# CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1

# FINAL DRAINAGE REPORT

#### Prepared for:

Jovenchi-I LLC. 4779 N Academy Blvd. Colorado Springs, CO 80918 719-491-2158

Prepared by:



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July 2024

Project No. 24.1382.003

PCD File SF

SF2420

#### Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Jesse Sullivan	Date
Registered Professional Engineer	
State of Colorado	
No. 55600	

#### Owner/Developer's Statement:

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

#### Jovenchi-I LLC.

Business Name

By: \_\_\_\_\_ Dean Venezia

Date

Title:

Address:

#### El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer, P.E. County Engineer / ECM Administrator Conditions:

Date

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## I. INTRODUCTION

The proposed Cimarron Hills Southeast Mixed Use Filing No. 1 development is comprised of approximately 32.99 acres of land previously platted under the Softball West Subdivision No. 2 development. The site is currently not being used. It is located northeast of the intersection of Peterson Road and Highway 24. Improvements proposed by the developments will extend Meadowbrook Parkway through the site to an intersection with Peterson Road. The site is bounded to the north by the East Fork of Sand Creek. Currently, the site is comprised of three (3) parcels.

#### a. PURPOSE AND SCOPE OF STUDY

The purpose of this Final Drainage Report (FDR) is to evaluate the specific drainage infrastructure requirements which will provide compliance with the El Paso County Drainage Criteria Manual (DCM). This study will identify off-site, and on-site drainage patterns associated with respective land uses, provide hydrologic and hydraulic analysis of tributary basins and conveyance structures to a detention pond, and identify effective, safe routing to the downstream outfall. The improvements associated with this report maintain compliance with the DCM by providing full spectrum detention where necessary, which is to be constructed concurrently with the improvements associated with this FDR.

### b. DBPS RELATED INVESTIGATIONS

The proposed development is located within the Sand Creek Drainage Basin. A Drainage Basin Planning Study (DBPS) was completed for this basin in 2021.

#### c. GENERAL PROJECT DESCRIPTION

The Cimarron Hills Southeast Mixed Use Filing No. 1 Subdivision is located to the northeast of the intersection of Peterson Road and Highway 24. The site is located as follows:

- 1. <u>General Location:</u> West ½ of the Southwest ¼ of Section 8, Range 65 West of the 6<sup>th</sup> P.M. in the County of El Paso, State of Colorado.
- 2. <u>Drainageway:</u> The proposed development is in the Sand Creek Drainage Basin. The site generally drains southwest eventually draining into East Fork Sand Creek at a point approximately 1,400 feet west of the site. East Fork Sand Creek is a tributary to Sand Creek which ultimately drains into Fountain Creek.
- 3. <u>Surrounding Developments:</u> The site is bounded on the east by Meadowbrook Crossing Filing No. 1 and Crossroads Mixed Use Filing No. 1, on the north by the East Fork of Sand Creek and Cimarron Southeast Filing No. 1, on the south by Highway 24 and on the west Peterson Road.
- 4. Lots to be Platted: The site is to be subdivided into 1 lot and 4 tracts.
- 5. <u>Area of Disturbance:</u> The proposed development is expected to disturb a total area of approximately 5.52 acres. doesnt match GEC
- 6. <u>Streamside Zone</u>: This project is not located within a streamside zone.
- 7. <u>Vegetation</u>: The site contains a small, paved area. The remainder of the site is sparsely vegetated, abandoned softball fields.

Refer to Appendix D for the Vicinity Map.

### d. SOILS CONDITIONS

Soils can be classified in four different hydrologic groups, A, B, C, or D to help predict stormwater runoff rates. Hydrologic group "A" is characterized by deep, well-drained coarse-grained soils with a rapid infiltration rate when thoroughly wet and having a low runoff potential. Group "D" typically has a clay layer at or near to the surface, or a very shallow depth to impervious bedrock and has a very slow infiltration rate and a high runoff potential. See Soils Map, Appendix C. The following soil types are present at the site:

1 4010 1.1 1	1100 0011 0uivey 101 Li 1 u	so county China	11011 I IIIS Southeast	inined 0.50	1 mig 1 (0.
Soil ID	Soil	Hydrologic	Drainage	Percent	
Number	3011	Classification	Class	of Site	
8	Blakeland loamy sand, 1 to 9 percent slopes	А	Well Drained	49.2%	
10	Blendon sandy loam, 0 to 3 percent slopes	В	Well Drained	50.8%	

Table 1.1 - NRCS Soil Survey for El Paso County - Cimarron Hills Southeast Mixed Use Filing No. 1

#### DATA SOURCES

Topographical information for the development area was found using a combination of *United States Geological Survey* (USGS) mapping as well as field surveying. The *Web Soil Survey*, created by the *Natural Resources Conservation Service*, was utilized to investigate the existing general soil types within the proposed development. Offsite contours may be taken from the *2018 El Paso County LIDAR* survey and/or USGS Quad Sheets.

#### e. APPLICABLE CRITERIA AND STANDARDS

This report has been prepared in accordance with the criteria set forth in the City of Colorado Springs and El Paso County DCM, El Paso County Engineering Criteria Manual (ECM) and El Paso County Resolutions 15-042 and 19-245. In addition to the DCM, the **Urban Storm Drainage Criteria Manuals, Volumes 1 through 3**, dated 2016 have been used to supplement the County's Criteria Manual.

## II. Hydrologic Methodology

#### a. MAJOR BASINS AND SUBBASINS

The proposed development is located within the Sand Creek Drainage Fee Basin. Runoff presently flows overland to the southwest until reaching the Highway 24 road ditch. Flows are conveyed west along Highway 24 until reaching the East Fork of Sand Creek.

#### b. METHODOLOGY

#### i. UD Methods

The hydrology for this project uses both the **SCS Hydrograph Procedure** and the **Rational Method** as recommended by the Drainage Criteria Manual (DCM) for the minor and major storms. The Rational Method is used for drainage basins less than 100-acres in size. The Rational Method uses the following equation:

Q=C\*i\*A

Where:

Q = Maximum runoff rate in cubic feet per second (cfs)

C = Runoff coefficient

i = Average rainfall intensity (inches per hour)

A = Area of drainage sub-basin (acres)

Rational Method coefficients from Table 6-6 of the Drainage Criteria Manual for developed land were utilized in the Rational Method calculations. This method will be used primarily for sizing of storm sewer infrastructure. See Appendix B for more information.

#### Time of Concentration

The time of concentration consists of the initial time of overland flow and the travel time in a channel to the inlet or point of interest. A minimum time of concentrations of 5 minutes is utilized for urban areas. The Rational Calculation spreadsheet included in Appendix A shows an initial overland flow length, a channel or street flow length for each sub-basin, and also demonstrates the time of concentration calculations for initial (overland) and channel (or street) conditions. A maximum "True Initial" Flow Length of 300 feet will be used for pre-developed sub-basins and a maximum length of 100 feet will be used for Developed sub-basins for time of concentration calculations in compliance with the DCM.

#### Rainfall Intensity

The hypothetical rainfall depths for the 1-hour storm duration were derive Please clarify the proposed DCM (shown below).

Return Period	1-Hour Depth	6-Hour Depth	24-Hour Depth
2	1.19	1.70	2.10
5	1.50	2.10	2.70
10	1.75	2.40	3.20
25	2.00	2.90	3.60
50	2.25	3.20	4.20
100	2.52	3.50	4.60

 Table 6-2. Rainfall Depths for Colorado Springs intent there is only one lot (13.8)

development. Per the Letter of intent there is only one lot (13.8 acres) that its land use will be a church/school/retirement facility. Please analyze for the proposed use. Tracts A and B identified as future single family attached in the TIS can be designed for upon the subdivision/plat of those tracts.

Where Z= 6,840 ft/100

The rainfall intensity equation for the Rational Method was taken from Drainage Criteria Manual Volume 1 Figure 6-5.

#### **C-Factors**

C-factors for the Rational Method are based on anticipated land use and are taken from Table 6-6. Proposed single family residential is considered as the Single Family – 5 acres category. Areas which will be future open spaces or detention facilities are modeled under the Parks and Cemeteries category. Undeveloped or pre-development areas are model under Undeveloped Areas-Historic Flow Analysis—Greenbelts, Agriculture category.

#### ii. HGL Profile Methods

Preliminary sizing of storm sewer has been completed using the Manning's channel flow calculation.

To confirm DCM compliant capacity and velocity values the site has been modeled in StormCAD using the Standard head loss method and head loss values taken from Table 9-4 of the DCM. HGL profiles modeled in StormCAD are included in Appendix C.

## **III.** Project Characteristics

#### a. MAJOR DRAINAGEWAYS

#### Sand Creek

Table 9-4. STORMCAD Standard Method Coefficients

Bend Loss											
Bend Angle	K Coef	ficient									
0°	0.05										
22.5°	0.10										
45°	45° 0.40										
60° 0.64											
90° 1.32											
LATERAL LOSS											
(	One Lateral K Coeffic	ient									
Bend Angle	Non-surcharged	Surcharged									
45°	0.27	0.47									
60°	0.52	0.90									
90°	1.02	1.77									
Т	wo Laterals K Coeffi	cient									
45°	0.9	06									
60°	1.1	6									
90°	1.5	52									

#### comments have been made on the plat that the roadway shall be platted ROW in lieu of

The proposed development is located within the Sand Creek Draina a tract. Revise within this basin presently flows overland with slopes ranging from 5 to 50% accordingly. actural drainage swale located within the site. This drainage swale directs the sites flows internally until discharging from the site near the northeastern corner. Drainage from the developed road will be directed to Pond 1, where the runoff will be treated for water quality and detained to maintain the

#### b. LAND USES

The proposed site was previously platted and contained softball fields. The 31.8-acre area is entirely zoned CR CAD-O. The site will consist of one lot and four tracts, one containing the proposed Pond 1, one containing the proposed roadway, and the other two containing undeveloped land.

## IV. BASIN HYDROLOGY

historic major event discharge rate from the site.

**a.** The <u>*Pre-development conditions*</u> for the Proposed development have been analyzed and are presented by design points and are described as follows:

Predevelopment conditions have been analyzed using the Rational Method. Runoff generated, either on-site or off-site, drains overland towards the southwest where it is ultimately captured by the existing road ditch along Highway 24, exiting the site and releasing flows to be collected in the East Fork of Sand Creek. Generally, all undeveloped basins are considered to be vegetated with sparse grasses. A delineation of the basin boundaries can be found in Appendix D in drawings DR-01. Runoff calculations can be found in Appendix A. The existing runoff design points are described below:

**Design Point EX-1** ( $Q_5 = 6.3$  cfs,  $Q_{100} = 37.6$  cfs) (sub-basins: OS1 and EX-1; Area: 32.23 Ac.) (Slopes: 2 to 25%) This point represents the discharge from sub-basins OS1 and EX-1 under predevelopment conditions. Under the predevelopment conditions Flows generated within sub-

basins OS1 and EX-1 drain overland to the southwest. Plows are ultimately captured by the Highway 24 (Public) Road Ditch and conveyed westward, eventually reaching the East Fork of Sand EX-2 is conveyed Creek. directly to East Fork

**Design Point EX-2** ( $Q_5 = 0.2 \text{ cfs}$ ,  $Q_{100} = 1.4 \text{ cfs}$ ) (sub-basin: EX-2; Area: 0.45 Ac.) (Sh Sand Creek. Revise 25%) This point represents the discharge from sub-basin EX-2 under predevelopment ( the narrative Under the predevelopment conditions sub-basin EX-2 drains to the north into East For accordingly. Creek. Please show on the drainage plan.

**Design Point DSCH** ( $Q_5 = 6.5$  cfs,  $Q_{100} = 39.0$  cfs) (sub-basins: OS1, EX-1 and EX-2; Area: 33.68) Ac.) (Slopes: 2 to 25%) This point represents the discharge from the site under predevelopment conditions. Under the predevelopment conditions the general drainage direction is to the southwest. Flows are ultimately captured by the Highway 24 (Public) Road Ditch and conveyed westward, eventually reaching the East Fork of Sand Creek.

**b.** The *<u>fully developed conditions</u>* for the site are as follows:

discuss NC-1 and NC-2, if they will be treated by the EDB or if an exclusion applies.

Post development conditions have been analyzed using the rational method. Runoff drains overland and in proposed private storm sewer towards the southwestern corner of the site where developed flows will be treated in the proposed private full spectrum detention facility. Flows will be discharged into the Highway 24 road ditch which will convey the flows to the west, eventually reaching the East Fork of Sand Creek. All proposed storm is to be public unless otherwise indicated.

A delineation of the basin boundaries can be found in Appendix D in drawing DR-02. Runoff calculations can be found in Appendix A. The proposed runoff design points are described below:

**Design Point 1** ( $Q_5 = 1.3 \text{ cfs}$ ,  $Q_{100} = 2.4 \text{ cfs}$ ) (sub-basin: PR-3; Area: 0.32 Ac.) (Slopes: 1 to 5%) This point represents the two at grade inlets capturing runoff in basin PR-3. The inlets are sized to capture the local flows. In the unlikely event of flooding from the East Fork of Sand Creek, the flows in excess of the designed capacity of the inlets will bypass to the south along historic paths. Stormwater collected in the inlets at DP1 is conveyed downstream toward the proposed full spectrum extended detention facility via 36-inch RCP.

**Design Point 2** ( $Q_5 = 6.0 \text{ cfs}$ ,  $Q_{100} = 10.9 \text{ cfs}$ ) (sub-basin: PR-2; Area: 1.82 Ac.) (Slopes: 1 to 5%) This point represents the two sump inlets capturing runoff in basin PR-2. Stormwater runoff generated within sub-basin PR-2 drains overland and in curb and gutter to the two inlets at DP-2. Stormwater collected in the inlets at DP2 is conveved downstream toward the proposed full spectrum extended detention facility via 36-inch BCP.

Map shows pipe size as 24". Please

**Design Point 3** ( $Q_5 = 11.0 \text{ cfs}$ ,  $Q_{100} = 23.4 \text{ cfs}$ ) (sub-basin: I  $R_{-1}$ ,  $R_{100} = 0.05 \text{ Ac.}$ ) (sub-basin: I  $R_{-1}$ ,  $R_{100} = 0.05 \text{ Ac.}$ ) (sub-basin) This point represents the stormwater runoff generated within sub-basin PR-1 collected in a temporary Type C inlet at DP3. Development of sub-basin PR-1 is not proposed with this project. In fully developed conditions flows generated within sub-basin PR-1 will be conveyed to DP3 via future storm sewer infrastructure to be designed with the FDR for Lot 2. The temporary type C inlet collects flows from the undeveloped site which are then conveyed downstream toward the proposed detention facility via proposed 30-inch RCP.

**Design Point 4** ( $Q_5 = 12.0 \text{ cfs}$ ,  $Q_{100} = 25.2 \text{ cfs}$ ) (sub-basins: PR-1, PR-3; Area: 6.37 Ac.) (Slopes: 1 to 10%) This point represents the combination of flows from DP1, and DP3 in the proposed storm sewer. The combined flows will continue in the proposed public 36-inch RCP storm sewer to the east eventually discharging into the proposed detention facility.

**Design Point 5** ( $Q_5 = 17.8 \text{ cfs}$ ,  $Q_{100} = 35.8 \text{ cfs}$ ) (sub-basins: PR-1, PR-2, PR-3; Area: 8.19 Ac.) (Slopes: 1 to 10%) This point represents the combination of flows from DP1, DP2, and DP3 in the proposed storm sewer. The combined flows will continue in the proposed private 42-inch RCP storm sewer to the south eventually discharging into the proposed detention facility. **tract B** 

**Design Point 6** ( $Q_5 = 30.5 \text{ cfs}$ ,  $Q_{100} = 62.9 \text{ cfs}$ ) (sub-basins: PR-1, PR-2, PR-3, PR-4; Area: 15.19 Ac.) (Slopes: 1 to 10%) This point represents the discharge from sub-basins PR-1, PR-2, PR-3, and PR-4 into the proposed detention facility. Flows at DP6 have been calculated assuming fully developed conditions even though the development of sub-basins PR-1, and PR-4 is not proposed at this time. In fully developed conditions stormwater runoff generated within sub-basin PR-4 will be directed to the proposed private manhole (MH-3) via future storm sewer infrastructure to be designed with the FDR for Lot 3. In the interim condition, stormwater generated in sub-basin PR-4 drains overland to the southwest exiting the site into the existing curb and gutter along the east side of Peterson Road before continuing along historic paths.

**Design Point 7** ( $Q_5 = 41.6 \text{ cfs}$ ,  $Q_{100} = 78.6 \text{ cfs}$ ) (sub-basin: PR-5; Area: 14.46 Ac.) (Slope description accordingly. 10%) This point represents the discharge from sub-basin PR-5 into the proposed detention facility. Flows at DP7 have been calculated assuming fully developed conditions even though the development of sub-basin PR-5 is not proposed at this time. In fully developed conditions stormwater runoff generated within sub-basin PR-5 will be directed to the proposed detention facility via future storm sewer infrastructure to be designed with the FDR for Lot 1. In the interim condition, stormwater generated in sub-basin PR-5 drains overland to the south exiting the site into the existing ditch along the north side of the Highway 24 off ramp before continuing along historic paths. Indicate what interim flows are entering pond.

**Design Point 8** ( $Q_5 = 71.6 \text{ cfs}$ ,  $Q_{100} = 143.6 \text{ cfs}$ ) (sub-basins: PR-1, PR-2, PR-3, PR-4, PR-5, PR-6; Area: 31.52 Ac.) (Slopes: 1 to 10%) This point represents the discharge from the fully developed site into the proposed private Full Spectrum Extended Detention Basin located in the southwestern corner of the site (Pond 1). Stormwater is collected in Pond 1 which provides water quality treatment and detention for the site.

**Design Point 9** ( $Q_5 = 4.7 \text{ cfs}$ ,  $Q_{100} = 31.9 \text{ cfs}$ ) (sub-basins: PR-1, PR-2, PR-3, PR-4, PR-5, PR-6; Area: 31.52 Ac.) (Slopes: 1 to 10%) This point represents the discharge from Pond 1 in fully developed conditions. Stormwater collected in the proposed detention facility will be discharged to the Roadside ditch along the north side of the Highway 24 off-ramp before continue historic paths.

please discuss the design points associated with sub-basins NC-1 and NC-2.

Notes:

• MHFD-Detention Analysis for the proposed detention pond (Pond 1) which will be constructed as part of the Improvements associated with Cimarron Hills Southeast Mixed Use Filing No. 1 can be found in Appendix A of this report.

Please also provide analysis of the interim condition to ensure drain times are met in this condition also. Identify if any changes to the orifice plate are needed between the interim and fully developed conditions

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- Tables summarizing inlet sizes and capacities, storm pipe sizes and capacities and swale capacities for the proposed improvements can be found in Appendix A and /or in the following section. Provide analysis of roadside ditch along Highway 24 with existing and proposed flows. Discuss if ditch still meets criteria with proposed flow
- All ponds and associated internal intrastructure are to be owned and maintained by the HOA.
- The ratio of the total site discharge in proposed conditions vs existing conditions is 0.8, representing no significant increase in flows in the proposed condition. Include interim

condition (No development to Tracts A & B).

## V. Hydraulic Analysis

#### a. Proposed Inlets

This project will use Type R inlets in both sump and at grade conditions. Sump inlet capacities were determined utilizing the nomographs available from the El Paso County Drainage Criteria Manual Volume 1 (DCM). The Type R inlet has a total depth in sump conditions of 9-inches based on a flow depth of 6-inches in the curb and gutter and an additional 3-inches of depth in the throat of the inlet. The table below lists inlets by design point and corresponding capacity. Figure 1 shows the capacities for Type R inlets in sump conditions.

	INLET SUMMARY CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1													
DESIGN POINT or SUB- BASIN	SUB-BASINS/ DESCRIPTION	TOTAL		INL	ET	0(5)	Of DUET	Q(100)	Q(100)					
		AREA (AC)	SIZE (Ft.)	TYPE	CONDITION	TOTAL INFLOW	Q5 INLE I CAPACTIY	BYPASS FLOWS (cfs)	IOTAL INFLOW (cfs)	MAX INLE I CAPACITY				
1	PR-3	0.32	2 x 5'	R	AT GRADE	1.3	1.3	0.0	2.4	2.4				
2	PR-2	1.82	2 x 5'	R	SUMP	6.0	22.0	0.0	10.9	22.0				

Note: Inlet sizes indicated are minimums. Larger sizes may be used in the construction plans for conservative design.



Figure 1

	Inlet Overflow Routing											
Inlet	Overflow Routing Under Sump Inlet Blockage Conditions											
2	Blockage of these inlets will force flows south along the nearby utility easement and into the proposed detention facility.											
	is the final drainage											

## b. Storm Pipes report.

Preliminary sizing of storm sewer has been completed using the Manning's channel flow calculation. To confirm DCM compliant capacity and velocity values the site has been modeled in StormCAD using the Standard head loss method and head loss values taken from Table 9-4 of the DCM. HGL profiles modeled in StormCAD are included in Appendix A. Outfall protection has been provided at discharge points in accordance with DCM standards. Outfall protection calculations are included in Appendix A. All outfalls have been designed to provide flow velocities consistent with a stable and suitable outfall.

#### c. Detention

Calculations were not seen in appendix. Please provide with next submittal.

The proposed private Extended Detention Basin (Pond 1) has been designed to detain stormwater flows to reduce the total site discharge to predevelopment levels. The pond will provide detention and water quality treatment for stormwater runoff generated within the Proposed development. The proposed private Forebay at the north side of Pond 1 has been sized based on the untreated WQCV calculated in the MHFD-DETENTION worksheet. The forebay calculations and MHFD-DETENTION worksheet can be found in Appendix A. The proposed private trickle channel has been sized to accommodate the release from the proposed private forebay. Trickle channel calculations are included in Appendix A. Pond 1 will outfall to a riprap pad to the southwest. Design information including calculations are included in Appendix A. The table below summarizes the detention provided for this development.

Proposed Pond Summary CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1													
Pond	Tributary	%	Pre-Devel	opment Peak	Pond	Outflow	Pre vs. Post Ratio						
	Area	impervious	Q5	Q100	Q5	Q100	Q5	Q100					
Pond 1	31.52	74.52	9.3	40.7	4.7	31.9	0.5	0.8					

How do flows from PR-5/DP 7 enter pond? Is forebay or rundown needed?

#### **Emergency Overflow**

**Pond 1:** If the emergency overflow weir receives flows, these flows will continue downstream and drain into the roadside ditch along the north side of the Highway 24 off-ramp. Provide analysis of

Provide analysis of roadside ditch with this flow.

## VI. Storm Water Quality

Per the DCM Volume 2, Section 4.1, El Paso County recommends the MHFD Four Step Process for receiving water protection that focuses on reducing runoff by disconnecting impervious area, eliminating "unnecessary" impervious area and encouraging infiltration into soils that are suitable, treat and slowly release the WQCV, stabilize stream channels, and implement source controls. The four-step process has been completed below.

#### **<u>Step 1:</u>** Employ Runoff Reduction Practices.

• Where possible runoff will be directed across and through grassed swales, however, please note that this report is for street infrastructure, which is difficult to drain across pervious areas and maintain compliance with the DCM and the County's standard street sections.

#### <u>Step 2:</u> Stabilize Drainageways.

• The site is in the Sand Creek Drainage Fee Basin. Drainage fees paid at the time of initial platting help fund proposed channel improvements. Information on planned future improvements to the Sand Creek channel was unavailable for this report.

#### <u>Step 3:</u> Provide Water Quality Capture Volume (WQCV).

• As required by the DCM, runoff from the proposed streets which is feasible to detain, is directed into a proposed detention pond (Pond 1) via proposed storm sewer. The pond has been designed to meet the DCM standards for the release rates of Full Spectrum Detention Ponds for Water Quality Capture Volumes, and all of the other storm events listed in the MHFD- Detention spreadsheet. Exclusions are listed below:

• Disturbed areas that are not practicable to detain are excluded from WQ treatment per section I.7.1.C.1.a. This includes sub-basin NC-1 which contains 0.27 acres or 1.0% of the overall site.

#### <u>Step 4:</u> Consider Need for Industrial and Commercial BMPs.

• There are no commercial or industrial components of this development, therefore no BMPs of this nature are required.

### VII. Erosion Control Plan

A grading and erosion control plan (GEC) for the proposed improvements will be submitted for review as a separate submittal. These plans will incorporate straw wattles, straw bale check dams, silt fence, vehicle tracking control, inlet & outlet control, sedimentation basins and other best management practices (CMs) identified in the DCM Volume 2.

## VIII. Floodplains

Per the *Flood Insurance Rate Maps (FIRM) 08041CO752 G & 08041C0754 G*, effective date December 7, 2018, published by the Federal Emergency Management Agency (FEMA), East Fork Sand Creek, a Tributary to Sand Creek runs along the northern bound of the Cimarron Hills Southeast Mixed Use Filing No. 1 area and has designated 100-year floodplain. The developed portion of the site is generally not touched by the 100 year floodplain, however the road improvements associated with this site will cross the FEMA floodplain along the western portion of the proposed roadway. Additionally, a portion of proposed Pond 1 is to be constructed within the floodplain. Both instances of construction in the floodplain will be demonstrated to cause "no rise" in the associated base flood elevations and a "no rise" certification will be submitted with the floodplain development permit application. Refer to the map in Appendix C.

#### IX. Fee Development

#### a. Previously Platted Land

The Proposed development is located within the Sand Creek Drainage Fee Basin and within previously platted land. The 2024 Drainage Basin Fees for the Sand Creek Drainage Fee Basin are: \$25,632/impervious acre for the Drainage Fee and \$10,484.00/impervious acre for the Bridge Fee. Drainage fees were paid at the time of the initial plat so no fees are due at this time.

Previous plats do not indicate that fees were paid, Regardless per ECM App. L, fees shall be paid for any increase in imperviousness. Previous development for the site was for softball fields. Please provide drainage basin fees due to the increase in impervious for lot 1 and the roadway.. Tracts are not assessed basin fees. Please submit with this final plat application. Please coordinate with Keith Curtis any requirements necessary for developing the roadway and pond within the floodplain.

### Cost Estimate

Table 9.1												
Engine	er's Es	timate of Pro	bable Construction	Costs								
SAND CREEK												
CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1												
Private Non-Reimbursable												
Item Unit Quantity Unit Cost Extension												
18" RCP/HP	LF	56	\$82.00	\$4,592.00								
24" RCP/HP	LF	57	\$98.00	\$5,586.00								
30" RCP/HP	LF	97	\$123.00	\$11,931.00								
36" RCP/HP	LF	545	\$151.00	\$82,295.00								
42" RCP/HP	LF	711	\$201.00	\$142,911.00								
30" FES	EA	1	\$738.00	\$738.00								
5' Type R Inlet	EA	4	\$9,377.00	\$37,508.00								
66" x 48" CCS Box												
Base MH	EA	5	\$15,130.00	\$75,650.00								
RIPRAP	CY	90	\$135.00	\$12,150.00								
			Sub Total	\$373,361.00								

10% Contingency	\$37,336.10
TOTAL:	\$410,697.10

Engineer's Estimate of Probable Construction Costs														
SAI	SAND CREEK													
CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1														
Permanent BMP (EDB): Private Non-reimbursable														
Item Unit Quantity Unit Cost Exten														
DETENTION POND GRADING	EA	1	\$35,000.00	\$35,000.00										
3' TRICKLE CHANNEL	LF	260	\$250.00	\$65,000.00										
FOREBAY	EA	1	\$40,000.00	\$40,000.00										
OUTLET STRUCTURE	EA	1	\$40,000.00	\$40,000.00										
EMERGENCY SPILLWAY	EA	1	\$5,000.00	\$5,000.00										
			Sub Total	\$185,000.00										
		10%	Contingency	\$18,500.00										
			TOTAL:	\$203,500.00										
		(	Overall Total	\$614,197.10										

Since the engineer has no control over the cost of labor, materials, equipment, or services furnished by others, or over the contractor's method of determining prices, or over the competitive bidding or market conditions, the opinion of probable construction costs provided herein are made on the basis of the engineer's experience and qualifications and represents the best judgment as an experienced and qualified professional familiar with the construction industry. The engineer cannot, and does not guarantee that proposals, bid or actual construction costs will not vary from the opinion of probable costs.

## X. Summary

This report demonstrates that the proposed infrastructure associated with Cimarron Hills Southeast Mixed Use Filing No. 1 is in conformance with the El Paso County Drainage Criteria Manual, Volumes 1 and 2, October 2018 and all previously approved studies related to the project site. Stormwater flows will generally remain the same in post-development conditions  $Q_5 = 7.8$  cfs,  $Q_{100} = 38.7$  cfs) as in pre-development conditions  $Q_5 = 6.5$  cfs,  $Q_{100} = 38.7$  cfs). These proposed improvements should not adversely affect downstream or surrounding developments and are in conformance with the pertinent studies for the area.

38.96 per drainage map

-Please provide analysis/ discussion of the east fork sand creek along the northern boundary of the site. Identify any improvements indicated in the DBPS. Is the creek stable, erosive, in need of improvements? is the crossing at Peterson adequate? Is this development responsible for any improvements to the creek (refer to DCMV1.4.2? please address.

-Provide analysis of the 100yr floodplain at the proposed meadowbrook parkway. Ensure cross flow in roadways for initial and major storms (DCMV1 table 6-1) is met.

#### XI. References

- El Paso County and City of Colorado Springs Drainage Criteria Manual, Volume 1 & 2, El Paso County, May 2014
- 2. *El Paso County Engineering Criteria Manual,* El Paso County, Rev. December 2016
- 3. Web Soil Survey of El Paso County Area, Colorado. Unites States Department of Agriculture Soil Conservation Service.
- 4. Flood Insurance Rate Maps for El Paso County, Colorado and Incorporated Areas, Panel 279 of 1275, Federal Emergency Management Agency, Effective Date December 7, 2018.
- 5. *Urban Storm Drainage Criteria Manual, Vol. 1-3* by Urban Drainage and Flood Control District (UDFCD), January 2016

# Appendices

# <u>APPENDIXA</u>

HYDROLOGIC AND HYDRAULIC CALCULATIONS

include forebay and trickle channel cals

Project Name: Project Location: Designer Notes: Average Channel Velocity Average Slope for Initial Flow	CIMARRON HILLS SOUTHEAST MIXED USI EL PASO COUNIY JIS EXISTING CONDITIONS 400 0.04	E FILING NO ft/s ft/ft	O. 1 (If speci (If Elev	ific channel rations are u	vel is used, thi sed, this will be	s will be ignored) e ignored)													Sho	<u>Channel Flow T</u> Heavy Meadov Tillage/Field rt Pasture and Lawn Nearly Bare Ground Grassed Waterway	<u>ype Key</u> w 2 d 3 s 4 d 5 y 6										
95% 2% Paved Areas 7														-																	
	Area Rational 'C' Values										Flo	w Lengths								Tc		Rai	nfall Intensi	y & Rational	Flow Rate						
Sub-basin	Comments			Soil Group		Commercial Area (95% Impervious	s )	Une	leveloped/Perv (2% Impervi	ious Areas ous)	Con	iposite	Percent Impervious	Initial	True Initial	Channel	True Channel	Average (decimal)	Initial	Average (%)	Channel Flow Type (See Key above)	Velocity	Channel	Total	i2	Q2	i5	Q5	i100	Q100	Sub-basin
		sf	acres		C5	C100		C5	C100	Area	C5	C100		ft	Length ft	ft	Length ft	Slope	Tc (min)	Slope	Ground Type	(ft/s)	Tc (min)	(min)	in/hr	cfs	in/hr	cfs	in/hr	cfs	
<i>OS-1</i>	OFFSITE BASIN SOUTHWEST OF SITE. CONTAINS EXISTING HOTEL.	52319	1.20	В	0.81	0.88	29246	0.09	0.36	23073	0.49	0.65	53.99	25	25	350	350	0.10	2.54	2.0	7	2.83	2.06	5.00	4.12	2.46	5.17	3.1	8.68	6.8	OS-1
EX-1	UNDEVELOPED SITE AREA	1395360	32.03	В	0.81	0.88		0.09	0.36	1395360	0.09	0.36	2.00	300	100	1800	2000	0.25	10.77	1.7	4	0.89	37.65	48.41	1.42	4.12	1.76	5.1	2.96	34.4	EX-1
EX-2	UNDEVELOPED SITE AREA	19495	0.45	В	0.81	0.88		0.09	0.36	19495	0.09	0.36	2.00	50	50	0	0	0.17	5.04	0.5	4	0.49	0.00	5.03	4.11	0.17	5.16	0.2	8.66	1.4	EX-2
DESIGN POINTS	Sub-basins																														DESIGN POINTS
EX-1	EXISTING SITE DISCHARGE	1447679	33.23	В	0.81	0.88	29246	0.09	0.36	1418433	0.10	0.37	3.88	300	100	1800	2000	0.25	10.61	2	4	0.91	36.52	47.13	1.45	5.08	1.80	6.3	3.03	37.6	EX-1
EX-2	EXISTING SITE DISCHARGE	19495	0.45	В	0.81	0.88		0.09	0.36	19495	0.09	0.36	2.00	50	50	0	0	0.17	5.04	1	4	0.49	0.00	5.03	4.11	0.17	5.16	0.2	8.66	1.4	EX-2
DSCH	EXISTING SITE DISCHARGE	1467174	33.68	В	0.81	0.88	29246	0.09	0.36	1437928	0.10	0.37	3.85	300	100	1800	2000	0.25	10.62	2.0	4	0.99	33.67	44.28	1.52	5.40	1.90	6.5	3.18	39.0	DSCH

#### **Rational Method - Existing Conditions**

Project Name: Project Location: Designer Notes:	CIMARRON HILLS SOUTHEAST MIXED EL PASO COUNTY JIS PROPOSED CONDITIONS	USE FILING NO	O. 1																			Sho	<u>Channel Flow T</u> Heavy Meadow Tillage/Fiel	<u>ype Key</u> v 2 d 3 s 4								
Average Channel Velocity Average Slope for Initial Flow	4.00 0.0-	00 ft/s 04 ft/ft	(If specifi (If Elevat	ic channel tions are us	vel is used, this ed, this will be	is will be ignored) e ignored) 95%			70%			2%										5110	Nearly Bare Groun Grassed Waterwa Paved Area	d 5 y 6 is 7								
		Area				7570			Rationa	d 'C' Values		270						Flo	w Lengths								Tc	Rainfa	ll Intensity &	& Rational Fl	ow Rate	T
Sub-basin	Comments			Soil Group		Commercial Are (95% Imperviou	as s)	Neig	hborhoods/Mu (70% Impervie	lti-Family ous)	Unc	developed/Per (2% Imperv	vious Areas ious)	Com	posite	Percent Impervious	Initial	True Initial	Channel	True Channel	Average (decimal)	Initial	Average (%)	Channel Flow Type (See Key above)	Velocity	Channel	Total	i5	Q5	i100	Q100	Sub-basin
		sf	acres		C5	C100		C5	C100	Area	C5	C100	Area	C5	C100		ft	Length ft	ft	Length ft	Slope	Tc (min)	Slope	Ground Type	(ft/s)	Tc (min)	(min)	in/hr	cfs	in/hr	cfs	
PR-1	NORTH OF MEADOWBROOK PKWY MULTIFAMILY	263491	6.05	в	0.81	0.88		0.49	0.62	263491	0.09	0.36		0.49	0.62	70.00%	100	100	640	640	0.05	6.42	2.0	7	2.83	3.77	10.19	4.10	12.3	6.89	26.0	PR-1
PR-2	MEADOWBROOK PKWY	79312	1.82	В	0.81	0.88	78822	0.49	0.62		0.09	0.36	490	0.81	0.88	94.43%	50	50	1024	1024	0.03	2.57	1.1	7	2.10	8.14	10.70	4.03	6.0	6.76	10.9	PR-2
PR-3	MEADOWBROOK PKWY	13794	0.32	В	0.81	0.88	13794	0.49	0.62		0.09	0.36		0.81	0.88	95.00%	50	50	136	136	0.02	2.93	1.1	7	2.10	1.08	5.00	5.17	1.3	8.68	2.4	PR-3
PR-4	MULTIFAMILY	304990	7.00	В	0.81	0.88		0.49	0.62	304990	0.09	0.36		0.49	0.62	70.00%	100	100	960	960	0.05	6.42	2.0	7	2.83	5.66	12.07	3.85	13.3	6.46	28.3	PR-4
PR-5	CHURCH PARCEL	630078	14.46	B	0.81	0.88	562345	0.49	0.62		0.09	0.36	67733	0.73	0.82	85.00%	100	100	1460	1460	0.10	3.07	2.0	7	2.83	8.60	11.67	3.90	41.6	6.54	78.6	PR-5
PR-6	DETENTION TRACT	81301	1.87	В	0.81	0.88		0.49	0.62		0.09	0.36	81301	0.09	0.36	2.00%	25	25	330	330	0.25	3.11	0.5	4	0.49	11.11	14.22	3.60	0.6	6.05	4.1	PR-6
NC-1	PORTION OF MEADOWBROOK PKWY IMPRACTICABLE TO DETAIN	Y 11613	0.27	В	0.81	0.88	11613	0.49	0.62		0.09	0.36		0.81	0.88	95.00%	25	25	136	136	0.02	2.07	1.0	7	2.00	1.13	5.00	5.17	1.1	8.68	2.1	NC-1
NC-2	UNDEVELOPABLE AREA DRAINING TO THE NORTH.	30344	0.70	В	0.81	0.88		0.49	0.62		0.09	0.36	30344	0.09	0.36	2.00%	25	25	188	188	0.05	5.32	12.0	4	2.42	1.29	6.60	4.75	0.3	7.98	2.0	NC-2
<i>OS-1</i>	OFFSITE BASIN SOUTHWEST OF SITE. CONTAINS EXISTING HOTEL.	52319	1.20	В	0.81	0.88	29246	0.49	0.62		0.09	0.36	23073	0.49	0.65	53.99%	25	25	350	350	0.10	2.54	2.0	7	2.83	2.06	5.00	5.17	3.1	8.68	6.8	<i>OS-1</i>
DESIGN POINTS	Sub-basins																															DESIGN POINTS
DP1	MEADOWBROOK PKWY- AT GRADE INLETS	13794	0.32	В	0.81	0.88	13794	0.49	0.62	0	0.09	0.36	0	0.81	0.88	95.00%	50	50	136	136	0.02	2.93	1.1	7	2.10	1.08	5.00	5.17	1.3	8.68	2.4	DP1
DP2	MEADOWBROOK PKWY- SUMP INLETS	79312	1.82	В	0.81	0.88	78822	0.49	0.62	0	0.09	0.36	490	0.81	0.88	94.43%	50	50	1024	1024	0.03	2.57	1.1	7	2.10	8.14	10.70	4.03	6.0	6.76	10.9	DP2
DP3	LOT 2	263491	6.05	В	0.81	0.88	0	0.49	0.62	263491	0.09	0.36	0	0.49	0.62	70.00%	50	50	1024	1024	0.03	5.32	1.1	7	2.10	8.14	13.46	3.68	11.0	6.18	23.4	DP3
DP4	DP1, DP3	277285	6.37	В	0.81	0.88	13794	0.49	0.62	263491	0.09	0.36	0	0.51	0.63	71.24%	50	50	1024	1024	0.03	5.19	1.1	7	2.10	8.14	13.32	3.70	12.0	6.21	25.2	DP4
DP5	DP 2, DP3, & DP 1	356597	8.19	В	0.81	0.88	92616	0.49	0.62	263491	0.09	0.36	490	0.57	0.69	76.40%	50	50	1024	1024	0.03	4.60	1.1	7	2.10	8.14	12.74	3.77	17.8	6.32	35.8	DP5
DP6	DP4 & LOT 3	661587	15.19	В	0.81	0.88	92616	0.49	0.62	568481	0.09	0.36	490	0.53	0.66	73.45%	50	50	1375	1375	0.03	4.94	2.0	7	2.83	8.10	13.03	3.73	30.5	6.27	62.9	DP6
DP7	CHURCH PARCEL	630078	14.46	В	0.81	0.88	562345	0.49	0.62	0	0.09	0.36	67733	0.73	0.82	85.00%	100	100	1460	1460	0.10	3.07	2.0	7	2.83	8.60	11.67	3.90	41.6	6.54	78.6	DP7
DP8	INTO DETENTION POND	1372966	31.52	В	0.81	0.88	654961	0.49	0.62	568481	0.09	0.36	149524	0.60	0.72	74.52%	100	100	1460	1460	0.10	4.19	2.0	7	2.83	8.60	12.78	3.76	71.6	6.31	143.6	DP8
DP9	OUT OF DETENTION POND	1372966	31.52	В	0.81	0.88	654961	0.49	0.62	568481	0.09	0.36	149524	0.60	0.72	74.52%	100	100	1460	1460	0.10	4.19	2.0	7	2.83	8.60	12.78	3.76	4.7	6.31	31.9	DP9
DSCH	SITE DISCHARGE	1436898	32.99	В	0.81	0.88	695820	0.49	0.62	568481	0.09	0.36	172597	0.60	0.71	73.94%	100	100	1810	1810	0.10	4.20	2.0	7	2.83	10.67	14.86	3.53	7.8	5.93	38.7	DSCH
																										4 1				1 2		

# **Rational Method - Proposed Conditions**

#### MHFD-Inlet, Version 5.03 (August 2023)

#### INLET MANAGEMENT Worksheet Protected

INLET NAME	<u>DP1</u>
Site Type (Urban or Rural)	URBAN
Inlet Application (Street or Area)	STREET
Hydraulic Condition	On Grade
Inlet Type	CDOT Type R Curb Opening

#### **USER-DEFINED INPUT**

User-Defined Design Flows							
Minor Q <sub>Known</sub> (cfs)	1.3						
Major Q <sub>Known</sub> (cfs)	2.4						

#### Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (lef

Receive Bypass Flow from:	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0

#### Watershed Characteristics

Subcatchment Area (acres)	
Percent Impervious	
NRCS Soil Type	

#### Watershed Profile

Overland Slope (ft/ft)	
Overland Length (ft)	
Channel Slope (ft/ft)	
Channel Length (ft)	

#### Minor Storm Rainfall Input

Design Storm Return Period, Tr (years)	
One-Hour Precipitation, P <sub>1</sub> (inches)	

#### Major Storm Rainfall Input

Design Storm Return Period, T <sub>r</sub> (years)	
One-Hour Precipitation, P <sub>1</sub> (inches)	

#### CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	1.3
Major Total Design Peak Flow, Q (cfs)	2.4
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	0.0
Major Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	0.0



#### INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.03 (August 2023)



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	-
Total Inlet Interception Capacity	Q =	1.3	2.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	0.0	cfs
Capture Percentage = $Q_a/Q_o$	C% =	100	100	%

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Optional User Override

1.19 inches 
 1.10
 inches

 1.50
 inches

 1.75
 inches

 2.00
 inches
 2.25 inches 2.52 inches inches

acre-feet



- T-- 6 ..... Water

ersned Information		
Selected BMP Type =	EDB	
Watershed Area =	31.52	acres
Watershed Length =	1,750	ft
Watershed Length to Centroid =	800	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	74.52%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

graphinoceae	
0.780	acre-feet
2.593	acre-feet
2.326	acre-feet
3.107	acre-feet
3.760	acre-feet
4.510	acre-feet
5.188	acre-feet
5.981	acre-feet
7.698	acre-feet
2.039	acre-feet
2.703	acre-feet
3.385	acre-feet
3.631	acre-feet
3.775	acre-feet
4.012	acre-feet
	0.780 2.593 2.326 3.107 3.760 4.510 5.188 2.039 2.703 3.385 3.631 3.775 4.012

Define	Zones	and	Basin	Geome	etry
		ž	Zone 1	Volume	(WC

Zone 1 Volume (WQCV) =	0.780	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.812	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.420	acre-feet
Total Detention Basin Volume =	4.012	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin (L <sub>MAIN</sub> ) =	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet

			1							
	Depth Increment =	0.50	ft				Ontinent			
	Stage - Storage	Stane	Override	Length	Width	Area	Override	Area	Volume	Volume
	Description	(ff)	Stage (ft)	(ff)	(ff)	(ff <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
	Top of Micropool	(10)	0.00	(14)	(10)	()	172	0.004	(10)	(uc it)
	тор от містороот		0.00				1/3	0.004		
	6279.5		0.09				173	0.004	16	0.000
	6280		0.59	-		-	330	0.008	141	0.003
	0200		0.55				550	0.000	111	0.005
			1.09				1,023	0.023	480	0.011
			1.59	-		-	4,425	0.102	1,842	0.042
			2.09				10.908	0.250	5.675	0.130
			2.50				10,207	0.410	12.052	0.207
			2.59				18,207	0.418	12,953	0.297
			3.09	-		-	24,964	0.573	23,746	0.545
			3.59				30.567	0.702	37.629	0.864
			4.00				24,244	0.705	52,022	4.000
			4.09			-	34,211	0.785	53,823	1.236
			4.59				37,846	0.869	71,838	1.649
			5.09				40.723	0.935	91,480	2.100
			5.50				43,733	0.001	112 244	2 570
			5.59				42,732	0.981	112,344	2.5/9
			6.09				44,518	1.022	134,156	3.080
r Overrides			6.59				46,283	1.063	156.856	3.601
acre-feet			7.09				48.076	1 104	180 446	4 147
dere rece			7.05				10,070	1.101	100,110	
acre-feet			7.59				49,886	1.145	204,937	4.705
inches			8.09			-	51,722	1.187	230,339	5.288
inches	6288		8 59				53 586	1 230	256 666	5 892
lashas			0.04				55,000	1.267	275,705	6 220
inches			0.54				33,200	1.207	2/3,/03	0.325
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#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



include workbook for interim conditions to ensure orifice plate is sized appropriately and not holding water

#### DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022) Project: PETERSON AND MEADOWBROOK Basin ID: SAND CREEK Estimated Estimated Stage (ft) Volume (ac-ft) Outlet Type Zone 1 (WQCV) 3.47 0.780 Orifice Plate Zone 2 (EURV 5.61 1.812 Circular Orifice 100-YEAF ZONE 1 AND 2 ORIFICES Zone 3 (100-year) 6.98 1.420 Weir&Pipe (Restrict) PERM Example Zone Configuration (Retention Pond) Total (all zones) 4.012 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area Underdrain Orifice Invert Depth = ft<sup>2</sup> N/A N/A Underdrain Orifice Diameter = N/A inches Underdrain Orifice Centroid = N/A feet User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row 1.833E-02 ft<sup>2</sup> Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width = 3.23 N/A feet Orifice Plate: Orifice Vertical Spacing N/A inches Elliptical Slot Centroid : N/A feet ft<sup>2</sup> Orifice Plate: Orifice Area per Row = 2.64 sq. inches (diameter = 1-13/16 inches) Elliptical Slot Area = N/A User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft 0.00 1.50 3.00 Orifice Area (sq. inches) 2 64 2 64 2 64 Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 9 (optional) Row 16 (optional) Stage of Orifice Centroid (ft Orifice Area (sg. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Zone 2 Circular Not Selected Zone 2 Circular Not Selected Invert of Vertical Orifice Vertical Orifice Area 3.47 N/A t (relative to basin bottom at Stage = 0 ft) 0.05 N/A Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft) 5.61 N/A Vertical Orifice Centroid 0.13 N/A feet Vertical Orifice Diameter = 3.00 N/A inches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe) Calculated Parameters for Overflow Weir Zone 3 Weir Not Selected Zone 3 Weir Not Selected Overflow Weir Front Edge Height, Ho 5.61 N/A Height of Grate Upper Edge, $H_t$ : N/A t (relative to basin bottom at Stage = 0 ft) 5.61 eet Overflow Weir Slope Length Overflow Weir Front Edge Length 6.00 N/A feet 6.00 N/A feet Overflow Weir Grate Slope = 0.00 N/A H:V Grate Open Area / 100-yr Orifice Area = 9.56 N/A Horiz. Length of Weir Sides : N/A feet Overflow Grate Open Area w/o Debris : 25.06 N/A +2 6.00 Overflow Grate Open Area w/ Debris = ft<sup>2</sup> Overflow Grate Type Type C Grate N/A 12.53 N/A Debris Clogging % = 50% N/A ٥/۵ User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe 0.25 N/A t (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area 2.62 N/A 0.76 Outlet Pipe Diameter 30.00 N/A Outlet Orifice Centroid N/A inches feet Restrictor Plate Height Above Pipe Invert = 15.80 inches Half-Central Angle of Restrictor Plate on Pipe = 1.62 N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= 7.00 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.95 feet Stage at Top of Freeboard = Spillway Crest Length 38.00 feet 8.95 feet Spillway End Slopes 4.00 H:V Basin Area at Top of Freeboard : 1.27 acres Freeboard above Max Water Surface = Basin Volume at Top of Freeboard = 1.00 feet 6.33 acre-ft Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by nterina new value in the Inflow Hydrographs table (Columns W through AF) Design Storm Return Period WOCV FURV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year One-Hour Rainfall Depth (in) N/A 1.50 2.00 2.52 3.14 N/A 1.19 1.75 2.25 0.780 2.593 3.760 4.510 5.188 5.981 7.698 CUHP Runoff Volume (acre-ft) 2.326 3.107 Inflow Hydrograph Volume (acre-ft) N/A N/A 2.326 3.107 3.760 4.510 5.188 5.981 7.698 25.4 CUHP Predevelopment Peak O (cfs) N/A N/A 3.4 9.3 14.1 31.9 40.7 56.8 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.11 0.30 0.45 0.81 1.01 1.29 1.80 Peak Inflow Q (cfs) N/A N/A 41.6 55.0 64.6 79.3 91.2 106.9 136.4 Peak Outflow Q (cfs) 0.3 0.9 0.8 4.7 10.0 21.0 30.3 31.9 61.4 Ratio Peak Outflow to Predevelopment O N/A N/A N/A 0.5 0.7 0.8 1.0 0.8 1.1 Structure Controlling Flow Plate rtical Orifice Overflow Weir 1 erflow Weir rflow Wei itlet Plate Spillway Öv Overflow Wei Overflow Wei Max Velocity through Grate 1 (fps) N/A N/A N/A 0.8 0.1 0.4 1.2 1.2 1.3 Max Velocity through Grate 2 (fps) N/A N/A N/A 65 N/A N/A N/A N/A N/A N/A 68 68 38 65 70 69 67 63 Time to Drain 97% of Inflow Volume (hours) Time to Drain 99% of Inflow Volume (hours) 40 72 69 75 75 74 74 73 72 Maximum Ponding Depth (ft) 7.39 5.61 5.82 5.99 6.44 6.89 3.47 5.20 6.26 Area at Maximum Ponding Depth (acres) 0.94 2.194 1.00 1.03 3.244

Maximum Volume Stored (acre-ft)

0.67

0.98

1.13

4 466

1.05

3 443

<u>1.01</u> 2.978

2.80

1.09 3.913



## DETENTION BASIN OUTLET STRUCTURE DESIGN

# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

	Inflow Hydrographs									
	The user can ov	verride the calcu	lated inflow hyd	rographs from t	his workbook wit	h inflow hydrogr	raphs developed	in a separate pro	ogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
ime Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cf:
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.56	0.06	1.78
	0:15:00	0.00	0.00	4.93	8.04	9.94	6.67	8.26	8.11	11.46
	0:20:00	0.00	0.00	17.06	22.24	26.66	16.36	18.97	20.39	26.84
	0:25:00	0.00	0.00	35.98	48.70	59.23	35.28	40.84	44.03	59.43
	0:30:00	0.00	0.00	41.62	55.03	64.59	74.53	86.20	95.75	123.30
	0:35:00	0.00	0.00	36.65	47.61	55.58	79.30	91.17	106.92	136.43
	0:40:00	0.00	0.00	31.11	39.69	46.42	/2.5/	83.23	97.19	123.83
	0:50:00	0.00	0.00	24.09	27.26	31.81	53.01	60.74	72.82	92.64
	0:55:00	0.00	0.00	17.19	23.08	27.38	43.05	49.37	60.85	77.54
	1:00:00	0.00	0.00	14.82	19.77	23.85	36.12	41.47	52.79	67.31
	1:05:00	0.00	0.00	12.68	16.83	20.63	30.75	35.35	46.52	59.34
	1:10:00	0.00	0.00	10.01	14.37	17.94	24.64	28.35	35.96	46.02
	1:15:00	0.00	0.00	8.13	12.17	16.29	19.64	22.63	27.37	35.25
	1:20:00	0.00	0.00	7.15	10.68	14.56	15.44	17.79	19.97	25.79
	1:25:00	0.00	0.00	6.62	9.82	12.60	12.94	14.90	15.29	19.79
	1:30:00	0.00	0.00	6.33	9.25	11.22	10.82	12.42	12.39	16.05
	1:35:00	0.00	0.00	6.16	8.88	10.26	9.40	10.75	10.53	13.64
	1:45:00	0.00	0.00	5.03	7.00	9.00	7.86	9.00	9.27	10.00
	1:50:00	0.00	0.00	5.88	6.59	8.82	7.44	8.44	7.86	10.91
	1:55:00	0.00	0.00	5.04	6.20	8.29	7.19	8.14	7.58	9.80
	2:00:00	0.00	0.00	4.39	5.74	7.43	7.03	7.96	7.48	9.66
	2:05:00	0.00	0.00	3.11	4.07	5.23	5.00	5.66	5.34	6.89
	2:10:00	0.00	0.00	2.13	2.78	3.59	3.43	3.88	3.69	4.76
	2:15:00	0.00	0.00	1.44	1.87	2.45	2.35	2.65	2.53	3.27
	2:20:00	0.00	0.00	0.95	1.22	1.62	1.56	1.76	1.68	2.17
	2:25:00	0.00	0.00	0.59	0.78	1.04	1.01	1.14	1.09	1.41
	2:30:00	0.00	0.00	0.35	0.50	0.64	0.65	0.73	0.70	0.90
	2:33:00	0.00	0.00	0.18	0.28	0.35	0.37	0.41	0.39	0.51
	2:45:00	0.00	0.00	0.07	0.03	0.03	0.10	0.05	0.10	0.22
	2:50:00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### Figure 13-12b. Emergency Spillway Profile at Embankment



Figure 13-12d. Riprap Types for Emergency Spillway Protection





	Label: Di Type: I ID	P1b INLET Manhole 9: 32	MEADOWBROOK PARKWAY (LAT-1) - Q5						
6,290.60									
6,290.40									
6,290.20			Type	:: Manhole					
6,290.00				ID: 34					
6,289.80									
6,289.40									
6,289.20									
6,289.00									
6,288.80									
6,288.60			Label: PIPE - 10						
6,288.40			Type: Conduit						
6,288.20				Type: Conduit					
£ 6,288.00				ID: 45					
<b>5</b> 6,287.80									
6,287.40									
6,287.20									
<b>6</b> ,287.00									
6,286.80									
6,286.60									
6,286.40									
6,286.20									
6,286.00									
6,285.80									
6 285 40									
6,285,20 -									
6,285.00									
6,284.80									
6,284.60									
6,284.40									
	-2.0 -1.0 0	.0 1.0 2.0	3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 11.0 12.0 13.0 14.0 15.0 16.0 17.0 18.0 19.0 20.0 21.0 22.0 23.0 24.0 25.0 26.0 27.0 2	28.0 29.0 30.0 31.0 32.0 33.0 34.0 35.0 36.0 37.0 38.0 39.0 40.0 41.0 42.0 43.0 44.0 45.0 46.0 47.0 48					
ID\Label			44 \ MPE - 10	45 \ PIPE - 9					
Link Length (ft)			28.3	28.1					
Rise (in)\Material			18.0 \ Concrete	18.0 \ Concrete					
Flow (cfs)			0.65	0.65					
Slope (ft/ft)			0.005	0.005					
ID\Label	32 \ DP	16 INLET	3	14 \ MH - 7					
Ground (ft)	629	90.55		6290.39					
Invert (ft)	628	86.10		6284.51					
Station (ft)	C	0.0		28.3					

	Label: DP Type: M ID:	1a INLET Ianhole 33		
				- EGL - HGL
49.0 50.0 51.0 52.0 53.0 54	4.0 55.0 56.0	57.0 58.0 5	9.0	
	33 \ DP1 6290	a INLET ).54		
	6286 56	.08		








	Label 🔺	Flow (cfs)	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Manning's n	Diameter (in)	Capacity (Full Flow) (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Hydraulic Grade Line (In) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (Out) (ft)	Material
52: PIPE - 1	PIPE - 1	30.50	DP6	6,282.03	0-1	6,281.50	85.5	0.006	0.013	42.0	79.23	7.70	6,287.18	6,283.74	6,285.30	6,283.01	Concrete
49: PIPE - 2	PIPE - 2	17.80	MH - 4	6,282.57	DP6	6,282.13	293.1	0.002	0.013	42.0	38.98	3.96	6,287.43	6,284.23	6,287.18	6,283.77	Concrete
47: PIPE - 3	PIPE - 3	17.80	DP5	6,283.18	MH - 4	6,282.67	332.9	0.002	0.013	42.0	39.38	3.99	6,289.66	6,284.82	6,287.43	6,284.24	Concrete
63: PIPE - 4	PIPE - 4	12.00	DP4	6,283.85	DP5	6,283.68	116.2	0.001	0.013	36.0	25.51	3.55	6,291.16	6,285.34	6,289.66	6,285.20	Concrete
46: PIPE - 5	PIPE - 5	1.30	MH - 7	6,284.77	DP4	6,283.95	248.4	0.003	0.013	36.0	38.32	2.52	6,290.39	6,285.62	6,291.16	6,285.62	Concrete
48: PIPE - 6	PIPE - 6	6.00	MH - 1	6,283.95	DP5	6,283.68	180.5	0.001	0.013	36.0	25.80	2.97	6,289.39	6,285.25	6,289.66	6,285.20	Concrete
50: PIPE - 7	PIPE - 7	3.00	INLET DP 2a	6,285.09	MH - 1	6,284.95	33.5	0.004	0.013	24.0	14.62	3.66	6,289.44	6,285.70	6,289.39	6,285.55	Concrete
51: PIPE - 8	PIPE - 8	3.00	INLET DP2b	6,285.09	MH - 1	6,284.95	23.6	0.006	0.013	24.0	17.43	4.15	6,289.44	6,285.69	6,289.39	6,285.51	Concrete
45: PIPE - 9	PIPE - 9	0.65	DP1a INLET	6,286.41	MH - 7	6,286.27	28.1	0.005	0.013	18.0	7.41	2.58	6,290.54	6,286.71	6,290.39	6,286.57	Concrete
44: PIPE - 10	PIPE - 10	0.65	DP 1b INLET	6,286.41	MH - 7	6,286.27	28.3	0.005	0.013	18.0	7.39	2.57	6,290.55	6,286.71	6,290.39	6,286.57	Concrete
43: PIPE - 11	PIPE - 11	11.00	DP3	6,284.75	DP4	6,284.35	39.9	0.010	0.013	36.0	66.77	6.98	6,292.00	6,285.80	6,291.16	6,285.62	Concrete
80: PIPE - 28	PIPE - 28	4.70	MH-3	6,279.16	0-2	6,278.99	56.7	0.003	0.013	30.0	22.46	3.62	6,285.01	6,279.94	6,281.49	6,279.70	Concrete

Figure 1-Q5 – Free Outfall CONDUIT SUMMARY

	Label 🔺	Flow (Total Out) (cfs)	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Headloss (ft)	Elevation (Invert in 1) (ft)	Elevation (Invert in 2) (ft)	Elevation (Invert in 3) (ft)	Elevation (Invert Out) (ft)	Hydraulic Grade Line (In) (ft)	Energy Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (Out) (ft)	He M
33: DP1a INLET	DP1a INLET	0.65	6,290.54	6,290.54	0.01	(N/A)	(N/A)	(N/A)	6,286.41	6,286.72	6,286.82	6,286.71	6,286.81	Sta
32: DP1b INLET	DP 1b INLET	0.65	6,290.55	6,290.55	0.01	(N/A)	(N/A)	(N/A)	6,286.41	6,286.72	6,286.82	6,286.71	6,286.81	Sta
53: DP3	DP3	11.00	6,292.00	6,292.00	0.02	(N/A)	(N/A)	(N/A)	6,284.75	6,285.82	6,286.21	6,285.80	6,286.19	Sta
62: DP4	DP4	12.00	6,291.16	6,291.16	0.28	6,284.35	6,283.95	(N/A)	6,283.85	6,285.62	6,285.62	6,285.34	6,285.52	Sta
35: DP5	DP5	17.80	6,289.66	6,289.66	0.38	6,283.68	6,283.68	(N/A)	6,283.18	6,285.20	6,285.37	6,284.82	6,285.07	Sta
40: DP6	DP6	30.50	6,287.18	6,287.18	0.03	6,282.13	(N/A)	(N/A)	6,282.03	6,283.77	6,284.02	6,283.74	6,284.40	Sta
37: INLET DP 2a	INLET DP 2a	3.00	6,289.44	6,289.44	0.01	(N/A)	(N/A)	(N/A)	6,285.09	6,285.71	6,285.92	6,285.70	6,285.91	Sta
39: INLET DP2b	INLET DP2b	3.00	6,289.44	6,289.44	0.01	(N/A)	(N/A)	(N/A)	6,285.09	6,285.71	6,285.92	6,285.69	6,285.91	Sta
38: MH - 1	MH - 1	6.00	6,289.39	6,289.39	0.10	6,284.95	6,284.95	(N/A)	6,283.95	6,285.35	6,285.62	6,285.25	6,285.32	Sta
36: MH - 4	MH - 4	17.80	6,287.43	6,287.43	0.01	6,282.67	(N/A)	(N/A)	6,282.57	6,284.24	6,284.52	6,284.23	6,284.47	Sta
34: MH - 7	MH - 7	1.30	6,290.39	6,290.39	0.01	6,286.27	6,286.27	(N/A)	6,284.77	6,285.63	6,285.74	6,285.62	6,285.63	Sta
78: MH-3	MH-3	4.70	6,285.01	6,285.01	0.01	(N/A)	(N/A)	(N/A)	6,279.16	6,279.95	6,280.15	6,279.94	6,280.14	Sta

Figure 2-Q5 – Free Outfall NODE SUMMARY

	Labe.≜	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)
54: 0-1	0-1	6,285.30	6,281.30	Free Outfall		6,283.01	30.50
81: 0-2	0-2	6,281.49	6,278.99	Free Outfall		6,279.70	4.70

Figure 3-Q5 – Free Outfall OUTFALL SUMMARY

adloss ethod
ndard



6 200 60	Label: DP1b INLET Type: Manhole ID: 32	MEADOWBROOK PARKWA	NY (LAT-1) - Q100
6,290.60			
6,290,20			
6,290.00			
6,289.80			MU 7
6,289.60		Laber 1 Type: M	anhole
6,289.40			34
6,289.20			
6,289.00			
6,288.80			
6,288.60		Label: PIPE - 10	
6,288.40		Type: Conduit Top.44	
6,288.20			Type: Conduit
€ <sup>6,288.00</sup>			ID: 45
£ 6,287.80			
6,287.60			
6 287 20			
G.287.00			
6,286.80			
6,286.60			
6,286.40			
6,286.20			
6,286.00			
6,285.80			
6,285.60			
6,285.40			
6,285.20			
6,285.00			
6,284.80			
6,284.60			
	-2.0 -1.0 0.0 1.0	2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 11.0 12.0 13.0 14.0 15.0 16.0 17.0 18.0 19.0 20.0 21.0 22.0 23.0 24.0 25.0 26.0 27.0 28.	0 29.0 30.0 31.0 32.0 33.0 34.0 35.0 36.0 37.0 38.0 39.0 40.0 41.0 42.0 43.0 44.0 45.0 46.0 47.0
ID\Label		44 \ MPE - 10	45 - 444 / 45
Link Length (ft)		28.3	28.1
Rise (in)\Material		18.0 \ Concrete	18.0 \ Concrete
Flow (cfs)		1.20	1.20
Slope (ft/ft)		0.005	0.005
ID\Label	32 \ DP1b INLET	34 \	мн - 7
Ground (ft)	6290.55	629	0.39
Invert (ft)	6286.10	628	4.51
Station (ft)	0.0	2	8.3











	Label 🔺	Flow (cfs)	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Manning's n	Diameter (in)	Capacity (Full Flow) (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Hydraulic Grade Line (In) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (Out) (ft)	Material
52: PIPE - 1	PIPE - 1	62.90	DP6	6,282.03	0-1	6,281.50	85.5	0.006	0.013	42.0	79.23	9.14	6,287.18	6,284.52	6,285.30	6,283.85	Concrete
49: PIPE - 2	PIPE - 2	35.80	MH - 4	6,282.57	DP6	6,282.13	293.1	0.002	0.013	42.0	38.98	4.60	6,287.43	6,285.11	6,287.18	6,284.57	Concrete
47: PIPE - 3	PIPE - 3	35.80	DP5	6,283.18	MH - 4	6,282.67	332.9	0.002	0.013	42.0	39.38	4.64	6,289.66	6,285.72	6,287.43	6,285.13	Concrete
63: PIPE - 4	PIPE - 4	25.20	DP4	6,283.85	DP5	6,283.68	116.2	0.001	0.013	36.0	25.51	4.11	6,291.16	6,286.41	6,289.66	6,286.26	Concrete
46: PIPE - 5	PIPE - 5	2.40	MH - 7	6,284.77	DP4	6,283.95	248.4	0.003	0.013	36.0	38.32	3.02	6,290.39	6,286.78	6,291.16	6,286.78	Concrete
48: PIPE - 6	PIPE - 6	10.90	MH - 1	6,283.95	DP5	6,283.68	180.5	0.001	0.013	36.0	25.80	3.50	6,289.39	6,286.30	6,289.66	6,286.26	Concrete
50: PIPE - 7	PIPE - 7	5.45	INLET DP 2a	6,285.09	MH - 1	6,284.95	33.5	0.004	0.013	24.0	14.62	4.31	6,289.44	6,286.39	6,289.39	6,286.38	Concrete
51: PIPE - 8	PIPE - 8	5.45	INLET DP2b	6,285.09	MH - 1	6,284.95	23.6	0.006	0.013	24.0	17.43	4.91	6,289.44	6,286.38	6,289.39	6,286.38	Concrete
45: PIPE - 9	PIPE - 9	1.20	DP1a INLET	6,286.41	MH - 7	6,286.27	28.1	0.005	0.013	18.0	7.41	3.08	6,290.54	6,286.82	6,290.39	6,286.78	Concrete
44: PIPE - 10	PIPE - 10	1.20	DP 1b INLET	6,286.41	MH - 7	6,286.27	28.3	0.005	0.013	18.0	7.39	3.08	6,290.55	6,286.82	6,290.39	6,286.78	Concrete
43: PIPE - 11	PIPE - 11	23.40	DP3	6,284.75	DP4	6,284.35	39.9	0.010	0.013	36.0	66.77	8.61	6,292.00	6,286.71	6,291.16	6,286.78	Concrete
80: PIPE - 28	PIPE - 28	31.90	MH-3	6,279.16	0-2	6,278.99	56.7	0.003	0.013	30.0	22.46	6.50	6,285.01	6,281.50	6,281.49	6,280.91	Concrete

Figure 4- Q100 – Free Outfall CONDUIT SUMMARY

	Label 🔺	Flow (Total Out) (cfs)	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Headloss (ft)	Elevation (Invert in 1) (ft)	Elevation (Invert in 2) (ft)	Elevation (Invert in 3) (ft)	Elevation (Invert Out) (ft)	Hydraulic Grade Line (In) (ft)	Energy Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (Out) (ft)	Headloss Method
33: DP1a INLET	DP1a INLET	1.20	6,290.54	6,290.54	0.01	(N/A)	(N/A)	(N/A)	6,286.41	6,286.83	6,286.97	6,286.82	6,286.97	Standard
32: DP1b INLET	DP1bINLET	1.20	6,290.55	6,290.55	0.01	(N/A)	(N/A)	(N/A)	6,286.41	6,286.83	6,286.97	6,286.82	6,286.97	Standard
53: DP3	DP3	23.40	6,292.00	6,292.00	0.02	(N/A)	(N/A)	(N/A)	6,284.75	6,286.73	6,287.08	6,286.71	6,287.07	Standard
62: DP4	DP4	25.20	6,291.16	6,291.16	0.36	6,284.35	6,283.95	(N/A)	6,283.85	6,286.78	6,286.78	6,286.41	6,286.65	Standard
35: DP5	DP5	35.80	6,289.66	6,289.66	0.54	6,283.68	6,283.68	(N/A)	6,283.18	6,286.26	6,286.50	6,285.72	6,286.08	Standard
40: DP6	DP6	62.90	6,287.18	6,287.18	0.06	6,282.13	(N/A)	(N/A)	6,282.03	6,284.57	6,284.96	6,284.52	6,285.67	Standard
37: INLET DP 2a	INLET DP 2a	5.45	6,289.44	6,289.44	0.00	(N/A)	(N/A)	(N/A)	6,285.09	6,286.40	6,286.50	6,286.39	6,286.49	Standard
39: INLET DP2b	INLET DP2b	5.45	6,289.44	6,289.44	0.00	(N/A)	(N/A)	(N/A)	6,285.09	6,286.39	6,286.49	6,286.38	6,286.48	Standard
38: MH - 1	MH - 1	10.90	6,289.39	6,289.39	0.08	6,284.95	6,284.95	(N/A)	6,283.95	6,286.38	6,286.46	6,286.30	6,286.35	Standard
36: MH - 4	MH - 4	35.80	6,287.43	6,287.43	0.02	6,282.67	(N/A)	(N/A)	6,282.57	6,285.13	6,285.51	6,285.11	6,285.47	Standard
34: MH - 7	MH - 7	2.40	6,290.39	6,290.39	0.01	6,286.27	6,286.27	(N/A)	6,284.77	6,286.78	6,286.86	6,286.78	6,286.78	Standard
78: MH-3	MH-3	31.90	6,285.01	6,285.01	0.03	(N/A)	(N/A)	(N/A)	6,279.16	6,281.53	6,282.23	6,281.50	6,282.19	Standard

Figure 5-Q100 – Free Outfall NODE SUMMARY

	Labe.≜	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)
54: 0-1	0-1	6,285.30	6,281.30	Free Outfall		6,283.85	62.90
81: 0-2	0-2	6,281.49	6,278.99	Free Outfall		6,280.91	31.90

Figure 6-Q100 Free Outfall OUTFALL SUMMARY

### APPENDIX B

STANDARD DESIGN CHARTS AND TABLES

Land Lice or Surface	Dorcont	Runoff Coefficients											
Characteristics	Impervious	2-y	ear	5-y	ear	10-1	/ear	25-1	/ear	50-1	year	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0 19	0.20	0.29	0.30	0.40	0 34	0.46	0.39	0.52
Playgrounds	13	0.05	0.05	0.12	0.15	0.20	0.23	0.30	0.42	0.37	0.48	0.35	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenbelts Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0 31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when													
landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

#### Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

#### **3.2** Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration  $(t_c)$  consists of an initial time or overland flow time  $(t_i)$  plus the travel time  $(t_i)$  in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time  $(t_i)$  plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion  $(t_i)$  of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas. IF.

Type of Development	Percent Impervious
Commercial	95%
Industrial	85%
Multi-Family	65%
Single Family - 0.1377 acre lots (6,000 SF)	53%
Single-Family - 0.20 acre lots	43%
Single-Family - 0.25 acre lots	40%
Single-Family - 0.33 acre lots	30%
Single-Family - 0.5 acre lots	25%
Single-Family - 1.0 acre lots	20%
Single-Family - 2.5 acre lots	11%
Single-Family - 5 acre lots	7%



Figure 6-25. Estimate of Average Concentrated Shallow Flow

#### El Paso County Drainage Basin Fees

Resolution No. 23-400

Basin Receiving			Drainage Basin Name	2024 Drainage Fee	2024 Bridge Fee	
Number	Waters	Studied		(per Impervious Acre)	(per Impervious Acre)	
Drainage Basins with	DBPS's:					
CHMS0200	Chico Creek	2013	Haegler Ranch	\$13,971	\$2,062	
CHWS1200	Chico Creek	2001	Bennett Ranch	\$15,641	\$6,000	
CHWS1400	Chico Creek	2013	Falcon	\$40,088	\$5,507	
FOFO2000	Fountain Creek	2001	West Fork Jimmy Camp Creek	\$17,003	\$5,031	
FOFO2600	Fountain Creek	1991*	Big Johnson / Crews Gulch	\$24,832	\$3,207	
FOFO2800	Fountain Creek	1988*	Widefield	\$24,832	\$0	
FOFO2900	Fountain Creek	1988*	Security	\$24,832	\$0	
FOFO3000	Fountain Creek	1991*	Windmill Gulch	\$24,832	\$372	
FOFO3100 / FOFO3200	Fountain Creek	1988*	Carson Street / Little Johnson	\$15,147	\$0	
FOFO3400	Fountain Creek	1984*	Peterson Field	\$17,911	\$1,358	
FOFO3600	Fountain Creek	1991*	Fisher's Canyon	\$24,832	\$0	
FOFO4000	Fountain Creek	1996	Sand Creek	\$25,632	\$10,484	
FOFO4200	Fountain Creek	1977	Spring Creek	\$12,879	\$0	
FOFO4600	Fountain Creek	1984*	Southwest Area	\$24,832	\$0	
FOFO4800	Fountain Creek	1991	Bear Creek	\$24,832	\$1,358	
FOFO5800	Fountain Creek	1964	Camp Creek	\$2,752	\$0	
FOMO1000	Monument Creek	1981	Douglas Creek	\$15,617	\$345	
FOMOI200	Monument Creek	1977	Templeton Gap	\$16,032	\$372	
FOMO2000	Monument Creek	1971	Pulpit Rock	\$8,234	\$0	
FOMO2200	Monument Creek	1994	Cottonwood Creek / S. Pine	\$24,832	\$1,338	
FOM02400	Monument Creek	1900	Dry Creek	\$19,003	\$710	
FOMO3000	Monument Creek	1989*	Black Squiffel Creek	\$11,275	\$710 #0	
FOMO3700	Monument Creek	1987*	Middle Hibutary	\$20,722	\$U	
FOMOS800	Monument Creek	198/*	Monument Branch	\$24,832 \$10,104	30U 181.259	
FUMU4000	Monument Creek	1090	Simul Creek	\$10,124 \$34,933	\$1,338 \$676	
FOM04200	Monument Creek	1909*	Diack rolest	324,032 \$24,932	4070 \$1259	
FOMO5200	Fountain Creek	1993*	Crustel Creek	\$24,032 \$74,837	\$1,358	
Macellancous Desines	Resinge 1	1995	Ciystal Cicck	Ψ <b>2</b> Τ,0J2	¢1,336	
Miscellaneous Drainas	e Dasins: -					
CHBS0800	Chico Creek		Book Ranch	\$23,300	\$3,373	
CHEC0400	Chico Creek		Upper East Chico	\$12,694	\$368	
CHWS0200	Chico Creek		Telephone Exchange	\$13,947	\$327	
CHWS0400	Chico Creek		Livestock Company	\$22,973	\$273	
CHWS0000	Chico Creek		West Squirrei	\$11,975	\$4,970	
CHWS0800	Chico Creek		Solderg Kanch	\$24,832	\$0 \$0	
FOF01200	Fountain Creek		Colhan Basamiain	ቅ/,49/ ድሩ ጋናር	фU Ф265	
FOF01400	Fountain Creek		Califian Reservoir	40,239 \$4,533	\$303 60	
FOF01000	Fountain Creek		Jimmy Camp Creek	\$7, <i>322</i> \$7/ 837	ΦU €1 161	
FOF02000	Fountain Creek		Fort Carron	\$10 602	\$1,101	
FOF02200	Fountain Creek		West Little Johnson	\$19,005	\$0	
FOFO3800	Fountain Creek		Stratton	\$11.911	\$533	
FOFO5000	Fountain Creek		Midland	\$19.603	\$710	
FOFO6000	Fountain Creek		Palmer Trail	\$19,603	\$710	
FOFO6800	Fountain Creek		Black Canvon	\$19,603	\$710	
FOMO4600	Monument Creek		Beaver Creek	\$14,846	\$0	
FOMO3000	Monument Creek		Kettle Creek	\$13.410	\$0	
FOMO3400	Monument Creek		Elkhorn	\$2,253	\$0	
FOMO5000	Monument Creek		Monument Rock	\$10,763	\$0	
FOMO5400	Monument Creek		Palmer Lake	\$17,210	\$0	
FOMO5600	Monument Creek		Raspberry Mountain	\$5,789	\$0	
PLPL0200	Monument Creek		Bald Mountain	\$12,337	\$0	
Interim Drainage Basis	ns: 2					
FOFO1800	Fountain Creek		Little Fountain Creek	\$3,175	\$0	
FOMO4400	Monument Creek		Jackson Creek	\$9,829	\$0	
FOMO4800	Monument Creek		Teachout Creek	\$6,825	\$1,026	

1. The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies performed within the last 14 years.

2. Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best available information suitable for setting a fee.)

### <u>Appendix C</u>

**REPORT REFERENCES** 

## National Flood Hazard Layer FIRMette



#### Legend



Basemap Imagery Source: USGS National Map 2023



United States Department of Agriculture

NATURAL NATURAL

Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for El Paso County Area, Colorado

APPROXIMATE SITE BOUNDARY



## Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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## **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



<ul> <li>Spoil Area</li> <li>Stony Spot</li> <li>Very Stony Spot</li> <li>Wet Spot</li> <li>Other</li> <li>Special Line Features</li> <li>Nater Features</li> <li>Streams and Canals</li> </ul>	The soil surveys that comprise your AOI were mapped at 1:24,000. Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.
<ul> <li>Very Stony Spot</li> <li>Wet Spot</li> <li>Other</li> <li>Special Line Features</li> <li>Nater Features</li> <li>Streams and Canals</li> </ul>	Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.
<ul> <li>HH Kaiis</li> <li>✓ Interstate Highways</li> <li>✓ US Routes</li> </ul>	Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
Major Roads Local Roads Background Aerial Photography	<ul> <li>Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.</li> <li>This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.</li> <li>Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 21, Aug 24, 2023</li> <li>Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.</li> <li>Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018</li> <li>The orthophoto or other base map on which the soil lines were</li> </ul>
3	<ul> <li>Interstate Highways</li> <li>US Routes</li> <li>Major Roads</li> <li>Local Roads</li> </ul> ackground Aerial Photography

### **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	16.6	49.2%
10	Blendon sandy loam, 0 to 3 percent slopes	17.2	50.8%
Totals for Area of Interest		33.8	100.0%

### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### El Paso County Area, Colorado

#### 8-Blakeland loamy sand, 1 to 9 percent slopes

#### **Map Unit Setting**

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Blakeland and similar soils: 98 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Blakeland**

#### Setting

Landform: Hills, flats Landform position (three-dimensional): Side slope, talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

#### **Typical profile**

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand C - 27 to 60 inches: sand

#### **Properties and qualities**

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

#### Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

#### **Minor Components**

#### Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

#### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

#### 10—Blendon sandy loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 3671 Elevation: 6,000 to 6,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

#### Map Unit Composition

Blendon and similar soils: 98 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Blendon**

#### Setting

Landform: Terraces, alluvial fans Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium derived from arkose

#### **Typical profile**

A - 0 to 10 inches: sandy loam Bw - 10 to 36 inches: sandy loam C - 36 to 60 inches: gravelly sandy loam

#### **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 2 percent
Available water supply, 0 to 60 inches: Moderate (about 6.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e

*Hydrologic Soil Group:* B *Ecological site:* R049XB210CO - Sandy Foothill *Hydric soil rating:* No

#### **Minor Components**

#### Other soils

Percent of map unit: 1 percent Hydric soil rating: No

#### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

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### <u>APPENDIX D</u>

MAPS



REFERENCE DRAWINGS X-1382-PR-UTIL	SI	SHEET KEY			EL PASO COUNTY	
X-1382-EX-SITE X-1382-PR-SITE X-1382-EX-MAP X-1382-EX-UTIL X-MDG30x42		R-Venezia.dwg		THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND	CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1 FINAL DRAINAGE REPORT	
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	CTB FILE: PLOT DATE: July 11, 2024 9:15:13 AM This drawing is current as of plot date and may be subject to change.		Excellence by Design	FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 24.1382.003	DESIGNED BY:WCGSCALEDATE ISSUED:JULY 2024DRAWING No.DRAWN BY:WCGHORIZ.1" = 60'SHEET1 OF 2DRO1CHECKED BY:JTSVERT.N/ASHEET1 OF 2DR01	

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REFERENCE DRAWINGS X-1382-PR-UTIL	Image:				EL PASO COUNTY
X-1382-EX-SITE X-1382-PR-SITE X-1382-EX-MAP X-1382-EX-UTIL X-MDG30x42				THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND	CIMARRON HILLS SOUTHEAST MIXED USE FILING NO. 1 FINAL DRAINAGE REPORT
	NO.     DATE     DESCRIPTION     BY       REVISIONS       COMPUTER FILE MANAGEMENT       FILE NAME: S:/24 1382 003 Peterson Road and Meadowbrook Parkway Overall Development/200 Design/220 Drainage-WR/222 Reports/EDR/DWG/DR-Vend	nezia dwa	PREPARED BY:	IS SUBJECT TO CHANGE	PROPOSED CONDITIONS DRAINAGE MAP
	CTB FILE: PLOT DATE: July 11, 2024 9:15:52 AM This drawing is current as of plot date and may be subject to change.		Excellence by Design	FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 24.1382.003	DESIGNED BY:WCGSCALEDATE ISSUED:JULY 2024DRAWING No.DRAWN BY:WCGHORIZ.1" = 60'SHEET2 OF 2DRO2CHECKED BY:JTSVERT.N/ASHEET2 OF 2DRO2

## v1\_Drainage Report - Final.pdf Markup Summary

Callout (34)		
2024 24.152.000 Re-SF SF2420	Subject: Callout Page Label: 1 Author: Daniel Torres Date: 1/2/2025 10:52:48 AM Status: Color: Layer: Space:	SF2420
	Subject: Callout Page Label: 6 Author: Daniel Torres Date: 1/4/2025 3:30:16 PM Status: Color: Layer: Space:	Please clarify the proposed development. Per the Letter of intent there is only one lot (13.8 acres) that its land use will be a church/school/retirement facility. Please analyze for the proposed use. Tracts A and B identified as future single family attached in the TIS can be designed for upon the subdivision/plat of those tracts.
	Subject: Callout Page Label: [1] DR-01 Author: Daniel Torres Date: 1/4/2025 7:50:44 PM Status: Color: Layer: Space:	label- the floodplain
Image:	Subject: Callout Page Label: 7 Author: Daniel Torres Date: 1/4/2025 7:56:01 PM Status: Color: Layer: Space:	comments have been made on the plat that the roadway shall be platted ROW in lieu of a tract. Revise accordingly.
Internet segment free           underset and compared and set of the set	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 1/4/2025 8:02:47 PM Status: Color: Layer: Space:	Please explain how flows are conveyed past Peterson Road.
nd 15.1 from module of the subsets first in a distantly of the (15.1 for a first in a disromy of second, small) smallper (15.1 for a first in a disromy of second small) smallper (15.1 for a first intervent of second small	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 1/4/2025 8:04:27 PM Status: Color: Layer: Space:	Please show on the drainage plan.
aptured by the the East Joek of Cond directly to East Fork (5.Ac) pits Sand Creak, Revise elogenetic, the initiative elogenetic, the initiative beta for accordingly.	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 1/4/2025 8:06:17 PM Status: Color: Layer: Space:	EX-2 is conveyed directly to East Fork Sand Creek. Revise the narrative accordingly.
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HISAC Internet	Subject: Callout Page Label: [1] DR-02 Author: Daniel Torres Date: 1/4/2025 8:27:04 PM Status: Color: Layer: Space:	fix flow arrow
	Subject: Callout Page Label: [1] DR-02 Author: Daniel Torres Date: 1/4/2025 8:31:53 PM Status: Color: Layer: Space:	provide contour labels
	Subject: Callout Page Label: [1] DR-02 Author: Daniel Torres Date: 1/4/2025 8:34:10 PM Status: Color: Layer: Space:	identify the type C inlet indicated in the narrative at DP3
in sub-basin PR-1 will be conveyed to I is the FDR for Loc T the temporary t then conveyed downstream toward the tract A map. Inc. 2024@	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 1/4/2025 8:34:33 PM Status: Color: Layer: Space:	tract A
m even. The combined flows will continue in a the start source local control of the pro- lated source of the source of the source of the source to 10% The project determine field in . How at DVb the dataset of the source of the source of the the proposed profiler matched (MH-3) is due to the PDR for Local. The bin intermit condition, so d to the sourthwest exiting the site into the exit	Subject: Callout Page Label: 9 Author: Daniel Torres Date: 1/4/2025 8:47:16 PM Status: Color: Layer:	tract B

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Interview           Image of the data of	Subject: Callout Page Label: 11 Author: Daniel Torres Date: 1/4/2025 9:47:53 PM Status: Color: Layer: Space:	Final sizing since this is the final drainage report.
<text></text>	Subject: Callout Page Label: 13 Author: Daniel Torres Date: 1/4/2025 10:50:34 PM Status: Color: Layer: Space:	Please submit with this final plat application. Please coordinate with Keith Curtis any requirements necessary for developing the roadway and pond within the floodplain.
And Mark Tay. Both Rear Rear Tay South Sou	Subject: Callout Page Label: 13 Author: Daniel Torres Date: 1/4/2025 10:23:12 PM Status: Color: Layer: Space:	Previous plats do not indicate that fees were paid, Regardless per ECM App. L, fees shall be paid for any increase in imperviousness. Previous development for the site was for softball fields. Please provide drainage basin fees due to the increase in impervious for lot 1 and the roadway Tracts are not assessed basin fees.
evelopment conditions Q <sub>2</sub> = 7.8 cfs, Q <sub>4</sub> cfs, Q <sub>100</sub> = 38.7 cfs). These propo or surrounding Developments and are 38.96 per drainage map	Subject: Callout Page Label: 15 Author: Daniel Torres Date: 1/4/2025 10:26:24 PM Status: Color: Layer: Space:	38.96 per drainage map
	Subject: Callout Page Label: [1] DR-02 Author: Daniel Torres Date: 1/4/2025 10:28:34 PM Status: Color: Layer: Space:	provide design point to properly compare the total flow in proposed conditions at this location with DP EX-1 of the existing conditions
A set of the set of th	Subject: Callout Page Label: 9 Author: Daniel Torres Date: 1/4/2025 10:37:18 PM Status: Color: Layer: Space:	Please also provide analysis of the interim condition to ensure drain times are met in this condition also. Identify if any changes to the orifice plate are needed between the interim and fully developed conditions



	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:43:55 PM Status: Color: Layer: Space:	Label all existing easements
1.4 Det word between example 6285	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:38:18 PM Status: Color: Layer: Space:	What is this? Please label or turn off
	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:38:42 PM Status: Color: Layer: Space:	Label existing structures
HIGHWAY 24 OFF F	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:43:29 PM Status: Color: Layer: Space:	Label roadside ditch
	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:40:37 PM Status: Color: Layer: Space:	Show and label existing structure conveying flows under roadway. Provide analysis of structure w/proposed detained flows and emergency overflow.
	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:41:16 PM Status: Color: Layer: Space:	What are these lines? Please label or turn off.

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Monte to have a former about or have of	Subject: Callout Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:43:58 PM Status: Color: Layer: Space:	What is this? Please label or turn off
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ing the Manning's channel flow exhainson, the size in the low modeled at Source(2004) RGL to the size in the size of the size	Subject: Callout Page Label: 11 Author: CDurham Date: 1/6/2025 4:33:59 PM Status: Color: Layer: Space:	Calculations were not seen in appendix. Please provide with next submittal.
Cloud+ (1)		
	Subject: Cloud+ Page Label: [1] DR-02 Author: Daniel Torres Date: 1/4/2025 9:13:22 PM	Due to the pond embankment, flow in the interim condition has been changed from historic. Please provide analysis of the flow and conveyance to the

## Contractor (5)

: under predevelopment lirection is to the southwest. 3d conveyed westward, discuss NC-1 and NC-2, if they will reated by the EDB or 1 an exclusio pplies. fbod. Runoff drains overland of the site where developed Subject: Contractor Page Label: 8 Author: Christina Prete Date: 1/2/2025 3:36:14 PM Status: Color: ■ Layer: Space:

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discuss NC-1 and NC-2, if they will be treated by the EDB or if an exclusion applies.

roadside ditch.

site is to be subdivided The proposed developn es. doesnt match GEC project is not located w ontains a small, paved oftball fields	Subject: Contractor Page Label: 4 Author: Christina Prete Date: 1/2/2025 4:24:37 PM Status: Color: ■ Layer: Space:	doesnt match GEC
Point excitos to region scattere la escate positiva escate despetitiva de la tableg escate de la construcción de la tableg escate de la construcción de la construcción de la construcción de la construcción de la construcci	Subject: Contractor Page Label: 26 Author: Christina Prete Date: 1/2/2025 4:55:46 PM Status: Color: ■ Layer: Space:	include workbook for interim conditions to ensure orifice plate is sized appropriately and not holding water
APPENDIX A THEOLOGIC NON FIGURE CLUCILITORS	Subject: Contractor Page Label: 18 Author: Christina Prete Date: 1/2/2025 5:05:55 PM Status: Color: ■ Layer: Space:	include forebay and trickle channel cals
	Subject: Contractor Page Label: [1] DR-02 Author: Christina Prete Date: 1/2/2025 5:12:44 PM Status: Color: ■ Layer: Space:	confirm inlet can handle all developed flows
Highlight (4)		
11. HGL	Subject: Highlight	
Prelim	Page Label: 7 Author: Daniel Torres	
usino	Date: 1/4/2025 3:37:51 PM Status: Color: Layer: Space:	
P2 is convey ia 3 <mark>6-inch</mark> R(	Subject: Highlight Page Label: 8 Author: CDurham Date: 1/6/2025 2:58:24 PM Status: Color: Layer: Space:	6-inch

cfs, Qu = 7.86 cfs) (sub-basin: PR-5; the discharge from sub-basin PR-5 into rulated assuming fully developed cond R 5 is non-proposed at the time. In full within sub-basin PR-5 will be directed in first-functure to be disapped with di- ated in sub-basin PR-5 drains overlaw worth side of the Highway 24 off ramp	Subject: Highlight Page Label: 9 Author: CDurham Date: 1/6/2025 3:07:39 PM Status: Color: Layer: Space: Subject: Highlight Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:41:29 PM Status:	not proposed at this time 5.12 34.39
Toyt Poy (14)	Layer: Space:	
nd i in fully will be dischared to this pediachared to this pediachared to associated with sub-basins NC-1 and NC-2. dt the southeast	Subject: Text Box Page Label: 9 Author: Daniel Torres Date: 1/4/2025 10:34:23 PM Status: Color: Layer: Space:	please discuss the design points associated with sub-basins NC-1 and NC-2.
	Subject: Text Box Page Label: 15 Author: Daniel Torres Date: 1/4/2025 10:49:44 PM Status: Color: Layer: Space:	<ul> <li>-Please provide analysis/ discussion of the east fork sand creek along the northern boundary of the site. Identify any improvements indicated in the DBPS. Is the creek stable, erosive, in need of improvements? is the crossing at Peterson adequate? Is this development responsible for any improvements to the creek (refer to DCMV1.4.2 ? please address.</li> <li>-Provide analysis of the 100yr floodplain at the proposed meadowbrook parkway. Ensure cross</li> </ul>
		flow in roadways for initial and major storms (DCMV1 table 6-1) is met.
(b) The point approach the dasharge from also have PR-5 transport functions of PR-1 is a semining field data have be adopted from the PR-1 is a semining field data have be address of the PR-1 is a seminimative seminimative memory model generated with the PR-1 behavior of the property of the PR-1 behavior of the memory of the PR-1 behavior of the PR-1 behavior results of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior results of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior results of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior results of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior results of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavior of the PR-1 behavioro	Subject: Text Box Page Label: 9 Author: CDurham Date: 1/6/2025 3:09:39 PM Status: Color: Layer: Space:	Indicate what interim flows are entering pond.
ditions is I. Include interim condition (No development to dracts A & B).	Subject: Text Box Page Label: 10 Author: CDurham Date: 1/6/2025 3:10:32 PM Status: Color: Layer: Space:	Include interim condition (No development to Tracts A & B).

No.         Description         Descriposcription         Description	Subject: Text Box Page Label: 12 Author: CDurham Date: 1/6/2025 3:13:43 PM Status: Color: Layer: Space:	How do flows from PR-5/DP 7 enter pond? Is forebay or rundown needed?
inue downstream and Provide analysis of roadside dith with this flow. Four Step Process for	Subject: Text Box Page Label: 12 Author: CDurham Date: 1/6/2025 3:14:19 PM Status: Color: Layer: Space:	Provide analysis of roadside ditch with this flow.
Marken Reg. ( 	Subject: Text Box Page Label: 10 Author: CDurham Date: 1/6/2025 3:16:54 PM Status: Color: Layer: Space:	Provide analysis of roadside ditch along Highway 24 with existing and proposed flows. Discuss if ditch still meets criteria with proposed flow
Bow of the Base Face Eventors	Subject: Text Box Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:44:06 PM Status: Color: Layer: Space:	Show and label Base Flood Elevations
Label Sand Creek	Subject: Text Box Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:44:27 PM Status: Color: Layer: Space:	Label Sand Creek
Provide additional contextu leader in the area and norm of 55 toe	Subject: Text Box Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:42:37 PM Status: Color: Layer: Space:	Provide additional contour labels in this area and north of SS line

HP or LP?	Subject: Text Box Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:42:59 PM Status: Color: Layer: Space:	HP or LP?
Sony and lated Base Flood Elevators 100 YEAR FLOODFL	Subject: Text Box Page Label: [1] DR-02 Author: CDurham Date: 1/6/2025 3:44:15 PM Status: Color: Layer: Space:	Show and label Base Flood Elevations
	Subject: Text Box Page Label: [1] DR-02 Author: CDurham Date: 1/6/2025 3:46:32 PM Status: Color: Layer: Space:	Address comments from previous sheet also.
Property information	Subject: Text Box Page Label: [1] DR-01 Author: CDurham Date: 1/6/2025 3:46:46 PM Status: Color: Layer: Space:	Property information