|  |  |  | Existing |  | Calculated |  | Used |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Element Name | Peak <br> Flow <br> (cfs) | Cross <br> Section | Rise | Span | Rise | Span | Rise | Span | Area $\left(\mathrm{ft}^{\wedge} 2\right)$ | Comment |
| 1 | 18.30 | CIRCULAR | 24.00 in | 24.00 in | 18.00 in | 18.00 in | 24.00 in | 24.00 in | 3.14 |  |
| 2 | 18.30 | CIRCULAR | 24.00 in | 24.00 in | 18.00 in | 18.00 in | 24.00 in | 24.00 in | 3.14 |  |
| 3 | 16.00 | CIRCULAR | 18.00 in | 18.00 in | 18.00 in | 18.00 in | 18.00 in | 18.00 in | 1.77 |  |

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics where calculated using the 'Used' parameters.


## Grade Line Summary:

Tailwater Elevation (ft): 6581.00

|  | Invert Elev. |  | Downstream Manhole <br> Losses |  | HGL |  | EGL |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Element <br> Name | Downstream <br> (ft) | Upstream <br> (ft) | Bend <br> Loss <br> (ft) | Lateral <br> Loss <br> (ft) | Downstream <br> (ft) | Upstream <br> (ft) | Downstream <br> (ft) | Friction <br> Loss <br> (ft) | Upstream <br> (ft) |
|  | 6579.00 | 6581.24 | 0.00 | 0.00 | 6581.00 | 6582.78 | 6581.53 | 2.02 | 6583.55 |
| 2 | 6581.24 | 6586.00 | 0.20 | 0.00 | 6582.98 | 6587.54 | 6586.97 | 1.34 | 6588.31 |
| 3 | 6587.71 | 6588.91 | 0.06 | 0.00 | 6588.85 | 6590.33 | 6590.77 | 0.89 | 6591.66 |

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer \#0, is not considered a sewer.
- Bend loss $=$ Bend $K * V \_f i \wedge 2 /(2 * g)$
- Lateral loss $=\mathrm{V}$ fo ${ }^{\wedge} 2 /(2 * \mathrm{~g})$ - Junction Loss K * V_fi ${ }^{\wedge} 2 /(2 * \mathrm{~g})$.
- Friction loss is always Upstream EGL - Downstream EGL.


## Excavation Estimate:

The trench side slope is $1.0 \mathrm{ft} / \mathrm{ft}$
The minimum trench width is 2.00 ft

See CD comments also

|  |  |  |  |  | Downstream |  |  | Upstream |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Element <br> Name | Length <br> (ft) | $\begin{array}{\|l} \text { Wall } \\ \text { (in) } \end{array}$ | Bedding <br> (in) | Bottom Width <br> (ft) | Top Width <br> (ft) | Trench Depth <br> (ft) | Cover (ft) | Top Width (ft) | Trench Depth <br> (ft) | Cover (ft) | Volume (cu. yd) | Comment |
| 1 | 22.76 | 3.00 | 4.00 | 5.50 | 0.00 | 0.00 | 0.00 | 6.52 | 4.34 | 1.51 | 10.18 | Sewer Too Shallow |
| 2 | 48.50 | 3.00 | 4.00 | 5.50 | 6.52 | 4.34 | 1.51 | 12.24 | 7.20 | 4.37 | 67.47 | Sewer Too Shallow |
| 3 | 38.26 | 2.50 | 4.00 | 4.92 | 9.32 | 5.45 | 3.20 | 6.78 | 4.18 | 1.93 | 37.61 | Sewer Too Shallow |

Total earth volume for sewer trenches $=115$ cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.


## DETENTION BASIN OUTLET STRUCTURE DESIGN

## MHFD-Detention, Version 4.03 (May 2020)

Project: Windermere Filing No. 1
$\square$
User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

| Inpu | liptica | Weir (typically used to drain WQCV and/or E | , | ted P | 边 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Invert of Lowest Orifice $=$ | 0.00 | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) | WQ Orifice Area per Row $=$ | N/A | $\mathrm{ft}^{2}$ |
| Depth at top of Zone using Orifice Plate $=$ | 4.26 | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) | Elliptical Half-Width $=$ | N/A | feet |
| Orifice Plate: Orifice Vertical Spacing = | 17.00 | inches | Elliptical Slot Centroid $=$ | N/A | eet |
| Orifice Plate: Orifice Area per Row $=$ | N/A | inches | Elliptical Slot Area $=$ | N/A | $\mathrm{ft}^{2}$ |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|  | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stage of Orifice Centroid (ft) | 0.00 | 1.42 | 2.84 |  |  |  |  |  |
| Orifice Area (sq. inches) | 11.00 | 11.00 | 11.00 |  |  |  |  |  |


|  | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stage of Orifice Centroid ( ft ) |  |  |  |  |  |  |  |  |
| Orifice Area (sq. inches) |  |  |  |  |  |  |  |  |


| User Input: Vertical Orifice (Circular or Rectangular) |  |  | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) inches | Calculated Parameters for Vertical Orifice |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Not Selected | Not Selected |  | Vertical Orifice Area $=$ <br> Vertical Orifice Centroid = | Not Selected | Not Selected |  |
| Invert of Vertical Orifice $=$ | N/A | N/A |  |  | N/A | N/A | $\mathrm{ft}^{2}$ |
| Depth at top of Zone using Vertical Orifice $=$ | N/A | N/A |  |  | N/A | N/A | eet |
| Vertical Orifice Diameter $=$ | N/A | N/A |  |  |  |  |  |


| User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectanqular/Trapezoidal Weir (and No Outlet Pipe) |  |  |  |  | Calculated Parameters for Overflow Weir |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = | Zone 3 Weir | Not Selected |  |  | Zone 3 Weir | Not Selected | feet feet |
|  | 4.30 | N/A |  |  | 4.30 | N/A |  |
|  | 6.75 | N/A | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) feet |  | 6.75 | N/A |  |
| Overflow Weir Grate Slope = | 0.00 | N/A | H:V Gr | Open Area / 100-yr Orifice Area | 4.51 | N/A |  |
| Horiz. Length of Weir Sides = | 6.75 | N/A | feet Ov | ow Grate Open Area w/o Debris = | 31.89 | N/A | $\mathrm{ft}^{2}$ |
| Overflow Grate Open Area \% = | 70\% | N/A | \%, grate open area/total area | ow Grate Open Area w/ Debris = | 15.95 | N/A | $\mathrm{ft}^{2}$ |
| Debris Clogging \% = | 50\% | N/A | \% |  |  |  |  |



| Zone 3 Circular | Not Selected |
| :---: | :---: |
| 7.07 | $\mathrm{~N} / \mathrm{A}$ |
| 1.50 | $\mathrm{f} / \mathrm{A}$ |
| $\mathrm{f} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| ry |  |

Half-Central Angle of Restrictor Plate on Pipe $=$

|  | Calculated Parameters for Spillway |  |
| :---: | :---: | :---: |
| Spillway Design Flow Depth= | 0.92 | feet |
| Stage at Top of Freeboard = | 7.92 | feet |
| Basin Area at Top of Freeboard = | 5.10 | acres |
| Basin Volume at Top of Freeboard $=$ | 21.63 | acre-ft |


| Routed Hydrograph Resul | The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design Storm Return Period $=$ | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
| One-Hour Rainfall Depth (in) = | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.49 |
| CUHP Runoff Volume (acre-ft) = | 2.016 | 5.899 | 4.497 | 6.048 | 7.280 | 9.553 | 11.773 | 14.673 | 24.739 |
| Inflow Hydrograph Volume (acre-ft) $=$ | N/A | N/A | 4.497 | 6.048 | 7.280 | 9.553 | 11.773 | 14.673 | 24.739 |
| CUHP Predevelopment Peak Q (cfs) = | N/A | N/A | 0.8 | 1.5 | 2.2 | 19.7 | 39.5 | 65.5 | 155.5 |
| OPTIONAL Override Predevelopment Peak Q (cfs) $=$ | N/A | N/A |  |  |  |  |  |  |  |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | N/A | N/A | 0.01 | 0.01 | 0.02 | 0.15 | 0.30 | 0.49 | 1.17 |
| Peak Inflow Q (cfs) $=$ | N/A | N/A | 49.7 | 67.5 | 81.3 | 119.9 | 153.1 | 194.1 | 328.3 |
| Peak Outflow Q (cfs) $=$ | 1.0 | 1.8 | 1.6 | 1.8 | 7.1 | 24.1 | 40.8 | 66.0 | 142.3 |
| Ratio Peak Outflow to Predevelopment $\mathrm{Q}=$ | N/A | N/A | N/A | 1.2 | 3.3 | 1.2 | 1.0 | 1.0 | 0.9 |
| Structure Controlling Flow = | Plate | Plate | Plate | Plate | Qvegflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Spillway |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | N/A | 10.2 | 0.7 | 1.2 | 2.0 | 2.3 |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97\% of Inflow Volume (hours) = | 38 | 66 | 59 | 68 | 71 | 69 | 67 | 65 | 58 |
| Time to Drain 99\% of Inflow Volume (hours) = | 40 | 71 | 63 | 73 | 76 | 76 | 75 | 74 | 71 |
| Maximum Ponding Depth (ft) $=$ | 2.59 | 4.26 | 3.63 | 4.18 | 4.50 | 4.82 | 5.06 | 5.36 | 6.46 |
| Area at Maximum Ponding Depth (acres) $=$ | 1.71 | 2.94 | 2.47 | 2.88 | 3.10 | 3.38 | 3.59 | 3.84 | 4.77 |
| Maximum Volume Stored (acre-ft) $=$ | 2.027 | 5.908 | 4.179 | 5.675 | 6.602 | 7.673 | 8.510 | 9.625 | 14.322 |



