

# FINAL DRAINAGE REPORT

## **FALCON MEADOWS AT BENT GRASS**

FILING NO. 2

PCD Filing No.: SF2134

El Paso County, Colorado

PREPARED FOR:

Challenger Communities 8605 Explorer Dr., Suite 250 Colorado Springs, CO 80920

PREPARED BY:

Galloway & Company, Inc. 1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920

DATE:

February 2022



#### **ENGINEER'S STATEMENT**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I according to the criteria with for any liability caused by any negligent acts, errors or omissions on my part in prepared with the proof of the criteria.

Grant Dennis, PE 51622

For and on behalf of Galloway Company Inc.

04/12/2022

#### **DEVELOPER'S CERTIFICATION**

I, The developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Address:

Challenger Communities, LLC 8605 Explorer Dr., Suite 250 Colorado Springs, CO 80920

#### **EL PASO COUNTY CERTIFICATION**

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

	APPROVED Engineering Department	
Jennifer Irvine, P.E. County Engineer/ECM Administrator	04/26/2022 7:51:10 AM dsdnijkamp  EPC Planning & Community Development Department	

Conditions:

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### I. Purpose

The intent of the developer is to develop the residential portion of the Bent Grass Subdivision. The purpose of this Final Drainage Report is to identify on and offsite drainage patterns, locate and identify tributary or downstream drainage features and facilities that impact the site, and to identify which types of drainage facilities will be needed and where they will be located. This report will remain in general compliance with the MDDP for the site, prepared by Galloway & Company.

#### **II.** General Description

The Falcon Meadows at Bent Grass Filing No. 2 is approximately 21.37 acres within the Bent Grass development. It is located north and west of Bent Grass Meadows Drive and west of the existing West Tributary of the Falcon Basin. The project is a single-family residential development of 108 lots, located in the Falcon area of El Paso County, Colorado. The site is located in the Northwest ¼ and Southwest ¼ of Section 1, Township 13S, Range 65W, of the Sixth Principal Meridian, County of El Paso, State of Colorado. The subject property is located to the south of The Meadows Filing No. 3; west of Bent Grass Residential Filing No. 2 and northwest of Falcon Meadows at Bent Grass Filing No. 1; north of Latigo Business Center Filing No. 1, undeveloped property, and the Mountain View Electric Association; and east of The Meadows Filing No. 2. A Vicinity Map is included in Appendix A.

A Planned Unit Development Plan Amendment was approved for the site, PUD-14-002 (July 2014). An additional Amendment to this PUD has also been approved (PUD-SP-205). The overall Bent Grass site consisted of approximately 103.4 acres and included 309 dwelling units.

The existing soil types within the proposed site as determined by the NRCS Web Soil Survey for El Paso County Area consist of Columbine gravelly sandy loam, Blakeland-Fluvaquentic Haplaquolls, and Blakeland loamy sand. All soils are defined as having a hydrologic soil group of A. See the soils map included in Appendix A.

## **III.** Previous Reports

The proposed site has been included in multiple drainage studies in the past. The following is a composite list of the existing reports pertaining to this site analysis.

- 1. Falcon Drainage Basin Planning Study, by Matrix Design Group, September 2015.
- 2. Master Development Drainage Plan Bent Grass Residential Subdivision, by Galloway & Company, September 2021.
- 3. *Master Development Drainage Plan and Preliminary Drainage Plan Bent Grass Subdivision*, by Kiowa Engineering Corporation, December 2006.
- 4. Final Drainage Report for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2014.
- 5. Final Drainage Report Addendum for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2015.
- 6. *Master Development Drainage Plan for The Ranch*, by Classic Consulting Engineers & Surveyors, LLC, November 2018.
- 7. Falcon Highlands Master Development Drainage Plan & Preliminary Drainage Report & Final Drainage Report for Filing 1, by URS, January 2005.

- 8. Final Drainage Report and Erosion Control Plan Latigo Business Center Filing No. 1 A Resubdivision of a Portion of Latigo Business and Research Center Filing No. 1, by Kiowa Engineering Corporation, November 2004.
- 9. Final Drainage Report Latigo Business Center Filing No. 2, by Kiowa Engineering Corporation, Revised December 13, 2007.
- 10. Final Drainage Letter Report for Lot 1, Latigo Business Center Filing No. 1, by Colorado Design Concepts, April 2005.
- 11. Final Drainage and Erosion Control for The Meadows Filing Three Subdivision, by LADD Engineering, July 2000.
- 12. Final Drainage Report Bent Grass Residential Subdivision, Filing No. 2, Galloway & Company, March 2020.
- 13. Preliminary Drainage Report Falcon Meadows at Bent Grass, by Galloway & Company, February 2021.
- 14. Final Drainage Report for Falcon Meadows at Bent Grass Filing No. 1, by Galloway & Company, under review.

## IV. Drainage Criteria

Hydrology calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014 and the El Paso County Engineering Criteria Manual (ECM) as revised in July 2019.

The drainage calculations were based on the criteria manual Figure 6-5 and IDF equations to determine the intensity and are listed in Table 1 below.

**Table 1 - Precipitation Data** 

Return Period	One Hour Depth (in).	Intensity (in/hr)
5-year	1.50	5.17
100-year	2.52	8.68

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has been proven to be accurate for basins of this size and is based on the following formula:

Q = CIA

Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff intensity (inches/hour)

A = Drainage area (acres)

The runoff coefficients are calculated based on land use, percent imperviousness, and design storm for each basin, as shown in the drainage criteria manual (Table 6-6). Composite percent impervious and C values were calculated using the residential, streets, roofs, and lawns coefficients found in Table 6-6 of the manual.

The 100-year event was used as the major storm event for pipes and inlets. The 5-year event was used as the minor event.

The UD-Detention spreadsheet was utilized for sizing the water quality orifices on the proposed water quality portion of the regional detention pond. This spreadsheet was also utilized for the design of the proposed on-site water quality ponds, Pond (North) and Pond (South).

UD-Inlet was utilized to calculate both the street capacities and the inlet capacities.

StormCAD was utilized to size the storm sewer systems.

#### V. Historic Drainage Conditions

The site is contained fully within one major drainage basin, the West Falcon Tributary. The site generally drains from north to south with an average slope of 2%. The rational method was used to analyze the individual basins within the site as the proposed drainage basins are less than 100 acres. The project site was studied in the Falcon Basin Drainage Basin Planning Study (DBPS) and in the Master Development and Drainage Plan (MDDP) for Bent Grass.

Per the Falcon DBPS by Matrix, the site lies within the basins, WT200, WT210, and WT220. These basins connect to channel reaches RWT202, RWT204, and RWT210. Both the RWT204 and RWT210 sections of channel currently exist and appear as a drainageway when visiting the site. Reach RWT202 appears to be a shallow overland flow through the project site. It is nearly unrecognizable through the site from a visual standpoint.

A historic basin map has been prepared for this site to analyze the historic basins as well as the offsite basins contributing to the site. Historic basins have been discussed in the Bent Grass Residential Filing No. 2 Final Drainage Report, El Paso County Project # SF-19-014. Copies of the hydrology calculations have been included in Appendix A and a copy of the historic map is included in Appendix E. Efforts have been made to comply with the recommendations set forth in the approved DBPS and MDDP.

## VI. Existing Drainage Conditions

An existing/current conditions basin map has been prepared for the development site, Falcon Meadows at Bent Grass Filing No. 2. Under this scenario, it is assumed that Bent Grass Residential Filing No. 2 and Falcon Meadows at Bent Grass Filing No. 1 are developed. This should be very similar to the proposed conditions from the Falcon Meadows at Bent Grass Filing No. 1 drainage report. An existing drainage map is included in Appendix E and the basins are described below.

**Basin OS-1** (32.28 AC, Q5 = 15.1 cfs, Q100 = 65.1 cfs) is associated with The Meadows Filing No. 3 lots 14, 15, 16, and 17. Runoff from this basin sheet flows to the northern property line of the Bent Grass Residential Filing No. 2 site and then flows, via an existing drainage swale, into the existing channel reach RWT204 from the Falcon DBPS at **DP 21**.

**Basin OS-4** (4.46 AC, Q5 = 5.6 cfs, Q100 = 14.0 cfs) is associated with The Bent Grass Residential Filing No. 2, lots 152-160, lots 163-168, Tract D, and portions of Thedford Court & Willmore Drive. Runoff from this basin flows via curb & gutter south on Thedford Court then continues flowing west along the northern curb & gutter along Willmore Drive before discharging into Basin EX-2 at **DP 1**.

**Basin OS-5** (0.46 AC, Q5 = 1.1 cfs, Q100 = 2.3 cfs): is associated with The Bent Grass Residential Filing No. 2, lots 161 & 162 along with a portion of Silky Thread Road. Runoff from this basin generally flows to the west via curb & gutter along Silky Thread Road before discharging into Basin EX-2 at **DP 2**.

**Basin OS-6** (1.17 AC, Q5 = 2.0 cfs, Q100 = 4.3 cfs): is associated with The Bent Grass Residential Filing No. 2, the northern halves of Lots 170-178 and a portion of the southern side of Willmore Drive. Runoff from this basin generally flows to the west via curb & gutter along Willmore Drive before discharging into Basin EX-2 at **DP 3**.

**Basin EX-1** (1.19 AC,  $Q_5 = 0.4$  cfs,  $Q_{100} = 2.5$  cfs): is associated with the northwestern portion of the Bent Grass Residential Filing No. 2 site east of the existing channel. The basin is currently undeveloped. Runoff from the basin generally flows to the southwest, into Basin EX-2.

**Basin EX-2** (1.60 AC,  $Q_5 = 0.5$  cfs,  $Q_{100} = 3.8$  cfs): is along the western boundary portion of the Bent Grass Residential Filing No. 2 site and is south of Basin EX-1, east of the existing channel. The basin is currently undeveloped and receives flows from Basins OS-4 & OS-5. Runoff from the basin generally flows to the southeast into Basin EX-3 at **DP 5** combined with flows from **DP 1, & 2**.

**Basin EX-3** (0.66 AC,  $Q_5 = 0.2$  cfs,  $Q_{100} = 1.6$  cfs): is along the western boundary portion of the Bent Grass Residential Filing No. 2 site south of Basin EX-2 and east of the existing channel. The basin currently contains an existing WQCV pond created as part of Bent Grass Residential Filing No. 2 (North Pond). This basin receives flows from **DP 5** and **DP 3**.

**Basin EX-4** (15.41 AC,  $Q_5 = 4.7$  cfs,  $Q_{100} = 31.8$  cfs): is located along the northern boundary, just south of the channel Reach RWT202, built with Bent Grass Residential Filing No. 2 and west of the existing channel. The basin is currently undeveloped. Runoff from the basin generally flows to the south onto Bent Grass Meadows Drive at **DP 6**. From there, it flows via curb & gutter to the east into an existing sump inlet, ultimately discharging into the existing WQCV pond in Bent Grass Residential Filing No. 2, located in Basin EX-3.

**Basin EX-5** (0.06 AC,  $Q_5 = 0.0$  cfs,  $Q_{100} = 0.2$  cfs): is west of Basin EX-4 and north of Bent Grass Meadows Drive. The basin is currently undeveloped. Runoff from the basin generally flows to the south onto Bent Grass Meadows Drive. From there, it flows via curb & gutter to the east into an existing sump inlet at **DP 8**, ultimately discharging into the existing WQCV pond from Bent Grass Residential Filing No. 2, located in Basin EX-3.

**Basin EX-6** (4.78 AC,  $Q_5 = 1.4$  cfs,  $Q_{100} = 9.5$  cfs): is along the west boundary of the site. The basin is currently undeveloped and receives off-site flows from Basins OS-2 & OS-3. Runoff from the basin generally flows to the south into the existing drainage ditch entering an existing area inlet at **DP 11**. This inlet is part of Storm System A, which eventually releases into the existing south WQVC facility built with Falcon Meadows at Bent Grass Filing No. 1 at **DP 31**.

**Basin EX-7** (12.18 AC,  $Q_5 = 3.5$  cfs,  $Q_{100} = 23.3$  cfs): is north & west of Bent Grass Meadows Drive, between Basins EX-5 & EX-6. The basin is currently undeveloped. Runoff from the basin generally flows to the southeast to the existing area inlet at **DP 11**. This inlet is part of Storm System A, which eventually releases into the existing south WQVC facility built with Falcon Meadows at Bent Grass Filing No. 1 at **DP 31**.

**Basin EX-8** (1.63 AC,  $Q_5 = 0.7$  cfs,  $Q_{100} = 4.7$  cfs): is a portion of Bent Grass Meadows Drive, along the western half of the road. The basin is currently undeveloped. Flows will enter the roadway and be conveyed to the south via curb and gutter to an existing at-grade inlet at **DP 24**. Intercepted flows will be conveyed via an existing storm system to the existing Swale F at **DP 26**. The existing swale will then continue carrying flows to the east to the existing south WQVC facility built with Falcon Meadows at Bent Grass Filing No. 1 at **DP 30**.

**Basin B-1** (6.78 AC, Q5 = 1.8 cfs, Q100 = 12.2 cfs): a basin that is in the center of the site along the north property boundary and encompasses the existing rerouted channel RWT202 and channel RWT204. Flows will continue south in the existing channel and twin 16'  $\times$  6' RCBC's where they will then be conveyed to **DP AA**.

**Basin OS-2** (20.07 AC, Q5 = 9.0 cfs, Q100 = 43.4 cfs): is associated with The Meadows Filing No. 1 lots 1, 2, 3, 4, 5, and 6. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site at **DP 9**. Flows will then be conveyed to the south where it will enter Basin EX-6 and tie-into the existing drainage swale (Swale E) along the southern boundary. It will then continue flowing east before entering an existing area inlet at **DP 11** where it will be piped, ultimately outfalling into the existing south WQCV pond at **DP 31**.

**Basin OS-3** (10.61 AC, Q5 = 4.7 cfs, Q100 = 22.6 cfs): is associated with The Meadows Filing No. 1 lot 11 and The Meadows Filing No. 2 Lots 1 & 2. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site into Basin EX-6 at **DP 10**. Flows will then be conveyed via an existing drainage swale (Swale E) to the east where it will enter an existing area inlet at **DP 11** where it will be piped, ultimately outfalling into the existing south WQCV pond at **DP 31**.

Below is a description of the basins which were developed as part of Falcon Meadows at Bent Grass Filing No. 1:

**Basin D-4a** (0.98 AC, Q5 = 2.1 cfs, Q100 = 4.4 cfs): a basin in Falcon Meadows at Bent Grass Filing No. 1 that is east of Bent Grass Meadows Drive. It encompasses single-family residential lots, north half of Rowena Way, & a portion of the west half of Nico Way. Runoff will flow from each lot onto the public R.O.W. where existing mountable curb and gutter will convey flows to **DP 17a**. Flow will continue as gutter flow in Nico Way, Linley Way and Jayla Trail to **DP 17b**.

**Basin D-4b** (0.95 AC, Q5 = 2.5 cfs, Q100 = 4.9 cfs): a basin in Falcon Meadows at Bent Grass Filing No. 1 that is east of Bent Grass Meadows Drive. It encompasses single-family residential lots, Rowena Way, & portions of Linley Way and Jayla Trail. Runoff will flow from each lot onto the public R.O.W. where existing mountable curb and gutter will convey flows to **DP 17b**, which is the combined flow from the south side of **DP 17**.

Basin D-4c (1.22 AC, Q5 = 2.4 cfs, Q100 = 5.0 cfs): a basin in Falcon Meadows at Bent Grass Filing No. 1 that is east of Henzlee Place and Jayla Trail and south of Bent Grass Meadows Drive. It encompasses single-family residential lots, & portions of Nico Way, Jayla Trail, and Henzlee Place. Runoff will flow from each lot onto the public R.O.W. where existing mountable curb and gutter will convey flows to DP 17c, the north side of DP 17. Flows at DP 17 (combined flows from DP 17b & DP 17c with bypass from DP 18) will then enter an existing sump CDOT Type 'R' inlet where it will then be piped and ultimately outfall in the existing south WQCV pond at DP 31. Overflow from this inlet would be to overtop the curb and then continue via an existing swale, following the same path as the existing pipe, to the east until flows are released into the existing south water quality pond, built with Falcon Meadows Filing No. 1.

**Basin D-5** (1.08 AC, Q5 = 2.2 cfs, Q100 = 4.6 cfs): a basin that is located at the southwest corner of Bent Grass Meadows Drive and Henzlee Place. It includes residential lots, as well as a portion of the north half of Nico Way and west half of Henzlee Place. Flows will be directed towards the public R.O.W. where existing curb and gutter will convey flows to the south along Henzlee Place to **DP 18**. Flows will then enter an existing CDOT Type 'R' inlet where it will then be piped and ultimately outfall in the existin south WQCV pond at **DP 31**.

**Basin D-6a** (1.33 AC, Q5 = 3.8 cfs, Q100 = 7.5 cfs): a basin in Falcon Meadows at Bent Grass Filing No. 1 that is south of Basin D-6b & east of Basin D-4a. It encompasses single-family residential lots & half of Linley Way, Jayla Trail, Henzlee Place, & Nico Way. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will convey flows to **DP 18.** 

**Basin D-6b** (2.69 AC, Q5 = 5.6 cfs, Q100 = 11.4 cfs): a basin in Falcon Meadows at Bent Grass Filing No. 1 that is south of Basin D-5 & east of Basin D-4a. It encompasses single-family residential lots & half of Linley Way, Jayla Trail, Henzlee Place, & Nico Way. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will convey flows to **DP 18**, along with flows from Basin D-6a. Flows will then enter an existing sump CDOT Type 'R' inlet where it will then be piped and ultimately outfall in the existing south WQCV pond at **DP 31**.

**Basin D-7** (7.65 AC, Q5 = 4.3 cfs, Q100 = 18.2 cfs): a basin that is in the south end of the site, east of Bent Grass Meadows Drive & west of the existing channel. It encompasses the back half of several single-family residential lots as well as existing south WQCV pond and an existing drainage swale. Runoff will flow, via sheet flow, until it enters the existing drainage swale (Swale F) and is conveyed to the existing south WQCV pond or will directly flow into the south WQCV pond at **DP 30**.

**Basin D-8** (1.69 AC, Q5 = 2.6 cfs, Q100 = 6.0 cfs): a basin that is west of the existing channel & south of Bent Grass Meadows Drive. It encompasses the back half of single-family residential lots. Runoff will flow from each lot and discharge into an existing drainage swale. The drainage swale (Swale C) will then convey flows to the south, ultimately discharging into the existing south WQCV pond at **DP 32**.

**Basin B-2** (4.16 AC, Q5 = 1.3 cfs, Q100 = 8.6 cfs): a basin that is located along the eastern property line of Falcon Meadows at Bent Grass Filing No. 1, south of Bent Grass Meadows Drive and encompasses channel reach RWT204/ RWT210. Flows will sheet flow into the channel where they will then be conveyed to **DP CC**, combining with other on-site flows, prior to exiting the site.

Basins E-1 thru E-5 and I-1 will be developed as part of Bent Grass Residential Filing No. 2 development. Information for those basins were taken from the accompanying Final Drainage Report for Filing No. 2. Flows within Basin E-4 are conveyed downstream via curb and gutter to Design Point 24 where runoff is captured by an existing 15' CDOT Type R at-grade inlet. At this location, no runoff bypasses in the minor storm event while in the major storm event, 3.1 cfs bypass the 15' CDOT Type R at-grade inlet and continue within Bent Grass Meadows Drive downstream to another 15' CDOT Type R at-grade inlet just north of the boundary between Falcon Storage Partners and Falcon District 49 properties. Per the approved *Final Drainage Report – Latigo Business Center Filing No. 2*, by Kiowa Engineering Corporation, Revised December 13, 2007, bypass flows continue downstream within the Bent Grass Meadows Drive roadway past Design Point 1 to Design Point 6, where runoff is directed the end of the existing curb and flows into the existing channel.

Basin RWT202 (1574.4 AC,Q5 = 200 cfs, Q100 = 1000 cfs), RWT204 (38.4 AC, Q5 = 7 cfs, Q100 = 43 cfs) and WT200 (192 AC, Q5 = 52 cfs, Q100 = 190 cfs) represent larger offsite basins to the north of the proposed project. These areas were studied as part of the Falcon Basin DBPS prepared by Matrix and were also part of the Bent Grass MDDP, approved September 21, 2021. There have been no changes to these basins as they are offsite and existing.

**Design Point CC** is the location in channel reach RWT210, where flows exit the Falcon Meadows development, including the offsite flows from RWT202, RWT204 and WT200. The minor flows are 314.8 cfs and the major flows are 1360.1 cfs.

### VII. Four Step Process

The Four Step Process is used to minimize the adverse impacts of urbanization and is a vital component of developing a balanced, sustainable project. Below identifies the approach to the four-step process:

#### 1. Employ Runoff Reduction Practices

The proposed development uses Low Impact Development (LID) practices to reduce runoff at the source. Rather than creating point discharges that are directly connected to impervious areas, runoff is routed through pervious areas to promote infiltration and minimize directly connected impervious areas (MDCIA). Grass buffers and swales are used where practical.

#### 2. Stabilize Drainageways

This step implements stabilization to channels to accommodate developed flows while protecting infrastructure and controlling sediment loading from erosion in the drainageways. Erosion protection in the form of riprap pads at all outfall points to the channel to prevent scouring of the channel from point discharges. A HEC-RAS model was created and used to evaluate the stability of the existing channels. The HEC-RAS results are included in previous reports. It was determined that given the channel is stable in its current state and the proposed velocities and Froude numbers are similar to those in the existing channel, no improvements will be made to the channel with this filing. This will be further discussed later in this report, see Section XI Channels and Swales.

#### 3. Provide Water Quality Capture Volume (WQCV)

This step utilizes formalized water quality capture volume to slow the release of runoff from the site. The WQCV will release in no less than 40 hours. On-site water quality control volume detention ponds will provide water quality treatment prior to the runoff being released into the channel.

#### 4. Consider Need for Industrial and Commercial BMPs

Industrial and Commercial BMP's are not applicable to this proposed site. Source control BMPs for homeowners include the use of garages as the primary area where pollutants can be stored. The single-family detached homes provide garages which can act as storage areas. The proposed development does not include outdoor storage or the potential for introduction of contaminants to the Counties' MS4, thus no targeted source control BMPs are necessary. The biggest source control BMP is public education which can be found on the El Paso County website and discuss topics such as: pet waste, car washing, lawn care, fall leaves, and snow melt and deicer.

## VIII. Proposed Drainage Conditions

The site will provide WQCV Detention Ponds to provide water quality treatment prior to discharging the runoff directly into the West Tributary channel RWT204/RWT210. There are 2 total basins, within the proposed development, which are not routed to any of the WQ facilities. Basins B-1 (6.06 acres) & B-2 (4.16 acres), although larger than 1 acre, do not count towards the allowable area of 1 acre or less to be released from a site, untreated, as these basins represent the channel reaches RWT204/210, and are described as undeveloped land remaining undeveloped. All on site flows eventually release into West Tributary of Falcon Basin, where flows will continue to the south, exiting the site at Design Point CC.

As mentioned previously, the site is proposed to be single family residential. The site is designed to provide a large lot buffer between the existing large lots to the north and west of the site and the proposed site. Beyond this buffer the majority of the site is smaller approximately 1/8 acre lots.

**Basin OS-1** (32.28 AC, Q5 = 15.1 cfs, Q100 = 65.1 cfs) is associated with The Meadows Filing No. 3 lots 14, 15, 16, and 17. Runoff from this basin sheet flows to the northern property line of the site and then flows, via an existing drainage swale, into the existing channel reach RWT204 from the Falcon DBPS at **DP 21**.

**Basin OS-4** (4.46 AC, Q5 = 5.6 cfs, Q100 = 14.0 cfs) is associated with The Bent Grass Residential Filing No. 2, lots 152-160, lots 163-168, Tract D, and portions of Thedford Court & Willmore Drive. Runoff from this basin flows via curb & gutter south on Thedford Court then continues flowing west along the northern curb & gutter along Willmore Drive before discharging into Basin A-1 at **DP 1**.

**Basin OS-5** (0.46 AC, Q5 = 1.1 cfs, Q100 = 2.3 cfs): is associated with The Bent Grass Residential Filing No. 2, lots 161 & 162 along with a portion of Silky Thread Road. Runoff from this basin generally flows to the west via curb & gutter along Silky Thread Road before discharging into Basin A-1 at **DP 2**.

**Basin OS-6** (1.17 AC, Q5 = 2.0 cfs, Q100 = 4.3 cfs): is associated with The Bent Grass Residential Filing No. 2, the northern halves of Lots 170-178 and a portion of the southern side of Willmore Drive. Runoff from this basin generally flows to the west via curb & gutter along Willmore Drive before discharging into Basin A-1 at **DP 3**.

**Basin EX-1** (1.19 AC,  $Q_5 = 0.4$  cfs,  $Q_{100} = 2.5$  cfs): is associated with the northwestern portion of the Bent Grass Residential Filing No. 2 site east of the existing channel. The basin is currently undeveloped. Runoff from the basin generally flows to the southwest, into Basin EX-2.

**Basin EX-2** (1.60 AC,  $Q_5 = 0.5$  cfs,  $Q_{100} = 3.8$  cfs): is along the western boundary portion of the Bent Grass Residential Filing No. 2 site and is south of Basin EX-1, east of the existing channel. The basin is currently undeveloped and receives flows from Basins OS-4 & OS-5. Runoff from the basin generally flows to the southeast into Basin EX-3 at **DP 5** combined with flows from **DP 1, & 2**.

**Basin EX-3** (0.66 AC,  $Q_5 = 0.2$  cfs,  $Q_{100} = 1.6$  cfs): is along the western boundary portion of the Bent Grass Residential Filing No. 2 site south of Basin EX-2 and east of the existing channel. The basin currently contains an existing WQCV pond created as part of Bent Grass Residential Filing No. 2 (North Pond). This basin receives flows from **DP 5** and **DP 3**.

**Basin C-6** (0.94 AC, Q5 = 1.0 cfs, Q100 = 3.4 cfs): a basin for this proposed development that will include mostly open area and some small areas of back residential lots. The basin is located on the west side of Bent Grass Meadows Drive. The basin drains towards the existing roadway. Flows will be conveyed via curb and gutter to the east to **DP 8**, an existing CDOT type R sump inlet, which releases into the existing WQCV pond in Bent Grass Residential Filing No. 2.

**Basin B-1** (6.06 AC, Q5 = 1.6 cfs, Q100 = 10.9 cfs): a basin that is along the north boundary of the site and through the center of the site, encompassing the existing rerouted channel RWT202 and channel RWT204. Flows will continue south in the existing channel where they will then be conveyed through the existing twin 16'  $\times$  6' RCBC's to **DP AA**.

**Basin C-1a** (0.38 AC, Q5 = 1.0 cfs, Q100 = 2.2 cfs): a basin located near the eastern edge of this filing. It contains the south half of Daelyn Drive, east of Kittrick Place, includes a temporary turnaround and residential lots adjacent to the roadway. A temporary drainage swale (Swale B) will collect flows at **DP 40**,

a low spot at the end of the temporary turnaround, and convey flows to the south, where they will be intercepted by a proposed 15' at grade CDOT Type R inlet at **DP 41**, which is part of Storm System B. Bypass flows will be conveyed to the south to **DP 15**.

**Basin C-1b** (0.45 AC, Q5 = 1.3 cfs, Q100 = 2.5 cfs): a basin that encompasses the proposed temporary Swale B. Flows will be conveyed to the south to **DP 41**.

**Basin C-1c** (1.77 AC, Q5 = 5.6 cfs, Q100 = 11.0 cfs): a basin for a future Falcon Meadows filing that will include a portion of the west half of Henzlee Place, north portion of Kittrick Place, and encompasses single-family residential lots. Runoff will flow towards the future road and will be directed towards the proposed 15' at-grade CDOT Type R inlet at **DP 41**.

**Basin C-1d** (1.72 AC, Q5 = 4.6 cfs, Q100 = 9.5 cfs): a basin that will include the north half of Kittrick Place and encompasses single-family residential lots. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 43.** Flows will continue to the south via curb and gutter to **DP 15**, where they will be intercepted by a 15' at grade CDOT Type R inlet, part of Storm System B and ultimately release into the proposed WQCV (North Pond), located north of Bent Grass Meadows Drive at **DP 13**. Bypass flows will continue to the south to **DP 45** and then eventually reaching **DP 8**, an existing CDOT sump Type R inlet, which releases into the existing WQCV pond in Bent Grass Filing No. 2.

**Basin C-1e** (0.29 AC, Q5 = 1.3 cfs, Q100 = 2.4 cfs): a basin that will include the east half of Henzlee Place. Runoff will flow from the R.O.W. into the proposed mountable curb and gutter where it will be conveyed to **DP 12.** Flows will then enter a proposed 15' at grade CDOT Type R inlet, part of Storm System B, where it will be piped to the proposed north WQCV pond at **DP 13**. Bypass flows will travel to the south then east in Bent Grass Meadows Drive to **DP 8**, an existing CDOT sump Type R inlet, which releases into the existing WQCV pond in Bent Grass Filing No. 2.

**Basin C-1f** (0.08 AC, Q5 = 0.4 cfs, Q100 = 0.7 cfs): a basin that includes the west half of Henzlee Place between Kittrick Place and the centerline of Henzlee Place. Runoff will flow from the proposed R.O.W. into the proposed mountable curb and gutter which will convey flows to **DP 15.** Flows will then enter a proposed 15' at grade CDOT Type R, part of Storm System B, inlet where it will be ultimately piped to the proposed north WQCV pond at **DP 13**. Bypass flows will continue to the south to DP 45 and ultimately to **DP 8**, existing sump CDOT Type R inlet, releasing into the existing WQCV pond in Bent Grass Filing No. 2.

**Basin C-2** (3.98 AC, Q5 = 10.1 cfs, Q100 = 21.1 cfs): Is a basin for a future Falcon Meadows filing which will encompass single-family residential lots including the east half of Henzlee Place. Runoff will flow from each lot onto the future public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 12.** Flows will then enter a proposed 15' at grade CDOT Type R inlet, part of Storm System B, where it will be piped to the proposed north WQCV pond at **DP 13**. Bypass flows will continue towards the south, eventually reaching, an existing sump CDOT Type R inlet, releasing into the existing WQCV pond in Bent Grass Filing No. 2. A storm stub has been provided at **DP19** for a future swale and area inlet to be constructed with the future development.

**Basin C-3** (0.18 AC, Q5 = 0.7 cfs, Q100 = 1.2 cfs): Is a basin that includes a south portion of Daelyn Drive between a high point and Kittrick Place. Flows will be conveyed as gutter flow to the east and then south along Kittrick Place to **DP 44**.

**Basin C-4** (2.67 AC, Q5 = 4.2 cfs, Q100 = 9.7 cfs): Is a basin which will encompass residential lots and open space easy of Henzlee Place. Runoff will flow from the open space onto the lots, eventually releasing into the public R.O.W. of Kittrick Place, where proposed mountable curb and gutter will convey flows to **DP 44.** Flows will then enter a proposed 15' at grade CDOT Type R inlet, part of Storm System B, where it will ultimately be released into the proposed north WQCV pond at **DP 13**. Bypass flow will travel to the south to be intercepted at **DP 15**.

**Basin C-7** (0.52 AC, Q5 = 1.4 cfs, Q100 = 2.9 cfs): Is a basin encompassing the west half of Henzlee Place and residential lots west, located between Kittrick Place and Bent Grass Meadows Drive. Flows will be directed towards Henzlee Place, where it will enter the proposed public R.O.W. and be conveyed as gutter flow to the south to **DP 45** at Bent Grass Meadows Drive. From here, flows will continue to the east to **DP 8**, where they will be intercepted by an existing CDOT Type R inlet, releasing into the existing WQCV pond in Bent Grass Filing No. 2.

**Basin C-5** (0.60 AC, Q5 = 0.3 cfs, Q100 = 1.9 cfs): Is a basin which will encompass the proposed north WQCV pond area. The stormwater within the proposed north WQCV pond will be released at a controlled rate, via an outlet structure with orifice holes, into the existing channel RWT204.

**Basin OS-2** (20.07 AC, Q5 = 9.0 cfs, Q100 = 43.4 cfs): is associated with The Meadows Filing No. 1 lots 1, 2, 3, 4, 5, and 6. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site at **DP 9**. Flows will then be conveyed via a drainage swale (Swale D) to the south where it will tie-into the existing drainage swale (Swale E) along the southern boundary of Basin D-3. It will then continue flowing east before entering an existing area inlet, which is part of Storm System A, at **DP 11** where it will be piped, ultimately outfalling into the existing south WQCV pond at **DP 31**.

**Basin OS-3** (10.61 AC, Q5 = 4.7 cfs, Q100 = 24.3 cfs): is associated with The Meadows Filing No. 1 lot 11 and The Meadows Filing No. 2 Lots 1 & 2. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site into Basin D-3 at **DP 10**. Flows will be conveyed via an existing drainage swale (Swale E) to the east where it will enter an existing area inlet at **DP 11** where it will be piped, ultimately outfalling into the existing south WQCV pond at **DP 31**.

**Basin D-1a** (2.97 AC, Q5 = 6.3 cfs, Q100 = 14.4 cfs): a basin for a future Falcon Meadows filing at the northeast corner of the future intersection of Isabel Place and Daelyn Drive. It encompasses single-family residential lots, a portion of Kittrick Place (future), & a portion of the north half of Daelyn Drive. Runoff will flow to the south to the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 51** where flows will be intercepted by a proposed 15' at grade CDOT Type R inlet, which is part of Storm System B. Bypass flows will continue to the east, releasing into the proposed temporary swale (Swale B) at **DP 40**.

**Basin D-1f** (1.61 AC, Q5 = 3.1 cfs, Q100 = 6.7 cfs): a basin for a future Falcon Meadows filing east of Basin D-1a and north of Daelyn Place. It encompasses single-family residential lots, & a portion of the north half of Daelyn Drive. Runoff will flow into the proposed public R.O.W. of Daelyn Drive where proposed mountable curb and gutter will convey flows across the temporary turnaround to a low point at **DP 40**, where flows will be released into a proposed temporary swale (Swale B).

**Basin D-1b** (2.54 AC, Q5 = 4.7 cfs, Q100 = 10.1 cfs): a basin for a future Falcon Meadows filing along the west property line of the site. It encompasses single-family residential lots & the remaining west half of Daelyn Drive. Runoff will flow into the proposed public R.O.W. of Daelyn Drive, at **DP 16a.** From here, flows will be released into proposed mountable curb and gutter which will deliver flows to the south to **DP** 

**16.** Flows will then enter an existing CDOT at grade Type R inlet, which is part of Storm System A, where captured flows will then be piped and ultimately outfall in the existing south WQCV pond at **DP 31**. Bypass flows from the inlet will continue to the south in Bent Grass Meadows Drive to be intercepted by the existing CDOT Type R inlet at **DP 24**.

**Basin D-1c** (4.34 AC, Q5 = 5.9 cfs, Q100 = 13.1 cfs): a basin along the west property line of the site. It encompasses single-family residential lots & the remaining west half of Daelyn Drive. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 16**, along with flows from **DP16a**. Flows will then enter an existing CDOT at grade Type 'R' inlet where captured flows will be piped and ultimately outfall in the existing south WQCV pond at **DP 31**. Bypass flows from the inlet will continue to the south in Bent Grass Meadows Drive to be intercepted by the existing CDOT Type R inlet at **DP 24**.

**Basin D-2a** (0.50 AC, Q5 = 1.9 cfs, Q100 = 3.6 cfs): a basin south of Basin D-1a. It encompasses a portion of the south half of Daelyn Drive. Runoff will flow from the proposed public R.O.W., where proposed mountable curb and gutter will convey flows to **DP 14a.** 

**Basin D-2b** (0.74 AC, Q5 = 1.4 cfs, Q100 = 3.2 cfs): a basin south of Basin D-2a. It encompasses single-family residential lots and the north half of Raylan Way. Runoff will flow from each lot onto the proposed public R.O.W, in Raylan Drive. where proposed mountable curb and gutter will convey flows to **DP 14a.** 

**Basin D-2c** (0.31 AC, Q5 = 1.1 cfs, Q100 = 2.1 cfs): a basin south of Basin D-2b. It encompasses the south half of Raylan Way. Runoff will be conveyed as gutter flow to **DP 14a**. Combined flows from DP 14a will continue south, as gutter flow, in the east side of Daelyn Drive to **DP 14b**.

**Basin D-2d** (0.24 AC, Q5 = 0.8 cfs, Q100 = 1.6 cfs): a basin east of Basin D-1c. It encompasses the east half of Daelyn Drive, between Raylan Way and Isabel Place. Runoff will be conveyed as gutter flow to **DP 14b.** 

**Basin D-2e** (1.41 AC, Q5 = 3.3 cfs, Q100 = 6.7 cfs): a basin east of Basin D-2d and south of D-2c. It encompasses single-family residential lots and the west half of Isabel Place. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 14d**, a low point on the west side of Isabel Place. Flows will be intercepted by a proposed 5' sump CDOT Type R inlet. These flows will be a part of Storm System A, which was built partially in Falcon Meadows at Bent Grass Filing No. 1 (**DP 14 & DP16**). This system ultimately outfalls into the existing south WQCV pond at **DP 31**.

**Basin D-2f** (2.43 AC, Q5 = 6.0 cfs, Q100 = 12.2 cfs): a basin east of Basin D-2e. It encompasses single-family residential lots, east half of Isabel Place and Jolie Court. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 14e**, a low point on the east side of Isabel Place. Flows will be intercepted by a proposed 10' sump CDOT Type R inlet, as part of Storm System A. Flows will ultimately outfall into the existing south WQCV pond at **DP 31**.

**Basin D-2g** (1.81 AC, Q5 = 2.9 cfs, Q100 = 6.5 cfs): a basin south of Basin D-2f. It encompasses single-family residential lots, east half of Daelyn Drive and north half of Rowena Way. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 14,** which combines with the flow from **DP 14b.** Flows will then enter an existing at grade CDOT Type R inlet where captured flows will then be piped and ultimately outfall in the existing south WQCV pond at **DP 31.** Bypass flows from the inlet would overtop Rowena Way to **DP 16.** 

**Basin D-2h** (0.23 AC, Q5 = 0.3 cfs, Q100 = 0.8 cfs): a basin south of Basin D-2d and east of Bent Grass Meadows Drive, containing residential lots which will flow into Bent Grass Meadows Drive. Flows will be conveyed via existing curb and gutter to the existing CDOT Type R inlet at **DP 24**.

**Basin D-3** (2.26 ac, Q5 = 2.6 cfs, Q100 = 6.3 cfs): a basin along the southwest property line adjacent to Basins OS-2 and OS-3. It encompasses the backs of several residential lots as well as Swales D and E. Runoff will flow from basins OS-2 and OS-3 into Swale D and convey flows east through Swale E to an existing area inlet at **DP11**. From there, flows will be piped and ultimately outfall at the south WQCV pond at **DP31**. Bypass flows will spill into Basin E-4 and flow to the existing inlet at **DP24**.

The following basins were all developed as part of Falcon Meadows at Bent Grass Filing No. 1.

**Basin D-4a** (0.98 AC, Q5 = 2.1 cfs, Q100 = 4.4 cfs): a basin that is east of Bent Grass Meadows Drive. It encompasses single-family residential lots, north half of Rowena Way, & a portion of the west half of Nico Way. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will convey flows to **DP 17a**. Flow will continue as gutter flow in Nico Way, Linley Way and Jayla Trail to **DP 17b**.

**Basin D-4b** (0.95 AC, Q5 = 2.5 cfs, Q100 = 4.9 cfs): a basin that is east of Bent Grass Meadows Drive. It encompasses single-family residential lots, Rowena Way, & portions of Linley Way and Jayla Trail. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will convey flows to **DP 17b**, which is the combined flow from the south side of **DP 17**.

Basin D-4c (1.22 AC, Q5 = 2.4 cfs, Q100 = 5.0 cfs): a basin that is east of Henzlee Place and south of Bent Grass Meadows Drive. It encompasses single-family residential lots, & portions of Nico Way, Jayla Trail, and Henzlee Place. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will convey flows to DP 17c, the north side of DP 17. Flows at DP 17 (combined flows from DP 17b & DP 17c with bypass from DP 18) will then enter an existing sump CDOT Type R inlet, part of Storm System A, where it will then be piped and ultimately outfall in the existing south WQCV pond at DP 31. Overflow from this inlet would be to overtop the curb and then continue via an existing swale, following the same path as the existing pipe, to the east until flows are released into the existing south water quality pond.

**Basin D-5** (1.08 AC, Q5 = 2.8 cfs, Q100 = 6.0 cfs): a basin that is located at the southwest corner of Bent Grass Meadows Drive and Henzlee Place. It includes residential lots, as well as a portion of the north half of Nico Way and west half of Henzlee Place. Flows will be directed towards the public R.O.W. where existing curb and gutter will convey flows to the south along Henzlee Place to **DP 18**. Flows will then enter an existing CDOT Type R inlet, part of Storm System A, where it will then be piped and ultimately outfall in the existing south WQCV pond at **DP 31**.

**Basin D-6a** (1.33 AC, Q5 = 3.8 cfs, Q100 = 7.5 cfs): a basin filing that is south of Basin D-6b & east of Basin D-4a. It encompasses single-family residential lots & half of Linley Way, Jayla Trail, Henzlee Place, & Nico Way. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will convey flows to **DP 18.** 

**Basin D-6b** (2.69 AC, Q5 = 5.6 cfs, Q100 = 11.4 cfs): a basin that is south of Basin D-5 & east of Basin D-4a. It encompasses single-family residential lots & half of Linley Way, Jayla Trail, Henzlee Place, & Nico Way. Runoff will flow from each lot onto public R.O.W. where existing mountable curb and gutter will

convey flows to **DP 18**, along with flows from Basin D-6a. Flows will then enter an existing sump CDOT Type R inlet where it will then be piped and ultimately outfall in the existing south WQCV pond at **DP 31**.

**Basin D-7** (7.65 AC, Q5 = 4.3 cfs, Q100 = 18.2 cfs): a basin that is in the south end of the site, east of Bent Grass Meadows Drive & west of the existing channel. It encompasses the back half of several single-family residential lots as well as the existing south WQCV pond and an existing drainage swale (Swale F). Runoff will flow, via sheet flow, until it enters the existing swale and is conveyed to the existing south WQCV pond or will directly flow into the existing south WQCV pond at **DP 30**.

**Basin D-8** (1.69 AC, Q5 = 2.6 cfs, Q100 = 6.0 cfs): a basin that is west of the existing channel & south of Bent Grass Meadows Drive. It encompasses the back half of single-family residential lots. Runoff will flow from each lot and discharge into an existing drainage swale (Swale C). The swale will convey flows to the south, ultimately discharging into the existing south WQCV pond at **DP 32**.

**Basin D-9** (0.72 AC, Q5 = 0.8 cfs, Q100 = 2.7 cfs): a basin that is east of Basin D-2f & west of Bent Grass Meadows Drive. It encompasses the back half of single-family residential lots. Runoff will flow from each lot and release into Bent Grass Meadows Drive. This flow will be conveyed as gutter flow to the south in the roadway, where it will be intercepted by an existing at grade inlet at **DP 24**.

**Basin B-2** (4.16 AC, Q5 = 1.3 cfs, Q100 = 8.6 cfs): a basin that is in the south area of the site and encompasses channel reach RWT204/ RWT210. Flows will sheet flow into the channel where they will then be conveyed to **DP CC**, combining with other on-site flows, prior to exiting the site.

Basins E-1 thru E-5 are the same as discussed under the Existing Conditions Section, as these basins represent the already built Bent Grass Meadows Drive through the proposed site.

Basin RWT202 (1574.4 AC,Q5 = 200 cfs, Q100 = 1000 cfs), RWT204 (38.4 AC, Q5 = 7 cfs, Q100 = 43 cfs) and WT200 (192 AC, Q5 = 52 cfs, Q100 = 190 cfs) represent larger offsite basins to the north of the proposed project. These areas were studied as part of the Falcon Basin DBPS prepared by Matrix and were also part of the Bent Grass MDDP, submitted for review in January. There have been no changes to these basins as they are offsite and existing.

**Design Point CC** is the location in channel reach RWT210, where flows exit the Bent Grass Site, including the offsite flows from RWT202, RWT204 and WT200. The minor flows are 336.3 cfs and the major flows are 1384.7 cfs. The MDDP Amendment, from the HEC-HMS model, has flows of 191.8 cfs and 1075.3 cfs for the 5- and 100-year flows under proposed/future conditions analysis. The FEMA FIS report has a total flow of 1400 cfs in channel reach RWT210.

## IX. Storm Sewer System

All development is anticipated to be urban and will include storm sewer & street inlets. Storm sewers collect storm water runoff and convey the stormwater to water quality facilities prior to discharging. Storm sewer systems will be designed to the 100-year storm and checked with the 5-year storm. All storm sewer piping will utilize watertight joints due to pipes being surcharged in the 100-year event. Inlets will be placed at sump areas and intersections where street flow is larger than street capacity. UDFCD Inlet spreadsheet will be used to determine the size of all at-grade and sump inlets. There will be a minimum of 2 proposed storm systems and two existing systems within the site. There will be two future storm system with subsequent filings of Falcon Meadows, as the area develops north of Bent Grass Meadows Drive.

There are two future storm systems. The first future storm system will collect the north and west portion of the site, intercepting flows prior to entering Bent Grass Meadows Drive. These flows will be released into the North water quality pond. Any flows bypassed from the storm system will enter Bent Grass Meadows Drive and travel east to an existing storm sewer system. The second future storm system will consist of an area inlet to collect flows before entering the existing channel. This system will release directly into the proposed north WQCV pond. The stub will be installed with this filing along with the pond construction.

The first proposed system has been designed for the area west of Bent Grass Meadows Drive and south of Daelyn Drive. The system is proposed to tie to the existing system (Storm System A), which was designed with Falcon Meadows at Bent Grass Filing No. 1. The system will connect to the existing stub from the manhole connecting existing inlets at **DP 16 and DP 14**. Flows intercepted by inlets will be released into the existing South water quality pond. All design calculations (StormCAD, inlet design & street capacity spreadsheets, etc.) have been included in Appendix C for this system.

The second proposed storm system (Storm System B) collects flows north of Bent Grass Meadows Drive, over to a "ridge line" located between Henzlee Place and the western property boundary. These flows are routed through the proposed development, with captured flows releasing into the proposed North water quality pond. Flows not intercepted from this area, reach the existing sump inlet at DP 8, which releases into the existing WQCV pond in Bent Grass Filing No. 2.

The inlets located within Bent Grass Meadows Drive (DP-8, DP-24, and DP-25) were all designed under the FDR for Bent Grass Residential Filing No. 2. The inlets were "rechecked" based on updated flows reaching each of these design points. The analysis of these inlets is included in Appendix C.

Final drainage reports for future filings will include details concerning inlet location, street capacity, storm sewer sizing, outlet protection and location for the future storm systems.

## X. Proposed Water Quality Detention Ponds

One Water Quality Capture Volume Detention Ponds will be provided for the Falcon Meadows Filing No. 2 site. There are two additional existing ponds built to help treat flows from this and future development, WQCV pond North in Bent Grass Filing No. 2 and existing south WQCV pond in Falcon Meadows at Bent Grass Filing No. 1. All ponds are private. These detention ponds will only provide water quality. The EURV and 100-year volumes will be conveyed via the emergency overflow weir, which will be lined. The water quality volume release will be controlled with an orifice plate that will release in 40 hours. The north water quality pond will release into RWT204 and the south will release into RWT210. Final design of the north pond and its components are provided in Appendix D. The existing South Pond was analyzed with respect to the flows of the tributary basin areas. Based on the provided pond calculations, it was determined the pond design within the approved grading and erosion control plans for Falcon Meadows at Bent Grass Filing No. 1 (Final Grading Erosion Control Plans, Falcon Meadows at Bent Grass Filing No. 1, by Galloway and Company, Inc. approved 09/28/2021) is in conformance with the required volume. Analysis of the existing South Pond has also been included in Appendix D.

There are two basins which are not provided with on-site water quality, as stated previously. Basins B-1 and B-2 (combined area of 8.87 acres) represents the area of the West Tributary Channel (RWT204/RWT210) for the Falcon Basin as it traverses the project site. As these areas are undeveloped, will remain undeveloped, and release onto undeveloped land (continuation of channel reach RWT210), they do not "count" towards the 1 acre of area being able to be released untreated from the site.

Total area which will not be treated via on-site facilities is less than 1.0 acre, as required.

#### XI. Channel and Swales

#### **Swales**

There are 5 swales associated with the proposed development, 3 existing (Swale C, E & F), 1 proposed (Swale D) and 1 temporary (Swale B). The swales have been designed to meet the 100-year design storm. Appendix C contains the analysis of these facilities. Swale E was designed in the FDR for Bent Grass Residential Filing No. 2 and Swales C & F were designed in the FDR for Falcon Meadows at Bent Grass Filing No. 1. The capacities of existing Swales C & F were analyzed based on the flows of the tributary basin areas. Based on the swale cross sections (sheet G5.1 – see Appendix C) within the approved grading and erosion control plans for Falcon Meadows at Bent Grass Filing No. 1 (*Final Grading Erosion Control Plans, Falcon Meadows at Bent Grass Filing No. 1*, by Galloway and Company, Inc. approved 09/28/2021), it was determined the approved swale configuration has adequate capacity to convey increased runoff from the upstream tributary area as outlined in this report while still maintaining the required freeboard.

Swale D is located along the west boundary of the site and will convey flows to the south towards existing Swale E. The swale will be a trapezoidal ditch with a bottom width of 2', minimum depth of 2.5' and 4:1 side slope. Longitudinal slope will be 2.0%, generating a flow depth of 1.58' and a velocity of 4.81 fps. Flows ultimately reach the existing South water quality pond.

Swale B connects the temporary turnaround for Daelyn Drive to the temporary turnaround for Henzlee Place. This swale is a temporary facility, until Falcon Meadows at Bent Grass Filing No. 3 is constructed. The swale will be a v-ditch with a minimum depth of 3.5' and 4:1 side slope. Longitudinal slope will be 1.0%, generating a flow depth of 1.27' and a velocity of 3.08 fps. Flows ultimately reach the proposed North water quality pond.

Refer to Appendix C for swale design calculations.

#### Channel

With the proposed development of Falcon Meadows at Bent Grass Filing No. 2, there is no encroachment (50' undisturbed buffer from FEMA floodplain) into the existing channel reaches RWT204/RWT210. It is intended to leave the channel in its existing condition, until development occurs adjacent to the channel (Future filing). Reach RWT204 does not lie within the FEMA 100-year floodplain. This development will define the 100-year floodplain into Tract H. Future development will reroute RWT204 into this tract.

Riprap protection will be provided at the north pond outfall from the site into the channel to prevent scouring from the point discharge.

The MDDP identifies the use of check structures for the RWT210 channel downstream of the site. Again, due to the existing stability of the channel and the minor increase in flows, velocities and Froude numbers have only slightly changed, but channel remains stable. Design of the channel will under a separate cover.

#### XII. Maintenance

The channel is to be a private facility until all DBPS identified improvements are complete. Once the DBPS improvements are completed, maintenance for the channel will transition to El Paso County. The

proposed water quality pond is to be privately maintained. Private facilities will be maintained by the Bent Grass Metropolitan District. After completion of construction and upon the Board of County Commissioners acceptance, all public drainage facilities within easements and public Right-of-Way will be owned and maintained by El Paso County. Channel improvements will be considered under the final drainage report for the channel improvement design package.

## XIII. Wetlands Mitigation

No wetlands are located on site.

### XIV. Floodplain Statement

A portion of the project site lies within Zone AE Special Flood Hazard Area as defined by the FIRM Map number 08041C0553G effective December 7, 2018. A copy of the FIRM Panel is included in Appendix A.

The portion of channel that has a floodplain designation is only the RWT210 and RWT204 portions of the channel. It is unknown why the western channel, RWT202 is unmapped since it is the larger contributor regarding flow rates. Discussions have occurred with PPRBD and a no rise certificate will be required for the existing channel. Models have been obtained from FEMA which show that the FEMA discharges are higher than the DBPS. Therefore, the culvert crossing at Bent Grass Meadows Parkway was sized per the FEMA flows and not the DBPS. The no rise certification will be provided under a separate report, when channel improvements are addressed with future fillings.

## XV. Drainage/Bridge Fees and Credits/Reimbursements

The site lies within the Falcon Drainage Basin. The DBPS was approved in 2013 and has drainage and bridge fees associated with the basin.

The project site has a total area of 36.40 acres. The tracts account for a total of 20.46 acres, 108 residential lots are 11.30 acres and 4.64 acres of right-of-way. The following calculations for the imperviousness of this development have been computed as follows:

Average Residential lot size: 11.30 acres / 108 lots = 4560 sf/lot

Average lot imperviousness = 2000 sf

Average Residential imperviousness: 2000/4560 = 43.86%

ROW area is 100% impervious Open Space is 0% impervious

Average imperviousness for developed area:  $(0.4386 \times 11.30) + (1.0 \times 4.64) + (0 \times 20.46) / 36.40 = 0.2636$ 

36.40 acres x 26.36% = 9.60 Impervious Acres

Therefore, the drainage and bridge fees (2021) are:

Drainage:  $$31,885 \times 9.60 \text{ Imp. Acres} = $306,096.00$ 

Bridge: \$4,380 x 9.60 lmp. Acres = \$42,048.00

Per discussions with EI Paso County the fees will be offset by the cost of regional improvements. These regional improvements include the construction of Pond WU (\$489,284.78) and the construction of the channel (\$948,491.50). From the construction of the channel improvements

Bent Grass Residential Subdivision Filing No. 2 Final Drainage Report 2019 Original Drainage and Bridge Fees									
	Impervious Area (Ac.)	Fee/ Platted	Fee Due	Reimbursable Const. Costs	Fee Due at Platting	Drainage Fee Credit			
	Alea (AC.)	Acre		Corist. Costs	rialling	ree Cleal			
		Falco	on Drainage Fe	e Basin					
Drainage Fee	23.45	\$29,622	\$694,635.90	\$489,284.78	\$205,351.12	\$0.00			
Bridge Fee	23.45	\$95,418.05	\$0.00						
				\$489,284.78	\$300,769.17	\$0.00			

Falcon Meadows at Bent Grass Filing No. 1 Final Drainage Report										
	2021 Original Drainage and Bridge Fees									
	Impervious	Fee/	Fee Due	Reimbursable	Fee Due at	Drainage				
	Area (Ac.)	Platted		Const. Costs	Platting	Fee Credit				
		Acre								
		Falco	on Drainage Fe	e Basin						
Drainage										
Fee	5.73	\$31,885	\$182,701.05	\$948,491.50	\$0.00	\$765,790.45				
Bridge										
Fee										
	\$948,491.50 \$0.00 \$740,693.05									

	Falcon Meadows at Bent Grass Filing No. 2									
	Final Drainage Report									
	2021 Original Drainage and Bridge Fees									
	Impervious	Fee/	Fee Due	Reimbursable	Fee Due at	Drainage				
	Area (Ac.)	Platted		Const. Costs	Platting	Fee Credit				
		Acre								
		Falco	on Drainage Fe	e Basin						
Drainage										
Fee	9.60	\$31,885	\$306,096.00	\$0.00	\$0.00	\$434,597.05				
Bridge										
Fee										
	\$0.00 \$0.00 \$392,549.05									

Below is a cost estimate for the improvements proposed with this filing.

Item	Item Quantity Unit					Cost		
Storm Drain Improvements (Public)								
5' CDOT Type R Inlet (Public)	1	EA	\$	6,500.00	\$	6,500.00		
10' CDOT Type R Inlet (Public)	1	EA	\$	8,000.00	\$	8,000.00		
15' CDOT Type R Inlet (Public)	4	EA	\$	9,800.00	\$	39,200.00		
4' Manhole - Type II (Public)	8	EA	\$	3,000.00	\$	24,000.00		
5' Manhole - Type II (Public)	2	EA	\$	3,500.00	\$	7,000.00		
6' Manhole - Type II (Public)	1	EA	\$	4,000.00	\$	4,000.00		
7' Manhole - Type II (Public)	1	EA	\$	4,500.00	\$	4,500.00		
18" RCP Storm Drain (Public)	268	LF	\$	60.00	\$	16,080.00		
24" RCP Storm Drain (Public)	997	LF	\$	70.00	\$	69,790.00		
30" RCP Storm Drain (Public)	137	LF	\$	95.00	\$	13,015.00		
36" RCP Storm Drain (Public)	44	LF	\$	135.00	\$	5,940.00		
42" RCP Storm Drain (Public)	60	LF	\$	160.00	\$	9,600.00		
18" FES	1	EA	\$	750.00	\$	750.00		
Subtotal					\$	208,375.00		
WQCV Detention Ponds (Private)								
Pond (North)	1	EA	\$	80,000.00	\$	80,000.00		
Subtotal					\$	80,000.00		
Total					\$	288,375.00		
Contingency				10%	\$	28,837.50		
Grand Total					\$	317,212.50		

#### XVI. Conclusion

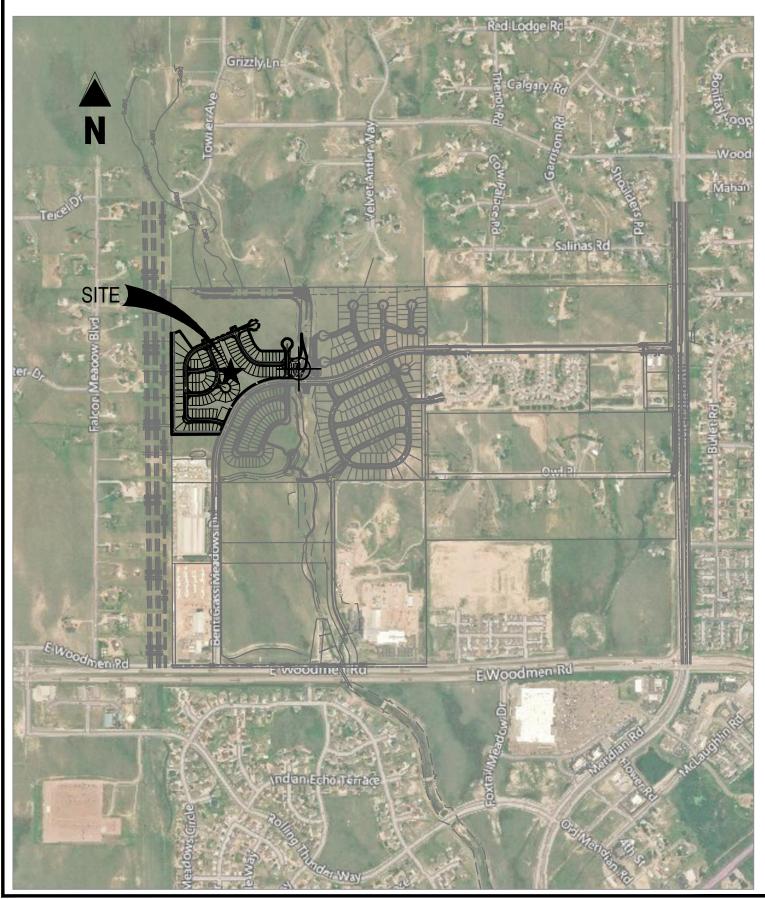
The Bent Grass Residential Subdivision lies within the West Tributary of the Falcon Area Watershed. Detention for the site is provided in two existing and one proposed on-site WQCV ponds to provide water quality for the entire tributary area. The proposed development will not have any adverse impacts on downstream developments or existing drainageways.

All drainage facilities within this report were sized according to the Drainage Criteria Manuals. Bent Grass Metropolitan District will own and maintain the channels until such a time that all final improvements have been constructed. At that time, channel corridors will become publicly owned and maintained and shall be the responsibility of El Paso County. Upon development of future filings within the Bent Grass Residential Subdivision, separate Final Drainage Reports will be required to be submitted and approved by El Paso County.

#### XVII. References

- 1. City of Colorado Springs/County of El Paso Drainage Criteria Manual, October 1991.
- 2. Drainage Criteria Manual, Volume 2, City of Colorado Springs, November 2002.
- 3. *Urban Storm Drainage Criteria Manual*, Urban Drainage and Flood Control District, January 2016 (with current revisions).
- 4. Falcon Drainage Basin Planning Study, by Matrix Design Group, September 2015.
- 5. Master Development Drainage Plan and Preliminary Drainage Plan Bent Grass Subdivision, by Kiowa Engineering Corporation, December 2006.
- 6. Final Drainage Report for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2014.
- 7. Final Drainage Report Addendum for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2015.
- 8. *Master Development Drainage Plan for The Ranch*, by Classic Consulting Engineers & Surveyors, LLC, November 2018.
- 9. Falcon Highlands Master Development Drainage Plan & Preliminary Drainage Report & Final Drainage Report for Filing 1, by URS, January 2005.
- Final Drainage Report and Erosion Control Plan Latigo Business Center Filing No. 1 A Resubdivision of a Portion of Latigo Business and Research Center Filing No. 1, by Kiowa Engineering Corporation, November 2004.
- 11. Final Drainage Report Latigo Business Center Filing No. 2, by Kiowa Engineering Corporation, Revised December 13, 2007.
- 12. Final Drainage Report for Bent Grass Residential (Filing No. 2), by Galloway & Company, May 2020.
- 13. Preliminary Drainage Report-Falcon Meadows at Bent Grass, by Galloway & Company, February 2021.
- 14. Final Drainage Report for Falcon Meadows at Bent Grass Filing No. 1, by Galloway & Company, under review.
- 15. Final Grading Erosion Control Plans, Falcon Meadows at Bent Grass Filing No. 1, by Galloway and Company, Inc. approved 09/28/2021.

# APPENDIX A Exhibits and Figures



FALCON MEADOWS AT BENT GRASS FILING NO. 2

BENT GRASS MEADOWS DRIVE

SCALE: 1"=1,000'

VICINITY MAP

 Project No:
 CLH000018.20

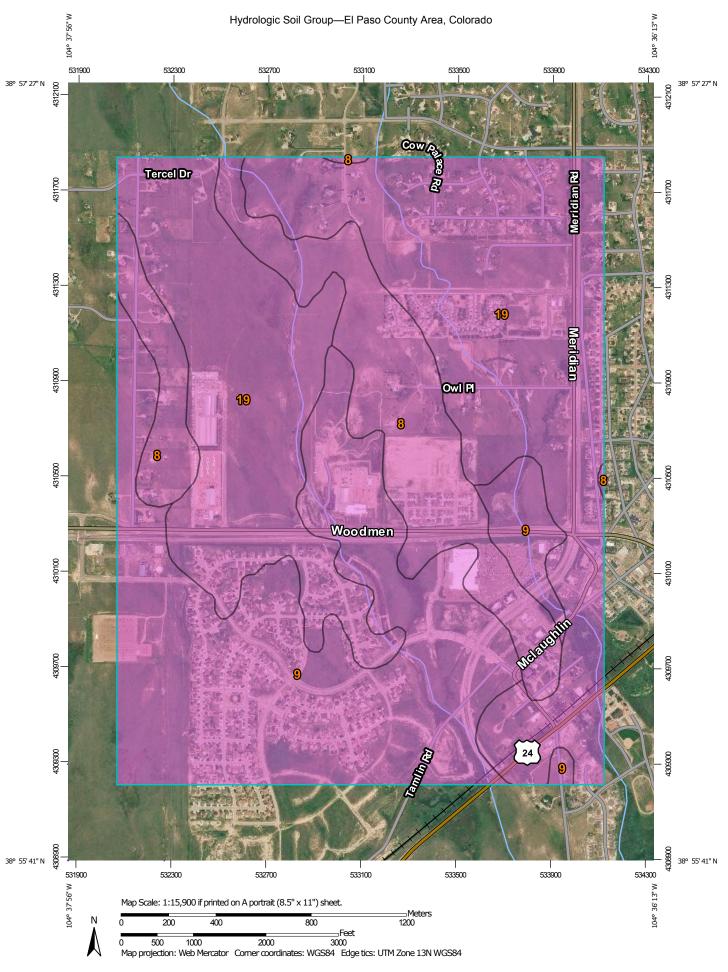
 Drawn By:
 TJE

 Checked By:
 CMD

 Date:
 06/19/2020



1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920 719.900.7220 • GallowayUS.com



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Please rely on the bar scale on each map sheet for map Soils D measurements. Soil Rating Polygons Not rated or not available Α Source of Map: Natural Resources Conservation Service Web Soil Survey URL: **Water Features** A/D Coordinate System: Web Mercator (EPSG:3857) Streams and Canals В Maps from the Web Soil Survey are based on the Web Mercator Transportation projection, which preserves direction and shape but distorts B/D Rails --distance and area. A projection that preserves area, such as the С Albers equal-area conic projection, should be used if more Interstate Highways accurate calculations of distance or area are required. C/D **US Routes** This product is generated from the USDA-NRCS certified data as D Major Roads of the version date(s) listed below. Not rated or not available -Local Roads Soil Survey Area: El Paso County Area, Colorado Soil Rating Lines Survey Area Data: Version 16, Sep 10, 2018 Background Aerial Photography Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. A/D Date(s) aerial images were photographed: Jun 7, 2016—Aug 17, 2017 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor C/D shifting of map unit boundaries may be evident. D Not rated or not available **Soil Rating Points** Α A/D B/D

## **Hydrologic Soil Group**

	_			
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	А	214.3	16.0%
9	Blakeland-Fluvaquentic Haplaquolls	А	465.8	34.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	662.6	49.3%
Totals for Area of Inter	est	1,342.6	100.0%	

## **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

#### NOTES TO USERS

obtain more detailed information in areas where Base Flood Elevations (BFEs o obtain more detailed information in areas where Base Flood Elevations (BFEs didor floodways have been determined, users are encouraged to consult the Floo roffles and Floodway Data and/or Summary of Stillwater Elevations tables contains tithin the Flood Insurance Study (FIS) report that accompanies this FIRM. User hould be aware that BFEs shown on the FIRM represent rounded whole-for levations. These BFEs are intended for flood insurance rating purposes only an hould not be used as the sole source of flood elevation information. Accordingly considerations are sold to the sole source of flood elevation information. od elevation data presented in the FIS report should be utilized in conjunction w FIRM for purposes of construction and/or floodplain managemen

Coastal Base Flood Elevations shown on this map apply only landward of 0. North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be waver that coastal flood elevations are also provided in the Summary of Stillwate clevations table in the Flood Insurance Study report for this jurisdiction. Elevation thown in the Summary of Stillwater Elevations table should be used for construction. d/or floodplain management purposes when they are higher than the elevation own on this FIRM.

oundaries of the **floodways** were computed at cross sections and interpolate tween cross sections. The floodways were based on hydraulic considerations wit gard to requirements of the National Flood Insurance Program. Floodway to do ther pertinent floodway data are provided in the Flood insurance Study repo

The projection used in the preparation of this map was Universal Transvers Mercator (UTM) zone 13. The horizontal datum was NADB3, GRS80 spheroic Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positions differences in map features across jurisdiction boundaries. These differences do no affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure am argound elevations referenced to the same verifical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following nerforess:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Iver Spring, MD 20910-3282

o obtain current elevation, description, and/or location information for **bench mar** hown on this map, please contact the Information Services Branch of the Natio leodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Pas County, Colorado Springs Utilities, City of Fountain, Bureau of Land Managemen National Oceanic and Atmospheric Administration, United States Geological Survey and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations an floodplain delineations than those shown on the previous FIRM for this jurisdiction for floodplains and floodways that were transferred from the previous FIRM manave been adjusted to conform to these new stream channel configurations. As result, the Flood Profles and Floodway Data tables in the Flood Insurance Stud suit, rine ricota ricinies and ricotavay Data latines in the ricota insurance study peport (which contains authoritistive hydraulic data) may reflect stream channel stances that differ from what is shown on this map. The profile baselines depicted this map represent the hydraulic modeling baselines that match the flood profile this map represent the hydraulic modeling baselines that when the flood profile depicts are some stream of the profile selficies may deviate significantly from the new base map channel representation. nd may appear outside of the floodplair

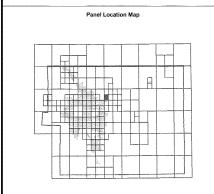
orporate limits shown on this map are based on the best data available at the tim publication. Because changes due to annexations or de-annexations may hav courred after this map was published, map users should contact appropriat ommunity officials to verify current corporate limit locations.

lease refer to the separately printed Map Index for an overview map of the count howing the layout of map panels; community map repository addresses; and a string of Communities table containing National Flood Insurance Program dates fo ach community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchang (FMIX) 1-877-336-2627 for information on available products associated with this FIRM, Available products may include previously issued Letters of Map Change, Flood Insurance Study Report, and/or digital versions of this map. The MSC mails be reached by Fax at 1-800-358-9620 and its website a http://www.msc.lena.gov/.

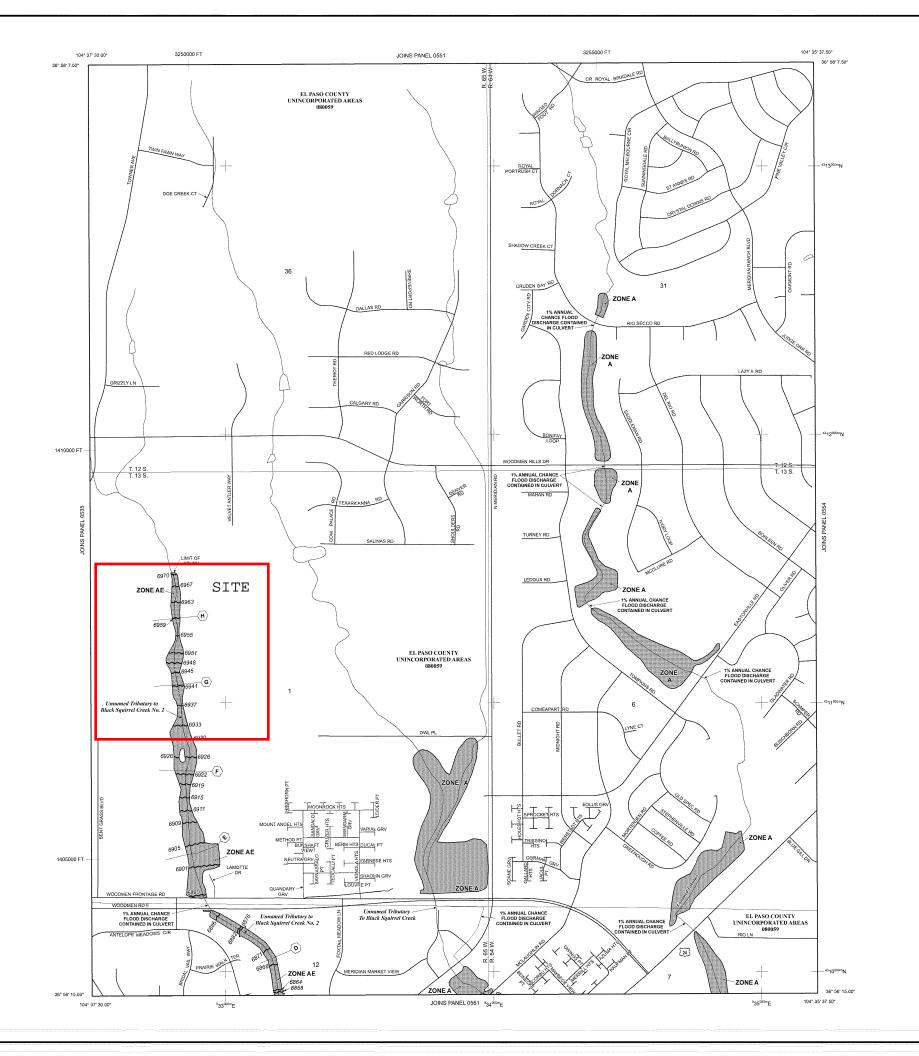
you have **questions about this map** or questions concerning the National Floc isurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) ( sit the FEMA website at http://www.fema.gov/business/nfip.

## El Paso County Vertical Datum Offset Table Flooding Source REFER TO SECTION 3.3 OF THE EL PASC FOR STREAM BY STREAM VERTICAL D



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Apaco





#### LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood tazard include Zones A, AE, AH, AD, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

No Base Flood Elevations determined.
Base Flood Elevations determined.
Flood depths of 1 to 3 feet (usuality areas of ponding); Base Flood
Elevations determined.

Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodway boundary

Zone D Boundary CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

~~ 513 ~~ Base Flood Elevation line and value; elevation in feet Base Flood Elevation value where uniform within zone; elevation in feet\*

 $\begin{picture}(100,0) \put(0,0){\line} \put(0,0){\li$ 

(23)-----(23)

97° 07' 30.00° 32° 22' 30.00° Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

\_ M1.5

MAP REPOSITORIES Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elev Special Flood Hazard Areas, to update map format, to add roads and road na incorporate previously issued Letters of Map Revision.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'

250 0 500 1000 FEET 

PANEL 0553G

FIRM FLOOD INSURANCE RATE MAP

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 553 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COMMUNITY NUMBER PANEL SUFFIX



MAP REVISED

MAP NUMBER

08041C0553G DECEMBER 7, 2018 Federal Emergency Management Agency

# APPENDIX B Hydrologic Computations

#### Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: CMWJ Galloway & Co. Company: \*\*\*Design Storm: 1-Hour Rain Depth WQCV Event 0.60 May 27, 2021 inches Date: ···Minor Storm: 1-Hour Rain Depth 5-Year Event 1.50 inches Project: Falcon Meadows at Bent Grass Filing No. 2 100-Year Event 2.52 North WQ Pond \*\*\*Major Storm: 1-Hour Rain Depth inches Location: Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency 100-Year Event Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier C-1a C-1b C-1d C-1e C-2 C-3 D-1a Receiving Pervious Area Soil Type Sandy Loam Sandy Loam Sandy Loar andy Loam Sandy Loam Sandy Loam Sandy Loam Sandy Loam Sandy Loam Sandy Loan Sandy Loam Sandy Loan Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 0.380 0.450 1.770 1.720 0.290 0.080 3.980 0.180 2.670 0.600 2.970 1.610 Directly Connected Impervious Area (DCIA, acres) 0.150 0.100 0.630 1.720 0.290 0.080 0.000 0.140 2.670 0.000 0.110 0.110 0.000 0.000 Unconnected Impervious Area (UIA, acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 Receiving Pervious Area (RPA, acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 Separate Pervious Area (SPA, acres) 0.230 0.350 1.140 0.000 0.000 0.000 3.980 0.040 0.000 0.600 2.860 1.500 RPA Treatment Type: Conveyance (C) С С С С С С С С ٧ С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 0.380 0.450 1.770 1.720 0.290 0.080 3.980 0.180 2.670 0.600 2.970 1.610 Directly Connected Impervious Area (DCIA. %) 39.5% 22.2% 35.6% 100.0% 100.0% 100.0% 0.0% 77.8% 100.0% 0.0% 3.7% 6.8% Unconnected Impervious Area (UIA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Receiving Pervious Area (RPA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Separate Pervious Area (SPA, %) 77.8% 64.4% 0.0% 0.0% 0.0% 100.0% 22.2% 0.0% 100.0% 96.3% 93.2% 60.5% A<sub>R</sub> (RPA / UIA) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1 000 1 000 I, Check 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 f / I for WQCV Event: 1.7 1.7 1.7 1.7 1.7 1.7 f / I for 5-Year Event: 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 f / I for 100-Year Event: 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP: IRF for WQCV Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.00 1.00 1.00 IRE for 5-Year Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP: Total Site Imperviousness: Inter-39.5% 22.2% 35.6% 100.0% 100.0% 100.0% 0.0% 77.8% 100.0% 0.0% 3.7% 6.8% Effective Imperviousness for WQCV Event: 22.2% 35.6% 100.0% 100.0% 100.0% 0.0% 77.8% 100.0% 0.0% 3.7% 6.8% Effective Imperviousness for 5-Year Event: 39.5% 22.2% 35.6% 100.0% 100.0% 100.0% 0.0% 77.8% 100.0% 0.0% 3.7% 6.8% 35.6% 100.0% 100.0% 100.0% 0.0% 77.8% 100.0% 0.0% 3.7% 6.8% Effective Imperviousness for 100-Year Event: 39.5% 22.2% Effective Imperviousness for Optional User Defined Storm CUHP. LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% N/A 0.0% N/A 0.0% N/A 0.0% 0.0% N/A This line only for 10-Year Event N/A 100-Year Event CREDIT\*\*: Reduce Detention By: 0.0% 0.2% 0.0% 0.0% 0.1% 0.3% N/A 0.1% 0.0% N/A 0.4% 0.2% N/A N/A User Defined CUHP CREDIT: Reduce Detention By 35.9% Total Site Imperviousness: Total Site Effective Imperviousness for WQCV Event: 35.9% Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 35.9% "Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: \*\*\* Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed Total Site Effective Imperviousness for Optional User Defined Storm CUHP.

CLH19\_IRF Calcs North Pond.xism, IRF

# **Historic Computations**

### **COMPOSITE % IMPERVIOUS CALCULATIONS: HISTORIC**

Subdivision: Falcon Meadows at Bent Grass Filing No. 2

Location: CO, Colorado Springs Project No.: CLH000019.20

Calculated By: CMWJ

Checked By:

**Date:** 4/15/21

		Pa	ved/Dirt Ro	oads		Lawns			Roofs		Basins Total
Basin ID	Total Area (ac)	% lmp.	Area (ac)	Weighted % Imp.	% lmp.	Area (ac)	Weighted % Imp.	% lmp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
A-1	5.42	100	0.16	3.00	2	5.26	1.90	90	0.00	0.00	4.9
A-2	18.00	100	0.00	0.00	2	18.00	2.00	90	0.00	0.00	2.0
A-3	19.59	100	0.00	0.00	2	19.59	2.00	90	0.00	0.00	2.0
A-4	23.81	100	0.57	2.40	2	23.12	1.90	90	0.12	0.50	4.8
B-1	32.53	100	0.00	0.00	2	32.53	2.00	90	0.00	0.00	2.0
B-2	4.51	100	0.00	0.00	2	4.51	2.00	90	0.00	0.00	2.0
B-3	16.18	100	1.00	6.20	2	15.18	1.90	90	0.00	0.00	8.1
OS-1	13.06	100	0.84	6.40	2	11.65	1.80	90	0.57	3.90	12.1
OS-2	17.81	100	2.00	11.20	2	15.18	1.70	90	0.63	3.20	16.1
OS-4	30.69	100	1.42	4.60	2	28.41	1.90	90	0.86	2.50	9.0
OS-5	14.13	100	0.17	1.20	2	13.74	1.90	90	0.22	1.40	4.5
OS-6	5.81	100	0.00	0.00	2	5.81	2.00	90	0.00	0.00	2.0

CLH19\_Hist-Drainage Calcs.xls Page 1 of 1 8/4/2021

## COMPOSITE RUNOFF COEFFICIENT CALCULATIONS: HISTORIC

Subdivision: Falcon Meadows at Bent Grass Filing No. 2

Location:CO, Colorado SpringsProject No.:CLH000019.20Calculated By:CMWJ

Checked By:

**Date:** 4/15/21

		P	aved Road	ds	Lawr	ns/Undeve	loped		Roofs	_	Composite	Composite
Basin ID	Total Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>
A-1	5.42	0.90	0.96	0.16	0.09	0.36	5.26	0.73	0.81	0.00	0.11	0.38
A-2	18.00	0.90	0.96	0.00	0.09	0.36	18.00	0.73	0.81	0.00	0.09	0.36
A-3	19.59	0.90	0.96	0.00	0.09	0.36	19.59	0.73	0.81	0.00	0.09	0.36
A-4	23.81	0.90	0.96	0.57	0.09	0.36	23.12	0.73	0.81	0.12	0.11	0.38
B-1	32.53	0.90	0.96	0.00	0.09	0.36	32.53	0.73	0.81	0.00	0.09	0.36
B-2	4.51	0.90	0.96	0.00	0.09	0.36	4.51	0.73	0.81	0.00	0.09	0.36
B-3	16.18	0.90	0.96	1.00	0.09	0.36	15.18	0.73	0.81	0.00	0.14	0.40
OS-1	13.06	0.90	0.96	0.84	0.09	0.36	11.65	0.73	0.81	0.57	0.17	0.42
OS-2	17.81	0.90	0.96	2.00	0.09	0.36	15.18	0.73	0.81	0.63	0.20	0.44
OS-4	30.69	0.90	0.96	1.42	0.09	0.36	28.41	0.73	0.81	0.86	0.15	0.40
OS-5	14.13	0.90	0.96	0.17	0.09	0.36	13.74	0.73	0.81	0.22	0.11	0.37
OS-6	5.81	0.90	0.96	0.00	0.09	0.36	5.81	0.73	0.81	0.00	0.09	0.36

C values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. (Referencing UDFCD 2001)

# STANDARD FORM SF-2: HISTORIC TIME OF CONCENTRATION

Subdivision: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass Filing No. 2

Project No.: CLH000019.20

Calculated By: CMWJ

Checked By:

**Date:** 4/15/21

		SUB-B	ASIN			INITIA	L/OVER	LAND		TR	AVEL TI	ME			Tc CHECK		
		DA	TA				$(T_i)$		$(\mathbf{T}_{\mathbf{t}})$					(UR	BANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>100</sub>	C <sub>5</sub>	L	S	T <sub>i</sub>	L	S	Cv	VEL.	T <sub>t</sub>	COMP. T <sub>c</sub>	TOTAL	Urbanized T <sub>c</sub>	$T_c$
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT)	(MIN)	(MIN)
A-1	5.42	A	4.90	0.38	0.11	300	2.5	23.0	466	2.5	15.0	2.4	3.3	26.3	766.0	14.3	14.3
A-2	18.00	A	2.00	0.36	0.09	300	2.4	23.9	1130	2.0	15.0	2.1	8.9	32.8	1430.0	17.9	17.9
A-3	19.59	A	2.00	0.36	0.09	300	2.7	23.0	760	2.7	15.0	2.5	5.1	28.1	1060.0	15.9	15.9
A-4	23.81	A	4.80	0.38	0.11	300	2.0	24.9	1500	2.0	15.0	2.1	11.8	36.6	1800.0	20.0	20.0
B-1	32.53	A	2.00	0.36	0.09	300	2.6	23.3	1100	2.6	15.0	2.4	7.6	30.9	1400.0	17.8	17.8
B-2	4.51	A	2.00	0.36	0.09	300	3.0	22.2	323	5.0	15.0	3.4	1.6	23.8	623.0	13.5	13.5
B-3	16.18	A	8.10	0.40	0.14	300	2.9	21.4	780	2.9	15.0	2.6	5.1	26.4	1080.0	16.0	16.0
OS-1	13.06	A	12.10	0.42	0.17	300	2.5	21.7	1420	2.5	15.0	2.4	10.0	31.7	1720.0	19.6	19.6
OS-2	17.81	A	16.10	0.44	0.20	300	2.3	21.6	1370	2.3	15.0	2.3	10.0	31.6	1670.0	19.3	19.3
OS-4	30.69	A	9.00	0.40	0.15	300	2.3	22.9	2600	2.3	15.0	2.3	19.0	42.0	2900.0	26.1	26.1
OS-5	14.13	A	4.50	0.37	0.11	300	2.5	23.1	1400	3.0	15.0	2.6	9.0	32.1	1700.0	19.4	19.4
OS-6	5.81	A	2.00	0.36	0.09	300	2.0	25.4	400	2.0	15.0	2.1	3.1	28.6	700.0	13.9	13.9

#### NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$ , S in ft/ft

T<sub>t</sub>=L/60V (Velocity From Fig. 501)

Velocity V=Cv\*S^0.5, S in ft/ft

Tc Check = 10 + L/180

For Urbanized basins a minimum T<sub>c</sub> of 5.0 minutes is required.

For non-urbanized basins a minimum T<sub>c</sub> of 10.0 minutes is required

CLH19\_Hist-Drainage Calcs.xls Page 1 of 1 8/4/2021

## STANDARD FORM SF-3: HISTORIC

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	<b>Project Name:</b> Falcon Meadows at Bent Grass Filing No. 2
Subdivision: Falcon Meadows at Bent Grass	Project No.: CLH000019.20
Location: CO, Colorado Springs	Calculated By: CMWJ
Design Storm: 5-Year	Checked By:
	<b>Date:</b> $4/15/21$

		DIDLOG DANIOTE																			
		DIRECT RUNOFF							TOTAL RUNOFF				STREET			PIPE		TRAVEL TIME			
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		OS-1	13.06	0.17	19.6	2.22	3.12	6.9													
		A-1	5.42	0.11	14.3	0.62	3.60	2.2													
	1								19.6	2.84	3.12	8.9									Total flow going offsite to Bent Grass F1 Residential
		OS-2	17.81	0.20	19.3	3.63	3.14	11.4													
		A-2	18.00	0.09	17.9	1.62	3.25	5.3													
	2								19.3	5.25	3.14	16.5									Total Flow entering Junction of RWT202&204
	3	A-3	19.59	0.09	15.9	1.76	3.43	6.0													
		OS-4	30.69	0.15	26.1	4.46	2.69	12.0													
		A-4	23.81	0.11	20.0	2.68	3.09	8.3													
	4								26.1	7.14	2.69	19.2									
	5	B-1	32.53	0.09	17.8	2.93	3.27	9.6													
	6	B-2	4.51	0.09	13.5	0.41	3.68	1.5													
	7	B-3	16.18	0.14	16.0	2.27	3.42	7.8													D. I. DIVITO 4 & D NITO O. D. M DDDC
	8							29.0													Reach RWT204 & Basin WT200 - Per Matrix DBPS Existing Hydrology
	9							14.0													RWT202 - Per Matrix DBPS Existing Hydrology
	10							32.0													RWT210 - Per Matrix DBPS Existing Hydrology
	20							98.1													Flows into Basin OS-5 from Bent Grass Filing No. 3
	1	OS-5	14.13	0.11	19.4	1.55	3.13	4.9													
	11											103.0									Flows into Basin OS-6
	1	OS-6	5.81	0.09	13.9	0.52	3.64	1.9													Existing Sediment Bond in Bosin and then States
	12											104.8									Existing Sediment Pond in Basin and then flows to Bent Grass Meadows Drive

CLH19\_Hist-Drainage Calcs.xls

# STANDARD FORM SF-3: HISTORIC STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Falcon Meadows at Bent Grass Filing No. 2
Subdivision: Falcon Meadows at Bent Grass	Project No.: CLH000019.20
Location: CO, Colorado Springs	Calculated By: CMWJ
Design Storm: 100-Year	Checked By:
	<b>Date:</b> 4/15/21

			]	DIRECT RUNOFF				1	OTAL	RUNO	FF	STF	REET		PIPE		TRA	VEL T	ГІМЕ		
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		OS-1	13.06	0.42	19.6	5.46	5.24	28.6													
		A-1	5.42			2.05	6.04	12.4													
	1	Α-1	3.42	0.36	14.3	2.03	0.04	12.4	10.6	7.51	5.24	39.4									Total Communication of City to Day Communication
	1								19.6	7.51	5.24	39.4									Total flow going offsite to Bent Grass F1 Residential
		OS-2	17.81	0.44	19.3	7.90	5.28	41.7													
		A-2	18.00	0.36	17.9	6.48	5.46	35.4													
	2								19.3	14.38	5.28	75.9	)								Total Flow entering Junction of RWT202&204
	3	A-3	19.59	0.36	15.9	7.05	5.77	40.7													
		OS-4	30.69	0.40	26.1	12.29	4.51	55.4													
		A-4	23.81	0.38	20.0	8.97	5.19	46.6													
	4								26.1	21.26	4.51	95.9									
	5	B-1	32.53	0.36	17.8	11.71	5.48	64.2													
	6	B-2	4.51			1.62	6.18	10.0													
	7	B-3	16.18	0.40	16.0	6.42	5.75														Reach RWT204 & Basin WT200 - Per Matrix DBPS
								233.0													Existing Hydrology
	9							770													RWT202 - Per Matrix DBPS Existing Hydrology
	10							880													RWT210 - Per Matrix DBPS Existing Hydrology
	20							226													Flows into Basin OS-5 from Bent Grass Filing No. 3
		OS-5	14.13	0.37	19.4	5.29	5.26	27.8													
	11											253.8	3								Flows into Basin OS-6
		OS-6	5.81	0.36	13.9	2.09	6.10	12.7													
	12											266.6	5								Existing Sediment Pond in Basin and then flows to Bent Grass Meadows Drive

CLH19\_Hist-Drainage Calcs.xls

# **Existing Computations**

### COMPOSITE % IMPERVIOUS CALCULATIONS: CURRENT/EXISTING CONDITIONS

Subdivision: Falcon Meadows Location: CO, Colorado Springs Project Name: Falcon Meadows at Bent Grass Filing No. 2
Project No.: CLH000019

0.00

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Calculated By: TJE

Checked By: CMD

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Date: 12/3/21

1	2	3	4	5	6	7	8	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
		Pav	ved/Gravel R	oads	La	wns/Undevelo	ped	Res	sidential - 1/8	Acre	Res	idential - 1/4	Acre	Res	idential - 1/3 A	Acre	Res	idential - 1/2	Acre	Re	sidential - 1 A	cre	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
B-1	6.78	100	0.00	0.0	2	6.78	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
B-2	4.16	100	0.00	0.0	2	4.16	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
D-4a	0.98	100	0.21	21.4	2	0.00	0.0	65.0	0.77	51.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	72.5
D-4b	0.95	100	0.43	45.3	2	0.00	0.0	65.0	0.52	35.6	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.9
D-4c	1.22	100	0.43	35.2	2	0.24	0.4	65.0	0.55	29.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	64.9
D-5	1.08	100	0.22	20.4	2	0.11	0.2	65.0	0.75	45.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.7
D-6a	1.33	100	0.44	33.1	2	0.00	0.0	65.0	0.89	43.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	76.6
D-6b	2.69	100	0.59	21.9	2	0.00	0.0	65.0	2.10	50.7	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	72.6
D-7	7.65	100	0.00	0.0	2	6.22	1.6	65.0	1.43	12.2	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	13.8
D-8	1.69	100	0.00	0.0	2	0.11	0.1	65.0	1.58	60.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	60.9
E-1	1.71	100	0.78	45.6	2	0.23	0.3	65.0	0.00	0.0	40	0.70	16.4	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.3
E-2	0.68	100	0.56	82.4	2	0.12	0.4	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	82.8
E-3	0.78	100	0.69	88.5	2	0.09	0.2	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	88.7
E-4	0.91	100	0.73	80.2	2	0.18	0.4	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.6
E-5	0.89	100	0.79	88.8	2	0.10	0.2	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	89.0
I-1	0.31	100	0.22	71.0	2	0.09	0.6	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	71.6
OS-1	32.28	100	2.15	6.7	2	29.25	1.8	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	11.0
OS-2	20.07	80	0.90	3.6	2	18.62	1.9	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
OS-3	10.61	80	0.48	3.6	2	9.84	1.9	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
OS-4	4.46	100	0.00	0.0	2	0.00	0.0	65.0	2.28	33.2	40	1.46	13.1	30	0.00	0.0	25	0.00	0.0	20	0.72	3.2	49.5
OS-5	0.46	100	0.00	0.0	2	0.00	0.0	65.0	0.46	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
OS-6	1.17	100	0.00	0.0	2	0.00	0.0	65.0	1.17	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
			_	,		•			1	_									, ,	•			
EX-1	1.19	100	0.00	0.0	2	1.19	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-2	1.60	100	0.00	0.0	2	1.60	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-3	0.66	100	0.00	0.0	2	0.66	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0

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Lot Type Id	entification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	1/8 Acre
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32 671 - 43 560	1 Acre

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1.63

EX-4

EX-5

EX-6

EX-7

EX-8

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% Impervious values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)

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12.18

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CLH19\_CUR-FDR-Drainage Calcs.xlsm Page 1 of 1 11/30/2021

#### COMPOSITE RUNOFF COEFFICIENT CALCULATIONS: CURRENT/EXISTING CONDITIONS

Subdivision: Falcon Meadows

Location: CO, Colorado Springs

**Project Name:** Falcon Meadows at Bent Grass Filing No. 2

Project No.: CLH000019

Calculated By: TJE

Checked By: CMD

**Date:** 12/3/21

Lawns/Undeveloped Residential - 1/4 Acre Paved/Gravel Roads Residential - 1/8 Acre Residential - 1/3 Acre Residential - 1/2 Acre Residential - 1 Acre Composite Basin ID Total Area (ac  $C_{100}$ Area (ac)  $C_5$  $C_{100}$ Area (ac) 0.25 6.78 0.90 0.09 0.36 6.78 0.73 0.81 0.45 0.30 0.50 0.00 0.00 0.22 0.20 0.44 0.00 B-1 0.96 0.00 0.00 0.59 0.00 0.47 0.46 0.00 0.09 0.36 B-2 4.16 0.90 0.96 0.00 0.09 0.36 4.16 0.73 0.81 0.00 0.45 0.59 0.00 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.09 0.36 D-4a 0.98 0.90 0.96 0.21 0.09 0.36 0.00 0.73 0.81 0.00 0.45 0.59 0.77 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.55 0.67 0.00 D-4b 0.95 0.90 0.96 0.43 0.09 0.36 0.00 0.73 0.81 0.00 0.45 0.59 0.52 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.65 0.76 0.54 D-4c 1.22 0.90 0.96 0.43 0.09 0.36 0.24 0.73 0.81 0.00 0.45 0.59 0.55 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.68 0.75 0.22 0.51 D-5 1.08 0.96 0.22 0.73 0.81 0.45 0.59 0.30 0.50 0.00 0.25 0.47 0.00 0.90 0.09 0.36 0.11 0.00 0.46 0.00 0.20 0.44 0.00 0.64 D-6a 1.33 0.90 0.96 0.44 0.09 0.36 0.00 0.73 0.81 0.00 0.45 0.59 0.89 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.60 0.71 0.30 0.55 D-6b 2.69 0.90 0.96 0.59 0.09 0.36 0.00 0.81 0.45 0.59 2.10 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.67 0.73 0.00 0.00 D-7 7.65 0.90 0.96 0.00 0.09 0.36 6.22 0.73 0.81 0.00 0.45 0.59 1.43 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.16 0.40 D-8 1.69 0.90 0.96 0.00 0.09 0.36 0.11 0.73 0.81 0.00 0.45 0.59 1.58 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.43 0.58 E-1 1.71 0.90 0.96 0.78 0.09 0.36 0.23 0.73 0.81 0.00 0.45 0.59 0.00 0.30 0.50 0.70 0.25 0.470.00 0.22 0.46 0.00 0.20 0.44 0.00 0.55 0.69 E-2 0.90 0.56 0.12 0.45 0.59 0.00 0.50 0.25 0.00 0.22 0.46 0.44 0.85 E-3 0.78 0.96 0.73 0.45 0.59 0.50 0.25 0.22 0.81 0.90 0.69 0.09 0.36 0.09 0.81 0.00 0.00 0.30 0.00 0.47 0.00 0.46 0.00 0.20 0.44 0.00 0.89 E-4 0.91 0.90 0.96 0.73 0.09 0.36 0.18 0.73 0.81 0.00 0.45 0.59 0.00 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.74 0.84 E-5 0.89 0.90 0.96 0.79 0.09 0.10 0.73 0.45 0.59 0.00 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.44 0.81 0.89 0.36 0.81 0.00 0.20 0.00 0.22 I-1 0.31 0.90 0.96 0.22 0.09 0.36 0.09 0.73 0.81 0.00 0.45 0.59 0.00 0.30 0.50 0.00 0.25 0.47 0.00 0.46 0.00 0.20 0.44 0.00 0.66 0.79 OS-1 32.28 0.90 0.96 2.15 0.36 29.25 0.73 0.81 0.88 0.45 0.59 0.00 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.16 0.41 0.09 OS-2 0.96 0.90 0.09 0.45 0.59 0.30 0.00 0.22 0.00 0.14 0.40 20.07 0.90 0.36 18.62 0.73 0.81 0.56 0.00 0.50 0.00 0.25 0.47 0.46 0.20 0.44 0.00 OS-3 10.61 0.90 0.96 0.48 0.09 0.36 9.84 0.73 0.81 0.30 0.45 0.59 0.00 0.30 0.50 0.00 0.25 0.47 0.00 0.22 0.46 0.00 0.20 0.44 0.00 0.14 0.40 2.28 0.22

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Lot Type Ide	entification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	= 1/8 Acre</th
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32 671 - 43 560	1 Acre

OS-4

OS-5

OS-6

EX-1

EX-2

EX-3

EX-4

EX-5

EX-6

EX-7

EX-8

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C values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001) Coeffficients use HSG A&B soils - Refer to "Appendix A: Exhibits and Figures" for soil map

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# STANDARD FORM SF-2: CURRENT/EXISTING CONDITIONS TIME OF CONCENTRATION

Subdivision: Falcon Meadows

Location: CO, Colorado Springs

**Project Name:** Falcon Meadows at Bent Grass Filing No. 2

Project No.: CLH000019

Calculated By: TJE

**Checked By:** CMD

**Date:** 12/3/21

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18

		SUB-B	ASIN			INITIA	L/OVER	LAND		TR	AVEL TI	ME			ζ		
		DAT	`A				$(T_i)$				$(T_t)$			(UR	BANIZED B.	ASINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S	T <sub>i</sub>	L	S	Cv	VEL.	T <sub>t</sub>	COMP. T <sub>c</sub>	TOTAL	Urbanized T <sub>c</sub>	T <sub>c</sub>
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT	(MIN)	(MIN)
B-1	6.78	A	2.0	0.09	0.36	90	6.4	9.5	2000	1.7	15	2.0	17.0	26.5	2090.0	21.6	21.6
B-2	4.16	A	2.0	0.09	0.36	160	11.0	10.5	920	1.6	15	1.9	8.1	18.6	1080.0	16.0	16.0
D-4a	0.98	A	72.5	0.55	0.67	100	2.3	7.6	420	1.0	20	2.0	3.5	11.1	520.0		11.1
D-4b	0.95	A	80.9	0.65	0.76	75	1.5	6.2	480	1.0	20	2.0	4.0	10.2	555.0	13.1	10.2
D-4c	1.22	A	64.9	0.54	0.68	70	0.5	10.8	690	1.0	20	2.0	5.8	16.6	760.0	14.2	14.2
D-5	1.08	A	65.7	0.51	0.64	100	2.0	8.6	300	1.1	20	2.1	2.4	11.0	400.0	12.2	11.0
D-6a	1.33	A	76.6	0.60	0.71	20	2.0	3.2	385	1.0	20	2.0	3.2		405.0	12.3	6.5
D-6b	2.69	A	72.6	0.55	0.67	45	2.0	5.4	870	1.0	20	2.0	7.3		915.0		12.6
D-7	7.65	A	13.8	0.16	0.40	200	7.5	12.4	665	1.0	15	1.5	7.4	19.8	865.0	14.8	14.8
D-8	1.69	A	60.9	0.43	0.58	125	3.7	8.9	600	1.0	15	1.5	6.7	15.5	725.0	14.0	14.0
E-1	1.71	A	62.3	0.55	0.69	25	2.0	4.0	940	1.0	20	2.0	7.8	11.8	965.0	15.4	11.8
E-2	0.68	A	82.8	0.76	0.85	25	2.0	2.5	665	1.6	20	2.5	4.4	6.9	690.0	13.8	6.9
E-3	0.78	A	88.7	0.81	0.89	25	2.0	2.1	632	1.0	20	2.0	5.3	7.4	657.0	13.7	7.4
E-4	0.91	A	80.6	0.74	0.84	25	2.0	2.6	913	2.0	20	2.8	5.4	8.0	938.0	15.2	8.0
E-5	0.89	A	89.0	0.81	0.89	25	2.0	2.1	903	2.1	20	2.9	5.2		928.0	15.2	7.3
I-1	0.31	A	71.6	0.66	0.79	25	2.0	3.2	135	2.0	20	2.8	0.8	4.0	160.0		5.0
OS-1	32.28	A	11.0	0.16	0.41	100	2.4	12.9	2100	2.2	15	2.2	15.7	28.6	2200.0	22.2	22.2
OS-2	20.07	A	8.0	0.14	0.40	100	2.3	13.3	1400	2.3	15	2.3	10.3	23.6	1500.0	18.3	18.3
OS-3	10.61	A	8.0	0.14	0.40	100	2.0	14.0	1500	2.0	15	2.1	11.8	25.7	1600.0	18.9	18.9
OS-4	4.46	A	49.5	0.36	0.54	100	2.0	10.8	910	1.2	20	2.2	6.9	17.7	1010.0	15.6	15.6
OS-5	0.46	A	65.0	0.45	0.59	15	2.0	3.7	190	1.0	20	2.0	1.6		205.0	11.1	5.2
OS-6	1.17	A	65.0	0.45	0.59	85	0.2	18.7	430	0.9	20	1.9	3.8	22.5	515.0	12.9	12.9
EX-1	1.19	A	2.0	0.09	0.36	300	2.7	23.0	690	2.7	15	2.5	4.7	27.7	990.0	15.5	15.5
EX-2	1.60	A	2.0	0.09	0.36	200	2.7	18.8	100	2.7	15	2.5	0.7	19.5	300.0	11.7	11.7
EX-3	0.66	A	2.0	0.09	0.36	100	5.0	10.8	30	2.7	15	2.5	0.2	11.0	130.0	10.7	10.7
EX-4	15.41	A	2.0	0.09	0.36	300	2.6	23.3	800	2.6	15	2.4	5.5	28.8	1100.0	16.1	16.1
EX-5	0.06	A	2.0	0.09	0.36	10	2.0	4.6	350	2.6	15	2.4	2.4	7.1	360.0	12.0	7.1
EX-6	4.78	A	2.0	0.09	0.36	300	2.3	24.3	1050	2.1	15	2.2	8.1	32.3	1350.0	17.5	17.5
EX-7	12.18	A	2.0	0.09	0.36	300	2.2	24.6	1300	2.0	15	2.1	10.2	34.8	1600.0	18.9	18.9

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
		SUB-B	ASIN			INITIA	L/OVER	LAND		TR	AVEL TI	ME			Tc CHECK	K	
		DAT	ſ <b>A</b>				$(T_i)$				$(T_t)$			(UF	RBANIZED B	ASINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S	T <sub>i</sub>	L	S	Cv	VEL.	T <sub>t</sub>	COMP. T <sub>c</sub>	TOTAL	Urbanized T <sub>c</sub>	T <sub>c</sub>
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT	(MIN)	(MIN)
EX-8	1.63	A	2.0	0.09	0.36	10	2.0	4.6	295	2.8	15	2.5	2.0	6.6	305.0	11.7	6.6

#### NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$ , S in ft/ft

T<sub>t</sub>=L/60V (Velocity From Fig. 501)

Velocity V=Cv\*S^0.5, S in ft/ft

Tc Check = 10+L/180

For Urbanized basins a minimum T<sub>c</sub> of 5.0 minutes is required.

For non-urbanized basins a minimum T<sub>c</sub> of 10.0 minutes is required

Type of Land Surface	Cv
Heavy Meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

CLH19\_CUR-FDR-Drainage Calcs.xlsm Page 2 of 2 11/30/2021

#### STANDARD FORM SF-3: CURRENT/EXISTING CONDITIONS STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision:	Falcon Meadows
Location:	CO, Colorado Springs
Docian Storm	5 Van

Project Name: Falcon Meadows at Bent Grass Filing No. 2
Project No.: CLH000019
Calculated By: TJE
Checked By: CMD
Date: 12/3/21

				DIRI	ECT RU	NOFF				ΓΟΤΑL	RUNOF	F	STR	REET		PIPI	Ε	TRA	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		RWT202	1574.40						46.6	120.88	1.82	220.0									From Falcon DBPS by Matrix
		RWT204	38.40						11.37	1.78	3.94	7.0									From Falcon DBPS by Matrix
	1	WT200	192.00						37.8	24.41	2.13	52.0									From Falcon DBPS by Matrix
	21	OS-1	32.28	0.16	22.2	5.16	2.93	15.1	46.6	152.23	1.82	277.1									Flows obtained from Bent Grass Filing No. 2 FDR. Q=65.1 CFS Cumulation of northern off-site flows entering Basin B-1
	1	OS-4	4.46	0.36	15.6	1.61	3.46	5.6					1.2	5.6				910	2.2	6.9	Flows from Basin B-1 of Bent Grass Filing No. 2 FDR into Basin EX-2
	2	OS-5	0.46	0.45	5.2	0.21	5.10	1.1					1	1.1				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR into Basin EX-2
	3	OS-6	1.17	0.45	12.9	0.53	3.75	2.0					0.9	2.0				430	1.9	3.8	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR into Basin EX-2
		EX-1	1.19	0.09	15.5	0.11	3.47	0.4													Flows to Basin EX-2
	5	EX-2	1.60	0.09	11.7	0.14	3.90	0.5	22.5	2.60	2.91	7.6									Flows to Basin EX-3
	7	E-3	0.78	0.81	7.4	0.63	4.59	2.9													
	6	EX-4	15.41	0.09	16.1	1.39	3.41	4.7					1	4.7				240	2.0	2.0	
		EX-5	0.06	0.09	7.1	0.01	4.65	0.0					1	0.0				475	2.0	4.0	
		E-2	0.68	0.76	6.9	0.52	4.70	2.4	18.1	1.92	3.24	6.2									Combination of EX-4, EX-5, E-2
	8	E-1	1.71	0.55	11.8	0.94	3.88	3.6	18.1	3.49	3.24	11.3									Combination of EX-4, EX-5, E-1, E-2, E-3. Flows to Basin EX-3
Existing Water Quality Detention Pond 1	15a	EX-3	0.66	0.09	10.7	0.06	4.02	0.2	22.5	6.15	2.91	17.9									Flows to Basin B-1
	AA	B-1	6.78	0.09	21.6	0.61	2.97	1.8	46.6	158.99	1.82	289.4									Passes through culvert under Bent Grass Meadows Dr to Basin B-2
		D-5	1.08	0.51	11.0	0.55	3.99	2.2					1.1	2.2				300	2.1	2.4	Overland flow into Basin D-6b
		D-6a	1.33	0.60	6.5	0.80	4.79	3.8													
	18	D-6b	2.69	0.55	12.6	1.48	3.78	5.6	13.3	2.83	3.70	10.5									
	17a	D-4a	0.98	0.55	11.1	0.54	3.97	2.1					1	2.1				650	2.0	5.4	Overland flow into Basin D-4b
	17b	D-4b	0.95	0.65	10.2	0.62	4.09	2.5	16.5	1.16	3.37	3.9									
	17c	D-4c	1.22	0.54	14.2	0.66	3.60	2.4	16.5	4.65	3.37	15.7									
	9	OS-2	20.07	0.14	18.3	2.81	3.22	9.0					2.5	9.0				700	3.2	3.7	Overland flow into Basin EX-6. Flow obtained from Bent Grass Filing No. 2 FDR Flow to DP10
	10	OS-3	10.61	0.14	18.9	1.49	3.18	4.7	22.0	4.30	2.94	12.6									Offsite flow into Basin EX-6. Flow obtained from Bent Grass Filing No. 2 FDR
		EX-6	4.78	0.09	17.5	0.43	3.29	1.4	22.0	4.73	2.94	13.9	0.5	1.4				450	1.4	5.3	Flow to DP11
	11	EX-7	12.18	0.09	18.9	1.10	3.18	3.5	22.0	5.83	2.94	17.1			17.1	1.0	42	942	2.0	7.9	Pipe flow to DP17
	17								22.0	10.48	2.94	30.8									Combination of DP17c and DP11, discharges into Basin D-7

CLH19\_CUR-FDR-Drainage Calcs.xlsm Page 1 of 2 11/30/2021

# STANDARD FORM SF-3: CURRENT/EXISTING CONDITIONS STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Falcon Meadows at Bent Grass Filing No. 2
Subdivision: Falcon Meadows	Project No.: CLH000019
Location: CO, Colorado Springs	Calculated By: TJE
Design Storm: 5-Year	Checked By: CMD
	Data: 12/2/21

				DIRE	CT RU	NOFF				FOTAL 1	RUNOF	F	STF	REET		PIPE		TRAV	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	12	EX-8	1.63	0.09	6.6	0.15	4.75	0.7						0.7				550	2.0	2.2	El . DDA D . E 4
													- 2	0.7				550	2.8		Flow to DP24, Basin E-4
		E-4	0.91	0.74	8.0	0.67	4.46	3.0													Flow into Ex inlet.
	24								9.8	0.82	4.15	3.4									
	25	E-5	0.89	0.81	7.3	0.72	4.60	3.3													Flow into Ex inlet.
	26								9.8	1.54	4.15	6.4									Flow in Swale F to pond in Basin D-7
	32	D-8	1.69	0.43	14.0	0.73	3.62	2.6													Flow in Swale C (Basin D-8) into proposed south pond
Pond South - Water Quality Detention Pond		D-7	7.65	0.16	14.8	1.22	3.54	4.3													
	30								22.0	13.97	2.94	41.1									Discharge to channel
		B-2	4.16	0.09	16.0	0.37	3.42	1.3													
	CC								46.6	172.96	1.82	314.8									Flows existing site in channel
		I-1	0.31	0.66	5.0	0.20	5.17	1.0			, and the second										Flows offsite south along Bent Grass Meadows Drive

Page 2 of 2 11/30/2021

### STANDARD FORM SF-3: CURRENT/EXISTING CONDITIONS STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision:	Falcon Meadows
Location:	CO, Colorado Springs
Design Storm:	100-Year

 Project Name:
 Falcon Meadows at Bent Grass Filing No. 2

 Project No.:
 CLH000019

 Calculated By:
 TJE

 Checked By:
 CMD

 Date:
 12/3/21

				DIRI	ECT RUI	NOFF				<b>FOTAL</b>	RUNOF	F	STR	EET		PIPE	1	TRA	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		RWT202	1574.40						46.6	327.87	3.05	1000.0									From Falcon DBPS by Matrix
		RWT204	38.40						11.37	6.51	6.61	43.0									From Falcon DBPS by Matrix
		WT200	192.00						37.8	53.07	3.58	190.0									From Falcon DBPS by Matrix
	21	OS-1	32.28	0.41	22.2	13.23	4.92	65.1	46.6	400.68	3.05	1222.1									Flows obtained from Bent Grass Filing No. 2 FDR. Q=65.1 CFS
	1	OS-4	4.46	0.54	15.6	2.41	5.81	14.0	40.0	400.00	3.03	1222.1	1.2	14.0				910	2.2	6.9	Cumulation of northern off-site flows entering Basin B-1 Flows from Basin B-1 of Bent Grass Filing No. 2 FDR into Basin EX-2
	2	OS-5	0.46	0.59	5.2	0.27	8.56	2.3					1	2.3				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR into Basin EX-2
	3	OS-6	1.17	0.59	12.9	0.69	6.30	4.3					0.9	4.3				430	1.9	3.8	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR into Basin EX-2
		EX-1	1.19	0.36	15.5	0.43	5.83	2.5													Flows to Basin EX-2
	5	EX-2	1.60	0.36	11.7	0.58	6.54	3.8	22.5	4.38	4.89	21.4									Flows to Basin EX-3
	7	E-3	0.78	0.89	7.4	0.69	7.70	5.3	22.0	1130		2									Flows to Bushi EXCS
	6	EX-4	15.41	0.36	16.1	5.55	5.73	31.8					1	31.8				240	2.0	2.0	
		EX-5	0.06	0.36	7.1	0.02	7.81	0.2					1	0.2				475	2.0	4.0	
		E-2	0.68	0.85	6.9	0.58	7.89	4.6	18.1	6.15	5.44	33.5									Combination of EX-4, EX-5, E-2
	8	E-1	1.71	0.69	11.8	1.18	6.51	7.7	18.1	8.02	5.44	43.6									Combination of EX-4, EX-5, E-1, E-2, E-3. Flows to Basin EX-3
Existing Water Quality Detention Pond 1	15a	EX-3	0.66	0.36	10.7	0.24	6.76	1.6	22.5	12.64	4.89	61.8									Flows to Basin B-1
	AA	B-1	6.78	0.36	21.6	2.44	4.99	12.2	46.6	415.76	3.05	1268.1									Passes through culvert under Bent Grass Meadows Dr to Basin B-2
	1.1.1	D-5	1.08	0.64	11.0	0.69	6.70	4.6	10.0	115.70	3.03	120011	1.1	4.6				300	2.1	2.4	Overland flow into Basin D-6b
		D-6a	1.33	0.71	6.5	0.94	8.03	7.5													
	18	D-6b	2.69	0.67	12.6	1.80	6.35	11.4	13.3	3.43	6.21	21.3									
	17a	D-4a	0.98	0.67	11.1	0.66	6.66	4.4	13.3	3113	0.21	21.0	1	4.4				650	2.0	5.4	Overland flow into Basin D-4b
	17b	D-4b	0.95	0.76	10.2	0.72	6.87	4.9	16.5	1.38	5.66	7.8									
	17c	D-4c	1.22	0.68	14.2	0.83	6.04	5.0	16.5	5.64	5.66	31.9									
	9	OS-2	20.07	0.40	18.3	8.03	5.41	43.4					2.5	43.4				700	3.2	3.7	Overland flow into Basin EX-6. Flow obtained from Bent Grass Filing No. 2 FDR Flow to DP10
	10	OS-3	10.61	0.40	18.9	4.24	5.33	22.6	22.0	12.27	4.94	60.6	2.3	.5.4				,,,,	1.2	1	Offsite flow into Basin EX-6. Flow obtained from Bent Grass Filing No. 2 FDR
		EX-6	4.78	0.36	17.5	1.72	5.52	9.5	22.0	13.99	4.94	69.1	0.5	9.5				450	1.4	5.3	Flow to DP11
	11	EX-7	12.18	0.36	18.9	4.38	5.33	23.3	22.0	18.37	4.94	90.7			90.7	1.0	42	942	2.0		Pipe flow to DP17
	17								22.0	24.01	4.94	118.6									Combination of DP17c and DP11, discharges into Basin D-7
	12	EX-8	1.63	0.36	6.6	0.59	7.98	4.7			-										

CLH19\_CUR-FDR-Drainage Cales.xlsm

# STANDARD FORM SF-3: CURRENT/EXISTING CONDITIONS STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Falcon Meadows at Bent Grass Filing No. 2
Subdivision: Falcon Meadows	Project No.: CLH000019
Location: CO, Colorado Springs	Calculated By: TJE
Design Storm: 100-Year	Checked By: CMD
	Date: 12/3/21

				DIRE	CT RU	NOFF				TOTAL	RUNOF	F	STR	EET		PIPE		TRAV	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
													2	4.7				550	2.8	3.2	Flow to DP24, Basin E-4
	24	E-4	0.91	0.84	8.0	0.76	7.50	5.7	9.8	1.35	6.97	9.4									Flow into Ex inlet.
	25	E-5	0.89	0.89	7.3	0.79	7.73	6.1	9.8	2.14	6.97	14.9									Flow into Ex inlet. Flow in Swale F to pond in Basin D-7
	32	D-8	1.69	0.58	14.0	0.98	6.08	6.0													Flow in Swale C (Basin D-8) into proposed south pond
Pond South - Water Quality Detention Pond	30	D-7	7.65	0.40	14.8	3.06	5.94	18.2	22.0	30.19	4.94	149.1									Discharge to channel
	СС	B-2	4.16	0.36	16.0	1.50	5.75	8.6	46.6	445.95	3.05	1360.1									Flows existing site in channel
		I-1	0.31	0.79	5.0	0.24	8.68	2.1													Flows offsite south along Bent Grass Meadows Drive

CLH19\_CUR-FDR-Drainage Cales.xlsm

### **Proposed Computations**

### COMPOSITE % IMPERVIOUS CALCULATIONS: PROPOSED

Subdivision: Falcon Meadows Location: CO, Colorado Springs **Project Name:** Falcon Meadows at Bent Grass Filing No. 2

Project No.: CLH000019

Calculated By: TJE
Checked By: CMD **Date:** 12/3/21

1	2	3	4	5	6	7	8	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
		Pa	ved/Gravel Ro	oads	La	wns/Undevelo	ped	Re	sidential - 1/8	Acre	Res	sidential - 1/4	Acre	Res	idential - 1/3 /	Acre	Res	idential - 1/2	Acre	Re	esidential - 1 A	cre	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	Weighted %
		/6 Hup.	Alea (ac)	% Imp.	/6 Hup.	Alea (ac)	% Imp.	/6 mp.	Area (ac)	% Imp.	/6 Imp.	Area (ac)	% Imp.	/6 Imp.	Area (ac)	% Imp.	/6 Hup.	Area (ac)	% Imp.	/6 Imp.	Alea (ac)	% Imp.	Imp.
OFFSITE																							
OS-1	32.28	100	2.15	6.7	2	29.25	1.8	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	11.0
OS-2	20.07	80	0.90	3.6	2	18.62	1.9	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
OS-3	10.61	80	0.48	3.6	2	9.84	1.9	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
BENT GRASS F	ILING NO. 2 & FAI	CON MEAI	DOWS AT BE	ENT GRASS F	TILING NO.	1																	
EX-1	1.19	100	0.00	0.0	2	1.19	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-2	1.60	100	0.00	0.0	2	1.60	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-3	0.66	100	0.00	0.0	2	0.66	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
B-1	6.06	100	0.00	0.0	2	6.06	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
B-2	4.16	100	0.00	0.0	2	4.16	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
D-4a	0.98	100	0.21	21.4	2	0.00	0.0	65.0	0.77	51.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	72.5
D-4b	0.95	100	0.43	45.3	2	0.00	0.0	65.0	0.52	35.6	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.9
D-4c	1.22	100	0.43	35.2	2	0.24	0.4	65.0	0.55	29.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	64.9
D-5	1.08	100	0.22	20.4	2	0.11	0.2	65.0	0.75	45.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.7
D-6a	1.33	100	0.44	33.1	2	0.00	0.0	65.0	0.89	43.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	76.6
D-6b	2.69	100	0.59	21.9	2	0.00	0.0	65.0	2.10	50.7	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	72.6
D-7	7.65	100	0.00	0.0	2	6.22	1.6	65.0	1.43	12.2	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	13.8
D-8	1.69	100	0.00	0.0	2	0.11	0.1	65.0	1.58	60.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	60.9
E-1	1.71	100	0.78	45.6	2	0.23	0.3	65.0	0.00	0.0	40	0.70	16.4	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.3
E-2	0.68	100	0.56	82.4	2	0.12	0.4	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	82.8
E-3	0.78	100	0.69	88.5	2	0.09	0.2	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	88.7
E-4	0.91	100	0.73	80.2	2	0.18	0.4	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.6
E-5	0.89 4.46	100	0.79	88.8	2 2	0.10	0.2	65.0	0.00	0.0	40	0.00	0.0	30 30	0.00	0.0	25	0.00	0.0	20	0.00	3.2	89.0
OS-4 OS-5	0.46	100	0.00	0.0	2	0.00	0.0	65.0 65.0	2.28 0.46	33.2 65.0	40	1.46 0.00	13.1 0.0	30	0.00	0.0	25 25	0.00	0.0	20 20	0.72	0.0	49.5 65.0
OS-6	1.17	100	0.00	0.0	2	0.00	0.0	65.0	1.17	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
	OWS FILING NO.		0.00	0.0	2	0.00	0.0	05.0	1.17	05.0	40	0.00	0.0	30	0.00	0.0	23	0.00	0.0	20	0.00	0.0	05.0
C-1a	0.38	100	0.16	41.1	2	0.14	0.7	65.0	0.09	14.9	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	56.7
C-1a C-1c	1.77	100	0.10	35.6	2	0.14	0.0	65.0	1.14	41.9	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	77.5
C-1d	1.72	100	0.40	23.3	2	0.00	0.0	65.0	1.32	49.9	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	73.2
C-1e	0.29	100	0.29	100.0	2	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	100.0
C-1f	0.08	100	0.08	100.0	2	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	100.0
C-3	0.18	100	0.14	77.8	2	0.02	0.3	65.0	0.02	7.6	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	85.7
C-4	2.67	100	0.41	15.4	2	0.84	0.6	65.0	1.41	34.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	50.3
C-5	0.60	100	0.00	0.0	2	0.60	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
C-6	0.94	100	0.00	0.0	2	0.65	1.4	65.0	0.29	20.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	21.5
C-7	0.52	100	0.15	29.4	2	0.00	0.0	65.0	0.37	46.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	75.7
D-9	0.72	100	0.00	0.0	2	0.46	1.3	65.0	0.26	23.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	24.8
D-1c	4.34	100	0.33	7.6	2	0.00	0.0	65.0	3.06	45.8	40	0.95	8.8	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.2
D-2a	0.50	100	0.33	66.0	2	0.00	0.0	65.0	0.17	22.7	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	88.7
D-2b	0.74	100	0.18	24.3	2	0.14	0.4	65.0	0.42	37.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	61.8
D-2c	0.31	100	0.15	50.0	2	0.00	0.0	65.0	0.16	33.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	83.5
D-2d	0.24	100	0.10	43.4	2	0.00	0.0	65.0	0.14	37.9	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	81.3
D-2e	1.41	100	0.41	29.3	2	0.00	0.0	65.0	1.00	46.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	75.4
D-2f	2.43	100	0.70	28.8	2	0.07	0.1	65.0	1.67	44.7	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	73.6
D-2g	1.81	100	0.48	26.5	2	0.57	0.6	65.0	0.76	27.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	54.4
D-2h	0.23	100	0.00	0.0	2	0.00	0.0	65.0	0.23	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
D-3	2.26	100	0.00	0.0	2	0.28	0.2	65.0	1.74	50.0	40	0.13	2.3	30	0.11	1.5	25	0.00	0.0	20	0.00	0.0	54.0
FUTURE FILIN		100	0.10	22.2	_	1 0.00		65.0	1 625	50.5	40	0.00	0.0	20	0.00	0.0	2.5	0.00		20	0.00		72.0
C-1b	0.45	100	0.10	22.2	2	0.00	0.0	65.0	0.35	50.6	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	72.8
C-2	3.98	100	0.75	18.8	2	0.00	0.0	65.0	3.23	52.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	71.6
D-1a	2.97 2.54	100	0.11	3.7	2	0.42	0.3	65.0	2.44 1.56	53.4 39.9	40	0.00	0.0	30	0.00	0.0	25 25	0.00	0.0	20	0.00	0.0	57.4 62.2
D-1b D-1f	2.54	100	0.56	22.0 6.8	2	0.42	0.3	65.0 65.0	1.50	60.6	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.2
D-11	1.01	100	0.11	0.8	2	0.00	0.0	05.0	1.50	0.00	40	0.00	0.0	30	0.00	0.0	23	0.00	0.0	20	0.00	0.0	07.4

#### Lot Type Identification: 0 - 8,167 1/8 Acre 8,168 - 12,704 1/4 Acre 12,705 - 18,149 1/3 Acre 18,150 - 32,670 1/2 Acre 32,671 - 43,560 1 Acre

NOTES:

 $\% \ Impervious \ values \ are \ taken \ directly \ from \ Table \ 6-6 \ in \ the \ Colorado \ Springs \ DCM \ Vol. \ 1. \ CH. \ 6 \ (Referencing \ UDFCD \ 2001)$ 

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#### COMPOSITE RUNOFF COEFFICIENT CALCULATIONS: PROPOSED

Subdivision: Falcon Meadows
Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass Filing No. 2
Project No.: CLH000019

Calculated By: TJE
Checked By: CMD
Date: 12/3/21

	I I	Pave	ed/Gravel	Roads	Law	ns/Undev	eloned	Resid	dential - 1	/8 Acre	Resid	lential - 1	/4 Acre	Resid	dential - 1	/3 Acre		ı
Basin ID	Total		<u> </u>	1			г -					I					Composite	Composite
	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	C <sub>5</sub>	C <sub>100</sub>
OFFSITE		0.00			0.00											1	0.4.6	
OS-1	32.28	0.90	0.96	2.15 0.90	0.09	0.36	29.25	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.16	0.41
OS-2 OS-3	20.07 10.61	0.90	0.96 0.96	0.90	0.09	0.36	18.62 9.84	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.14	0.40
BENT GRASS FI								0.43	0.39	0.00	0.30	0.30	0.00	0.23	0.47	0.00	0.14	0.40
EX-1								0.45	0.50	1 0.00	0.20	0.50	0.00	0.25	0.47	I 0.00	0.00	0.26
EX-1 EX-2	1.19 1.60	0.90	0.96 0.96	0.00	0.09	0.36	1.19 1.60	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.09	0.36
EX-2 EX-3	0.66	0.90	0.96	0.00	0.09	0.36	0.66	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.09	0.36
B-1	6.06	0.90	0.96	0.00	0.09	0.36	6.06	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.09	0.36
B-1 B-2	4.16	0.90	0.96	0.00	0.09	0.36	4.16	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.09	0.36
D-4a	0.98	0.90	0.96	0.00	0.09	0.36	0.00	0.45	0.59	0.77	0.30	0.50	0.00	0.25	0.47	0.00	0.55	0.67
D-4b	0.95	0.90	0.96	0.43	0.09	0.36	0.00	0.45	0.59	0.52	0.30	0.50	0.00	0.25	0.47	0.00	0.65	0.76
D-4c	1.22	0.90	0.96	0.43	0.09	0.36	0.24	0.45	0.59	0.55	0.30	0.50	0.00	0.25	0.47	0.00	0.54	0.68
D-5	1.08	0.90	0.96	0.22	0.09	0.36	0.11	0.45	0.59	0.75	0.30	0.50	0.00	0.25	0.47	0.00	0.51	0.64
D-6a	1.33	0.90	0.96	0.44	0.09	0.36	0.00	0.45	0.59	0.89	0.30	0.50	0.00	0.25	0.47	0.00	0.60	0.71
D-6b	2.69	0.90	0.96	0.59	0.09	0.36	0.00	0.45	0.59	2.10	0.30	0.50	0.00	0.25	0.47	0.00	0.55	0.67
D-7	7.65	0.90	0.96	0.00	0.09	0.36	6.22	0.45	0.59	1.43	0.30	0.50	0.00	0.25	0.47	0.00	0.16	0.40
D-8	1.69	0.90	0.96	0.00	0.09	0.36	0.11	0.45	0.59	1.58	0.30	0.50	0.00	0.25	0.47	0.00	0.43	0.58
E-1	1.71	0.90	0.96	0.78	0.09	0.36	0.23	0.45	0.59	0.00	0.30	0.50	0.70	0.25	0.47	0.00	0.55	0.69
E-2	0.68	0.90	0.96	0.56	0.09	0.36	0.12	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.76	0.85
E-3	0.78	0.90	0.96	0.69	0.09	0.36	0.09	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.81	0.89
E-4	0.91	0.90	0.96	0.73	0.09	0.36	0.18	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.74	0.84
E-5	0.89	0.90	0.96	0.79	0.09	0.36	0.10	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.81	0.89
OS-4	4.46	0.90	0.96	0.00	0.09	0.36	0.00	0.45	0.59	2.28	0.30	0.50	1.46	0.25	0.47	0.00	0.36	0.54
OS-5 OS-6	0.46 1.17	0.90	0.96	0.00	0.09	0.36	0.00	0.45	0.59	0.46 1.17	0.30	0.50	0.00	0.25	0.47	0.00	0.45 0.45	0.59
FALCON MEAD				0.00	0.09	0.36	0.00	0.43	0.39	1.1/	0.30	0.30	0.00	0.23	0.47	0.00	0.45	0.39
C-1a	0.38	0.90	0.96	0.16	0.09	0.36	0.14	0.45	0.59	0.09	0.30	0.50	0.00	0.25	0.47	0.00	0.51	0.66
C-1a C-1c	1.77	0.90	0.96	0.16	0.09	0.36	0.14	0.45	0.59	1.14	0.30	0.50	0.00	0.25	0.47	0.00	0.61	0.00
C-1d	1.72	0.90	0.96	0.03	0.09	0.36	0.00	0.45	0.59	1.32	0.30	0.50	0.00	0.25	0.47	0.00	0.55	0.72
C-1e	0.29	0.90	0.96	0.29	0.09	0.36	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.90	0.96
C-1f	0.08	0.90	0.96	0.08	0.09	0.36	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.90	0.96
C-3	0.18	0.90	0.96	0.14	0.09	0.36	0.02	0.45	0.59	0.02	0.30	0.50	0.00	0.25	0.47	0.00	0.76	0.86
C-4	2.67	0.90	0.96	0.41	0.09	0.36	0.84	0.45	0.59	1.41	0.30	0.50	0.00	0.25	0.47	0.00	0.41	0.57
C-5	0.60	0.90	0.96	0.00	0.09	0.36	0.60	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.09	0.36
C-6	0.94	0.90	0.96	0.00	0.09	0.36	0.65	0.45	0.59	0.29	0.30	0.50	0.00	0.25	0.47	0.00	0.20	0.43
C-7	0.52	0.90	0.96	0.15	0.09	0.36	0.00	0.45	0.59	0.37	0.30	0.50	0.00	0.25	0.47	0.00	0.58	0.70
D-9	0.72	0.90	0.96	0.00	0.09	0.36	0.46	0.45	0.59	0.26	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.44
D-1c	4.34	0.90	0.96	0.33	0.09	0.36	0.00	0.45	0.59	3.06	0.30	0.50	0.95	0.25	0.47	0.00	0.45	0.60
D-2a	0.50	0.90	0.96	0.33	0.09	0.36	0.00	0.45	0.59	0.17	0.30	0.50	0.00	0.25	0.47	0.00	0.75	0.84
D-2b	0.74	0.90	0.96	0.18	0.09	0.36	0.14	0.45	0.59	0.42	0.30	0.50	0.00	0.25	0.47	0.00	0.49	0.64
D-2c	0.31	0.90	0.96	0.15	0.09	0.36	0.00	0.45	0.59	0.16	0.30	0.50	0.00	0.25	0.47	0.00	0.68	0.78
D-2d	0.24	0.90	0.96	0.10	0.09	0.36	0.00	0.45	0.59	0.14	0.30	0.50	0.00	0.25	0.47	0.00	0.65	0.76
D-2e	1.41	0.90	0.96	0.41	0.09	0.36	0.00	0.45	0.59	1.00	0.30	0.50	0.00	0.25	0.47	0.00	0.58	0.70
D-2f	2.43	0.90	0.96	0.70	0.09	0.36	0.07	0.45	0.59	1.67	0.30	0.50	0.00	0.25	0.47	0.00	0.57	0.69
D-2g	1.81	0.90	0.96	0.48	0.09	0.36	0.57	0.45	0.59	0.76	0.30	0.50	0.00	0.25	0.47	0.00	0.46	0.62
D-2h D-3	0.23 2.26	0.90	0.96 0.96	0.00	0.09	0.36	0.00	0.45	0.59	0.23 1.74	0.30	0.50	0.00	0.25	0.47	0.00	0.45	0.59 0.55
FUTURE FILING		0.90	0.90	0.00	0.09	0.30	0.28	0.43	0.39	1./4	0.30	0.30	0.13	0.23	I 0.4/	J 0.11	0.39	0.33
C-1b	0.45	0.90	0.96	0.10	0.09	0.36	0.00	0.45	0.59	0.35	0.30	0.50	0.00	0.25	0.47	0.00	0.55	0.67
C-16 C-2	3.98	0.90	0.96	0.10	0.09	0.36	0.00	0.45	0.59	3.23	0.30	0.50	0.00	0.25	0.47	0.00	0.53	0.66
D-1a	2.97	0.90	0.96	0.73	0.09	0.36	0.00	0.45	0.59	2.44	0.30	0.50	0.00	0.25	0.47	0.00	0.33	0.66
D-1a D-1b	2.54	0.90	0.96	0.11	0.09	0.36	0.42	0.45	0.59	1.56	0.30	0.50	0.00	0.25	0.47	0.00	0.42	0.63
D 10	1.61	0.90	0.96	0.30	0.09	0.36	0.00	0.75	0.59	1.50	0.50	0.50	0.00	0.25	0.47	0.00	0.48	0.62

Lot Type Identif	ication:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	:/= 1/8 Acr
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32 671 - 43 560	1 Acre

C values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001) Coeffficients use HSG A&B soils - Refer to "Appendix A: Exhibits and Figures" for soil map

# STANDARD FORM SF-2: PROPOSED TIME OF CONCENTRATION

Subdivision: Falcon Meadows

Location: CO, Colorado Springs

**Project Name:** Falcon Meadows at Bent Grass Filing No. 2

Project No.: CLH000019

**Calculated By:** TJE

Checked By: CMD

**Date:** 12/3/21

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
		SUB-BA	SIN			INITIA	L/OVEF	RLAND		TRA	VEL TI	ME			Tc CHECK		
		DAT	4				$(T_i)$				$(T_t)$			(UI	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	$C_5$	$C_{100}$	L	S	$T_{i}$	L	S	Cv	VEL.	$T_t$	COMP. T <sub>c</sub>	TOTAL	Urbanized T <sub>c</sub>	T <sub>c</sub>
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT)	(MIN)	(MIN)
<b>OFFSITE</b>																	
OS-1	32.28	A	11.0	0.16	0.41	100	2.4	12.9	2100	2.2	15	2.2	15.7	28.6	2200.0	22.2	22.2
OS-2	20.07	A	8.0	0.14	0.40	100	2.3	13.3	1400	2.3	15	2.3	10.3	23.6	1500.0	18.3	18.3
OS-3	10.61	A	8.0	0.14	0.40	100	2.0	14.0	1500	2.0	15	2.1	11.8	25.7	1600.0	18.9	18.9
BENT GR	ASS FILI	NG NO. 2 & 1	FALCON ME	ADOWS	S AT BE	NT GRA	SS FILE	NG NO.	1								
EX-1	1.19	A	2.0	0.09	0.36	300	2.7	23.0	690	2.7	15	2.5	4.7	27.7		15.5	15.5
EX-2	1.60	A	2.0	0.09	0.36	200	2.7	18.8	100	2.7	15	2.5	0.7	19.5	300.0	11.7	11.7
EX-3	0.66	A	2.0	0.09	0.36	100	5.0	10.8	30	2.7	15	2.5	0.2	11.0	130.0	10.7	10.7
B-1	6.06	A	2.0	0.09	0.36	90	6.4	9.5	2000	1.7	15	2.0	17.0	26.5		21.6	21.6
B-2	4.16	A	2.0	0.09	0.36	160	11.0	10.5	920	1.6	15	1.9	8.1	18.6		16.0	16.0
D-4a	0.98	A	72.5	0.55	0.67	100	2.3	7.6	420	1.0	20	2.0	3.5	11.1	520.0	12.9	11.1
D-4b	0.95	A	80.9	0.65	0.76	75	1.5	6.2	480	1.0	20	2.0	4.0	10.2		13.1	10.2
D-4c	1.22	A	64.9	0.54	0.68	70	0.5	10.8	690	1.0	20	2.0	5.8	16.6	760.0	14.2	14.2
D-5	1.08	A	65.7	0.51	0.64	10	2.0	2.7	300	1.1	20	2.1	2.4	5.1		11.7	5.1
D-6a	1.33	A	76.6	0.60	0.71	20	2.0	3.2	385	1.0	20	2.0	3.2	6.5		12.3	6.5
D-6b	2.69	A	72.6	0.55	0.67	45	2.0	5.4	870	1.0	20	2.0	7.3	12.6		15.1	12.6
D-7	7.65	A	13.8	0.16	0.40	200	7.5	12.4	665	1.0	15	1.5	7.4	19.8		14.8	14.8
D-8	1.69	A	60.9	0.43	0.58	125	3.7	8.9	600	1.0	15	1.5	6.7	15.5		14.0	14.0
E-1	1.71	A	62.3	0.55	0.69	25	2.0	4.0	940	1.0	20	2.0	7.8	11.8		15.4	11.8
E-2	0.68	A	82.8	0.76	0.85	25	2.0	2.5	665	1.6	20	2.5	4.4	6.9		13.8	6.9
E-3	0.78	A	88.7	0.81	0.89	25	2.0	2.1	632	1.0	20	2.0	5.3	7.4		13.7	7.4
E-4	0.91	A	80.6	0.74	0.84	25	2.0	2.6	913	2.0	20	2.8	5.4	8.0		15.2	8.0
E-5	0.89	A	89.0	0.81	0.89	25	2.0	2.1	903	2.1	20	2.9	5.2	7.3		15.2	7.3
OS-4	4.46	A	49.5	0.36	0.54	100	2.0	10.8	910	1.2	20	2.2	6.9	17.7		15.6	15.6
OS-5	0.46	A	65.0	0.45	0.59	15	2.0	3.7	190	1.0	20	2.0	1.6	5.2		11.1	5.2
OS-6	1.17	A	65.0	0.45	0.59	85	0.2	18.7	430	0.9	20	1.9	3.8	22.5	515.0	12.9	12.9
	MEADO	WS FILING N	O. 2														
C-1a	0.38	A	56.7	0.51	0.66	10	2.0		220	1.0	20		1.8	4.5	230.0	11.3	5.0
C-1c	1.77	A	77.5	0.61	0.72	10	2.0	2.3	370	3.0	20	3.5	1.8	4.0	380.0	12.1	5.0
C-1d	1.72	A	73.2	0.55	0.68	10	2.0	2.5	620	2.0	20	2.8	3.7	6.2	630.0	13.5	6.2
C-1e	0.29	A	100.0	0.90	0.96	10	2.0	0.9	275	1.7	20	2.6	1.8	2.7	285.0	11.6	5.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
		SUB-BA	SIN			INITIA	L/OVEF	RLAND		TRA	AVEL TI	ME			Tc CHECK		
		DAT	A				$(T_i)$				$(T_t)$			(UR	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S	T <sub>i</sub>	L	S	Cv	VEL.	T <sub>t</sub>	COMP. T <sub>c</sub>	TOTAL	Urbanized T <sub>c</sub>	T <sub>c</sub>
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT)	(MIN)	(MIN)
C-1f	0.08	A	100.0	0.90	0.96	10	2.0	0.9	130	1.7	20	2.6	0.8	1.8	140.0	10.8	5.0
C-3	0.18	A	85.7	0.76	0.86	10	2.0	1.6	580	1.0	20	2.0	4.8	6.4	590.0	13.3	6.4
C-4	2.67	A	50.3	0.41	0.57	100	3.0	8.8	600	2.0	20	2.8	3.5	12.3	700.0	13.9	12.3
C-5	0.60	A	2.0	0.09	0.36	5	2.0	3.3		1.0	15	1.5	0.0	3.3	5.0	10.0	5.0
C-6	0.94	A	21.5	0.20	0.43	20	3.3	5.0	90	5.0	15	3.4	0.4	5.4	110.0	10.6	5.4
C-7	0.52	A	75.7	0.58	0.70	100	6.8	5.0	165	1.3	15	1.7	1.6	6.7	265.0	11.5	6.7
D-9	0.72	A	24.8	0.22	0.44	10	2.0	4.0	250	3.6	15	2.8	1.5	0.0	260.0	11.4	5.5
D-1c	4.34	A	62.2	0.45	0.60	100	2.6	8.7	1900	1.3	20	2.3	13.9	22.5	2000.0	21.1	21.1
D-2a	0.50	A	88.7	0.75	0.84	10	2.0	1.6	495	1.3	20	2.3	3.6	5.2	505.0	12.8	5.2
D-2b	0.74	A	61.8	0.49	0.64	100	1.7	9.4	189	1.0	20	2.0	1.6	10.9	289.0	11.6	10.9
D-2c	0.31	A	83.5	0.68	0.78	5	2.0	1.4	275	1.0	20	2.0	2.3	3.7	280.0	11.6	5.0
D-2d	0.24	A	81.3	0.65	0.76	5	2.0	1.5	200	1.3	20	2.3	1.5	2.9	205.0	11.1	5.0
D-2e	1.41	A	75.4	0.58	0.70	100	1.9	7.7	340	0.8	20	1.8	3.2		440.0	12.4	10.9
D-2f	2.43	A	73.6	0.57	0.69	75	2.0	6.7	175	0.5	20	1.4	2.1	8.7	250.0	11.4	8.7
D-2g	1.81	A	54.4	0.46	0.62	35	2.0	5.5	1355	1.3	20	2.3	9.9	15.4	1390.0	17.7	15.4
D-2h	0.23	A	65.0	0.45	0.59	35	2.0	5.6	1355	1.3	20	2.3	9.9		1390.0		15.5
D-3	2.26	A	54.0	0.39	0.55	25	8.0	3.3	1960	1.0	15	1.5	21.8	25.0	1985.0	21.0	21.0
<b>FUTURE I</b>	FILINGS																
C-1b	0.45	A	72.8	0.55	0.67	10	2.0	2.5	365	1.9	15	2.1	2.9	5.5	375.0	12.1	5.5
C-2	3.98	A	71.6	0.53	0.66	10	2.0	2.6	650	2.0	20	2.8	3.8	6.4	660.0	13.7	6.4
D-1a	2.97	A	57.4	0.42	0.57	5	1.0	2.8	360	2.4	15	2.3	2.6		365.0	12.0	5.4
D-1b	2.54	A	62.2	0.49	0.63	100	3.2	7.6	540	1.3	15	1.7	5.3	12.8	640.0	13.6	12.8
D-1f	1.61	A	67.4	0.48	0.62	100	2.7	8.2	380	2.0	15	2.1	3.0	11.1	480.0	12.7	11.1

#### **NOTES:**

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$ , S in ft/ft

T<sub>t</sub>=L/60V (Velocity From Fig. 501)

Velocity V=Cv\*S^0.5, S in ft/ft

Tc Check = 10+L/180

For Urbanized basins a minimum  $T_{\rm c}$  of 5.0 minutes is required.

For non-urbanized basins a minimum  $T_c$  of 10.0 minutes is required

Type of Land Surface	Cv
Heavy Meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

CLH19\_PR-FDR-Drainage Calcs.xlsm Page 2 of 2 11/30/2021

# STANDARD FORM SF-3: PROPOSED STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows
Location: CO, Colorado Springs
Design Storm: 5-Year

C-5

0.60

0.09

0.05

5.17

 Project Name:
 Falcon Meadows at Bent Grass Filing No. 2

 Project No.:
 CLH000019

 Calculated By:
 TJE

 Checked By:
 CMD

North Pond

Flows to Basin B-1

Date: 12/3/21

				DIRE	CT RUN	OFF				TOTAL :	RUNOF	F	STR	REET		PIPE		TRA	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		RWT202	1574.40						46.6	120.88	1.82	220.0									From Falcon DBPS by Matrix
		RWT204	38.40						11.37	1.78	3.94	7.0									From Falcon DBPS by Matrix
		WT200	192.00						37.8	24.41	2.13	52.0									From Falcon DBPS by Matrix
	21	OS-1	32.28	0.16	22.2	5.16	2.93	15.1	46.6	152.23	1.82	277.1									Flows obtained from Bent Grass Filing No. 2 FDR. Q=65.1 CFS Cumulation of northern off-site flows entering Basin B-1
	1	OS-4	4.46	0.36	15.6	1.61	3.46	5.6					1.2	5.6				910	2.2	6.9	Flows from Basin B-1 of Bent Grass Filing No. 2 FDR into Basin EX-2
	2	OS-5	0.46	0.45	5.2	0.21	5.10	1.1					1	1.1				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR into Basin EX-2
	3	OS-6	1.17	0.45	12.9	0.53	3.75	2.0					0.9	2.0				430	1.9	3.8	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR into Basin EX-2
		EX-1	1.19	0.09	15.5	0.11	3.47	0.4													Flows to Basin EX-2
	5	EX-2	1.60	0.09	11.7	0.14	3.90	0.5	22.5	2.60	2.91	7.6									Flows to Basin EX-3
	7	E-3	0.78	0.81	7.4	0.63	4.59	2.9													
		C-6	0.94	0.20	5.4	0.19	5.05	1.0					1	1.0				216	2.0	1.8	
	45	C-7	0.52	0.58	6.7	0.30	4.74	1.4					1	1.4				216	2.0	1.8	
		E-2	0.68	0.76	6.9	0.52	4.70	2.4	8.5	1.01	4.38	4.4									Combination of C-6, C-7, E-2
	8	E-1	1.71	0.55	11.8	0.94	3.88	3.6	11.8	2.58	3.88	10.0									Ex Basin from Filing No. 2(East side of BGMD)  Combination of EX-4, EX-5, E-1, E-2, E-3. Flows to Basin EX-3
	15a	EX-3	0.66	0.09	10.7	0.06	4.02	0.2	22.5	5.24	2.91	15.2									Flows to Basin B-1
	51	D-1a	2.97	0.42	5.4	1.25	5.06	6.3							6.3	1.2	18	217	2.2	1.7	
		D-1f	1.61	0.48	11.1	0.77	3.97	3.1													
	40	C-1a	0.38	0.51	5.0	0.19	5.17	1.0	11.1	2.21	3.97	8.8									Flows to Swale B
		C-1b	0.45	0.55	5.5	0.25	5.03	1.3	11.1	2.46	3.97	9.8	1	9.8				175	2.0	1.5	Flows exiting Swale B towards DP41
	41	C-1c	1.77	0.61	5.0	1.08	5.17	5.6	11.1	3.54	3.97	14.1			14.1	1.3	30	180	2.2	1.3	Flow into inlet at DP41
		C-3	0.18	0.76	6.4	0.14	4.80	0.7					1	0.7				660	2.0	5.5	Gutter flow through C-4 to DP44
	44	C-4	2.67	0.41	12.3	1.09	3.82	4.2	12.3	1.23	3.82	4.7			4.7	1.3	24	70	2.2	0.5	Flow into inlet at DP44
	42	C-1f	0.08	0.90	5.0	0.07	5.17	0.4					1	0.4				185	2.0	1.5	Gutter flow to DP15
	43 15	C-1d	1.72	0.55	6.2	0.95	4.85	4.6	6.5	1.02	4.77	4.9									Flow into inlet at DP15
	12 13	C-1e	0.29	0.90	5.0	0.26	5.17	1.3	12.8	6.05	3.76	22.7			22.7	1.0	42	33	2.0	0.3	Flow into inlet at DP12 Combination of flow from DP12, DP15, DP41, DP44 into North Pond
	19	C-2	3.98	0.53	6.4	2.11	4.79	10.1													Flow into Pond North

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# STANDARD FORM SF-3: PROPOSED STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows

Location: CO, Colorado Springs

Design Storm: 5-Year

 Project Name:
 Falcon Meadows at Bent Grass Filing No. 2

 Project No.:
 CLH000019

 Calculated By:
 TJE

Checked By: CMD

Date: 12/3/21

				DIRE	CT RUN	OFF			Í	ГОТАL	RUNOF	F	STR	REET		PIPE		TRA	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	AA	B-1	6.06	0.09	21.6	0.55	2.97	1.6	46.6	166.23	1.82	302.5									Total flow under BGMD into Basin B-2
		D-2b	0.74	0.49	10.9	0.36	4.00	1.4													
		D-2a	0.50	0.75	5.2	0.38	5.10	1.9													
	14a	D-2c	0.31	0.68	5.0	0.21	5.17	1.1	10.9	0.95	4.00	3.8	1.3	3.8				230	2.3	1.7	Gutter flow through D-2d to DP14b
	14b	D-2d	0.24	0.65	5.0	0.16	5.17	0.8	12.6	1.11	3.78	4.2	1.3	4.2				625	2.3	4.6	Gutter flow through D-2d to DP14b
	14	D-2g	1.81	0.46	15.4	0.83	3.48	2.9	17.2	1.94	3.32	6.4									Flow into existing inlet at DP14
	9	OS-2	20.07	0.14	18.3	2.81	3.22	9.0													Overland flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
	10	OS-3	10.61	0.14	18.9	1.49	3.18	4.7													Offsite flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
	11	D-3	2.26	0.39	21.0	0.88	3.01	2.6	21.0	5.18	3.01	15.6			15.6	1.0	42	100	2.0	0.8	Flows conveyed via existing ditch into proposed area inlet.
	14e	D-2f	2.43	0.57	8.7	1.39	4.33	6.0													
	14d	D-2e	1.41	0.58	10.9	0.82	4.01	3.3	10.9	2.21	4.01	8.9			8.9	1.0	42	100	2.0	0.8	Flows conveyed storm sewer to DP16
	16a	D-1b	2.54	0.49	12.8	1.24	3.75	4.7					1.3	4.7				1300	2.3	9.5	Gutter flow through Basin D-1c to DP16
	16	D-1c	4.34	0.45	21.1	1.95	3.01	5.9	22.3	10.58	2.92	30.9			30.9	2.0	48	835	2.8	4.9	Combination of flows to existing inlets at DP14 and DP16. Flows to DP 17
		D-5	1.08	0.51	5.1	0.55	5.14	2.8					1	2.8				600	2.0	5.0	Gutter flow through Basin D-6b to DP18
		D-6b	2.69	0.55	12.6	1.48	3.78	5.6													
	18	D-6a	1.33	0.60	6.5	0.80	4.79	3.8	12.6	2.83	3.78	10.7			10.7	2.0	24	38	2.8	0.2	Flow to existing inlet. Flow out of inlet to DP17c
	17a	D-4a	0.98	0.55	11.1	0.54	3.97	2.1					1	2.1				700	2.0	5.8	Gutter flow through Basin D-4b to DP17b
	17b	D-4b	0.95	0.65	10.2	0.62	4.09	2.5	17.0	1.16	3.34	3.9									Gutter flow to DP17c
	17c	D-4c	1.22	0.54	14.2	0.66	3.60	2.4	17.0	3.99	3.34	13.3			13.3	2.0	24	8	2.8	0.0	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR. Flows at existing inlet. Flow out to DP17
	17								27.3	14.57	2.62	38.2									Storm system entering existing pond at Basin D-7
		D-9	0.72	0.22	5.5	0.16	5.02	0.8					1.5	0.8				625	2.4	4.3	Gutter flow through Basin E-4 to DP24
		D-2h	0.23	0.45	15.5	0.10	3.47	0.3					1.5	0.3				550	2.4	3.7	Gutter flow through Basin E-4 to DP24
	24	E-4	0.91	0.74	8.0	0.67	4.46	3.0	19.2	0.93	3.15	2.9									Flow to existing inlet at DP24
	25 26	E-5	0.89	0.81	7.3	0.72	4.60	3.3	19.2	1.65	3.15	5.2									Flow to existing inlet at DP25 Flow into existing pond via Swale F at DP26
	32	D-8	1.69	0.43	14.0	0.73	3.62	2.6													Flow in Swale C (Basin D-8) into existing pond
	30	D-7	7.65	0.16	14.8	1.22	3.54	4.3	27.3	18.17	2.62	47.6									Exisitng Water quality pond Outlet to existing channel Basin B-2
	СС	B-2	4.16	0.09	16.0	0.37	3.42	1.3	46.6	184.77	1.82	336.3									

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#### STANDARD FORM SF-3: PROPOSED

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows

Location: CO, Colorado Springs

Design Storm: 100-Year

 Project Name:
 Falcon Meadows at Bent Grass Filing No. 2

 Project No.:
 CLH000019

 Calculated By:
 TJE

 Checked By:
 CMD

 Date:
 12/3/21

	Ι			DIRE	CT RUI	NOFF				ΓΟΤΑL	RUNOF	F	STR	EET		PIPE		TRAV	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		RWT202	1574.40						46.6	327.87	3.05	1000.0									From Falcon DBPS by Matrix
		RWT204	38.40						11.37	6.51	6.61	43.0									From Falcon DBPS by Matrix
		WT200	192.00						37.8	53.07	3.58	190.0									From Falcon DBPS by Matrix
	21	OS-1	32.28	0.41	22.2	13.23	4.92	65.1	46.6	400.68	3.05	1222.1									Flows obtained from Bent Grass Filing No. 2 FDR. Q=65.1 CFS Cumulation of northern off-site flows entering Basin B-1
	1	OS-4	4.46	0.54	15.6	2.41	5.81	14.0					1.2	14.0				910	2.2	6.9	Flows from Basin B-1 of Bent Grass Filing No. 2 FDR into Basin EX-2
	2	OS-5	0.46	0.59	5.2	0.27	8.56	2.3					1	2.3				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR into Basin EX-2
	3	OS-6	1.17	0.59	12.9	0.69	6.30	4.3					0.9	4.3				430	1.9	3.8	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR into Basin EX-2
		EX-1	1.19	0.36	15.5	0.43	5.83	2.5													Flows to Basin EX-2
	5	EX-2	1.60	0.36	11.7	0.58	6.54	3.8	22.5	4.38	4.89	21.4									Flows to Basin EX-3
	7	E-3	0.78	0.89	7.4	0.69	7.70	5.3													
		C-6	0.94	0.43	5.4	0.40	8.49	3.4					1	3.4				216	2.0	1.8	
	45	C-7	0.52	0.70	6.7	0.36	7.95	2.9					1	2.9				216	2.0	1.8	
		E-2	0.68	0.85	6.9	0.58	7.89	4.6	8.5	1.34	7.35	9.8									Combination of C-6, C-7, E-2
	8	E-1	1.71	0.69	11.8	1.18	6.51	7.7	11.8	3.21	6.51	20.9									Ex Basin from Filing No. 2(East side of BGMD) Combination of EX-4, EX-5, E-1, E-2, E-3. Flows to Basin EX-3
	15a	EX-3	0.66	0.36	10.7	0.24	6.76	1.6	22.5	7.83	4.89	38.3									Flows to Basin B-1
	51	D-1a	2.97	0.57	5.4	1.69	8.50	14.4							14.4	1.2	18	217	2.2	1.7	
		D-1f	1.61	0.62	11.1	1.00	6.66	6.7													
	40	C-1a	0.38	0.66	5.0	0.25	8.68	2.2	11.1	2.94	6.66	19.6									Flows to Swale B
		C-1b	0.45	0.67	5.5	0.30	8.45	2.5	11.1	3.24	6.66	21.6	1	21.6				175	2.0	1.5	Flows exiting Swale B towards DP41
	41	C-1c	1.77	0.72	5.0	1.27	8.68	11.0	11.1	4.51	6.66	30.0			30.0	1.3	30	180	2.2	1.3	Flow into inlet at DP41
		C-3	0.18	0.86	6.4	0.15	8.06	1.2					1	1.2				660	2.0	5.5	Gutter flow through C-4 to DP44
	44	C-4	2.67	0.57	12.3	1.52	6.41	9.7	12.3	1.67	6.41	10.7			10.7	1.3	24	70	2.2	0.5	Flow into inlet at DP44
	42	C-1f	0.08	0.96	5.0	0.08	8.68	0.7					1	0.7				185	2.0	1.5	Gutter flow to DP15
	43 15	C-1d	1.72	0.68	6.2	1.17	8.14	9.5	6.5	1.25	8.00	10.0									Flow into inlet at DP15
	12 13	C-1e	0.29	0.96	5.0	0.28	8.68	2.4	12.8	7.71	6.31	48.7			48.7	1.0	42	33	2.0	0.3	Flow into inlet at DP12 Combination of flow from DP12, DP15, DP41, DP44 into North Pond
	19	C-2	3.98	0.66	6.4	2.63	8.04	21.1													Flow into Pond North
	13a	C-5	0.60	0.36	5.0	0.22	8.68	1.9	13.1	10.56	6.25	66.0									North Pond Flows to Basin B-1
	AA	B-1	6.06	0.36	21.6	2.18	4.99	10.9	46.6	421.25	3.05	1284.8									Total flow under BGMD into Basin B-2
		D-2b	0.74	0.64	10.9	0.47	6.71	3.2													

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#### STANDARD FORM SF-3: PROPOSED

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows

Location: CO, Colorado Springs

Design Storm: 100-Year

 Project Name:
 Falcon Meadows at Bent Grass Filing No. 2

 Project No.:
 CLH000019

 Calculated By:
 TJE

 Checked By:
 CMD

 Date:
 12/3/21

				DIRE	CT RUN	NOFF				ΓΟΤΑL	RUNOF	F	STF	REET		PIPE	2	TRAV	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		D-2a	0.50	0.84	5.2	0.42	8.57	3.6													
	14a	D-2c	0.31	0.78	5.0	0.24	8.68	2.1	10.9	1.13	6.71	7.6	1.3	7.6				230	2.3	1.7	Gutter flow through D-2d to DP14b
	14b	D-2d	0.24	0.76	5.0	0.18	8.68	1.6	12.6	1.31	6.35	8.3	1.3					625	2.3		Gutter flow through D-2d to DP14b
	14	D-2g	1.81	0.62	15.4	1.12	5.84	6.5	17.2	2.43	5.57	13.5	1.3	0.5				023	2.3	4.0	Flow into existing inlet at DP14
	9	OS-2	20.07	0.40	18.3	8.03	5.41	43.4	17.2	2.43	3.31	13.3									Overland flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
	10	OS-3	10.61	0.40	18.9	4.24	5.33	22.6													Offsite flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
	11	D-3	2.26	0.55	21.0	1.24	5.06	6.3	21.0	12.51	5.06	60.4			68.4	1.0	42	100	2.0	0.0	
	11 14e	D-2f	2.43	0.69	8.7	1.68	7.27	12.2	21.0	13.51	5.06	68.4			68.4	1.0	42	100	2.0	0.8	Flows conveyed via existing ditch into proposed area inlet.
	14d	D-2e	1.41	0.70	10.9	0.99	6.73	6.7													
	16a	D-1b	2.54	0.63	12.8	1.60	6.30	10.1	10.9	2.67	6.73	18.0			18.0	1.0	42	100	2.0		Flows conveyed storm sewer to DP16
		D-1c	4.34	0.60	21.1	2.60	5.05	13.1					1.3	10.1				1300			Gutter flow through Basin D-1c to DP16
	16	D-5	1.08	0.64	5.1	0.69	8.63	6.0	22.3	20.38	4.91	100.1			100.1	2.0	48	835	2.8		Combination of flows to existing inlets at DP14 and DP16. Flows to DP 17
		D-6b	2.69	0.67	12.6	1.80	6.35	11.4					1	6.0				600	2.0	5.0	Gutter flow through Basin D-6b to DP18
		D-6a	1.33	0.71	6.5	0.94	8.03	7.5													
	18 17a	D-4a	0.98	0.67	11.1	0.66	6.66	4.4	12.6	3.43	6.35	21.8			21.8	2.0	24	38	2.8	0.2	Flow to existing inlet. Flow out of inlet to DP17c
		D-4b	0.95	0.76	10.2	0.72	6.87	4.9					1	4.4				700	2.0	5.8	Gutter flow through Basin D-4b to DP17b
	17b	D-4c	1.22	0.68	14.2	0.83	6.04	5.0	17.0	1.38	5.60	7.7	1								Gutter flow to DP17c Flows from Basin B-3 of Bent Grass Filing No. 2 FDR.
	17c	D-10	1.22	0.00	14.2	0.05	0.04	3.0	17.0	4.81	5.60	26.9			26.9	2.0	24	8	2.8		Flows at existing inlet. Flow out to DP17
	17	D-9	0.72	0.44	5.5	0.32	8.44	2.7	27.3	25.19	4.40	110.8									Storm system entering existing pond at Basin D-7
													1.5	2.7				625	2.4	4.3	Gutter flow through Basin E-4 to DP24
		D-2h	0.23	0.59	15.5	0.14	5.83	0.8					1.5	0.8				550	2.4	3.7	Gutter flow through Basin E-4 to DP24
	24	E-4	0.91	0.84	8.0	0.76	7.50	5.7	19.2	1.22	5.28	6.4									Flow to existing inlet at DP24
	25 26	E-5	0.89	0.89	7.3	0.79	7.73	6.1	19.2	2.01	5.28	10.6									Flow to existing inlet at DP25 Flow into existing pond via Swale F at DP26
	32	D-8	1.69	0.58	14.0	0.98	6.08	6.0													Flow in Swale C (Basin D-8) into existing pond
	30	D-7	7.65	0.40	14.8	3.06	5.94	18.2	27.3	31.24	4.40	137.5									Exisiting Water quality pond Outlet to existing channel Basin B-2
	CC	B-2	4.16	0.36	16.0	1.50	5.75	8.6	46.6	453.99	3.05	1384.7									

CLH19\_PR-FDR-Drainage Cales.xlsm

# APPENDIX C Hydraulic Computations

### **Swales**

### Worksheet for Swale - C (Proposed)

	Norksheet for Swa	ale - C	(Proposed)
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.030	
Channel Slope		0.01500	ft/ft
Left Side Slope		4.00	ft/ft (H:V)
Right Side Slope		4.00	ft/ft (H:V)
Bottom Width		1.00	ft
Discharge		8.50	ft³/s
Results			
Normal Depth		0.69	ft
Flow Area		2.63	ft²
Wetted Perimeter		6.73	ft
Hydraulic Radius		0.39	ft
Top Width		6.56	ft
Critical Depth		0.66	ft
Critical Slope		0.01867	ft/ft
Velocity		3.24	ft/s
Velocity Head		0.16	ft
Specific Energy		0.86	ft
Froude Number		0.90	
Flow Type	Subcritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity		Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.69	ft
Critical Depth		0.66	ft
Channal Clans		0.01500	£4/£4

0.01500 ft/ft

Channel Slope

### Worksheet for Swale - C (Proposed)

### **GVF** Output Data

Critical Slope 0.01867 ft/ft

#### Worksheet for Swale - F (Proposed)

	Worksheet for	Swaie - F	(Proposea)
Project Description			
Friction Method Solve For	Manning Formula Normal Depth		
Input Data			
Roughness Coefficient Channel Slope Left Side Slope Right Side Slope Bottom Width Discharge		0.030 0.01000 4.00 4.00 6.00 35.00	ft/ft ft/ft (H:V) ft/ft (H:V) ft ft ft³/s
Results			
Normal Depth Flow Area Wetted Perimeter Hydraulic Radius Top Width Critical Depth Critical Slope Velocity Velocity Head Specific Energy Froude Number Flow Type	Subcritical	0.94 9.23 13.79 0.67 13.55 0.84 0.01573 3.79 0.22 1.17	ft ft² ft ft ft ft ft ft ft ft ft/ft ft/s ft/s
GVF Input Data			
Downstream Depth Length Number Of Steps		0.00 0.00 0	ft ft

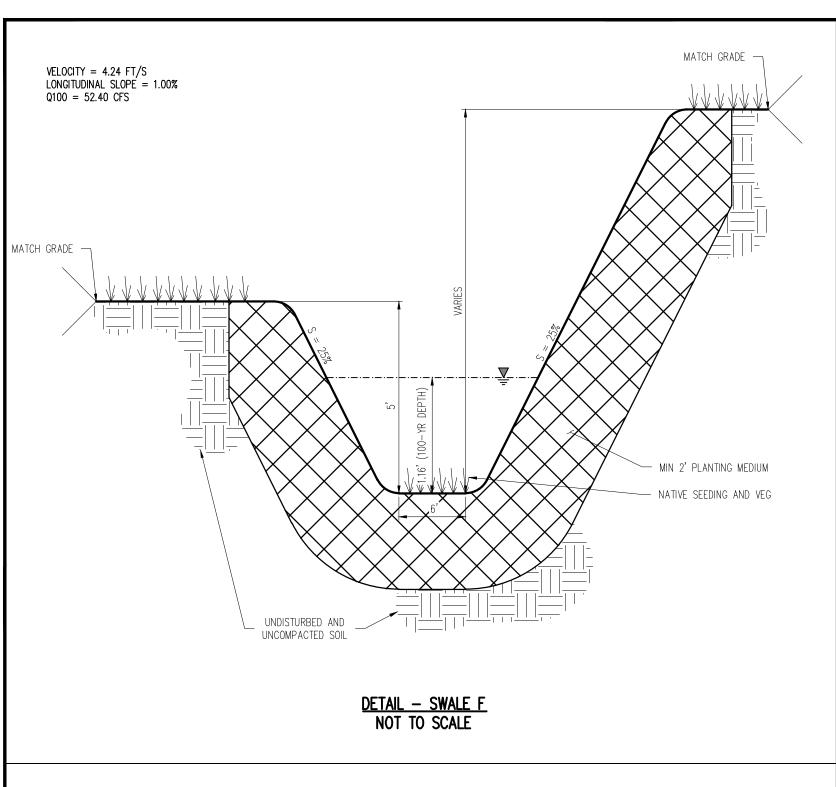
#### **GVF Output Data**

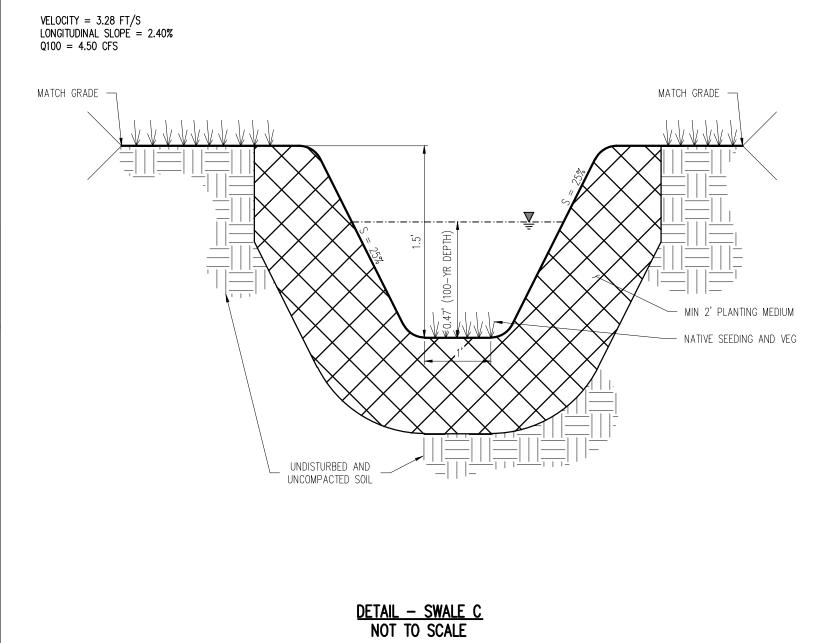
Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.94	ft
Critical Depth	0.84	ft
Channel Slope	0.01000	ft/ft

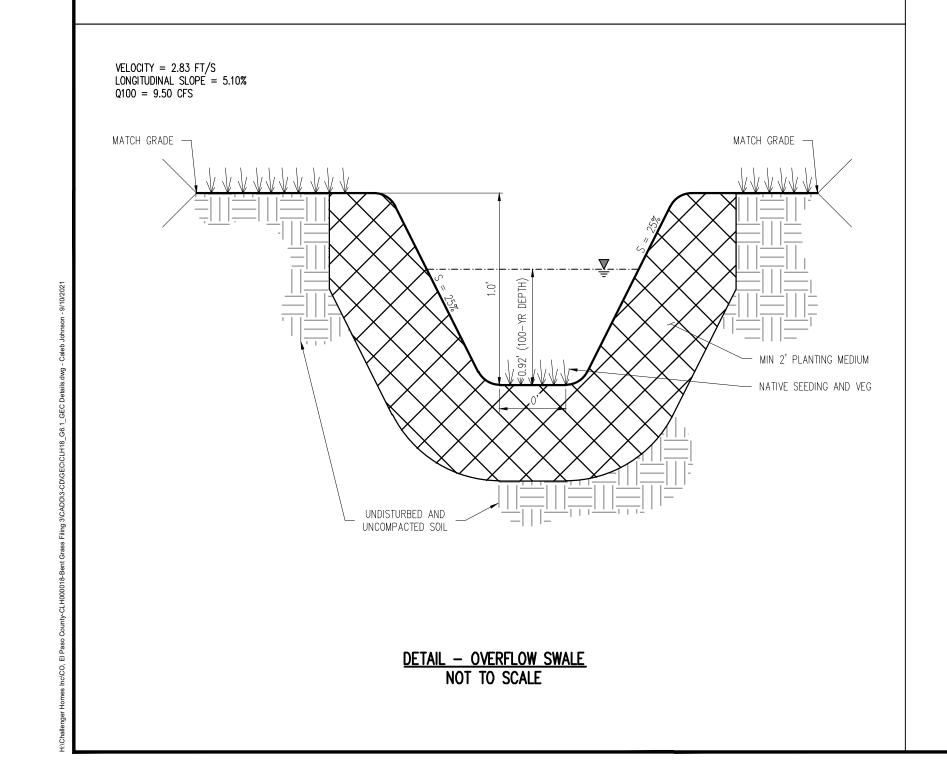
### Worksheet for Swale - F (Proposed)

### **GVF** Output Data

Critical Slope 0.01573 ft/ft









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FILING NO. CONSTRUCTION DOCUMENTS FALCON MEADOWS AT BENT FOR CHALLENGER COMMUNTIES,

# Date Issue / Description

CLH000018 RGD Date: 09/10/202
SWALE CROSS SECTIONS 09/10/2021

Sheet 17 of 23

EPC 9/28/2021

	Worksheet for Swale - B	Temporary)	
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient	0.03		
Channel Slope	0.010	ft/ft	
Left Side Slope	4.0	ft/ft (H:V)	
Right Side Slope	4.0	ft/ft (H:V)	
Bottom Width	0.0	ft	
Discharge	19.0	ft³/s	
Results			
Normal Depth	1.:	ft	
Flow Area	6.	ft²	
Wetted Perimeter	10.4	ft	
Hydraulic Radius	0.0	ft	
Top Width	10.	ft	
Critical Depth	1.	ft	
Critical Slope	0.022	ft/ft	
Velocity	3.0	ft/s	
Velocity Head	0.	ft	
Specific Energy	1.4	ft	
Froude Number	0.0		
Flow Type	Subcritical		
GVF Input Data			
Downstream Depth	0.	ft	
Length	0.0	ft	
Number Of Steps			
GVF Output Data			
Upstream Depth	0.	ft	
Profile Description			
Profile Headloss	0.	ft	
Downstream Velocity	Infin	ft/s	
Upstream Velocity	Infin	ft/s	
Normal Depth	1.:	ft	

1.08 ft

0.01000 ft/ft

Critical Depth

Channel Slope

	Worksheet	for Swa	le - D	
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.040		
Channel Slope		0.02000	ft/ft	
Left Side Slope		4.00	ft/ft (H:V)	
Right Side Slope		4.00	ft/ft (H:V)	
Bottom Width		2.00	ft	
Discharge		66.00	ft³/s	
Results				
Normal Depth		1.61	ft	
Flow Area		13.58	ft²	
Wetted Perimeter		15.27	ft	
Hydraulic Radius		0.89	ft	
Top Width		14.88	ft	
Critical Depth		1.53	ft	
Critical Slope		0.02526	ft/ft	
Velocity		4.86	ft/s	
Velocity Head		0.37	ft	
Specific Energy		1.98	ft	
Froude Number		0.90		
Flow Type	Subcritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	#	

•		
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	1.61	ft
Critical Depth	1.53	ft
Channel Slope	0.02000	ft/ft

nula	
0.030	
0.00500	ft/ft
4.00	ft/ft (H:V)
4.00	ft/ft (H:V)
3.00	ft
68.40	ft³/s
1.83	ft
18.95	ft²
18.12	ft
1.05	ft
17.67	ft
1.46	ft
0.01415	ft/ft
3.61	ft/s
0.20	ft
2.04	ft
0.61	
0.00	ft
0.00	ft
0	
0.00	ft
0.00	ft
Infinity	ft/s
	1.46 0.01415 3.61 0.20 2.04 0.61

1.83 ft

1.46 ft

0.00500 ft/ft

Normal Depth

Critical Depth

Channel Slope



Subject: SWALE BEND CALCULATIONS

H= CV2W

FIZON EL PASO COUNTY Den 10.5.6

C=0.5 (SUBCRITICAL FLOW)

V= AVERAGE VELOCITY = 3.61 PM fps

W=CHANNEL WINDTH AT WATER SURFACE = 17.67'

g=GRAVITY=32.2 fx=

-ADDITIONAL FIZEBOAIZED FOR CHANNEL BEND

RE RADIUS OF CURVATURE: 12'
HEADDITIONAL HEIGHT OF FREE BOARD

H= 0.5(3.61) (17.67) = 0.29'

FLOW DEPTH : 1.83'

=> FLOW DEPTH THEROUGH BEND=2.12'

### **Inlets-Proposed Design**

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Filing No. 2 Project: Inlet ID: DP 14a-Street Cap Check STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb $S_{\text{BACK}}$ Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 17.0 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d<sub>MAX</sub> Allow Flow Depth at Street Crown (leave blank for no) check = yes

Minor Storm

12.4

Major Storm

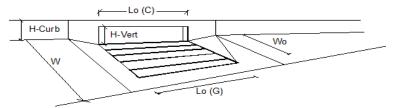
MINOR STORM Allowable Capacity is based on Spread Criterion

MAJOR STORM Allowable Capacity is based on Spread Criterion

inor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' ajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

#### **INLET ON A CONTINUOUS GRADE**

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =			inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =			
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =			ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =			ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f$ - $G =$			
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}C =$			
		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =			cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$			cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =			%

#### Version 4.06 Released August 2018 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Filing No. 2 Project: DP 14b-Street Cap Check Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb $S_{\text{BACK}}$ Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 17.0 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

MINOR STORM Allowable Capacity is based on Spread Criterion MAJOR STORM Allowable Capacity is based on Spread Criterion Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Max. Allowable Spread for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

Minor Storm Major Storm
Q<sub>allow</sub> = 12.4 12.4

Minor Storm

d<sub>MAX</sub>

Major Storm

check = yes

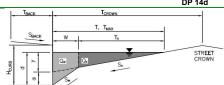
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

#### Version 4.06 Released August 2018

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

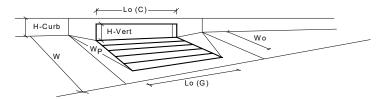
Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2 DP 14d



#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

#### **INLET IN A SUMP OR SAG LOCATION**

Version 4.06 Released August 2018



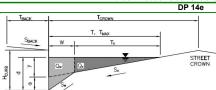
Design Information (Input)	CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	CDO1 Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.6	8.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (t	ypical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical val	lue 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical v	value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L <sub>0</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in	n Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in In	nches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (ty	ypically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	ypical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduct	ion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	uation	d <sub>Curb</sub> =	0.30	0.50	ft
Combination Inlet Performance R	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.72	1.00	
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reducti	ion Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
			MINOR	MAJOR	_
Total Inlet Interception Ca	apacity (assumes clogged condition)	Q <sub>a</sub> =	4.6	9.3	cfs
Inlet Capacity IS GOOD for Mine	or and Major Storms(>Q PEAK)	Q <sub>PEAK REQUIRED</sub> =	3.3	6.7	cfs

#### Version 4.06 Released August 2018

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

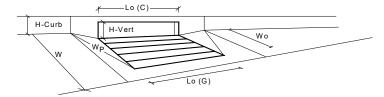
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2



#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

#### **INLET IN A SUMP OR SAG LOCATION**

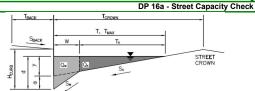


Design Information (Input)	ODOTT D Out - Out - Out -		MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.6	8.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (t	ypical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical val	lue 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical v	ralue 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L <sub>0</sub> (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in	n Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in In	ches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	pical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduct	ion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	uation	d <sub>Curb</sub> =	0.30	0.50	ft
Combination Inlet Performance R	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.53	0.75	
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	0.91	1.00	
Grated Inlet Performance Reducti	on Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception Ca	apacity (assumes clogged condition)	$Q_a =$	6.9	16.3	cfs
Inlet Capacity IS GOOD for Mine	or and Major Storms(>Q PEAK)	Q <sub>PEAK REQUIRED</sub> =	6.0	12.2	cfs

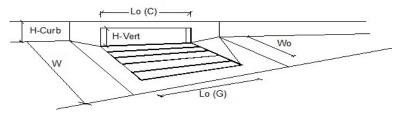
#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2



#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 12.4 12.4 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managem lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managem



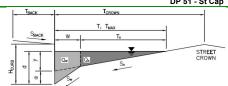
Design Information (Input)			MINOR	MAJOR	
Type of Inlet	Ту	oe =			
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOO</sub>	:AL =			inches
Total Number of Units in the Inlet (Grate or Curb Opening)	ı	1o =			
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =			ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	\	V <sub>o</sub> =			ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub>	·G =			
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f$	-C =			
			MINOR	MAJOR	
Total Inlet Interception Capacity		Q =			cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Չ <sub>Ի</sub> =			cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C	% =			%

#### Version 4.06 Released August 2018

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
Falcon Meadows at Bent Grass Filing No. 2
DP 51 - St Cap

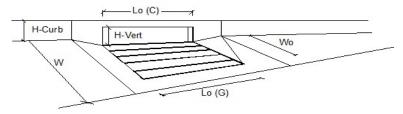
Project: Inlet ID:



MAJOR STORM Allowable Capacity is based on Spread Criterion	Q <sub>allow</sub> =	10.9	10.9	cfs
MINOR STORM Allowable Capacity is based on Spread Criterion	_	Minor Storm	Major Storm	_
NIOW Flow Deput at Street Clown (leave blank for no)				check – yes
Now Flow Depth at Street Crown (leave blank for no)	UMAX -	6.0	12.0	check = ves
Max. Allowable Spread for Minor & Major Storm  Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	T <sub>MAX</sub> = d <sub>MAX</sub> =	17.0 6.0	17.0 12.0	ft inches
Ann Allewahle Courselfor Minera O Malon Champ	т -Г	Minor Storm	Major Storm	
, , , , , , , , , , , , , , , , , , , ,	-		•	
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n <sub>STREET</sub> =	0.016		
Street Longitudinal Slope - Enter 0 for sump condition	s <sub>o</sub> =	0.010	ft/ft	
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S <sub>W</sub> =	0.083	ft/ft	
Street Transverse Slope	VV - S <sub>X</sub> =	0.020	ft/ft	
Sutter Width	V =	2.00	ft	
Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown	H <sub>CURB</sub> = T <sub>CROWN</sub> =	6.00 17.0	inches ft	
naming 5 Rooginios5 Bernita Galb (typicany between 6.512 and 6.526)	- BACK	0.013	1	
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n <sub>BACK</sub> =	0.020	TUTE	
Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	T <sub>BACK</sub> = S <sub>BACK</sub> =	0.020	ft ft/ft	
Gutter Geometry (Enter data in the blue cells)	F		1.	

DP 51-St Cap.xlsm, DP 51 - St Cap 11/30/2021, 8:11 AM

#### Version 4.06 Released August 2018



Design Information (Input)  CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.3	11.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	2.9	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	80	%

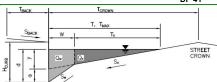
DP 51-St Cap.xlsm, DP 51 - St Cap 11/30/2021, 8:11 AM

### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2

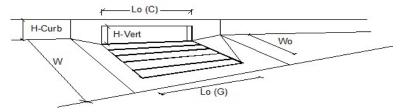
DP 41



#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.028 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 18.1 18.2 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management /ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Manag

DP 41-St Cap.xlsm, DP 41 11/30/2021, 8:17 AM

#### Version 4.06 Released August 2018

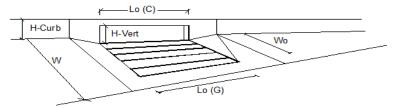


Design Information (Input)  CDOT Type R Curb Opening	ī .	MINOR	MAJOR	_
Type of Inlet	☐ Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>r</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	11.5	17.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	2.6	13.0	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	82	57	%

DP 41-St Cap.xlsm, DP 41 11/30/2021, 8:17 AM

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Filing No. 2 Project: DP 42-Street Capacity Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 17.0 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.030 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d<sub>MAX</sub> Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 18.8 inor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

ajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =			inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =			
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>0</sub> =			ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =			ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =			
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =			
	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =			cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =			cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =			%

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Filing No. 2 Project: DP 43-Street Capacity Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 17.0 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.010 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d<sub>MAX</sub> Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 10.9 10.9 inor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

ajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

#### Version 4.06 Released August 2018

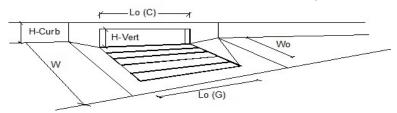
#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2 DP 44-Street Capacity

Toron Toron

#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 10.9 10.9 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managem lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managem



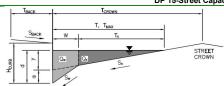
Design Information (Input) Type of Inlet  CDOT Type R Curb Opening  ▼	Type =	MINOR CDOT Type F	MAJOR Curb Opening	1
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.7	9.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	1.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	90	%

#### Version 4.06 Released August 2018

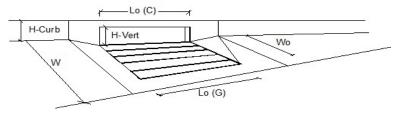
#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2 DP 15-Street Capacity



#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 10.9 10.9 cfs linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management /ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Manag



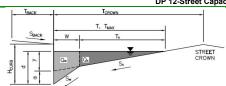
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type :	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> :	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No :	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> :	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> ·G :	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C :	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q:	4.9	15.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b$ :	0.0	9.0	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% :	100	63	%

#### Version 4.06 Released August 2018

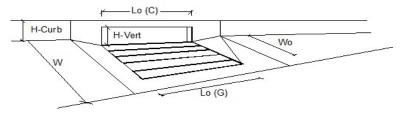
#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: Falcon Meadows at Bent Grass Filing No. 2 DP 12-Street Capacity



#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 17.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.030 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 17.7 18.8 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managem lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managem

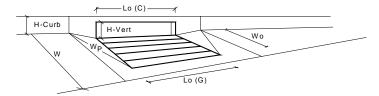


Design Information (Input)  CDOT Type R Curb Opening	_	MINOR	MAJOR	7
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.3	10.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	1.3	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	89	%

## Inlets – Existing Analysis

#### Inlet DP 8 - Existing Sump Inlet

#### **INLET IN A SUMP OR SAG LOCATION**



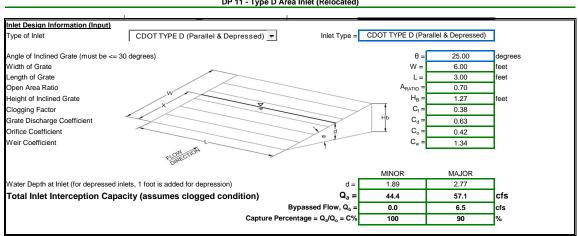
Design Information (Input)  CDOT Type R Curb Opening  ▼	_	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.57	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.79	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
	_	MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	14.4	52.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	7.7	28.7	cfs

#### Inlet DP 11 - Existing Area Inlet

Version 4.06 Released August 2018

#### **AREA INLET IN A SWALE**

# Falcon Meadows at Bent Grass Filing No. 2 - Existing Inlet Analysis DP 11 - Type D Area Inlet (Relocated)

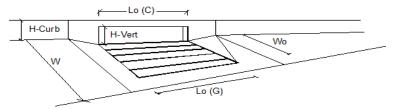


Warning 04: Froude No. exceeds USDCM Volume I recommendation.

#### Inlet DP 16 - Existing At-Grade Inlet

#### **INLET ON A CONTINUOUS GRADE**

Version 4.06 Released August 2018

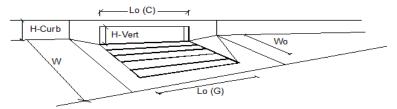


Design Information (Input)	_	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening  ▼	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f - C =$	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.1	11.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	3.1	15.8	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	70	42	%

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### Inlet DP 14 - Existing At-Grade Inlet

#### **INLET ON A CONTINUOUS GRADE**

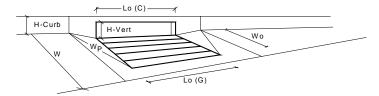


Design Information (Input)  CDOT Type R Curb Opening  ▼	_	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.6	8.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.9	5.8	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	85	59	%

#### Inlet DP 17 - Existing Sump Inlet

#### INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



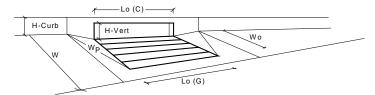
WARNING: Inlet Capacity less than Q Peak for Minor Storm	Q <sub>PEAK REQUIRED</sub> =	8.4	12.7	cfs
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	8.0	39.1	cfs
	_	MINOR	MAJOR	_
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	_
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.76	1.00	-
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.53	1.00	4
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.30	0.83	ft
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Low Head Performance Reduction (Calculated)	_	MINOR	MAJOR	_
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	15.00	15.00	feet
Curb Opening Information	-0(-)	MINOR	MAJOR	_
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	-
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Grate Information	Foliality Depth =	MINOR	MAJOR	✓ Override Depths
Nater Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	12.0	inches
Local Depression (additional to continuous gutter depression 'a' from above)  Number of Unit Inlets (Grate or Curb Opening)	a <sub>local</sub> = No =	3.00	3.00	inches
type of inlet	Type =		Curb Opening	
Design Information (Input)  CDOT Type R Curb Opening  ▼	_	MINOR	MAJOR	

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#### Inlet DP 18 - Existing Sump Inlet

#### INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018

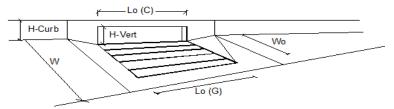


Design Information (Input)	CDOT Type R Curb Opening   ▼	_	MINOR	MAJOR	_
Type of Inlet	CDO1 Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to c	ontinuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.6	12.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (	typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grat	e (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical va	lue 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	1
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L <sub>0</sub> (C) =	15.00	15.00	feet
Height of Vertical Curb Opening i	n Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in I	nches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curt	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Eq	uation	d <sub>Curb</sub> =	0.30	0.83	ft
Combination Inlet Performance R	Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.53	1.00	
Curb Opening Performance Redu	uction Factor for Long Inlets	RF <sub>Curb</sub> =	0.76	1.00	
Grated Inlet Performance Reduct	tion Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		_	MINOR	MAJOR	
Total Inlet Interception Ca	apacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	8.0	39.1	cfs
WARNING: Inlet Capacity less	than Q Peak for Minor Storm	Q PEAK REQUIRED =	10.4	21.9	cfs

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#### Inlet DP 24 - Existing At-Grade Inlet

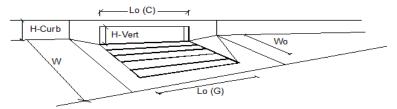
#### **INLET ON A CONTINUOUS GRADE**



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	25.00	25.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	1
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	7.1	22.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	3.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	88	%

#### Inlet DP 25 - Existing At-Grade Inlet

#### **INLET ON A CONTINUOUS GRADE**

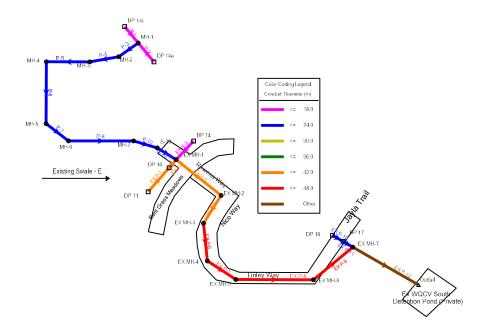


Design Information (Input)				MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	-	Type =		Curb Opening	7
Local Depression (additional to cor	ntinuous gutter depression 'a')		a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (	Grate or Curb Opening)		No =	1	1	1
Length of a Single Unit Inlet (Grate	or Curb Opening)		L <sub>o</sub> =	25.00	25.00	ft
Width of a Unit Grate (cannot be gi	reater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit (	Grate (typical min. value = 0.5)		C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)		C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allov	vable Street Capacity'			MINOR	MAJOR	_
Total Inlet Interception Capacity			Q =	2.8	8.4	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	0.0	cfs	
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =		C% =	100	100	%	

### **StormCAD**

### Falcon Meadows at Bent Grass Filing No. 2 Scenario: 5 YR

**Active Scenario: 5 YR** 



# Falcon Meadows at Bent Grass Filing No. 2 FlexTable: Conduit Table Active Scenario: 100 YR

Label	Start Node	Stop Node	Length (User Defined) (ft)	Diameter (in)	Manning's n	Capacity (Full Flow) (cfs)	Flow (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Hydraulic Grade Line (In) (ft)	Elevation Ground (Stop) (ft)	Invert (Stop) (ft)	Hydraulic Grade Line (Out) (ft)	Slope (Calculated) (ft/ft)
EX P-1	DP 11	DP 16	99.5	42.0	0.013	152.97	57.03	5.93	6,946.03	6,940.50	6,944.06	6,948.24	6,938.20	6,943.74	0.023
EX P-2	DP 16	EX MH-1	7.5	42.0	0.013	201.21	79.06	8.22	6,948.24	6,937.90	6,943.22	6,948.02	6,937.60	6,943.17	0.040
EX P-3	DP 14	EX MH-1	27.5	18.0	0.013	10.41	11.78	6.67	6,948.30	6,939.57	6,943.52	6,948.02	6,939.30	6,943.17	0.010
EX P-4	EX MH-1	EX MH-2	211.5	42.0	0.013	100.50	101.84	10.59	6,948.02	6,937.30	6,941.95	6,946.72	6,935.19	6,939.78	0.010
EX P-5	EX MH-2	EX MH-3	132.1	42.0	0.013	100.95	101.05	10.50	6,946.72	6,934.89	6,938.58	6,945.39	6,933.56	6,937.25	0.010
EX P-6	EX MH-3	EX MH-4	75.2	48.0	0.013	143.41	100.55	12.35	6,945.39	6,933.06	6,936.35	6,944.74	6,932.31	6,936.31	0.010
EX P-7	EX MH-4	EX MH-5	61.2	48.0	0.013	120.39	100.31	10.72	6,944.74	6,932.01	6,935.50	6,944.31	6,931.58	6,935.35	0.007
EX P-8	EX MH-5	EX MH-6	235.3	48.0	0.013	122.08	100.08	10.84	6,944.31	6,931.28	6,934.31	6,942.08	6,929.58	6,933.33	0.007
EX P-9	EX MH-6	EX MH-7	119.8	48.0	0.013	149.66	99.22	12.73	6,942.08	6,929.28	6,932.30	6,941.78	6,927.98	6,932.23	0.011
EX P-10	DP 18	DP 17	35.0	24.0	0.013	48.52	18.25	5.81	6,941.57	6,931.85	6,934.94	6,941.57	6,930.24	6,934.71	0.046
EX P-11	DP 17	EX MH-7	9.2	24.0	0.013	50.53	41.50	13.21	6,941.57	6,929.94	6,932.54	6,941.78	6,929.48	6,932.23	0.050
EX P-12	EX MH-7	Outfall	253.3	54.0	0.013	150.31	134.16	10.68	6,941.78	6,927.48	6,930.89	6,932.00	6,926.00	6,929.31	0.006
P-1	DP 14d	MH-1	6.3	18.0	0.013	15.08	7.48	8.52	6,955.22	6,950.84	6,952.19	6,954.90	6,950.71	6,952.19	0.021
P-2	DP 14e	MH-1	28.7	18.0	0.013	10.56	10.34	6.81	6,955.22	6,951.00	6,952.42	6,954.90	6,950.71	6,952.19	0.010
P-3	MH-1	MH-2	68.5	24.0	0.013	32.79	16.92	10.52	6,954.90	6,950.21	6,951.69	6,955.44	6,948.77	6,950.38	0.021
P-4	MH-2	MH-3	84.1	24.0	0.013	35.40	16.86	11.13	6,955.44	6,948.47	6,949.95	6,956.29	6,946.41	6,949.01	0.024
P-5	MH-3	MH-4	133.9	24.0	0.013	20.22	16.80	5.35	6,956.29	6,946.11	6,948.74	6,956.38	6,945.04	6,948.00	0.008
P-6	MH-4	MH-5	260.9	24.0	0.013	20.49	16.57	5.27	6,956.38	6,944.74	6,947.66	6,953.14	6,942.60	6,946.26	0.008
P-7	MH-5	MH-6	49.0	24.0	0.013	20.18	16.12	5.13	6,953.14	6,942.30	6,945.97	6,952.59	6,941.91	6,945.72	0.008
P-8	MH-6	MH-7	218.3	24.0	0.013	18.63	16.04	5.11	6,952.59	6,941.61	6,945.44	6,949.80	6,940.13	6,944.34	0.007
P-10	MH-7	S-30	66.8	24.0	0.013	19.96	15.65	4.98	6,949.80	6,939.83	6,944.07	6,948.86	6,939.31	6,943.75	0.008
P-10(1)	S-30	EX MH-1	66.8	24.0	0.013	19.77	15.53	4.94	6,948.86	6,939.31	6,943.48	6,948.02	6,938.80	6,943.17	0.008

# Falcon Meadows at Bent Grass Filing No. 2 FlexTable: Manhole Table Active Scenario: 100 YR

Label	Elevation (Rim) (ft)	Headloss Method	Headloss (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Diameter (in)
EX MH-1	6,948.02	Standard	1.22	6,943.17	6,941.95	6,943.86	6,943.69	84.0
EX MH-2	6,946.72	Standard	1.20	6,939.78	6,938.58	6,941.53	6,940.30	84.0
EX MH-3	6,945.39	Standard	0.90	6,937.25	6,936.35	6,938.97	6,937.64	84.0
EX MH-4	6,944.74	Standard	0.81	6,936.31	6,935.50	6,937.30	6,936.65	84.0
EX MH-5	6,944.31	Standard	1.04	6,935.35	6,934.31	6,936.39	6,935.80	84.0
EX MH-6	6,942.08	Standard	1.03	6,933.33	6,932.30	6,934.37	6,933.78	84.0
EX MH-7	6,941.78	Standard	1.34	6,932.23	6,930.89	6,933.20	6,932.56	96.0
MH-1	6,954.90	Standard	0.50	6,952.19	6,951.69	6,952.73	6,952.41	48.0
MH-2	6,955.44	Standard	0.43	6,950.38	6,949.95	6,950.98	6,950.66	48.0
MH-3	6,956.29	Standard	0.27	6,949.01	6,948.74	6,949.45	6,949.18	48.0
MH-4	6,956.38	Standard	0.35	6,948.00	6,947.66	6,948.45	6,948.09	48.0
MH-5	6,953.14	Standard	0.29	6,946.26	6,945.97	6,946.69	6,946.38	48.0
MH-6	6,952.59	Standard	0.28	6,945.72	6,945.44	6,946.13	6,945.84	48.0
MH-7	6,949.80	Standard	0.27	6,944.34	6,944.07	6,944.75	6,944.46	48.0
S-30	6,948.86	Standard	0.27	6,943.75	6,943.48	6,944.14	6,943.86	48.0

## Falcon Meadows at Bent Grass Filing No. 2

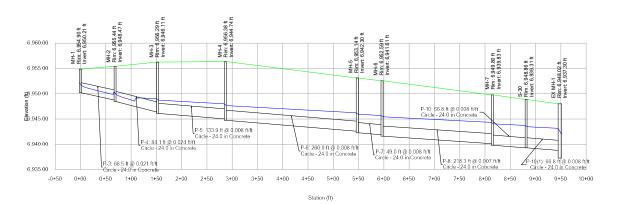
#### FlexTable: Outfall Table

**Active Scenario: 100 YR** 

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)	
Outfall	6,932.00	6,926.00	User Defined Tailwater	6,927.87	6,929.31	6,929.31	132.89	

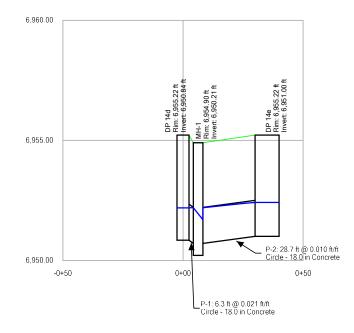
# Falcon Meadows at Bent Grass Filing No. 2 Profile Report

# Engineering Profile - Mainline Storm Sys (FM Filing 2 System A.stsw) Active Scenario: 100 YR



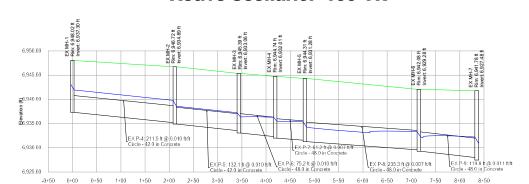
# evation (ft)

# Falcon Meadows at Bent Grass Filing No. 2 Profile Report Engineering Profile - Laterals (FM Filing 2 System A.stsw) Active Scenario: 100 YR



Station (ft)

# Falcon Meadows at Bent Grass Filing No. 2 Profile Report Engineering Profile - Ex Mainline (FM Filing 2 System A.stsw) Active Scenario: 100 YR

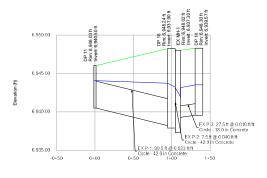


Station (ft)

# Falcon Meadows at Bent Grass Filing No. 2 Profile Report

# Engineering Profile - Ex Rowena Way Laterals (FM Filing 2 System A.stsw)

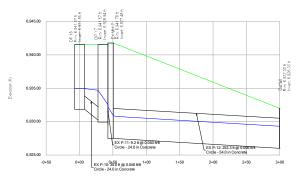
**Active Scenario: 100 YR** 



Station (ft)

### Falcon Meadows at Bent Grass Filing No. 2 Profile Report

#### Engineering Profile - Ex Jayla Laterals & Outlet (FM Filing 2 System A.stsw)



## Falcon Meadows at Bent Grass Filing No. 2 FlexTable: Conduit Table

Label	Start Node	Stop Node	Length (User Defined) (ft)	Diameter (in)	Manning's n	Capacity (Full Flow) (cfs)	Flow (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Hydraulic Grade Line (In) (ft)	Elevation Ground (Stop) (ft)	Invert (Stop) (ft)	Hydraulic Grade Line (Out) (ft)	Slope (Calculated) (ft/ft)
EX P-1	DP 11	DP 16	99.5	42.0	0.013	152.97	11.46	9.34	6,946.03	6,940.50	6,941.53	6,948.24	6,938.20	6,939.49	0.023
EX P-2	DP 16	EX MH-1	7.5	42.0	0.013	201.21	19.13	13.18	6,948.24	6,937.90	6,939.24	6,948.02	6,937.60	6,939.38	0.040
EX P-3	DP 14	EX MH-1	27.5	18.0	0.013	10.41	4.93	5.81	6,948.30	6,939.57	6,940.42	6,948.02	6,939.30	6,940.04	0.010
EX P-4	EX MH-1	EX MH-2	211.5	42.0	0.013	100.50	28.27	8.97	6,948.02	6,937.30	6,938.94	6,946.72	6,935.19	6,936.96	0.010
EX P-5	EX MH-2	EX MH-3	132.1	42.0	0.013	100.95	28.01	8.98	6,946.72	6,934.89	6,936.52	6,945.39	6,933.56	6,934.83	0.010
EX P-6	EX MH-3	EX MH-4	75.2	48.0	0.013	143.41	27.85	8.84	6,945.39	6,933.06	6,934.62	6,944.74	6,932.31	6,933.98	0.010
EX P-7	EX MH-4	EX MH-5	61.2	48.0	0.013	120.39	27.76	7.78	6,944.74	6,932.01	6,933.57	6,944.31	6,931.58	6,933.24	0.007
EX P-8	EX MH-5	EX MH-6	235.3	48.0	0.013	122.08	27.67	7.86	6,944.31	6,931.28	6,932.84	6,942.08	6,929.58	6,931.23	0.007
EX P-9	EX MH-6	EX MH-7	119.8	48.0	0.013	149.66	27.35	9.06	6,942.08	6,929.28	6,930.83	6,941.78	6,927.98	6,929.80	0.011
EX P-10	DP 18	DP 17	35.0	24.0	0.013	48.52	7.89	11.37	6,941.57	6,931.85	6,932.85	6,941.57	6,930.24	6,931.74	0.046
EX P-11	DP 17	EX MH-7	9.2	24.0	0.013	50.53	13.64	13.66	6,941.57	6,929.94	6,931.27	6,941.78	6,929.48	6,930.44	0.050
EX P-12	EX MH-7	Outfall	253.3	54.0	0.013	150.31	38.67	7.92	6,941.78	6,927.48	6,929.27	6,932.00	6,926.00	6,927.56	0.006
P-1	DP 14d	MH-1	6.3	18.0	0.013	15.08	2.42	6.26	6,955.22	6,950.84	6,951.43	6,954.90	6,950.71	6,951.36	0.021
P-2	DP 14e	MH-1	28.7	18.0	0.013	10.56	4.48	5.73	6,955.22	6,951.00	6,951.81	6,954.90	6,950.71	6,951.40	0.010
P-3	MH-1	MH-2	68.5	24.0	0.013	32.79	6.51	8.13	6,954.90	6,950.21	6,951.11	6,955.44	6,948.77	6,949.38	0.021
P-4	MH-2	MH-3	84.1	24.0	0.013	35.40	6.48	8.58	6,955.44	6,948.47	6,949.37	6,956.29	6,946.41	6,946.99	0.024
P-5	MH-3	MH-4	133.9	24.0	0.013	20.22	6.45	5.72	6,956.29	6,946.11	6,947.01	6,956.38	6,945.04	6,945.82	0.008
P-6	MH-4	MH-5	260.9	24.0	0.013	20.49	6.37	5.76	6,956.38	6,944.74	6,945.63	6,953.14	6,942.60	6,943.37	0.008
P-7	MH-5	MH-6	49.0	24.0	0.013	20.18	6.21	5.65	6,953.14	6,942.30	6,943.18	6,952.59	6,941.91	6,942.67	0.008
P-8	MH-6	MH-7	218.3	24.0	0.013	18.63	6.18	5.33	6,952.59	6,941.61	6,942.49	6,949.80	6,940.13	6,940.92	0.007
P-10	MH-7	S-30	66.8	24.0	0.013	19.96	6.04	5.57	6,949.80	6,939.83	6,940.70	6,948.86	6,939.31	6,940.41	0.008
P-10(1)	S-30	EX MH-1	66.8	24.0	0.013	19.77	5.99	5.52	6,948.86	6,939.31	6,940.18	6,948.02	6,938.80	6,939.56	0.008

### Falcon Meadows at Bent Grass Filing No. 2 FlexTable: Manhole Table

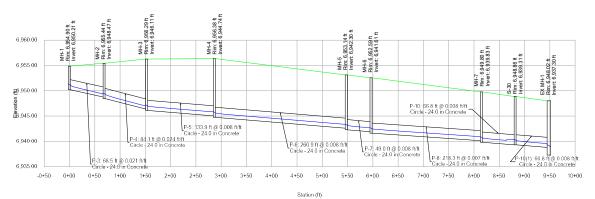
Label	Elevation (Rim) (ft)	Headloss Method	Headloss (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Diameter (in)
EX MH-1	6,948.02	Standard	0.44	6,939.38	6,938.94	6,939.62	6,939.57	84.0
EX MH-2	6,946.72	Standard	0.44	6,936.96	6,936.52	6,937.48	6,937.15	84.0
EX MH-3	6,945.39	Standard	0.41	6,935.03	6,934.62	6,936.27	6,935.21	84.0
EX MH-4	6,944.74	Standard	0.41	6,933.98	6,933.57	6,934.47	6,934.15	84.0
EX MH-5	6,944.31	Standard	0.41	6,933.24	6,932.84	6,933.73	6,933.42	84.0
EX MH-6	6,942.08	Standard	0.40	6,931.23	6,930.83	6,931.73	6,931.40	84.0
EX MH-7	6,941.78	Standard	0.54	6,929.80	6,929.27	6,930.18	6,929.94	96.0
MH-1	6,954.90	Standard	0.24	6,951.36	6,951.11	6,951.53	6,951.46	48.0
MH-2	6,955.44	Standard	0.21	6,949.58	6,949.37	6,950.59	6,949.72	48.0
MH-3	6,956.29	Standard	0.21	6,947.22	6,947.01	6,948.36	6,947.35	48.0
MH-4	6,956.38	Standard	0.27	6,945.91	6,945.63	6,946.42	6,945.98	48.0
MH-5	6,953.14	Standard	0.24	6,943.42	6,943.18	6,943.93	6,943.52	48.0
MH-6	6,952.59	Standard	0.23	6,942.72	6,942.49	6,943.22	6,942.82	48.0
MH-7	6,949.80	Standard	0.23	6,940.93	6,940.70	6,941.37	6,941.03	48.0
S-30	6,948.86	Standard	0.23	6,940.41	6,940.18	6,940.59	6,940.50	48.0

### Falcon Meadows at Bent Grass Filing No. 2 FlexTable: Outfall Table

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,932.00	6,926.00	User Defined Tailwater	6,926.56	6,927.56	6,927.56	38.18

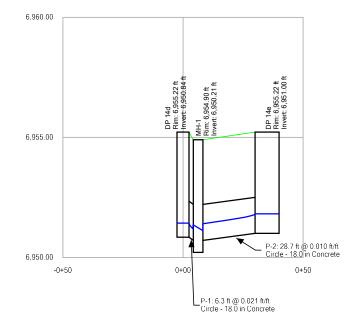
### Falcon Meadows at Bent Grass Filing No. 2 Profile Report

### Engineering Profile - Mainline Storm Sys (FM Filing 2 System A.stsw)

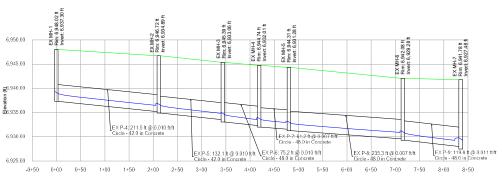


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# Falcon Meadows at Bent Grass Filing No. 2 Profile Report Engineering Profile - Laterals (FM Filing 2 System A.stsw) Active Scenario: 5 YR



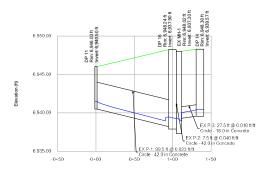
# Falcon Meadows at Bent Grass Filing No. 2 Profile Report Engineering Profile - Ex Mainline (FM Filing 2 System A.stsw) Active Scenario: 5 YR



## Falcon Meadows at Bent Grass Filing No. 2 Profile Report

#### Engineering Profile - Ex Rowena Way Laterals (FM Filing 2 System A.stsw)

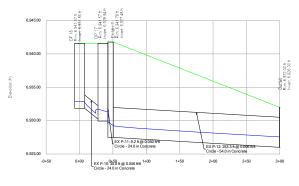
**Active Scenario: 5 YR** 



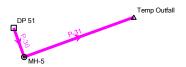
## Falcon Meadows at Bent Grass Filing No. 2 Profile Report

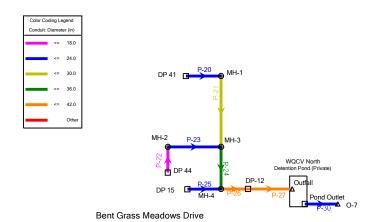
#### Engineering Profile - Ex Jayla Laterals & Outlet (FM Filing 2 System A.stsw)

**Active Scenario: 5 YR** 



System B Scenario: 100 YR Active Scenario: 100 YR





#### System B

FlexTable: Conduit Table Active Scenario: 100 YR

Label	Start Node	Stop Node	Length (User Defined) (ft)	Diameter (in)	Manning's n	Capacity (Full Flow) (cfs)	Flow (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Hydraulic Grade Line (In) (ft)	Elevation Ground (Stop) (ft)	Invert (Stop) (ft)	Hydraulic Grade Line (Out) (ft)	Slope (Calculated) (ft/ft)
P-20	DP 41	MH-1	6.4	24.0	0.013	17.84	22.78	7.25	6,952.21	6,946.36	6,948.18	6,951.95	6,946.32	6,948.02	0.006
P-21	MH-1	MH-3	136.7	30.0	0.013	45.73	22.76	9.30	6,951.95	6,945.82	6,947.44	6,949.54	6,944.12	6,946.93	0.012
P-22	DP 44	MH-2	7.5	18.0	0.013	10.85	11.36	6.43	6,949.87	6,945.66	6,947.27	6,949.58	6,945.58	6,947.18	0.011
P-23	MH-2	MH-3	36.8	24.0	0.013	25.30	11.36	7.84	6,949.58	6,945.08	6,947.01	6,949.54	6,944.62	6,946.93	0.013
P-24	MH-3	MH-4	43.8	36.0	0.013	74.10	30.92	4.37	6,949.54	6,943.62	6,946.66	6,949.05	6,943.08	6,946.57	0.012
P-25	DP 15	MH-4	7.5	24.0	0.013	23.36	17.02	5.42	6,949.27	6,944.16	6,946.61	6,949.05	6,944.08	6,946.57	0.011
P-26	MH-4	DP-12	27.5	42.0	0.013	101.51	46.30	4.81	6,949.05	6,942.58	6,946.28	6,949.29	6,942.30	6,946.22	0.010
P-27	DP-12	Outfall	32.8	42.0	0.013	100.96	61.44	6.39	6,949.29	6,942.20	6,945.71	6,948.20	6,941.87	6,945.59	0.010
P-30	Pond Outlet	0-7	27.8	24.0	0.013	22.69	32.80	10.44	6,946.00	6,940.33	6,942.59	6,942.00	6,940.05	6,941.95	0.010
P-30	DP 51	MH-5	7.5	18.0	0.013	10.85	11.98	6.78	6,963.48	6,959.19	6,960.81	6,963.25	6,959.11	6,960.71	0.011
P-31	MH-5	Temp Outfall	217.1	18.0	0.013	11.29	11.97	7.21	6,963.25	6,958.81	6,960.14	6,958.41	6,956.30	6,957.61	0.012

#### System B

FlexTable: Manhole Table Active Scenario: 100 YR

Label	Elevation (Rim) (ft)	Headloss Method	Headloss (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Diameter (in)
MH-1	6,951.95	Standard	0.57	6,948.01	6,947.44	6,949.01	6,948.15	60.0
MH-2	6,949.58	Standard	0.17	6,947.18	6,947.01	6,947.82	6,947.22	60.0
MH-3	6,949.54	Standard	0.27	6,946.93	6,946.66	6,947.13	6,946.96	72.0
MH-4	6,949.05	Standard	0.29	6,946.57	6,946.28	6,946.86	6,946.64	84.0
MH-5	6,963.25	Standard	0.57	6,960.71	6,960.14	6,961.42	6,960.95	48.0

System B

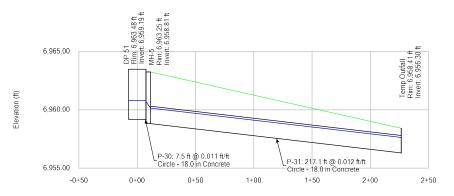
FlexTable: Outfall Table Active Scenario: 100 YR

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,948.20	6,941.87	User Defined Tailwater	6,945.59	6,945.59	6,945.59	61.33
0-7	6,942.00	6,940.05	Free Outfall		6,941.95	6,941.95	32.80
Temp Outfall	6,958.41	6,956.30	Free Outfall		6,957.61	6,957.61	11.73

#### System B

Profile Report
Engineering Profile - Temp Outfall (FM Filing 2 System B.stsw)

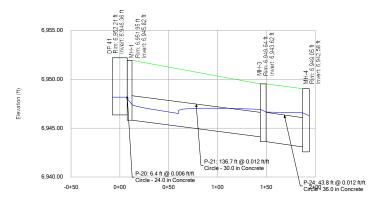
Active Scenario: 100 YR



#### System B

Profile Report
Engineering Profile - Mainline (FM Filing 2 System B.stsw)

Active Scenario: 100 YR

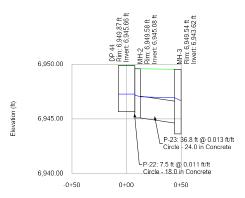


#### System B

#### Profile Report

Engineering Profile - Laterals - DP 44 (FM Filing 2 System B.stsw)

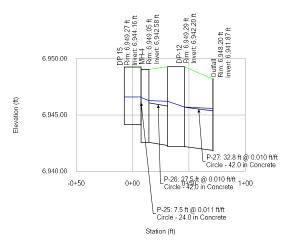
Active Scenario: 100 YR



#### System B

#### Profile Report

Engineering Profile - Laterals and Outfall to Pond (FM Filing 2 System B.stsw)

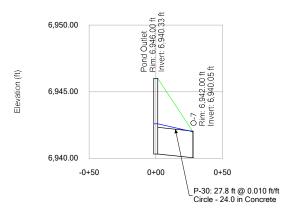


#### System B

#### Profile Report

Engineering Profile - Pond Outlet (FM Filing 2 System B.stsw)

Active Scenario: 100 YR



### System B FlexTable: Conduit Table

Label	Start Node	Stop Node	Length (User Defined) (ft)	Diameter (in)	Manning's n	Capacity (Full Flow) (cfs)	Flow (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Hydraulic Grade Line (In) (ft)	Elevation Ground (Stop) (ft)	Invert (Stop) (ft)	Hydraulic Grade Line (Out) (ft)	Slope (Calculated) (ft/ft)
P-20	DP 41	MH-1	6.4	24.0	0.013	17.84	9.37	5.75	6,952.21	6,946.36	6,947.45	6,951.95	6,946.32	6,947.37	0.006
P-21	MH-1	MH-3	136.7	30.0	0.013	45.73	9.36	7.32	6,951.95	6,945.82	6,946.84	6,949.54	6,944.12	6,945.24	0.012
P-22	DP 44	MH-2	7.5	18.0	0.013	10.85	4.38	5.81	6,949.87	6,945.66	6,946.46	6,949.58	6,945.58	6,946.29	0.011
P-23	MH-2	MH-3	36.8	24.0	0.013	25.30	4.38	6.04	6,949.58	6,945.08	6,945.81	6,949.54	6,944.62	6,945.19	0.013
P-24	MH-3	MH-4	43.8	36.0	0.013	74.10	12.47	7.79	6,949.54	6,943.62	6,945.04	6,949.05	6,943.08	6,945.13	0.012
P-25	DP 15	MH-4	7.5	24.0	0.013	23.36	3.78	5.46	6,949.27	6,944.16	6,945.12	6,949.05	6,944.08	6,945.13	0.011
P-26	MH-4	DP-12	27.5	42.0	0.013	101.51	15.62	7.64	6,949.05	6,942.58	6,945.08	6,949.29	6,942.30	6,945.08	0.010
P-27	DP-12	Outfall	32.8	42.0	0.013	100.96	21.72	8.36	6,949.29	6,942.20	6,945.00	6,948.20	6,941.87	6,945.00	0.010
P-30	Pond Outlet	0-7	27.8	24.0	0.013	22.69	6.20	6.15	6,946.00	6,940.33	6,941.21	6,942.00	6,940.05	6,940.78	0.010
P-30	DP 51	MH-5	7.5	18.0	0.013	10.85	4.64	5.90	6,963.48	6,959.19	6,960.02	6,963.25	6,959.11	6,959.84	0.011
P-31	MH-5	Temp Outfall	217.1	18.0	0.013	11.29	4.63	6.07	6,963.25	6,958.81	6,959.64	6,958.41	6,956.30	6,956.97	0.012

#### System B

FlexTable: Manhole Table
Active Scenario: 5 YR

Label	Elevation (Rim) (ft)	Headloss Method	Headloss (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Diameter (in)
MH-1	6,951.95	Standard	0.31	6,947.15	6,946.84	6,947.64	6,947.22	60.0
MH-2	6,949.58	Standard	0.22	6,946.03	6,945.81	6,946.47	6,946.09	60.0
MH-3	6,949.54	Standard	0.20	6,945.24	6,945.04	6,945.78	6,945.26	72.0
MH-4	6,949.05	Standard	0.06	6,945.13	6,945.08	6,945.22	6,945.15	84.0
MH-5	6,963.25	Standard	0.23	6,959.87	6,959.64	6,960.32	6,959.97	48.0

#### System B

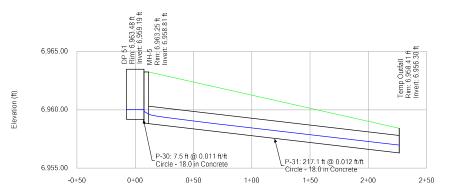
FlexTable: Outfall Table Active Scenario: 5 YR

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,948.20	6,941.87	User Defined Tailwater	6,945.00	6,945.00	6,945.00	21.69
0-7	6,942.00	6,940.05	Free Outfall		6,940.78	6,940.78	6.20
Temp Outfall	6,958.41	6,956.30	Free Outfall		6,956.97	6,956.97	4.52

#### System B

Profile Report
Engineering Profile - Temp Outfall (FM Filing 2 System B.stsw)

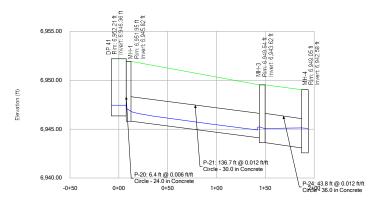
Active Scenario: 5 YR



#### System B

Profile Report
Engineering Profile - Mainline (FM Filing 2 System B.stsw)

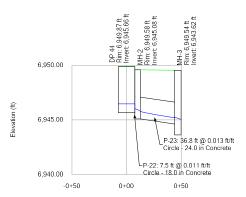
Active Scenario: 5 YR



#### System B

Profile Report
Engineering Profile - Laterals - DP 44 (FM Filing 2 System B.stsw)

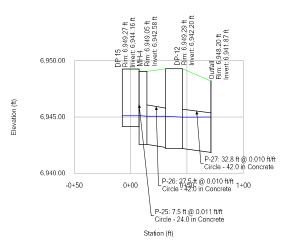
Active Scenario: 5 YR



#### System B

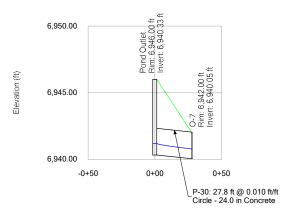
#### Profile Report

Engineering Profile - Laterals and Outfall to Pond (FM Filing 2 System B.stsw)



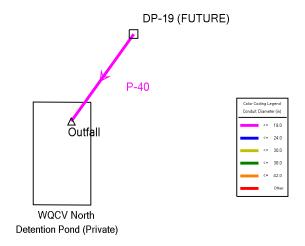
#### System B

Profile Report
Engineering Profile - Pond Outlet (FM Filing 2 System B.stsw)



Station (ft)

## Falcon Meadows at Bent Grass Filing No. 2 Storm System C (Future) Active Scenario: 100 YR



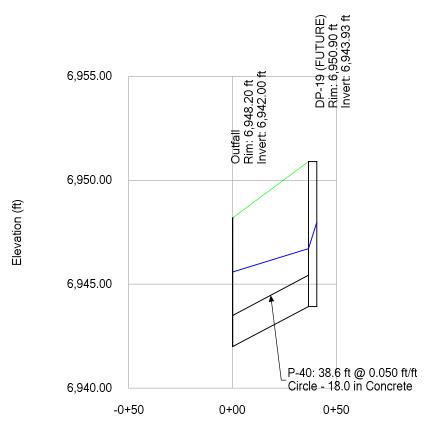
**Bent Grass Meadows Drive** 

#### Storm System C (Future)

Label	Start Node	Stop Node	Length (User	Diameter (in)	Manning's n	Capacity (Full	Flow (cfs)	Velocity (ft/s)	Elevation Ground	Invert (Start)	Hydraulic Grade	Elevation Ground	Invert (Stop)	Hydraulic Grade Line	Slope (Calculated)
			Defined) (ft)	` ,		Flow) (cfs)	, ,	, ,	(Start) (ft)	(ft)	Line (In) (ft)	(Stop) (ft)	(ft)	(Out) (ft)	(ft/ft)
P-40	DP-19 (FUTURE)	Outfall	38.6	18.0	0.013	23.49	17.90	10.13	6,950.90	6,943.93	6,946.71	6,948.20	6,942.0 0	6,945.59	0.050

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,948.20	6,942.00	User Defined Tailwater	6,945.59	6,945.59	6,945.59	17.85

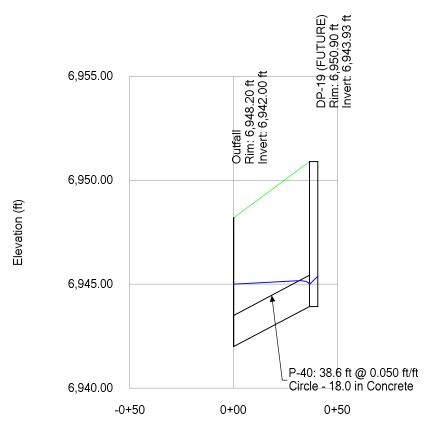
Active Scenario: 100 YR



Label	Start Node	Stop Node	Length	Diameter	Manning's	Capacity	Flow	Velocity	Elevation	Invert	Hydraulic	Elevation	Invert	Hydraulic	Slope
			(User	(in)	n	(Full	(cfs)	(ft/s)	Ground	(Start)	Grade	Ground	(Stop)	Grade Line	(Calculated)
			Defined)			Flow)			(Start)	(ft)	Line (In)	(Stop)	(ft)	(Out)	(ft/ft)
			(ft)			(cfs)			(ft)		(ft)	(ft)		(ft)	
P-40	DP-19 (FUTURE)	Outfall	38.6	18.0	0.013	23.49	7.52	11.82	6,950.90	6,943.93	6,944.99	6,948.20	6,942.0 0	6,945.00	0.050

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,948.20	6,942.00	User Defined Tailwater	6,945.00	6,945.00	6,945.00	7.50

Active Scenario: 5 YR



#### PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Falcon Meadows
Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass Filing N
Calculated By: TJE
Checked By: CMD
Date: 12/3/21

		Storm Dr	7		
	Temp Outfall Stm B	Pond Outfall	Forebay A	Forebay B	
Q100 (cfs)	19.6	38.7	61.5	23.5	
D or H (in)	18	24	42	18	
W (ft)					
Slope (%)	1.16	1.00	2.00	5.00	
Yn (in)	14.04	15.72	44.64	43.08	
Yt (ft)	Unknown	Unknown	1.06	2.39	If "Unknown" Yt/D=0.4
Yt/D, Yt/H	0.40	0.40	0.30	1.59	
Supercritical	Yes	No	No	No	Based on Froud Number >/< 1
Q/D^2.5, Q/WH^1.5	7.11	6.84	2.68	8.53	
Q/D^1.5, Q/WH^0.5		13.68	9.39	12.79	
Da, Ha (in) *	16.02				Da=0.5(D+Yn), Ha=0.5(H+Yn)
Q/Da^1.5, Q/WHa^0.5 *	12.71				
d50 (in), Required	10.99	11.34	10.87	2.02	
Required Riprap Size	M	M	M	L	
Use Riprap Size	L	M	M	L	Found using Figure 9-38 (USDCM)
d50 (in)	9	12	12	9	
1/(2 tan θ)	2.20	1.90	5.30	1.00	Found using Figure 9-35/9-36 (USDCM)
Erosive Soils	Yes	No	No	No	
At	3.56	5.03	7.99	3.05	A t = Q/5.5
L	9.8	8.1	21.4	-0.2	$L=(1/(2 \tan \theta))(A t/Yt - D)$
Min L	4.5	6.0	10.5	4.5	Min L=3D or 3H
Max L	15.0	20.0	35.0	15.0	Max L=10D or 10H
Length (ft)	10.0	9.0	22.0	4.5	
Bottom Width (ft)	4.5	6.0	10.5	4.5	Width=3D (Minimum)
Riprap Depth (in)	18	24	24	18	Depth=2(d 50)
Type II Base Depth (in)	6	6	6	6	
Cutoff Wall	No	No	No	No	
Cutoff Wall Depth (ft)					Depth of Riprap and Base
Cutoff Wall Width (ft)					

Note: No Type II Base to be used if Soil Riprap is specified within the plans

<sup>\*</sup> For use when the flow in the culvert is supercritical (and less than full).

<sup>\*\*</sup> This is a temporary minor storm culvert and the riprap has been sized for minor storm flows

Chapter 9 Hydraulic Structures

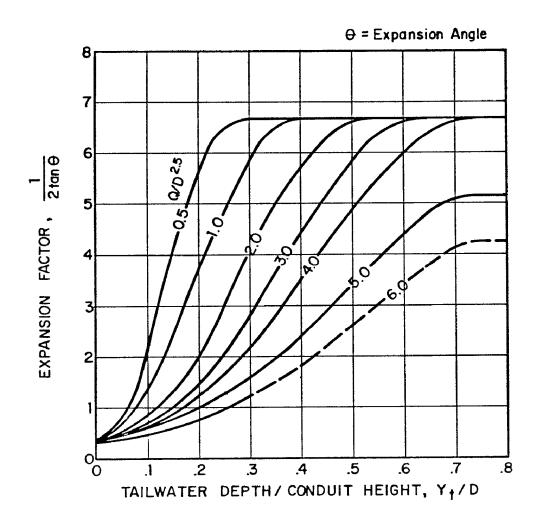


Figure 9-35. Expansion factor for circular conduits

Hydraulic Structures Chapter 9

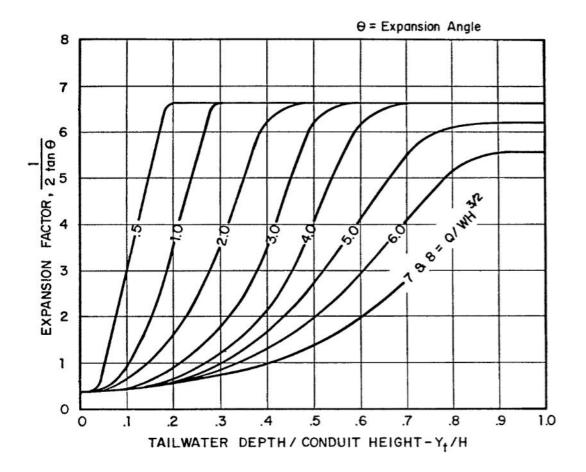


Figure 9-36. Expansion factor for rectangular conduits

# APPENDIX D On-Site Pond Calculations

### **Detention Pond Tributary Areas**

 Subdivision:
 Falcon Meadows

 Project Name:
 Falcon Meadows

Location:CO, Colorado SpringsProject No.:CLH000019Calculated By:TJE

Checked By: CMD

Date: 12/3/21

#### Pond (North)

Basin	Area	% Imp
C-1a	0.38	56.7
C-1b	0.45	72.8
C-1c	1.77	77.5
C-1d	1.72	73.2
C-1e	0.29	100
C-1f	0.08	100
C-2	3.98	71.6
C-3	0.18	85.7
C-4	2.67	50.3
C-5	0.60	2
D-1a	2.97	57.4
D-1f	1.61	67.4
Total	16.70	64.0

#### **Pond (South-Existing)**

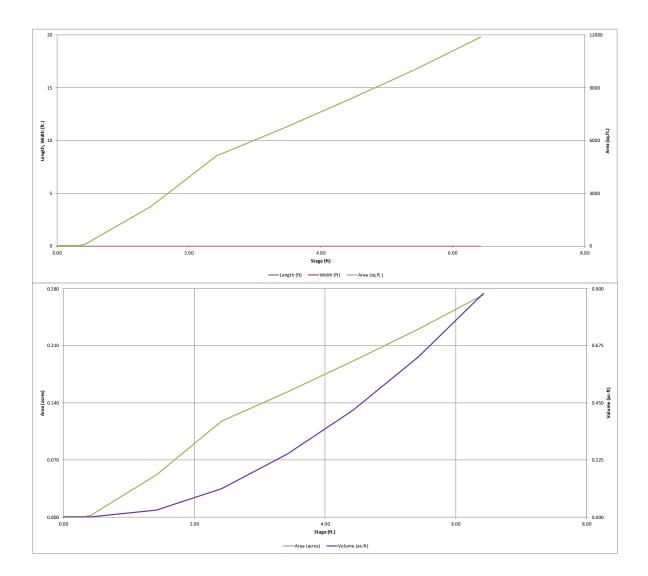
Basin	Area	% Imp
D-1b	2.54	62.2
D-2a	0.50	88.7
D-2b	0.74	61.8
D-2c	0.31	83.5
D-2d	0.24	81.3
D-2e	1.41	75.4
D-2f	2.43	73.6
D-2g	1.81	54.4
D-2h	0.23	65
D-3	2.26	54
D-4a	0.98	72.5
D-4b	0.95	80.9
D-4c	1.22	64.9
D-5	1.08	65.7
D-6a	1.33	76.6
D-6b	2.69	72.6
D-7	7.65	13.8
D-8	1.69	60.9
D-9	0.72	24.8
E-4	0.91	80.6
E-5	0.89	89
OS-2	20.07	8
OS-3	10.61	8
Total	63.26	32.1

## Pond (North) Calculations – Proposed Design

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.03 (May 2020)

Project:	Falcon Mead	ows at Bent	Grass Filing	No. 2										
	WQCV Pond	- North												
ZONE 3 ZONE	2	_	200											
100-YR VOLUME EURY WQCV	ONE 1	1												
VOLUME, EURV WQCV														
T ZONE	1 AND 2	100-YEA ORIFICE	R		Depth Increment =		ft							
PERMANENT— ORIFI POOL Example Zone	CES	(D-44)	DI\		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Example 20116	Comiguration	on (Retentio	on Fond)		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft 2)	(acre)	(ft <sup>3</sup> )	(ac-ft)
Watershed Information		_		6940.58	Top of Micropool		0.00	-		-	40	0.001		
Selected BMP Type =	EDB			6940.91	Trickle Channel Inv		0.33				40	0.001	13	0.000
Watershed Area =	16.70	acres			6941		0.42				102	0.002	20	0.000
Watershed Length =	1,275	ft			6942		1.42	-		-	2,246	0.052	1,194	0.027
Watershed Length to Centroid =	750	ft			6943		2.42				5,126	0.118	4,880	0.112
Watershed Slope =	0.030	ft/ft			6944		3.42				6,678	0.153	10,782	0.248
Watershed Imperviousness =	65.00%	percent			6945		4.42				8,308	0.191	18,275	0.420
Percentage Hydrologic Soil Group A =	100.0%	percent			6946		5.42	-		-	10,025	0.230	27,441	0.630
Percentage Hydrologic Soil Group B =	0.0%	percent		6947.00	Top of Bank		6.42				11,873	0.273	38,390	0.881
Percentage Hydrologic Soil Groups C/D = Target WQCV Drain Time =	0.0% 40.0	percent						_		_				
Location for 1-hr Rainfall Depths =		nours						-		-				
		-1-6-11						-		-				
After providing required inputs above inc depths, click 'Run CUHP' to generate rund	off hydrographs	rainirali s using												
the embedded Colorado Urban Hydro	graph Procedu	re.	Optional User	Overrides										
Water Quality Capture Volume (WQCV) =	0.354	acre-feet		acre-feet										
Excess Urban Runoff Volume (EURV) =	1.347	acre-feet		acre-feet				-		-				
2-yr Runoff Volume (P1 = 1.19 in.) =	0.978	acre-feet	1.19	inches				-		-				
5-yr Runoff Volume (P1 = 1.5 in.) =	1.283	acre-feet	1.50	inches				1	1	1				
10-yr Runoff Volume (P1 = 1.75 in.) =	1.526	acre-feet	1.75	inches				-		-				
25-yr Runoff Volume (P1 = 2 in.) =	1.845	acre-feet	2.00	inches				-		-				
50-yr Runoff Volume (P1 = 2.25 in.) =	2.158	acre-feet	2.25	inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	2.538	acre-feet	2.52	inches				-		-				
500-yr Runoff Volume (P1 = 3.68 in.) = Approximate 2-yr Detention Volume =	4.122	acre-feet	3.68	inches				-		-				
	0.876	acre-feet												<b></b>
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	1.146	acre-feet acre-feet						-		-				
Approximate 10-yr Detention Volume = Approximate 25-yr Detention Volume =	1.662	acre-reet acre-feet						-		-				
Approximate 50-yr Detention Volume =	1.831	acre-feet						-		-				
Approximate 100-yr Detention Volume =	2.007	acre-feet												
Define Zones and Basin Geometry								-		-				
Zone 1 Volume (WQCV) =	0.354	acre-feet						-		-				
Select Zone 2 Storage Volume (Optional) =		acre-feet	Total deten	tion volume				-		-				
Select Zone 3 Storage Volume (Optional) =		acre-feet	is less than					1	-	1				
Total Detention Basin Volume =	0.354	acre-feet	volume.											
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>												
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft												
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft						-		-				
Slope of Trickle Channel ( $S_{TC}$ ) =	user	ft/ft						-		-				
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V												
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	J						-		-				
Initial Curchavao Arca (A ) =	user	ft <sup>2</sup>						_		_				
Initial Surcharge Area ( $A_{ISV}$ ) = Surcharge Volume Length ( $L_{ISV}$ ) =	user	ft.						-		_				
Surcharge Volume Width (W <sub>ISV</sub> ) =	user	ft						_		_				
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	user	ft												
Length of Basin Floor (L <sub>FLOOR</sub> ) =	user	ft												
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft						-		-				
Area of Basin Floor $(A_{FLOOR})$ =	user	ft²						-	-	-				
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>												
Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft												
Length of Main Basin (L <sub>MAIN</sub> ) =	user	ft												
Width of Main Basin (W <sub>MAIN</sub> ) =	user	ft - 2												
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>						-		-				
Volume of Main Basin $(V_{MAIN})$ = Calculated Total Basin Volume $(V_{total})$ =	user	ft 3 acro-foot						-		-				
carculated Foral basin volume (V <sub>total</sub> ) =	user	acre-feet						1 1	1	1 1				<b></b>
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CLH19 WQCV North\_Detention\_v4 03.xlsm, Basin 2/10/2022, 11:09 AM



CLH19 WQCV North\_Detention\_v4 03.xlsm, Basin 2/10/2022, 11:09 AM

# DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.03 (May 2020) Project: Falcon Meadows at Bent Grass Filing No. 2 Basin ID: WQCV Pond - North

Basin 1D: WQCV Pond - North
ZONE 3 ZONE 2 ZONE 2 ZONE 2 ZONE 1 ZONE 2 ZO
POOL Example Zone Configuration (Retention Pond)

	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.07	0.354	Orifice Plate
Zone 2			
Zone 3			
_	Total (all zones)	0.354	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area = Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = inches Underdrain Orifice Centroid =

User Input: Orifice Plate with one or more orifice	Calculated Parame	ters for Plate			
Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	7.014E-03	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	4.07	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	1.01	sq. inches (diameter = 1-1/8 inches)	Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.10	2.20					
Orifice Area (sq. inches)	1.01	1.01	1.01					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

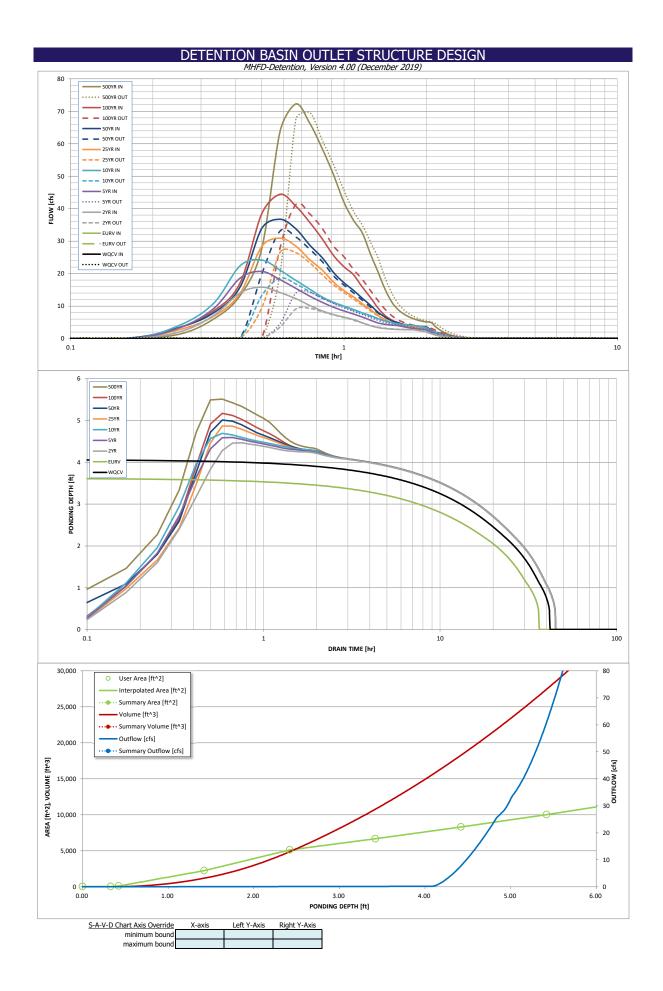
User Input: Vertical Orifice (Circular or Rectangu	lar)				Calculated Paramet	ters for Vertical Ori	fice
	Not Selected	Not Selected			Not Selected	Not Selected	1
Invert of Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =			ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =			feet
Vertical Orifice Diameter -			inches	'			-

User Input: Overflow Weir (Dropbox with Flat or	Calculated Parameters for Overflow Weir					
	Not Selected	Not Selected		Not Selected	Not Selected	1
Overflow Weir Front Edge Height, Ho =	4.08		ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, $H_t$ =	4.08		feet
Overflow Weir Front Edge Length =	6.00		feet Overflow Weir Slope Length =	3.00		feet
Overflow Weir Grate Slope =	0.00		H:V Grate Open Area / 100-yr Orifice Area =	4.01		
Horiz. Length of Weir Sides =	3.00		feet Overflow Grate Open Area w/o Debris =	12.60		ft <sup>2</sup>
Overflow Grate Open Area % =	70%		%, grate open area/total area Overflow Grate Open Area w/ Debris =	6.30		ft <sup>2</sup>
Debris Clogging % =	50%		<u> </u> %			

User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re	estrictor Plate, or R	ectangular Orifice)	Calculated Parameters	for Outlet Pipe w/	Flow Restriction Plant	<u>ate</u>
	Not Selected	Not Selected			Not Selected	Not Selected	
Depth to Invert of Outlet Pipe =	0.25		ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	3.14		ft <sup>2</sup>
Circular Orifice Diameter =	24.00		inches	Outlet Orifice Centroid =	1.00		feet
		•	Half-Central Angle	of Restrictor Plate on Pipe =	N/A	N/A	radians

User Input: Emergency Spillway (Rectangular or	Calculated Paramet	ters for Spillway			
Spillway Invert Stage=	4.92	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.66	feet
Spillway Crest Length =	25.00	feet	Stage at Top of Freeboard =	5.58	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.24	acres
Freeboard above Max Water Surface =	0.00	feet	Basin Volume at Top of Freeboard =	0.67	acre-ft

Routed Hydrograph Results	The user can overr	ide the default CUF	HP hydrographs and	runoff volumes by	entering new value	s in the Inflow Hydi	ographs table (Coll	umns W through Ai	F).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.68
CUHP Runoff Volume (acre-ft) =	0.354	1.347	0.978	1.283	1.526	1.845	2.158	2.538	4.122
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.978	1.283	1.526	1.845	2.158	2.538	4.122
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.2	0.3	3.0	6.0	9.8	24.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.18	0.36	0.58	1.49
Peak Inflow Q (cfs) =	N/A	N/A	15.8	20.7	24.2	30.9	36.8	44.4	72.3
Peak Outflow Q (cfs) =	0.2	155.3	9.3	14.2	18.6	26.6	33.1	41.3	69.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	61.7	57.4	8.9	5.5	4.2	2.8
Structure Controlling Flow =	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway	Spillway	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	0.71	1.1	1.5	2.1	2.5	2.5	2.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	28	36	34	33	32	30	28	23
Time to Drain 99% of Inflow Volume (hours) =	40	33	41	40	39	39	38	37	34
Maximum Ponding Depth (ft) =	4.07	3.61	4.46	4.59	4.69	4.87	5.01	5.17	5.51
Area at Maximum Ponding Depth (acres) =	0.18	0.16	0.19	0.20	0.20	0.21	0.21	0.22	0.23
Maximum Volume Stored (acre-ft) =	0.355	0.276	0.427	0.453	0.472	0.507	0.537	0.571	0.651



	Design Procedure Form:	Extended Detention Basin (EDB)
		Sheet 2 of 3
Designer:	Callaviav	
Company:	Galloway	
Date: Project:	July 20, 2021  Falcon Meadows at Bent Grass Filing No. 2	
Location:	WQCV - North Pond	
200410111		
6. Trickle Channel		Choose One  ● Concrete
A) Type of Tric	kle Channel	Soft Bottom
F) Slope of Tric	ckle Channel	S = 0.0050 ft / ft
7. Micropool and 0	Outlet Structure	
A) Depth of Mid	cropool (2.5-feet minimum)	$D_{M} = \boxed{2.5} ft$
B) Surface Are	a of Micropool (10 ft² minimum)	$A_{M} = $ sq ft
C) Outlet Type		Choose One  Orlfice Plate Other (Describe):
D) Smallest Dir (Use UD-Detent	mension of Orifice Opening Based on Hydrograph Routing tion)	D <sub>office</sub> = 1.19 inches
E) Total Outlet	Area	A <sub>ot</sub> = 3.33 square inches
8. Initial Surcharge	e Volume	
	ial Surcharge Volume commended depth is 4 inches)	D <sub>IS</sub> = 4 in
	ial Surcharge Volume lume of 0.3% of the WQCV)	V <sub>IS</sub> = 46 cu ft
C) Initial Surcha	arge Provided Above Micropool	V <sub>s</sub> = 16.0 cu ft
9. Trash Rack		
A) Water Quali	ty Screen Open Area: A <sub>t</sub> = A <sub>ot</sub> * 38.5*(e <sup>-0.095D</sup> )	A <sub>t</sub> = 115 square inches
in the USDCM,	en (If specifying an alternative to the materials recommended indicate "other" and enter the ratio of the total open are to the for the material specified.)	S.S. Well Screen with 60% Open Area
	Other (Y/N): N	
C) Ratio of Tota	al Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water	Quality Screen Area (based on screen type)	$A_{total} =                                   $
	sign Volume (EURV or WQCV) design concept chosen under 1E)	H= 3.72 feet
F) Height of Wa	ater Quality Screen (H <sub>TR</sub> )	H <sub>TR</sub> = 72.64 inches
	ter Quality Screen Opening (W <sub>opening</sub> ) inches is recommended)	W <sub>opening</sub> = 12.0 inches VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.

UD-BMP\_v3.07.xlsm, EDB 7/20/2021, 12:31 PM

#### NORTH POND - NORTH FOREBAY CALCULATIONS (FALCON MEADOWS FILING NO. 2)

1) WQCV (inches) =  $a(.911^3 - 1.191^2 + .781)$ 

I = impervious percentage = 72%

a = Coefficient corresponding to WQCV drain time = 1 (40 hours)

WQCV (inches) = 0.28 inches

2) WQCV (ac-ft) = (WQCV (inches))/12 x A

Area = tributary area = 3.98 acres

WQCV (ac-ft) = 0.09 WQCV (cubic feet) = 4,108

3) Forebay Volume

Per Table EDB-4, Section T-5 of USDCM Volume 3 - Forebay Volume = 2% of WQCV and be 18" max depth since watershed is under 5 impervious acres

Forebay Volume = 2% of WQCV = 82 cubic feet

with pond depth at 1.0', Forebay Area = 82.2 sq-ft (minimum)

4) Forebay Discharge

Per Table EDB-4, Section T-5 of USDCM Volume 3 - Forebay Discharge = 2% of 100-yr Flow into pond

Q100 = 21.1 cfs

Forebay discharge = 0.42 cfs

### Worksheet for North Forebay Release Slots

Project Description			
Solve For	Crest Length		
Input Data			
Discharge		0.42	ft³/s
Headwater Elevation		1.25	ft
Crest Elevation		0.00	ft
Tailwater Elevation		0.00	ft
Weir Coefficient		3.00	US
Number Of Contractions	0		
Results			
Crest Length		0.10	ft
Headwater Height Above Crest		1.25	ft
Tailwater Height Above Crest		0.00	ft
Flow Area		0.13	ft²
Velocity		3.35	ft/s
Wetted Perimeter		2.60	ft
Top Width		0.10	ft

#### Worksheet for North Trickle Channel

	WOLKSHEET TO	INOI LII IIICI	CIC CHAINICI	
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
Input Data				
		0.013		
Roughness Coefficient		0.50000	££ /££	
Channel Slope  Bottom Width		2.00	ft/ft ft	
Discharge		0.42		
		0.12	1173	
Results				
Normal Depth		0.03	ft	
Flow Area		0.06	ft²	
Wetted Perimeter		2.06	ft	
Hydraulic Radius		0.03	ft	
Top Width		2.00	ft	
Critical Depth		0.11	ft	
Critical Slope		0.00589	ft/ft	
Velocity		7.36	ft/s	
Velocity Head		0.84	ft	
Specific Energy		0.87	ft	
Froude Number	Company sistemal	7.69		
Flow Type	Supercritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Downstream Velocity		Infinity	ft/s	
Upstream Velocity		Infinity	ft/s	
Normal Depth		0.03	ft	
Critical Depth		0.11	ft	
Channel Slope		0.50000	ft/ft	
Critical Slope		0.00589	ft/ft	

#### NORTH POND - WEST FOREBAY CALCULATIONS (FALCON MEADOWS FILING NO. 2)

1) WQCV (inches) =  $a(.911^3 - 1.191^2 + .781)$ 

I = impervious percentage = 62%

a = Coefficient corresponding to WQCV drain time = 1 (40 hours)

WQCV (inches) = 0.24 inches

2) WQCV (ac-ft) = (WQCV (inches))/12 x A

Area = tributary area = 12.72 acres

WQCV (ac-ft) = 0.26 WQCV (cubic feet) = 11,222

3) Forebay Volume

Per Table EDB-4, Section T-5 of USDCM Volume 3 - Forebay Volume = 3% of WQCV and be 18" max depth since watershed is over 5 impervious acres

Forebay Volume = 3% of WQCV = 337 cubic feet

with pond depth at 1.5', Forebay Area = 224.4 sq-ft (minimum)

4) Forebay Discharge

Per Table EDB-4, Section T-5 of USDCM Volume 3 - Forebay Discharge = 2% of 100-yr Flow into pond

Q100 = 44.4 cfs

Forebay discharge = 0.89 cfs

#### Worksheet for West Forebay Release Slots

		<u> </u>		
Project Description				
Solve For	Crest Length			
Input Data				
Discharge		0.89	ft³/s	
Headwater Elevation		1.25	ft	
Crest Elevation		0.00	ft	
Tailwater Elevation		0.00	ft	
Weir Coefficient		3.00	US	
Number Of Contractions	0			
Results				
Crest Length		0.21	ft <del>&lt;</del>	Minimum slot size is 3"
Headwater Height Above Crest		1.25	ft	
Tailwater Height Above Crest		0.00	ft	
Flow Area		0.27	ft²	
Velocity		3.35	ft/s	
Wetted Perimeter		2.71	ft	
Top Width		0.21	ft	

	Worksheet for	West Trick	de Channel
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.50000	ft/ft
Bottom Width		2.00	ft
Discharge		0.89	ft³/s
Results			
Normal Depth		0.04	ft
Flow Area		0.09	ft²
Wetted Perimeter		2.09	ft
Hydraulic Radius		0.04	ft
Top Width		2.00	ft
Critical Depth		0.18	ft
Critical Slope		0.00543	ft/ft
Velocity		9.94	ft/s
Velocity Head		1.53	ft
Specific Energy		1.58	ft
Froude Number		8.28	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity		Infinity	ft/s

ft/ft

Infinity ft/s

0.04 ft

0.18 ft

0.00543 ft/ft

0.50000

Upstream Velocity

Normal Depth Critical Depth

Channel Slope

Critical Slope

#### POND RIPRAP EMBANKMENT SIZING - North Pond

Subdivision:Bent GrassProject Name:Falcon Meadows at Bent Grass Filing No. 2Location:El Paso CountyProject No.:CLH000019

Calculated By: CMD

Checked By: CD

**Date:**  $\overline{5/3/21}$ 

Pond	Riprap Type	D50*	Slope, S	Concentration Factor	Unit discharge	Spillway Flow***	Spillway Width
		(in)	(ft/ft)	(1.0 to 3.0)	(cfs/ft)**	(cfs)	(ft)
North Pond	M	9.3	50.00%	2	1.78	44.4	25

<sup>\*</sup>From DCM Chapter 13 Eqn 13-9

<sup>\*\*</sup> Spillway Flow/Spillway Width

<sup>\*\*\*</sup>Peak Inflow Q100

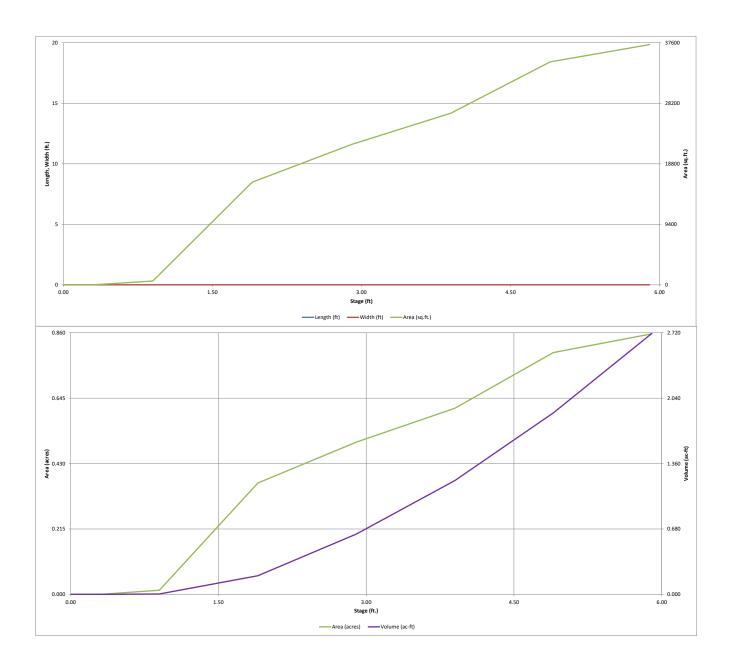
## **Pond (South) Calculations – Existing Analysis**

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

Project: Falcon Meadows at Bent Grass Filing No. 2 Basin ID: WQCV Pond - South (Analysis) NE 3 ZONE 2 ZONE 1 100-YR VOLUME EURV WQCV ZONE 1 AND 2 ORIFICE
ORIFICES

Example Zone Configuration (Retention Pond) Depth Increment 1.00 Stage - Storage Stage Length Width Volume Volume Description (ft) (ft) (ac-ft) (acre) 6923.1 Top of Micropoo Watershed Information 0.00 35 0.001 Selected BMP Type : EDB (Trickle Channel Inv) 6923.43 0.33 35 0.001 12 0.000 63.22 6924 0.90 593 0.014 191 0.004 Watershed Length 0.366 0.194 3,600 6925 1.90 Watershed Length to Centroid 1,500 6926 2.90 21,804 0.501 27,335 0.628 Watershed Slope 0.030 ብ/ብ 6927 3.90 26,657 0.612 51,565 1.184 Watershed Imperviousness 31.20% ercent (Spillway Invert) 6928 4.90 34,630 0.795 82,209 1.887 Percentage Hydrologic Soil Group A 100.0% ercent (Top of Bank) 6929 5.90 37,309 0.856 118,178 2.713 Percentage Hydrologic Soil Group B : 0.0% ercent Percentage Hydrologic Soil Groups C/D = 0.0% ercent Target WQCV Drain Time = 40.0 ours Location for 1-hr Rainfall Depths = User Input After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure. Water Quality Capture Volume (WQCV) = acre-feet Excess Urban Runoff Volume (EURV) = 1.993 acre-feet cre-feet 2-yr Runoff Volume (P1 = 1.19 in.) 1.410 acre-feet 1.19 inches 5-yr Runoff Volume (P1 = 1.5 in.) = 1.935 acre-feet 1.50 inches 10-yr Runoff Volume (P1 = 1.75 in.) 2.372 acre-feet 1.75 inches 25-yr Runoff Volume (P1 = 2 in.) = 3.443 acre-feet 2.00 inches 50-vr Runoff Volume (P1 = 2.25 in.) 4.443 acre-feet 2.25 inches 100-yr Runoff Volume (P1 = 2.52 in.) = inches 5.780 acre-feet 2.52 500-yr Runoff Volume (P1 = 3.68 in.) 11.410 acre-feet 3.68 inches Approximate 2-yr Detention Volume = 1.255 acre-feet Approximate 5-yr Detention Volume 1.673 Approximate 10-yr Detention Volume : acre-feet Approximate 25-yr Detention Volume 2.630 acre-feet Approximate 50-yr Detention Volume : 3.031 acre-feet Approximate 100-yr Detention Volume = 3,666 acre-feet Define Zones and Basin Geometry Zone 1 Volume (WQCV) = 0.817 acre-feet Select Zone 2 Storage Volume (Optional) = acre-feet Select Zone 3 Storage Volume (Optional) acre-feet Total Detention Basin Volume 0.817 Initial Surcharge Volume (ISV) user Initial Surcharge Depth (ISD) Total Available Detention Depth (H<sub>total</sub>) user Depth of Trickle Channel (H<sub>TC</sub>) Slope of Trickle Channel ( $S_{TC}$ ) = user ft/ft Slopes of Main Basin Sides (Smale) H:V Basin Length-to-Width Ratio ( $R_{L/W}$ ) = Initial Surcharge Area (Arsy) = user Surcharge Volume Length (LISV) user Surcharge Volume Width (W<sub>ISV</sub>) = Depth of Basin Floor (H<sub>FLOOR</sub>) Length of Basin Floor (LFLOOR) Width of Basin Floor (W<sub>FLOOR</sub>) user Area of Basin Floor (A<sub>FLOOR</sub>) user Volume of Basin Floor (V<sub>FLOOR</sub>) user Depth of Main Basin ( $H_{MAIN}$ ) user Length of Main Basin (L<sub>MAIN</sub>) user Width of Main Basin (WMAIN) user Area of Main Basin (AMAIN) user Volume of Main Basin (V<sub>MAIN</sub>) user Calculated Total Basin Volume (Vtotal) = user

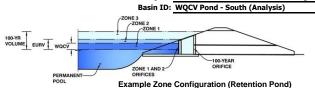


CLH19 WQCV South\_Analysis.xlsm, Basin 4/21/2022, 1:55 PM

#### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: Falcon Meadows at Bent Grass Filing No. 2



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.27	0.817	Orifice Plate
Zone 2			
Zone 3			
•	Total (all zones)	0.817	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area Underdrain Orifice Invert Depth =

ft (relative to basin bottom at Stage = 0 ft)

Underdrain Orifice Diameter = inches Underdrain Orifice Centroid = User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentatio

Depth at top of Zone using Orifice Plate = 3.39 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = N/A inches

0.00

Orifice Plate: Orifice Area per Row = 2.41 sq. inches (diameter = 1-3/4 inches)

n BMP)	Calculated Parame	ters for Plate
WQ Orifice Area per Row =	1.670E-02	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

ft<sup>2</sup>

feet

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Invert of Lowest Orifice =

Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) 0.00 1.14 2.27 2.41 Orifice Area (sq. inches) 2.41 2.41

Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sq. inches)

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice = Vertical Orifice Area ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Vertical Orifice = Vertical Orifice Centroid = ft (relative to basin bottom at Stage = 0 ft) feet Vertical Orifice Diameter = inches

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Weir

	Not Selected	Not Selected			Not Selected	Not Selected	]
Overflow Weir Front Edge Height, Ho =	3.50		ft (relative to basin bottom at Stage = $0 \text{ ft}$ )	Height of Grate Upper Edge, $H_t$ =	3.50		feet
Overflow Weir Front Edge Length =	6.00		feet	Overflow Weir Slope Length =	6.00		feet
Overflow Weir Grate Slope =	0.00		H:V Grat	e Open Area / 100-yr Orifice Area =	5.87		
Horiz. Length of Weir Sides =	6.00		feet Over	flow Grate Open Area w/o Debris =	28.80		ft <sup>2</sup>
Overflow Grate Open Area % =	80%		%, grate open area/total area Ove	erflow Grate Open Area w/ Debris =	14.40		ft <sup>2</sup>
Debris Clogging % =	50%		%				_

<u>User Input: Outlet Pipe w/</u> Flow Restriction Plate (Circular Orifice. Restrictor Plate, or Rectangular Orifice)

Outlet Pipe W/ Flow Restriction Plate (Circular Office, Restrictor Plate, or Rectangular Office)			<u>Rectangular Office)</u>	Calculated Parameters	s for Outlet Pipe w/	Flow Restriction P	iale
	Not Selected	Not Selected			Not Selected	Not Selected	1
Depth to Invert of Outlet Pipe =	0.25		ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	4.91		ft <sup>2</sup>
Circular Orifice Diameter =	30.00		inches	Outlet Orifice Centroid =	1.25		feet
			Half-Central Angle	of Restrictor Plate on Pipe =	N/A	N/A	radians

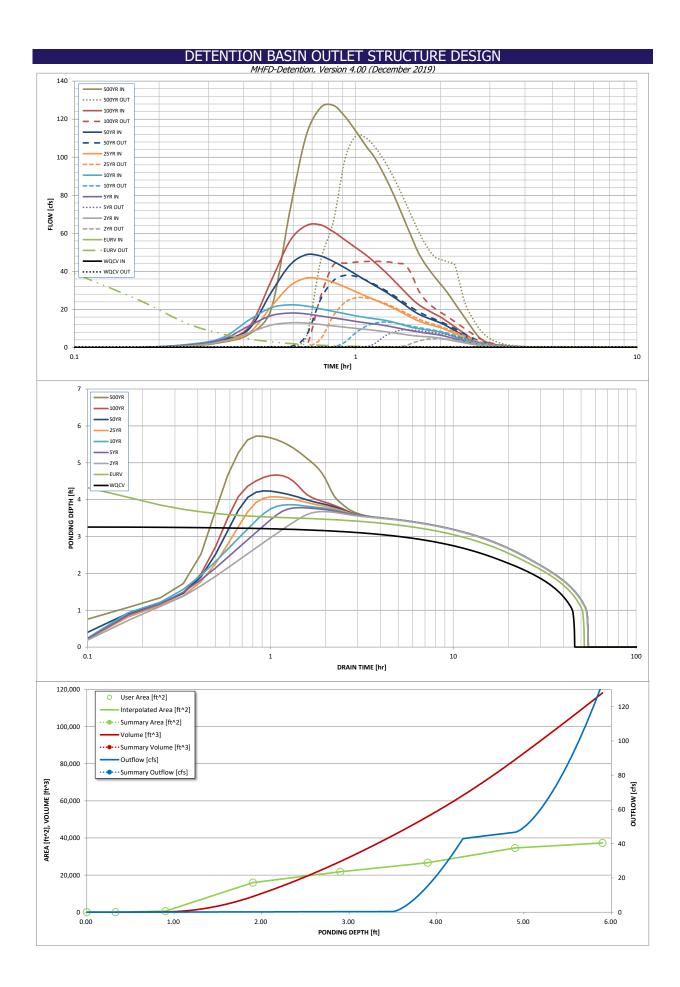
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= 4.90 ft (relative to basin bottom at Stage = 0 ft) Spillway Crest Length = 24.00 feet Spillway End Slopes = 4.00 H:V Freeboard above Max Water Surface = 0.00 feet

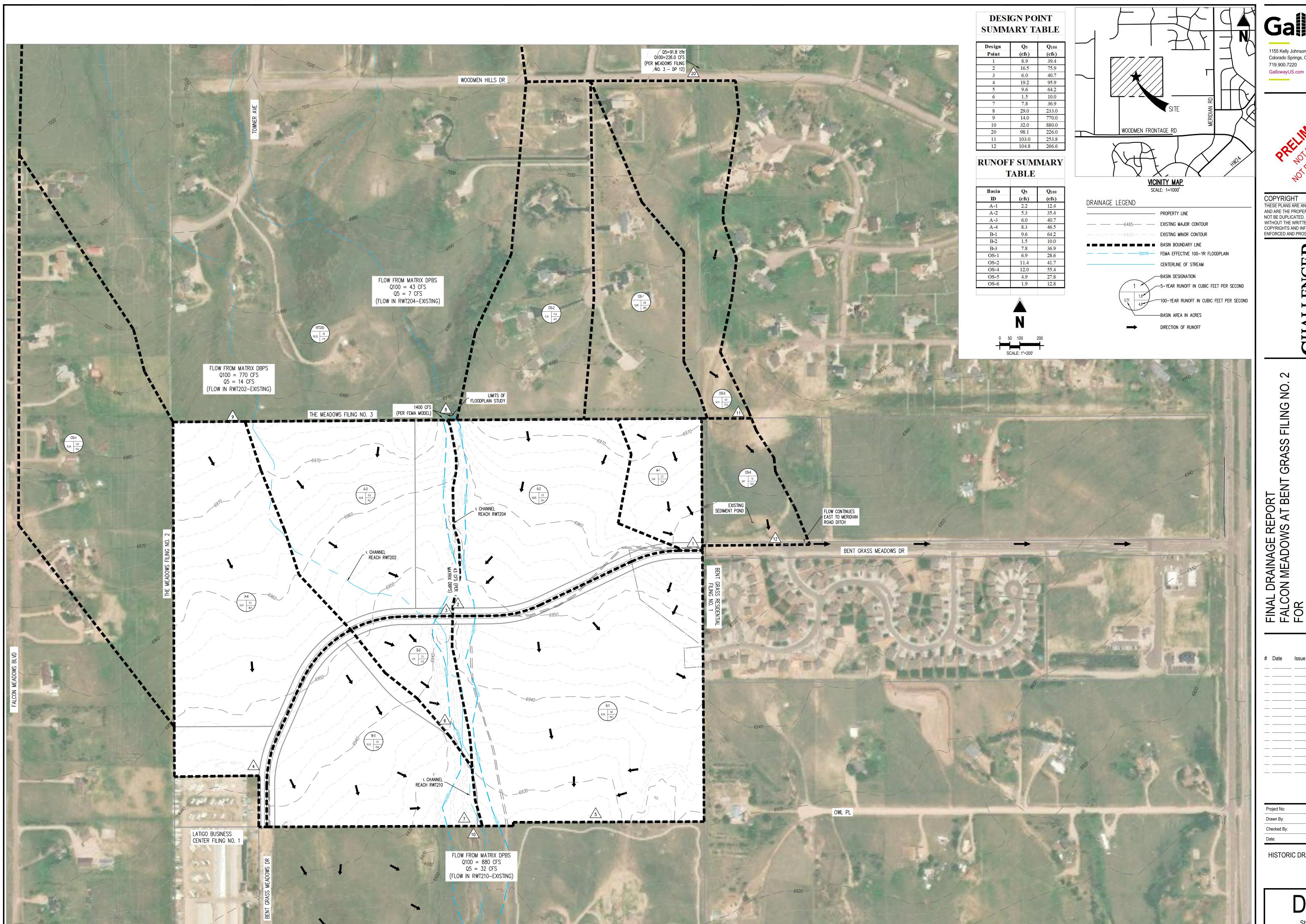
	Calculated Parameters for Spillwa		
Spillway Design Flow Depth=	0.93	feet	
Stage at Top of Freeboard =	5.83	feet	
Basin Area at Top of Freeboard =	0.85	acres	
Basin Volume at Top of Freeboard =	2.65	acre-ft	

Calculated Parameters for Outlet Pine w/ Flow Postriction Plate

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF Routed Hydrograph Results Design Storm Return Period : WQCV **EURV** 2 Year 10 Year 25 Year 50 Year 100 Year One-Hour Rainfall Depth (in) = N/A N/A 1.19 1.50 1.75 2.00 2.25 2.52 3.68 CUHP Runoff Volume (acre-ft) = 2.372 3,443 0.817 1.993 1.410 1.935 4.443 5.780 11.410 Inflow Hydrograph Volume (acre-ft) : 4.443 5.780 N/A N/A 1.410 1.935 3.443 11.410 CUHP Predevelopment Peak Q (cfs) = N/A N/A 0.4 0.7 1.0 9.1 18.4 30.5 79.9 OPTIONAL Override Predevelopment Peak Q (cfs) = N/A N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) = N/A 0.01 0.01 0.02 0.14 0.29 0.48 1.26 Peak Inflow Q (cfs) = N/A N/A 13.0 18.1 22.4 36.4 48.7 64.4 127.2 Peak Outflow O (cfs) : 13.3 37.9 0.3 46.3 4.7 9.3 26.1 45.3 111.0 Ratio Peak Outflow to Predevelopment Q = N/A N/A N/A 1.4 Structure Controlling Flow Plate Spillway Overflow Weir 1 Outlet Plate 1 Spillway Max Velocity through Grate 1 (fps) = N/A 1.63 0.16 1.8 1.6 Max Velocity through Grate 2 (fps) = N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) = 43 49 48 47 42 39 29 Time to Drain 99% of Inflow Volume (hours) = 45 44 49 51 50 49 48 52 52 Maximum Ponding Depth (ft) 5.04 5.72 3.27 3.68 3.78 3.86 4.07 4.24 4.67 Area at Maximum Ponding Depth (acres) 0.80 0.64 0.67 0.85 0.54 0.59 0.60 0.61 0.75 Maximum Volume Stored (acre-ft) = 0.820



# APPENDIX E Drainage Maps



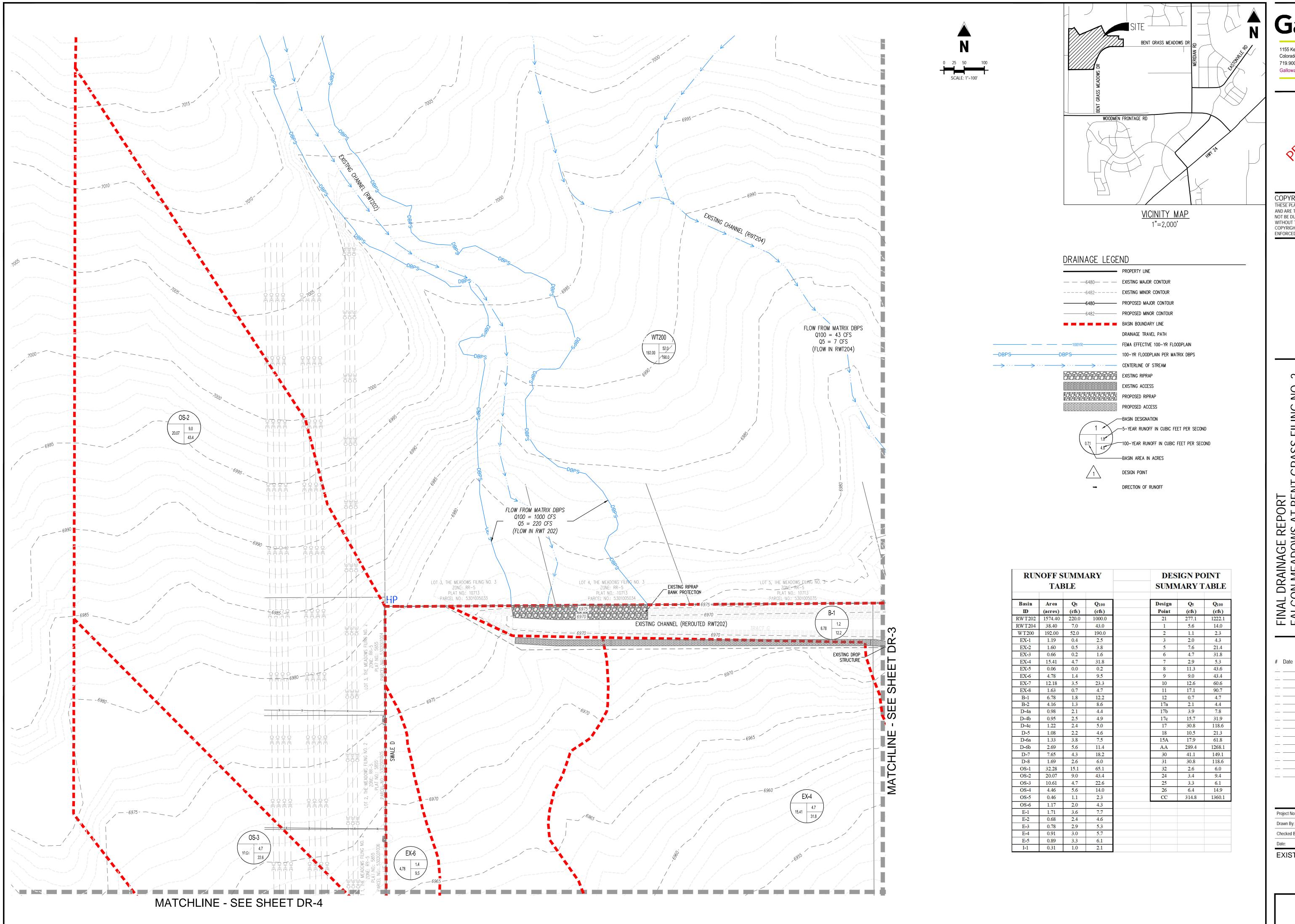
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OCTOBER 2019

HISTORIC DRAINAGE MAP



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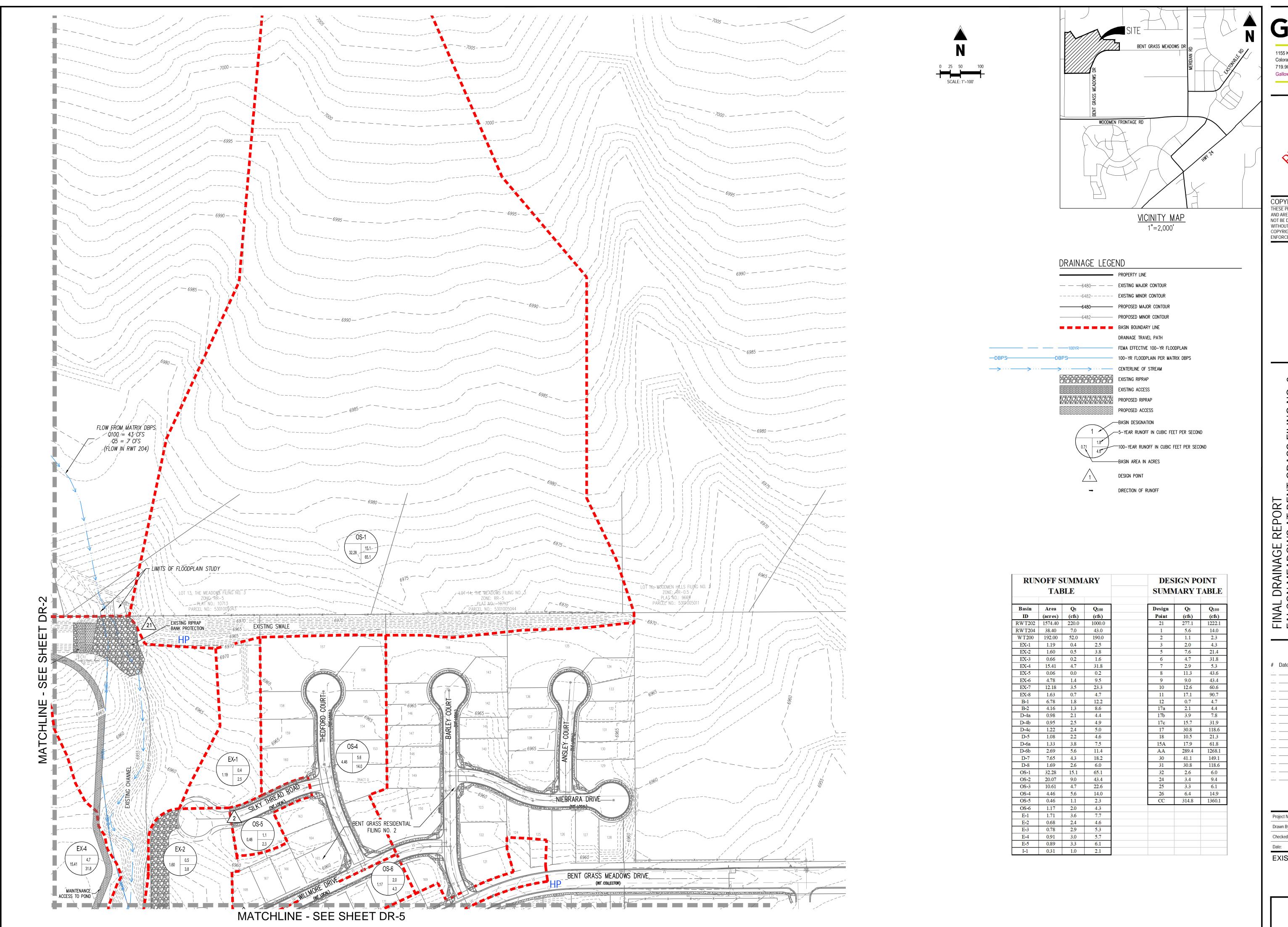
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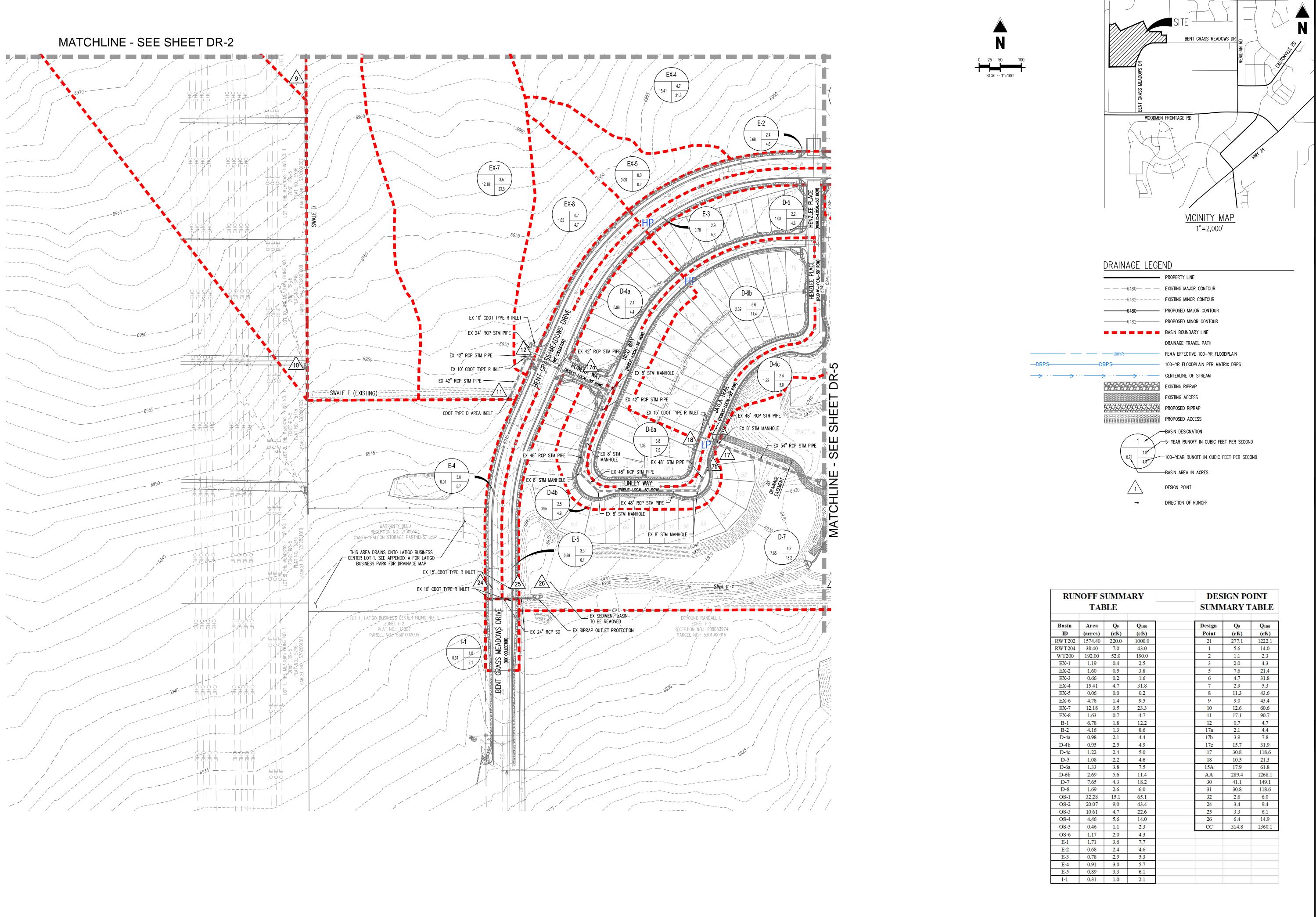
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FINAL DRAINAGE REPORT FALCON MEADOWS AT BENT FOR CHALLENGER COMMUNTIES,

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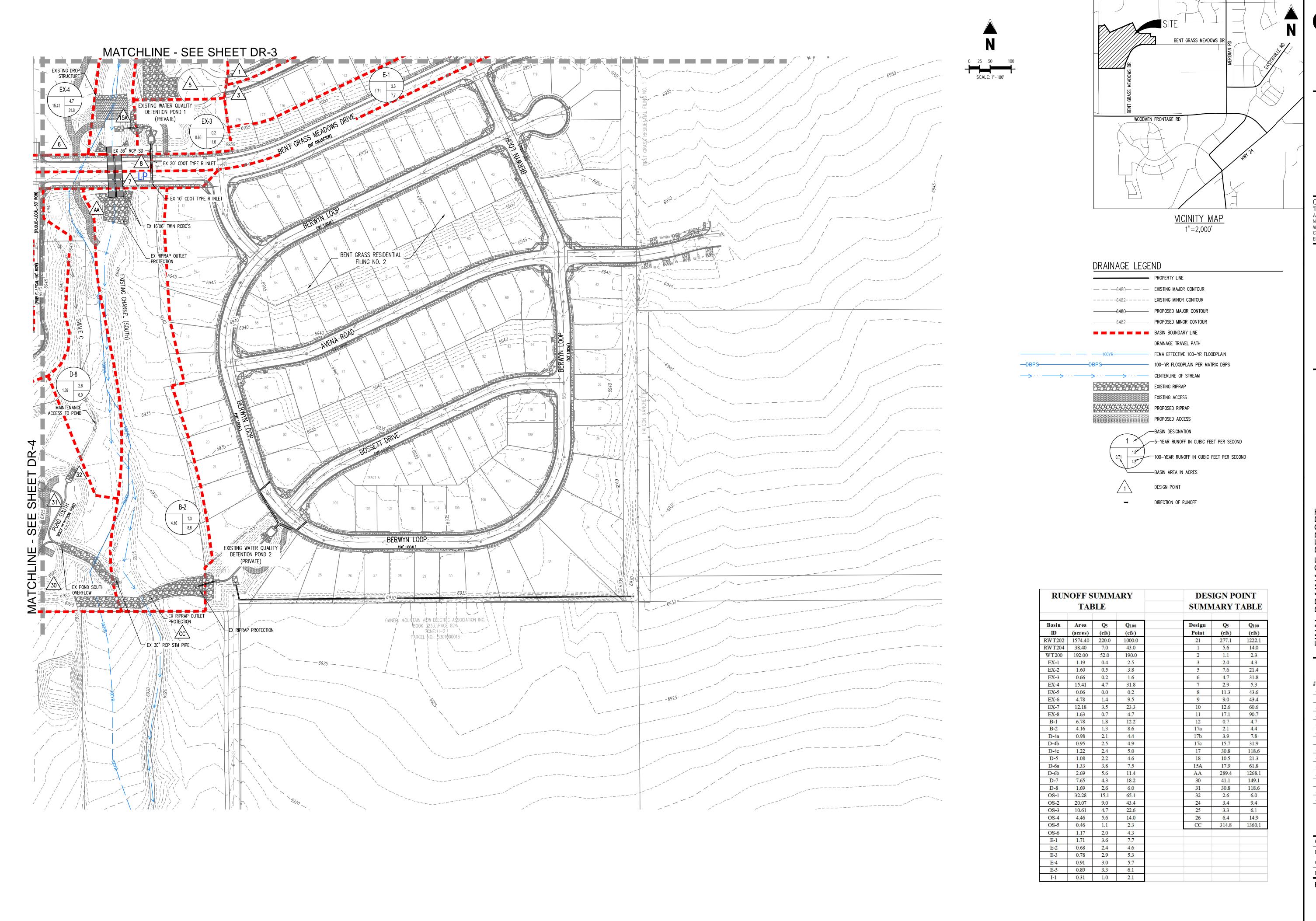
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 Drawn By:
 DDJ

 Checked By:
 GD

 Date:
 12/03/2021

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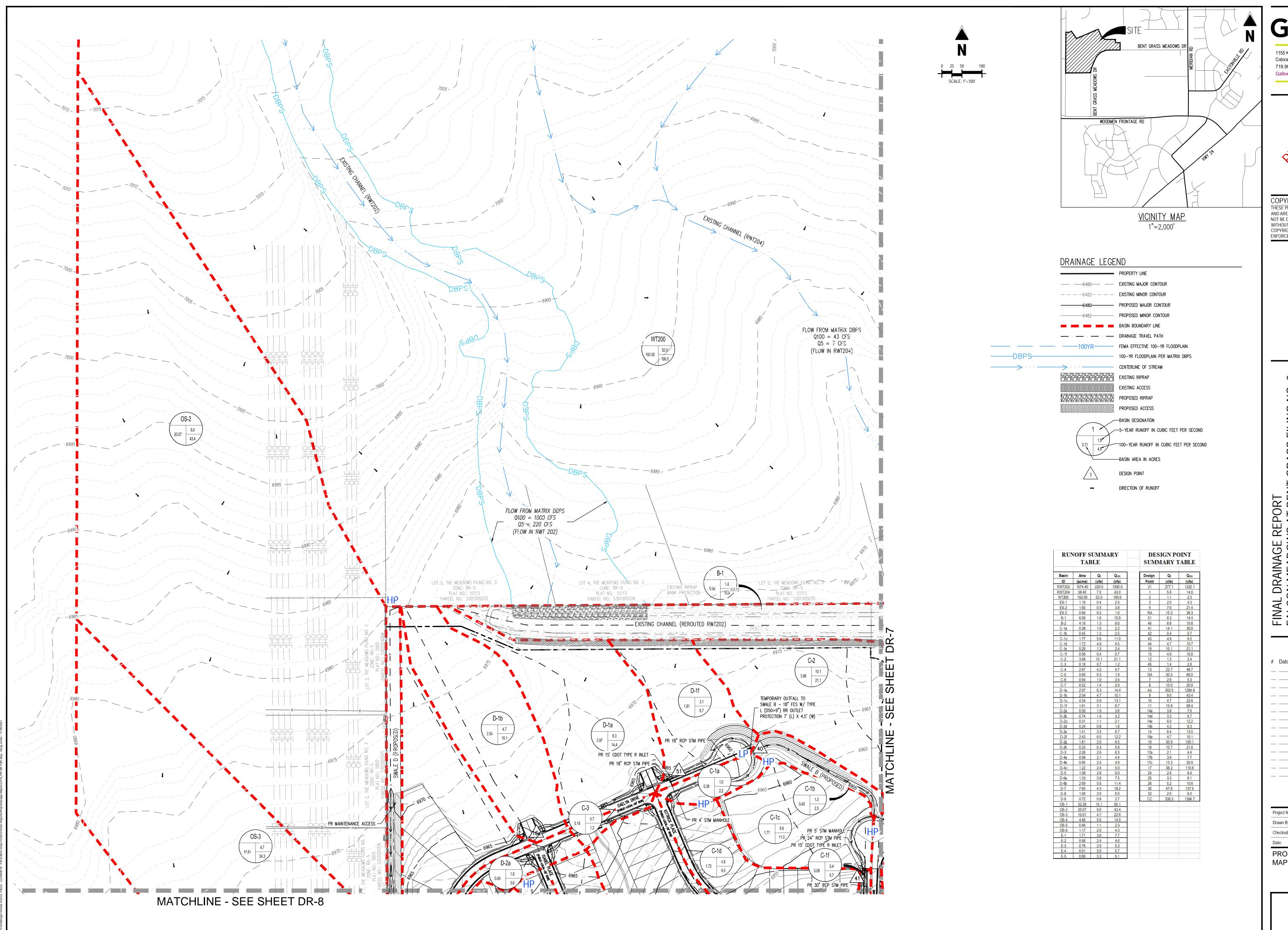
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 Date:
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EXISTING DRAINAGE MAP

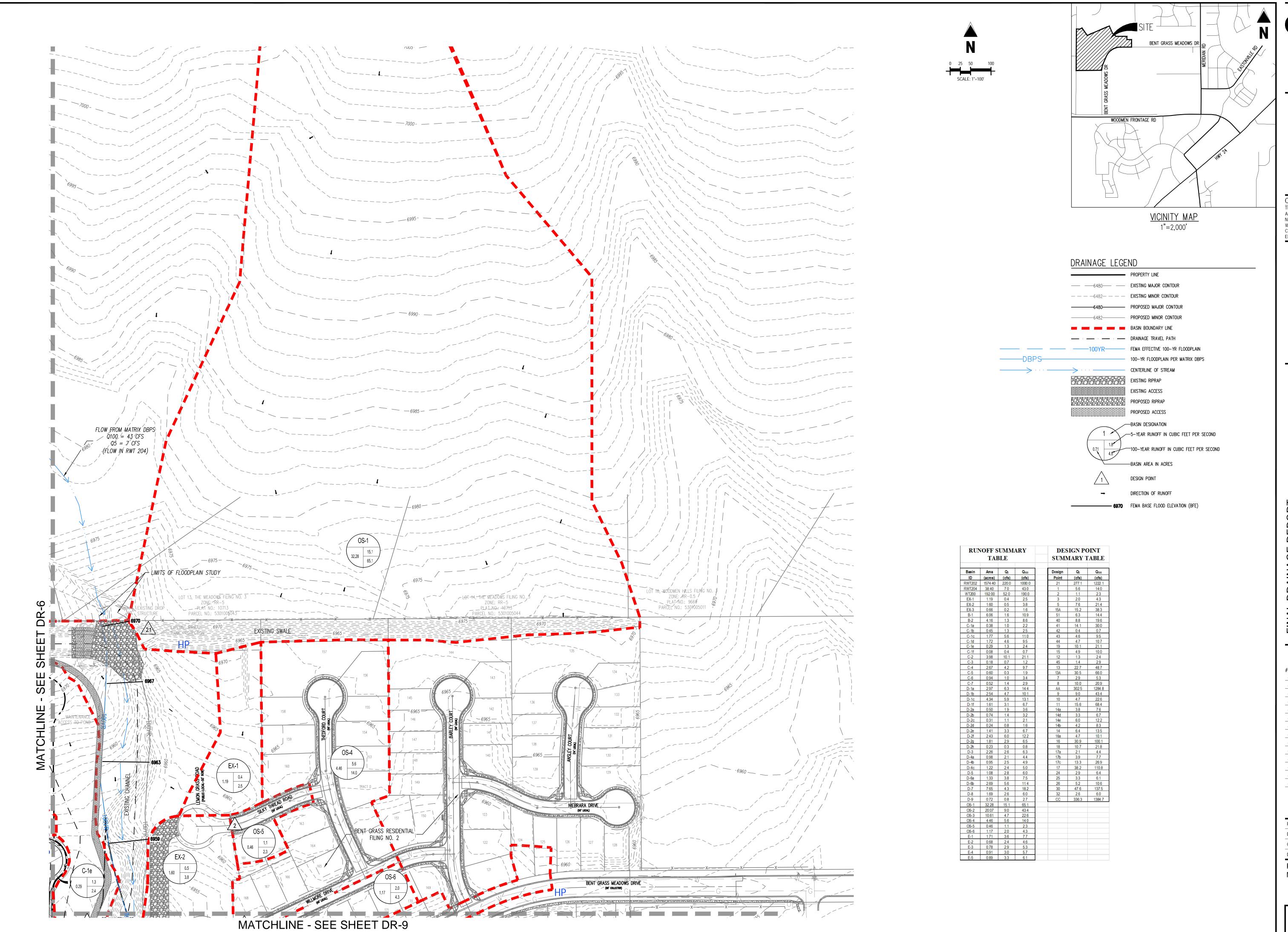


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PROPOSED DRAINAGE



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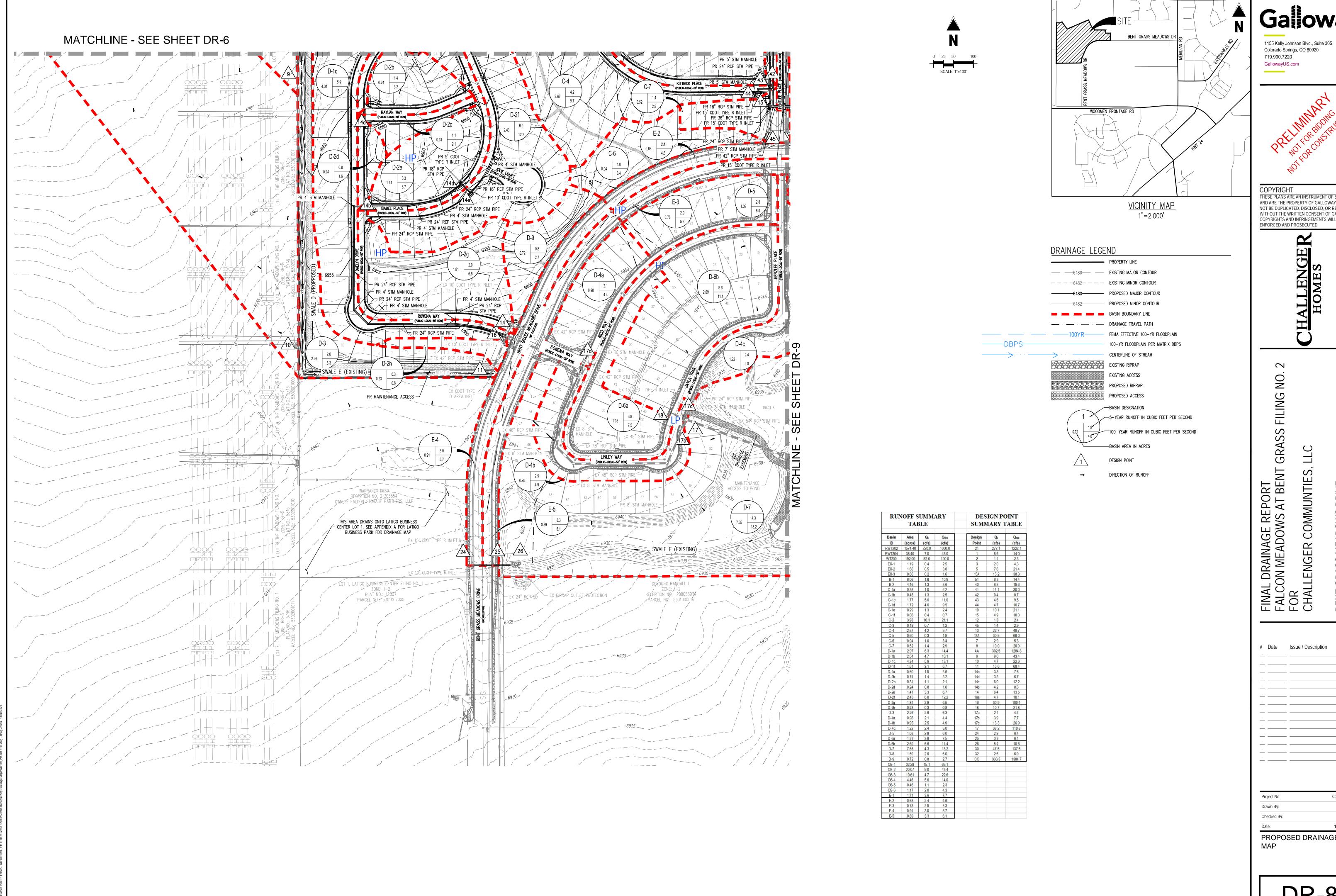
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PROPOSED DRAINAGE MAP





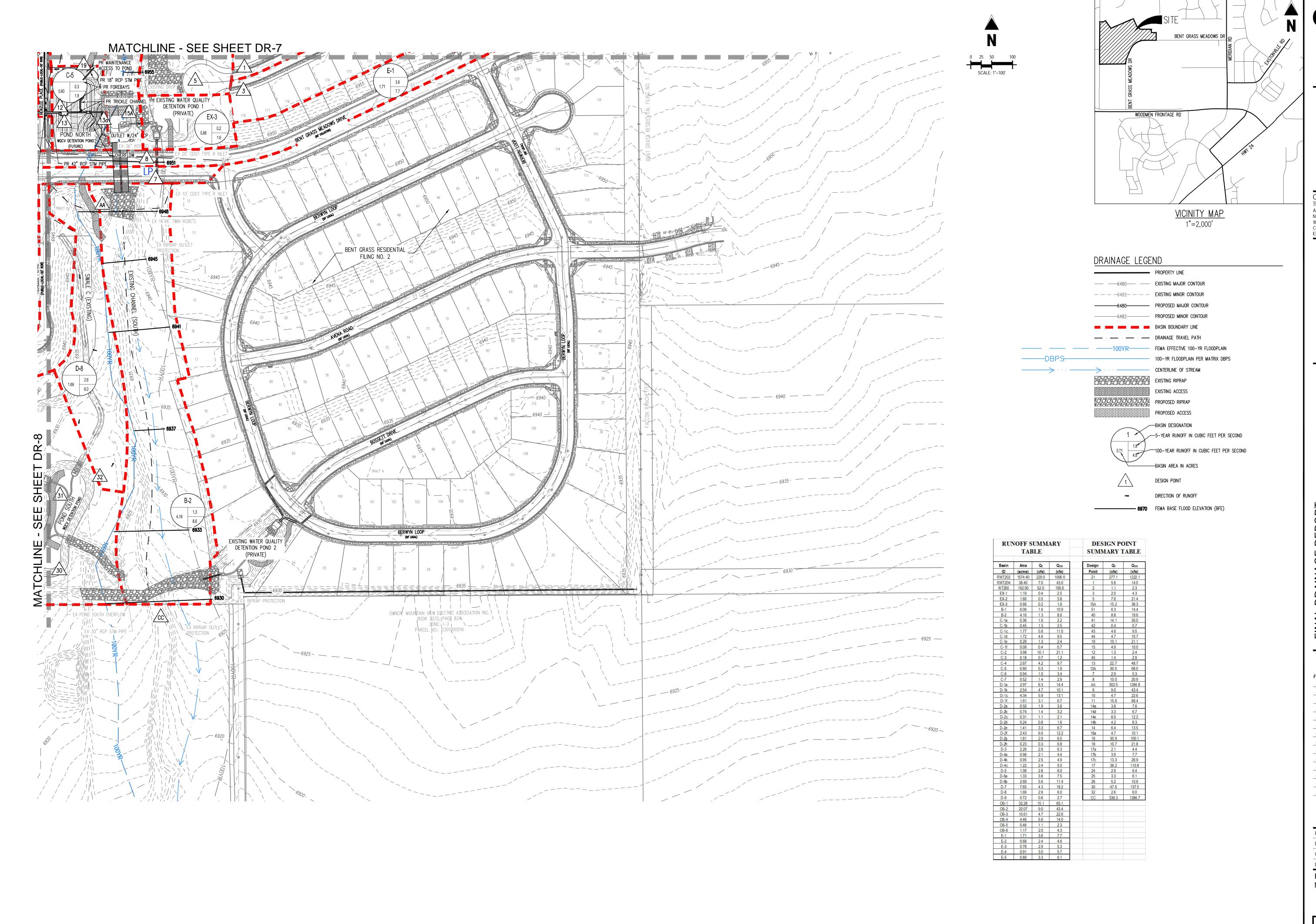
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PROPOSED DRAINAGE



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# Date Issue / Description II

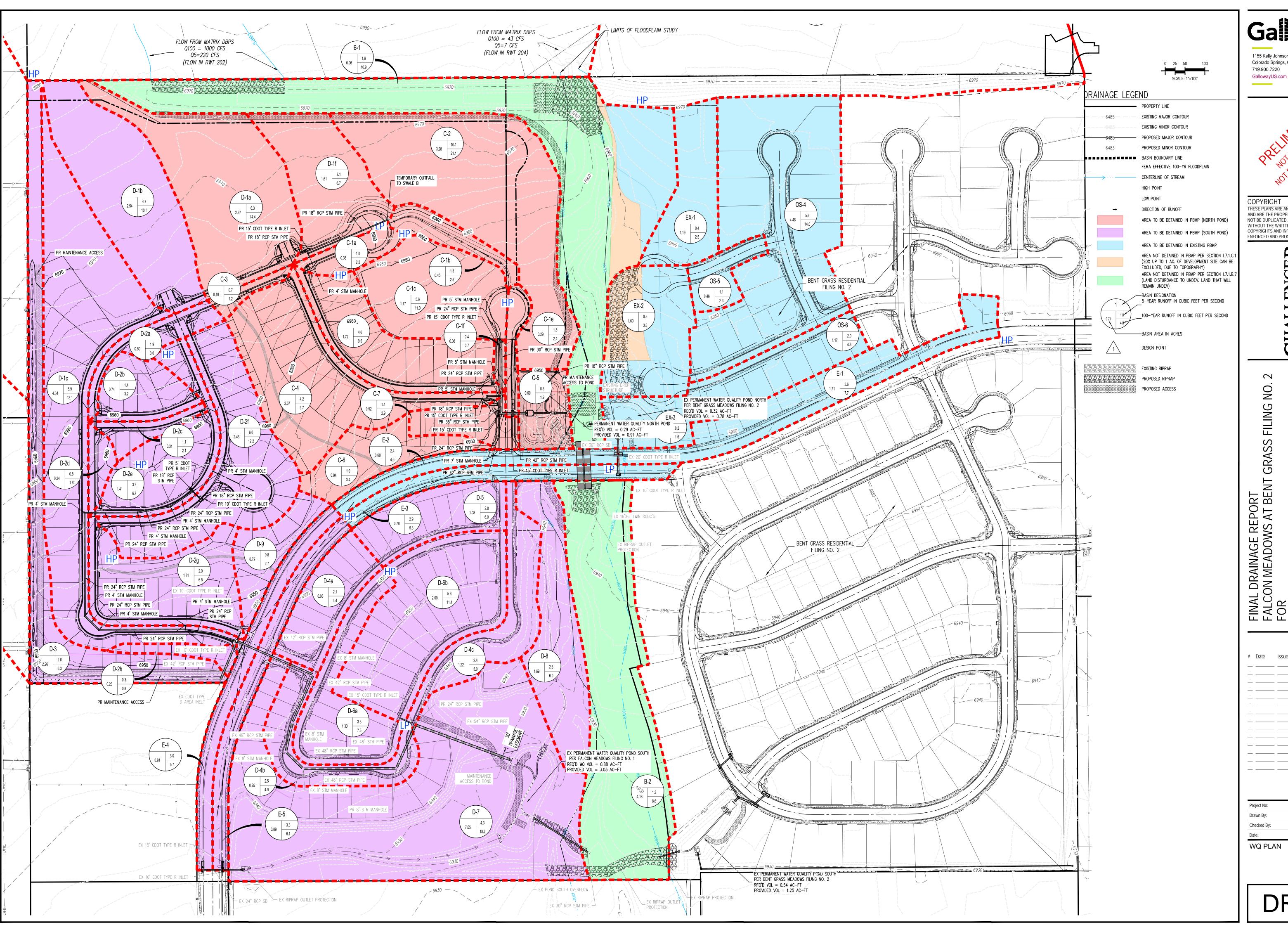
 Project No:
 CLH000019

 Drawn By:
 DDJ

 Checked By:
 GD

 Date:
 12/03/2021

PROPOSED DRAINAGE MAP



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# Date Issue / Description

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WQ PLAN