6%	Moisture increase	
100	39.1%	Initial dry density (pcf	
200	31.5%	Swell (psf)	

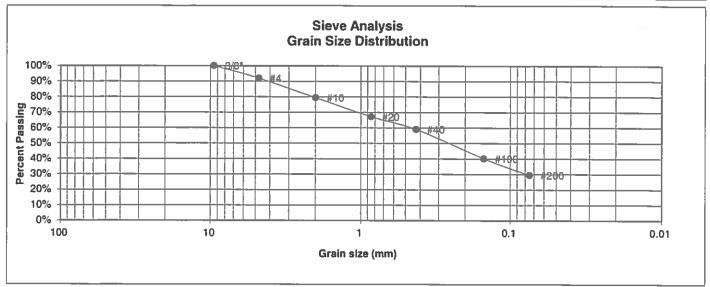


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JOB NO.:

FIG NO:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	1	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	6	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4_	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	92.0%	Swell
10	79.4%	Moisture at start
20 40	67.1% 59.1%	Moisture at finish Moisture increase
100 200	40.2% 29.5%	Initial dry density (pcf) Swell (psf)

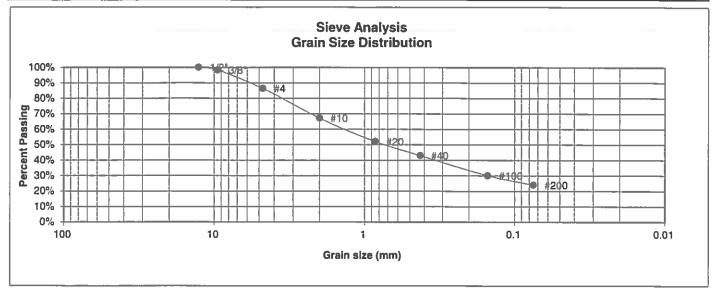


LABOR RESUI	RATORY TI LTS	EST		
DATE:	CHECKED:	a	PATE:	

JOB NO.: 201782 FIG NO.:

B-7

UNIFIED CLASSIFICATION SM CLIENT FLRD #2 SOIL TYPE # 1 **PROJECT** FOREST LAKES, FILING 5 **TEST BORING #** 7 JOB NO. 201782 DEPTH (FT) 1-2 **TEST BY** BLAASHTO CLASSIFICATION A-1-b **GROUP INDEX 0**



U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	98.3%	
4	86.5%	<u>Swell</u>
10	67.2%	Moisture at start
20	52.1%	Moisture at finish
40	43.0%	Moisture increase
100 200	30.1% 24.0%	Initial dry density (pcf) Swell (psf)

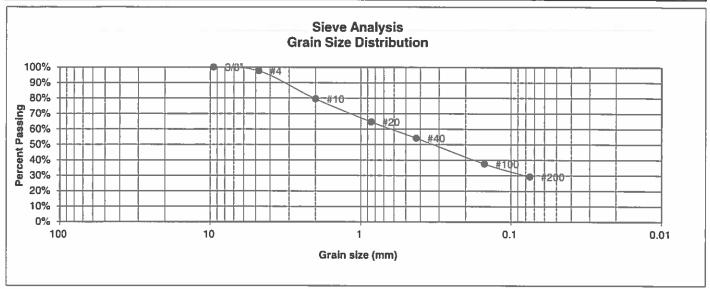


	LABOF RESUL	RATORY TE LTS	EST	
DRAWN:	DATE	CHECKED:	h	DATE: 9/11/20
			· · · · · · · · · · · · · · · · · · ·	

JOB NO. 201782

FIG NO.

UNIFIED CLASSIFICATION SC CLIENT FLRD #2 SOIL TYPE # **PROJECT** 1 FOREST LAKES, FILING 5 TEST BORING # 8 JOB NO. 201782 DEPTH (FT) 1-2 **TEST BY** BLAASHTO CLASSIFICATION A-2-4 **GROUP INDEX** 0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 18 Liquid Limit 26 Plastic Index 8
4	97.6%	Swell
10	79.5%	Moisture at start
20 40	64.6% 54.2%	Moisture at finish
		Moisture increase
100 200	37.5% 29.2%	Initial dry density (pcf) Swell (psf)

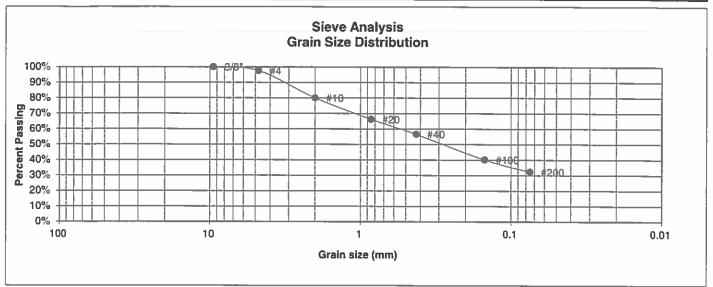


	LABOF RESUL	RATORY T .TS	EST	
DRAWN:	DATE	CHECKED:	2	9/11/20

JOB NO.:

201782 FIG NO.:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	1	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	9	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



U.S. Sieve # 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	97.5%	Swell
10	80.0%	Moisture at start
20	66.2%	Moisture at finish
40	56.6%	Moisture increase
100 200	40.1% 32.3%	Initial dry density (pcf) Swell (psf)

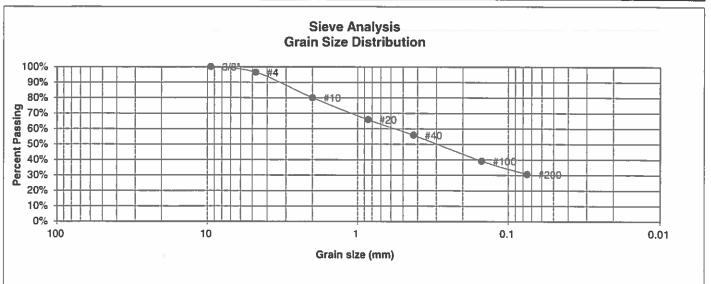


	RESUL	TS	= S1
DRAWN:	DATE	CHECKED:	h 9/1/20

JOB NO.: 201782

FIG NO.:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	I	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	10	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	96.5%	<u>Swell</u>
10	80.0%	Moisture at start
20	65.8%	Moisture at finish
40	55.9%	Moisture increase
100	39.1%	Initial dry density (pcf)
200	30.6%	Swell (psf)

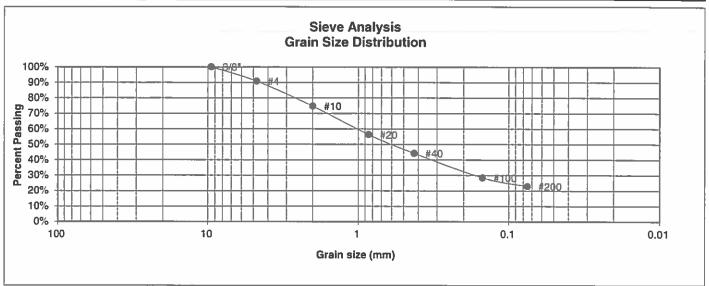


LABORATORY TEST RESULTS				
	DATE	CHECKED:	4	BATE/20

JOB NO

201782 FIG NO:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	1	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	15	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-1-b	GROUP INDEX	0



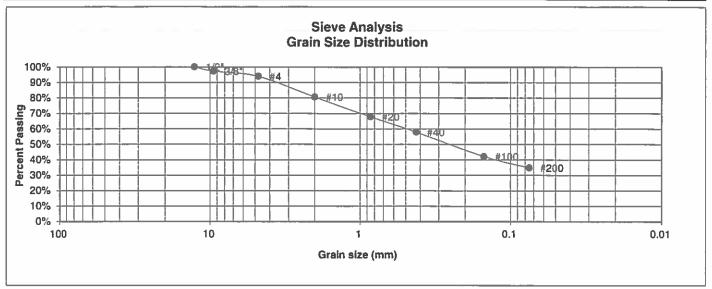
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	90.8%	Swell
10	74.7%	Moisture at start
20	56.3%	Moisture at finish
40	44.2%	Moisture increase
100 200	28.4% 22.9%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS				
·	DATE	CHECKED:	h	Alir/20

JOB NO: 201782 FIG NO:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	1A	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	11	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



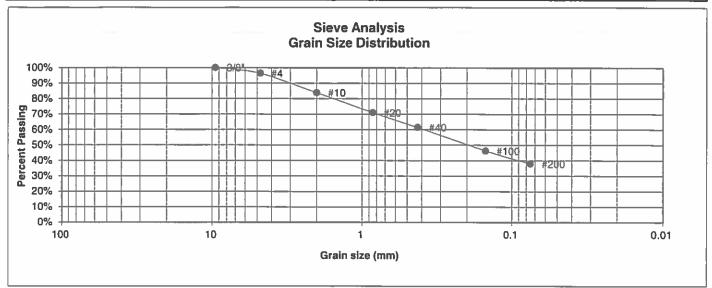
U.S. Sieve # 3" 1 1/2" 3/4"	Percent Finer	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
1/2" 3/8" 4 10	100.0% 97.3% 93.9% 80.6%	<u>Swell</u> Moisture at start
20 40 100 200	67.8% 57.9% 42.1% 34.8%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS				
	DATE	CHECKED:	h	DATE: 9/11/20

JOB NO.: 201782 FIG NO.;

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	2A	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	12	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	96.4%	<u>Swell</u>
10	83.8%	Moisture at start
20	71.0%	Moisture at finish
40	61.4%	Moisture increase
100	46.3%	Initial dry density (pcf)
200	38.0%	Swell (psf)

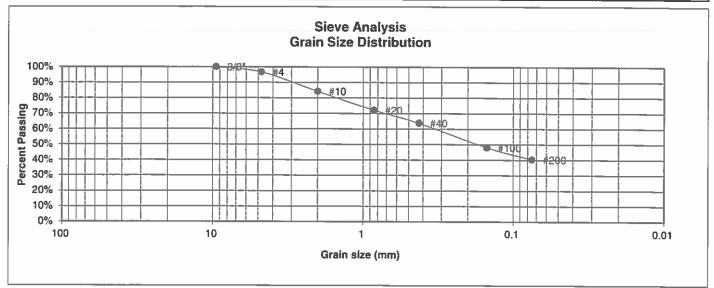


LABORATORY TEST RESULTS			
DATE:	CHECKED	h	9/11/Zo

JOB NO.: 201782 FIG NO.:

B-14

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	2	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	13	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u> 100.0%	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP		
4	96.7%	<u>Swell</u>		
10	84.2%	Moisture at start		
20	72.1%	Moisture at finish		
40	63.8%	Moisture increase		
100	48.1%	Initial dry density (pcf)		
200	40.4%	Swell (psf)		

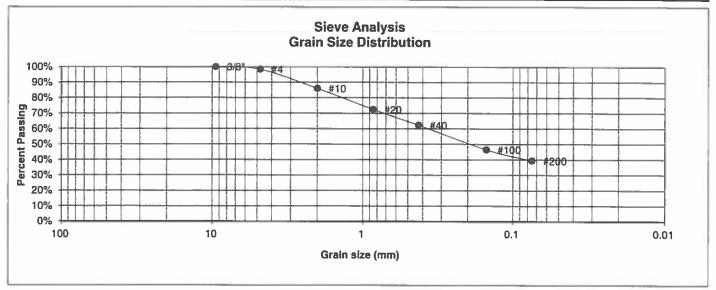


LABOR RESUL	ATORY TEST TS	
DATE	CHECKED: DATE:	

JOB NO: 201782 FIG NO:

B-15

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	2	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	14	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-4	GROUP INDEX	0



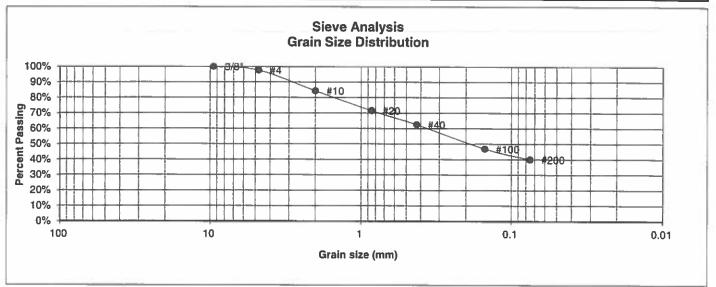
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP		
3/8"	100.0%			
4	98.3%	<u>Swell</u>		
10	86.0%	Moisture at start		
20	72.4%	Moisture at finish		
40	62.3%	Moisture increase		
100	46.4%	Initial dry density (pcf)		
200	39.4%	Swell (psf)		



LABORATORY TEST RESULTS					
DRAWN	DATE	CHECKED:	h	PATE Zo	_

JOB NO.:
201782
FIG NO.:
B1C

UNIFIED CLASSIFICATION	SC	CLIENT	FLRD #2
SOIL TYPE #	2A	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	16	JOB NO.	201782
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 15 Liquid Limit 24 Plastic Index 9
3/8"	100.0%	
4	97.6%	<u>Swell</u>
10	84.3%	Moisture at start
20	71.5%	Moisture at finish
40	62.4%	Moisture increase
100	46.8%	Initial dry density (pcf)
200	39.9%	Swell (psf)

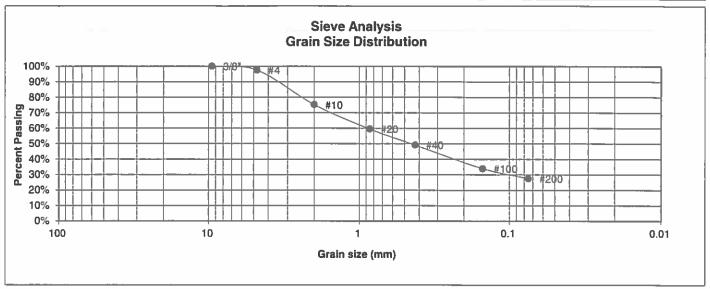


LABOF RESUI	RATORY TI LTS	EST	
DATE	CHECKED	h	DATE:

JOB NO.:

FIGNO:

UNIFIED CLASSIFICATION	SM	CLIENT	FLRD #2
SOIL TYPE #	3	PROJECT	FOREST LAKES, FILING 5
TEST BORING #	10	JOB NO.	201782
DEPTH (FT)	10	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	97.6%	Swell
10	75.2%	Moisture at start
20 40	59.5% 49.2%	Moisture at finish Moisture increase
100 200	33.9% 27.5%	Initial dry density (pcf) Swell (psf)



LABOF RESUI	RATORY TE LTS	EST	
DATE	CHECKED:	2	9/11/20

FIG NO.:

8-18

 CLIENT
 FLRD #2
 JOB NO.
 201782

 PROJECT
 FOREST LAKES, FILING 5
 DATE
 9/3/2020

 LOCATION
 FOREST LAKES, FILING 5
 TEST BY
 BL

BORING NUMBER	DEPTH, (ft)	SOIL TYPE NUMBER	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (wt%)
TB-2	1-2	1	SM	<0.01
TB-5	1-2	1	SM	<0.01
TB-8	1-2	1	sc	<0.01
TB-11	1-2	1A	SM	<0.01
TB-14	1-2	2	SM	0.03

DRAWN:

QC BLANK PASS



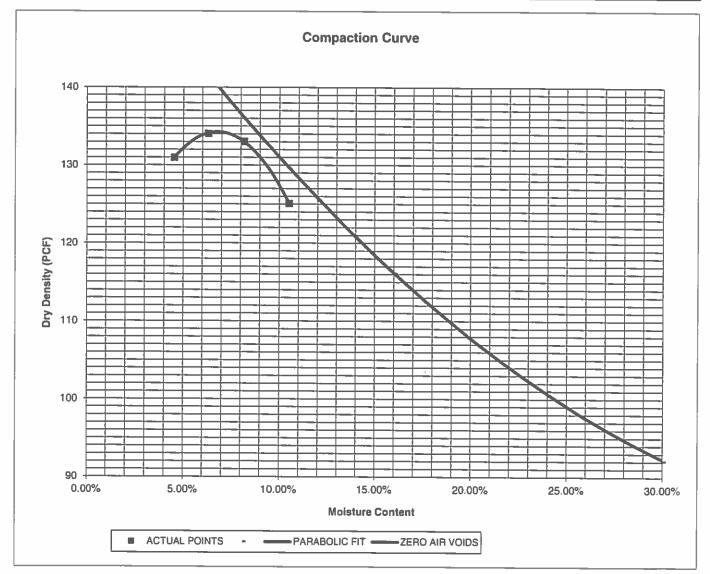
LABORATORY TEST SULFATE RESULTS					
DATE	CHECKED	9/11/20			

JOB NO.: 201782 FIG NO.:
 PROJECT
 FOREST LAKES, FILING 5
 CLIENT
 FLRD #2

 SAMPLE LOCATION
 TB-7 @ 0-3'
 JOB NO.
 201782

 SOIL DESCRIPTION
 SAND, SILTY, RED BROWN
 DATE
 08/27/20

| IDENTIFICATION | SM | COMPACTION TEST # 1 |
| TEST DESIGNATION / METHOD | ASTM D-1557-A | TEST BY | BL |
| MAXIMUM DRY DENSITY (PCF) | 134.2 | OPTIMUM MOISTURE | 6.8%







DRAWN: DATE: CHECKED: QUIL 20

JOB NO.:

201782 FIG NO.:

B-20

CBR TEST LOAD DATA

JOB NO:

201782

PISTON DIAMETER (cm) 4.958

PISTON AREA (in²) 2.993

CLIENT: FLRD #2 PROJECT: FOREST LAKES, FILING 5

SOIL TYPE: 1

		_				
	10 BLOWS		25 BLOWS		56 BLOWS	
PENETRATION	MOLD #	1	MOLD #	6	MOLD #	13
DEPTH	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS
(INCHES)	(LBS)	(PSI)	(LBS)	(PSI)	(LBS)	(PSI)
0.000	0	0.00	0	0.00	0	0.00
0.025	62	20.72	153	51.13	194	64.83
0.050	112	37.43	349	116.62	681	227.57
0.075	184	61.49	435	145.36	1072	358.23
0.100	265	88.55	563	188.14	1512	505.26
0.125	337	112.61	665	222.22	1910	638.26
0.150	389	129.99	736	245.95	2295	766.91
0.175	456	152.38	817	273.02	2777	927.98
0.200	515	172.10	970	324.14	3124	1043.94
0.300	599	200.17	1337	446.78	4500	1503.75
0.400	679	226.90	1661	555.05	5545	1852.96
0.500	824	275.35	2051	685.38	6000	2005.01

FINAL MOISTURE CONTENT

	MOLD #	1	MOLD #	6	MOLD #	13
CAN #		303		345		341
WT. CAN		7.89		8.4	j	8.34
WT. CAN+WET		211.21		232.12		183.39
WT. CAN+DRY		189.36		205.85		166.13
<u>WT. H20</u>		21.85		26.27		17.26
WT. DRY SOIL		181.47		197.45		157.79
MOISTURE CONTENT		12.04%		13.30%		10.94%

WET DENSITY (PCF) DRY DENSITY (PCF)	130.7	135.5	141.4
	122.4	126.9	132.4
BEARING RATIO	8.86	18.81	50.53

90% OF DRY DENSITY

120.8

95% OF DRY DENSITY 127.5

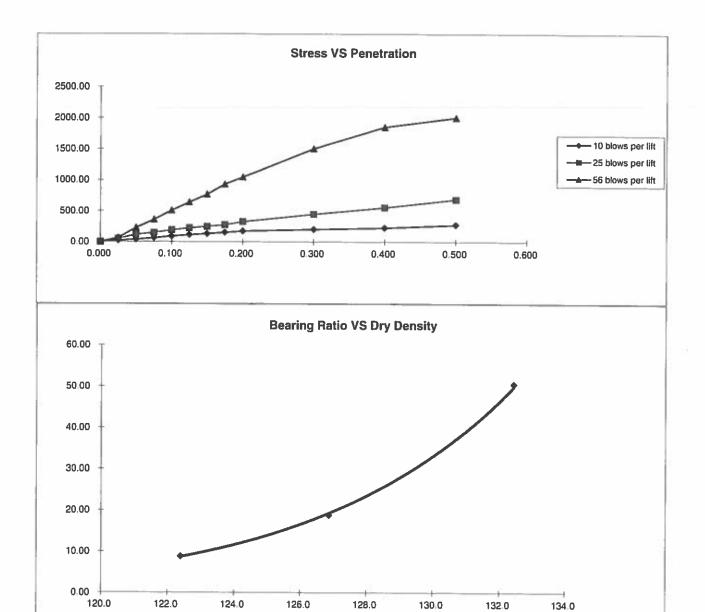
BEARING RATIO AT 90% OF MAX	5.27 ~ R VALUE	12
BEARING RATIO AT 95% OF MAX	22.30 ~ R VALUE	71



	CBR TEST DATA				
DRAWN	DATE:	CHECKED:	9/11/2		

JOB NO. 201782

FIG NO Bal



 BEARING RATIO AT 90% OF MAX
 5.27 ~ R VALUE
 12.00

 BEARING RATIO AT 95% OF MAX
 22.30 ~ R VALUE
 71.00

JOB NO: 201782 SOIL TYPE: 1



	CALIFORNIA BEARING RATIO					
DRAWN:	DATE	CHECKED:	9/11/20			

JOB NO.: 201782

APPENDIX C: Pavement Design Calculations

FLEXIBLE PAVEMENT DESIGN

DESIGN DATA

FLRD#5 - FOREST LAKES FILING NO.5 URBAN RESIDENTIAL COLLECTOR ROADS - SOIL TYPE 1

Equivalent (18 kip) Single Axle Load Applications (ESAL): $ESAL(W_{18}) =$ 821,000 Hveem Stabilometer (R Value) Results: 50 R =Standard Deviation $S_o =$ 0.45 Loss in Serviceability $\Delta psi =$ 2.2 Reliability Reliability = 85 Reliability (z-statistic) -1.036 $Z_R =$ Soil Resilient Modulus $M_R =$ 13168

Weighted Structural Number (WSN):

WSN =

2.54

DESIGN TABLES AND EQUATIONS

$$S_1 = [(R - 5) / 11.29] + 3$$

 $M_R = 10^{[(S_1 + 1872)/624]}$

 $k = M_R/19.4$

Where:

M_R = resilient modulus (psi)

 S_1 = the soil support value

R = R-value obtained from the Hveem stabilometer

CBR = California Bearing Ratio

Reliability (%)	Z _R (z-statistic)
60	-0.253

60	-0.253
70	-0.524
75	-0.674
80	-0.841
85	-1.036
90	-1.282
95	-1.65
97	-1.88
98	-2.05
99	-2.33
99.9	-3.09
99.99	-3.75

$$\log_{10}W_{18} = Z_{R}^{*} S_{O}^{+} 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\frac{\Delta PSI}{4.2 - 1.5}\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R}^{-} 8.07$$

Left Right		Difference	
5.91	5.91	0.0	

Job No. 201782 Fig. No. C-. I

DESIGN CALCULATIONS

<u>DESIGN DATA</u> CLASSIC COMMUNITIES - MIDTOWN AT HANNAH RIDGE, F1 URBAN RESIDENTIAL COLLECTOR ROADS - SOIL TYPE 1

Equivalent (18 kip) Single Axle Load Applications (ESAL):

ESAL = 821,000

Hveem Stabilometer (R Value) Results:

R = 50

Weighted Structural Number (WSN):

WSN = 2.54

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

C₁ = 0.44 Strength Coefficient - Hot Bituminous Asphalt

C₂ = 0.11 Strength Coefficient - Aggregate Base Course

 $D_1 = Depth of Asphalt (inches)$

 D_2 = Depth of Base Course (inches)

FOR FULL DEPTH ASPHALT SECTION

 $D_1 = (WSN)/C_1 = 5.8$ inches of Full Depth Asphalt

Use 6.0 inches Full Depth

FOR ASPHALT + AGGREGATE BASE COURSE SECTION

Asphalt Thickness (t) = 4 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 7.1$ inches of Aggregate

Base Course, use 8.0 inches

RECOMMENDED ALTERNATIVES

1. 4.0 inches of Asphalt +

8.0 inches of Aggregate Base Course, or

2. 6.0 inches of Asphalt

Job No. 201782 Fig. No. C- **2**

DESIGN CALCULATIONS

CEMENT TREATED SECTIONS

DESIGN DATA: FLRD#5 - FOREST LAKES FILING NO. 5

URBAN RESIDENTIAL COLLECTOR ROADS - SOIL TYPE 1

ALL ROADWAYS

Equivalent (18 kip) Single Axle Load Applications (ESAL):

ESAL = 821,000

Hveem Stabilometer (R Value) Results:

50 R =

Weighted Structural Number (WSN):

WSN = 2.54

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

C₁ = 0.44 Strength Coefficient - Hot Bituminous Asphalt

 $C_2 = 0.12$ Strength Coefficient - Cement Treated Subgrade.

 $D_1 = Depth of Asphalt (inches)$

 D_2 = Depth of Cement Treated Subgrade (inches)

FOR FULL DEPTH ASPHALT SECTION - (CURRENTLY NOT ALLOWED)

 $D_1 = (WSN)/C_1 = 5.8$ inches of Full Depth Asphalt

Use 6.0 inches Full Depth

FOR ASPHALT + CEMENT TREATED SUBGRADE SECTION

Asphalt Thickness (t) = 4 inches

 $D_2 = ((WSN) - (t)(C_1))/C_2 = 6.5$ inches

Use 10.0 inches of Cement Treated Subgrade.

RECOMMENDED ALTERNATIVES

- 1. 4.0 inches of Asphalt + 10 inches of Cement Treated Subgrade.
- 2. 6.0 inches of Full Depth Asphalt

Job No. 201782

Fig. No. C-3





505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

September 15, 2020

FLRD #5 2138 Flying Horse Club Drive Colorado Springs, Colorado 80921

Attn: Mark Sherwood

Re: Cement Stabilized Subgrade Results - Laboratory Testing

Forest Lakes Filing No. 5 El Paso county of Colorado

Ref: Pavement Recommendations Report by Entech Engineering, Inc., dated September 15,

2020, Entech Job No. 201782.

Dear Mr. Sherwood:

As requested, personnel of Entech Engineering, Inc. have performed strength testing on two sets of three soil/cement composite samples for the above reference project. Testing was performed on soil samples prepared with 2% and 4% Portland Cement Type 1/2, from Martin Marietta, near Pueblo, Colorado.

A compression strength of 160 psi is recommended for cement stabilized subgrade. The 5-day average strength value of the 2% mix was 209 psi. The 5-day average strength value of the 4% mix was 243 psi. A 2% mix is recommended based on the laboratory test results. A summary of the testing results is attached.

Pending the results of the field density testing, microfracturing of the stabilized subgrade may be required. Soil strengths in excess 200 psi require microfracturing.

We trust this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Daniel P. Stegman

DPS/bs

Encl.

Entech Job No. 201782 AAprojects/2020/201782 cssr – lab Reviewed by:

Mark H. Hauschild, P.E. Senior Engineer

SUMMARY OF CTS TEST RESULTS LAB TESTING

CLIENT FLRD #5

PROJECT FOREST LAKES, FILING 5

FIELD SAMPLE ID TB-7 @ 0-3'

SOIL ADDITIVE TYPE I/II CEMENT

JOB NO 201782

9/15/20

BY

BL

ADDITIVE %	WATER %	DENSITY (dry)	AGE (days)	STRENGTH (psi)
2	6.8	127.1	5	199
2	6.8	126.6	5	216
2	6.8	127.4	5	211
			AVERAGE:	209
4	6.8	127.2	5	249
4	6.8	127.0	5	252
4	6.8	126.8	5	230
			AVERAGE:	243

CURING METHOD

100° HUMIDIFIED OVEN