

City of Fountain Engineering Department 116 South Main St. Fountain, CO 80817 February 2022

RE: Corvallis MDDP

Dear Sir or Madam,

Please find enclosed the MDDP Amendment for the proposed Corvallis development. The purpose of this amendment is to address the addition of the 22-acre "Lacy Parcel" to the Corvallis development. This parcel will add 9.7 acres of Open Space, 9.9 acres of single-family, and 2.4 acres of roadways. The site indicated in the original ODP included 140.8 acres of single-family, 16.1 acres of multi-family, and 36 acres of commercial. 45.6 acres as park area or open space were also proposed, in addition to the open spaces associated with the gas easement running through the property. Additionally, 12 acres will be used for a school.

Drainage analysis for the project has been completed in accordance with the current City of Colorado Springs drainage criteria manual which the city of Fountain has adopted as its governing drainage criteria.

If there are any comments or questions regarding this submittal, please feel free to contact me by phone: 719-575-0100 or email: jesse.sullivan@matrixdesigngroup.com.

Thank you,

Jesse Sullivan, P.E.

Enclosures.

# MASTER DEVELOPMENT DRAINAGE PLAN AMENDMENT

For

# **CORVALLIS**

Prepared for: City of Fountain 116 S. Main Street Fountain, CO 80817

On Behalf of:

## **HPHR Properties, LLC**

555 Middle Creek Parkway, Suite 380 Colorado Springs, CO 80921

Prepared by:



2435 Research Parkway, Suite 300 Colorado Springs, CO 80920 (719) 575-0100 fax (719) 572-0208

February 2022

Project No. 20.1105.002

## **ENGINEER'S STATEMENT:**

Conditions:

This report and plan for the drainage design of <u>Corvallis</u> was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Fountain does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, error or omissions on my part in preparing this report.

Signature:	<u>-</u>	<u></u>	
Jesse Sulliva Colorado Pi	in rofessional Engineer No. 55600		
to the design presented liability for the drainage of Fountain pursuant to drainage design review v	hereby certifies that the drainage in this report. I understand the facilities designed and/or certife the City Code; and cannot, on will absolve <u>HPHR Properties</u> , asign. I further understand that	at the City of Fountain fied by my engineer and behalf of <u>HPHR Prope</u> LLC and/or their succe	does not and will not assume that are submitted to the City rties, LLC, guarantee that final essors and/or assigns of future
Name of Developer:	HPHR Properties, LLC		
Authorized Signature:		Date:	
Printed Name: Ed Ho	oule		
Title: Director of Lan	d Acquisition and Developme	ent	
	14160 Gleneagle Drive Colorado Springs, CO 80921		
<b>CITY OF FOUNTAI</b> Filed in accordance with	<b>N STATEMENT:</b> In the Code of the City of Founta	in, 2009, as amended.	
For the City Engineer		Date	

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#### I. Introduction

#### A. PURPOSE AND SCOPE OF STUDY

The purpose of this report is to amend the approved Master Development Drainage Plan (MDDP) to account for the inclusion of the previously excluded 22.072-acre Lacy Parcel to the development. This revision will be submitted to the City as an Overall Development Plan for the (ODP) for the parcel. This Master Development Drainage Plan Amendment (MDDPA) report provides a summary of the site drainage issues impacting the overall proposed Corvallis development, including identification and evaluation of the offsite and onsite drainage patterns associated with the project, analysis of upstream impacts from upstream drainage, and impacts to downstream facilities. This MDDPA has been prepared based on the guidelines and criteria presented in the City of Colorado Springs Drainage Criteria Manual (DCM).

## B. AGENCY JURISDICTIONS

This project is located within the City of Fountain and is subject to the design criteria set forth in the City of Colorado Springs Drainage Criteria Manual, Volumes I and II, dated May 2014 (DCM).

## C. GENERAL PROJECT DESCRIPTION

Corvallis is a 297-acre (22 Acre "Lacy Parcel" & 275 Acre Original ODP) mixed-use parcel located at the southwest intersection of Marksheffel Road and Fontaine Boulevard. The Corvallis ODP amendment prepared by Matrix Design Group, Inc dated October 2021 includes single-family and multi-family residential units, commercial development, a school site, and dedicated open space. Figure 1 below displays in further detail the Land Use Summary:

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Figure 1. Land Use Summary of proposed Corvallis site

Original ODP				
	Commercial (office/retail)	36.0	Acres	
	Residential (single-family)	140.8	Acres	
	Residential (multi-family)	16.1	Acres	
	School Site	12	Acres	
	Collector Roadways	25.4	Acres	
	Open Space	45.6	Acres	
Lacy Parcel				
	Open Space	10.3	Acres	
	Residential (single-family)	9.9	Acres	
	Collector Roadways	1.8	Acres	

More specifically, the site is located as follows:

- 1. <u>General Location</u>: Part of the Northeast ½ of Section 21, and the Northwest ¼ and a Portion of the Southwest ¼ of the Northeast ¼ of Section 22, all in Township 15 South, Range 65 West of the 6<sup>th</sup> P.M. in the City of Fountain, County of El Paso, State of Colorado.
- 2. <u>Surrounding Streets:</u> Fontaine Boulevard directly borders the parcel to the north, and a portion of the eastern boundary is bordered directly by Marksheffel Road. Powers Boulevard (State Highway 21) is located approximately ½ mile to the west.
- 3. <u>Drainageway:</u> The proposed site lies entirely within the West Fork Jimmy Camp Creek Drainage Basin and is currently undeveloped land, mostly covered by natural vegetation. The Fountain Mutual Irrigation Company (FMIC) irrigation ditch also enters and exits the site multiple times.
- 4. <u>Surrounding Developments:</u> The site is bound by vacant land to the north, the Peaceful Valley Estates development to the West, The Glen at Widefield Subdivisions to the south, and Lorson Ranch to the east.

Refer to Appendix D for the Vicinity Map.

#### D. DATA SOURCES

Topographical information for the site was found using a combination of *United States Geological Survey* (USGS) mapping, GIS LIDAR, as well as field surveying. The *Web Soil Survey*, created by the *Natural Resources Conservation Service*, was utilized to investigate the existing general soil types within the site.

#### E. APPLICABLE CRITERIA AND STANDARDS

As required by the City of Fountain, Colorado, this report has been prepared in accordance to the criteria set forth in the *City of Colorado Springs Drainage Criteria Manual Volume 1* (Drainage Criteria Manual), dated May 2014, updated January 2021 and *Volume 2 Stormwater Quality Policies, Procedures, and BMP's*, dated May 2014, updated December 2020.

In addition to the City Criteria Manual, the *Urban Storm Drainage Criteria Manuals*, *Volumes 1-3* (UDFCD), published by the Urban Drainage and Flood Control District, latest update, have been used to supplement the Drainage Criteria Manual for water quality capture volume (WQCV).

#### F. REFERENCED DRAINAGE REPORTS

West Fork Jimmy Camp Creek Drainage Basin Planning Study (WFJCC DBPS), by Kiowa Engineering Corp. October 2003.

Master Drainage Development Plan (MDDP) The Glen at Widefield, by Kiowa Engineering Corp. December 1999.

Master Drainage Development Plan Amendment (MDDPA) The Glen at Widefield, by Kiowa Engineering Corp. June 2007.

Final Drainage Report (FDR F9) The Glen at Widefield Filing No. 9, by Kiowa Engineering Corp. July 2018.

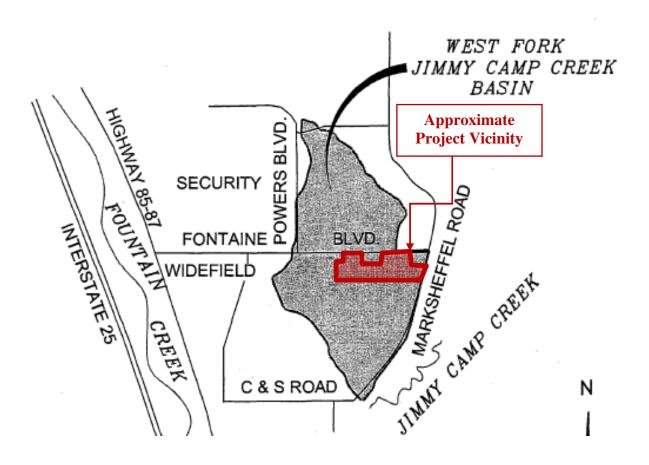
Final Drainage Report (FDR F11) The Glen at Widefield Filing No. 11, by Kiowa Engineering Corp. December 2019.

Master Drainage Development Plan (MDDP) Corvallis, by Matrix Design Group, September 2021.

## II. Project Characteristics

## A. MAJOR BASIN

Corvallis lies entirely within the West Fork Jimmy Camp Creek (WFJCC) Drainage Basin. The project includes offsite and onsite drainage area with the major confluence of offsite drainage happening at an existing bridge crossing that conveys the WFJCC flows southerly across Fontaine Boulevard. These flows continue south through the Corvallis site until they enter the Glen at Widefield Subdivision Filing No. 9. Two more natural channels run through the site, draining north to south, and join with the WFJCC after they have left the Corvallis development. The West Fork of Jimmy Camp Creek covers a total of 4 square miles. The developed area for the site of 297-acres is approximately 11.6% of the total drainage area within the WFJCC.



#### B. COMPLIANCE WITH DBPS

This study complies with the latest DBPS study (*WFJCC DBPS*) of the West Fork Jimmy Camp Creek basin dated October 2003. All developed runoff from the site will be detained and released at pre-development peak rates, and the water quality volume will be treated. Both as determined by the UDFCD detention spreadsheet UD-Detention.

#### C. GEOLOGY

The majority of the site is currently undeveloped and consists of natural vegetative land cover, as well as multiple natural creeks.

Soils can be classified in four different hydrologic groups, A, B, C, or D to help predict storm water runoff rates. Hydrologic group "A" is characterized by deep, well-drained coarse-grained soils with a rapid infiltration rate when thoroughly wet and having a low runoff potential. Group "D" typically has a clay layer at or near to the surface, or a very shallow depth to impervious bedrock and has a very slow infiltration rate and a high runoff potential. See Soils Map; Appendix D. Table 1.1, below, indicates which soil types are present in the development area:

Table 1.1 – NRCS Soil Survey for El Paso County

Soil ID	Soil	Hydrologic	Permeability	Percent
Number		Classification		on Site
30	Fort Collins Loam (0% - 3% slopes)	В	Moderately Rapid	3.9%
52	Manzanst Clay Loam (0% - 3% slopes)	С	Low Rapidity	1.8%
56	Nelson-Tassel Fine Sandy Loams (3% - 18% slopes)	В	Moderately Rapid	34.5%
59	Nunn Clay Loam (0% - 3% slopes)	С	Low Rapidity	16.2%
75	Razor-Midway Complex	D	Very Low Rapidity	0.9%
86	Stoneham Sandy Loam (3% - 8% slopes)	В	Moderately Rapid	35.6%
101	Ustic Torrifluvents, Loamy	В	Moderately Rapid	0.8%
108	Wiley Silt Loam (3% - 9% slopes)	В	Moderately Rapid	6.3%

#### D. GROUNDWATER

According to the Geo-tech report for the site, groundwater levels vary. There is some seasonal and temporary raising of the water table along the FMIC and natural ditches. This fluctuation is likely due to irrigation water releases during the growing season; therefore, it is anticipated that the rerouting of the FMIC ditch via storm sewer, described in Section F below, will mitigate some of the water table fluctuations. Groundwater will be mitigated for in the construction plans as recommended in future Geo-tech reports which will be referenced in the appropriate future PDR/FDRs.

#### E. LAND USES

Presently, the site is unplatted and consists of undeveloped land. Corvallis is a proposed planned unit development (PUD) which includes both residential and commercial uses. Development of utilities and internal roadways are to be included in this parcel.

#### F. UTILITIES AND ENCUMBERANCES

- Storm Sewer: Existing storm sewer includes a 30-inch CMP culvert that crosses Fontaine Boulevard. In addition, WFJCC and associated proposed storm infrastructure will run through the site. Sizing is as described within this report and subject to change as site design progresses.
- Sanitary Sewer: An existing 24-inch sanitary sewer main lies within the intersection of Marksheffel Road and Lorson Boulevard near the site's southeast corner which will take flow east of the ridge internal to Corvallis Development. There is also an existing 12-inch sanitary sewer main which runs north-south through the site that will tie into the sanitary system at The Glen at Widefield development to the south of the site and will take the site's internal sanitary flow west of the ridge.
- **Gas**: Gas service to the proposed development will be provided by Black Hills Energy through the extension of the existing gas main infrastructure that currently lies adjacent to the site. No encumbrance to the project is anticipated.
- Water: The following existing water mains surround the site: a 16-inch water main in Marksheffel Road, a 24-inch water main in Spring Glen, a 12-inch water stub at Dutch Loop, and an 8-inch water main at Fontaine Boulevard near Cottonwood Grove. A network of new 12-inch and 8-inch water mains will be constructed throughout the Corvallis site to provide looping and water services to the development.
- **Electric:** There is existing overhead electric power in Fontaine Boulevard along the north side of the property and along the site's western property line. Underground electric power is also located within the residential developments to the south and east of the site. Electric service will be provided to the Corvallis Development by extending underground electric throughout the subdivision for residential and commercial services. No encumbrance to the project is anticipated.
- Communications: Underground communication lines currently serve the residential neighborhoods adjacent to the project site which will be extended underground to serve Corvallis Development. No encumbrance to the project is anticipated.
- Irrigation: There is an existing FMIC irrigation ditch meandering through both the east and west portions of the site. Both sections of the FMIC ditch running through the Corvallis site will be rerouted via 60-inch storm pipes sized to convey the 60 cfs that FMIC has indicated as a peak irrigation flow. Due to the lack of grade in the existing ditch, both sections of pipe are very flat with the west section at 0.06% and the east section at 0.08% grade. Entry and exit locations to and from the site will remain unchanged.

Written acceptance of planned modifications to FMIC ditch must be acquired from FMIC prior to beginning construction of these improvements. Pursuit of this acceptance is in progress. Documentation will be added to the MDDP when it is available.

Once completed, the FMIC approved irrigation conveyances will be privately owned and maintained by the FMIC.

## III. Hydrologic Analysis

## A. GENERAL CONCEPT

The general concept for management of storm water for the proposed Corvallis development will be to provide clear conveyance through the property to the multiple onsite detention facilities to mitigate developed runoff flows from the site. Development of the site will require over-lot grading, roadway paving, residential and commercial construction which will increase the imperviousness of the property from existing conditions. The general drainage patterns will consist of positive drainage away from building sites, across lawns, parking lots, or open space, to curb and gutter within the internal roadways. Storm water within the roadways will be directed to inlet collection points, where it is captured and conveyed through a pipe network system to a full spectrum detention pond. Majority of offsite runoff will be either be diverted around the site or collected and directed separately through the site before being discharged at historic drainage locations and discharge.

The Water Quality Capture Volume (WQCV) is comprised within the proposed Full Spectrum Extended Detention Basin (EDB), where the "initial flush" of storm water will be drained over a 40-hour time period. The onsite ponds have been evaluated to reduce the developed flows from the site to a maximum of the historic peak flows. The detention pond has been sized and evaluated based upon the 100-year storm events in accordance with City Criteria.

#### B. METHODOLOGY

#### a. Rational Method

#### i. Method of Analysis

Storm sewer sizing for this project uses the Rational Method as recommended by the Drainage Criteria Manual for the minor and major storms for drainage basins less than 100-acres in size (Inlets will also be sized using this method in the subsequent FDRs). The Rational Method uses the following equation:

#### Q=C\*i\*A

Where:

Q = Maximum runoff rate in cubic feet per second (cfs)

C = Runoff coefficient

i = Average rainfall intensity (inches per hour)

A = Area of drainage sub-basin (acres)

#### ii. Runoff Coefficient

Coefficients from Table 6-6 of the Drainage Criteria Manual for developed land were utilized in the Rational Method calculations. See Appendix B for more information.

#### iii. Time of Concentration

The time of concentration consists of the initial time of overland flow and the travel time in a channel to the inlet or point of interest. A minimum time of concentrations of 5 minutes is utilized for urban areas.

## iv. Rainfall Intensity

The hypothetical rainfall depths for the 1-hour storm duration were taken from Table 6-2 of the Colorado Springs Drainage Criteria Manual. Table 3.1, below, lists the rainfall depth for the Major and Minor 1-hour storm events.

Table 3.1 - Project Area 1-Hour Rainfall Depth

Storm Recurrence	Rainfall Depth
Interval	(inches)
5-year	1.50
100-year	2.52

The rainfall intensity equation for the Rational Method was taken from Drainage Criteria Manual Volume 1 Figure 6-5.

#### C. BASIN HYDROLOGY

#### EXISTING DRAINAGE CONDITIONS

Under the existing conditions, the site flows in a general north to south pattern until reaching one of three low points. As such, the site has been divided into major basin delineations (west, central, east) which collect flow at these three discharge points, in conformance with the **WFJCC DBPS**, **MDDP**, and **FDR**s for the area.

#### West Basin:

<u>Sub-basin OS-1</u> borders the site to the west and is comprised of large lot, single-family residential homes. Runoff from this site drains to the east until reaching the Corvallis boundary, represented at Design Point E1.

<u>Sub-basin OS-2</u> borders the site to the northwest and consists of drainage on Fontaine Boulevard from the crown of the roadway to the south. These flows drain from the existing roadway high point to the east until reaching the existing low point at Design Point E2. In the existing conditions, this road corridor drainage connects with a 30-inch CMP that directs localized flows from the north underneath Fontaine Boulevard and discharging into the WFJCC.

<u>Sub-basin EX-2</u> is an onsite, undeveloped basin that sheet flows in a general southwest to northeast pattern until it combines with Sub-basin OS-2 at Design Point E2. Runoff from this design point discharges directly into the WFJCC.

<u>Sub-basin OS-3</u> is an offsite, undeveloped basin that drains to the southeast until reaching the WFJCC floodway at Design Point E3.

<u>Sub-basin OS-4</u> is an offsite, undeveloped basin adjacent to the WFJCC which drains to the southeast until reaching Design Point E3.

In addition to the above listed sub-basin flows that reach Design Point E3, the approved **WFJCC DBPS** also specifies a Design Point 3020 which consists of the upstream flows, including the existing 30" CMP mentioned previously) collected in the WFJCC as it enters the Corvallis site. In a conservative effort, the approved existing **WFJCC DBPS** flows have been added to the previously described sub-basins to achieve the flows at Design Point E3.

<u>Sub-basin EX-1</u> is comprised of the west quarter of the Corvallis site. Currently undeveloped, flows generated in this basin combine with offsite flows from Sub-basin OS-1 and drain in a general northwest to south east pattern until reaching the WFJCC at Design Point E4.

<u>Sub-basin 1-D (Formerly OS-8)</u> is now included in the project by the new Lacy ODP. Under existing conditions this area is agriculturally zoned and sheet flows from west to east until reaching the WFJCC at Design Point E4.

<u>Sub-basin OS-5</u> contains the southern half of Fontaine Boulevard as it drains from an existing roadway high point to the west until discharging and combining with onsite drainage.

<u>Sub-basin EX-3</u> accepts the flows from Sub-basin OS-5 and continues to drain from the northeast to southwest until reaching Design Point E5 at the site's southern border.

Flows from Design Points E4 and E5 combine at the West Basin's final discharge point, Design Point E8. This is located at the flowline of the WFJCC drainageway as it leaves the Corvallis development and continues into the Glen at Widefield development located to the south. In both the approved **WFJCC DBPS** and **MDDP**, the flowrates at this point are  $Q_5 = 601$  cfs and  $Q_{100} = 2216$  cfs. As previously mentioned, rational calculations were performed for all onsite basins and added to the **MDDPA** Design Point R3030 existing condition flows ( $Q_5 = 347$  cfs and  $Q_{100} = 1761$  cfs) located at the WFJCC entrance into the site. This results in Design Point 8 flows of  $Q_5 = 403.5$  cfs and  $Q_{100} = 2040.7$  cfs. The previously approved **WFJCC DBPS** and **MDDP** will govern on the discharge flows at this point.

A summary of the existing basins and design points contributing to the West Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions Map.

West Basin				
Basin Name	A	Peak Flows		
Dasin Name	Acreage	5-Year	100-Year	
OS-1a	38.5	19.2	70.9	
OS-1b	38.3	12.3	47.7	
OS-2	1.0	3.9	7.1	
OS-3	1.9	0.6	4.0	
OS-4	18.3	3.3	21.8	
OS-5	0.8	3.2	5.8	
OS-8	22.1	4.2	28.1	
EX-1	67.9	9.0	60.3	
EX-2	10.3	2.5	17.0	
EX-3	51.9	8.2	54.8	

West Basin			
Dogiom Boint	Peak Flows		
Design Point	5-Year	100-Year	
E1: OS-1	25.3	98.5	
E2: OS-2, EX-2	5.4	22.5	
E3: E2, OS-3, OS-4	6.5	34.4	
E4: E1, E3, EX-1, OS-8	46.3	222.3	
E5: OS-5, EX-3	10.2	57.5	
E8: E4, E5, +DPBS3020	403.5	2040.7	

#### Central Basin

<u>Sub-basin EX-4</u> is an onsite, undeveloped portion of land that drains from the northeast to the southwest until reaching Design Point E6, the final discharge point of the Central Basin.

This discharge point is centrally located on the southern border of the Corvallis development. An existing area inlet and corresponding 48-inch RCP collects the flows ( $Q_5 = 7.2$  cfs and  $Q_{100} = 48.1$  cfs) and conveys them directly to the WFJCC. Per the approved FDR for the Glen at Widefield Filing No. 9, this point collects 44.8 cfs in the 5-year storm and 163 cfs in the 100-year storm. As with Design Point E8, the allowable release of flows for this point are set by the approved **WFJCC DPBS** and **MDDP**.

A summary of the existing basins and design points contributing to the Central Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions Map.

Central Basin			
Basin	<b>A</b> ama a ara	Peak Flows	
Name	Acreage	5-Year	100-Year
EX-4	58.6	7.2	48.1

Central Basin			
Dogiom Point	Peak Flows		
Design Point	5-Year	100-Year	
E6: EX-4	7.2	48.1	

#### East Basin

<u>Sub-basin OS-6</u> contains the southern portion of Fontaine Boulevard, to the crown of the roadway, that the borders the site to the northeast. These flows are collected in a roadside swale and discharge onsite.

<u>Sub-basin OS-7</u> consists of a single-family residential development located on the east side of the side. The back half of the existing residential lots drain to the south and west until discharging onto the Corvallis site.

<u>Sub-basin EX-5</u> is the easternmost onsite basin. Currently undeveloped, this basin collects the flows from Sub-basins OS-6 and OS-7 and slopes from the northwest to the southeast until reaching Design Point E7.

The final discharge point for the East Basin (Design Point E7,  $Q_5 = 16.5$  cfs and  $Q_{100} = 93.1$  cfs) is located at the southeast corner of the site. These flows will be conveyed to the south in the existing roadside swale that runs parallel to Marksheffel Road. Discharge at this design point was set in the **WFJCC DBPS** and **MDDP** as  $Q_5 = 38$  cfs and  $Q_{100} = 153$  cfs and will control the allowable discharge in developed conditions.

A summary of all existing basins and design points, offsite and onsite, as well as a summary of design points contributing to the East Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions drainage maps.

East Basin				
Dagin Nama	<b>A</b> ama a ara	Peak Flows		
Basin Name	Acreage			
OS-6	0.8	3.2	5.8	
OS-7	2.9	2.5	9.4	
EX-5	86.5	12.8	86.3	

East Basin			
Danian Bains	Peak Flows		
Design Point	5-Year	100-Year	
E7: EX-5, OS-6, OS-7	16.5	93.1	

As previously mentioned, the Fountain Mutual Irrigation Company (FMIC) ditch system enters and exits the site periodically. The ditch in this area is approximated to have flows of 60 cfs as it meanders through the Corvallis site. This MDDP follows the guidelines previously set in the **WFJCC DPBS** that states, "Existing and proposed runoff was assumed to be passed over or under the ditch in the hydrologic modeling of the basin. There was no diversion of runoff by the ditch assumed in compilation of the hydrologic model for this basin." As such, no additional drainage from the site is anticipated to be conveyed by the FMIC and all flows released into the ditch are assumed to remain within the canal. There is a possibility of a bypass pipeline being constructed that will convey flows from Big Johnson Reservoir to the east side of Marksheffel Road, near Jimmy Camp Creek, however this has not been considered for this report.

#### DEVELOPED DRAINAGE CONDITIONS

As explained in the existing conditions, the developed site drainage will also discharge at three site low points and has been broken down into three drainage basins for clarity. These design points have been specified in the *WFJCC DBPS* and subsequent reports as the discharge points from the Corvallis development. Runoff from the developed site will conform to these specified flows. Developed hydrology calculations for the basins and design points can be found in Appendix A. Preliminary hydraulic calculations have been completed for the anticipated trunk mains. Storm infrastructure internal to the sub-basins will be completed with each filing's Final Drainage Report.

#### West Basin:

<u>Sub-basin OS-1</u> previously explained in the existing conditions will continue to drain easterly until reaching the Corvallis site boundary. At this point, the offsite flows will either be conveyed via swale or pipe to the north and east until reaching Design Point E1. Preliminary calculations have been completed for this swale (OS-1 Swale) or pipe (OS-1 Pipe) and can be found in Appendix A. Once entering the Corvallis site, these offsite flows will be conveyed via storm drain to the east and south until reaching DP1. This drainage will be kept separate from any untreated, developed runoff and will therefore not require any detention or water quality treatment.

<u>Sub-basin OS-2</u> collects the runoff from required improvements to Fontaine Boulevard, adjacent to the Corvallis development which will have the required improvements at the time of development. Runoff from the roadway crown to the south will be collected in the proposed curb and gutter and directed to required inlets at the road low point. From here, flows will be conveyed to Sub-basin 2 via proposed storm drain.

<u>Sub-basin 1B</u> includes both commercial and multi-family development at the northwest corner of the site. The commercial and multi-family parcels will each have their own onsite water quality and detention facilities, DF-1 and DF-2, respectively. Discharge from these facilities will be

released at prehistoric peak flow values as required per the City criteria. Treated flows leaving DF-1 will be conveyed to the south via an 18-inch storm drain until reaching DP1. Preliminary calculations for the ponds and storm drain have been calculated and can be found in Appendix A. Discharge from DF-2 will be conveyed to DP2 via a 24-inch storm drain.

Design Point DP1 combines Design Point E1 and Sub-basin 1B. At this point, treated flows combine with routed flows. In an effort to be conservative, the treated discharge has simply been added to the routed flow, resulting in 25.0 cfs and 107.0 cfs in the minor and major storms, respectively. These combined flows will be carried in a 36-inch storm drain to along Autumn Glen and Residential Collector A road corridors until reaching Design Point DP3.

<u>Sub-basin 1A</u> is comprised of 1/8 acre or less, single-family residential lots. Runoff generated from this basin will be conveyed via curb and gutter and storm drain eventually to be collected and conveyed via 42-inch storm sewer to DF-3 (at DP2).

<u>Sub-basin 2</u> is planned for 1/8 acre (or less) single-family residential. Developed runoff will be directed to the south via curb, gutter, and proposed internal storm drains, crossing beneath Residential Collector A, until reaching Design Point DP2.

<u>Sub-basin 3</u> will consist of undeveloped land and detention and water quality pond DF-3.

Detention facility DF-3 will collect developed runoff from Sub-basins 1A, 1D, 2, 3, and OS-2 and will then release at historic rates via a 36-inch storm drain until combining with flows from DP 1 in a storm manhole where the combined flows will be conveyed via 54-inch storm sewer until reaching Design Point DP3.

<u>Sub-basin 1-D (Formerly OS-8)</u> is now included in the Corvallis development per the Lacy ODP. The developed portion of this sub-basin will sheet flow towards the adjacent road which will convey the flows towards curb inlets near DP2. The captured flows will be directed into DF-3 for water quality treatment and detention.

<u>Sub-basin 7</u> will remain undeveloped open space in the proposed conditions and, therefore, does not require any detention or water quality. This sub-basin will drain to the south and west until reaching Sub-basin OS-4 and Design Point DP5.

<u>Sub-basin OS-3</u> is unchanged from the existing conditions and will continue to drain to the south and east until reaching Design Point DP5.

<u>Sub-basin OS-4</u> is unchanged from the existing conditions and will continue to drain to the south and west until reaching Design Point DP5.

As previously mentioned, flow at Design Point 5 (E3 in the existing conditions discussion) includes *WFJCC DBPS* Design Point 3020 existing flows. The approved *WFJCC DBPS* also recommends removal of the existing 30-inch CMP crossing Fontaine Boulevard and, instead, routing these flows to the east until reaching the WFJCC bridge crossing at the north side of Fontaine Boulevard. The DBPS includes calculations show that this crossing is adequately sized to handle the additional flows. As such, it has been assumed that the *WFJCC DBPS* Design Point 3020 flows include those from the 30-inch CMP, and all converge north of Fontaine

Boulevard. From here, Design Point DP5 flows continue south within the WFJCC floodway until reaching the West Basin discharge point at DP 7.

<u>Sub-basin 5</u> will be a proposed single-family development with lot sizes equal or lesser than 1/8 of an acre. Developed runoff will be taken to the south and west by internal curb, gutter and storm drain. The collected stormwater will cross underneath Residential Collector A, until reaching Sub-basin 4.

<u>Sub-basin 4</u> will be comprised of 1/8 acre, or less, single-family lots. This basin will accept flows from Sub-basin 6 and continue to direct them to the basin low point, located at the southwest corner, Design Point DP6. At this point, detention and water quality pond DF-4 will accept and treat the flows, then discharge into the WFJCC via a 24-inch storm drain.

The convergence of Design Points DP3, DP5, and DP6 results in the ultimate West Basin discharge point, DP7 ( $Q_5 = 391.0$  cfs and  $Q_{100} = 2006.1$  cfs). These flows are less than both the routed calculations completed for Design Point E8, as well as the previously approved and governing releases specified in the **WFJCC DBPS** and **MDDP**. Drainage from this point will continue to the south until reaching the Glen at Widefield developments.

A summary of the sub-basins and design points within the West Basin is shown below:

West Basin				
Basin	<b>A</b>	Peak	Flows	
Name	Acreage	5-Year	100-Year	
OS-1a	38.5	12.7	49.3	
OS-1b	38.3	12.3	47.7	
OS-2	1.0	3.9	7.1	
OS-3	1.9	0.5	3.5	
OS-4	18.3	2.5	16.6	
OS-5	0.8	3.2	5.8	
1-D	22.1	18.4	40.5	
1A	28.3	43.1	94.9	
1B	15.9	51.4	99.3	
2	26.9	40.5	89.2	
3	7.5	2.7	13.6	
4	17.0	25.9	53.8	
6	10.0	15.5	34.1	
7	19.3	2.6	17.8	

West Basin								
Design	Peak Flows							
Point	5-Year	100-Year						
E1	21.7	84.4						
DP1	25.3	110.3						
DP2	127.1	311.7						
DP3	33.6	185.2						
DP4	2.6	17.8						
DP5	352.6	1798.9						
DP6	22.3	47.7						
DP7	391.0	2006.1						

DP7 Summary									
Approved Glen at Widefield MDDPA MDDP  DBPS/MDDP FDR 9 (Dev. Cond.) (Pr. Cond.)									
5-Year	100.					5-Year	100- Year		
601.0	2216.0	601.0	2216.0	401.0	2020.0	391.0	2006.1		

#### Central Basin:

<u>Sub-basin OS-5</u> collects the runoff from required improvements to Fontaine Boulevard, adjacent to the Corvallis development which will have the required improvements at the time of development. Runoff from the roadway crown to the south will be collected in the proposed curb and gutter and directed to required inlets at the road low point. From here, flows will be conveyed to Sub-basin 9 via proposed storm drain.

<u>Sub-basins 9 & 10</u> includes single-family development with lots equal to or less than 1/8 of an acre in size. Proposed curb, gutter, and storm drain will collect the developed runoff and direct it to the south, until reaching Residential Collector A. Flows will cross underneath this roadway and join with Sub-basin 10.

<u>Sub-basin 11</u> is currently designated single-family residential. Runoff from this site will join with incoming Sub-basin 9 & 10 flows and continue to the south and west until crossing underneath the proposed Spring Glen Drive roadway, discharging into detention and water quality pond DF-5 at Design Point DP10. This basin is considered to be approximately 65 percent impervious per Table 6-3 of the USDCM.

<u>Sub-basin 5</u> contains single-family residential units with maximum lot sizes of 1/8 acre. Developed runoff will be accumulated within the internal curb, gutter, and storm drain system until discharging into pond DF-5 at Design Point DP9.

Design Point DP11 is the ultimate discharge point for the Central Basin and consists of the historical release from proposed detention and water quality pond DF-5 ( $Q_5 = 6.6$  cfs and  $Q_{100} = 48.1$  cfs). This discharge point is comparative to Design Point E6 in the existing conditions. The prehistoric discharge is equal to the calculated routed flows in the existing conditions and well underneath the approved flows from the *WFJCC DBPS* and *MDDP*, as well as the anticipated flows per the Glen at Widefield Filing No. 9 FDR.

A summary of the sub-basins and design points within the Central Basin are summarized below:

Central Basin									
Basin	A 0#0000	Peak Flows							
Name	Acreage	5-Year	100-Year						
OS-5	0.8	3.2	5.8						
5	5.9	19.4	38.6						
9	20.1	34.4	80.5						
10	15.8	24.3	57.2						
11	14.9	21.8	49.8						

Central Basin									
Design Peak Flows									
Point	5-Year	100-Year							
DP8	45.8	106.9							
DP9	33.4	74.7							
DP10	54.9	123.8							
DP11	6.6	48.1							

	DP11 Summary									
Appı	Approved Glen at Widefield MDDP MDDP									
DBPS/	DBPS/MDDP FDR 9				Cond.)	(Pr. Cond.)				
5-Year	100-Year	5-Year	100-Year	5-Year	100-	5-Year	100-			
J-1 Cai	100-1 Cai	3-1 Ca1	100-1 Cai	Year		J-1Cal	Year			
48.0	163.0	44.8	163.0	7.2	48.1	7.2	48.1			

#### East Basin:

<u>Sub-basin OS-6</u> consists of the southern half of Fontaine Boulevard, to include the proposed improvements that will be required adjacent to the Corvallis development. Inlets will need to be designed to capture this flow and route it south to Sub-basin 12 at time of Final Drainage Report for the adjacent filing.

<u>Sub-basin 8</u> is a proposed commercial development that will have its own onsite water quality and detention pond, DF-6. Once treated, the historic release will be directed to the west in an 18-inch storm drain, combining with discharges from DF-7 at DP 12a.

<u>Sub-basin 12</u> is a proposed multi-family development that will convey drainage via proposed curb, gutter, and storm drain to the south and east until reaching Design Point DP12 at detention facility DF-7. This parcel will have its own onsite water quality and detention to treat its runoff as well as the runoff from Sub-basin OS-6. Treated runoff will be released at historical peak discharge by a 30-inch storm drain. This storm drain will combine with flows from Sub-basin 8 at DP 12a and continue to the south and east, separated from any untreated flows, until reaching Design Point DP15.

<u>Sub-basin OS-7</u> is a large acre, single-family subdivision located at the Corvallis site's northeastern corner. Stormwater from the backs of these lots will drain through side lot swales until discharging onto Sub-basin 16 and eventually being treated in detention and water quality pond DF-9.

<u>Sub-basin 16</u> is a proposed commercial development. Developed runoff will drain to the southeast via internal curb, gutter, and storm drain until reaching the onsite water quality and detention facility, DF-9. This pond will release the treated flow via a 36-inch storm drain, combining with the above-mentioned East Basin flows at DP15.

Treated flows from Design Point DP15 will be conveyed in a 42-inch storm drain until reaching Design Point DP16.

<u>Sub-basin 13</u> is to be comprised of single-family housing. The lots within this basin are expected to have a maximum size of 1/8 acre. Internal site curb, gutter, and storm drain will direct the flows to the south and east until reaching Sub-basin 14.

<u>Sub-basin 14</u> will also be single-family residential with lot sizes equal or less than 1/8 of an acre. Runoff internal to this basin, as well as the accepted flows from Sub-basin 13, will be routed via curb, gutter, and storm drain to the south and east until entering Sub-basin 15.

<u>Sub-basin 15</u> is a proposed single-family subdivision with 1/8 acre, or less, lot sizes. Developed runoff from this basin (as well as Sub-basins 13 and 14) will be collected in the onsite curb, gutter, and storm drain and directed to the basin low point at the southeastern corner. At this point, detention and water quality facility DF-8 will accept the flows at Design Point DP14.

<u>Sub-basin 17</u> is currently designated as commercial. Runoff from this site will be collected in curb, gutter, and onsite storm drain and directed to the west to discharge into detention and water quality pond DF-8 at Design Point DP14.

Discharge from DF-8 will be equal to or lesser than the historical peak discharge as required by the City. From here, flows will be conveyed to the south via a 36-inch storm drain until reaching Design Point DP16.

Design Point DP16 is the ultimate discharge for the East Basin. The combined flows calculated for this design point result in 12.8 cfs in the minor storm event and 110.1 cfs in the major storm event. In the existing conditions, this discharge point was estimated to have 16.5 cfs in the minor storm and 93.1 cfs in the major storm. However, the previously approved *MDDP* and *WFJCC DBPS* for the area specify an allowable release of 38 cfs for the 5-year storm and 153 cfs in the 100-year storm.

The current report in review with the City of Fountain for the Glen at Widefield Filing No. 11, which receives the discharge from Corvallis DP16 has proposed two 36-inch culverts to convey the drainage from the Corvallis East Basin to the roadside swale being constructed as a part of the Marksheffel Road improvements. The capacity of these culverts is 87.06 cfs. Refer to Appendix C for the structures (CV177) referenced from the Final Drainage Report for the Glen at Widefield Filing No. 11.

As basins tributary to the East Basin are designed, additional analysis will be required in order to confirm the downstream capacity available.

A summary of the sub-basins and design points within the East Basin are summarized below:

	East	Basin					
Basin		Peak Flows					
Name	Acreage	5-Year	100- Year				
OS-6	0.8	3.2	5.8				
OS-7	2.9	2.5	9.4				
8	6.5	28.7	52.2				
12	17.2	28.3	62.4				
13	5.2	10.6	23.3				
14	11.1	18.5	40.6				
15	17.6	30.1	66.2				
16	32.5	96.9	184.8				
17	3.3	14.6	26.5				

Central Basin								
Design	Peak Flows							
Point	5-Year	100-Year						
DP12	24.5	53.5						
DP12a	3.2	28.8						
DP13	20.4	44.9						
DP14	35.3	76.2						
DP15	7.8	65.8						
DP16	12.8	110.1						

	DP16 Summary									
Approved Glen at Widefield MDDP MDDP (Pr.										
DBPS/	DBPS/MDDP FDR 11				Cond.)	Cond.)				
5-Year	100-Year	5-Year	100-Year	5-Year	5 Voor 100-		100-			
3 Tear	100 1001	3 Tear	100 1 car	Year Year		5-Year	Year			
38.0	153.0	153.0 N/A 87.1 16.5 93.1 12.8 110.								

## **Full Spectrum Detention Facilities**

In accordance with the City of Fountain drainage criteria, the proposed Corvallis development will provide onsite full spectrum detention facilities to mitigate developed drainage impacts. Detained flows will release at historic rates and drainage patterns. At this time, ponds in series are not anticipated. This requires treated flows and offsite flows to be conveyed separately from untreated flows. Further design will need to be done if this design intent changes. A breakdown of the required storage volume and historic release rates for each of the water quality and detention facilities are summarized below:

	PR	OPOSED WA'	TER QUALI	TYAND I	DETENTIO	N SUMMA	RY
				Corvallis			
Detention/ WQ Pond	TOTAL AREA (AC)	CONTRIBUTING BASINS	% IMPERVIOUS	VOLUME REQUIRED (AC-FT)	Q(5) DISCHARGE (cfs)	Q(100) DISCHARGE (cfs)	DESCRIPTION:
DF-1	5.65	1B- COMMERCIAL	95%	0.89	2.1	8.8	Northwest Commercial
DF-2	8.25	1B-MULTIFAMILY	70%	1.00	1.2	13.8	Northwest Multi- Family
DF-3*	61.51	1A, 1D, 2, 3, OS-2	65%	7.22	8.3	74.9	West Single-Family (Slight over-detention to maintain flows listed in Glen at Widefield MDDP Amendment)
DF-4*	23.14	4, 6	65%	2.64	4.8	22.0	Southwest Single- Family
DF-5*	57.54	5, 9,10, 11, OS-5	70%	6.98	6.6	48.1	South Single-Family & School Site
DF-6	6.50	8	95%	1.02	0.2	9.3	Northeast Commercial
DF-7	18.00	12, OS-6	70%	2.18	3.0	19.5	Northeast Multi- Family
DF-8*	37.24	13, 14, 15, 17	70%	4.51	5.0	44.3	Southeast Single- Family & Commercial
DF-9*	35.45	16	80%	4.79	4.8	46.3	Southeast Commercial Pond

Asterisk \* denotes "Sub-Regional" Detention. The other ponds are considered "Onsite" Detention.

## IV. Hydraulic Analysis

#### A. OVERVIEW, METHODOLOGY & DESIGN

Developed sub-basins and proposed drainage improvements are depicted on the attached Developed Drainage Basin Map (DR02) in Appendix D. Preliminary hydraulic design calculations for sizing of onsite facilities are provided for in Appendix A. In general, the hydraulic criteria and intent are summarized as follows:

In accordance with City of Fountain drainage criteria, major drainage will be conveyed through the Corvallis development using a combination of open channels, underground storm sewer capacity and allowable street capacity. For local residential streets, the maximum allowable depth during the 100-year event is 8-inches or the extent of the street right-of-way such that buildings are not inundated at the ground line.

The interior roads will be graded with a minimum longitudinal slope of 1.0 percent. In accordance with the street spread calculations in the DCM, the allowable minor storm street capacity is 8 cfs per side for 6-inch ramp curb and 12 cfs per side for 6-inch vertical curb. The allowable major storm street capacity is approximately 36 cfs per side (72 cfs full width). Reference Appendix B for sizing chart.

Curb inlets (CDOT Type R or equivalent City approved 6-inch curb inlet type) will be specified where required for at-grade and sump collection point locations. Inlets will convey runoff to a storm sewer consisting of reinforced pipes (RCP) with a minimum pipe diameter of 18-inches. Preliminary storm sewer sizing has been provided based on full flow capacity at a minimum slope of 1.0 percent and can be referenced in Appendix A. Riprap stilling basins will be utilized at storm pipe outfalls. Detailed inlet, storm sewer and riprap sizing calculations will be provided with the Final Drainage Reports for each filing.

A preliminary hydraulic analysis been completed as part of this study to determine the required storm pipe sizing for the site trunk mains. Hydraulic grade lines (calculated in StormCAD and using head loss coefficients from Table 9-4 of the DCM) will be provided with either the FDR or along with construction drawings. Initial sizing of the onsite detention ponds was completed using UDFCD Detention Pond software for Extended Detention Basins. The ponds have been evaluated to determine the peak release rates from the proposed detention ponds and the storage required for the 100-year storm event. Most proposed storm pipes have been upsized to accommodate larger flows as a conservative design.

If further design of the site alters the design intent as discussed within this MDDP, an amendment will be required to show compliance with the City of Fountain criteria.

#### B. FLOODPLAINS

Per the *Flood Insurance Rate Map (FIRM) 08041C 0956 G and 08041C 0957 G*, effective date December 7, 2018, published by the Federal Emergency Management Agency (FEMA), a portion of Corvallis lies within the designated 100-year floodplain of Jimmy Camp Creek West Tributary. A FIRMette of the project area is included in Appendix D.

Per the approved *WFJCC DBPS*, as land is developed adjacent to the WFJCC (Corvallis-West Basin), channel improvements (and associated Channel Design Report) will be required.

WFJCC DBPS Map 4A (Appendix D) shows the existing 30-inch culvert to be removed north of Fontaine Boulevard and directed to the existing bridge crossing. The sections of the WFJCC that traverse through the Corvallis site are specified as 3030-2 and 3030-1. The WFJCC DBPS recommends channel improvements to include a rip-rap lined channel up to the 100-year water surface elevation as well as check dams at 150' intervals in both sections (These are anticipated to be replaced with less frequent grouted rip rap drop structures with larger drops). Actual channel design will differ from the DBPS recommendations slightly and will follow the governing channel design criteria at that time and likely act to preserve the existing wetlands (to be delineated in the future).

Creek improvements will be triggered when development within the sub-basins listed as a part of this MDDP's West Basin begins and will be paid for by the Metropolitan District via mill levees. After this trigger occurs, further investigation into the true creek requirements based on actual field conditions will be required.

A Letter of Map Amendment (LOMA) and/or Letter of Map Revision (CLOMR/LOMR) will be required once channel improvements are triggered by the above indicated criteria in order to show the revised extent of the regulatory floodplain through the site. The channel and improvements will be located within a tract and will be owned and maintained by the metro district. Maintenance access to the channel must also be provided in accordance with Channel Design Criteria.

## V. Environmental Evaluations

#### A. WETLAND IMPACTS

Per the U.S. Fish and Wildlife National Wetlands Inventory, there are freshwater emergent wetlands located onsite. Wetland delineation will be required once channel improvements are triggered by future development in the Corvallis-West Basin.

#### B. STORMWATER QUALITY

All onsite detention facilities shall be designed to accommodate water quality requirements. As the development of each parcel progresses, the detention guidelines outlined in this report are to be upheld.

Per the DCM Chapter 1, Section 4, the City of Fountain requires the UDFCD Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls.

Step 1: Reduce runoff by disconnecting impervious area, eliminating "unnecessary" impervious area and encouraging infiltration into soils that are suitable.

Site specific landscaping will be done on each lot to decrease the connectivity of impervious areas. Grass lined swales will be used where possible to allow ground infiltration. The open

space running along the existing gas right of way is a site-specific example of disconnection between impervious surfaces on this project.

## Step 2: Treat and slowly release the WQCV.

The proposed detention ponds meet or exceed the DCM standards for the release rates of Full Spectrum Detention Ponds for Water Quality Capture Volumes.

#### Step 3: Stabilize stream channels.

Drainage fees paid at the time of platting will be utilized in the construction of the future stream improvements in the Jimmy Camp Creek Drainage Fee Basin according to the City.

#### Onsite

Based on the available LIDAR contour data for the site, the existing channel has a slope of approximately 0.65%. Field investigations of the site appear to show a stable channel. There are four pond areas in the channel bottom providing stilling and energy dissipation. Per the DCM Figure 12-4 and the indicated DBPS Q100 of 2216 cfs the anticipated design slope for channel changes is 0.19%. Using these two slopes and a channel length through the Corvallis site of 2,652 feet, we anticipate approximately 12 feet of drop structures will be required. This will likely mean three 4' drop structures designed and placed to preserve the existing ponds. Depth of drop may vary slightly if the future channel improvements recommend changes to the sinuosity of the stream bed to optimize the synergy between the channel and the development and thereby alter the length and slope of the channel through this development.

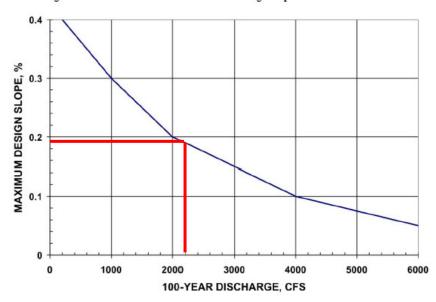


Figure 12-4. Maximum Low-flow Channel Design Slope for Sand-bed Channels

Another likely improvement will be rip rap slope protection along the outside banks on the bends of the channel meander to preserve the current or, if modifications are required, future planned stream path and protect adjacent infrastructure.

Field investigations of the channel show a series of three small, elongated ponds and one smaller pond.



Figure 1-South Pond

Southernmost pond above. The southernmost, as shown above, and the northernomost two ponds have flat and stable banks. (Note: Based on the South Pond's stable banks, improvements on the property to the west of Parcel D are not anticipated; however, if such improvements prove to be necessary, the developer will be required to coordinate with the owner of said property to achieve a construction easement or other form of access in order to complete channel improvements.)

Other ponds, as shown below, have short sections with steeper banks.



Figure 2-North End of Middle Pond

Sloughing of banks is very minimal and only evident in a couple of instances. One instance is visible in the upper right bank in the photo above. Most of the bare soil along the channel is caused by cattle grazing the area. The south end of the same pond shown in Figure 2 shows stable banks



Figure 3-South end of Middle Pond



Figure 4-North Elongated Pond Looking South

The northernmost of the elongated ponds is shown above. Note the shallow, steeper banks closer to the north end of the pond and the flatter banks towards the south end of the pond.



Figure 5-Northernmost Pond

Future improvements to the channel will likely involve laying back some of the steeper banks and providing a channel section more in line with the typical section indicated in the DCM.

INCORPORATE AQUATIC ECOLOGY CONSIDERATIONS FOR MAJOR 5. THE EXISTING CHANNEL CONDITIONS AND PROPOSED STREAMS IMPROVEMENTS SHALL BE MODELED IN HEC-RAS BASED ON THE CHANNEL AND OVERBANK DEFINITION SHOWN IMPROVEMENTS ONLY AS SHOWN IN HYDRAULIC PARAMETERS SHALL COMPLY WITH VALUES MASTER PLANS OR MAJOR IN TABLE 12-2. DRAINAGEWAY PLANS AS APPROVED. 100-YEAR FLOODPLAIN LOW FLOW LEFT OVERBANK CHANNEL RIGHT OVERBANK BASE FLOW CHANNEL LOW FLOW 100-YR WATER SURFACE WATER SURFACE POSSIBLE BASE FLOWS CREATE A STABLE LOW 4. UNSTABLE BANKS WITHIN THE 100-YR FLOW CHANNEL AND RESTORE FLOODPLAIN SHALL BE STABILIZED AS RESTORE CHANNEL STREAM APPROVED INVERT AS NECESSARY INVERT POSSIBLE EXISTING DEGRADATION VEGETATED BENCHES ADJACENT TO THE LOW FLOW CHANNEL SPREAD FLOWS GRADE CONTROL STRUCTURES TO THAT EXCEED LOW FLOW CHANNEL PROVIDE A STABLE LOW FLOW

Figure 12-3. Design Elements Associated With Major Natural Drainageways

The above section is already reflected in much of the channel. It is anticipated that future improvements will regrade the steeper banks of the channel to more closely match this section, add overbanks for lower probability flows where they are lacking, and armor the outside banks of bends in the stream. Drop structures will likely be constructed between the existing pond areas in an attempt to preserve, and limit disturbance to, the wetlands, but some minor modifications of the middle pond location may be required to facilitate the proposed crossing of the stream by Residential Collector A.

Given the existing apparent stability of much of the channel, it may be more optimal to use some buried drop structures in some locations of the channel design to preserve the existing channel conditions, spot fix areas with bank issues and place normal drop structures as appropriate to preserve the channel flow line and ponded areas.

The future channel design report will consider the above factors as well as any potential changes to the design criteria which have arisen in the interim.





Figure 6 & 7-Jimmy Camp Creek-West Fork Looking North from South End of Property

## **Downstream of Corvallis**

Just south of the south boundary of this proposed development Jimmy Camp Creek-West Fork discharges across what appears to be an existing utility maintenance road. HEC-RAS analysis of the stream using the 2018 LIDAR elevation info and the MDDPA flows indicates that both the 5-year and the 100-year events will surcharge the road (See section below). The analysis also indicates that the velocities anticipated across the structure appear to be within the DCM criteria for stable channel design in erosive soils (Q100  $\leq$  5.0 ft/s and Q5  $\leq$  3.5 ft/s).

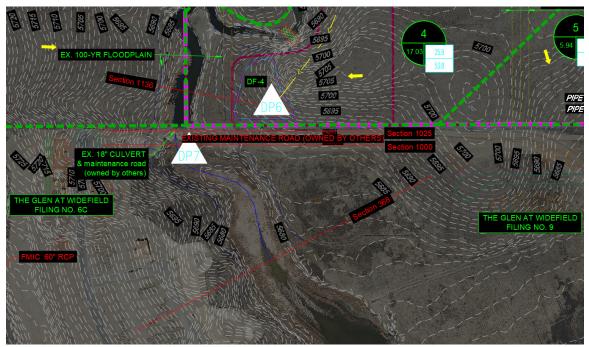


Figure 7 - HEC-RAS: Layout

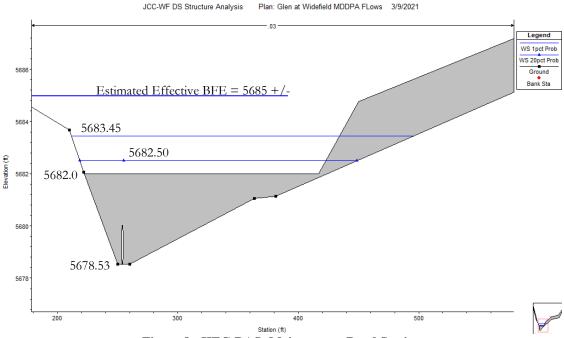


Figure 8 - HEC-RAS: Maintenance Road Section

Reach	River Sta	Profile	E.G. US.	W.S. US.	E.G. IC	E.G. OC	Min El Weir Flow	Q Culv Group	Q Weir	Delta WS	Culv Vel US	Culv Vel DS
			(ft)	(ft)	(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft/s)	(ft/s)
WF	1012.5 Culvert #2	1pct Prob	5684.61	5684.54	5682.05	5684.61	5682.01	13.57	2017.97	2.09	7.68	7.68
WF	1012.5 Culvert #2	20pct Prob	5682.94	5682.94	5682.93	5682.94	5682.01	14.00	388.20	2.30	7.92	7.92

Figure 9 - HEC-RAS: Culvert Analysis Results

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
WF	1851	1pct Prob	2020.00	5680.00	5684.73		5684.77	0.000202	1.69	1219.95	358.39	0.15
WF	1851	20pct Prob	401.00	5680.00	5682.96		5682.97	0.000068	0.64	624.39	317.40	0.08
WF	1686	1pct Prob	2020.00	5677.20	5684.71		5684.75	0.000113	1.50	1390.34	401.09	0.12
WF	1686	20pct Prob	401.00	5677.20	5682.96		5682.96	0.000017	0.46	871.17	255.99	0.04
WF	1637	1pct Prob	2020.00	5677.20	5684.70		5684.74	0.000113	1.50	1387.99	400.80	0.12
WF	1637	20pct Prob	401.00	5677.20	5682.96		5682.96	0.000017	0.46	870.92	255.98	0.04
WF	1136	1pct Prob	2020.00	5678.70	5684.56		5684.65	0.000324	2.35	875.24	264.83	0.20
WF	1136	20pct Prob	401.00	5678.70	5682.94		5682.95	0.000043	0.72	553.86	166.40	0.07
WF	1025	1pct Prob	2020.00	5678.70	5684.54	5680.64	5684.61	0.000230	2.19	944.30	257.31	0.17
WF	1025	20pct Prob	401.00	5678.70	5682.94	5679.37	5682.94	0.000029	0.63	632.19	173.53	0.06
WF	1012.5		Culvert									
WF	1000	1pct Prob	2020.00	5678.53	5682.45	5681.69	5682.77	0.003526	4.58	441.30	226.99	0.58
WF	1000	20pct Prob	401.00	5678.53	5680.64	5680.09	5680.78	0.003246	3.09	129.86	113.29	0.51
WF	368	1pct Prob	2020.00	5678.00	5680.84	5679.70	5681.11	0.002002	4.15	486.25	188.99	0.46
WF	368	20pct Prob	401.00	5678.00	5679.09	5678.59	5679.18	0.002002	2.29	175.36	167.11	0.39

Figure 10 - HEC-RAS: Cross Section Analysis (Maintenance Road at Section 1012.5)

Jimmy Camp Creek-West Fork, immediately downstream of the above-mentioned structure, runs through the Glen at Widefield development in El Paso County. Specifically, the stream runs between Filings 6 and 9 of Glen at Widefield. (The photo below is looking southeasterly towards Filing 6.) As part of these developments, improvements to WFJCC were required and have been constructed. According to MDDPA, these improvements anticipated flows of Q5: 401 cfs and Q100: 2020 cfs. Our proposed discharge from the site is lower for both storms. (Q5: 396.4 cfs & Q100: 2009.1 cfs); therefore, the proposed Corvallis development complies with the design of the downstream infrastructure. Field visits to the site appear to confirm that the channel through Glen at Widefield has been stabilized. Please note the well vegetated channel in the photo looking southwesterly into Glen at Widefield below:



Figure 11- Jimmy Camp Creek-West Fork Looking South into Glenn at Widefield

## Step 4: Implement source controls.

During construction, the contractor will have designated concrete washout areas and will implement sediment control logs and inlet protection in order to control pollutants at their source. If long term stockpiling of materials is desired, further source controls must be designed to comply with the GEC and SWMP criteria.

#### C. PERMITTING REQUIREMENTS

A USACE 404 permit and PPRBD floodplain development permit are anticipated permits which will be required along with the future channel improvements.

## VI. Selected Plan

#### A. PLAN HYDROLOGY

#### Land Use

In the approved *WFJCC DBPS*, this area was specified as the "Crescent Heights Development" and was anticipated to have medium/high density residential as well as office and commercial. In compliance with the *WFJCC DBPS*, Corvallis is anticipated to be a multi-use planned unit development. Anticipated developed uses include commercial, multi-family residential, and single-family residential (1/8 acre or less). Some portions of the site will remain as undeveloped open space. The land use map from the *WFJCC DBPS* is included in the Appendix D.

#### Runoff

The proposed 297-acre site is located entirely within the West Fork Jimmy Camp Creek. This tributary has a drainage area of 4 square miles according to *WFJCC DBPS*. The developed area makes up less than 11% of the tributary's drainage area.

As noted in Section II-C, 81 percent of the site is made up of Type B soils. Drainage coefficients for HSG A&B soil types used were per Table 6-6 in the DCM. Refer to Appendix A for specific runoff coefficient values.

#### Flows

According to **WFJCC DBPS**, the Corvallis (Crescent Heights) development will discharge at 3 separate points. Per UD-Detention modeling of the proposed detention basin, detention from this project will either be equal to or reduce the Q100 (Major Storm) discharge from the property from the pre-development. As the proposed development is not projected to increase runoff from the site, no additional burden should be placed on downstream drainage and detention basins. Additionally, due to the large size of the offsite drainage areas, the peak discharges from the proposed detention ponds are significantly offset from the peak flows from the offsite basins.

The hydrology for the site, which has been provided above, shows that this development complies with the latest study (*WFJCC DBPS*).

#### B. SYSTEM PRIORITIES/PHASING

No phasing of the development has been provided at this time. Once development of any portion of the site begins, the owner will be responsible for providing detention and water quality in accordance with this *MDDP* and the *WFJCC DBPS*, before releasing downstream.

Additionally, any proposed development within the West Basin (Which contains all portions of the first developable piece of property measured perpendicularly from the channel outwards.) within Corvallis will initiate the requirement for a channel design study of WFJCC through the development to be submitted to the City along with the PDR/FDR.

#### C. GOVERNMENTAL AGENCY REQUIREMENTS

Other than the USACE 404 permit, there are no external governmental agency requirements for this development. A final Drainage Report for each future phase of development will be presented to the City of Fountain with the development of the construction documents.

## D. MAINTENANCE REQUIREMENTS

All proposed road and drainage construction within the Corvallis development will be performed to City of Fountain standards. Proposed roads and drainage facilities within the public right of way will be maintained by the City of Fountain upon acceptance of these facilities after the warranty period. The proposed detention ponds will be privately owned and maintained by the metropolitan district. Maintenance requirements for all stormwater quality and erosion control procedures will be outlined in individual Erosion Control and Storm Water Management Plans. A Maintenance Road (as well as access to this road from public right-of-way) for the portion of West Fork of Jimmy Camp Creek running through the Corvallis site must be provided.

#### E. RECOMMENDATION FOR IMPLEMENTATION

It is recommended that any development of the site initiates the implementation of the detention and water quality procedures that have been detailed in this report. In doing so, the developed conditions will produce runoff comparable to or lower than existing conditions, which allows continued adherence to **WFJCC DBPS** and protects downstream owners and facilities.

#### F. EXCLUSIONS FROM ORIGINAL DBPS RECOMMENDATIONS:

A few items which are recommended in the initial DBPS have fallen out of favor in the governing drainage design criteria and will not be implemented in the proposed development. One item is the on-stream detention pond located on Jimmy Camp Creek-West Fork (Detention Basin 3031). This will be replaced by on-site or sub-regional detention basins which are offline from West Fork Jimmy Camp Creek.

The other item is the concrete checks called out every 150-200 feet along the channels through the site. Current best practice channel design criteria do not recommend these checks in this application due to associated channel maintenance/stability issues. The general guidelines (described in Section V. B. Step 3) call for grouted rip rap drop structures which is a current best practice device for channel drops, however this item will be subject to the best practices at time of design.

Other than the two above items, proposed detention pond locations for this development do not match exactly the locations indicated in the DBPS, but fulfill the intent described in that report. The proposed development will discharge to downstream infrastructure at or below the predevelopment rates indicated in the referenced studies.

## VII. Fee Development

## A. Construction Cost Opinion

An engineer's estimate of probable construction costs will be provided with the Final Drainage Report for each phase of the development. The developer will pay all capital costs for the proposed roadway and drainage facilities.

## B. Drainage Basin Fees

Drainage basin fees will be paid at the time of plat recordation. More detailed analysis of these fees will be completed in the appropriate PDR/FDR for each phase of the development.

## a. Estimated Cost of Channel Improvements

	Corvallis PUD West Fork - Jimmy Camp Creek Engineer's Opinion of Probable Cost									
BID ITEM NO.	DESCRIPTION OF BID ITEM	QUANTITY	PAY UNIT	UNIT PRICE	TOTAL COST OF BID ITEM					
1	Mobilization	1	LS	\$100,000.00	\$100,000					
2	Water Control & Dewatering	1	LS	\$60,000.00	\$60,000					
3	Erosion & Sediment Control	1	LS	\$30,000.00	\$30,000					
4	Clearing & Grubbing	1	LS	\$10,000.00	\$10,000					
5	Drop Structures (4 ft)	4	EA	\$190,000.00	\$760,000					
6	Seeding (Wetland, Riparian, Upland)	1	LS	\$20,000.00	\$20,000					
7	Willow Stakes	1	LS	\$10,000.00	\$10,000					
8	Erosion Control Blanket	500	SY	\$20.00	\$10,000					
9	Earthwork (Onsite Cut & Fill)	1	LS	\$20,000.00	\$20,000					
10	Soil Rip Rap (Outside Bends)	2,200	SY	\$100.00	\$220,000					
11	CDOT Class II Road Base (Access Road)	765	СУ	\$85.00	\$65,000					
	/			Subtotal	\$1,305,000					
			100	√₀ Contingency	\$130,500					
				Engineering	\$78,300					
			Estin	nated Total Cost	\$1,513,800					
			De	eveloped Acres	297					
				Anticipated / Developed AC.	\$5,093					

Since the engineer has no control over the cost of labor, materials, equipment or services furnished by others, or over the contractor's method of determining prices, or over the competitive bidding or market conditions, the opinion of probable construction costs provided herein are made on the basis of the engineer's experience and qualifications and represents the best judgment as an experienced and qualified professional familiar with the construction industry. The engineer cannot, and does not guarantee that proposals, bid or actual construction costs will not vary from the opinion of probable costs.

Construction costs for channel improvements will be paid for by the Metropolitan District and provided by the developer. The Metropolitan District will be reimbursed via mill levees. To the extent possible, acquisition of easements, tracts or land will be the responsibility of the developer.

## VIII. Summary

As described above, this report demonstrates compliance with the governing DCM and DBPS and will comply with downstream drainage reports.

## IX. References

- 1. City of Colorado Springs Drainage Criteria Manual, City of Colorado Springs, May 2014
- 2. Web Soil Survey of El Paso County Area, Colorado. Unites States Department of Agriculture Soil Conservation Service, November 2015.
- 3. Flood Insurance Rate Maps for El Paso County, Colorado and Incorporated Areas, Panel 958 of 1300, Federal Emergency Management Agency, Effective Date December 7, 2018.
- **4.** *Urban Storm Drainage Criteria Manual, Vol. 1-3* by Urban Drainage and Flood Control District (UDFCD), January 2016
- 5. West Fork Jimmy Camp Creek Drainage Basin Planning Study (WFJCC DBPS), by Kiowa Engineering Corp. October 2003.
- **6.** *Master Drainage Development Plan (MDDP) The Glen at Widefield,* by Kiowa Engineering Corp. December 1999.
- 7. *Master Drainage Development Plan Amendment (MDDPA) The Glen at Widefield,* by Kiowa Engineering Corp. June 2007.
- **8.** Final Drainage Report (FDR F9) The Glen at Widefield Filing No. 9, by Kiowa Engineering Corp. July 2018.
- 9. Final Drainage Report (FDR F11) The Glen at Widefield Filing No. 11, by Kiowa Engineering Corp. December 2019.

# **APPENDIXA**

HYDROLOGIC AND HYDRAULIC CALCULATIONS

Page 1 Corvallis - Rational Calculations.xls

cet Name:
Corvallis
Pountain, CO
Igner
NMS
Existing Conditions

Average Channel Velocity

Corvallis
Fountain, CO
Fountain,

Channel Flow Type Key

Heavy Meadow 2

Tillage/Field 3

Short Pasture and Lawns 4

Nearly Bare Ground 5

Grassed Waterway 6

Payed Accor 7

Average Channel Velocity  Average Slope for Initial Flow		0.04			are used, this	u, this will be ig vill be ignored)	norea)																		Paved Areas														
		In	pervious %		7			2			65		100																										
		ea	Rational 'C' Values										Flow Lengths Initial Flow										Chann	nel Flow			Tc		Ra	Rainfall Inte		4							
Basin	Description		Surface Type 1 (Single-Family 1 & 1/3 Ac. Lots						Surface Type 2 (Greenbelts & Agriculture)					e 4 s)	Weighted C-Factor	Initi	l True Initial	Channel	True Channe	High Poin	Low Point	Average	Initial High	n Point	Low Point	Average	Channel Flow Type (See Key above)	Velocity	Channel	Γotal i2	ı (	Q2 i	i5	Q5	i10	Q10	i100	Q100	% Imp
		SF	Acres	C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C5 C100	Area	C5 C100	ft	Length ft	ft	Length ft	Elevation	Elevation	Slope	Tc (min) Ele	vation	Elevation	Slope	Ground Type	(ft/s)	Tc (min) (	min) in/	hr	cfs in/	in/hr	cfs i	in/hr	cfs	in/hr	cfs	1 !
OS-1a	Single Family > 2.5 Acre Lots (12% Impervious (min.))	1,675,407	38.46	0.20	0.44		0.09	0.36	1474358	0.45	0.59		0.90 0.96 2	201049	0.19 0.44	300	300	2,290	2290	5,807	5,800	0.023	22.2 5	800	5,725	3.28	4	1.3	30.5	52.7 1.4	4 1	10.1	1.7	12.7	2.0	14.8	2.9	49.3	13.8%
OS-1b	Single Family > 2.5 Acre Lots (12% Impervious (min.))	1,668,351	38.30	0.20	0.44		0.09	0.36	1468149	0.45	0.59		0.90 0.96 2	200202	0.19 0.44	900	300	1,871	2471	5,894	5,820	0.082	14.6 5	820	5,780	2.14	4	1.0	40.6	55.2 1.3	3	9.7	1.7	12.3	1.9	14.3	2.8	47.7	13.8%
OS-2	Fontaine Boulevard to crown of road	42809	0.98	0.20	0.44		0.09	0.36		0.45	0.59		0.90 0.96 4	42809	0.90 0.96	25	25	1362	1362	5758	5757	0.040	1.2 5	757	5719	2.79	7	3.3	6.9	8.1 3	.5	3.1 4.	4.4	3.9	5.2	4.6	7.4	7.1	100.0%
OS-3	Offsite undeveloped parcel	80878	1.86	0.20	0.44		0.09	0.36	80878	0.45	0.59		0.90 0.96		0.09 0.36	170	170	275	275	5739	5718	0.124	10.7 5	718	5703	5.45	3	1.2	3.9	14.6 2.5	.8	0.5 3.	3.5	0.6	4.1	0.7	5.9	4.0	2.0%
OS-4	Offsite undeveloped parcel	797941	18.32	0.20	0.44		0.09	0.36	797941	0.45	0.59		0.90 0.96		0.09 0.36	301	300	1018	1019	5732	5719	0.043	20.1 5	719	5696	2.26	3	0.7	22.9	43.0 1.0	.6	2.6 2	2.0	3.3	2.3	3.8	3.3	21.8	2.0%
OS-5	Fontaine Boulevard to crown of road	32917	0.76	0.20	0.44		0.09	0.36		0.45	0.59		0.90 0.96 3	32917	0.90 0.96	25	25	1100	1100	5771	5770	0.040	1.2 5	770	5740	2.73	7	3.3	5.6	6.8 3.	.7	2.6	4.7	3.2	5.5	3.8	7.9	5.8	100.0%
OS-6	Fontaine Boulevard to crown of road	33529	0.77	0.20	0.44		0.09	0.36		0.45	0.59		0.90 0.96 3	33529	0.90 0.96	25	25	1100	1100	5771	5770	0.040	1.2 5	770	5743	2.45	7	3.1	5.9	7.1 3.	.7	2.6	4.6	3.2	5.4	3.8	7.8	5.8	100.0%
OS-7	Single Family Residential to east	126529	2.90	0.20	0.44	126529	0.09	0.36		0.45	0.59		0.90 0.96		0.20 0.44	40	40	160	160	5708	5706	0.050	6.2 5	706	5702	2.50	4	1.1	2.4	8.6 3.4	.4 2	2.0 4.	4.3	2.5	5.1	3.0	7.3	9.4	7.0%
1-D (OS-8)	Offsite undeveloped parcel	961463	22.07	0.20	0.44		0.09	0.36	961463	0.45	0.59		0.90 0.96		0.09 0.36	300	300	1055	1055	5731	5715	0.053	18.7 5	715	5682	3.13	3	0.9	20.0	38.7 1.	.7	3.3 2	2.1	4.2	2.4	4.9	3.5	28.1	2.0%
EX-1	West side of site	2959892	67.95	0.20	0.44		0.09	0.36	2959892	0.45	0.59		0.90 0.96		0.09 0.36	300	300	2266	2266	5753	5736	0.057	18.3 5	736	5682	2.38	3	0.8	49.8	68.2 1.3	.2 /	7.1 1	1.5	9.0	1.7	10.5	2.4	60.3	2.0%
EX-2	Northwest corner	449242	10.31	0.20	0.44		0.09	0.36	449242	0.45	0.59		0.90 0.96		0.09 0.36	300	300	350	350	5752	5738	0.047	19.6 5	738	5719	5.43	3	1.2	5.0	24.6 2.1	1 /	2.0 2	2.7	2.5	3.2	3.0	4.5	17.0	2.0%
EX-3	Central-west	2262585	51.94	0.20	0.44		0.09	0.36	2262585	0.45	0.59		0.90 0.96		0.09 0.36		300	1530	1530	5740	5728	0.040	20.6 5	728	5688	2.61	3	0.8	31.6	52.2	.4 6	6.5		8.2		9.5		54.8	
EX-4	Central-east	2551274	58.57	0.20	0.44		0.09	0.36	2551274	0.45	0.59		0.90 0.96		0.09 0.36		300	2710	2710	5768	5756	0.040	20.6 5	756	5685	2.62	3	0.8	56.0	76.6			1.3	7.2	1.6	8.3	2.3	48.1	
EX-5	East side of site	3769253	86.53	0.20	0.44		0.09	0.36	3769253	0.45	0.59		0.90 0.96		0.09 0.36	300	300	1830	1830	5770	5765	0.017	27.6 5	765	5686	4.32	3	1.0	29.4	57.0 1.3	.3 1	10.2	1.6	12.8	1.9	15.0	2.7	86.3	2.0%
									Rational '	C! Values							Flow	Lengths	1			Flow				Chann	nel Flow			Tc		D.	ainfall Int	ancity & D	Rational Flow Rate				1
DESIGN POINT		Ar	ea		Surface Type Family 1 & 1/			Surface Type nbelts & Agr	e 2 iculture)	Single- &	urface Type 3 Family 1/8 Ac. Multi-Family)	)	Surface Type (Imperviou	is)	Weighted C-Factor	Initi			True Channe	l High Poin			Initial High	n Point	Low Point		Channel Flow	Velocity	Channel		2 1					Q10			% Imp
	Description	SF		C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C10 C100	Area	C5 C100	ft	Length ft	ft	Length ft	Elevation	Elevation	Slope	Tc (min) Ele	vation	Elevation	Slope	Ground Type	(ft/s)	Tc (min) (	min) in/	hr	cfs in/	n/hr	cfs i	in/hr	cfs		cfs	
	OS-1, OS-2		76.76		0.44	0	0.09	0.36	2942507	0.45	0.59	0	0.90 0.96 4	01251	0.19 0.44	300		2290	2290	5807	5800	0.023	22.2 5	800	5725	3.28	4	1.3	30.5	52.7 1.4	.4 2	20.1 1.				29.5		7.010	13.8%
	OS-2, EX-2	492051		0.20	0.44	0	0.09	0.36	449242	0.45	0.59		0.90 0.96	1000	0.17 0.42	300	300	350	350	0.02	5738	0.00.11	10.0	738	5719	5.43	3	1.2	5.0	23.0 2.:		110		5.4	0.0	6.3		22.5	10.5%
	E2, OS-3, OS-4		31.47			0	0.09						0.90 0.96 4					1550	1000	5752	5738	010 11	1710		5703	2.26	3	0.7	34.8	0010		5.1 1.					2.9		
	E1, E3, EX-1, OS-8	8635982	198.25	0.20	0.44	0	0.09	0.36	8191923	0.45	0.59	0	0.90 0.96 4	144060	0.14 0.40	300	300	2290	2290	5807	5800	0.023	22.2 5	800	5682	5.15	3	1.1	33.8	56.0 1.:	.3 3	36.7 1.	1.7	46.3	1.9	54.0	2.8	222.3	7.0%

Note: Q2, Q5 & Q10 are based on C5; Q25, Q50 & Q100 are based on C100

oject Name: Corv oject Location: Four **Matrix** 

Channel Flow Type Key
Heavy Meadow 2
Tillage/Field 3
Short Pasture and Lawns 4
Nearly Bare Ground 5
Grassed Waterway 6
Paved Areas 7

Average Channel Velocity 5 ft/s (If specific channel vel is used, this will be ignored) rerage Slope for Initial Flow 0.04 ft/ft (If Elevations are used, this will be ignored)

		Area				•		•	Ration	al 'C' Values						,	Flow L	engths	,		Initial Flo	v			Channe	el Flow			Tc	Rainfall	Intensity & I	Rational Flow	Rate		
Basin	Description				Surface Type amily 1 & 1/2		(Gre	Surface Type enbelts & Agric		(Singl	Surface Type e-Family 1/8 & Multi-Fami	Ac. Lots	Surface Type 4 (Impervious)		ghted actor	Initial	True Initial	Channel	True Channel	High Point	Low Point A	erage Init	ial High Point	t Low Point	Average	Channel Flow Type (See Key above)	Velocity	y Channel	Total	Q2 is	Q5	i100	Q100	% Imp	Impervious (Acres)
	SF	Ac	cres	C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C5 C100 Area	C5	C100	ft	Length ft	ft	Length ft	Elevation	Elevation	lope Tc (r	nin) Elevation	Elevation	Slope	Ground Type	(ft/s)	Tc (min)	(min)	cfs in/	hr cfs	in/hr	cfs		
OS-1a	Single Family > 2.5 Acre Lots (12% Impervious (min.)) 1,675,	407 38.	3.46	0.20	0.44		0.09	0.36	1474358	0.45	0.59		0.90 0.96 201049	0.19	0.44	300	300	2,290	2290	5,807	5,800	0.023 22	2 5800	5,725	3.28	4	1.3	30.5	52.7	10.1	12.7	2.9	49.3	13.8%	
OS-1b	Single Family > 2.5 Acre Lots (12% Impervious (min.)) 1,668,	351 38.	3.30	0.20	0.44		0.09	0.36	1468149	0.45	0.59		0.90 0.96 200202	0.19	0.44	900	300	1,871	2471	5,894	5,820	0.082 14	6 5820	5,780	2.14	4	1.0	40.6	55.2	9.7 1.	12.3	2.8	47.7	13.8%	
OS-2	Fontaine BLVD 42,80	09 0.	.98	0.20	0.44		0.09	0.36		0.45	0.59		0.90 0.96 42809	0.90	0.96	25	25	1,362	1362	5,758	5,757	0.040 1.3	2 5757	5,719	2.79	7	3.3	6.9	8.1	3.1 4.	3.9	7.4	7.1	100.0%	
OS-3			.86	0.20	0.44		0.09	0.36	80878	0.45	0.59		0.90 0.96	0.09	0.36	170	170	275	275	5,739	5,718	0.124 10.	7 5718	5,703	5.45	2	0.6	7.9	18.5	0.4 3.	0.5	5.3	3.5	2.0%	
OS-4	Aggricultural Land 797,9	18.	3.32	0.20	0.44		0.09	0.36	797941	0.45	0.59		0.90 0.96	0.09	0.36	300	300	1,018	1018	5,732	5,719	0.043 20.	1 5719	5,696	2.26	2	0.4	45.8	65.8	2.0 1.	2.5	2.5	16.6	2.0%	
OS-5	Fontaine BLVD 32,9	17 0.	.76	0.20	0.44		0.09	0.36		0.45	0.59		0.90 0.96 32917	0.90	0.96	25	25	1,100	1100	5,771	5,770	0.040 1.3	2 5770	5,740	2.73	7	3.3	5.6	6.8	2.6 4.	3.2	7.9	5.8	100.0%	
OS-6	Fontaine BLVD 33,52	29 0.	.77	0.20	0.44		0.09	0.36		0.45	0.59		0.90 0.96 33529	0.90	0.96	25	25	1,100	1100	5,771	5,770	0.040 1.3	2 5770	5,743	2.45	7	3.1	5.9	7.1	2.6 4.	3.2	7.8	5.8	100.0%	
OS-7	Back of Lots in Cottonwood Grove F1 126,5	29 2.	.90	0.20	0.44	126529	0.09	0.36		0.45	0.59		0.90 0.96	0.20	0.44	40	40	160	160	5,708	5,706	0.050 6.3	2 5706	5,702	2.50	4	1.1	2.4	8.6	2.0 4.	2.5	7.3	9.4	30.0%	
1.4	Single Family Residential 1,205,	866 27.	7.68	0.20	0.44		0.09	0.36		0.45	0.59	1205866	0.90 0.96	0.45	0.59	50	50	2,025	2025	5,775	5,772	0.070 4.	5 5772	5,694	3.85	6	2.9	11.5	16.0	33.4 3.	42.2	5.6	92.9	65.0%	17.99
1B	Commercial 693,8	368 15.	5.93	0.20	0.44		0.09	0.36	146832	0.45	0.59		0.90 0.96 547036	0.73	0.84	50	50	940	940	5,745	5,744	0.020 3.	5744	5,714	3.19	7	3.5	4.4	8.3	40.8 4.	51.4	7.4	99.3	79.3%	12.63
1D (Formerly OS-8)	Single-Family Residential/Open Space 961,4	163 22	2.07	0.20	0.44		0.09	0.36	426983	0.45	0.59	534480	0.90 0.96	0.30	0.49	50	50	940	940	5,745	5,744	0.020 8.	4 5744	5,714	3.19	7	3.5	4.4	12.8	19.6 3.	24.8	6.2	67.9	37.0%	8.17
2	Single Family Residential 1,171,	681 26.	5.90	0.20	0.44		0.09	0.36		0.45	0.59	1171681	0.90 0.96	0.45	0.59	50	50	1,916	1916	5,758	5,746	0.240 3.0	5746	5,698	2.51	6	2.4	13.5	16.4	32.1 3.	40.5	5.6	89.2	65.0%	17.48
3	Open Space 701,9	088 16.	5.12	0.20	0.44		0.09	0.36	647388	0.45	0.59	54600	0.90 0.96	0.12	0.38	50	50	875	875	5,714	5,712	0.040 8.3	2 5712	5,682	3.43	3	0.9	15.8	24.0	4.2 2.	5.3	4.6	28.4	6.9%	1.11
4	School 741,7	755 17.	7.03	0.20	0.44		0.09	0.36	97368	0.45	0.59	417195	0.90 0.96 227192	0.55	0.68	50	50	1,390	1390	5,707	5,704	0.060 4.	5704	5,695	0.65	6	1.2	19.9	23.9	20.6 2.	25.9	4.6	53.8	67.5%	11.49
5		738 5.1	.94	0.20	0.44		0.09	0.36	77622	0.45	0.59		0.90 0.96 181117	0.66	0.78	50	50	425	425	5,710	5,708	0.040 3.	7 5708	5,686	5.18	6	3.4	2.1	5.8	15.4 4.	19.4	8.3	38.6	70.6%	4.19
6	Single-Family Residential 437,6	10.	0.05	0.20	0.44		0.09	0.36		0.45	0.59	437611	0.90 0.96	0.45	0.59	50	50	1,039	1039	5,717	5,716	0.020 6.3	3 5716	5,698	1.78	6	2.0	8.9	15.7	12.3 3.	15.5	5.7	34.1	65.0%	6.53
7	Open Space / Single-Family Residential 840,2	270 19.	).29	0.20	0.44		0.09	0.36	840270	0.45	0.59		0.90 0.96	0.09	0.36	300	300	1,477	1477	5,739	5,736	0.010 32	7 5736	5,700	2.44	3	0.8	31.8	64.5	2.1 1.	2.6	2.5	17.8	2.0%	0.39
8	Commercial 282,9	034 6	.50	0.20	0.44		0.09	0.36	14147	0.45	0.59		0.90 0.96 268787	0.86	0.93	50	50	610	610	5,767	5,763	0.080 1.	5 5763	5,749	2.30	7	3.0	3.4	5.0	22.8 5.	28.7	7 8.6	52.2	95.1%	6.18
9	Single-Family Residential 875,9	72 20.	).11	0.20	0.44		0.09	0.36	106346	0.45	0.59	769626	0.90 0.96	0.41	0.57	50	50	827	827	5,767	5,764	0.060 5.	5764	5,732	3.87	6	2.9	4.7	9.7	27.3 4.	34.4	7.0	80.5	57.4%	11.53
10	Single-Family Residential 688,5	24 15	5.81	0.20	0.44		0.09	0.36	112459	0.45	0.59	576065	0.90 0.96	0.40	0.56	50	50	960	960	5,730	5,728	0.050 5.	4 5728	5,702	2.66	6	2.4	6.6	12.0	<b>19.3</b> 3.	24.3	6.4	57.2	54.7%	8.65
11	Multi-Family Residential 650,5	06 14	1.93	0.20	0.44		0.09	0.36	68366	0.45	0.59	582140	0.90 0.96	0.42	0.57	50	50	1,241	1241	5,725	5,724	0.020 7.	1 5724	5,686	3.06	6	2.6	8.0	15.1	17.3 3.	21.8	5.8	49.8	58.4%	8.72
12	Single-Family Residential 750,7	53 17.	7.23	0.20	0.44		0.09	0.36		0.45	0.59	750753	0.90 0.96	0.45	0.59	50	50	1,484	1484	5,770	5,768	0.040 5.	4 5768	5,733	2.36	7	3.0	8.2	13.6	22.5 3.	28.3	6.1	62.4	65.0%	11.20
13	Single-Family Residential 227,9	143 5	.23	0.20	0.44		0.09	0.36		0.45	0.59	227943	0.90 0.96	0.45	0.59	50	50	484	484	5,756	5,754	0.040 5.	4 5754	5,731	4.75	6	3.3	2.5	7.9	8.4 4.	10.6	7.5	23.3	65.0%	3.40
14	Single-Family Residential 485,4	74 11.	.14	0.20	0.44		0.09	0.36		0.45	0.59	485474	0.90 0.96	0.45	0.59	50	50	1,030	1030	5,728	5,727	0.020 6.3	3 5727	5,695	3.11	6	2.6	6.5	13.3	14.6 3.	18.5	6.1	40.6	65.0%	7.24
15	Single-Family Residential 765,2	200 17.	7.57	0.20	0.44		0.09	0.36		0.45	0.59	765200	0.90 0.96	0.45	0.59	50	50	1,095	1095	5,725	5,723	0.040 5	4 5723	5,688	3.20	6	2.6	6.9	12.3	23.9 3.	30.1	6.3	66.2	65.0%	11.42
16	Commercial and Park 1,417,	785 32	2.55	0.20	0.44		0.09	0.36	286493	0.45	0.59		0.90 0.96 1131292	2 0.74	0.84	50	50	1,511	1511	5,727	5,724	0.060 2.	5 5724	5,687	2.45	7	3.1	8.1	10.7	76.9 4.	96.9	6.7	184.8	80.2%	26.10
17	Commercial 143,5	72 3.	.30	0.20	0.44		0.09	0.36	7179	0.45	0.59		0.90 0.96 136393	0.86	0.93	50	50	175	175	5,688	5,687	0.020 2.	5 5687	5,686	0.57	7	1.4	2.1	5.0	11.6 5.	14.6	8.6	26.5	95.1%	3.13
						·	·		•		•						•			•				•										44%	177.56
									Ration	al 'C' Values							Flow L	engths			Initial Flo	v			Channe	el Flow			Tc	Rainfall	Intensity & I	Rational Flow	Rate		
											C. of an Tona															Channel Flow									7

																								itial Flow														44%	177.56
				Rational 'C' Values														Flow Lengths									Chan	nel Flow			Tc	Rai	ainfall Intensit						
PROPOSED DESIGN POINT			Area		Surface Type -Family 1 & 1/		(Gre	Surface Ty eenbelts & Aş		(Sing	Surface Typ de-Family 1/ & Multi-Far	8 Ac. Lots		Surface (Imper	rious)		ighted Factor	Initial	True Initi	al Channel	True Char	nel High Poir	nt Low Po	oint Averag	ge Initia	l High Point	Low Point	Average	Channel Flow Type (See Key above)		Channel	Total	Q2	i5	Q5	i100	Q100 %	% Imp	
	Description	SF	Acres	C5	C100	Area (SF)	C5	C100	Area (SF	C5	C100	Are	ea C	10 C100	Area	C5	C100	ft	Length i	t ft	Length	t Elevation	n Elevati	ion Slope	Tc (m	in) Elevation	Elevation	Slope	Ground Type	(ft/s)	Tc (min)	(min)	cfs	in/hr	cfs	in/hr	cfs		
E1	OS-1a and OS-1b	3,343,757	76.76	0.20	0.44	0	0.09	0.36	2942507	0.45	0.59	0	0.	90 0.96	401251	0.19	0.44	900	300	3,152	3752	5,885	5,820	0.072	15.2	5820	5,725	3.01	4	1.2	51.6	66.8	17.2	1.5	21.7	2.5	84.4	13.8%	10.56
DP1	E1+DF-1 Release+DF-2 Release	4,549,623	104.44	0.20	0.44	0	0.09	0.36	2942507	0.45	0.59	1205	866 0.	90 0.96	401251	0.26	0.48	900	300	5,177	5777	5,885	5,820	0.072	14.1	5820	5,694	2.44	7	3.1	31.1	45.2			25.3		110.3	27.3%	28.56
DP2	OS-2, 1.A, 1D, 2, 3	4,083,807	93.75	0.20	0.44	0	0.09	0.36	1,074,371	0.45	0.59	2,966	,627 0.	90 0.96	42,809	0.37	0.54	50	50	1,916	1916	5,758	5,746	0.240	3.3	5746	5,698	2.51	7	3.2	10.1	13.4	100.9	3.6	127.1	6.1	311.7	48.8%	45.74
DP3	DP1+DP2 Treated (DF-3 Release)	8,633,430	198.20	0.20	0.44	0	0.09	0.36	4016878	0.45	0.59	4172	493 0.	90 0.96	444060	0.31	0.51	900	300	5,177	5777	5,885	5,820	0.072	13.2	5820	5,681	2.68	7	3.2	29.9	43.1	96.0		33.6		185.2	37.5%	74.30
DP4	7	840,270	19.29	0.20	0.44	0	0.09	0.36	854416	0.45	0.59	0	0.	90 0.96	268787	0.38	0.68	50	50	2,087	2087	5,767	5,763	0.080	4.8	5763	5,700	3.02	7	3.5	10.0	14.8	20.4		2.6		17.8	34.0%	6.56
DP5	OS-3, OS4, DPBS 3020, DP4	2,011,951	46.19	0.20	0.44	0	0.09	0.36	1733235	0.45	0.59	0	0.	90 0.96	268787	0.20	0.44	300	300	1,018	1018	5,732	5,719	0.043	17.9	5719	5,696	2.26	6	2.2	7.6	25.5	19.6		352.6		1798.9	15.1%	6.97
DP6	4, 6	1,179,360	27.07	0.20	0.44	0	0.09	0.36	97368	0.45	0.59	8548	306 0.	90 0.96	227192	0.51	0.65	50	50	2,106	2106	5,717	5,716	0.020	6.2	5716	5,695	1.00	4	0.7	52.9	59.0	17.7	1.6	22.3	2.7	47.7	66.5%	18.02
DP7	DP3+DP5+DP6 Treated (DF-4 Release)	11,824,74	7 271.46	0.20	0.44	0	0.09	0.36	5847481	0.45	0.59	5027	299 0.	90 0.96	940039	0.31	0.51	300	300	5,177	5177	5,885	5,820	0.217	9.2	5820	5,695	2.41	6	2.3	37.1	46.3	125.7		391.0	7	2006.1	36.6%	99.28
DP8	9, 10, OS-5	1,597,413	36.67	0.20	0.44	0	0.09	0.36	218805	0.45	0.59	1345	691 0.	90 0.96	32917	0.41	0.57	25	25	2,887	2887	5,771	5,770	0.040	4.1	5770	5,702	2.36	7	3.0	15.9	19.9	36.3	3.0	45.8	5.1	106.9	57.1%	20.94
DP9	DP8, 5	1,856,152	42.61	0.20	0.44	0	0.09	0.36	296426	0.45	0.59	1345	691 0.	90 0.96	214034	0.45	0.60	25	25	4,128	4128	5,771	5,770	0.040	3.8	5770	5,686	2.03	5	1.4	48.6	52.5	26.5	1.7	33.4	2.9	74.7	59.0%	25.13
DP10	DP9, 11	2,506,658	0.101	0.20	0.44	0	0.09	0.36	364792	0.45	0.59	1927	831 0.	90 0.96	214034	0.44	0.59	25	25	4,178	4178	5,771	5,770	0.040	3.9	5770	5,686	2.01	6	2.1	32.8	36.7	43.6	2.2	54.9	3.6	123.8	58.8%	33.85
DP11	DP10 Treated (DF-5 Release)	2,506,658	57.54	0.20	0.44	0	0.09	0.36	364792	0.45	0.59	1927	831 0.	90 0.96	441226	0.52	0.68	25	25	4,178	4178	5,771	5,770	0.040	3.4	5770	5,686	2.01	6	2.1	32.8	36.2	51.9		6.6		48.1	67.9%	39.06
DP12	OS-6, 12		18.00	0.20	0.44	0	0.09	0.36	0	0.45	0.59	7507	753 0.	90 0.96	33529	0.47	0.61	25	25	2,584	2584	5,771	2,770	0.010	3.7	5770	5,733	1.43	7	2.4	18.2	21.9	19.5	2.9	21.0	4.8	33.3	66.5%	11.97
DP12a	DP-12 Treated (DF-7 Release) & DF-6 Release	1,067,210	24.50	0.20	0.44	0	0.09	0.36	14,147	0.45	0.59	750,	753 0.	90 0.96	302,316	0.58	0.70	25	25	2,584	2584	5,708	5,706	0.080	2.4	5706	5,731	1.43	7	2.4	18.2	20.6	33.7		3.2		28.8	74.1%	18.15
DP13	13, 14	713,417	16.38	0.20	0.44	0	0.09	0.36	0	0.45	0.59	7134	117 0.	90 0.96	0	0.45	0.59	50	50	1,514	1514	5,756	5,754	0.040	5.4	5754	5,695	3.90	4	1.4	18.5	23.9	16.2	2.7	20.4	4.6		65.0%	10.65
DP14	DP13, 15, 17	1,622,189	37.24	0.20	0.44	0	0.09	0.36	7179	0.45	0.59	1478	617 0.	90 0.96	136393	0.49	0.63	50	50	2,609	2609	5,756	5,754	0.040	5.1	5754	5,688	2.53	4	1.1	39.3	44.4	28.0	1.9	35.3	3.2	76.2	67.7%	25.20
DP15	DP12 Treated (DF-7Release), 16 Treated (DF-9 Release), & DF6 Release	2,611,529	59.95	0.20	0.44	0	0.09	0.36	300,640	0.45	0.59	750,	753 0.	90 0.96	1,433,608	0.64	0.74	50	50	4,095	4095	5,727	5,724	0.060	3.3	5724	5,687	0.90	7	1.9	36.0	39.3	63.4	7	7.8	7	65.8	73.8%	44.25
DD44	DRACE - LONG OR L 1 DRAG	1.000.744	07.40	0.00	0.44	0	0.00	0.04	207040	0.45	0.50	2220	070 0	00.06	4.550004	0.50	0.70	50	50	4.704	(70.4	5 707	5.704	0.060	2.0	5704	5 (07	0.55	-	4	70.0	00.0			40.0		440.4	74 507	10.15

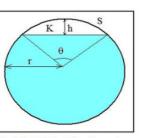
DP16

DP16 Traited (DF-8 Relaux)+DP15

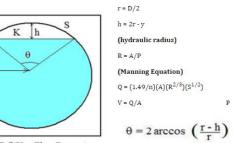
Note: DPs 3, 5, & 7 were updated to reflect an altered value at upstream Design Point R3030 (Q100: 1761 cfs & Q5: 347 cfs)from the MDDP Amendment for Glen at Widefield. The Amendment reduced flows to the north boundary of Glen at Widefield at DP 7 to Q100: 2,020 cfs and Q5: 401.

Note: Q2, Q5 & Q10 are based on C5; Q25, Q50 & Q100 are based on C100

					Storm Pipe												
Design Point	Notes		Max Q (Q100) Proposed	Capacity Analysis	Calculated Max Q for Pipe (CFS)	Percent of Pipe Capacity Used	n(full)	Slope (ft/ft)	n	Pipe Diameter (ft)	Width (ft) Box Culvert Only	Pipe Depth (inches)	Optimum Flow Depth (+/- 0.94 x D)	Θ (Radians)	A (Sq. Ft.)	Wetted Perimeter (ft)	Velocity at Max Pipe Capacity
E1	OS-1a and OS-1b		84.4	Adequate	105.4	80%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DP1	E1+DF-1 Release+DF-2 Release		107.0	Adequate	150.4	71%	0.013	0.010	0.013	4		48	3.76	0.990	12.259	10.587	12.27
1A	Sub-basin 1A		92.9	Adequate	105.4	88%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DP2	OS-2, 1A, 1D, 2, 3	Very Conservative at Residential Collector. Flows will likely be split by a future FDR.	283.4	Pressure Flow	272.7	104%	0.013	0.010	0.013	5		60	4.7	0.990	19.154	13.233	14.24
DP3	DP1+DP2 Treated (DF-3 Release)		181.9	Adequate	205.9	88%	0.013	0.010	0.013	4.5		54	4.23	0.990	15.515	11.910	13.27
DP4	7		17.8	Adequate	43.0	41%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
6	Sub-basin 6		34.1	Adequate	43.0	79%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
DP6	4, 6		47.7	Adequate	52.6	91%	0.013	0.015	0.013	2.5		30	2.35	0.990	4.788	6.617	10.99
DP8	9, 10, OS-5		106.9	Adequate	129.0	83%	0.013	0.015	0.013	3.5		42	3.29	0.990	9.385	9.263	13.75
DP9	DP8, 5		74.7	Adequate	105.4	71%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DP11	DP10 Treated (DF-5 Release)		48.1	Adequate	69.8	69%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DP12a	DP-12 Treated (DF-7 Release) & DF-6 Release		28.8	Adequate	43.0	67%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
13	Sub-basin 13		23.3	Adequate	43.0	54%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
DP13	13, 14		44.9	Adequate	69.8	64%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DP15	DP12 Treated (DF-7Release), 16 Treated (DF-9 Release), & DF6 Release		65.8	Adequate	105.4	62%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DF-1	PRELIMINARY DETENTION	N POND OUTFALL PIPE	8.8	Adequate	11.0	80%	0.013	0.010	0.013	1.5		18	1.41	0.990	1.724	3.970	6.38
DF-2	PRELIMINARY DETENTION	N POND OUTFALL PIPE	13.8	Adequate	23.7	58%	0.013	0.010	0.013	2		24	1.88	0.990	3.065	5.293	7.73
DF-3	PRELIMINARY DETENTION	N POND OUTFALL PIPE	74.9	Pressure Flow	69.8	107%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DF-4	PRELIMINARY DETENTION	N POND OUTFALL PIPE	22.0	Adequate	23.7	93%	0.013	0.010	0.013	2		24	1.88	0.990	3.065	5.293	7.73
DF-5	PRELIMINARY DETENTION	N POND OUTFALL PIPE	48.1	Adequate	69.8	69%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DF-6	PRELIMINARY DETENTION	PRELIMINARY DETENTION POND OUTFALL PIPE		Adequate	11.0	85%	0.013	0.010	0.013	1.5		18	1.41	0.990	1.724	3.970	6.38
DF-7	PRELIMINARY DETENTION POND OUTFALL PIPE		19.5	Adequate	43.0	45%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
DF-8	PRELIMINARY DETENTION	N POND OUTFALL PIPE	44.3	Adequate	69.8	63%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DF-9	PRELIMINARY DETENTION	N POND OUTFALL PIPE	46.3	Adequate	69.8	66%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13



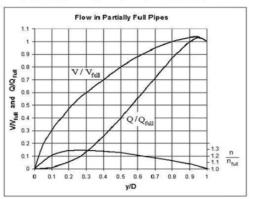
Partially Full Pipe Flow Parameters (More Than Half Full)



 $A = \pi r^2 - \frac{r^2(\theta - \sin \theta)}{2}$ 

$$P = 2\pi r - r * \theta$$

Equation used for  $n/n_{full}\colon\, n/n_{full}$  = 1.25 - (y/D -0.5)\*0.5 (for 0.5  $\leq$  y/D  $\leq$  1)



Flow In Partially Full Pipes

PROPOSED WATER QUALITY AND DETENTION SUMMARY											
	Corvallis										
Detention/W Q Pond	TOTAL AREA (AC)	CONTRIBUTING SUB-BASINS	% IMPERVIOUS	VOLUME REQUIRED (AC-FT)	Q(5) DISCHARGE (cfs)	Q(100) DISCHARGE (cfs)	DESCRIPTION:	Discharge Pipe Size			
DF-1	5.65	1B-COMMERCIAL	95%	0.89	2.1	8.8	Northwest Commercial	18.0			
DF-2	8.25	1B-MULTIFAMILY	70%	1.00	1.2	13.8	Northwest Multi-Family	24.0			
DF-3*	81.82	1A, 1D, 2, 3,OS-2	65%	7.22	8.3	74.9	West Single-Family (Slight over-detention to maintain Q listed in Glen at Widefield MDDP Amendment)	36.0			
DF-4*	23.14	4, 6	65%	2.64	4.8	22.0	Southwest Single-Family	24.0			
DF-5*	57.54	5, 9,10, 11, OS-5	70%	6.98	6.6	48.1	South Single-Family & School Site	36.0			
DF-6	6.50	8	95%	1.02	0.2	9.3	Northeast Commercial	18.0			
DF-7	18.00	12, OS-6	70%	2.18	3.0	19.5	Northeast Multi-Family	30.0			
DF-8*	37.24	13, 14, 15, 17	70%	4.51	5.0	44.3	Southeast Single-Family & Commercial	36.0			
DF-9*	35.45	16	80%	4.79	4.8	46.3	Southeast Commercial Pond	36.0			

### **Culvert Calculator Report CV177**

#### Solve For: Headwater Elevation

Culvert Summary					
Allowable HW Elevation	5,688.70	ft	Headwater Depth/Height	1.13	
Computed Headwater Elevation	5,688.17	ft	Discharge	87.06	cfs
Inlet Control HW Elev.	5,688.06	ft	Tailwater Elevation	5,684.52	ft
Outlet Control HW Elev.	5,688.17	ft	Control Type	Outlet Control	
Grades					
Upstream Invert	5,684.78	ft	Downstream Invert	5,684.52	ft
Length	77.00	ft	Constructed Slope	0.003377	ft/ft
Hydraulic Profile					
Profile	M2		Depth, Downstream	2.15	ft
Slope Type	Mild		Normal Depth	N/A	ft
Flow Regime	Subcritical		Critical Depth	2.15	ft
Velocity Downstream	8.03	ft/s	Critical Slope	0.005723	ft/ft
Section					
Section Shape	Circular		Mannings Coefficient	0.013	
Section Material	Concrete		Span	3.00	ft
Section Size	36 inch		Rise	3.00	ft
Number Sections	2				
Outlet Control Properties					
Outlet Control HW Elev.	5,688.17	ft	Upstream Velocity Head	0.74	ft
Ke	0.20		Entrance Loss	0.15	ft
Inlet Control Properties					
Inlet Control HW Elev.	5,688.06	ft	Flow Control	Transition	
Inlet Type Beveled ris	ng, 33.7° bevels		Area Full	14.1	ft²
K	0.00180		HDS 5 Chart	3	
M	2.50000		HDS 5 Scale	В	
С	0.02430		Equation Form	1	
Υ	0.83000				

MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

## 

Watershed Information

rshed Information		
Selected BMP Type =	EDB	
Watershed Area =	5.66	acres
Watershed Length =	585	ft
Watershed Length to Centroid =	430	ft
Watershed Slope =	0.055	ft/ft
Watershed Imperviousness =	95.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
ercentage Hydrologic Soil Groups C/D =	0.0%	percent

Percentage Hydrologic Soll Groups C/D = 0.0% percent Target WOCV Drain Time = 40.0 hours Location for 1-hr Rainfall Depths = User Input After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP to generate runoff hydrographs using the embedded Clorada Ultan Hydrorada Procedure

the embedded Colorado Urban Hydro	graph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.211	acre-feet
Excess Urban Runoff Volume (EURV) =	0.605	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.498	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.643	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.760	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.880	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.998	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.127	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	1.615	acre-feet
Approximate 2-yr Detention Volume =	0.488	acre-feet
Approximate 5-yr Detention Volume =	0.633	acre-feet
Approximate 10-yr Detention Volume =	0.771	acre-feet
Approximate 25-yr Detention Volume =	0.827	acre-feet
Approximate 50-yr Detention Volume =	0.858	acre-feet
Approximate 100-yr Detention Volume =	0.885	acre-feet

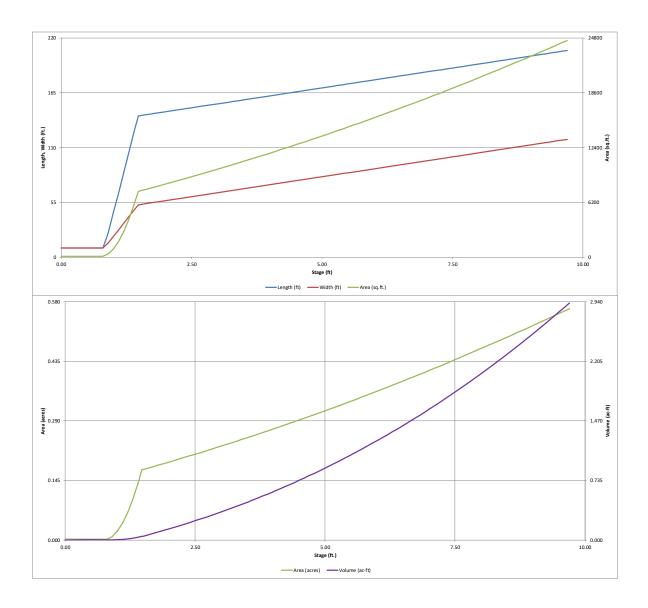
Optional User Override								
	acre-feet							
	acre-feet							
1.19	inches							
1.50	inches							
1.75	inches							
2.00	inches							
2.25	inches							
2.52	inches							
3.55	inches							
	-							

Define Zones and Basin Geometry

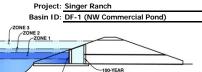
Initial Surcharge Area (A <sub>ISV</sub> ) =	83	ft <sup>2</sup>
Surcharge Volume Length (L <sub>ISV</sub> ) =	9.1	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	9.1	ft
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	0.65	ft
Length of Basin Floor $(L_{FLOOR})$ =	141.7	ft
Width of Basin Floor (W <sub>FLOOR</sub> ) =	52.5	ft
Area of Basin Floor $(A_{FLOOR})$ =		ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	1,800	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	3.52	ft
Length of Main Basin $(L_{MAIN})$ =	169.9	ft
Width of Main Basin (W <sub>MAIN</sub> ) =	80.6	ft
Area of Main Basin (A <sub>MAIN</sub> ) =		ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	36,642	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	0.884	acre-feet

Depth Increment =	0.10	ft		,		College			,
Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description Top of Micropool	(ft) 0.00	Stage (ft)	(ft) 9.1	(ft) 9.1	(ft ²) 83	Area (ft <sup>2</sup> )	(acre) 0.002	(ft 3)	(ac-ft)
ISV	0.33		9.1	9.1	83		0.002	28	0.001
	0.40		9.1	9.1	83		0.002	33	0.001
	0.50		9.1	9.1	83		0.002	42	0.001
	0.60		9.1	9.1 9.1	83		0.002	50 58	0.001
	0.80		9.1	9.1	83		0.002	67	0.001
	0.90		23.4	13.8	323		0.007	83	0.002
	1.00		43.8	20.5	897		0.021	141	0.003
	1.10		64.2 84.6	27.1 33.8	1,743 2,860		0.040	271 499	0.006
	1.30		105.0	40.5	4,250		0.098	852	0.020
	1.40		125.4	47.1	5,912		0.136	1,358	0.031
Floor	1.48		141.7 141.9	52.5 52.6	7,437		0.171	1,891 2,040	0.043
	1.60		142.7	53.4	7,624		0.175	2,795	0.064
	1.70		143.5	54.2	7,782		0.179	3,565	0.082
	1.80		144.3	55.0	7,941		0.182	4,351	0.100
	1.90 2.00		145.1 145.9	55.8 56.6	8,101 8,262		0.186	5,153 5,971	0.118 0.137
	2.10		146.7	57.4	8,425		0.193	6,805	0.156
	2.20		147.5	58.2	8,589		0.197	7,656	0.176
7ano 1 (MOCIO	2.30		148.3 148.9	59.0 59.7	8,754		0.201	8,523 9,229	0.196
Zone 1 (WQCV)	2.38		149.1	59.7	8,887 8,920		0.204	9,229	0.212
	2.50		149.9	60.6	9,088		0.209	10,307	0.237
	2.60		150.7	61.4	9,257		0.213	11,225	0.258
	2.70		151.5 152.3	62.2	9,428 9,599		0.216	12,159 13,110	0.279
	2.90		153.1	63.8	9,772		0.224	14,079	0.323
	3.00		153.9	64.6	9,946		0.228	15,065	0.346
	3.10		154.7	65.4	10,122		0.232	16,068	0.369
	3.20		155.5 156.3	66.2	10,299		0.236	17,089 18,128	0.392
	3.40		157.1	67.8	10,656		0.245	19,184	0.440
	3.50		157.9	68.6	10,836		0.249	20,259	0.465
	3.60		158.7 159.5	69.4 70.2	11,018		0.253	21,352	0.490
	3.80		160.3	71.0	11,386		0.261	22,463 23,592	0.516 0.542
	3.90		161.1	71.8	11,572		0.266	24,740	0.568
7 0 (511010	4.00		161.9	72.6	11,759		0.270	25,906	0.595
Zone 2 (EURV)	4.04		162.2 162.7	72.9 73.4	11,834 11,947		0.272	26,378 27,092	0.606
	4.20		163.5	74.2	12,136		0.279	28,296	0.650
	4.30		164.3	75.0	12,327		0.283	29,519	0.678
	4.40		165.1 165.9	75.8 76.6	12,519 12,713		0.287	30,761 32,023	0.706 0.735
	4.60		166.7	77.4	12,713		0.292	33,304	0.765
	4.70		167.5	78.2	13,103		0.301	34,604	0.794
	4.80		168.3	79.0	13,300		0.305	35,925	0.825
Zone 3 (100-year)	4.90 5.00		169.1 169.9	79.8 80.6	13,499		0.310	37,265 38,624	0.855
	5.10		170.7	81.4	13,900		0.319	40,004	0.918
	5.20		171.5	82.2	14,102		0.324	41,404	0.951
	5.30		172.3 173.1	83.0 83.8	14,306 14,511		0.328	42,825 44,266	0.983 1.016
	5.50		173.9	84.6	14,717		0.338	45,727	1.050
	5.60		174.7 175.5	85.4	14,924 15,133		0.343	47,209	1.084
	5.70 5.80		176.3	86.2 87.0	15,343		0.347 0.352	48,712 50,236	1.118 1.153
	5.90 6.00		177.1 177.9	87.8 88.6	15,554 15,767		0.357	51,781 53,347	1.189 1.225
	6.10		178.7 179.5	89.4 90.2	15,981 16,196		0.367	54,934 56,543	1.261 1.298
	6.30		180.3	91.0 91.8	16,412 16,630		0.377	58,173 59,825	1.335
	6.50		181.9	92.6	16,849		0.387	61,499	1.412
	6.60		182.7 183.5	93.4 94.2	17,069 17,291		0.392 0.397	63,195 64,913	1.451 1.490
	6.80		184.3 185.1	95.0 95.8	17,514 17,738		0.402	66,653 68,416	1.530 1.571
	7.00 7.10		185.9 186.7	96.6 97.4	17,963 18,190		0.412	70,201 72,009	1.612 1.653
	7.20		187.5	98.2	18,418		0.423	73,839	1.695
	7.30 7.40		188.3 189.1	99.0 99.8	18,647 18,877		0.428 0.433	75,692 77,568	1.738 1.781
	7.50 7.60		189.9 190.7	100.6 101.4	19,109 19,342		0.439	79,468 81,390	1.824 1.868
	7.70 7.80		191.5 192.3	102.2 103.0	19,577 19,812		0.449	83,336 85,306	1.913 1.958
	7.90		193.1	103.8	20,049		0.460	87,299 89,316	2.004
	8.10		194.7	105.4	20,527		0.471	91,356	2.097
	8.20 8.30		195.5 196.3	106.2 107.0	20,768 21,010		0.477	93,421 95,510	2.145 2.193
	8.40 8.50		197.1 197.9	107.8 108.6	21,253		0.488	97,623 99,760	2.241
	8.60		198.7	109.4	21,743		0.499	101,922	2.340
	8.70 8.80		199.5 200.3	110.2 111.0	21,990 22,239		0.505 0.511	104,109 106,321	2.390 2.441
	8.90 9.00		201.1 201.9	111.8 112.6	22,489 22,740		0.516 0.522	108,557 110,818	2.492 2.544
	9.10 9.20		202.7	113.4 114.2	22,992 23.245		0.528	113,105 115,417	2.597 2.650
	9.30		204.3	115.0	23,500		0.539	117,754	2.703
	9.40 9.50		205.1 205.9	115.8 116.6	23,756 24,014		0.545 0.551	120,117 122,505	2.758 2.812
	9.60 9.70		206.7 207.5	117.4 118.2	24,272 24,532		0.557 0.563	124,920 127,360	2.868 2.924

DF-1.x/sm, Basin 12/3/2020, 3.41 PM



MHFD-Detention, Version 4.02 (February 2020)



**Example Zone Configuration (Retention Pond)** 

	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.38	0.211	Orifice Plate
Zone 2 (EURV)	4.04	0.394	Circular Orifice
Zone 3 (100-year)	5.00	0.281	Weir&Pipe (Restrict)
•	Total (all zones)	0.885	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = N/A Underdrain Orifice Diameter = N/A

Calculated Parameters for Underdrain Underdrain Orifice Area = N/A Underdrain Orifice Centroid = N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

r Input: Orifice Plate with one or more orific	es or Elliptical Slot V	Veir (typically used to drain WQCV and/or EURV in a sedimer	ntation BMP)	Calculated Parame	eters for Plate
Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	5.069E-03	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	2.38	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	9.50	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	0.73	sq. inches (diameter = 15/16 inch)	Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.79	1.59					
Orifice Area (sq. inches)	0.73	0.73	0.73					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

Iser Input: Vertical Orifice (Circular or Rectangu	lar)				Calculated Paramet	ers for Vertical Orifi	ice
	Zone 2 Circular	Not Selected			Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.38	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.01	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	4.04	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.05	N/A	feet
Vertical Orifice Diameter =	1 23	N/A	inches	•			-

User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and C	Outlet Pipe OR Recta	angular/Trapezoidal Weir (and No Outlet Pipe)	Calculated Paramet	ers for Overflow We	<u>eir</u>
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	l
Overflow Weir Front Edge Height, Ho =	4.04	N/A	ft (relative to basin bottom at Stage = 0 ft) $\frac{1}{2}$ Height of Grate Upper Edge, $\frac{1}{2}$	4.04	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	22.14	N/A	l
Horiz. Length of Weir Sides =	4.00	N/A	feet Overflow Grate Open Area w/o Debris =	16.80	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	% grate open area/total area	8.40	N/A	ft <sup>2</sup>

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)</u>

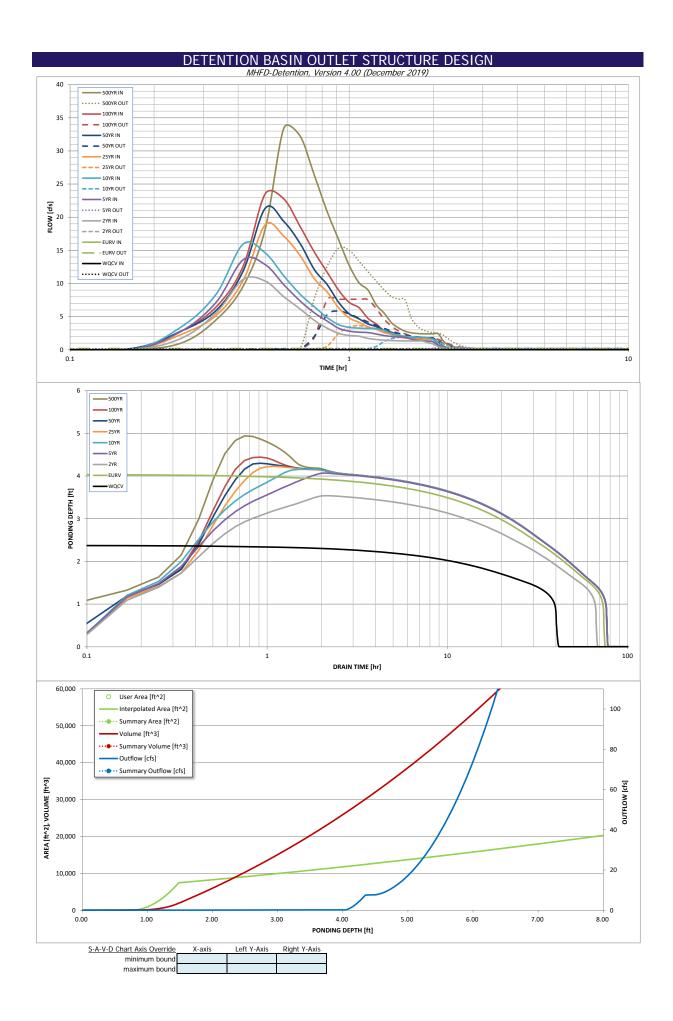
Outlet Pipe W/ Flow Restriction Plate	<u>(Circular Orifice, Re</u>	<u>strictor Plate, or Re</u>	ctangular Orifice)	Calculated Parameter	s for Outlet Pipe W/	Flow Restriction Pla	<u>te</u>
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.76	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.39	N/A	feet
ctor Plate Height Above Pipe Invert =	8.00		inches Half-Central Angle	of Restrictor Plate on Pipe =	1.46	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Debris Clogging % =

out: Emergency Spillway (Rectangular or 1	<u> [rapezoidal]</u>	_		Calculated Parame	ters for Spillway
Spillway Invert Stage=	4.50	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.79	feet
Spillway Crest Length =	7.00	feet	Stage at Top of Freeboard =	6.29	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.38	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	1.33	acre-ft
		•			-

Routed Hydrograph Results	The user can overr	ide the default CUH	IP hydrographs and	runoff volumes by a	entering new values	in the Inflow Hydro	ographs table (Colur	nns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.211	0.605	0.498	0.643	0.760	0.880	0.998	1.127	1.615
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.498	0.643	0.760	0.880	0.998	1.127	1.615
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.8	2.1	3.2	5.6	7.0	8.8	14.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.14	0.38	0.56	0.99	1.24	1.55	2.58
Peak Inflow Q (cfs) =	N/A	N/A	10.6	13.6	15.9	18.8	21.3	23.5	33.5
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.4	1.9	3.6	5.8	7.6	15.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.6	0.6	0.8	0.9	1.1
Structure Controlling Flow =	Vertical Orifice 1	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.1	0.2	0.3	0.4	0.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	69	63	71	70	69	68	68	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	66	75	75	74	74	73	72
Maximum Ponding Depth (ft) =	2.38	4.04	3.54	4.07	4.16	4.22	4.30	4.44	4.94
Area at Maximum Ponding Depth (acres) =	0.20	0.27	0.25	0.27	0.28	0.28	0.28	0.29	0.31
Maximum Volume Stored (acre-ft) =	0.212	0.606	0.473	0.611	0.636	0.655	0.675	0.718	0.865



MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

# Basin ID: <u>DF-2 (NW Multi-Family Pond)</u> 2008 1 AND 2 OPERATOR OF THE PERMANENT TOOLME EURY WOOV Example Zone Configuration (Retention Pond)

#### Watershed Information

tersned information		
Selected BMP Type =	EDB	
Watershed Area =	10.30	acres
Watershed Length =	550	ft
Watershed Length to Centroid =	540	ft
Watershed Slope =	0.060	ft/ft
Watershed Imperviousness =	70.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	igraph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.236	acre-feet
Excess Urban Runoff Volume (EURV) =	0.792	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.673	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.907	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.105	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	1.338	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	1.545	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.791	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	2.665	acre-feet
Approximate 2-yr Detention Volume =	0.619	acre-feet
Approximate 5-yr Detention Volume =	0.824	acre-feet
Approximate 10-yr Detention Volume =	1.041	acre-feet
Approximate 25-yr Detention Volume =	1.118	acre-feet
Approximate 50-yr Detention Volume =	1.163	acre-feet
Approximate 100-yr Detention Volume =	1.246	acre-feet

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.236	acre-fee
Zone 2 Volume (EURV - Zone 1) =	0.556	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	0.454	acre-fee
Total Detention Basin Volume =	1.246	acre-fee
Initial Surcharge Volume (ISV) =	31	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (Htotal) =	5.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	3	

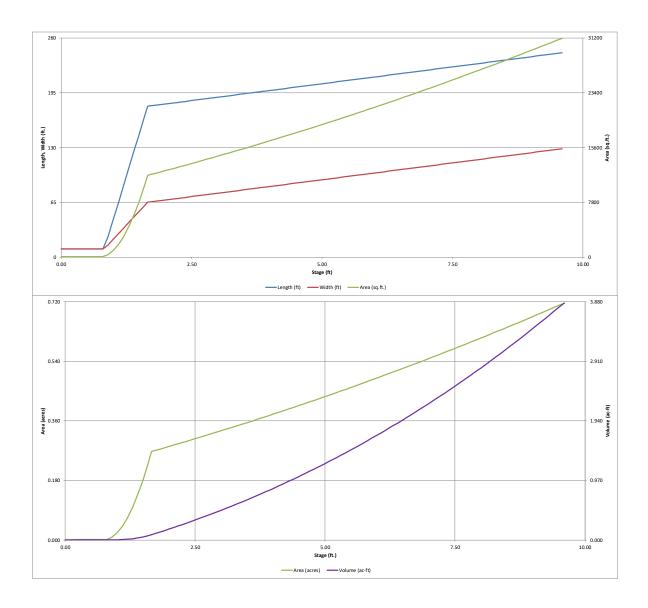
Initial Surcharge Area $(A_{ISV}) =$	93	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	9.7	ft
Surcharge Volume Width $(W_{ISV}) =$	9.7	ft
Depth of Basin Floor $(H_{FLOOR})$ =	0.83	ft
Length of Basin Floor $(L_{FLOOR})$ =	179.0	ft
Width of Basin Floor $(W_{FLOOR}) =$	65.0	ft
Area of Basin Floor $(A_{FLOOR}) =$	11,635	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	3,533	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	3.34	ft
Length of Main Basin $(L_{MAIN}) =$	205.7	ft
Width of Main Basin ( $W_{MAIN}$ ) =	91.7	ft
Area of Main Basin $(A_{MAIN}) =$	18,868	ft <sup>2</sup>
Volume of Main Basin $(V_{MAIN}) =$	50,455	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	1.241	acre-fee

	10
Note: L / W Ratio < 1	
L / W Ratio = 0.67	
Note: Lc/L Ratio > 0.9	
Lc / L Ratio = 0.98	

Optional 03	er Overrides acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.55	inches

Depth Increment =	0.10	ft							
Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool	0.00		9.7	9.7	93		0.002		
ISV	0.33		9.7	9.7	93		0.002	31	0.001
	0.40		9.7	9.7	93		0.002	37	0.001
	0.50		9.7	9.7	93		0.002	47	0.001
	0.60		9.7	9.7	93		0.002	56	0.001
	0.70		9.7	9.7	93		0.002	65	0.002
	0.80		9.7	9.7	93		0.002	75	0.002
	0.90		23.9	14.3	343		0.008	92	0.002
	1.00		44.3	21.0	931		0.021	154	0.004
	1.10		64.7	27.7	1,792		0.041	287	0.007
	1.20		85.1	34.3	2,924		0.067	521	0.012
	1.30		105.5	41.0	4,328		0.099	881	0.020
	1.40		125.9	47.7	6,004		0.138	1,396	0.032
	1.50		146.3	54.3	7,952		0.183	2,091	0.048
	1.60		166.7	61.0	10,172		0.234	2,995	0.069
Floor	1.66		179.0	65.0	11,635		0.267	3,649	0.084
	1.70		179.3	65.3	11,713		0.269	4,116	0.094
	1.80		180.1	66.1	11,909		0.273	5,297	0.122
	1.90		180.9	66.9	12,107		0.278	6,498	0.149
	2.00		181.7	67.7	12,306		0.282	7,718	0.177
	2.10		182.5	68.5	12,506		0.287	8,959	0.206
	2.20		183.3	69.3	12,707		0.292	10,219	0.235
Zone 1 (WQCV)	2.21		183.4	69.4	12,728		0.292	10,347	0.238
	2.30		184.1	70.1	12,910		0.296	11,500	0.264
	2.40		184.9	70.9	13,114		0.301	12,801	0.294
	2.50		185.7	71.7	13,319		0.306	14,123	0.324
	2.60		186.5	72.5	13,526		0.311	15,465	0.355
	2.70		187.3	73.3	13,734		0.315	16,828	0.386
	2.80		188.1	74.1	13,943		0.320	18,212	0.418
	2.90		188.9	74.9	14,153		0.325	19,617	0.450
	3.00		189.7	75.7	14,365		0.330	21,043	0.483
	3.10		190.5	76.5	14,578		0.335	22,490	0.516
	3.20		191.3	77.3	14,792		0.340	23,959	0.550
	3.30		192.1	78.1	15,008		0.345	25,449	0.584
	3.40		192.9	78.9	15,225		0.350	26,960	0.619
	3.50		193.7	79.7	15,443		0.355	28,494	0.654
	3.60		194.5	80.5	15,662		0.360	30,049	0.690
	3.70		195.3	81.3	15,883		0.365	31,626	0.726
	3.80		196.1	82.1	16,105		0.370	33,225	0.763
Zone 2 (EURV)	3.88		196.7	82.8	16,283		0.374	34,521	0.792
	3.90		196.9	82.9	16,328		0.375	34,847	0.800
	4.00		197.7	83.7	16,553		0.380	36,491	0.838
	4.10		198.5	84.5	16,778		0.385	38,158	0.876
	4.20		199.3	85.3	17,005		0.390	39,847	0.915
	4.30		200.1	86.1	17,234		0.396	41,559	0.954
	4.40		200.9	86.9	17,463		0.401	43,294	0.994
	4.50		201.7	87.7	17,694		0.406	45,051	1.034
	4.60		202.5	88.5	17,926		0.412	46,832	1.075
	4.70		203.3	89.3	18,160		0.417	48,637	1.117
	4.80		204.1	90.1	18,395		0.422	50,464	1.159
	4.90		204.9	90.9	18,631		0.428	52,316	1.201
7 2 (400 )	5.00		205.7	91.7	18,868		0.433	54,191	1.244
Zone 3 (100-year)	5.01		205.8	91.8	18,892		0.434	54,379	1.248
	5.10		206.5	92.5	19,107		0.439	56,089	1.288
	5.20		207.3	93.3	19,346		0.444	58,012	1.332
	5.30		208.1	94.1	19,588		0.450	59,959 61,930	1.376
	5.40		208.9	94.9 95.7	19,830 20,074		0.455		1.422
	5.60		210.5	95.7	20,074		0.461	63,925 65,944	1.468
	5.70		211.3	97.3	20,565		0.472	67,989	1.561
	5.80 5.90		212.1 212.9	98.1 98.9	20,813 21,061		0.478	70,057 72,151	1.608 1.656
	6.00		213.7	99.7	21,311		0.489	74,270	1.705
	6.10		214.5	100.5	21,563		0.495	76,413	1.754
	6.20		215.3 216.1	101.3 102.1	21,815 22,069		0.501	78,582 80,777	1.804 1.854
	6.40		216.9	102.9	22,325		0.513	82,996	1.905
	6.50 6.60		217.7 218.5	103.7 104.5	22,581 22,839		0.518 0.524	85,242 87,513	1.957 2.009
	6.70		219.3	104.5	22,839		0.524	89,809	2.062
	6.80		220.1	106.1	23,358		0.536	92,132	2.115
	6.90 7.00		220.9	106.9 107.7	23,620 23,883		0.542 0.548	94,481 96,856	2.169
	7.10		222.5	108.5	24,147		0.554	99,258	2.279
			223.3	109.3 110.1	24,413		0.560	101,686	2.334
	7.20		2244		24,679	1	0.567	104,140 106,622	2.391 2.448
	7.20 7.30		224.1		24,947		0.573		
	7.20 7.30 7.40 7.50		224.1 224.9 225.7	110.9 111.7	24,947 25,217		0.573 0.579	109,130	2.505
	7.20 7.30 7.40 7.50 7.60		224.1 224.9 225.7 226.5	110.9 111.7 112.5	25,217 25,487		0.579 0.585	109,130 111,665	2.505 2.563
	7.20 7.30 7.40 7.50		224.1 224.9 225.7	110.9 111.7	25,217 25,487 25,759		0.579	109,130 111,665 114,227	2.505
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90		224.1 224.9 225.7 226.5 227.3 228.1 228.9	110.9 111.7 112.5 113.3 114.1 114.9	25,217 25,487 25,759 26,032 26,307		0.579 0.585 0.591 0.598 0.604	109,130 111,665 114,227 116,817 119,434	2.505 2.563 2.622 2.682 2.742
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7	110.9 111.7 112.5 113.3 114.1 114.9 115.7	25,217 25,487 25,759 26,032 26,307 26,582		0.579 0.585 0.591 0.598 0.604 0.610	109,130 111,665 114,227 116,817 119,434 122,078	2.505 2.563 2.622 2.682 2.742 2.803
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.10 8.20		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.10 8.20 8.30		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.10 8.20 8.30 8.40		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1 118.9	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417 27,698		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629 0.636	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178 132,934	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988 3.052
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.10 8.20 8.30 8.40 8.50 8.60		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1 232.9 233.7 234.5	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417 27,698 27,980 28,263		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178 132,934 135,717 138,530	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988 3.052 3.116 3.180
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.10 8.20 8.30 8.40 8.50 8.60 8.70		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1 232.9 233.7 234.5 235.3	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1 118.9 119.7 120.5	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417 27,698 27,980 28,263 28,548		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629 0.636 0.642 0.649	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178 132,934 135,717 138,530 141,370	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988 3.052 3.116 3.180 3.245
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.10 8.20 8.30 8.40 8.50 8.60		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1 232.9 233.7 234.5	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1 118.9 119.7 120.5	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417 27,698 27,980 28,263 28,263 28,548 28,834 29,121		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629 0.636 0.642 0.649 0.655 0.6662	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178 132,934 135,717 138,530	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.926 3.052 3.116 3.180
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 8.00 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.80		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.1 232.9 233.7 234.5 235.3 236.1 236.9 237.7	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1 118.9 119.7 120.5 121.3 122.1 122.9	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417 27,698 27,980 28,263 28,548 28,548 28,834 29,121 29,410		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629 0.636 0.642 0.649 0.655 0.662 0.669	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178 132,934 135,717 138,530 141,370 144,239 147,137 150,064	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988 3.052 3.116 3.180 3.245 3.311 3.378 3.445
	7.20 7.30 7.40 7.50 7.60 7.70 8.00 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.80 9.00		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1 232.9 233.7 234.5 235.1 236.9 237.7 236.9 237.7	110.9 111.7 112.5 113.3 114.1 114.9 115.7 116.5 117.3 118.1 118.9 119.7 120.5 121.3 122.1 122.9 123.7 124.5	25,217 25,487 25,759 26,032 26,307 26,582 27,138 27,417 27,698 27,980 28,263 28		0.579 0.585 0.591 0.598 0.604 0.617 0.623 0.629 0.636 0.642 0.649 0.655 0.662 0.669 0.675	109,130 111,665 114,227 116,817 119,434 122,078 127,450 130,178 132,934 135,717 138,530 141,370 144,239 147,137 150,064 153,019	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988 3.052 3.116 3.245 3.311 3.378 3.3445 3.513
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.89 9.00 9.10 9.20		224.1 224.9 225.7 226.5 227.3 228.1 228.9 229.7 230.5 231.3 232.1 232.9 233.7 234.5 235.3 236.1 236.1 236.9 237.7 238.5 237.7 238.5 239.5 239.5 239.5 240.1	110.9 111.7 112.5 113.3 114.1 115.7 116.5 117.3 118.1 119.7 120.5 122.1 122.9 122.9 124.5 125.1 126.1	25,217 25,487 25,759 26,032 26,307 26,582 26,859 27,138 27,417 27,698 27,990 28,253 28,253 28,244 28,241 29,121 29,121 29,700 29,991		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629 0.636 0.642 0.655 0.662 0.662 0.663 0.662 0.668 0.668	109,130 111,665 114,227 116,817 119,434 122,078 122,4750 127,450 130,178 132,934 135,717 138,530 141,370 144,239 147,137 150,064 153,019 156,003 159,017	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.926 3.052 3.116 3.245 3.311 3.378 3.513 3.551
	7.20 7.30 7.40 7.50 7.60 7.70 7.80 8.00 8.10 8.20 8.30 8.40 8.50 8.70 8.89 9.00 9.10		224.1 224.9 225.7 226.5 227.7 226.5 228.1 228.9 229.7 230.5 231.3 232.1 232.9 233.7 234.5 235.3 236.1 236.9 237.7 238.5 239.3	110.9 111.7 112.5 113.3 114.1 115.7 116.5 117.3 118.1 118.9 119.7 120.5 121.3 122.1 122.9 123.7 124.5 125.3	25,217 25,487 25,789 26,032 26,307 26,582 26,859 27,138 27,417 27,980 28,263 28,263 28,548 29,121 29,410 29,901		0.579 0.585 0.591 0.598 0.604 0.610 0.617 0.623 0.629 0.636 0.642 0.649 0.652 0.662 0.662 0.662 0.663 0.664 0.665 0.	109,130 111,665 114,227 116,817 119,434 122,078 124,750 127,450 130,178 132,934 135,717 138,530 141,370 144,239 147,137 150,064 153,019	2.505 2.563 2.622 2.682 2.742 2.803 2.864 2.926 2.988 3.116 3.180 3.245 3.311 3.378 3.445 3.451 3.351 3.513

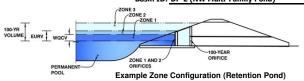
DF-2, Basin 10/21/2021, 12:40 PM



MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

Basin ID: DF-2 (NW Multi-Family Pond)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.21	0.236	Orifice Plate
Zone 2 (EURV)	3.88	0.556	Circular Orifice
Zone 3 (100-year)	5.01	0.454	Weir&Pipe (Restrict)
•	Total (all zones)	1.246	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = N/A Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain Underdrain Orifice Area = N/A Underdrain Orifice Centroid = N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) 2.18 Orifice Plate: Orifice Vertical Spacing = 8.70 inches Orifice Plate: Orifice Area per Row 0.78 sq. inches (diameter = 1 inch)

Calculated Parameters for Plate WQ Orifice Area per Row 5.417E-03 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

and rotarrica or Each Office	NOW (Hambered He	THE TOTAL CO. HIGHES	<del>- /</del>					
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.73	1.45					
Orifice Area (sq. inches)	0.78	0.78	0.78					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Not Selected Zone 2 Circular Invert of Vertical Orifice = 2.21 N/A ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Vertical Orifice = 3.88 N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Diameter = inches 2.15 N/A

Calculated Parameters for Vertical Orifice Zone 2 Circular Not Selected Vertical Orifice Area 0.03 N/A Vertical Orifice Centroid = 0.09 N/A

User Input: Overflow Weir (Drophox with Flat or Sloped Grate and Outlet Pine OR Rectangular/Trapezoidal Weir (and No Outlet Pine) Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	]		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.87	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, $H_t$ =	3.87	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grat	te Open Area / 100-yr Orifice Area =	9.51	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet Ove	rflow Grate Open Area w/o Debris =	16.80	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Ov	erflow Grate Open Area w/ Debris =	8.40	N/A	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%				

<u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

r Input: Outlet Pipe W/ Flow Restriction Plate	(Circular Orifice, Res	strictor Plate, or Re	ctangular Orifice)	Calculated Parameters	s for Outlet Pipe W/ I	Flow Restriction Pla	ite
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.77	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.75	N/A	feet
Restrictor Plate Height Above Pipe Invert =	18.00		inches Half-Central Angle	of Restrictor Plate on Pipe =	3.14	N/A	radiar

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Maximum Volume Stored (acre-ft)

4.80 ft (relative to basin bottom at Stage = 0 ft) Spillway Invert Stage= Spillway Crest Length = 14.00 feet Spillway End Slopes 4.00 H:V Freeboard above Max Water Surface = feet

	Calculated Paramet	ters for Spillway
Spillway Design Flow Depth=		feet
Stage at Top of Freeboard =	6.66	feet
Basin Area at Top of Freeboard =	0.53	acres
Basin Volume at Top of Freeboard =		acre-ft

0 911

00 Year

30.4

1.0

1.1 N/A

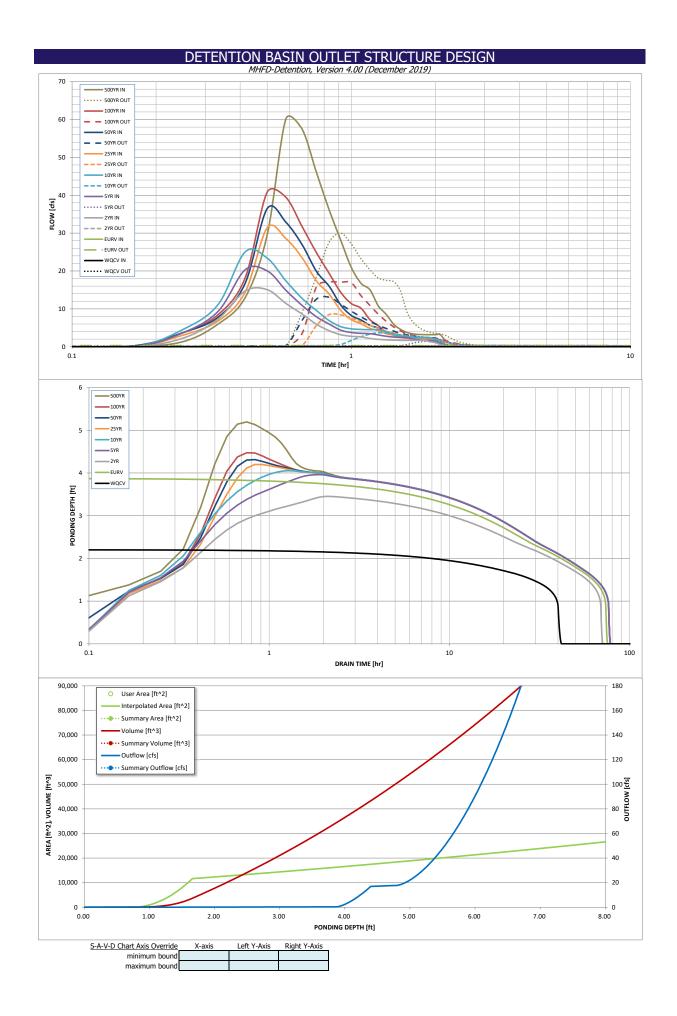
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1 327

Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). Design Storm Return Period WQCV EURV 10 Year 25 Year 100 Year 2 Year 5 Year 50 Year One-Hour Rainfall Depth (in) N/A N/A 1.19 2.00 1.545 1.545 CUHP Runoff Volume (acre-ft) 0.236 0.792 0.673 0.907 1.105 1.338 1.791 Inflow Hydrograph Volume (acre-ft) 1.338 N/A N/A 0.673 0.907 1.105 1.791

2.665 2.665 CUHP Predevelopment Peak Q (cfs) 14.7 18.4 N/A N/A 1.7 4.5 6.8 11.8 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A 1 79 2 95 Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.16 0.44 0.66 1.14 1.43 Peak Inflow Q (cfs) N/A N/A 15.1 20.3 25.0 31.4 36.5 40.8 60.2 Peak Outflow O (cfs) 13.1 0.1 0.3 0.3 1.5 8.5 17.1 30.0 Ratio Peak Outflow to Predevelopment Q N/A N/A N/A 0.3 0.5 0.7 0.9 0.9 Structure Controlling Flow Plate flow Weir ical Orifice rflow Wei Overflow Weir 1 Overflow Weir 1 Overflow Weir Outlet Plate 1 Spillway Max Velocity through Grate 1 (fps) N/A N/A 0.2 0.5 0.7 Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) 39 68 64 70 69 67 66 64 Time to Drain 99% of Inflow Volume (hours) 40 68 Maximum Ponding Depth (ft) 3.88 3.45 3.96 4.05 4.20 4.31 4.47 5.20 2.21 Area at Maximum Ponding Depth (acres) 0.38 0.40



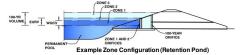
MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

#### Basin ID: DF-3 (W Single Family Pond)(Sub-basin 1-D Added)

acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches

2.25 inches 2.52 inches 3.55 inches



#### Watershed Information

		icci sirca Tili oli liadioi i
	EDB	Selected BMP Type =
acres	83.58	Watershed Area =
ft	2,720	Watershed Length =
ft	1,735	Watershed Length to Centroid =
ft/ft	0.030	Watershed Slope =
percent	65.00%	Watershed Imperviousness =
percent	0.0%	Percentage Hydrologic Soil Group A =
percent	100.0%	Percentage Hydrologic Soil Group B =
percent	0.0%	Percentage Hydrologic Soil Groups C/D =
hours	40.0	Target WQCV Drain Time =
	User Input	Location for 1-hr Rainfall Depths =

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	igraph Procedu	ire.
Water Quality Capture Volume (WQCV) =	1.770	acre-feet
Excess Urban Runoff Volume (EURV) =	5.931	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	5.483	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	7.478	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	9.176	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	11.254	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	13.050	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	15.227	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	22.864	acre-feet
Approximate 2-yr Detention Volume =	4.599	acre-feet
Approximate 5-yr Detention Volume =	6.166	acre-feet
Approximate 10-yr Detention Volume =	7.860	acre-feet
Approximate 25-yr Detention Volume =	8.468	acre-feet
Approximate 50-yr Detention Volume =	8.817	acre-feet
Approximate 100-yr Detention Volume =	9.532	acre-feet

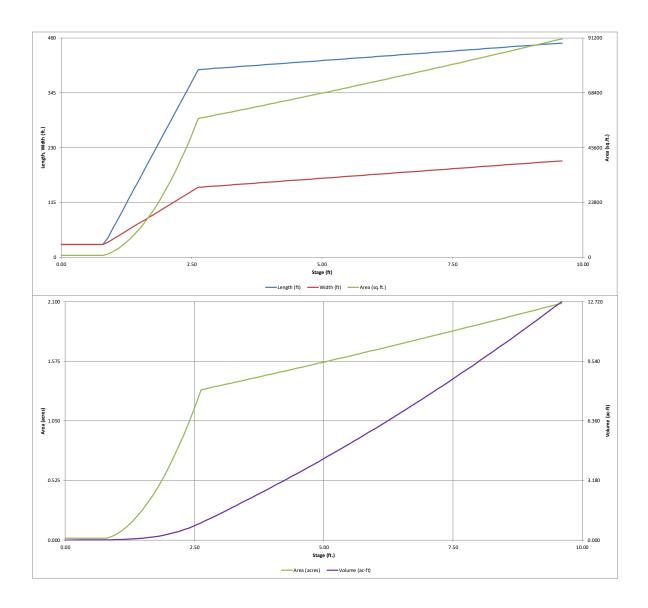
### Define Zones and Basin Geometry

chine zones and basin decinedy		
Zone 1 Volume (WQCV) =	1.770	acre-fee
Zone 2 Volume (EURV - Zone 1) =	4.161	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	3.601	acre-fee
Total Detention Basin Volume =	9.532	acre-fee
Initial Surcharge Volume (ISV) =	231	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (Htotal) =	8.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	3	

Calculated Total Basin Volume $(V_{total}) =$	9.511	acre-feet
Volume of Main Basin ( $V_{MAIN}$ ) =	374,898	ft 3
Area of Main Basin $(A_{MAIN}) =$	82,714	ft <sup>2</sup>
Width of Main Basin $(W_{MAIN}) =$	189.4	ft
Length of Main Basin $(L_{MAIN}) =$	436.6	ft
Depth of Main Basin (H <sub>MAIN</sub> ) =	5.37	ft
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	38,833	ft <sup>3</sup>
Area of Basin Floor $(A_{FLOOR}) =$	57,664	ft <sup>2</sup>
Width of Basin Floor (W <sub>FLOOR</sub> ) =	146.5	ft
Length of Basin Floor $(L_{FLOOR}) =$	393.7	ft
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	1.80	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	26.5	ft
Surcharge Volume Length (L <sub>ISV</sub> ) =	26.5	ft
Initial Surcharge Area $(A_{ISV}) =$	701	ft 2

Depth Increment =	0.10	ft							
Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool	0.00		26.5	26.5	701		0.016		
ISV	0.33		26.5	26.5	701		0.016	231	0.005
	0.40		26.5	26.5	701		0.016	280	0.006
	0.50		26.5	26.5	701		0.016	350	0.008
	0.60		26.5	26.5	701		0.016	421	0.010
	0.70		26.5	26.5	701		0.016	491	0.011
	0.80		26.5	26.5	701		0.016	561	0.013
	0.90		40.8	31.1	1,269		0.029	650	0.015
	1.00		61.2	37.8	2,312		0.053	827	0.019
	1.10		81.6	44.5	3,627		0.083	1,121	0.026
	1.20		102.0	51.1	5,214 7,073		0.120	1,561	0.036
	1.30		122.4 142.8	57.8 64.5	9,204		0.162 0.211	2,173 2,985	0.050
	1.50		163.2	71.1	11,607		0.211	4,023	0.009
	1.60		183.6	77.8	14,282		0.328	5,315	0.122
	1.70		204.0	84.5	17,229		0.396	6,889	0.158
	1.80		224.4	91.1	20,448		0.469	8,770	0.201
	1.90		244.8	97.8	23,939		0.550	10,987	0.252
	2.00		265.2	104.5	27,702		0.636	13,567	0.311
	2.10		285.6	111.1	31,737		0.729	16,537	0.380
	2.20		306.0	117.8	36,044		0.827	19,924	0.457
	2.30		326.4	124.5	40,623		0.933	23,755	0.545
	2.40		346.8	131.1	45,474		1.044	28,057	0.644
	2.50		367.2	137.8	50,597		1.162	32,859	0.754
	2.60		387.6	144.5	55,992		1.285	38,186	0.877
Floor	2.63		393.7	146.5	57,664		1.324	39,891	0.916
	2.70		394.2	147.0	57,966		1.331	43,938	1.009
	2.80		395.0	147.8	58,400		1.341	49,756	1.142
	2.90		395.8	148.6	58,835		1.351	55,618	1.277
	3.00		396.6	149.4	59,271			61,523	1.412
	3.10		397.4 398.2	150.2 151.0	59,709 60 148		1.371	67,472 73,465	1.549
Zone 1 (WQCV)	3.20		398.2	151.0	60,148		1.381	77,686	1.783
Zolle I (WQCV)	3.30		399.0	151.8	60,588		1.391	79,502	1.825
	3.40		399.8	152.6	61,029		1.401	85,582	1.965
	3.50		400.6	153.4	61,472		1.411	91,707	2.105
	3.60		401.4	154.2	61,915		1.421	97,877	2.247
	3.70		402.2	155.0	62,361		1.432	104,091	2.390
	3.80		403.0	155.8	62,807		1.442	110,349	2.533
	3.90		403.8	156.6	63,255		1.452	116,652	2.678
	4.00		404.6	157.4	63,704		1.462	123,000	2.824
	4.10		405.4	158.2	64,154		1.473	129,393	2.970
	4.20		406.2	159.0	64,606		1.483	135,831	3.118
	4.30		407.0	159.8	65,059		1.494	142,314	3.267
	4.40		407.8	160.6	65,513		1.504	148,843	3.417
	4.50		408.6	161.4	65,968		1.514	155,417	3.568
	4.60		409.4	162.2	66,425		1.525	162,036	3.720
	4.70		410.2	163.0	66,883		1.535	168,702	3.873
	4.80		411.0	163.8	67,342		1.546	175,413	4.027
	5.00		411.8 412.6	164.6 165.4	67,803 68,264		1.557 1.567	182,170 188,973	4.182 4.338
	5.10		413.4	166.2	68,727		1.578	195,823	4.495
	5.20		414.2	167.0	69,192		1.588	202,719	4.654
	5.30		415.0	167.8	69,658		1.599	209,661	4.813
	5.40		415.8	168.6	70,124		1.610	216,651	4.974
	5.50		416.6	169.4	70,593		1.621	223,686	5.135
	5.60		417.4	170.2	71,062		1.631	230,769	5.298
	5.70		418.2	171.0	71,533		1.642	237,899	5.461
	5.80 5.90		419.0 419.8	171.8 172.6	72,005 72,478		1.653 1.664	245,076 252,300	5.626 5.792
Zone 2 (EURV)	5.99		420.6	173.4	72,905		1.674	258,842	5.942
	6.00		420.6 421.4	173.4 174.2	72,953 73,429		1.675 1.686	259,571 266,891	5.959 6.127
	6.20		422.2	175.0	73,906		1.697	274,257	6.296
	6.30		423.0 423.8	175.8	74,384		1.708	281,672	6.466
	6.40		424.6	176.6 177.4	74,864 75,345		1.730	289,134 296,645	6.638 6.810
	6.60		425.4 426.2	178.2 179.0	75,828		1.741 1.752	304,203	6.984
	6.70 6.80		426.2 427.0	179.0 179.8	76,311 76,796		1.763	311,810 319,466	7.158 7.334
	6.90		427.8	180.6	77,282		1.774	327,169	7.511
			428.6	181.4	77,770 78,258		1.785 1.797	334,922 342,723	7.689 7.868
	7.00 7.10		429.4	182.2					8.048
	7.00 7.10 7.20		430.2	183.0	78,748		1.808	350,574	
	7.00 7.10 7.20 7.30		430.2 431.0	183.0 183.8	78,748 79,239		1.808 1.819	358,473	8.229 8.412
	7.00 7.10 7.20 7.30 7.40 7.50		430.2 431.0 431.8 432.6	183.0 183.8 184.6 185.4	78,748 79,239 79,732 80,226		1.808 1.819 1.830 1.842	358,473 366,422 374,420	8.229 8.412 8.595
	7.00 7.10 7.20 7.30 7.40 7.50 7.60		430.2 431.0 431.8 432.6 433.4	183.0 183.8 184.6 185.4 186.2	78,748 79,239 79,732 80,226 80,721		1.808 1.819 1.830 1.842 1.853	358,473 366,422 374,420 382,467	8.229 8.412 8.595 8.780
	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80		430.2 431.0 431.8 432.6 433.4 434.2 435.0	183.0 183.8 184.6 185.4 186.2 187.0 187.8	78,748 79,239 79,732 80,226 80,721 81,217 81,715		1.808 1.819 1.830 1.842 1.853 1.864 1.876	358,473 366,422 374,420 382,467 390,564 398,710	8.229 8.412 8.595 8.780 8.966 9.153
	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214		1.808 1.819 1.830 1.842 1.853 1.864 1.876	358,473 366,422 374,420 382,467 390,564 398,710 406,907	8.229 8.412 8.595 8.780 8.966 9.153 9.341
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.01		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214 82,714 82,764		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.899	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.550
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.01 8.10		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7 437.4	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214 82,764 83,216		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.899 1.900	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.550 9.721
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.01		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7 437.4 438.2	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214 82,714 82,764 83,216 83,718		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.899	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450 431,796	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.550 9.721
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.01 8.10 8.20 8.30 8.40		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7 437.4 438.2 439.0 439.8	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214 82,714 82,764 83,216 83,718 84,222 84,728		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.899 1.900 1.910 1.922 1.933 1.945	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450 431,796 440,193 448,641	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.550 9.721 9.721 10.105
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.00 8.01 8.10 8.20 8.30 8.40 8.50		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7 437.4 438.2 439.0 449.6	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8 192.6 193.4	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214 82,714 82,764 83,216 83,718 84,222 84,728		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.990 1.910 1.922 1.933 1.945	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450 431,796 440,193 448,641 457,139	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.550 9.721 9.913 10.105 10.299 10.494
Zone 3 (100-year)	7.00 7.10 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 8.00 8.01 8.10 8.20 8.30 8.40 8.50 8.60		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7 437.4 438.2 439.0 439.8 440.6 441.4	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8 192.6 193.4 194.2 195.0	78,748 79,239 79,732 80,226 80,721 81,217 81,217 82,714 82,714 82,764 83,216 83,718 84,222 84,728 85,234 85,742		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.899 1.900 1.910 1.922 1.933 1.945 1.957 1.968	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450 440,193 448,641 457,139 465,688 474,287	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.550 9.721 9.721 10.105
Zone 3 (100-year)	7.00 7.10 7.10 7.20 7.30 7.40 7.50 7.60 7.70 8.00 8.01 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.80		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.0 436.6 436.7 437.2 439.0 439.0 439.0 440.6 441.4 442.2	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8 192.6 193.4 194.2 195.0 195.8	78,748 79,239 79,732 80,226 80,721 81,217 81,715 82,214 82,764 83,216 83,718 84,222 84,728 85,234 85,742 86,251 86,762		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.887 1.899 1.900 1.910 1.922 1.932 1.945 1.957 1.968 1.992	358,473 366,422 374,420 382,467 390,564 406,907 415,153 415,981 423,450 431,796 440,193 448,641 457,139 465,688 474,287 482,938	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.551 9.721 9.913 10.105 10.299 10.494 10.691 10.888
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.01 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.80 8.90		430.2 431.0 431.8 432.6 433.4 434.2 435.0 435.6 436.6 436.7 437.4 438.2 439.0 440.6 441.4 442.2 443.0 443.8 444.6	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8 192.6 193.4 194.2 195.0 195.8 196.8	78,748 79,239 79,732 80,226 80,721 81,715 82,714 82,764 83,718 84,728 84,728 85,234 85,742 86,762 87,727		1.808 1.819 1.830 1.842 1.854 1.876 1.876 1.899 1.900 1.910 1.922 1.933 1.945 1.957 1.968 1.992 2.004	358,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450 440,193 448,641 457,139 448,641 457,139 482,938 491,640 500,393	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.721 9.913 10.105 10.299 10.494 10.691 10.888 11.087
Zone 3 (100-year)	7.00 7.10 7.10 7.20 7.30 7.40 7.50 7.60 7.70 8.00 8.01 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.89 9.00		430.2 431.8 431.8 432.6 433.4 434.2 435.5 436.5 436.6 437.4 438.2 439.9 439.9 441.4 442.2 443.0 443.8	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8 192.6 193.4 194.2 195.8 196.6 197.8	78,748 79,239 79,732 80,226 80,721 81,715 82,714 82,714 82,714 82,764 83,718 84,222 84,728 85,234 85,742 86,762 87,787 88,787 88,787 88,787		1.808 1.819 1.830 1.842 1.853 1.864 1.876 1.889 1.900 1.910 1.922 1.933 1.945 1.957 1.968 1.992 2.004 2.015	388,473 366,422 374,420 382,467 399,540 406,907 415,153 415,153 415,153 440,193 440,193 448,641 457,139 465,688 474,287 482,938 491,640 500,393 509,197	8.229 8.412 8.595 8.780 8.965 9.153 9.341 9.551 9.721 9.913 10.105 10.299 10.691 10.888 11.087 11.286 11.286
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.01 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.80 8.90		430.2 431.8 431.8 432.6 433.4 434.2 435.8 436.6 436.7 437.4 438.2 439.0 439.0 441.4 442.2 441.4 442.2 443.8 444.6 445.4 446.6 447.0	183.0 183.8 184.6 185.4 186.2 187.0 187.8 188.6 189.4 189.5 190.2 191.0 191.8 192.6 193.4 194.2 195.0 195.8 196.8	78,748 79,239 79,732 80,226 80,721 81,715 82,714 82,764 83,718 84,728 84,728 85,234 85,742 86,762 87,727		1.808 1.819 1.830 1.842 1.842 1.864 1.876 1.897 1.900 1.910 1.922 1.935 1.945 1.968 1.980 1.990 2.004 2.015 2.027 2.039 2.051	388,473 366,422 374,420 382,467 380,748 389,710 406,907 415,153 415,981 423,450 431,796 440,193 448,641 457,139 448,641 457,139 482,938 491,640 500,393 491,640 500,393	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.721 9.913 10.105 10.299 10.494 10.691 10.888 11.087
Zone 3 (100-year)	7.00 7.10 7.20 7.30 7.40 7.50 7.60 7.70 7.80 7.90 8.01 8.10 8.20 8.30 8.40 8.50 8.60 8.70 8.80 9.00 9.10		430.2 431.8 431.8 432.6 433.4 434.2 435.0 435.8 436.6 436.7 437.4 438.2 439.8 440.6 441.4 442.2 443.0 444.6 445.4	183.0 183.8 184.6 185.4 186.2 187.0 187.8 189.4 189.5 190.2 191.0 191.6 192.6 193.4 194.2 195.0 195.8 196.6 197.4 196.2 197.4	78,748 79,239 79,732 80,226 80,721 81,715 82,714 82,714 82,764 83,718 84,728 84,728 85,234 85,742 86,251 86,762 87,787 88,301		1.808 1.819 1.830 1.842 1.854 1.876 1.876 1.899 1.900 1.910 1.922 1.935 1.945 1.960 1.960 1.992 2.004 2.015 2.039	388,473 366,422 374,420 382,467 390,564 398,710 406,907 415,153 415,981 423,450 431,796 440,193 445,688 474,287 482,938 491,640 500,393 509,197 518,053	8.229 8.412 8.595 8.780 8.966 9.153 9.341 9.531 9.571 9.913 10.105 10.299 10.494 10.691 10.888 11.087 11.286 11.487 11.690 11.487

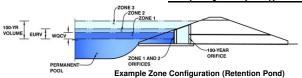
DF-3, Basin 10/20/2021, 4:32 PM



MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch

Basin ID: DF-3 (W Single Family Pond)(Sub-basin 1-D Added)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.27	1.770	Orifice Plate
Zone 2 (EURV)	5.99	4.161	Circular Orifice
Zone 3 (100-year)	8.01	3.601	Weir&Pipe (Restrict)
-	Total (all zones)	9.532	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = N/A Underdrain Orifice Diameter = N/A

Calculated Parameters for Underdrain Underdrain Orifice Area N/A Underdrain Orifice Centroid = N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) 3.27 Orifice Plate: Orifice Vertical Spacing = 12.60 inches Orifice Plate: Orifice Area per Row sq. inches (use rectangular openings)

Calculated Parameters for Plate WQ Orifice Area per Row 3.590E-02 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.09	2.18					
Orifice Area (sq. inches)	5.17	5.17	5.17					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Zone 2 Circular Not Selected Invert of Vertical Orifice 3.27 N/A ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Vertical Orifice = 5.99 N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Diameter = 4.90 inches N/A

Calculated Parameters for Vertical Orifice Zone 2 Circular Not Selected Vertical Orifice Area 0.13 N/A Vertical Orifice Centroid = 0.20 N/A

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.10	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, $H_t$ =	7.10	N/A	feet
Overflow Weir Front Edge Length =	12.00	N/A	feet	Overflow Weir Slope Length =	4.12	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V Gra	ate Open Area / 100-yr Orifice Area =	6.09	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet Ov	erflow Grate Open Area w/o Debris =	34.63	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area O	verflow Grate Open Area w/ Debris =	17.32	N/A	ft²
Debris Clogging % =	50%	N/A	%				-

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe = 0.30 Outlet Orifice Area 5.69 N/A ft (distance below basin bottom at Stage = 0 ft) N/A Outlet Orifice Centroid = Outlet Pipe Diameter = 36.00 N/A inches 1.24 N/A feet Restrictor Plate Height Above Pipe Invert = 27.00 inches Half-Central Angle of Restrictor Plate on Pipe = 2.09 adians

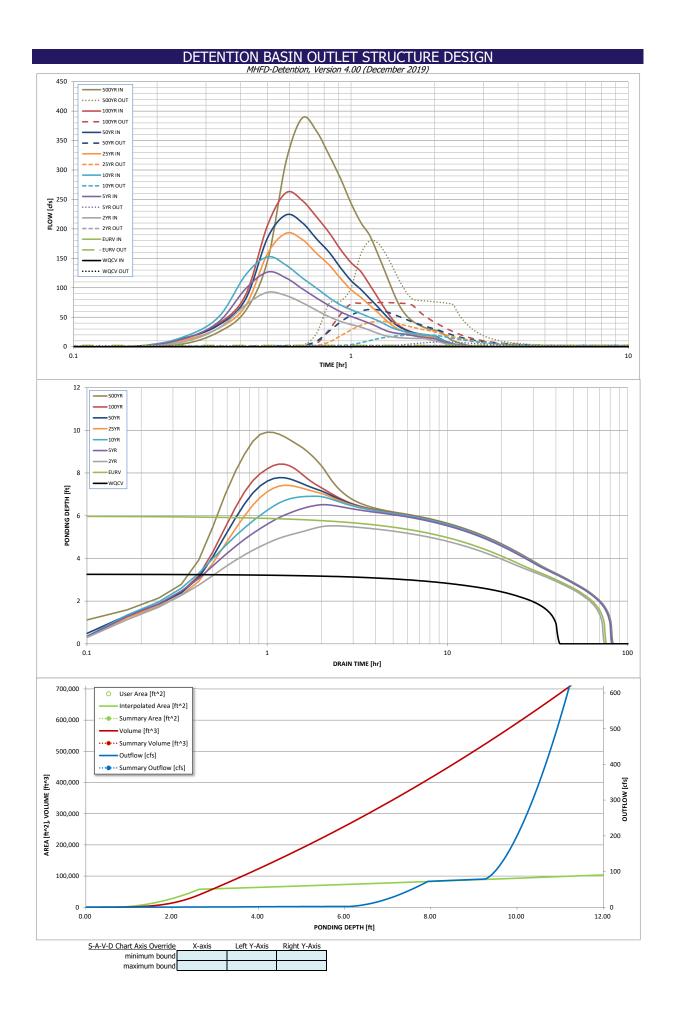
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= 9.25 ft (relative to basin bottom at Stage = 0 ft) Spillway Crest Length = 58.00 feet Spillway End Slopes 4.00 H:V Freeboard above Max Water Surface = 1.00 feet

	Calculated Paramet	ers for Spillway
Spillway Design Flow Depth=	0.96	feet
Stage at Top of Freeboard =		feet
Basin Area at Top of Freeboard =	2.28	acres
asin Volume at Top of Freeboard =	16.23	acre-ft

Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	1.770	5.931	5.483	7.478	9.176	11.254	13.050	15.227	22.864
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	5.483	7.478	9.176	11.254	13.050	15.227	22.864
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	8.6	24.3	36.9	66.0	82.8	105.1	175.9
OPTIONAL Override Predevelopment Peak Q (cfs) =		N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.10	0.29	0.44	0.79	0.99	1.26	2.10
Peak Inflow Q (cfs) =	N/A	N/A	92.2	126.7	152.5	192.6	223.8	261.5	388.1
Peak Outflow Q (cfs) =	0.7	2.1	2.0	8.3	20.1	43.0	63.2	74.9	179.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.5	0.7	0.8	0.7	1.0
Structure Controlling Flow =	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.5	1.2	1.8	2.1	2.3
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	72	71	69	68	66	61
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	77	77	76	76	75	73
Maximum Ponding Depth (ft) =	3.27	5.99	5.53	6.52	6.91	7.42	7.79	8.42	9.91
Area at Maximum Ponding Depth (acres) =	1.39	1.67	1.62	1.73	1.78	1.83	1.87	1.95	2.12
Maximum Volume Stored (acre-ft) =	1.783	5.942	5.168	6.827	7.529	8.449	9.116	10.319	13.371



## DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00 8.41	0.00 13.72	0.00 16.98	0.00 11.40	0.95 14.42	0.10 13.90	5.01 24.97
	0:20:00	0.00	0.00	31.65	42.17	50.61	31.46	36.74	39.14	61.26
	0:25:00	0.00	0.00	70.93	98.29	121.78	69.32	80.81	87.94	145.77
	0:30:00	0.00	0.00	92.24	126.71	152.46	157.88	184.62	205.94	314.53
	0:35:00	0.00	0.00	86.69 74.67	116.67 98.48	138.30 116.87	192.58 182.14	223.78 210.64	261.45 248.19	388.14 366.31
	0:45:00	0.00	0.00	61.91	82.73	99.55	158.62	183.32	220.66	325.51
	0:50:00	0.00	0.00	50.91	69.93	83.33	138.85	160.44	193.74	285.41
	0:55:00	0.00	0.00	42.96	59.13	70.89	115.92	134.04	165.05	243.48
	1:00:00	0.00	0.00	37.64 33.41	51.44 45.40	62.86 56.32	96.83 83.96	112.19 97.46	142.63 127.75	211.10 189.27
	1:10:00	0.00	0.00	27.93	39.71	49.95	70.46	81.90	105.27	156.81
	1:15:00	0.00	0.00	22.63	33.44	44.21	57.88	67.39	83.05	124.70
	1:20:00	0.00	0.00	18.54	27.39	37.41	45.56	53.00	62.28	93.59
	1:25:00	0.00	0.00	16.23 15.09	23.91 22.14	31.62 27.69	35.37 28.66	41.11 33.23	45.16 34.85	68.26 52.87
	1:35:00	0.00	0.00	14.47	21.00	25.06	24.12	27.83	28.60	43.45
	1:40:00	0.00	0.00	14.14	18.98	23.19	21.25	24.39	24.47	37.14
	1:45:00	0.00	0.00	13.88	17.09	21.87	19.28	22.02	21.62	32.80
	1:50:00	0.00	0.00	13.68 12.15	15.78 14.81	20.94 19.79	18.03 17.14	20.51 19.42	19.68 18.31	29.83 27.71
	2:00:00	0.00	0.00	10.54	13.73	17.92	16.55	18.69	17.51	26.44
	2:05:00	0.00	0.00	8.06	10.54	13.58	12.88	14.53	13.65	20.56
	2:10:00	0.00	0.00	5.75	7.45	9.52	9.04	10.18	9.60	14.42
	2:15:00	0.00	0.00	4.07 2.86	5.27 3.67	6.74 4.75	6.41 4.53	7.21 5.08	6.87 4.87	7.31
	2:25:00	0.00	0.00	1.95	2.47	3.26	3.11	3.49	3.35	5.01
	2:30:00	0.00	0.00	1.29	1.64	2.20	2.12	2.38	2.28	3.41
	2:35:00	0.00	0.00	0.80	1.09	1.42	1.41	1.58	1.51	2.26
	2:40:00	0.00	0.00	0.44 0.19	0.64	0.82	0.85 0.42	0.95 0.47	0.91 0.45	1.35 0.67
	2:50:00	0.00	0.00	0.07	0.10	0.12	0.14	0.16	0.15	0.22
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00 3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00 3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00 3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.02 (February 2020)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft <sup>3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of a
							outlets (e.g. vertical orifice,
							overflow grate, and spillway where applicable).
							1
						1	
							1
		1	l	l	l		J

MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

# Basin ID: <u>DF-4 (SW Single Family Pond)</u> 2008 1 AMD 2 ORIFICE PERMANENT PERMANENT Example Zone Configuration (Retention Pond)

#### Watershed Information

ACTURIOU TITOTTICATION		
Selected BMP Type =	EDB	
Watershed Area =	23.14	acres
Watershed Length =	1,970	ft
Watershed Length to Centroid =	991	ft
Watershed Slope =	0.013	ft/ft
Watershed Imperviousness =	65.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Rainfall Denths =	User Innut	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.490	acre-feet
Excess Urban Runoff Volume (EURV) =	1.642	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.513	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	2.063	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.531	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	3.104	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.598	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.197	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	6.300	acre-feet
Approximate 2-yr Detention Volume =	1.273	acre-feet
Approximate 5-yr Detention Volume =	1.707	acre-feet
Approximate 10-yr Detention Volume =	2.176	acre-feet
Approximate 25-yr Detention Volume =	2.344	acre-feet
Approximate 50-yr Detention Volume =	2.441	acre-feet
Approximate 100-yr Detention Volume =	2.639	acre-feet

	dare reet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.55	inches

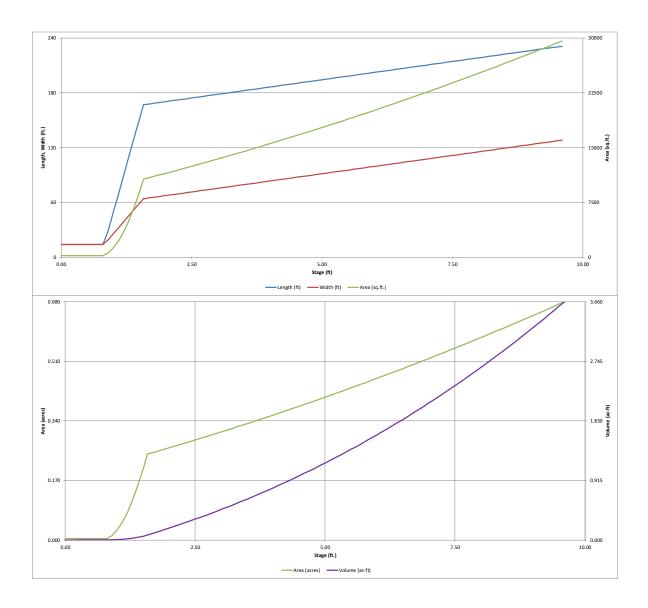
#### Define Zones and Basin Geometry

Jefine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.490	acre-f
Zone 2 Volume (EURV - Zone 1) =	1.152	acre-f
Zone 3 Volume (100-year - Zones 1 & 2) =	0.997	acre-f
Total Detention Basin Volume =	2.639	acre-f
Initial Surcharge Volume (ISV) =	64	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (H <sub>total</sub> ) =	8.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	3	

Initial Surcharge Area (A <sub>ISV</sub> ) =	194	ft 2
Surcharge Volume Length (L <sub>ISV</sub> ) =	13.9	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	13.9	ft
Depth of Basin Floor $(H_{FLOOR})$ =	0.75	ft
Length of Basin Floor $(L_{FLOOR})$ =	166.9	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	63.9	ft
Area of Basin Floor $(A_{FLOOR})$ =	10,672	ft <sup>2</sup>
Volume of Basin Floor $(V_{FLOOR})$ =	3,076	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	6.42	ft
Length of Main Basin ( $L_{MAIN}$ ) =	218.3	ft
Width of Main Basin ( $W_{MAIN}$ ) =	115.3	ft
Area of Main Basin $(A_{MAIN}) =$	25,167	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	111,766	ft <sup>3</sup>
Calculated Total Basin Volume (Vtotal) =	2.640	acre-feet

Depth Increment =	0.10	π Optional				Optional			Γ
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description Top of Micropool	(ft) 0.00	Stage (ft)	(ft) 13.9	(ft) 13.9	(ft <sup>2</sup> )	Area (ft 2)	(acre) 0.004	(ft 3)	(ac-ft)
ISV	0.00		13.9	13.9	194		0.004	64	0.001
130	0.40		13.9	13.9	194		0.004	78	0.001
	0.50		13.9	13.9	194		0.004	97	0.002
	0.60		13.9	13.9	194		0.004	116	0.003
	0.70		13.9	13.9	194		0.004	136	0.003
	0.80		13.9	13.9	194		0.004	155	0.004
	0.90		28.2	18.6	525		0.012	185	0.004
	1.00		48.6 69.0	25.3 31.9	1,228		0.028	271 440	0.006
	1.10		89.4	38.6	3,451		0.031	721	0.010
	1.30		109.8	45.3	4,970		0.114	1,139	0.026
	1.40		130.2	51.9	6,762		0.155	1,724	0.040
	1.50		150.6	58.6	8,825		0.203	2,501	0.057
Floor	1.58		166.9	63.9	10,672		0.245	3,280	0.075
	1.60		167.1 167.9	64.1	10,709		0.246	3,493 4,574	0.080
	1.80		168.7	65.7	11,081		0.254	5,672	0.130
	1.90		169.5	66.5	11,270		0.259	6,790	0.156
	2.00		170.3	67.3	11,459		0.263	7,926	0.182
	2.10		171.1	68.1	11,650		0.267	9,082	0.208
	2.20		171.9	68.9	11,842		0.272	10,256	0.235
	2.30		172.7	69.7 70.5	12,035		0.276	11,450	0.263
	2.40		173.5 174.3	70.5	12,229 12,425		0.281	12,663 13,896	0.291
	2.60		175.1	72.1	12,622		0.290	15,148	0.348
	2.70		175.9	72.9	12,821		0.294	16,421	0.377
	2.80		176.7	73.7	13,020		0.299	17,713	0.407
	2.90		177.5	74.5	13,221		0.304	19,025	0.437
7ano 1 (14)0010	3.00		178.3	75.3	13,424		0.308	20,357	0.467
Zone 1 (WQCV)	3.08		178.9 179.1	75.9 76.1	13,586 13,627		0.312	21,437	0.492
	3.20		179.1	76.1	13,832		0.318	23,082	0.530
	3.30		180.7	77.7	14,038		0.322	24,476	0.562
	3.40		181.5	78.5	14,245		0.327	25,890	0.594
	3.50		182.3	79.3	14,454		0.332	27,325	0.627
	3.60		183.1	80.1	14,664		0.337	28,781	0.661
	3.70		183.9 184.7	80.9 81.7	14,875 15,087		0.341	30,258 31,756	0.695
	3.90		185.5	82.5	15,301		0.351	33,275	0.764
	4.00		186.3	83.3	15,516		0.356	34,816	0.799
	4.10		187.1	84.1	15,733		0.361	36,379	0.835
	4.20		187.9	84.9	15,950		0.366	37,963	0.872
	4.30		188.7	85.7	16,169		0.371	39,569	0.908
	4.40		189.5 190.3	86.5 87.3	16,389 16,611		0.376	41,197 42,847	0.946
	4.60		191.1	88.1	16.833		0.386	44.519	1.022
	4.70		191.9	88.9	17,057		0.392	46,213	1.061
	4.80		192.7	89.7	17,283		0.397	47,930	1.100
	4.90		193.5	90.5	17,509		0.402	49,670	1.140
	5.00		194.3 195.1	91.3 92.1	17,737 17,966		0.407	51,432 53.217	1.181
	5.10		195.1	92.1	18,196		0.412	55,025	1.263
	5.30		196.7	93.7	18,428		0.418	56,857	1.305
	5.40		197.5	94.5	18,661		0.428	58,711	1.348
	5.50		198.3	95.3	18,895		0.434	60,589	1.391
	5.60		199.1	96.1	19,131		0.439	62,490	1.435
	5.70 5.80		199.9 200.7	96.9 97.7	19,368 19,606		0.445	64,415 66,364	1.479
	5.90		201.5	98.5	19,845		0.456	68,336	1.569
Zone 2 (EURV)	6.00		202.3 202.8	99.3 99.8	20,086		0.461	70,333 71,542	1.615
	6.10		203.1 203.9	100.1 100.9	20,327 20,571		0.467 0.472	72,353 74,398	1.661 1.708
	6.30		204.7	101.7	20,815		0.478	76,467	1.755
	6.40		205.5 206.3	102.5 103.3	21,061 21,308		0.483	78,561 80,680	1.804 1.852
	6.60		207.1	104.1	21,556		0.495	82,823	1.901
	6.70 6.80		208.7	105.7	21,806 22,057		0.501 0.506	84,991 87,184	2.001
	6.90 7.00		209.5 210.3	106.5 107.3	22,309 22,562		0.512 0.518	89,402 91,646	2.052
	7.10		211.1	108.1	22,817		0.524	93,915	2.156
	7.20 7.30		211.9 212.7	108.9 109.7	23,073 23,330		0.530 0.536	96,209 98,529	2.209 2.262
	7.40 7.50		213.5 214.3	110.5 111.3	23,589 23,849		0.542	100,875 103,247	2.316
	7.60		215.1	112.1	24,110		0.553	105,645	2.425
	7.70 7.80		215.9 216.7	112.9 113.7	24,372 24,636		0.560	108,069 110,520	2.481
ono 2 (100 ···· `	7.90		217.5	114.5	24,901		0.572	112,996	2.594
one 3 (100-year)	7.98 8.00		218.3	115.1 115.3	25,114 25,167		0.577 0.578	114,997 115,500	2.640 2.652
	8.10 8.20		219.1 219.9	116.1 116.9	25,434 25,703		0.584	118,030 120,587	2.710 2.768
	8.30		220.7	117.7	25,973		0.596	123,170	2.828
	8.40 8.50		221.5 222.3	118.5 119.3	26,245 26,517		0.602	125,781 128,419	2.888
	8.60		223.1	120.1	26,791		0.615	131,085	3.009
	8.70 8.80		223.9 224.7	120.9 121.7	27,066 27,343		0.621	133,778 136,498	3.071 3.134
	8.90 9.00		225.5 226.3	122.5 123.3	27,620 27,900		0.634	139,246 142,022	3.197 3.260
	9.10		227.1	124.1	28,180		0.647	144,826	3.325
	9.20 9.30		227.9 228.7	124.9 125.7	28,461 28,744		0.653	147,658 150,519	3.390 3.455
	9.40		229.5	126.5	29,028		0.666	153,407	3.522
	9.50		230.3	127.3	29,314		0.673	156,324	3.589

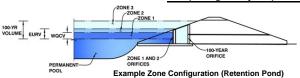
DF-4.x/sm, Basin 12/4/2020, 10:12 AM



MHFD-Detention, Version 4.02 (February 2020)



Basin ID: DF-4 (SW Single Family Pond)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.08	0.490	Orifice Plate
Zone 2 (EURV)	6.06	1.152	Circular Orifice
Zone 3 (100-year)	7.98	0.997	Weir&Pipe (Restrict)
	Total (all zones)	2.639	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = N/A Underdrain Orifice Diameter = N/A

Calculated Parameters for Underdrain Underdrain Orifice Area : N/A Underdrain Orifice Centroid = N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

ft (relative to basin bottom at Stage = 0 ft) Invert of Lowest Orifice = Depth at top of Zone using Orifice Plate = 3.08 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 12.30 inches Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-7/16 inches)

Calculated Parameters for Plate WQ Orifice Area per Row = 1.139E-02 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

Calculated Parameters for Vertical Orifice

Not Selected N/A

<u>User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)</u>

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.03	2.05					
Orifice Area (sq. inches)	1.64	1.64	1.64					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected			Zone 2 Circular
Invert of Vertical Orifice =	3.08	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.02
Depth at top of Zone using Vertical Orifice =	6.06	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.08
Vertical Orifice Diameter =	1 97	N/A	inches		

User Input: Overflow Weir (Dropbox with Flat or	Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.25	N/A	ft (relative to basin bottom at Stage = 0 ft) $$ Height of Grate Upper Edge, $H_t =$	6.25	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	10.16	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet Overflow Grate Open Area w/o Debris =	16.80	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Overflow Grate Open Area w/ Debris =	8.40	N/A	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%	•		

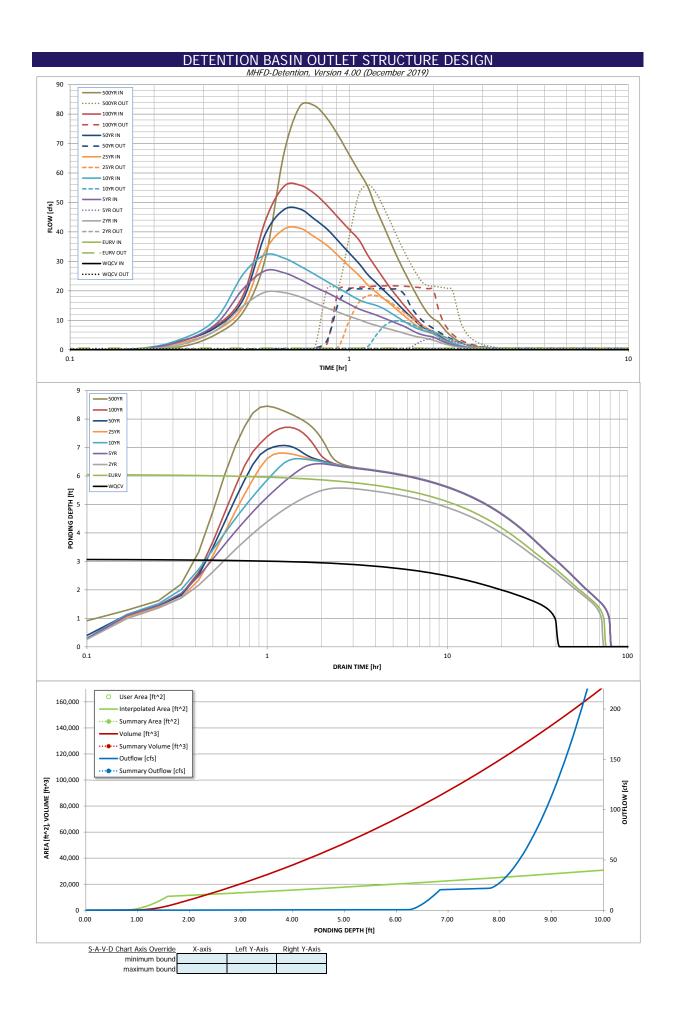
<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restric</u>tor Plate, or Rectangular Orifice)

er input: Outlet Pipe W/ Flow Restriction Plate (Circular Office, Restrictor Plate, or Recta			ctangular Orifice)	Calculated Parameters	s for Outlet Pipe w/	Flow Restriction Pla	<u>ate</u>
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.65	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.60	N/A	feet
Restrictor Plate Height Above Pipe Invert =	12.50		inches Half-Central Angle	of Restrictor Plate on Pipe =	1.61	N/A	radiar

User Input: Emergency Spillway (Rectangular or Trapezoidal)

out: Emergency Spillway (Rectangular or 1	<u> [rapezoidal]</u>	_		Calculated Parame	ters for Spillway
Spillway Invert Stage=	7.80	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.89	feet
Spillway Crest Length =	19.00	feet	Stage at Top of Freeboard =	9.69	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.69	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	3.72	acre-ft

Routed Hydrograph Results	The user can over	ride the default CUH	IP hydrographs and	runoff volumes by a	entering new values	in the Inflow Hydro	ngraphs table (Colur	nns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.490	1.642	1.513	2.063	2.531	3.104	3.598	4.197	6.300
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.513	2.063	2.531	3.104	3.598	4.197	6.300
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.7	4.8	7.4	13.7	17.2	22.0	36.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.07	0.21	0.32	0.59	0.74	0.95	1.60
Peak Inflow Q (cfs) =	N/A	N/A	19.5	26.8	32.2	41.2	47.8	55.9	82.9
Peak Outflow Q (cfs) =	0.2	0.5	0.5	3.9	9.8	18.4	20.7	21.7	56.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.8	1.3	1.3	1.2	1.0	1.5
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.6	1.0	1.2	1.3	1.3
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	72	70	68	67	65	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	77	76	75	75	74	72
Maximum Ponding Depth (ft) =	3.08	6.06	5.58	6.43	6.61	6.80	7.07	7.71	8.45
Area at Maximum Ponding Depth (acres) =	0.31	0.46	0.44	0.49	0.49	0.51	0.52	0.56	0.61
Maximum Volume Stored (acre-ft) =	0.492	1.642	1.421	1.818	1.901	2.001	2.140	2.487	2.918



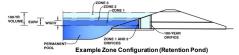
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acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches

2.25 inches 2.52 inches 3.55 inches

#### Project: Singer Ranch

#### Basin ID: DF-5 (S Single Family & School Pond)



#### Watershed Information

	EDB	Selected BMP Type =
acres	57.54	Watershed Area =
ft	2,851	Watershed Length =
ft	1,555	Watershed Length to Centroid =
ft/ft	0.013	Watershed Slope =
percen	70.00%	Watershed Imperviousness =
percen	0.0%	Percentage Hydrologic Soil Group A =
percen	100.0%	Percentage Hydrologic Soil Group B =
percen	0.0%	Percentage Hydrologic Soil Groups C/D =
hours	40.0	Target WQCV Drain Time =
	Hear Innut	Location for 1 br Rainfall Donths -

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Procedu	ire.
Water Quality Capture Volume (WQCV) =	1.319	acre-feet
Excess Urban Runoff Volume (EURV) =	4.423	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	4.049	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	5.460	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	6.650	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	8.056	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	9.300	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	10.782	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	16.053	acre-feet
Approximate 2-yr Detention Volume =	3.456	acre-feet
Approximate 5-yr Detention Volume =	4.606	acre-feet
Approximate 10-yr Detention Volume =	5.814	acre-feet
Approximate 25-yr Detention Volume =	6.247	acre-feet
Approximate 50-yr Detention Volume =	6.498	acre-feet
Approximate 100-yr Detention Volume =	6.961	acre-feet

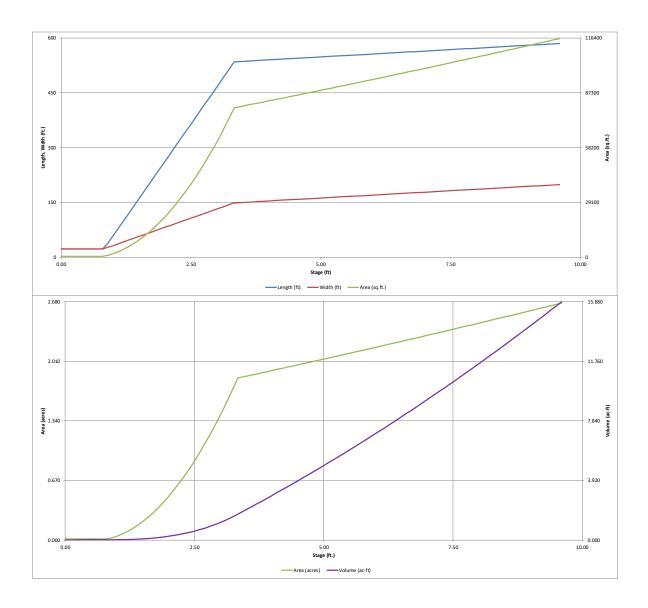
#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.319	acre-feet
Zone 2 Volume (EURV - Zone 1) =	3.105	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	2.538	acre-fee
Total Detention Basin Volume =	6.961	acre-fee
Initial Surcharge Volume (ISV) =	172	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.005	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	4	

Initial Surcharge Area $(A_{ISV}) =$	522	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	22.9	ft
Surcharge Volume Width $(W_{ISV}) =$	22.9	ft
Depth of Basin Floor $(H_{FLOOR})$ =	2.51	ft
Length of Basin Floor $(L_{FLOOR})$ =	534.9	ft
Width of Basin Floor $(W_{FLOOR}) =$	148.4	ft
Area of Basin Floor $(A_{FLOOR})$ =	79,353	ft <sup>2</sup>
Volume of Basin Floor $(V_{FLOOR}) =$	72,215	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	2.66	ft
Length of Main Basin $(L_{MAIN}) =$	556.2	ft
Width of Main Basin ( $W_{MAIN}$ ) =	169.6	ft
Area of Main Basin $(A_{MAIN}) =$	94,345	ft²
Volume of Main Basin $(V_{MAIN}) =$	230,730	ft <sup>3</sup>
Calculated Total Basin Volume $(V_{total}) =$	6.965	acre-feet

Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool	0.00		22.9	22.9	522		0.012		
ISV	0.33		22.9	22.9	522		0.012	172	0.004
	0.40		22.9	22.9	522		0.012	209	0.005
	0.50		22.9	22.9	522		0.012	261	0.006
	0.60		22.9	22.9	522 522		0.012	313 366	0.007
	0.70		22.9	22.9	522		0.012	418	0.008
	0.90		37.1	26.4	979		0.022	485	0.011
	1.00		57.5	31.4	1,804		0.041	623	0.014
	1.10		77.9	36.4	2,833		0.065	853	0.020
	1.20		98.3	41.4	4,066		0.093	1,196	0.027
	1.30		118.7	46.4	5,504		0.126	1,673	0.038
	1.40		139.1	51.4	7,145		0.164	2,304	0.053
	1.50		159.5	56.4	8,990		0.206	3,109	0.071
	1.60		179.9 200.3	61.4 66.4	11,039 13,293		0.253	4,109 5,323	0.094
	1.80		220.7	71.4	15,750		0.362	6,774	0.122
	1.90		241.1	76.4	18,411		0.423	8,480	0.195
	2.00		261.5	81.4	21,276		0.488	10,463	0.240
	2.10		281.9	86.4	24,346		0.559	12,742	0.293
	2.20		302.3	91.4	27,619		0.634	15,339	0.352
	2.30		322.7	96.4	31,096		0.714	18,273	0.419
	2.40		343.1	101.4	34,777		0.798	21,565	0.495
	2.50		363.5	106.4	38,663		0.888	25,235	0.579
	2.60		383.9	111.4	42,752		0.981	29,304	0.673
	2.70		404.3 424.7	116.4 121.4	47,045 51,542		1.080	33,792	0.776
	2.80		424.7	121.4	51,542		1.183	38,720 44,107	1.013
	3.00		465.5	131.4	61,149		1.404	49,975	1.013
	3.10		485.9	136.4	66,258		1.521	56,344	1.293
Zone 1 (WQCV)	3.12		490.0	137.4	67,304		1.545	57,680	1.324
,	3.20		506.3	141.4	71,571		1.643	63,234	1.452
	3.30		526.7	146.4	77,089		1.770	70,665	1.622
Floor	3.34		534.9	148.4	79,353		1.822	73,794	1.694
	3.40		535.4	148.8	79,681		1.829	78,565	1.804
	3.50		536.2	149.6	80,229		1.842	86,560	1.987
	3.60		537.0	150.4	80,778		1.854	94,611	2.172
	3.70		537.8	151.2	81,329		1.867	102,716	2.358
	3.80		538.6	152.0	81,880		1.880	110,876	2.545
	4.00		539.4 540.2	152.8 153.6	82,434 82,988		1.892	119,092 127,363	2.734
	4.10		541.0	154.4	83,544		1.918	135,690	3.115
	4.20		541.8	155.2	84,101		1.931	144,072	3.307
	4.30		542.6	156.0	84,659		1.944	152,510	3.501
	4.40		543.4	156.8	85,218		1.956	161,004	3.696
	4.50		544.2	157.6	85,779		1.969	169,554	3.892
	4.60		545.0	158.4	86,341		1.982	178,160	4.090
	4.70		545.8	159.2	86,905		1.995	186,822	4.289
Zone 2 (EURV)	4.77		546.3 546.6	159.8 160.0	87,300		2.004	192,919	4.429 4.489
	4.90		547.4	160.0	87,469 88,035		2.008	195,541 204,316	4.690
	5.00		548.2	161.6	88,602		2.021	213,148	4.893
	5.10		549.0	162.4	89,171		2.047	222,036	5.097
	5.20		549.8	163.2	89,741		2.060	230,982	5.303
	5.30		550.6	164.0	90,312		2.073	239,984	5.509
	5.40		551.4	164.8	90,884		2.086	249,044	5.717
	5.50		552.2	165.6	91,458		2.100	258,161	5.927
	5.60		553.0	166.4	92,033		2.113	267,336	6.137
	5.70 5.80		553.8 554.6	167.2 168.0	92,609 93,186		2.126	276,568 285,858	6.349
2 /400	5.90		555.4	168.8	93,765		2.153	295,205	6.777
one 3 (100-year)	5.99 6.00		556.1 556.2	169.6 169.6	94,287 94,345		2.165	303,667 304,611	6.971
	6.10		557.0	170.4	94,926		2.179	314,074	7.210
	6.20		557.8 558.6	171.2 172.0	95,509 96,093		2.193	323,596 333,176	7.429 7.649
	6.40		559.4	172.8	96,678		2.219	342,814	7.870
	6.50		560.2 561.0	173.6 174.4	97,264 97,852		2.233	352,512 362,267	8.093 8.317
	6.70		561.8	175.2 176.0	98,441		2.260	372,082	8.542
	6.80 6.90		562.6 563.4	176.8	99,031 99,622		2.273 2.287	381,955 391,888	8.768 8.997
	7.00		564.2	177.6	100,215		2.301	401,880	9.226
	7.10 7.20		565.0 565.8	178.4 179.2	100,809 101,405		2.328	411,931 422,042	9.457 9.689
-	7.30 7.40		566.6 567.4	180.0 180.8	102,001 102,599		2.342	432,212 442,442	9.922
	7.50		568.2	181.6	103,199		2.369	452,732	10.393
	7.60 7.70		569.0 569.8	182.4 183.2	103,799 104,401		2.383	463,082 473,492	10.631
	7.80		570.6	184.0	105,004		2.411	483,962	11.110
	7.90 8.00		571.4 572.2	184.8 185.6	105,608		2.424	494,493	11.352 11.595
	8.10		573.0	186.4	106,214 106,821		2.452	505,084 515,736	11.840
	8.20		573.8	187.2	107,429		2.466	526,448	12.086
	8.30 8.40		574.6 575.4	188.8	108,038 108,649		2.494	537,221 548,056	12.582
	8.50		576.2	189.6	109,261		2.508	558,951	12.832
	8.60 8.70		577.0 577.8	190.4 191.2	109,874 110,489		2.522	569,908 580,926	13.083
	8.80		578.6	192.0	111,105		2.551	592,006	13.591
	8.90 9.00		579.4 580.2	192.8 193.6	111,722 112,340		2.565	603,147 614,350	13.846
	9.10		581.0	194.4	112,960		2.593	625,615	14.362
	9.20		581.8 582.6	195.2 196.0	113,581 114,203		2.607	636,942 648,331	14.622
	9.40		583.4	196.8	114,827		2.636	659,783	15.147
	9.50		584.2	197.6	115,451		2.650	671,297	15.411

DF-5.xkm, Basin 3/10/2021, 2:13 PM

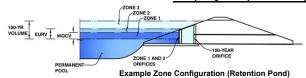


DF-5.xkm, Basin 3/10/2021, 2:13 PM

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch

#### Basin ID: DF-5 (S Single Family & School Pond)



	Locimacca	Locimacca	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.12	1.319	Orifice Plate
Zone 2 (EURV)	4.77	3.105	Circular Orifice
one 3 (100-year)	5.99	2.538	Weir&Pipe (Restrict)
•	Total (all zones)	6.961	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = N/A inches

	Calculated Parameters for Underdrain			
Underdrain Orifice Area =	N/A	ft <sup>2</sup>		
Underdrain Orifice Centroid =	N/A	feet		

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) 3.12 Orifice Plate: Orifice Vertical Spacing = 12.50 inches Orifice Plate: Orifice Area per Row = 3.79 sq. inches (use rectangular openings)

)	Calculated Paramet	ers for Plate
/Q Orifice Area per Row =	2.632E-02	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

<u>User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)</u>

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.04	2.08					
Orifice Area (sq. inches)	3.79	3.79	3.79					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	3.12	N/A	ft (
Depth at top of Zone using Vertical Orifice =	4.77	N/A	ft (
Vertical Orifice Diameter =	5.74	N/A	inc

		Calculated Paramet	ters for vertical Orifi	ice
		Zone 2 Circular	Not Selected	İ
ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.18	N/A	ft <sup>2</sup>
ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.24	N/A	feet
inches				

User Input: Ove

input: Overflow Weir (Dropbox with Flat or	Calculated Parameters for Overflow Weir						
	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.82	N/A	ft (relative to basin bottom at Stage = 0 ft) Heigh	ht of Grate Upper Edge, $H_t$ =	4.82	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet Ov	Overflow Weir Slope Length =	6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open	Area / 100-yr Orifice Area =	5.84	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet Overflow Gra	rate Open Area w/o Debris =	25.20	N/A	ft²
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Overflow G	Grate Open Area w/ Debris =	12.60	N/A	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%	-			

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)</u>

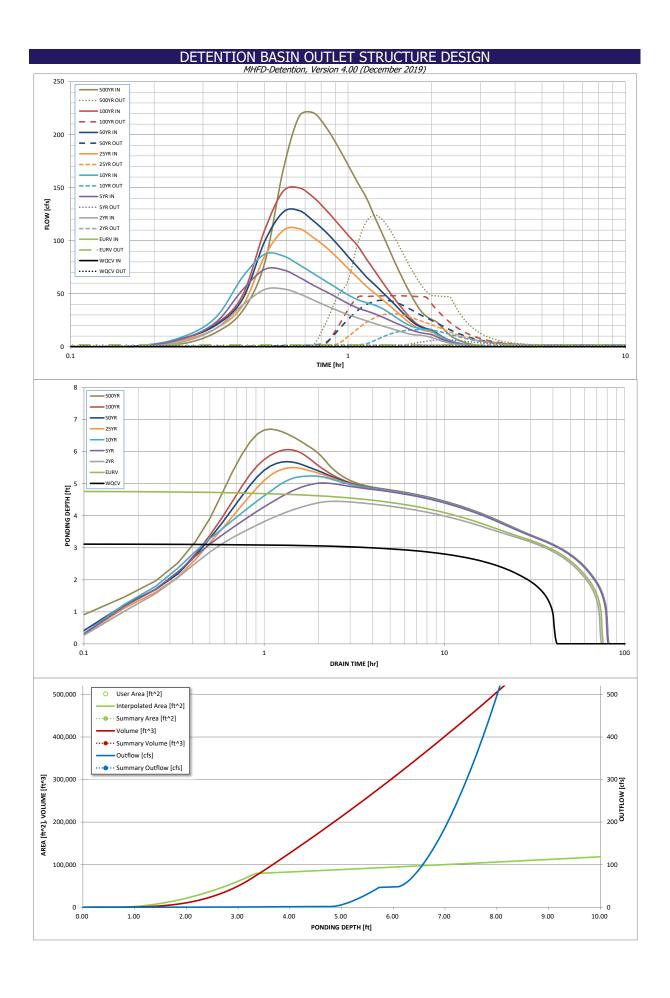
utlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re	strictor Plate, or Re	<u>ctangular Orifice)</u>	Calculated Parameters	s for Outlet Pipe W/	riow Restriction Piz	<u>ate</u>
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	1
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	4.32	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	36.00	N/A	inches	Outlet Orifice Centroid =	1.00	N/A	feet
or Plate Height Above Pipe Invert =	21.15		inches Half-Central Angle of	Restrictor Plate on Pipe =	1.75	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	6.10	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	50.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

	Calculated Paramet	ers for Spillway
Spillway Design Flow Depth=	0.96	feet
Stage at Top of Freeboard =	8.06	feet
Basin Area at Top of Freeboard =	2.45	acres
Basin Volume at Top of Freeboard =	11.72	acre-ft

Routed Hydrograph Results	The user can overr	ide the default CUH	P hydrographs and	runoff volumes by e	entering new values	in the Inflow Hydro	ngraphs table (Colum	nns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	1.319	4.423	4.049	5.460	6.650	8.056	9.300	10.782	16.053
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	4.049	5.460	6.650	8.056	9.300	10.782	16.053
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.3	12.2	18.9	34.6	43.4	56.0	93.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.08	0.21	0.33	0.60	0.75	0.97	1.63
Peak Inflow Q (cfs) =	N/A	N/A	54.5	72.9	87.1	111.3	128.4	149.8	220.6
Peak Outflow Q (cfs) =	0.5	1.8	1.6	6.6	16.1	31.1	43.9	48.1	124.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.9	0.9	1.0	0.9	1.3
Structure Controlling Flow =	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.6	1.2	1.7	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	67	71	70	68	67	66	61
Time to Drain 99% of Inflow Volume (hours) =	40	72	71	76	76	75	75	74	72
Maximum Ponding Depth (ft) =	3.12	4.77	4.45	5.02	5.24	5.50	5.69	6.06	6.70
Area at Maximum Ponding Depth (acres) =	1.55	2.00	1.96	2.04	2.07	2.10	2.12	2.17	2.26
Maximum Volume Stored (acre-ft) =	1.324	4.429	3.774	4.934	5.385	5.927	6.307	7.123	8.542



MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

# Basin ID: DF-6 (NE Commercial Pond)

#### Watershed Information

100-YR VOLUME EURV WQCV	ZONE 2 ZONE 1	
PERMANENT—POOL	ZONE 1 AND 2 ORIFICES  Example Zone Configura	100-YEAR ORIFICE ation (Retention Pond)

tersifed milorifiation		
Selected BMP Type =	EDB	
Watershed Area =	6.50	acres
Watershed Length =	660	ft
Watershed Length to Centroid =	175	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	95.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.242	acre-feet			
Excess Urban Runoff Volume (EURV) =	0.695	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	0.544	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	0.703	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	0.831	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	0.961	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	1.091	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	1.232	acre-feet			
500-yr Runoff Volume (P1 = 3.55 in.) =	1.765	acre-feet			
Approximate 2-yr Detention Volume =	0.561	acre-feet			
Approximate 5-yr Detention Volume =	0.728	acre-feet			
Approximate 10-yr Detention Volume =	0.886	acre-feet			
Approximate 25-yr Detention Volume =	0.950	acre-feet			
Approximate 50-yr Detention Volume =	0.986	acre-feet			
Approximate 100-yr Detention Volume =	1.017	acre-feet			

Optional User Overrides					
	acre-feet				
	acre-feet				
1.19	inches				
1.50	inches				
1.75	inches				
2.00	inches				
2.25	inches				
2.52	inches				
3.55	inches				

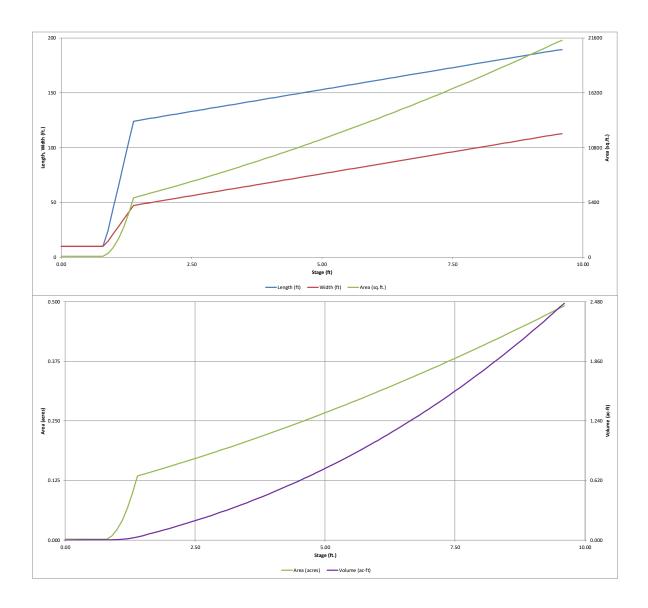
#### Define Zones and Basin Geometry

ACTIFIC ZOTICS UTIL DUSITI OCOTICULY		
Zone 1 Volume (WQCV) =	0.242	acre-fee
Zone 2 Volume (EURV - Zone 1) =	0.453	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	0.322	acre-fee
Total Detention Basin Volume =	1.017	acre-fee
Initial Surcharge Volume (ISV) =	32	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (Htotal) =	6.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel $(S_{TC}) =$	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio ( $R_{L/W}$ ) =	3	

Initial Surcharge Area $(A_{ISV}) =$	96	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	9.8	ft
Surcharge Volume Width $(W_{ISV}) =$	9.8	ft
Depth of Basin Floor $(H_{FLOOR}) =$	0.56	ft
Length of Basin Floor $(L_{FLOOR})$ =	124.0	ft
Width of Basin Floor $(W_{FLOOR}) =$	47.1	ft
Area of Basin Floor $(A_{FLOOR}) =$	5,845	ft <sup>2</sup>
Volume of Basin Floor $(V_{FLOOR}) =$	1,249	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	4.61	ft
Length of Main Basin $(L_{MAIN}) =$	160.9	ft
Width of Main Basin $(W_{MAIN}) =$	84.0	ft
Area of Main Basin $(A_{MAIN}) =$	13,518	ft²
Volume of Main Basin $(V_{MAIN}) =$	43,415	ft <sup>3</sup>
Calculated Total Basin Volume $(V_{total}) =$	1.027	acre-feet

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft <sup>2</sup> )	Area (acre)	Volume (ft <sup>3</sup> )	Volum (ac-ft
Top of Micropool	0.00		9.8	9.8	96		0.002		
ISV	0.33		9.8	9.8	96		0.002	32	0.001
	0.40		9.8	9.8	96		0.002	38	0.001
	0.50		9.8	9.8	96		0.002	48	0.001
	0.60		9.8	9.8	96		0.002	58	0.001
	0.70		9.8	9.8	96		0.002	67	0.002
	0.80		9.8	9.8	96		0.002	77	0.002
	0.90		24.1	14.5	348		0.008	94	0.002
	1.00		44.5	21.1	940		0.022	157	0.004
	1.10		64.9	27.8	1,803		0.041	291	0.007
	1.20		85.3	34.5	2,939		0.067	526	0.012
Floor	1.30		105.7	41.1 47.1	4,346		0.100	1 245	
Floor	1.39		124.0 124.1	47.1	5,845 5,859		0.134	1,345 1,404	0.031
	1.50		124.9	48.0	5,997		0.138	1,996	0.046
	1.60		125.7	48.8	6,136		0.141	2,603	0.060
	1.70		126.5	49.6	6,276		0.144	3,224	0.074
	1.80		127.3	50.4	6,418		0.147	3,858	0.089
	1.90		128.1	51.2	6,560		0.151	4,507	0.103
	2.00		128.9	52.0	6,705		0.154	5,170	0.119
	2.10		129.7	52.8	6,850		0.157	5,848	0.134
	2.20		130.5	53.6	6,997		0.161	6,541	0.150
	2.30		131.3	54.4	7,145		0.164	7,248	0.166
	2.40		132.1	55.2	7,294		0.167	7,969	0.183
	2.50		132.9	56.0	7,444		0.171	8,706	0.200
	2.60		133.7	56.8	7,596		0.174	9,458	0.217
	2.70		134.5	57.6	7,749		0.178	10,226	0.235
Zone 1 (WQCV)	2.75		134.9	58.0	7,826		0.180	10,615	0.24
	2.80		135.3	58.4	7,903		0.181	11,008	0.253
	2.90		136.1	59.2	8,059		0.185	11,806	0.271
	3.00		136.9 137.7	60.0	8,216 8,374		0.189	12,620 13,450	0.290
	3.20		137.7	61.6	8,534		0.192	14,295	0.30
	3.30		139.3	62.4	8,694		0.196	15,156	0.348
	3.40		140.1	63.2	8,856		0.203	16,034	0.368
	3.50		140.9	64.0	9,020		0.207	16,928	0.389
	3.60		141.7	64.8	9,184		0.211	17,838	0.409
	3.70		142.5	65.6	9,350		0.215	18,765	0.431
	3.80		143.3	66.4	9,517		0.218	19,708	0.452
	3.90		144.1	67.2	9,686		0.222	20,668	0.474
	4.00		144.9	68.0	9,855		0.226	21,645	0.497
	4.10		145.7	68.8	10,026		0.230	22,639	0.520
	4.20		146.5	69.6	10,199		0.234	23,650	0.543
	4.30		147.3	70.4	10,372		0.238	24,679	0.567
	4.40		148.1	71.2	10,547		0.242	25,725	0.591
	4.50		148.9	72.0	10,723		0.246	26,788	0.615
	4.60		149.7	72.8	10,900		0.250	27,869	0.640
	4.70		150.5	73.6	11,079		0.254	28,968	0.665
	4.80		151.3	74.4	11,259		0.258	30,085	0.691
Zone 2 (EURV)	4.82		151.5	74.6	11,295		0.259	30,311	0.696
	4.90 5.00		152.1 152.9	75.2 76.0	11,440		0.263	31,220	0.717
	5.10		153.7	76.8	11,623 11,806		0.207	32,373 33,545	0.770
	5.20		154.5	77.6	11,992		0.275	34,735	0.797
	5.30		155.3	78.4	12,178		0.280	35,943	0.825
	5.40		156.1	79.2	12,365		0.284	37,170	0.853
	5.50		156.9	80.0	12,554		0.288	38,416	0.882
	5.60		157.7	80.8	12,745		0.293	39,681	0.911
	5.70		158.5	81.6	12,936		0.297	40,965	0.940
	5.80 5.90		159.3 160.1	82.4 83.2	13,129 13,323		0.301 0.306	42,269 43,591	0.970 1.001
one 3 (100-year)	5.96		160.6	83.7	13,440		0.309	44,394	1.019
	6.00 6.10		160.9 161.7	84.0 84.8	13,518 13,715		0.310	44,933 46,295	1.032
	6.20		162.5	85.6	13,913		0.319	47,676	1.094
	6.30 6.40		163.3 164.1	86.4 87.2	14,112		0.324 0.329	49,077 50,498	1.127
	6.50		164.1	88.0	14,312 14,514		0.333	51,940	1.192
	6.60		165.7	88.8	14,717		0.338	53,401	1.226
	6.70 6.80		166.5 167.3	89.6 90.4	14,921 15,127		0.347	54,883 56,385	1.29
	6.90		168.1	91.2	15,333		0.352	57,908	1.329
	7.00 7.10		168.9 169.7	92.0 92.8	15,541 15,751		0.357 0.362	59,452 61,017	1.365
	7.20		170.5	93.6	15,961		0.366	62,602	1.437
	7.30 7.40		171.3 172.1	94.4 95.2	16,173 16,387		0.371	64,209 65,837	1.474
	7.50		172.9	96.0	16,601		0.381	67,487	1.549
	7.60 7.70		173.7 174.5	96.8 97.6	16,817 17,034		0.386 0.391	69,157 70,850	1.588
	7.80		175.3	98.4	17,252		0.396	72,564	1.66
	7.90 8.00		176.1 176.9	99.2 100.0	17,472 17,693		0.401	74,300 76,059	1.706
	8.10		177.7	100.8	17,915		0.411	77,839	1.787
	8.20		178.5	101.6	18,138		0.416	79,642	1.828
	8.30 8.40		179.3 180.1	102.4 103.2	18,363 18,589		0.422	81,467 83,314	1.870
	8.50		180.9	104.0	18,817		0.432	85,185	1.95
	8.60 8.70		181.7 182.5	104.8 105.6	19,045 19,275		0.437 0.442	87,078 88,994	1.999 2.043
	8.80		183.3	106.4	19,506		0.448	90,933	2.088
	8.90 9.00		184.1 184.9	107.2	19,739 19,972		0.453 0.458	92,895 94,881	2.133
	9.00		184.9 185.7	108.0 108.8	20,207		0.458	94,881 96,890	2.178
	9.20		186.5	109.6	20,443		0.469	98,922	2.271
	9.30 9.40		187.3 188.1	110.4 111.2	20,681 20,920		0.475	100,978 103,058	2.318
			188.9	112.0	21,160			105,162	2.414

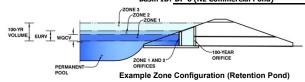
DF-6.xlsm, Basin 3/8/2021, 12:55 PM



DF-6.xlsm, Basin 38/2021, 12:55 PM

MHFD-Detention, Version 4.02 (February 2020)

#### **Project: Singer Ranch** Basin ID: DF-6 (NE Commercial Pond)



	Estillateu	Estillateu	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.75	0.242	Orifice Plate
Zone 2 (EURV)	4.82	0.453	Circular Orifice
Zone 3 (100-year)	5.96	0.322	Weir&Pipe (Restrict)
•	Total (all zones)	1.017	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = N/A inches

<u></u>	Calculated Parameters for Underdrain			
Underdrain Orifice Area =	N/A	ft <sup>2</sup>		
Underdrain Orifice Centroid =	N/A	feet		

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

ft (relative to basin bottom at Stage = 0 ft) Invert of Lowest Orifice = 0.00 Depth at top of Zone using Orifice Plate = 2.81 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 11.20 Orifice Plate: Orifice Area per Row = 0.85 sq. inches (diameter = 1 inch)

WO Orifice Area per Row 5.903E-03 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.94	1.87					
Orifice Area (sq. inches)	0.85	0.85	0.85					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	l
Invert of Vertical Orifice =	2.75	N/A	f
Depth at top of Zone using Vertical Orifice =	4.82	N/A	f
Vertical Orifice Diameter =	0.97	N/A	i

		Calculated Paramet	ers for Vertical Ori	fice
		Zone 2 Circular	Not Selected	
ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.01	N/A	ft <sup>2</sup>
ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.04	N/A	fee
inches				

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.82	N/A	ft (rel
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, g
Debris Clogging % =	50%	N/A	%
· ·			-

Height of Grate Upper Edge, H ft (relative to basin bottom at Stage = 0 ft) Overflow Weir Slope Length Grate Open Area / 100-yr Orifice Area Overflow Grate Open Area w/o Debris %, grate open area/total area Overflow Grate Open Area w/ Debris

	Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected				
H <sub>t</sub> =	4.82	N/A	feet			
h =	4.00	N/A	feet			
a =	13.42	N/A				
is =	16.80	N/A	ft <sup>2</sup>			
is =	8.40	N/A	ft <sup>2</sup>			
			-			

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Restrictor	Not Selected	
0.30	N/A	ft (dista
18.00	N/A	inches
12.00		inches
	Zone 3 Restrictor 0.30 18.00	0.30 N/A 18.00 N/A

ft (distance below basin bottom at Stage = 0 ft) inches

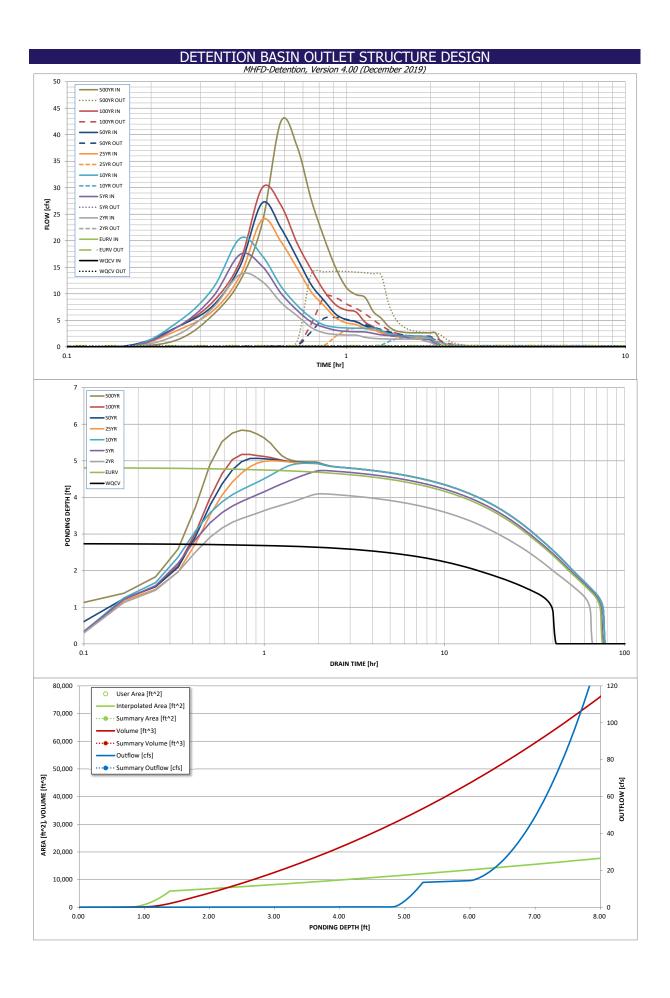
Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Outlet Orifice Area 1.25 N/A Outlet Orifice Centroid = 0.56 N/A eet Half-Central Angle of Restrictor Plate on Pipe = 1.91 N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= 6.00 ft (relative to basin bottom at Stage = 0 ft) Spillway Crest Length = 8.00 feet Spillway End Slopes 4.00 H:V Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway Spillway Design Flow Depth= 0.79 feet Stage at Top of Freeboard = feet 7.79 Basin Area at Top of Freeboard 0.40 acres Basin Volume at Top of Freeboard = 1.66 acre-ft

Routed Hydrograph Results	The year can ayer	rida tha dafault CIII	ID budua avanha and	www.aff.valumaa.hu		in the Inflant Under	assamba tabla (Cali		
Routed Hydrograph Results		ride the default CUH	, , ,					nns vv through AF)	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.242	0.695	0.544	0.703	0.831	0.961	1.091	1.232	1.765
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.544	0.703	0.831	0.961	1.091	1.232	1.765
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	3.0	4.6	7.8	9.7	12.1	20.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.17	0.47	0.71	1.20	1.49	1.87	3.11
Peak Inflow Q (cfs) =	N/A	N/A	13.7	17.4	20.4	24.0	27.1	30.0	42.5
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.2	2.0	3.5	5.5	9.3	14.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.1	0.4	0.4	0.6	0.8	0.7
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.2	0.3	0.5	0.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	61	69	70	69	68	67	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	64	73	74	74	74	73	72
Maximum Ponding Depth (ft) =	2.75	4.82	4.10	4.74	4.94	5.00	5.07	5.17	5.84
Area at Maximum Ponding Depth (acres) =	0.18	0.26	0.23	0.26	0.26	0.27	0.27	0.27	0.30
Maximum Volume Stored (acre-ft) =	0.244	0.696	0.517	0.673	0.725	0.741	0.759	0.789	0.979



MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

# Basin ID: DF-7 (NE Multi-Family Pond)

#### Watershed Information

100-YR EURV WQCV	ZONE 1
PERMANENT—POOL	ZONE 1 AND 2 ORIFICE ORIFICES  xample Zone Configuration (Retention Pond)

Cronca Information		
Selected BMP Type =	EDB	
Watershed Area =	18.00	acres
Watershed Length =	1,535	ft
Watershed Length to Centroid =	525	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	70.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Painfall Denths -	User Innut	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.413	acre-feet
Excess Urban Runoff Volume (EURV) =	1.384	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.222	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.648	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.007	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.432	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	2.808	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.256	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	4.847	acre-feet
Approximate 2-yr Detention Volume =	1.081	acre-feet
Approximate 5-yr Detention Volume =	1.441	acre-feet
Approximate 10-yr Detention Volume =	1.819	acre-feet
Approximate 25-yr Detention Volume =	1.954	acre-feet
Approximate 50-yr Detention Volume =	2.033	acre-feet
Approximate 100-yr Detention Volume =	2.178	acre-feet

Optional U	ser Override
	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3,55	inches

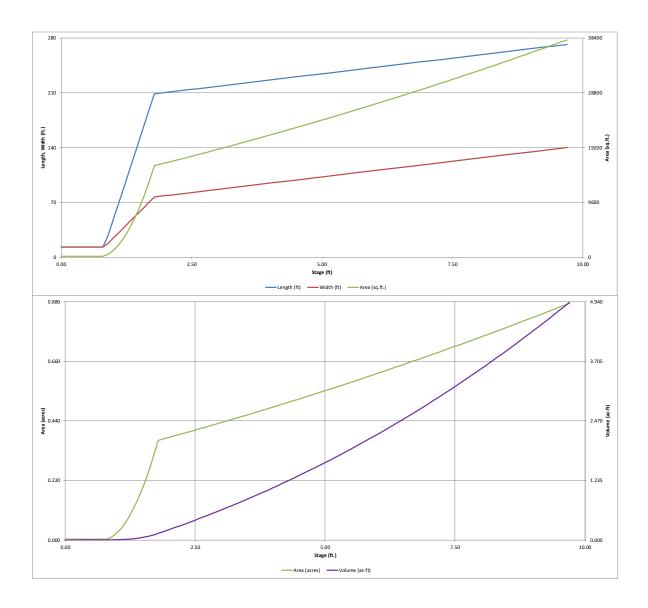
#### Define Zones and Basin Geometry

Chine Edited and Dabin Occinical		
Zone 1 Volume (WQCV) =	0.413	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.971	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.794	acre-feet
Total Detention Basin Volume =	2.178	acre-feet
Initial Surcharge Volume (ISV) =	54	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel $(S_{TC}) =$	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	3	

Calculated Total basin volume (v <sub>total</sub> ) =	2.179	acre-leet
Calculated Total Basin Volume (V <sub>total</sub> ) =	2.179	acre-feet
Volume of Main Basin (V <sub>MAIN</sub> ) =	89,096	ft <sup>3</sup>
Area of Main Basin $(A_{MAIN}) =$	26,765	ft <sup>2</sup>
Width of Main Basin $(W_{MAIN}) =$	110.5	ft
Length of Main Basin $(L_{MAIN}) =$	242.3	ft
Depth of Main Basin $(H_{MAIN}) =$	4.21	ft
Volume of Basin Floor $(V_{FLOOR}) =$	5,696	ft <sup>3</sup>
Area of Basin Floor $(A_{FLOOR}) =$	16,018	ft²
Width of Basin Floor $(W_{FLOOR}) =$	76.8	ft
Length of Basin Floor $(L_{FLOOR})$ =	208.6	ft
Depth of Basin Floor $(H_{FLOOR}) =$	0.96	ft
Surcharge Volume Width $(W_{ISV}) =$	12.8	ft
Surcharge Volume Length $(L_{ISV}) =$	12.8	ft
Initial Surcharge Area (A <sub>ISV</sub> ) =	163	ft²

	0.10	Optional				Optional		14.1	
Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft <sup>2</sup> )	Area (acre)	Volume (ft 3)	Volum (ac-ft
Top of Micropool	0.00	Stage (It)	12.8	12.8	163	Alca (IC)	0.004	(10)	(ac it
ISV	0.33		12.8	12.8	163		0.004	54	0.001
	0.40		12.8	12.8	163		0.004	65	0.002
	0.50		12.8	12.8	163		0.004	82	0.002
	0.60		12.8	12.8	163		0.004	98	0.002
	0.70		12.8	12.8	163		0.004	114	0.002
	0.80		12.8	12.8	163		0.004	131	0.003
	0.90		27.1	17.4	472		0.011	157	0.004
	1.00		47.5	24.1	1,145		0.026	236	0.005
	1.10		67.9	30.8	2,089		0.048	395	0.009
	1.20		88.3	37.4	3,305		0.076	662	0.015
	1.30		108.7	44.1	4,794		0.110	1,065	0.024
	1.40		129.1	50.8	6,554		0.150	1,630	0.037
	1.50		149.5	57.4	8,586		0.197	2,385	0.055
	1.60		169.9	64.1	10,891		0.250	3,357	0.077
	1.70		190.3	70.8	13,467		0.309	4,572	0.105
Floor	1.79		208.6	76.8	16,018		0.368	5,897	0.135
	1.80		208.7	76.9	16,041		0.368	6,058	0.139
	1.90		209.5	77.7	16,270		0.374	7,673	0.176
	2.00		210.3	78.5	16,501		0.379	9,312	0.214
	2.10		211.1	79.3	16,732		0.384	10,973	0.252
	2.20		211.9	80.1	16,965		0.389	12,658	0.291
	2.30		212.7	80.9	17,199		0.395	14,366	0.330
	2.40		213.5	81.7	17,435		0.400	16,098	0.370
	2.50		214.3	82.5	17,672		0.406	17,853	0.410
Zone 1 (WQCV)	2.51		214.4	82.5	17,695		0.406	18,030	0.414
-	2.60		215.1	83.3	17,910		0.411	19,633	0.451
	2.70		215.9	84.1	18,149		0.417	21,435	0.492
	2.80		216.7	84.9	18,390		0.422	23,262	0.534
	2.90		217.5	85.7	18,632		0.428	25,113	0.577
	3.00		218.3	86.5	18,875		0.433	26,989	0.620
	3.10		219.1	87.3	19,119		0.439	28,888	0.663
	3.20		219.9	88.1	19,365		0.445	30,813	0.707
	3.30		220.7	88.9	19,612		0.450	32,761	0.752
	3.40		221.5	89.7	19,860		0.456	34,735	0.797
	3.50		222.3	90.5	20,110		0.462	36,734	0.843
	3.60		223.1	91.3	20,361		0.467	38,757	0.890
	3.70		223.9	92.1	20,613		0.473	40,806	0.937
	3.80		224.7	92.9	20,866		0.479	42,880	0.984
	3.90		225.5	93.7	21,121		0.485	44,979	1.033
	4.00		226.3	94.5	21,377		0.491	47,104	1.081
	4.10		227.1	95.3	21,634		0.497	49,254	1.131
	4.20		227.9	96.1 96.9	21,893		0.503	51,431 53.633	1.181
	4.40		229.5	97.7	22,152 22,413		0.509	55,861	1.282
	4.50		230.3	98.5	22,676		0.513		1.334
Zono 2 (ELIBV)	4.60		231.1	99.3	22,676		0.521	58,116 60,396	1.387
Zone 2 (EURV)	4.70		231.1	100.1	23,204		0.527	62,704	1.439
	4.80		232.7	100.1	23,471		0.539	65,037	1.493
	4.90		233.5	100.9	23,738		0.539	67,398	1.547
	5.00		234.3 235.1	102.5 103.3	24,007		0.551	69,785	1.602
	5.20		235.9	103.3	24,277 24,548		0.564	72,199 74,640	1.714
	5.30		236.7	104.9	24,821		0.570	77,109	1.770
	5.40		237.5	105.7	25,095		0.576	79,605	1.827
	5.50		238.3	106.5	25,370		0.582	82,128	1.885
	5.60		239.1	107.3	25,646		0.589	84,679	1.944
	5.70		239.1	107.3	25,924		0.595	87,257	2.003
	5.80		240.7	108.9	26,203		0.602	89,864	2.063
3/400	5.90		241.5	109.7	26,483		0.608	92,498	2.123
one 3 (100-year)	5.99 6.00		242.2	110.4 110.5	26,737 26,765		0.614	94,893 95,160	2.178
	6.10		243.1	111.3	27,048		0.621	97,851	2.246
	6.20		243.9 244.7	112.1 112.9	27,332 27,617		0.627 0.634	100,570 103,317	2.309
	6.40		245.5	113.7	27,904		0.641	106,093	2.436
	6.50		246.3	114.5	28,192		0.647	108,898	2.500
	6.60 6.70		247.1 247.9	115.3 116.1	28,481 28,772		0.654	111,732 114,594	2.565 2.631
	6.80		248.7	116.9	29,064		0.667	117,486	2.697
	6.90 7.00		249.5 250.3	117.7 118.5	29,357 29,651		0.674	120,407 123,358	2.764 2.832
	7.10		251.1	119.3	29,947		0.687	126,338	2.900
	7.20		251.9	120.1	30,244		0.694	129,347	2.969
	7.30 7.40		252.7 253.5	120.9 121.7	30,542 30,841		0.701 0.708	132,386 135,455	3.039 3.110
	7.50		254.3	122.5	31,142		0.715	138,555	3.181
	7.60		255.1 255.9	123.3 124.1	31,444 31,748		0.722	141,684 144,844	3.253 3.325
	7.80		256.7	124.9	32,052		0.736	148,033	3.398
	7.90		257.5	125.7	32,358 32,665		0.743	151,254	3.472
	8.00 8.10		258.3 259.1	126.5 127.3	32,665 32,974		0.750 0.757	154,505 157,787	3.547 3.622
	8.20		259.9	128.1	33,283		0.764	161,100	3.698
	8.30 8.40		260.7 261.5	128.9 129.7	33,594 33,907		0.771 0.778	164,444	3.775 3.853
	8.50		262.3	130.5	34,220		0.786	167,819 171,225	3.931
	8.60		263.1	131.3	34,535		0.793	174,663	4.010
	8.70 8.80		263.9 264.7	132.1 132.9	34,851 35,169		0.800 0.807	178,132 181,633	4.089 4.170
	8.90		265.5	133.7	35,487		0.815	185,166	4.251
	9.00 9.10		266.3	134.5 135.3	35,807		0.822 0.829	188,731	4.333 4.415
	9.10		267.1 267.9	135.3 136.1	36,129 36,451		0.829	192,328 195,956	4.415
	9.30		268.7	136.9	36,775		0.844	199,618	4.583
					37,100		0.852	203,312	4.667
	9.40		269.5 270.3	137.7 138.5	37,426		0.859	207,038	4.753

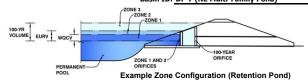
DF-7.xlsm, Basin 3/8/2021, 1:05 PM



DF-7.xkm, Basin 3/8/2021, 1.05 PM

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-7 (NE Multi-Family Pond)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.51	0.413	Orifice Plate
Zone 2 (EURV)	4.60	0.971	Circular Orifice
Zone 3 (100-year)	5.99	0.794	Weir&Pipe (Restrict)
•	Total (all zones)	2.178	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 2.51 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 10.00 inches

Orifice Plate: Orifice Area per Row = 1.34 sq. inches (diameter = 1-5/16 inches)

 MP)
 Calculated Parameters for Plate

 WQ Orifice Area per Row =
 9.306E-03
 ft²

 Elliptical Half-Width =
 N/A
 feet

 Elliptical Slot Centroid =
 N/A
 feet

 Elliptical Slot Area =
 N/A
 ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.84	1.67					
Orifice Area (sq. inches)	1.34	1.34	1.34					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.51	N/A	ft
Depth at top of Zone using Vertical Orifice =	4.60	N/A	ft
Vertical Orifice Diameter =	2.55	N/A	in

ft (relative to basin bottom at Stage = 0 ft)

Vertical O

inches

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

ipaci overnou iven (Broppost inci nac or	Diopea Grace and C	ratice i ipe on nece	
	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.60	N/A	ft
Overflow Weir Front Edge Length =	5.00	N/A	fe
Overflow Weir Grate Slope =	0.00	N/A	H
Horiz. Length of Weir Sides =	5.00	N/A	fe
Overflow Grate Open Area % =	70%	N/A	%
Debris Clogging % =	50%	N/A	%

ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H<sub>t</sub> = feet Overflow Weir Slope Length = H:V Grate Open Area / 100-yr Orifice Area = feet Overflow Grate Open Area w/o Debris = %, grate open area/total area Overflow Grate Open Area w/ Debris =

	Calculated Parameters for Overflow Weir						
	Zone 3 Weir	Not Selected					
l <sub>t</sub> =	4.60	N/A	feet				
h =	5.00	N/A	feet				
a =	10.07	N/A					
s =	17.50	N/A	ft <sup>2</sup>				
s =	8.75	N/A	ft <sup>2</sup>				
	•	•	-				

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.30	N/A
Outlet Pipe Diameter =	24.00	N/A
Restrictor Plate Height Above Pipe Invert =	13.00	

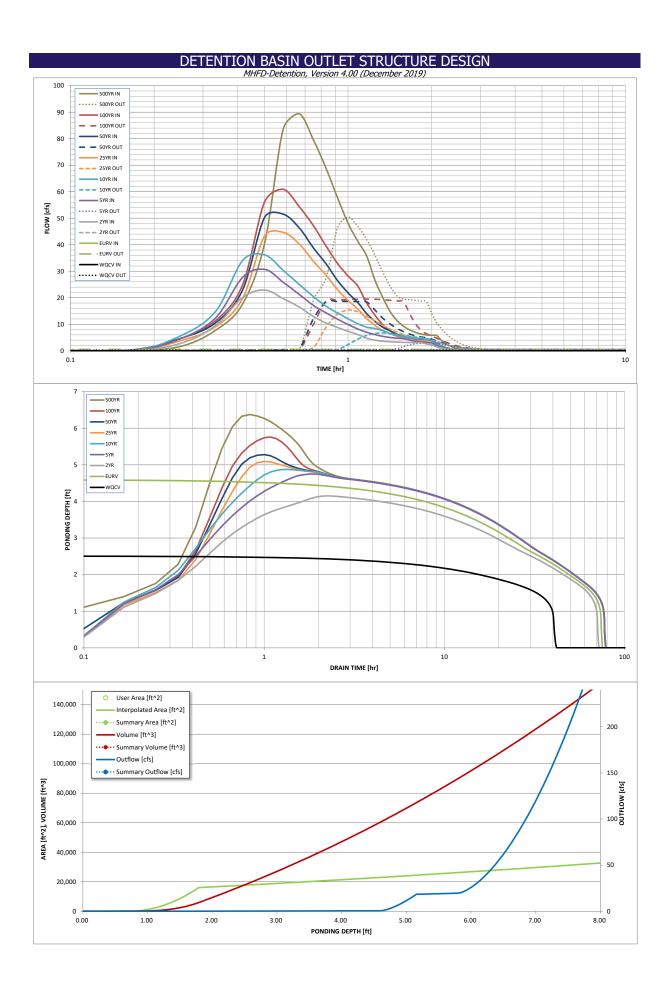
ft (distance below basin bottom at Stage = 0 ft) inches

inches

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= 5.80 ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = 21.00 feet
Spillway End Slopes = 4.00 H:V
Freeboard above Max Water Surface = 1.00 feet

Routed Hydrograph Results	The user can over	ride the default CUH	IP hydrographs and	runoff volumes by a	entering new values	in the Inflow Hydro	ngraphs table (Colui	nns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.413	1.384	1.222	1.648	2.007	2.432	2.808	3.256	4.847
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.222	1.648	2.007	2.432	2.808	3.256	4.847
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	2.1	5.9	8.9	15.7	19.7	24.8	41.3
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.33	0.49	0.87	1.10	1.38	2.29
Peak Inflow Q (cfs) =	N/A	N/A	22.9	30.7	36.2	44.7	51.6	60.9	89.4
Peak Outflow Q (cfs) =	0.2	0.5	0.5	3.0	6.7	15.3	18.6	19.5	50.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.8	1.0	0.9	0.8	1.2
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.3	0.8	1.0	1.1	1.1
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	65	70	69	67	66	64	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	69	75	74	74	73	72	70
Maximum Ponding Depth (ft) =	2.51	4.60	4.15	4.75	4.87	5.09	5.28	5.76	6.37
Area at Maximum Ponding Depth (acres) =	0.41	0.53	0.50	0.54	0.54	0.56	0.57	0.60	0.64
Maximum Volume Stored (acre-ft) =	0.414	1.387	1.151	1.461	1.531	1.646	1.753	2.033	2.416



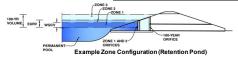
MHFD-Detention, Version 4.02 (February 2020)

#### Project: Singer Ranch

#### Basin ID: DF-8 (SE Single-Family & Commercial Pond)

acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches

2.25 inches 2.52 inches 3.55 inches



#### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	37.24	acres
Watershed Length =	2,040	ft
Watershed Length to Centroid =	925	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	70.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Lichap Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.						
Water Quality Capture Volume (WQCV) =	0.854	acre-feet				
Excess Urban Runoff Volume (EURV) =	2.863	acre-feet				
2-yr Runoff Volume (P1 = 1.19 in.) =	2.594	acre-feet				
5-yr Runoff Volume (P1 = 1.5 in.) =	3.498	acre-feet				
10-yr Runoff Volume (P1 = 1.75 in.) =	4.260	acre-feet				
25-yr Runoff Volume (P1 = 2 in.) =	5.161	acre-feet				
50-yr Runoff Volume (P1 = 2.25 in.) =	5.958	acre-feet				
100-yr Runoff Volume (P1 = 2.52 in.) =	6.907	acre-feet				
500-yr Runoff Volume (P1 = 3.55 in.) =	10.282	acre-feet				
Approximate 2-yr Detention Volume =	2.237	acre-feet				
Approximate 5-yr Detention Volume =	2.981	acre-feet				
Approximate 10-yr Detention Volume =	3.763	acre-feet				
Approximate 25-yr Detention Volume =	4.043	acre-feet				
Approximate 50-yr Detention Volume =	4.206	acre-feet				
Approximate 100-yr Detention Volume =	4.505	acre-feet				
		-				

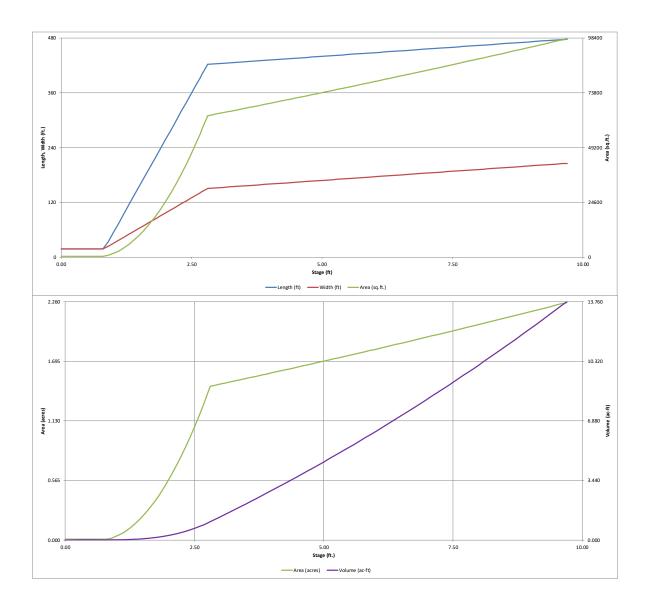
#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.854	acre-fee
Zone 2 Volume (EURV - Zone 1) =	2.009	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	1.642	acre-fee
Total Detention Basin Volume =	4.505	acre-fee
Initial Surcharge Volume (ISV) =	112	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (Htotal) =	5.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel $(S_{TC}) =$	0.005	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	3	

Initial Surcharge Area $(A_{ISV}) =$	338	ft <sup>2</sup>
Surcharge Volume Length ( $L_{ISV}$ ) =	18.4	ft
Surcharge Volume Width $(W_{ISV}) =$	18.4	ft
Depth of Basin Floor $(H_{FLOOR})$ =	1.98	ft
Length of Basin Floor $(L_{FLOOR})$ =	422.3	ft
Width of Basin Floor $(W_{FLOOR}) =$	150.4	ft
Area of Basin Floor $(A_{FLOOR})$ =	63,508	ft <sup>2</sup>
Volume of Basin Floor $(V_{FLOOR}) =$	45,196	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	2.19	ft
Length of Main Basin $(L_{MAIN}) =$	439.8	ft
Width of Main Basin ( $W_{MAIN}$ ) =	167.9	ft
Area of Main Basin $(A_{MAIN}) =$	73,849	ft²
Volume of Main Basin $(V_{MAIN}) =$	150,263	ft <sup>3</sup>
Calculated Total Basin Volume $(V_{total}) =$	4.494	acre-feet

Depth Increment =	0.10	ft							
Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool	0.00		18.4	18.4	338		0.008		
ISV	0.33		18.4	18.4	338		0.008	112	0.003
	0.40		18.4	18.4	338		0.008	135	0.003
	0.50		18.4	18.4	338		0.008	169	0.004
	0.60		18.4	18.4	338		0.008	203	0.005
	0.70		18.4	18.4	338		0.008	237	0.005
	0.80		18.4	18.4	338		0.008	270	0.006
	0.90		32.7	23.1	753		0.017	318	0.007
	1.00		53.1	29.7	1,577		0.036	432	0.010
	1.10		73.5 93.9	36.4 43.1	2,673		0.061	642 976	0.015
					4,041				
	1.30		114.3 134.7	49.7 56.4	5,681 7,593		0.130 0.174	1,460	0.034
	1.50		155.1	63.1	9,777		0.174	2,121	0.049
	1.60		175.5	69.7	12,233		0.281	4,086	0.003
	1.70		195.9	76.4	14,961		0.343	5,443	0.125
	1.80		216.3	83.1	17,961		0.412	7,087	0.163
	1.90		236.7	89.7	21,233		0.487	9,044	0.208
	2.00		257.1	96.4	24,777		0.569	11,342	0.260
	2.10		277.5	103.1	28,593		0.656	14,009	0.322
	2.20		297.9	109.7	32,681		0.750	17,070	0.392
	2.30		318.3	116.4	37,041		0.850	20,554	0.472
	2.40		338.7	123.1	41,673		0.957	24,487	0.562
	2.50		359.1	129.7	46,577		1.069	28,898	0.663
	2.60		379.5	136.4	51,753		1.188	33,812	0.776
Zone 1 (WQCV)	2.67		393.7	141.1	55,538		1.275	37,566	0.862
	2.70		399.9	143.1	57,201		1.313	39,257	0.901
Ele	2.80		420.3	149.7	62,921		1.444	45,261 45,902	1.039
Floor	2.81		422.3 423.0	150.4 151.1	63,508 63,921		1.458	45,893 51,628	1.054
	3.00		423.8	151.1	64,381		1.467	58,043	1.332
	3.10		424.6	152.7	64,842		1.489	64,504	1.481
	3.20		425.4	153.5	65,305		1.499	71,011	1.630
	3.30		426.2	154.3	65,768		1.510	77,565	1.781
	3.40		427.0	155.1	66,233		1.521	84,165	1.932
	3.50		427.8	155.9	66,700		1.531	90,812	2.085
	3.60		428.6	156.7	67,167		1.542	97,505	2.238
	3.70		429.4	157.5	67,636		1.553	104,245	2.393
	3.80		430.2	158.3	68,106		1.564	111,032	2.549
	3.90		431.0	159.1	68,578		1.574	117,866	2.706
Zone 2 (EURV)	4.00		431.8	159.9	69,051		1.585	124,748	2.864
	4.10		432.6	160.7	69,525		1.596	131,677	3.023
	4.20		433.4 434.2	161.5 162.3	70,000		1.607	138,653	3.183
	4.40		435.0	163.1	70,477		1.629	145,677 152,748	3.507
	4.50		435.8	163.9	71,434		1.640	159,868	3.670
	4.60		436.6	164.7	71,914		1.651	167.035	3.835
	4.70		437.4	165.5	72,396		1.662	174,250	4.000
	4.80		438.2	166.3	72,879		1.673	181,514	4.167
	4.90		439.0	167.1	73,363		1.684	188,826	4.335
	5.00		439.8	167.9	73,849		1.695	196,187	4.504
Zone 3 (100-year)	5.01		439.9	168.0	73,897		1.696	196,925	4.521
	5.10		440.6	168.7	74,335		1.707	203,596	4.674
	5.20		441.4	169.5	74,823		1.718	211,054	4.845
	5.30		442.2	170.3	75,313		1.729	218,561	5.017
	5.50		443.0 443.8	171.1 171.9	75,803 76,295		1.740	226,116	5.191
	5.60		444.6	172.7	76,789		1.763	241,376	5.541
	5.70		445.4	173.5	77,283		1.774	249,079	5.718
	5.80 5.90		446.2 447.0	174.3 175.1	77,779 78,276		1.786 1.797	256,832 264,635	5.896 6.075
	6.00		447.8	175.9	78,774		1.808	272,488	6.255
	6.10		448.6 449.4	176.7 177.5	79,274 79,775		1.820 1.831	280,390 288,342	6.437 6.619
	6.30		450.2	178.3	80,277		1.843	296,345	6.803
	6.40 6.50		451.0 451.8	179.1 179.9	80,781 81,285		1.854 1.866	304,398 312,501	6.988 7.174
	6.60		452.6	180.7	81,791		1.878	320.655	7.361
	6.70 6.80		453.4 454.2	181.5 182.3	82,299 82,807		1.889 1.901	328,859 337,115	7.550 7.739
	6.90		455.0	183.1	83,317		1.913	345,421	7.930
	7.00 7.10		455.8 456.6	183.9 184.7	83,828 84,341		1.924 1.936	353,778 362,187	8.122 8.315
	7.20		457.4	185.5	84,854		1.948	370,646	8.509
	7.30 7.40		458.2 459.0	186.3 187.1	85,369 85,886		1.960 1.972	379,157 387,720	8.704 8.901
	7.50		459.8	187.9	86,403		1.984	396,335	9.099
	7.60 7.70		460.6 461.4	188.7 189.5	86,922 87,442		1.995 2.007	405,001 413,719	9.298 9.498
	7.80		462.2	190.3	87,963		2.019	422,489	9.699
	7.90		463.0	191.1 191.9	88,486		2.031	431,312	9.902
	8.00 8.10		463.8 464.6	192.7	89,010 89,535		2.043 2.055	440,187 449,114	10.105 10.310
	8.20		465.4	193.5	90,062		2.068	458,094	10.516
	8.30 8.40		466.2 467.0	194.3 195.1	90,590 91,119		2.080 2.092	467,126 476,212	10.724 10.932
	8.50		467.8	195.9	91,649		2.104	485,350	11.142
	8.60 8.70		468.6 469.4	196.7 197.5	92,181 92,713		2.116 2.128	494,541 503,786	11.353 11.565
	8.80		470.2	198.3	93,248		2.141	513,084	11.779
	8.90		471.0	199.1 199.9	93,783 94,320		2.153 2.165	522,436 531,841	11.993 12.209
					J-1,J2U		4.103		12.209
	9.00 9.10		471.8 472.6	200.7	94,858		2.178	541,300	
	9.00 9.10 9.20		472.6 473.4	200.7 201.5	95,397		2.190	550,812	12.645
	9.00 9.10 9.20 9.30 9.40		472.6 473.4 474.2 475.0	200.7 201.5 202.3 203.1	95,397 95,938 96,480		2.190 2.202 2.215	550,812 560,379 570,000	12.645 12.865 13.085
	9.00 9.10 9.20 9.30		472.6 473.4 474.2	200.7 201.5 202.3	95,397 95,938		2.190 2.202	550,812 560,379	12.645 12.865

DF-8.x/sm, Basin 3/8/2021, 4:53 PM

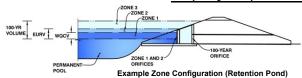


DF-8.xkm, Basin 3/8/2021, 4:53 PM

MHFD-Detention, Version 4.02 (February 2020)

**Project: Singer Ranch** 

Basin ID: DF-8 (SE Single-Family & Commercial Pond)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.67	0.854	Orifice Plate
Zone 2 (EURV)	4.00	2.009	Circular Orifice
Zone 3 (100-year)	5.01	1.642	Weir&Pipe (Restrict)
•	Total (all zones)	4.505	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain Underdrain Orifice Area N/A Underdrain Orifice Centroid = feet N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = 2.66 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 10.60 Orifice Plate: Orifice Area per Row = 2.56 sg. inches (diameter = 1-13/16 inches)

WQ Orifice Area per Row = 1.778E-02 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) 0.00 0.89 1.77 Orifice Area (sq. inches) 2 56 2.56 2.56

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.67	N/A	ft (relat
Depth at top of Zone using Vertical Orifice =	4.00	N/A	ft (relat
Vertical Orifice Diameter =	5.27	N/A	inches

Calculated Parameters for Vertical Orifice Zone 2 Circular Not Selected (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area 0.15 N/A (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = 0.22 N/A

Bas

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

		Zone 3 Weir	Not Selected	
٥١	erflow Weir Front Edge Height, Ho =	4.00	N/A	ft (relative to basin bottom at Stage = 0
	Overflow Weir Front Edge Length =	6.00	N/A	feet
	Overflow Weir Grate Slope =	0.00	N/A	H:V (
	Horiz. Length of Weir Sides =	6.00	N/A	feet (
	Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
	Debris Clogging % =	50%	N/A	%
				=

utlet Pi	pe)	Calculated Parameters for Overflow Weir			
		Zone 3 Weir	Not Selected		
0 ft)	Height of Grate Upper Edge, $H_{\rm t}$ =	4.00	N/A	feet	
	Overflow Weir Slope Length =	6.00	N/A	feet	
Grate	Open Area / 100-yr Orifice Area =	5.63	N/A		
Overf	low Grate Open Area w/o Debris =	25.20	N/A	ft <sup>2</sup>	
Ove	rflow Grate Open Area w/ Debris =	12.60	N/A	ft <sup>2</sup>	
				_	

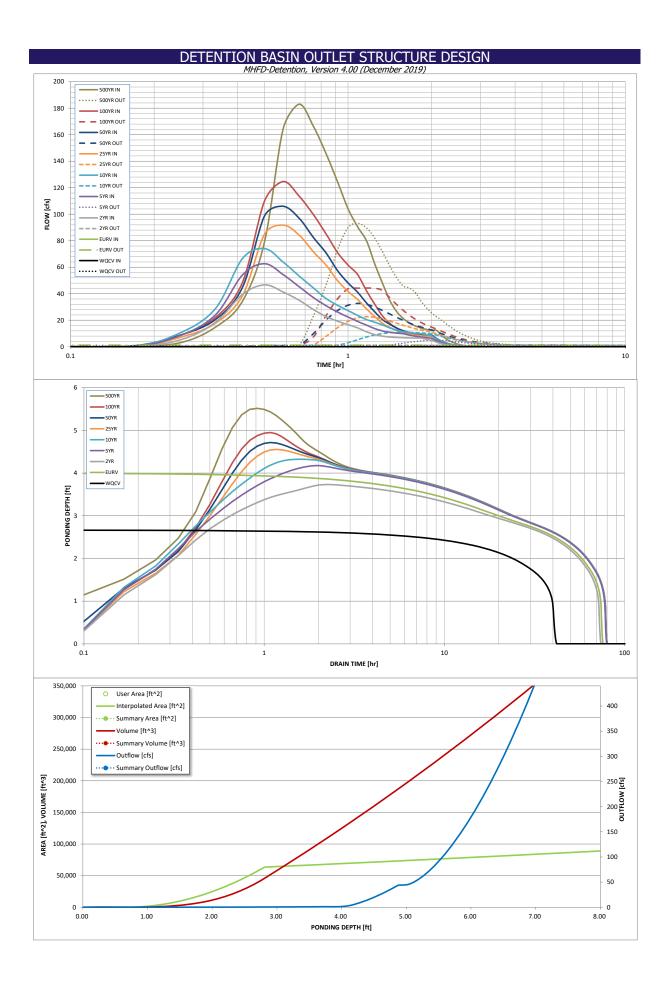
er Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)			Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate				
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	4.48	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	36.00	N/A	inches	Outlet Orifice Centroid =	1.03	N/A	feet
Restrictor Plate Height Above Pipe Invert =	21.80		inches Half-Central Angle of	Restrictor Plate on Pipe =	1.78	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	5.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	40.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

	Calculated Paramet	ers for Spillway
Spillway Design Flow Depth=		feet
Stage at Top of Freeboard =	6.95	feet
Basin Area at Top of Freeboard =	1.92	acres
sin Volume at Top of Freeboard =	8.03	acre-ft

Routed Hydrograph Results	The user can overr	ide the default CUH	IP hydrographs and	runoff volumes by e	entering new values	in the Inflow Hydro	ngraphs table (Colum	nns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.854	2.863	2.594	3.498	4.260	5.161	5.958	6.907	10.282
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.594	3.498	4.260	5.161	5.958	6.907	10.282
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.1	11.3	17.1	30.8	38.6	49.3	81.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.11	0.30	0.46	0.83	1.04	1.32	2.20
Peak Inflow Q (cfs) =	N/A	N/A	46.6	62.6	74.1	91.8	106.0	124.6	183.0
Peak Outflow Q (cfs) =	0.3	1.2	1.1	5.0	10.8	22.7	32.7	44.3	93.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.8	0.9	1.1
Structure Controlling Flow =	Vertical Orifice 1	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.2	1.7	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	70	69	68	66	65	60
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	75	75	74	74	73	71
Maximum Ponding Depth (ft) =	2.67	4.00	3.73	4.17	4.32	4.55	4.71	4.95	5.51
Area at Maximum Ponding Depth (acres) =	1.27	1.59	1.55	1.60	1.62	1.65	1.66	1.69	1.75
Maximum Volume Stored (acre-ft) =	0.862	2.864	2.424	3.135	3.377	3.752	4.017	4.402	5.383



### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.02 (February 2020)

### Project: Singer Ranch

## Basin ID: DF-9 (SE Commercial Pond)

### Watershed Information

100-YR VOLUME EURV WQCV	ZONE 1	
PERMANENT——POOL	ZONE 1 AND 2 ORIFICES  Example Zone Configura	100-YEAR ORIFICE

Selected BMP Type =	EDB	
Watershed Area =	35.45	acres
Watershed Length =	1,960	ft
Watershed Length to Centroid =	730	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	80.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Liban Hydrograph Procedure

the embedded Colorado Urban Hydro	ıgraph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.970	acre-feet
Excess Urban Runoff Volume (EURV) =	3.148	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	2.780	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	3.677	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	4.421	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	5.244	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	6.012	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	6.889	acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	10.097	acre-feet
Approximate 2-yr Detention Volume =	2.494	acre-feet
Approximate 5-yr Detention Volume =	3.286	acre-feet
Approximate 10-yr Detention Volume =	4.080	acre-feet
Approximate 25-yr Detention Volume =	4.373	acre-feet
Approximate 50-yr Detention Volume =	4.542	acre-feet
Approximate 100-yr Detention Volume =	4.786	acre-feet
		-

Optional User	r Overrides
	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.55	inches

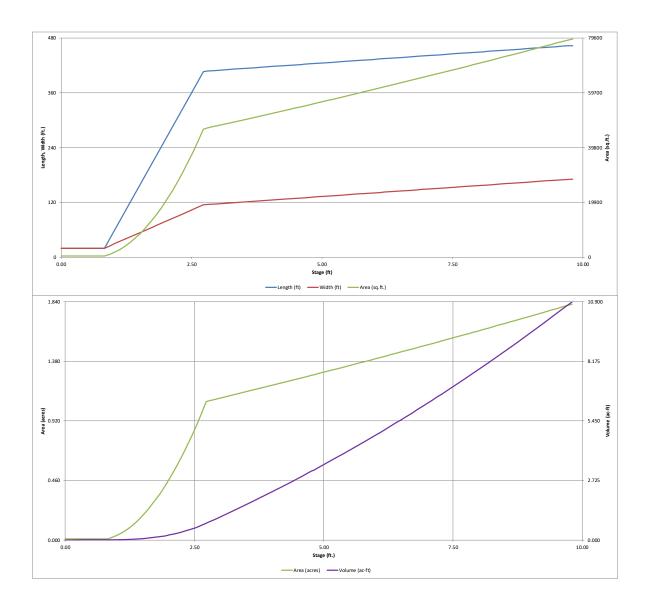
### Define Zones and Basin Geometry

ACTIFIC ZOTICS WITH DUSITI OCOTICETY		
Zone 1 Volume (WQCV) =	0.970	acre-fee
Zone 2 Volume (EURV - Zone 1) =	2.178	acre-fee
Zone 3 Volume (100-year - Zones 1 & 2) =	1.638	acre-fee
Total Detention Basin Volume =	4.786	acre-fee
Initial Surcharge Volume (ISV) =	127	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (Htotal) =	6.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel $(S_{TC}) =$	0.005	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	4	

carcarated rotal basin volume (violal)	4.773	Jucie icce
Calculated Total Basin Volume (Vtotal) =	4.773	acre-feet
Volume of Main Basin (V <sub>MAIN</sub> ) =	175,165	ft <sup>3</sup>
Area of Main Basin $(A_{MAIN}) =$	60,934	ft <sup>2</sup>
Width of Main Basin $(W_{MAIN}) =$	140.6	ft
Length of Main Basin $(L_{MAIN}) =$	433.2	ft
Depth of Main Basin $(H_{MAIN}) =$	3.27	ft
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	32,434	ft <sup>3</sup>
Area of Basin Floor $(A_{FLOOR}) =$	46,618	ft <sup>2</sup>
Width of Basin Floor $(W_{FLOOR}) =$	114.5	ft
Length of Basin Floor $(L_{FLOOR}) =$	407.1	ft
Depth of Basin Floor $(H_{FLOOR}) =$	1.90	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	19.5	ft
Surcharge Volume Length $(L_{ISV}) =$	19.5	ft
Initial Surcharge Area $(A_{ISV}) =$	381	ft 2

0.10	ft			1	Ontional			
Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
(ft)	Stage (ft)	(ft)	(ft)		Area (ft 2)	(acre)	(ft <sup>3</sup> )	(ac-ft)
							126	0.003
								0.003
								0.005
0.63		19.5	19.5	381		0.009	240	0.006
0.73		19.5	19.5	381		0.009	278	0.006
0.83		19.5	19.5	381		0.009	316	0.007
								0.009
								0.012
1.23		100.5						0.025
1.33		120.9	44.4	5,363		0.123	1,536	0.035
1.43		141.3	49.4	6,974		0.160	2,151	0.049
1.53		161.7	54.4	8,790		0.202	2,937	0.067
								0.090 0.117
			69.4					0.150
1.93		243.3	74.4	18,092		0.415	8,205	0.188
2.03		263.7	79.4	20,927		0.480	10,154	0.233
2.13		284.1	84.4	23,966		0.550	12,397	0.285
								0.343
			_					0.410
2.53		365.7	104.4	38,164		0.876	24,714	0.567
2.63		386.1	109.4	42,223		0.969	28,732	0.660
2.73		406.5	114.4	46,487		1.067	33,166	0.761
								0.836
		- ' '						0.945
3.00		409.2	116.6	47,737		1.009	45,901	1.054
3.10		410.0	117.4	48,158		1.106	50,696	1.164
3.20		410.8	118.2	48,581		1.115	55,533	1.275
3.30				49,005		1.125	60,412	1.387
								1.500 1.614
3.60								1.729
3.70		414.8	122.2	50,713		1.164	80,355	1.845
3.80		415.6	123.0	51,143		1.174	85,448	1.962
3.90		416.4	123.8	51,575		1.184	90,584	2.080
								2.198 2.318
								2.439
4.30		419.6	127.0			1.224		2.561
4.40		420.4	127.8	53,752		1.234	116,914	2.684
4.50		421.2	128.6	54,191		1.244	122,311	2.808
								2.933
								3.059 3.160
4.80		423.6				1.274		3.186
4.90		424.4	131.8	55,961		1.285	144,341	3.314
5.00		425.2	132.6	56,407		1.295	149,960	3.443
5.10		426.0	133.4	56,854		1.305	155,623	3.573
								3.704 3.836
								3.969
5.50		429.2	136.6	58,655		1.347	178,724	4.103
5.60		430.0	137.4	59,108		1.357	184,612	4.238
5.70		430.8	138.2	59,563		1.367	190,545	4.374
5.90		432.4	139.8	60,476		1.388	202,549	4.512 4.650
6.00 6.10		433.2 434.0	140.6 141.4	60,934 61,394		1.399	208,619 214,736	4.789 4.930
6.20		434.8	142.2	61,855		1.420	220,898	5.071
6.30 6.40		436.4	143.0 143.8	62,317 62,781		1.441	227,107 233,362	5.214 5.357
6.50		437.2	144.6	63,246		1.452	239,663	5.502 5.648
6.70		438.8	146.2	64,179		1.473	252,405	5.794
6.90		440.4	147.8	65,118		1.495	265,335	5.942 6.091
7.00		441.2	148.6	65,589		1.506	271,870	6.241 6.392
7.20		442.8	150.2	66,536		1.527	285,083	6.545
			151.0 151.8	67,011 67,487				6.698 6.852
7.50		445.2	152.6	67,965		1.560	305,258	7.008 7.164
7.70		446.8	154.2	68,924		1.582	318,946	7.322
7.80 7.90		447.6 448.4	155.0 155.8	69,405		1.593	325,863	7.481 7.641
8.00		449.2	156.6	70,372		1.616	339,840	7.802
8.20		450.8	158.2	71,344		1.638	354,012	7.964 8.127
8.30 8.40		451.6 452.4	159.0 159.8	71,832		1.649	361,171	8.291 8.457
8.50		453.2	160.6	72,812		1.672	375,635	8.623
8.60 8.70		454.0 454.8	161.4 162.2	73,304		1.683 1.694	382,941	8.791 8.960
8.80		455.6	163.0	74,291		1.705	397,700	9.130
9.00		457.2	164.6	75,283		1.728	412,658	9.301 9.473
9.10 9.20		458.0 458.8	165.4 166.2	75,782		1.740 1.751	420,211	9.647 9.821
9.30 9.40		459.6	167.0	76,782		1.763	435,467	9.997
		460.4	167.8	77,284		1.774	443,171	10.174
9.50 9.60		461.2 462.0	168.6 169.4	77,787 78,292		1.786 1.797	450,924 458,728	10.352
	(r) 0.00 0.03 0.43 0.43 0.43 0.53 0.63 0.73 0.88 0.93 1.13 1.23 1.23 1.33 1.43 1.53 1.43 1.53 1.73 1.83 1.83 1.83 1.83 1.83 1.83 1.83 1.8	Stage (R)   Cherrical Stage (R)   Cherrica	Stage (R)         Override (Sage (R)         Length (th)           0.00         19.5           0.33         19.5           0.43         19.5           0.63         19.5           0.63         19.5           0.77         19.5           0.83         19.5           0.93         39.3           1.03         59.7           1.13         80.1           1.23         100.5           1.33         120.9           1.43         141.3           1.53         161.7           1.63         182.1           1.73         202.5           1.83         222.9           1.93         243.3           1.93         243.3           2.03         263.7           2.13         284.1           2.23         304.5           2.33         324.9           2.43         345.3           2.53         365.7           2.80         407.6           2.90         408.4           2.93         408.7           3.00         409.2           2.93         408.4           2.	Stage (R)   Common   Length (R) (R)	Stage   Override   Chep   Ch	Sage (ft) (ft)   Length (ft)   Width   Area (ft)	Sage (R)   Sage (R)   (R)   Width   Area (R)   Area (	Sage (b)   Compt   C

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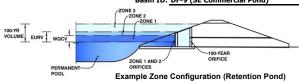


DF-9.xkm, Basin 3/8/2021, 2:21 PM

### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

### Project: Singer Ranch Basin ID: DF-9 (SE Commercial Pond)



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.93	0.970	Orifice Plate
Zone 2 (EURV)	4.78	2.178	Circular Orifice
Zone 3 (100-year)	6.00	1.638	Weir&Pipe (Restrict)
-	Total (all zones)	4.786	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = N/A inches

	Calculated Parameters for Underdrain					
Underdrain Orifice Area =	N/A	ft <sup>2</sup>				
Underdrain Orifice Centroid =	N/A	feet				

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) 2.91 Orifice Plate: Orifice Vertical Spacing = 11.60 2.84 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-7/8 inches)

WQ Orifice Area per Row 1.972E-02 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet N/A Elliptical Slot Area =

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.97	1.94					
Orifice Area (sq. inches)	2.84	2.84	2.84					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

3 N/A	ft (re
8 N/A	ft (re
3 N/A	inch
	8 N/A

		Calculated Parameters for Vertical O					
		Zone 2 Circular	Not Selected				
ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.10	N/A	ft <sup>2</sup>			
ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.18	N/A	feet			
inches	·						

User In

input: Overflow Weir (Dropbox with Flat or	Calculated Parame	Calculated Parameters for Overflow Wei				
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.78	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H	t = 4.78	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet Overflow Weir Slope Length	n = 6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area	1 = 5.89	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet Overflow Grate Open Area w/o Debris	5 = 25.20	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Overflow Grate Open Area w/ Debris	s = 12.60	N/A	ft²
Debris Clogging % =	50%	N/A	%			_

User Input: Outle

utlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re:	<u>strictor Plate, or Re</u>	ctangular Orifice)	Calculated Parameter	s for Outlet Pipe w/	Flow Restriction Pla	<u>ate</u>
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	1
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	4.28	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	36.00	N/A	inches	Outlet Orifice Centroid =	1.00	N/A	feet
or Plate Height Above Pipe Invert =	21.00		inches Half-Central Angle of	f Restrictor Plate on Pipe =	1.74	N/A	radians

Bas

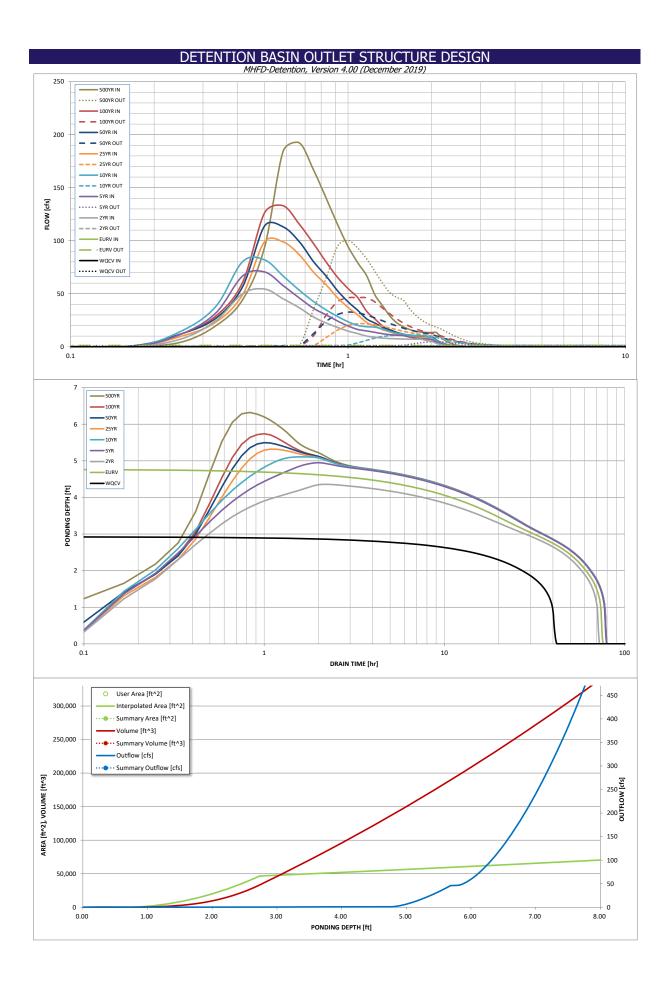
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Restrictor

Spillway Invert Stage=	5.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	44.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

	Calculated Paramet	ters for Spillway
Spillway Design Flow Depth=	0.96	feet
Stage at Top of Freeboard =	7.76	feet
Basin Area at Top of Freeboard =	1.59	acres
sin Volume at Top of Freeboard =	7.42	acre-ft

Routed Hydrograph Results	The user can over	ride the default CUH	IP hydrographs and	runoff volumes by e	entering new values	in the Inflow Hydro	ographs table (Colur	nns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.970	3.148	2.780	3.677	4.421	5.244	6.012	6.889	10.097
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.780	3.677	4.421	5.244	6.012	6.889	10.097
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.2	11.9	18.0	31.7	39.8	50.4	83.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.34	0.51	0.89	1.12	1.42	2.36
Peak Inflow Q (cfs) =	N/A	N/A	54.4	70.6	81.9	99.0	113.8	133.0	192.4
Peak Outflow Q (cfs) =	0.4	1.2	1.0	4.8	10.9	21.7	32.7	46.3	100.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.8	0.9	1.2
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.3	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	65	71	70	68	67	66	61
Time to Drain 99% of Inflow Volume (hours) =	40	72	69	75	75	74	74	73	72
Maximum Ponding Depth (ft) =	2.93	4.78	4.36	4.95	5.11	5.32	5.50	5.74	6.32
Area at Maximum Ponding Depth (acres) =		1.27	1.23	1.29	1.31	1.33	1.35	1.37	1.43
Maximum Volume Stored (acre-ft) =	0.977	3.160	2.622	3.365	3.573	3.849	4.089	4.415	5.242



## <u>APPENDIX B</u> Standard Design Charts and Tables

Chapter 6 Hydrology

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent						Runoff Co	efficients						
Characteristics	Impervious	2-year		5-year		10-year		25-	/ear	50-year		100-	100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	
Business														
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89	
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68	
Residential														
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65	
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58	
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57	
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56	
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55	
Industrial														
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74	
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52	
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54	
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58	
Undeveloped Areas														
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51	
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59	
landuse is undefined)		0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59	
Streets														
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74	
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	

### 3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration  $(t_c)$  consists of an initial time or overland flow time  $(t_i)$  plus the travel time  $(t_i)$  in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time  $(t_i)$  plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion  $(t_i)$  of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Hydrology Chapter 6

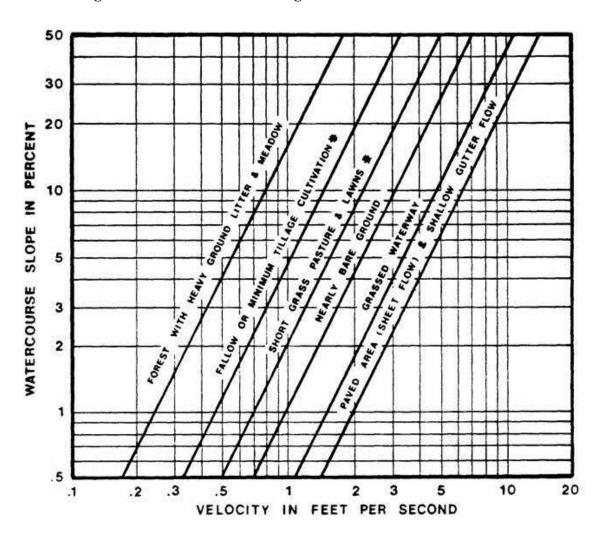
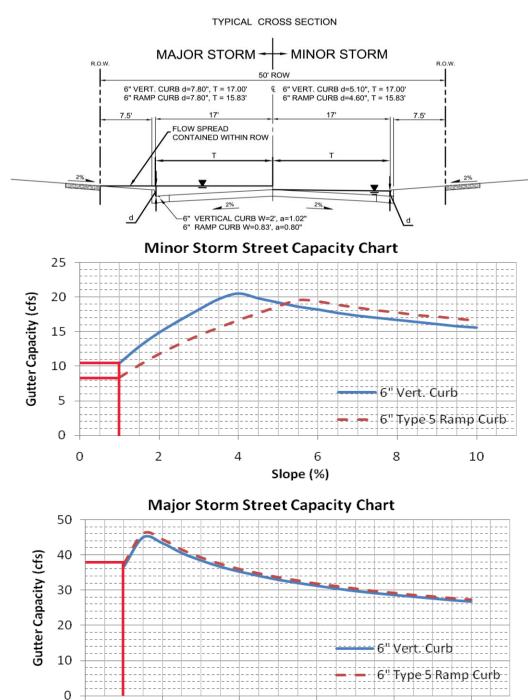


Figure 6-25. Estimate of Average Concentrated Shallow Flow

Chapter 7 Street Drainage

Figure 7-7. Street Capacity Charts Residential (Detached Sidewalk)



These charts shall only be used for the standard street sections as shown. The capacity shown is based on ½ the street section as calculated by the UD-Inlet spreadsheets. Minor storm capacities are based on no crown overtopping, curb height or maximum allowable spread widths. Major storm capacities are based on flow being containing within the public right-of-way, including conveyance capacity behind the curb. The UDFCD Safety Reduction Factor was applied. An 'nstreet' of 0.016 and 'nback' of 0.020 was used. Calculations were done using UD-Inlet 3.00.xls, March, 2011.

Slope (%)

4

8

10

2

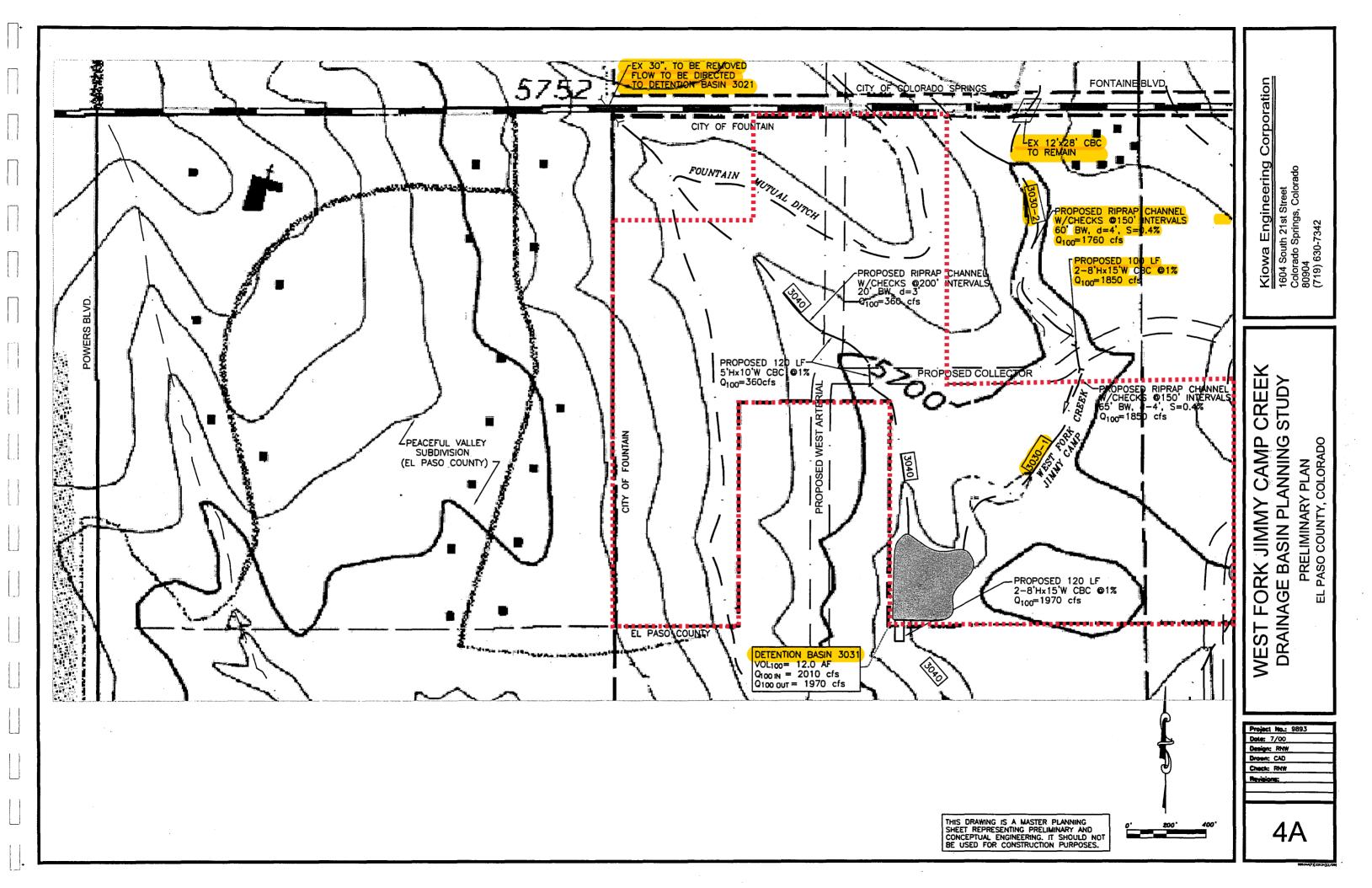
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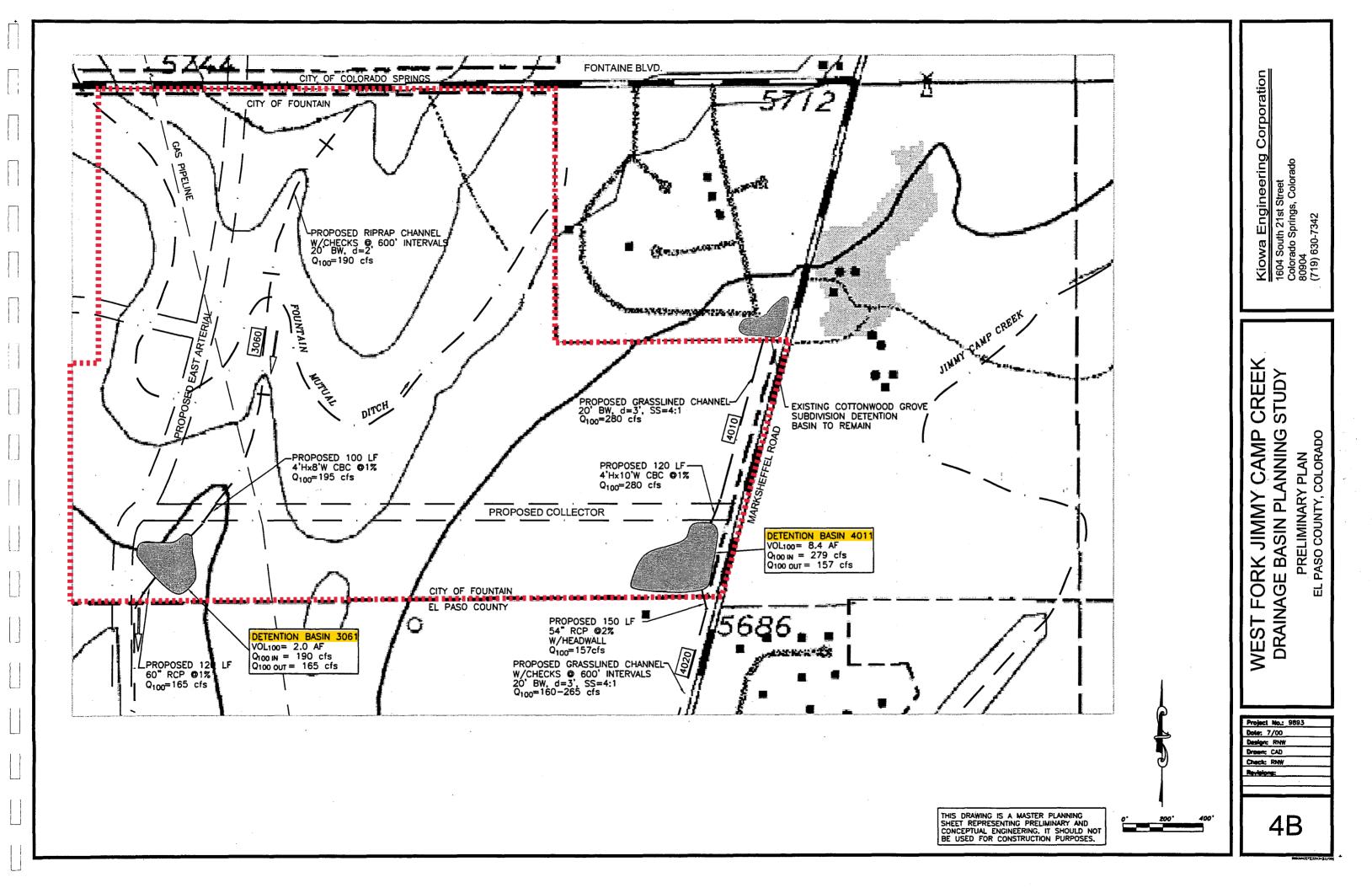
Runoff Chapter 6

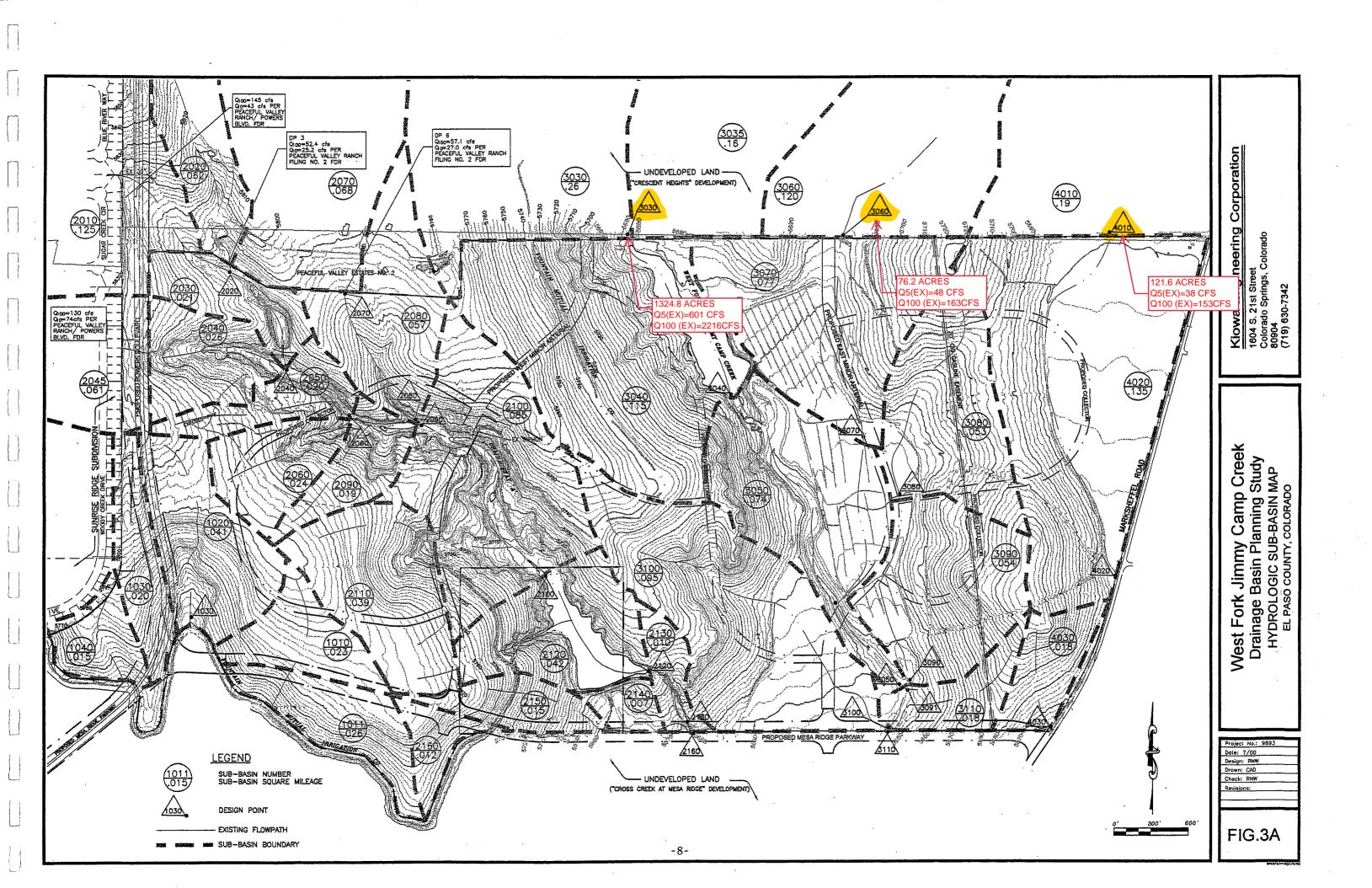
Table 6-3. Recommended percentage imperviousness values

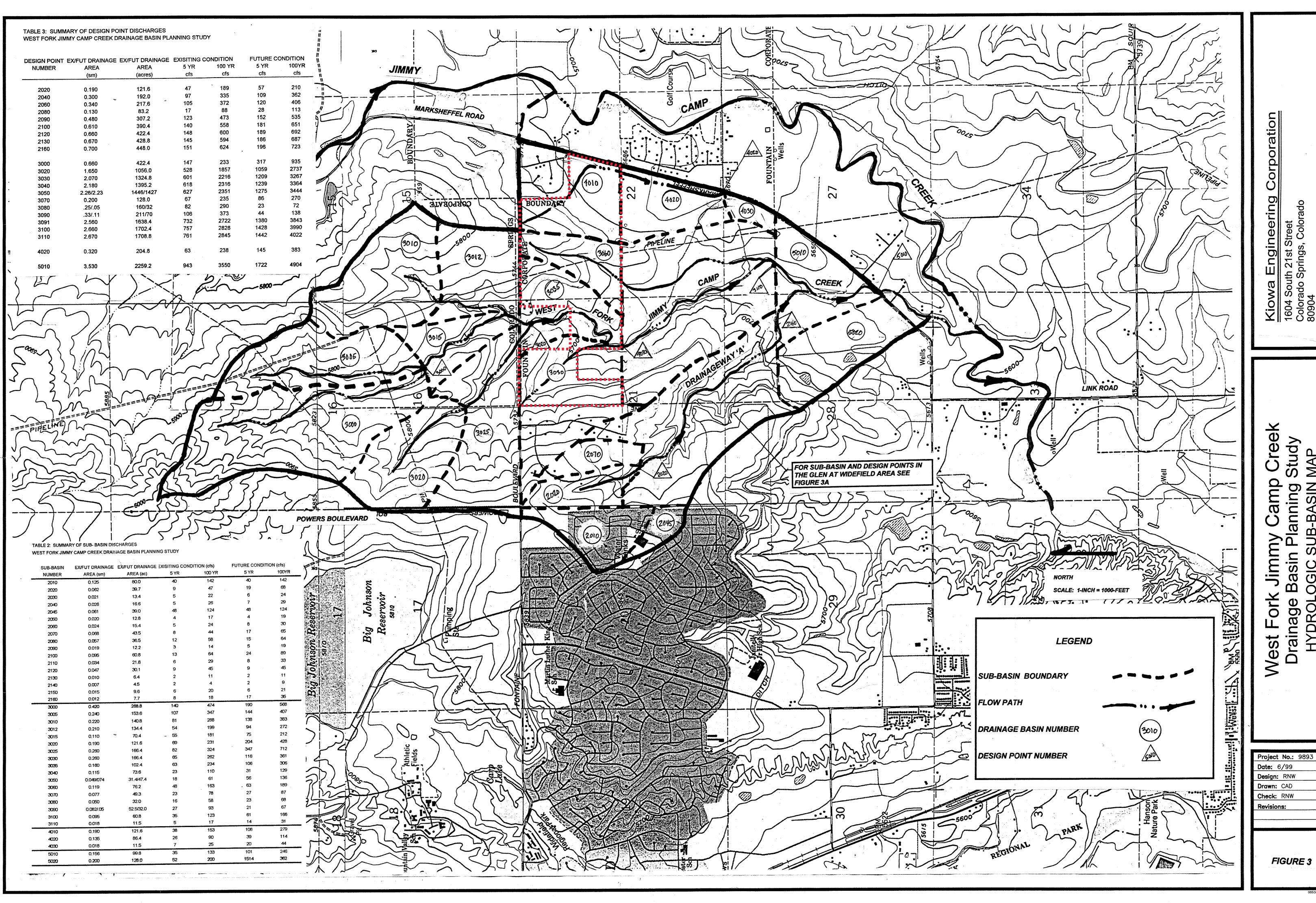
Land Use or	Percentage Imperviousness
Surface Characteristics	(%)
Business:	
Downtown Areas	95
Suburban Areas	75
Residential lots (lot area only):	-
Single-family	
2.5 acres or larger	12
0.75 – 2.5 acres	20
0.25 - 0.75 acres	30
0.25 acres or less	45
Apartments	75
Industrial:	
Light areas	80
Heavy areas	90
Parks, cemeteries	10
Playgrounds	25
Schools	55
Railroad yard areas	50
Undeveloped Areas:	·
Historic flow analysis	2
Greenbelts, agricultural	2
Off-site flow analysis (when land use not defined)	45
Streets:	
Paved	100
Gravel (packed)	40
Drive and walks	90
Roofs	90
Lawns, sandy soil	2
Lawns, clayey soil	2

## APPENDIX C **REPORT REFERENCES**



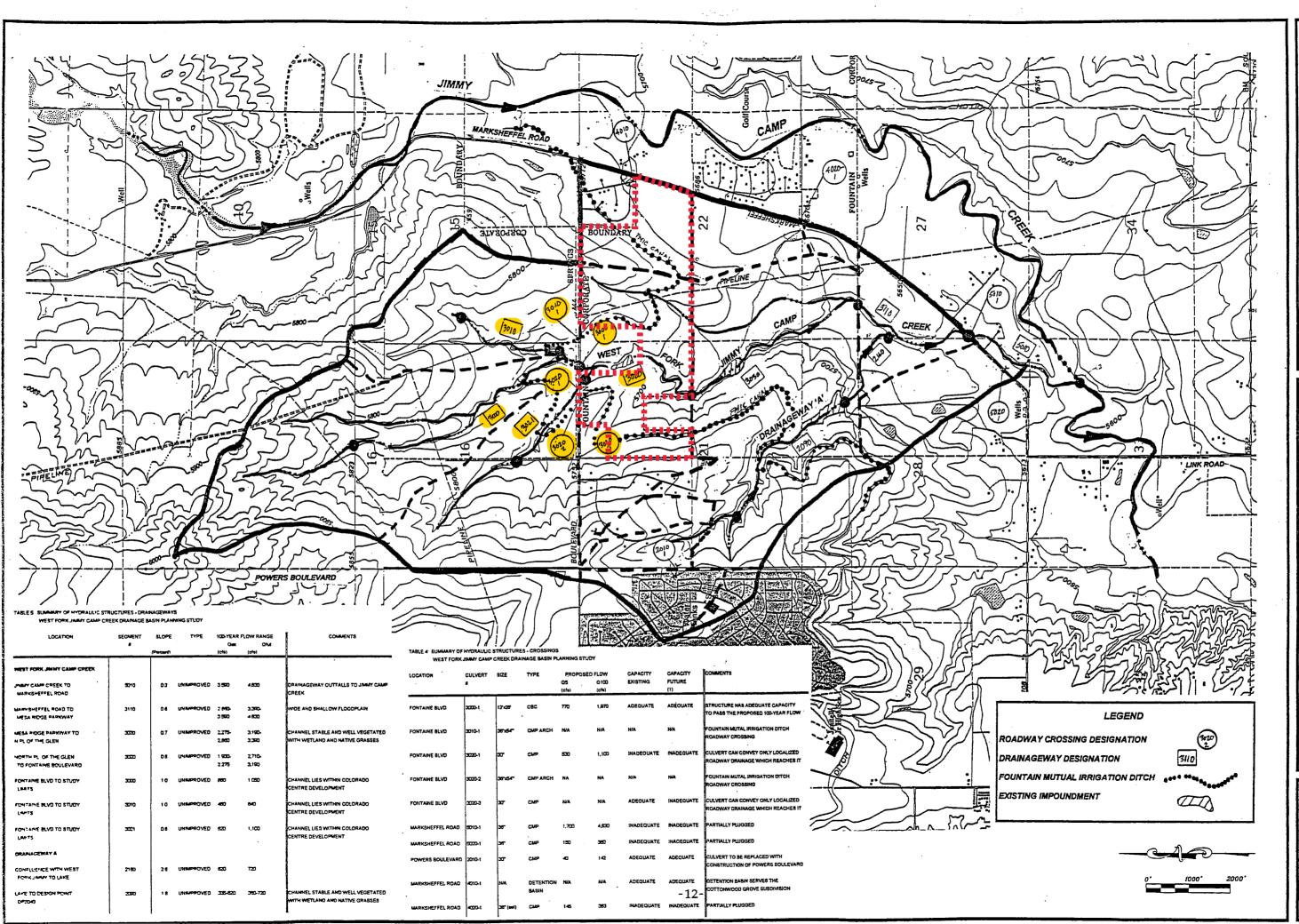






Study MAP ork

1604 S Colore 80904 (719)

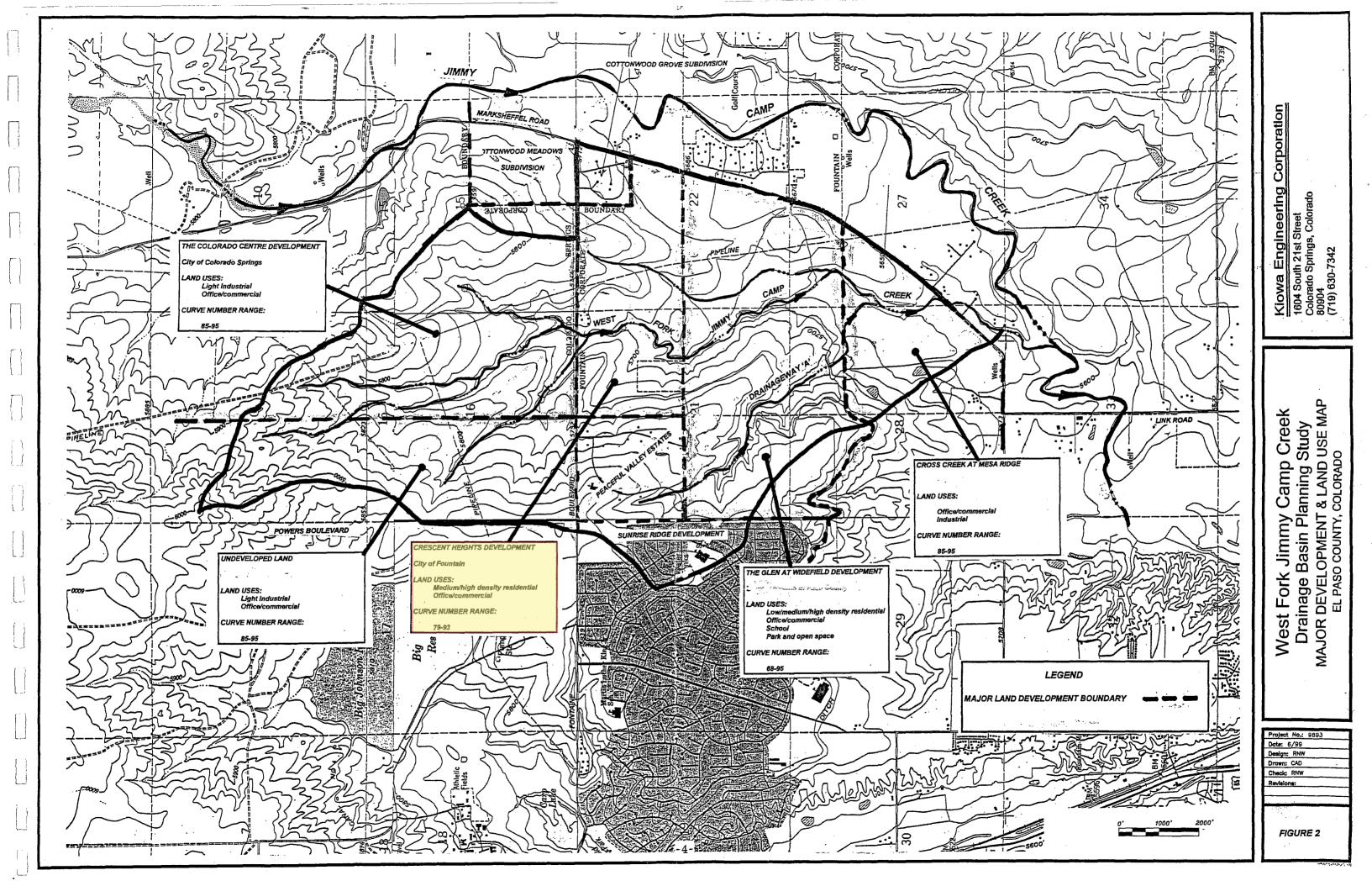


Kiowa Engineering Corporation 1604 South 21st Street Colorado Springs, Colorado 80904 (719) 630-7342

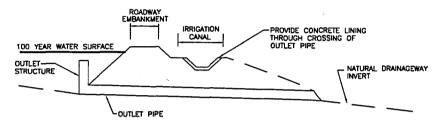
West Fork Jimmy Camp Creek
Drainage Basin Planning Study
INVENTORY OF EXISTING DRAINAGE STRUCTURES
EL PASO COUNTY, COLORADO

Project No.: 9893
Date: 6/99
Design: RNW
Drawn: CAD
Check: RNW
Revisions:

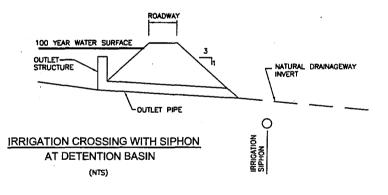
FIGURE 4

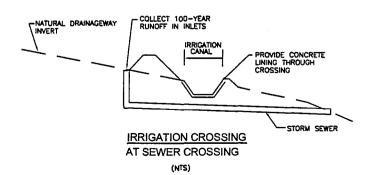


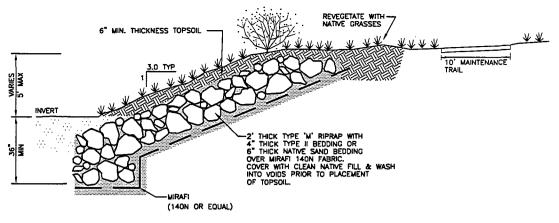
GRASSLINED BANK DETAIL



IRRIGATION CANAL CROSSING
AT DETENTION BASIN
(NTS)







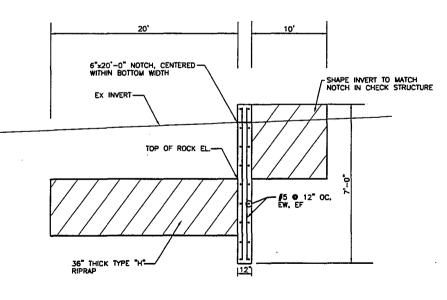
RIPRAP BANK LINING DETAIL

### RIPRAP GRADATIONS

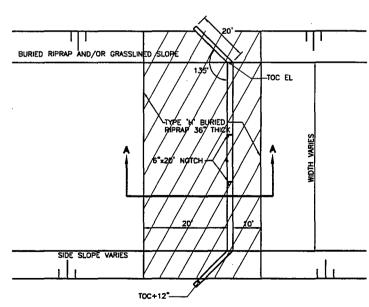
TYPE H RIPRAP INTERMEDIATE ROCK DIMENSION IN INCHES	% SMALLER THAN GIVEN SIZE BY WEIGHT	D 50 INCHES
30 24 18 6	100 50-70 35-50 2-10	18
TYPE M RIPRAP INTERMEDIATE ROCK DIMENSION IN INCHES	% SMALLER THAN GIVEN SIZE BY WEIGHT	D 50 INCHES
21 18 12 4	100 50-70 35-50 2-10	12

### SEED\_MIX

	THE EARTHWORK SHALL BE PERMANENTLY IVE GRASSES. NATIVE SEED MIX FOR TH FOLLOWS:	
NATIVE SEED MIX	pis	/acre
BLUE GRAMA SIDEOATS GRAMA SLENDER WHEATGRASS WESTERN WHEATGRASS	Chondrosum hirsutum Bouteloua curtipendula Agropyron trachycaulm trachycaulm Agropyron smithii	2.0 3.0 2.0 4.0
	-	11.0 lbs



SECTION A-A



TYPICAL CHECK STRUCTURE PLAN

NO SCALE

West Fork Jimmy Camp Creek Drainage Basin Planning Study TYPICAL DRAINAGEWAY DETAILS EL PASO COUNTY, COLORADO

Drawn: CAD
Check: RNW
Revisions:

Date: 7/00

Design: RNW

SHEET 7

And Marriage III

TABLE 2: SUMMARY OF SUB- BASIN DISCHARGES
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

	100YR	5 YR	100 YR	5 YR	AREA (ac)	AREA (sm)	NUMBER
_	142	40	142	40	80.0	0.125	2010
	68	19	47	9	39.7	0.062	2020
	24	6	22	5	13.4	0.021	2030
•	29	7	26	5	16.6	0.026	2040
	124	48	124	48	39.0	0.061	2045
	19	4	17	4	12.8	0.020	2050
	30	8	24	5	15.4	0.024	2060
	65	17	44	8	43.5	0.068	2070
	64	15	58	12	36.5	0.057	2080
	19	5	14	3	12.2	0.019	2090
	89	24	64	13	60.8	0.095	2100
	33	8	29	6	21.8	0.034	2110
	45	9	45	9	30.1	0.047	2120
	11	2	11	2	6.4	0.010	2130
WFCC FLOW	9	2	4	2	4.5	0.007	2140
SITE ENTRAI	21	6	20	6	9.6	0.015	2150
	35	17	18	8	7.7	0.012	2160
<b>-</b>	568	190	474	140	268.8	0.420	3000
WFCC FLOV	407	144	347	107	153.6	0.240	3005
SITE EXIT	383	138	288	81	140.8	0.220	3010
	272	94	199	54	134.4	0.210	3012
	212	75	181	55	70.4	0.110	3015
	428	204	231	69	121.6	0.190	3020
	712	347	324	82	166.4	0.260	3025
	<b>361</b>	116	262	<b>65</b>	166.4	0.260	3030
	306	106	234	<b>63</b>	102.4	0.160	3035
	129	31	110	23	73.6	0.115	3040
	136	56	61	18	31.4/47.4	0.049/074	3050
	189	<b>63</b>	163	48	76.2	0.119	3060
	87	27	78	23	49.3	0.077	3070
	68	23	58	16	32.0	0.050	3080
	67	21	93	27	52.5/32.0	0.082/.05	3090
	166	61	123	35	60.8	0.095	3100
-	31	14	17	5	11.5	0.018	3110
	279	108	153	38	121.6	0.190	4010
	114	39	90	26	86.4	0.135	4020
	44	20	25	7	11.5	0.018	4030
	246	101	133	35	99.8	0.156	5010

TABLE 3: SUMMARY OF DESIGN POINT DISCHARGES
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

DESIGN POINT	EX/FUT DRAINAGE	EX/FUT DRAINAGE	EXISITING C	ONDITION	FUTURE CO	NOITION
NUMBER	AREA	AREA	5 YR	100 YR	5 YR	100YR
	(sm)	(acres)	cfs	cfs	cfs	cfs
2020	0.190	121.6	47	189	57	210
2040	0.300	192.0	97	335	109	362
2060	0.340	217.6	105	372	120	406
2080	0.130	83.2	17	88	28	113
2090	0.480	307.2	123	473	152	535
2100	0.610	390.4	140	558	181	651
2120	0.660	422.4	148	600	189	692
2130	0.670	428.8	145	594	186	687
2160	0.700	448.0	151	624	196	723
$\vdash$						
<mark>-                                    </mark>	0.660	422.4	147	233	317	935
3020	1.650	1056.0	528	1857	1059	2737
3030	2.070	1324.8	601	2216	1209	3267
3040	2.180	1395.2	618	2316	1239	3364
3050	2.26/2.23	1446/1427	627	2351	1275	3444
3070	0.200	128.0	67	235	86	270
3080	.25/.05	160/32	82	290	23	72
3090	.33/.11	211/70	106	373	44	138
3091	2.560	1638.4	732	2722	1380	3843
3100	2.660	1702.4	757	2828	1428	3990
3110	2.670	1708.8	761	2845	1442	4022
			•			
4020	0.320	204.8	63	238	145	383
	<i>*</i> .					
5010	3.730	2387.2	943	3550	1722	4904

### Amended Master Development Drainage Plan The Glen at Widefield

El Paso County, Colorado

2

Prepared for:
New Generation Homes
3 Widefield Boulevard
Colorado Springs, Colorado 80911

Prepared by:
Kiowa Engineering Corporation

1604 South 21" Street Colorado Springs, Colorado 80904-4208

Kiowa Project No. 06026

June 21, 2007

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1 ID.....1....2....3....4.....5.....6.....7....8.....9....10 LINE THE GLEN AT WIDEFIELD FILING NO. 6 1 KIOWA ENGINEERING - PROJECT NO. 06026 2 2, 5, 10 & 100 YEAR STORMS FILENAME: GLENGDET.DAT DEV COND WITH DETENTION 3 ID 4 ID 24HR STORM DURATION \*DIAGRAM IT5 250 5 6 IO .56 PREC .70 JR .47 1 8 E1010 KK 9 .05 ΒA 10 ΤN 15 11 PB 4.4

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.0120 .0143

2 COMBINED AT									
+	DP3000	.66	1	FLOW TIME	215. 6.25	317. 6.25	493. 6.25	935. 6.17	
ROUTED TO									
+	R3015	.66	1	FLOW TIME	210. 6.33	313. 6.25	493. 6.25	925. 6.25	
HYDROGRAPH AT									
+	E3015	.11	1	FLOW TIME	51. 6.08	75. 6.08	115. 6.08	212. 6.08	
2 COMBINED AT								0.00	
+	DP3020	.77	1	FLOW TIME	245. 6.25	365. 6.25	570. 6.25	1077. 6.17	
HYDROGRAPH AT									
+	E3010	.22	1	FLOW TIME	96. 6.17	138. 6.17	211. 6.17	383. 6.17	
ROUTED TO								0.17	
+	R3012	.22	1	FLOW	93.	124	204		
			_	TIME	6.25	134. 6.25	204. 6.17	378. 6.17	
HYDROGRAPH AT							***	0.17	
+	E3012	.21	1	FLOW	64.	94.	1 47	070	
				TIME	6.33	6.33	1 <b>47.</b> 6.33	272. 6.33	
HYDROGRAPH AT									
+	E3020	.19	1	FLOW	159.	204.	275.	428.	
				TIME	6.17	6.17	6.17	6.17	
ROUTED TO									
+	R3025	.19	1	FLOW	158.	201.	270.	418.	
				TIME	6.25	6.25	6.25	6.25	
HYDROGRAPH AT									
+	E3025	.26	1	FLOW	273.	347.	463.	712.	
				TIME	6.08	6.08	6.08	6.08	
5 COMBINED AT									
+	DP3020	1.65	1	FLOW	761.	1059.	1562.	2737.	
				TIME	6.17	6.17	6.17	6.17	
ROUTED TO									
+	DB3021	1.65	1	FLOW	255.				
				TIME	6.75	6.75	6.67	6.42	
			**	PEAK STAG	ES IN FEET	**			
			1	STAGE	102.84	103.58	105.54		
				TIME	6.75	6.75	6.67	6.42	

.

PLAN Kiowa Engineering Corporation 1604 South 21st Street Colored Springs, Colored SP094 (719) 830-7342

THE GLEN AT WIDEFIELD
AMENDED MASTER DEVELOPMENT DRAINAGE PLAN
WEST FORK JIMMY CAMP CREEK DEVELOPED CONDITION
EL PASO COUNTY, COLORADO

Project No.: 06026 Date: June 21, 2007 Design: JGD Drawn: JGO Check: AWMC Revisions:

FIG. 3

NOTES TO USERS

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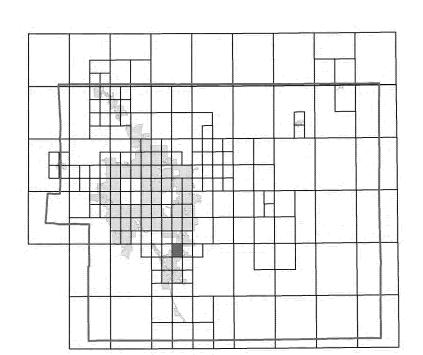
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**El Paso County Vertical Datum Offset Table** 

**Vertical Datum** Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

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### LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

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**ZONE A** No Base Flood Elevations determined. **ZONE AE** Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined

protection from the 1% annual chance or greater flood.

**ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

**ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide

**ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

**ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. **ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood

Elevations determined. FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

**ZONE X** Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. Floodolain boundary

Floodway boundary Zone D Boundary CBRS and OPA boundary ..........

> Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

~~ 513 ~~ Base Flood Elevation line and value; elevation in feet\* (EL 987) Base Flood Elevation value where uniform within zone; elevation in feet\* \* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

97° 07' 30.00"

Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, 4275000mN

5000-foot grid ticks: Colorado State Plane coordinate 6000000 FT system, central zone (FIPSZONE 0502),

Bench mark (see explanation in Notes to Users section of this FIRM panel)

ALOK GRAVANI

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE

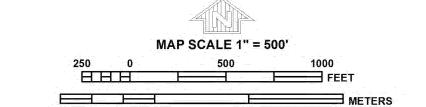
EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to

FLOOD INSURANCE RATE MAP

incorporate previously issued Letters of Map Revision. For community map revision history prior to countywide mapping, refer to the Community

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PANEL 0956G

**FIRM** 

**FLOOD INSURANCE RATE MAP** EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

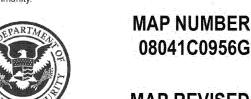
PANEL 956 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

**CONTAINS:** 

EL PASO COUNTY FOUNTAIN CITY OF 080061

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the subject



MAP REVISED **DECEMBER 7, 2018** 

08041C0956G

Federal Emergency Management Agency

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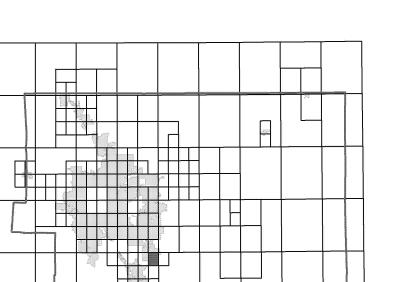
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### **El Paso County Vertical Datum Offset Table** Vertical Datum

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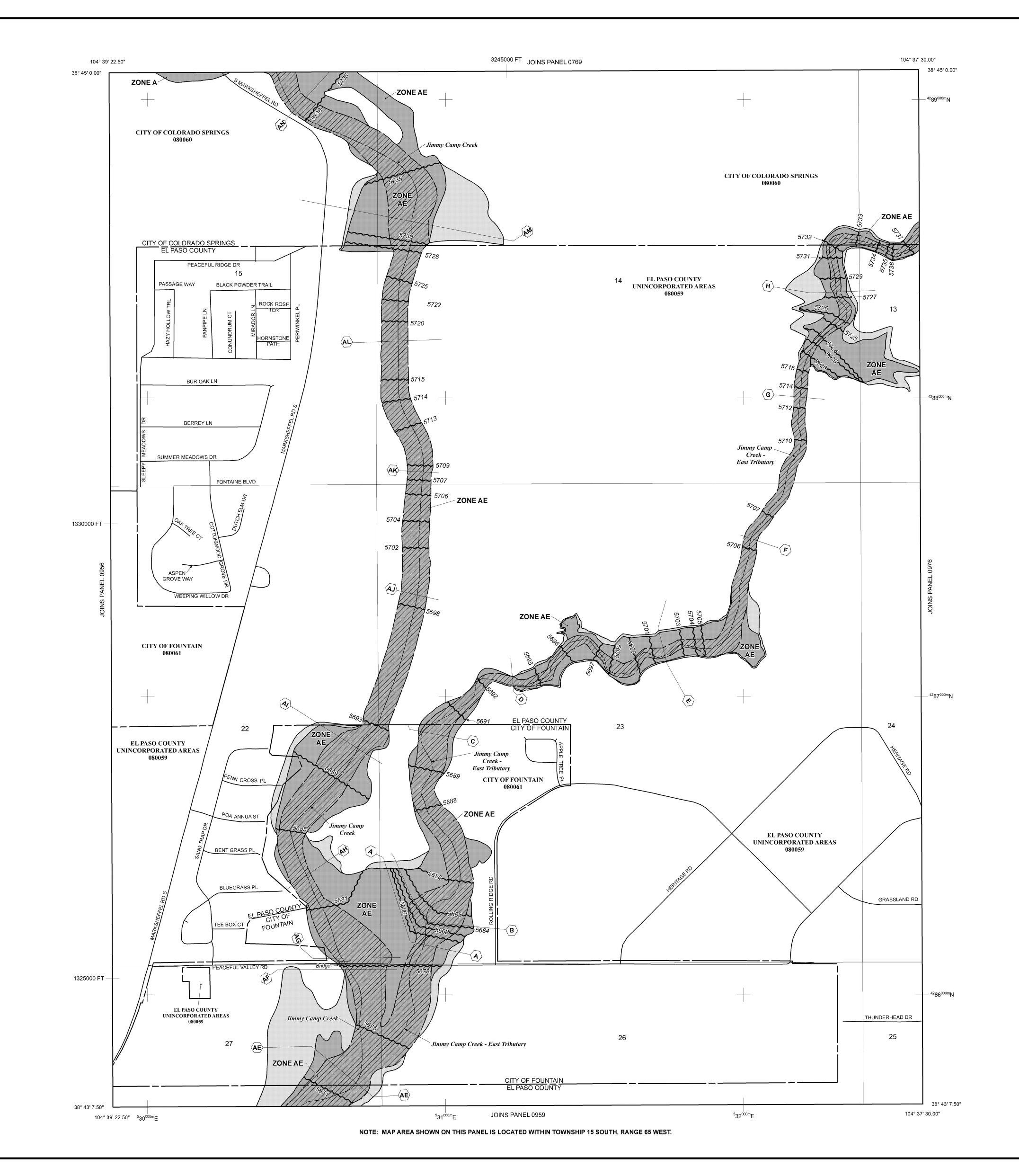
Panel Location Map



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Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

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Floodplain boundary Floodway boundary Zone D Boundary .......... CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. **∼∼** 513 **∼∼** Base Flood Elevation line and value; elevation in feet\*

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5000-foot grid ticks: Colorado State Plane coordinate 6000000 FT system, central zone (FIPSZONE 0502),

Bench mark (see explanation in Notes to Users section of this FIRM panel)

MAP REPOSITORIES

Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997

**DECEMBER 7, 2018** - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

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**PANEL 0957G** 

**FIRM** FLOOD INSURANCE RATE MAP **EL PASO COUNTY,** 

**PANEL 957 OF 1300** 

COLORADO

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

AND INCORPORATED AREAS

this correction for details.

FOUNTAIN, CITY OF Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the

Notice-to-User Letter that accompanied

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the



**MAP REVISED DECEMBER 7, 2018** 

MAP NUMBER

08041C0957G

Federal Emergency Management Agency

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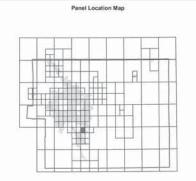
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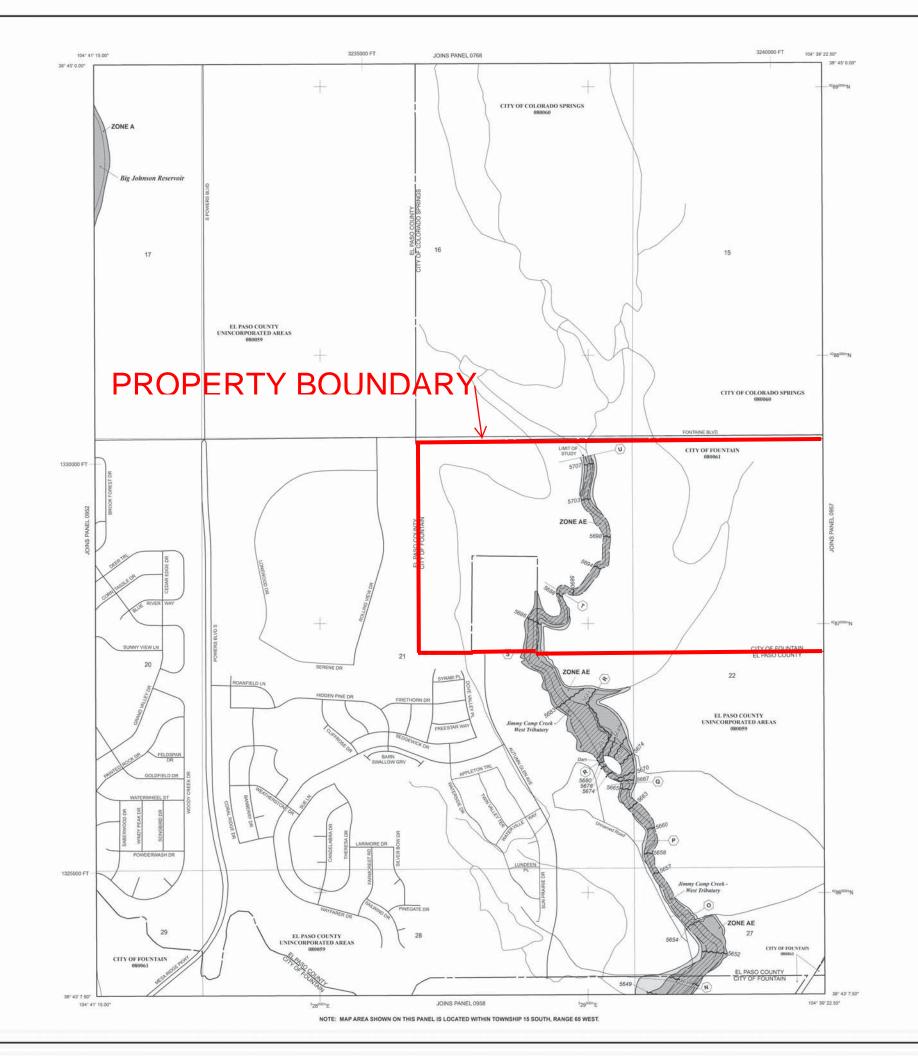
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ZONE VE

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OTHER FLOOD AREAS

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Floodway boundary Zone D Boundary

~~ 513 ~~ Base Flood Elevation line and value; elevation in feet\*

A Cross section line 23 ---- (23)

MAP SCALE 1" = 500'

250 0 500 1000 HHH FEET 

### FIRM

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 0956G

### PANEL 956 OF 1300

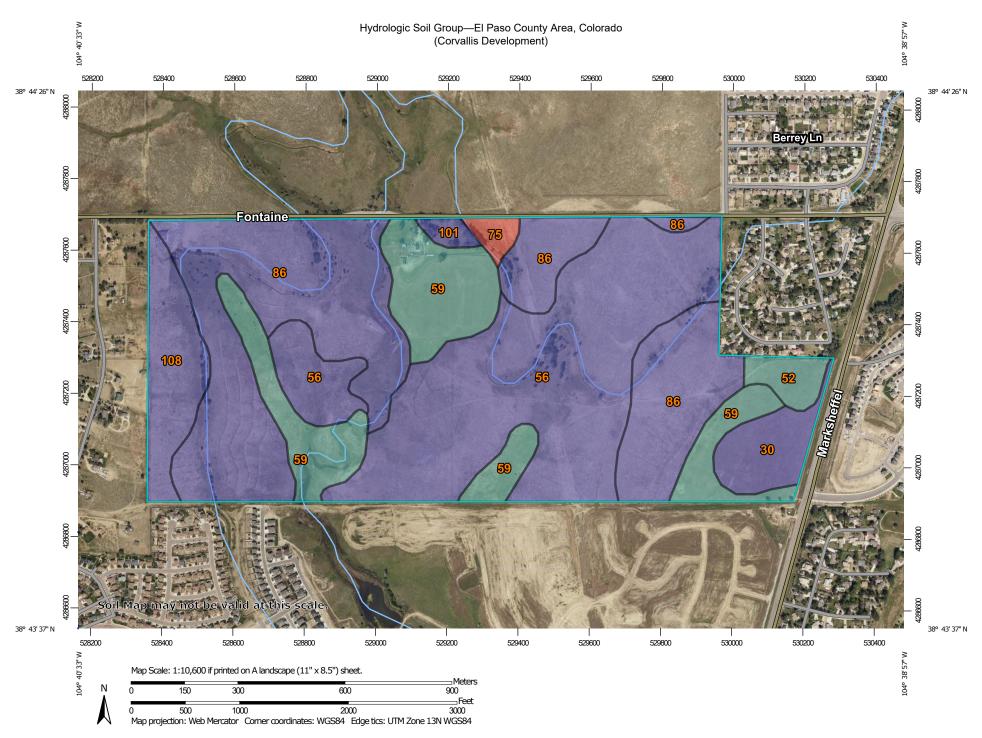
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COMMUNITY NUMBER PANEL SUFFIX COLORADO SIPRINDE, CITY OF 080060 0856
EL PASO COUNTY 080058 0856
FOUNTAIN, CITY OF 080061 0858

MAP NUMBER 08041C0956G

MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency



### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 17, Sep 13, 2019 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Aug 14, 2018—Sep 23. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

### **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
30	Fort Collins loam, 0 to 3 percent slopes	В	13.3	3.9%
52	Manzanst clay loam, 0 to 3 percent slopes	С	6.3	1.8%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	В	118.2	34.5%
59	Nunn clay loam, 0 to 3 percent slopes	С	55.5	16.2%
75	Razor-Midway complex	D	3.1	0.9%
86	Stoneham sandy loam, 3 to 8 percent slopes	В	122.1	35.6%
101	Ustic Torrifluvents, loamy	В	2.6	0.8%
108	Wiley silt loam, 3 to 9 percent slopes	В	21.4	6.3%
Totals for Area of Inter	rest		342.5	100.0%

### **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Figure 1-Existing 34" HDPE FMIC Pipe at Weeping Willow and Fontaine (Northeast of Corvallis)



Figure 2-Existing 56" x 38" CMAP FMIC Culvert across Fontaine



Figure 3-Existing 10' x 28' Concrete Box Culvert across Fontaine (Jimmy Camp Creek-West Fork)



Figure 4-Existing 69" x 46" CMAP FMIC Culvert across Fontaine



Figure 5-Existing 29" x 19" CMAP Fontaine Road Ditch Across Rolling View Drive (Appears to be grouted in insert) (NW of development)



Figure 6-Existing 60" RCP FMIC Culvert in Glens at Widefield Filing No. 6 (South of Corvallis)



Figure 7-Existing 18" CMP and Embankment (Jimmy Camp Creek-West Fork) Located south of proposed Corvallis Development



Figure 8-Existing 18" CMP and Embankment (Jimmy Camp Creek-West Fork) Located south of proposed Corvallis Development

### U.S. Fish and Wildlife Service

### **National Wetlands Inventory**

### Corvallis



September 10, 2020

### Wetlands

Estuarine and Marine Deepwater

Estuarine and Marine Wetland

Freshwater Emergent Wetland

Freshwater Forested/Shrub Wetland

Freshwater Pond

Lake

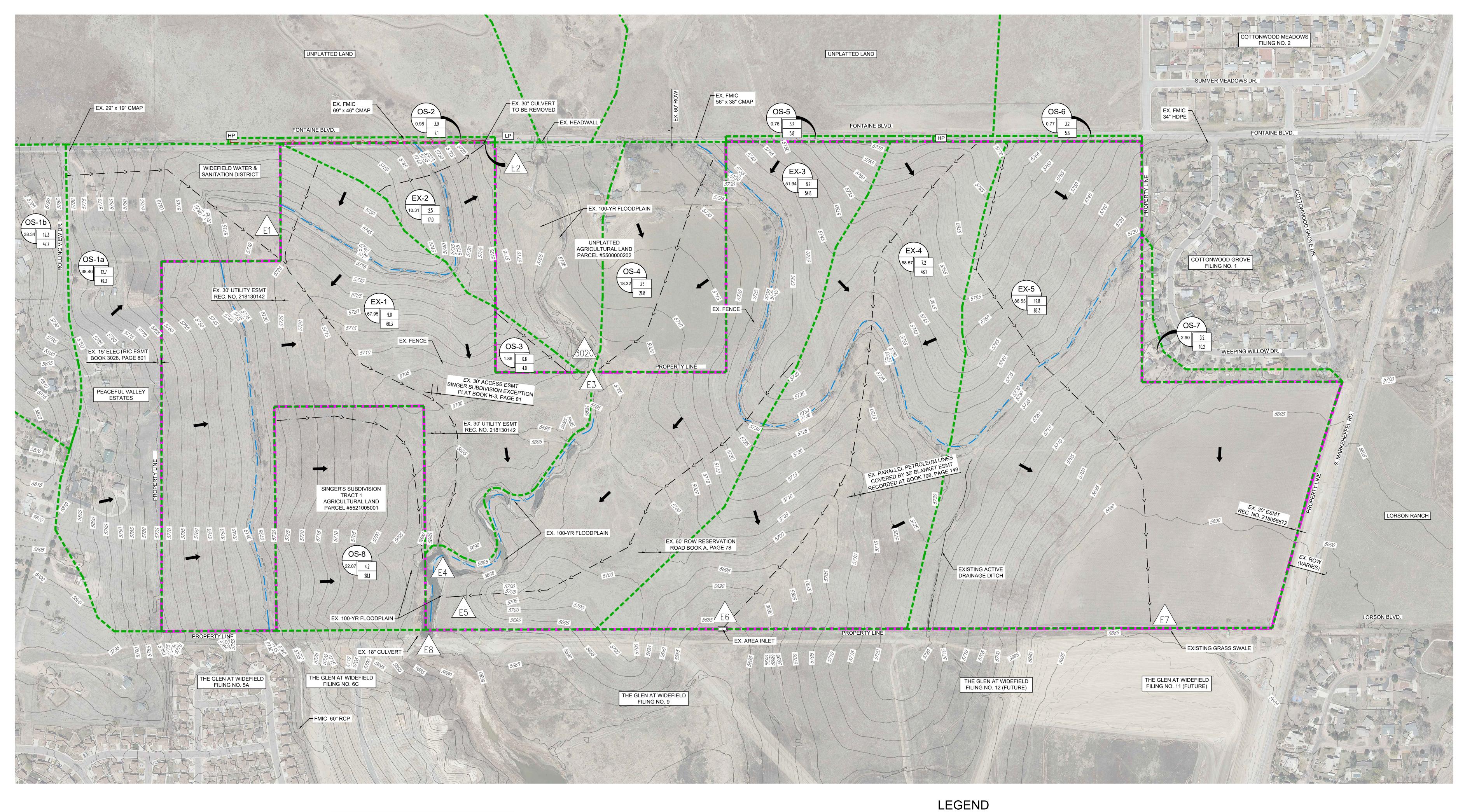
Other

Riverine

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.

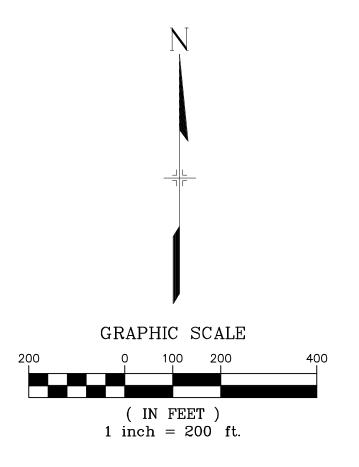
## APPENDIX D **M**APS





<u>Corvallis</u> Existing Conditions Basin Summary Table						
Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)			
OS-1a	38.5	12.7	49.3			
OS-1b	38.3	12.3	47.7			
OS-2	1.0	3.9	7.1			
OS-3	1.9	0.6	4.0			
OS-4	18.3	3.3	21.8			
OS-5	0.8	3.2	5.8			
OS-6	0.8	3.2	5.8			
OS-7	2.9	2.5	9.4			
OS-8	22.1	4.2	28.1			
EX-1	67.9	9.0	60.3			
EX-2	10.3	2.5	17.0			
EX-3	51.9	8.2	54.8			
EX-4	58.6	7.2	48.1			
EX-5	86.5	12.8	86.3			

Corvallis Existing Conditions Design Point Summary Table					
Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)		
<b>E1:</b> OS-1	76.8	25.3	98.5		
<b>E2:</b> OS-2, EX-2	11.3	5.4	22.5		
<b>E3:</b> E2, OS-3, OS-4	31.5	6.5	34.4		
<b>E4:</b> E1, E3, EX-1, OS-8	198.3	46.3	222.3		
<b>E5</b> : OS-5, EX-3	52.7	10.2	57.5		
<b>E6:</b> EX-4	58.6	7.2	48.1		
<b>E7:</b> EX-5, OS-6, OS-7	90.2	16.5	93.1		
<b>E8:</b> E4, E5, +DPBS3020	251.0	403.5	2040.7		



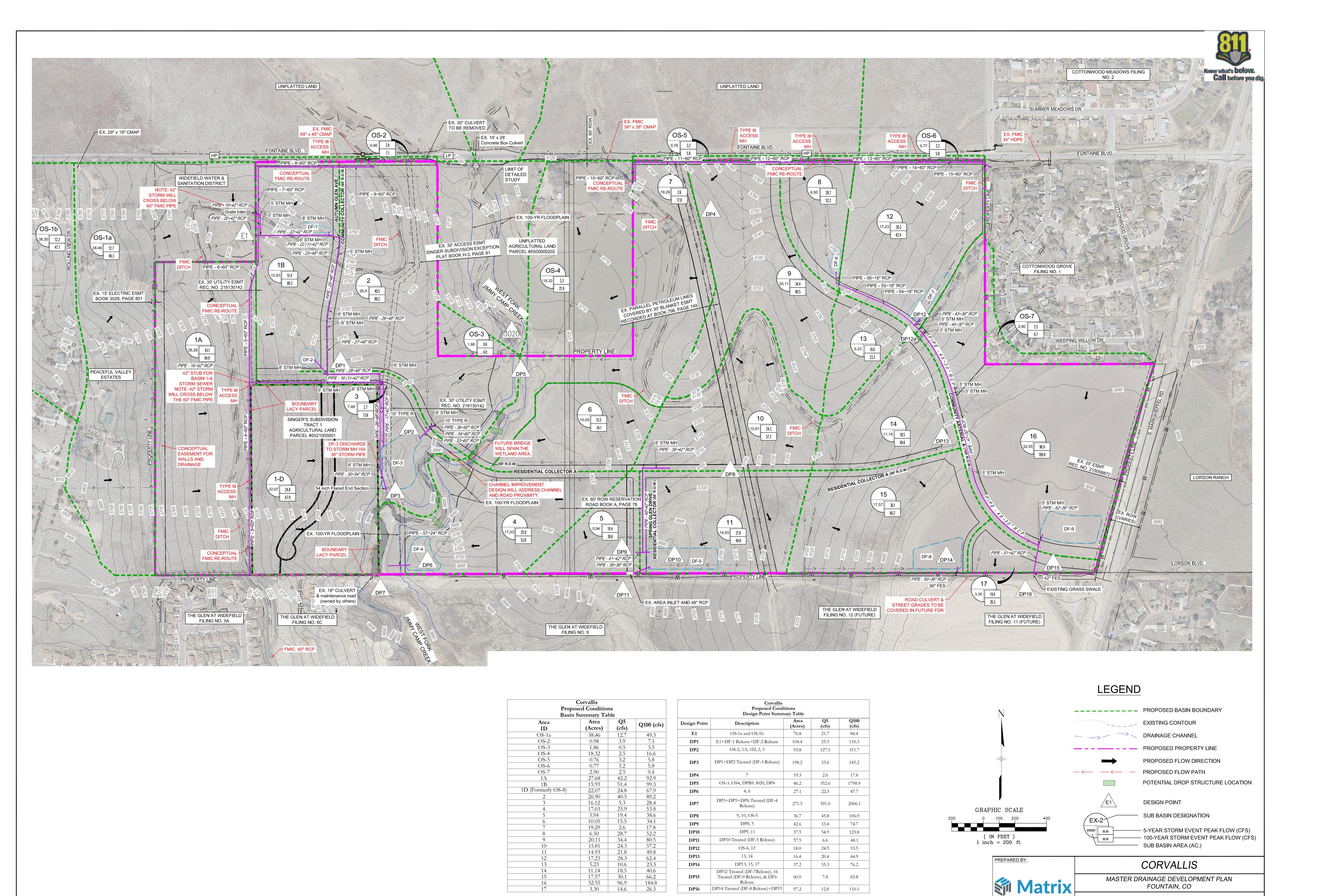
# EXISTING BASIN BOUNDARY EXISTING CONTOUR DRAINAGE CHANNEL PROPOSED PROPERTY LINE EXISTING FLOW DIRECTION EXISTING FLOW PATH DESIGN POINT SUB BASIN DESIGNATION 5-YEAR STORM EVENT PEAK FLOW (CFS) 100-YEAR STORM EVENT PEAK FLOW (CFS) SUB BASIN AREA (AC.)

PREPARED BY:			<u> </u>		10				
	CORVALLIS								
<b>Matrix</b>	MASTER DRAINAGE DEVELOPMENT PLAN FOUNTAIN, CO								
2435 Research Pkwy, Suite300 Colorado Springs, CO 80920 Phone 719.575.0100	EXISTING CONDITIONS								
	DESIGNED BY:	NMS	SCALE	DATE ISSUED:	MARCH 2021	DRAWING No.			
	DRAWN BY: CHECKED BY:	JTS NMS	HORIZ. $1'' = 200'$ VERT. $N/A$	SHEET	01 OF 04	DR01			

THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.

March 11, 2021 2:39 PM

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184.8

14.6

**DP16** DP14 Treated (DF-8 Release)+DP15 97.2

12.8

110.1

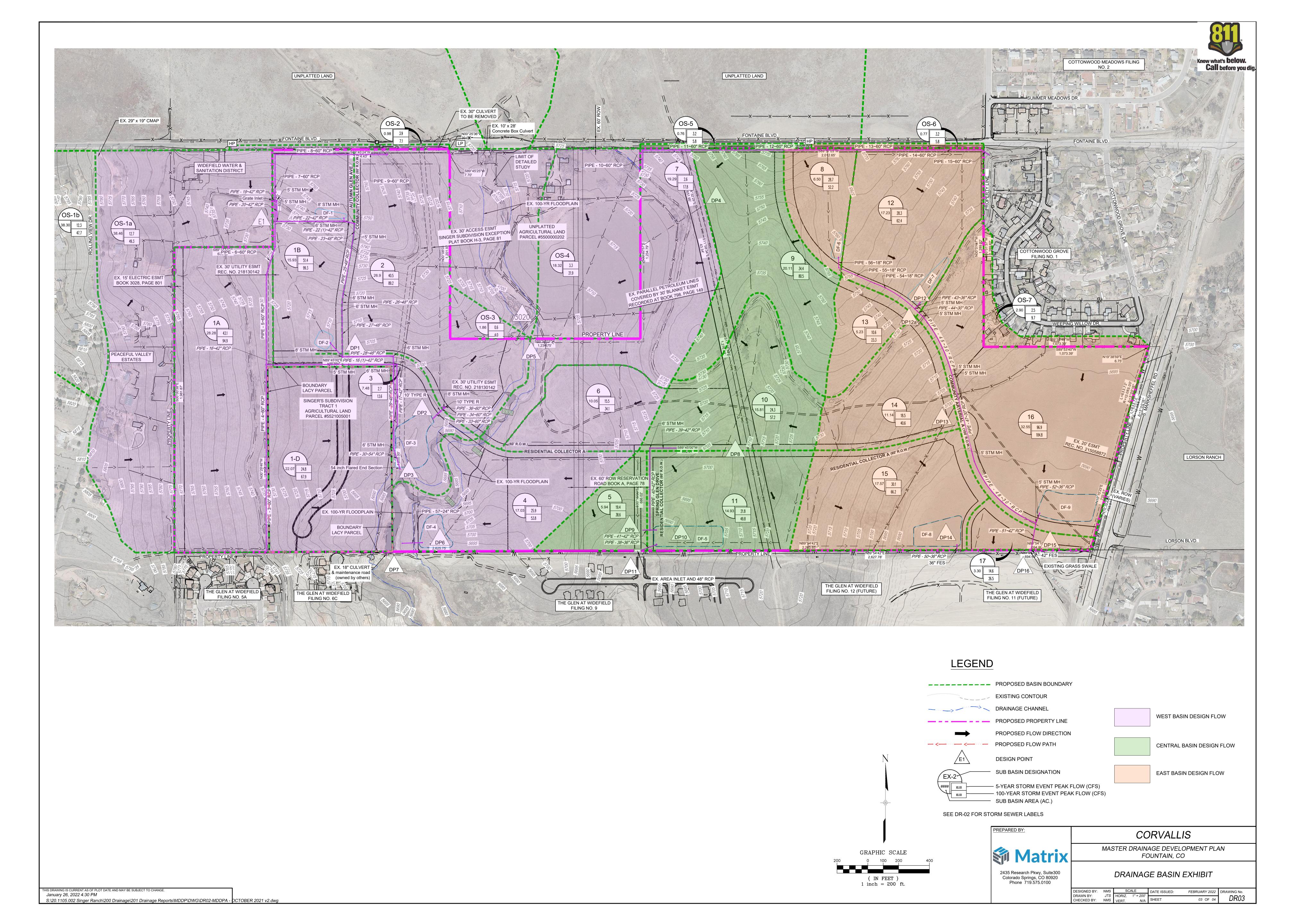
FOUNTAIN, CO

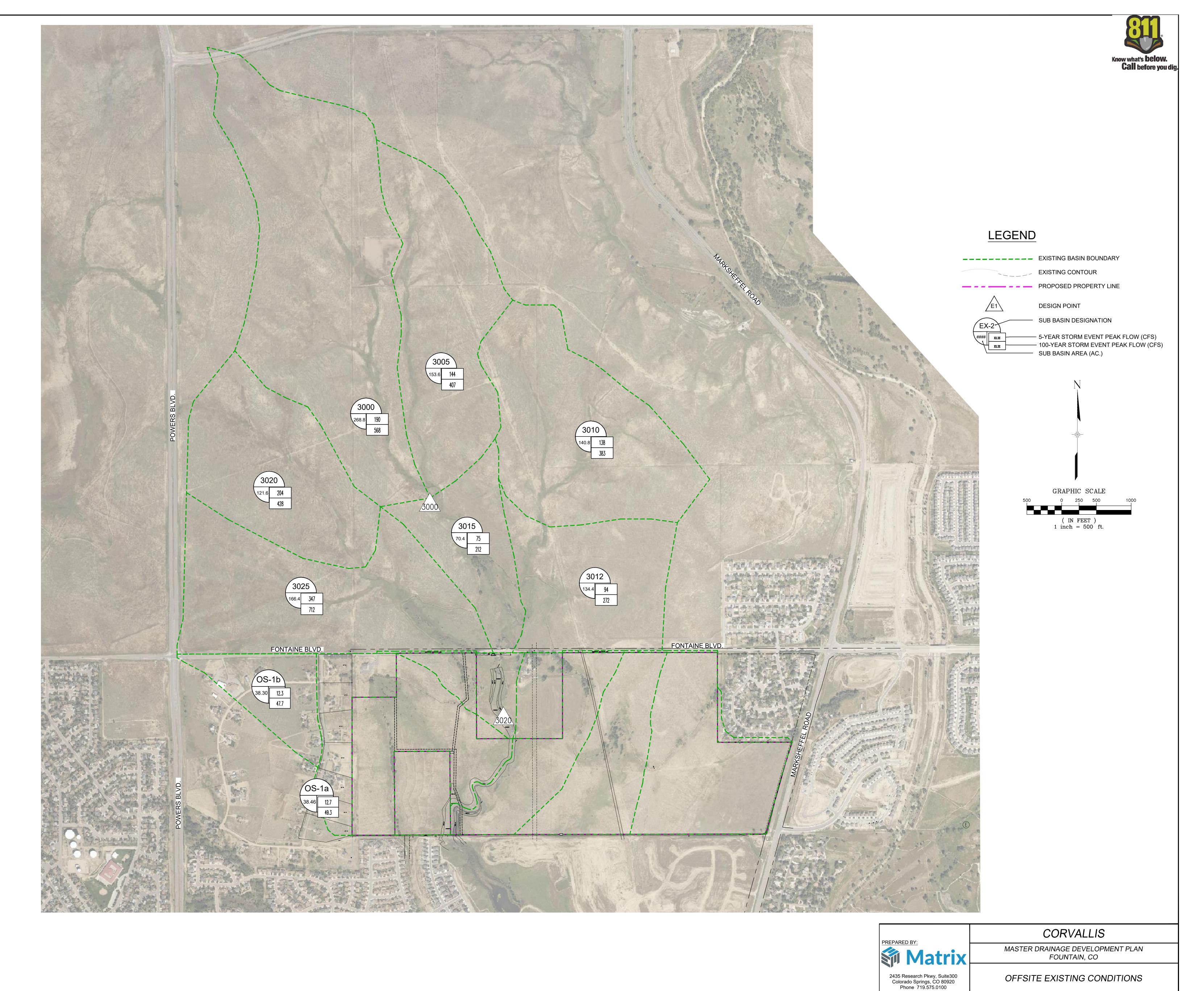
PROPOSED CONDITIONS

DR02

DESIGNED BY: NMS SCALE DATE ISSUED: FEBRUARY 2022 DRAWING No. PROVIDED BY: NMS VERT. N/A SHEET 02 OF 04 DROPE DROP

2435 Research Pkwy, Suite300 Colorado Springs, CO 80920 Phone 719.575.0100





DESIGNED BY: NMS SCALE DATE ISSUED:
DRAWN BY: JTS HORIZ. 1" = 200'
CHECKED BY: NMS VERT. N/A SHEET

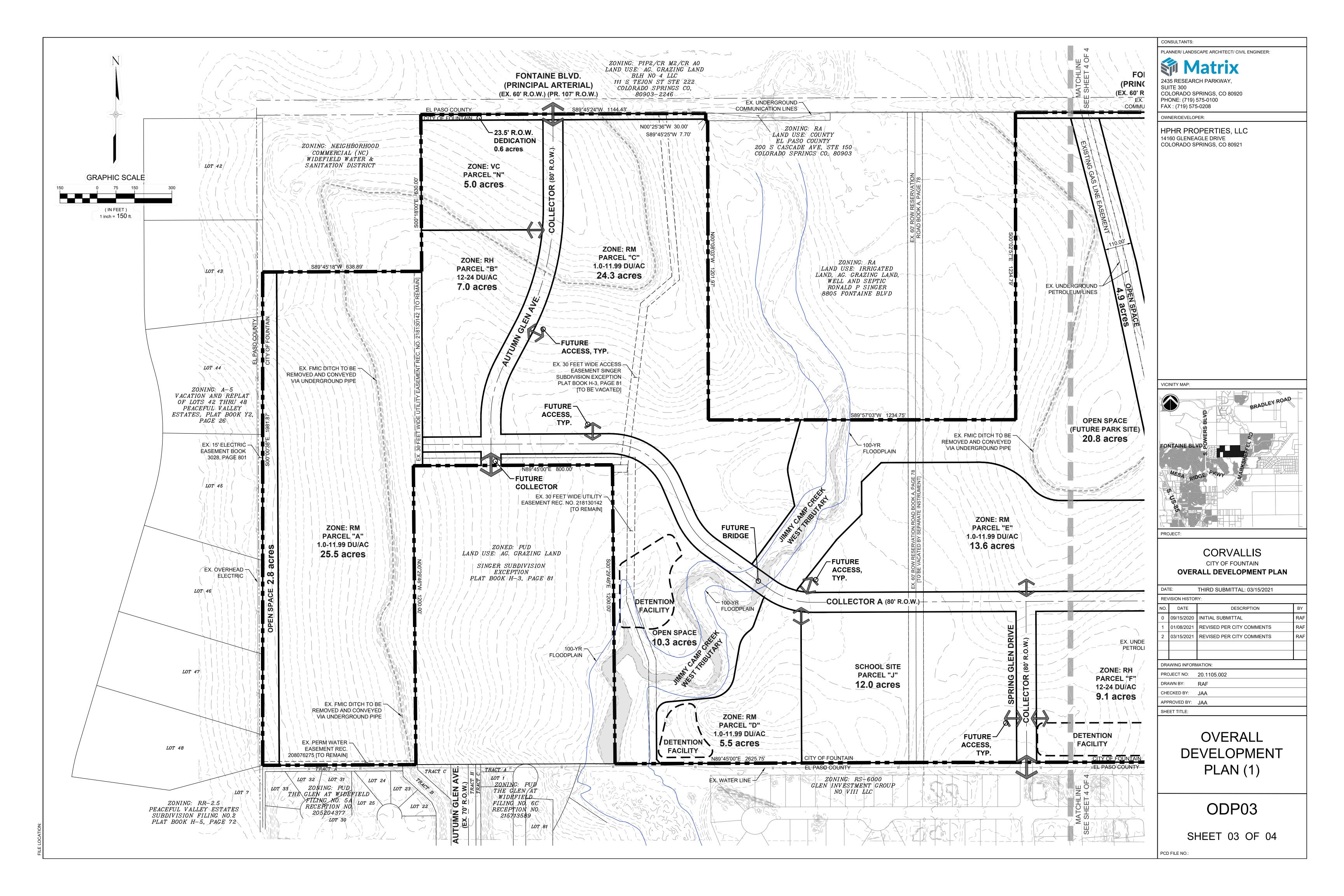
JANUARY 2021 DRAWING No.

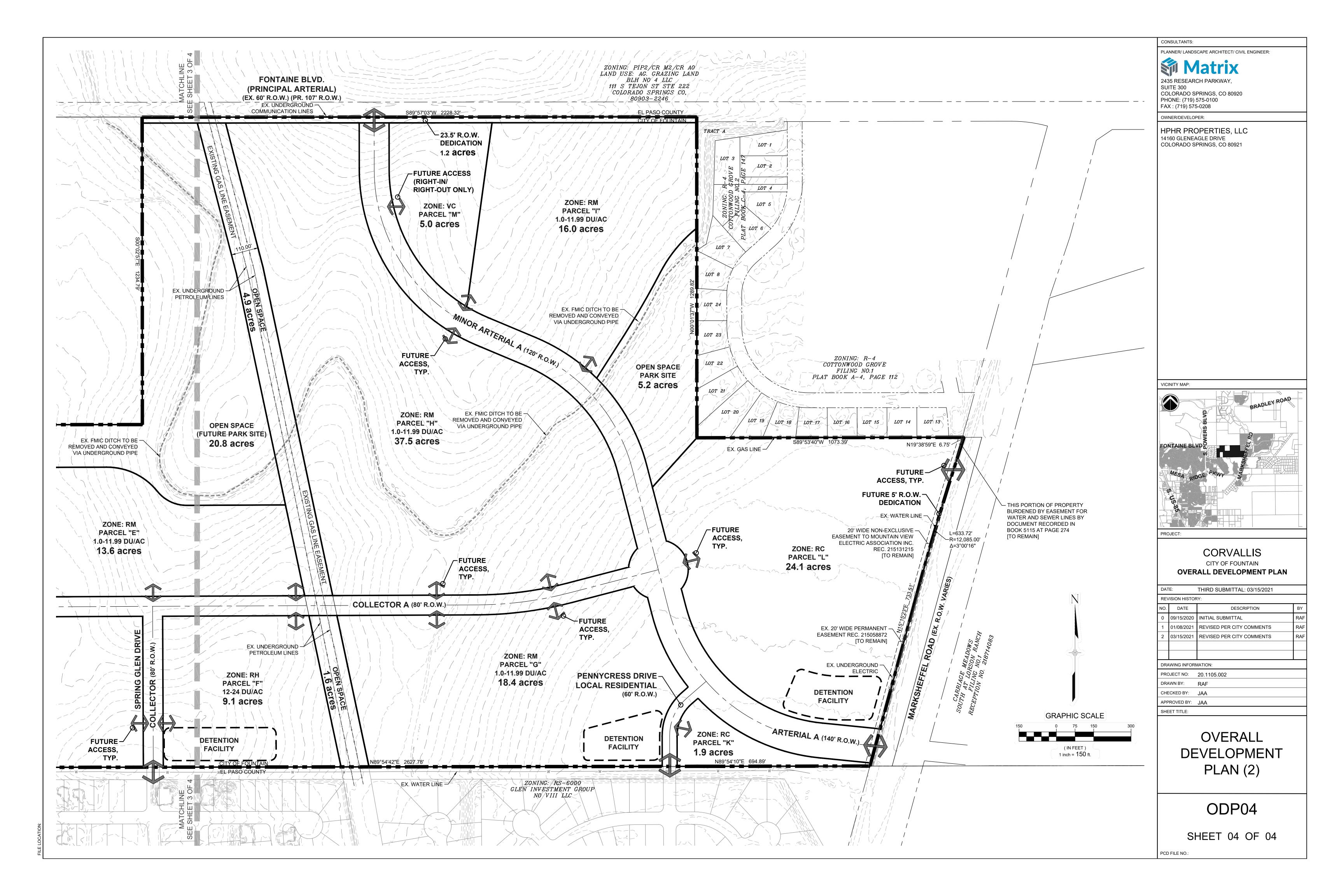
04 OF 04 DROS

THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.

January 5, 2021 8:52 AM

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## CORVALLIS - LACY PARCEL

CITY OF FOUNTAIN

## OVERALL DEVELOPMENT PLAN

### **DIMENSIONAL STANDARDS AND GUIDELINES:**

ZONE DISTRICT: RESIDENTIAL MEDIUM (RM) 1-10 DU/AC DIMENSIONAL STANDARDS FOR PARCEL A

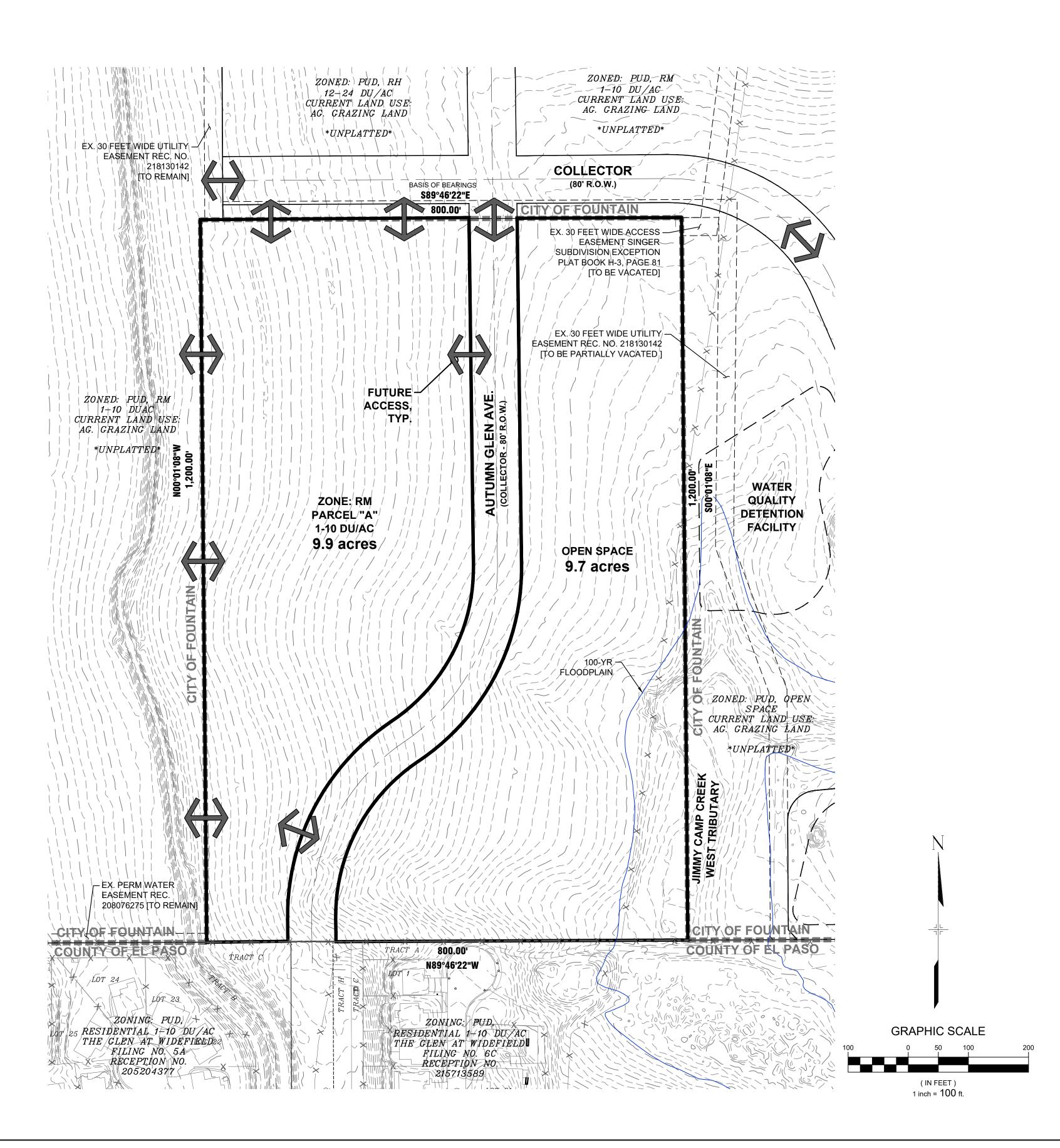
- PERMITTED LAND USE: SINGLE FAMILY RESIDENTIAL, MAIL KIOSKS, TRAIL CORRIDORS, DEVELOPMENT SIGNAGE, ENTRY MONUMENT SIGNAGE, PEDESTRIAN WALKWAYS, FENCING, UTILITIES, METRO DISTRICT MAINTENANCE FACILITIES, STORMWATER FACILITIES, DRAINAGE IMPROVEMENTS, OPEN SPACE AND LANDSCAPE IMPROVEMENTS, PARKS AND ASSOCIATED PARK RELATED EQUIPMENT, COMMUNITY CLUBHOUSE.
- MINIMUM LOT AREA FOR SINGLE FAMILY DETACHED: A. SINGLE FAMILY DWELLING: 3,800 SF
- MAXIMUM PERCENTAGE OF STRUCTURAL COVERAGE: 50%
- MAXIMUM STRUCTURAL HEIGHT: 40'
- MINIMUM WIDTH OF LOT AT FRONT BUILDING SETBACK LINE: 30' OR AS OTHERWISE SHOWN
- PROJECTIONS INTO SETBACKS ARE GOVERNED BY THE CITY OF FOUNTAIN ZONING CODE. AS AMENDED
- MINIMUM SETBACK REQUIREMENTS: A. FRONT YARD: 18' TO FACE OF GARAGE FROM PROPERTY LINE
- 15' TO FRONT PROJECTION OF HOUSE FROM PROPERTY LINE
- B. SIDE YARD: 5' C. REAR YARD: 15'
- D. CORNER YARD (NON-DRIVEWAY SIDE): 10'
- 18' IF SIDE GARAGE ACCESS IS PROVIDED
- E. CHAMFERED CORNER FRONT SETBACK: 8'

### DEVELOPMENT STANDARDS AND GUIDELINES

- TEMPORARY USES ARE SUBJECT TO THE REQUIREMENTS OF THE CITY OF FOUNTAIN ZONING CODE, AS AMENDED.
- ACCESSORY USES ARE SUBJECT TO THE REQUIREMENTS OF THE CITY OF FOUNTAIN ZONING CODE, AS AMENDED. FENCING GUIDELINES TO BE PER THE FUTURE CORVALLIS CC&R'S AND/ OR DESIGN GUIDELINES
- 4. A MINIMUM 4' FRONT YARD BUILDING STAGGER IS REQUIRED BETWEEN ADJACENT UNITS.

### **GENERAL LOT DEVELOPMENT NOTES:**

- 1. LOCATION OF PRIVATE SIDEWALKS TO FRONT ENTRY TO BE DETERMINED BY INDIVIDUAL HOUSE INGRESS/ EGRESS
- OWNER/ BUILDER TO ENSURE DRIVEWAYS DO NOT CONFLICT WITH PEDESTRIAN RAMP TRANSITIONS.
- ALL SIGHT DISTANCE TRIANGLES MUST BE WITHIN THE PUBLIC RIGHT-OF-WAY OR A SIGHT DISTANCE EASEMENT. IF THE LINE OF SIGHT CROSSES ONTO PRIVATE PROPERTY, A "SIGHT DISTANCE EASEMENT" SHALL BE DEDICATED TO PROVIDE THE REQUIRED SIGHT DISTANCE AT TIME OF FINAL PLAT. MAINTENANCE OF A SIGHT DISTANCE EASEMENT SHALL BE THE RESPONSIBILITY OF THE PROPERTY OWNER OR METROPOLITAN DISTRICT UNLESS OTHERWISE APPROVED BY THE CITY OF



PLANNER/ LANDSCAPE ARCHITECT/ CIVIL ENGINEER: COLORADO SPRINGS, CO 80920 PHONE: (719) 575-0100

OWNER/DEVELOPER:

FAX: (719) 575-0208

HPHR PROPERTIES, LLC 14160 GLENEAGLE DRIVE

COLORADO SPRINGS, CO 80921

APPROVAL:

FONTAINE BLVD

**CORVALLIS - LACY PARCEL** OVERALL DEVELOPMENT PLAN

SOUTH SEGMENT OF CORVALLIS

10/22/2021

REVISION HISTORY:						
NO.	DATE	DESCRIPTION	BY			
			-			
DRAWING INFORMATION:						

PROJECT NO: 21.1105.009

CHECKED BY: JAA APPROVED BY: JAA

> **OVERALL** DEVELOPMENT PLAN

> > ODP02

SHEET 2 OF 2

CITY FILE NO.: X