

FINAL DRAINAGE REPORT

For

MAYBERRY, COLORADO SPRINGS – FILING NO. 2A

PREPARED FOR:

MAYBERRY COMMUNITIES, LLC 3296 DEVINE HEIGHTS #208 COLORADO SPRINGS, CO 80922

PREPARED BY:

R & R ENGINEERS - SURVEYORS, INC. 1635 W. 13TH AVE, SUITE 310 DENVER, CO 80204 CONTACT: TIM STACKHOUSE, P.E. (303) 753-6730

> R&R JOB #MC22249 EPC PROJECT NO. VR2323

> > **JANUARY 2024**

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for liability caused by negligent acts, errors, or omissions on my part in preparing this report.

SIGNATURE:

Tim Stackhouse, P.E. Registered Professional Engineer State of Colorado No. 0061924

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

SIGNATURE: _____

John Mick Colorado Springs Mayberry, LLC 3296 Devine Heights #208 Colorado Springs, CO 80922

EL PASO COUNTY'S STATEMENT:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2, and Engineering Criteria Manual as amended.

SIGNATURE:

Joshua Palmer, P.E. County Engineer/ECM Administrator

TABLE OF CONTENTS

I.	GENERAL LOCATION AND DESCRIPTION
A.	Background1
В.	Scope 1
C.	Site Location and Description2
D.	General Soil Conditions 2
Ε.	References
II.	DRAINAGE BASINS AND SUB-BASINS
Α.	Major Drainage Basins
В.	Floodplain Impacts
C.	Sub-Basin Description
III.	DRAINAGE DESIGN CRITERIA
Α.	Development Criteria Reference
В.	Hydrologic Criteria
C.	Hydraulic Criteria5
IV.	DRAINAGE PLANNING FOUR STEP PROCESS
v.	GENERAL DRAINAGE RECOMMENDATIONS
VI.	DRAINAGE FACILITY DESIGN
Α.	General Concept
В.	Specific Details
C.	Comparison of Developed to Filing 3 FDR
D.	Onsite Drainage Facility Design
E.	Analysis of Existing and Proposed Downstream Facilities9
F.	Anticipated Drainage Problems and Solutions9
VII.	EROSION CONTROL
VIII.	COST ESTIMATE AND DRAINAGE FEES
IX.	MAINTENANCE
Х.	SUMMARY 10
XI.	APPENDICES 11
Ap	ppendix A - Hydrologic Computations

Appendix B – Hydraulic Computations	11
Appendix C – Reference Information	11

I. GENERAL LOCATION AND DESCRIPTION

A. Background

Mayberry Filing 2A encompasses 4.48 acres southwest of the Springs Road and Highway 94 intersection. Filing 2A is adjacent to Filing 3 along its west and south borders. The previous layout/design of this area was named Mayberry Filing 2 by JPS Engineering. JPS had submitted construction documents, a SWMP report, and a Final Drainage Report for Filing 2 which was approved by El Paso County in November of 2020.

Final Drainage Report for Mayberry Colorado Springs – Filing No. 3 (referred to as Filing 3 FDR hereon) by R&R Engineers-Surveyors has been approved by El Paso County and is currently under construction. Filing 3 FDR has designed and sized all drainage infrastructure that Filing 2A is tributary to. This Drainage Conformance Letter will include documentation and calculations to support that the new layout of this area is still in compliance with the in process Filing 3 FDR.

B. Scope

This Drainage Conformance Letter has been prepared to fulfill the El Paso County requirements for a "Letter Type" drainage report, as this area is within Mayberry Filing 2, which incorporated a previously approved Filing 2 FDR by JPS Engineering and is tributary to the Filing 3 FDR by R&R Engineers-Surveyors.

Mayberry Filing 2A proposes a cul-de-sac in place of the previously extended road. The previous design in Filing 2 extended Cattlemen Run through Filing 2, connecting to Positive Place. This cul-de-sac will include a six-inch vertical curb and adjacent sidewalk. Like Filing 2, Filing 2A has three total lots. These lots are configured differently as each lot fronts the cul-de-sac instead of being separated by an intersection.

The report will provide a summary of site drainage issues impacting the proposed development, including analysis of impacts from upstream drainage patterns, site-specific developed drainage patterns, and impacts on downstream facilities. This drainage compliance letter was prepared based on the guidelines and criteria presented in the El Paso County Drainage Criteria Manual, providing design of required drainage facilities for this phase of the project.

C. Site Location and Description

The Mayberry, Colorado Springs (Ellicott Town Center) parcel comprises the west half of Section 14 along with the contiguous east quarter of Section 15, as well the west half of the northeast quarter of Section 14, Township 14 South, Range 63 West of the 6th Principal Meridian. The site is located at an elevation of approximately 6,060 feet above mean sea level. Filing No. 2A comprises 4.48-acres in the north/central area of the Mayberry development.

State Highway 94 borders Filing 2A to the north, Filing 3 to the south and west, and Filing 4 to the east.

The primary access to Filing 2A will be provided by Business Park Drive via Springs Road.

The terrain is generally flat with gentle northwest to southeast slopes ranging from one to two percent. Historic drainage patterns from the site are conveyed overland to the south and east boundaries of the site. The entire site is covered with native grasses.

D. General Soil Conditions

According to the Soil Survey of El Paso County prepared by the Soil Conservation Service, on-site soils are comprised primarily of Blakeland series (type 8) and Truckton series (type 95) soils. Both soils are characterized as well-drained loamy sand with rapid permeability, slow surface runoff rates, and moderate hazard of erosion. These soils are classified as hydrologic soils group "A" for drainage analysis purposes.

E. References

El Paso County "Engineering Criteria Manual," January 9, 2006.

El Paso County "Drainage Criteria Manual County of El Paso, Colorado – Volumes 1 and 2" dated October 31, 2018.

El Paso County Resolution No. 15-042 (El Paso County adoption of "Chapter 6: Hydrology" and "Chapter 13, Section 3.2.1: Full Spectrum Detention" of the City of Colorado Springs Drainage Criteria Manual dated May 2014).

JPS Engineering, "Final Drainage Report for Mayberry, Colorado Springs - Filing No. 2," revised October 27, 2020 (approved by El Paso County November 5, 2020).

R&R Engineers-Surveyors, "Final Drainage Report for Mayberry Colorado Springs – Filing No. 3," *Approved June 14th, 2023.*

II. DRAINAGE BASINS AND SUB-BASINS

A. Major Drainage Basins

The proposed development lies primarily within the Ellicott Consolidated Drainage Basin (CHBS1200) as classified by El Paso County. This basin is comprised of the area tributary to the West Fork of Black Squirrel Creek, with the majority of the basin bounded by SH94 to the north and Ellicott Highway to the east. No drainage planning study has been completed for the Ellicott Consolidated Drainage Basin or any adjacent drainage basins.

The major drainage basins lying in and around the proposed development are depicted in the Phase 1 PUD Amended Drainage Report. Mayberry, Colorado Springs is located primarily within the Ellicott Consolidated Drainage Basin, which comprises a tributary area of about 13 square miles, or 8,320 acres. Filing 2A represents a total of 9.48 acres of development, or less than one percent of the total basin area. An "onsite" drainage planning approach has been proposed in Filing 2A based on the relatively small developed area in comparison to the remaining undeveloped basin area, which is primarily agricultural land.

B. Floodplain Impacts

Mayberry – Filing 2A, Colorado Springs is located approximately one mile southwest of the 100-year floodplain limits for the West Fork of Black Squirrel Creek, as delineated by the Federal Emergency Management Agency (FEMA). The floodplain limits in the vicinity of the site are shown in Flood Insurance Rate Map (FIRM) Number 08041C0810G, dated December 7, 2018.

C. Sub-Basin Description

The developed drainage basins lying within Filing 2A are depicted in Figure D1.1. The interior site layout has been delineated into three drainage basins based on the proposed interior road layout and grading scheme. The natural drainage patterns will be impacted through development by site grading and concentration of runoff in the street gutters, storm drains, and channels. Most sub-basins drain to the southeast, collecting in the interior roadway, Business Park Drive, and drainage channels. On-site flows will be diverted to an extended detention basin (EDB), Pond D, assumed as existing per the approved Mayberry Filing 3 Final Drainage Report, and detained flows will discharge to the east, following historic drainage paths.

III. DRAINAGE DESIGN CRITERIA

A. Development Criteria Reference

The Ellicott Consolidated Drainage Basin has not had a Drainage Basin Planning Study performed for the basin. Most areas within the basin are comprised of agricultural lands and rural residential uses.

A "Master Development Drainage Plan (MDDP) for Ellicott Town Center" was approved concurrent with the original Overall PUD, and a Preliminary Drainage Report for Ellicott Town Center Phase One was approved with the original Phase One PUD and Preliminary Plan.

JPS Engineering prepared the "Preliminary & Final Drainage Report for Mayberry, Colorado Springs - Filing No. 1," revised October 27, 2020 (approved by El Paso County November 5, 2020) in support of the final approval and recording of Filing No. 1.

The "Final Drainage Report for Mayberry, Colorado Springs – Filing No. 3" fully conforms to the previously approved MDDP and Preliminary/Final Drainage Reports, along with the "Preliminary Drainage Report Amendment for Mayberry, Colorado Springs Phase 1 PUD" dated February, 2022 prepared in support of the Phase 1 PUD Amendment.

This, "Final Drainage Report for Mayberry, Colorado Springs – Filing No. 2A" fully conforms to the approved "Final Drainage Report for Mayberry, Colorado Springs – Filing No. 3".

B. Hydrologic Criteria

Rational method procedures were utilized for calculation of peak flows within the onsite drainage basins. Rational method hydrologic calculations were based on the following assumptions:

•	Design storm (minor)	5-year
•	Design storm (major)	100-year
•	Rainfall Intensities	El Paso County I-D-F Curve
•	Hydrologic soil type	A

Composite runoff coefficients for the developed commercial areas have been calculated based *Table 6-6 Runoff Coefficients for Rational Method* in Chapter 6, Section 3.1 in the El Paso County Drainage Criteria Manual. A rational method spreadsheet was utilized for modeling these flows.

C. Hydraulic Criteria

Most of the hydraulic elements of Filing 2A have already been analyzed and provided in the approved Filing 3 Final Drainage Report as it relates to inlet and street capacity and storm pipe capacity. The supporting pages from the Filing 3 Final Drainage Report are provided within the appendix.

One grass lined swale is proposed as part of the Filing 2A development. The swale will be lined in wetland native seed. The grass swale, located along the southern property boundary, was calculated using flow master, the supporting calculation sheet and cross section can be found in Appendix B.

IV. DRAINAGE PLANNING FOUR STEP PROCESS

El Paso County Drainage Criteria require drainage planning to include a Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls. A new ESQCP will be acquired for Mayberry Filing 2A.

As stated in DCM Volume 2, the Four Step Process is applicable to all new and redevelopment projects with construction activities that disturb 1 acre or greater or that disturb less than 1 acre but are part of a larger common plan of development. The Four Step Process has been implemented as follows in the planning of this project:

Step 1: Employ Runoff Reduction Practices

- Minimize Impacts: The approved Planned Unit Development includes commercial use areas resulting in a moderate level of impervious site development.
- Minimize Directly Connected Impervious Areas (MDCIA): The proposed development will include landscaped areas adjoining the proposed building and parking lots, providing for impervious areas to drain across pervious areas where feasible.
- Grass Swales: The proposed drainage plan incorporates grass-lined swales in selected locations to encourage stormwater infiltration while providing positive drainage through the site.

Step 2: Stabilize Drainageways

• Proper erosion control measures will be implemented along the grass-lined drainage swale to provide stabilized drainageways within the site.

Step 3: Provide Water Quality Capture Volume (WQCV)

• EDB: This development will drain through an existing Full-Spectrum Extended

- Detention Basins (EDB) southeast of the developed areas. Site drainage will be routed through the extended detention basin, which will capture and slowly release the WQCV over an extended release period.
- Stormwater detention and WQCV for Filing 2A will be provided by the existing EDB-D, designed within the Filing 3 Final Drainage Report.
- The existing offsite detention basin and a

Step 4: Consider Need for Industrial and Commercial BMPs

• Commercial land uses are proposed as part of Filing No. 2A development. The individual commercial site owners for each lot will be encouraged to provide additional water quality treatment such as grass lined swales, porous landscape, permeable pavement, etc. however this is not required if the developed lot remains in compliance with the pre-determined impervious area set forth in this drainage report. Water quality is treated in the down stream grass lined swales and existing extended detention pond.

V. GENERAL DRAINAGE RECOMMENDATIONS

The developed drainage plan for the site is to provide and maintain positive drainage away from structures and conform to the established drainage patterns for the overall site. Positive drainage shall be established and maintained away from all structures within the site in conformance with applicable building codes and geotechnical engineering recommendations.

In general, it is recommended that positive drainage slopes should be maintained away from all structures, with a minimum recommended slope of 5 percent for the first 10 feet away from buildings in landscaped areas, a minimum recommended slope of 2 percent for the first 10 feet away from buildings in paved areas, and a minimum slope of 1 percent for paved areas beyond buildings.

VI. DRAINAGE FACILITY DESIGN

A. General Concept

Consistent with generally accepted practices in eastern El Paso County, the general concept for stormwater management from development of Mayberry – Filing 2A will be to construct curb and gutter and a grass swale to connect to the existing storm sewer system, channels, and extended detention basin constructed in Mayberry Filing No. 3.

Runoff from Lot 1A, which includes the existing InteliFab building and associated

asphalt parking lot, will drain to Business Park Drive primarily through the existing sidewalk chase designed and constructed per the approved Filing 2 construction documents and Final Drainage Report by JPS. Runoff from Lots 2A and 3A will drain toward the southeast, and be captured by the proposed grass swale. Depending on the future developers' preference for Lots 2A and 3A, he or she can choose to keep the open ditch, or choose to fill in the ditch and replace with an underground storm pipe. Should one lot owner choose to provide an underground storm pipe and the other lot owner choose to keep the provided open ditch, a flared end section must be constructed to keep the positive drainage to the overall stormwater network.

B. Specific Details

Existing Drainage

The existing site spans three basins defined in the Filing 3 FDR: Basins D1.1, D1.13, and D1.14. The site generally drains from northwest to southeast. Undeveloped flows sheet flow generally towards Springs Road and Besseyi Way, ultimately entering multiple existing inlets (Design Points 5B and 7B per Filing 3 FDR). Existing inlets exist near the intersection of Business Park Drive and Springs Road and the intersection of Besseyi Way and Springs Road. An existing 24" RCP stub exists in the southwest corner of the site. There is no other existing stormwater conveyance infrastructure currently on site (piping, inlets, channels, etc) and no detention/water quality facilities existing on the site.

Proposed Drainage

The proposed site is split between Filing 3 FDR Basins D1.1, D1.13, and D1.14. Runoff from the site will generally flow northwest to southeast and flow into either Business Park Drive or a swale on the southern property line, ultimately being conveyed to the existing storm sewer system.

The existing detention basin, Pond D (designed with the approvedbu Filing 3 FDR) has been designed to detain and treat flows from the entirety of Filing 2A. Therefore, no stormwater quality or detention facilities will be installed on the site.

Basin D1.1 is a 1.73 acre basin originally defined in the Filing 3 FDR. It comprises the southern commercial developments of Filing 2A. The basin drains towards the southern property line and is collected by a swale which conveys water to a proposed flared end section in the southeast corner of the site at design point 7C, and ultimately enters the existing storm sewer system within Springs Road. The 5 year and 100 year developed peak flows are 6.7 and 12.2 cfs respectively.

Basin D1.13 is a 3.07 acre basin originally defined in the Filing 3 FDR. It comprises the northern commercial development of Filing 2A and a portion of Springs Road. The basin ultimately drains into existing storm sewer system within Springs Road via an existing Type R curb inlet at design point 7B. The 5 year and 100 year developed peak flows are 9.2 and 17.6 cfs respectively.

Basin D1.14 is a 0.91 acre basin originally defined in the Filing 3 FDR. It comprises the south eastern commercial portion of Filing 2 and a portion of single family housing in Filing 3. The basin drains into Springs Road and is collected by an existing Type R curb inlet at design point 5B near the intersection of Besseyi Way and Springs Road. The 5 year and 100 year developed peak flows are 1.8 and 3.9 cfs respectively.

C. Comparison of Developed to Filing 3 FDR

The development of Filing 2A is in compliance with Filing 3 FDR in regard to both impervious percentages and peak flows. All Filing 2A impervious percentages and peak flows are equal to or below the limits listed in Filing 3 FDR. The following table provides a comparison of these value.

	Basir	ו D1.1	Basin	D1.13	Basin	D1.14
	Filing 3	Filing 2A	Filing 3	Filing 2A	Filing 3	Filing 2A
5 Year Flow	6.7	6.7	10.9	9.2	1.8	1.8
100 Year Flow	12.2	12.2	19.9	17.6	3.9	3.9
% Impervious	95%	95%	95%	80%	64%	64%

D. Onsite Drainage Facility Design

Curb and Gutter

Basin D1.13 will drain towards Business Park Drive and be captured by the existing and proposed curb and gutter. Business Park Drive is pitched to drain toward the east, and be ultimately captured by the existing cross pan designed and constructed per the Filing 2 plans by JPS. Flows will continue south and be captured by the existing type R inlet designed and constructed per the approved Filing 3 plans. The cross section of Business Park Drive is designed as the typical 2%, pushing water from the centerlines to curb and gutter systems.

Open Channel System Layout

One grass swale is proposed as part of the Filing 2A development located along the southern boundary which will capture all stormwater runoff from lots 2A and 3A. The V-

shaped swale is designed with side slopes of 4:1. The swale will convey stormwater runoff to the southeast corner of the Filing 2A boundary, and ultimately to the existing stormwater network designed within Filing 3.

E. Analysis of Existing and Proposed Downstream Facilities

The general concept of the proposed drainage plan is to attenuate peak flows from the developed site by routing flows to the existing detention pond, Pond D. An analysis of drainage patterns downstream of the subdivision was performed as part of the approved Filing 3 report to ensure historic drainage patterns are maintained. Filing 2A will remain in compliance with Filing 3, as the developed flows associated with this project remain equal or below what was anticipated within the approved Filing 3 Final Drainage report.

F. Anticipated Drainage Problems and Solutions

The existing stormwater detention pond is designed to mitigate the impacts of developed drainage from this project. The overall drainage plan for Filing 2A includes a public street with curb and gutter, an existing cross-pan at Business Park Drive and Springs Road, an existing sidewalk chase, and a grass swale. The primary drainage problems anticipated within this development will consist of maintenance of the sidewalk chase and drainage swale. The sidewalk chase will convey the 100-year flow and not overtop the sidewalk. Please refer to Appendix B for additional calculations. Care will need to be taken to implement proper erosion control measures in the proposed swale, which will be designed to meet allowable velocity criteria.

VII. EROSION CONTROL

The Contractor will be required to implement best management practices (BMP's) for erosion control during construction. The proposed erosion control plan is included in the Grading & Erosion Control (GEC) Plans submitted with the subdivision construction drawings. Erosion control measures will include installation of silt fence at the toe of disturbed slopes and hay bales protecting drainage ditches. Cut and fill slopes will be stabilized during excavation if necessary and vegetation will be established for stabilization of the disturbed areas. All ditches have been designed to meet El Paso County criteria for slope and velocity. Additionally, a gravel vehicle tracking pad will be installed at construction access point and inlet protection will be provided to minimize conveyance of sediment into storm inlets.

VIII. COST ESTIMATE AND DRAINAGE FEES

The developer will pay all capital costs for roadway and drainage improvements. As detailed in Appendix C. The engineer's estimate for Filing 2A drainage improvements is approximately \$627.90. Filing 2A is located entirely within the Ellicott Consolidated Drainage Basin, which currently does not have a drainage or bridge fee requirement. As such, no drainage basin fees are applicable.

IX. MAINTENANCE

All proposed road and drainage construction within the Mayberry – Filing 2A, Colorado Springs project will be performed to El Paso County Standards. Interior roads will be dedicated as public right-of-way. Roads and drainage facilities within the public right-of-way will be maintained by El Paso County upon final acceptance of these facilities after the warranty period. The Metropolitan District will maintain drainage channels and stormwater detention pond within the proposed open space areas.

X. SUMMARY

The Mayberry – Filing 2A, Colorado Springs consists of 3 commercial lots in the northwest of Springs Road and Business Park Drive, with access connections to State Highway 94 at Springs Road. The commercial lots are platted within Filing 2A. The development will generate an increase in developed runoff from the site, which will be mitigated through an existing stormwater detention and water quality facility designed and constructed within Filing 3, which accounted for these developed flows.

The proposed drainage patterns will remain consistent with historic conditions, and new drainage facilities constructed to El Paso County standards will safely convey runoff to adequate outfalls. The existing detention pond, Pond D southeast of the development areas will ensure that developed flows remain below historic levels. Construction and proper maintenance of the proposed drainage and erosion control facilities will ensure that this development has no significant adverse drainage impacts on downstream or surrounding areas.

XI. APPENDICES

Appendix A - Hydrologic Computations

- 1. Hydrologic References from Approved Filing 3 FDR
- 2. Filing 2A Post Developed Flow Rates

Appendix B – Hydraulic Computations

- 1. MHFD Spreadsheet from Approved Filing 3 FDR
- 2. Sidewalk Chase
- 3. Swale Design

Appendix C – Reference Information

- 1. Vicinity Map
- 2. Cost Estimate
- 3. NRCS Soils Report
- 4. FEMA Flood Insurance Maps
- 5. Referenced Narrative and Drainage Maps from Filing 3
- 6. Filing 2A Developed Drainage Map

APPENDIX A - HYDROLOGIC COMPUTATIONS



POST-DEVELOPMENT C VALUES

Designer:	FSI					Glob	al Parameters ¹			1	Sumn	narv	1				
	R&R Engineers-Survey	/ors				and Use	% Imp.	C ₅	C ₁₀₀	1	Total Area (ac)	561.92					
	1/5/2023		-		SF LOTS (1/6 A		47.5	0.375	0.545		Composite Impervious	33.1%					
8	Mayberry Filing 3				Hardscape		100	0.9	0.96			55.170					
· · ·			-	R&R					1					1 F			
Location:	El Paso County				Commercial		95	0.81	0.88						e 6-6 in El Pa		
			ENGIN	EERS Z	Landscape/Park	<	2	0.08	0.35					From Table	e 6-6 in El Pa	so County D	CM
			SORVE	KOK2 CD							Cells of this color are fo						
	1		1				1		1		Cells of this color are fo	or optional user-input					
Basin Name	Area	NRCS Hydrologic Soil	SF LOT	S (1/6 AC)	н	lardscape	Comm	ercial	Landsca	ape/Park	% Check	Percent Imperviousness		Run	off Coefficie	ent, C ²	
	(ac)	Group	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%			2-yr	5-yr	10-yr	25-yr	100-yr
C2.1	0.77	A	0.77	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C2.2	0.33	A	0.33	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C2.3	1.81	A	1.81	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C2.4	1.16	A	0.00	0.0%	0.93	80.0%	0.00	0.0%	0.23	20.0%	100.00%	80%		0.74			0.84
C2.5	9.61	A	9.61	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38	-		0.55
C3.0 D1.1	35.40 1.73	A	17.70 0.00	50.0% <mark>0.0%</mark>	0.00	0.0% 0.0%	0.00 1.73	0.0% 100.0%	17.70 0.00	50.0%	100.00% 100.00%	25% 95%		0.23 0.81			0.45
D1.1 D1.2	2.56	A	2.56	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.81			0.88
D1.2 D1.3	2.02	A	2.02	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38	+		0.55
D1.3 D1.4	3.75	A	3.52	93.9%	0.00	0.0%	0.23	6.1%	0.00	0.0%	100.00%	50%		0.38			0.53
D1.5	9.88	A	0.00	0.0%	0.00	0.0%	9.88	100.0%	0.00	0.0%	100.00%	95%		0.81			0.88
D1.6	1.96	A	1.96	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.7	1.56	A	1.56	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.8	1.27	A	1.27	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.9	0.54	A	0.54	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.10	2.13	А	2.13	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.11	1.23	А	0.00	0.0%	0.98	80.0%	0.00	0.0%	0.25	20.0%	100.00%	80%		0.74			0.84
D1.12	3.42	А	3.42	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.13	3.07	A	0.00	<mark>0.0%</mark>	0.00	<mark>0.0%</mark>	<mark>3.07</mark>	100.0%	0.00	<mark>0.0%</mark>	100.00%	<mark>95%</mark>		<mark>0.81</mark>			0.88
D1.14	0.91	A	0.60	<mark>65.9%</mark>	0.00	<mark>0.0%</mark>	<mark>0.31</mark>	<mark>34.1%</mark>	0.00		100.00%	<mark>64%</mark>		<mark>0.52</mark>			0.66
D2.0	11.90	A	9.50	79.8%	0.00	0.0%	0.00	0.0%	2.40	20.2%	100.00%	38%		0.32			0.51
E1	3.92	A	0.00	0.0%	0.00	0.0%	0.00	0.0%	3.92	100.0%	100.00%	2%		0.08			0.35
D2.1	3.15	A	0.00	0.0%	0.00	0.0%	0.00	0.0%	3.15	100.0%	100.00%	2%		0.08			0.35
OS-1	2.65	A	0.00	0.0%	0.91	34.3%	0.00	0.0%	1.74	65.7%	100.00%	36%		0.36			0.56
C Basins	49.08	Α	30.22	61.6%	0.93	1.9%	0.00	0.0%	17.93	36.5%	100.00%	32%		0.28			0.48
D Basins	51.08	A	29.08	56.9%	0.98	1.9%	15.22	29.8%	2.65	5.2%	93.83%	57%		0.48			0.61
													İ	-	1	1	1
Pond - Developed	100.16	A	59.30	59.2%	1.91	1.9%	15.22	15.2%	20.58	20.5%	96.86%	45%		0.38			0.55
D1.5 (pre-dev)	9.88	А	0.00	0.0%	0.00	0.0%	0.00	0.0%	9.88	100.0%	100.00%	2%		0.08			0.35
D2.0 (pre-dev)	11.90	A	0.00	0.0%	0.00	0.0%	0.00	0.0%	11.90	100.0%	100.00%	2%		0.08			0.35
C3.0 (pre-dev)	35.40	А	0.00	0.0%	0.00	0.0%	0.00	0.0%	35.40	100.0%	100.00%	2%		0.08			0.35
Pond - F2 & F3 Dev only	100.16	A	32.10	32.0%	1.91	1.9%	5.34	5.3%	60.81	60.7%	100.00%	23%					
*highlighted basins are			R.														+
tributary to Pond D in				Pond D	was sized f	or Filing 2A											
Interim condition																	
GALV	4.44	A	4.44	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C Basins - Pre Dev	49.08	A	12.52	25.5%	0.93	1.9%	0.00	0.0%	35.63	72.6%	100.00%	15.5%		0.17			0.41
D Basins - Pre Dev	49.08	A	12.52	40.9%	0.93	2.1%	5.34	11.1%	22.03	46.0%	100.00%	33.0%		0.17	1		0.41

TIME OF CONCENTRATION

Designer: Company:	ESJ R&R Engineers-3	Surveyors] [$t_i = \frac{0.395}{1000}$			mputed $t_c = t_c$	$t_i + t_t$ t_r	_{ninimum} = 5 (urba _{ninimum} = 10 (no	an)	Non Urban Li ma Urban Li Max = 1 			
		Surveyors		4	+	L _t L	t a		6						
	1/5/2023	-			$l_t = -60H$	$\frac{L_t}{\zeta \sqrt{S_t}} = \frac{L}{60}$	V _t Sel	ected t _c = max	(t _{minimum} , n	nin(Computed t	_c , Regional t _c)}				R&R
-	Mayberry Filing	3						L I					1	=	
Location:	El Paso County				Regional t	_e = (26 –	$17i) + \frac{1}{60(14)}$	$\frac{L_t}{1+9)\sqrt{S_t}}$		Cells of this c	olor are for require	ed user-input			ENGINEERS SURVEYORS
	Subbasin I	Data		1	nd (Initial) Flo				elized (Travel) F	low Time			Tiı	me of Concentra	ation
Basin	Area	% Impervious	C5	Overland Flow Length L _i (ft)	Overland Flow Slope S _i (ft/ft)	Overland Flow Time t _i (min)	Channelized Flow Length L _t (ft)	Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)	Channelized Flow Time t _t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	Remarks
C2.1	0.77	47.5%	0.38	100.00	0.020	10.41	242.00	0.020	20	2.83	1.43	11.84	19.75	11.84	
C2.2	0.33	47.5%	0.38	36.00	0.020	6.25	152.00	0.020	20	2.83	0.90	7.14	19.07	7.14	
C2.3	1.81	47.5%	0.38	100.00	0.020	10.41	1033.00	0.010	20	2.00	8.61	19.02	28.93	19.02	
C2.4	1.16	80.4%	0.74	12.00	0.020	1.81	534.00	0.009	20	1.90	4.69	6.50	16.96	6.50	
C2.5	9.61	47.5%	0.38	36.00	0.020	6.25	513.00	0.007	20	1.67	5.11	11.36	24.45	11.36	
C3.0	35.40	24.8%	0.23	100.00	0.020	12.53	1536.00	0.010	20	2.00	12.80	25.33	42.33	25.33	
D1.1	1.73	95.0%	0.81	100.00	0.020	4.17	405.00	0.020	20	2.83	2.39	6.55	11.99	6.55	
D1.2	2.56	47.5%	0.38	100.00	0.020	10.41	533.00	0.010	20	2.00	4.44	14.86	23.60	14.86	
D1.2	2.02	47.5%	0.38	36.00	0.020	6.25	495.00	0.010	20	2.00	4.13	10.37	23.20	10.37	
D1.4	3.75	50.4%	0.40	100.00	0.020	10.03	634.00	0.010	20	2.37	4.47	14.50	22.99	14.50	
D1.4	9.88	95.0%	0.40	100.00	0.020	4.17	856.00	0.014	20	2.00	7.13	11.30	16.25	11.30	
D1.6	1.96	47.5%	0.38	100.00	0.020	10.41	534.00	0.010	20	2.00	4.45	14.86	23.61	14.86	
D1.0	1.56	47.5%	0.38	100.00	0.020	10.41	530.00	0.010	20	2.00	4.42	14.83	23.57	14.83	
D1.7	1.30	47.5%	0.38	100.00	0.020	10.41	325.00	0.010	20	2.00	2.71	13.12	23.37	13.12	
D1.9	0.54	47.5%	0.38	36.00	0.020	6.25	323.00	0.010	20	2.00	3.24	9.49	21.39	9.49	
D1.10	2.13	47.5%	0.38	36.00	0.020	6.25	465.00	0.010	20	2.00	3.88	10.12	22.07	10.12	
D1.10	1.23	80.4%	0.38	12.00	0.020	1.81	962.00	0.010	20	2.61	6.15	7.96	18.40	7.96	
D1.11 D1.12	3.42	47.5%	0.74	100.00	0.020	10.41	1356.00	0.017	20	2.00	11.30	21.71	32.37	21.71	
	3.07	95.0%	0.38	100.00	0.020	4.17	456.00	0.010	20	1.79	4.25	8.41	13.66	8.41	
D1.13 D1.14	0.91	63.7%	0.81	100.00	0.020	4.17 8.28	400.00	0.008	20	1.79	3.73	12.01	19.33	12.01	
				1											
D2.0	11.90	38.3%	0.32	100.00	0.020	11.27	1750.00	0.011	20	2.10	13.90	25.17	38.84	25.17	
D2.1	3.15	2.0%	0.08	100.00	0.021	14.42						14.42		14.42	
E1	3.92	2.0%	0.08				2811.00	0.008							Tc calculated using TR55 - see Hydraflow Hydrographs Model
EC10	320.00		0.08	300.00	0.020		5250.00	0.013							Tc calculated using TR55 - see Hydraflow Hydrographs Model
OS-1	2.65	35.7%	0.36	50.00	0.020		2525.00	0.007							Tc calculated using TR55 - see Hydraflow Hydrographs Model
													 		
GALV	4.44	47.5%	0.38	36.00	0.020	6.25	1007.00	0.010	20	2.00	8.39	14.64	28.65	14.64	
D2.0 (pre-dev)	11.90	2.0%	0.08	100.00	0.020	14.65	1750.00	0.011	20	2.10	13.90	28.56	55.63	28.56	
C3.0 (pre-dev)	35.40	2.0%	0.08	100.00	0.020	14.65	1536.00	0.010	20	2.00	12.80	27.45	53.25	27.45	



Designer:	ESJ
Company:	R&R Engineers-Surveyors
Date:	1/5/2023
Project:	Mayberry Filing 3
Location:	El Paso County

Cells of this color are for required user-input Cells of this color are for optional user-input

$I_5 = -1.50 \ln(D) + 7.583$

				DIRI	ECT RUNOF	F				Т	OTAL RUNG	OFF		STREET	BYPASS		PIPE			TRAVE	EL TIME		
DESGIN POINT	STREET/ CONTRIBUTING BASINS	Basin Name	Area	Coeff	Тс	C*A	I	Q	Тс	Sum Area	Sum C*A	I	Q	Slope	Street Q	Design Q	Slope	PIPE	L	VEL	Tt	Q add'l	Remarks
			(ac)	с	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	%	cfs	cfs	%	SIZE	ft	ft/sec	min		
		C2.1	0.77	0.38	11.8	0.29	3.88	1.12															
1	C2.1								11.8	0.77	0.29	3.88	1.12						33	4	0.10		
		C2.2	0.33	0.38	7.1	0.12	4.63	0.57															
2	DP1, C2.2								11.9	1.10	0.41	3.86	1.59						450	4	1.90		
		C2.5	9.61	0.38	11.4	3.60	3.94	14.19											10	4	0.00		
3A	C2.5								11.4	9.61	3.60	3.94	14.19						196	4	0.80		
		C2.3	1.81	0.38	19.0	0.68	3.16	2.15															
3B	C2.3, DP3A								19.0	12.52	4.70	3.16	14.86						70	4	0.30		
		C2.4	1.16	0.74	6.5	0.85	4.77	4.08															
4	C2.4, DP3B			0.00		1.00	0.07		19.3	13.68	5.55	3.14	17.43						1590	4	6.60		
F A	54.42	D1.12	3.42	0.38	21.7	1.28	2.97	3.80	24 7	2.42	1.20	2.07	2.00						70	4	0.20		
5A	D1.12	D1 1 1	0.04	0.50	12.0	0.40	2.05	1.02	21.7	3.42	1.28	2.97	3.80						72	4	0.30		
5.0		D1.14	0.91	0.52	12.0	0.48	3.85	1.83	22.0	4.22	4.70	2.05	Г 10						20	4	0.10		
5B	D1.14, DP5A	D1 2	2.50	0.20	14.0	0.06	3.54	3.39	22.0	4.33	1.76	2.95	5.18						28	4	0.10		
6	D1.2	D1.2	2.56	0.38	14.9	0.96	3.54	3.39	14.9	2.56	0.96	3.54	3.39						10	4	0.00		
0	D1.2								14.9	2.50	0.90	5.54	5.55						10	4	0.00		
7A	DP5B, DP6								22.1	6.89	2.72	2.94	7.99						44	4	0.20		
78	DF3B, DF0	D1.13	3.07	0.81	8.4	2.49	4.39	10.91	22.1	0.89	2.72	2.94	7.55							4	0.20		
7B	D1.13	01.13	5.07	0.01	0.4	2.45	4.35	10.51	8.4	3.07	2.49	4.39	10.91						150	4	0.60		
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	01.13	D1.1	1.73	0.81	6.6	1.40	4.76	6.67	0.4	5.07	2.45	4.55	10.51						150		0.00		
7C	D1.1		1	0.01	0.0				6.6	1.73	1.40	4.76	6.67						63	4	0.30		
									0.0				0.07								0.00		
7D	DP7B, DP7C								9.0	4.80	3.89	4.28	16.66						280	4	1.20		
	,																						
7E	DP7D, DP7A								22.3	11.69	6.61	2.93	19.33						513	4	2.10		
		D1.3	2.02	0.38	10.4	0.76	4.07	3.09															
8	D1.3								10.4	2.02	0.76	4.07	3.09						27	4	0.10		
9	DP7, DP8								24.41	13.71	7.36	2.79	20.55						10	4	0.00		
		D1.4	3.75	0.40	14.5	1.51	3.57	5.38															
10	DP9, D1.4								24.41	17.5	8.9	2.79	24.75						827	4	3.40		
													18.43										Offsite flow, Input from Hydraflow
		EC10	320.00		0.0								10.45										Hydrographs, Calculated via SCS Method
													1.40										Offsite flow, Input from Hydraflow
		OS-1	2.65		0.0								1.40										Hydrographs, Calculated via SCS Method
													0.30										Input from Hydraflow Hydrographs,
		E1	3.92		0.0			ļ	ļ		ļ					ļ							Calculated via SCS Method
11	EC10, OS-1, E1												18.90						2811.6	4	11.70		Input from Hydraflow Hydrographs,
	,,																						Calculated via SCS Method



Des	igner:	ESJ

Company: R&R Engineers-Surveyors

Date: 1/5/2023

Project: Mayberry Filing 3

Location: El Paso County

Cells of this color are for required user-input Cells of this color are for optional user-input

 $I_{100} = -2.52 \ln(D) + 12.735$

	STREET/			DIRE	CT RUNOFF	-				т	OTAL RUN	OFF		STREET	BYPASS		PIPE			TRAVE	L TIME		
DESGIN POINT	CONTRIBUTING	Basin Name	Area	Coeff	Тс	C*A	I	Q	Тс	Sum Area	Sum C*A	I	Q	Slope	Street Q	Design Q	Slope	PIPE	L	VEL	Tt	Q add'l	Remarks
POINT	BASINS		(ac)	с	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	%	cfs	cfs	%	SIZE	ft	ft/sec	min		
		C2.1	0.77	0.55	11.8	0.42	6.51	2.73															
1	C2.1								11.8	0.77	0.42	6.51	2.73						33	4	0.10		
		C2.2	0.33	0.55	7.1	0.18	7.78	1.40															
2	DP1, C2.2								11.9	1.10	0.60	6.49	3.89						450	4	1.90		
		C2.5	9.61	0.55	11.4	5.24	6.61	34.63											10	4	0.00		
3A	C2.5								11.4	9.61	5.24	6.61	34.63						196	4	0.80		
		C2.3	1.81	0.55	19.0	0.99	5.31	5.24															
3B	C2.3, DP3A						1		19.0	12.52	6.82	5.31	36.25						70	4	0.30		
		C2.4	1.16	0.84	6.5	0.97	8.02	7.79															
4	C2.4, DP3B								19.3	13.68	7.80	5.27	41.10						1590	4	7.60		
		D1.12	3.42	0.55	21.7	1.86	4.98	9.28		1													
5A	D1.12								21.7	3.42	1.86	4.98	9.28						72	4	0.30		
		D1.14	0.91	0.66	12.0	0.60	6.47	3.88															
5B	D1.14, DP5A								22.0	4.33	2.46	4.94	12.18						28	4	0.10	1	
		D1.2	2.56	0.55	14.9	1.40	5.94	8.28		1													
6	D1.2								14.9	2.56	1.40	5.94	8.28						10	4	0.00		
7A	DP5B, DP6								22.1	6.89	3.86	4.93	19.03						44	4	0.20		
		D1.13	3.07	0.88	8.4	2.70	7.37	19.90															
7B	D1.13								8.4	3.07	2.70	7.37	19.90						150	4	0.70		
		D1.1	1.73	0.88	6.6	1.52	8.00	12.18															
7C	D1.1								6.6	1.73	1.52	8.00	12.18						63	4	0.30		
7D	DP7B, DP7C								9.1	4.80	4.22	7.17	30.27						280	4	1.30		
7E	DP7D, DP7A								22.3	11.69	8.08	4.91	39.69						513	4	2.40		
	,	D1.3	2.02	0.55	10.4	1.10	6.84	7.53	-			_											
8	D1.3								10.4	2.02	1.10	6.84	7.53						27	4	0.10		
9	DP7E, DP8								24.71	13.71	9.18	4.65	42.73						10	4	0.00		
		D1.4	3.75	0.57	14.5	2.12	6.00	12.72															
10	DP9, D1.4								24.71	17.5	11.3	4.65	52.59						827	4	3.90		
													144.70										Offsite flow, Input from Hydraflow Hydrographs,
		EC10	320.00		0.0								144.70										Calculated via SCS Method
													4.30										Offsite flow, Input from Hydraflow Hydrographs,
		OS-1	2.65		0.0								4.30										Calculated via SCS Method
													2.90										Input from Hydraflow Hydrographs, Calculated via
		E1	3.92		0.0								2.90										SCS Method
1 1													140.50						2011.0	4	11 70		Input from Hydraflow Hydrographs, Calculated via
11	EC10, OS-1, E1												148.50						2811.6	4	11.70		SCS Method
		D1.5	9.88	0.88	11.3	8.69	6.62	57.6															



POST-DEVELOPMENT C VALUES

Designer	r: LAO					Glob	oal Parameters1						Sumr	mary					
Company	r: R&R Engineers-Surveyo	ors			L	and Use	% Imp.	C ₅	C ₁₀₀				Total Area (ac)	0.91					
Date	e: 1/16/2024				SF LOTS (1/6 A	(C)	47.5	0.375	0.545				Composite Impervious	64%					
Project	t: Mayberry Filing 2A			RER	Hardscape		100	0.9	0.96										
Location	: El Paso County				Commercial/Inc	lustrial	95	0.81	0.88						¹ Fr	om Table 6	6-6 in El Pasc	County DCM	Λ
			ENGIN	EERS Z	Landscape		0	0.08	0.35						² Fr	om Table 6	6-6 in El Pasc	County DCM	Л
			SURVE	YORS 🗖	Roof		90	0.73	0.81				Cells of this color are for	or required user-input					
				•									Cells of this color are f	or optional user-input					
Basin Name	Area	NRCS Hydrologic Soil Group	SF LOT	S (1/6 AC)	н	ardscape	Commercial	'Industrial	Land	scape	Ro	oof	% Check	Percent Imperviousness		Runc	off Coefficier	ıt, C ²	
	(ac)	······	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%	· · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	2-yr	5-yr	10-yr	25-yr	100-yr
D1.1	1.73	A	0.00	0.0%	0.00	0.0%	1.73	100.0%	0.00	0.0%	0.00	0.0%	100.00%	95.0%		0.81			0.88
D1.13	3.07	А	0.00	0.0%	1.17	38.1%	0.92	30.0%	0.52	16.9%	0.46	15.0%	100.00%	80.1%		0.71			0.81
D1.14	0.91	A	0.60	65.9%	0.00	0.0%	0.31	34.1%	0.00	0.0%	0.00	0.0%	100.00%	63.7%		0.52			0.66
Sidewalk Chase	1.15	A	0.00	0.0%	0.69	60.0%	0.00	0.0%	0.00	0.0%	0.46	40.0%	100.00%	96.0%		0.83			0.90

TIME OF CONCENTRATION

Date: 1	LAO R&R Engineers 1/16/2024 Mayberry Filinį				t _i =	$\frac{S(1.1 - C_5)}{S_i^{0.33}}$ $\frac{L_t}{C_t - S_t} = \frac{L}{60}$		computed $t_c = t$ elected $t_c = mat$	t,	minimum= 5 (urba minimum= 10 (no min(Computed t	n-urban)	Non Urban Li ma: Urban Li Max = 1 }			RER
=	El Paso County	-			Regional $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$ Cells of this color are for required user-input									-	ENGINEERS SURVEYORS
	Subbasin	Data		Overla	nd (Initial) Flo	ow Time		Chann	elized (Travel) F	low Time			Time of C	Concentration	
Basin	Area	% Impervious	C5	Overland Flow Length L _i (ft)	Overland Flow Slope S _i (ft/ft)	Overland Flow Time t _i (min)	Channelized Flow Length L _t (ft)	Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)	Channelized Flow Time t _t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	Remarks
D1.1	1.73	95.0%	0.81	100.00	0.020	4.17	405.00	0.020	20	2.83	2.39	6.55	11.99	6.55	
D1.13	3.07	80.1%	0.71	100.00	0.020	5.62	456.00	0.010	20	2.00	3.80	9.42	16.15	9.42	
D1.14	0.91	63.7%	0.52	100.00	0.020	8.28	400.00	0.008	20	1.79	3.73	12.01	19.33	12.01	
Sidewalk Chase	1.15	96.0%	0.83	115.00	0.020	4.13	300.00	0.010	20	2.00	2.50	6.63	11.91	6.63	



Designer:	LAO
Company:	R&R Engineers-Surveyors
Date:	1/16/2024
Project:	Mayberry Filing 2A
Location:	El Paso County

Cells of this color are for required user-input Cells of this color are for optional user-input

$I_5 = -1.50 \ln(D) + 7.583$

	STREET/			DIF	RECT RUNC	DFF				Т	OTAL RUN	OFF		STREET	BYPASS		PIPE			TRAVE	L TIME		•
DESGIN POINT	CONTRIBUTING	Basin Name	Area	Coeff	Тс	C*A	I	Q	Тс	Sum Area	Sum C*A	I	Q	Slope	Street Q	Design Q	Slope	PIPE	L	VEL	Tt	Q add'l	Remarks
	BASINS		(ac)	С	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	%	cfs	cfs	%	SIZE	ft	ft/sec	min		
		D1.14	0.91	0.52	12.0	0.48	3.85	1.83															
5B	D1.14								12.0	0.91	0.48	3.85	1.83										
		D1.13	3.07	0.71	9.4	2.18	4.22	9.18															
7B	D1.13								9.4	3.07	2.18	4.22	9.18										
		D1.1	1.73	0.81	6.6	1.40	4.76	6.67															
7C	D1.1								6.6	1.73	1.40	4.76	6.67										
		Sidewalk																					
		Chase	1.15	0.83	6.6	0.96	4.75	4.54															
1cc	Sidewalk Chase								6.6	1.15	0.96	4.75	4.54										



Designer:	LAO
Company:	R&R Engineers-Surveyors
Date:	1/16/2024
Project:	Mayberry Filing 2A
Location:	El Paso County

Cells of this color are for required user-input Cells of this color are for optional user-input

$I_{100} = -2.52 \ln(D) + 12.735$

	STREET/			DIRE	CT RUNOFI	F				Т	OTAL RUNG	OFF		STREET	BYPASS		PIPE			TRAVE	L TIME		
DESGIN POINT	CONTRIBUTING	Basin Name	Area	Coeff	Тс	C*A	I	Q	Tc	Sum Area	Sum C*A	I	Q	Slope	Street Q	Design Q	Slope	PIPE	L	VEL	Tt	Q add'l	Remarks
	DASINS		(ac)	С	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	%	cfs	cfs	%	SIZE	ft	ft/sec	min		
		D1.14	0.91	0.66	12.0	0.60	6.47	3.88															
5B	D1.14								12.0	0.91	0.60	6.47	3.88										
		D1.13	3.07	0.81	9.4	2.49	7.08	17.62															
7B	D1.13								9.4	3.07	2.49	7.08	17.62										
		D1.1	1.73	0.88	6.6	1.52	8.00	12.18															
7C	D1.1								6.6	1.73	1.52	8.00	12.18										
		Sidewalk																					
		Chase	1.15	0.90	6.6	1.04	7.97	8.25															
1cc	Sidewalk Chase								6.6	1.15	1.04	7.97	8.25										



APPENDIX B - HYDRAULIC COMPUTATIONS

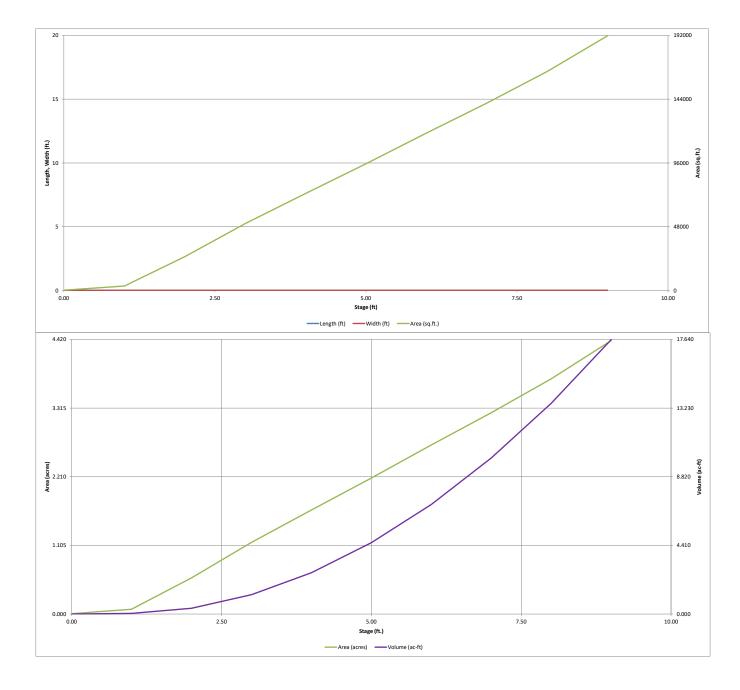
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

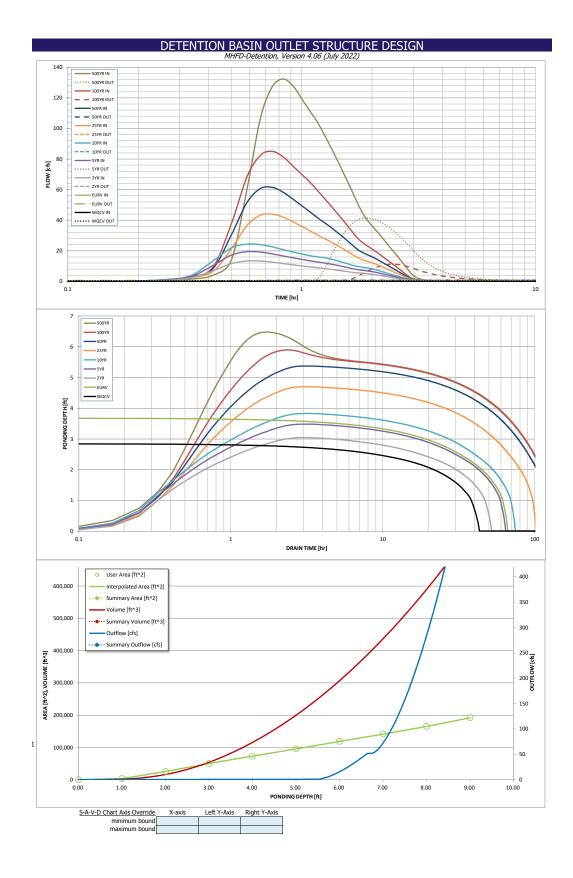
P	MAYPERRY		MHF	D-Detention, Versio	on 4.06 (Jul	v 2022)							
	MAYBERRY INTERIM D		POND D										
(ZONE 3	<u>,</u> ,												
	ÓNE 1												
						_							
ZONE	1 AND 2	100-YE ORIFIC	AR CE	Depth Increment =		ft	r	r	r			r	
POX Example Zone C	CES	n Retentio	on Pond)	Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volu
			λ'	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac
Watershed Information		1)	Top of Micropool		0.00				170	0.004		
Selected BMP Type =	EDB	-	1	6027		1.00				3,344	0.077	1,757	0.0
Watershed Area = Watershed Length =	100.20 2,867	acres ft	ノ	6028 6029		2.00 3.00				25,396 50,286	0.583 1.154	16,127 53,968	0.3
Watershed Length to Centroid =	1,433	ft)	6030		4.00				72,956	1.675	115,589	2.6
Watershed Slope =	0.010	ft/ft	4	6031		5.00				95,393	2.190	199,763	4.5
Watershed Imperviousness =	23.00%	percent	7	6032		6.00				118,525	2.721	306,722	7.0
Percentage Hydrologic Soil Group A =	100.0%	percent)	6033		7.00				141,085	3.239	436,527	10.0
Percentage Hydrologic Soil Group B =	0.0%	percent	イ	6034		8.00				164,866	3.785	589,503	13.5
Percentage Hydrologic Soil Groups C/D = Target WQCV Drain Time =	0.0%	percent hours	2	6035		9.00				191,669	4.400	767,770	17.0
Location for 1-hr Rainfall Depths =		nours	-) -)										
Afts: providing required pouts stove in		rainfa	1	Inclu	doe d		boad						
depths, click 'Run CUMP' to generate rune	off nydrograpi	ns using				ever	peq						
the embedded Colorado Urban Hydro		-	Optional User Overrides	Filing	12A								
Water Quality Capture Volume (WQCV) =	1.065	acre-feet	acre-feet				1						
Excess Urban Runoff Volume (EURV) = 2-yr Runoff Volume (P1 = 1.19 in.) =	2.138	acre-feet acre-feet	acre-feet 1.19 inches										
5-yr Runoff Volume (P1 = 1.19 iii.) =	1.404	acre-feet	1.19 inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	2.522	acre-feet	1.75 inches										
25-yr Runoff Volume (P1 = 2 in.) =	4.117	acre-feet	2.00 inches										
50-yr Runoff Volume (P1 = 2.25 in.) =	5.623	acre-feet	2.25 inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	7.666 12.108	acre-feet	2.52 inches 3.14 inches										
500-yr Runoff Volume (P1 = 3.14 in.) = Approximate 2-yr Detention Volume =	12.108	acre-feet acre-feet	3.14 inches										
Approximate 5-yr Detention Volume =	1.785	acre-feet											
Approximate 10-yr Detention Volume =	2.259	acre-feet											
Approximate 25-yr Detention Volume =	2.902	acre-feet											
Approximate 50-yr Detention Volume =	3.440	acre-feet											
Approximate 100-yr Detention Volume =	4.428	acre-feet											
Define Zones and Basin Geometry													
Zone 1 Volume (WQCV) =	1.065	acre-feet											
Zone 2 Volume (EURV - Zone 1) =	1.073	acre-feet											
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	2.823	acre-feet											
Total Detention Basin Volume =	4.961	acre-feet											
Initial Surcharge Volume (ISV) = Initial Surcharge Depth (ISD) =	user	ft ³ ft											
Total Available Detention Depth $(H_{total}) =$	user	ft											
Depth of Trickle Channel (H _{TC}) =	user	ft											
Slope of Trickle Channel (S_{TC}) =	user	ft/ft											
Slopes of Main Basin Sides (S _{main}) =	user	H:V											
Basin Length-to-Width Ratio ($R_{L/W}$) =	user												
Initial Surcharge Area (A _{ISV}) =	user	ft ²											
Surcharge Volume Length (L_{ISV}) =		ft											
Surcharge Volume Width (W_{ISV}) =	user	ft											
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft											
Length of Basin Floor $(L_{FLOOR}) =$		ft											
Width of Basin Floor (W_{FLOOR}) = Area of Basin Floor (A_{FLOOR}) =	user	ft ft ²											
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³											
Depth of Main Basin (H _{MAIN}) =	user	ft											
Length of Main Basin $(L_{MAIN}) =$	user	ft											
Width of Main Basin (W_{MAIN}) =	user	ft											
Area of Main Basin (A _{MAIN}) =	user	ft ²											
Volume of Main Basin (V_{MAIN}) = Calculated Total Basin Volume (V_{total}) =	user user	ft ³ acre-feet											
	4301	acre reet											
				-									
										1		1	<u> </u>

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



		TENTION				STON			
Project:	MAYBERRY FILING	M		CLET STRU Version 4.06 (July 2		SIGN			
Basin ID:	INTERIM DETENTI	ON POND D							
ZONE 3 ZONE 2 ZONE 2	_			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
VOLUME EURV WQCV			Zone 1 (WQCV)	2.85	1.065	Orifice Plate			
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	3.68	1.073	Orifice Plate			
PERMANENT ORIFICES	Danfinunstian (Data	ation Dend)	Z3 (100+1/2WQCV)	5.17	2.823	Weir&Pipe (Restrict)			
	Configuration (Rete			Total (all zones)	4.961				
Jser Input: Orifice at Underdrain Outlet (typically								ters for Underdrain	
Underdrain Orifice Invert Depth =		-	the filtration media s	surface)		drain Orifice Area =	N/A	ft ²	
Underdrain Orifice Diameter =	N/A	inches			Underdrai	n Orifice Centroid =	N/A	feet	
Iser Input: Orifice Plate with one or more orifice	s or Elliptical Slot W	eir (typically used to	drain WOCV and/o	r FLIRV in a sedime	ntation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =		1	bottom at Stage =			fice Area per Row =	N/A	ft ²	
Depth at top of Zone using Orifice Plate =			bottom at Stage =		-	iptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	14.40	inches			Ellipt	tical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			E	Elliptical Slot Area =	N/A	ft ²	
Iser Input: Stage and Total Area of Each Orifice	· ·	-	i		Dam 5 (11 11	Dame C (D7.4	Daw 0 (1
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	-
Stage of Orifice Centroid (ft)		1.20	2.40						1
Orifice Area (sq. inches)	4.00	4.00	4.00						J
Stage of Orifice Centroid (ft)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Orifice Area (sq. inches)									1
,									1
ser Input: Vertical Orifice (Circular or Rectangu							Calculated Parame	ters for Vertical Orif	ice
	Not Selected	Not Selected					Not Selected	Not Selected	
Invert of Vertical Orifice =		N/A		bottom at Stage =		rtical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice = Vertical Orifice Diameter =		N/A N/A	ft (relative to basin inches	bottom at Stage =	0 ft) Vertica	al Orifice Centroid =	N/A	N/A	feet
]						
Jser Input: Overflow Weir (Dropbox with Flat or			ngular/Trapezoidal \	Weir and No Outlet	Pipe)			ters for Overflow W	eir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	5.50	N/A N/A	ft (relative to basin t feet	bottom at Stage = 0 f		te Upper Edge, $H_t =$ Veir Slope Length =	5.50 6.00	N/A N/A	feet feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope =		N/A	H:V	G		00-yr Orifice Area =	6.46	N/A N/A	ieet
Horiz. Length of Weir Sides =		N/A	feet		verflow Grate Open		29.23	N/A	ft ²
Overflow Grate Type =		N/A			Overflow Grate Ope		14.62	N/A	ft ²
Debris Clogging % =	50%	N/A	%						-
ser Input: Outlet Pipe w/ Flow Restriction Plate			tangular Orifice)						
	Zone 3 Restrictor	Not Selected			<u>C</u>	alculated Parameter			<u>ite</u>
Depth to Invert of Outlet Pipe =			-				Zone 3 Restrictor	Not Selected	I
		N/A		asin bottom at Stage	= 0 ft) O	outlet Orifice Area =	Zone 3 Restrictor 4.53	Not Selected N/A	ft²
Outlet Pipe Diameter =	36.00		inches		= 0 ft) O Outle	outlet Orifice Area = et Orifice Centroid =	Zone 3 Restrictor 4.53 1.04	Not Selected N/A N/A	ft² feet
	36.00	N/A			= 0 ft) O Outle	outlet Orifice Area =	Zone 3 Restrictor 4.53	Not Selected N/A	ft²
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	36.00 22.00	N/A	inches		= 0 ft) O Outle	outlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe =	Zone 3 Restrictor 4.53 1.04	Not Selected N/A N/A N/A	ft² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	36.00 22.00	N/A N/A	inches	Half-Cen	= 0 ft) O Outle Itral Angle of Restric	outlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe =	Zone 3 Restrictor 4.53 1.04 1.79	Not Selected N/A N/A N/A	ft ² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Iser Input: Emergency Spillway (Rectangular or	36.00 22.00 <u>Trapezoidal)</u> 6.75	N/A N/A	inches inches	Half-Cen	= 0 ft) O Outle htral Angle of Restric Spillway [Putlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe =	Zone 3 Restrictor 4.53 1.04 1.79 <u>Calculated Parame</u>	Not Selected N/A N/A N/A ters for Spillway	ft² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage=	36.00 22.00 Trapezoidal) 6.75 50.00	N/A N/A	inches inches	Half-Cen	= 0 ft) O Outle ttral Angle of Restric Spillway [Stage at	butlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth=	Zone 3 Restrictor 4.53 1.04 1.79 <u>Calculated Parame</u> 0.65	Not Selected N/A N/A N/A ters for Spillway feet	ft ² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00	N/A N/A ft (relative to basin feet	inches inches	Half-Cen	= 0 ft) O Outle Itral Angle of Restric Spillway [Stage at Basin Area at	utlet Orifice Area = tt Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard =	Zone 3 Restrictor 4.53 1.04 1.79 <u>Calculated Parame</u> 0.65 8.40	Not Selected N/A N/A N/A ters for Spillway feet feet	ft² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00	N/A N/A ft (relative to basin feet H:V	inches inches	Half-Cen	= 0 ft) O Outle Itral Angle of Restric Spillway [Stage at Basin Area at	Putlet Orifice Area = tt Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	Zone 3 Restrictor 4.53 1.04 1.79 <u>Calculated Parame</u> 0.65 8.40 4.03	Not Selected N/A N/A N/A ters for Spillway feet feet acres	ft² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00	N/A N/A ft (relative to basin feet H:V feet	inches inches bottom at Stage =	Half-Cen 0 ft)	= 0 ft) O Outle htral Angle of Restrict Spillway [Stage at Basin Area at Basin Volume at	Putlet Orifice Area = tt Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	Zone 3 Restrictor 4.53 1.04 1.79 <u>Calculated Parame</u> 0.65 8.40 4.03 15.10	Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft	ft² feet
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Stopes = Freeboard above Max Water Surface = outed Hydrograph Results Design Storm Return Period =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00	N/A N/A ft (relative to basin feet H:V feet ide the default CU/h EURV	inches inches bottom at Stage = IP hydrographs and 2 Year	Half-Cen 0 ft) runoff volumes by e 5 Year	= 0 ft) O Outle atral Angle of Restric Spillway [Stage at Basin Area at Basin Volume at entering new values 10 Year	butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydroo</i> 25 Year	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year	Not Selected N/A N/A N/A ters for Spillway feet feet acres acres acre-ft 100 Year	ft ² feet radians
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = outed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overn WQCV N/A	N/A N/A ft (relative to basin feet H:V feet ide the default CUh EURV N/A	inches inches bottom at Stage = <i>IP hydrographs and</i> <u>2 Year</u> 1.19	Half-Cen 0 ft) runoff volumes by e 5 Year 1.50	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at <u>entering new values</u> 10 Year 1.75	butlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>in the Inflow Hydro</u> 25 Year 2.00	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25	Not Selected N/A N/A N/A feet feet acres acre-ft 100 Year 2.52	ft ² feet radians 500 Yeau 3.14
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Stopes = Freeboard above Max Water Surface = outed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00	N/A N/A ft (relative to basin feet H:V feet ide the default CU/h EURV	inches inches bottom at Stage = IP hydrographs and 2 Year	Half-Cen 0 ft) runoff volumes by e 5 Year	= 0 ft) O Outle atral Angle of Restric Spillway [Stage at Basin Area at Basin Volume at entering new values 10 Year	butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydroo</i> 25 Year	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year	Not Selected N/A N/A N/A ters for Spillway feet feet acres acres acre-ft 100 Year	ft ² feet radians 500 Yea 3.14 12.108 12.108
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = outed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acreft) = Inflow Hydrograph Volume (acreft) = CUHP Predevelopment Peak Q (cfs) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overn WQCV N/A 1.065 N/A N/A	N/A N/A N/A ft (relative to basin feet H:V feet EURV N/A 2.138 N/A N/A	inches inches bottom at Stage = //P hydrographs and 2 Year 1.19 1.404	Half-Cen 0 ft) <u>runoff volumes by e</u> <u>5 Year</u> <u>1.50</u> <u>1.992</u>	= 0 ft) O Outle Utral Angle of Restrict Spillway (D Stage at Basin Area at Basin Volume at Entering new values 10 Year 1.75 2.522	butlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>in the Inflow Hydro</u> <u>25 Year</u> 2.00 4.117	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623	Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 7.666	ft ² feet radians 500 Yeaa 3.14 12.108
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Outlet Alundor Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Rundf Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Prodevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overr WQCV N/A N/A N/A N/A	N/A N/A N/A ft (relative to basin feet H:V feet EURV N/A 2.138 N/A N/A N/A	inches inches bottom at Stage = <i>IP hydrographs and</i> 2 Year 1.19 1.404 1.404 0.6	Half-Cen 0 ft) <u>runoff volumes by e</u> <u>5 Year</u> <u>1.50</u> <u>1.992</u> <u>1.992</u> <u>1.2</u>	= 0 ft) O Outle atral Angle of Restric Spillway [Stage at Basin Area at Basin Volume at entering new values 10 Year 1.75 2.522 2.522 1.7	butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydroo</i> 4.117 4.117 15.6	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623 5.623 3.1.3	Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 7.666 7.666 51.8	ft ² feet radians <u>500 Yea</u> <u>3.14</u> 12.108 <u>94.2</u>
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = outled Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Prodevelopment Peak Q (cfs) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overnow WQCV N/A N/A N/A N/A N/A N/A	N/A N/A N/A ft (relative to basin feet H:V feet EURV N/A 2.138 N/A N/A	inches inches bottom at Stage = Phydrographs and 2 Year 1.19 1.404 1.404	Half-Cen 0 ft) <u>runoff volumes by e</u> <u>5 Year</u> <u>1.50</u> <u>1.992</u>	= 0 ft) O Outle traal Angle of Restric Spillway [Stage at Basin Area at Basin Volume at <u>entering new values</u> 10 Year 1.75 2.522 2.522	butlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = In the Inflow Hydrog 25 Year 2.00 4.117	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623 5.623	Not Selected N/A N/A N/A feet feet acres acre-ft 100 Year 2.52 7.666 7.666	ft ² feet radians 500 Year 3.14 12.108 12.108
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Outlet Aunof Volume (acreft) = CUHP Runoff Volume (acreft) = Predevelopment Paek Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overry WQCV N/A N/A N/A N/A N/A N/A N/A O.5	N/A N/A N/A If (relative to basin feet H:V feet <i>ide the default CUh</i> EURV N/A 2.138 N/A N/A N/A N/A N/A N/A N/A O.6	Inches Inches bottom at Stage = 1.19 1.404 1.404 0.6 0.01 13.3 0.5	Half-Cen 0 ft)	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at Intering new values 10 Year 1.75 2.522 2.522 1.7 0.02 24.4 0.6	butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydro</i> 25 Year 2.00 4.117 4.117 15.6 0.16 4.3.9 0.7	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 yraphs table (Colun 50 Year 2.25 5.623 31.3 0.31 61.4 0.8	Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 7.666 51.8 0.52 85.0 11.2	500 Yea radians 3.14 12.108 94.2 0.94 13.2.3 41.4
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Ends Slopes = Spillway End Slopes = Freeboard above Max Water Surface = Executed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CHHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Unflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overn WQCV N/A 1.065 N/A	N/A N/A N/A ft (relative to basin feet H:V feet EURV N/A 2.138 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Inches inches bottom at Stage = 1.19 1.404 1.404 0.6 0.01 13.3 0.5 N/A	Half-Cen 0 ft)	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at Intering new values 2.522 2.522 1.7 0.02 24.4 0.6 0.4	butlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydro</i> 25 Year 2.00 4.117 4.117 15.6 0.16 43.9 0.7 0.0	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623 5.623 3.13 	Not Selected N/A N/A N/A Inters for Spillway feet acres acre-ft 100 Year 2.52 7.666 7.666 51.8 0.52 85.0 11.2 0.2	500 Yea radians 3.14 12.108 94.2
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Cuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) CUHP Profedevelopment Peak Q (cfs) = CUHP Profedevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs)	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overn WQCV N/A	N/A N/A N/A If (relative to basin feet H:V feet <i>ide the default CUh</i> EURV N/A 2.138 N/A N/A N/A N/A N/A N/A N/A O.6	Inches Inches bottom at Stage = 1.19 1.404 1.404 0.6 0.01 13.3 0.5	Half-Cen 0 ft)	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at Intering new values 10 Year 1.75 2.522 2.522 1.7 0.02 24.4 0.6	butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydro</i> 200 4.117 4.117 15.6 0.16 4.3.9 0.7	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 yraphs table (Colun 50 Year 2.25 5.623 31.3 0.31 61.4 0.8	Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 7.666 51.8 0.52 85.0 11.2	500 Year radians 3.14 12.108 12.108 94.2 0.94 132.3 41.4 0.4
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Ser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Invert Stage= Spillway End Slopes = Freeboard above Max Water Surface = Entreboard above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Prodevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Unit Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fbs) = Max Velocity through Grate 1 (fbs) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can over N/A	N/A N/A N/A fet feet H:V feet EURV N/A 2.138 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	inches inches bottom at Stage = // hydrographs and 2 Year 1.19 1.404 0.6 0.01 13.3 0.5 N/A Plate N/A N/A	Half-Cen 0 ft)	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at Intering new values 2.522 2.522 1.7 0.02 24.4 0.6 0.4 Plate N/A N/A	butlet Orifice Area = the Orifice Centroid = the Orifice Centroid = the Orifice Centroid = Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 10 pof Free	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623 3.1.3 	Not Selected N/A N/A N/A feet feet acres acre-ft 100 Year 2.52 7.666 7.666 51.8 0.52 85.0 11.2 0.2 Overflow Weir 1 0.3 N/A	500 Year radians 3.14 12.108 12.108 94.2
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Spillway Invert Stage= Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Cuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Winder Volume (acre-ft) = CUHP Predevelopment Peak Q(cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q(cfs) = Ratio Peak Outflow to Predevelopment Q(cfs) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Tirme to Drain 97% of Inflow Volume (Aurs)	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overr WQCV N/A	N/A N/A N/A N/A feet H:V feet <i>ide the default CUh</i> feet N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	inches inches bottom at Stage = // <i>hydrographs and</i> 2 Year 1.19 1.404 1.404 0.6 0.01 13.3 0.5 N/A Plate N/A N/A 47	Half-Cen 0 ft)	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at entering new values 10 Year 1.75 2.522 2.522 1.7 0.02 24.4 0.6 0.4 0.6 0.4 0.6 0.4 0.6 0.6 0.7	butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydro</i> 25 Year 2.00 4.117 4.117 15.6 0.16 4.3.9 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 yraphs table (Colun 50 Year 2.25 5.623 3.1.3 0.31 61.4 0.8 0.0 Plate N/A N/A N/A 112	Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 7.666 51.8 0.52 85.0 11.2 0.2 Overflow Weir 1 0.3 N/A 118	500 Year radians 3.14 12.108 94.2 0.94 132.3 41.4 0.4 Dverflow We 14 N/A 113
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Jser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = CHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overnow WQCV N/A	N/A N/A N/A fet feet H:V feet EURV N/A 2.138 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	inches inches bottom at Stage = // hydrographs and 2 Year 1.19 1.404 0.6 0.01 13.3 0.5 N/A Plate N/A N/A	Half-Cen 0 ft)	= 0 ft) O Outle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at Intering new values 2.522 2.522 1.7 0.02 24.4 0.6 0.4 Plate N/A N/A	butlet Orifice Area = the Orifice Centroid = the Orifice Centroid = the Orifice Centroid = Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 10 pof Free	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623 3.1.3 	Not Selected N/A N/A N/A feet feet acres acre-ft 100 Year 2.52 7.666 7.666 51.8 0.52 85.0 11.2 0.2 Overflow Weir 1 0.3 N/A	500 Year radians 3.14 12.108 12.108 94.2 0.94 132.3 41.4 0.94 Verflow We 1.4 N/A
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Jser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = Om-Hour Rainfall Depth (in) = OHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs) = Predevelopment Unit Peak Flow, q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours)	36.00 22.00 Trapezoidal) 6.75 50.00 4.00 1.00 The user can overr WQCV N/A N/A	N/A N/A N/A N/A feet H:V feet EURV N/A 2.138 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Inches Inches bottom at Stage = <i>IP hydrographs and</i> 2 Year 1.19 1.404 1.404 0.6 0.01 13.3 0.5 N/A Plate N/A N/A 47 50	Half-Cen 0 ft) 7 Year 1.50 1.992 1.992 1.2 0.01 1.2 0.01 1.2 0.0 1.2 0.5 Plate N/A N/A 58 62	= 0 ft) O Outle Spillway I Stage at Basin Area at Basin Volume at Intering new values 2.522 2.522 1.7 0.02 24.4 0.6 0.4 Plate N/A N/A N/A 71	butlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <i>in the Inflow Hydro</i> 2.00 4.117 15.6 0.16 43.9 0.7 0.0 Plate N/A N/A 97	Zone 3 Restrictor 4.53 1.04 1.79 Calculated Parame 0.65 8.40 4.03 15.10 graphs table (Colum 50 Year 2.25 5.623 31.3 0.31 61.4 0.8 0.0 Plate N/A N/A N/A 112 119	Not Selected N/A N/A N/A N/A ters for Spillway feet acres acre-ft 100 Year 2.52 7.666 51.8 0.52 85.0 11.2 0.2 Overflow Weir 1 0.3 N/A 118 >120	500 Year 3.14 12.108 12.108 94.2 0.94 132.3 41.4 0.4 Vverflow We 1.4 N/A 1.13



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

[SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	ographs develop CUHP	CUHP	CUHP	CUHP
ime Interval	TIME								100 Year [cfs]	
		WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]		500 Year [cfs
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.01	0.19
	0:15:00	0.00	0.00	0.52	0.84	1.05	0.71	0.93	0.88	1.40
	0:20:00	0.00	0.00	2.21	3.02	3.61	2.32	2.77	2.90	3.93
	0:25:00	0.00	0.00	6.84	10.28	13.24	6.42	8.22	9.22	13.63
	0:30:00	0.00	0.00	11.56	17.17	21.81	21.20	30.19	37.45	60.06
		0.00	0.00	13.31	19.38	24.37	36.53	51.53	68.30	106.83
	0:40:00	0.00	0.00	13.29	19.14	24.06	43.28	60.70	82.43	127.49
	0:50:00	0.00	0.00	12.57 11.64	17.98 16.64	22.51 20.75	43.90 42.00	61.45 58.29	85.01 81.36	132.35 127.98
	0:55:00	0.00	0.00	10.85	15.49	19.26	38.96	53.86	75.47	119.59
	1:00:00	0.00	0.00	10.05	14.42	17.93	35.90	49.52	70.00	111.45
	1:05:00	0.00	0.00	9.52	14.42	16.79	33.17	45.60	65.06	104.31
	1:10:00	0.00	0.00	8.96	12.71	16.05	30.40	41.73	59.52	95.89
	1:15:00	0.00	0.00	8.42	12.03	15.46	27.99	38.44	54.32	87.69
	1:20:00	0.00	0.00	7.88	11.28	14.65	25.79	35.33	49.47	79.73
	1:25:00	0.00	0.00	7.34	10.49	13.59	23.60	32.22	44.70	71.79
	1:30:00	0.00	0.00	6.79	9.69	12.44	23.00	29.10	40.13	64.24
	1:35:00	0.00	0.00	6.27	8.93	11.32	19.25	26.03	35.71	56.97
	1:40:00	0.00	0.00	5.80	8.15	10.32	19.25	23.07	31.46	50.01
	1:45:00	0.00	0.00	5.49	7.60	9.69	15.30	20.46	27.72	44.02
	1:50:00	0.00	0.00	5.29	7.19	9.21	14.00	18.67	25.06	39.74
	1:55:00	0.00	0.00	5.01	6.80	8.75	13.02	17.30	23.03	36.32
	2:00:00	0.00	0.00	4.69	6.41	8.24	12.16	16.09	21.24	33.29
	2:05:00	0.00	0.00	4.29	5.88	7.55	11.14	14.71	19.36	30.22
	2:10:00	0.00	0.00	3.84	5.28	6.76	10.04	13.25	17.41	27.12
	2:15:00	0.00	0.00	3.41	4.68	5.99	8.96	11.81	15.51	24.13
	2:20:00	0.00	0.00	3.00	4.12	5.25	7.92	10.42	13.70	21.28
	2:25:00	0.00	0.00	2.62	3.58	4.55	6.93	9.09	11.97	18.58
	2:30:00	0.00	0.00	2.26	3.08	3.90	5.98	7.81	10.28	15.92
	2:35:00	0.00	0.00	1.91	2.59	3.29	5.05	6.56	8.62	13.31
	2:40:00	0.00	0.00	1.51	2.13	2.70	4.14	5.34	6.99	10.74
	2:45:00	0.00	0.00	1.26	1.69	2.14	3.27	4.15	5.39	8.22
	2:50:00	0.00	0.00	0.98	1.30	1.64	2.43	3.01	3.85	5.80
	2:55:00	0.00	0.00	0.77	1.02	1.32	1.68	2.01	2.50	3.79
	3:00:00	0.00	0.00	0.64	0.85	1.10	1.00	1.44	1.70	2.62
	3:05:00	0.00	0.00	0.54	0.72	0.93	0.94	1.11	1.26	1.90
	3:10:00	0.00	0.00	0.46	0.61	0.79	0.75	0.88	0.95	1.40
	3:15:00	0.00	0.00	0.39	0.51	0.67	0.61	0.71	0.74	1.04
	3:20:00	0.00	0.00	0.33	0.43	0.56	0.50	0.58	0.57	0.78
	3:25:00	0.00	0.00	0.28	0.36	0.47	0.41	0.47	0.44	0.57
	3:30:00	0.00	0.00	0.23	0.30	0.38	0.33	0.38	0.34	0.43
	3:35:00	0.00	0.00	0.19	0.24	0.31	0.27	0.30	0.28	0.35
	3:40:00	0.00	0.00	0.15	0.20	0.24	0.22	0.24	0.23	0.28
	3:45:00	0.00	0.00	0.12	0.15	0.19	0.17	0.19	0.18	0.22
	3:50:00	0.00	0.00	0.09	0.12	0.15	0.13	0.15	0.14	0.17
	3:55:00	0.00	0.00	0.07	0.09	0.11	0.10	0.11	0.10	0.13
	4:00:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.07	0.09
	4:05:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	4:10:00	0.00	0.00	0.02	0.03	0.03	0.03	0.03	0.03	0.03
	4:15:00	0.00	0.00	0.01	0.01	0.02	0.01	0.02	0.01	0.02
	4:20:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

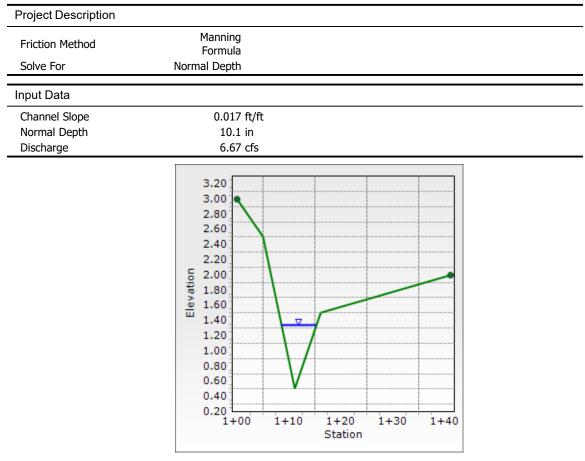
Worksheet for FILING 2A 5-YEAR

Project Description				
Fristian Mathed	Manning			
Friction Method	Formula			
Solve For	Normal Depth			
Input Data				
Channel Slope	0.017 ft/ft			
Discharge	6.67 cfs			
	Se	ction Definitions		
Stati			Elevation	
(ft)		(ft)	
		1+00		3.00
		1+05		2.50
		1+11		0.50
		1+16 1+41		1.50
		1+41		2.00
	Roughne	ss Segment Definitions		
Start Station		Ending Station	Roughness Coefficient	
(1+00, 3.00)		(1+41, 2.00)	-	0.045
Options				
Current Roughness Weighted Method	Pavlovskii's Method			
Open Channel Weighting Method	Pavlovskii's Method			
Closed Channel Weighting	Pavlovskii's			
Method	Method			
Results				
Normal Depth	10.1 in			
Roughness Coefficient	0.045			
Elevation	1.34 ft			
Elevation Range	0.5 to 3.0 ft			
Flow Area	2.8 ft ²			
Wetted Perimeter	6.9 ft			
Hydraulic Radius	4.9 in			
Top Width	6.72 ft			
Normal Depth	10.1 in			
Critical Depth	8.4 in			
Critical Slope	0.044 ft/ft			
Velocity	2.36 ft/s			
Velocity Head	0.09 ft			
Specific Energy	0.93 ft			
Froude Number	0.643			
Flow Type	Subcritical			

Untitled1.fm8 9/25/2023 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 FlowMaster [10.03.00.03] Page 1 of 2

GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	10.1 in	
Critical Depth	8.4 in	
Channel Slope	0.017 ft/ft	
Critical Slope	0.044 ft/ft	

Worksheet for FILING 2A 5-YEAR



Cross Section for FILING 2A 5-YEAR

Worksheet for FILING 2A 100-YEAR

Project Description				
Friction Method	Manning			
	Formula			
Solve For	Normal Depth			
Input Data				
Channel Slope	0.017 ft/ft			
Discharge	12.18 cfs			
	Se	ction Definitions		
Stati	ion		Elevation	
(ft			(ft)	
		1+00		3.00
		1+05		2.50
		1+11		0.50
		1+16		1.50
		1+41		2.00
	Roughne	ss Segment Definitions		
Start Station	-	Ending Station	Roughness Coefficient	
(1+00, 3.00)		(1+41, 2.00)	Roughness coemcient	0.045
(1,00,000)		(1 + 11/ 2100)		010 10
Options				
Current Roughness Weighted Method	Pavlovskii's			
Open Channel Weighting	Method Pavlovskii's			
Method	Method			
Closed Channel Weighting	Pavlovskii's			
Method	Method			
Results				
Normal Depth	13.6 in			
Roughness Coefficient	0.045			
Elevation	1.64 ft			
Elevation Range	0.5 to 3.0 ft			
Flow Area	5.6 ft ²			
Wetted Perimeter	15.5 ft			
Hydraulic Radius	4.3 in			
Top Width	15.26 ft			
Normal Depth	13.6 in			
Critical Depth	10.7 in			
Critical Slope	0.040 ft/ft			
Velocity	2.18 ft/s			
Velocity Head	0.07 ft			
Specific Energy	1.21 ft			
Froude Number	0.634			
Flow Type	Subcritical			

Untitled1.fm8 9/25/2023 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 FlowMaster [10.03.00.03] Page 1 of 2

GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	13.6 in	
Critical Depth	10.7 in	
Channel Slope	0.017 ft/ft	
Critical Slope	0.040 ft/ft	

Worksheet for FILING 2A 100-YEAR

Project Description					
Friction Method Solve For	Manning Formula Normal Depth				
501761101	Normal Depth				
Input Data					
Channel Slope Normal Depth Discharge	0.017 ft/ft 13.6 in 12.18 cfs				
	3.20 3.00 2.80 2.40 2.20 5 2.00 1.80 1.60 1.40 1.20 1.00 0.80 0.60 0.40 0.20 1+00	1+10	1+20 Station	1+30	1+40

Cross Section for FILING 2A 100-YEAR

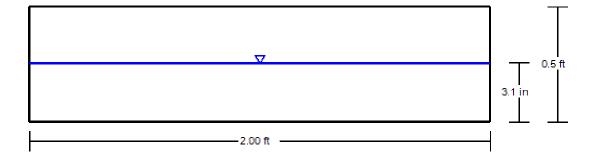
Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.030 ft/ft	
Height	0.5 ft	
Bottom Width	2.00 ft	
Discharge	4.54 cfs	
Results		
Normal Depth	3.1 in	
Flow Area	0.5 ft ²	
Wetted Perimeter	2.5 ft	
Hydraulic Radius	2.3 it	
Top Width	2.00 ft	
Critical Depth	6.0 in	
Percent Full	51.0 %	
Critical Slope	0.003 ft/ft	
Velocity	8.90 ft/s	
Velocity Head	1.23 ft	
Specific Energy	1.49 ft	
Froude Number	3.106	
Discharge Full	8.80 cfs	
Slope Full	0.030 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
·		
Downstream Depth	0.0 in	
Length Number Of Stone	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	51.0 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	3.1 in	
Critical Depth	6.0 in	
Channel Slope	0.030 ft/ft	
Critical Slope	0.003 ft/ft	

Worksheet for Sidewalk Chase (5-YEAR)

Untitled1.fm8 1/11/2024 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.030 ft/ft	
Normal Depth	3.1 in	
Height	0.5 ft	
Bottom Width	2.00 ft	
Discharge	4.54 cfs	

Cross Section for Sidewalk Chase (5-YEAR)





Untitled1.fm8 1/11/2024 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.030 ft/ft	
Height	0.5 ft	
Bottom Width	2.00 ft	
Discharge	8.25 cfs	
Results		
Normal Depth	4.6 in	
Flow Area	0.8 ft ²	
Wetted Perimeter	2.8 ft	
Hydraulic Radius	3.3 in	
Top Width	2.00 ft	
Critical Depth	6.0 in	
Percent Full	75.9 %	
Critical Slope	0.006 ft/ft	
Velocity	10.88 ft/s	
Velocity Head	1.84 ft	
Specific Energy	2.22 ft	
Froude Number	3.114	
Discharge Full	8.80 cfs	
Slope Full	0.030 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.00 %	
Normal Depth Over Rise	75.9 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	4.6 in	
Critical Depth	6.0 in	
Channel Slope	0.030 ft/ft	
Critical Slope	0.006 ft/ft	

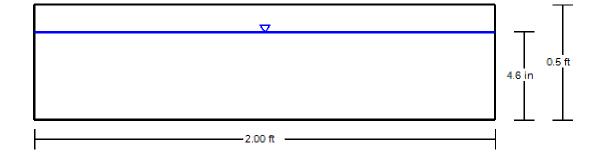
Worksheet for Sidewalk Chase (100-YEAR)

Sidewalk Chase.fm8 1/16/2024

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.030 ft/ft	
Normal Depth	4.6 in	
Height	0.5 ft	
Bottom Width	2.00 ft	
Discharge	8.25 cfs	

Cross Section for Sidewalk Chase (100-YEAR)

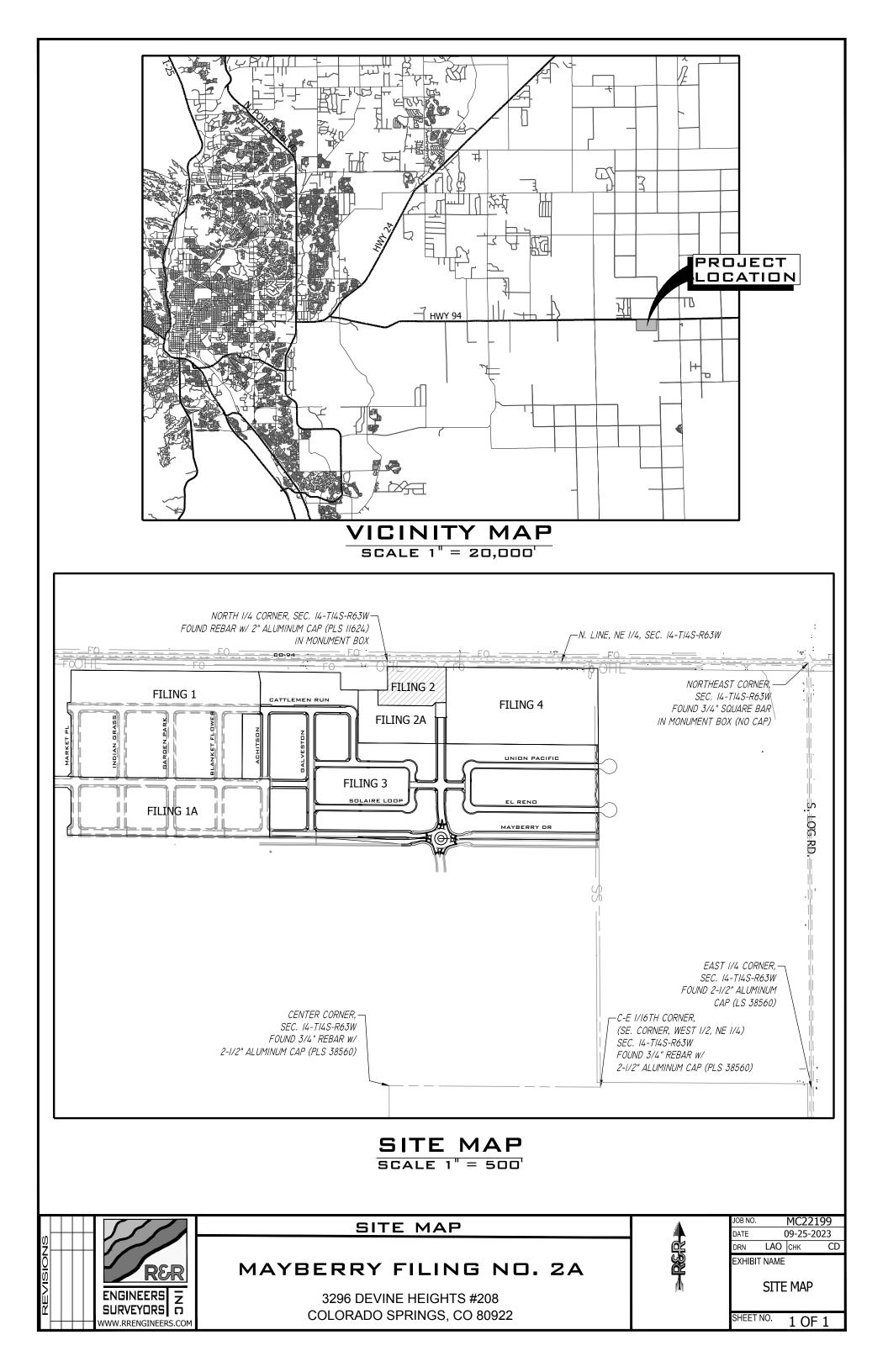


V: 1 \(\begin{bmatrix} H: 1 \\ H: 1 \end{bmatrix} \)

Sidewalk Chase.fm8 1/16/2024

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

APPENDIX C – REFERENCE INFORMATION





ENGINEER'S OPINION OF PROBABLE COSTS FOR Mayberry Filing 2A - Drainage Improvements

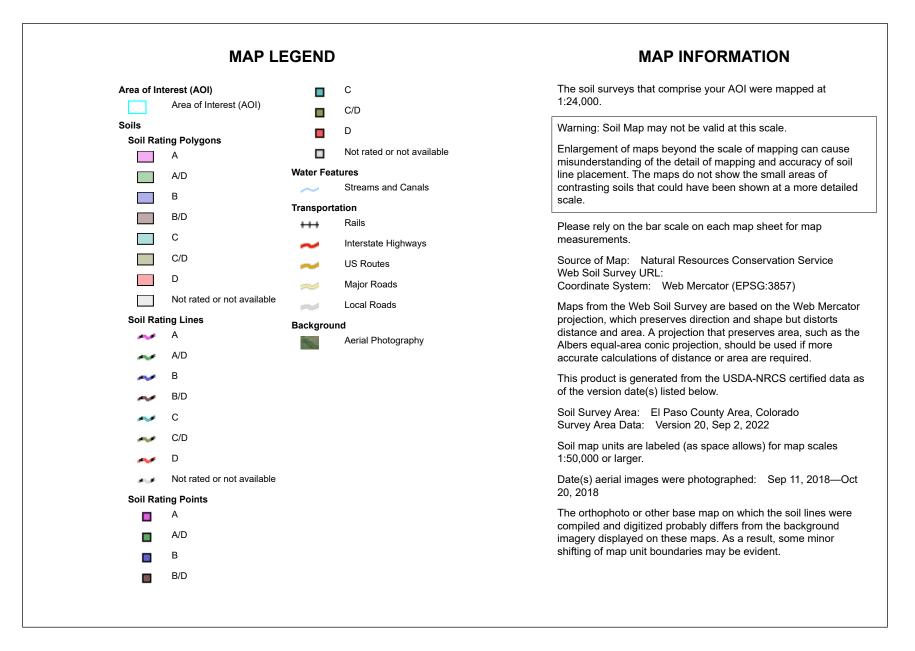
Item	Description	Total Work Units	Unit Price (\$)	Total Cost (\$)
Riprap		0 Ton	97.00 Ton	0.00
18" RCP		0 LF \$		\$ 0.00
24" RCP		0 LF \$	91.00 LF	\$ 0.00
30" RCP		0 LF \$	114.00 LF	\$ 0.00
60" RCP		0 LF \$	348.00 LF	\$ 0.00
5' Type R		0 EA \$	6,703.00 EA	\$ 0.00
Storm Manhole		0 EA \$	7,734.00 EA	\$ 0.00
24" FES		1 EA \$	546.00 EA	\$ 546.00
60" FES		0 EA \$	2,088.00 EA	\$ 0.00
Grass Channels		0.22 AC \$	1,520.00 EA	\$ 334.40
SUBTOTAL				\$ 546.00
Contingency (15%)				\$ 81.90
TOTAL				\$ 627.90



Natural Resources

Conservation Service

Web Soil Survey National Cooperative Soil Survey





Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	1.2	23.2%
95	Truckton loamy sand, 1 to 9 percent slopes	A	3.9	76.8%
Totals for Area of Interest		5.0	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

USDA

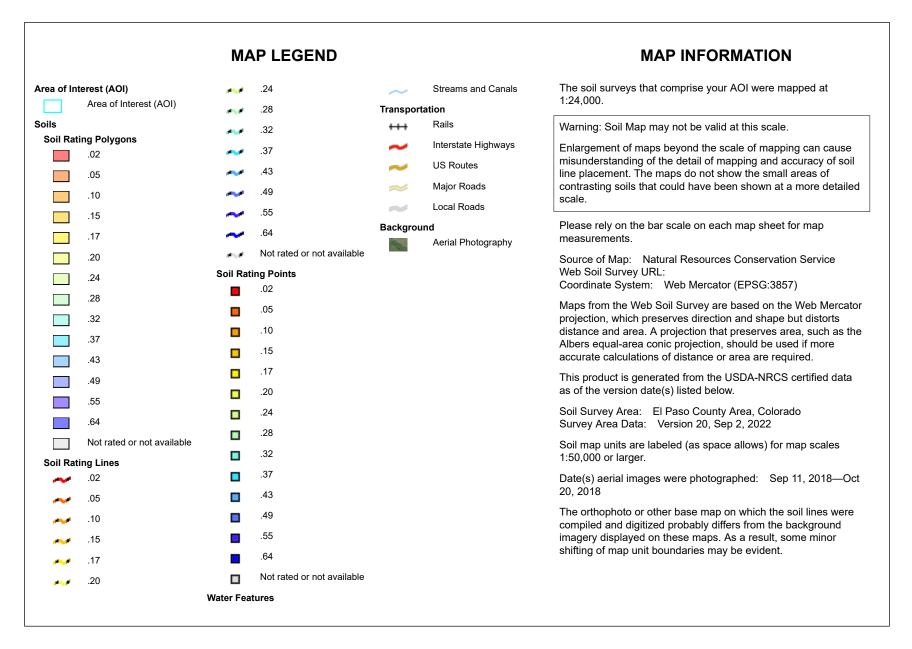
Component Percent Cutoff: None Specified Tie-break Rule: Higher





USDA Natural Resources

Conservation Service



K Factor, Whole Soil

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	.10	1.2	23.2%
95	Truckton loamy sand, 1 to 9 percent slopes	.24	3.9	76.8%
Totals for Area of Interest			5.0	100.0%

Description

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Factor K does not apply to organic horizons and is not reported for those layers.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher Layer Options (Horizon Aggregation Method): Surface Layer (Not applicable)

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum** of **1988** (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services

NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center** (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

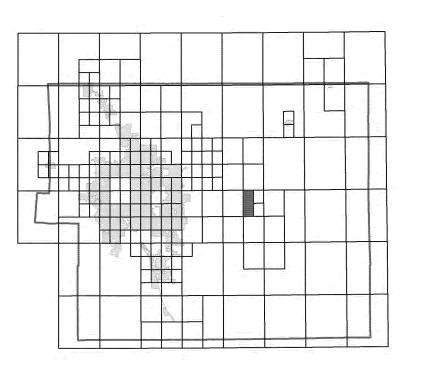
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

Flooding Source

El Paso County Vertical Datum Offset Table Vertical Datum

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

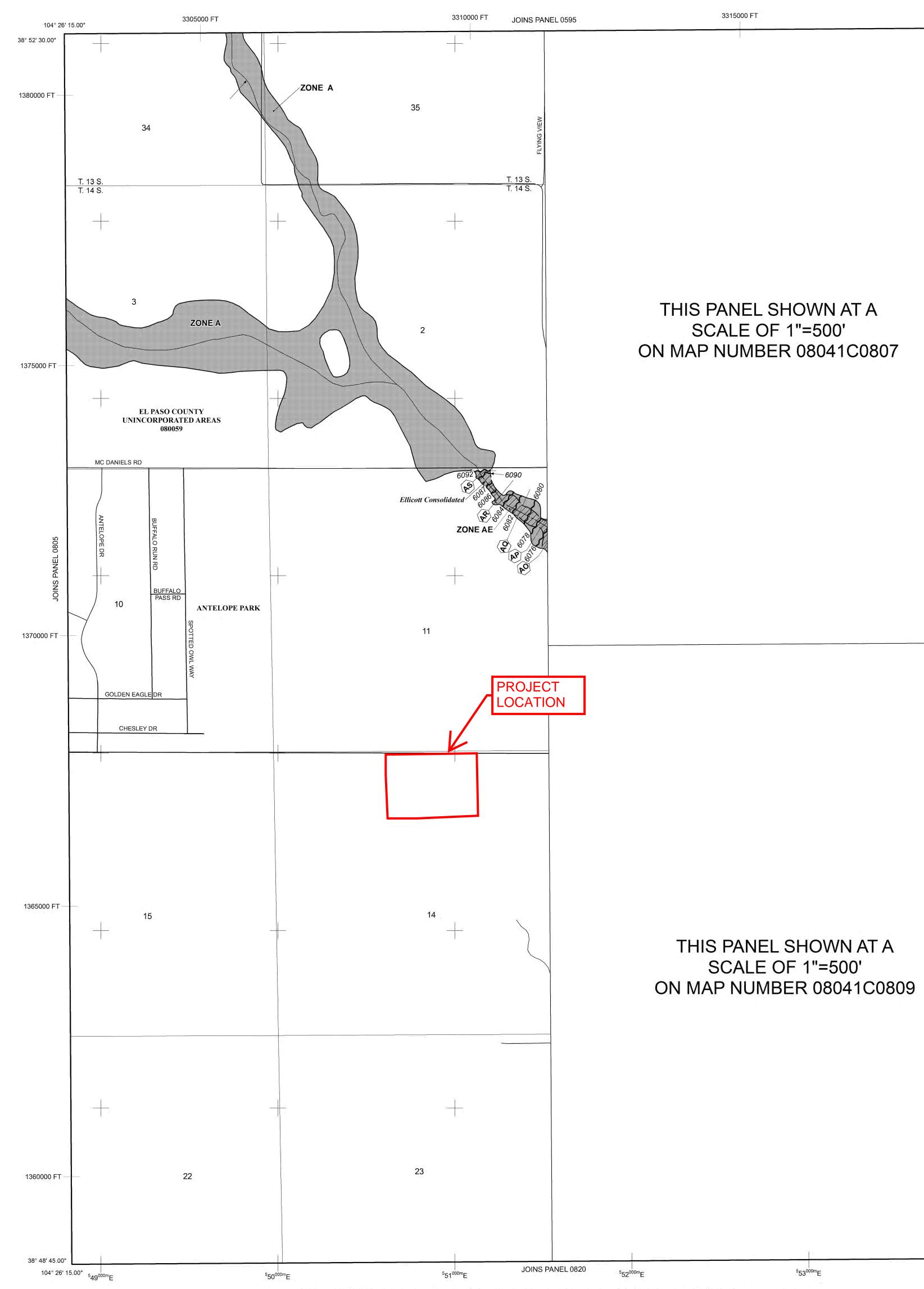
Panel Location Map



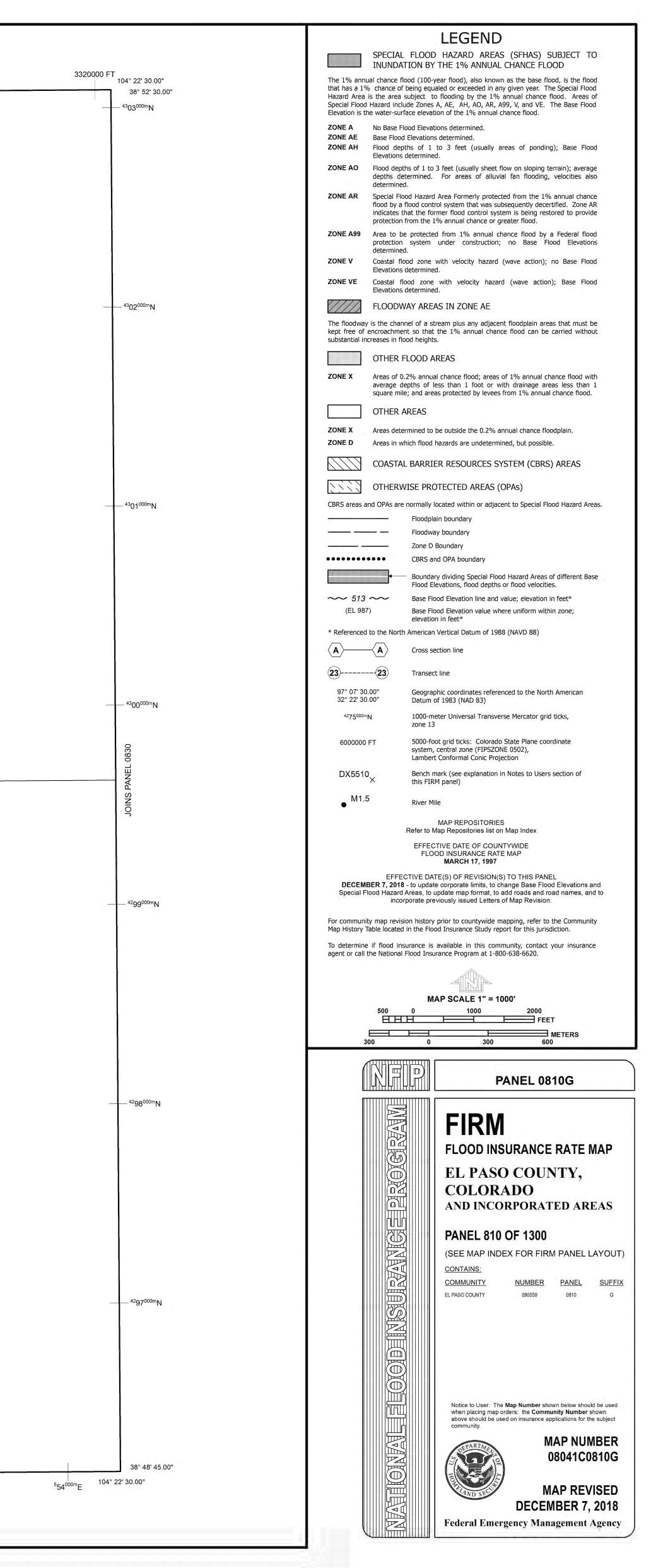
This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 13 SOUTH, RANGE 63 WEST, AND TOWNSHIP 14 SOUTH, RANGE 63 WEST.





FINAL DRAINAGE REPORT

For

MAYBERRY, COLORADO SPRINGS – FILING NO. 3

PREPARED FOR:

COLORADO SPRINGS MAYBERRY, LLC 3296 DEVINE HEIGHTS #208 COLORADO SPRINGS, CO 80922

PREPARED BY:

R & R ENGINEERS - SURVEYORS, INC. 1635 W. 13[™] AVE, SUITE 310 DENVER, CO 80204 CONTACT: CLIF DAYTON, P.E. (303) 753-6730

> R&R JOB #MC22110 EPC PROJECT NO. SF2219

ORIGINAL SUBMITTAL: MAY 2022 2ND SUBMITTAL: SEPTEMBER 2022 3RD SUBMITTAL: JANUARY 2023 4TH SUBMITTAL: APRIL 2023

1635 West 13th Avenue - Suite 310, Denver, Colorado 80204 Phone - (303) 753-6730 Fax - (303) 753-6568

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for liability caused by negligent acts, errors or omissions on my part in preparing this report.



SIGNATURE:

Clif Davton, P.E. Registered Professional Engineer State of Colorado No. 51674

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

SIGNATURE:

John Mick Colorado Springs Mayberry, LLC 3296 Devine Heights #208 Colorado Springs, CO 80922

EL PASO COUNTY'S STATEMENT:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2, and Engineering Criteria Manual as amended.



Joshua Palmer, P.E. County Engineer/ECM Administrator respectively.

Sub-basin C2.5 is a 9.61 acre onsite area that is collected by a curb inlet in Mayberry Drive. This basin consists of single family lots and a portion of Solaire Loop, Galveston Terrace, Cattlemen Run, Achison Way, and Village Main Street. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 14.2 and 34.6 cfs respectively.

Sub-basin C3.0* is a 35.40 acre basin south of the Filing 3 development. The basin was analyzed for future development and assumed to comprise both single family lots and park area. During the interim condition the basin will be undeveloped with part of the basin bypassing Pond D following existing drainage patterns. Once fully developed, the entire basin will ultimately drain to Pond D via future storm sewer improvements. The 5 year and 100 year developed peak flows are 22 and 72.7 cfs respectively.

***C3.0** was also analyzed using an interim condition that represents the runoff patterns prior to development. Under this condition the basin would flow southeast and southwest into Channel C2, ultimately discharging into Pond D. The 5 year and 100 year undeveloped peak flows are 7.4 and 54.4 cfs respectively.

Sub-basin D1.1 is a 1.73 acre basin comprising commercial lots of Filing 2. The basin was analyzed for future development of Filing 2. The developed basin will drain via a swale along the southern Filing 2 boundary and enter the Springs Road storm system via a flared end section. The 5 year and 100 year developed peak flows are 6.7 and 12.2 cfs respectively.

Sub-basin D1.2 is a 2.56 acre basin comprising single family lots and portions of Solaire Loop and Besseyi Way. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet on the south side of Besseyi Way, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 3.4 and 8.3 cfs respectively.

Sub-basin D1.3 is a 2.02 acre basin comprising single family lots and portions of Union Pacific Way and El Reno Way. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet on the north side of El Reno Way, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 3.1 and 7.5 cfs respectively.

Sub-basin D1.4 is a 3.75 acre basin comprising single family lots and portions of Besseyi Way, Union Pacific Way, Springs Road and El Reno Way. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet on the south side of El Reno Way, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 5.4 and 12.7 cfs respectively.

MAYBERRY – FILING 3 FINAL DRAINAGE REPORT

Filing 3 and the future Type R inlet will discharge to the main storm sewer system via this stub. The 5 year and 100 year developed peak flows are 3.3 and 8.0 cfs respectively.

Sub-basin D1.11 is a 1.23 acre onsite area that will not be fully developed until future phases. In the future the basin will be collected by a curb inlet on the south side of Mayberry Drive. This basin consists of the south section of the Mayberry Drive ROW. Runoff from this basin will be routed via curb/gutter, enter a Type R curb inlet, and will be discharged into the piped storm sewer system. A stub will be installed during Filing 3 and the future Type R inlet will discharge to the main storm sewer system via this stub. The 5 year and 100 year developed peak flows are 4 and 7.7 cfs respectively.

Sub-basin D1.12 is a 3.42 acre basin comprising single family lots and portions of Cattlemen Run, Solaire Loop, and Besseyi Way. The basin drains via curb and gutter to a Type R inlet on the north side of Besseyi Way. The 5 year and 100 year developed peak flows are 3.8 and 9.3 cfs respectively.

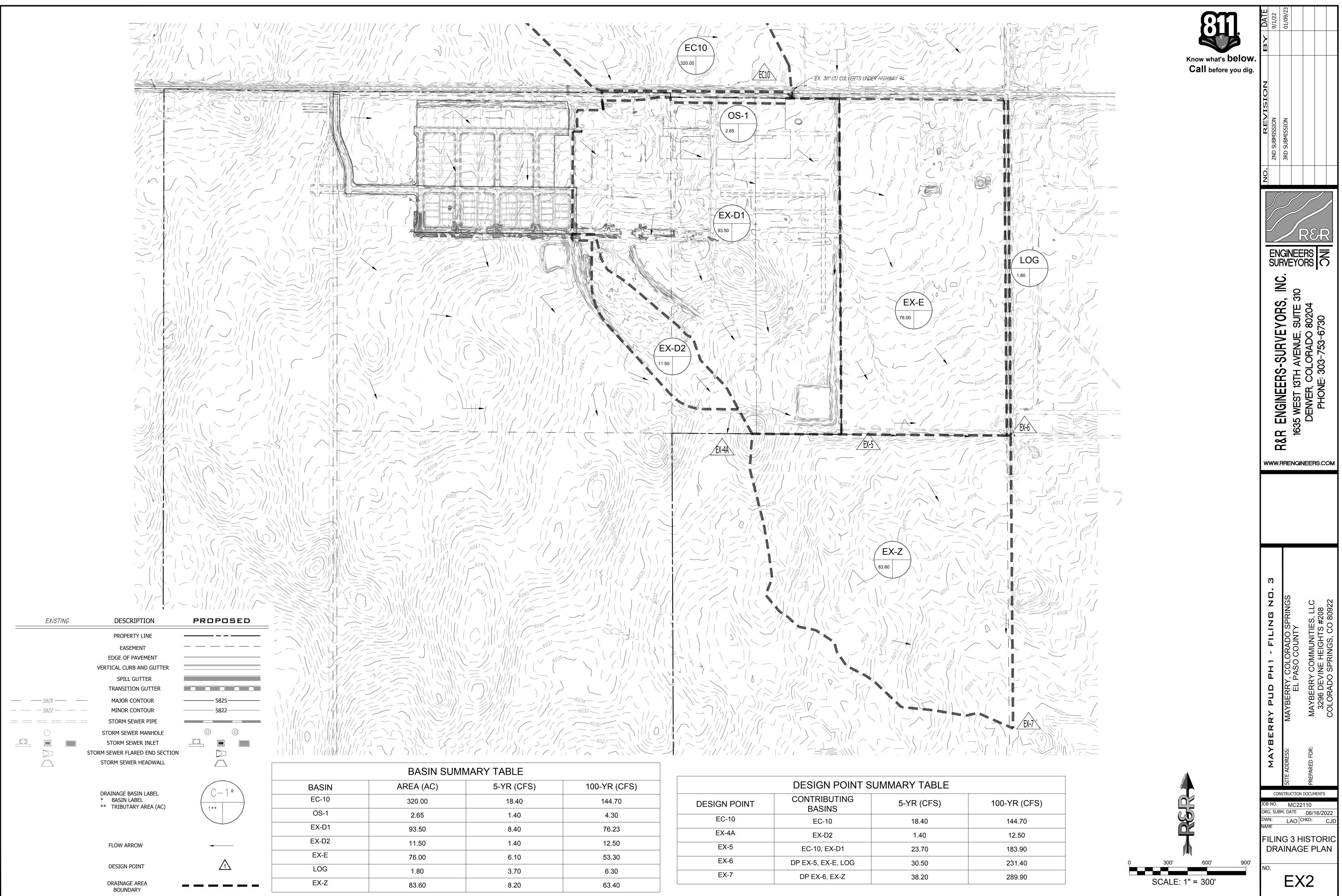
Sub-basin D1.13 is a 3.07 acre basin comprising commercial lots of Filing 2. The basin was analyzed for future development of Filing 2. The developed basin will drain into a future road's curb and gutter system and enter the Springs Road storm system via a Type R inlet within Springs Road. The 5 year and 100 year developed peak flows are 10.9 and 19.9 cfs respectively.

Sub-basin D1.14 is a 0.91 acre basin comprising both single family lots and the southeast commercial lots of Filing 2. The basin was analyzed for future development of Filing 2. The basin drains via curb and gutter to a Type R inlet on the north side of Besseyi Way. The 5 year and 100 year developed peak flows are 1.8 and 3.9 cfs respectively.

Sub-basin D2.0* is a 11.90 acre basin south of the Filing 3 development. The basin was analyzed for future development and assumed to comprise both single family lots and park area. The basin will ultimately drain to Pond D via future storm sewer improvements. The 5 year and 100 year developed peak flows are 10.3 and 27.7 cfs respectively.

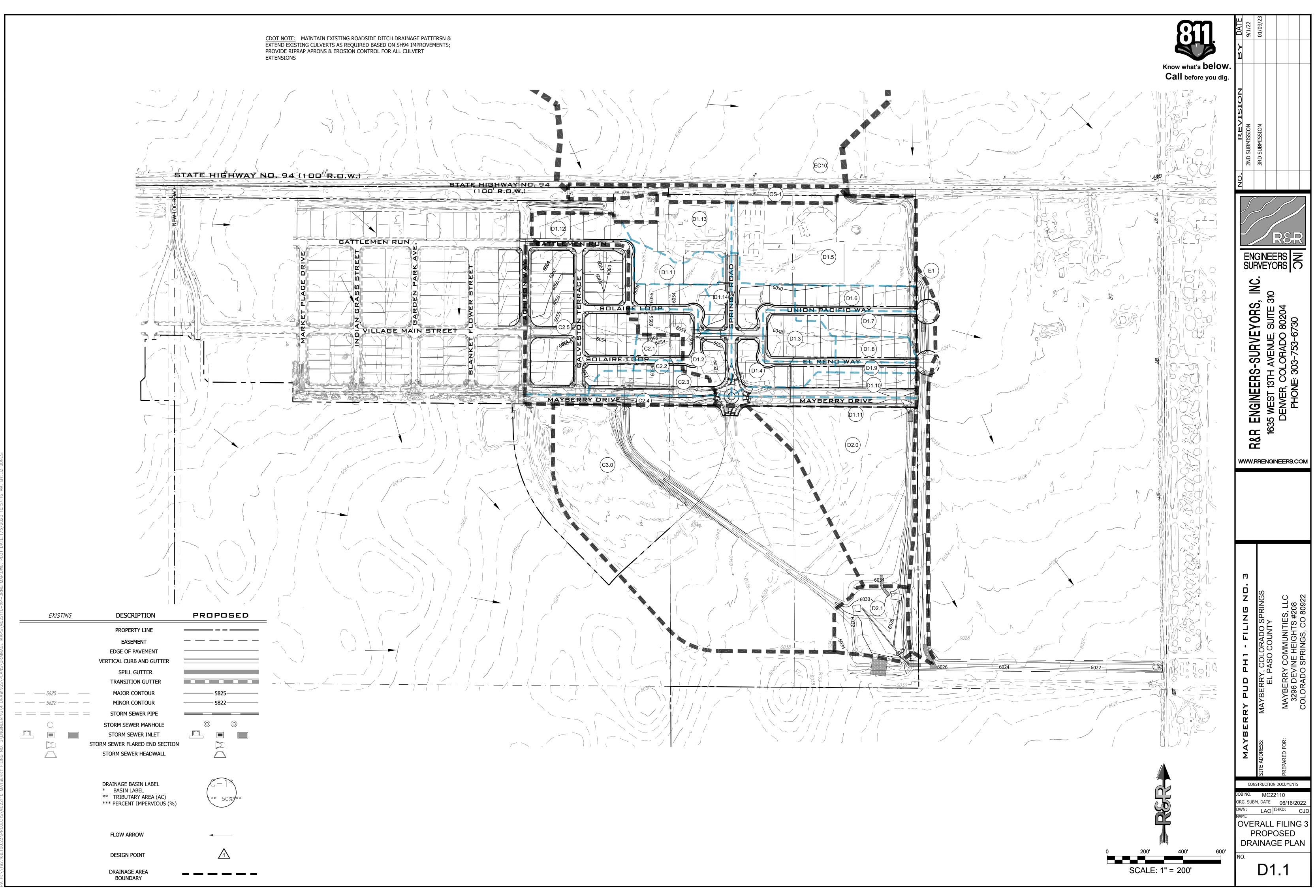
***D3.0** was also analyzed using an interim condition that represents the runoff patterns prior to development. Under this condition the basin would flow southeast into Channel D, ultimately discharging into Pond D. The 5 year and 100 year undeveloped peak flows are 2.4 and 17.9 cfs respectively.

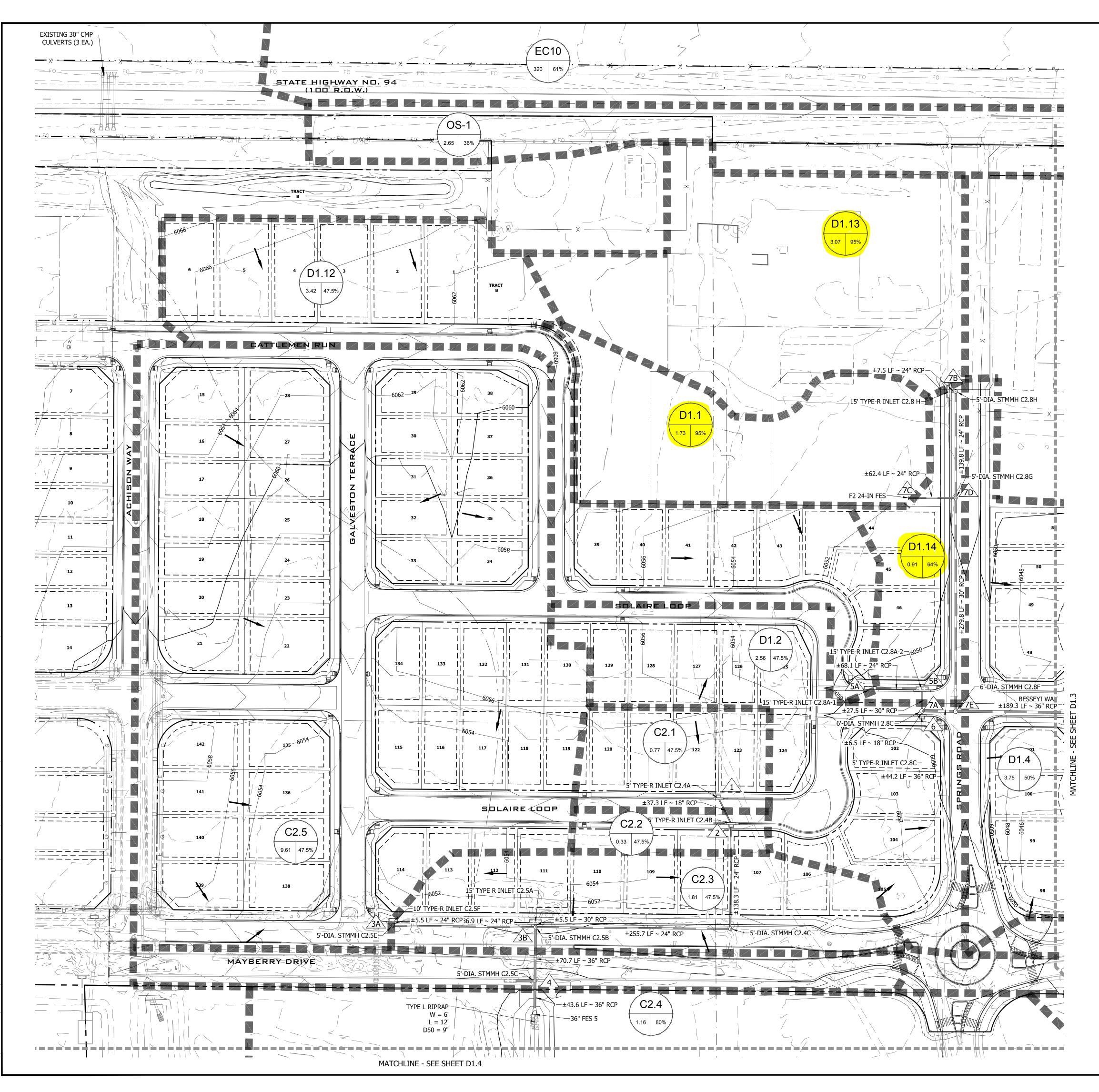
Sub-basin D2.1 is a 3.15 acre basin south of the Filing 3 development. The basin comprises the area around Detention Pond D. The basin will ultimately surface flow. The 5 year and 100 year developed peak flows are 0.9 and 6.6 cfs respectively.



	5-YR (CFS)	100-YR (CFS)		
	18.40	144.70		
	1.40	4.30		
	8.40	76.23		
	1.40	12.50		
	6.10	53.30		
	3.70	6.30		
	8.20	63.40		

		••••••
DESIGN POINT	CONTRIBUTING BASINS	5-YR (CF
EC-10	EC-10	18.40
EX-4A	EX-D2	1.40
EX-5	EC-10, EX-D1	23.70
EX-6	DP EX-5, EX-E, LOG	30.50
EX-7	DP EX-6, EX-Z	38.20
		·





Path: \\192.168.100.23\PROJECTS\MC22110 MAYBERRY FILING NO. 3\ENGINEERING\4 DRAWINGS\PLANS\DRAINAGE MAPS\MC22110-XP-DRNG MAP DTL.DWG, PLOT DATE: 1/5/2023 2:50:12 PM, BY:LIZ JONES

