

June 15, 2018

County of El Paso
Engineering Division
2880 International Circle, Suite 110
Colorado Springs, Colorado 80910

Re: Academy Village Filing No. 3 - Drainage Addendum Letter

### **Design Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negregatives, before the omissions on my part in preparing this report.

Glenn Ellis, Colorado P.E. # 38861
For and On Behalf of JR Engineering, LLC

### Owner/Developer's Statement:

I, the owner/developer have read and will comply with all of the replan.	quirements specified in this drainage report and
onde forth	6-21-2018
Ron Covington	Date
Ron Covington Homes	
13725 Struthers Road, Suite 200	
Colorado Springs, CO 80920	

### El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Conditions:

### To Whom It May Concern:

This letter is an addendum to the "Final Drainage Report for Academy Village", dated April 1999, prepared by HMS Group, LLC. This addendum will address the reconfiguration of the drainage pattern within Basin 1a of the approved report. The purpose of this addendum is to quantify the changes to the drainage condition due to site variations from the approved report.

The site was originally intended to drain to a CDOT Type D Catch Basin located at the north end of the site. The Type D catch basin can be seen within the approved "Drainage Map – Developed Academy Village", located in Appendix B. The existing site currently drains to two locations. The first site outfall is a 24" RCP with a flared end section located at where the Type D Catch Basin was originally planned to the northeast. The second site outfall is at a 24" RCP with a flared end section located northeast of the existing bank parking lot. Both 24" RCPs connect to an existing 54" RCP storm drain that flows northwest, ultimately outfalling to a detention pond west of Struthers Road, approximately 1,200 feet northwest of the site.

### **General Location**

The legal description for the property is as follows: Academy Village Filing No. 3, Lot 4, "Academy Village Filing No. 2", being a portion of the southeast quarter of Section 1, Township 12 South, Range 67 West of the 6<sup>th</sup> P.M., County of El Paso, State of Colorado. The site is bounded by Academy Village Filing 3, Lot 1 to the southeast, Struthers Road to the west and south, and Paradise Villas Phases 1E, 1F and 1C to the northeast. Surrounding platted developments are the Gleneagle Executive Office Condominiums to the west, Paradise Villas to the east, Lot 1 of the Academy Village Filing 3 to the south, and an unplatted piece of property further south across Struthers Road. The legal description for the property is as follows: Academy Village Filing No. 3, Lot 4, "Academy Village Filing No. 2", being a portion of the southeast quarter of Section 1, Township 12 South, Range 67 West of the 6<sup>th</sup> P.M., County of El Paso, State of Colorado.

### **Description of Property**

Academy Village Filing 3, Lot 2 is composed of approximately 0.709 acres of vacant land. The site has a large ditch running parallel to Struthers Road along the western edge of the property that generally slopes from southeast to northwest with slopes ranging from 0-3%. Academy Village Filing 3 is generally made up of Type B Soil, classified as Pring Coarse Sandy Loam as can be seen in the NRCS Map located within Appendix B. The vacant land is vegetated with native grasses. The site is located within the Black Forest FOMO 4200 drainage basin. The associated drainage fee for the project is \$8,536.22 (\$16,270 x 0.709 acres x 0.74 (%

impervious)). The associated bridge fee for the project is \$232.42 (\$443 x 0.709 acres x 0.74 (% impervious)).

### Hydrology

All hydrologic data was obtained from the "El Paso County Drainage Criteria Manual," Volume 2 and the "Urban Drainage and Flood Control District Urban Drainage Criteria Manual" Volumes 1, 2, and 3 (DCM). Onsite drainage improvements were designed based on the 5-year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the Colorado Springs Criteria. One hour point rainfall data for the storm events is identified in the Table below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the DCM. Time of concentrations were developed using equations from the DCM. All runoff calculations and applicable charts and graphs are included in Appendix B.

Storm Rainfall (in.)
5-year 1.50

2.52

**Table 1- 1-hr Point Rainfall Data** 

100-year

The proposed improvements have been designed with the intent to maintain the hydrology of the approved report. The approved report conveyed the generated runoff untreated to the existing 54" RCP. The proposed drainage condition for Academy Village will convey the generated runoff to an on-site water quality pond before ultimately outfalling to the same 54" RCP as in the approved report. The drainage map for Academy Village is located in Appendix B. Runoff from Basin A will be routed via curb and gutter, a natural swale, and a 12" PVC pipe to a water quality capture pond at the northern end of the site. The water quality pond is sized to treat 0.014 ac-ft, and release the treated runoff to the existing 54" RCP via a 12" RCP outfall. The runoff from Basin B will be collected in a natural grass swale that runs along the southeast edge of the site. Flows from Basin B will go to an existing 24" RCP that ties into the 54" RCP to the north of the site. All basin calculations can be found in Appendix A. The runoff from Basin OS1 is primarily sheet flow off of Struthers into the natural swale within Basin B.

Basin OS2 is composed of a portion of the adjacent Bank site drive, drainage swale, and Struthers Road. Basin OS2 was evaluated in order to determine the offsite flows that made their way into the drainage ditch on Lot 2 via a culvert at design point 3 (DP3). The runoff from OS2 ultimately makes its way to DP2 and into the 54" RCP.

**Table 2 – Basin Summary** 

Tributary	Area	Percent			t <sub>c</sub>	<b>Q</b> <sub>5</sub>	Q <sub>100</sub>
Sub-basin	(acres)	Impervious	C <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)
А	0.46	86%	0.65	0.79	6.9	1.4	2.8
В	0.22	50%	0.12	0.38	10.1	0.1	0.6
OS1	0.51	88%	0.71	0.82	6.6	1.7	3.3
OS2	0.71	84%	0.65	0.77	7.1	2.1	4.3

Therefore, the total inflows as determined in the approved Final Drainage Report are still valid and no revisions to the existing storm sewer are necessary.

### **Hydraulic Criteria**

The Rational Method and UDDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD UD-Detention v3.07 spreadsheet was utilized for sizing and release rate of the water quality pond.

### **Water Quality**

In accordance with the El Paso County Drainage Criteria Manual, Volume 2 this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls. In order to reduce runoff volume the new impervious area for the site was minimized. The WQCV is treated through an on-site water quality pond located at the northeast portion of the site. The pond was designed using the Urban Drainage spreadsheet, "UD Detention v3.07" located in Appendix A. The water quality pond was sized to treat 0.014 ac-ft of site runoff. The pond is relatively small so rather than implementing a trickle channel, the pond bottom will be sloped at 1.0 percent minimum to the water quality structure. The emergency spillway for the pond is located along its western border with an elevation of 6763.49. One foot of freeboard has been provided above the emergency spillway water surface elevation as well. The emergency spillway will outfall towards the existing natural grass swale inside the western property line. The restrictor plate, as well as pond storage design details, can be located in Appendix B. There are no proposed major drainageways for the site that would need to be stabilized. Some site specific source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated concrete truck washout basin, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The IRF calculations were performed, and can be found attached within Appendix A.

Maintenance access will be provided via an eight-foot wide maintenance access path. The path follows the western border of the pond and services to the outlet structure. The path maintenance access crosses the emergency spillway, therefore; side slopes of the spillway do not exceed 10% to allow for maintenance truck access.

### **Conclusion**

The proposed changes to the hydrologic configuration and drainage calculations including storm sewer and water quality pond pose no significant changes to the concepts presented within the "Final Drainage Report for Academy Village", dated April 1999, prepared by HMS Group, LLC. This addendum is in conformance with the originally intended design and meets the latest criteria requirements.

Sincerely,

Glenn Ellis, P.E.

Slenn P. Ellis

Project Manager

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Academy Village Filing Number 3

June 15, 2018

## Appendix A

### **COMPOSITE % IMPERVIOUS CALCULATIONS**

Subdivision: Academy Village Filing Number 3
Location: El Paso County , CO

 Project Name:
 Struthers Road

 Project No.:
 25123.00

 Calculated By:
 AJH

 Checked By:
 12/22/17

		Pave	ed Roads &	Walks		Roofs			Lawns		Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
А	0.46	100%	0.25	55.0%	90%	0.09	17.0%	48%	0.14	14.0%	86.0%
В	0.22	100%	0.01	5.0%	90%	0.00	0.0%	48%	0.21	45.0%	50.0%
OS1	0.51	100%	0.39	77.0%	90%	0.00	0.0%	48%	0.12	11.0%	88.0%
OS2	0.71	100%	0.50	70.0%	90%	0.00	0.0%	48%	0.21	14.0%	84.0%
TOTAL	1.91										81.5%

### COMPOSITE % RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Academy Village Filing Number 3
Location: El Paso County , CO

 Project Name:
 Struthers Road

 Project No.:
 25123.00

 Calculated By:
 AJH

 Checked By:
 12/22/17

		Pave	ed Roads &	Walks		Roofs			Lawns		Basins Total			
Basin ID	Total Area (ac)	С	Area (ac)	Weighted C	С	Area (ac)	Weighted C	С	Area (ac)	Weighted C	Runoff Coeff.			
					5 year, H	5 year, HSG A								
Α	0.46	0.90	0.25	0.49	0.73	0.09	0.14	0.08	0.14	0.02	0.65			
В	0.22	0.90	0.01	0.04	0.73	0.00	0.00	0.08	0.21	0.08	0.12			
OS1	0.51	0.90	0.39	0.69	0.73	0.00	0.00	0.08	0.12	0.02	0.71			
OS2	0.71	0.90	0.50	0.63	0.73	0.00	0.00	0.08	0.21	0.02	0.65			
TOTAL	1.91										0.60			
					100 year,	HSG A								
Α	0.46	0.96	0.25	0.53	0.81	0.09	0.15	0.35	0.14	0.11	0.79			
В	0.22	0.96	0.01	0.05	0.81	0.00	0.00	0.35	0.21	0.33	0.38			
OS1	0.51	0.96	0.39	0.74	0.81	0.00	0.00	0.35	0.12	0.08	0.82			
OS2	0.71	0.96	0.50	0.67	0.81	0.00	0.00	0.35	0.21	0.10	0.77			
TOTAL	1.91										0.74			

### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision:	Academy Village Filing Number 3	
Location:	El Paso County, CO	

Project Name: Struthers Road Project No.: 25123.00 Calculated By: AJH Checked By: Date: 12/22/17

		SUB-BA	ASIN			INITI	AL/OVER	LAND			TRAVEL TI	IME			tc CHECK		
		DAT	A				(T <sub>i</sub> )				$(T_t)$			(L	FINAL		
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	So	t <sub>i</sub>	$L_t$	So	Κ	VEL.	t <sub>t</sub>	COMP. $t_c$	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
Α	0.46	В	86%	0.65	0.79	45	1.8%	4.5	226	0.6%	20.0	1.5	2.4	6.9	271.0	6.9	6.9
В	0.22	В	50%	0.12	0.38	49	8.0%	6.2	326	0.5%	20.0	1.4	3.8	10.1	375.0	14.2	10.1
OS1	0.51	В	88%	0.71	0.82	49	5.6%	2.8	326	0.5%	20.0	1.4	3.8	6.6	375.0	7.5	6.6
OS2	0.71	В	84%	0.65	0.77	63	5.6%	3.6	253	0.5%	20.0	1.4	3.0	6.6	316.0	7.7	6.6

NOTES:

(Equation 6-2)  $t_c = t_i + t_t$  $t_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S_0)^0.33)$ (Equation 6-3)

 $t_i$  = overland (initial) flow time (minutes)

S = Average Slope along the overland flow path, ft/ft

 $t_t = L/(60K^*(S_0)^0.5$ (Equation 6-4)

 $t_t$  = channelized flow time (minutes)

S = waterway slope, ft/ft

 $V_t$  = travel time velocity (ft/sec) = K\*S<sub>o</sub>^0.5

First Design Point Time of Concentration:

 $t_c = (18-15*i) + L/(60*(24*i+12)*(S_0)^0.5)$ 

(Equation 6-5)

i = imperviousness (expressed as a decimal)

 $t_c$  is lesser of Equation 6-2 and Equation 6-5.

For Urbanized basins a minimum  $t_c$  of 5.0 minutes is required.

For non-urbanized basins a minimum  $t_c$  of 10.0 minutes is required.

Table 6-2. NRCS Conveyance Factors, K

Type of Land Surface	K
Heavy Meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

### STANDARD FORM SF-3

### STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name:	Struthers Road

Subdivision: Academy Village Filing Number 3 Project No.: 25123.00 Calculated By: AJH

Design Storm: 5-Year Checked By: Da

ı Dy.		
ate:	12/22/17	

				DIRE	CT RUI	NOFF				TOTAL I	RUNOF	F	Street	/Swale		PIPE		TRAV	EL TIN	ΛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	${ m t_c}$ (min)	C*A (Ac)	I (in/hr)	Q (cfs)	tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Slope (%)	Flow (cfs)	Design Flow (cf	Slope (%)	Pipe Size (inche	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1	Α	0.46	0.65	6.9	0.30	4.7	1.4													Flow to pond through pipe to 54" pipe
	2	В	0.22	0.12	10.1	0.03	4.1	0.1	10.1	0.85	4.1	3.5									Flow through Swale
		OS1	0.51	0.71	6.6	0.36	4.7	1.7													Struthers Road sheet flow into ditch
	3	OS2	0.71	0.65	6.6	0.46	4.7	2.2													Bank ditch/culvert

Location: El Paso County , CO

### STANDARD FORM SF-3

## STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Academy Village Filing Number 3	Pro
Location: El Paso County , CO	Calcul
Design Storm: 100-Year	Chec

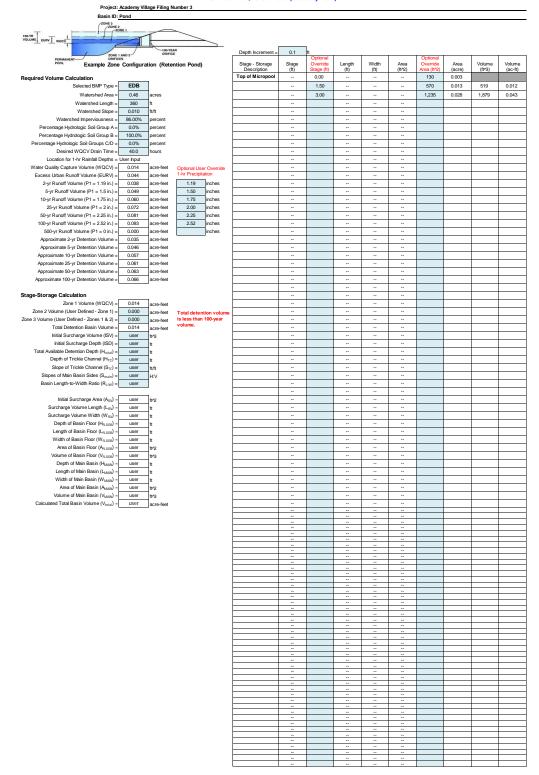
Project Name: Struthers Road
Project No.: 25123.00
Calculated By: AJH
Checked By:

Date:	12/22/17
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				DIRE	CT RUN	IOFF				TOTAL	RUNOF	F	Street	/Swale		PIPE		TRAV	EL TIN	ΛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	O (cfs)	tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Flow (cfs)	Design Flow (cf	Slope (%)	Pipe Size (inche	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1	Α	0.46	0.79	6.9	0.36	7.87	2.8							2.8	1.0	18	56	5.0	0.2	Flow to pond through pipe to 54" pipe
	2	В	0.22	0.38	10.1	0.09	6.91	0.6	10.1	1.06	6.91	7.3									Flow through Swale
		OS1	0.51	0.82	6.6	0.42	7.97	3.3													
	3	OS2	0.71	0.77	6.6	0.55	7.97	4.4													

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

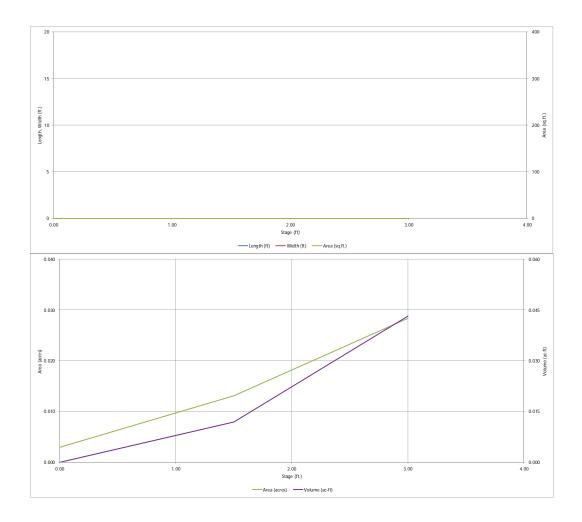
UD-Detention, Version 3.07 (February 2017)



25123.00UD-Detention\_v3.07\_nq.islen, Basin 1,52018, 11:24 AM

### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

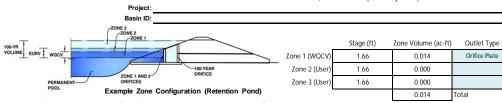
UD-Detention, Version 3.07 (February 2017)



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### **Detention Basin Outlet Structure Design**

UD-Detention, Version 3.07 (February 2017)



User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

| Calculated Parameters for Underdrain | Underdrain Orifice Area = | N/A | ft² | Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)  Calculate									
Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	8.333E-04	ft <sup>2</sup>				
Depth at top of Zone using Orifice Plate =	1.13	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet				
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	Elliptical Slot Centroid =	N/A	feet				
Orifice Plate: Orifice Area per Row =	0.12	sq. inches (diameter = 3/8 inch)	Elliptical Slot Area =	N/A	ft <sup>2</sup>				
		=	-		-				

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	0.80					
Orifice Area (sq. inches)	0.12	0.12						

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								•

User Input: Vertical Orifice (Circ	ular or Rectangular)			Calculated	Parameters for Vert	ical Orifice	
	Not Selected	Not Selected			Not Selected	Not Selected	l
Invert of Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =			ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =			feet
Vertical Orifice Diameter =			inches	•			

User Input: Overflow Weir (Dropbox) and G	rate (Flat or Sloped)		_	Calculated	Parameters for Ove	rflow Weir	
	Not Selected	Not Selected			Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.40		ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, $H_t$ =	1.40		feet
Overflow Weir Front Edge Length =	5.00		feet	Over Flow Weir Slope Length =	5.00		feet
Overflow Weir Slope =	0.00		H:V (enter zero for flat grate)	Grate Open Area / 100-yr Orifice Area =	22.28		should be > 4
Horiz. Length of Weir Sides =	5.00		feet	Overflow Grate Open Area w/o Debris =	17.50		ft <sup>2</sup>
Overflow Grate Open Area % =	70%		%, grate open area/total area	Overflow Grate Open Area w/ Debris =	8.75		ft <sup>2</sup>
Debris Clogging % =	50%		%	•			

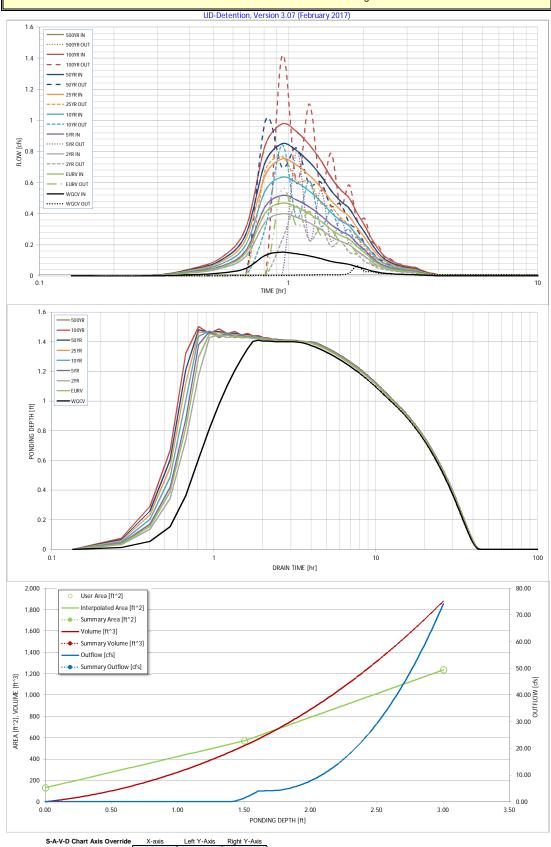
User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

i i ipe w i iow kesti iction i iate (ci	rcular Office, Restric	tor rate, or nectari	guiai Office) Calculated Farameter	3 for Outlet ripe w	.6	
	Not Selected	Not Selected		Not Selected	Not Selected	]
Depth to Invert of Outlet Pipe =	0.00		ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area =	0.79		ft <sup>2</sup>
Circular Orifice Diameter =	12.00		inches Outlet Orifice Centroid =	0.50		feet
			Half-Central Angle of Restrictor Plate on Pipe =	N/A	N/A	radians

User Input: Emergency Spillway (Rectang	jular or Trapezoidal)		Calculated Parameters for Spillwa							
Spillway Invert Stage=	1.74	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.12	feet					
Spillway Crest Length =	6.00	feet	Stage at Top of Freeboard =	2.86	feet					
Spillway End Slopes =	10.00	H:V	Basin Area at Top of Freeboard =	0.03	acres					
Freeboard above Max Water Surface =	1.00	feet	•							

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.014	0.044	0.038	0.049	0.060	0.072	0.081	0.093	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.014	0.044	0.037	0.049	0.060	0.071	0.081	0.093	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.01	0.11	0.39	0.54	0.75	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.0
Peak Inflow Q (cfs) =	0.2	0.5	0.4	0.5	0.6	0.8	0.8	1.0	#N/A
Peak Outflow Q (cfs) =	0.1	0.6	0.4	0.8	0.8	0.8	1.0	1.4	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	146.5	17.1	4.3	4.0	4.1	#N/A
Structure Controlling Flow =	Overflow Grate 1	#N/A							
Max Velocity through Grate 1 (fps) =	0.00	0.02	0.02	0.0	0.0	0.0	0.0	0.1	#N/A
Max Velocity through Grate 2 (fps) =	N/A	#N/A							
Time to Drain 97% of Inflow Volume (hours) =	37	32	33	31	29	28	27	25	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	37	38	37	36	36	35	34	#N/A
Maximum Ponding Depth (ft) =	1.41	1.45	1.45	1.47	1.47	1.47	1.48	1.50	#N/A
Area at Maximum Ponding Depth (acres) =	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	#N/A
Maximum Volume Stored (acre-ft) =	0.011	0.011	0.011	0.012	0.012	0.012	0.012	0.012	#N/A

### Detention Basin Outlet Structure Design



minimum bound maximum bound

### **Detention Basin Outlet Structure Design**

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK #N/A

	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	#N/A
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
8.10 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	0:08:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Hydrograph	0:16:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Constant	0:24:18	0.01	0.02	0.02	0.02	0.03	0.03	0.04	0.05	#N/A
0.617	0:32:24	0.02	0.06	0.05	0.06	0.08	0.09	0.10	0.12	#N/A
	0:40:30	0.05	0.15	0.13	0.16	0.20	0.24	0.27	0.31	#N/A
	0:48:36	0.13	0.41	0.35	0.45	0.55	0.65	0.73	0.84	#N/A
	0:56:42	0.15	0.47	0.40	0.52	0.64	0.75	0.85	0.98	#N/A
	1:04:48	0.14	0.44	0.38	0.49	0.60	0.71	0.81	0.93	#N/A
	1:12:54 1:21:00	0.13	0.40	0.34	0.44	0.54	0.65	0.73	0.84	#N/A
	1:29:06	0.11	0.35	0.30 0.25	0.39	0.48	0.57	0.65 0.55	0.74	#N/A #N/A
	1:37:12	0.09	0.26	0.23	0.33	0.36	0.42	0.55	0.55	#N/A #N/A
	1:45:18	0.07	0.24	0.20	0.26	0.32	0.38	0.43	0.50	#N/A
	1:53:24	0.06	0.19	0.16	0.21	0.26	0.31	0.35	0.40	#N/A
	2:01:30	0.05	0.15	0.13	0.17	0.21	0.25	0.28	0.32	#N/A
	2:09:36	0.03	0.11	0.09	0.12	0.15	0.18	0.21	0.24	#N/A
	2:17:42	0.02	0.08	0.07	0.09	0.11	0.13	0.15	0.17	#N/A
	2:25:48	0.02	0.06	0.05	0.06	0.08	0.10	0.11	0.13	#N/A
	2:33:54	0.01	0.05	0.04	0.05	0.06	0.08	0.09	0.10	#N/A
	2:42:00	0.01	0.04	0.03	0.04	0.05	0.06	0.07	0.08	#N/A
	2:50:06 2:58:12	0.01	0.03	0.03	0.04	0.05	0.05	0.06	0.07	#N/A #N/A
	3:06:18	0.01	0.03	0.02	0.03	0.04	0.05	0.05	0.06	#N/A #N/A
	3:14:24	0.01	0.03	0.02	0.03	0.04	0.04	0.05	0.06	#N/A #N/A
	3:22:30	0.01	0.03	0.02	0.03	0.03	0.03	0.03	0.04	#N/A
	3:30:36	0.00	0.01	0.01	0.01	0.02	0.02	0.02	0.03	#N/A
	3:38:42	0.00	0.01	0.01	0.01	0.01	0.02	0.02	0.02	#N/A
	3:46:48	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02	#N/A
	3:54:54	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	#N/A
	4:03:00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	#N/A
	4:11:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:19:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:27:18 4:35:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:43:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:51:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:59:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:07:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:15:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:24:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:32:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:40:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:48:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:56:24 6:04:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:04:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	6:20:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	6:28:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:36:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:53:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	7:01:12 7:09:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	7:09:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	7:25:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	7:33:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	7:41:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	7:49:48 7:57:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	8:06:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	8:14:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	8:22:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	8:30:18 8:38:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	8:46:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	8:54:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	9:02:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	9:10:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	9:18:54 9:27:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	9:27:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	9:43:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A

#### Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: AJH JR ENGINEERING Company: \*\*\*Design Storm: 1-Hour Rain Depth WQCV Event 0.22 inches August 28, 2017 ACADEMY VILLAGE FILING NUMBER 3 ···Minor Storm: 1-Hour Rain Depth 10-Year Event 1.75 inches 100-Year Event 2.52 EL PASO COUNTY, CO \*\*\*Major Storm: 1-Hour Rain Depth inches Location: Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency 2.52 100-Year Event Max Intensity for Optional User Defined Storm 2.51496 SITE INFORMATION (USER-INPUT) Sub-basin Identifier Receiving Pervious Area Soil Type oamy Sand Loamy Sand Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 0.460 0.220 Directly Connected Impervious Area (DCIA, acres) 0.000 0.000 Unconnected Impervious Area (UIA, acres) 0.320 0.010 Receiving Pervious Area (RPA, acres) 0.001 0.000 Separate Pervious Area (SPA, acres) 0.139 0.210 RPA Treatment Type: Conveyance (C) ٧ Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 0 0.220 Directly Connected Impervious Area (DCIA, %) 0.0% 0.0% Unconnected Impervious Area (UIA, %) 69.6% 4.5% Receiving Pervious Area (RPA, %) 0.1% 0.0% Separate Pervious Area (SPA, %) 30.3% 95.5% A<sub>R</sub> (RPA / UIA) 0.002 0.000 I, Check 1 000 1.000 f / I for WQCV Event: 8.7 8.7 f / I for 10-Year Event: 0.5 0.5 f / I for 100-Year Event: 0.4 0.4 f / I for Optional User Defined Storm CUHP. 0.39 0.39 IRF for WQCV Event: 0.00 0.00 IRF for 10-Year Event: 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 IRF for Optional User Defined Storm CUHP. Total Site Imperviousness: I<sub>total</sub> 69.6% 4.5% Effective Imperviousness for WQCV Event: 0.0% 0.0% Effective Imperviousness for 10-Year Event: 69.6% 4.5% Effective Imperviousness for 100-Year Event: 69.6% 4.5% Effective Imperviousness for Optional User Defined Storm CUHP. LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: N/A 10-Year Event CREDIT\*\*: Reduce Detention By: 0.0% 6.5% N/A 100-Year Event CREDIT\*\*: Reduce Detention By: 0.0% 4.1% N/A User Defined CUHP CREDIT: Reduce Detention By Total Site Imperviousness: 48.5% Notes: Total Site Effective Imperviousness for WQCV Event: Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 10-Year Event: 48.5% \*\* Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: $^{\star\star\star} \text{Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed}$ 48.5% Total Site Effective Imperviousness for Optional User Defined Storm CUHP: 48.5%

UD-BMP\_v3.06.4/sm, IRF

## **Channel Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, May 3 2018

## **Emergency Spillway (Q100 = 2.8 cfs)**

**Trapezoidal** 

Bottom Width (ft) = 12.00 Side Slopes (z:1) = 10.00, 10.00

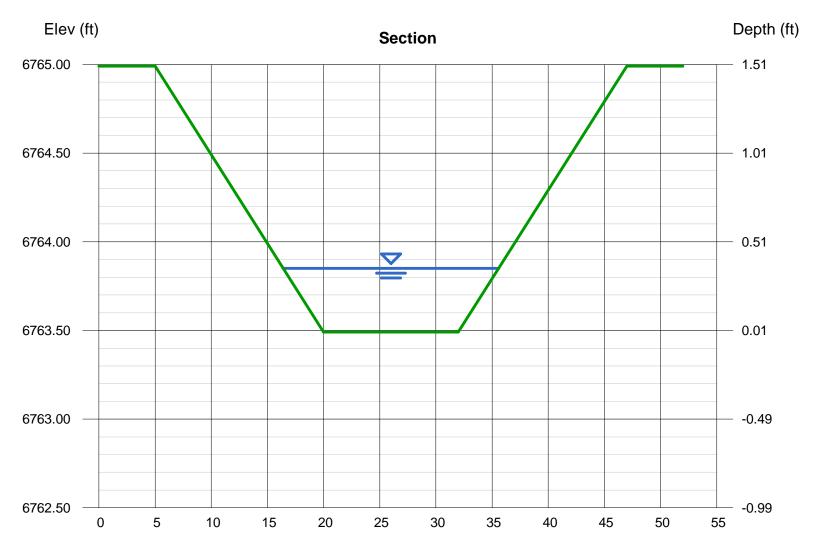
Total Depth (ft) = 1.50 Invert Elev (ft) = 6763.49 Slope (%) = 0.01 N-Value = 0.013

**Calculations** 

Compute by: Known Q Known Q (cfs) = 2.80

Highlighted

Depth (ft) = 0.36Q (cfs) = 2.800Area (sqft) = 5.62Velocity (ft/s) = 0.50Wetted Perim (ft) = 19.24Crit Depth, Yc (ft) = 0.12Top Width (ft) = 19.20EGL (ft) = 0.36



Dooch (ft)

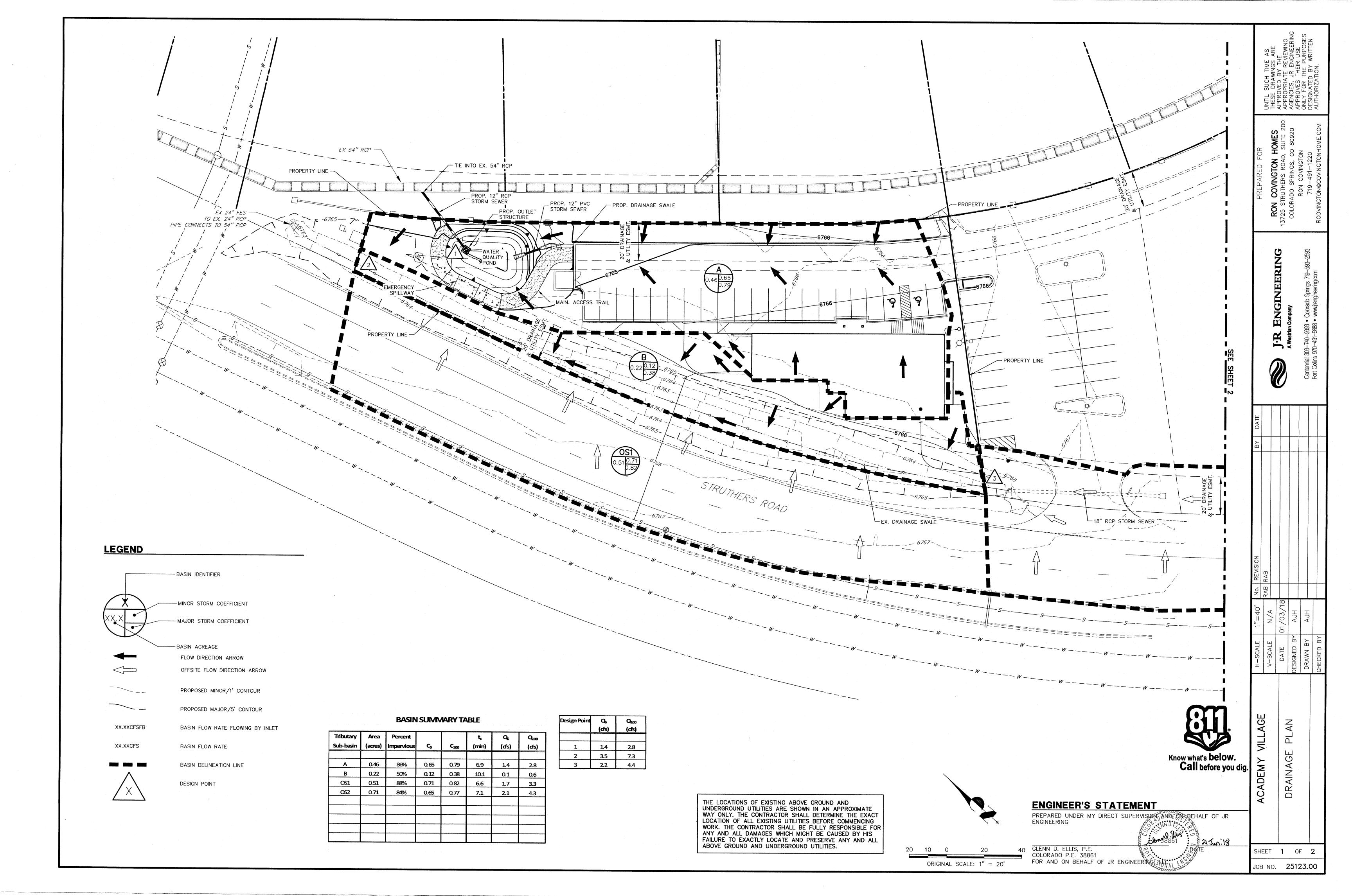
You created this PDF from an application that is not licensed to print to novaPDF printer (http://www.novapdf.com)

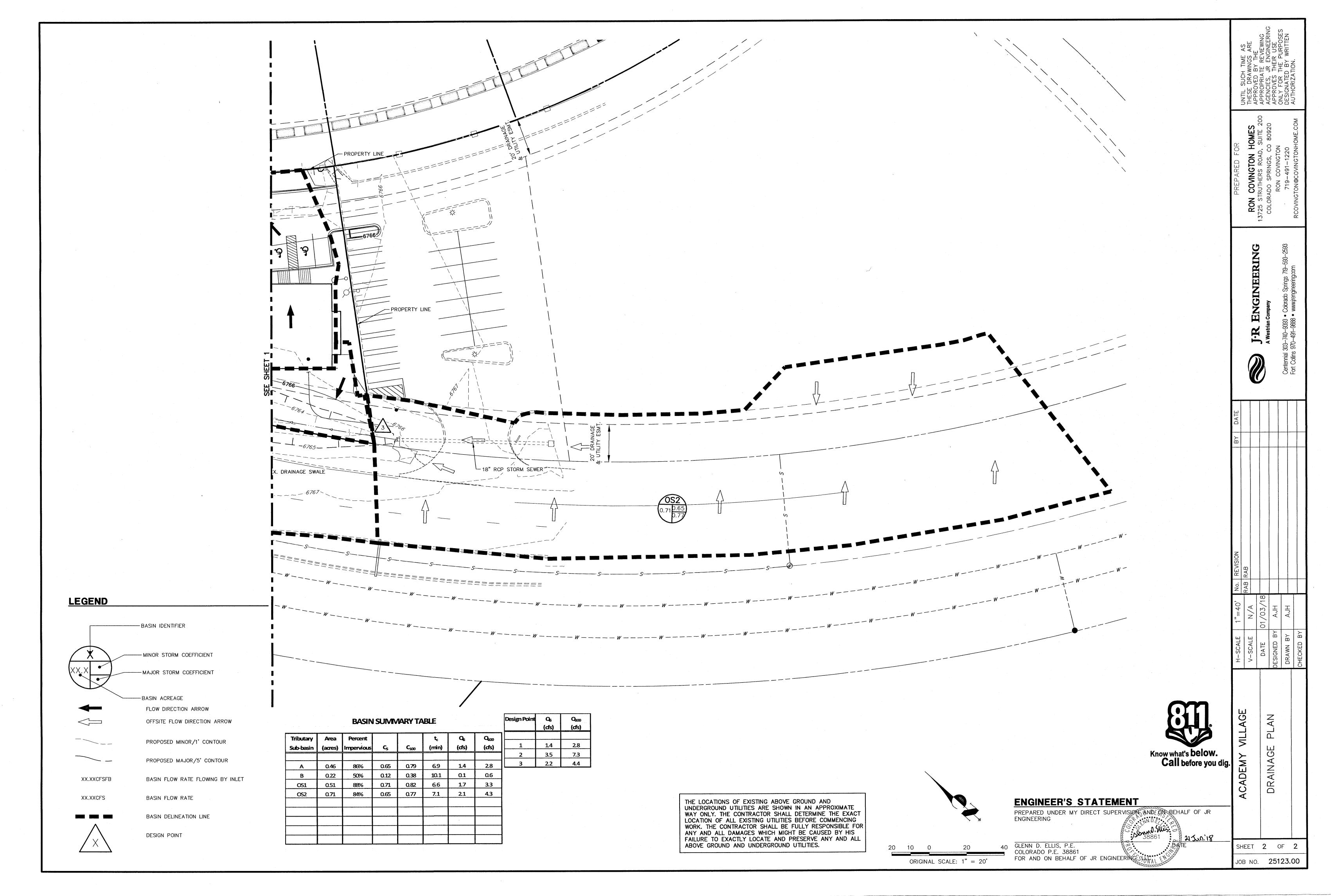
Page	7	0	f 7	

Academy Village Filing Number 3

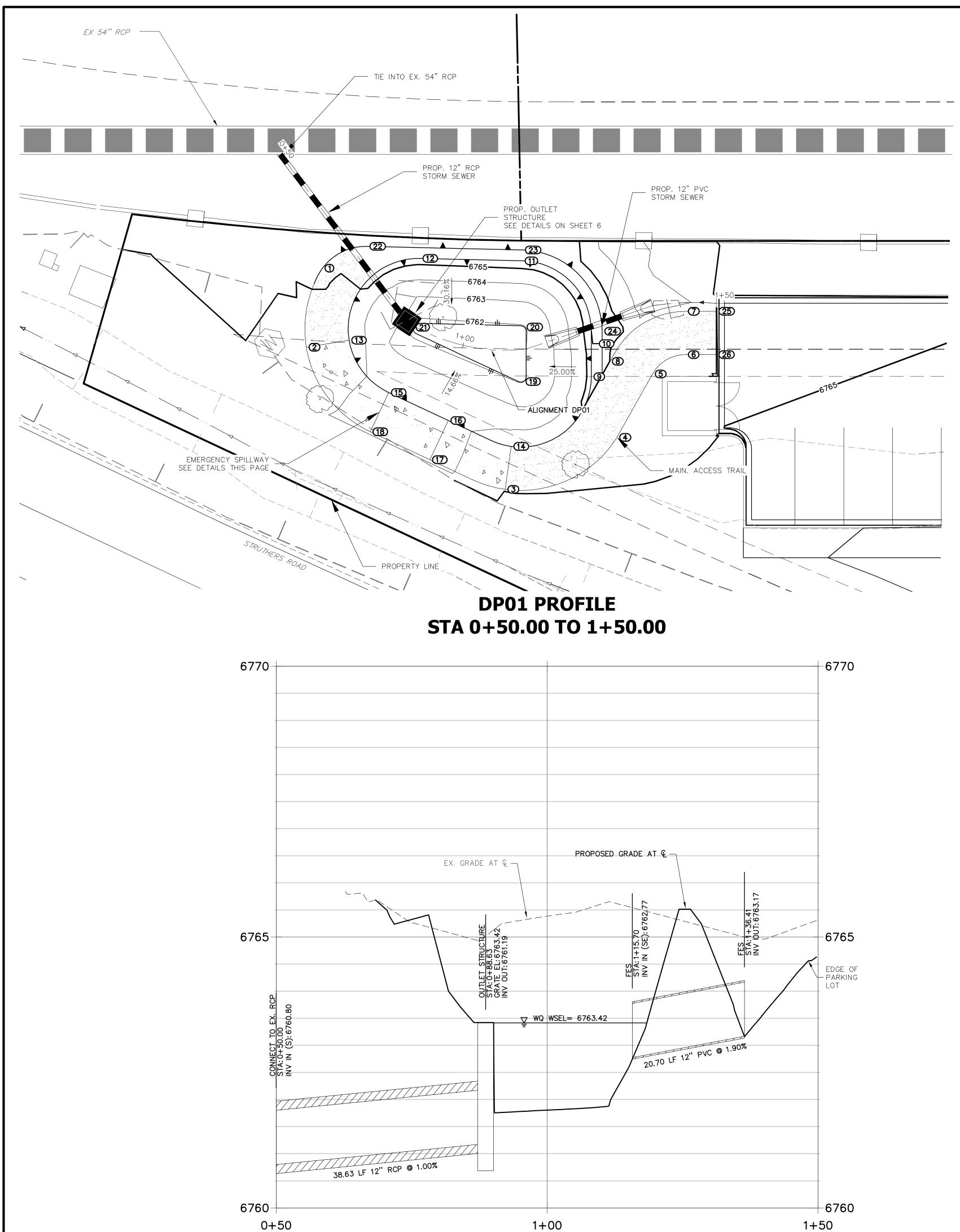
June 15, 2018

## Appendix B





twings\Sheet Dwgs\Drainage\2512300DR.dwg, DR (2), 6/27/2018 7:59:06 AN





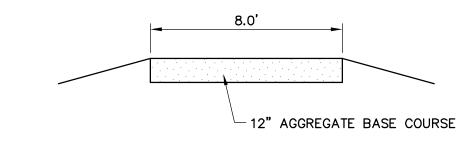
THE LOCATIONS OF EXISTING ABOVE GROUND AND

ABOVE GROUND AND UNDERGROUND UTILITIES.

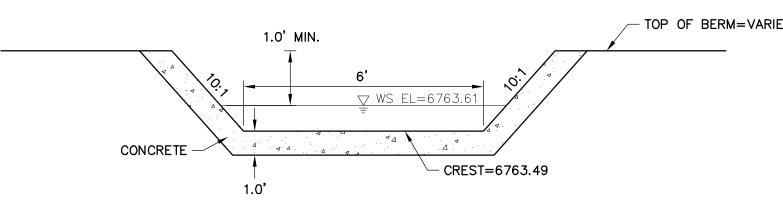
UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT

LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS

FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL



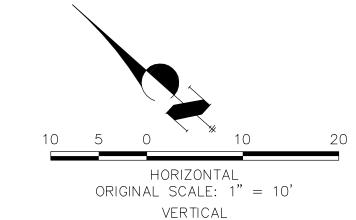
# GRAVEL MAINTENANCE ACCESS ROAD



EMERGENCY SPILLWAY

1.0' MIN.	SPRINGS.
6' 0. WS EL=6763.61	PREP RON COVII
CRETE ———————————————————————————————————	

JOB NO. **25123.00** 

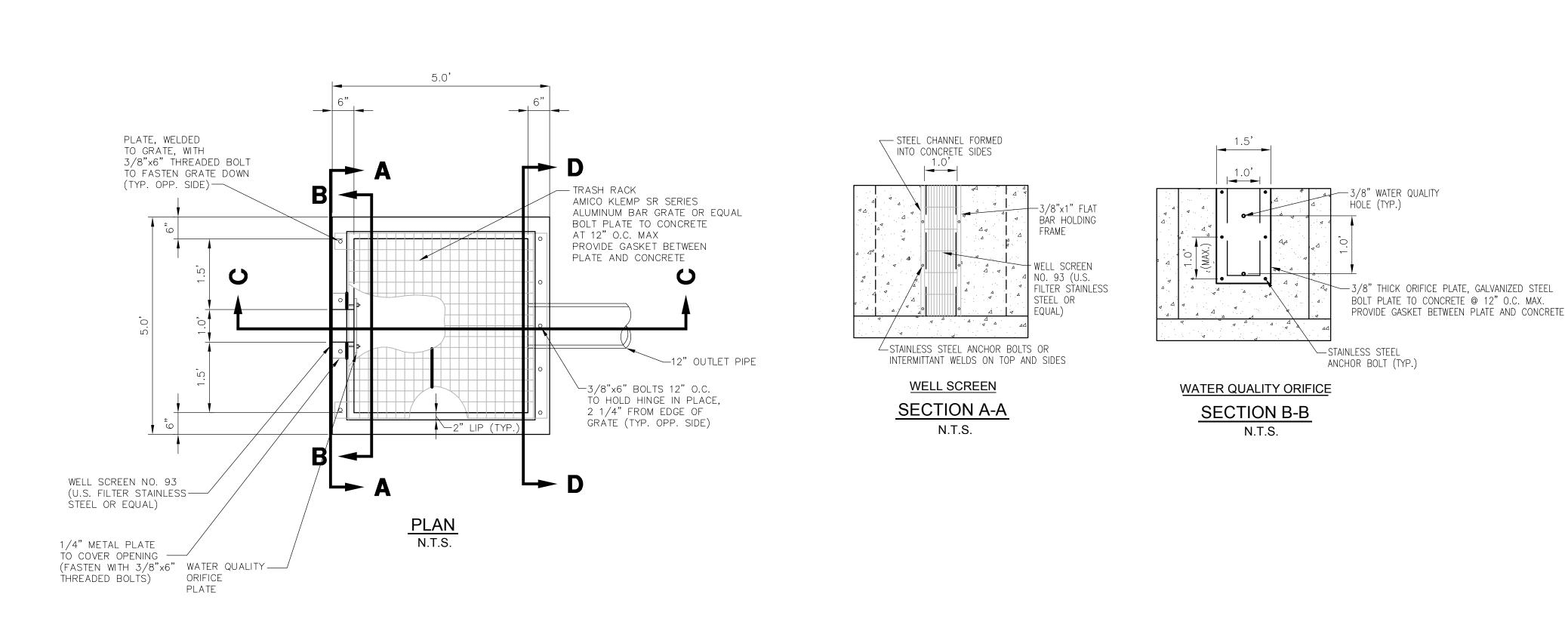


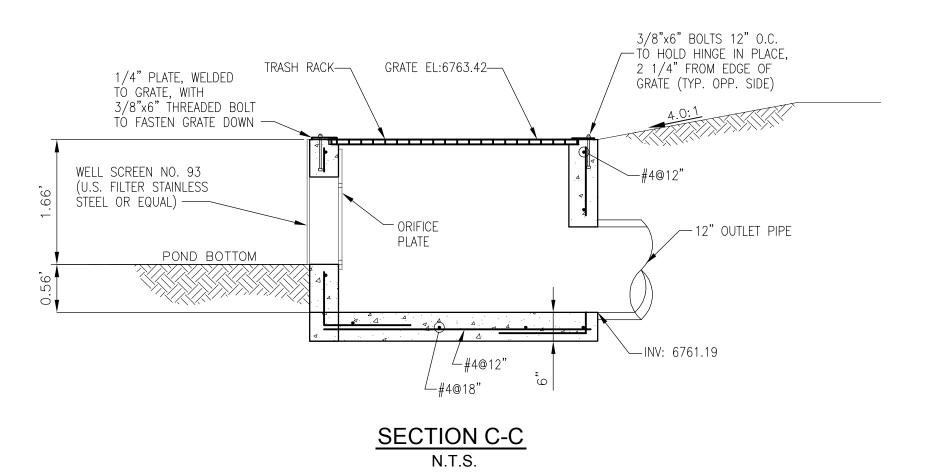
ORIGINAL SCALE: 1" = 1'

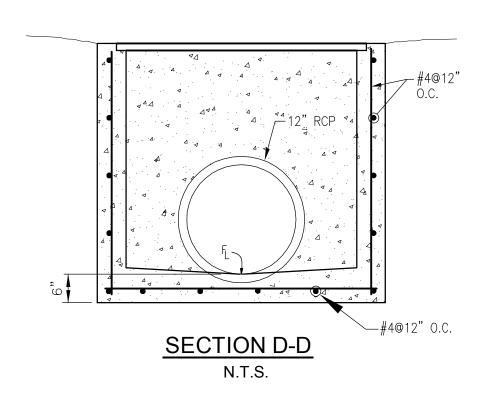


SHEET 5 OF 6

CADEMY	VILLAGE	FILING	NO.	3	SITE	DE	VEL	OPMEN	ГР	$\bot \land$
				Р	ROJE	СТ	NO:	PPR-	18-	- 0 2







Know what's below.
Call before you dig.

AN SHEET 6 OF 6
021 JOB NO. 25123.00

STRUCTURE

VILLAGE 3

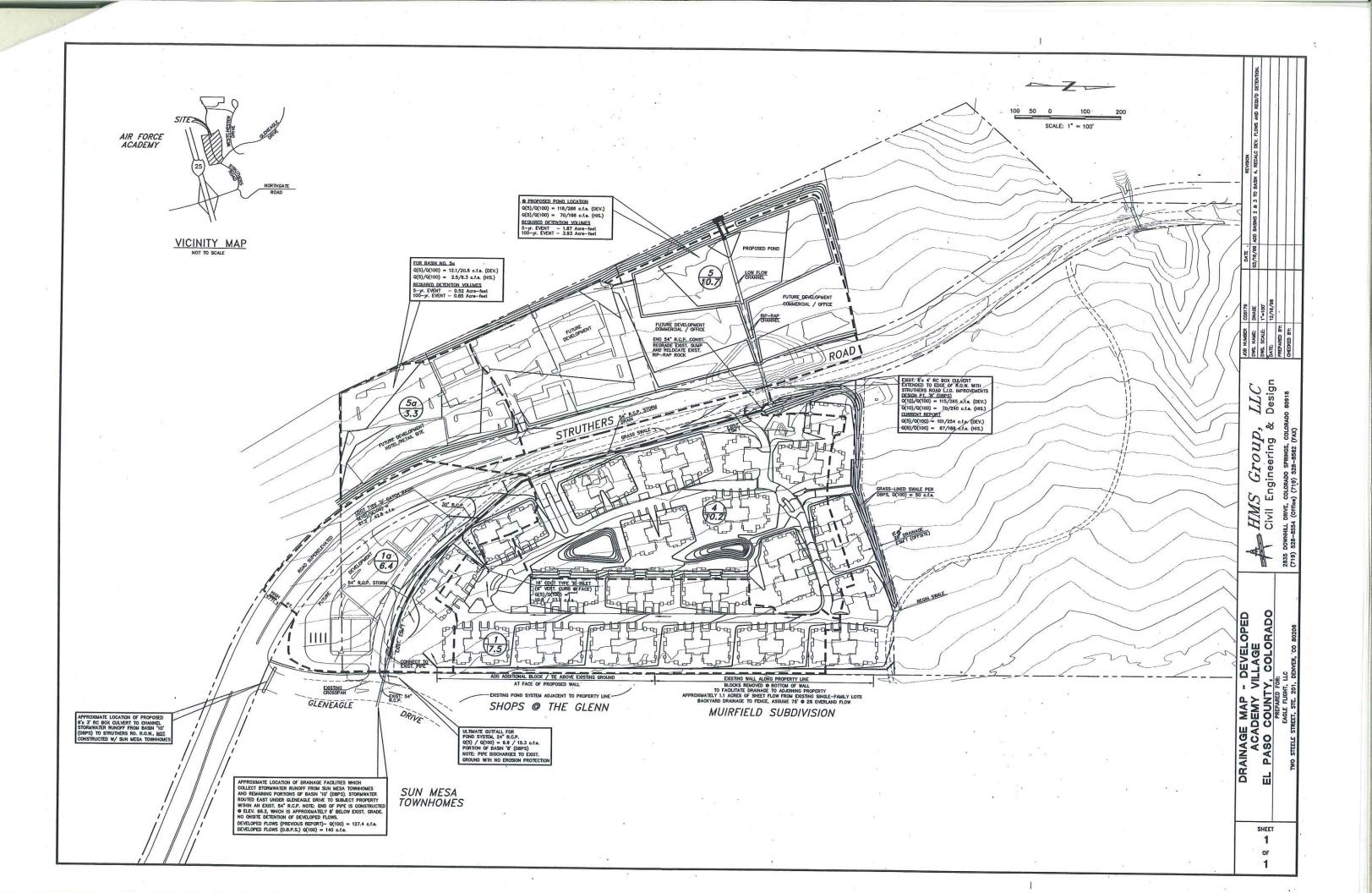
ACADEMY

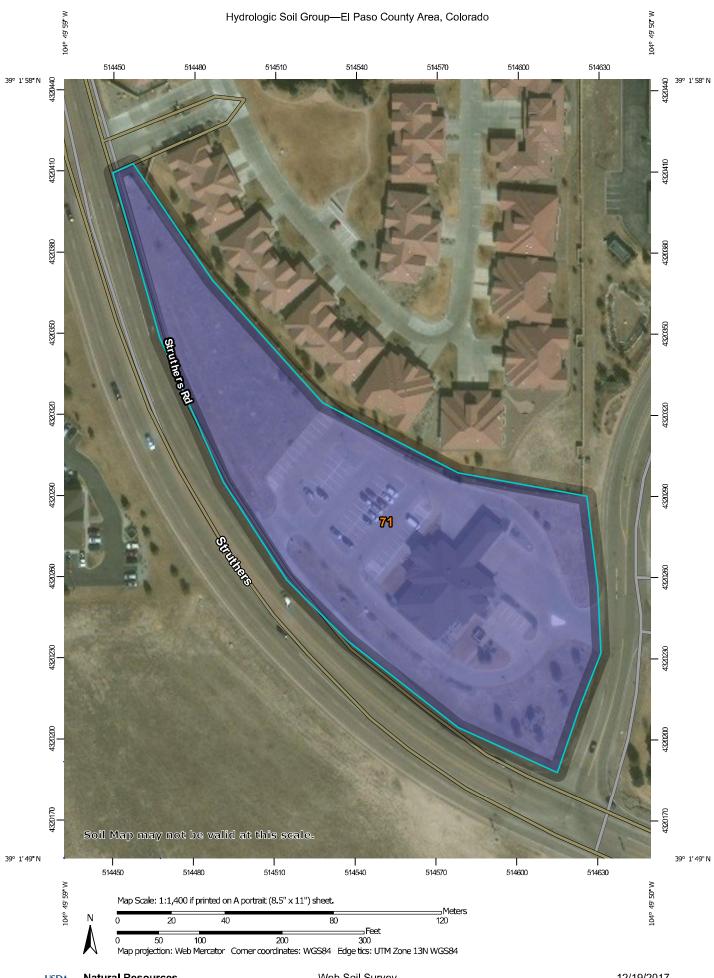
COVINGTON

RON 725 ST COLORA

ENGINEERING

ACADEMY VILLAGE FILING NO. 3 SITE DEVELOPMENT PLAN PROJECT NO: PPR-18-021





## **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	3.5	100.0%
Totals for Area of Intere	est	•	3.5	100.0%

### **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

Aggregation Method: Dominant Condition

