Preliminary Drainage Report

Villas at Aspen Trails El Paso County, Colorado

PCD File No.: PUDSP208 SF-21-025

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Prepared for:

ROS Equity Holdings – Independence, LLC 17 S. Wahsatch Avenue Colorado Springs, Colorado 80903

Prepared by: Kimley-Horn and Associates, Inc. 2 North Nevada Ave Suite 900 Colorado Springs, CO 80903 (719) 284-7273 Contact: Jared Roberts, P.E.

Project #: 096668022

Prepared: November 3, 2022

Kimley »Horn



Table of Contents

CERTIFICATION	.3
ENGINEERS STATEMENT DEVELOPER'S STATEMENT EL PASO COUNTY STATEMENT	.3
GENERAL LOCATION AND DESCRIPTION	.4
PURPOSE AND SCOPE OF STUDY LOCATION VICINITY MAP DESCRIPTION OF PROPERTY PROJECT CHARACTERISTICS	.4 .4 .4 .5
DRAINAGE BASINS AND SUB-BASINS	
MAJOR BASIN DESCRIPTIONS SUB-BASIN DESCRIPTION Historic Drainage Patterns Off-Site Drainage Flow Patterns	.5 .5 .6
DRAINAGE DESIGN CRITERIA	
DEVELOPMENT CRITERIA REFERENCE	
DRAINAGE FACILITY DESIGN	.6
GENERAL CONCEPT PROPOSED DRAINAGE PATTERNS Sub-Basin A1 Sub-Basin A2 Sub-Basin A3 Sub-Basin A4 Sub-Basin A5 Sub-Basin OS-1 Sub-Basin OS-2 EMERGENCY OVERFLOW ROUTING DETENTION AND WATER QUALITY Four-Step Process Detention and Water Quality Design Outlet Requirements Emergency Spillway Path COST OF PROPOSED DRAINAGE FACILITIES	.6 .7 .7 .7 .7 .7 .8 .8 .8 .8 .9 .9 .9 .9
COST OF PROPOSED DRAINAGE FACILITIES	.9
DRAINAGE AND BRIDGE FEES	.9
GRADING AND EROSION CONTROL1	0
MAINTENANCE AND OPERATIONS1	0
OTHER GOVERNMENT AGENCY REQUIREMENTS1	0

SUMMARY	10
COMPLIANCE WITH STANDARDS	10
REFERENCES	11
APPENDIX	12
APPENDIX A – FEMA FIRM MAP AND USGS SOILS MAP	13
APPENDIX B – SITE DRAINAGE CALCULATIONS (PROPOSED)	14
APPENDIX C – SITE DRAINAGE CALCULATIONS (EXISTING)	15
APPENDIX D – SITE DRAINAGE MAP (PROPOSED AND EXISTING)	
APPENDIX E – HYDRAULIC COMPUTATIONS	17
APPENDIX F – OPINION OF PROBABLE CONSTRUCTION COST	

CERTIFICATION

ENGINEERS STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

SIGNATURE (Affix Seal):

Colorado P.E. No. 60470

Date

DEVELOPER'S STATEMENT

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name

By:

Title:

Address:

EL PASO COUNTY STATEMENT

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code, as amended.

County Engineer/ECM Administrator

Date

Conditions:

GENERAL LOCATION AND DESCRIPTION

- Preliminary drainage report

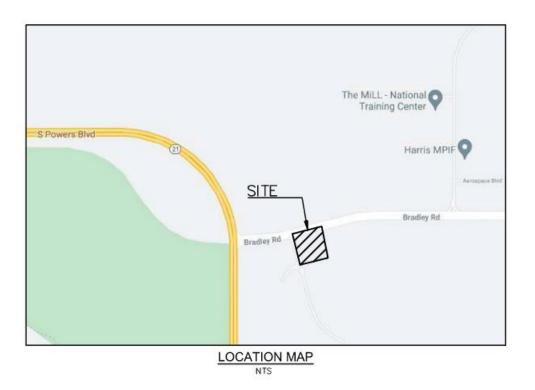
PURPOSE AND SCOPE OF STUDY

The purpose of this Final Drainage Report (FDR) is to provide the hydrologic and hydraulic calculations and to document and finalize the drainage design methodology in support of the proposed Villas at Aspen Trails residential development (the "Project"). The Project is located within the jurisdictional limits of El Paso County (the "County"). Thus, the guidelines for the hydrologic and hydraulic design were based on the criteria outlined by the County's Engineering Criteria Manual.

LOCATION

The Project is located south of the Colorado Springs Airport and at the southeast corner of Bradley Road and Legacy Hill Drive. More specifically, the Project is within portions of Section 8 & 9, Township 15 South, Range 65 West of the 6th Principal Meridian, County of El Paso, State of Colorado (parcel number 5509200003). A vicinity map is provided below.

VICINITY MAP



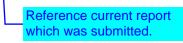
DESCRIPTION OF PROPERTY

The Project is located on approximately 4.25 acres of undeveloped land with limited vegetation and grass cover. The site is currently vacant and does not provide stormwater quality or detention and there are no known major drainage ways or irrigation facilities on the site. The proposed services in the development include the following: water, sewer, electric service,



natural gas service, telephone service, and fire protection. The site generally drains from the north to south with slopes ranging from 1.75% to 3.60%. The Project is no Indicate where flows do major drainageways and does not outfall directly to any major drainageways.

NRCS soil data is available for the Site (See Appendix) and the onsite soils are USCS Hydrologic Soil Group B. Group B soils have a moderate infiltration rate when thoroughly wet and mainly consist of well drained soils that have moderately fine texture to moderately coarse texture. This site specifically is predominately comprised of fine sandy loams, with a mix of stoneham sandy loam. A Soil, Geology, and Geologic Hazard report was prepared for the site by Entech Engineering, Inc. dated February 21, 2018 and is provided in the Appendix of this report for reference.



Delete this portion of sentence as it is not located within appendix.

PROJECT CHARACTERISTICS

The Project is a proposed single family attached development that will include single-family lots attached with private road access. The site will be configured in seven attached (townhome) 3-plex units across 21 lots and five attached (townhome) 4-plex units across 20 lots. The project will include the construction of tracts for buffering, landscaping, open spaces, pedestrian corridors, private roads, and a full spectrum extended detention pond to serve the Project. Water quaility and detention is required for the site improvements and will be accomplished with the construction of a full spectrum extended detention pond located on the southwest corner of the site. As part of the utility infrastructure improvements, a proposed storm sewer system will be constructed to collect runoff. Stormwater will be conveyed via overland flow across the lots, within the curb and gutter of the proposed streets before being captured in proposed storm pond before being discharged offsite.

DRAINAGE BASINS AND SUB-BASINS

MAJOR BASIN DESCRIPTIONS

The site is located within the Jimmy Camp Creek Basin. It is within the service area of the Widefield Water and Sanitation District (WWSD).

The Site is also located outside the 100-year floodplain and within Zone X (an area of minimal flood hazard) as noted on the FEMA FIRM Map No. 08041C0752G revised on December 7, 2018 (See Appendix).

There are no identified nearby irrigation facilities or other obstructions which could influence the local drainage.

SUB-BASIN DESCRIPTION

Historic Drainage Patterns

The existing drainage is divided into two sub-basins, Basin EX-1 and EX-2. Sub-Basin EX-1 is approximately 3.27 acres and consists of most of the on-site area within the property line. Runoff generated from this Sub-Basin drains overland from north to south. The weighted imperviousness for Sub-Basin EX-1 with existing conditions is 2% and the runoff for the 5-year and 100-year storm events are 1.33 cfs and 9.77 cfs respectively. Sub-Basin EX-2 is approximately 0.98 acres and consists of the northeast portion of this site. Runoff generated



from this Sub-Basin drains overland from west to east. The weighted imperviousness of Sub-Basin EX-2 is 2% and the runoff for the 5-year and 100-year storm events are 0.40 cfs and 2.97 cfs respectively.

Off-Site Drainage Flow Patterns

The site experiences offsite runoff from the north but is accounted for in proposed Sub-Basin A1. This offsite flow will be captured by the proposed storm sewer infrastructure and routed to the detention pond for water quality treatment and detention. See comments on drainage maps regarding offsite flows

DRAINAGE DESIGN CRITERIA

DEVELOPMENT CRITERIA REFERENCE

The proposed storm facilities follow the EI Paso County Drainage Criteria Manual (the "CRITERIA"), EI Paso Engineering Criteria Manual (the "ECM"), and the Mile High Flood Control District Urban Storm Drainage Criteria Manual (the "MANUAL"). Site drainage is not significantly impacted by such constraints as utilities or existing development. Further detail regarding onsite drainage patterns is provided in the Proposed Drainage Conditions Section.

HYDROLOGIC CRITERIA

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per chapter 6 of the CRITERIA. Table 6-2 of the CRITERIA is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the CRITERIA and MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the CRITERIA by calculating weighted impervious values for each specific site basin. The detention storage requirement was calculated using Full Spectrum Detention methods as specified in the CRITERIA and MANUAL. The Full Spectrum Extended Detention Basin's outlet structure will be designed to release the Water Quality Capture Volume (WQCV) in at least 40 hours and the EURV will be released with a 72 hour drain time. Outlet structure calculations will be provided in the Final Drainage Report. Based upon this approach, we feel that the drainage design provided for the Site is conservative and in keeping with the historic drainage patterns for the Site.

The proposed drainage facilities are designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using FIRM panels by FEMA. Hydraulic calculations will be computed using StormCAD for the proposed storm sewer system and provided in the Final Drainage Report.

DRAINAGE FACILITY DESIGN

GENERAL CONCEPT

PROPOSED DRAINAGE PATTERNS

The developed runoff from the Project will generally be collected by means of a curb and gutter and storm sewer system with inlets located on the west street within each delineated sub-basin area. Additionally, there will be a proposed 6' wide concrete v-gutter that captures flows and



routes them to a 8' curb cut to discharge directly into the detention pond. A proposed 6' vshaped vegetated swale will be located on the south portion of the project to direct the runoff to the detention pond. The runoff collected from each Sub-Basin A1 and A2 will be captured by storm inlets and conveyed through storm pipes to a Full Spectrum Extended Detention Basin located in the southwest corner of the site.

SPECIFIC DETAILS <

Please discuss how water quality and detention are provided (or excluded) for each sub-basin.

The property has been divided into seven sub-basins, A1 through A5 and OS-1 - OS-2. Subbasins A1 through A5 make up the Project on-site area and Sub-Basins OS-1 - OS-2 are the offsite basins consisting of the runoff that sheet flows offsite.

The weighted imperviousness of the Site area (Sub-basins A1 through A5) is 49.4%. The weighted imperviousness of the offsite area (Sub-basin OS1-OS2) with Sub-Basins A1 through A5 is 45.68%. Cumulative runoff for the 5-year and 100-year storm events are 8.02 cfs and 18.75 cfs, respectively.

Sub-Basin A1

This is a city type inlet. Please use a Type R inlets

Sub-basin A1 consists of approximately 0.84 acres and is the area along the north and central portions of the site, consisting of rooftops, landscaping, pavement, Road D and a portion of Road C. A Proposed 4' COS D-10-R storm inlet (Design point A1) on Road C captures this runoff and routes it to the detention pond. Developed runoff during the 5-year and 100-year events are 1.39 cfs and 3.32 cfs respectively.

Sub-Basin A2

Sub-basin A2 consists of approximately 0.45 acres and is made up of a portion of the west buildings along Road C, a portion of Road C, and a section of landscaping in the central portion of the site. A proposed 4' COS D-10-R storm inlet on Road C (Design Point A2) will capture the runoff from the roofs, landscaping, and pavement and route this runoff to the detention pond. Developed runoff during the 5-year and 100-year events are 0.69 cfs and 1.71 cfs respectively.

Sub-Basin A3

Sub-basin A3 consists of approximately 1.96 acres and is the south and eastern portions of the site, consisting of pavement, landscaping, roofing, Road A, Road B, and a portion of Road C. The runoff from this area is conveyed via curb and gutter before being collected by an 8-foot curb cut (Design point A3) that is discharged directly into the detention pond. Developed runoff during the 5-year and 100-year events are 5.17 cfs and 10.53 cfs respectively. With FDR will need to

Sub-Basin A4

Sub-basin A4 consists of approximately 0.40 acres and consists of runoff within the private detention basin. The runoff from this area is directly into the pond (Design Point A4). Developed runoff during the 5-year and 100-year events are 0.15 cfs and 1.10 cfs respectively.

Sub-Basin A5

Sub-basin A5 consists of approximately 0.15 acres and consists of landscaping and an associated drainage swale directed from east to west into the proposed detention pond. Developed runoff during the 5-year and 100-year events are 0.08 cfs and 0.40 cfs respectively.

Provide a design point that accounts for total flow into pond.

address if flow in c&g exceeds gutter capacity.

Sub-Basin OS-1

Sub-Basin OS-2

Sub-basin OS-1 consists of approximately 0.55 acres and consists of an eastern portion of the site which is vegetated hillside. Runoff will sheet flow to the portion of land that is east of the project (Design Point OS1), following historic drainage patterns. Developed runoff during the 5-year and 100-year events are 0.47 cfs and 1.58 cfs respectively.

Please discuss how water quality and detention are provided (or excluded) for each sub-basin.

Include where the flows go, intercepted, sheet flow, etc?

Sub-basin OS-2 consists of approximately 0.01 acres and consists of the western section of Road B that runs outside of the proposed property boundary. Runoff from this Sub-Basin is conveyed offsite to the intersection of Legacy Hill Drive and Road B (Design Point OS2). following historic drainage patterns. Developed runoff during the 5-year and 100-year events are 0.06 cfs and 0.11 cfs respectively.

Include where the flows go, intercepted, sheet flow, etc?

EMERGENCY OVERFLOW ROUTING

Emergency overflow routing consists of flows following historic drainage patterns from north to south and discharging into Frontside Drive.

DETENTION AND WATER QUALITY

The WQCV and 100-year detention is required for this Project. This is accomplished through the proposed private Full Spectrum Extended Detention Basin on the southwest corner of the Site. The Extended Detention Basin was sized to provide water quality and detention for the entire Site (Sub-Basins A1-A5 and OS-1 and OS-2) per UDFCD criteria. The water quality and detention calculations are provided in the Appendix of this report. The proposed Extended Detention Basin will be maintained by the homeowner's association. The label in the calcs on pg 50 below is

The label in the calcs on pg 50 below is "South Pond" add this to the report text and dwgs/maps for consistency.

Four-Step Process

The four-step process per the MANUAL provides guidance and requirements for the selection of siting of structural Construction Control Measures (CCMs) for new development and significant redevelopment.

Step 1: Employ Runoff Reduction Practices

Currently the site is vacant undeveloped land. Development of the site will increase current runoff conditions due to increased imperviousness values. However, implementation of landscaping throughout the site, the proposed storm sewer infrastructure, and the proposed Extended Detention Basin will help slow runoff and encourage infiltration.

Step 2: Provide Water Quality Capture Volume (WQCV)

The water quality capture volume will be detained using a full spectrum extended detention basin on the southwest corner of the Site. The water quality outlet structure will control the release of stormwater to at or less than historic rates.

Step 3: Stabilize Drainageways

There are no current drainageways conveyed through this property. No improvements to stabilize drainageways are a part of this Project.

Step 4: Consider need for Industrial and Commercial BMPs

Erosion control features for the final stages of the Project will be designed to reduce contamination. Source control BMPs will include the use of, inlet protection, silt fences,



concrete washout areas, stockpile management, and stabilized staging areas. The Grading and Erosion Control Plans will be submitted as a separate construction document set.

Detention and Water Quality Design

The proposed private Full Spectrum Extended Detention Basin will be designed with an outlet structure that is fitted with an orifice plate and restrictor plate to release the WQCV in at least a 40-hour drain time period and the EURV in a 72 hour drain time period per the MANUAL.

Calculations included in the Appendix provide details regarding the private water quality and detention basins design. The calculations include determination of the storage volumes required for full spectrum detention for the WQCV and 100 year detention and allowable release rates. The Final Drainage Report will provide calculations for the proposed outlet structure.

Overall, 0.352 acre-feet of WQCV is required. The total area contributing to the Extended Detention Basin consists of 3.80 acres (49.4% imperviousness).

Outlet Requirements

The water quality standards established by the CRITERIA are met by the proposed Full Spectrum Extended Detention Basin. The water quality outlet structures will be designed per the specifications in the CRITERIA. The outlet structure for the extended detention basin will meet the micro-pool requirement that it be integrated into the design of the structure with an additional initial surcharge volume. The orifice plates of the structures will be designed based on the CRITERIA. The orifice plates will allow the WQCV to be drained from the structure in at least 40 hours and the EURV in 72 hours. The calculations for the design of the outlet structures will be provided in the Final Drainage Report. Provide comparison of existing to proposed flows.

Emergency Spillway Path

The emergency overflow from the Extended Detention Basin will be located on the south side of the pond and will discharge into Frontside Drive. The Final Drainage Report will provide calculations on the emergency overflow spillway for the pond which will be located on the south side of the detention pond. In FDR, also include what happens to existing inlet & storm system with spillway flows.

COST OF PROPOSED DRAINAGE FACILITIES

An Estimated Opinion of Probable Construction Cost (EOPCC) is provided in the Appendix of the report. There are no public drainage facilities. All improvements with this Project will be private.

DRAINAGE AND BRIDGE FEES

Calculations will need to be provided as to how impervious acres were determined.

The Site is located in the Jimmy Camp Creek Drainage Basin. The total imperviou Full review of drainage & the parcel (5509200003) is 2.08 acres. The total drainage and bridge fees due for bridge fees will be \$36,449.92.

		2022 Fees (\$ / Impervious acre)	Impervious Area (Acre)	Amount Due (\$)
loes not ees for	Drainage Fee	\$9,185	2.08	\$19,104.80
ek Basin	Pond Facility Fee	\$8,339	2.08	\$17,345.12
		·	Total amount due:	\$36,449.92

Per my comment on the FAE:

Include a cost estimate for each PBMP with line items for all components (ex: riprap, road base, forebay, trickle channel, outlet structure, outlet pipe, spillway, etc). Input the total value into the FAE form under "Permanent Pond/BMP (provide engineer's estimate)" in Section 1. The total should not include grading, which is a separate line item in Section 1: "Earthwork."

GRADING AND EROSION CONTROL

The GEC plans will be submitted to El Paso County Planning and Community Development Department for review and approval prior to construction.

MAINTENANCE AND OPERATIONS

Maintenance of the extended detention basin is provided by the homeowner's association.

OTHER GOVERNMENT AGENCY REQUIREMENTS

Approval from other agencies such as the FEMA, the Army Corps of Engineers, Colorado State Engineer, Colorado Water Conservation Board, and others are not needed with this Project.

SUMMARY

The Project will provide water quality and detention for the Site per a full spectrum detention pond located in the southwest corner of the Site. The proposed cumulative 5-year runoff is 8.02 cfs and the cumulative 100-year runoff is 18.75 cfs. The overall imperviousness tributary to the pond is 49.4%, with a total site imperviousness of 45.7%.

COMPLIANCE WITH STANDARDS

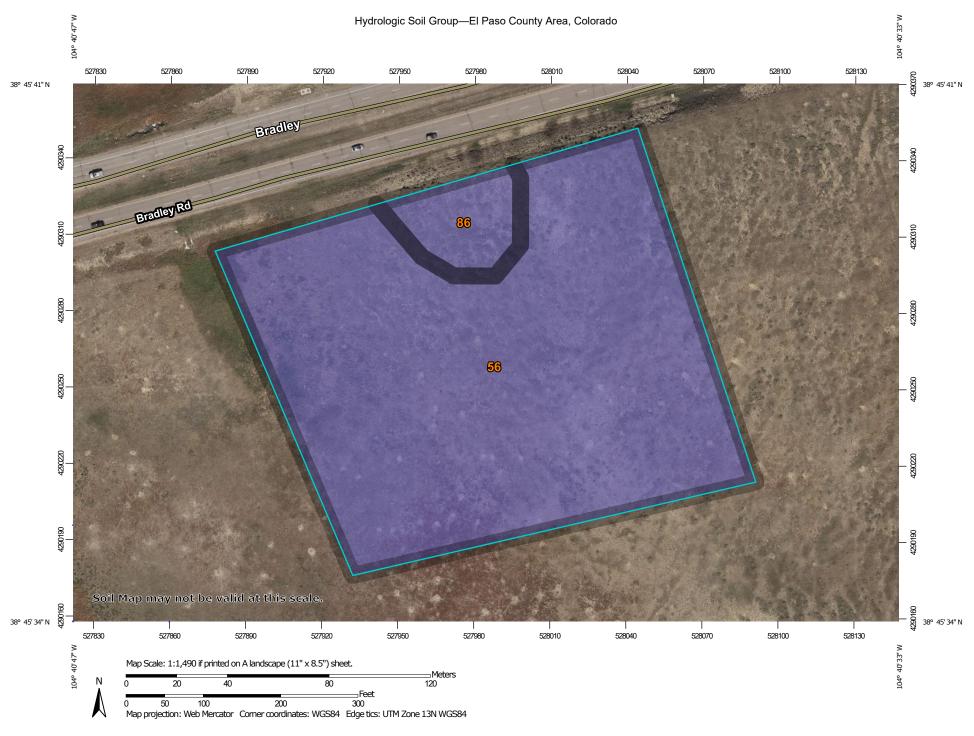
The drainage design presented within this report for Villas at Aspen Trails, conforms to the El Paso County Drainage Criteria Manual and the Mile High Flood District Urban Storm Drainage Criteria Manual. Additionally, the Site runoff and storm drain facilities will not adversely affect the downstream and surrounding developments. The proposed flows entering the extended detention basin will be released at or less than historic rates via an outlet structure which will be designed with the Final Drainage Report.

REFERENCES

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. El Paso County Drainage Criteria Manual, Vol. 1 and 2, October 1994.
- 3. Mile High Flood District Drainage Criteria Manual (MHFDCM), Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
- 4. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0459G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).

APPENDIX

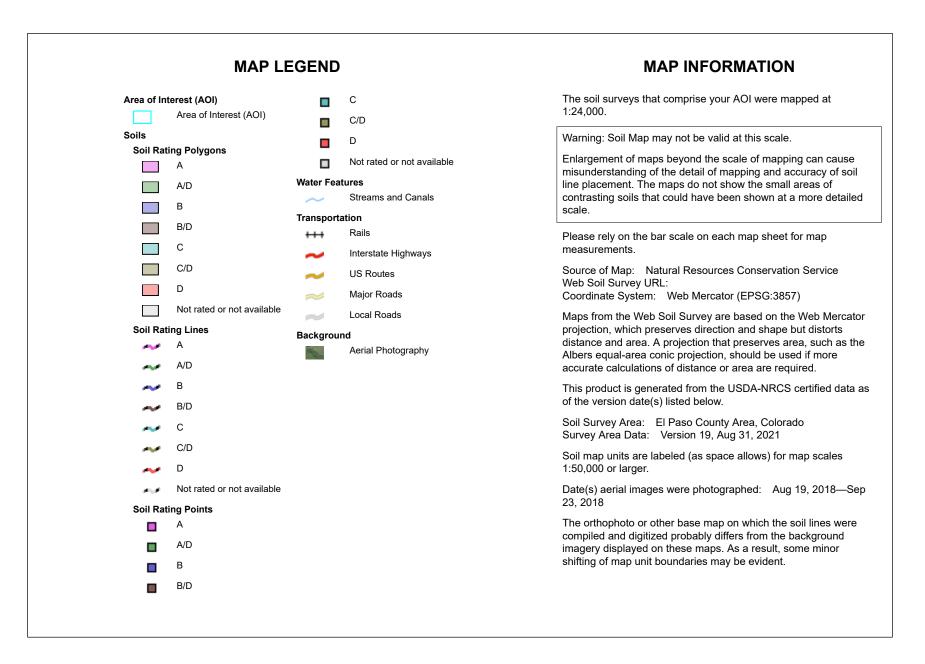
APPENDIX A – FEMA FIRM MAP AND USGS SOILS MAP



USDA Natural Resources

Conservation Service

Web Soil Survey National Cooperative Soil Survey 2/14/2022 Page 1 of 4



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	В	5.5	93.1%
86	Stoneham sandy loam, 3 to 8 percent slopes	В	0.4	6.9%
Totals for Area of Intere	est		5.9	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



National Flood Hazard Layer FIRMette



Legend

104°40'58"W 38°45'52"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF Area with Flood Risk due to Levee Zone D FLOOD HAZARD NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance <u>17.5</u> Water Surface Elevation EL PASO COUNTY **AREAOFMINIMAL FLOOD HAZARD Coastal Transect** 080059 Mase Flood Elevation Line (BFE) Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** OTHER **Profile Baseline** 08041C0768G FEATURES Hydrographic Feature eff. 12/7/2018 **Digital Data Available** No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 2/21/2022 at 7:00 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 104°40'21"W 38°45'24"N Feet 1:6.000 unmapped and unmodernized areas cannot be used for

250 500

n

1.500

1,000

2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

regulatory purposes.

APPENDIX B – SITE DRAINAGE CALCULATIONS (PROPOSED)

Move proposed calculations after existing calculations

IDF Equations:

I ₁₀₀ = -2.52In(D) + 12.735
I _{so} = -2.25In(D) + 11.375
I ₂₅ -2.00In(D) + 10.111
I₁₀ -1.75ln(D) + 8.847
l₅ -1.50ln(D) + 7.583
l₂ -1.19ln(D) + 6.035

Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P 1 =	1.19	1.5	1.75	2.52

Time Intensity Frequency Tabulation

Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

Villas at Aspen Trails Drainage Report El Paso County, CO

Weighted Imperviousness Calculations

	AREA	AREA	ROOF	ROOF		RO	OF		LANDSCAPE	LANDSCAPE		LAND	DSCAPE		PAVEMENT	PAVEMENT		PAVE	MENT		WEIGHTED		WEIGHTED	COEFFICIEN	ITS
SUB-BASIN	(SF)	(Acres)	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	IMPERVIOUSNESS	C2	C5	C10	C100
A1	36,687	0.84	8,090	90%	0.71	0.73	0.75	0.81	19,797	0%	0.02	0.08	0.15	0.35	8,800	100%	0.89	0.90	0.92	0.96	43.8%	0.38	0.42	0.47	0.60
A2	19,652	0.45	3,564	90%	0.71	0.73	0.75	0.81	11,350	0%	0.02	0.08	0.15	0.35	4,738	100%	0.89	0.90	0.92	0.96	40.4%	0.35	0.40	0.44	0.58
A3	85,176	1.96	24,866	90%	0.71	0.73	0.75	0.81	25,379	0%	0.02	0.08	0.15	0.35	34,931	100%	0.89	0.90	0.92	0.96	67.3%	0.58	0.61	0.64	0.73
A4	17,452	0.40	0	90%	0.71	0.73	0.75	0.81	17,452	0%	0.02	0.08	0.15	0.35	0	100%	0.89	0.90	0.92	0.96	0.0%	0.02	0.08	0.15	0.35
A5	6,520	0.15	0	90%	0.71	0.73	0.75	0.81	6,100	0%	0.02	0.08	0.15	0.35	420	100%	0.89	0.90	0.92	0.96	6.4%	0.08	0.13	0.20	0.39
OS1	24,090	0.55	0	90%	0.71	0.73	0.75	0.81	19,546	0%	0.02	0.08	0.15	0.35	4,544	100%	0.89	0.90	0.92	0.96	18.9%	0.18	0.23	0.30	0.47
OS2	602	0.01	0	90%	0.71	0.73	0.75	0.81	35	0%	0.02	0.08	0.15	0.35	567	100%	0.89	0.90	0.92	0.96	94.2%	0.84	0.85	0.88	0.92
(A1-A5)	165,487	3.80	36,520	90%	0.71	0.73	0.75	0.81	80,078	0%	0.02	0.08	0.15	0.35	48,889	100%	0.89	0.90	0.92	0.96	49.4%	0.43	0.47	0.51	0.63

Villas at A	Aspen Trails	- Drainag	e Report							Watercou	irse Coeffic	ient				
Proposed	d Runoff Cal	culations			Forest	& Meadow	2.50	Short G	rass Pastur	e & Lawns	7.00			Grasse	d Waterway	15.00
Time of C	Concentratio	n			Fallow or	Cultivation	5.00		Nearly Ba	re Ground	10.00		Paveo	l Area & Sha	allow Gutter	20.00
		SUB-BASIN			INIT	IAL / OVERL	AND	Т	RAVEL TIN	IE				T(c) CHECK		FINAL
		DATA				TIME			T(t)				(URE	BANIZED BA	SINS)	T(c)
DESIGN	DRAIN	AREA	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(t)	COMP.	TOTAL	L/180+10	
POINT	BASIN	sq. ft.	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	LENGTH		min.
A1	A1	36,687	0.84	0.42	100	0.4%	16.9	148	3.2%	20.00	3.6	0.7	17.6	248	11.4	11.4
A2	A2	19,652	0.45	0.40	20	1.3%	5.3	304	0.7%	7.00	0.6	8.7	14.0	324	11.8	11.8
A3	A3	85,176	1.96	0.61	70	2.4%	5.7	494	2.1%	20.00	2.9	2.8	8.5	564	13.1	8.5
A4	A4	17,452	0.40	0.08	67	13.8%	6.4	111	20.0%	7.00	3.1	0.6	7.0	178	11.0	7.0
A5	A5	6,520	0.15	0.13	18	6.0%	4.1	245	1.0%	7.00	0.7	5.8	9.9	263	11.5	9.9
OS1	OS1	24,090	0.55	0.23	100	2.5%	11.7	563	1.9%	7.00	1.0	9.7	21.4	663	13.7	13.7
OS2	OS2	602	0.01	0.85	33	3.6%	1.7	0	0.0%	20.00	0.0	0.0	5.0	33	10.2	5.0

Initial flow paths seem long for such a high density site. Please show flow paths on proposed map.

Proposed R	Illas at Aspen Trails - Drainage Report roposed Runoff Calculations Design Storm 5 Year ational Method Procedure)														
B	ASIN INFORMATIO	ON			DIRECT	RUNOFF		C	UMULATI	VE RUNO	FF				
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	СхА	l in/hr	Q cfs	T(c) min	СхА	l in/hr	Q cfs	NOTES			
A1	A1	0.84	0.42	11.4	0.35	3.93	1.39								
A2	A2	0.45	0.40	11.8	0.18	3.88	0.69								
A3	A3	1.96	0.61	8.5	1.19	4.37	5.17								
A4	A4	0.40	0.08	7.0	0.03	4.67	0.15								
A5	A5	0.15	0.13	9.9	0.02	4.14	0.08								
OS1	OS1	0.55	0.23	13.7	0.13	3.66	0.47								
OS2	OS2	0.01	0.85	5.0	0.01	5.17	0.06								

8.02

Villas at	Aspen Trails - Di	rainage	Report									
	d Runoff Calcula	-	•		Des	ign Storm	100 Year					
(Rational N	Aethod Procedure)											
E	ASIN INFORMATIO	N		DIF	RECT RUN	OFF		(CUMULATI	VE RUNOF	F	
DESIGN	DRAIN	AREA	RUNOFF	T(c)	СхА	I	Q	T(c)	СхА	I	Q	NOTES
POINT	BASIN	ac.	COEFF	min		in/hr	cfs	min		in/hr	cfs	
A1	A1	0.84	0.60	11.4	0.50	6.60	3.32					
A2	A2	0.45	0.58	11.8	0.26	6.52	1.71					
A3	A3	1.96	0.73	8.5	1.44	7.33	10.53					
A4	A4	0.40	0.35	7.0	0.14	7.83	1.10					
A5	A5	0.15	0.39	9.9	0.06	6.95	0.40					
OS1	OS1	0.55	0.47	13.7	0.26	6.14	1.58					
OS2	OS2	0.01	0.92	5.0	0.01	8.68	0.11					

18.75

esign points need to count for mulation of flow rough basins

	SUMMARY - PROPOSED RUNOFF TABLE											
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	BASIN IMP. (%)	100-YR RUNOFF COEF.						
Al	A1	0.84	1.39	3.32	43.8%	0.60						
A2	A2	0.45	0.69	1.71	40.4%	0.58						
> A3 -	A3	1.96	5.17	10.53	67.3%	0.73						
A4	A4	0.40	0.15	1.10	0.0%	0.35						
A5	A5	0.15	0.08	0.40	6.4%	0.39						
OS1	OS1	0.55	0.47	1.58	0.0%	0.47						
OS2	OS2	0.01	0.06	0.11	94.2%	0.92						
TOTAL		4.37	8.02	18.75								

APPENDIX C – SITE DRAINAGE CALCULATIONS (EXISTING)

IDF Equations:

I ₁₀₀ = -2.52In(D) + 12.735
I _{so} = -2.25In(D) + 11.375
I₂₅ -2.00In(D) + 10.111
I₁₀ -1.75ln(D) + 8.847
l₅ -1.50ln(D) + 7.583
l₂ -1.19ln(D) + 6.035

Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P1 =	1.19	1.5	1.75	2.52

Time Intensity Frequency Tabulation

			<u> </u>			
Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

Ray O 5.2 Single Family Attached Drainage Report El Paso County, CO

Weighted Imperviousness Calculations

	AREA	AREA	ROOF	ROOF		RO	OF		LANDSCAPE	LANDSCAPE		LAND	SCAPE		PAVEMENT	PAVEMENT		PAVE	MENT		WEIGHTED		WEIGHTED	COEFFICIEN	ITS
SUB-BASIN	(SF)	(Acres)	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	IMPERVIOUSNESS	C2	C5	C10	C100
E1	142,523	3.27	0	90%	0.71	0.73	0.75	0.81	140,089	2%	0.02	0.08	0.15	0.35	0	100%	0.89	0.90	0.92	0.96	2.0%	0.02	0.08	0.15	0.34
E2	42,715	0.98	0	90%	0.71	0.73	0.75	0.81	42,634	2%	0.02	0.08	0.15	0.35	0	100%	0.89	0.90	0.92	0.96	2.0%	0.02	0.08	0.15	0.35

sting																
Ray 0 5.2	Single Fan	nily Attach	ed - Drair	nage Rep	ort					Watercou	Irse Coeffic	ient				
Proposed	Runoff Cal	culations			Forest	& Meadow	2.50	Short Gr	rass Pastur	e & Lawns	7.00			Grasse	d Waterway	15.00
Time of C	oncentratio	on			Fallow or	Cultivation	5.00		Nearly Ba	re Ground	10.00		Paveo	l Area & Sha	allow Gutter	20.00
		SUB-BASIN			INITIAL / OVERLAND			Т	RAVEL TIN	1E				T(c) CHECK		FINAL
		DATA			TIME			T(t)				(URBANIZED BASINS)		T(c)		
DESIGN	DRAIN	AREA	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(t)	COMP.	TOTAL	L/180+10	
POINT	BASIN	sq. ft.	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	LENGTH		min.
1	E1	142,523	3.27	0.08	0	17.0%	0.0	431	2.5%	20.00	3.2	2.3	5.0	431	12.4	5.0
2	E2	42,715	0.98	0.08	0	12.0%	0.0	141	2.4%	20.00	3.1	0.8	5.0	141	10.8	5.0

Existing												
	Single Family A Runoff Calculat thod Procedure)	ttached ions	- Drainage	e Repoi	rt Desi	gn Storm	5 Year					
B	ASIN INFORMATIO	DN			DIRECT	RUNOFF		C	UMULATI	VE RUNO	FF	
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	СхА	l in/hr	Q cfs	T(c) min	СхА	ا in/hr	Q cfs	NOTES
1	E1	3.27	0.08	5.0	0.26	5.17	1.33					
2	E2	0.98	0.08	5.0	0.08	5.17	0.40					

1.73

— Existing

Ray O 5 Z Single Family Attached - Drainage Report

Proposed Runoff Calculations

Design Storm 100 Year

(Rational Method Procedure)

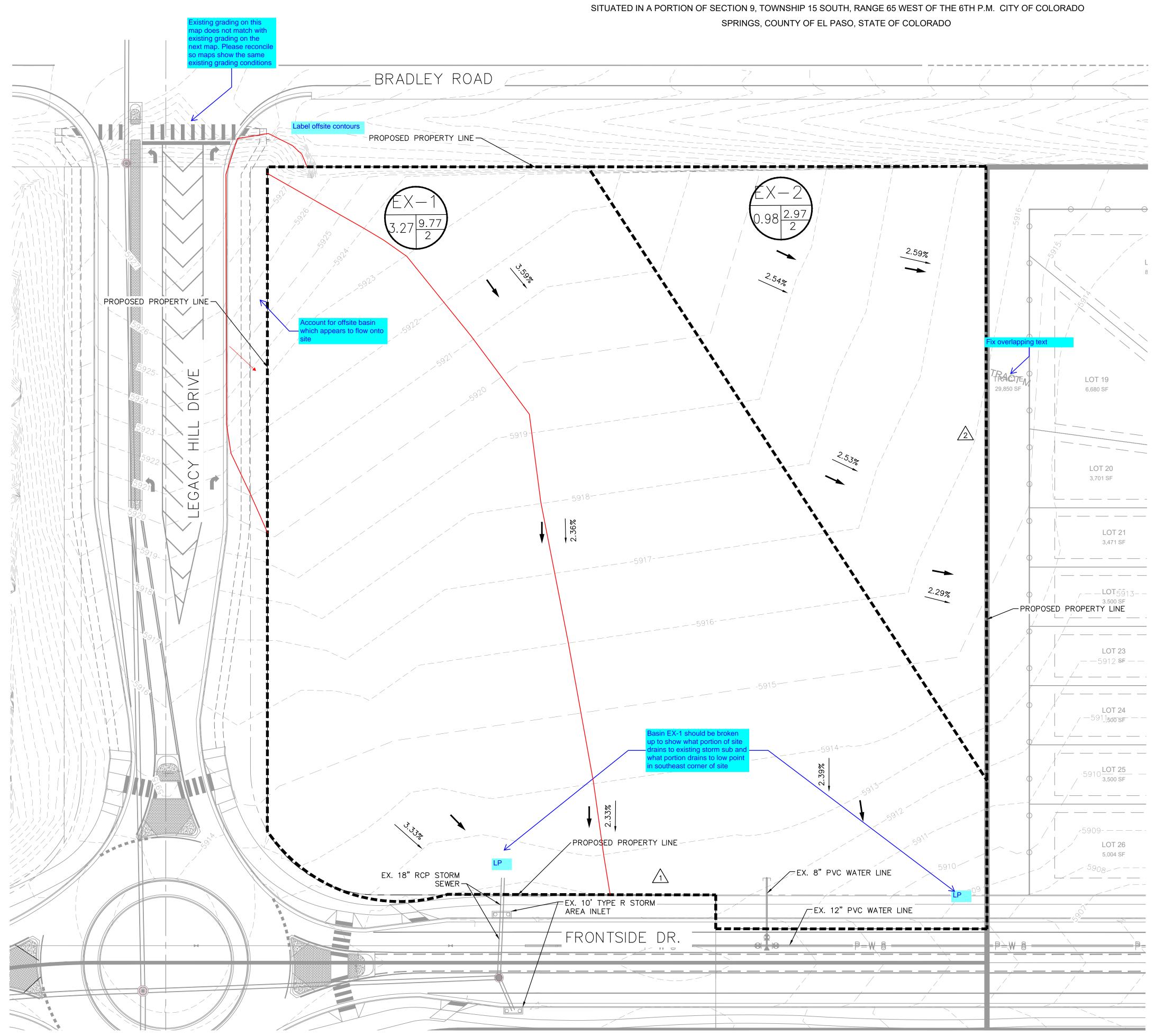
F	BASIN INFORMATIO	DIR	RECT RUN)FF		(CUMULATI	VE RUNOF	F			
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c)	CxA	I in/hr	Q cfs	T(c) min	CxA	I in/hr	Q cfs	NOTES
1	E1	3.27	0.34	5.0	1.13	8.68	9.77			,		
2	E2	0.98	0.35	5.0	0.34	8.68	2.97					

12.74

	Existing		_								
SUMMARY - PROPOSED RUNOFF TABLE											
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	BASIN IMP. (%)	100-YR RUNOFF COEF.					
1	E1	3.27	1.33	9.77	0.02	0.34					
2	E2	0.98	0.40	2.97	0.02	0.35					
TOTAL		4.25	1.73	12.74							

APPENDIX D – SITE DRAINAGE MAP (PROPOSED AND EXISTING)

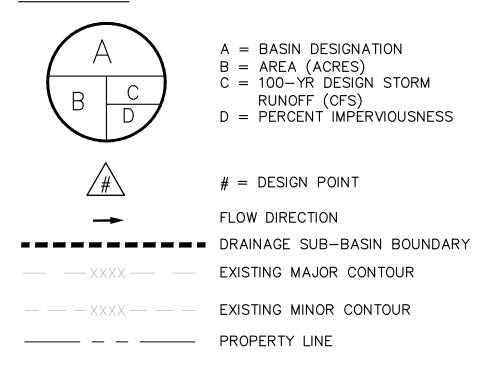
Move maps to end of report



RAY O 5.2 SINGLE FAMILY ATTACHED

EXISTING DRAINAGE EXHIBIT

LEGEND



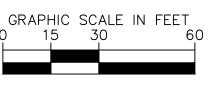
SUMMARY - PROPOSED RUNOFF TABLE

DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)		DIRECT 100-YR RUNOFF (CFS)	BASIN IMP. (%)	100-YR RUNOFF COEF.
1	E1	3.27	1.33	9.77	0.02	0.34
2	E2	0.98	0.40	2.97	0.02	0.35

Label adjacent property owners.

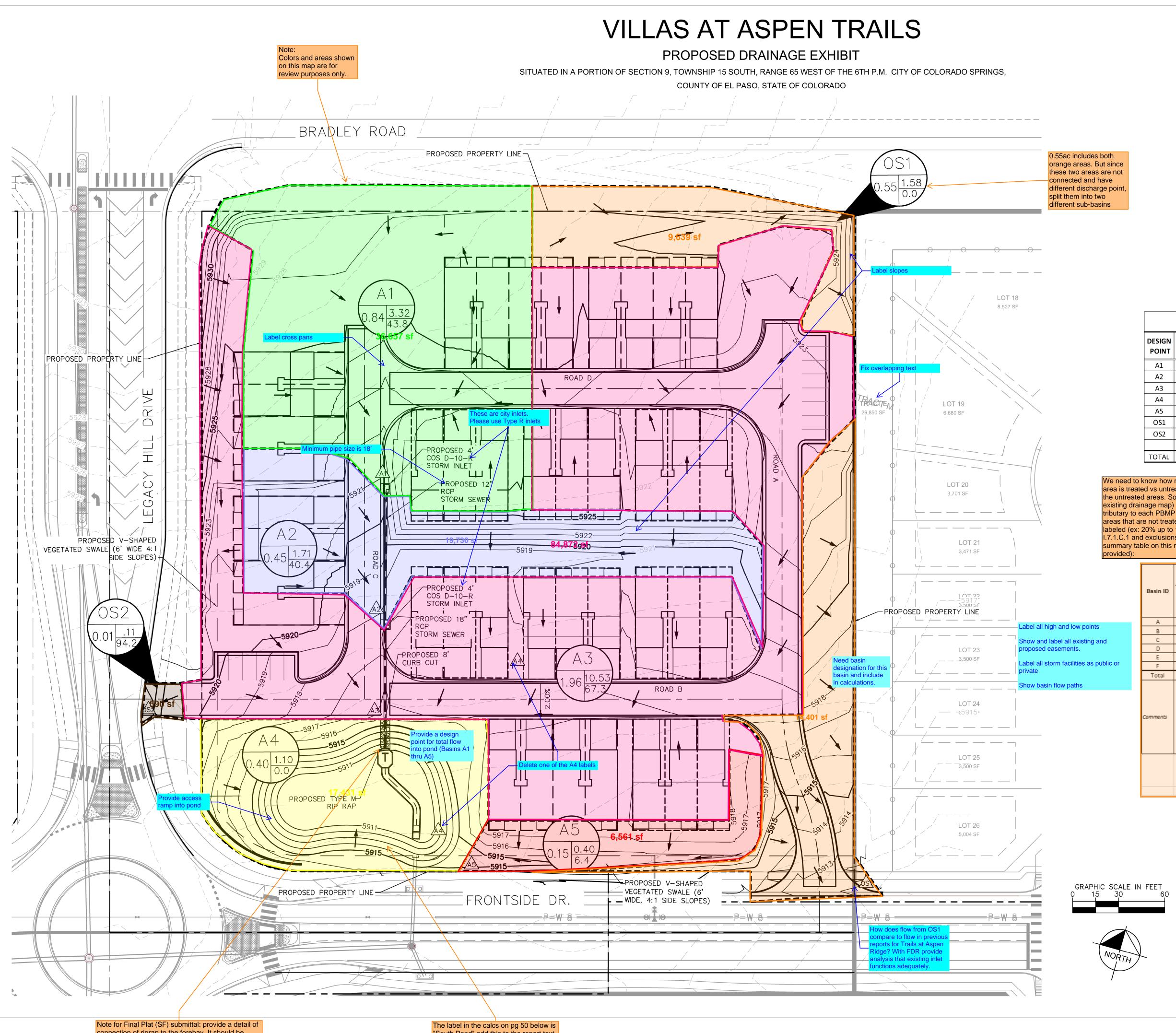
Show and label all existing easements

Label high and low points





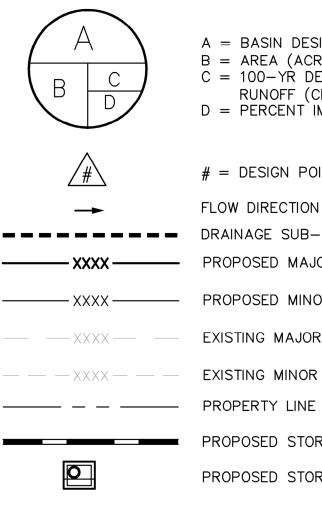




connection of riprap to the forebay. It should be designed such that the water does not pond behind the forebay wall and thus contribute to erosion around the sidewalls.

The label in the calcs on pg 50 below is "South Pond" add this to the report text and dwgs/maps for consistency.





RUNOFF (CFS) D = PERCENT IMPERVIOUSNESS # = DESIGN POINTFLOW DIRECTION DRAINAGE SUB-BASIN BOUNDARY -XXXX ------ PROPOSED MAJOR CONTOUR EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR PROPOSED STORM SEWER

A = BASIN DESIGNATION

B = AREA (ACRES)C = 100-YR DESIGN STORM

PROPOSED STORM INLET

	SUMMARY - PROPOSED RUNOFF TABLE											
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	BASIN IMP. (%)	100-YR RUNOFF COEF.						
A1	A1	0.84	1.39	3.32	43.8%	0.60						
A2	A2	0.45	0.69	1.71	40.4%	0.58						
A3	A3	1.96	5.17	10.53	67.3%	0.73						
A4	A4	0.40	0.15	1.10	0.0%	0.35						
A5	A5	0.15	0.08	0.40	6.4%	0.39						
OS1	OS1	0.55	0.47	1.58	0.0%	0.47						
OS2	OS2	0.01	0.06	0.11	94.2%	0.92						
TOTAL		4.37	8.02	18.75								

We need to know how much of the proposed disturbed (not impervious) area is treated vs untreated and if there are any exclusions that apply to he untreated areas. So please create a basic overview map (or modify ar existing drainage map) with color shading/hatching that shows areas tributary to each PBMP (pond, runoff reduction, etc.) and those disturbed areas that are not treated by a PBMP, with the applicable exclusion labeled (ex: 20% up to 1ac of development can be excluded per ECM App I.7.1.C.1 and exclusions listed in ECM App I.7.1.B.#). An accompanying summary table on this map would also be very helpful (examples

	Basin ID	Total Area (ac)	Total Proposed Disturbed Area (ac)	Area Trib to Pond A (ac)	Distunbed Area Treated via Runoff Reduction (ac)	Disturbed Area Excluded from WQ per ECM App I.7.1.C.1 (ac)	Excluded from	Applicable WQ Exclusions (App I.7.1.B.#)
nts	A	4.50	4.50	4.50	-	-	-	
11.5	В	1.25	1.25	-	1.25	-	-	
g and	C	6.00	4.00	-	-	-	4.00	ECM App I.7.1.B.5
	D	2.50	2.50	1.00	-	0.50	1.00	ECM App I.7.1.B.7
, auchlie ex	E	3.00	-	3.00	-	-	-	
s public or	F	8.25	-	-	-	-	-	
	Total	25.50	12.25	8.50	1.25	0.50	5.00	
	Comments		values in Columns 4-7 must be greater than or equal to the value in	[Values in this column can be more than Column 3 if over- treating non- disturbed areas of the same land- use.]	[See RR calc spreadsheet.]	[Total must be <20% of site and <1ac.]		
			Total Proposed Disturbed Area (ac)	Total Proposed Treated Area (ac)		Total Proposed Disturbed Area Excluded from WQ (ac)		Non-Excluded Areato be Treated (value must ≤ Total Proposed Treated Area) (ac)
			12.25	9.	.75	5.	50	6.75

PBMP BASINS A1.1 A3.1 B1,B2 OA2,A2	SUMMARY PBMP TRIBUTARY AREA (AC) 1.43 1.87 8.60 0.95							
 EXCLUDED BASED ON < 1-ACRE OF DEVELOPED ROADWAY AREA PER ECM APP. 17.C.1.g 								



COLORADO SPRINGS, COLORADO 80903 (719) 453-0180

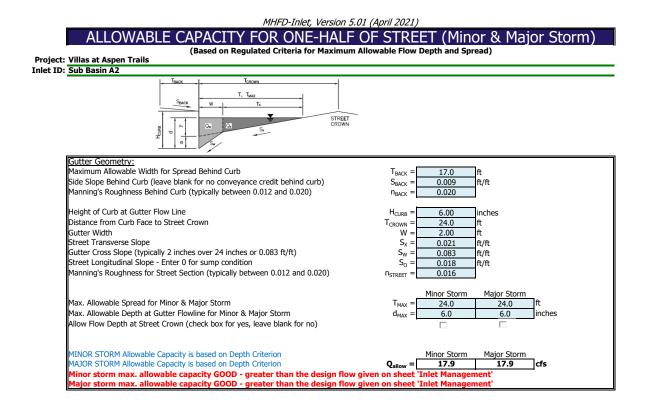
APPENDIX E – HYDRAULIC COMPUTATIONS

Hydraulic computations will be fully reviewed with final drainage report. Some initial comments have been provided.

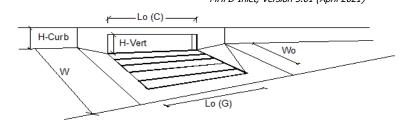
Deale at Danami, ti		
Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.020 ft/ft	
Diameter	12.0 in	
Discharge	2.10 cfs	
Results		
Normal Depth	5.4 in	
Flow Area	0.3 ft ²	
Wetted Perimeter	1.5 ft	
Hydraulic Radius	2.8 in	
Top Width	1.00 ft	
Critical Depth	7.4 in	
Percent Full	45.0 %	
Critical Slope	0.007 ft/ft	
Velocity	6.12 ft/s	
Velocity Head	0.58 ft	
Specific Energy	1.03 ft	
Froude Number	1.837	
Maximum Discharge	5.42 cfs	
Discharge Full	5.04 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.0 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.4 in	
Critical Depth	7.4 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.007 ft/ft	

Worksheet for Storm Line A1-2

CurbCut-FlowMaster.fm8 11/3/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666



INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input) Colorado Springs D-10-R		MINOR	MAJOR	
Type of Inlet	Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	4.0	4.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	4.00	4.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _F G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.8	1.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	1.0	cfs
Capture Percentage = Q_a/Q_a =	C% =	100	65	%

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		How was this flow determined?
Roughness Coefficient	0.013	Does not match flow on hydrology
Channel Slope	0.005 ft/ft	spreadsheets for Design Point A3
Bottom Width	8.00 ft	
Discharge	15.53 cfs	
Results		
Normal Depth	5.3 in	
Flow Area	3.5 ft ²	
Wetted Perimeter	8.9 ft	
Hydraulic Radius	4.8 in	
Top Width	8.00 ft	
Critical Depth	5.9 in	
Critical Slope	0.004 ft/ft	
Velocity	4.38 ft/s	
Velocity Head	0.30 ft	
Specific Energy	0.74 ft	
Froude Number	1.161	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.3 in	
Critical Depth	5.9 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.004 ft/ft	

Worksheet for Design Point A3 Curb Cut

Deale at Danami, ti		
Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.020 ft/ft	
Diameter	12.0 in	
Discharge	2.10 cfs	
Results		
Normal Depth	5.4 in	
Flow Area	0.3 ft ²	
Wetted Perimeter	1.5 ft	
Hydraulic Radius	2.8 in	
Top Width	1.00 ft	
Critical Depth	7.4 in	
Percent Full	45.0 %	
Critical Slope	0.007 ft/ft	
Velocity	6.12 ft/s	
Velocity Head	0.58 ft	
Specific Energy	1.03 ft	
Froude Number	1.837	
Maximum Discharge	5.42 cfs	
Discharge Full	5.04 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.0 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.4 in	
Critical Depth	7.4 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.007 ft/ft	

Worksheet for Storm Line A1-2

CurbCut-FlowMaster.fm8 11/3/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.020 ft/ft	
Diameter	18.0 in	
Discharge	4.00 cfs	
Results		
Normal Depth	6.4 in	
Flow Area	0.6 ft ²	
Wetted Perimeter	1.9 ft	
Hydraulic Radius	3.5 in	
Top Width	1.44 ft	
Critical Depth	9.2 in	
Percent Full	35.4 %	
Critical Slope	0.005 ft/ft	
Velocity	7.13 ft/s	
Velocity Head	0.79 ft	
Specific Energy	1.32 ft	
Froude Number	2.012	
Maximum Discharge	15.98 cfs	
Discharge Full	14.85 cfs	
Slope Full	0.001 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	35.4 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	6.4 in	
Critical Depth	9.2 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.005 ft/ft	

Worksheet for Storm Line A2-3

CurbCut-FlowMaster.fm8 11/3/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

	Ternsheet	
Project Description		
Friction Method	Manning	
	Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.080 ft/ft	
Normal Depth	6.0 in	
Left Side Slope	50.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	84.81 cfs 📉	
Flow Area	6.6 ft ²	
Wetted Perimeter	26.6 ft	、 、
Hydraulic Radius	3.0 in	Where did these flows
Top Width	26.50 ft	come from?
Critical Depth	11.0 in	come nom:
Critical Slope	0.003 ft/ft	
Velocity	12.80 ft/s	
Velocity Head	2.55 ft	
Specific Energy	3.05 ft	
Froude Number	4.514	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	6.0 in	
Critical Depth	11.0 in	
Channel Slope	0.080 ft/ft	
Critical Slope	0.003 ft/ft	

Worksheet for Swale A1 proposed drainage map

Show and label swale on

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.020 ft/ft	
Normal Depth	9.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	10.000 H:V	
Results		
Discharge	13.18 cfs	
Flow Area	3.7 ft ²	
Wetted Perimeter	9.9 ft	
Hydraulic Radius	4.4 in	Flows do not match with
Top Width	9.75 ft	hydrology spreadsheet for
Critical Depth	9.1 in	basin or design point A2
Critical Slope	0.018 ft/ft	
Velocity	3.60 ft/s	
Velocity Head	0.20 ft	
Specific Energy	0.95 ft	
Froude Number	1.037	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	9.0 in	
Critical Depth	9.1 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.018 ft/ft	

Worksheet for Swale A2

Show and label swale on

proposed drainage map

CurbCut-FlowMaster.fm8 9/19/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

	worksneet	
Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.007 ft/ft	Map calls out 4:1 sides
Normal Depth	7.0 111	Map Calls Out 4.1 Sides
Left Side Slope	5.000 H:V	
Right Side Slope	50.000 H:V	
Results		
Discharge	17.03 cfs	
Flow Area	9.4 ft ²	
Wetted Perimeter	32.1 ft	
Hydraulic Radius	3.5 in	
Top Width	32.08 ft	Flows do not match with
Critical Depth	5.7 in	
Critical Slope	0.021 ft/ft	hydrology spreadsheet for basin or design point A3
Velocity	1.82 ft/s	basin of design point AS
Velocity Head	0.05 ft	
Specific Energy	0.63 ft	
Froude Number	0.594	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	7.0 in	
Critical Depth	5.7 in	
Channel Slope	0.007 ft/ft	
Critical Slope	0.021 ft/ft	

Worksheet for Swale A3

CurbCut-FlowMaster.fm8 9/19/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

		et for Swale AS
Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	— Map calls out 4:1 sides
Channel Slope	0.020 ft/ft	
Normal Depth	12.0 in	
Left Side Slope	8.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	23.94 cfs	
Flow Area	5.5 ft ²	
Wetted Perimeter	11.2 ft	
Hydraulic Radius	5.9 in	
Top Width	11.00 ft	Flows do not match with
Critical Depth	12.4 in	hydrology spreadsheet for
Critical Slope	0.017 ft/ft	basin or design point A3
Velocity	4.35 ft/s	
Velocity Head	0.29 ft	
Specific Energy	1.29 ft	
Froude Number	1.085	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	12.0 in	
Critical Depth	12.4 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.017 ft/ft	

Worksheet for Swale A5

CurbCut-FlowMaster.fm8 9/19/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Kimley »	lorn											
Extended Detent	ion Basin (EDB)	Calculations										
Prepared By	11/3/2022 JAR JAR		Manual Input Multipliers									
Release Factor:	0.02											
undetained 100-year	and Configuration: I r peak discharge by w erm/pipe configuratio	vay of a wall/notch or										
Forebay	Incoming Pipe Diameter (in)	Release Rate (cfs)										
Α	18	0.31										
					I							
	IV	laximum Forebay Dep	oth									
Forebay	Impervious Area in Watershed (ac)	Maximum Forebay Depth (in)	Design Forebay Depth (in)		Note: a forebay depth of 30" requires handrails by most City Standards							
Α	1.96	12	12	1								
					. \							
	I	Baffle Block Design	T. T									
Forebay	Incoming Pipe Diameter (in)	1/4 of Diameter	Side length (in)	Height (in)	County							
A	18	4.5	8.00	9								
			Minigarum		nuired, 2% MOCV					Maluma Fasta	0.02	
		[IVIINIMUM F	orebay Volume Red	quirea: 3% wQCV	Con	ner Calculations			Volume Factor:	0.03	
Forebay	WQCV (ac-ft)	Required Volume (ac ft)	Required Volume (cf)	Total Length (ft)	Total Width (ft)	Triangle Height (ft)	Triangle Base	Triangle Area (sf)	Design Volume (cf)			
Α	0.065	0.002	85	12	9	2.5	2.5	3.125	95.5	1		
			•									

MHFD-Detention, Version 4.04 (February 2021)

Project:	Villas at Aspen Trails
Basin ID:	South Pond
	2 ONE 1

-100-YEAR ORIFICE ZONE 1 AND 2-ORIFICES PERMA Example Zone Configuration (Retention Pond)

Watershed Information

tersneu information		
Selected BMP Type =	EDB	
Watershed Area =	3.80	acres
Watershed Length =	500	ft
Watershed Length to Centroid =	250	ft
Watershed Slope =	0.035	ft/ft
Watershed Imperviousness =	49.40%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colo		giapinnocca	ure.
Water Quality Capture Ve	olume (WQCV) =	0.065	acre-feet
Excess Urban Runoff V	olume (EURV) =	0.200	acre-feet
2-yr Runoff Volume	(P1 = 1.19 in.) =	0.180	acre-feet
5-yr Runoff Volume	e (P1 = 1.5 in.) =	0.257	acre-feet
10-yr Runoff Volume	(P1 = 1.75 in.) =	0.326	acre-feet
25-yr Runoff Volume	(P1 = 1.69 in.) =	0.327	acre-feet
50-yr Runoff Volume	(P1 = 1.99 in.) =	0.415	acre-feet
100-yr Runoff Volume	(P1 = 2.52 in.) =	0.587	acre-feet
500-yr Runoff Volume	(P1 = 3.14 in.) =	0.780	acre-feet
Approximate 2-yr Det	ention Volume =	0.151	acre-feet
Approximate 5-yr Det	ention Volume =	0.207	acre-feet
Approximate 10-yr Det	ention Volume =	0.275	acre-feet
Approximate 25-yr Det	ention Volume =	0.255	acre-feet
Approximate 50-yr Det	ention Volume =	0.279	acre-feet
Approximate 100-yr Det	ention Volume =	0.352	acre-feet

Define Zones and Basin Geometry

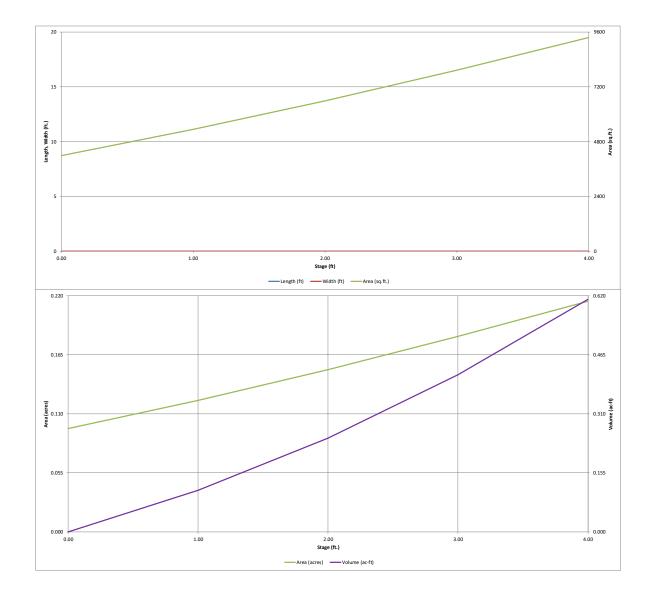
Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.065	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.136	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.152	acre-feet
Total Detention Basin Volume =	0.352	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

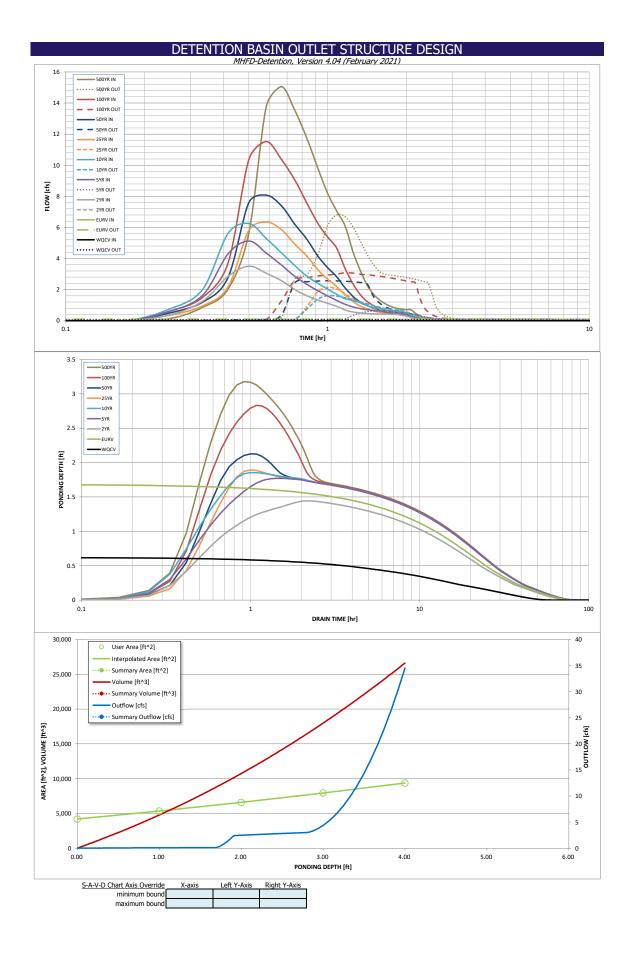
R	Depth Increment =		ft							
tion Pond)	Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
	Top of Micropool		0.00	-			4,193	0.096	4.765	0.400
			1.00 2.00				5,337 6,581	0.123	4,765 10,724	0.109
			3.00	-		-	7,925	0.131	17,977	0.413
			4.00				9,371	0.215	26,625	0.611
				-	-	-				
				-						
Optional User Overrides acre-feet				-	-					
acre-feet				-						
1.19 inches						-				
1.50 inches										
1.75 inches										
inches inches				-				-		
2.52 inches				-	-	-		-		
inches				-	-					
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN									
Project	Villas at Aspen Tra		D-Detention, Vers	sion 4.04 (Februar	y 2021)				
-	South Pond	lis							
ZONE 3 ZONE 2				Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	0.63	0.065	Orifice Plate			
	100-YEAR		Zone 2 (EURV)	1.69	0.136	Circular Orifice			
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	2.66	0.152	Weir&Pipe (Restrict)			
POOL Example Zone	Configuration (Re			Total (all zones)	0.352	·····			
User Input: Orifice at Underdrain Outlet (typically	y used to drain WQ	CV in a Filtration BM	1P)				Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =	N/A	ft (distance below t	the filtration media	surface)	Underd	rain Orifice Area =	N/A	ft ²	
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orifice			-			ce Area per Row =	Calculated Parame		
Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate =		ft (relative to basin ft (relative to basin	-		•	ptical Half-Width =	N/A N/A	ft ² feet	
Orifice Plate: Orifice Vertical Spacing =	2.50	inches	- bottom ut bitage -	010)		cal Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	inches				lliptical Slot Area =	N/A	ft ²	
								1	
User Input: Stage and Total Area of Each Orifice	Row (numbered fr	om lowest to highe	<u>st)</u>						-
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.21	0.42						-
Orifice Area (sq. inches)	0.79	0.79	0.79						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)	Row 9 (optional)	Row 10 (optional)	Row II (optional)	Row 12 (optional)	Row 15 (optional)	(optional)	Row 15 (optional)	Now 10 (optional)	
Orifice Area (sq. inches)									
				•					
User Input: Vertical Orifice (Circular or Rectange							Calculated Parame	ters for Vertical Ori	ifice
	Zone 2 Circular	Not Selected					Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	0.63		•	bottom at Stage =		tical Orifice Area =	0.00	N/A	ft ²
Depth at top of Zone using Vertical Orifice = Vertical Orifice Diameter =	1.69 0.47		inches	bottom at Stage =	UTC) Vertical	Orifice Centroid =	0.02	N/A	feet
	0.47	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and	Outlet Pipe OR Rect	angular/Trapezoida	al Weir (and No Out	let Pipe)		Calculated Parame	ters for Overflow W	Veir
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and C Zone 3 Weir	Outlet Pipe OR Rect Not Selected	angular/Trapezoida	al Weir (and No Out	let Pipe)_		Calculated Parame Zone 3 Weir	ters for Overflow W Not Selected	<u>Veir</u>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 1.69	Not Selected N/A		al Weir (and No Out		e Upper Edge, H _t =	Zone 3 Weir 1.69	Not Selected N/A	<u>Veir</u> feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	Zone 3 Weir 1.69 4.00	Not Selected N/A N/A	ft (relative to basin t feet	pottom at Stage = 0 f	t) Height of Grati Overflow W	eir Slope Length =	Zone 3 Weir 1.69 2.92	Not Selected N/A N/A]
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	Zone 3 Weir 1.69 4.00 0.00	Not Selected N/A N/A N/A	ft (relative to basin t feet H:V	oottom at Stage = 0 f Gr	t) Height of Grati Overflow W ate Open Area / 10	eir Slope Length = 0-yr Orifice Area =	Zone 3 Weir 1.69 2.92 20.70	Not Selected N/A N/A N/A	feet feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 1.69 4.00 0.00 2.92	Not Selected N/A N/A N/A N/A	ft (relative to basin t feet	pottom at Stage = 0 f Gr ດາ	t) Height of Grati Overflow W ate Open Area / 10 verflow Grate Open	eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 1.69 2.92 20.70 8.13	Not Selected N/A N/A N/A N/A	feet feet ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate	Not Selected N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet	pottom at Stage = 0 f Gr ດາ	t) Height of Grati Overflow W ate Open Area / 10	eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 1.69 2.92 20.70	Not Selected N/A N/A N/A	feet feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 1.69 4.00 0.00 2.92	Not Selected N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V	pottom at Stage = 0 f Gr ດາ	t) Height of Grati Overflow W ate Open Area / 10 verflow Grate Open	eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 1.69 2.92 20.70 8.13	Not Selected N/A N/A N/A N/A	feet feet ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50%	Not Selected N/A N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %	pottom at Stage = 0 f Gr ດາ	t) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06	Not Selected N/A N/A N/A N/A N/A	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50%	Not Selected N/A N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %	pottom at Stage = 0 f Gr ດາ	t) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open	eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06	Not Selected N/A N/A N/A N/A N/A	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50% (Circular Orifice, Re	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or Ro Not Selected	ft (relative to basin t feet H:V feet % ectangular Orifice)	pottom at Stage = 0 f Gr ດາ	t) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06 s for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50% (Circular Orifice, Re Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or Rr Not Selected N/A	ft (relative to basin t feet H:V feet % ectangular Orifice)	bottom at Stage = 0 f Gr Ov C	t) Height of Grat Overflow W ate Open Area / 10 erflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	leir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameters	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06 s for Outlet Pipe w/ Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A Flow Restriction PI Not Selected	feet feet ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50% (Circular Orifice, Re Zone 3 Restrictor 0.00	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or Ro Not Selected N/A N/A	ft (relative to basin t feet H:V feet <u>ectangular Orifice</u>) ft (distance below ba	oottom at Stage = 0 f Gr OO C	t) Height of Grat Overflow W ate Open Area / 10 erflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = h Area w/ Debris = lculated Parameter: utlet Orifice Area = 0 Orifice Centroid =	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06 5 for Outlet Pipe w/ Zone 3 Restrictor 0.39	Not Selected N/A N/A N/A N/A Flow Restriction Pl Not Selected N/A	feet feet ft ² ft ² ft ²
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50% (Circular Orifice, R Con 3 Restrictor 0.00 12.00 6.00	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or Ro Not Selected N/A N/A	ft (relative to basin t feet H:V feet <u>ectangular Orifice)</u> ft (distance below ba inches	oottom at Stage = 0 f Gr OO C	t) Height of Grat Overflow W ate Open Area / 10 erflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Or Outlet	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = h Area w/ Debris = lculated Parameter: utlet Orifice Area = 0 Orifice Centroid =	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06 5 for Outlet Pipe w/ Zone 3 Restrictor 0.39 0.29 1.57	Not Selected N/A N/A N/A N/A N/A N/A Flow Restriction PI Not Selected N/A N/A N/A N/A	feet feet ft ² ft ² ft ² ft ²
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Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (arcert) = Inflow Hydrograph Volume (arcert) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, Q (cfs/arce) = Peak Inflow Q (cfs) = Ratio Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 99% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	Zone 3 Weir 1.69 4.00 0.00 2.92 Type C Grate 50% (Circular Orifice, Ra Zone 3 Restrictor 0.00 12.00 6.00 Trapezoidal) 2.80 4.00 4.00 1.00 The user can overn WQCV N/A 0.065 N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A	ft (relative to basin t feet H:V feet % ectangular Orifice) ft (distance below be inches inches bottom at Stage = CMV2 Section nould be 18" <i>IP hydrographs and</i> 2 Year 1.19 0.180 0.5 0.14 0.5 0.5 0.14 0.5 0.14 0.5 0.5 0.14 0.5 0.5 0.14 0.5 0.5 0.14 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	asin bottom at Stage = 0 f Gr Or asin bottom at Stage Half-Cent 0 ft) In 4.3, outlet 'minimum. I runoff volumes by 5 Year 0.257 0.257 0.257 0.39 5.1 0.6 0.4 Overflow Weir 1 0.1 N/A 59 69	t) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open Overflow Grate Open Definition of the open Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca	eir Slope Length = 0-yr Orifice Area = Area w/o Debris = h Area w/o Debris = in Area w/ Debris = lculated Parameters utlet Orifice Area = Orifice Centroid = tor Plate on Pipe = esign Flow Depth= op of Freeboard = op of Freeboard = 0.327 0.327 0.327 0.327 0.70 6.3 2.1 0.8 Overflow Weir 1 0.2 N/A 56 68	Zone 3 Weir 1.69 2.92 20.70 8.13 4.06 Zone 3 Restrictor 0.39 0.29 1.57 <u>Calculated Parame</u> 0.71 4.51 0.22 0.61 <i>tographs table (Co.</i> 50 Year 1.99 0.415 0.415 3.8 1.01 8.1 2.6 0.7 Outlet Plate 1 0.3 N/A 52 66	Not Selected N/A	F). 500 Year ate ft ² feet radians 500 Year 3.14 0.780 0.8 0.780 0.8 0.9 0.9 0.4 0.79 0.9 0.780 0.8 0.8 0.9 0.4 0.741 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.780 0.8 0.8 0.9 0.4 0.741 0.790 0.780 0.780 0.780 0.780 0.780 0.8 0.8 0.8 0.9 0.4 0.4 0.790 0.4 0.4 0.790 0.4 0.790 0.4 0.4 0.790 0.4 0.4 0.790 0.4 0.790 0.4 0.4 0.790 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.
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DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

-	The user can o	verride the calcu	lated inflow hyd	lrographs from t	his workbook w	ith inflow hydro	graphs develope	ed in a separate p	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.14
	0:15:00	0.00	0.00	0.37	0.61	0.75	0.35	0.50	0.62	0.86
	0:20:00	0.00	0.00	1.26	1.64	2.03	0.96	1.20	1.51	2.03
	0:25:00	0.00	0.00	2.85	4.30	5.61	2.17	2.78	3.70	5.62
	0:30:00	0.00	0.00	3.50	5.12	6.26	5.81	7.59	10.36	13.76
	0:35:00	0.00	0.00	3.05	4.35	5.28	6.35	8.07	11.52	15.05
	0:40:00	0.00	0.00	2.57	3.57	4.36	5.86	7.39	10.37	13.52
	0:45:00	0.00	0.00	2.00	2.84	3.54	4.91	6.20	9.04	11.75
	0:50:00	0.00	0.00	1.60	2.34	2.86	4.16	5.24	7.57	9.84
	0:55:00 1:00:00	0.00	0.00	1.34 1.12	1.93 1.59	2.41	3.29 2.67	4.17 3.42	6.28 5.39	8.20 7.05
	1:05:00	0.00	0.00	0.92	1.39	1.69	2.87	2.83	4.66	6.11
	1:10:00	0.00	0.00	0.32	1.06	1.42	1.66	2.05	3.37	4.45
	1:15:00	0.00	0.00	0.56	0.89	1.30	1.24	1.57	2.39	3.24
	1:20:00	0.00	0.00	0.49	0.77	1.15	0.95	1.20	1.68	2.29
	1:25:00	0.00	0.00	0.46	0.70	0.96	0.77	0.98	1.24	1.69
	1:30:00	0.00	0.00	0.44	0.66	0.84	0.63	0.79	0.96	1.32
	1:35:00	0.00	0.00	0.43	0.63	0.75	0.54	0.67	0.78	1.07
	1:40:00	0.00	0.00	0.42	0.55	0.70	0.49	0.60	0.66	0.91
	1:45:00	0.00	0.00	0.41	0.49	0.65	0.45	0.54	0.58	0.80
	1:50:00	0.00	0.00	0.41	0.46	0.62	0.43	0.51	0.54	0.73
	1:55:00 2:00:00	0.00	0.00	0.35	0.43	0.58	0.42	0.49	0.52	0.71
	2:00:00	0.00	0.00	0.30	0.40	0.51	0.41	0.48	0.52	0.70
	2:10:00	0.00	0.00	0.21	0.27	0.35	0.28	0.33	0.36	0.48
	2:15:00	0.00	0.00	0.09	0.10	0.16	0.13	0.22	0.24	0.22
	2:20:00	0.00	0.00	0.06	0.08	0.10	0.08	0.10	0.11	0.14
	2:25:00	0.00	0.00	0.04	0.05	0.06	0.05	0.06	0.07	0.09
	2:30:00	0.00	0.00	0.02	0.03	0.04	0.03	0.04	0.04	0.05
	2:35:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
	2:40:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00 3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00 4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

APPENDIX F – OPINION OF PROBABLE CONSTRUCTION COST

Kimley **»Horn**

Kimley-Horn & Associates, Inc.

Opinion of Probable Construction Cost

1 of 1

Sheet:

Project:Villas at Aspen TrailsPrepared By:JAKHA No.:096668022Checked By:JA	Client:	ROS Equity Holdings - Independence, LLC	Date:	11/4/2022
KHA No.: 096668022 Checked By: JA	Project:	Villas at Aspen Trails	Prepared By:	JAR
	KHA No.	: 096668022	Checked By:	JAR

No:

Kimley-Horn & Associates, Inc. has not prepared fully engineered construction drawings for this site; therefore, the final quantities are subject to change. Additionally, the final land plan could change significantly through the development process. This OPC is not intended for basing financial decisions, or securing funding. Review all notes and assumptions. Since Kimley-Horn & Associates, Inc. has no control over the cost of labor, materials, equipment, or services furnished by others, or over methods of determining price, or over competitive bidding or market conditions, any and all opinions as to the cost herein, including but not limited to opinions as to the costs of construction materials, shall be made on the basis of experience and best available data. Kimley-Horn & Associates, Inc. cannot and does not guarantee that proposals, bids, or actual costs will not vary from the opinions on costs shown herein. The total costs and other numbers in this Opinion of Probable Cost have been rounded.

Item No.	Item Description	Quantity	Unit	Unit Price	Item Cost
1 2	Storm Sewer Costs for Ray O 5.2 Multi-Family (Non-reimbursable) 12" RCP Storm Sewer 18" RCP Storm Sewer	83 78	LF LF	\$20.00 \$25.00	\$1,660 \$1,950
3	Type M Rip Rap	1	CY	\$50.00	\$50
4	4' COS D-10-R Storm Inlet	2	EA	\$2,500.00	\$5,000
	·	Subtotal: Contingency	y (%,+/-)	10%	\$8,660 \$866
		Project Tot	al:		\$9,526

Basis for Cost Projection:

- No Design Completed
- Preliminary Design
- Final Design

Per my comment on the FAE:

Include a cost estimate for each PBMP with line items for all components (ex: riprap, road base, forebay, trickle channel, outlet structure, outlet pipe, spillway, etc). Input the total value into the FAE form under "Permanent Pond/BMP (provide engineer's estimate)" in Section 1. The total should not include grading, which is a separate line item in Section 1: "Earthwork." **Design Engineer:**

Jared A. Roberts

Registered Professional Engineer, State of Colorado No. 60470