

City of Fountain  
Engineering Department  
116 South Main St.  
Fountain, CO 80817

February 2022

RE: Corvallis MDDP

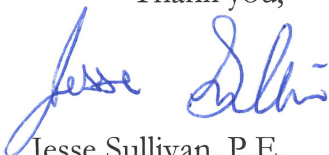
Dear Sir or Madam,

Please find enclosed the MDDP Amendment for the proposed Corvallis development. The purpose of this amendment is to address the addition of the 22-acre “Lacy Parcel” to the Corvallis development. This parcel will add 9.7 acres of Open Space, 9.9 acres of single-family, and 2.4 acres of roadways. The site indicated in the original ODP included 140.8 acres of single-family, 16.1 acres of multi-family, and 36 acres of commercial. 45.6 acres as park area or open space were also proposed, in addition to the open spaces associated with the gas easement running through the property. Additionally, 12 acres will be used for a school.

Drainage analysis for the project has been completed in accordance with the current City of Colorado Springs drainage criteria manual which the city of Fountain has adopted as its governing drainage criteria.

If there are any comments or questions regarding this submittal, please feel free to contact me by phone: 719-575-0100 or email: [jesse.sullivan@matrixdesigngroup.com](mailto:jesse.sullivan@matrixdesigngroup.com).

Thank you,

  
Jesse Sullivan, P.E.

Enclosures.

**MASTER DEVELOPMENT DRAINAGE PLAN  
AMENDMENT**

**For**

**CORVALLIS**

Prepared for:  
**City of Fountain**  
116 S. Main Street  
Fountain, CO 80817

On Behalf of:  
**HPHR Properties, LLC**  
555 Middle Creek Parkway, Suite 380  
Colorado Springs, CO 80921

Prepared by:



**Matrix**

2435 Research Parkway, Suite 300  
Colorado Springs, CO 80920  
(719) 575-0100  
fax (719) 572-0208

February 2022

Project No. 20.1105.002

**ENGINEER'S STATEMENT:**

This report and plan for the drainage design of Corvallis was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Fountain does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, error or omissions on my part in preparing this report.

**Signature:** \_\_\_\_\_

Jesse Sullivan  
Colorado Professional Engineer No. 55600

**DEVELOPER'S STATEMENT:**

HPHR Properties, LLC hereby certifies that the drainage facilities for Corvallis shall be constructed according to the design presented in this report. I understand that the City of Fountain does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Fountain pursuant to the City Code; and cannot, on behalf of HPHR Properties, LLC, guarantee that final drainage design review will absolve HPHR Properties, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

**Name of Developer:** HPHR Properties, LLC

**Authorized Signature:** \_\_\_\_\_ **Date:** \_\_\_\_\_

**Printed Name:** Ed Houle

**Title:** *Director of Land Acquisition and Development*

Address: 14160 Gleneagle Drive  
Colorado Springs, CO 80921

**CITY OF FOUNTAIN STATEMENT:**

Filed in accordance with the Code of the City of Fountain, 2009, as amended.

\_\_\_\_\_  
For the City Engineer Date

Conditions:

**TABLE OF CONTENTS**

I. INTRODUCTION ..... 4

II. PROJECT CHARACTERISTICS..... 6

III. HYDROLOGIC ANALYSIS..... 9

IV. HYDRAULIC ANALYSIS ..... 20

V. ENVIRONMENTAL EVALUATIONS ..... 21

VI. SELECTED PLAN..... 29

VII. FEE DEVELOPMENT ..... 31

VIII. SUMMARY ..... 32

IX. REFERENCES ..... 32

**APPENDIX**

**A. Hydrologic and Hydraulic Calculations**

- 1. Existing and Proposed Rational Calculations
- 2. Storm Infrastructure Sizing
- 3. Storm System Capacity modeling
- 4. UDFCD Detention Basin Design Workbook

**B. Standard Design Charts and Tables**

- 1. 2019 Drainage Fee Schedule
- 2. Shallow Flow Velocities Figure 6-25
- 3. DCM Street Capacity Chart Figure 7-7
- 4. DCM Runoff Coefficients Table 6-6

**C. Report References**

- 1. Soils Map
- 2. FEMA FIRM Floodplain Maps
- 3. Report Maps

**D. Maps**

- 1. Existing Conditions Drainage Basin Map
- 2. Proposed Conditions Drainage Basin Map
- 3. National Wetlands Inventory Map
- 4. WFJCC DBPS Land Use Map

# I. Introduction

## A. PURPOSE AND SCOPE OF STUDY

The purpose of this report is to amend the approved Master Development Drainage Plan (MDDP) to account for the inclusion of the previously excluded 22.072-acre Lacy Parcel to the development. This revision will be submitted to the City as an Overall Development Plan for the (ODP) for the parcel. This Master Development Drainage Plan Amendment (MDDPA) report provides a summary of the site drainage issues impacting the overall proposed Corvallis development, including identification and evaluation of the offsite and onsite drainage patterns associated with the project, analysis of upstream impacts from upstream drainage, and impacts to downstream facilities. This MDDPA has been prepared based on the guidelines and criteria presented in the City of Colorado Springs Drainage Criteria Manual (DCM).








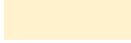

## B. AGENCY JURISDICTIONS

This project is located within the City of Fountain and is subject to the design criteria set forth in the *City of Colorado Springs Drainage Criteria Manual, Volumes I and II, dated May 2014 (DCM)*.

## C. GENERAL PROJECT DESCRIPTION

Corvallis is a 297-acre (22 Acre “Lacy Parcel” & 275 Acre Original ODP) mixed-use parcel located at the southwest intersection of Marksheffel Road and Fontaine Boulevard. The Corvallis ODP amendment prepared by Matrix Design Group, Inc dated October 2021 includes single-family and multi-family residential units, commercial development, a school site, and dedicated open space. Figure 1 below displays in further detail the Land Use Summary:

Figure 1. Land Use Summary of proposed Corvallis site

Original ODP			
	Commercial (office/retail)	36.0	Acres
	Residential (single-family)	140.8	Acres
	Residential (multi-family)	16.1	Acres
	School Site	12	Acres
	Collector Roadways	25.4	Acres
	Open Space	45.6	Acres
Lacy Parcel			
	Open Space	10.3	Acres
	Residential (single-family)	9.9	Acres
	Collector Roadways	1.8	Acres

More specifically, the site is located as follows:

1. **General Location:** Part of the Northeast  $\frac{1}{4}$  of Section 21, and the Northwest  $\frac{1}{4}$  and a Portion of the Southwest  $\frac{1}{4}$  of the Northeast  $\frac{1}{4}$  of Section 22, all in Township 15 South, Range 65 West of the 6<sup>th</sup> P.M. in the City of Fountain, County of El Paso, State of Colorado.
2. **Surrounding Streets:** Fontaine Boulevard directly borders the parcel to the north, and a portion of the eastern boundary is bordered directly by Marksheffel Road. Powers Boulevard (State Highway 21) is located approximately  $\frac{1}{2}$  mile to the west.
3. **Drainageway:** The proposed site lies entirely within the West Fork Jimmy Camp Creek Drainage Basin and is currently undeveloped land, mostly covered by natural vegetation. The Fountain Mutual Irrigation Company (FMIC) irrigation ditch also enters and exits the site multiple times.
4. **Surrounding Developments:** The site is bound by vacant land to the north, the Peaceful Valley Estates development to the West, The Glen at Widefield Subdivisions to the south, and Lorson Ranch to the east.

Refer to Appendix D for the Vicinity Map.

#### ***D. DATA SOURCES***

Topographical information for the site was found using a combination of ***United States Geological Survey*** (USGS) mapping, GIS LIDAR, as well as field surveying. The ***Web Soil Survey***, created by the ***Natural Resources Conservation Service***, was utilized to investigate the existing general soil types within the site.

#### ***E. APPLICABLE CRITERIA AND STANDARDS***

As required by the City of Fountain, Colorado, this report has been prepared in accordance to the criteria set forth in the ***City of Colorado Springs Drainage Criteria Manual Volume 1*** (Drainage Criteria Manual), dated May 2014, updated January 2021 and ***Volume 2 Stormwater Quality Policies, Procedures, and BMP's***, dated May 2014, updated December 2020.

In addition to the City Criteria Manual, the ***Urban Storm Drainage Criteria Manuals, Volumes 1-3*** (UDFCD), published by the Urban Drainage and Flood Control District, latest update, have been used to supplement the Drainage Criteria Manual for water quality capture volume (WQCV).

#### ***F. REFERENCED DRAINAGE REPORTS***

***West Fork Jimmy Camp Creek Drainage Basin Planning Study (WFJCC DBPS)***, by Kiowa Engineering Corp. October 2003.

***Master Drainage Development Plan (MDDP) The Glen at Widefield***, by Kiowa Engineering Corp. December 1999.

***Master Drainage Development Plan Amendment (MDDPA) The Glen at Widefield***, by Kiowa Engineering Corp. June 2007.

*Final Drainage Report (FDR F9) The Glen at Widefield Filing No. 9*, by Kiowa Engineering Corp. July 2018.

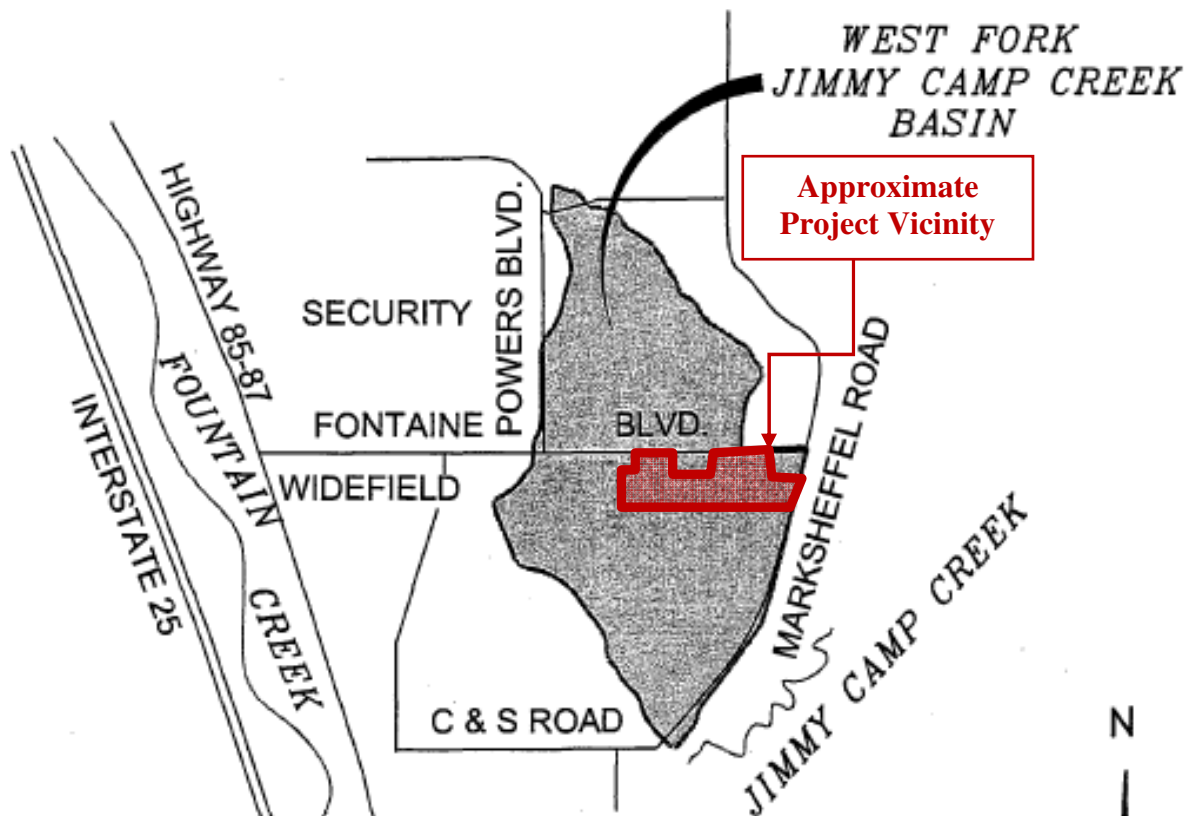
*Final Drainage Report (FDR F11) The Glen at Widefield Filing No. 11*, by Kiowa Engineering Corp. December 2019.

*Master Drainage Development Plan (MDDP) Corvallis*, by Matrix Design Group, September 2021.

## II. Project Characteristics

### A. MAJOR BASIN

Corvallis lies entirely within the West Fork Jimmy Camp Creek (WFJCC) Drainage Basin. The project includes offsite and onsite drainage area with the major confluence of offsite drainage happening at an existing bridge crossing that conveys the WFJCC flows southerly across Fontaine Boulevard. These flows continue south through the Corvallis site until they enter the Glen at Widefield Subdivision Filing No. 9. Two more natural channels run through the site, draining north to south, and join with the WFJCC after they have left the Corvallis development. The West Fork of Jimmy Camp Creek covers a total of 4 square miles. The developed area for the site of 297-acres is approximately 11.6% of the total drainage area within the WFJCC.



## ***B. COMPLIANCE WITH DBPS***

This study complies with the latest DBPS study (*WFJCC DBPS*) of the West Fork Jimmy Camp Creek basin dated October 2003. All developed runoff from the site will be detained and released at pre-development peak rates, and the water quality volume will be treated. Both as determined by the UDFCD detention spreadsheet UD-Detention.

## ***C. GEOLOGY***

The majority of the site is currently undeveloped and consists of natural vegetative land cover, as well as multiple natural creeks.

Soils can be classified in four different hydrologic groups, A, B, C, or D to help predict storm water runoff rates. Hydrologic group “A” is characterized by deep, well-drained coarse-grained soils with a rapid infiltration rate when thoroughly wet and having a low runoff potential. Group “D” typically has a clay layer at or near to the surface, or a very shallow depth to impervious bedrock and has a very slow infiltration rate and a high runoff potential. See Soils Map; Appendix D. Table 1.1, below, indicates which soil types are present in the development area:

***Table 1.1 – NRCS Soil Survey for El Paso County***

<b><i>Soil ID Number</i></b>	<b><i>Soil</i></b>	<b><i>Hydrologic Classification</i></b>	<b><i>Permeability</i></b>	<b><i>Percent on Site</i></b>
30	Fort Collins Loam (0% - 3% slopes)	B	Moderately Rapid	3.9%
52	Manzanst Clay Loam (0% - 3% slopes)	C	Low Rapidity	1.8%
56	Nelson-Tassel Fine Sandy Loams (3% - 18% slopes)	B	Moderately Rapid	34.5%
59	Nunn Clay Loam (0% - 3% slopes)	C	Low Rapidity	16.2%
75	Razor-Midway Complex	D	Very Low Rapidity	0.9%
86	Stoneham Sandy Loam (3% - 8% slopes)	B	Moderately Rapid	35.6%
101	Ustic Torrfluvents, Loamy	B	Moderately Rapid	0.8%
108	Wiley Silt Loam (3% - 9% slopes)	B	Moderately Rapid	6.3%

## ***D. GROUNDWATER***

According to the Geo-tech report for the site, groundwater levels vary. There is some seasonal and temporary raising of the water table along the FMIC and natural ditches. This fluctuation is likely due to irrigation water releases during the growing season; therefore, it is anticipated that the rerouting of the FMIC ditch via storm sewer, described in Section F below, will mitigate some of the water table fluctuations. Groundwater will be mitigated for in the construction plans as recommended in future Geo-tech reports which will be referenced in the appropriate future PDR/FDRs.



## ***E. LAND USES***

Presently, the site is unplatted and consists of undeveloped land. Corvallis is a proposed planned unit development (PUD) which includes both residential and commercial uses. Development of utilities and internal roadways are to be included in this parcel.

## ***F. UTILITIES AND ENCUMBERANCES***

- **Storm Sewer:** Existing storm sewer includes a 30-inch CMP culvert that crosses Fontaine Boulevard. In addition, WFJCC and associated proposed storm infrastructure will run through the site. Sizing is as described within this report and subject to change as site design progresses.
- **Sanitary Sewer:** An existing 24-inch sanitary sewer main lies within the intersection of Marksheffel Road and Lorson Boulevard near the site's southeast corner which will take flow east of the ridge internal to Corvallis Development. There is also an existing 12-inch sanitary sewer main which runs north-south through the site that will tie into the sanitary system at The Glen at Widefield development to the south of the site and will take the site's internal sanitary flow west of the ridge.
- **Gas:** Gas service to the proposed development will be provided by Black Hills Energy through the extension of the existing gas main infrastructure that currently lies adjacent to the site. No encumbrance to the project is anticipated.
- **Water:** The following existing water mains surround the site: a 16-inch water main in Marksheffel Road, a 24-inch water main in Spring Glen, a 12-inch water stub at Dutch Loop, and an 8-inch water main at Fontaine Boulevard near Cottonwood Grove. A network of new 12-inch and 8-inch water mains will be constructed throughout the Corvallis site to provide looping and water services to the development.
- **Electric:** There is existing overhead electric power in Fontaine Boulevard along the north side of the property and along the site's western property line. Underground electric power is also located within the residential developments to the south and east of the site. Electric service will be provided to the Corvallis Development by extending underground electric throughout the subdivision for residential and commercial services. No encumbrance to the project is anticipated.
- **Communications:** Underground communication lines currently serve the residential neighborhoods adjacent to the project site which will be extended underground to serve Corvallis Development. No encumbrance to the project is anticipated.
- **Irrigation:** There is an existing FMIC irrigation ditch meandering through both the east and west portions of the site. Both sections of the FMIC ditch running through the Corvallis site will be rerouted via 60-inch storm pipes sized to convey the 60 cfs that FMIC has indicated as a peak irrigation flow. Due to the lack of grade in the existing ditch, both sections of pipe are very flat with the west section at 0.06% and the east section at 0.08% grade. Entry and exit locations to and from the site will remain unchanged.

Written acceptance of planned modifications to FMIC ditch must be acquired from FMIC prior to beginning construction of these improvements. Pursuit of this acceptance is in progress. Documentation will be added to the MDDP when it is available.

Once completed, the FMIC approved irrigation conveyances will be privately owned and maintained by the FMIC.

### III. Hydrologic Analysis

#### A. GENERAL CONCEPT

The general concept for management of storm water for the proposed Corvallis development will be to provide clear conveyance through the property to the multiple onsite detention facilities to mitigate developed runoff flows from the site. Development of the site will require over-lot grading, roadway paving, residential and commercial construction which will increase the imperviousness of the property from existing conditions. The general drainage patterns will consist of positive drainage away from building sites, across lawns, parking lots, or open space, to curb and gutter within the internal roadways. Storm water within the roadways will be directed to inlet collection points, where it is captured and conveyed through a pipe network system to a full spectrum detention pond. Majority of offsite runoff will be either be diverted around the site or collected and directed separately through the site before being discharged at historic drainage locations and discharge.

The Water Quality Capture Volume (WQCV) is comprised within the proposed Full Spectrum Extended Detention Basin (EDB), where the “initial flush” of storm water will be drained over a 40-hour time period. The onsite ponds have been evaluated to reduce the developed flows from the site to a maximum of the historic peak flows. The detention pond has been sized and evaluated based upon the 100-year storm events in accordance with City Criteria.

#### B. METHODOLOGY

##### a. Rational Method

###### i. Method of Analysis

Storm sewer sizing for this project uses the Rational Method as recommended by the Drainage Criteria Manual for the minor and major storms for drainage basins less than 100-acres in size (Inlets will also be sized using this method in the subsequent FDRs). The Rational Method uses the following equation:

$$Q=C*i*A$$

Where:

Q	=	Maximum runoff rate in cubic feet per second (cfs)
C	=	Runoff coefficient
i	=	Average rainfall intensity (inches per hour)
A	=	Area of drainage sub-basin (acres)

###### ii. Runoff Coefficient

Coefficients from Table 6-6 of the Drainage Criteria Manual for developed land were utilized in the Rational Method calculations. See Appendix B for more information.

###### iii. Time of Concentration

The time of concentration consists of the initial time of overland flow and the travel time in a channel to the inlet or point of interest. A minimum time of concentrations of 5 minutes is utilized for urban areas.

iv. **Rainfall Intensity**

The hypothetical rainfall depths for the 1-hour storm duration were taken from Table 6-2 of the Colorado Springs Drainage Criteria Manual. Table 3.1, below, lists the rainfall depth for the Major and Minor 1-hour storm events.

**Table 3.1 – Project Area 1-Hour Rainfall Depth**

Storm Recurrence Interval	Rainfall Depth (inches)
5-year	1.50
100-year	2.52

The rainfall intensity equation for the Rational Method was taken from Drainage Criteria Manual Volume 1 Figure 6-5.

**C. BASIN HYDROLOGY**

**EXISTING DRAINAGE CONDITIONS**

Under the existing conditions, the site flows in a general north to south pattern until reaching one of three low points. As such, the site has been divided into major basin delineations (west, central, east) which collect flow at these three discharge points, in conformance with the **WFJCC DBPS, MDDP, and FDRs** for the area.

**West Basin:**

Sub-basin OS-1 borders the site to the west and is comprised of large lot, single-family residential homes. Runoff from this site drains to the east until reaching the Corvallis boundary, represented at Design Point E1.

Sub-basin OS-2 borders the site to the northwest and consists of drainage on Fontaine Boulevard from the crown of the roadway to the south. These flows drain from the existing roadway high point to the east until reaching the existing low point at Design Point E2. In the existing conditions, this road corridor drainage connects with a 30-inch CMP that directs localized flows from the north underneath Fontaine Boulevard and discharging into the WFJCC.

Sub-basin EX-2 is an onsite, undeveloped basin that sheet flows in a general southwest to northeast pattern until it combines with Sub-basin OS-2 at Design Point E2. Runoff from this design point discharges directly into the WFJCC.

Sub-basin OS-3 is an offsite, undeveloped basin that drains to the southeast until reaching the WFJCC floodway at Design Point E3.

Sub-basin OS-4 is an offsite, undeveloped basin adjacent to the WFJCC which drains to the southeast until reaching Design Point E3.

In addition to the above listed sub-basin flows that reach Design Point E3, the approved **WFJCC DBPS** also specifies a Design Point 3020 which consists of the upstream flows, including the existing 30" CMP mentioned previously) collected in the WFJCC as it enters the Corvallis site. In a conservative effort, the approved existing **WFJCC DBPS** flows have been added to the previously described sub-basins to achieve the flows at Design Point E3.

Sub-basin EX-1 is comprised of the west quarter of the Corvallis site. Currently undeveloped, flows generated in this basin combine with offsite flows from Sub-basin OS-1 and drain in a general northwest to south east pattern until reaching the WFJCC at Design Point E4.

Sub-basin 1-D (Formerly OS-8) is now included in the project by the new Lacy ODP. Under existing conditions this area is agriculturally zoned and sheet flows from west to east until reaching the WFJCC at Design Point E4.

Sub-basin OS-5 contains the southern half of Fontaine Boulevard as it drains from an existing roadway high point to the west until discharging and combining with onsite drainage.

Sub-basin EX-3 accepts the flows from Sub-basin OS-5 and continues to drain from the northeast to southwest until reaching Design Point E5 at the site's southern border.

Flows from Design Points E4 and E5 combine at the West Basin's final discharge point, Design Point E8. This is located at the flowline of the WFJCC drainageway as it leaves the Corvallis development and continues into the Glen at Widefield development located to the south. In both the approved **WFJCC DBPS** and **MDDP**, the flowrates at this point are  $Q_5 = 601$  cfs and  $Q_{100} = 2216$  cfs. As previously mentioned, rational calculations were performed for all onsite basins and added to the **MDDPA** Design Point R3030 existing condition flows ( $Q_5 = 347$  cfs and  $Q_{100} = 1761$  cfs) located at the WFJCC entrance into the site. This results in Design Point 8 flows of  $Q_5 = 403.5$  cfs and  $Q_{100} = 2040.7$  cfs. The previously approved **WFJCC DBPS** and **MDDP** will govern on the discharge flows at this point.

A summary of the existing basins and design points contributing to the West Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions Map.

West Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
<b>OS-1a</b>	38.5	19.2	70.9
<b>OS-1b</b>	38.3	12.3	47.7
<b>OS-2</b>	1.0	3.9	7.1
<b>OS-3</b>	1.9	0.6	4.0
<b>OS-4</b>	18.3	3.3	21.8
<b>OS-5</b>	0.8	3.2	5.8
<b>OS-8</b>	22.1	4.2	28.1
<b>EX-1</b>	67.9	9.0	60.3
<b>EX-2</b>	10.3	2.5	17.0
<b>EX-3</b>	51.9	8.2	54.8

West Basin		
Design Point	Peak Flows	
	5-Year	100-Year
<b>E1: OS-1</b>	25.3	98.5
<b>E2: OS-2, EX-2</b>	5.4	22.5
<b>E3: E2, OS-3, OS-4</b>	6.5	34.4
<b>E4: E1, E3, EX-1, OS-8</b>	46.3	222.3
<b>E5: OS-5, EX-3</b>	10.2	57.5
<b>E8: E4, E5, +DPBS3020</b>	403.5	2040.7

### ***Central Basin***

Sub-basin EX-4 is an onsite, undeveloped portion of land that drains from the northeast to the southwest until reaching Design Point E6, the final discharge point of the Central Basin.

This discharge point is centrally located on the southern border of the Corvallis development. An existing area inlet and corresponding 48-inch RCP collects the flows ( $Q_5 = 7.2$  cfs and  $Q_{100} = 48.1$  cfs) and conveys them directly to the WFJCC. Per the approved FDR for the Glen at Widefield Filing No. 9, this point collects 44.8 cfs in the 5-year storm and 163 cfs in the 100-year storm. As with Design Point E8, the allowable release of flows for this point are set by the approved ***WFJCC DPBS*** and ***MDDP***.

A summary of the existing basins and design points contributing to the Central Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions Map.

Central Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
EX-4	58.6	7.2	48.1

Central Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E6: EX-4	7.2	48.1

### ***East Basin***

Sub-basin OS-6 contains the southern portion of Fontaine Boulevard, to the crown of the roadway, that borders the site to the northeast. These flows are collected in a roadside swale and discharge onsite.

Sub-basin OS-7 consists of a single-family residential development located on the east side of the site. The back half of the existing residential lots drain to the south and west until discharging onto the Corvallis site.

Sub-basin EX-5 is the easternmost onsite basin. Currently undeveloped, this basin collects the flows from Sub-basins OS-6 and OS-7 and slopes from the northwest to the southeast until reaching Design Point E7.

The final discharge point for the East Basin (Design Point E7,  $Q_5 = 16.5$  cfs and  $Q_{100} = 93.1$  cfs) is located at the southeast corner of the site. These flows will be conveyed to the south in the existing roadside swale that runs parallel to Marksheffel Road. Discharge at this design point was set in the ***WFJCC DBPS*** and ***MDDP*** as  $Q_5 = 38$  cfs and  $Q_{100} = 153$  cfs and will control the allowable discharge in developed conditions.

A summary of all existing basins and design points, offsite and onsite, as well as a summary of design points contributing to the East Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions drainage maps.

East Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-6	0.8	3.2	5.8
OS-7	2.9	2.5	9.4
EX-5	86.5	12.8	86.3

East Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E7: EX-5, OS-6, OS-7	16.5	93.1

As previously mentioned, the Fountain Mutual Irrigation Company (FMIC) ditch system enters and exits the site periodically. The ditch in this area is approximated to have flows of 60 cfs as it meanders through the Corvallis site. This MDDP follows the guidelines previously set in the **WFJCC DPBS** that states, “Existing and proposed runoff was assumed to be passed over or under the ditch in the hydrologic modeling of the basin. There was no diversion of runoff by the ditch assumed in compilation of the hydrologic model for this basin.” As such, no additional drainage from the site is anticipated to be conveyed by the FMIC and all flows released into the ditch are assumed to remain within the canal. There is a possibility of a bypass pipeline being constructed that will convey flows from Big Johnson Reservoir to the east side of Marksheffel Road, near Jimmy Camp Creek, however this has not been considered for this report.

#### **DEVELOPED DRAINAGE CONDITIONS**

As explained in the existing conditions, the developed site drainage will also discharge at three site low points and has been broken down into three drainage basins for clarity. These design points have been specified in the **WFJCC DBPS** and subsequent reports as the discharge points from the Corvallis development. Runoff from the developed site will conform to these specified flows. Developed hydrology calculations for the basins and design points can be found in Appendix A. Preliminary hydraulic calculations have been completed for the anticipated trunk mains. Storm infrastructure internal to the sub-basins will be completed with each filing’s Final Drainage Report.

#### ***West Basin:***

Sub-basin OS-1 previously explained in the existing conditions will continue to drain easterly until reaching the Corvallis site boundary. At this point, the offsite flows will either be conveyed via swale or pipe to the north and east until reaching Design Point E1. Preliminary calculations have been completed for this swale (OS-1 Swale) or pipe (OS-1 Pipe) and can be found in Appendix A. Once entering the Corvallis site, these offsite flows will be conveyed via storm drain to the east and south until reaching DP1. This drainage will be kept separate from any untreated, developed runoff and will therefore not require any detention or water quality treatment.

Sub-basin OS-2 collects the runoff from required improvements to Fontaine Boulevard, adjacent to the Corvallis development which will have the required improvements at the time of development. Runoff from the roadway crown to the south will be collected in the proposed curb and gutter and directed to required inlets at the road low point. From here, flows will be conveyed to Sub-basin 2 via proposed storm drain.

Sub-basin 1B includes both commercial and multi-family development at the northwest corner of the site. The commercial and multi-family parcels will each have their own onsite water quality and detention facilities, DF-1 and DF-2, respectively. Discharge from these facilities will be

released at prehistoric peak flow values as required per the City criteria. Treated flows leaving DF-1 will be conveyed to the south via an 18-inch storm drain until reaching DP1. Preliminary calculations for the ponds and storm drain have been calculated and can be found in Appendix A. Discharge from DF-2 will be conveyed to DP2 via a 24-inch storm drain.

Design Point DP1 combines Design Point E1 and Sub-basin 1B. At this point, treated flows combine with routed flows. In an effort to be conservative, the treated discharge has simply been added to the routed flow, resulting in 25.0 cfs and 107.0 cfs in the minor and major storms, respectively. These combined flows will be carried in a 36-inch storm drain to along Autumn Glen and Residential Collector A road corridors until reaching Design Point DP3.

Sub-basin 1A is comprised of 1/8 acre or less, single-family residential lots. Runoff generated from this basin will be conveyed via curb and gutter and storm drain eventually to be collected and conveyed via 42-inch storm sewer to DF-3 (at DP2).

Sub-basin 2 is planned for 1/8 acre (or less) single-family residential. Developed runoff will be directed to the south via curb, gutter, and proposed internal storm drains, crossing beneath Residential Collector A, until reaching Design Point DP2.

Sub-basin 3 will consist of undeveloped land and detention and water quality pond DF-3.

Detention facility DF-3 will collect developed runoff from Sub-basins 1A, **1D**, 2, 3, and OS-2 and will then release at historic rates via a 36-inch storm drain until combining with flows from DP 1 in a storm manhole where the combined flows will be conveyed via 54-inch storm sewer until reaching Design Point DP3.

Sub-basin 1-D (Formerly OS-8) is now included in the Corvallis development per the Lacy ODP. The developed portion of this sub-basin will sheet flow towards the adjacent road which will convey the flows towards curb inlets near DP2. The captured flows will be directed into DF-3 for water quality treatment and detention.

Sub-basin 7 will remain undeveloped open space in the proposed conditions and, therefore, does not require any detention or water quality. This sub-basin will drain to the south and west until reaching Sub-basin OS-4 and Design Point DP5.

Sub-basin OS-3 is unchanged from the existing conditions and will continue to drain to the south and east until reaching Design Point DP5.

Sub-basin OS-4 is unchanged from the existing conditions and will continue to drain to the south and west until reaching Design Point DP5.

As previously mentioned, flow at Design Point 5 (E3 in the existing conditions discussion) includes **WFJCC DBPS** Design Point 3020 existing flows. The approved **WFJCC DBPS** also recommends removal of the existing 30-inch CMP crossing Fontaine Boulevard and, instead, routing these flows to the east until reaching the WFJCC bridge crossing at the north side of Fontaine Boulevard. The DBPS includes calculations show that this crossing is adequately sized to handle the additional flows. As such, it has been assumed that the **WFJCC DBPS** Design Point 3020 flows include those from the 30-inch CMP, and all converge north of Fontaine

Boulevard. From here, Design Point DP5 flows continue south within the WFJCC floodway until reaching the West Basin discharge point at DP 7.

Sub-basin 5 will be a proposed single-family development with lot sizes equal or lesser than 1/8 of an acre. Developed runoff will be taken to the south and west by internal curb, gutter and storm drain. The collected stormwater will cross underneath Residential Collector A, until reaching Sub-basin 4.

Sub-basin 4 will be comprised of 1/8 acre, or less, single-family lots. This basin will accept flows from Sub-basin 6 and continue to direct them to the basin low point, located at the southwest corner, Design Point DP6. At this point, detention and water quality pond DF-4 will accept and treat the flows, then discharge into the WFJCC via a 24-inch storm drain.

The convergence of Design Points DP3, DP5, and DP6 results in the ultimate West Basin discharge point, DP7 ( $Q_5 = 391.0$  cfs and  $Q_{100} = 2006.1$  cfs). These flows are less than both the routed calculations completed for Design Point E8, as well as the previously approved and governing releases specified in the **WFJCC DBPS** and **MDDP**. Drainage from this point will continue to the south until reaching the Glen at Widefield developments.

A summary of the sub-basins and design points within the West Basin is shown below:

West Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-1a	38.5	12.7	49.3
OS-1b	38.3	12.3	47.7
OS-2	1.0	3.9	7.1
OS-3	1.9	0.5	3.5
OS-4	18.3	2.5	16.6
OS-5	0.8	3.2	5.8
1-D	22.1	18.4	40.5
1A	28.3	43.1	94.9
1B	15.9	51.4	99.3
2	26.9	40.5	89.2
3	7.5	2.7	13.6
4	17.0	25.9	53.8
6	10.0	15.5	34.1
7	19.3	2.6	17.8

West Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E1	21.7	84.4
DP1	25.3	110.3
DP2	127.1	311.7
DP3	33.6	185.2
DP4	2.6	17.8
DP5	352.6	1798.9
DP6	22.3	47.7
DP7	391.0	2006.1

DP7 Summary							
Approved DBPS/MDDP		Glen at Widefield FDR 9		MDDPA (Dev. Cond.)		MDDP (Pr. Cond.)	
5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
601.0	2216.0	601.0	2216.0	401.0	2020.0	391.0	2006.1



**Central Basin:**

Sub-basin OS-5 collects the runoff from required improvements to Fontaine Boulevard, adjacent to the Corvallis development which will have the required improvements at the time of development. Runoff from the roadway crown to the south will be collected in the proposed curb and gutter and directed to required inlets at the road low point. From here, flows will be conveyed to Sub-basin 9 via proposed storm drain.

Sub-basins 9 & 10 includes single-family development with lots equal to or less than 1/8 of an acre in size. Proposed curb, gutter, and storm drain will collect the developed runoff and direct it to the south, until reaching Residential Collector A. Flows will cross underneath this roadway and join with Sub-basin 10.

Sub-basin 11 is currently designated single-family residential. Runoff from this site will join with incoming Sub-basin 9 & 10 flows and continue to the south and west until crossing underneath the proposed Spring Glen Drive roadway, discharging into detention and water quality pond DF-5 at Design Point DP10. This basin is considered to be approximately 65 percent impervious per Table 6-3 of the USDCM.

Sub-basin 5 contains single-family residential units with maximum lot sizes of 1/8 acre. Developed runoff will be accumulated within the internal curb, gutter, and storm drain system until discharging into pond DF-5 at Design Point DP9.

Design Point DP11 is the ultimate discharge point for the Central Basin and consists of the historical release from proposed detention and water quality pond DF-5 ( $Q_5 = 6.6$  cfs and  $Q_{100} = 48.1$  cfs). This discharge point is comparative to Design Point E6 in the existing conditions. The prehistoric discharge is equal to the calculated routed flows in the existing conditions and well underneath the approved flows from the **WFJCC DBPS** and **MDDP**, as well as the anticipated flows per the Glen at Widefield Filing No. 9 FDR.

A summary of the sub-basins and design points within the Central Basin are summarized below:

Central Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-5	0.8	3.2	5.8
5	5.9	19.4	38.6
9	20.1	34.4	80.5
10	15.8	24.3	57.2
11	14.9	21.8	49.8

Central Basin		
Design Point	Peak Flows	
	5-Year	100-Year
DP8	45.8	106.9
DP9	33.4	74.7
DP10	54.9	123.8
DP11	6.6	48.1

DP11 Summary							
Approved DBPS/MDDP		Glen at Widefield FDR 9		MDDP (Ex. Cond.)		MDDP (Pr. Cond.)	
5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
48.0	163.0	44.8	163.0	7.2	48.1	7.2	48.1

***East Basin:***

Sub-basin OS-6 consists of the southern half of Fontaine Boulevard, to include the proposed improvements that will be required adjacent to the Corvallis development. Inlets will need to be designed to capture this flow and route it south to Sub-basin 12 at time of Final Drainage Report for the adjacent filing.

Sub-basin 8 is a proposed commercial development that will have its own onsite water quality and detention pond, DF-6. Once treated, the historic release will be directed to the west in an 18-inch storm drain, combining with discharges from DF-7 at DP 12a.

Sub-basin 12 is a proposed multi-family development that will convey drainage via proposed curb, gutter, and storm drain to the south and east until reaching Design Point DP12 at detention facility DF-7. This parcel will have its own onsite water quality and detention to treat its runoff as well as the runoff from Sub-basin OS-6. Treated runoff will be released at historical peak discharge by a 30-inch storm drain. This storm drain will combine with flows from Sub-basin 8 at DP 12a and continue to the south and east, separated from any untreated flows, until reaching Design Point DP15.

Sub-basin OS-7 is a large acre, single-family subdivision located at the Corvallis site's northeastern corner. Stormwater from the backs of these lots will drain through side lot swales until discharging onto Sub-basin 16 and eventually being treated in detention and water quality pond DF-9.

Sub-basin 16 is a proposed commercial development. Developed runoff will drain to the southeast via internal curb, gutter, and storm drain until reaching the onsite water quality and detention facility, DF-9. This pond will release the treated flow via a 36-inch storm drain, combining with the above-mentioned East Basin flows at DP15.

Treated flows from Design Point DP15 will be conveyed in a 42-inch storm drain until reaching Design Point DP16.

Sub-basin 13 is to be comprised of single-family housing. The lots within this basin are expected to have a maximum size of 1/8 acre. Internal site curb, gutter, and storm drain will direct the flows to the south and east until reaching Sub-basin 14.

Sub-basin 14 will also be single-family residential with lot sizes equal or less than 1/8 of an acre. Runoff internal to this basin, as well as the accepted flows from Sub-basin 13, will be routed via curb, gutter, and storm drain to the south and east until entering Sub-basin 15.

Sub-basin 15 is a proposed single-family subdivision with 1/8 acre, or less, lot sizes. Developed runoff from this basin (as well as Sub-basins 13 and 14) will be collected in the onsite curb, gutter, and storm drain and directed to the basin low point at the southeastern corner. At this point, detention and water quality facility DF-8 will accept the flows at Design Point DP14.

Sub-basin 17 is currently designated as commercial. Runoff from this site will be collected in curb, gutter, and onsite storm drain and directed to the west to discharge into detention and water quality pond DF-8 at Design Point DP14.

Discharge from DF-8 will be equal to or lesser than the historical peak discharge as required by the City. From here, flows will be conveyed to the south via a 36-inch storm drain until reaching Design Point DP16.

Design Point DP16 is the ultimate discharge for the East Basin. The combined flows calculated for this design point result in 12.8 cfs in the minor storm event and 110.1 cfs in the major storm event. In the existing conditions, this discharge point was estimated to have 16.5 cfs in the minor storm and 93.1 cfs in the major storm. However, the previously approved **MDDP** and **WFJCC DBPS** for the area specify an allowable release of 38 cfs for the 5-year storm and 153 cfs in the 100-year storm.

The current report in review with the City of Fountain for the Glen at Widefield Filing No. 11, which receives the discharge from Corvallis DP16 has proposed two 36-inch culverts to convey the drainage from the Corvallis East Basin to the roadside swale being constructed as a part of the Marksheffel Road improvements. The capacity of these culverts is 87.06 cfs. Refer to Appendix C for the structures (CV177) referenced from the Final Drainage Report for the Glen at Widefield Filing No. 11.

As basins tributary to the East Basin are designed, additional analysis will be required in order to confirm the downstream capacity available.

A summary of the sub-basins and design points within the East Basin are summarized below:

East Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-6	0.8	3.2	5.8
OS-7	2.9	2.5	9.4
8	6.5	28.7	52.2
12	17.2	28.3	62.4
13	5.2	10.6	23.3
14	11.1	18.5	40.6
15	17.6	30.1	66.2
16	32.5	96.9	184.8
17	3.3	14.6	26.5

Central Basin		
Design Point	Peak Flows	
	5-Year	100-Year
DP12	24.5	53.5
DP12a	3.2	28.8
DP13	20.4	44.9
DP14	35.3	76.2
DP15	7.8	65.8
DP16	12.8	110.1

DP16 Summary							
Approved DBPS/MDDP		Glen at Widefield FDR 11		MDDP (Ex. Cond.)		MDDP (Pr. Cond.)	
5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
38.0	153.0	N/A	87.1	16.5	93.1	12.8	110.1

## Full Spectrum Detention Facilities

In accordance with the City of Fountain drainage criteria, the proposed Corvallis development will provide onsite full spectrum detention facilities to mitigate developed drainage impacts. Detained flows will release at historic rates and drainage patterns. At this time, ponds in series are not anticipated. This requires treated flows and offsite flows to be conveyed separately from untreated flows. Further design will need to be done if this design intent changes. A breakdown of the required storage volume and historic release rates for each of the water quality and detention facilities are summarized below:

<b>PROPOSED WATER QUALITY AND DETENTION SUMMARY</b>							
<i>Corvallis</i>							
<i>Detention/ WQ Pond</i>	<i>TOTAL AREA (AC)</i>	<i>CONTRIBUTING BASINS</i>	<i>% IMPERVIOUS</i>	<i>VOLUME REQUIRED (AC-FT)</i>	<i>Q(5) DISCHARGE (cfs)</i>	<i>Q(100) DISCHARGE (cfs)</i>	<i>DESCRIPTION:</i>
<b>DF-1</b>	5.65	1B- COMMERCIAL	95%	0.89	<b>2.1</b>	<b>8.8</b>	<i>Northwest Commercial</i>
<b>DF-2</b>	8.25	1B-MULTIFAMILY	70%	1.00	<b>1.2</b>	<b>13.8</b>	<i>Northwest Multi- Family</i>
<b>DF-3*</b>	61.51	1A, <b>1D</b> , 2, 3, OS-2	65%	7.22	<b>8.3</b>	<b>74.9</b>	<i>West Single-Family (Slight over-detention to maintain flows listed in Glen at Widfield MDDP Amendment)</i>
<b>DF-4*</b>	23.14	4, 6	65%	2.64	<b>4.8</b>	<b>22.0</b>	<i>Southwest Single- Family</i>
<b>DF-5*</b>	57.54	5, 9, 10, 11, OS-5	70%	6.98	<b>6.6</b>	<b>48.1</b>	<i>South Single-Family &amp; School Site</i>
<b>DF-6</b>	6.50	8	95%	1.02	<b>0.2</b>	<b>9.3</b>	<i>Northeast Commercial</i>
<b>DF-7</b>	18.00	12, OS-6	70%	2.18	<b>3.0</b>	<b>19.5</b>	<i>Northeast Multi- Family</i>
<b>DF-8*</b>	37.24	13, 14, 15, 17	70%	4.51	<b>5.0</b>	<b>44.3</b>	<i>Southeast Single- Family &amp; Commercial</i>
<b>DF-9*</b>	35.45	16	80%	4.79	<b>4.8</b>	<b>46.3</b>	<i>Southeast Commercial Pond</i>

*Asterisk \* denotes "Sub-Regional" Detention. The other ponds are considered "Onsite" Detention.*

## IV. Hydraulic Analysis

### ***A. OVERVIEW, METHODOLOGY & DESIGN***

Developed sub-basins and proposed drainage improvements are depicted on the attached Developed Drainage Basin Map (DR02) in Appendix D. Preliminary hydraulic design calculations for sizing of onsite facilities are provided for in Appendix A. In general, the hydraulic criteria and intent are summarized as follows:

In accordance with City of Fountain drainage criteria, major drainage will be conveyed through the Corvallis development using a combination of open channels, underground storm sewer capacity and allowable street capacity. For local residential streets, the maximum allowable depth during the 100-year event is 8-inches or the extent of the street right-of-way such that buildings are not inundated at the ground line.

The interior roads will be graded with a minimum longitudinal slope of 1.0 percent. In accordance with the street spread calculations in the DCM, the allowable minor storm street capacity is 8 cfs per side for 6-inch ramp curb and 12 cfs per side for 6-inch vertical curb. The allowable major storm street capacity is approximately 36 cfs per side (72 cfs full width). Reference Appendix B for sizing chart.

Curb inlets (CDOT Type R or equivalent City approved 6-inch curb inlet type) will be specified where required for at-grade and sump collection point locations. Inlets will convey runoff to a storm sewer consisting of reinforced pipes (RCP) with a minimum pipe diameter of 18-inches. Preliminary storm sewer sizing has been provided based on full flow capacity at a minimum slope of 1.0 percent and can be referenced in Appendix A. Riprap stilling basins will be utilized at storm pipe outfalls. Detailed inlet, storm sewer and riprap sizing calculations will be provided with the Final Drainage Reports for each filing.

A preliminary hydraulic analysis been completed as part of this study to determine the required storm pipe sizing for the site trunk mains. Hydraulic grade lines (calculated in StormCAD and using head loss coefficients from Table 9-4 of the DCM) will be provided with either the FDR or along with construction drawings. Initial sizing of the onsite detention ponds was completed using UDFCD Detention Pond software for Extended Detention Basins. The ponds have been evaluated to determine the peak release rates from the proposed detention ponds and the storage required for the 100-year storm event. Most proposed storm pipes have been upsized to accommodate larger flows as a conservative design.

If further design of the site alters the design intent as discussed within this MDDP, an amendment will be required to show compliance with the City of Fountain criteria.

### ***B. FLOODPLAINS***

Per the *Flood Insurance Rate Map (FIRM) 08041C 0956 G and 08041C 0957 G*, effective date December 7, 2018, published by the Federal Emergency Management Agency (FEMA), a portion of Corvallis lies within the designated 100-year floodplain of Jimmy Camp Creek West Tributary. A FIRMette of the project area is included in Appendix D.

Per the approved **WFJCC DBPS**, as land is developed adjacent to the WFJCC (Corvallis-West Basin), channel improvements (and associated Channel Design Report) will be required.

**WFJCC DBPS** Map 4A (Appendix D) shows the existing 30-inch culvert to be removed north of Fontaine Boulevard and directed to the existing bridge crossing. The sections of the WFJCC that traverse through the Corvallis site are specified as 3030-2 and 3030-1. The **WFJCC DBPS** recommends channel improvements to include a rip-rap lined channel up to the 100-year water surface elevation as well as check dams at 150' intervals in both sections (These are anticipated to be replaced with less frequent grouted rip rap drop structures with larger drops). Actual channel design will differ from the DBPS recommendations slightly and will follow the governing channel design criteria at that time and likely act to preserve the existing wetlands (to be delineated in the future).

Creek improvements will be triggered when development within the sub-basins listed as a part of this MDDP's West Basin begins and will be paid for by the Metropolitan District via mill levees. After this trigger occurs, further investigation into the true creek requirements based on actual field conditions will be required.

A Letter of Map Amendment (LOMA) and/or Letter of Map Revision (CLOMR/LOMR) will be required once channel improvements are triggered by the above indicated criteria in order to show the revised extent of the regulatory floodplain through the site. The channel and improvements will be located within a tract and will be owned and maintained by the metro district. Maintenance access to the channel must also be provided in accordance with Channel Design Criteria.

## **V. Environmental Evaluations**

### ***A. WETLAND IMPACTS***

Per the U.S. Fish and Wildlife National Wetlands Inventory, there are freshwater emergent wetlands located onsite. *Wetland delineation will be required once channel improvements are triggered by future development in the Corvallis-West Basin.*

### ***B. STORMWATER QUALITY***

All onsite detention facilities shall be designed to accommodate water quality requirements. As the development of each parcel progresses, the detention guidelines outlined in this report are to be upheld.

Per the DCM Chapter 1, Section 4, the City of Fountain requires the UDFCD Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls.

***Step 1: Reduce runoff by disconnecting impervious area, eliminating “unnecessary” impervious area and encouraging infiltration into soils that are suitable.***

Site specific landscaping will be done on each lot to decrease the connectivity of impervious areas. Grass lined swales will be used where possible to allow ground infiltration. The open

space running along the existing gas right of way is a site-specific example of disconnection between impervious surfaces on this project.

**Step 2: *Treat and slowly release the WQCV.***

The proposed detention ponds meet or exceed the DCM standards for the release rates of Full Spectrum Detention Ponds for Water Quality Capture Volumes.

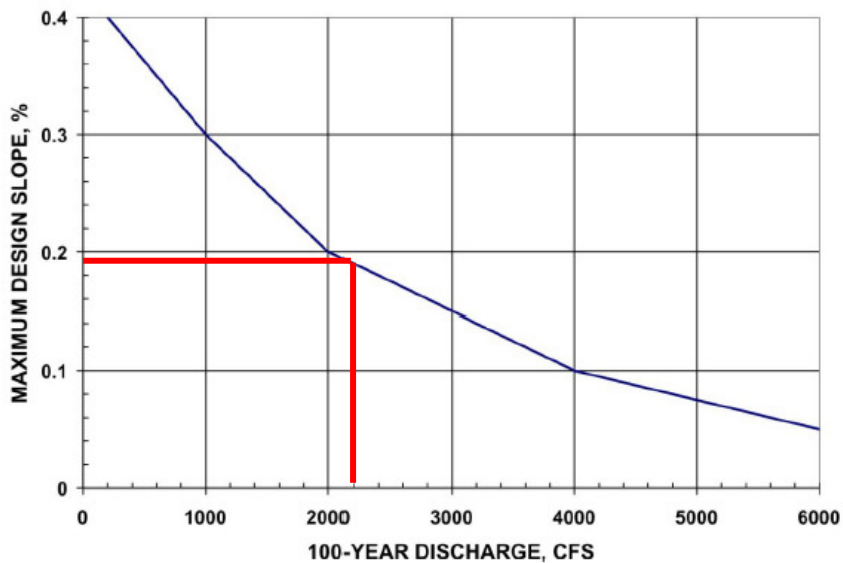
**Step 3: *Stabilize stream channels.***

Drainage fees paid at the time of platting will be utilized in the construction of the future stream improvements in the Jimmy Camp Creek Drainage Fee Basin according to the City.

**Onsite**

Based on the available LIDAR contour data for the site, the existing channel has a slope of approximately 0.65%. Field investigations of the site appear to show a stable channel. There are four pond areas in the channel bottom providing stilling and energy dissipation. Per the DCM Figure 12-4 and the indicated DBPS Q100 of 2216 cfs the anticipated design slope for channel changes is 0.19%. Using these two slopes and a channel length through the Corvallis site of 2,652 feet, we anticipate approximately 12 feet of drop structures will be required. This will likely mean three 4' drop structures designed and placed to preserve the existing ponds. Depth of drop may vary slightly if the future channel improvements recommend changes to the sinuosity of the stream bed to optimize the synergy between the channel and the development and thereby alter the length and slope of the channel through this development.

**Figure 12-4. Maximum Low-flow Channel Design Slope for Sand-bed Channels**



Another likely improvement will be rip rap slope protection along the outside banks on the bends of the channel meander to preserve the current or, if modifications are required, future planned stream path and protect adjacent infrastructure.

Field investigations of the channel show a series of three small, elongated ponds and one smaller pond.



**Figure 1-South Pond**

Southernmost pond above. The southernmost, as shown above, and the northernmost two ponds have flat and stable banks. (Note: Based on the South Pond's stable banks, improvements on the property to the west of Parcel D are not anticipated; however, if such improvements prove to be necessary, the developer will be required to coordinate with the owner of said property to achieve a construction easement or other form of access in order to complete channel improvements.)

Other ponds, as shown below, have short sections with steeper banks.



**Figure 2-North End of Middle Pond**

Sloughing of banks is very minimal and only evident in a couple of instances. One instance is visible in the upper right bank in the photo above. Most of the bare soil along the channel is caused by cattle grazing the area. The south end of the same pond shown in Figure 2 shows stable banks





**Figure 3-South end of Middle Pond**



**Figure 4-North Elongated Pond Looking South**

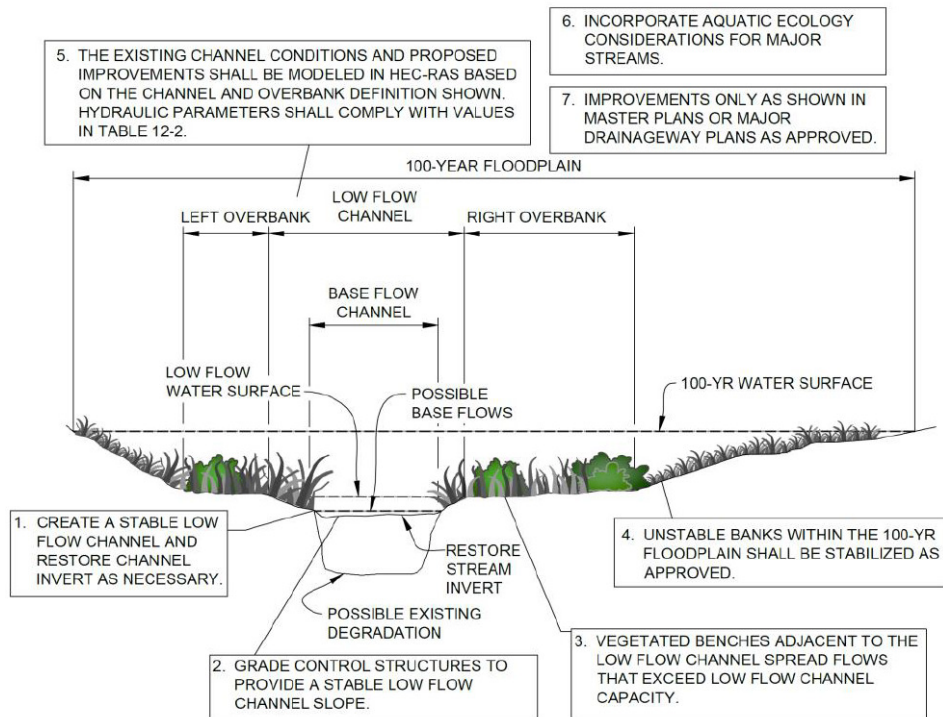
The northernmost of the elongated ponds is shown above. Note the shallow, steeper banks closer to the north end of the pond and the flatter banks towards the south end of the pond.



Figure 5-Northernmost Pond

Future improvements to the channel will likely involve laying back some of the steeper banks and providing a channel section more in line with the typical section indicated in the DCM.

Figure 12-3. Design Elements Associated With Major Natural Drainageways



The above section is already reflected in much of the channel. It is anticipated that future improvements will regrade the steeper banks of the channel to more closely match this section, add overbanks for lower probability flows where they are lacking, and armor the outside banks of bends in the stream. Drop structures will likely be constructed between the existing pond areas in an attempt to preserve, and limit disturbance to, the wetlands, but some minor modifications of the middle pond location may be required to facilitate the proposed crossing of the stream by Residential Collector A.

Given the existing apparent stability of much of the channel, it may be more optimal to use some buried drop structures in some locations of the channel design to preserve the existing channel conditions, spot fix areas with bank issues and place normal drop structures as appropriate to preserve the channel flow line and ponded areas.

The future channel design report will consider the above factors as well as any potential changes to the design criteria which have arisen in the interim.



**Figure 6 & 7-Jimmy Camp Creek-West Fork Looking North from South End of Property**

### Downstream of Corvallis

Just south of the south boundary of this proposed development Jimmy Camp Creek-West Fork discharges across what appears to be an existing utility maintenance road. HEC-RAS analysis of the stream using the 2018 LIDAR elevation info and the MDDPA flows indicates that both the 5-year and the 100-year events will surcharge the road (See section below). The analysis also indicates that the velocities anticipated across the structure appear to be within the DCM criteria for stable channel design in erosive soils ( $Q_{100} < 5.0$  ft/s and  $Q_5 < 3.5$  ft/s).

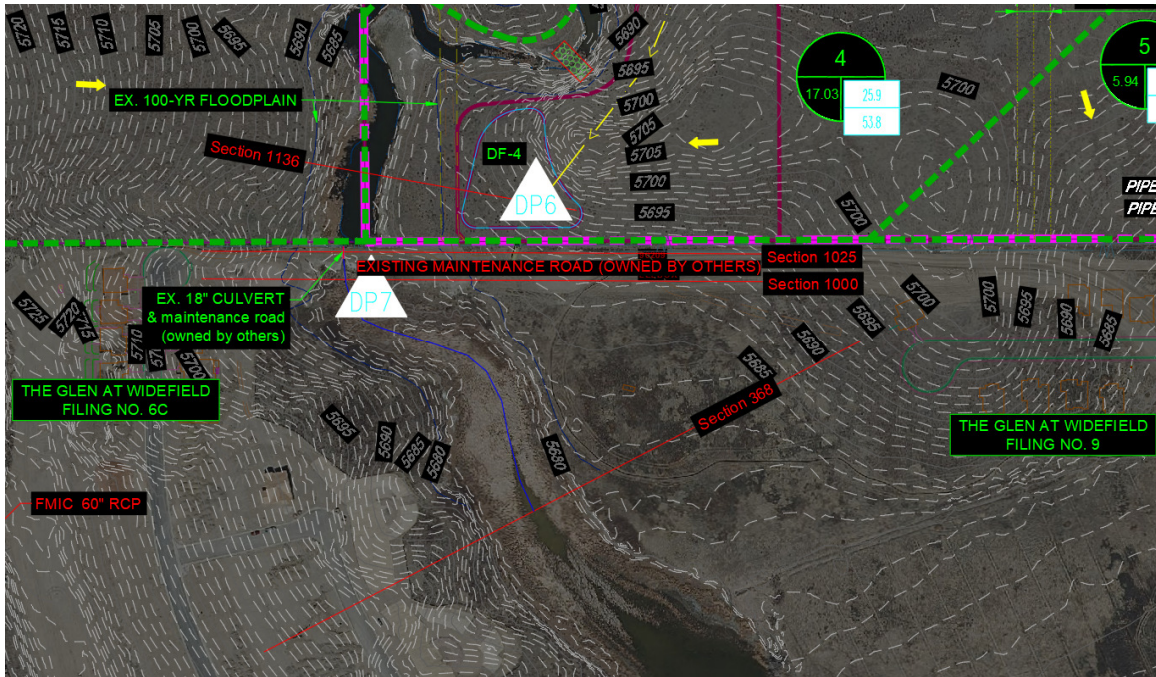


Figure 7 - HEC-RAS: Layout

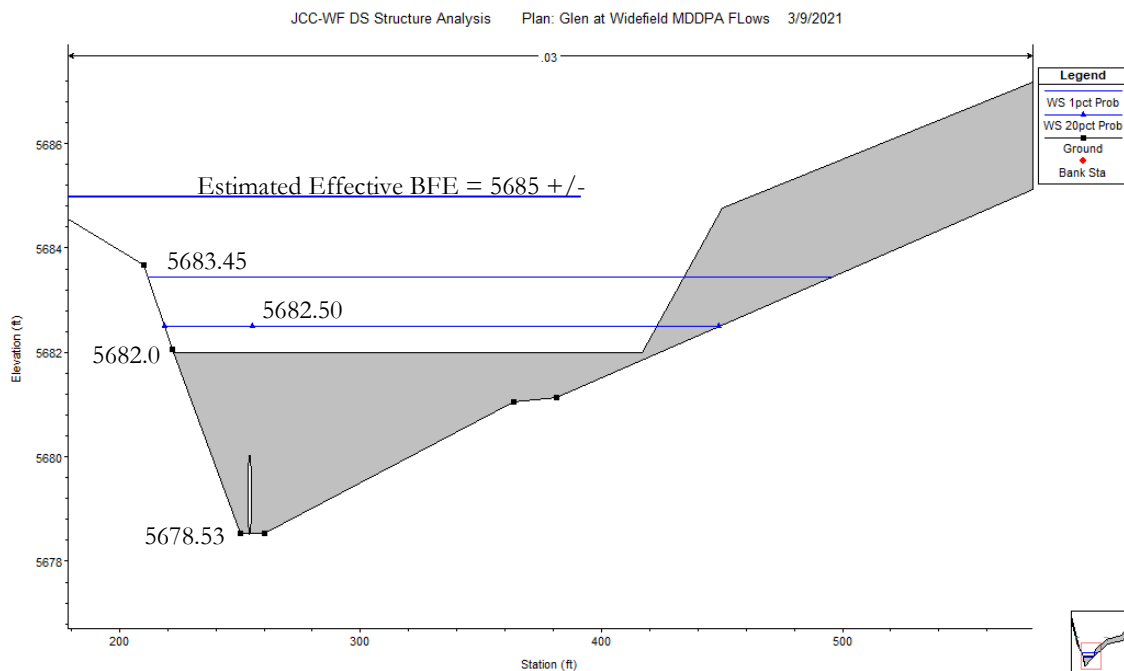


Figure 8 - HEC-RAS: Maintenance Road Section

Reach	River Sta	Profile	E.G. US. (ft)	W.S. US. (ft)	E.G. IC (ft)	E.G. OC (ft)	Min El Weir Flow (ft)	Q Culv Group (cfs)	Q Weir (cfs)	Delta WS (ft)	Culv Vel US (ft/s)	Culv Vel DS (ft/s)
WF	1012.5 Culvert #2	1pct Prob	5684.61	5684.54	5682.05	5684.61	5682.01	13.57	2017.97	2.09	7.68	7.68
WF	1012.5 Culvert #2	20pct Prob	5682.94	5682.94	5682.93	5682.94	5682.01	14.00	388.20	2.30	7.92	7.92

Figure 9 - HEC-RAS: Culvert Analysis Results

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
WF	1851	1pct Prob	2020.00	5680.00	5684.73		5684.77	0.000202	1.69	1219.95	358.39	0.15
WF	1851	20pct Prob	401.00	5680.00	5682.96		5682.97	0.000068	0.64	624.39	317.40	0.08
WF	1686	1pct Prob	2020.00	5677.20	5684.71		5684.75	0.000113	1.50	1390.34	401.09	0.12
WF	1686	20pct Prob	401.00	5677.20	5682.96		5682.96	0.000017	0.46	871.17	255.99	0.04
WF	1637	1pct Prob	2020.00	5677.20	5684.70		5684.74	0.000113	1.50	1387.99	400.80	0.12
WF	1637	20pct Prob	401.00	5677.20	5682.96		5682.96	0.000017	0.46	870.92	255.98	0.04
WF	1136	1pct Prob	2020.00	5678.70	5684.56		5684.65	0.000324	2.35	875.24	264.83	0.20
WF	1136	20pct Prob	401.00	5678.70	5682.94		5682.95	0.000043	0.72	553.86	166.40	0.07
WF	1025	1pct Prob	2020.00	5678.70	5684.54	5680.64	5684.61	0.000230	2.19	944.30	257.31	0.17
WF	1025	20pct Prob	401.00	5678.70	5682.94	5679.37	5682.94	0.000029	0.63	632.19	173.53	0.06
WF	1012.5	Culvert										
WF	1000	1pct Prob	2020.00	5678.53	5682.45	5681.69	5682.77	0.003526	4.58	441.30	226.99	0.58
WF	1000	20pct Prob	401.00	5678.53	5680.64	5680.09	5680.78	0.003246	3.09	129.86	113.29	0.51
WF	368	1pct Prob	2020.00	5678.00	5680.84	5679.70	5681.11	0.002002	4.15	486.25	188.99	0.46
WF	368	20pct Prob	401.00	5678.00	5679.09	5678.59	5679.18	0.002002	2.29	175.36	167.11	0.39

Figure 10 - HEC-RAS: Cross Section Analysis (Maintenance Road at Section 1012.5)

Jimmy Camp Creek-West Fork, immediately downstream of the above-mentioned structure, runs through the Glen at Widefield development in El Paso County. Specifically, the stream runs between Filings 6 and 9 of Glen at Widefield. (The photo below is looking southeasterly towards Filing 6.) As part of these developments, improvements to WFJCC were required and have been constructed. According to MDDPA, these improvements anticipated flows of Q5: 401 cfs and Q100: 2020 cfs. Our proposed discharge from the site is lower for both storms. (Q5: 396.4 cfs & Q100: 2009.1 cfs); therefore, the proposed Corvallis development complies with the design of the downstream infrastructure. Field visits to the site appear to confirm that the channel through Glen at Widefield has been stabilized. Please note the well vegetated channel in the photo looking southwesterly into Glen at Widefield below:



Figure 11- Jimmy Camp Creek-West Fork Looking South into Glenn at Widefield

Step 4: ***Implement source controls.***

During construction, the contractor will have designated concrete washout areas and will implement sediment control logs and inlet protection in order to control pollutants at their source. If long term stockpiling of materials is desired, further source controls must be designed to comply with the GEC and SWMP criteria.

***C. PERMITTING REQUIREMENTS***

A USACE 404 permit and PPRBD floodplain development permit are anticipated permits which will be required along with the future channel improvements.

**VI. Selected Plan**

***A. PLAN HYDROLOGY***

**Land Use**

In the approved ***WFJCC DBPS***, this area was specified as the “Crescent Heights Development” and was anticipated to have medium/high density residential as well as office and commercial. In compliance with the ***WFJCC DBPS***, Corvallis is anticipated to be a multi-use planned unit development. Anticipated developed uses include commercial, multi-family residential, and single-family residential (1/8 acre or less). Some portions of the site will remain as undeveloped open space. The land use map from the ***WFJCC DBPS*** is included in the Appendix D.

**Runoff**

The proposed 297-acre site is located entirely within the West Fork Jimmy Camp Creek. This tributary has a drainage area of 4 square miles according to ***WFJCC DBPS***. The developed area makes up less than 11% of the tributary’s drainage area.

As noted in Section II-C, 81 percent of the site is made up of Type B soils. Drainage coefficients for HSG A&B soil types used were per Table 6-6 in the DCM. Refer to Appendix A for specific runoff coefficient values.

**Flows**

According to ***WFJCC DBPS***, the Corvallis (Crescent Heights) development will discharge at 3 separate points. Per UD-Detention modeling of the proposed detention basin, detention from this project will either be equal to or reduce the Q100 (Major Storm) discharge from the property from the pre-development. As the proposed development is not projected to increase runoff from the site, no additional burden should be placed on downstream drainage and detention basins. Additionally, due to the large size of the offsite drainage areas, the peak discharges from the proposed detention ponds are significantly offset from the peak flows from the offsite basins.

The hydrology for the site, which has been provided above, shows that this development complies with the latest study (***WFJCC DBPS***).

***B. SYSTEM PRIORITIES/PHASING***

No phasing of the development has been provided at this time. Once development of any portion of the site begins, the owner will be responsible for providing detention and water quality in accordance with this ***MDDP*** and the ***WFJCC DBPS***, before releasing downstream.

Additionally, any proposed development within the West Basin (Which contains all portions of the first developable piece of property measured perpendicularly from the channel outwards.) within Corvallis will initiate the requirement for a channel design study of WFJCC through the development to be submitted to the City along with the PDR/FDR.

### ***C. GOVERNMENTAL AGENCY REQUIREMENTS***

Other than the USACE 404 permit, there are no external governmental agency requirements for this development. A final Drainage Report for each future phase of development will be presented to the City of Fountain with the development of the construction documents.

### ***D. MAINTENANCE REQUIREMENTS***

All proposed road and drainage construction within the Corvallis development will be performed to City of Fountain standards. Proposed roads and drainage facilities within the public right of way will be maintained by the City of Fountain upon acceptance of these facilities after the warranty period. The proposed detention ponds will be privately owned and maintained by the metropolitan district. Maintenance requirements for all stormwater quality and erosion control procedures will be outlined in individual Erosion Control and Storm Water Management Plans. A Maintenance Road (as well as access to this road from public right-of-way) for the portion of West Fork of Jimmy Camp Creek running through the Corvallis site must be provided.

### ***E. RECOMMENDATION FOR IMPLEMENTATION***

It is recommended that any development of the site initiates the implementation of the detention and water quality procedures that have been detailed in this report. In doing so, the developed conditions will produce runoff comparable to or lower than existing conditions, which allows continued adherence to ***WFJCC DBPS*** and protects downstream owners and facilities.

### ***F. EXCLUSIONS FROM ORIGINAL DBPS RECOMMENDATIONS:***

A few items which are recommended in the initial DBPS have fallen out of favor in the governing drainage design criteria and will not be implemented in the proposed development. One item is the on-stream detention pond located on Jimmy Camp Creek-West Fork (Detention Basin 3031). This will be replaced by on-site or sub-regional detention basins which are offline from West Fork Jimmy Camp Creek.

The other item is the concrete checks called out every 150-200 feet along the channels through the site. Current best practice channel design criteria do not recommend these checks in this application due to associated channel maintenance/stability issues. The general guidelines (described in Section V. B. Step 3) call for grouted rip rap drop structures which is a current best practice device for channel drops, however this item will be subject to the best practices at time of design.

Other than the two above items, proposed detention pond locations for this development do not match exactly the locations indicated in the DBPS, but fulfill the intent described in that report. The proposed development will discharge to downstream infrastructure at or below the pre-development rates indicated in the referenced studies.

## VII. Fee Development

### A. Construction Cost Opinion

An engineer's estimate of probable construction costs will be provided with the Final Drainage Report for each phase of the development. The developer will pay all capital costs for the proposed roadway and drainage facilities.

### B. Drainage Basin Fees

Drainage basin fees will be paid at the time of plat recordation. More detailed analysis of these fees will be completed in the appropriate PDR/FDR for each phase of the development.

#### a. Estimated Cost of Channel Improvements

<b>Corvallis PUD</b> <b>West Fork - Jimmy Camp Creek</b> <b>Engineer's Opinion of Probable Cost</b>					
BID ITEM NO.	DESCRIPTION OF BID ITEM	QUANTITY	PAY UNIT	UNIT PRICE	TOTAL COST OF BID ITEM
1	Mobilization	1	LS	\$100,000.00	\$100,000
2	Water Control & Dewatering	1	LS	\$60,000.00	\$60,000
3	Erosion & Sediment Control	1	LS	\$30,000.00	\$30,000
4	Clearing & Grubbing	1	LS	\$10,000.00	\$10,000
5	Drop Structures (4 ft)	4	EA	\$190,000.00	\$760,000
6	Seeding (Wetland, Riparian, Upland)	1	LS	\$20,000.00	\$20,000
7	Willow Stakes	1	LS	\$10,000.00	\$10,000
8	Erosion Control Blanket	500	SY	\$20.00	\$10,000
9	Earthwork (Onsite Cut & Fill)	1	LS	\$20,000.00	\$20,000
10	Soil Rip Rap (Outside Bends)	2,200	SY	\$100.00	\$220,000
11	CDOT Class II Road Base (Access Road)	765	CY	\$85.00	\$65,000
Subtotal					\$1,305,000
10% Contingency					\$130,500
Engineering					\$78,300
Estimated Total Cost					\$1,513,800
Developed Acres					297
Anticipated Cost / Developed AC.					\$5,093



Since the engineer has no control over the cost of labor, materials, equipment or services furnished by others, or over the contractor's method of determining prices, or over the competitive bidding or market conditions, the opinion of probable construction costs provided herein are made on the basis of the engineer's experience and qualifications and represents the best judgment as an experienced and qualified professional familiar with the construction industry. The engineer cannot, and does not guarantee that proposals, bid or actual construction costs will not vary from the opinion of probable costs.

Construction costs for channel improvements will be paid for by the Metropolitan District and provided by the developer. The Metropolitan District will be reimbursed via mill levees. To the extent possible, acquisition of easements, tracts or land will be the responsibility of the developer.

## **VIII. Summary**

As described above, this report demonstrates compliance with the governing DCM and DBPS and will comply with downstream drainage reports.

## **IX. References**

1. *City of Colorado Springs Drainage Criteria Manual*, City of Colorado Springs, May 2014
2. *Web Soil Survey of El Paso County Area, Colorado. Unites States Department of Agriculture Soil Conservation Service*, November 2015.
3. *Flood Insurance Rate Maps for El Paso County, Colorado and Incorporated Areas, Panel 958 of 1300, Federal Emergency Management Agency*, Effective Date December 7, 2018.
4. *Urban Storm Drainage Criteria Manual, Vol. 1-3* by Urban Drainage and Flood Control District (UDFCD), January 2016
5. *West Fork Jimmy Camp Creek Drainage Basin Planning Study (WFJCC DBPS)*, by Kiowa Engineering Corp. October 2003.
6. *Master Drainage Development Plan (MDDP) The Glen at Widefield*, by Kiowa Engineering Corp. December 1999.
7. *Master Drainage Development Plan Amendment (MDDPA) The Glen at Widefield*, by Kiowa Engineering Corp. June 2007.
8. *Final Drainage Report (FDR F9) The Glen at Widefield Filing No. 9*, by Kiowa Engineering Corp. July 2018.
9. *Final Drainage Report (FDR F11) The Glen at Widefield Filing No. 11*, by Kiowa Engineering Corp. December 2019.

# **APPENDIX A**

## ***HYDROLOGIC AND HYDRAULIC CALCULATIONS***

Project Name: Corvallis  
 Project Location: Fourrain, CO  
 Designer: NMS  
 Notes: Existing Conditions



Channel Flow Type Key  
 Heavy Meadow 2  
 Tillage/Field 3  
 Short Pasture and Lawns 4  
 Nearly Bare Ground 5  
 Grassed Waterway 6  
 Paved Areas 7

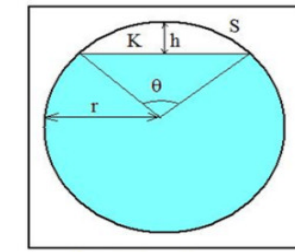
Average Channel Velocity: 5 ft/s (If specific channel vel is used, this will be ignored)  
 Average Slope for Initial Flow: 0.04 ft/ft (If Elevations are used, this will be ignored)

Basin	Description	Area		Rational 'C' Values												Flow Lengths				Initial Flow			Channel Flow					Tc	Rainfall Intensity & Rational Flow Rate								% Imp				
		SF	Acres	Surface Type 1 (Single-Family 1 & 1/3 Ac. Lots)			Surface Type 2 (Greenbelts & Agriculture)			Surface Type 3 (Single-Family 1/8 Ac. Lots & Multi-Family)			Surface Type 4 (Impervious)			Weighted C-Factor		Initial	True Initial	Channel	True Channel	High Point	Low Point	Average	Initial	High Point	Low Point		Average	Channel Flow Type (See Key above)	Velocity	Channel	i2	Q2	i5	Q5		i10	Q10	i100	Q100
		C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C5	C100	Area	C5	C100	Area	C5	C100	ft	Length ft	ft	Length ft	Elevation	Elevation	Slope	Tc (min)	Elevation		Elevation	Slope	Ground Type	(ft/s)	Tc (min)	(min)	in/hr	cfs		in/hr	cfs	in/hr	cfs
OS-1a	Single Family > 2.5 Acres (12% Impervious (min.))	1,675,407	38.46	0.20	0.44	0.09	0.36	1474358	0.45	0.59	0.90	0.96	201049	0.19	0.44	300	300	2,290	2290	5,807	5,800	0.023	22.2	5800	5,725	3.28	4	1.3	30.5	52.7	1.4	10.1	1.7	12.7	2.0	14.8	2.9	49.3	13.8%		
OS-1b	Single Family > 2.5 Acres (12% Impervious (min.))	1,668,351	38.30	0.20	0.44	0.09	0.36	1468149	0.45	0.59	0.90	0.96	200202	0.19	0.44	900	300	1,871	2471	5,894	5,820	0.082	14.6	5820	5,780	2.14	4	1.0	40.6	65.2	1.3	9.7	1.7	12.3	1.9	14.3	2.8	47.7	13.8%		
OS-2	Frontage Backward to cross of road	42809	0.98	0.20	0.44	0.09	0.36	42809	0.45	0.59	0.90	0.96	42809	0.90	0.96	25	25	1362	1362	5738	5757	0.040	1.2	5757	5719	2.79	7	3.3	6.9	8.1	3.5	3.1	4.4	3.9	5.2	4.6	7.4	7.1	100.0%		
OS-3	Offsite undeveloped parcel	80878	1.86	0.20	0.44	0.09	0.36	80878	0.45	0.59	0.90	0.96	80878	0.90	0.96	170	170	275	275	5739	5718	0.124	10.7	5718	5703	5.45	3	1.2	3.9	14.6	2.8	0.5	3.5	0.6	4.1	0.7	5.9	4.0	2.0%		
OS-4	Offsite undeveloped parcel	797941	18.32	0.20	0.44	0.09	0.36	797941	0.45	0.59	0.90	0.96	797941	0.90	0.96	301	300	1018	1019	5732	5719	0.043	20.1	5719	5696	2.26	3	0.7	22.9	43.0	1.6	2.6	2.0	3.3	2.3	3.8	3.3	21.8	2.0%		
OS-5	Frontage Backward to cross of road	32917	0.76	0.20	0.44	0.09	0.36	32917	0.45	0.59	0.90	0.96	32917	0.90	0.96	25	25	1100	1100	5771	5770	0.040	1.2	5770	5740	2.73	7	3.3	5.6	6.8	3.7	2.6	4.7	3.2	5.5	3.8	7.9	5.8	100.0%		
OS-6	Frontage Backward to cross of road	33529	0.77	0.20	0.44	0.09	0.36	33529	0.45	0.59	0.90	0.96	33529	0.90	0.96	25	25	1100	1100	5771	5770	0.040	1.2	5770	5743	2.45	7	3.1	5.9	7.1	3.7	2.6	4.6	3.2	5.4	3.8	7.8	5.8	100.0%		
OS-7	Single Family Residential in east	126529	2.90	0.20	0.44	0.09	0.36	126529	0.45	0.59	0.90	0.96	126529	0.90	0.96	40	40	160	160	5708	5706	0.050	6.2	5706	5702	2.50	4	1.1	2.4	8.6	3.4	2.0	4.3	2.5	5.1	3.0	7.3	9.4	7.0%		
EX-1	Offsite undeveloped parcel	961463	22.07	0.20	0.44	0.09	0.36	961463	0.45	0.59	0.90	0.96	961463	0.90	0.96	300	300	1055	1055	5731	5715	0.053	18.7	5715	5682	3.13	3	0.9	30.0	38.7	1.7	3.3	2.1	4.2	3.4	4.9	3.5	28.1	2.0%		
EX-2	West side of site	2959892	67.95	0.20	0.44	0.09	0.36	2959892	0.45	0.59	0.90	0.96	2959892	0.90	0.96	300	300	2266	2266	5753	5736	0.057	18.3	5736	5682	2.38	3	0.8	49.8	68.2	1.2	7.1	1.5	9.0	1.7	10.5	2.4	60.3	2.0%		
EX-3	Northeast corner	449242	10.31	0.20	0.44	0.09	0.36	449242	0.45	0.59	0.90	0.96	449242	0.90	0.96	300	300	350	350	5752	5738	0.047	19.6	5738	5719	5.43	3	1.2	5.0	24.6	2.1	2.0	2.7	2.5	3.2	3.0	4.5	17.0	2.0%		
EX-4	Central-west	2262585	51.94	0.20	0.44	0.09	0.36	2262585	0.45	0.59	0.90	0.96	2262585	0.90	0.96	300	300	1530	1530	5740	5728	0.040	20.6	5728	5688	2.61	3	0.8	31.6	52.2	1.4	6.5	1.7	8.2	2.0	9.5	2.9	54.8	2.0%		
EX-4	Central-east	2551274	58.57	0.20	0.44	0.09	0.36	2551274	0.45	0.59	0.90	0.96	2551274	0.90	0.96	300	300	2710	2710	5768	5756	0.040	20.6	5756	5685	2.62	3	0.8	56.0	76.6	1.1	5.7	1.3	7.2	1.6	8.3	2.3	48.1	2.0%		
EX-5	East side of site	3769253	86.53	0.20	0.44	0.09	0.36	3769253	0.45	0.59	0.90	0.96	3769253	0.90	0.96	300	300	1830	1830	5770	5765	0.017	27.6	5765	5686	4.32	3	1.0	29.4	57.0	1.3	10.2	1.6	12.8	1.9	15.0	2.7	86.3	2.0%		

Note: Q2, Q5 & Q10 are based on C5; Q25, Q50 & Q100 are based on C100



Design Point	Notes	Max Q (Q100) Proposed	Capacity Analysis	Storm Pipe		Percent of Pipe Capacity Used	n(full)	Slope (ft/ft)	n	Pipe Diameter (ft)	Width (ft) Box Culvert Only	Pipe Depth (inches)	Optimum Flow Depth (+/- 0.94 x D)	θ (Radians)	A (Sq. Ft.)	Wetted Perimeter (ft)	Velocity at Max Pipe Capacity
				Calculated Max Q for Pipe (CFS)	Storm Pipe												
E1	OS-1a and OS-1b	84.4	Adequate	105.4	Storm Pipe	80%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DP1	E1+DF-1 Release+DF-2 Release	107.0	Adequate	150.4	Storm Pipe	71%	0.013	0.010	0.013	4		48	3.76	0.990	12.259	10.587	12.27
1A	Sub-basin 1A	92.9	Adequate	105.4	Storm Pipe	88%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DP2	OS-2, 1A, 1D, 2, 3	283.4	Pressure Flow	272.7	Storm Pipe	104%	0.013	0.010	0.013	5		60	4.7	0.990	19.154	13.233	14.24
DP3	DP1+DP2 Treated (DF-3 Release)	181.9	Adequate	205.9	Storm Pipe	88%	0.013	0.010	0.013	4.5		54	4.23	0.990	15.515	11.910	13.27
DP4	7	17.8	Adequate	43.0	Storm Pipe	41%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
6	Sub-basin 6	34.1	Adequate	43.0	Storm Pipe	79%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
DP6	4, 6	47.7	Adequate	52.6	Storm Pipe	91%	0.013	0.015	0.013	2.5		30	2.35	0.990	4.788	6.617	10.99
DP8	9, 10, OS-5	106.9	Adequate	129.0	Storm Pipe	83%	0.013	0.015	0.013	3.5		42	3.29	0.990	9.385	9.263	13.75
DP9	DP8, 5	74.7	Adequate	105.4	Storm Pipe	71%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DP11	DP10 Treated (DF-5 Release)	48.1	Adequate	69.8	Storm Pipe	69%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DP12a	DP-12 Treated (DF-7 Release) & DF-6 Release	28.8	Adequate	43.0	Storm Pipe	67%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
13	Sub-basin 13	23.3	Adequate	43.0	Storm Pipe	54%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
DP13	13, 14	44.9	Adequate	69.8	Storm Pipe	64%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DP15	DP12 Treated (DF-7Release), 16 Treated (DF-9 Release), & DF6 Release	65.8	Adequate	105.4	Storm Pipe	62%	0.013	0.010	0.013	3.5		42	3.29	0.990	9.385	9.263	11.23
DF-1	PRELIMINARY DETENTION POND OUTFALL PIPE	8.8	Adequate	11.0	Storm Pipe	80%	0.013	0.010	0.013	1.5		18	1.41	0.990	1.724	3.970	6.38
DF-2	PRELIMINARY DETENTION POND OUTFALL PIPE	13.8	Adequate	23.7	Storm Pipe	58%	0.013	0.010	0.013	2		24	1.88	0.990	3.065	5.293	7.73
DF-3	PRELIMINARY DETENTION POND OUTFALL PIPE	74.9	Pressure Flow	69.8	Storm Pipe	107%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DF-4	PRELIMINARY DETENTION POND OUTFALL PIPE	22.0	Adequate	23.7	Storm Pipe	93%	0.013	0.010	0.013	2		24	1.88	0.990	3.065	5.293	7.73
DF-5	PRELIMINARY DETENTION POND OUTFALL PIPE	48.1	Adequate	69.8	Storm Pipe	69%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DF-6	PRELIMINARY DETENTION POND OUTFALL PIPE	9.3	Adequate	11.0	Storm Pipe	85%	0.013	0.010	0.013	1.5		18	1.41	0.990	1.724	3.970	6.38
DF-7	PRELIMINARY DETENTION POND OUTFALL PIPE	19.5	Adequate	43.0	Storm Pipe	45%	0.013	0.010	0.013	2.5		30	2.35	0.990	4.788	6.617	8.97
DF-8	PRELIMINARY DETENTION POND OUTFALL PIPE	44.3	Adequate	69.8	Storm Pipe	63%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13
DF-9	PRELIMINARY DETENTION POND OUTFALL PIPE	46.3	Adequate	69.8	Storm Pipe	66%	0.013	0.010	0.013	3		36	2.82	0.990	6.895	7.940	10.13



Partially Full Pipe Flow Parameters (More Than Half Full)

$$r = D/2$$

$$h = 2r - y$$

(hydraulic radius)

$$R = A/P$$

(Manning Equation)

$$Q = (1.49/n)(A)(R^{2/3})(S^{1/2})$$

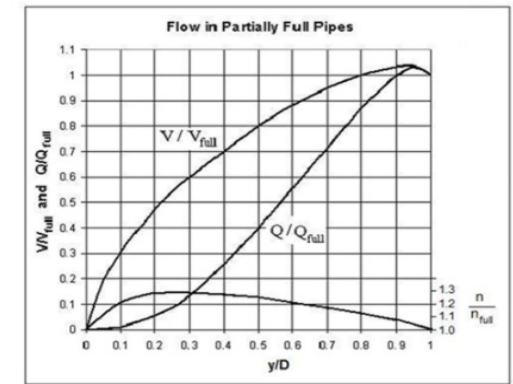
$$V = Q/A$$

$$\theta = 2 \arccos \left( \frac{r-h}{r} \right)$$

$$A = \pi r^2 - \frac{r^2(\theta - \sin \theta)}{2}$$

$$P = 2\pi r - r*\theta$$

Equation used for  $n/n_{full}$ :  $n/n_{full} = 1.25 \cdot (y/D - 0.5)^{0.5}$  (for  $0.5 \leq y/D \leq 1$ )



Flow in Partially Full Pipes

**PROPOSED WATER QUALITY AND DETENTION SUMMARY**

**Corvallis**

<i>Detention/W Q Pond</i>	<i>TOTAL AREA (AC)</i>	<i>CONTRIBUTING SUB-BASINS</i>	<i>% IMPERVIOUS</i>	<i>VOLUME REQUIRED (AC-FT)</i>	<i>Q(5) DISCHARGE (cfs)</i>	<i>Q(100) DISCHARGE (cfs)</i>	<i>DESCRIPTION:</i>	<i>Discharge Pipe Size</i>
DF-1	5.65	1B-COMMERCIAL	95%	0.89	2.1	8.8	Northwest Commercial	18.0
DF-2	8.25	1B-MULTIFAMILY	70%	1.00	1.2	13.8	Northwest Multi-Family	24.0
DF-3*	81.82	1A, 1D, 2, 3, OS-2	65%	7.22	8.3	74.9	West Single-Family (Slight over-detention to maintain Q listed in Glen at Widefield MDDP Amendment)	36.0
DF-4*	23.14	4, 6	65%	2.64	4.8	22.0	Southwest Single-Family	24.0
DF-5*	57.54	5, 9,10, 11, OS-5	70%	6.98	6.6	48.1	South Single-Family & School Site	36.0
DF-6	6.50	8	95%	1.02	0.2	9.3	Northeast Commercial	18.0
DF-7	18.00	12, OS-6	70%	2.18	3.0	19.5	Northeast Multi-Family	30.0
DF-8*	37.24	13, 14, 15, 17	70%	4.51	5.0	44.3	Southeast Single-Family & Commercial	36.0
DF-9*	35.45	16	80%	4.79	4.8	46.3	Southeast Commercial Pond	36.0

# Culvert Calculator Report

## CV177

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	5,688.70 ft	Headwater Depth/Height	1.13
Computed Headwater Elevation	5,688.17 ft	Discharge	87.06 cfs
Inlet Control HW Elev.	5,688.06 ft	Tailwater Elevation	5,684.52 ft
Outlet Control HW Elev.	5,688.17 ft	Control Type	Outlet Control

Grades			
Upstream Invert	5,684.78 ft	Downstream Invert	5,684.52 ft
Length	77.00 ft	Constructed Slope	0.003377 ft/ft

Hydraulic Profile			
Profile	M2	Depth, Downstream	2.15 ft
Slope Type	Mild	Normal Depth	N/A ft
Flow Regime	Subcritical	Critical Depth	2.15 ft
Velocity Downstream	8.03 ft/s	Critical Slope	0.005723 ft/ft

Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	5,688.17 ft	Upstream Velocity Head	0.74 ft
Ke	0.20	Entrance Loss	0.15 ft

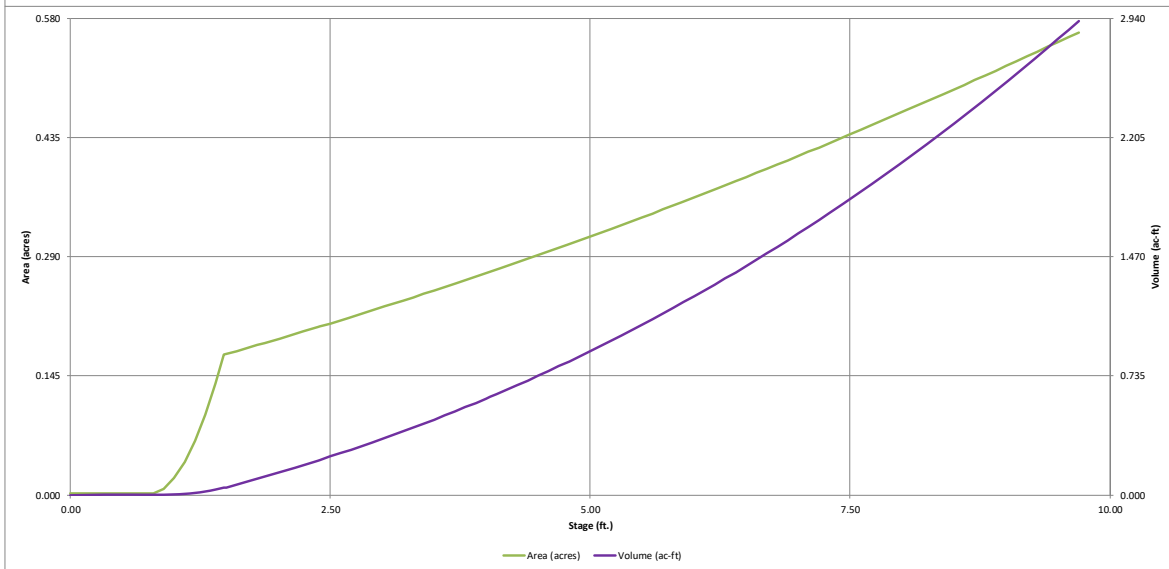
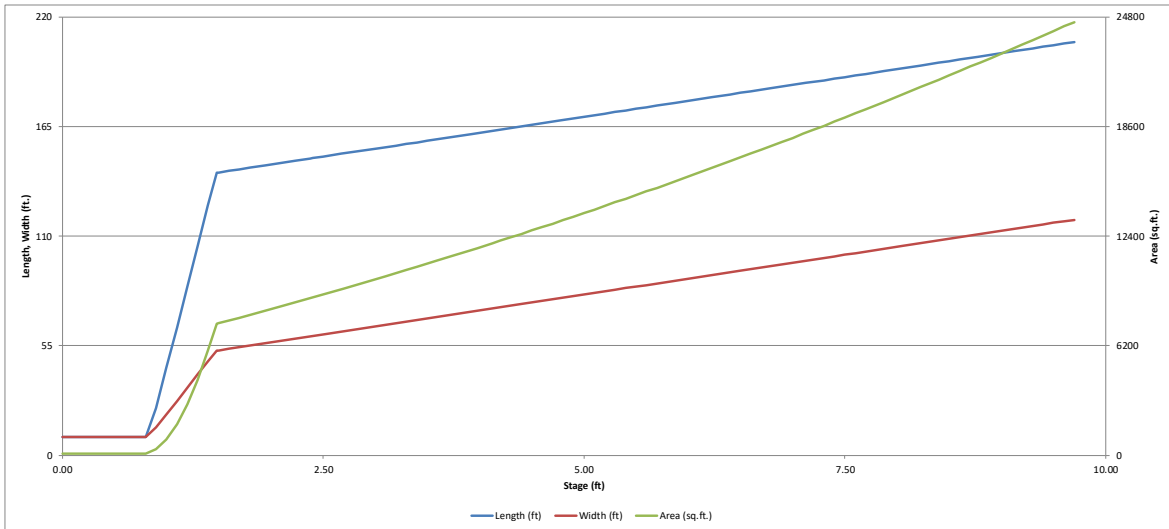
Inlet Control Properties			
Inlet Control HW Elev.	5,688.06 ft	Flow Control	Transition
Inlet Type	Beveled ring, 33.7° bevels	Area Full	14.1 ft <sup>2</sup>
K	0.00180	HDS 5 Chart	3
M	2.50000	HDS 5 Scale	B
C	0.02430	Equation Form	1
Y	0.83000		





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

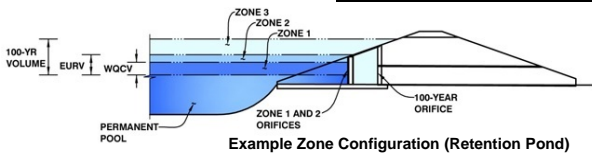
*MHFD-Detention, Version 4.02 (February 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

**Project:** Singer Ranch  
**Basin ID:** DF-1 (NW Commercial Pond)



**Example Zone Configuration (Retention Pond)**

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.38	0.211	Orifice Plate
Zone 2 (EURV)	4.04	0.394	Circular Orifice
Zone 3 (100-year)	5.00	0.281	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>0.885</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.38	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	9.50	inches
Orifice Plate: Orifice Area per Row =	0.73	sq. inches (diameter = 15/16 inch)

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	5.069E-03	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.79	1.59					
Orifice Area (sq. inches)	0.73	0.73	0.73					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.38	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.04	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	1.23	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.01	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.05	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))**

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H <sub>o</sub> =	4.04	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>i</sub> =	4.04	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	22.14	N/A	
Overflow Gate Open Area w/o Debris =	16.80	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	8.40	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	8.00	N/A	inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.76	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.39	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.46	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage =	4.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	7.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.79	feet
Stage at Top of Freeboard =	6.29	feet
Basin Area at Top of Freeboard =	0.38	acres
Basin Volume at Top of Freeboard =	1.33	acre-ft

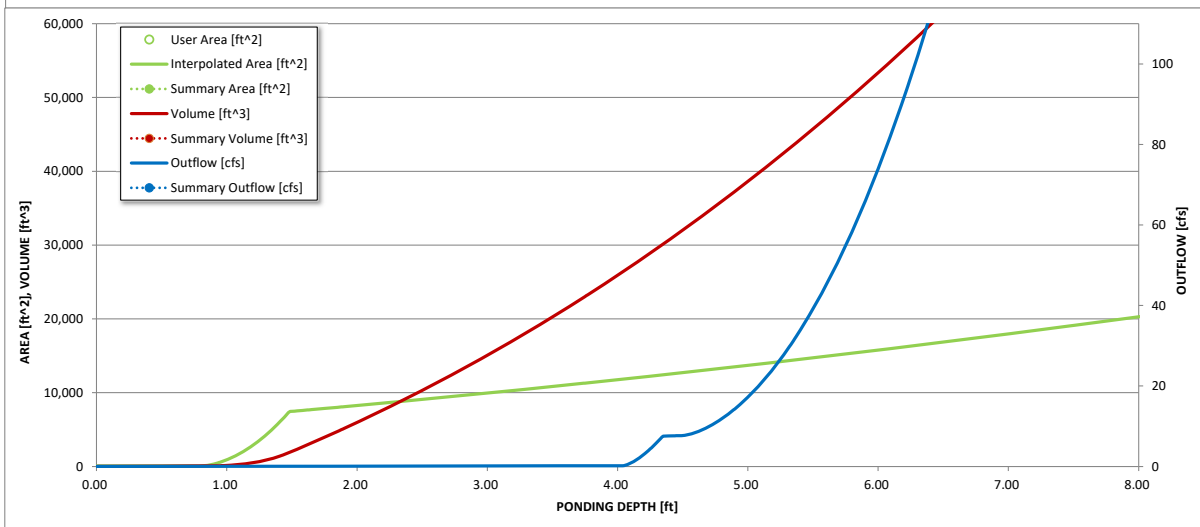
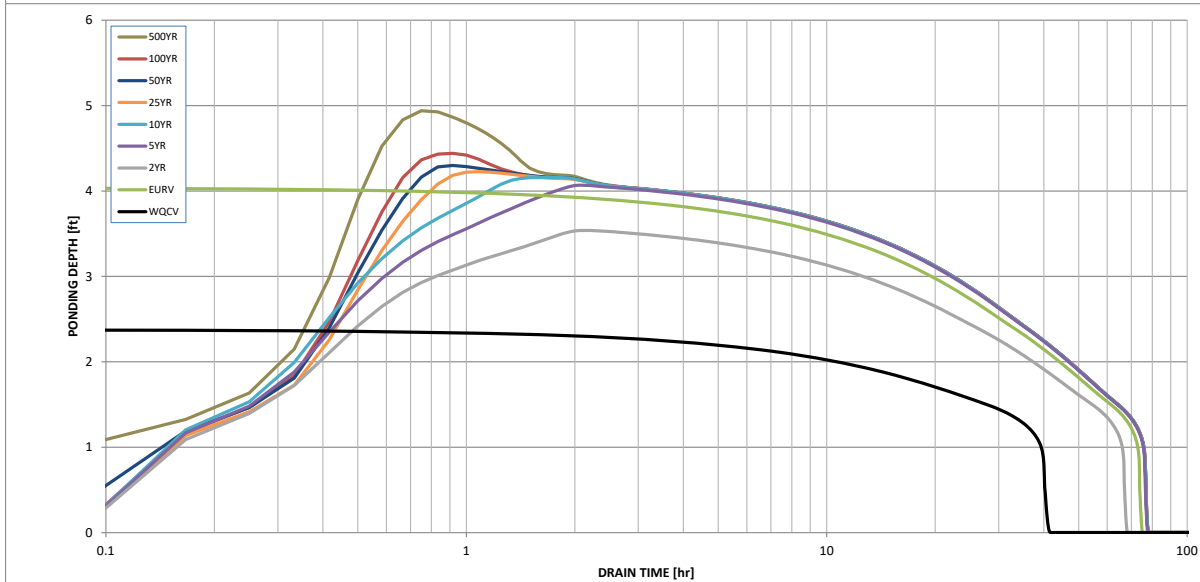
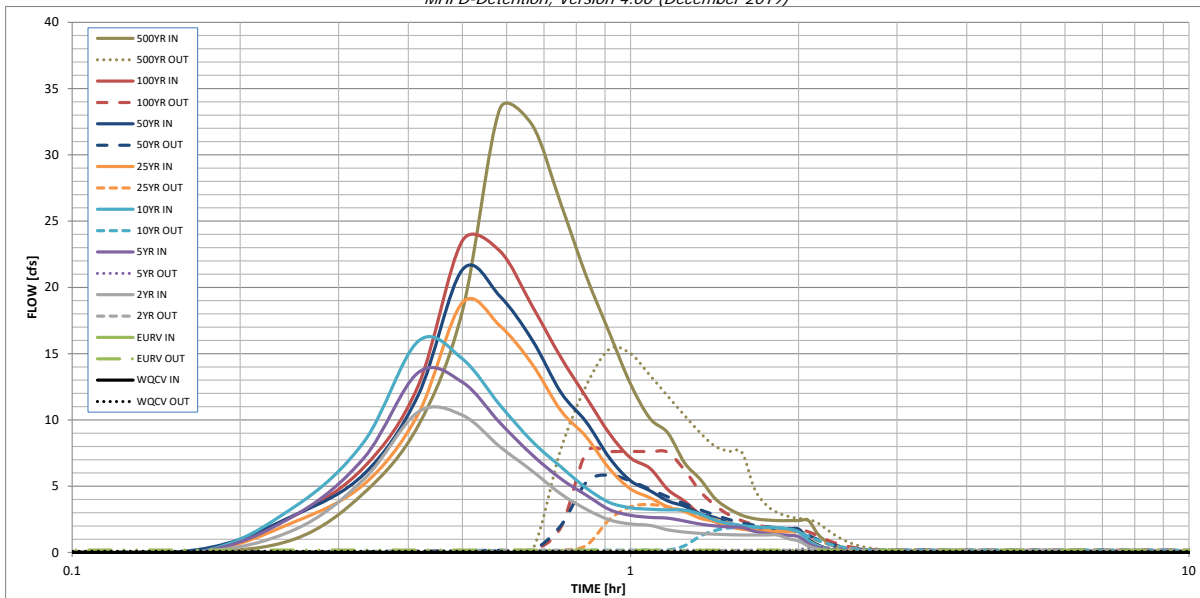
**Routed Hydrograph Results**

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.211	0.605	0.498	0.643	0.760	0.880	0.998	1.127	1.615
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.498	0.643	0.760	0.880	0.998	1.127	1.615
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.8	2.1	3.2	5.6	7.0	8.8	14.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.14	0.38	0.56	0.99	1.24	1.55	2.58
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	10.6	13.6	15.9	18.8	21.3	23.5	33.5
Peak Inflow Q (cfs) =	0.1	0.2	0.2	0.4	1.9	3.6	5.8	7.6	15.3
Peak Outflow Q (cfs) =	N/A	N/A	N/A	0.2	0.6	0.6	0.8	0.9	1.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.6	0.6	0.8	0.9	1.1
Structure Controlling Flow =	Vertical Orifice 1	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.1	0.2	0.3	0.4	0.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	69	63	71	70	69	68	68	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	66	75	75	74	74	73	72
Maximum Ponding Depth (ft) =	2.38	4.04	3.54	4.07	4.16	4.22	4.30	4.44	4.94
Area at Maximum Ponding Depth (acres) =	0.20	0.27	0.25	0.27	0.28	0.28	0.28	0.29	0.31
Maximum Volume Stored (acre-ft) =	0.212	0.606	0.473	0.611	0.636	0.655	0.675	0.718	0.865

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*

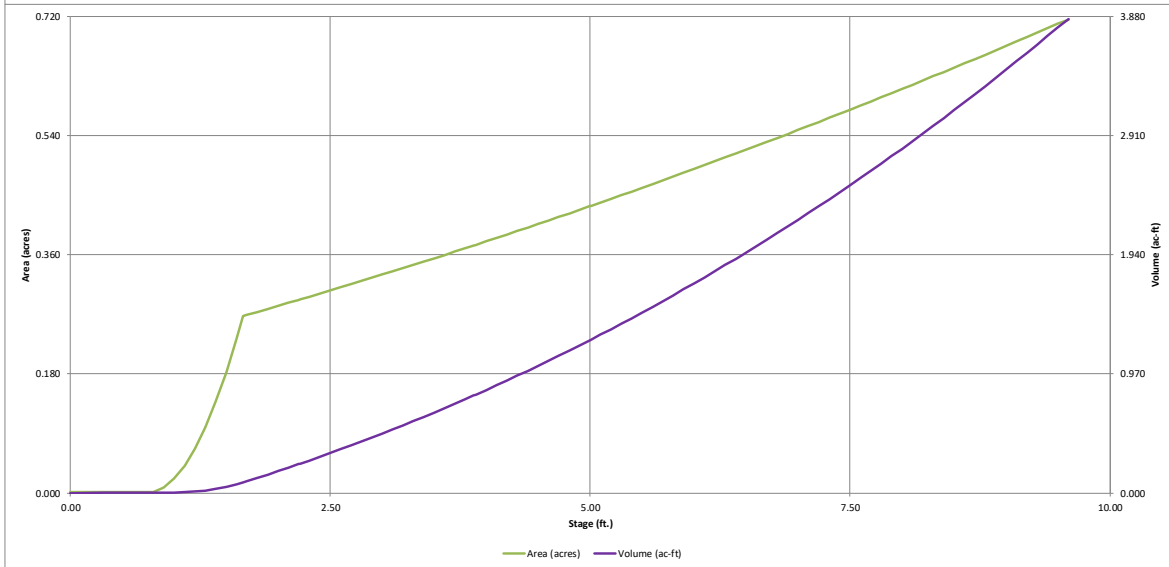
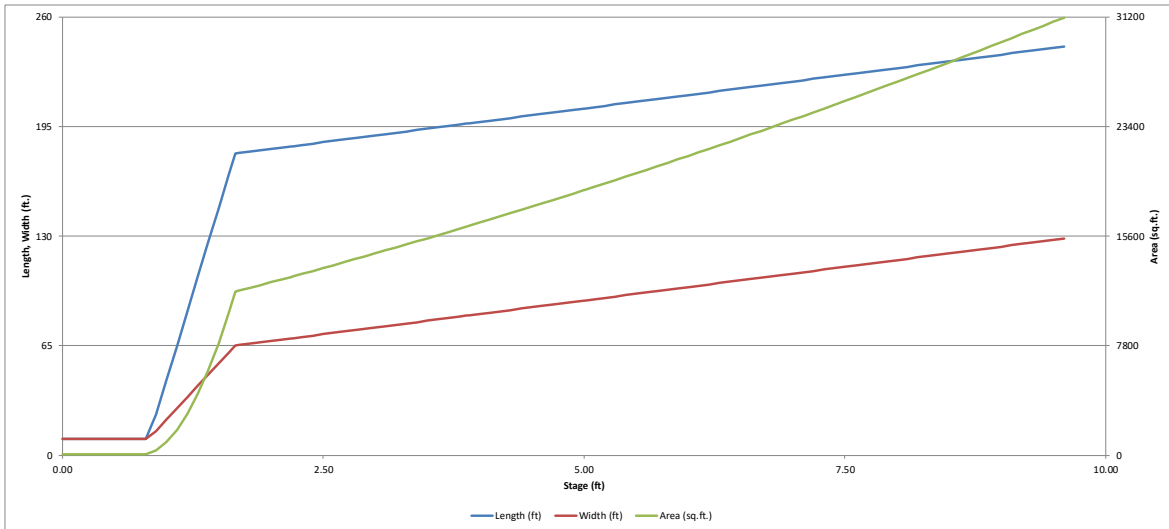


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maximum bound			



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

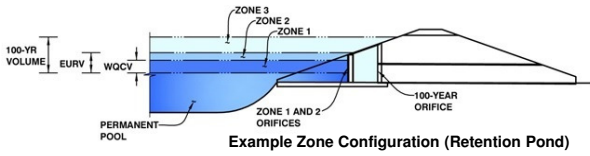
*MHFD-Depotion, Version 4.02 (February 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

**Project: Singer Ranch**  
**Basin ID: DF-2 (NW Multi-Family Pond)**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.21	0.236	Orifice Plate
Zone 2 (EURV)	3.88	0.556	Circular Orifice
Zone 3 (100-year)	5.01	0.454	Weir&Pipe (Restrict)
Total (all zones)		1.246	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter =  inches

**Calculated Parameters for Underdrain**  
 Underdrain Orifice Area =  ft<sup>2</sup>  
 Underdrain Orifice Centroid =  feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
 Orifice Plate: Orifice Vertical Spacing =  inches  
 Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 1 inch)

**Calculated Parameters for Plate**  
 WQ Orifice Area per Row =  ft<sup>2</sup>  
 Elliptical Half-Width =  feet  
 Elliptical Slot Centroid =  feet  
 Elliptical Slot Area =  ft<sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.73	1.45					
Orifice Area (sq. inches)	0.78	0.78	0.78					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.21	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.88	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	2.15	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.03	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.09	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))**

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H <sub>o</sub> =	3.87	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>t</sub> =	3.87	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	9.51	N/A	
Overflow Gate Open Area w/o Debris =	16.80	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	8.40	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	18.00		inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.77	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.75	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage =	4.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	14.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.86	feet
Stage at Top of Freeboard =	6.66	feet
Basin Area at Top of Freeboard =	0.53	acres
Basin Volume at Top of Freeboard =	2.04	acre-ft

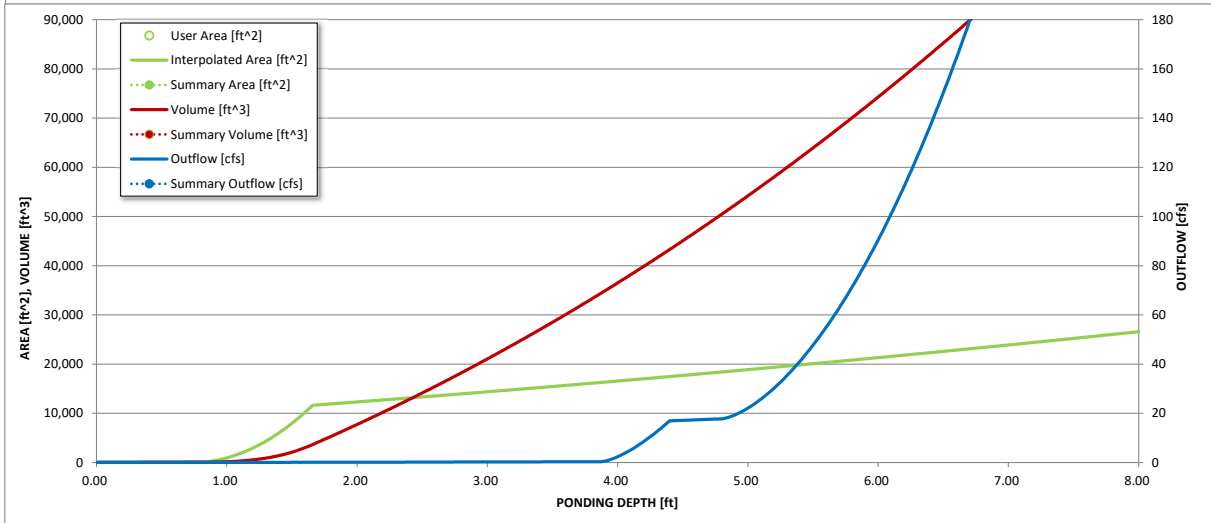
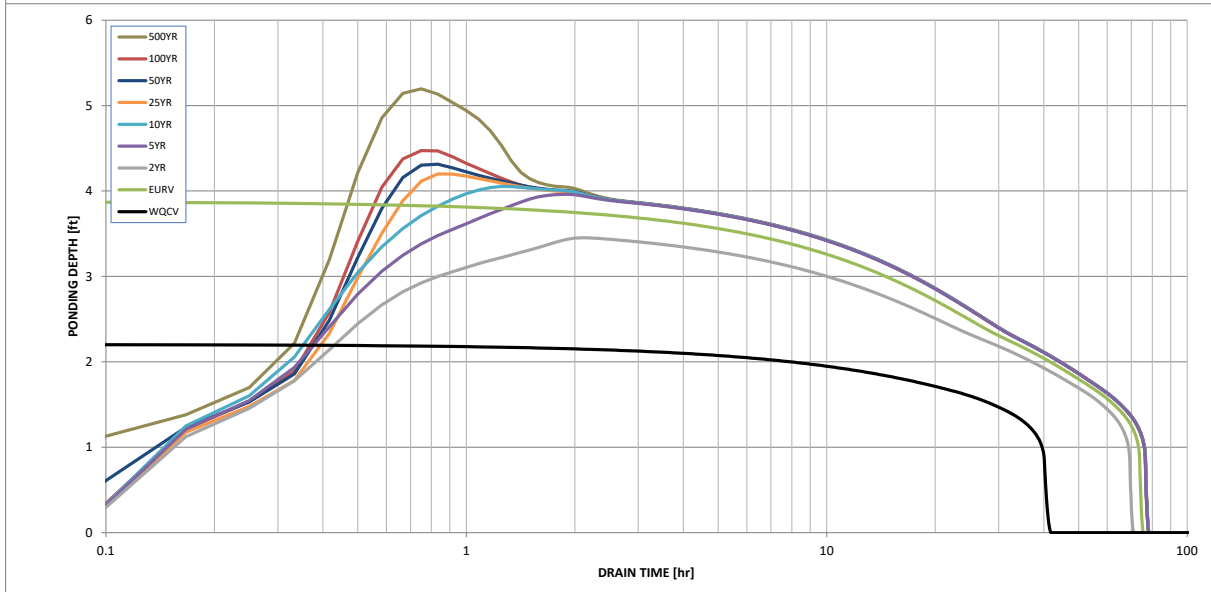
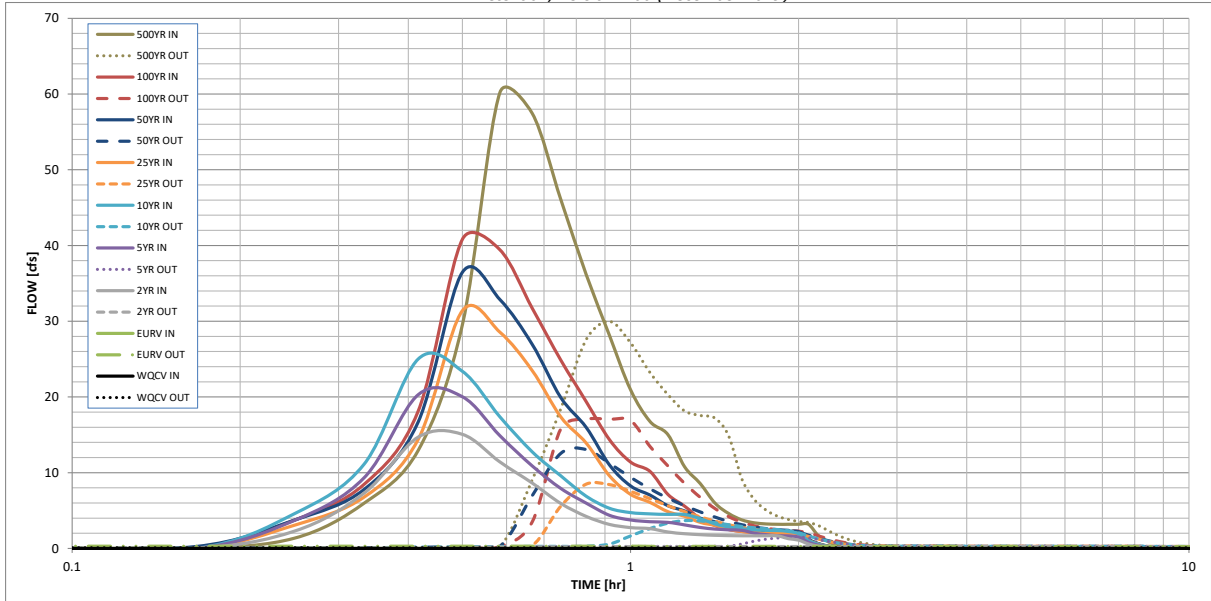
## Routed Hydrograph Results

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.236	0.792	0.673	0.907	1.105	1.338	1.545	1.791	2.665
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.673	0.907	1.105	1.338	1.545	1.791	2.665
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.7	4.5	6.8	11.8	14.7	18.4	30.4
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.16	0.44	0.66	1.14	1.43	1.79	2.95
Peak Inflow Q (cfs) =	N/A	N/A	15.1	20.3	25.0	31.4	36.5	40.8	60.2
Peak Outflow Q (cfs) =	0.1	0.3	0.3	1.5	3.7	8.5	13.1	17.1	30.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.5	0.7	0.9	0.9	1.0
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	0.00	N/A	0.1	0.2	0.5	0.7	1.0	1.1
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	64	70	69	67	66	64	60
Time to Drain 99% of Inflow Volume (hours) =	40	72	68	74	74	73	73	72	70
Maximum Ponding Depth (ft) =	2.21	3.88	3.45	3.96	4.05	4.20	4.31	4.47	5.20
Area at Maximum Ponding Depth (acres) =	0.29	0.37	0.35	0.38	0.38	0.39	0.40	0.40	0.44
Maximum Volume Stored (acre-ft) =	0.238	0.792	0.636	0.823	0.857	0.911	0.958	1.022	1.327

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



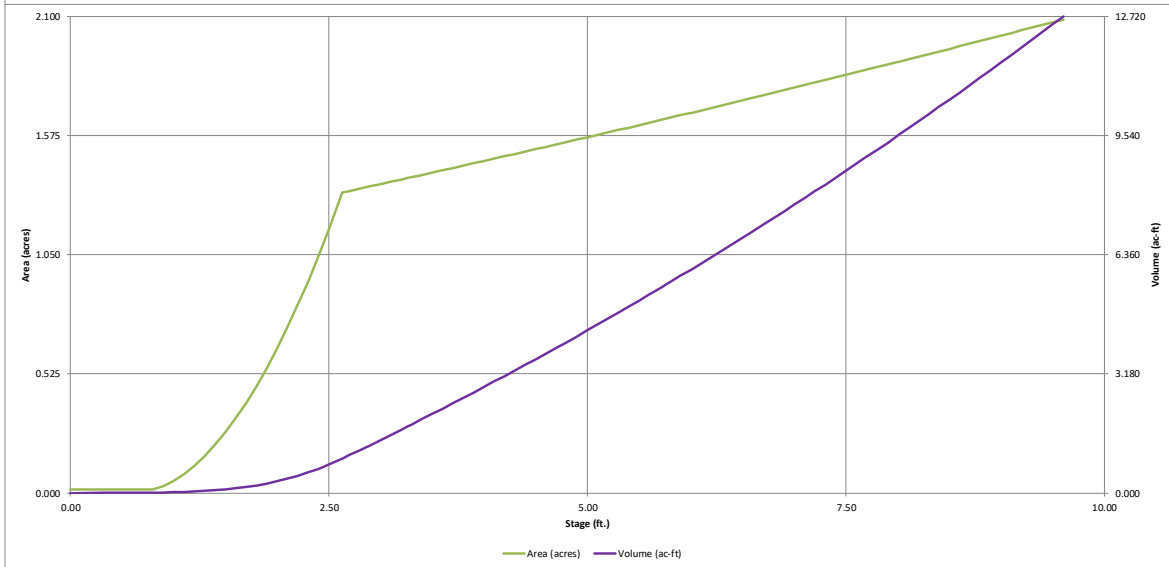
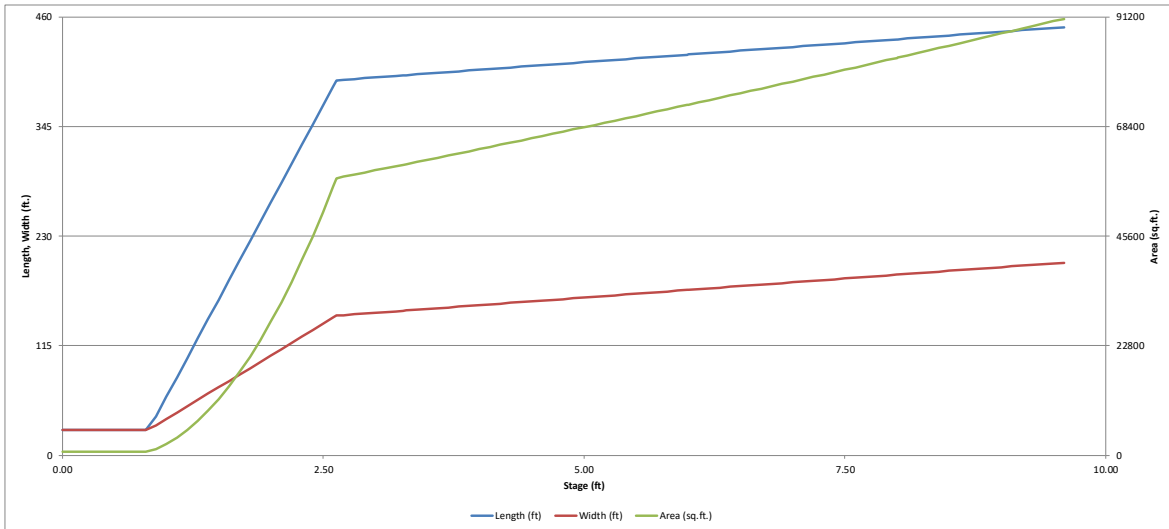
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maximum bound			





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

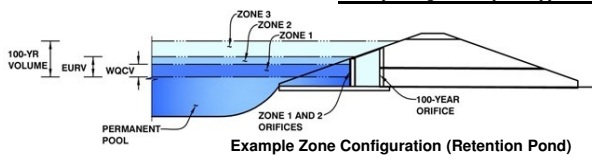
*MHFD-Detention, Version 4.02 (February 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

**Project: Singer Ranch**  
**Basin ID: DF-3 (W Single Family Pond)(Sub-basin 1-D Added)**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.27	1.770	Orifice Plate
Zone 2 (EURV)	5.99	4.161	Circular Orifice
Zone 3 (100-year)	8.01	3.601	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>9.532</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	3.27	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	12.60	inches
Orifice Plate: Orifice Area per Row =	5.17	sq. inches (use rectangular openings)

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	3.590E-02	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.09	2.18					
Orifice Area (sq. inches)	5.17	5.17	5.17					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	3.27	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.99	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	4.90	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.13	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.20	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))**

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.10	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	12.00	N/A	feet
Overflow Weir Gate Slope =	4.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>1</sub> =	7.10	N/A	feet
Overflow Weir Slope Length =	4.12	N/A	feet
Gate Open Area / 100-yr Orifice Area =	6.09	N/A	
Overflow Gate Open Area w/o Debris =	34.63	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	17.32	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	36.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	27.00	N/A	inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	5.69	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	1.24	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	2.09	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage =	9.25	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	58.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.96	feet
Stage at Top of Freeboard =	11.21	feet
Basin Area at Top of Freeboard =	2.28	acres
Basin Volume at Top of Freeboard =	16.23	acre-ft

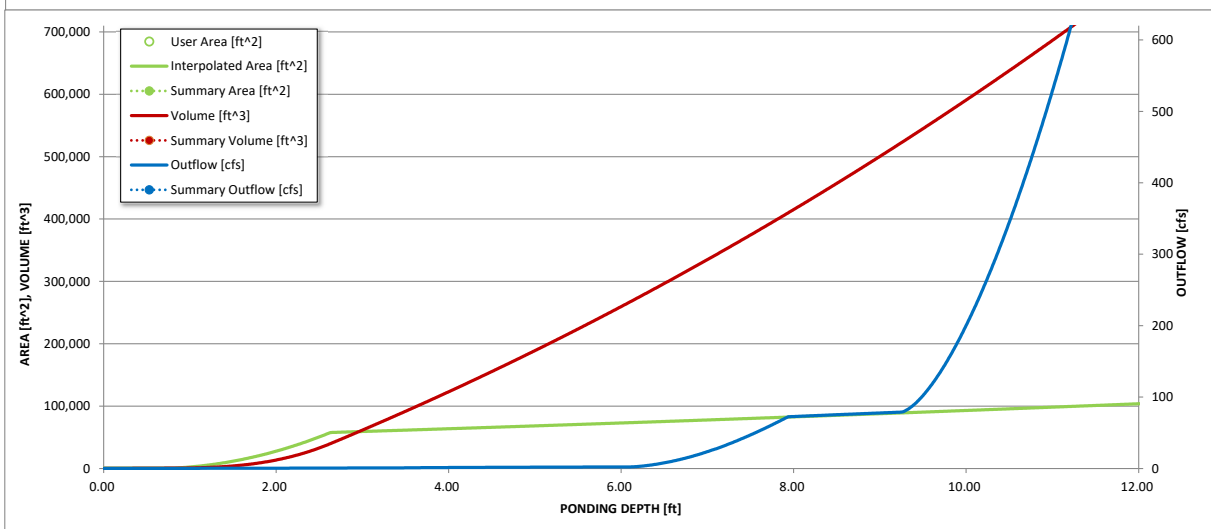
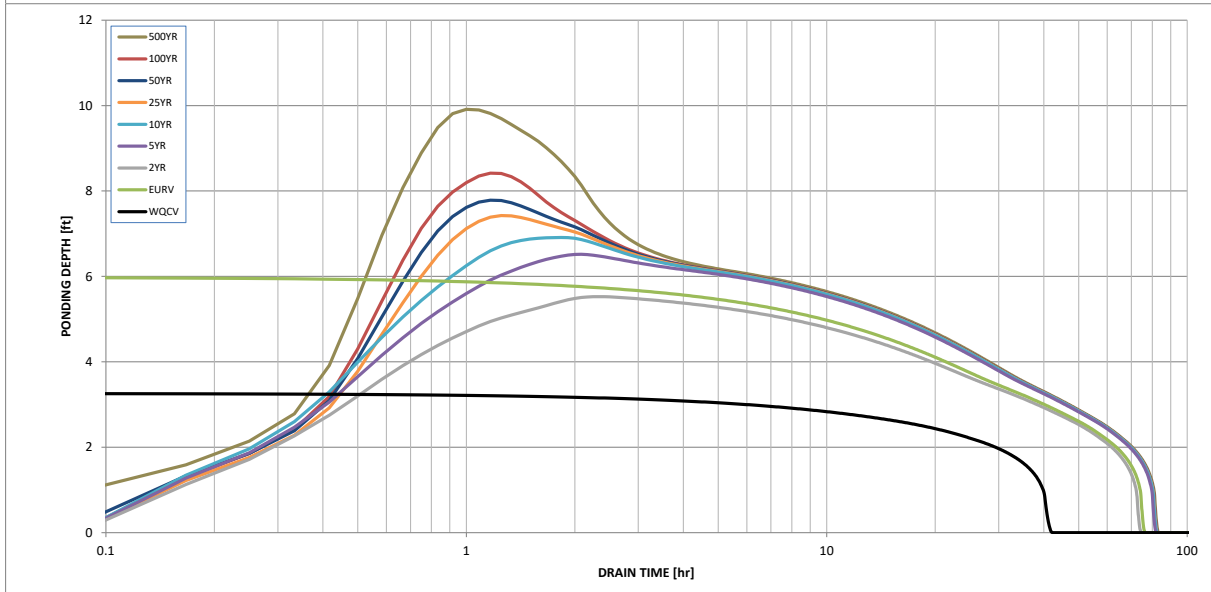
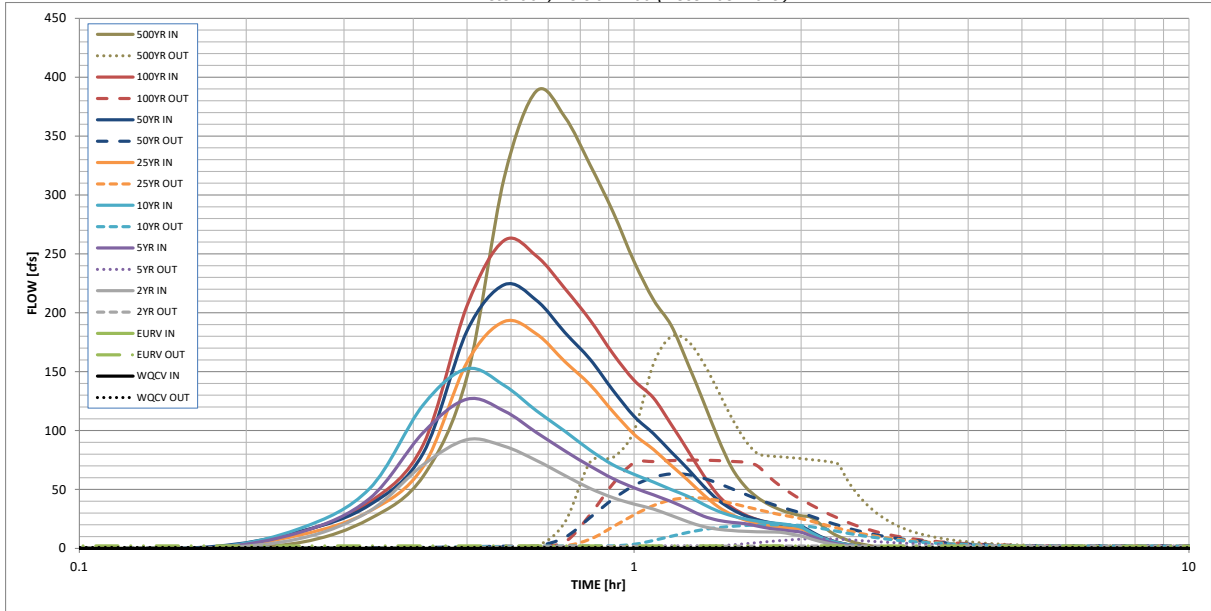
## Routed Hydrograph Results

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	1.770	5.931	5.483	7.478	9.176	11.254	13.050	15.227	22.864
CUHP Runoff Volume (acre-ft) =	N/A	N/A	5.483	7.478	9.176	11.254	13.050	15.227	22.864
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	8.6	24.3	36.9	66.0	82.8	105.1	175.9
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.10	0.29	0.44	0.79	0.99	1.26	2.10
Peak Inflow Q (cfs) =	N/A	N/A	92.2	126.7	152.5	192.6	223.8	261.5	388.1
Peak Outflow Q (cfs) =	0.7	2.1	2.0	8.3	20.1	43.0	63.2	74.9	179.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.5	0.7	0.8	0.7	1.0
Structure Controlling Flow =	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.5	1.2	1.8	2.1	2.3
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	72	71	69	68	66	61
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	77	77	76	76	75	73
Maximum Ponding Depth (ft) =	3.27	5.99	5.53	6.52	6.91	7.42	7.79	8.42	9.91
Area at Maximum Ponding Depth (acres) =	1.39	1.67	1.62	1.73	1.78	1.83	1.87	1.95	2.12
Maximum Volume Stored (acre-ft) =	1.783	5.942	5.168	6.827	7.529	8.449	9.116	10.319	13.371

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

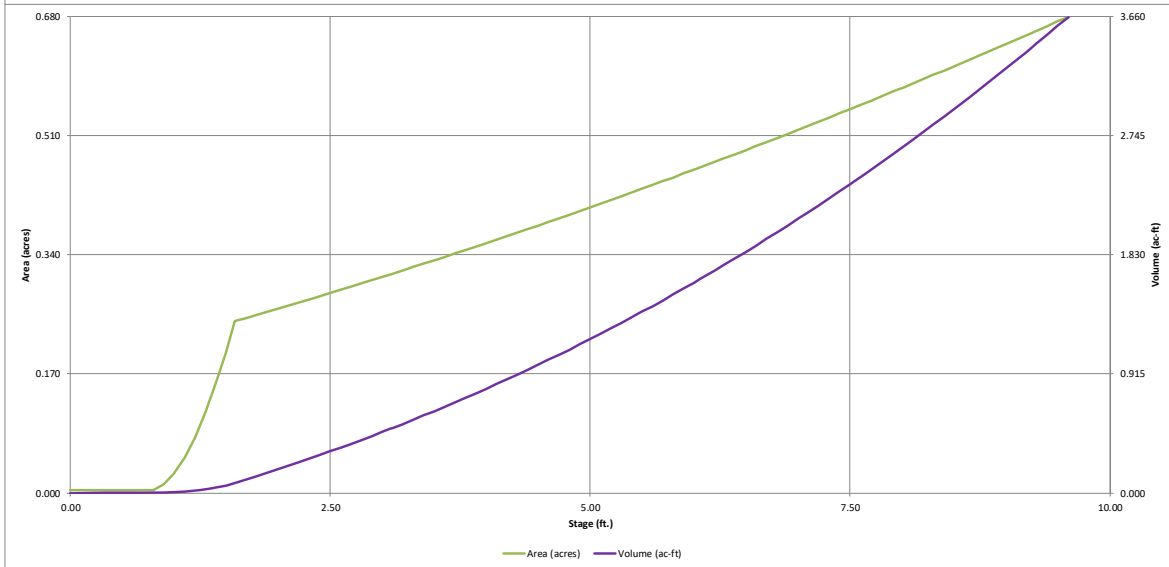
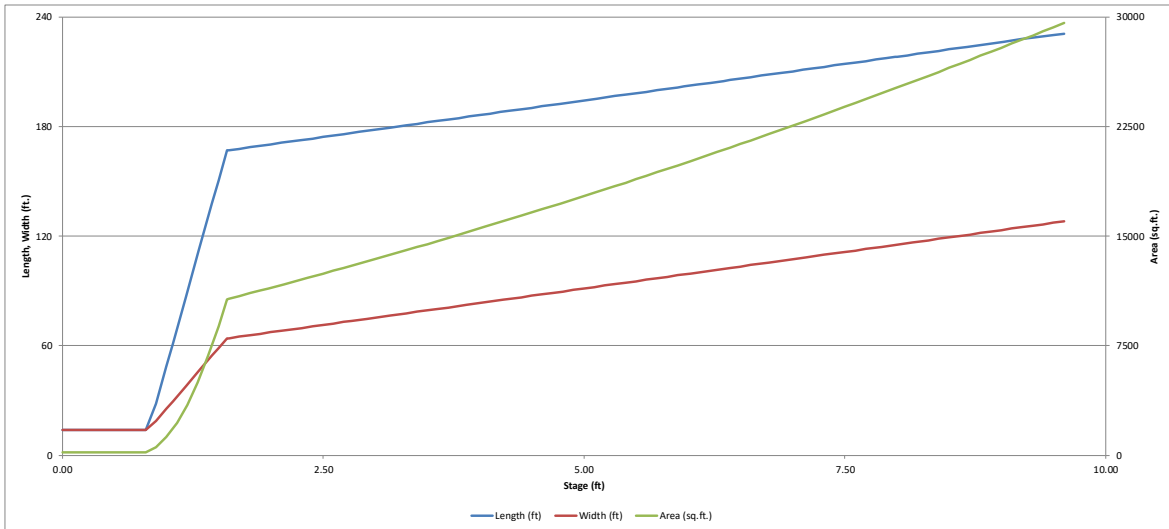






# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

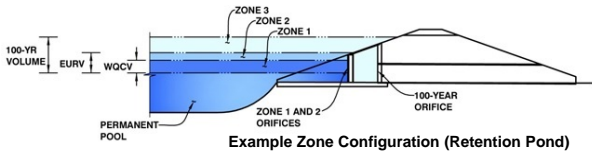
*MHFD-Detention, Version 4.02 (February 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

**Project:** Singer Ranch  
**Basin ID:** DF-4 (SW Single Family Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.08	0.490	Orifice Plate
Zone 2 (EURV)	6.06	1.152	Circular Orifice
Zone 3 (100-year)	7.98	0.997	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>2.639</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

**Calculated Parameters for Underdrain**

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

**Calculated Parameters for Plate**

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	1.139E-02	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	3.08	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	12.30	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	1.64	sq. inches (diameter = 1-7/16 inches)	Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.03	2.05					
Orifice Area (sq. inches)	1.64	1.64	1.64					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected		Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	3.08	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.02	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	6.06	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.08	feet
Vertical Orifice Diameter =	1.97	N/A	inches			

**User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))**

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.25	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Gate Upper Edge, H <sub>1</sub> =	6.25	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	Overflow Weir Slope Length =	4.00	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V	Gate Open Area / 100-yr Orifice Area =	10.16	N/A
Horiz. Length of Weir Sides =	4.00	N/A	feet	Overflow Gate Open Area w/o Debris =	16.80	ft <sup>2</sup>
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area	Overflow Gate Open Area w/ Debris =	8.40	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%			

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected		Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.65	ft <sup>2</sup>
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.60	feet
Restrictor Plate Height Above Pipe Invert =	12.50		inches	Half-Central Angle of Restrictor Plate on Pipe =	1.61	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

**Calculated Parameters for Spillway**

Spillway Invert Stage =	7.80	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth =	0.89	feet
Spillway Crest Length =	19.00	feet	Stage at Top of Freeboard =	9.69	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.69	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	3.72	acre-ft

**Routed Hydrograph Results**

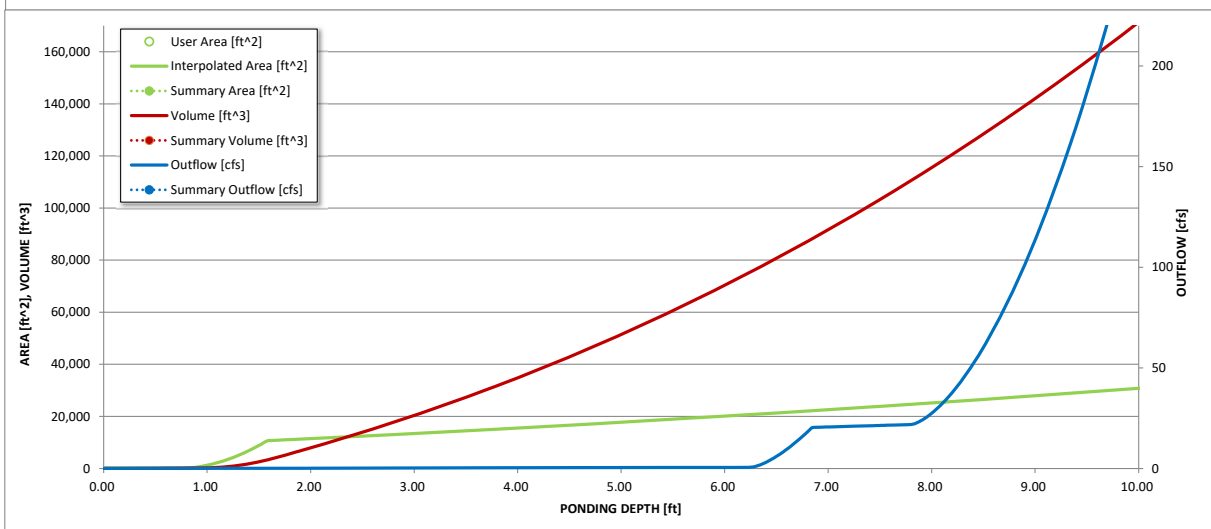
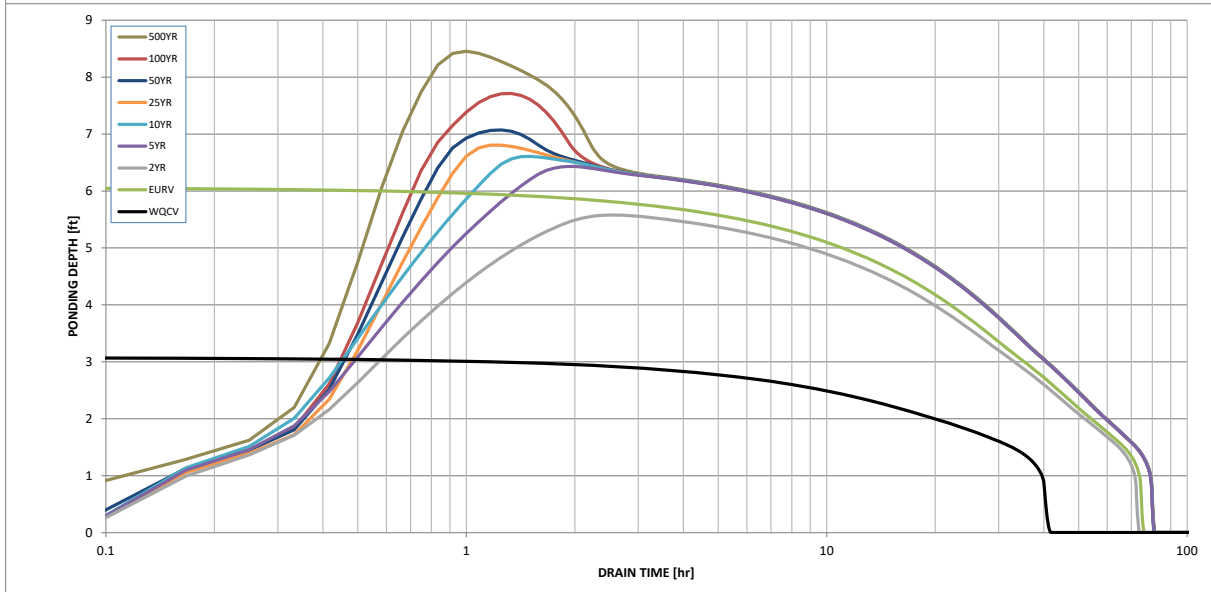
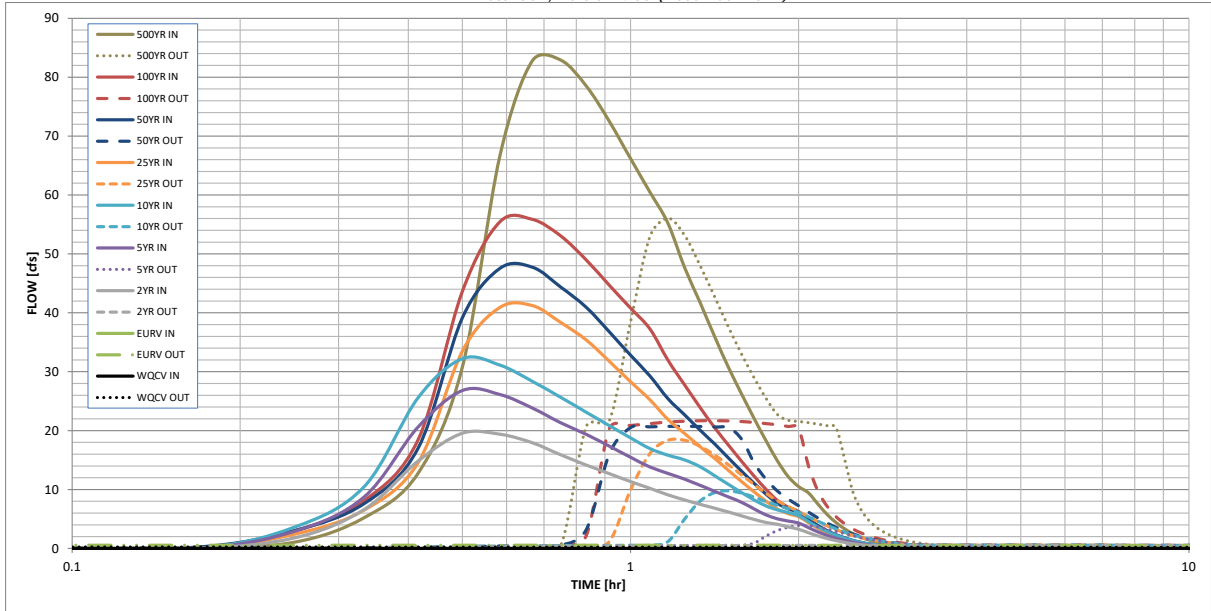
*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.490	1.642	1.513	2.063	2.531	3.104	3.598	4.197	6.300
CUHP Runoff Volume (acre-ft) =	N/A	N/A	1.513	2.063	2.531	3.104	3.598	4.197	6.300
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.7	4.8	7.4	13.7	17.2	22.0	36.9
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.07	0.21	0.32	0.59	0.74	0.95	1.60
Peak Inflow Q (cfs) =	N/A	N/A	19.5	26.8	32.2	41.2	47.8	55.9	82.9
Peak Outflow Q (cfs) =	0.2	0.5	0.5	3.9	9.8	18.4	20.7	21.7	56.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.8	1.3	1.3	1.2	1.0	1.5
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.6	1.0	1.2	1.3	1.3
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	72	70	68	67	65	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	77	76	75	75	74	72
Maximum Ponding Depth (ft) =	3.08	6.06	5.58	6.43	6.61	6.80	7.07	7.71	8.45
Area at Maximum Ponding Depth (acres) =	0.31	0.46	0.44	0.49	0.49	0.51	0.52	0.56	0.61
Maximum Volume Stored (acre-ft) =	0.492	1.642	1.421	1.818	1.901	2.001	2.140	2.487	2.918



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*

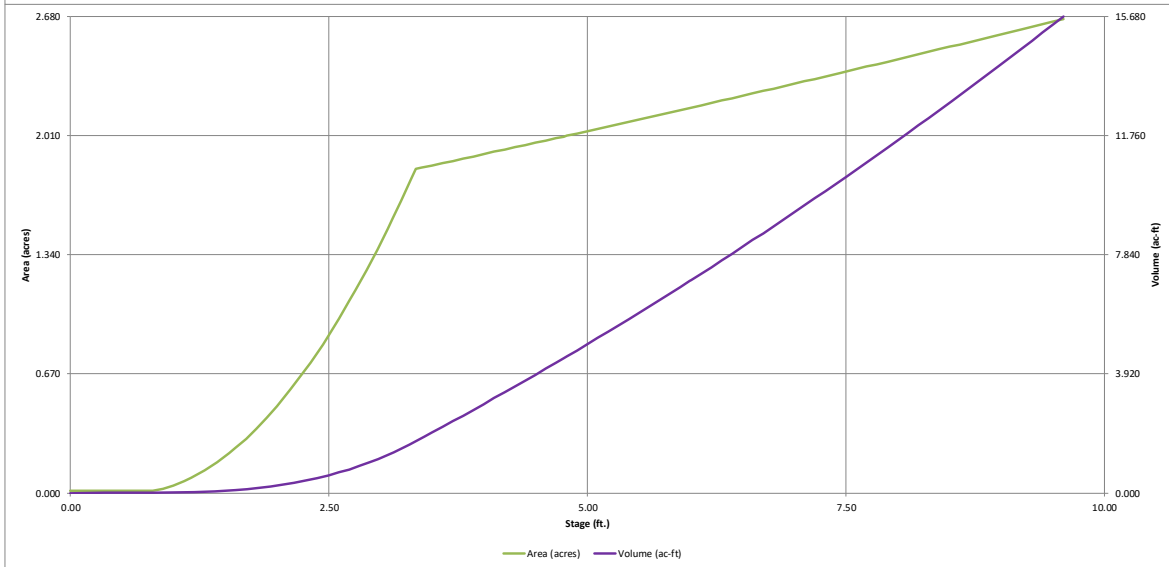
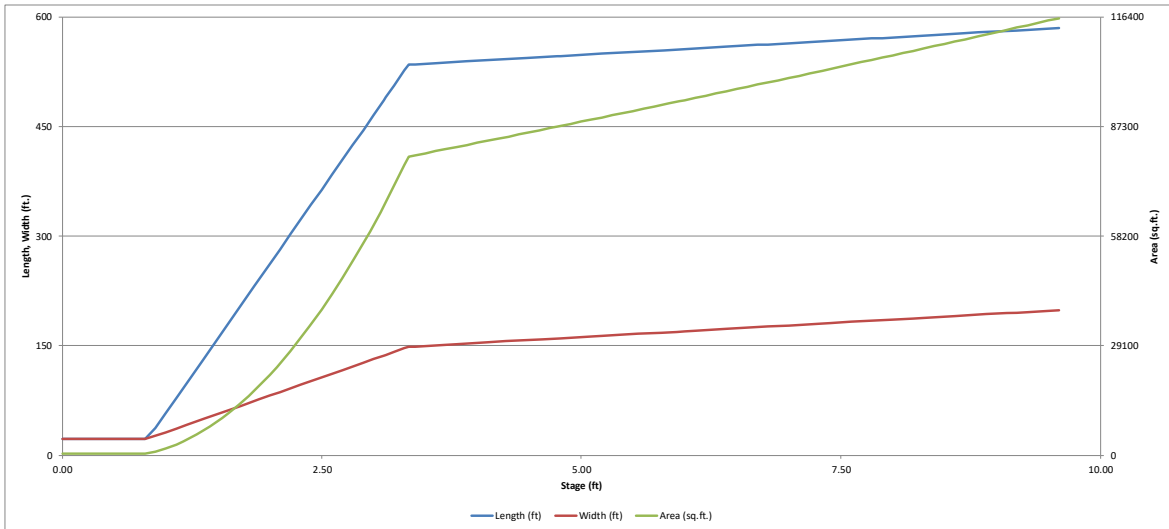


S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

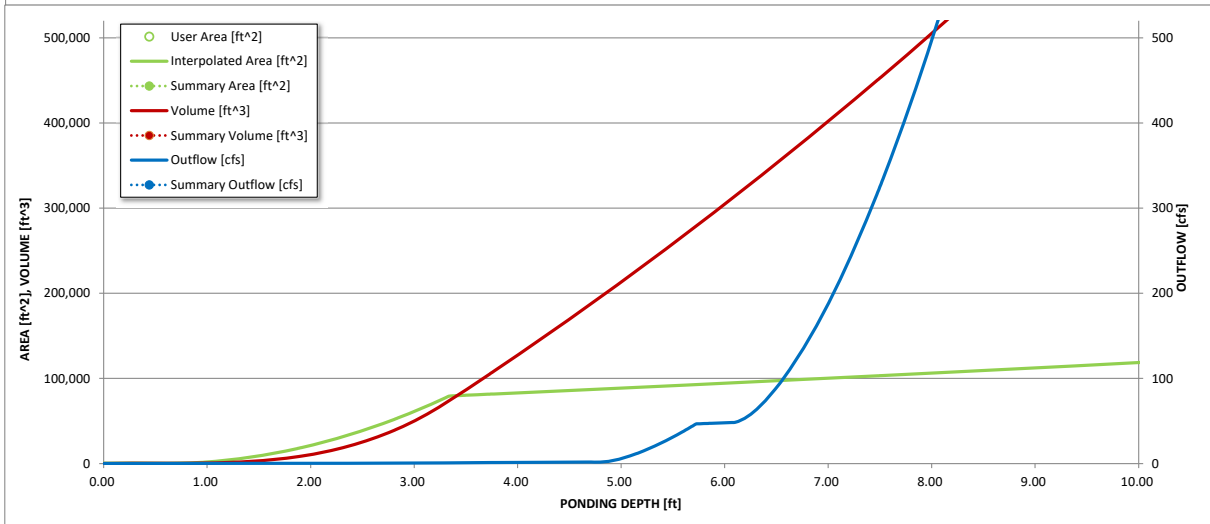
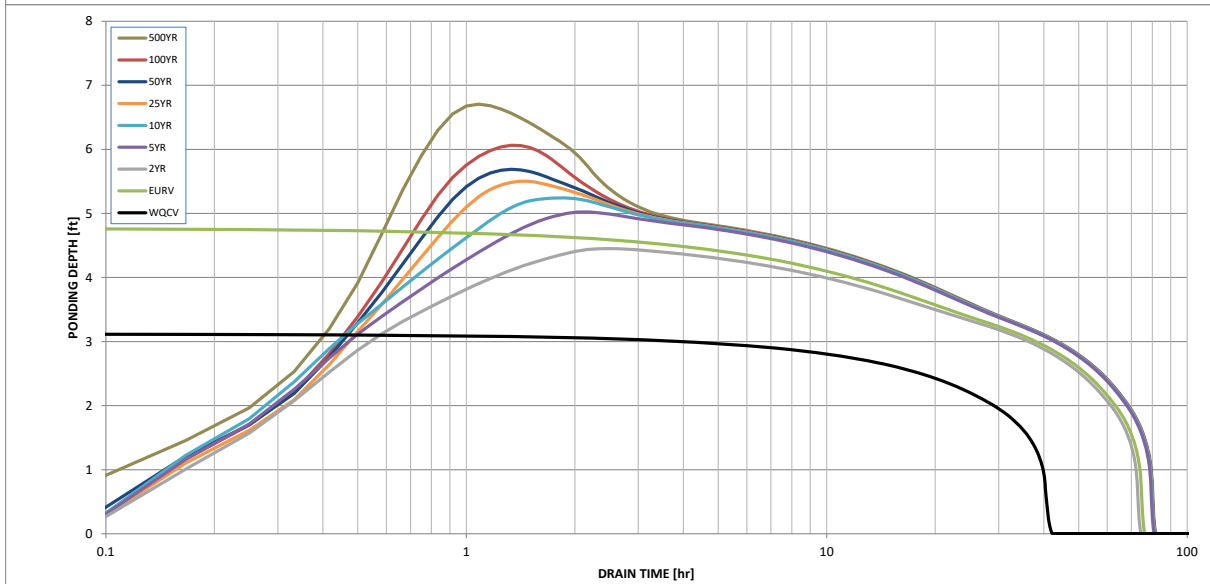
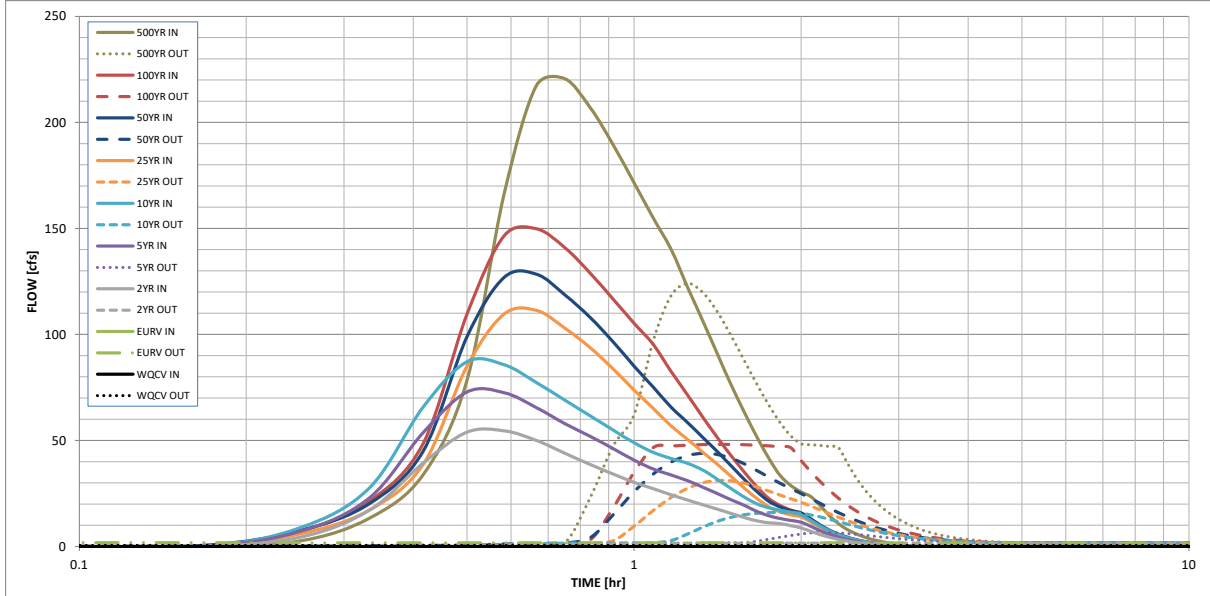
*MHFD-Detention, Version 4.02 (February 2020)*





# DETENTION BASIN OUTLET STRUCTURE DESIGN

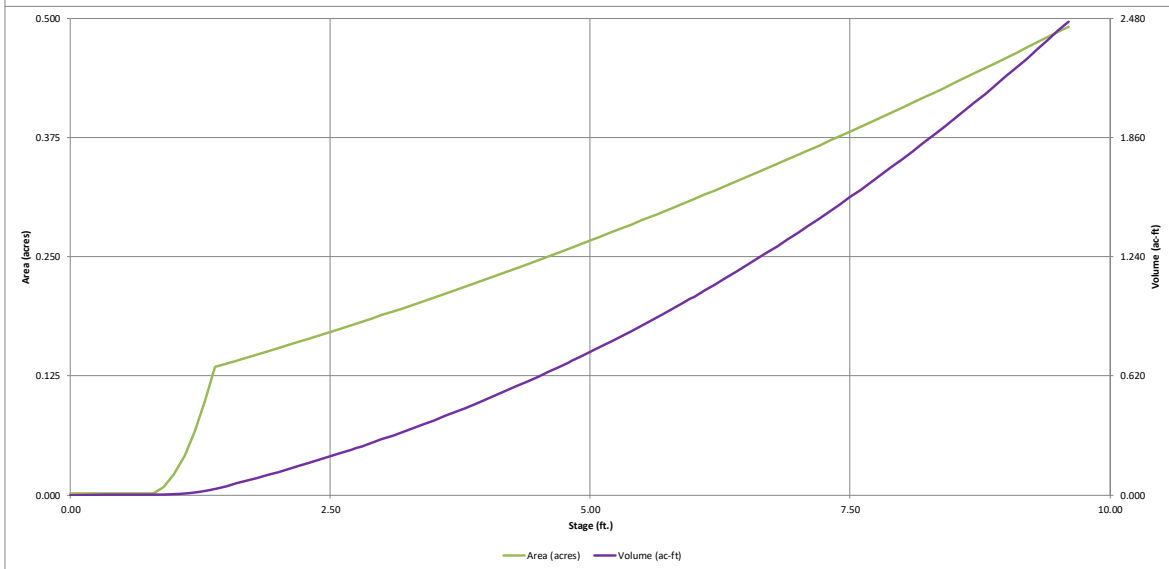
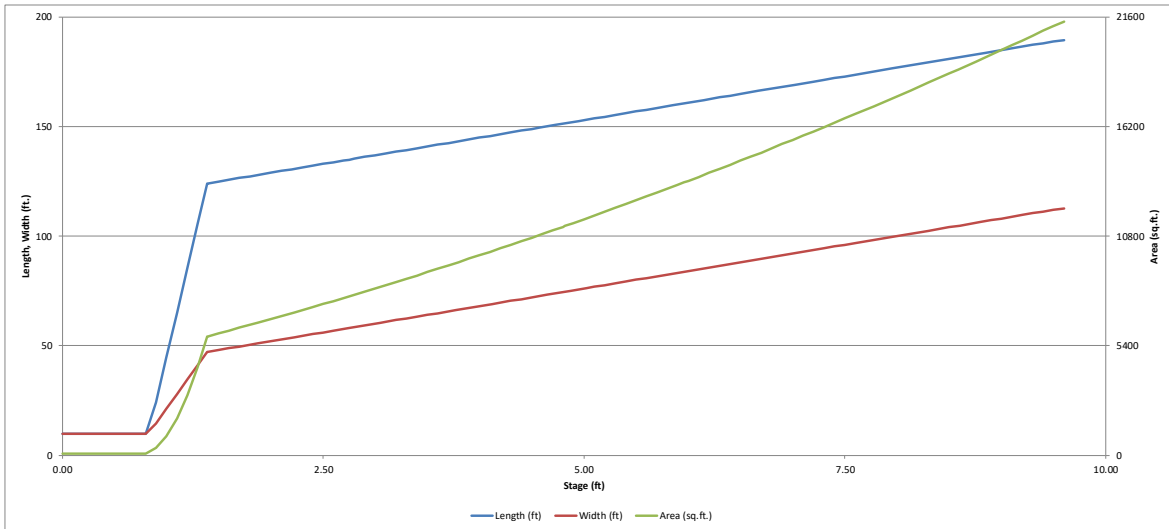
*MHFD-Detention, Version 4.00 (December 2019)*





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

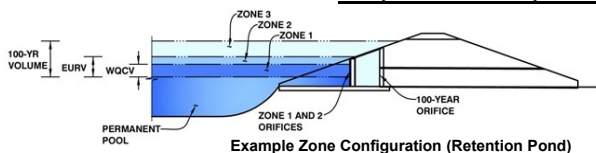
*MHFD-Depotion, Version 4.02 (February 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

**Project:** Singer Ranch  
**Basin ID:** DF-6 (NE Commercial Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.75	0.242	Orifice Plate
Zone 2 (EURV)	4.82	0.453	Circular Orifice
Zone 3 (100-year)	5.96	0.322	Weir&Pipe (Restrict)
Total (all zones)		1.017	

**User Input:** Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input:** Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.81	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	11.20	inches
Orifice Plate: Orifice Area per Row =	0.85	sq. inches (diameter = 1 inch)

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	5.903E-03	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input:** Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.94	1.87					
Orifice Area (sq. inches)	0.85	0.85	0.85					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input:** Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.75	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.82	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	0.97	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.01	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.04	N/A	feet

**User Input:** Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.82	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>u</sub> =	4.82	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	13.42	N/A	
Overflow Gate Open Area w/o Debris =	16.80	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	8.40	N/A	ft <sup>2</sup>

**User Input:** Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	12.00		inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.25	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.56	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.91	N/A	radians

**User Input:** Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	6.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	8.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.79	feet
Stage at Top of Freeboard =	7.79	feet
Basin Area at Top of Freeboard =	0.40	acres
Basin Volume at Top of Freeboard =	1.66	acre-ft

## Routed Hydrograph Results

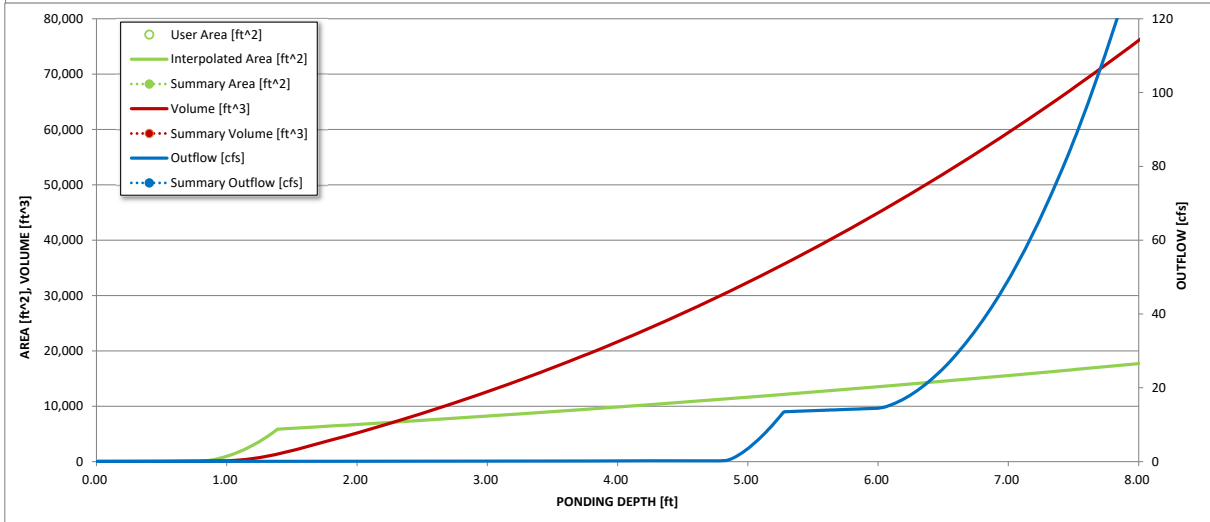
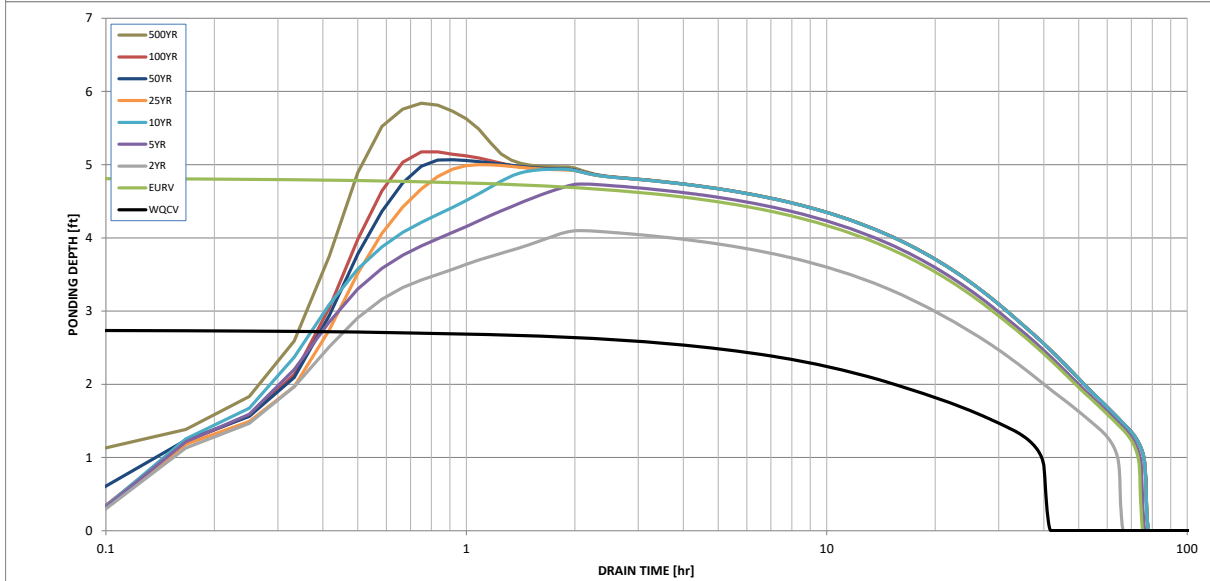
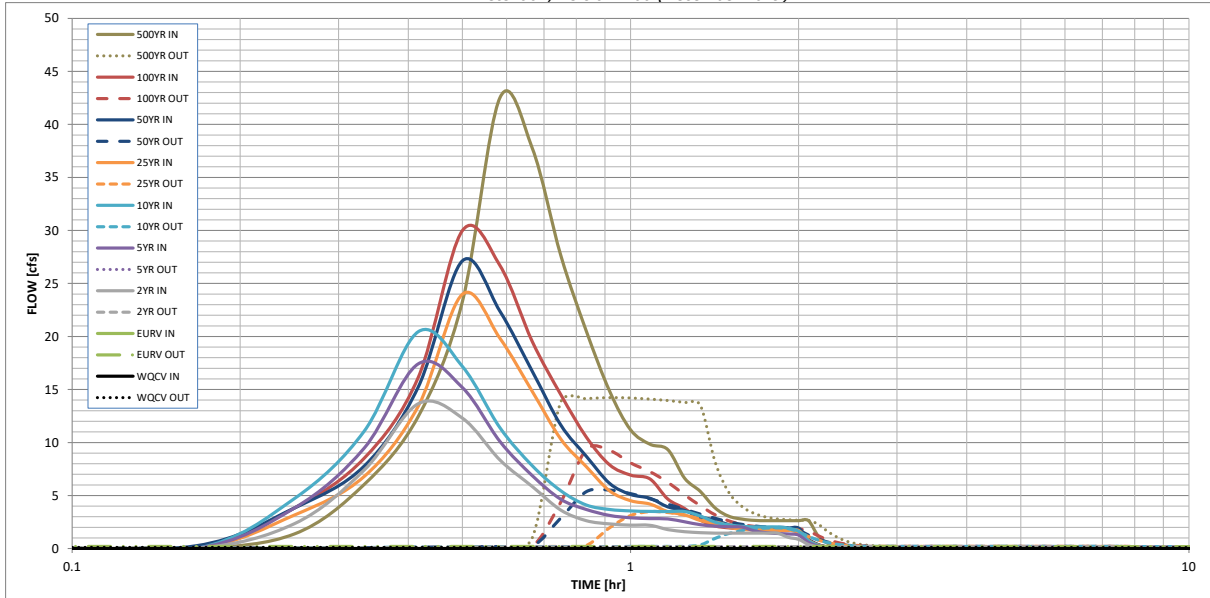
*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.242	0.695	0.544	0.703	0.831	0.961	1.091	1.232	1.765
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.544	0.703	0.831	0.961	1.091	1.232	1.765
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	3.0	4.6	7.8	9.7	12.1	20.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.17	0.47	0.71	1.20	1.49	1.87	3.11
Peak Inflow Q (cfs) =	N/A	N/A	13.7	17.4	20.4	24.0	27.1	30.0	42.5
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.2	2.0	3.5	5.5	9.3	14.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.1	0.4	0.4	0.6	0.8	0.7
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.2	0.3	0.5	0.8
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	61	69	70	69	68	67	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	64	73	74	74	74	73	72
Maximum Ponding Depth (ft) =	2.75	4.82	4.10	4.74	4.94	5.00	5.07	5.17	5.84
Area at Maximum Ponding Depth (acres) =	0.18	0.26	0.23	0.26	0.26	0.27	0.27	0.27	0.30
Maximum Volume Stored (acre-ft) =	0.244	0.696	0.517	0.673	0.725	0.741	0.759	0.789	0.979



# DETENTION BASIN OUTLET STRUCTURE DESIGN

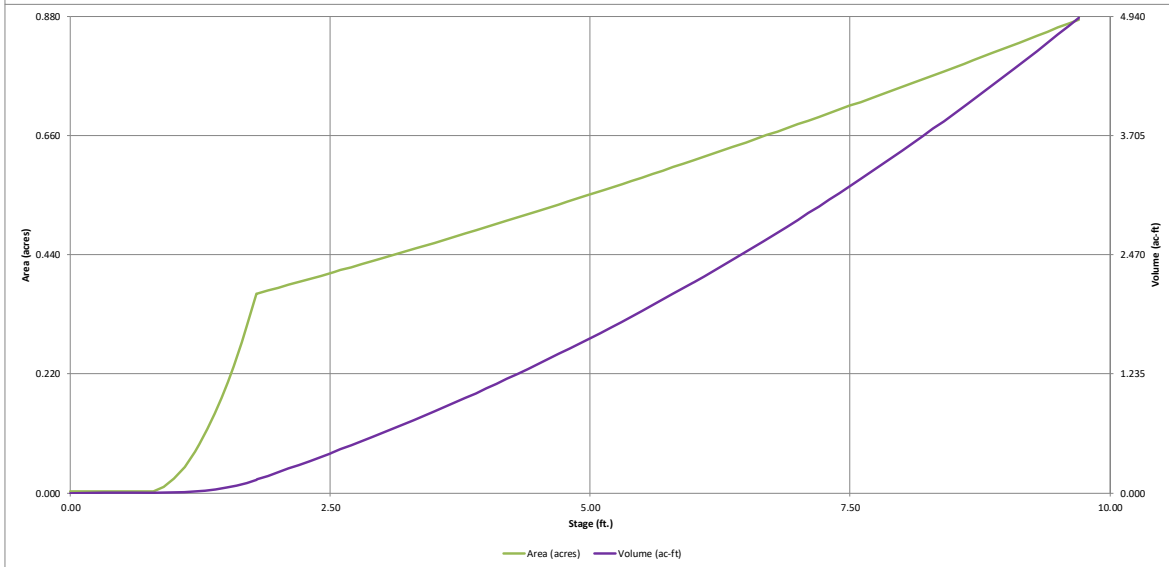
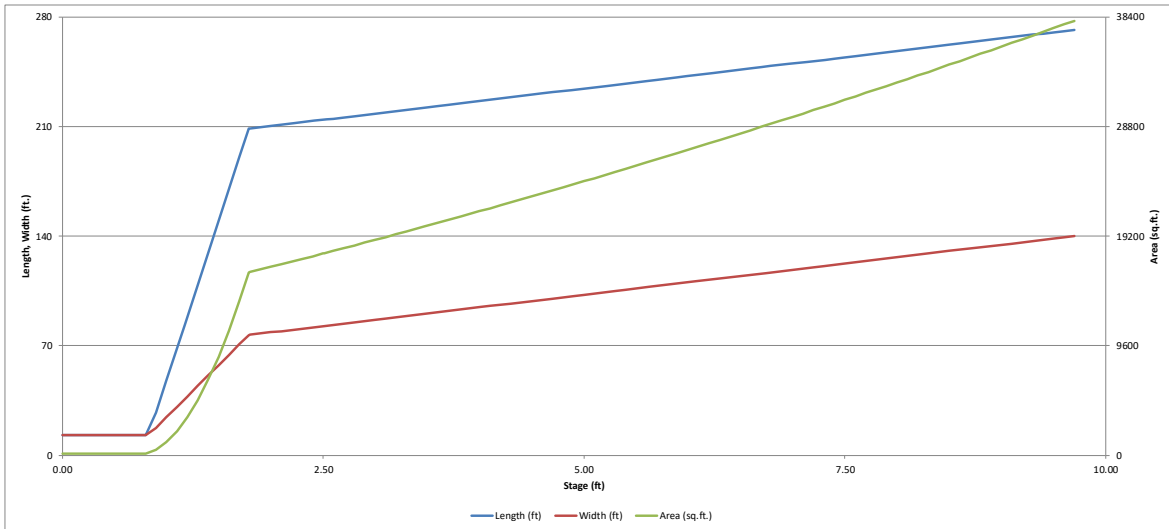
*MHFD-Detention, Version 4.00 (December 2019)*





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

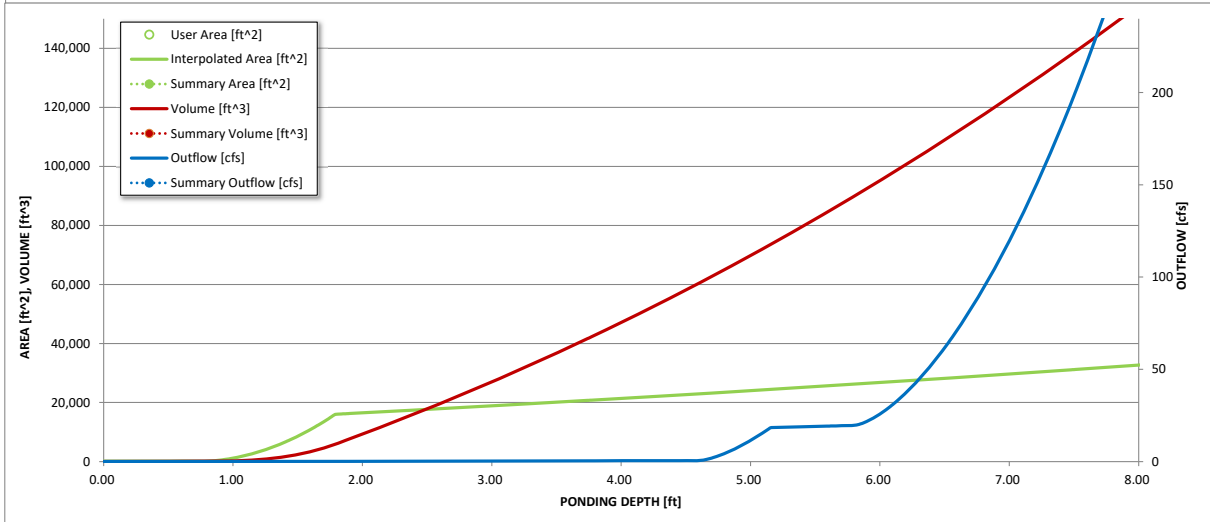
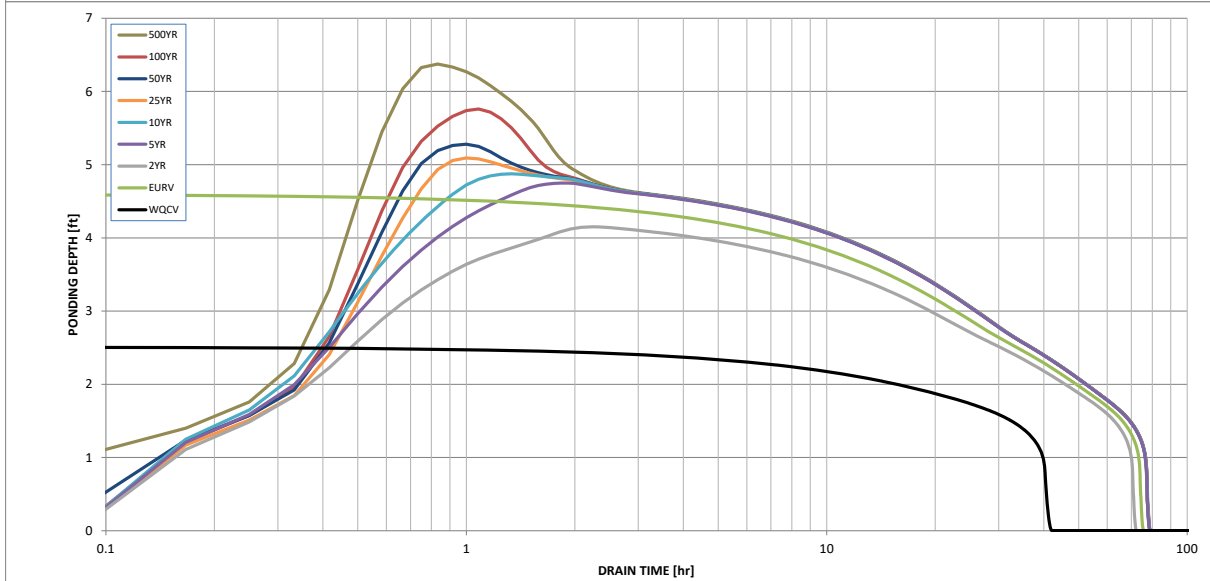
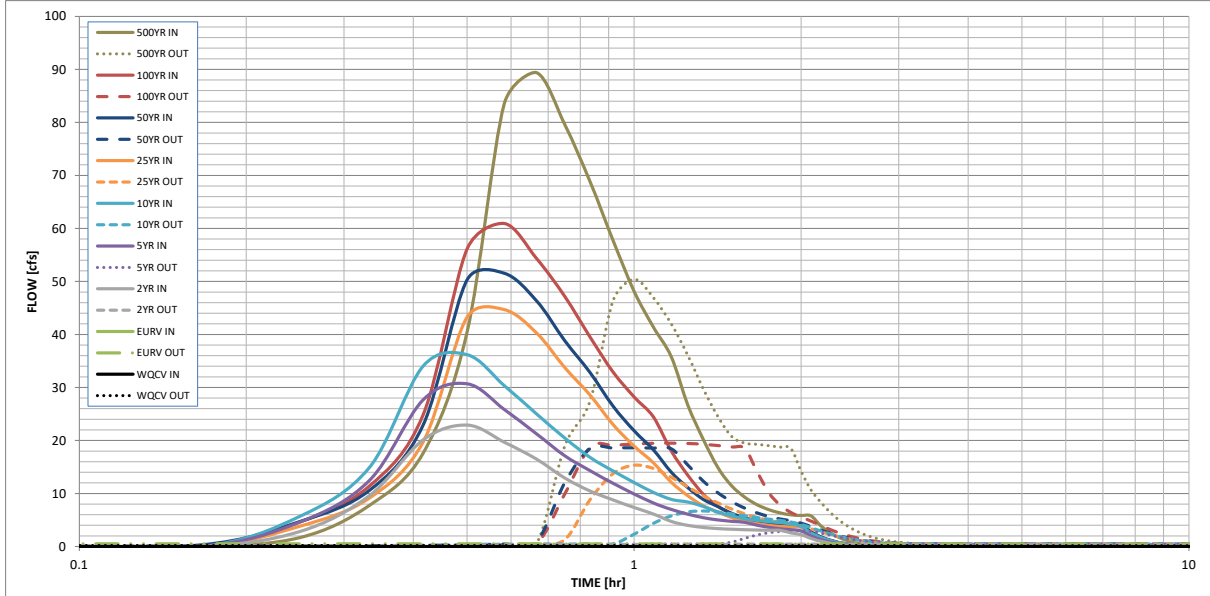
*MHFD-Detention, Version 4.02 (February 2020)*





# DETENTION BASIN OUTLET STRUCTURE DESIGN

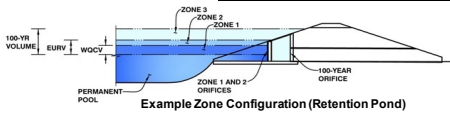
*MHFD-Detention, Version 4.00 (December 2019)*



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-DETENTION, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-8 (SE Single-Family & Commercial Pond)



Watershed Information table with fields like Selected BMP Type, Watershed Area, Watershed Length, Watershed Length to Centroid, Watershed Slope, Watershed Imperviousness, etc.

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) and other volume-related metrics table.

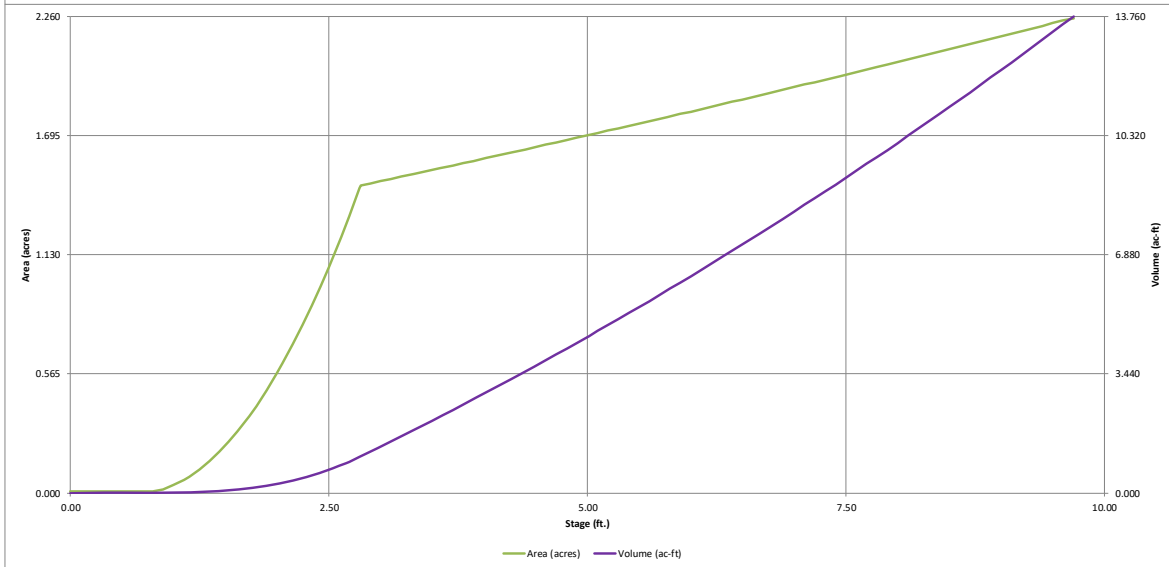
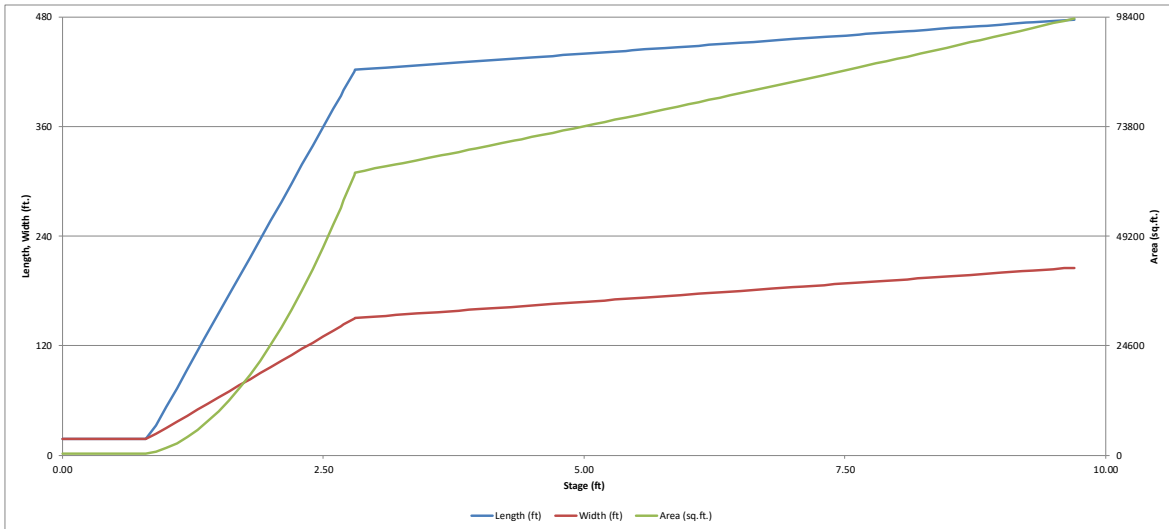
Optional User Overrides table with columns for depth increment, stage, length, width, area, and volume.

Define Zones and Basin Geometry table with various geometric and volume parameters like Zone 1 Volume, Zone 2 Volume, etc.

Main Stage-Storage Table with columns: Stage (ft), Length (ft), Width (ft), Area (ft^2), Volume (ft^3), and Volume (ac-ft). Rows include Top of Micropool, ISV, Zone 1 (WQCV), Floor, Zone 2 (EURV), and Zone 3 (100-year).

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.02 (February 2020)*

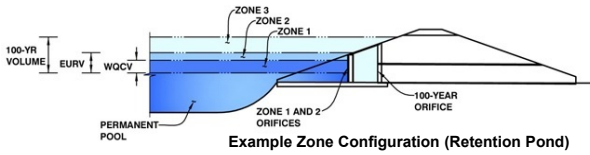


# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.02 (February 2020)*

**Project: Singer Ranch**

**Basin ID: DF-8 (SE Single-Family & Commercial Pond)**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.67	0.854	Orifice Plate
Zone 2 (EURV)	4.00	2.009	Circular Orifice
Zone 3 (100-year)	5.01	1.642	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>4.505</b>	

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

Calculated Parameters for Underdrain

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	1.778E-02	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	2.66	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	10.60	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	2.56	sq. inches (diameter = 1-13/16 inches)	Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.89	1.77					
Orifice Area (sq. inches)	2.56	2.56	2.56					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected		Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.67	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.15	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.22	feet
Vertical Orifice Diameter =	5.27	N/A	inches			

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H <sub>g</sub> =	4.00	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	Overflow Weir Slope Length =	6.00	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	5.63	N/A
Horiz. Length of Weir Sides =	6.00	N/A	feet	Overflow Grate Open Area w/o Debris =	25.20	ft <sup>2</sup>
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area	Overflow Grate Open Area w/ Debris =	12.60	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%			

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected		Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	4.48	ft <sup>2</sup>
Outlet Pipe Diameter =	36.00	N/A	inches	Outlet Orifice Centroid =	1.03	feet
Restrictor Plate Height Above Pipe Invert =	21.80		inches	Half-Central Angle of Restrictor Plate on Pipe =	1.78	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

Spillway Invert Stage =	5.00	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth =	0.95	feet
Spillway Crest Length =	40.00	feet	Stage at Top of Freeboard =	6.95	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	1.92	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	8.03	acre-ft

## Routed Hydrograph Results

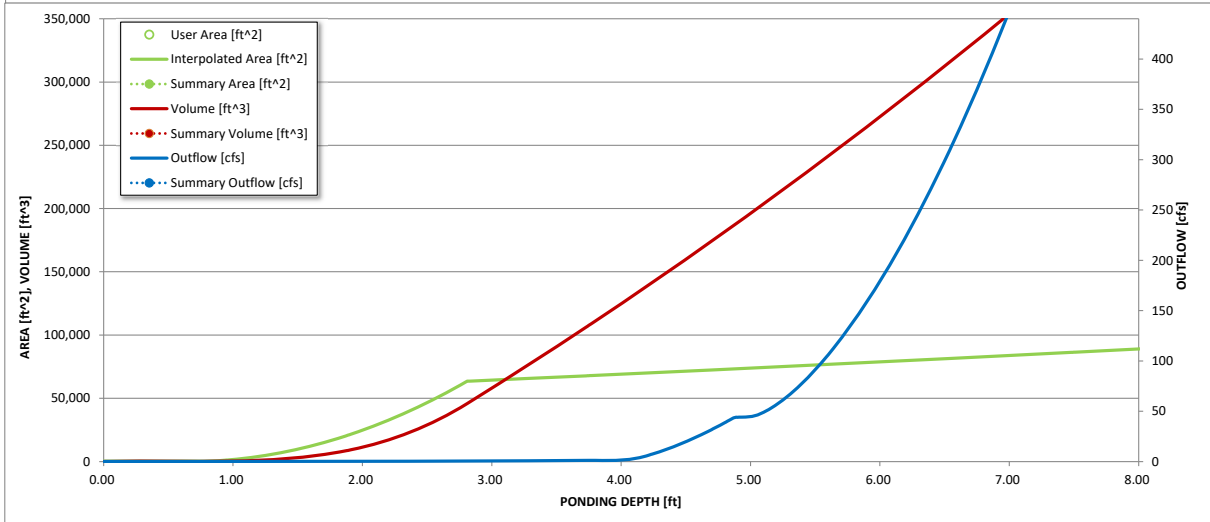
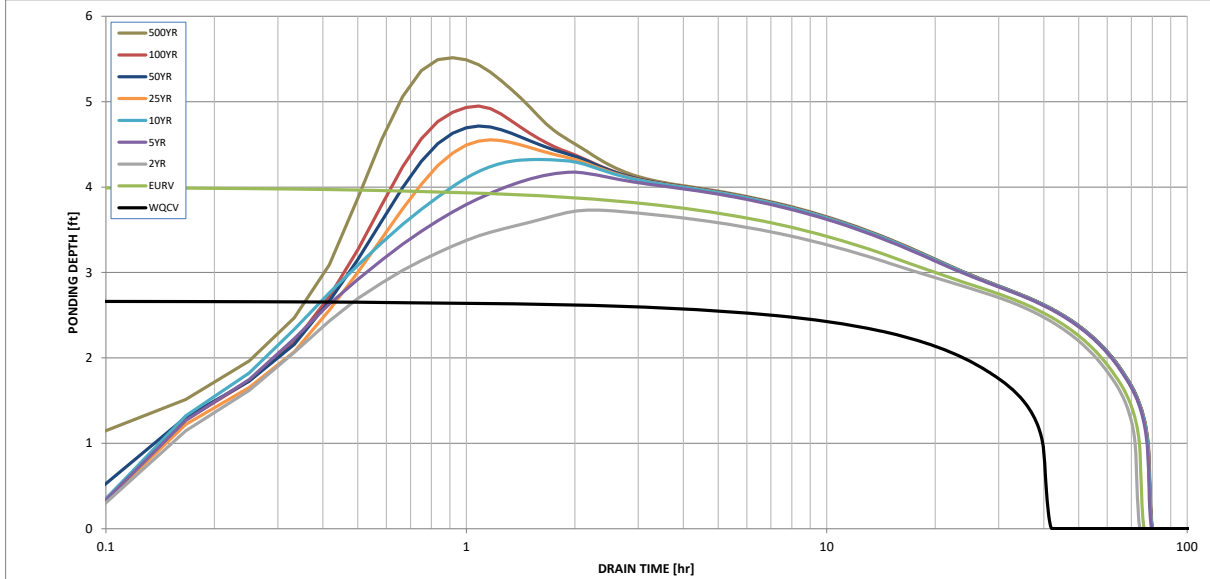
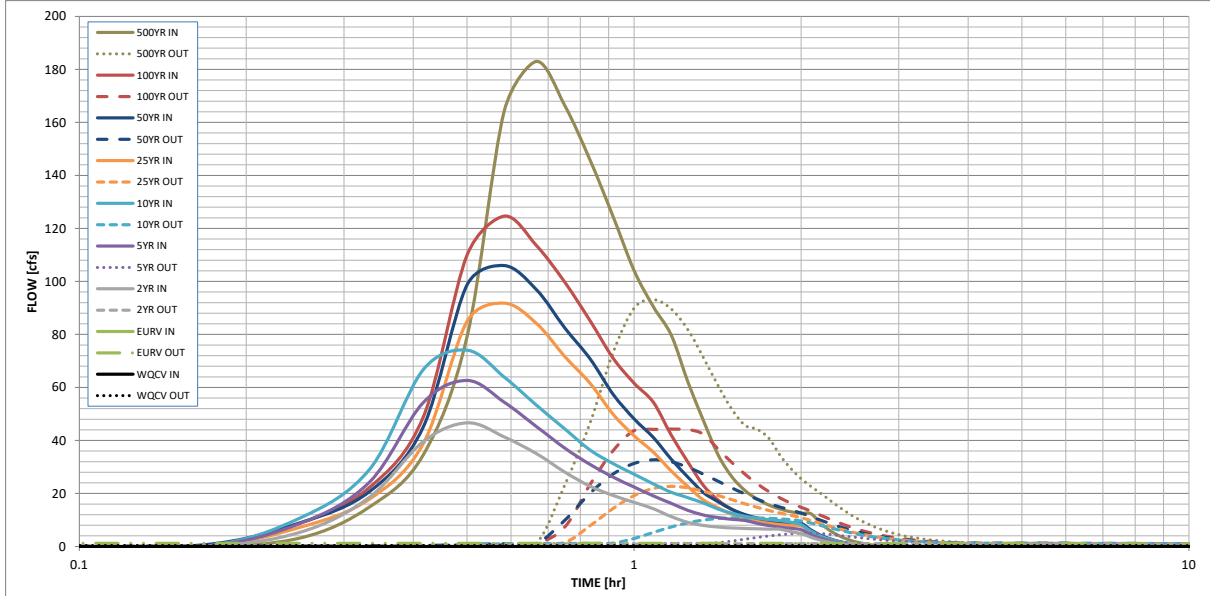
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.854	2.863	2.594	3.498	4.260	5.161	5.958	6.907	10.282
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.594	3.498	4.260	5.161	5.958	6.907	10.282
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.1	11.3	17.1	30.8	38.6	49.3	81.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.11	0.30	0.46	0.83	1.04	1.32	2.20
Peak Inflow Q (cfs) =	N/A	N/A	46.6	62.6	74.1	91.8	106.0	124.6	183.0
Peak Outflow Q (cfs) =	0.3	1.2	1.1	5.0	10.8	22.7	32.7	44.3	93.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.8	0.9	1.1
Structure Controlling Flow =	Vertical Orifice 1	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.2	1.7	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	70	69	68	66	65	60
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	75	75	74	74	73	71
Maximum Ponding Depth (ft) =	2.67	4.00	3.73	4.17	4.32	4.55	4.71	4.95	5.51
Area at Maximum Ponding Depth (acres) =	1.27	1.59	1.55	1.60	1.62	1.65	1.66	1.69	1.75
Maximum Volume Stored (acre-ft) =	0.862	2.864	2.424	3.135	3.377	3.752	4.017	4.402	5.383



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*

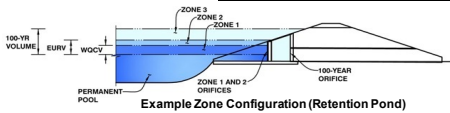


DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-DETENTION, Version 4.02 (February 2020)

Project: Singer Ranch

Basin ID: DF-9 (SE Commercial Pond)



Watershed Information

Table of watershed information including Selected BMP Type (EDB), Watershed Area (35.45 acres), Watershed Length (1,960 ft), Watershed Slope (0.030 ft/ft), and various runoff and detention volumes.

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Optional User Overrides

Table of optional user overrides for various parameters such as Water Quality Capture Volume (WQCV), Excess Urban Runoff Volume (EURV), and various runoff volumes.

Define Zones and Basin Geometry

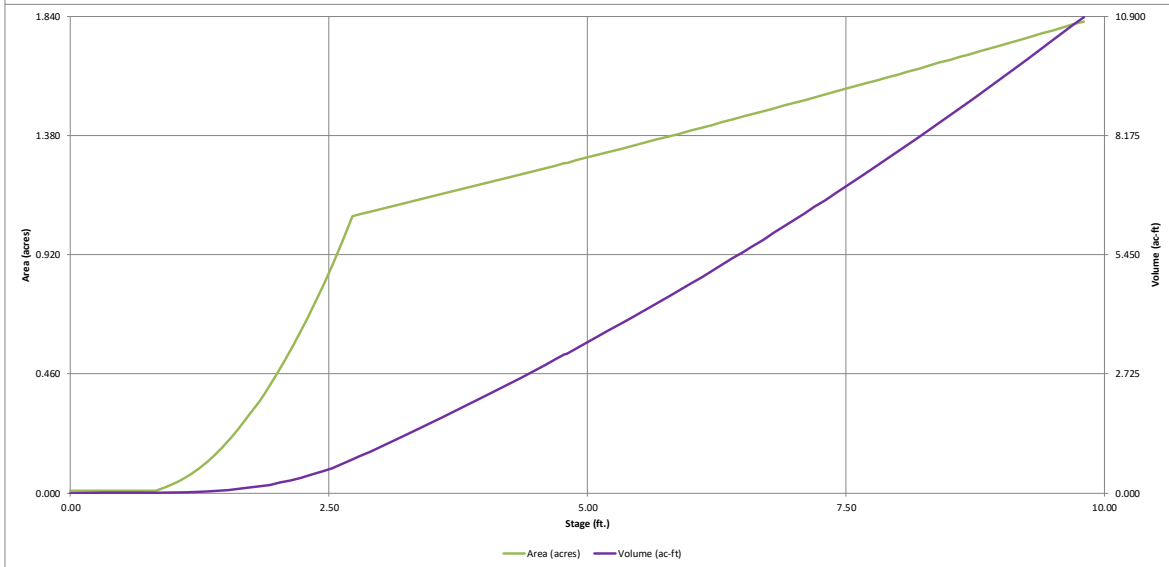
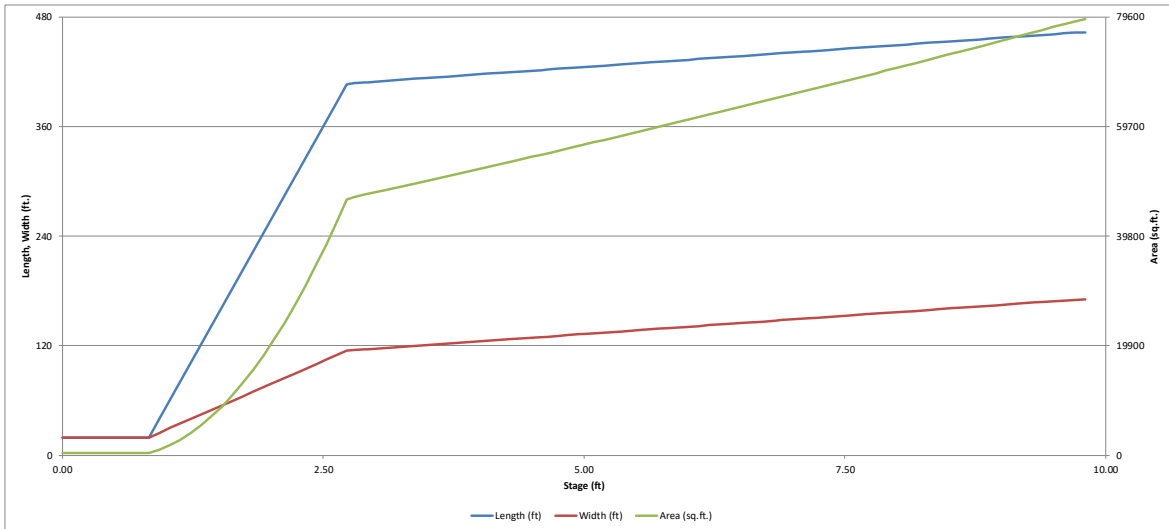
Table of zone and basin geometry parameters including Zone 1 Volume (WQCV), Zone 2 Volume (EURV - Zone 1), Zone 3 Volume (100-year - Zones 1 & 2), and various detention and channel dimensions.

Table of basin geometry parameters including Initial Surcharge Area (A<sub>ISV</sub>), Surcharge Volume Length (L<sub>LSV</sub>), Surcharge Volume Width (W<sub>LSV</sub>), and various basin dimensions and volumes.

Main stage-storage table with columns: Depth Increment (ft), Stage (ft), Optional Override Stage (ft), Length (ft), Width (ft), Area (ft²), Optional Override Area (ft²), Area (acre), Volume (ft³), and Volume (ac-ft). Rows include Top of Micropool, Floor, Zone 1 (WQCV), Zone 2 (EURV), and Zone 3 (100-year).

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

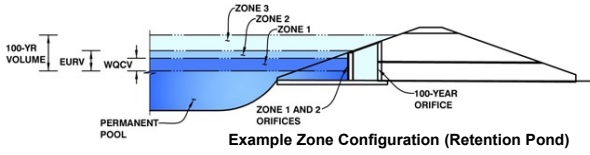
*MHFD-Detention, Version 4.02 (February 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

**Project:** Singer Ranch  
**Basin ID:** DF-9 (SE Commercial Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.93	0.970	Orifice Plate
Zone 2 (EURV)	4.78	2.178	Circular Orifice
Zone 3 (100-year)	6.00	1.638	Weir&Pipe (Restrict)
Total (all zones)		4.786	

**User Input:** Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input:** Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.91	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	11.60	inches
Orifice Plate: Orifice Area per Row =	2.84	sq. inches (diameter = 1-7/8 inches)

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	1.972E-02	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input:** Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.97	1.94					
Orifice Area (sq. inches)	2.84	2.84	2.84					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input:** Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.93	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.78	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	4.23	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.10	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.18	N/A	feet

**User Input:** Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.78	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	6.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H <sub>1</sub> =	4.78	N/A	feet
Overflow Weir Slope Length =	6.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	5.89	N/A	
Overflow Grate Open Area w/o Debris =	25.20	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	12.60	N/A	ft <sup>2</sup>

**User Input:** Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	36.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	21.00		inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	4.28	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	1.00	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.74	N/A	radians

**User Input:** Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	44.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.96	feet
Stage at Top of Freeboard =	7.76	feet
Basin Area at Top of Freeboard =	1.59	acres
Basin Volume at Top of Freeboard =	7.42	acre-ft

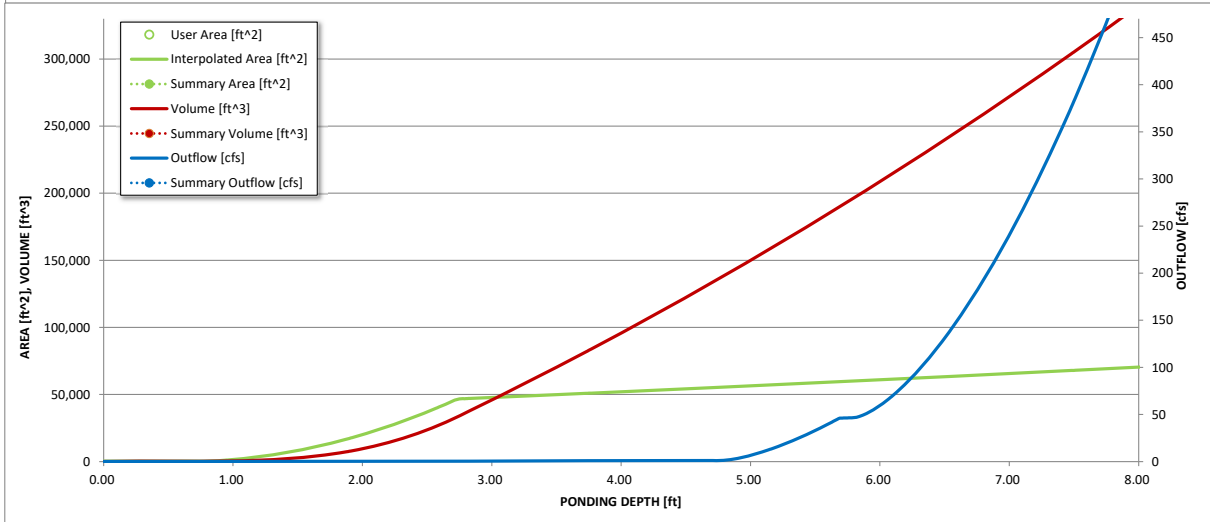
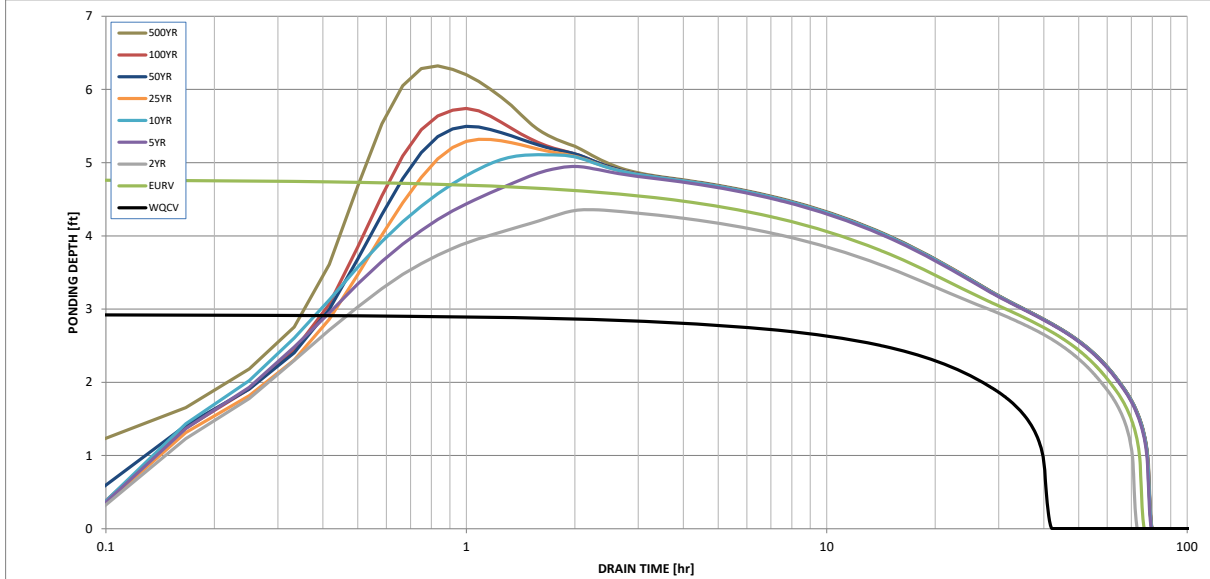
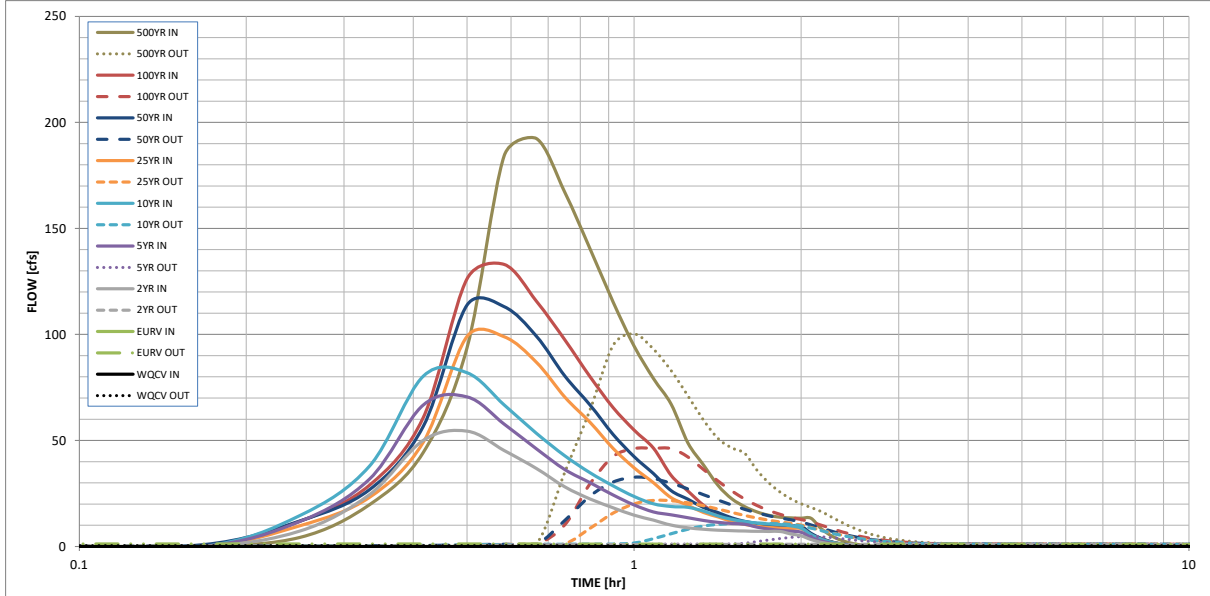
## Routed Hydrograph Results

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
CUHP Runoff Volume (acre-ft) =	0.970	3.148	2.780	3.677	4.421	5.244	6.012	6.889	10.097
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.780	3.677	4.421	5.244	6.012	6.889	10.097
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.2	11.9	18.0	31.7	39.8	50.4	83.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.34	0.51	0.89	1.12	1.42	2.36
Peak Inflow Q (cfs) =	N/A	N/A	54.4	70.6	81.9	99.0	113.8	133.0	192.4
Peak Outflow Q (cfs) =	0.4	1.2	1.0	4.8	10.9	21.7	32.7	46.3	100.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.8	0.9	1.2
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.3	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	65	71	70	68	67	66	61
Time to Drain 99% of Inflow Volume (hours) =	40	72	69	75	75	74	74	73	72
Maximum Ponding Depth (ft) =	2.93	4.78	4.36	4.95	5.11	5.32	5.50	5.74	6.32
Area at Maximum Ponding Depth (acres) =	1.09	1.27	1.23	1.29	1.31	1.33	1.35	1.37	1.43
Maximum Volume Stored (acre-ft) =	0.977	3.160	2.622	3.365	3.573	3.849	4.089	4.415	5.242

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



# **APPENDIX B**

## ***STANDARD DESIGN CHARTS AND TABLES***

**Table 6-6. Runoff Coefficients for Rational Method**

(Source: UDFCD 2001)

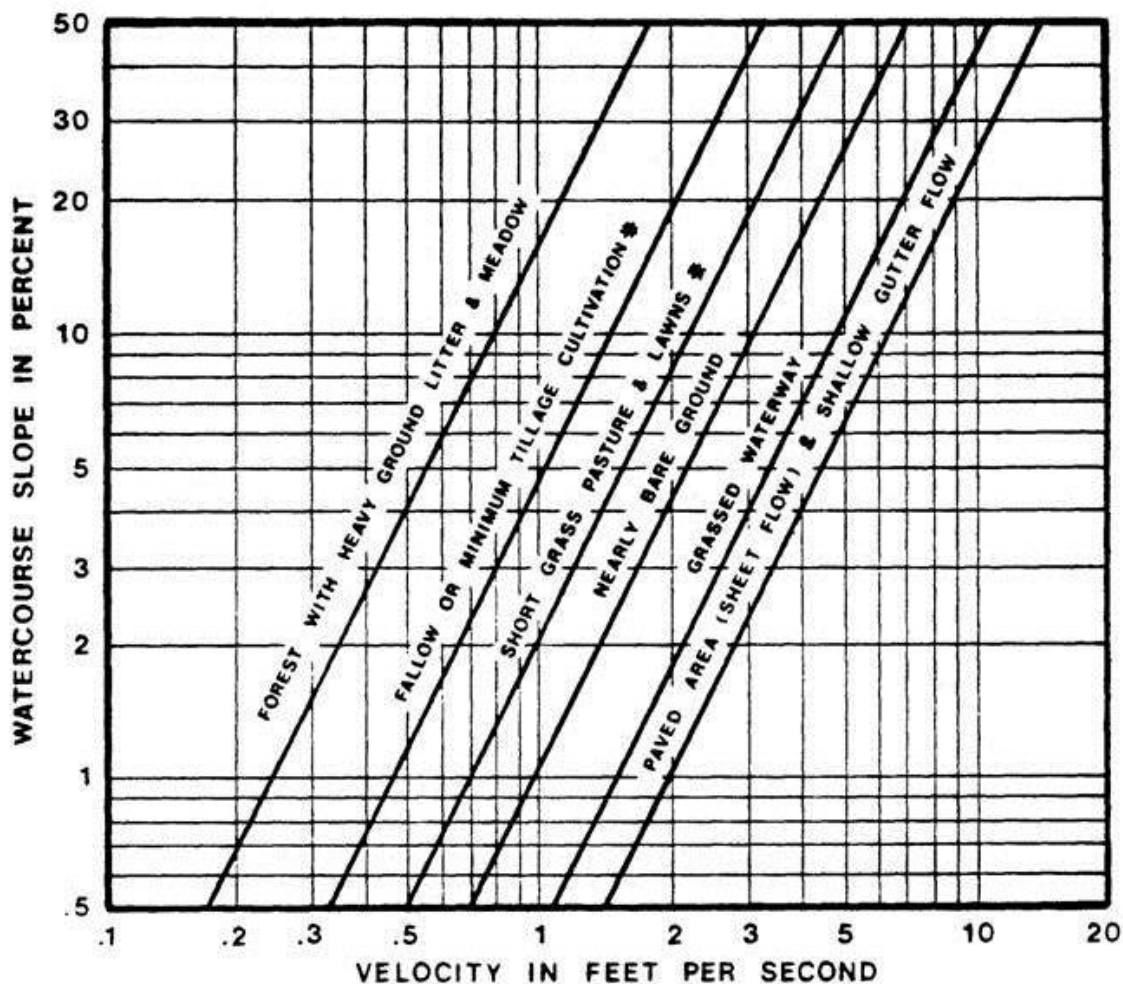
Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis-- Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

### 3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

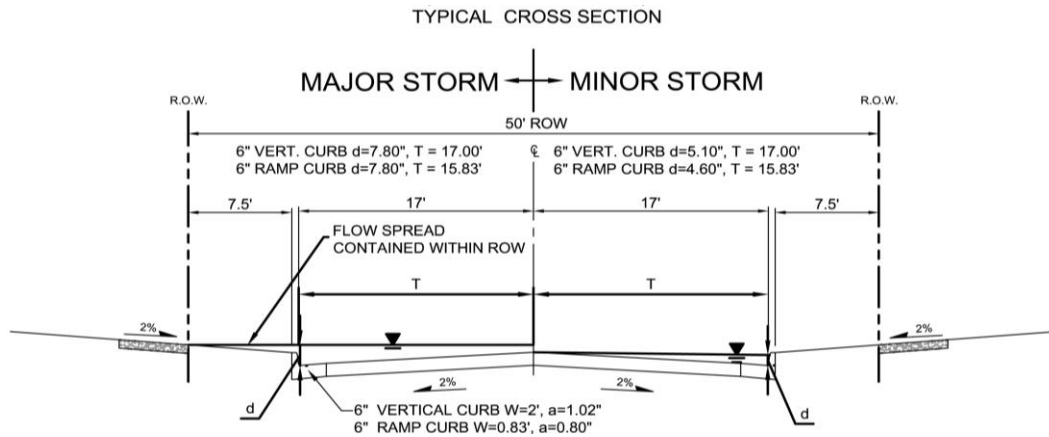
For urban areas, the time of concentration ( $t_c$ ) consists of an initial time or overland flow time ( $t_i$ ) plus the travel time ( $t_t$ ) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time ( $t_i$ ) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion ( $t_t$ ) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Figure 6-25. Estimate of Average Concentrated Shallow Flow

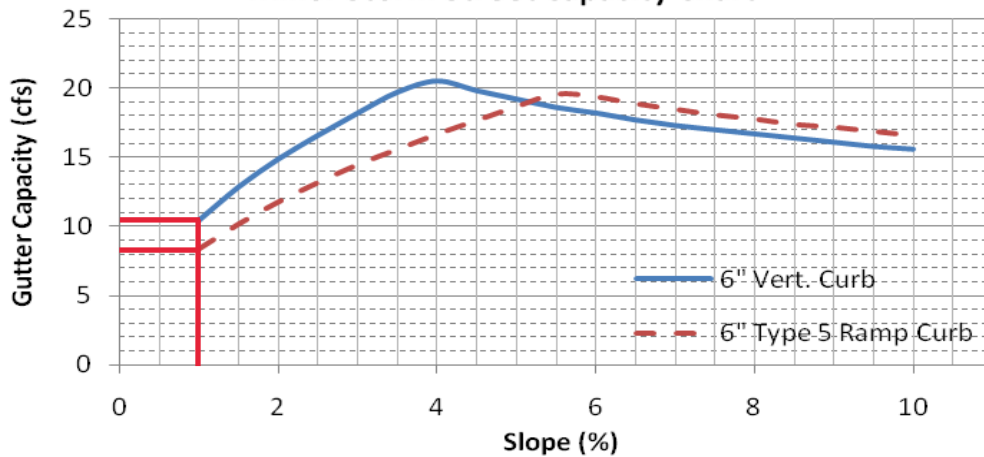




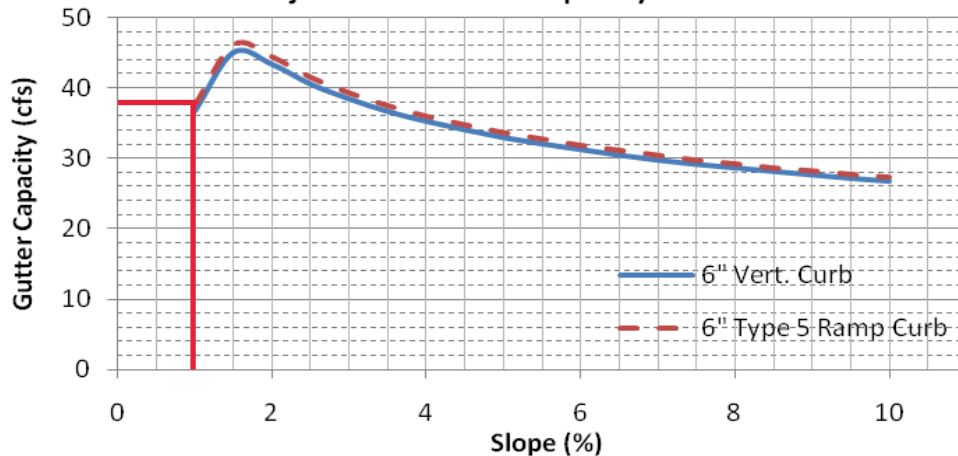
**Figure 7-7. Street Capacity Charts Residential (Detached Sidewalk)**



**Minor Storm Street Capacity Chart**



**Major Storm Street Capacity Chart**



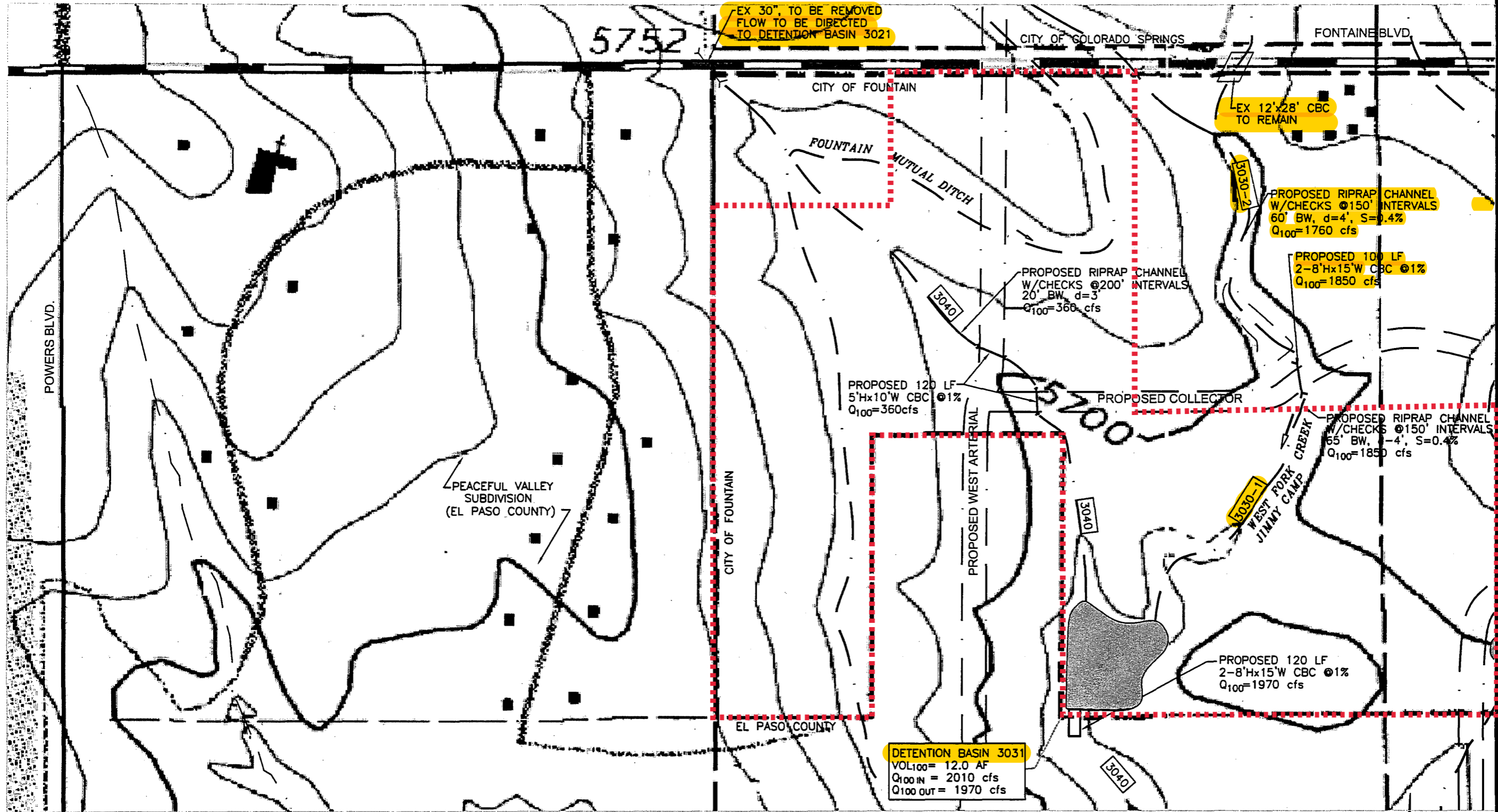
These charts shall only be used for the standard street sections as shown. The capacity shown is based on 1/2 the street section as calculated by the UD-Inlet spreadsheets. Minor storm capacities are based on no crown overtopping, curb height or maximum allowable spread widths. Major storm capacities are based on flow being contained within the public right-of-way, including conveyance capacity behind the curb. The UDFCD Safety Reduction Factor was applied. An 'n<sub>STREET</sub>' of 0.016 and 'n<sub>BACK</sub>' of 0.020 was used. Calculations were done using UD-Inlet 3.00.xls, March, 2011.

**Table 6-3. Recommended percentage imperviousness values**

Land Use or Surface Characteristics	Percentage Imperviousness (%)
<b>Business:</b>	
Downtown Areas	95
Suburban Areas	75
<b>Residential lots (lot area only):</b>	
Single-family	
2.5 acres or larger	12
0.75 – 2.5 acres	20
0.25 – 0.75 acres	30
0.25 acres or less	45
Apartments	75
<b>Industrial:</b>	
Light areas	80
Heavy areas	90
<b>Parks, cemeteries</b>	10
<b>Playgrounds</b>	25
<b>Schools</b>	55
<b>Railroad yard areas</b>	50
<b>Undeveloped Areas:</b>	
Historic flow analysis	2
Greenbelts, agricultural	2
Off-site flow analysis (when land use not defined)	45
<b>Streets:</b>	
Paved	100
Gravel (packed)	40
Drive and walks	90
Roofs	90
Lawns, sandy soil	2
Lawns, clayey soil	2

## **APPENDIX C**

### ***REPORT REFERENCES***



EX 30" TO BE REMOVED  
FLOW TO BE DIRECTED  
TO DETENTION BASIN 3021

EX 12'x28' CBC  
TO REMAIN

PROPOSED RIPRAP CHANNEL  
W/CHECKS @150' INTERVALS  
60' BW, d=4', S=0.4%  
Q<sub>100</sub>=1760 cfs

PROPOSED 100 LF  
2-8'Hx15'W CBC @1%  
Q<sub>100</sub>=1850 cfs

PROPOSED RIPRAP CHANNEL  
W/CHECKS @200' INTERVALS  
20' BW, d=3'  
Q<sub>100</sub>=360 cfs

PROPOSED 120 LF  
5'Hx10'W CBC @1%  
Q<sub>100</sub>=360 cfs

PROPOSED RIPRAP CHANNEL  
W/CHECKS @150' INTERVALS  
65' BW, d=4', S=0.4%  
Q<sub>100</sub>=1850 cfs

3030-1  
WEST FORK  
JIMMY CAMP

PROPOSED 120 LF  
2-8'Hx15'W CBC @1%  
Q<sub>100</sub>=1970 cfs

DETENTION BASIN 3031  
VOL<sub>100</sub>= 12.0 AF  
Q<sub>100 IN</sub> = 2010 cfs  
Q<sub>100 OUT</sub> = 1970 cfs

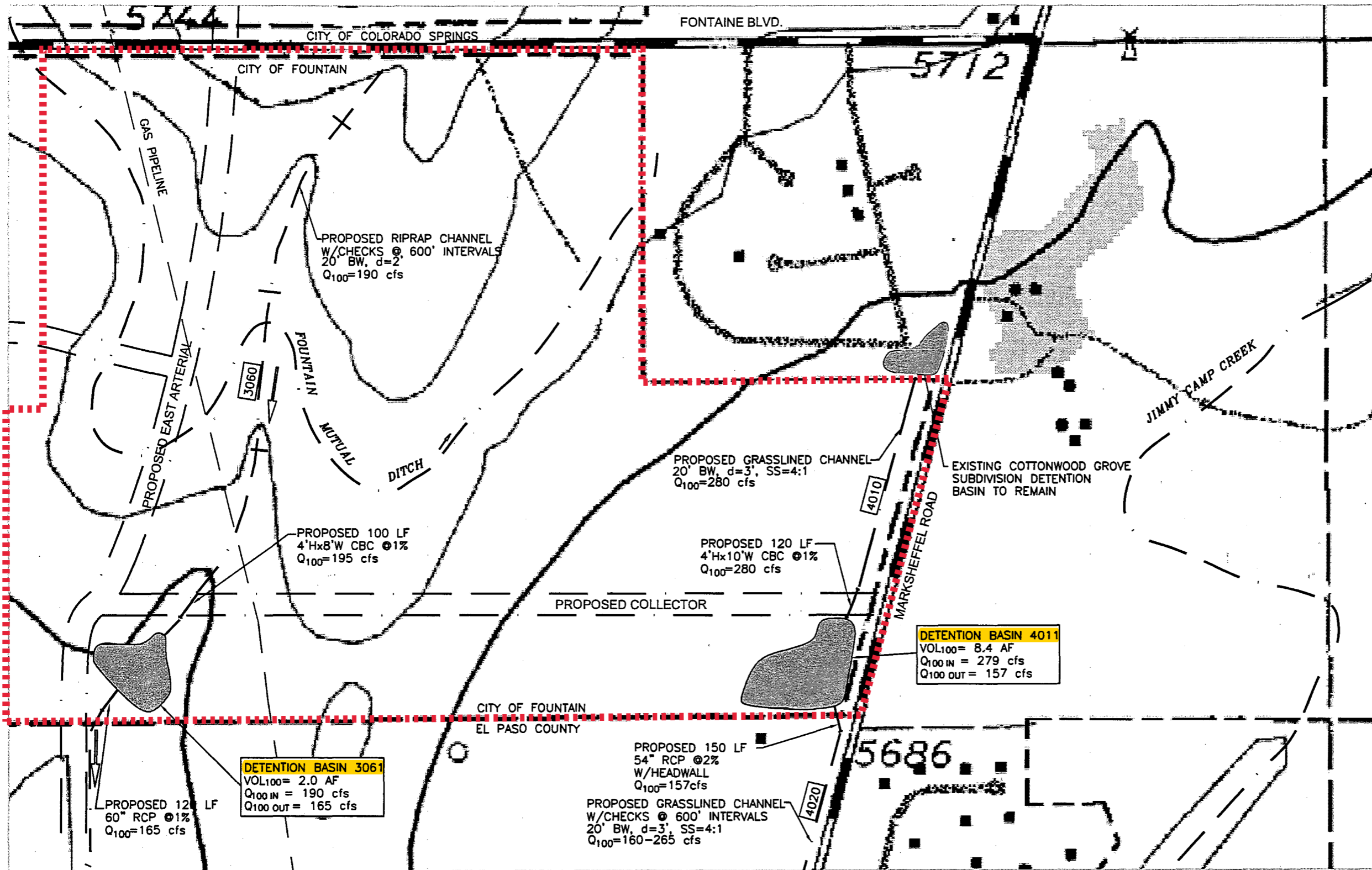
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Colorado Springs, Colorado  
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(719) 630-7342

WEST FORK JIMMY CAMP CREEK  
DRAINAGE BASIN PLANNING STUDY  
PRELIMINARY PLAN  
EL PASO COUNTY, COLORADO

Project No.:	9893
Date:	7/00
Design:	RNW
Drawn:	CAD
Check:	RNW
Revisions:	

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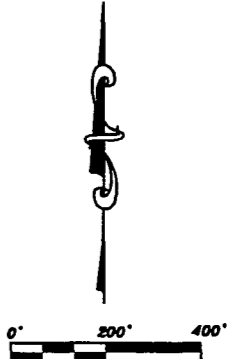


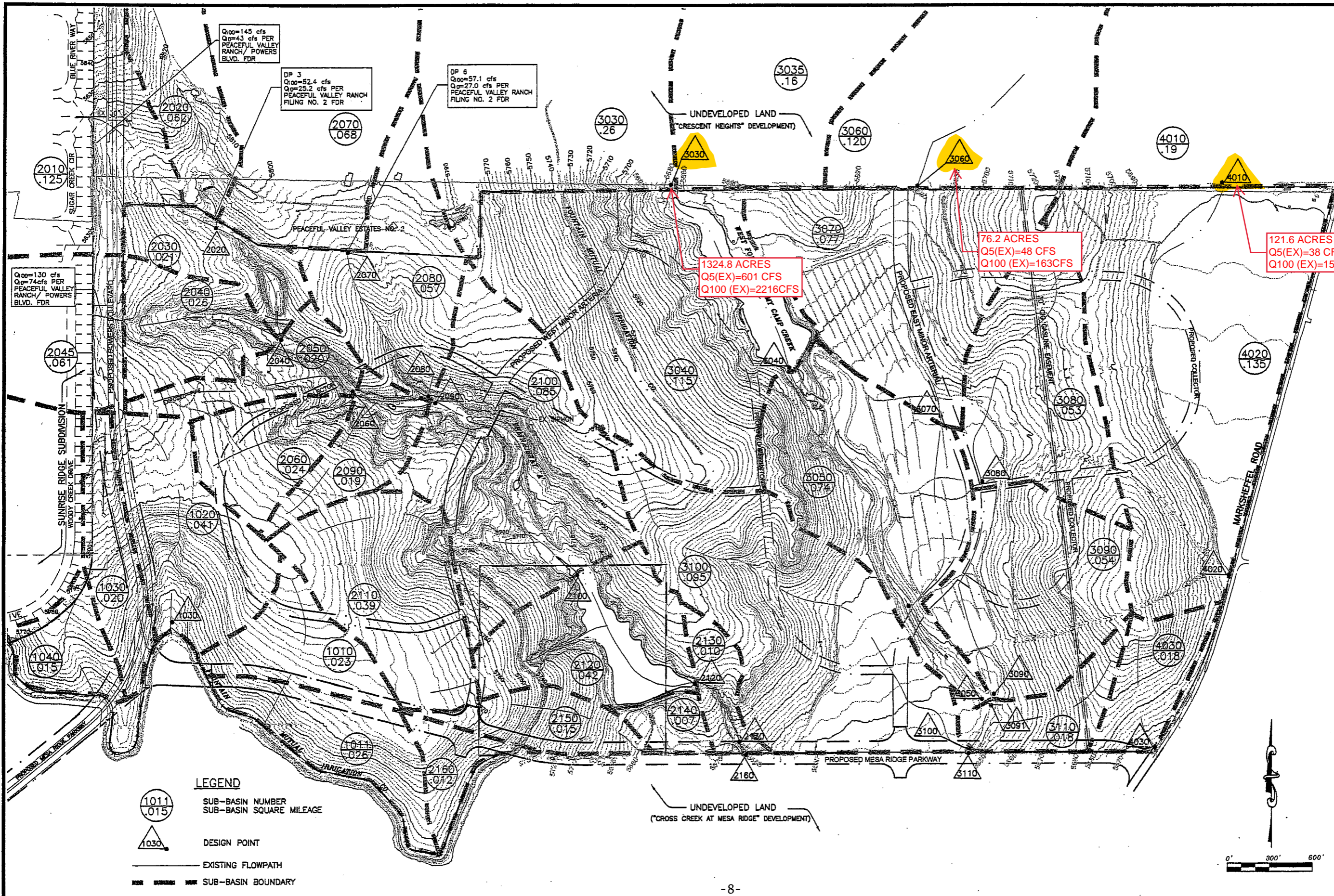
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**WEST FORK JIMMY CAMP CREEK  
 DRAINAGE BASIN PLANNING STUDY**  
 PRELIMINARY PLAN  
 EL PASO COUNTY, COLORADO





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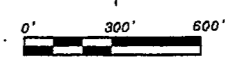




**LEGEND**

 SUB-BASIN NUMBER  
 SUB-BASIN SQUARE MILEAGE  
 DESIGN POINT  
 EXISTING FLOWPATH  
 SUB-BASIN BOUNDARY

UNDEVELOPED LAND  
 ("CROSS CREEK AT MESA RIDGE" DEVELOPMENT)



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**West Fork Jimmy Camp Creek  
 Drainage Basin Planning Study  
 HYDROLOGIC SUB-BASIN MAP  
 EL PASO COUNTY, COLORADO**

Project No.:	9893
Date:	7/00
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Revisions:	

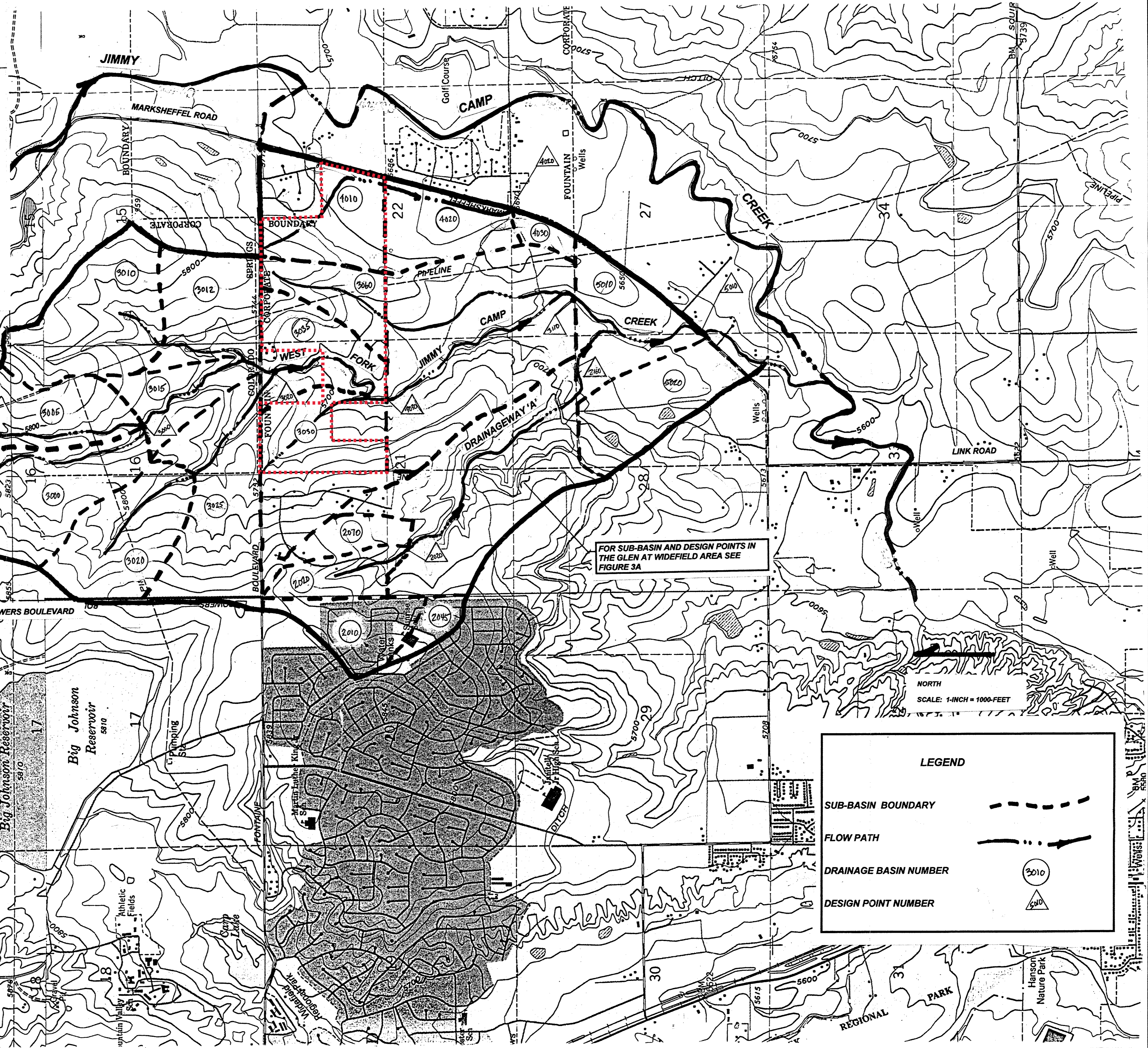
**FIG.3A**

TABLE 3: SUMMARY OF DESIGN POINT DISCHARGES  
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

DESIGN POINT NUMBER	EX/FUT DRAINAGE AREA (sqm)	EX/FUT DRAINAGE AREA (acres)	EXISTING CONDITION		FUTURE CONDITION	
			5 YR cfs	100 YR cfs	5 YR cfs	100YR cfs
2020	0.190	121.6	47	189	57	210
2040	0.300	192.0	97	335	109	362
2060	0.340	217.6	105	372	120	406
2080	0.130	83.2	17	88	28	113
2090	0.480	307.2	123	473	152	535
2100	0.610	390.4	140	558	181	651
2120	0.660	422.4	148	600	189	692
2130	0.670	428.8	145	594	186	687
2160	0.700	448.0	151	624	196	723
3000	0.660	422.4	147	233	317	935
3020	1.650	1056.0	528	1857	1059	2737
3030	2.070	1324.8	601	2216	1209	3267
3040	2.180	1395.2	618	2316	1239	3364
3050	2.28/2.23	1446/1427	627	2351	1275	3444
3070	0.200	128.0	67	235	86	270
3080	25/05	160/32	82	290	23	72
3090	33/11	211/70	106	373	44	138
3091	2.560	1638.4	732	2722	1380	3843
3100	2.660	1702.4	757	2828	1428	3990
3110	2.670	1708.8	761	2845	1442	4022
4020	0.320	204.8	63	238	145	383
5010	3.530	2259.2	943	3550	1722	4904

TABLE 2: SUMMARY OF SUB-BASIN DISCHARGES  
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

SUB-BASIN NUMBER	EX/FUT DRAINAGE AREA (sqm)	EX/FUT DRAINAGE AREA (ac)	EXISTING CONDITION (cfs)		FUTURE CONDITION (cfs)	
			5 YR	100 YR	5 YR	100YR
2010	0.125	80.0	40	142	40	142
2020	0.062	39.7	47	19	68	68
2030	0.021	13.4	5	22	6	24
2040	0.026	16.6	5	26	7	29
2045	0.061	39.0	48	124	48	124
2050	0.020	12.8	4	17	4	19
2060	0.024	15.4	5	24	6	30
2070	0.068	43.5	12	58	15	64
2080	0.057	36.5	3	14	5	19
2090	0.019	12.2	63	24	89	89
2100	0.056	36.8	6	29	8	33
2110	0.034	21.8	6	29	8	33
2120	0.047	30.1	2	11	2	11
2130	0.010	6.4	2	4	2	9
2140	0.007	4.5	6	20	6	21
2150	0.015	9.6	8	18	17	35
2160	0.012	7.7	8	18	17	35
3000	0.420	268.8	140	474	190	598
3005	0.240	153.6	107	347	144	407
3010	0.220	140.8	81	288	138	383
3012	0.210	134.4	54	199	94	272
3015	0.110	70.4	95	181	75	212
3020	0.190	121.6	89	231	204	428
3025	0.290	186.4	82	324	347	712
3030	0.290	186.4	85	262	116	391
3035	0.190	122.4	63	234	106	306
3040	0.190	122.4	23	110	31	129
3045	0.115	73.6	18	61	56	136
3050	0.049/074	31.447/4	48	163	63	189
3060	0.119	76.2	23	78	27	87
3070	0.077	49.3	16	58	23	68
3080	0.050	32.0	27	93	21	67
3090	0.062/05	52.532/0	63	123	61	166
3100	0.095	60.8	36	117	14	31
3110	0.018	11.5	5	17	14	31
4010	0.190	121.6	38	153	108	279
4020	0.135	86.4	26	90	39	114
4030	0.018	11.5	7	25	20	44
5010	0.156	99.8	35	133	101	248
5020	0.200	128.0	52	200	151/4	392



FOR SUB-BASIN AND DESIGN POINTS IN THE GLEN AT WIDEFIELD AREA SEE FIGURE 3A

**LEGEND**

- SUB-BASIN BOUNDARY: - - - - -
- FLOW PATH: - · - · -
- DRAINAGE BASIN NUMBER: (3010)
- DESIGN POINT NUMBER: (4010)

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**West Fork Jimmy Camp Creek  
 Drainage Basin Planning Study  
 HYDROLOGIC SUB-BASIN MAP  
 EL PASO COUNTY, COLORADO**

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 Revisions:

**FIGURE 3**

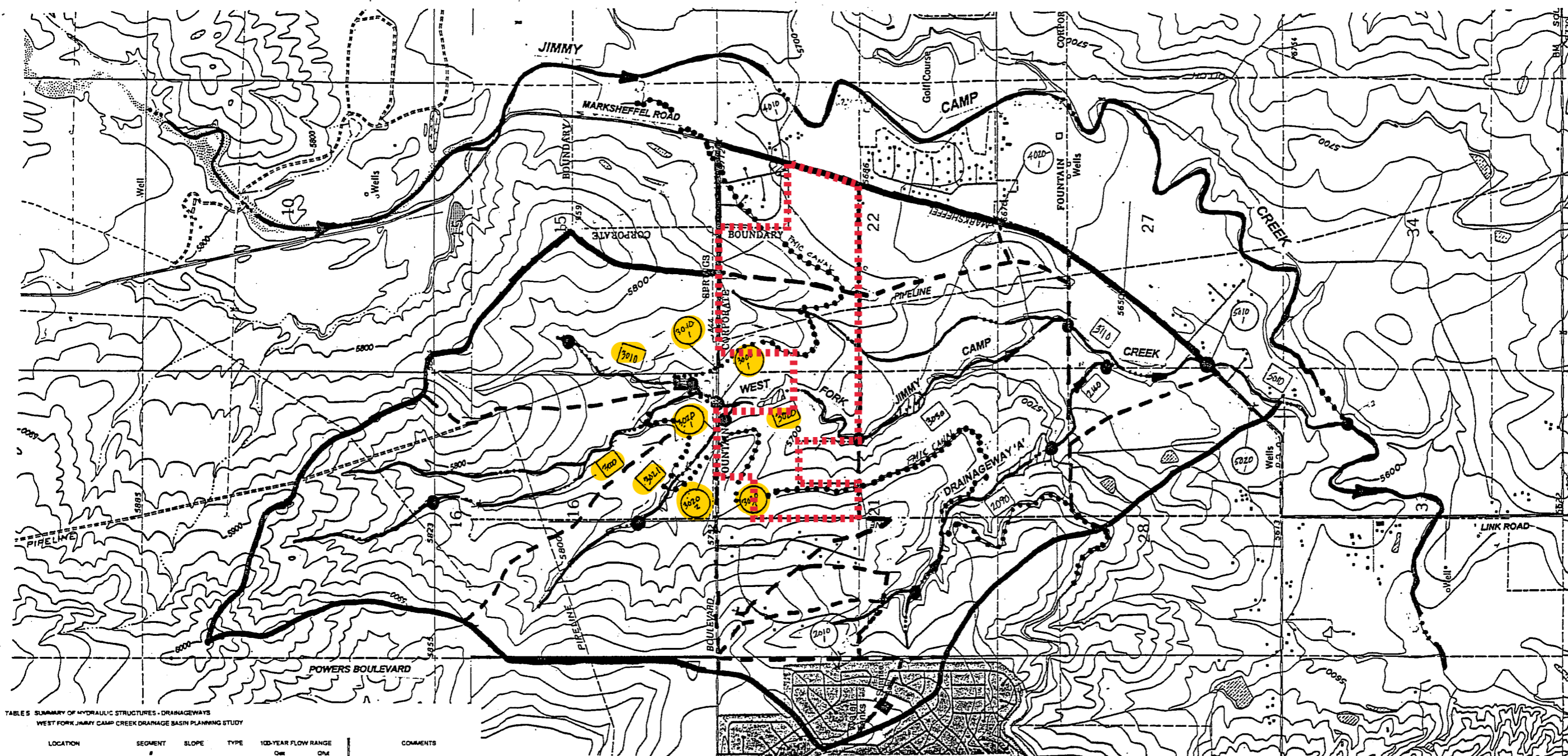



TABLE 3 SUMMARY OF HYDRAULIC STRUCTURES - DRAINAGEWAYS  
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY


LOCATION	SEGMENT #	SLOPE (Percent)	TYPE	100-YEAR FLOW RANGE		COMMENTS
				Old (cfs)	Old (cfs)	
<b>WEST FORK JIMMY CAMP CREEK</b>						
JIMMY CAMP CREEK TO MARKSHEFFEL ROAD	3010	0.2	UNIMPROVED	3,500	4,800	DRAINAGEWAY OUTFALLS TO JIMMY CAMP CREEK
MARKSHEFFEL ROAD TO MESA RIDGE PARKWAY	3110	0.6	UNIMPROVED	2,800-3,500	3,300-4,800	WIDE AND SHALLOW FLOODPLAIN
MESA RIDGE PARKWAY TO N PL OF THE GLEN	3000	0.7	UNIMPROVED	2,275-2,800	3,150-3,300	CHANNEL STABLE AND WELL VEGETATED WITH WETLAND AND NATIVE GRASSES
NORTH PL OF THE GLEN TO FONTAINE BOULEVARD	3000	0.8	UNIMPROVED	1,900-2,275	2,710-3,150	
FONTAINE BLVD TO STUDY LOTS	3000	1.0	UNIMPROVED	800	1,050	CHANNEL LIES WITHIN COLORADO CENTRE DEVELOPMENT
FONTAINE BLVD TO STUDY LOTS	3010	1.0	UNIMPROVED	400	640	CHANNEL LIES WITHIN COLORADO CENTRE DEVELOPMENT
FONTAINE BLVD TO STUDY LOTS	3021	0.8	UNIMPROVED	600	1,100	CHANNEL LIES WITHIN COLORADO CENTRE DEVELOPMENT
<b>DRAINAGEWAY A</b>						
CONFLUENCE WITH WEST FORK JIMMY TO LAKE	2180	2.6	UNIMPROVED	600	700	
LAKE TO DESIGN POINT OF 2000	3300	1.8	UNIMPROVED	335-600	390-700	CHANNEL STABLE AND WELL VEGETATED WITH WETLAND AND NATIVE GRASSES


TABLE 4 SUMMARY OF HYDRAULIC STRUCTURES - CROSSINGS  
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY


LOCATION	CULVERT #	SIZE	TYPE	PROPOSED FLOW		CAPACITY EXISTING	CAPACITY FUTURE (I)	COMMENTS
				OS (cfs)	O100 (cfs)			
FONTAINE BLVD	3000-1	12'-0"	CBC	770	1,070	ADEQUATE	ADEQUATE	STRUCTURE HAS ADEQUATE CAPACITY TO PASS THE PROPOSED 100-YEAR FLOW
FONTAINE BLVD	3010-1	30"-54"	CMP ARCH	N/A	N/A	N/A	N/A	FONTAINE MUTUAL IRRIGATION DITCH ROADWAY CROSSING
FONTAINE BLVD	3020-1	30"	CMP	500	1,100	INADEQUATE	INADEQUATE	CULVERT CAN CONVEY ONLY LOCALIZED ROADWAY DRAINAGE WHICH REACHES IT
FONTAINE BLVD	3020-2	30"-54"	CMP ARCH	NA	NA	N/A	N/A	FONTAINE MUTUAL IRRIGATION DITCH ROADWAY CROSSING
FONTAINE BLVD	3020-3	30"	CMP	N/A	N/A	ADEQUATE	INADEQUATE	CULVERT CAN CONVEY ONLY LOCALIZED ROADWAY DRAINAGE WHICH REACHES IT
MARKSHEFFEL ROAD	3010-1	30"	CMP	1,700	4,800	INADEQUATE	INADEQUATE	PARTIALLY PLUGGED
MARKSHEFFEL ROAD	3020-1	30"	CMP	100	300	INADEQUATE	INADEQUATE	PARTIALLY PLUGGED
POWERS BOULEVARD	2010-1	30"	CMP	40	142	ADEQUATE	ADEQUATE	CULVERT TO BE REPLACED WITH CONSTRUCTION OF POWERS BOULEVARD
MARKSHEFFEL ROAD	4010-1	N/A	DETENTION BASIN	N/A	N/A	ADEQUATE	ADEQUATE	DETENTION BASIN SERVES THE COTTONWOOD GROVE SUBDIVISION
MARKSHEFFEL ROAD	4020-1	30" (wall)	CMP	145	383	INADEQUATE	INADEQUATE	PARTIALLY PLUGGED

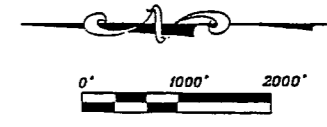
**LEGEND**

ROADWAY CROSSING DESIGNATION 

DRAINAGEWAY DESIGNATION 

FONTAINE MUTUAL IRRIGATION DITCH 

EXISTING IMPOUNDMENT 



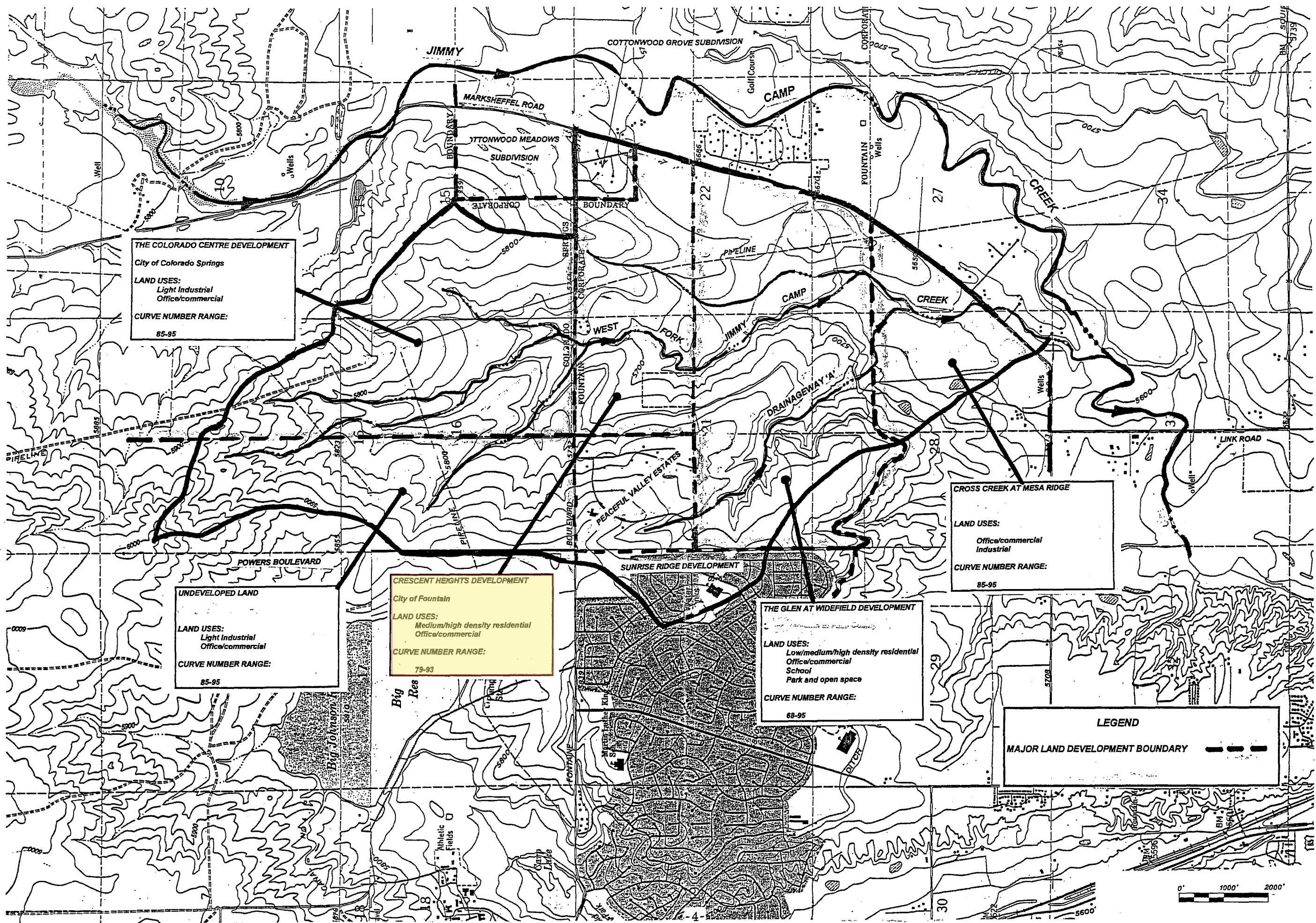
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**West Fork Jimmy Camp Creek  
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 INVENTORY OF EXISTING DRAINAGE STRUCTURES  
 EL PASO COUNTY, COLORADO**

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 Check: RNW  
 Revision:

FIGURE 4





**THE COLORADO CENTRE DEVELOPMENT**  
 City of Colorado Springs  
**LAND USES:**  
 Light Industrial  
 Office/commercial  
**CURVE NUMBER RANGE:**  
 85-95

**UNDEVELOPED LAND**  
**LAND USES:**  
 Light Industrial  
 Office/commercial  
**CURVE NUMBER RANGE:**  
 85-95

**CRESCENT HEIGHTS DEVELOPMENT**  
 City of Fountain  
**LAND USES:**  
 Medium/high density residential  
 Office/commercial  
**CURVE NUMBER RANGE:**  
 79-93

**THE GLEN AT WIDEFIELD DEVELOPMENT**  
**LAND USES:**  
 Low/medium/high density residential  
 Office/commercial  
 School  
 Park and open space  
**CURVE NUMBER RANGE:**  
 68-95

**CROSS CREEK AT MESA RIDGE**  
**LAND USES:**  
 Office/commercial  
 Industrial  
**CURVE NUMBER RANGE:**  
 85-95

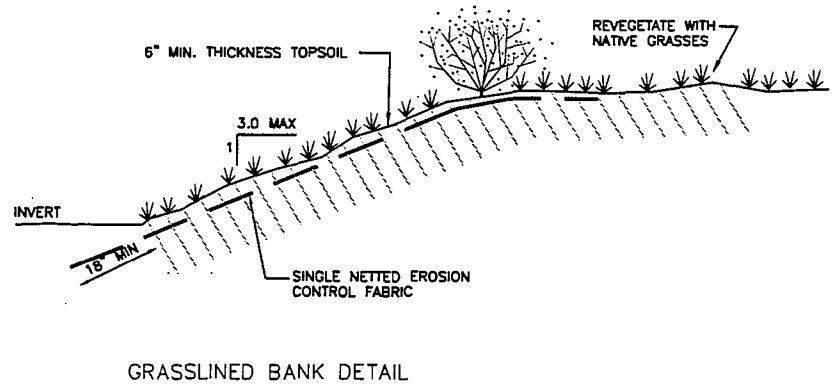
**LEGEND**  
 MAJOR LAND DEVELOPMENT BOUNDARY

**Kiowa Engineering Corporation**  
 1604 South 21st Street  
 Colorado Springs, Colorado  
 80904  
 (719) 630-7342

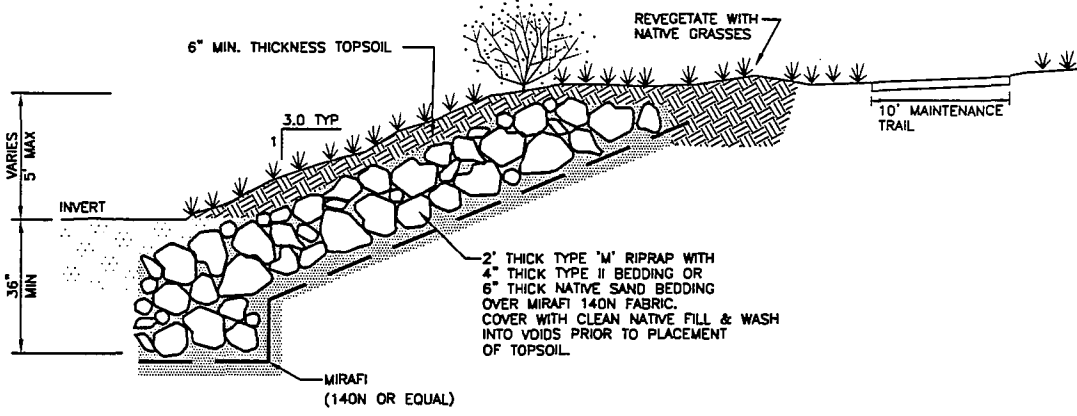
**West Fork Jimmy Camp Creek  
 Drainage Basin Planning Study  
 MAJOR DEVELOPMENT & LAND USE MAP**  
 EL PASO COUNTY, COLORADO

Project No.: 9893  
 Date: 6/99  
 Design: RNW  
 Drawn: CAD  
 Check: RNW  
 Revisions:

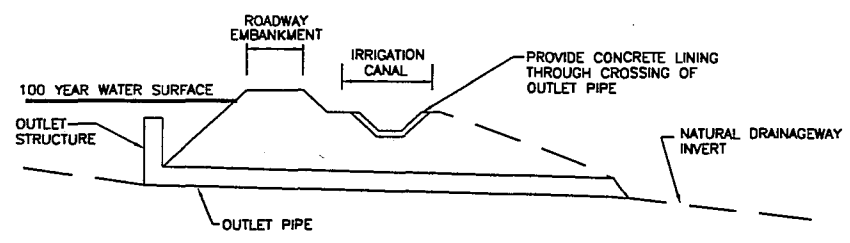
**FIGURE 2**



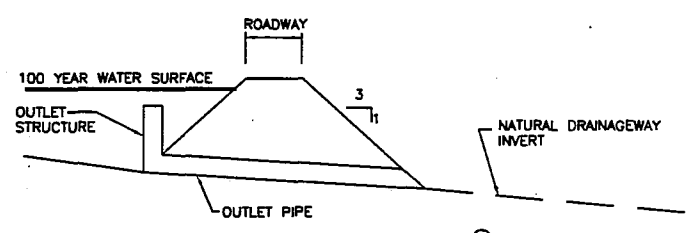
GRASSLINED BANK DETAIL



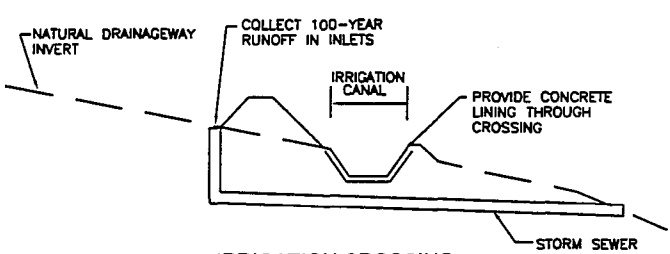
RIPRAP BANK LINING DETAIL  
NTS



IRRIGATION CANAL CROSSING  
AT DETENTION BASIN  
(NTS)



IRRIGATION CROSSING WITH SIPHON  
AT DETENTION BASIN  
(NTS)



IRRIGATION CROSSING  
AT SEWER CROSSING  
(NTS)

RIPRAP GRADATIONS

TYPE H RIPRAP INTERMEDIATE ROCK DIMENSION IN INCHES	% SMALLER THAN GIVEN SIZE BY WEIGHT	D <sub>50</sub> INCHES
30	100	18
24	50-70	
18	35-50	
6	2-10	

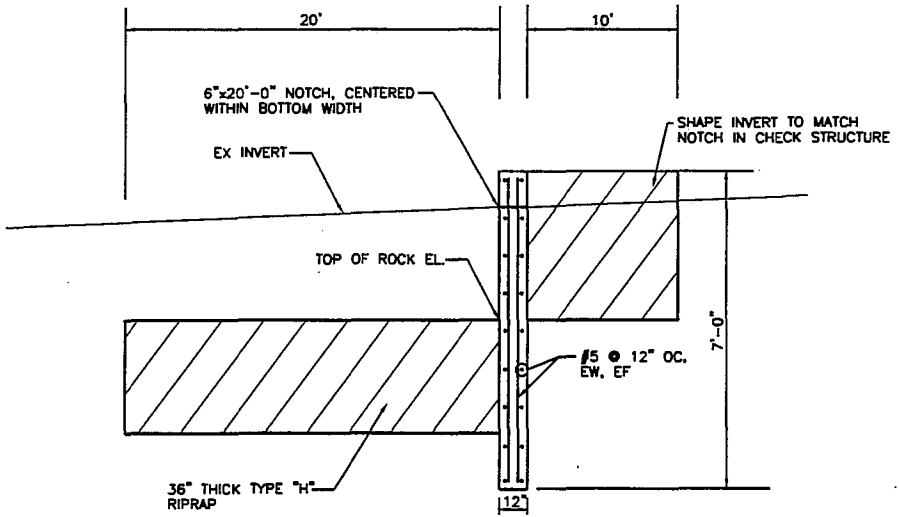
  

TYPE M RIPRAP INTERMEDIATE ROCK DIMENSION IN INCHES	% SMALLER THAN GIVEN SIZE BY WEIGHT	D <sub>50</sub> INCHES
21	100	12
18	50-70	
12	35-50	
4	2-10	

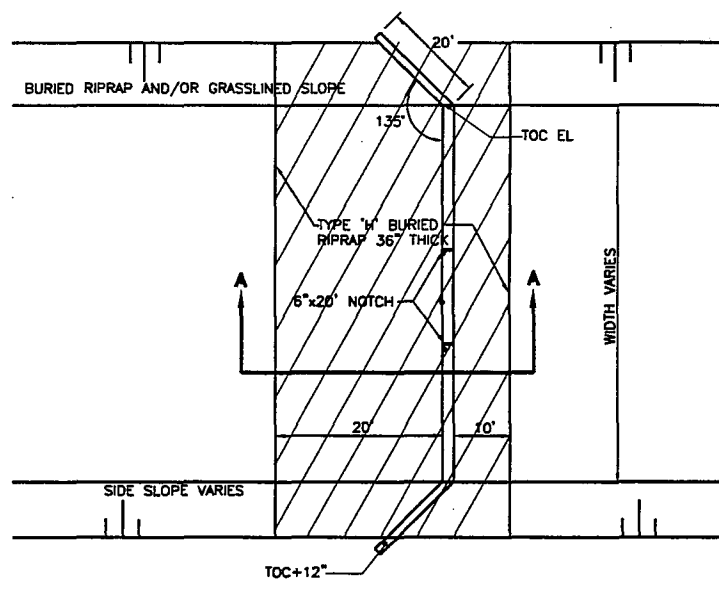
SEED MIX

AREAS DISTURBED BY THE EARTHWORK SHALL BE PERMANENTLY REVEGETATED WITH NATIVE GRASSES. NATIVE SEED MIX FOR THIS PROJECT SHALL BE AS FOLLOWS:

NATIVE SEED MIX		pls/acre
BLUE GRAMA	<i>Chondrosium hirsutum</i>	2.0
SIDEOATS GRAMA	<i>Bouteloua curtipendula</i>	3.0
SLENDER WHEATGRASS	<i>Agropyron trachycalum trachycalum</i>	2.0
WESTERN WHEATGRASS	<i>Agropyron smithii</i>	4.0
		11.0 lbs



SECTION A-A



TYPICAL CHECK STRUCTURE PLAN  
NO SCALE

Kiowa Engineering Corporation  
 1604 South 21st Street  
 Colorado Springs, Colorado  
 8004  
 (719) 630-7342

West Fork Jimmy Camp Creek  
 Drainage Basin Planning Study  
 TYPICAL DRAINAGEWAY DETAILS  
 EL PASO COUNTY, COLORADO

Project No.: 9893
Date: 7/00
Design: RNW
Drawn: CAD
Check: RNW
Revisions:

TABLE 2: SUMMARY OF SUB- BASIN DISCHARGES  
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

SUB-BASIN NUMBER	EX/FUT DRAINAGE		EXISTING CONDITION (cfs)		FUTURE CONDITION (cfs)	
	AREA (sm)	AREA (ac)	5 YR	100 YR	5 YR	100YR
2010	0.125	80.0	40	142	40	142
2020	0.062	39.7	9	47	19	68
2030	0.021	13.4	5	22	6	24
2040	0.026	16.6	5	26	7	29
2045	0.061	39.0	48	124	48	124
2050	0.020	12.8	4	17	4	19
2060	0.024	15.4	5	24	8	30
2070	0.068	43.5	8	44	17	65
2080	0.057	36.5	12	58	15	64
2090	0.019	12.2	3	14	5	19
2100	0.095	60.8	13	64	24	89
2110	0.034	21.8	6	29	8	33
2120	0.047	30.1	9	45	9	45
2130	0.010	6.4	2	11	2	11
2140	0.007	4.5	2	4	2	9
2150	0.015	9.6	6	20	6	21
2160	0.012	7.7	8	18	17	35
3000	0.420	268.8	140	474	190	568
3005	0.240	153.6	107	347	144	407
3010	0.220	140.8	81	288	138	383
3012	0.210	134.4	54	199	94	272
3015	0.110	70.4	55	181	75	212
3020	0.190	121.6	69	231	204	428
3025	0.260	166.4	82	324	347	712
3030	0.260	166.4	65	262	116	361
3035	0.160	102.4	63	234	106	306
3040	0.115	73.6	23	110	31	129
3050	0.049/074	31.4/47.4	18	61	56	136
3060	0.119	76.2	48	163	63	189
3070	0.077	49.3	23	78	27	87
3080	0.050	32.0	16	58	23	68
3090	0.082/05	52.5/32.0	27	93	21	67
3100	0.095	60.8	35	123	61	166
3110	0.018	11.5	5	17	14	31
4010	0.190	121.6	38	153	108	279
4020	0.135	86.4	26	90	39	114
4030	0.018	11.5	7	25	20	44
5010	0.156	99.8	35	133	101	246
5020	0.200	128.0	52	200	1514	362

TABLE 3: SUMMARY OF DESIGN POINT DISCHARGES  
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

DESIGN POINT NUMBER	EX/FUT DRAINAGE		EXISTING CONDITION		FUTURE CONDITION	
	AREA (sm)	AREA (acres)	5 YR cfs	100 YR cfs	5 YR cfs	100YR cfs
2020	0.190	121.6	47	189	57	210
2040	0.300	192.0	97	335	109	362
2060	0.340	217.6	105	372	120	406
2080	0.130	83.2	17	88	28	113
2090	0.480	307.2	123	473	152	535
2100	0.610	390.4	140	558	181	651
2120	0.660	422.4	148	600	189	692
2130	0.670	428.8	145	594	186	687
2160	0.700	448.0	151	624	196	723
3000	0.660	422.4	147	233	317	935
3020	1.650	1056.0	528	1857	1059	2737
3030	2.070	1324.8	601	2216	1209	3267
3040	2.180	1395.2	618	2316	1239	3364
3050	2.26/2.23	1446/1427	627	2351	1275	3444
3070	0.200	128.0	67	235	86	270
3080	.25/.05	160/32	82	290	23	72
3090	.33/.11	211/70	106	373	44	138
3091	2.560	1638.4	732	2722	1380	3843
3100	2.660	1702.4	757	2828	1428	3990
3110	2.670	1708.8	761	2845	1442	4022
4020	0.320	204.8	63	238	145	383
5010	3.730	2387.2	943	3550	1722	4904

WFCC FLOWS @  
SITE ENTRANCE

WFCC FLOWS @  
SITE EXIT

**Amended Master Development Drainage Plan  
The Glen at Widefield**

**El Paso County, Colorado**

Prepared for:  
New Generation Homes  
3 Widefield Boulevard  
Colorado Springs, Colorado 80911

Prepared by:  
Kiowa Engineering Corporation  
1604 South 21<sup>st</sup> Street  
Colorado Springs, Colorado 80904-4208

Kiowa Project No. 06026

June 21, 2007

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 04MAY07 TIME 17:33:30 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

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X X XXXXXXX XXXXX X
X X X X X XX
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XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

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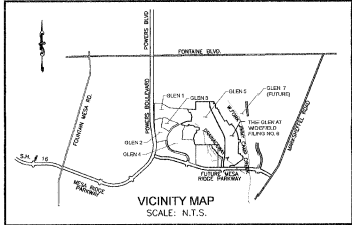
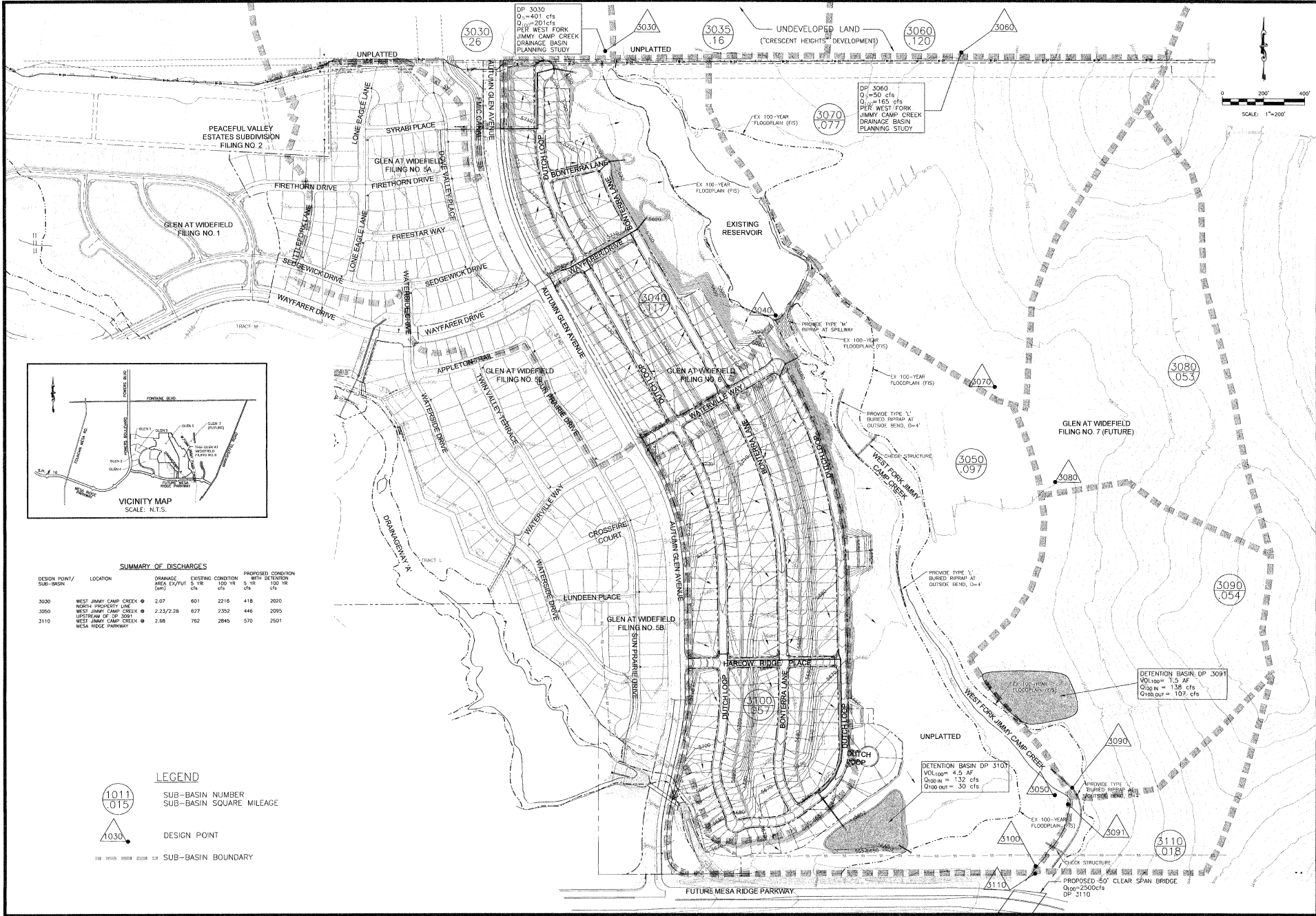
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2 ID KIOWA ENGINEERING - PROJECT NO. 06026
3 ID 2, 5, 10 & 100 YEAR STORMS FILENAME: GLEN6DET.DAT DEV COND WITH DETENTION
4 ID 24HR STORM DURATION
  *DIAGRAM
5 IT 5 0 0 250
6 IO 5
7 JR PREC .47 .56 .70 1
8 KK E1010
9 BA .05
10 IN 15
11 PB 4.4
12 PC 0.0 .0005 .0015 .0030 .0045 .0060 .0080 .0100 .0120 .0143

```

2 COMBINED AT									
+	DP3000	.66	1	FLOW TIME	215. 6.25	317. 6.25	493. 6.25	935. 6.17	
ROUTED TO									
+	R3015	.66	1	FLOW TIME	210. 6.33	313. 6.25	493. 6.25	925. 6.25	
HYDROGRAPH AT									
+	E3015	.11	1	FLOW TIME	51. 6.08	75. 6.08	115. 6.08	212. 6.08	
2 COMBINED AT									
+	DP3020	.77	1	FLOW TIME	245. 6.25	365. 6.25	570. 6.25	1077. 6.17	
HYDROGRAPH AT									
+	E3010	.22	1	FLOW TIME	96. 6.17	138. 6.17	211. 6.17	383. 6.17	
ROUTED TO									
+	R3012	.22	1	FLOW TIME	93. 6.25	134. 6.25	204. 6.17	378. 6.17	
HYDROGRAPH AT									
+	E3012	.21	1	FLOW TIME	64. 6.33	94. 6.33	147. 6.33	272. 6.33	
HYDROGRAPH AT									
+	E3020	.19	1	FLOW TIME	159. 6.17	204. 6.17	275. 6.17	428. 6.17	
ROUTED TO									
+	R3025	.19	1	FLOW TIME	158. 6.25	201. 6.25	270. 6.25	418. 6.25	
HYDROGRAPH AT									
+	E3025	.26	1	FLOW TIME	273. 6.08	347. 6.08	463. 6.08	712. 6.08	
5 COMBINED AT									
+	DP3020	1.65	1	FLOW TIME	761. 6.17	1059. 6.17	1562. 6.17	2737. 6.17	
ROUTED TO									
+	DB3021	1.65	1	FLOW TIME	255. 6.75	348. 6.75	554. 6.67	1808. 6.42	

\*\* PEAK STAGES IN FEET \*\*





1	STAGE	102.94	103.58	105.54	108.68
	TIME	6.75	6.75	6.67	6.42



**SUMMARY OF DISCHARGES**

DESIGN POINT/ SUB-BASIN	LOCATION	DRAINAGE AREA (SQ FT) (SQ MI)	EXISTING CONDITION 100 YR CFD	PROPOSED CONDITION WITH DETENTION 100 YR CFD	100 YR CFD	100 YR CFD
3030	WEST JIMMY CAMP CREEK	2.07	601	2216	418	2620
	NORTH PROPERTY LINE					
3060	WEST JIMMY CAMP CREEK	2.23/2.28	627	2352	446	2095
	LIFETIME OF DP 3091					
3110	WEST JIMMY CAMP CREEK	2.66	762	2845	570	2501
	MESA RIDGE PARKWAY					

**LEGEND**

-  SUB-BASIN NUMBER
-  SUB-BASIN SQUARE MILEAGE
-  DESIGN POINT
-  SUB-BASIN BOUNDARY

**Kiowa Engineering Corporation**  
 1604 South 21st Street  
 Colorado Springs, Colorado 80904  
 (719) 530-7342

**THE GLEN AT WIDEFIELD  
 AMENDED MASTER DEVELOPMENT DRAINAGE PLAN  
 WEST FORK JIMMY CAMP CREEK DEVELOPED CONDITION**  
 EL PASO COUNTY, COLORADO

Project No.: 06026  
 Date: June 21, 2007  
 Design: JGD  
 Drawn: JGD  
 Check: AWMc  
 Revisions:

SHEET

**FIG. 3**

**NOTES TO USERS**

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
 NOAA, NINGS12  
 National Geodetic Survey  
 SSMC-3, #9202  
 1315 East-West Highway  
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

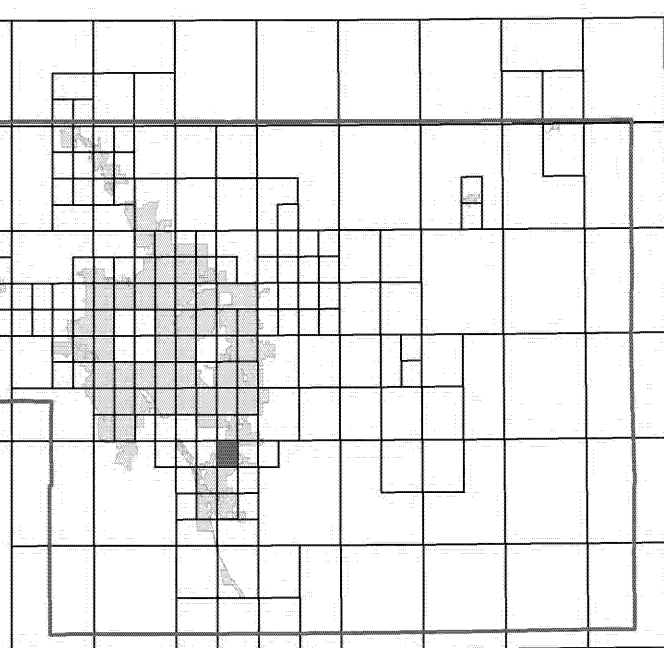
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FIMX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip>.

**El Paso County Vertical Datum Offset Table**

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	

**Panel Location Map**



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

**LEGEND**

- SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD
- The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equalled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.
- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decreedified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.
- FLOODWAY AREAS IN ZONE AE
- The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.
- OTHER FLOOD AREAS**
- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot, or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.
- OTHER AREAS**
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS
- OTHERWISE PROTECTED AREAS (OPAs)

- CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.
- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

- Base Flood Elevation line and value; elevation in feet\* (EL 987)
- Base Flood Elevation value where uniform within zone; elevation in feet\*

\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

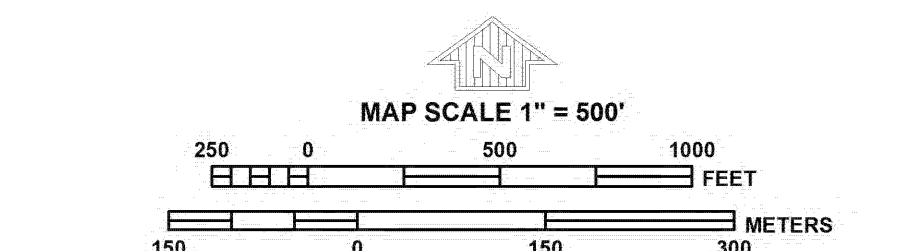
- Cross section line
- Transsect line
- 97° 07' 30.00" 32° 22' 30.00" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 4750000N 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 6000000 FT 5000-foot grid ticks; Colorado State Plane coordinate system, central zone (FIPSZONE 0902), Lambert Conformal Conic Projection
- DX5510 Bench mark (see explanation in Notes to Users section of this FIRM panel)
- M1.5 River Mile

MAP REPOSITORIES  
 Refer to Map Repository list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP  
**MARCH 17, 1997**

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL  
**DECEMBER 7, 2018** - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.  
 To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



**NFP**

**PANEL 0956G**

**FIRM**  
 FLOOD INSURANCE RATE MAP  
**EL PASO COUNTY, COLORADO**  
 AND INCORPORATED AREAS

**PANEL 956 OF 1300**  
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

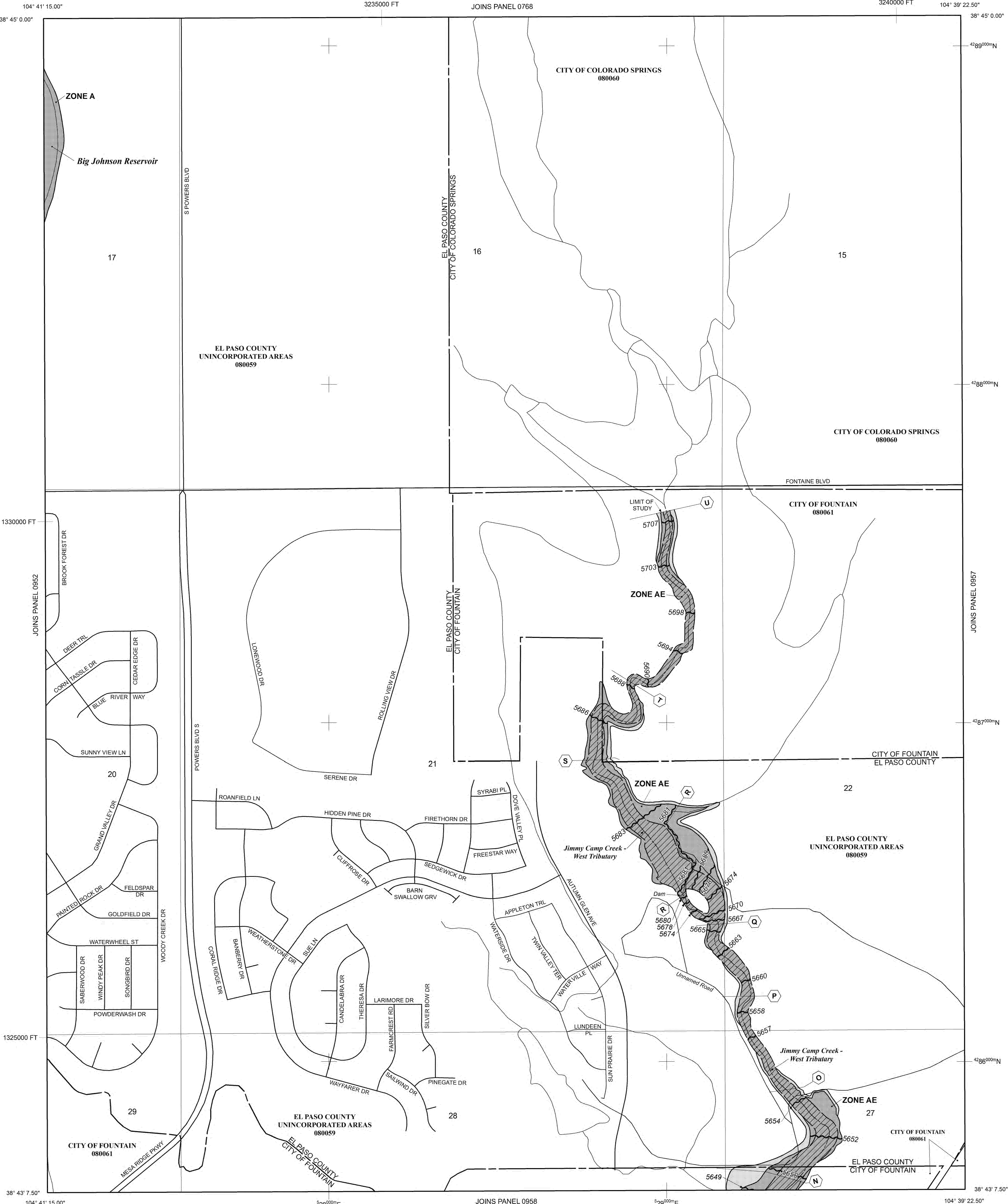
CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0956	G
EL PASO COUNTY	080259	0956	G
FOUNTAIN, CITY OF	080261	0956	G

Notice to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

**MAP NUMBER**  
**08041C0956G**

**MAP REVISED**  
**DECEMBER 7, 2018**  
 Federal Emergency Management Agency



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST.



**NOTES TO USERS**

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

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Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

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NGS Information Services  
NOAA, NIMS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, MD 20910-3282

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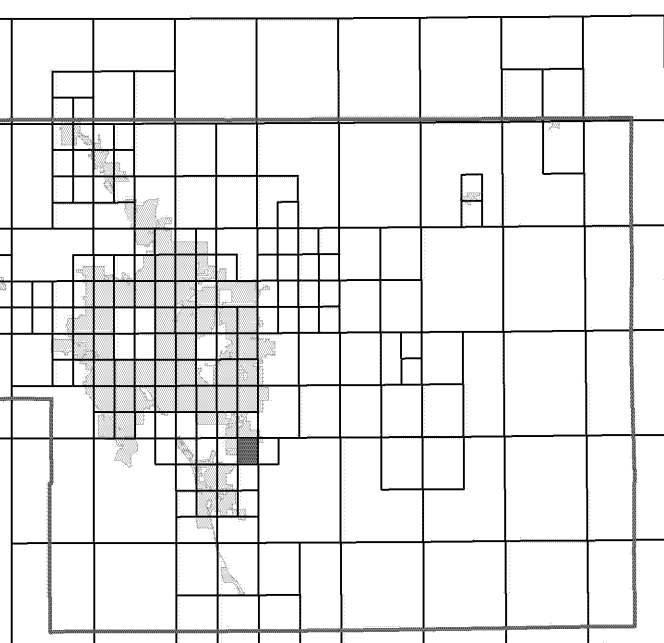
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FIMX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfp>.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	

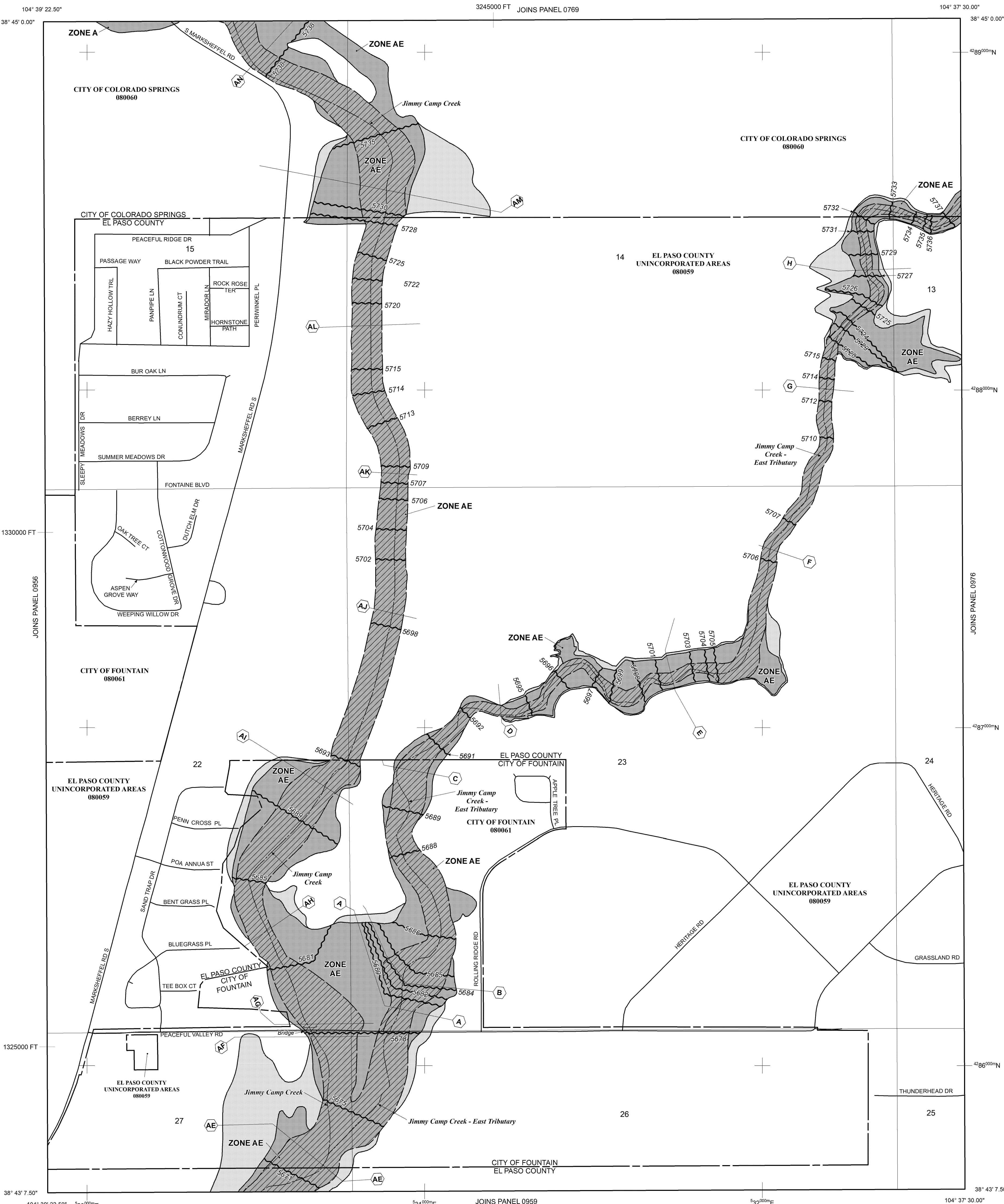
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST.

**LEGEND**

**SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equalled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
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- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**  
The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

**OTHER FLOOD AREAS**  
**ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot, or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

**OTHER AREAS**  
**ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.

**ZONE D** Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**

**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D Boundary
- CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

Base Flood Elevation value where uniform within zone; elevation in feet\*

\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

— Cross section line

— Transsect line

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks, zone 13

5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection

Bench mark (see explanation in Notes to Users section of this FIRM panel)

River Mile

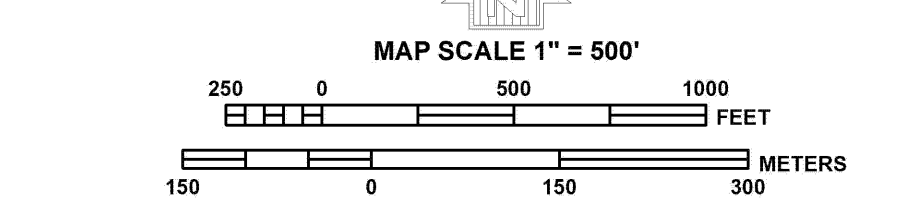
MAP REPOSITORIES  
Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP  
MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL  
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



**NFIP** **PANEL 0957G**

**FIRM**  
**FLOOD INSURANCE RATE MAP**  
**EL PASO COUNTY, COLORADO AND INCORPORATED AREAS**

**PANEL 957 OF 1300**  
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	08060	0957	G
EL PASO COUNTY	08059	0957	G
FOUNTAIN, CITY OF	08061	0957	G

Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the Notice-to-User Letter that accompanied this correction for details.

Notice to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

**MAP NUMBER**  
**08041C0957G**

**MAP REVISED**  
**DECEMBER 7, 2018**

Federal Emergency Management Agency

**NOTES TO USERS**

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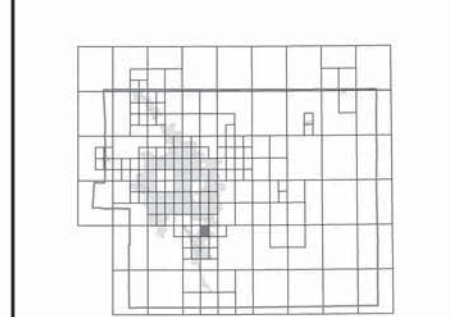
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**El Paso County Vertical Datum Offset Table**

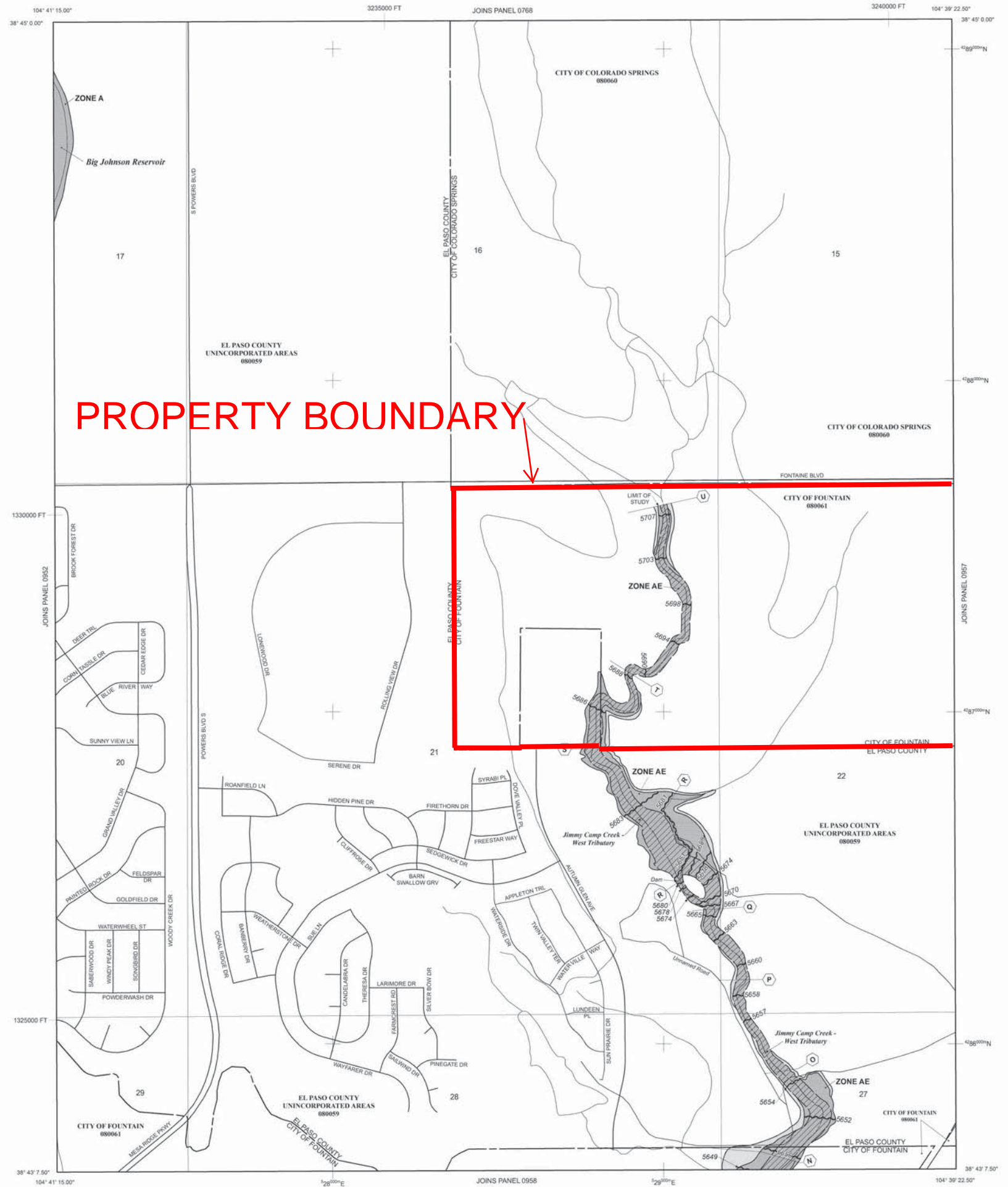
Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	

**Panel Location Map**



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**PROPERTY BOUNDARY**

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST.

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- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation line and value, elevation in feet\* (EL 987)
- Base Flood Elevation value where uniform within zone; elevation in feet\*
- \* Referenced to the North American Vertical Datum of 1988 (NAVD 88)
- Cross section line
- Transect line
- Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 5502), Lambert Conformal Conic Projection
- Bench mark (see explanation in Notes to Users section of this FIRM panel)
- River Mile
- MAP REPOSITORIES**
- Refer to Map Repositories list on Map Index
- EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP**  
MARCH 17, 1997
- EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL**  
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.
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**NFP**

**PANEL 0956G**

**FIRM**  
FLOOD INSURANCE RATE MAP  
EL PASO COUNTY,  
COLORADO  
AND INCORPORATED AREAS

**PANEL 956 OF 1300**  
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	08060	0956	G
EL PASO COUNTY	08059	0956	G
FOUNTAIN, CITY OF	08061	0956	G

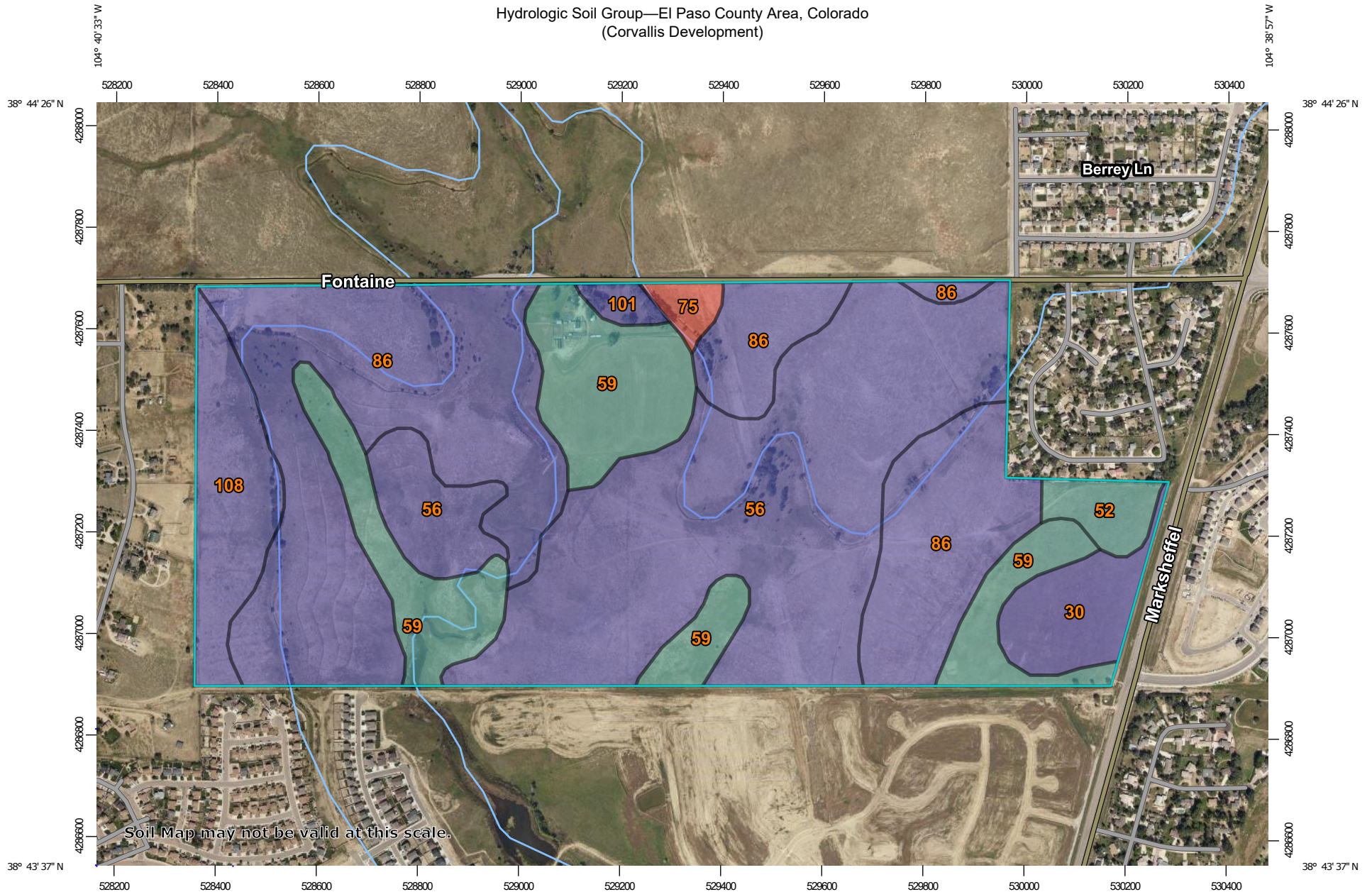
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**MAP NUMBER**  
08041C0956G

**MAP REVISED**  
DECEMBER 7, 2018

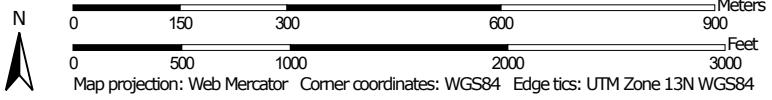
Federal Emergency Management Agency

Hydrologic Soil Group—El Paso County Area, Colorado  
(Corvallis Development)



Soil Map may not be valid at this scale.

Map Scale: 1:10,600 if printed on A landscape (11" x 8.5") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84

Hydrologic Soil Group—El Paso County Area, Colorado  
(Corvallis Development)

### MAP LEGEND

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**


-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
Survey Area Data: Version 17, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 14, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
30	Fort Collins loam, 0 to 3 percent slopes	B	13.3	3.9%
52	Manzanst clay loam, 0 to 3 percent slopes	C	6.3	1.8%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	B	118.2	34.5%
59	Nunn clay loam, 0 to 3 percent slopes	C	55.5	16.2%
75	Razor-Midway complex	D	3.1	0.9%
86	Stoneham sandy loam, 3 to 8 percent slopes	B	122.1	35.6%
101	Ustic Torrfluvents, loamy	B	2.6	0.8%
108	Wiley silt loam, 3 to 9 percent slopes	B	21.4	6.3%
<b>Totals for Area of Interest</b>			<b>342.5</b>	<b>100.0%</b>

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher



*Figure 1-Existing 34" HDPE FMIC Pipe at Weeping Willow and Fontaine (Northeast of Corvallis)*



*Figure 2-Existing 56" x 38" CMAP FMIC Culvert across Fontaine*



*Figure 3-Existing 10' x 28' Concrete Box Culvert across Fontaine (Jimmy Camp Creek-West Fork)*



*Figure 4-Existing 69" x 46" CMAP FMIC Culvert across Fontaine*





*Figure 5-Existing 29" x 19" CMAP Fontaine Road Ditch Across Rolling View Drive (Appears to be grouted in insert)  
(NW of development)*



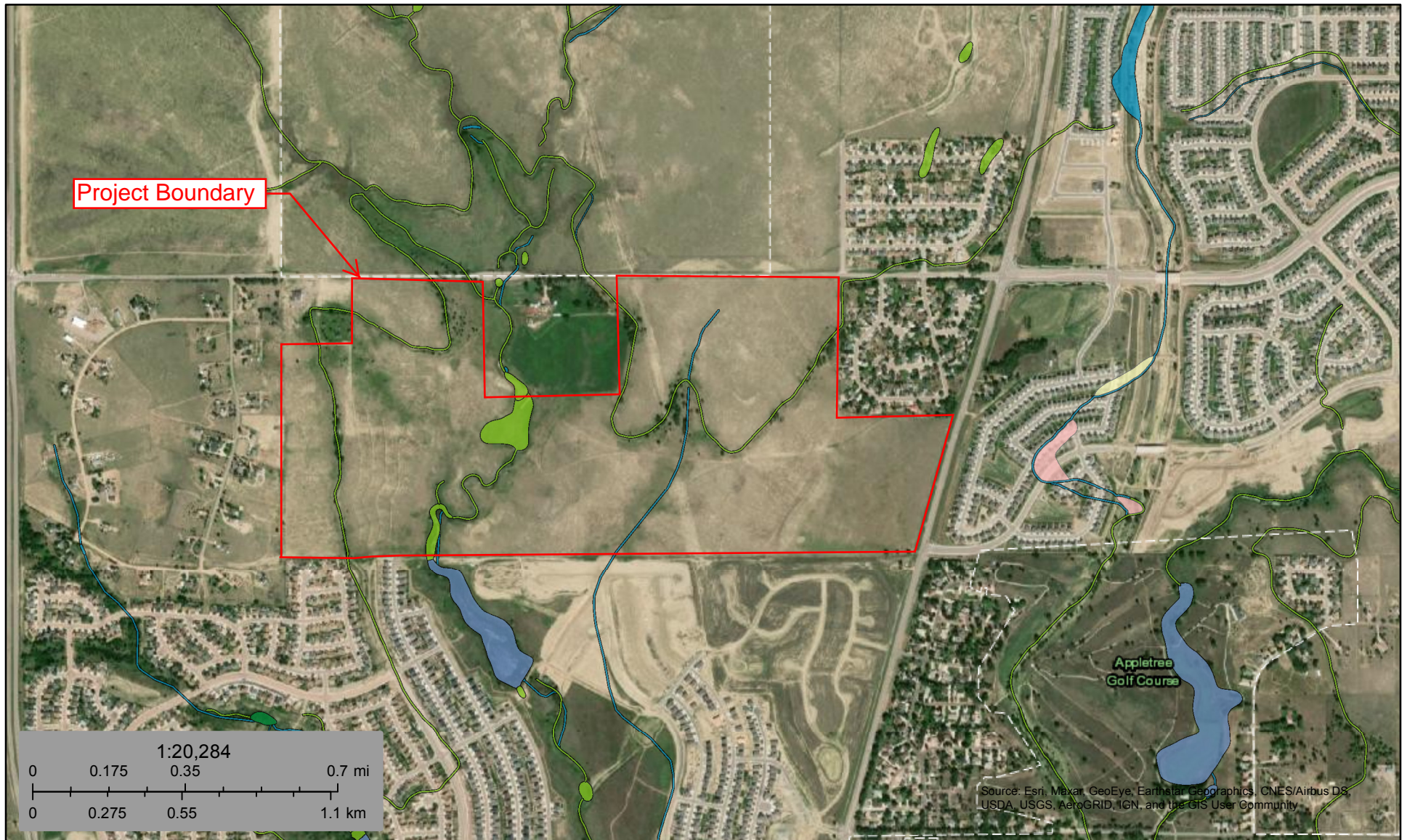
*Figure 6-Existing 60" RCP FMIC Culvert in Glens at Widefield Filing No. 6 (South of Corvallis)*



Figure 7-Existing 18" CMP and Embankment (Jimmy Camp Creek-West Fork) Located south of proposed Corvallis Development




Figure 8-Existing 18" CMP and Embankment (Jimmy Camp Creek-West Fork) Located south of proposed Corvallis Development



September 10, 2020

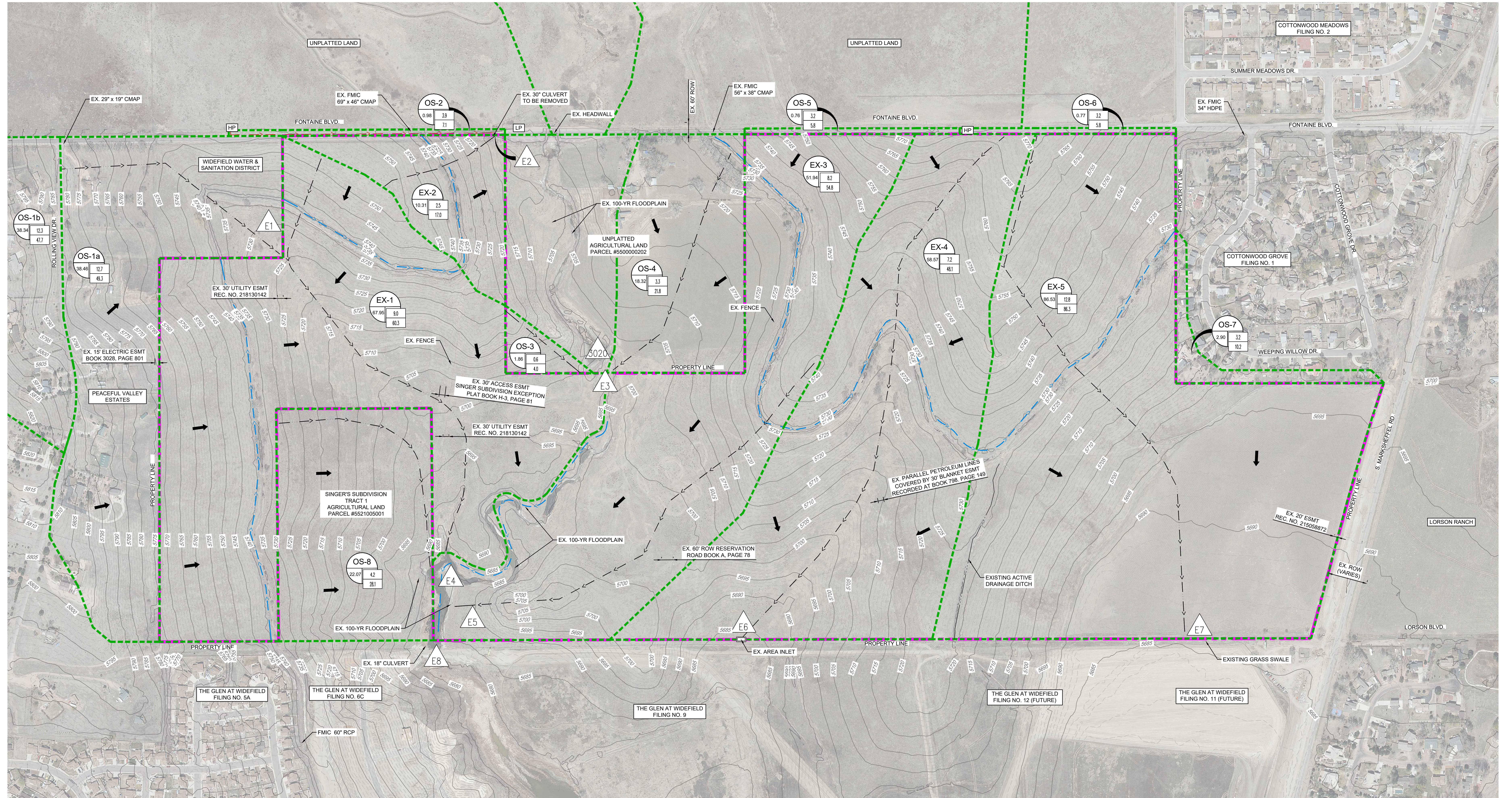
**Wetlands**

- |  |   |  |
|--|---|--|
|  Estuarine and Marine Deepwater |  Freshwater Emergent Wetland       |  Lake     |
|  Estuarine and Marine Wetland   |  Freshwater Forested/Shrub Wetland |  Other    |
|  |  Freshwater Pond                   |  Riverine |

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.

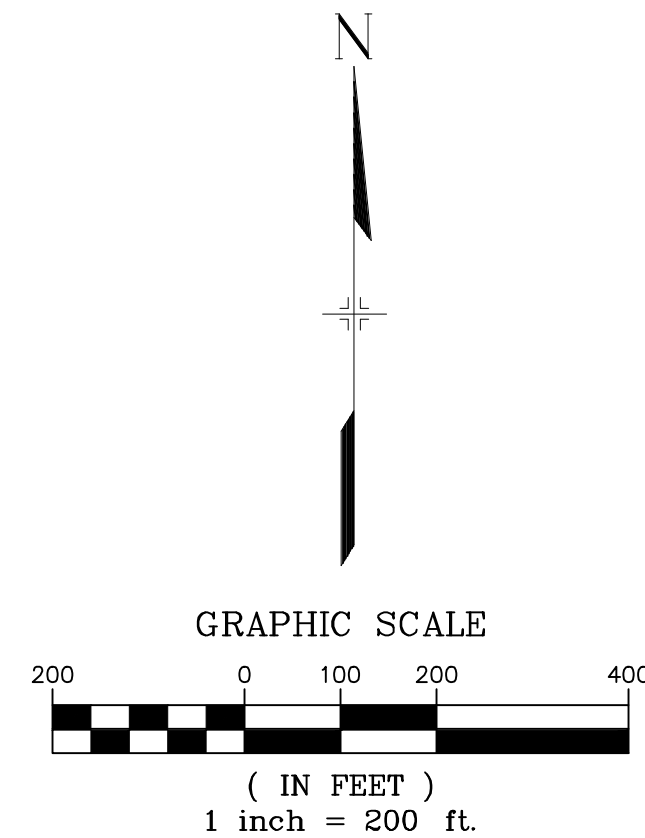
# **APPENDIX D**

## ***MAPS***



**Corvallis Existing Conditions Design Point Summary Table**

Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)
E1: OS-1	76.8	25.3	98.5
E2: OS-2, EX-2	11.3	5.4	22.5
E3: OS-3, OS-4	31.5	6.5	34.4
E4: E1, E3, EX-1, OS-8	198.3	46.3	222.3
E5: OS-5, EX-3	52.7	10.2	57.5
E6: EX-4	58.6	7.2	48.1
E7: EX-5, OS-6, OS-7	90.2	16.5	93.1
E8: E4, E5, +DPBS3020	251.0	403.5	2040.7

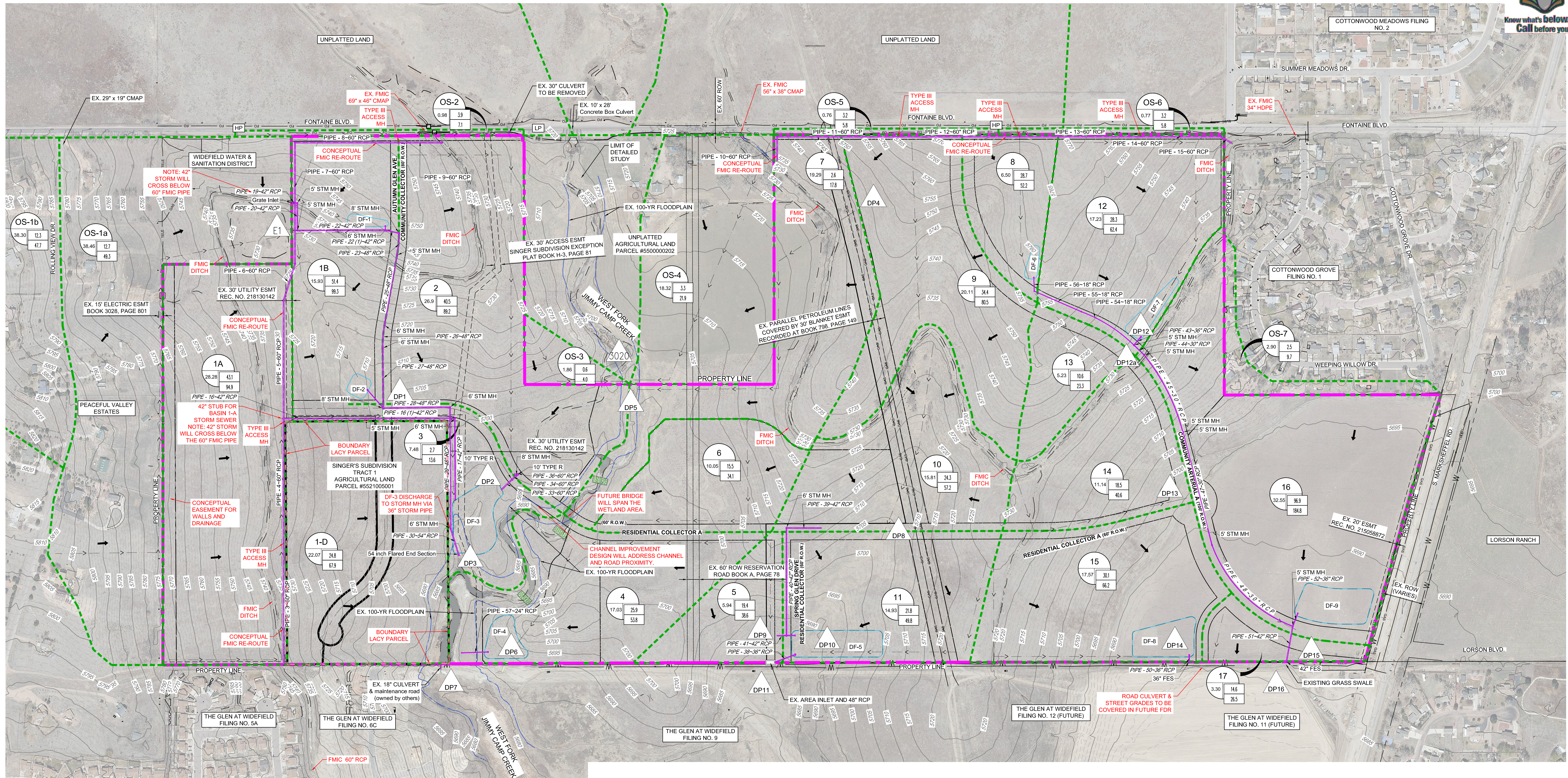


**LEGEND**

- EXISTING BASIN BOUNDARY
- EXISTING CONTOUR
- DRAINAGE CHANNEL
- PROPOSED PROPERTY LINE
- EXISTING FLOW DIRECTION
- EXISTING FLOW PATH
- E1 DESIGN POINT
- EX-2 SUB BASIN DESIGNATION
- █ 5-YEAR STORM EVENT PEAK FLOW (CFS)
- █ 100-YEAR STORM EVENT PEAK FLOW (CFS)
- █ SUB BASIN AREA (AC.)

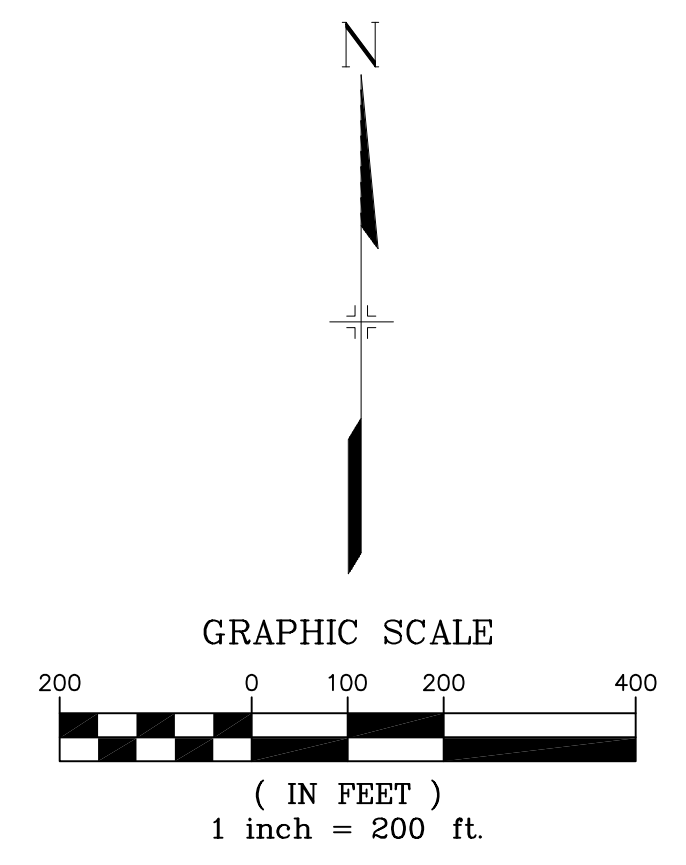
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<p>PREPARED BY:</p> <p>2435 Research Pkwy, Suite 300          Colorado Springs, CO 80920          Phone 719.575.0100</p>		<p><b>CORVALLIS</b></p> <p>MASTER DRAINAGE DEVELOPMENT PLAN          FOUNTAIN, CO</p> <p><b>EXISTING CONDITIONS</b></p>	
<p>DESIGNED BY: NMS          DRAWN BY: JTS          CHECKED BY: NMS</p>	<p>SCALE: HORIZ. 1" = 200'          VERT. N/A</p>	<p>DATE ISSUED: MARCH 2021          SHEET: 01 OF 04</p>	<p>DRAWING No: <b>DR01</b></p>



**LEGEND**

- PROPOSED BASIN BOUNDARY
- EXISTING CONTOUR
- DRAINAGE CHANNEL
- PROPOSED PROPERTY LINE
- PROPOSED FLOW DIRECTION
- PROPOSED FLOW PATH
- POTENTIAL DROP STRUCTURE LOCATION
- E1 DESIGN POINT
- EX-2 SUB BASIN DESIGNATION
- ### 5-YEAR STORM EVENT PEAK FLOW (CFS)
- ### 100-YEAR STORM EVENT PEAK FLOW (CFS)
- ### SUB BASIN AREA (AC.)



Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)
OS-1a	38.46	12.7	49.3
OS-2	0.98	3.9	7.1
OS-3	1.86	0.5	3.5
OS-4	18.32	2.5	16.6
OS-5	0.76	3.2	5.8
OS-6	0.77	3.2	5.8
OS-7	2.90	2.5	9.4
1A	27.68	42.2	92.9
1B	15.93	51.4	99.3
1D (Formerly OS-8)	22.07	24.8	67.9
2	26.90	40.5	89.2
3	16.12	5.3	28.4
4	17.03	25.9	53.8
5	5.94	19.4	38.6
6	10.05	15.5	34.1
7	19.29	2.6	17.8
8	6.50	24.7	52.2
9	20.11	34.4	80.5
10	15.81	24.3	57.2
11	14.93	21.8	49.8
12	17.23	28.3	62.4
13	5.23	10.6	23.3
14	11.14	18.5	40.6
15	17.57	30.1	66.2
16	32.55	96.9	184.8
17	3.30	14.6	26.5

Design Point	Description	Area (Acres)	Q5 (cfs)	Q100 (cfs)
E1	OS-1a and OS-1b	76.8	21.7	84.4
DP1	E1+DF-1 Release+DF-2 Release	104.4	25.3	110.3
DP2	OS-2, 1A, 1D, 2, 3	93.8	127.1	311.7
DP3	DP1+DP2 Treated (DF-3 Release)	198.2	33.6	185.2
DP4	7	19.3	2.6	17.8
DP5	OS-3, OS4, DPBS 3020, DP4	46.2	352.6	1798.9
DP6	4, 6	27.1	22.3	47.7
DP7	DP3+DP5+DP6 Treated (DF-4 Release)	271.5	391.0	2006.1
DP8	9, 10, OS-5	36.7	45.8	106.9
DP9	DP8, 5	42.6	33.4	74.7
DP10	DP9, 11	57.5	54.9	123.8
DP11	DP10 Treated (DF-5 Release)	57.5	6.6	48.1
DP12	OS-6, 12	18.0	24.5	53.5
DP13	13, 14	16.4	20.4	44.9
DP14	DP13, 15, 17	37.2	35.3	76.2
DP15	DP12 Treated (DF-7 Release), 16 Treated (DF-9 Release), & DP6 Release	60.0	7.8	65.8
DP16	DP14 Treated (DF-8 Release)+DP15	97.2	12.8	110.1

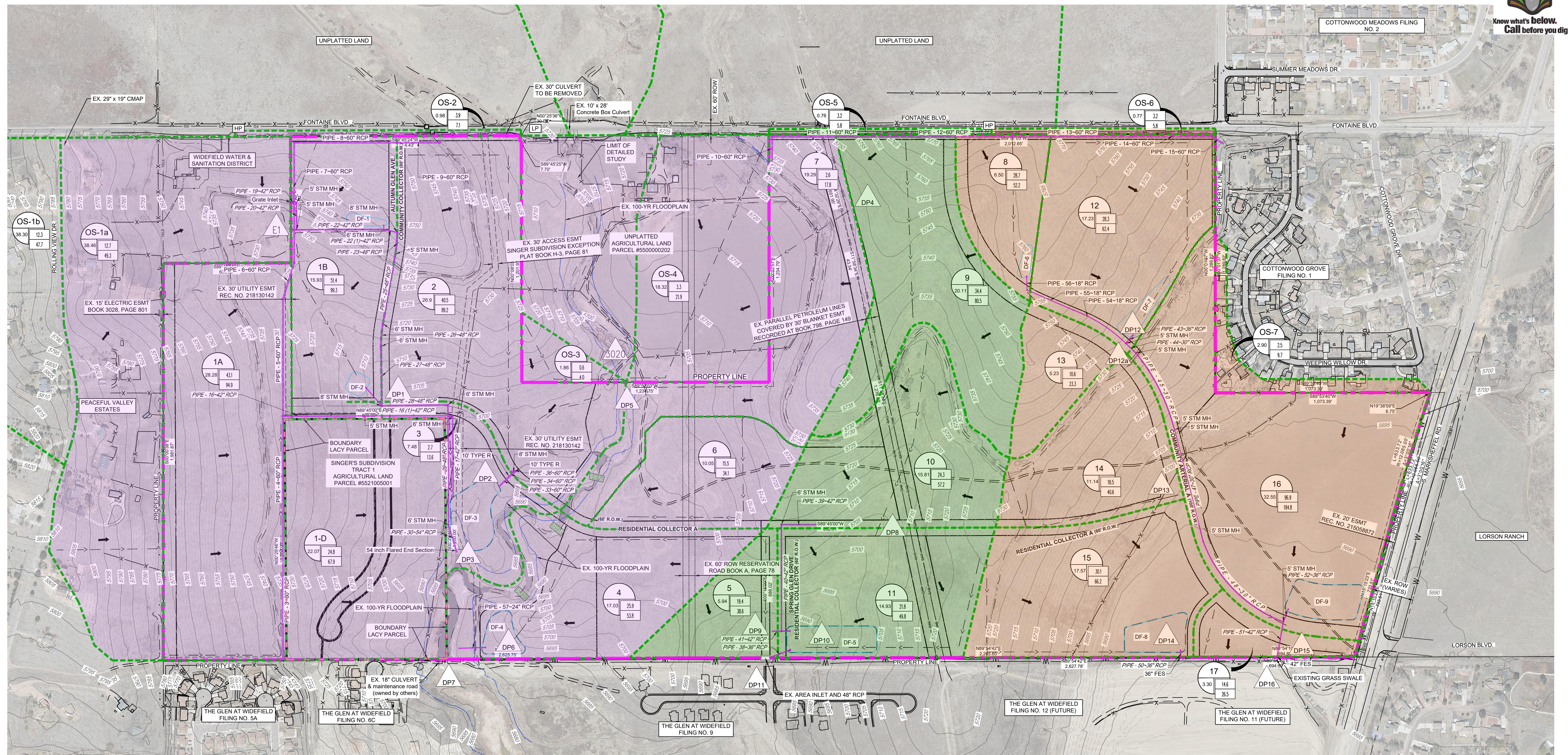
PREPARED BY:  
 Matrix  
 2435 Research Pkwy, Suite 300  
 Colorado Springs, CO 80920  
 Phone: 719.575.0100

**CORVALLIS**  
 MASTER DRAINAGE DEVELOPMENT PLAN  
 FOUNTAIN, CO

**PROPOSED CONDITIONS**

DESIGNED BY: NMS SCALE: DATE ISSUED: FEBRUARY 2022 DRAWING No.  
 DRAWN BY: JTS HORIZ: 1" = 200' SHEET 02 OF 04 DR02  
 CHECKED BY: NMS VERT: NA

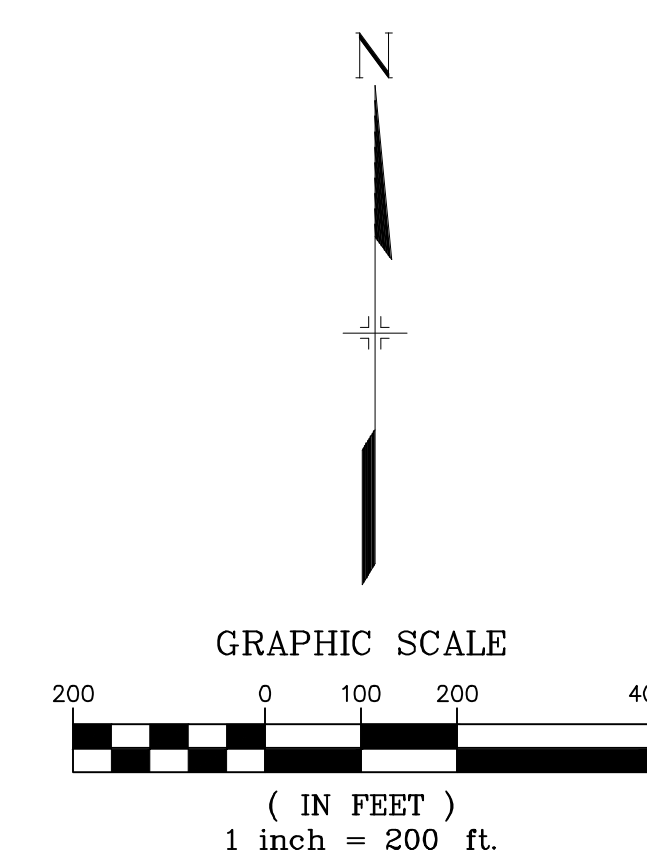
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### LEGEND

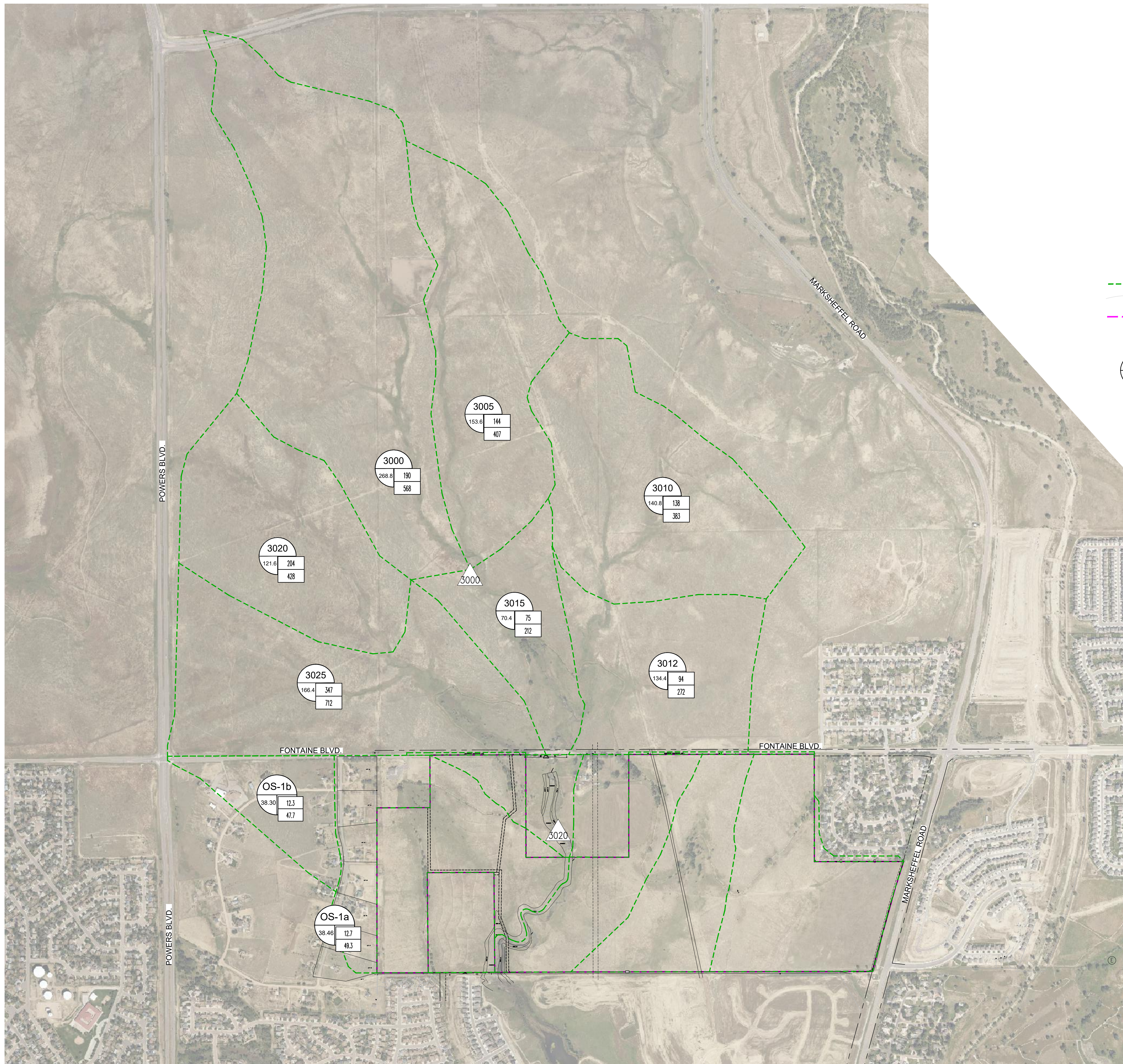
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- EXISTING CONTOUR
- DRAINAGE CHANNEL
- PROPOSED PROPERTY LINE
- PROPOSED FLOW DIRECTION
- PROPOSED FLOW PATH
- DESIGN POINT
- SUB BASIN DESIGNATION
- 5-YEAR STORM EVENT PEAK FLOW (CFS)
- 100-YEAR STORM EVENT PEAK FLOW (CFS)
- SUB BASIN AREA (AC.)
- WEST BASIN DESIGN FLOW
- CENTRAL BASIN DESIGN FLOW
- EAST BASIN DESIGN FLOW

SEE DR-02 FOR STORM SEWER LABELS



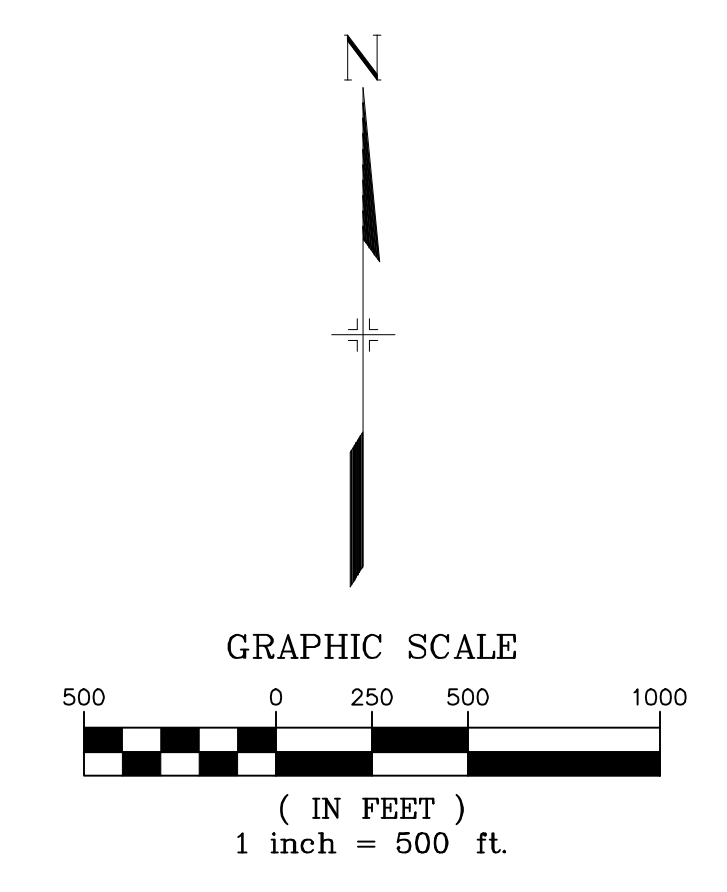
PREPARED BY:		<b>CORVALLIS</b>	
		MASTER DRAINAGE DEVELOPMENT PLAN FOUNTAIN, CO	
		<b>DRAINAGE BASIN EXHIBIT</b>	
DESIGNED BY: NMS	SCALE: 1" = 200'	DATE ISSUED: FEBRUARY 2022	DRAWING No. DR03
DRAWN BY: JTS	HORIZ. N/A	SHEET 03 OF 04	
CHECKED BY: NMS	VERT. N/A		

2435 Research Pkwy, Suite 300  
Colorado Springs, CO 80920  
Phone 719.575.0100

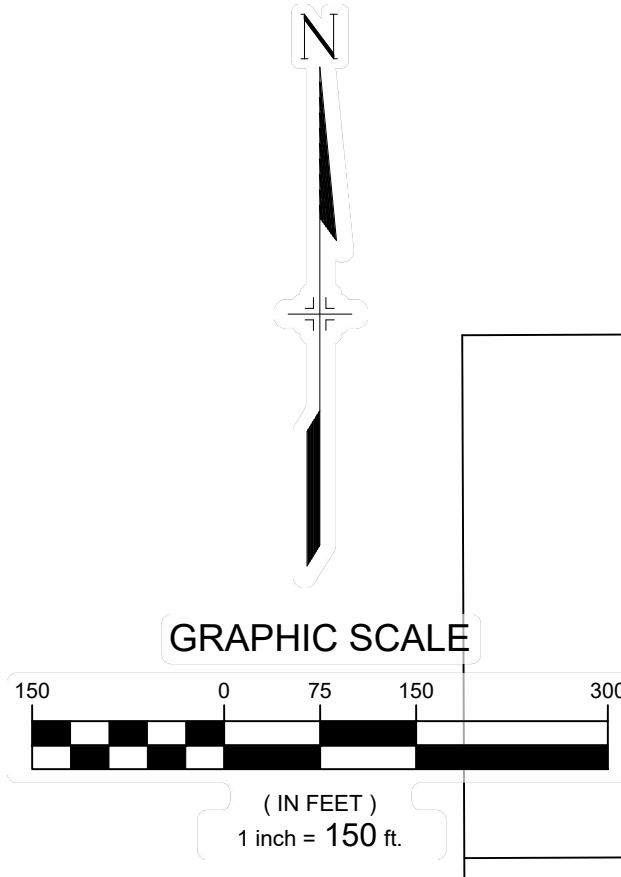
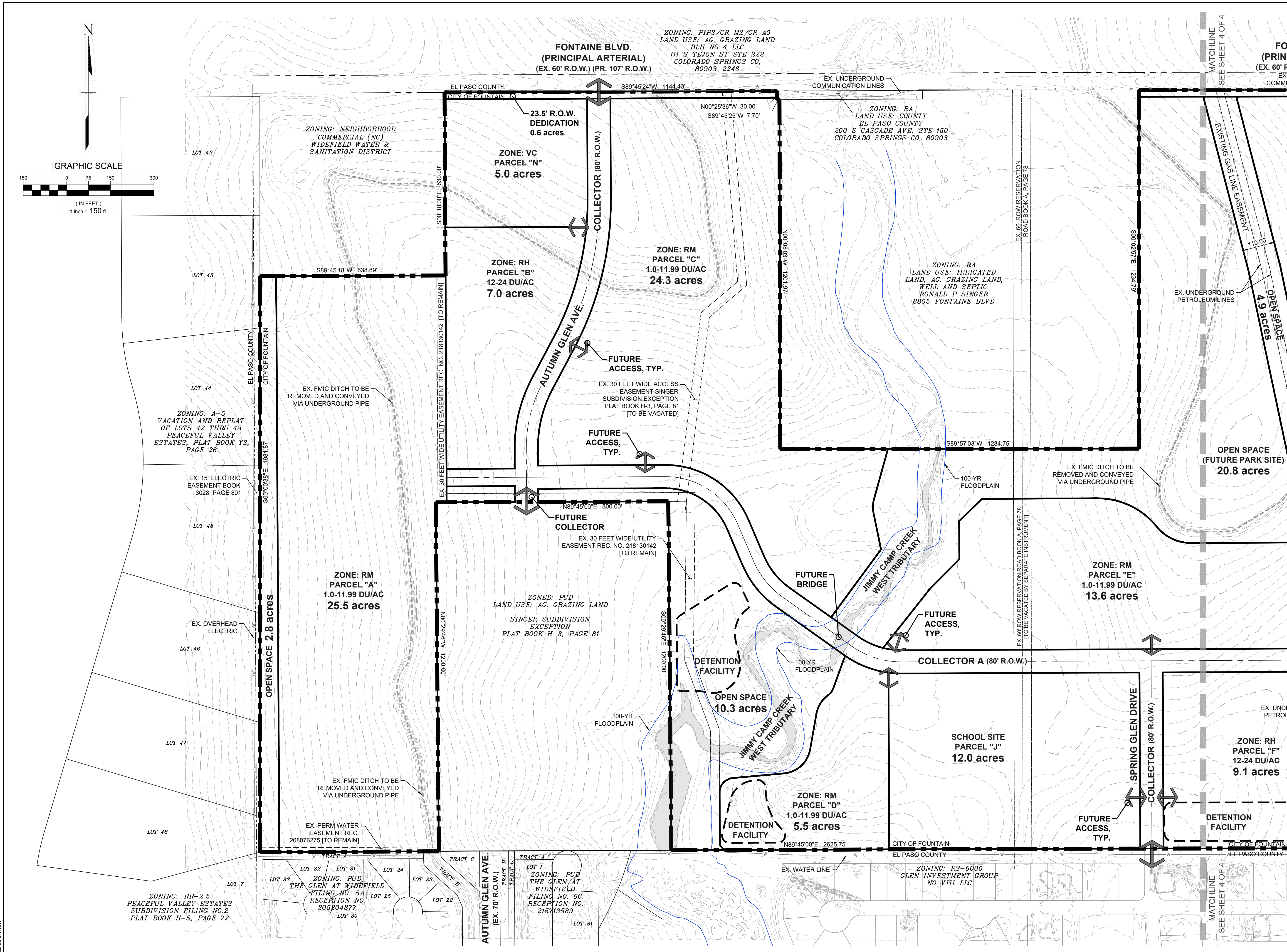


**LEGEND**

- EXISTING BASIN BOUNDARY
- EXISTING CONTOUR
- PROPOSED PROPERTY LINE
- DESIGN POINT
- SUB BASIN DESIGNATION
- 5-YEAR STORM EVENT PEAK FLOW (CFS)
- 100-YEAR STORM EVENT PEAK FLOW (CFS)
- SUB BASIN AREA (AC.)

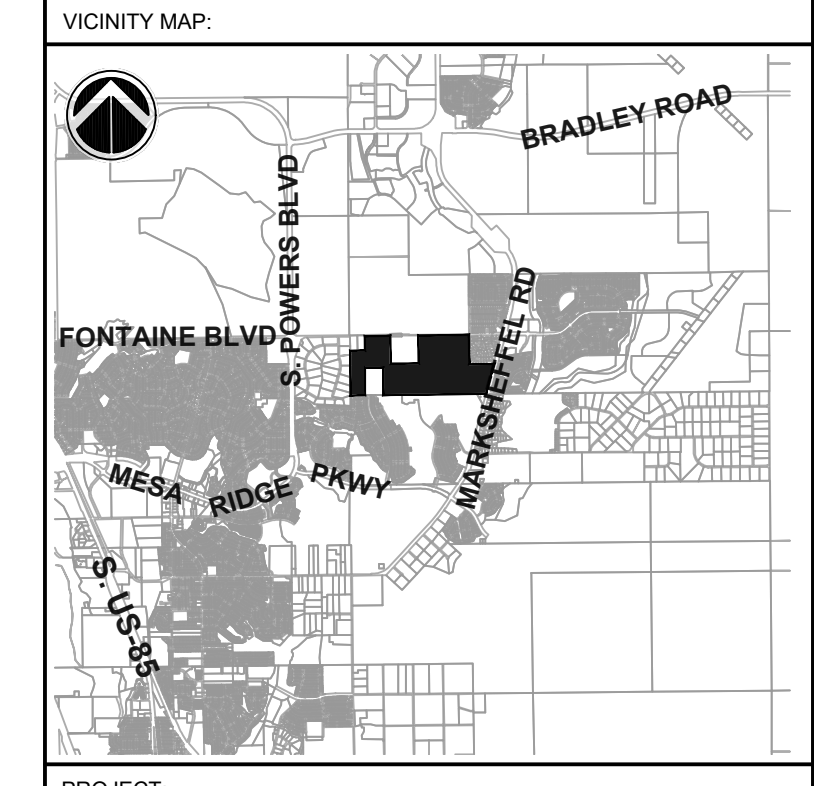
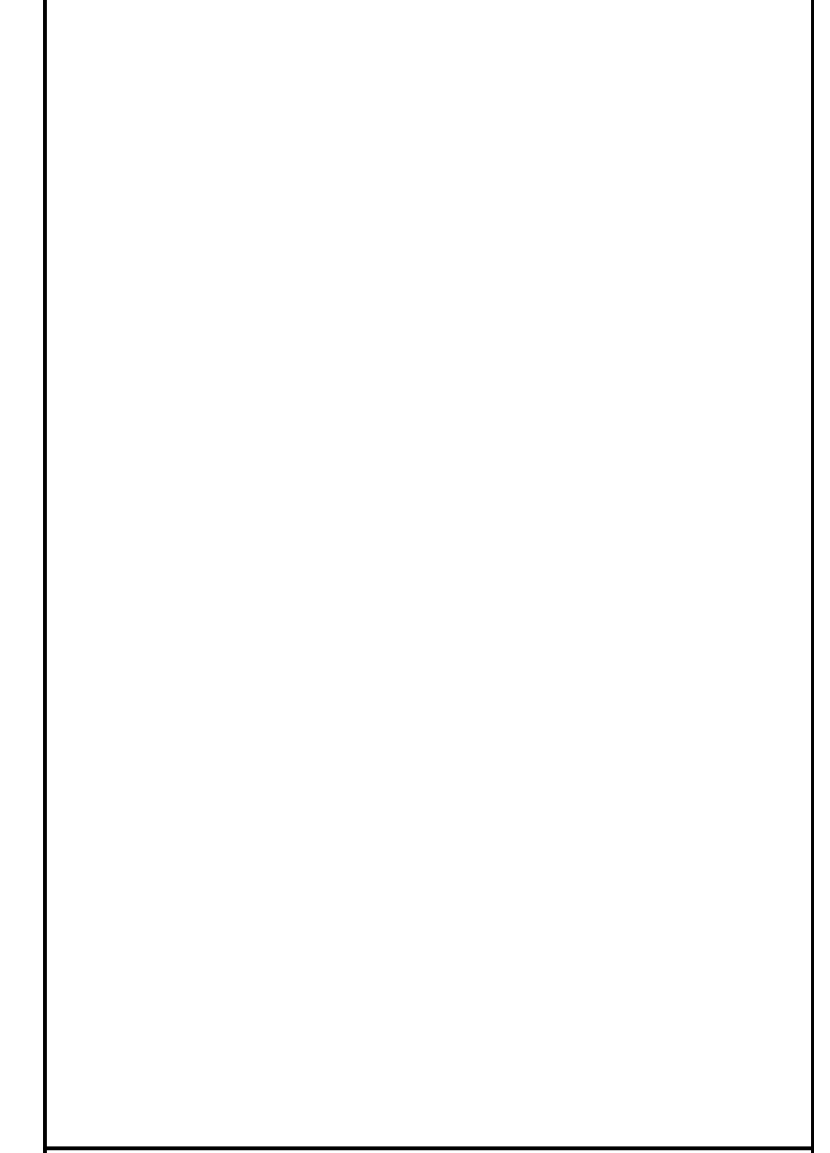






CONSULTANTS:  
PLANNER/LANDSCAPE ARCHITECT/CIVIL ENGINEER:  
**Matrix**  
2435 RESEARCH PARKWAY,  
SUITE 300  
COLORADO SPRINGS, CO 80920  
PHONE: (719) 575-0100  
FAX: (719) 575-0208

OWNER/DEVELOPER:  
**HPHR PROPERTIES, LLC**  
14160 GLENEAGLE DRIVE  
COLORADO SPRINGS, CO 80921



DATE: THIRD SUBMITTAL: 03/15/2021

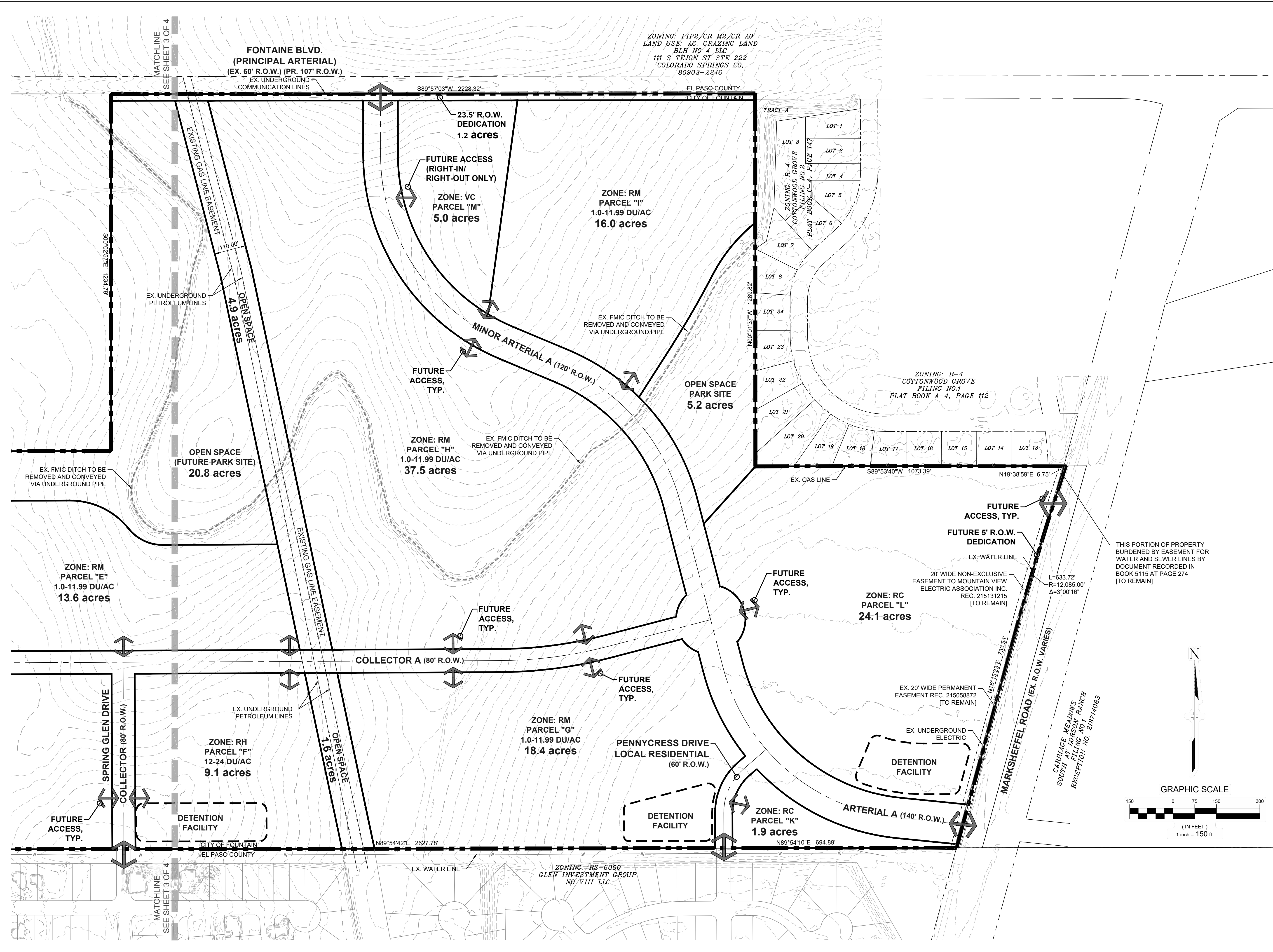
REVISION HISTORY:

NO.	DATE	DESCRIPTION	BY
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1	01/08/2021	REVISED PER CITY COMMENTS	RAF
2	03/15/2021	REVISED PER CITY COMMENTS	RAF

DRAWING INFORMATION:  
PROJECT NO: 20.1105.002  
DRAWN BY: RAF  
CHECKED BY: JAA  
APPROVED BY: JAA  
SHEET TITLE:

**OVERALL DEVELOPMENT PLAN (1)**  
**ODP03**  
SHEET 03 OF 04

PCD FILE NO.:



CONSULTANTS:  
 PLANNER/LANDSCAPE ARCHITECT/CIVIL ENGINEER:  
 Matrix  
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 SUITE 300  
 COLORADO SPRINGS, CO 80920  
 PHONE: (719) 575-0100  
 FAX: (719) 575-0208

OWNER/DEVELOPER:  
 HPHR PROPERTIES, LLC  
 14160 GLENEAGLE DRIVE  
 COLORADO SPRINGS, CO 80921

VICINITY MAP:

PROJECT:  
**CORVALLIS**  
 CITY OF FOUNTAIN  
**OVERALL DEVELOPMENT PLAN**

DATE: THIRD SUBMITTAL: 03/15/2021

REVISION HISTORY:

NO.	DATE	DESCRIPTION	BY
0	09/15/2020	INITIAL SUBMITTAL	RAF
1	01/08/2021	REVISED PER CITY COMMENTS	RAF
2	03/15/2021	REVISED PER CITY COMMENTS	RAF

DRAWING INFORMATION:  
 PROJECT NO: 20.1105.002  
 DRAWN BY: RAF  
 CHECKED BY: JAA  
 APPROVED BY: JAA  
 SHEET TITLE:

**OVERALL DEVELOPMENT PLAN (2)**  
**ODP04**  
 SHEET 04 OF 04

PCD FILE NO.:

# CORVALLIS - LACY PARCEL

## CITY OF FOUNTAIN

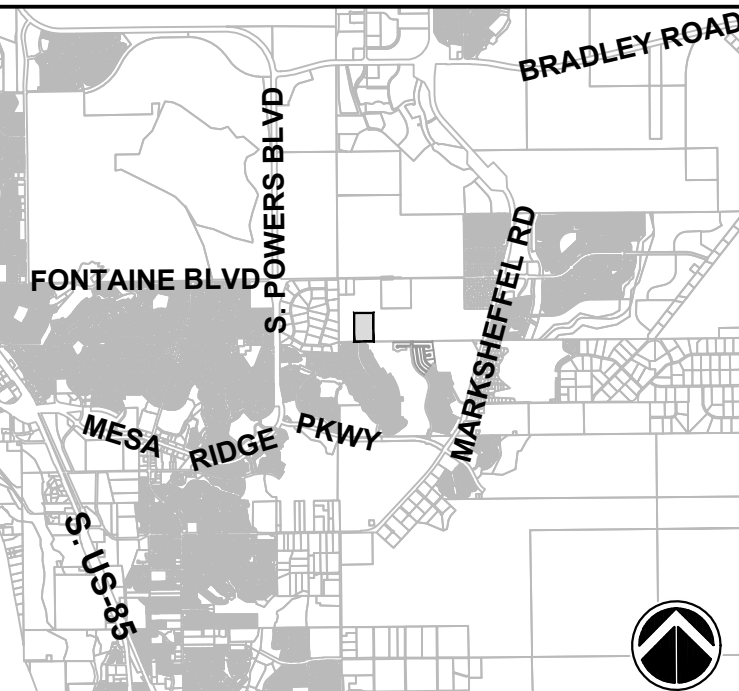
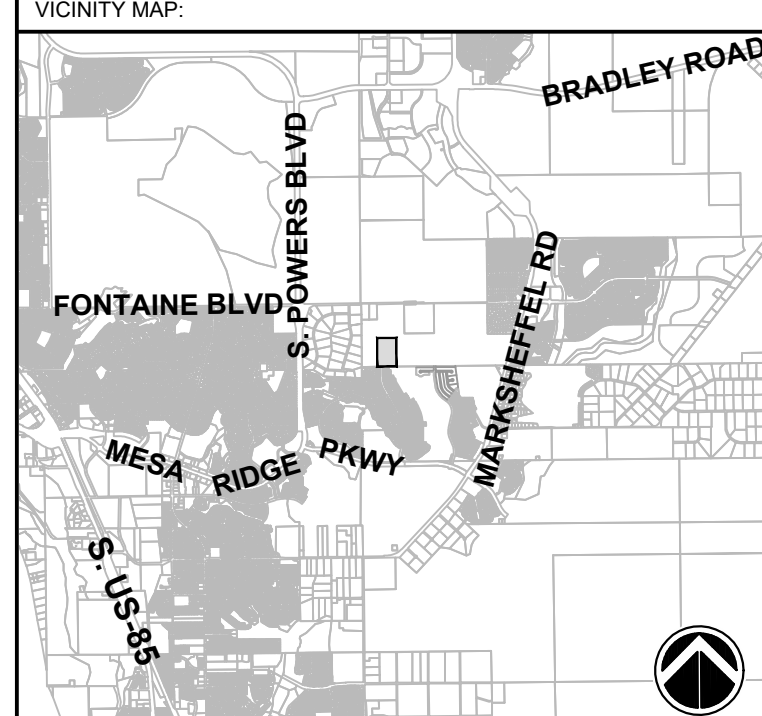
### OVERALL DEVELOPMENT PLAN

CONSULTANTS:  
 PLANNER/ LANDSCAPE ARCHITECT/ CIVIL ENGINEER:  
  
 2435 RESEARCH PARKWAY, SUITE 300  
 COLORADO SPRINGS, CO 80920  
 PHONE: (719) 575-0100  
 FAX: (719) 575-0208

OWNER/DEVELOPER:  
**HPHR PROPERTIES, LLC**  
 14160 GLENEAGLE DRIVE  
 COLORADO SPRINGS, CO 80921  
 (XXX) XXX-XXXX

APPROVAL:

VICINITY MAP:

PROJECT:  
**CORVALLIS - LACY PARCEL**  
**OVERALL DEVELOPMENT PLAN**  
 SOUTH SEGMENT OF CORVALLIS  
 10/22/2021

REVISION HISTORY:

NO.	DATE	DESCRIPTION	BY

DRAWING INFORMATION:  
 PROJECT NO: 21.1105.009  
 DRAWN BY: KMM  
 CHECKED BY: JAA  
 APPROVED BY: JAA  
 SHEET TITLE:

## OVERALL DEVELOPMENT PLAN

ODP02

SHEET 2 OF 2

CITY FILE NO.: X

#### DIMENSIONAL STANDARDS AND GUIDELINES:

ZONE DISTRICT: RESIDENTIAL MEDIUM (RM) 1-10 DU/AC  
 DIMENSIONAL STANDARDS FOR PARCEL A

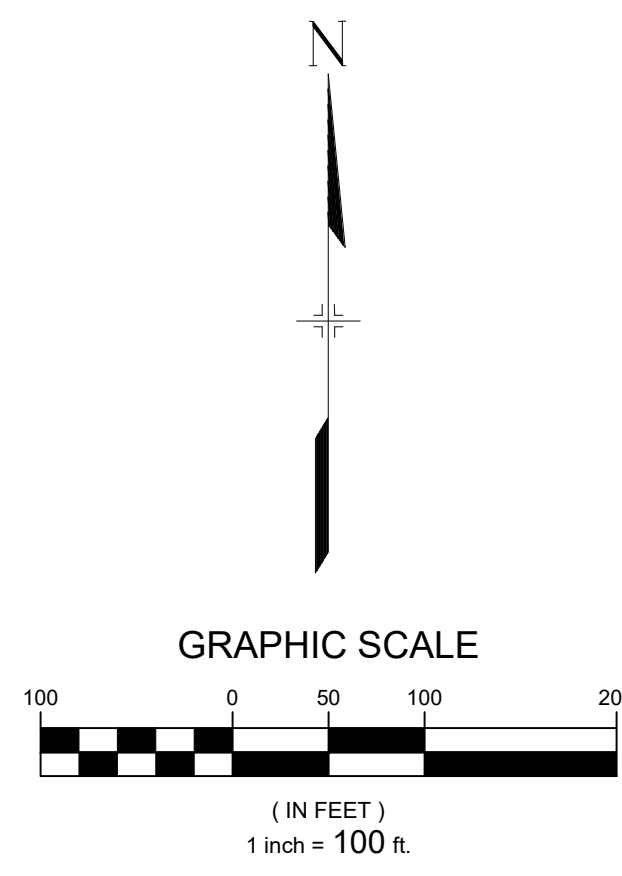
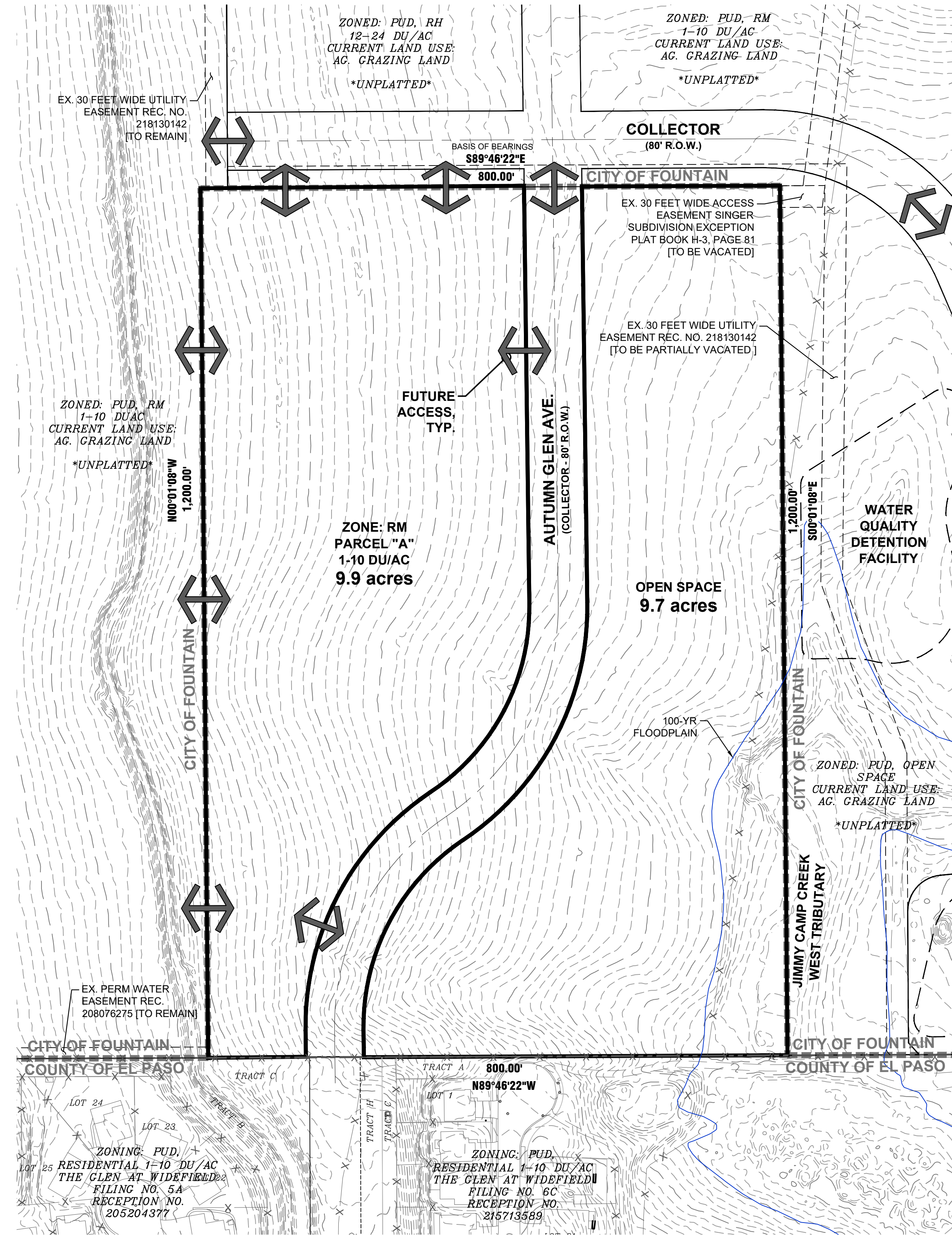
- PERMITTED LAND USE: SINGLE FAMILY RESIDENTIAL, MAIL KIOSKS, TRAIL CORRIDORS, DEVELOPMENT SIGNAGE, ENTRY MONUMENT SIGNAGE, PEDESTRIAN WALKWAYS, FENCING, UTILITIES, METRO DISTRICT MAINTENANCE FACILITIES, STORMWATER FACILITIES, DRAINAGE IMPROVEMENTS, OPEN SPACE AND LANDSCAPE IMPROVEMENTS, PARKS AND ASSOCIATED PARK RELATED EQUIPMENT, COMMUNITY CLUBHOUSE.
- MINIMUM LOT AREA FOR SINGLE FAMILY DETACHED:
  - SINGLE FAMILY DWELLING: 3,800 SF
- MAXIMUM PERCENTAGE OF STRUCTURAL COVERAGE: 50%
- MAXIMUM STRUCTURAL HEIGHT: 40'
- MINIMUM WIDTH OF LOT AT FRONT BUILDING SETBACK LINE: 30' OR AS OTHERWISE SHOWN
- PROJECTIONS INTO SETBACKS ARE GOVERNED BY THE CITY OF FOUNTAIN ZONING CODE, AS AMENDED
- MINIMUM SETBACK REQUIREMENTS:
  - FRONT YARD: 18' TO FACE OF GARAGE FROM PROPERTY LINE  
15' TO FRONT PROJECTION OF HOUSE FROM PROPERTY LINE
  - SIDE YARD: 5'
  - REAR YARD: 15'
  - CORNER YARD (NON-DRIVEWAY SIDE): 10'  
18' IF SIDE GARAGE ACCESS IS PROVIDED
  - CHAMFERED CORNER FRONT SETBACK: 8'

#### DEVELOPMENT STANDARDS AND GUIDELINES

- TEMPORARY USES ARE SUBJECT TO THE REQUIREMENTS OF THE CITY OF FOUNTAIN ZONING CODE, AS AMENDED.
- ACCESSORY USES ARE SUBJECT TO THE REQUIREMENTS OF THE CITY OF FOUNTAIN ZONING CODE, AS AMENDED.
- FENCING GUIDELINES TO BE PER THE FUTURE CORVALLIS CC&R'S AND/ OR DESIGN GUIDELINES
- A MINIMUM 4' FRONT YARD BUILDING STAGGER IS REQUIRED BETWEEN ADJACENT UNITS.

#### GENERAL LOT DEVELOPMENT NOTES:

- LOCATION OF PRIVATE SIDEWALKS TO FRONT ENTRY TO BE DETERMINED BY INDIVIDUAL HOUSE INGRESS/ EGRESS CONFIGURATION.
- OWNER/ BUILDER TO ENSURE DRIVEWAYS DO NOT CONFLICT WITH PEDESTRIAN RAMP TRANSITIONS.
- ALL SIGHT DISTANCE TRIANGLES MUST BE WITHIN THE PUBLIC RIGHT-OF-WAY OR A SIGHT DISTANCE EASEMENT. IF THE LINE OF SIGHT CROSSES ONTO PRIVATE PROPERTY, A "SIGHT DISTANCE EASEMENT" SHALL BE DEDICATED TO PROVIDE THE REQUIRED SIGHT DISTANCE AT TIME OF FINAL PLAT. MAINTENANCE OF A SIGHT DISTANCE EASEMENT SHALL BE THE RESPONSIBILITY OF THE PROPERTY OWNER OR METROPOLITAN DISTRICT UNLESS OTHERWISE APPROVED BY THE CITY OF FOUNTAIN.



FILE LOCATION: S:\21.1105.009\CORVALLIS PARCEL CORVALLIS ENTITLEMENT\100 DWG\104 PLAN SETS\CONCEPT PLAN COPR\1105.009-ODP.DWG