

# **FINAL DRAINAGE PLAN**

## **CREEKSIDE SOUTH AT LORSON RANCH FILING NO. 1**

**JUNE 15, 2020  
REV 9/10/2020**

**SF-20-017**

***Prepared for:***

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Project No. 100.051



**CORE**  

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**ENGINEERING GROUP**

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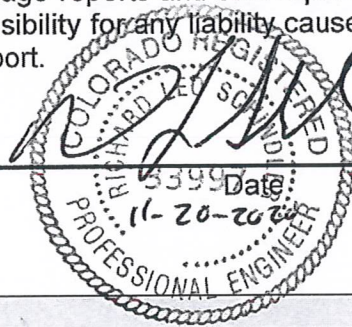
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## ENGINEER'S STATEMENT

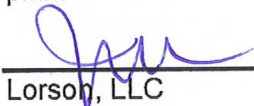
The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Richard L. Schindler, P.E. #33997  
For and on Behalf of Core Engineering Group, LLC



## OWNER'S STATEMENT

I, the Owner, have read and will comply with all the requirements specified in the drainage report and plan.

  
Lorson, LLC

11/20/20  
Date

By  
Jeff Mark  
Title  
Manager

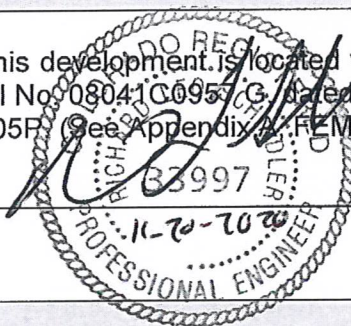
Address  
212 N. Wahsatch Avenue, Suite 301, Colorado Springs, CO 80903

## FLOODPLAIN STATEMENT

To the best of my knowledge and belief, this development is located within a designated floodplain as shown on Flood Insurance Rate Map Panel No. 08041C0953G, dated December 7, 2018 and modified by modified per LOMR Case No. 19-08-0605R (See Appendix A: FEMA FIRM Exhibit)

Richard L. Schindler, #33997

Date



## EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volume 1 and 2, and Engineering Criteria Manual, As Amended.

Jennifer Irvine  
County Engineer/ECM Administrator

Date

Conditions: \_\_\_\_\_

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## 1.0 LOCATION and DESCRIPTION

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**Creekside South at Lorson Ranch** is located south of the East Tributary of Jimmy Camp Creek (Etrib). The site is located on approximately 64.257 acres of vacant land. Future plans are to develop this site into single-family residential developments. Also included in this report and plan is the proposed layout for Creekside South at Lorson Ranch which is located east and south of the East Tributary of Jimmy Camp Creek. The land is currently owned by Lorson LLC or its nominees for Lorson Ranch.

The site is located in the North 1/2 of Section 23, Township 15 South and Range 65 West of the 6<sup>th</sup> Principal Meridian. The property is bounded on the north and west by the East Tributary of Jimmy Camp Creek, on the northeast by Lorson Ranch East Filing #4, single-family residential development and on the south by the Lorson Ranch South Boundary and Peaceful Valley Lake Estates. For reference, a vicinity map is included in Appendix A of this report.

### Conformance with applicable Drainage Basin Planning Studies

There is an existing (unapproved) DBPS for Jimmy Camp Creek prepared by Wilson & Company in 1987, and is referenced in this report. The only major drainage improvements for this study area according to the 1987 Wilson study was the reconstruction of the East Tributary of Jimmy Camp Creek (East Tributary). In 2014, a portion of the East Tributary was reconstructed from Fontaine Boulevard south 2,800 feet in accordance with the 1987 study, which is located within this project. This section of the East Tributary included a trapezoidal channel section with 6:1 side slopes and a sand bottom. On March 9, 2015, a new DBPS for Jimmy Camp Creek and the East Tributary was completed by Kiowa Engineering. The Kiowa Engineering DBPS for Jimmy Camp Creek has not been adopted by El Paso County but is allowed for concept design. The concept design for the remaining portions of the Etrib include an armoring concept and full spectrum detention pond requirements. The Kiowa DBPS did not calculate drainage fees so current El Paso County drainage/bridge fees apply to this development. Per the Kiowa DBPS concept, the preferred channel improvements include selective channel armoring on outer bends and a low flow channel for the East Tributary. Channel improvements in the East Tributary are potentially reimbursable against drainage fees for future development but need to be processed through the county process for reimbursement. Kiowa Engineering Corporation is nearing completion of construction plans for the East Tributary of Jimmy Camp Creek from the south property line of Lorson Ranch north and east to the channel improvements constructed by Lorson Ranch in 2014.

### Conformance with Lorson Ranch MDDP1 by Pentacor Engineering

Lorson Ranch MDDP1 (October 26, 2006) includes this project area and the East Tributary. This PDR conforms to the MDDP1 for Lorson Ranch and is referenced in this report. The major infrastructure referenced in the MDDP includes the Etrib armoring from the south property line of Lorson Ranch east and north to the previously reconstructed Etrib completed in 2014 and construction of several on-site detention ponds. Kiowa Engineering is currently designing this section of the East Tributary and is included in the appendix of this report. Detention/WQ Pond E2 (existing pond) will be increased in volume and will include a full spectrum outlet structure and emergency overflow structure. Proposed Detention/WQ pond J is shown as a full spectrum detention /WQ pond in the MDDP and will be designed/constructed as part of Creekside South at Lorson Ranch. Pond I and K as shown in the MDDP will not be constructed because the runoff has been redirected to Pond J reducing the number of ponds Lorson Ranch will have to maintain.

### Reconstruction of the East Tributary of Jimmy Camp Creek

The Kiowa DBPS shows the East Tributary to be protected using selective armoring (soil rip rap) at the outside stream bends (500' minimum radius) and a stabilized low flow channel. The East Tributary has been divided into three different sections, south, middle, and north. The first section (south) is from the south property line east and north to design point ET-3 (see drainage map) and is roughly 2,900 feet in length. The south section is within this preliminary plan area and will be armored in accordance with the Kiowa DBPS and is currently being designed by Kiowa Engineering and construction will begin in

2020. The 100-year flow rate for design is 5,500cfs for the south section. The middle section is from Design Point ET-3 north 2,800 feet to the future extension of Fontaine Boulevard. The channel for this section was reconstructed and stabilized in 2014 in accordance with the 1987 Wilson DBPS. LOMR Case No. 14-08-0534P was approved by FEMA for this middle section. The northern section is from Fontaine Boulevard and extends north to the north property line. The north section was constructed in 2018 as part of Lorson Ranch East Filing No. 1 improvements. The channel consists of a stabilized low flow channel and soil rip rap armored outer bends and followup LOMR Case No. 19-08-0605P has been approved. The 100-year flow rate for design is from FEMA FIS data and is from 4,400cfs to 4,750cfs for this section. The low flow channel is sized using 10% of the 100-yr FEMA flow rates and is from 440cfs to 475cfs.

Creekside South at Lorson Ranch is located within the ***“Jimmy Camp Creek Drainage Basin”***, which is a fee basin in El Paso County.

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## **2.0 DRAINAGE CRITERIA**

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The supporting drainage design and calculations were performed in accordance with the City of Colorado Springs and El Paso County “Drainage Criteria Manual (DCM)”, dated November, 1991, the El Paso County “Engineering Criteria Manual”, Chapter 6 and Section 3.2.1 Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014, and the UDFCD “Urban Storm Drainage Criteria Manual” Volumes 1, 2 and 3 for inlet sizing and full spectrum ponds. No deviations from these published criteria are requested for this site. The proposed improvements to the Lorson Ranch Development will be in substantial compliance with the “Jimmy Camp Creek Drainage Basin Planning Study”, prepared by Kiowa Engineering Corp., Colorado Springs, CO.

The Rational Method as outlined in Section 6.3.0 of the May 2014 “Drainage Criteria Manual” and in Section 3.2.8.F of the El Paso County “Engineering Criteria Manual” was used for basins less than 130 acres to determine the rainfall and runoff conditions for the proposed development of the site. The runoff rates for the 5-year initial storm and 100-year major design storm were calculated.

Current updates to the Drainage Criteria manual for El Paso County indicates if detention is necessary, Full Spectrum Detention will be included in the design, based on this criteria, Full Spectrum Detention will be required for this development

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## **3.0 EXISTING HYDROLOGICAL CONDITIONS**

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The site is currently undeveloped with native vegetation (grass with no shrubs) and slopes in a northerly direction to the East Tributary of Jimmy Camp Creek.

The Soil Conservation Service (SCS) classifies the soils within the Creekside South at Lorson Ranch site and the offsite drainage basin boundary as; 3-Ascalon Sandy Loam (2%), 10-Blendon Sandy Loam (1%), 52-Manzanst clay loam (11%), 54-Midway Clay Loam (10%), 56-Nelson-Tassel fine sandy loams (29%), 104-Vona Sandy Loam (12%), 108-Wiley silt loam (35%). The sandy loams are considered hydrologic soil group A/B soils with moderate to moderately rapid permeability. The clay loams are considered hydrologic soil group C/D soils with slow permeability. All of these soils are susceptible to erosion by wind and water, have low bearing strength, moderate to high shrink-swell potential, and high frost heave potential. The sandy loams are comprised of the hydrologic soil group B with moderate to moderately rapid permeability. The Manzanst and Midway clay loams are considered hydrologic soil group C and D soils with slow permeability. The clay loam soils are susceptible to erosion by wind and water, have low bearing strength, moderate to high shrink-swell potential, and high frost heave potential (see table 3.1 below). The clay loams are difficult to vegetate. The clay loams are difficult to vegetate. These soils can be mitigated easily by limiting their use as topsoil.

**Table 3.1: SCS Soils Survey.**

Soil	Hydro. Group	Shrink/Swell Potential	Permeability	Surface Runoff Potential	Erosion Hazard
3-Ascalon Sandy Loam (2%)	B	Moderate	Moderate	Slow to Medium	Moderate
10-Blendon Sandy Loam (1%)	B	Low	Moderately Rapid	Slow	Moderate
52-Manzanst Clay Loam (11%)	C	Moderate to high	Slow	Medium	Moderate
54-Midway Clay Loam (10%)	D	High	Slow	Medium to Rapid	Moderate to High
56-Nelson-Tassel sandy loam (29%)	B	Moderate	Moderately Rapid	Slow	Moderate
104-Vona Sandy Loam (12%)	C	Moderate to High	Slow	Medium	Moderate
108-Vona Sandy Loam (35%)	B	Moderate	Moderate	Medium	Moderate

Excerpts from the SCS “Soil Survey of El Paso County Area, Colorado” are provided in **Appendix A** for further reference.

For the purpose of preparing hydrologic calculations for this report, the soil of each basin was weighted and used for runoff calculations.

Portions of the site are located within the delineated 100-year floodplain of the East Tributary of Jimmy Camp Creek per the Federal Emergency Management Agency (FEMA) Flood Rate Insurance Map (FIRM) number 08041C0957 G, effective December 7, 2018 [2]. Floodplain along the East Tributary of Jimmy Camp Creek was modified per LOMR 19-08-0605P effective May 4, 2020 (see appendix). Floodplain designations include Zone AE and Zone X within the property boundary. A portion of this map is provided in **Appendix A** for reference. A CLOMR for the creek construction by Kiowa Engineering will not be necessary since BFE's are not changing.

#### Basin OS-E2 (overall offsite basin)

This 43.18 acre offsite basin contributes flow from the Peaceful valley Lake Estates subdivision overland onto Basin EX-E2. It is estimated that the flow to Basin EX-E2 will be 18.0cfs and 78.4cfs for 5-year and 100-year events respectively.

#### Basin EX-E2

This 31.81 acre basin includes areas between the east tributary of Jimmy Camp Creek, Lorson Ranch East Filing #4 and the South Boundary of Lorson Ranch. Under existing conditions, this area flows northwesterly to the East Tributary and contributes 10.7cfs and 56.9cfs for 5-year and 100-year events respectively.

#### Design Point 3 (OS-E2.1 & EX-E2)

This 74.99 acre design point is comprised of Basins OS-E2.1 and EX-E2; runoff flows in a northwesterly direction to the East Tributary of Jimmy Camp Creek and generates a peak flow of 23.9cfs and 112.0cfs for 5-year and 100-year events respectively

#### Basin OS-I1.1

This 15.54 acre offsite basin contributes flow from the Peaceful Valley Lake Estates subdivision overland onto Basin EX-I1. It is estimated that the flow to Basin EX-I1 will be 6.7cfs and 30.7cfs for the 5-year and 100-year storm events respectively.

#### Basin EX-I1

This 12.78 acre basin includes that area between the east tributary of Jimmy Camp Creek and the South Boundary of Lorson Ranch. Under existing conditions, this area flows northwesterly to the East Tributary and contributes 3.4cfs and 22.7cfs for 5-year and 100-year events respectively.

#### Design Point 2 (OS-I1.1 & EX-I1)

This 28.32 acre design point is comprised of Basins OS-I1.1 and EX-I1; runoff flows in a northwesterly direction to the East Tributary of Jimmy Camp Creek and generates a peak flow of 8.7cfs and 46.1cfs for 5-year and 100-year events respectively

#### Basin OS-J1.1

This 11.55 acre offsite basin contributes flow from the Peaceful Valley Lake Estates subdivision and a portion of Apple Ridge Subdivision overland onto Basin EX-J1. It is estimated that the flow to Basin EX-J1 will be 5.7cfs and 23.0cfs for the 5-year and 100-year storm events respectively.

#### Basin EX-J1

This 15.29 acre basin includes that area between the east tributary of Jimmy Camp Creek and the South Boundary of Lorson Ranch. Under existing conditions, this area flows northwesterly to the East Tributary and contributes 6.9cfs and 31.6cfs for 5-year and 100-year events respectively.

#### Design Point 1 (OS-J1.1 & EX-J1)

This 26.84 acre design point is comprised of Basins OS-J1.1 and EX-J1; runoff flows in a northwesterly direction to the East Tributary of Jimmy Camp Creek and generates a peak flow of 10.8cfs and 46.6cfs for 5-year and 100-year events respectively

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### **4.0 DEVELOPED HYDROLOGICAL CONDITIONS**

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Hydrology for the **Creekside South at Lorson Ranch** drainage report was based on the City of Colorado Springs/El Paso County Drainage Criteria. Sub-basins that lie within this project were determined and the 5-year and 100-year peak discharges for the developed conditions have been presented in this report. Based on these flows, storm inlets will be added when the street capacity is exceeded.

This site can be broken into two soil types. The westerly portion is Soil Type A/B and a small area on the east edge consists of Soil Type C/D. See Appendix A for SCS Soils Map.

The time of concentration for each basin and sub-basins were developed by using overland, ditch, street and pipe flow components. The maximum overland flow length for developed conditions was limited to 100 feet. Travel time velocities ranged from 2 to 6 feet per second. The travel time calculations are included in the back of this report. Runoff coefficients for the various land uses were obtained from the City of Colorado Springs/El Paso County Drainage Criteria Manual.

Drainage concepts for each of the basins are briefly discussed as follow:

#### Basin E7

This basin consists of runoff from residential development. Runoff will be directed east to Trappe Drive and then routed north via existing curb and gutter to a low point in Trappe Drive where it will be collected by an existing Type R inlet constructed as part of Lorson Ranch East Filing No. 4. Basin E7 was included in the final drainage report for Lorson Ranch East Filing No. 4. The developed flow from this 0.60-acre basin E7 is 1.2cfs for the 5-year storm event and 2.7cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.1

This basin consists of runoff from 2.5-acre rural residential land and open space areas under the existing electric powerline. Runoff will be directed northwesterly to Horton Drive, then routed west in Horton Drive to Design Point 16 via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 4.00-acre is 4.0cfs for the 5-year storm event and 12.9cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin OS-E2.1

This offsite basin consists of runoff from existing offsite 5.0-acre rural residential development located south of Lorson Ranch. These flows will be directed north through onsite basin E8.2 to Design Point 14 and intercepted by a storm sewer system in Horton Drive. The developed flow from this 36.66-acre basin OS-E2.1 is 15.3cfs for the 5-year storm event and 68.1cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.2

This basin consists of runoff from 2.5-acre rural residential development land. These flows will be directed north to Design Point 14 and intercepted by a storm sewer system in Horton Drive, and will also intercept overland runoff from basin OS-E2.1. The developed flow from this 1.70-acre basin E8.2 is 1.2cfs for the 5-year storm event and 4.9cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin OS-E2.2

This offsite basin consists of runoff from offsite existing 5.0-acre rural residential development. These flows will be directed north through onsite basin E8.3 to Horton Drive, then southwesterly in Horton Drive to Design Point 15 and a Type R inlet. The developed flow from this 6.52-acre basin is 3.4cfs for the 5-year storm event and 15.4cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.3

This basin consists of runoff from on-site 2.5-acre lots and urban residential development. These flows will be directed north to Horton Drive, then southwesterly in Horton Drive to Design Point 15 via curb and gutter where it will be collected by a Type R inlet, and will also intercept overland runoff from basin OS-E2.2. The developed flow from this 5.37-acre basin E8.3 is 4.7cfs for the 5-year storm event and 14.3cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.4

This basin consists of runoff from the urban residential development. These flows will be directed south to Horton Drive, then southeasterly in Horton Drive to Shunka Lane at Design Point 17. The developed flow from this 1.20-acre basin is 1.9cfs for the 5-year storm event and 4.3cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.5

This basin consists of runoff from the urban residential development. These flows will be directed north and east to Shunka Lane, then northerly in Shunka Lane and Luneth Drive to Design Point 19 via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 4.27-acre basin is



6.8cfs for the 5-year storm event and 15.0cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.6

This basin consists of runoff from the urban residential development. These flows will be directed west to Akela Lane, then northerly in Akela Lane and west in Luneth Drive to Design Point 19 via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 1.02-acre basin is 2.0cfs for the 5-year storm event and 4.5cfs for the 100-year storm event. See the appendix for detailed calculations

#### Basin E8.7

This basin consists of runoff from the urban residential development. These flows will be directed east to Akela Lane, then northerly in Akela Lane and west in Luneth Drive to Design Point 19 via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 0.71-acre basin is 1.4cfs for the 5-year storm event and 3.1cfs for the 100-year storm event. See the appendix for detailed calculations

#### Basin E8.8

This basin consists of runoff from the urban residential development. These flows will be directed south to Horton Drive and west to Shunka Lane, then northerly in Shunka Lane and west in Luneth Drive to Design Point 19 via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 2.43-acre basin is 4.1cfs for the 5-year storm event and 9.1cfs for the 100-year storm event. See the appendix for detailed calculations

#### Basin E8.9

This basin consists of runoff from the urban residential development. These flows will be directed south to Luneth Drive, then southeasterly in Luneth Drive to Design Point 20 via curb and gutter where it will be collected by Type R inlets. The developed flow from this 1.52-acre basin is 2.4cfs for the 5-year storm event and 5.4cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin E8.10

This basin consists of runoff from the urban residential development. These flows will be directed south to Luneth Drive, then southwesterly in Luneth Drive to Design Point 20 via curb and gutter where it will be collected by Type R inlets. The developed flow from this 0.38-acre basin is 0.9cfs for the 5-year storm event and 2.0cfs for the 100-year storm event. See the appendix for detailed calculations

#### Basin E8.11

This basin consists of runoff from backyards of urban residential development and open space areas draining directly to Pond E2. The developed flow from this 3.99-acre basin is 3.2cfs for the 5-year storm event and 12.2cfs for the 100-year storm event. See the appendix for detailed calculations

#### Basin OS-I1.1

This offsite basin consists of runoff from offsite existing 5.0-acre rural residential development. These flows will be directed north through onsite basin I1.2 to Design Point 4 and intercepted by a Type R inlet in Horton Drive. The developed flow from this 15.54-acre basin is 6.7cfs for the 5-year storm event and 30.7cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin I1.2

This basin consists of runoff from 2.5-acre rural residential development. These flows will be directed north to Design Point 4 and intercepted by a Type R inlet in Horton Drive, and will also intercept runoff from basin OS-I1.1 The developed flow from this 6.23-acre basin is 5.8cfs for the 5-year storm event and 17.6cfs for the 100-year storm event. See the appendix for detailed calculations

### Overall Basin I1

This overall basin combines basins OS-I1.1 and I1.2 and develops peak flow from offsite 5.0-acre and 2.5-acre rural residential development. These flows will be directed north to Design Point 4 and intercepted by a Type R inlet in Horton Drive. The developed flow from this overall 21.77-acre basin is 11.1cfs for the 5-year storm event and 43.6cfs for the 100-year storm event. See the appendix for detailed calculations

### Basin I2

This basin consists of runoff from the urban residential development. These flows will be directed south to Horton Drive, then east to Nakai Lane, then northerly in Nakai Lane and west in Luneth Drive to Design Point 5 via curb and gutter where it will be collected by a Type R inlet on a continuous grade. The developed flow from this 1.12-acre basin is 1.9cfs for the 5-year storm event and 4.2cfs for the 100-year storm event. See the appendix for detailed calculations

### Basin I3

This basin consists of runoff from the urban residential development. These flows will be directed south to Horton Drive, then westerly and southwesterly in Horton Drive to Nakai Lane. The developed flow from this 1.01-acre basin is 1.7cfs for the 5-year storm event and 3.8cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin I4

This basin consists of runoff from the urban residential development. These flows will be directed north to Luneth Drive and west to Nakai Lane, then northerly in Nakai Lane and then continues west in Luneth Drive to Design Point 5 via curb and gutter where it will be collected by a Type R inlet on a continuous grade. The developed flow from this 3.45-acre basin is 5.6cfs for the 5-year storm event and 12.3cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin I5

This basin consists of runoff from the urban residential development. These flows will be directed north to Luneth Drive, runoff then continues west in Luneth Drive to Design Point 7 via curb and gutter where it will be collected by a Type R inlet on a continuous grade. The developed flow from this 1.44-acre basin is 2.7cfs for the 5-year storm event and 5.8cfs for the 100-year storm event. See the appendix for detailed calculations

### Basin I6

This basin consists of runoff from the urban residential development. These flows will be directed northerly and westerly to Luneth Drive, runoff continues westerly and southerly in Luneth Drive to Design Point 8 via curb and gutter where it will be collected by a sump Type R inlet. The developed flow from this 1.18-acre basin is 2.0cfs for the 5-year storm event and 4.4cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin I7

This basin consists of runoff from the street and the urban residential development. These flows will be directed southerly to Luneth Drive, then westerly and southwesterly in Luneth Drive to via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 2.01-acre basin I7 is 2.8cfs for the 5-year storm event and 6.2cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin I8

This basin consists of runoff from backyards of urban residential development and open space areas draining directly to pond J. The developed flow from this 2.44-acre basin is 1.9cfs for the 5-year storm event and 6.6cfs for the 100-year storm event. See the appendix for detailed calculations

### Overall Basin I

This basin contains a total area of 34.42 acres and runoff is routed to proposed detention pond J via overland, street and storm system from the I1 to I8 offsite and onsite sub-basins. The peak developed flow from basin is 24.3cfs for the 5-year storm event and 73.8cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin OS-J1.1

This offsite basin consists of runoff from existing offsite 5.0-acre rural residential development. These flows will be directed north through onsite basin J1.2 to Design Point 1 and intercepted by a storm sewer in Horton Drive. The developed flow from this 11.55-acre basin is 5.7cfs for the 5-year storm event and 23.0cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin J1.2

This basin consists of runoff from 2.5-acre rural residential development. These flows will be directed north to Design Point 1 and intercepted by a storm sewer system in Horton Drive, and will also intercept runoff from basin OS-J1.1. The developed flow from this 2.01-acre basin is 1.3cfs for the 5-year storm event and 5.3cfs for the 100-year storm event. See the appendix for detailed calculations.

### Overall Basin J1

This overall basin combines basins OS-J1.1 and J1.2 and develops peak flow from existing offsite 5.0-acre and 2.5-acre rural residential development. These flows will be directed north to Design Point 1 and intercepted by a storm sewer system in Horton Drive. The developed flow from this 13.56-acre basin is 6.4cfs for the 5-year storm event and 26.0cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin J2

This basin consists of runoff from the street and urban residential development. These flows will be directed north to Horton Drive, runoff then continues west in Luneth Drive to Design Point 2 via curb and gutter where it will be collected by a Type R inlet on a continuous grade. The developed flow from this 0.36-acre basin is 1.1cfs for the 5-year storm event and 2.2cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin J3

This basin consists of runoff from the urban residential development, open space, and offsite urban development. These flows will be directed north to Luneth Drive, then easterly and northeasterly in Luneth Drive to Design Point 2a. The developed flow from this 3.40-acre basin is 5.5cfs for the 5-year storm event and 12.0cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin J4

This basin consists of runoff from the urban residential development and open space. These flows will be directed southerly to Horton Drive and westerly to Luneth Drive, runoff continues westerly in Horton Drive and northeasterly in Luneth Drive to Design Point 3a via curb and gutter where it will be collected by a Type R inlet. The developed flow from this 1.93-acre basin is 3.4cfs for the 5-year storm event and 7.4cfs for the 100-year storm event. See the appendix for detailed calculations.

### Basin J5

This basin consists of runoff from the urban residential development. These flows will be directed south to Luneth Drive, then easterly and northeasterly in Luneth Drive to Design Point 10 via curb and gutter where it will be collected by sump Type R inlets. The developed flow from this 1.93-acre basin is 3.1cfs for the 5-year storm event and 6.9cfs for the 100-year storm event. See the appendix for detailed calculations.

### Overall Basin J

This basin contains a total area of 21.18 acres and runoff is routed to proposed detention pond J via overland, street and storm system from the J1 to the J5 offsite and onsite sub-basins. The peak

developed flow from this overall basin is 15.4cfs for the 5-year storm event and 45.9cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Combined Basins I & J

These basins contain a total area of 55.60 acres and runoff is routed to proposed detention Pond J via overland, street and storm system from the I1 to I8 offsite and onsite sub-basins. The peak developed flow from this overall basin is 38.7cfs for the 5-year storm event and 116.7cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin K1

This basin consists of runoff from open space areas that sheet flows directly to the East Tributary. The developed flow from this 2.65-acre basin is 1.2cfs for the 5-year storm event and 6.6cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin K2

This basin consists of runoff from open space areas that sheet flows directly to the East Tributary. The developed flow from this 2.14-acre basin is 1.2cfs for the 5-year storm event and 6.8cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin L

This basin consists of runoff from open space areas that sheet flows directly to the East Tributary. The developed flow from this 2.30-acre basin is 1.4cfs for the 5-year storm event and 7.8cfs for the 100-year storm event. See the appendix for detailed calculations.

#### Basin M

This basin consists of runoff from open space areas that sheet flows directly to the East Tributary. The developed flow from this 0.48-acre basin is 0.3cfs for the 5-year storm event and 1.5cfs for the 100-year storm event. See the appendix for detailed calculations.

See the Developed Conditions Hydrology Calculations in the back of this report and the Developed Conditions Drainage Map (Map Pocket) for the 5-year and 100-year storm event amounts.

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## **5.0 HYDRAULIC SUMMARY**

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The sizing of the hydraulic structures and detentions ponds were prepared by using the *StormSewers* and *Hydrographs* computer software programs developed by Intellisolve, which conforms to the methods outlined in the "City of Colorado Springs/El Paso County Drainage Criteria Manual". Street capacities and Inlets were sized by Denver Urban Drainage's excel spreadsheet UD-Inlet.

It is the intent of this drainage report to use the proposed curb/gutter and storm sewer in the streets to convey runoff to detention and water quality ponds then to the East Tributary of Jimmy Camp Creek. Inlet size and location are preliminary only as shown on the storm sewer layout in the appendix. See Appendix C for detailed hydraulic calculations and the storm sewer model.

Table 1: Street Capacities (100-year capacity is only ½ of street)

Street Slope	Residential Local		Residential Collector		Principal Arterial	
	5-year	100-year	5-year	100-year	5-year	100-year
0.5%	6.3	26.4	9.7	29.3	9.5	28.5
0.6%	6.9	28.9	10.6	32.1	10.4	31.2
0.7%	7.5	31.2	11.5	34.6	11.2	33.7
0.8%	8.0	33.4	12.3	37.0	12.0	36.0
0.9%	8.5	35.4	13.0	39.3	12.7	38.2
1.0%	9.0	37.3	13.7	41.4	13.4	40.2

1.4%	10.5	44.1	16.2	49.0	15.9	47.6
1.8%	12.0	45.4	18.4	50.4	18.0	50.4
2.2%	13.3	42.8	19.4	47.5	19.5	47.5
2.6%	14.4	40.7	18.5	45.1	18.5	45.1
3.0%	15.5	39.0	17.7	43.2	17.8	43.2
3.5%	16.7	37.2	16.9	41.3	17.0	41.3
4.0%	17.9	35.7	16.2	39.7	16.3	29.7
4.5%	19.0	34.5	15.7	38.3	15.7	38.3
5.0%	19.9	33.4	15.2	37.1	15.2	37.1

Note: all flows are in cfs (cubic feet per second)

#### Design Point 1

Design Point 1 is the overland runoff flowing north to a 24" storm sewer (end section) located at Horton Drive. The total flow into the storm sewer system is 6.4cfs and 26.0cfs in the 5/100-year storm events. The Hw/D is 1.69' for a 24" RCP end section in the 100-year storm event.

#### Design Point 2

Design Point 2 is located in Horton Drive (south side) east of Luneth Drive

##### (5-year storm)

**Tributary Basins:** J1

**Inlet/MH Number:** Inlet J2

**Upstream flowby:** 0cfs

**Total Street Flow:** 1.1cfs

**Flow Intercepted:** 1.1cfs

**Flow Bypassed:** 0

**Inlet Size:** 5' type R

**Street Capacity:** Street slope = 2%, capacity = 12cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** J1

**Inlet/MH Number:** Inlet J2

**Upstream flowby:** 0cfs

**Total Street Flow:** 2.2cfs

**Flow Intercepted:** 1.9cfs

**Flow Bypassed:** 0.3cfs to Des. Pt 8

**Inlet Size:** 5'type R

**Street Capacity:** Street slope = 2%, capacity = 45.4cfs (half street) is okay

#### Design Point 3

Design Point 3 is the total pipe flow in a 24" RCP storm sewer in Horton Drive to Luneth Drive and is located west of Design Point 2. The total pipe flow is 7.5cfs and 27.9cfs in the 5/100-year storm events.

#### Design Point 3a

Design Point 3a is located in Luneth Drive (east side) south of the low point at Pond J

##### (5-year storm)

**Tributary Basins:** J3+J4

**Upstream flowby:** 0cfs

**Inlet/MH Number:** Inlet J4

**Total Street Flow:** 8.6cfs

**Flow Intercepted:** 6.6cfs

**Inlet Size:** 10' type R

**Flow Bypassed:** 2.0cfs to Des. Pt. 8

**Street Capacity:** Street slope = 1.9%, capacity = 12cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** J3+J4

**Upstream flowby:** 0.3cfs

**Inlet/MH Number:** Inlet J4

**Total Street Flow:** 19.2cfs

**Flow Intercepted:** 9.9cfs

**Inlet Size:** 10' type R

**Flow Bypassed:** 9.3cfs to Des. Pt. 8

**Street Capacity:** Street slope = 1.9%, capacity = 45.4cfs (half street) is okay

#### Design Point 3b

Design Point 3b is the total pipe flow in a 30" RCP storm sewer in Luneth Drive and is located south of Design Point 8. The total pipe flow is 14.1cfs and 37.8cfs in the 5/100-year storm events.

#### Design Point 4

Design Point 4 is located at a low point in Horton Drive (south side) at Nakai Lane

##### (5-year storm)

**Tributary Basins:** I-1

**Upstream flowby:** 0cfs

**Inlet/MH Number:** Inlet I-1

**Total Street Flow:** 11.1cfs

**Flow Intercepted:** 11.1cfs

**Inlet Size:** 20' type R, sump

**Flow Bypassed:** 0

**Street Capacity:** Street slope = 2.3%, capacity = 13.3cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** I-1

**Upstream flowby:** 0cfs

**Inlet/MH Number:** Inlet I-1

**Total Street Flow:** 43.6cfs

**Flow Intercepted:** 15.5cfs

**Inlet Size:** 20' type R, sump

**Flow Bypassed:** 28.1cfs to Des. Pt. 5

**Street Capacity:** Street slope = 2.3%, capacity = 32.8cfs (half street). Flow uses north half of street

#### Design Point 5

Design Point 5 is located in Luneth Drive (south side) west of Nakai Lane

##### (5-year storm)

**Tributary Basins:** I2, I3, I4

**Upstream flowby:** 0cfs

**Inlet/MH Number:** Inlet I-2

**Total Street Flow:** 8.7cfs

**Flow Intercepted:** 3.6cfs

**Inlet Size:** 5' type R, on-grade

**Flow Bypassed:** 5.1cfs to Des. Pt. 7

**Street Capacity:** Street slope = 0.8%, capacity = 8.0cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** I2, I3, I4

**Upstream flowby:** 28.1cfs

**Inlet/MH Number:** Inlet I-2

**Total Street Flow:** 47.4cfs

**Flow Intercepted:** 7.1cfs

**Inlet Size:** 5' type R, on-grade

**Flow Bypassed:** 40.3cfs to Des. Pt 7

**Street Capacity:** Street slope = 0.8%, capacity = 33.4cfs (half street). Flow overtops crown and flows on north side of Luneth Dr. Only flow from Basin I7 (6.2cfs) is on north side. Capacity okay

#### Design Point 6

Design Point 6 is the total pipe flow in a 30" RCP storm sewer in Luneth Drive and is located west of Nakai Lane. The total pipe flow is 14.7cfs and 22.6cfs in the 5/100-year storm events.

#### Design Point 7

Design Point 7 is located in Luneth Drive (south side) west of Nakai Lane and Des. Pt. 5

##### (5-year storm)

**Tributary Basins:** I5

**Upstream flowby:** 5.1cfs

**Inlet/MH Number:** Inlet I-5

**Total Street Flow:** 7.8cfs

**Flow Intercepted:** 3.5cfs

**Inlet Size:** 5' type R, on-grade

**Flow Bypassed:** 4.3cfs to Des. Pt. 8

**Street Capacity:** Street slope = 0.8%, capacity = 8.0cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** I5

**Upstream flowby:** 40.3cfs

**Inlet/MH Number:** Inlet I-5

**Total Street Flow:** 46.1cfs

**Flow Intercepted:** 7.0cfs

**Inlet Size:** 5' type R, on-grade

**Flow Bypassed:** 24.1cfs to Des. Pt 8  
15.0cfs to Des. Pt.10

**Street Capacity:** Street slope = 0.8%, capacity = 33.4cfs (half street). Flow overtops crown and flows on north side of Luneth Dr to Des. Pt.10. Only flow from Basin I7 (6.2cfs) is on north side. Capacity okay

#### Design Point 7a

Design Point 7a is the total pipe flow in a 30" RCP storm sewer in Luneth Drive and is located west of Design Point 7. The total pipe flow is 18.2cfs and 29.6cfs in the 5/100-year storm events.

#### Design Point 8

Design Point 8 is located in Luneth Drive (east side) at a low point east of Pond J

##### (5-year storm)

**Tributary Basins:** I6

**Upstream flowby:**  $2.0+4.3 = 6.3\text{cfs}$

**Inlet/MH Number:** Inlet I6

**Total Street Flow:** 8.3cfs

**Flow Intercepted:** 8.3cfs

**Inlet Size:** 10' type R, sump

**Flow Bypassed:** 0

**Street Capacity:** Street slope = 1.0%, capacity = 9.0cfs, capacity okay since flow is from both ways

##### (100-year storm)

**Tributary Basins:** I6

**Upstream flowby:**  $0.3+9.3+24.1=33.7\text{cfs}$

**Inlet/MH Number:** Inlet I6

**Total Street Flow:** 38.1cfs

**Flow Intercepted:** 15.5cfs

**Inlet Size:** 10' type R, sump

**Flow Bypassed:** 22.6cfs to Des. Pt 10

**Street Capacity:** Street slope = 1.0%, capacity = 37.3cfs (half street). Flow overtops crown and flows on west side of Luneth Dr. Only flow from Basin J5 (6.9cfs) is on westside. Capacity okay

#### Design Point 9

Design Point 9 is the total pipe flow in a 36" RCP storm sewer in Luneth Drive and is located west of Design Point 8. The total pipe flow is 22.4cfs and 53.3cfs in the 5/100-year storm events.



#### Design Point 10

Design Point 10 is located in Luneth Drive (west side) at a low point east of Pond J

##### (5-year storm)

**Tributary Basins:** J5+I7

**Upstream flowby:** 0

**Inlet/MH Number:** Inlet I7

**Total Street Flow:** 5.0cfs

**Flow Intercepted:** 5.0cfs

**Flow Bypassed:** 0

**Inlet Size:** 45' type R, sump

**Street Capacity:** Street slope = 1.0%, capacity = 9.0cfs, capacity okay since flow is from both ways

##### (100-year storm)

**Tributary Basins:** J5+I7

**Upstream flowby:** 37.6cfs

**Inlet/MH Number:** Inlet I7

**Total Street Flow:** 50.7cfs

**Flow Intercepted:** 50.7cfs

**Flow Bypassed:** 0

**Inlet Size:** 45' type R, sump (flow depth = 7.8" at flowline curb, flow spreads to ROW line and does not inundate lots)

#### Design Point 11

Design Point 11 is the total pipe flow in a 42" RCP storm sewer in Luneth Drive and is located west of Design Point 10. The total pipe flow is 27.4cfs and 104.0cfs in the 5/100-year storm events.

#### Design Point 12

Design Point 12 is the total pipe flow in a 48" RCP storm sewer in Luneth Drive and is located west of Design Point 11. The total pipe flow is 45.6cfs and 133.6cfs in the 5/100-year storm events and outlets into Pond J.

#### Design Point 13

Design Point 13 is located west of Pond J and is the total flow from the outlet structure for Pond J in a 36" RCP storm sewer. The total outflow is 1.2cfs and 55.5cfs in the 5/100-year storm events from the Pond J full spectrum EDB worksheets. The Pond Outflow Channel is a trapezoidal swale with a 5' bottom, 3:1 side slopes, 0.5% channel slope, and is lined with 12" D50 rip rap. This flow enters the low flow channel of the East Tributary of Jimmy Camp Creek in a rip rap swale. Kiowa Engineering has accommodated the low flow channel for this swale.

#### Design Point 14

Design Point 14 is the overland runoff flowing north to a 36" storm sewer (end section) located at Horton Drive and Shunka Lane. The total flow into the storm sewer system is 15.8cfs and 70.0cfs in the 5/100-year storm events. The Hw/D is 1.72' for a 36" RCP end section in the 100-year storm event.

#### Design Point 15

Design Point 15 is located on the south side of Horton Drive at Shunka Lane. This design point was added to verify the street capacity of Horton Drive on the south side of the street from the west. The total street flow is 6.2cfs and 22.9cfs in the 5/100-year storm events from Basins OS E2.2 & E8.3. The street capacity of Horton Drive at 0.7% slope is 7.5cfs (5-yr) and 31.2cfs (100-yr). The street capacity is not exceeded at this design point from the west.

#### Design Point 16

Design Point 16 is located in Horton Drive (south side) at a low point at Shunka Lane

##### (5-year storm)

**Tributary Basins:** E8.1 + Des. Pt 15

**Upstream flowby:** 0

**Inlet/MH Number:** Inlet E8.1

**Total Street Flow:** 9.4cfs

**Flow Intercepted:** 9.4cfs

**Inlet Size:** 25' type R, sump

**Flow Bypassed:** 0

**Street Capacity:** Street slope = 1.5%, capacity = 10.5cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** E8.1+ Des. Pt 15

**Upstream flowby:** 0

**Inlet/MH Number:** Inlet E8.1

**Total Street Flow:** 33.0cfs

**Flow Intercepted:** 18.9cfs

**Inlet Size:** 25' type R, sump

**Flow Bypassed:** 14.1cfs to Des. Pt.20

**Street Capacity:** Street slope = 1.5%, capacity = 44.1cfs, capacity okay

#### Design Point 17

Design Point 17 is the total pipe flow in a 36" RCP storm sewer in Shunka Lane. The total pipe flow is 25.2cfs and 85.5cfs in the 5/100-year storm events.

#### Design Point 18

Design Point 18 is located on the south side of Luneth Drive at Akela Lane. This design point was added to verify the street capacity of Luneth Drive on the south side of the street from the east. The total street flow is 3.4cfs and 7.5cfs in the 5/100-year storm events from Basins E8.6 & E8.7. The street capacity of Luneth Drive at 1.7% slope is 10.5cfs (5-yr) and 44.1cfs (100-yr). The street capacity is not exceeded at this design point.

#### Design Point 19

Design Point 19 is located in Luneth Drive (south side) at a low point at Shunka Lane

##### (5-year storm)

**Tributary Basins:** E8.4-E8.8

**Upstream flowby:** 0

**Inlet/MH Number:** Inlet E8.5

**Total Street Flow:** 15.0cfs

**Flow Intercepted:** 15.0cfs

**Inlet Size:** 25' type R, sump

**Flow Bypassed:** 0

**Street Capacity:** Street slope = 1.5%, capacity = 10.5cfs, capacity okay since half flow is from the west

##### (100-year storm)

**Tributary Basins:** E8.1+ Des. Pt 15

**Upstream flowby:** 0

**Inlet/MH Number:** Inlet E8.5

**Total Street Flow:** 33.1cfs

**Flow Intercepted:** 32.0cfs

**Inlet Size:** 25' type R, sump

**Flow Bypassed:** 1.1cfs to Des. Pt.20

**Street Capacity:** Street slope = 1.5%, capacity = 44.1cfs, capacity okay

#### Design Point 20

Design Point 20 is located in Luneth Drive (north side) at a low point at Shunka Lane

##### (5-year storm)

**Tributary Basins:** E8.9+E8.10

**Upstream flowby:** 0

**Inlet/MH Number:** Inlet E8.9

**Total Street Flow:** 3.1cfs

**Flow Intercepted:** 3.1cfs

**Inlet Size:** double 10' type R, sump

**Flow Bypassed:** 0

**Street Capacity:** Street slope = 1.5%, capacity = 10.5cfs, capacity okay

##### (100-year storm)

**Tributary Basins:** E8.9+E8.10

**Upstream flowby:** 1.1+14.1=15.2cfs

**Inlet/MH Number:** Inlet E8.9

**Total Street Flow:** 22.0cfs

**Flow Intercepted:** 22.0cfs

**Inlet Size:** double 10' type R, sump

**Flow Bypassed:** 0

**Street Capacity:** Street slope = 1.5%, capacity = 44.1cfs (half street). Capacity okay

#### Design Point 21

Design Point 21 is the total pipe flow in a 30" RCP storm sewer in Luneth Drive connecting Inlets E8.9 to a 48" storm sewer flowing to Pond E2. The total pipe flow is 18.1cfs and 54.0cfs in the 5/100-year storm events.

#### Design Point 22

Design Point 22 is the total pipe flow in a 48" RCP storm sewer in from Luneth Drive flowing north into Pond E2. The total pipe flow is 43.3cfs and 139.5cfs in the 5/100-year storm events and outlets into Pond E2.

#### Design Point 22a

Design Point 22a is the total inflow from this development and Lorson Ranch East Filing No. 4 into Pond E2. The total pond inflow is 102.8cfs and 333.2cfs in the 5/100-year storm events and outlets into Pond E2.

#### Design Point 23

Design Point 23 is located west of Pond E2 and is the total flow from the outlet structure for Pond E2 in a 48" RCP storm sewer. The pond outlet structure is built as part of Lorson Ranch East Filing No. 4 but will be modified to account for development in Creekside South. The total pond outflow is 4.5cfs and 151.3cfs in the 5/100-year storm events from the Pond E2 full spectrum EDB worksheets. The outlet structure, outflow pipe, and creek outfall are all constructed as part of the Lorson Ranch East Filing 4 development. This flow enters the reconstructed portion of the East Tributary of Jimmy Camp Creek.

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## 6.0 DETENTION AND WATER QUALITY PONDS

Detention and Storm Water Quality for Creekside South at Lorson Ranch is required per El Paso County criteria. We have implemented the Full Spectrum approach for detention for Creekside South at Lorson Ranch per the Denver Urban Drainage Districts specifications. There is one existing detention pond to be expanded and one proposed detention pond for this project site. All developed runoff from this site will flow to ponds and will incorporate storm water quality features prior to discharge into the East Tributary. Open space areas (no development) will be allowed to flow directly to the East Tributary of Jimmy Camp Creek.

### Full Spectrum Pond Construction Requirements

Design calculations for full spectrum ponds will include a 15' wide gravel access road on a 15' wide bench at a maximum 10% slope to the pond bottom. The final design of the full spectrum ponds consists of an outlet structure, storm sewer outfall to the East Tributary, concrete low flow channels, sediment forebays, and overflow weirs to the East Tributary. Soil borings, embankment, slope, and compaction requirements for detention ponds can be found in the geotechnical report for the Creekside South prepared by RMG.

### Detention Pond E2 (Full Spectrum Design)

This is an on-site permanent full spectrum extended detention pond that includes water quality and discharges directly into the East Tributary. Pond E2 was partially constructed as part of Lorson Ranch East Filing No. 4 with a full spectrum outlet structure, forebay, and concrete low flow channel designed using the UDCF Full Spectrum spreadsheets. The existing outlet structure is a 6.7'x6.7' full spectrum sloped outlet structure with an interim overflow structure. Creekside South will add more developed area to the pond's tributary area requiring the pond to be expanded and the outlet structure to be modified. This development will expand the existing pond, update the existing outlet structure, construct additional forebay, construct additional concrete low flow channel, and construct a new concrete weir overflow spillway set above the outlet structure designed by the full spectrum spreadsheets to match pre-developed rates. The full spectrum print outs are in the appendix of this report. See map in appendix for watershed areas.

- Watershed Ares: 125 acres (full buildout of watershed including offsite 5-acre rural residential lots)
- Watershed Imperviousness: 35%
- Hydrologic Soils Group B (40%) and C/D (60%)
- Forebay: 0.0256ac-ft (see spreadsheet in appendix). (one existing and one new forebay)
- Zone 1 WQCV: 1.617ac-ft, WSEL: 5696.05, 0.8cfs
- Zone 2 EURV: 3.868ac-ft, WSEL: 5697.57, Top EURV set at 5698.85, 6.7'x17' outlet with flat top, 3.5cfs
- (5-yr): 5.072ac-ft, WSEL: 5698.34, 4.5cfs
- Zone 3 (100-yr): 9.855ac-ft, WSEL: 5701.16, 151.3cfs
- Pipe Outlet: 48" RCP at 0.5% with no restrictor plate
- Overflow Spillway: 55' wide bottom, elevation=5701.20, 4:1 side slopes
- Pre-development release rate into creek compliance from full spectrum pond spreadsheets
- Pond Bottom Elevation: 5693.00

### Existing Pond E2 and Existing Pond E2 Outlet Structure Modifications:

- Expand pond size to accommodate full buildout area
- Construct one additional concrete forebay at new 48" RCP storm sewer
- Construct new concrete low flow channel from new forebay to existing outlet structure
- Construct additional access road to new forebay
- Construct additional 11' length to 6.7'x6.7' outlet structure
- Modify Zone 1 WQ plate to larger size openings
- Modify Zone 2 square opening to 4"x18"
- Construct permanent concrete overflow weir

### Detention Pond J (Full Spectrum Design)

This is an on-site permanent full spectrum extended detention pond that includes water quality and discharges directly into the East Tributary. Pond J is designed using the UDCF Full Spectrum spreadsheets. The outlet structure is a standard full spectrum sloped outlet structure and the overflow spillway is a concrete weir set above the outlet structure designed by the full spectrum spreadsheets to match pre-developed rates. The full spectrum print outs are in the appendix of this report. See map in appendix for watershed areas.

- Watershed Area: 54 acres including offsite 5-acre rural residential lots
- Watershed Imperviousness: 26%
- Hydrologic Soils Group B (90%), C/D (10%)
- Forebay: 0.024ac-ft, 24" depth, std concrete forebay
- Zone 1 WQCV: 0.575ac-ft, WSEL: 5684.13, 0.3cfs
- Zone 2 EURV: 1.272ac-ft, WSEL: 5685.10, Top EURV wall set at 5685.37, 6'x6' outlet with 6:1 slope, 1.1cfs
- (5-yr): 1.442ac-ft, WSEL: 5685.31, 1.2cfs
- Zone 3 (100-yr): 3.545ac-ft, WSEL: 5687.67, 55.5cfs
- Pipe Outlet: 36" RCP at 0.5% with restrictor plate up 25"
- Overflow Spillway: 25' wide bottom, elevation=5687.77, 4:1 side slopes, flow depth=1.2'
- Pre-development release rate into creek compliance from full spectrum pond spreadsheets
- Pond Bottom Elevation: 5681.67

### Water Quality Design

Water quality will be provided by two permanent extended detention basins (Pond E2, J) for all of the developed areas of this site.

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## **7.0 DRAINAGE AND BRIDGE FEES**

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Creekside South at Lorson Ranch is located within the Jimmy Camp Creek drainage basin which is currently a fee basin in El Paso County. Current El Paso County regulations require drainage and bridge fees to be paid for platting of land as part of the plat recordation process. Lorson Ranch Metro District will be constructing the major drainage infrastructure as part of the district improvements.

Lorson Ranch Metro District will compile and submit to the county on a yearly basis the Drainage and bridge fees for the approved plats, and shall show all credits they have received for the same yearly time frame.

Creekside South at Lorson Ranch Filing No. 1 contains 64.257 acres. This project consists of 13.037 acres of open space (2% impervious), 30.458 acres residential (57% impervious based on 4600sf lots), 14.753 acres of large lots (5% impervious). Tract A (6.009 acres) which is a future development tract will defer fees until it is platted into lots. The 2020 drainage fees are \$19,084, bridge fees are \$893 and Drainage Surety fees are \$7,285 per impervious acre per Resolution 18-470. The drainage and bridge fees are calculated when the final plat is submitted. The fees are due at plat recordation. The following table details the drainage fees for the platted area. Lorson Ranch intends to use the Drainage Fee Pre-credits for the surety, drainage fee, and the bridge fee credits for the bridge fee.

**Table 1: Drainage/Bridge Fees**

Type of Land Use	Total Area (ac)	Imperviousness	Drainage Fee	Bridge Fee	Surety Fee
Residential Area	30.458	51%	\$296,442	\$13,871	\$113,162

Large Lots	14.753	11%	\$30,970	\$1,449	\$11,822
Open Space, Landscape Tracts,	13.037	2%	\$4,975	\$232	\$1,899
Total			\$332,387	\$15,552	\$126,883

**Table 7.1: Public Drainage Facility Costs (non-reimbursable)**

Item	Quantity	Unit	Unit Cost	Item Total
Rip Rap	200	CY	\$50/CY	\$10,000
Manholes	11	EA	\$3000/EA	\$33,000
Inlets	12	EA	\$3,000	\$36,000
18" Storm	54	LF	\$35	\$1,890
24" Storm	760	LF	\$40	\$30,400
30" Storm	775	LF	\$45	\$34,875
36" Storm	560	EA	\$50	\$28,000
42" Storm	29	EA	\$55	\$1,595
48" Storm	202	EA	\$60	\$12,120
24" FES	1	EA	\$250	\$250
36" FES	1	EA	\$300	\$300
			Subtotal	\$188,430
			Eng/Cont 15%)	\$28,264
			Total Est. Cost	\$216,694

**Table 7.2: Lorson Ranch Metro District Drainage Facility Costs (non-reimbursable)**

Item	Quantity	Unit	Unit Cost	Item Total
Full Spectrum Ponds and Outlet	2	LS	\$100,000	\$100,000
			Subtotal	\$100,000
			Eng/Cont (15%)	\$15,000
			Total Est. Cost	\$115,000

## 8.0 FOUR STEP PROCESS

The site has been developed to minimize wherever possible the rate of developed runoff that will leave the site and to provide water quality management for the runoff produced by the site as proposed on

the development plan. The following four step process should be considered and incorporated into the storm water collection system and storage facilities where applicable.

#### Step 1: Employ Runoff Reduction Practices

Creekside South at Lorson Ranch has employed several methods of reducing runoff.

- The street configuration was laid out to minimize the length of streets. Many streets are straight and perpendicular resulting in lots with less wasted space.
- A buffer tract added along the East Tributary which reduces impervious areas
- Larger 2.5-acre lots added on south side to reduce impervious area
- Lorson Ranch Metro District requires homeowners to maintain landscaping on lots
- Full Spectrum Detention Pond J and E2 will be constructed. The full spectrum detention mimics existing storm discharges

#### Step 2: Implement BMP's that Slowly Release the Water Quality Capture Volume

Treatment and slow release of the water quality capture volume (WQCV) is required. Creekside South at Lorson Ranch will utilize Pond J and E2 which are full spectrum stormwater detention ponds which includes Water Quality Volumes and WQ outlet structures.

#### Step 3: Stabilize Drainageways

East Tributary of Jimmy Camp Creek is a major drainageway located west of this site. In 2020 the East Tributary of JCC adjacent to this site will be reconstructed and stabilized per county criteria. The design included a low flow channel bottom and selectively armored sides.

#### Step 4: Implement Site Specific & Source Control BMP's

There are no potential sources of contaminants that could be introduced to the County's MS4. During construction source control will be provided with the proper installation of erosion control BMPs to limit erosion and transport of sediment. Area disturbed by construction will be seeded and mulched. Cut and fill slopes will be reseeded, and the slopes equal to or greater than three-to-one will be protected with erosion control fabric. Silt fences will be placed at the bottom of re-vegetated and rough graded slopes. Inlet protection will be used around proposed inlets. In addition, temporary sediment basins will be constructed so runoff will be treated prior to discharge. Construction BMPs in the form of vehicle tracking control, sediment basins, concrete washout area, rock socks, buffers, and silt fences will be utilized to protect receiving waters.

---

## **9.0 CONCLUSIONS**

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This drainage report has been prepared in accordance with the City of Colorado Springs/El Paso County Drainage Criteria Manual. The proposed development and drainage infrastructure will not cause adverse impacts to adjacent properties or properties located downstream. Several key aspects of the development discussed above are summarized as follows:

- Developed runoff will be conveyed via curb/gutter and storm sewer facilities
- The East Tributary of Jimmy Camp Creek will be reconstructed within this study area
- Detention and water quality for this preliminary plan area will be provided in two permanent ponds

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## **10.0 REFERENCES**

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1. City of Colorado Springs/El Paso County Drainage Criteria Manual DCM, dated November, 1991
2. Soil Survey of El Paso County Area, Colorado by USDA, SCS

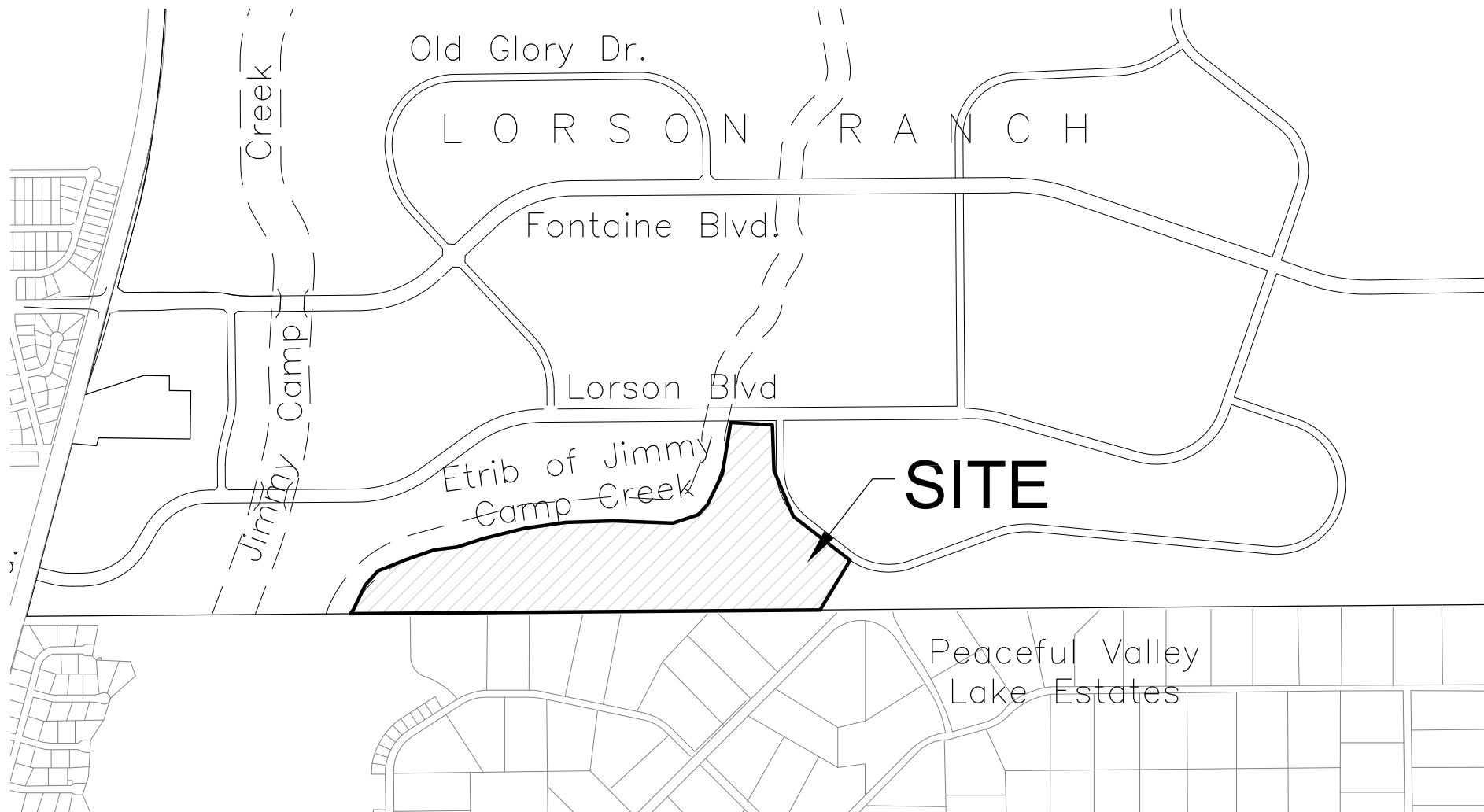
3. Jimmy Camp Creek Drainage Basin Planning Study, Dated March 9, 2015, by Kiowa Engineering Corporation
4. City of Colorado Springs "Drainage Criteria Manual, Volume 2
5. El Paso County "Engineering Criteria Manual"
6. Lorson Ranch East MDDP, June 30, 2017 by Core Engineering.
7. Final construction plans "East Fork Jimmy Camp Creek Channel Design", Dated April 1, 2020 by Kiowa Engineering Corporation
8. El Paso County Resolution #15-042, El Paso County adoption of Chapter 6 and Section 3.2.1 of the City of Colorado Springs Drainage Criteria Manual dated May, 2014.
9. Final Drainage Report for Lorson Ranch East Filing No. 4 by Core Engineering, approved September 12, 2019 (SF19-008)



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**APPENDIX A – VICINTIY MAP, SOILS MAP, FEMA MAP**

---



**VICINITY MAP**  
NO SCALE



**CORE**  
ENGINEERING GROUP

15004 1ST AVE. S.  
BURNSVILLE, MN 55306  
PH: 719.570.1100

CONTACT: RICHARD L. SCHINDLER, P.E.  
EMAIL: Rich@ceg1.com

**CREEKSIDE SOUTH AT LORSON RANCH  
VICINITY MAP**

SCALE:  
NTS

DATE:  
JANUARY, 2020

FIGURE NO.  
--

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST.

City of Colorado Springs  
080060

14

REVISED  
AREA

5733.0

5731.2

5730.9

5728.6

ZONE AE

5726.2

13

REVISED  
AREA

5719.6

5724.3

ZONE AE

5718.8

5718.8

5718.8

5718.8

5718.8

5718.2

42° 88' 00.00" N

FONTAINE BLVD

Bridge

5710.4

Jimmy Camp Creek -  
East Tributary

5709.2

5709.7

5709.5

5709.3

5709.2

LORSON BLVD

5705.2

5705.0

SITE

JOINS PANEL 0976

El Paso County  
Unincorporated Areas  
080059

ZONE AE

ZONE AE

5704.7

ZONE AE

5697.2

5698.8

5701.6

City of  
Fountain

080061

APPLE  
TREE PL

23

ROLLING RIDGE RD

HERITAGE RD

**SPECIAL FLOOD HAZARD AREAS**

- Without Base Flood Elevation (BFE)  
Zone A, V, AS9
- With BFE or Depth  
Zone AE, AD, AH, VE, AR
- Regulatory Floodway
- 0.2 % Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile  
Zone X
- Future Conditions 1% Annual Chance Flood Hazard  
Zone X
- Area with Reduced Flood Risk due to Levee  
See Notes, Zone X

**OTHER AREAS OF FLOOD HAZARD**

**SCALE**

Map Projection:  
Universal Transverse Mercator (NAD 1983 UTM Zone 13N)  
Western Hemisphere, Vertical Datum: NAVD 88

1 inch = 500 feet 1:6,000

0 250 500 1,000 Feet

0 62.5 125 250 Meters

**FEDERAL EMERGENCY MANAGEMENT AGENCY**

**National Flood Insurance Program**

**NATIONAL FLOOD INSURANCE PROGRAM**

**FLOOD INSURANCE RATE MAP**

**EL PASO COUNTY, COLORADO**  
and Incorporated Areas

PANEL 957 OF 1300

Panel Contains:

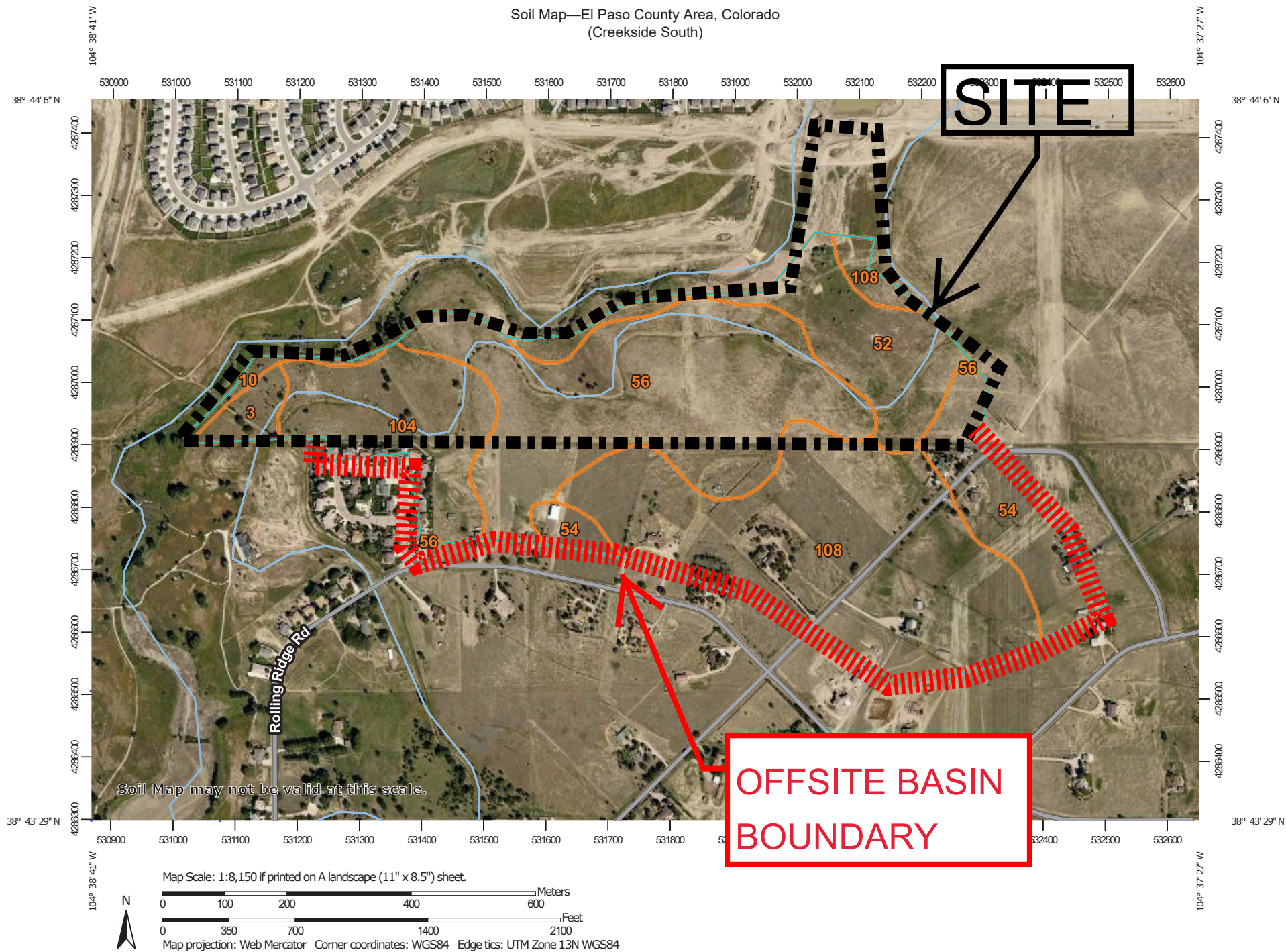
COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0957	G
EL PASO COUNTY	080059	0957	G
FOUNTAIN, CITY OF	080061	0957	G

REVISED TO REFLECT LOMR  
EFFECTIVE: May 4, 2020

VERSION NUMBER  
1.1.1.0  
MAP NUMBER  
08041C0957G  
MAP REVISED  
DECEMBER 7, 2018




Soil Map—El Paso County Area, Colorado  
(Creekside South)



Soil Map—El Paso County Area, Colorado  
(Creekside South)

## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)

### Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

### Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

### Water Features



Streams and Canals

### Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

### Background



Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 17, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 14, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
3	Ascalon sandy loam, 3 to 9 percent slopes	2.6	2.0%
10	Blendon sandy loam, 0 to 3 percent slopes	1.2	0.9%
52	Manzanst clay loam, 0 to 3 percent slopes	14.5	11.2%
54	Midway clay loam, 3 to 25 percent slopes	12.9	10.0%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	37.6	29.2%
104	Vona sandy loam, warm, 0 to 3 percent slopes	15.7	12.2%
108	Wiley silt loam, 3 to 9 percent slopes	44.5	34.5%
<b>Totals for Area of Interest</b>		<b>128.8</b>	<b>100.0%</b>

---

## APPENDIX B – HYDROLOGY CALCULATIONS

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Job No: 100.050  
Project: Creekside South at Lorson Ranch  
Design Storm: **100-Year Event (Current)**

P:\100\100.051\drainage\100.051 Flows-alt 1 of 1 1/21/2020



PROJECT NAME: Creekside South at Lorson Ranch  
PROJECT NUMBER: 100.051  
ENGINEER: LAB  
DATE: December 16, 2019

### CURRENT CONDITIONS COEFFICIENT "C" CALCULATIONS

P:\100\100.051\drainage\100.051 Flows-alt

**Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)**

 Calculated By: Leonard Beasley

Date: January 15, 2020

 Checked By: Leonard Beasley

Job No: 100.051

Project: Creekside South at Lorson Ranch

 Design Storm: **5 - Year Event (Proposed)**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	$t_c$	CA	i	Q	$t_c$	$\Sigma$ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	$t_t$	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
E7			0.60	0.49	10.1	0.29	4.12	1.2													
E8.1			4.00	0.30	16.6	1.20	3.37	4.0													
OS-E2.1			36.66	0.17	30.5	6.23	2.46	15.3													
E8.2			1.70	0.19	12.8	0.32	3.76	1.2													
OS-E2.1 - E8.2	<b>14</b>	38.36							31.4	6.56	2.41	15.8									
OS-E2.2			6.52	0.15	16.0	0.98	3.43	3.4													
E8.3			5.37	0.26	16.6	1.40	3.37	4.7													
OS-E2.2 - E8.3	<b>15</b>	11.89							27.2	2.37	2.63	6.2									
E8.1 & DP-15	<b>16</b>	15.89							27.2	3.57	2.63	9.4									
DP-14 thru DP-16		54.25							31.4	10.13	2.41	24.4									
E8.4			1.20	0.45	14.3	0.54	3.59	1.9													
E8.5			4.27	0.45	14.7	1.92	3.55	6.8													
E8.6			1.02	0.49	10.5	0.50	4.06	2.0													
E8.7			0.71	0.47	9.4	0.33	4.22	1.4													
E8.6 & E8.7	<b>18</b>	1.73							10.5	0.83	4.06	3.4									
E8.8			2.43	0.45	12.8	1.09	3.76	4.1													

**Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)**

 Calculated By: Leonard Beasley

Date: January 15, 2020

 Checked By: Leonard Beasley

Job No: 100.051

Project: Creekside South at Lorson Ranch

 Design Storm: **5 - Year Event (Proposed)**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	$t_c$	CA	i	Q	$t_c$	$\Sigma$ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	$t_t$	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
E8.4 - E8.8	<b>19</b>	9.63							16.1	4.39	3.42	15.0									
E8.1 - E8.8		63.88							32.2	14.52	2.38	34.5									
E8.9			1.52	0.45	14.5	0.68	3.57	2.4													
E8.10			0.38	0.47	5.2	0.18	5.12	0.9													
E8.9 - E8.10	<b>20</b>	1.90							14.5	0.86	3.57	3.1									
OS-E2.1 - E8.10		65.78							31.8	15.38	2.40	36.8									
E8.11			3.99	0.21	12.4	0.84	3.80	3.2													
E8		69.77							31.8	16.22	2.40	38.8									
OS-I1.1			15.54	0.15	23.1	2.33	2.87	6.7													
I1.2			6.23	0.27	16.0	1.68	3.43	5.8													
I1	<b>4</b>	21.77							25.0	4.01	2.76	11.1									
I2			1.12	0.45	12.7	0.50	3.77	1.9													
I3			1.01	0.45	12.5	0.45	3.79	1.7													
I4			3.45	0.45	14.2	1.55	3.61	5.6													
I2 - I4		5.58							15.4	2.51	3.48	8.7									
OS-I1.1-I4		27.35							25.2	6.52	2.74	17.9									

**Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)**

 Calculated By: Leonard Beasley

Date: January 15, 2020

 Checked By: Leonard Beasley

 Job No: 100.051

 Project: Creekside South at Lorson Ranch

 Design Storm: **5 - Year Event (Proposed)**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t <sub>c</sub>	CA	i	Q	t <sub>c</sub>	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t <sub>t</sub>	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
I5			1.44	0.45	10.3	0.65	4.09	2.7													
OS-I1.1-I5		28.79							25.7	7.17	2.71	19.5									
I6			1.18	0.45	12.6	0.53	3.78	2.0													
OS-I1.1-I6		29.97							26.6	7.70	2.66	20.5									
DP-2a & DP-8		35.30							28.6	10.10	2.55	25.8									
I7			2.01	0.45	19.4	0.90	3.13	2.8													
I7 & J5	<b>10</b>	3.94							19.4	1.77	3.13	5.6									
DP-9 & DP-10	<b>11</b>	39.24							28.6	11.87	2.55	30.3									
I8			2.44	0.21	13.7	0.51	3.66	1.9													
I	<b>12</b>	34.42							26.6	9.12	2.66	24.3									
OS-J1.1			11.55	0.19	28.1	2.19	2.58	5.7													
J1.2			2.01	0.17	12.8	0.34	3.76	1.3													
J1	<b>1</b>	13.56							29.4	2.54	2.51	6.4									
J2			0.36	0.62	6.0	0.22	4.90	1.1													
OS-J1.1 - J2	<b>2</b>	13.92							29.4	2.76	2.51	6.9									
J3			3.40	0.45	14.5	1.53	3.57	5.5													

Design Storm: **5 - Year Event (Proposed)**1/22/2020



**Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)**

Calculated By: Leonard Beasley

Date: January 15, 2020

Checked By: Leonard Beasley

Job No: 100.051

Project: Creekside South at Lorson Ranch

Design Storm: **100 - Year Event (Proposed)**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t <sub>c</sub>	CA	i	Q	t <sub>c</sub>	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t <sub>t</sub>	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
E7			0.60	0.65	10.1	0.39	6.91	2.7													
E8.1			4.00	0.57	16.6	2.28	5.66	12.9													
OS-E2.1			36.66	0.45	30.5	16.50	4.13	68.1													
E8.2			1.70	0.46	12.8	0.78	6.31	4.9													
OS-E2.1 - E8.2	14	38.36							31.4	17.28	4.05	70.0									
OS-E2.2			6.52	0.41	16.0	2.67	5.75	15.4													
E8.3			5.37	0.47	16.6	2.52	5.65	14.3													
OS-E2.2 - E8.3	15	11.89							27.2	5.20	4.42	22.9									
E8.1 & DP-15	16	15.89							27.2	7.48	4.42	33.0									
DP-14 thru DP-16		54.25							31.4	24.76	4.05	100.2									
E8.4			1.20	0.59	14.3	0.71	6.03	4.3													
E8.5			4.27	0.59	14.7	2.52	5.96	15.0													
E8.6			1.02	0.65	10.5	0.66	6.81	4.5													
E8.7			0.71	0.62	9.4	0.44	7.08	3.1													
E8.6 & E8.7	18	1.73							10.5	1.10	6.81	7.5									
E8.8			2.43	0.59	12.8	1.43	6.31	9.1													
E8.4 - E8.8	19	9.63							16.1	5.76	5.73	33.1									
E8.1 - E8.8		63.88							32.2	30.52	3.99	121.7									



# **Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)**

Calculated By: Leonard Beasley  
 Date: January 15, 2020  
 Checked By: Leonard Beasley

Job No: 100.051  
 Project: Creekside South at Lorson Ranch  
 Design Storm: **100 - Year Event (Proposed)**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t <sub>c</sub>	CA	i	Q	t <sub>c</sub>	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t <sub>t</sub>	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
E8.9			1.52	0.59	14.5	0.90	5.99	5.4													
E8.10			0.38	0.62	5.2	0.24	8.59	2.0													
E8.9 - E8.10	20	1.90							14.5	1.13	5.99	6.8									
OS-E2.1 - E8.10		65.78							31.8	31.65	4.02	127.2									
E8.11			3.99	0.48	12.4	1.92	6.38	12.2													
E8		69.77							34.1	33.57	3.84	129.0									
OS-I1.1			15.54	0.41	23.1	6.37	4.82	30.7													
I1.2			6.23	0.49	16.0	3.05	5.75	17.6													
I1	4	21.77							25.0	9.42	4.62	43.6									
I2			1.12	0.59	12.7	0.66	6.34	4.2													
I3			1.01	0.59	12.5	0.60	6.37	3.8													
I4			3.45	0.59	14.2	2.04	6.05	12.3													
I2 - I4		5.58							15.4	3.29	5.85	19.3									
OS-I1.1-I4		27.35							25.2	12.72	4.61	58.6									
I5			1.44	0.59	10.3	0.85	6.87	5.8													
OS-I1.1-I5		28.79							25.7	13.57	4.55	61.8									
I6			1.18	0.59	12.6	0.70	6.35	4.4													
OS-I1.1-I6		29.97							26.6	14.26	4.47	63.7									
DP-2a & DP-8		35.30							28.6	23.83	4.29	102.2									





**Standard Form SF-2. Storm Drainage System Design (Rational Method Procedure)**

Calculated By: Leonard Beasley

Date: January 15, 2020

Checked By: Leonard Beasley

Job No: 100.051

Project: Creekside South at Lorson Ranch

Design Storm: **100 - Year Event (Proposed)**

Street or Basin	Design Point	Direct Runoff							Total Runoff				Street		Pipe			Travel Time			Remarks
		Area Design	Area (A)	Runoff Coeff. (C)	t <sub>c</sub>	CA	i	Q	t <sub>c</sub>	Σ (CA)	i	Q	Slope	Street Flow	Design Flow	Slope	Pipe Size	Length	Velocity	t <sub>t</sub>	
			ac.		min.		in/hr	cfs	min		in/hr	cfs	%	cfs	cfs	%	in	ft	ft/sec	min	
I7			2.01	0.59	19.4	1.19	5.26	6.2													
I7 & J5		3.94							19.4	2.32	5.26	12.2									
DP-9 & DP-10		39.24							28.6	26.16	4.29	112.1									
I8			2.44	0.44	13.7	1.07	6.14	6.6													
I		34.42							26.6	16.52	4.47	73.8									
OS-J1.1			11.55	0.46	28.1	5.31	4.33	23.0													
J1.2			2.01	0.42	12.8	0.84	6.32	5.3													
J1	1	13.56							29.4	6.16	4.22	26.0									
J2			0.36	0.75	6.0	0.27	8.23	2.2													
OS-J1.1 - J2	2	13.92							29.4	6.43	4.22	27.1									
J3			3.40	0.59	14.5	2.01	5.99	12.0													
J4			1.93	0.59	11.8	1.14	6.52	7.4													
J3-J4		5.33							14.5	3.14	6.00	18.9									
J5			1.93	0.59	14.1	1.14	6.08	6.9													
J		21.18							28.6	10.71	4.29	45.9									
I & J		55.60							28.6	27.23	4.29	116.7									
K1			2.65	0.39	12.5	1.03	6.37	6.6													
K2			2.14	0.39	6.2	0.83	8.13	6.8													



Calculated By: Leonard Beasley  
Date: January 15, 2020  
Checked By: Leonard Beasley

Job No: 100.051  
Project: Creekside South at Lorson Ranch  
Design Storm: **100 - Year Event (Proposed)**

[illegible]

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## APPENDIX C – HYDRAULIC CALCULATIONS

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# Channel Report

Hydraflow Express by Intelisolve

Monday, May 11 2020, 11:38 AM

## DES.PT. 1 SWALE

### Trapezoidal

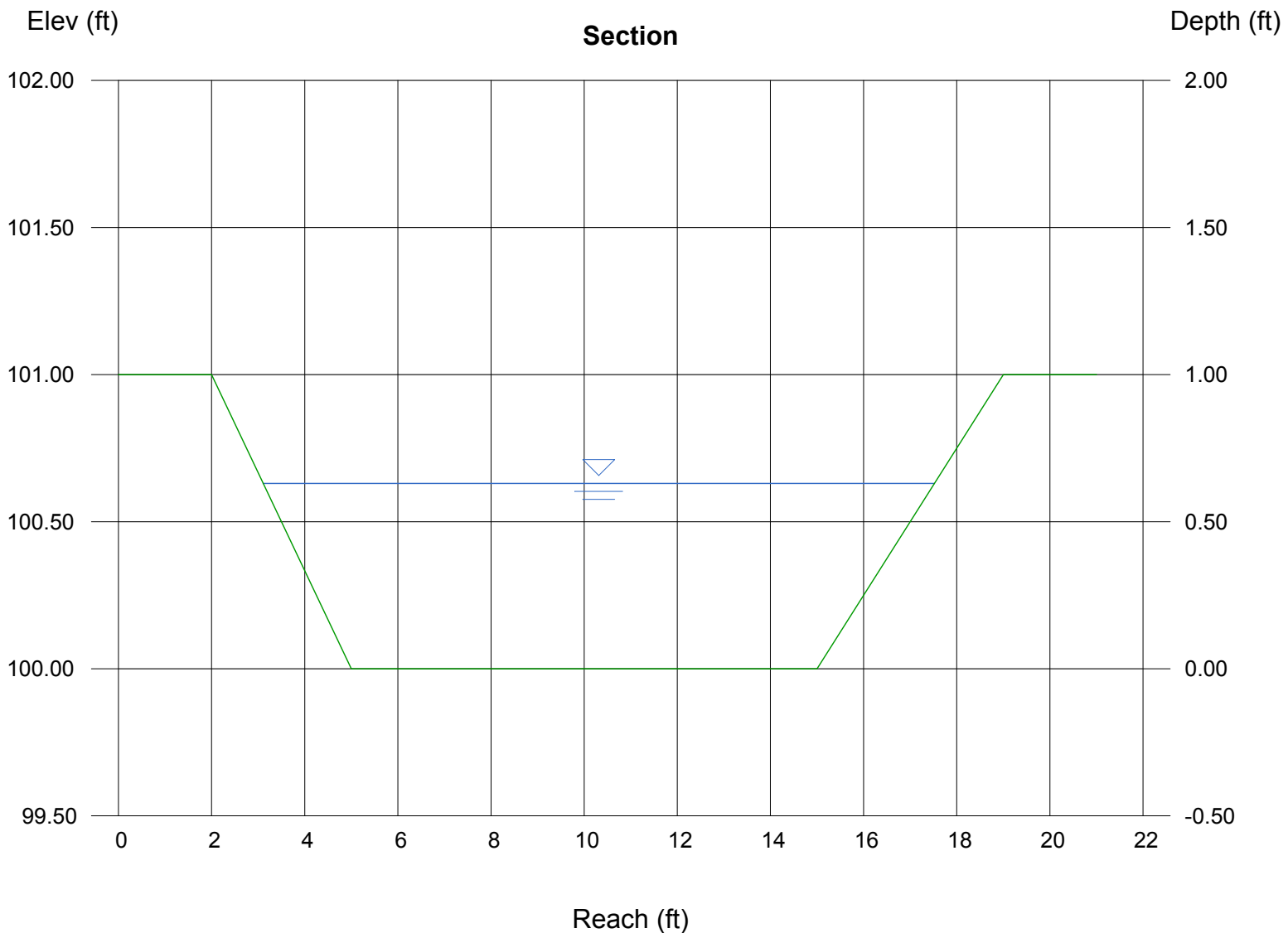
Bottom Width (ft) = 10.00  
Side Slope (z:1) = 3.00  
Total Depth (ft) = 1.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.50  
N-Value = 0.020

### Calculations

Compute by: Known Q  
Known Q (cfs) = 26.00

### Highlighted

Depth (ft) = 0.63  
Q (cfs) = 26.00  
Area (sqft) = 7.69  
Velocity (ft/s) = 3.38  
Wetted Perim (ft) = 14.59  
Crit Depth,  $Y_c$  (ft) = 0.56  
Top Width (ft) = 14.41  
EGL (ft) = 0.81



# Culvert Report

Hydraflow Express by Intelisolve

Tuesday, Jan 7 2020, 1:39 PM

## End Section Des. Pt. 1

Invert Elev Dn (ft) = 100.00  
Pipe Length (ft) = 23.00  
Slope (%) = 1.00  
Invert Elev Up (ft) = 100.23  
Rise (in) = 24.0  
Shape = Cir  
Span (in) = 24.0  
No. Barrels = 1  
n-Value = 0.013  
Inlet Edge = Projecting  
Coeff. K,M,c,Y,k = 0.0045, 2, 0.0317, 0.69, 0.5

### Embankment

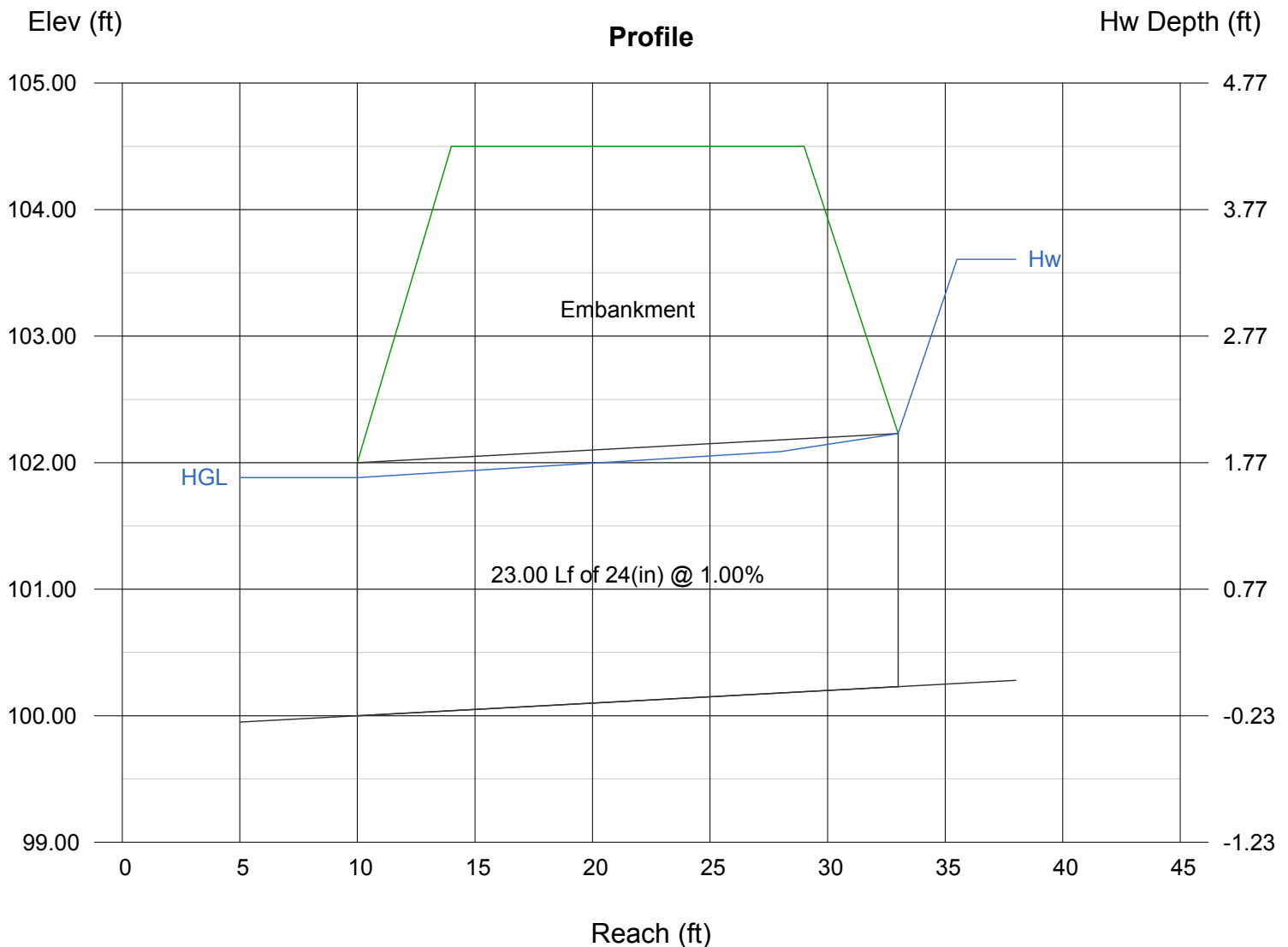
Top Elevation (ft) = 104.50  
Top Width (ft) = 15.00  
Crest Width (ft) = 100.00

### Calculations

Qmin (cfs) = 0.00  
Qmax (cfs) = 30.00  
Tailwater Elev (ft) = (dc+D)/2

### Highlighted

Qtotal (cfs) = 25.00  
Qpipe (cfs) = 25.00  
Qovertop (cfs) = 0.00  
Veloc Dn (ft/s) = 9.65  
Veloc Up (ft/s) = 9.55  
HGL Dn (ft) = 101.88  
HGL Up (ft) = 102.14  
Hw Elev (ft) = 103.61  
Hw/D (ft) = 1.69  
Flow Regime = Inlet Control



# Culvert Report

Hydraflow Express by Intelisolve

Wednesday, Jan 22 2020, 4:59 PM

## 36inch end section -Horton-Shunka

Invert Elev Dn (ft) = 99.58  
Pipe Length (ft) = 50.00  
Slope (%) = 0.84  
Invert Elev Up (ft) = 100.00  
Rise (in) = 36.0  
Shape = Cir  
Span (in) = 36.0  
No. Barrels = 1  
n-Value = 0.013  
Inlet Edge = Projecting  
Coeff. K,M,c,Y,k = 0.0045, 2, 0.0317, 0.69, 0.5

### Embankment

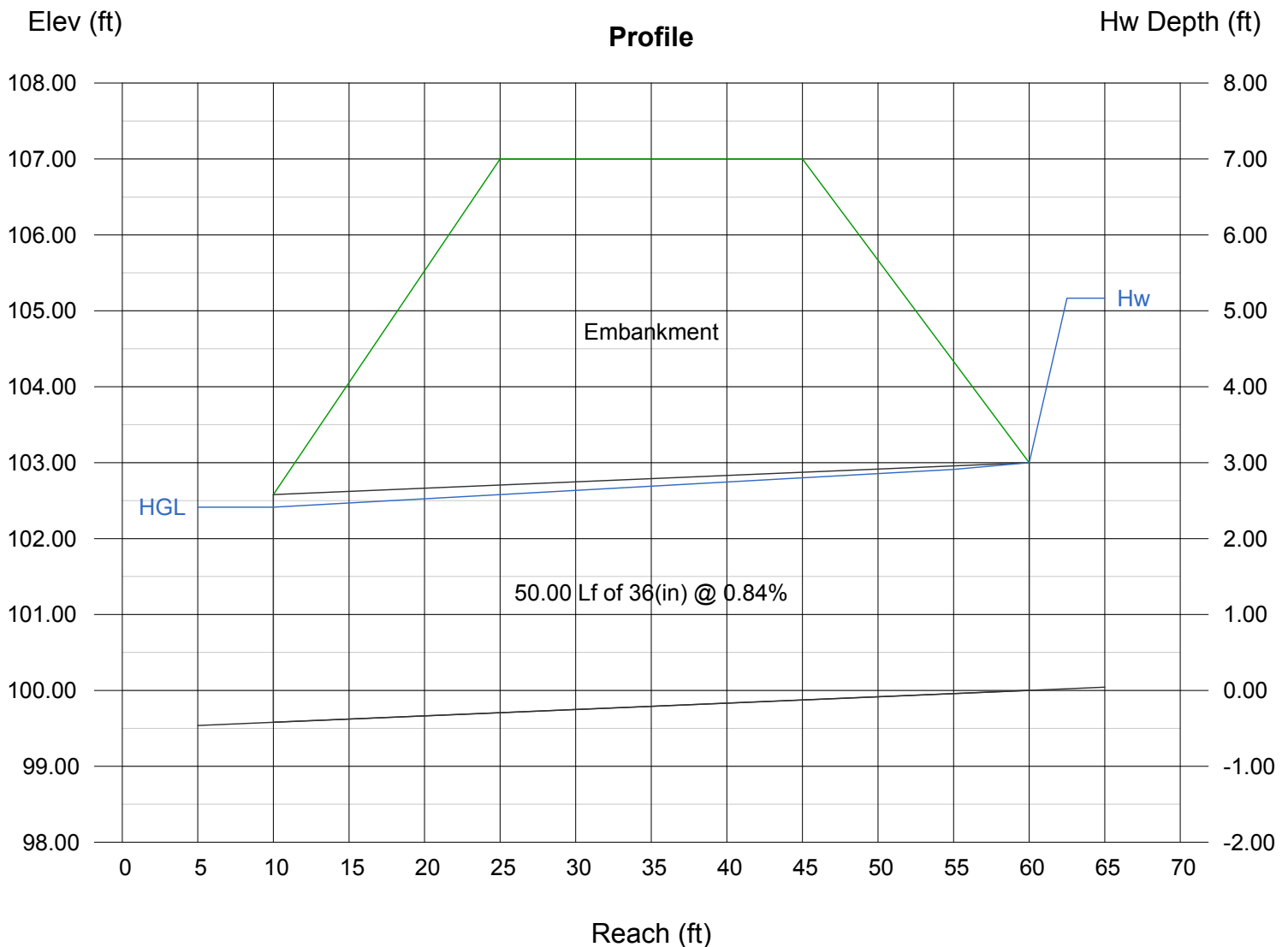
Top Elevation (ft) = 107.00  
Top Width (ft) = 20.00  
Crest Width (ft) = 100.00

### Calculations

Qmin (cfs) = 70.00  
Qmax (cfs) = 70.00  
Tailwater Elev (ft) = (dc+D)/2

### Highlighted

Qtotal (cfs) = 70.00  
Qpipe (cfs) = 70.00  
Qovertop (cfs) = 0.00  
Veloc Dn (ft/s) = 10.13  
Veloc Up (ft/s) = 9.92  
HGL Dn (ft) = 102.41  
HGL Up (ft) = 102.97  
Hw Elev (ft) = 105.17  
Hw/D (ft) = 1.72  
Flow Regime = Inlet Control



# Channel Report

Hydraflow Express by Intelisolve

Friday, Jan 10 2020, 2:46 PM

## pond J outflow channel

### Trapezoidal

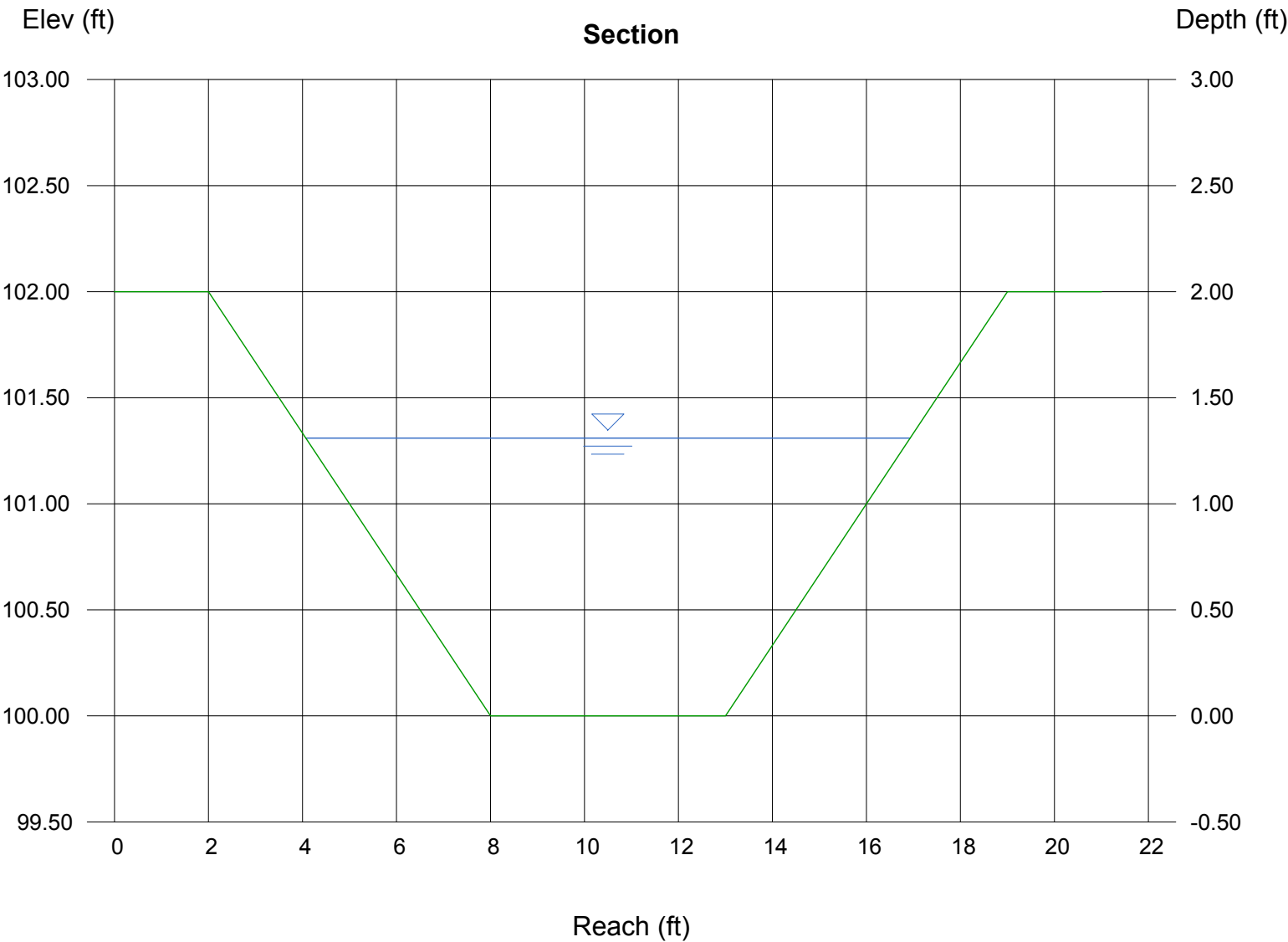
Bottom Width (ft) = 5.00  
Side Slope (z:1) = 3.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.50  
N-Value = 0.020

### Calculations

Compute by: Known Q  
Known Q (cfs) = 56.00

### Highlighted

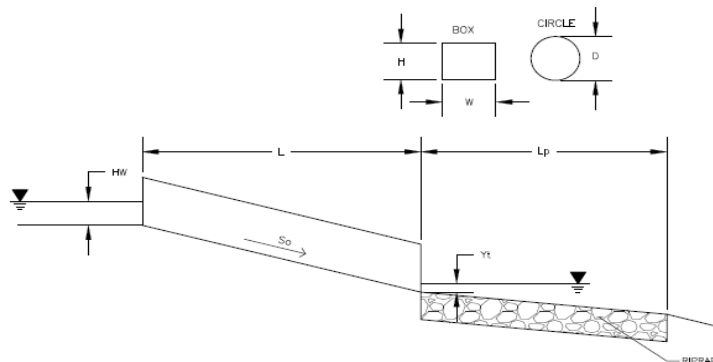
Depth (ft) = 1.31  
Q (cfs) = 56.00  
Area (sqft) = 11.70  
Velocity (ft/s) = 4.79  
Wetted Perim (ft) = 13.29  
Crit Depth, Yc (ft) = 1.23  
Top Width (ft) = 12.86  
EGL (ft) = 1.67



## Determination of Culvert Headwater and Outlet Protection

Project: **Creekside South**

Basin ID: **Rip Rap sizing for outlet pipe from Pond J to Etrib**



### Design Information (Input):

Design Discharge	Q = 55.5 cfs
<b>Circular Culvert:</b>	
Barrel Diameter in Inches	D = 36 inches
Inlet Edge Type (Choose from pull-down list)	Square End Projection
<b>Box Culvert:</b>	
Barrel Height (Rise) in Feet	Height (Rise) =
Barrel Width (Span) in Feet	Width (Span) =
Inlet Edge Type (Choose from pull-down list)	
Number of Barrels	No = 1
Inlet Elevation	Elev IN = 100 ft
Outlet Elevation <b>OR</b> Slope	Elev OUT = 99.75 ft
Culvert Length	L = 50 ft
Manning's Roughness	n = 0.013
Bend Loss Coefficient	$k_b$ = 0
Exit Loss Coefficient	$k_x$ = 1
Tailwater Surface Elevation	Elev $Y_t$ = 101 ft
Max Allowable Channel Velocity	V = 5 ft/s

### Required Protection (Output):

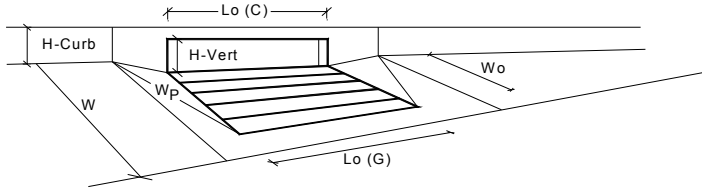
Tailwater Surface Height	$Y_t$ = 1.25 ft
Flow Area at Max Channel Velocity	$A_t$ = 11.10 ft <sup>2</sup>
Culvert Cross Sectional Area Available	A = 7.07 ft <sup>2</sup>
Entrance Loss Coefficient	$k_e$ = 0.50
Friction Loss Coefficient	$k_f$ = 0.36
Sum of All Losses Coefficients	$k_s$ = 1.86
Culvert Normal Depth	$Y_n$ = 2.11 ft
Culvert Critical Depth	$Y_c$ = 2.42 ft
Tailwater Depth for Design	d = 2.71 ft
Adjusted Diameter <b>OR</b> Adjusted Rise	$D_a$ = - ft
Expansion Factor	$1/(2 \cdot \tan(\theta))$ = 4.16
Flow/Diameter <sup>2.5</sup> <b>OR</b> Flow/(Span * Rise <sup>1.5</sup> )	$Q/D^{2.5}$ = 3.56 ft <sup>0.5</sup> /s
Froude Number	Fr = -
Tailwater/Adjusted Diameter <b>OR</b> Tailwater/Adjusted Rise	$Y_t/D$ = 0.42
Inlet Control Headwater	$HW_i$ = 4.51 ft
Outlet Control Headwater	$HW_o$ = 4.24 ft
<b>Design Headwater Elevation</b>	<b>HW</b> = 104.51 ft
<b>Headwater/Diameter <b>OR</b> Headwater/Rise Ratio</b>	<b>HW/D</b> = 1.50 <b>HW/D &gt; 1.5!</b>
Minimum Theoretical Riprap Size	$d_{50}$ = 8 in
Nominal Riprap Size	$d_{50}$ = 9 in
<b>UDFCD Riprap Type</b>	<b>Type</b> = L
<b>Length of Protection</b>	$L_p$ = 25 ft
<b>Width of Protection</b>	T = 10 ft



# INLET E8.1

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017

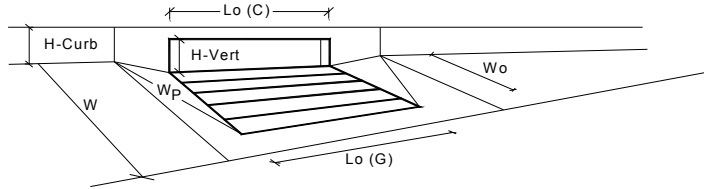


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	5.4	6.5	inches
<b>Grate Information</b>			MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C <sub>r</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C <sub>o</sub> (G) =	N/A	N/A	
<b>Curb Opening Information</b>			MINOR	MAJOR	
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	25.00	25.00	feet
Height of Vertical Curb Opening in Inches		H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C <sub>r</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C <sub>o</sub> (C) =	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>			MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d <sub>Curb</sub> =	0.29	0.38	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF <sub>Combination</sub> =	0.51	0.61	
Curb Opening Performance Reduction Factor for Long Inlets		RF <sub>Curb</sub> =	0.75	0.82	
Grated Inlet Performance Reduction Factor for Long Inlets		RF <sub>Grate</sub> =	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			MINOR	MAJOR	
		Q <sub>a</sub> =	11.5	18.9	cfs
<b>WARNING: Inlet Capacity less than Q Peak for Major Storm</b>		Q <sub>PEAK REQUIRED</sub> =	9.4	33.0	cfs

# INLET E8.5

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017

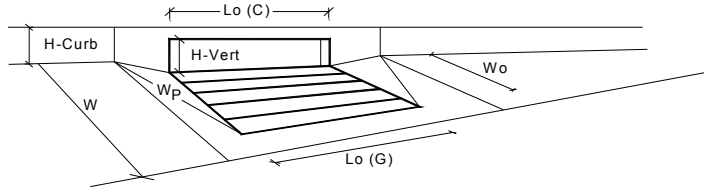


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	6.0	8.0	inches
<b>Grate Information</b>			MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C <sub>r</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C <sub>o</sub> (G) =	N/A	N/A	
<b>Curb Opening Information</b>			MINOR	MAJOR	
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	25.00	25.00	feet
Height of Vertical Curb Opening in Inches		H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C <sub>r</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C <sub>o</sub> (C) =	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>			MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d <sub>Curb</sub> =	0.33	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF <sub>Combination</sub> =	0.57	0.76	
Curb Opening Performance Reduction Factor for Long Inlets		RF <sub>Curb</sub> =	0.79	0.89	
Grated Inlet Performance Reduction Factor for Long Inlets		RF <sub>Grate</sub> =	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			MINOR	MAJOR	
		Q <sub>a</sub> =	15.2	32.0	cfs
<b>WARNING: Inlet Capacity less than Q Peak for Major Storm</b>		Q <sub>PEAK REQUIRED</sub> =	15.0	33.1	cfs

# INLET E8.9

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017

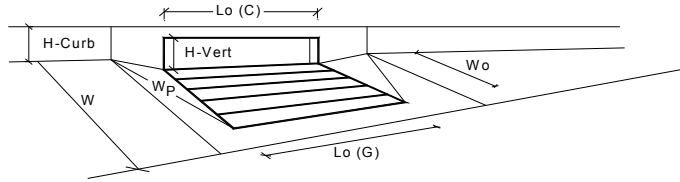


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	2	2	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	4.2	7.2	inches
<b>Grate Information</b>			MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C <sub>r</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C <sub>o</sub> (G) =	N/A	N/A	
<b>Curb Opening Information</b>			MINOR	MAJOR	
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches		H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C <sub>r</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C <sub>o</sub> (C) =	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>			MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d <sub>Curb</sub> =	0.18	0.43	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF <sub>Combination</sub> =	0.39	0.68	
Curb Opening Performance Reduction Factor for Long Inlets		RF <sub>Curb</sub> =	0.65	0.85	
Grated Inlet Performance Reduction Factor for Long Inlets		RF <sub>Grate</sub> =	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			MINOR	MAJOR	
		Q <sub>a</sub> =	4.7	23.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)		Q <sub>PEAK REQUIRED</sub> =	3.1	22.0	cfs

# INLET I1

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017

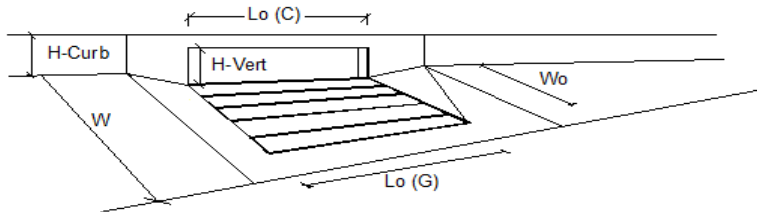


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	6.0	6.5	inches
<b>Grate Information</b>		MINOR		MAJOR	
Length of a Unit Grate		L <sub>g</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>g</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C <sub>g</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C <sub>o</sub> (G) =	N/A	N/A	
<b>Curb Opening Information</b>		MINOR		MAJOR	
Length of a Unit Curb Opening		L <sub>g</sub> (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches		H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C <sub>r</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C <sub>o</sub> (C) =	0.67	0.67	
<b>Grate Flow Analysis (Calculated)</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple Units		Coef =	N/A	N/A	
Clogging Factor for Multiple Units		Clog =	N/A	N/A	
<b>Grate Capacity as a Weir (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>all</sub> =	N/A	N/A	cfs
Interception with Clogging		Q <sub>we</sub> =	N/A	N/A	cfs
<b>Grate Capacity as an Orifice (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>or</sub> =	N/A	N/A	cfs
Interception with Clogging		Q <sub>or</sub> =	N/A	N/A	cfs
<b>Grate Capacity as Mixed Flow</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>mi</sub> =	N/A	N/A	cfs
Interception with Clogging		Q <sub>mi</sub> =	N/A	N/A	cfs
<b>Resulting Grate Capacity (assumes clogged condition)</b>		MINOR		MAJOR	
		Q <sub>Grate</sub> =	N/A	N/A	cfs
<b>Curb Opening Flow Analysis (Calculated)</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple Units		Coef =	1.33	1.33	
Clogging Factor for Multiple Units		Clog =	0.03	0.03	
<b>Curb Opening as a Weir (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>all</sub> =	12.9	16.0	cfs
Interception with Clogging		Q <sub>we</sub> =	12.5	15.5	cfs
<b>Curb Opening as an Orifice (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>or</sub> =	39.0	40.5	cfs
Interception with Clogging		Q <sub>or</sub> =	37.7	39.2	cfs
<b>Curb Opening Capacity as Mixed Flow</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>mi</sub> =	20.9	23.7	cfs
Interception with Clogging		Q <sub>mi</sub> =	20.2	22.9	cfs
<b>Resulting Curb Opening Capacity (assumes clogged condition)</b>		MINOR		MAJOR	
		Q <sub>Curb</sub> =	12.5	15.5	cfs
<b>Resultant Street Conditions</b>		MINOR		MAJOR	
Total Inlet Length		L =	20.00	20.00	feet
Resultant Street Flow Spread (based on street geometry from above)		T =	18.7	20.8	ft. > T-Crown
Resultant Flow Depth at Street Crown		d <sub>CROWN</sub> =	0.4	0.9	inches
<b>Low Head Performance Reduction (Calculated)</b>		MINOR		MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d <sub>Curb</sub> =	0.33	0.38	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF <sub>Combination</sub> =	0.57	0.61	
Curb Opening Performance Reduction Factor for Long Inlets		RF <sub>Curb</sub> =	0.79	0.82	
Grated Inlet Performance Reduction Factor for Long Inlets		RF <sub>Grate</sub> =	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>		MINOR		MAJOR	
		Q <sub>s</sub> =	12.5	15.5	cfs
<b>WARNING: Inlet Capacity less than Q Peak for Major Storm</b>		MINOR		MAJOR	
		Q <sub>PEAK REQUIRED</sub> =	11.1	43.4	cfs

# INLET I2

## INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

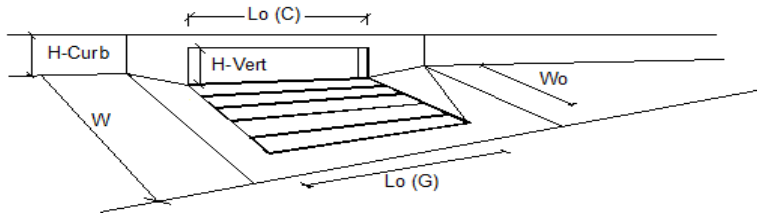


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>T-G</sub> =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C <sub>T-C</sub> =	0.10	0.10	
<b>Street Hydraulics: WARNING: Q &gt; ALLOWABLE Q FOR MAJOR STORM</b>					
<b>Design Discharge for Half of Street (from Sheet Inlet Management)</b>		MINOR		MAJOR	
Water Spread Width		Q <sub>o</sub> =	8.7	47.4	cfs
Water Depth at Flowline (outside of local depression)		T =	16.7	17.0	ft
Water Depth at Street Crown (or at T <sub>MAX</sub> )		d =	5.5	9.4	inches
Ratio of Gutter Flow to Design Flow		d <sub>CROWN</sub> =	0.0	3.8	inches
Discharge outside the Gutter Section W, carried in Section T <sub>x</sub>		E <sub>o</sub> =	0.358	0.205	
Discharge within the Gutter Section W		Q <sub>s</sub> =	5.6	33.6	cfs
Discharge Behind the Curb Face		Q <sub>w</sub> =	3.1	8.7	cfs
Flow Area within the Gutter Section W		Q <sub>BACK</sub> =	0.0	5.1	cfs
Velocity within the Gutter Section W		A <sub>w</sub> =	0.75	1.40	sq ft
Water Depth for Design Condition		V <sub>w</sub> =	4.1	6.2	fps
		d <sub>LOCAL</sub> =	8.5	12.4	inches
<b>Grate Analysis (Calculated)</b>		MINOR		MAJOR	
Total Length of Inlet Grate Opening		L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow		E <sub>o-GRATE</sub> =	N/A	N/A	
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Interception Capacity		Q <sub>i</sub> =	N/A	N/A	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet		GrateCoef =	N/A	N/A	
Clogging Factor for Multiple-unit Grate Inlet		GrateClog =	N/A	N/A	
Effective (unclogged) Length of Multiple-unit Grate Inlet		L <sub>e</sub> =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Actual Interception Capacity		Q <sub>s</sub> =	N/A	N/A	cfs
Carry-Over Flow = Q <sub>o</sub> - Q <sub>s</sub> (to be applied to curb opening or next d/s inlet)		Q <sub>b</sub> =	N/A	N/A	cfs
<b>Curb or Slotted Inlet Opening Analysis (Calculated)</b>		MINOR		MAJOR	
Equivalent Slope S <sub>e</sub> (based on grate carry-over)		S <sub>e</sub> =	0.087	0.059	ft/ft
Required Length L <sub>T</sub> to Have 100% Interception		L <sub>T</sub> =	17.33	46.62	ft
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L <sub>T</sub> )		L =	5.00	5.00	ft
Interception Capacity		Q <sub>i</sub> =	4.0	7.8	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient		CurbCoef =	1.00	1.00	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet		CurbClog =	0.10	0.10	
Effective (Unclogged) Length		L <sub>e</sub> =	4.50	4.50	ft
Actual Interception Capacity		Q <sub>s</sub> =	3.6	7.1	cfs
Carry-Over Flow = Q <sub>b(Grate)</sub> - Q <sub>s</sub>		Q <sub>b</sub> =	5.1	40.3	cfs
<b>Summary</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	3.6	7.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q <sub>b</sub> =	5.1	40.3	cfs
Capture Percentage = Q <sub>s</sub> /Q <sub>o</sub> =		C% =	42	15	%

# INLET I5

## INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

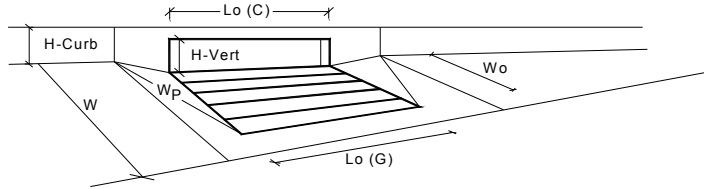


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>T-G</sub> =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C <sub>T-C</sub> =	0.10	0.10	
<b>Street Hydraulics: WARNING: Q &gt; ALLOWABLE Q FOR MAJOR STORM</b>					
<b>Design Discharge for Half of Street (from Sheet Inlet Management)</b>		MINOR		MAJOR	
Water Spread Width		Q <sub>o</sub> =	7.8	46.1	cfs
Water Depth at Flowline (outside of local depression)		T =	16.0	17.0	ft
Water Depth at Street Crown (or at T <sub>MAX</sub> )		d =	5.3	9.3	inches
Ratio of Gutter Flow to Design Flow		d <sub>CROWN</sub> =	0.0	3.7	inches
Discharge outside the Gutter Section W, carried in Section T <sub>x</sub>		E <sub>o</sub> =	0.374	0.206	
Discharge within the Gutter Section W		Q <sub>s</sub> =	4.9	32.8	cfs
Discharge Behind the Curb Face		Q <sub>w</sub> =	2.9	8.5	cfs
Flow Area within the Gutter Section W		Q <sub>BACK</sub> =	0.0	4.8	cfs
Velocity within the Gutter Section W		A <sub>w</sub> =	0.72	1.38	sq ft
Water Depth for Design Condition		V <sub>w</sub> =	4.0	6.2	fps
		d <sub>LOCAL</sub> =	8.3	12.3	inches
<b>Grate Analysis (Calculated)</b>		MINOR		MAJOR	
Total Length of Inlet Grate Opening		L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow		E <sub>o-GRATE</sub> =	N/A	N/A	
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Interception Capacity		Q <sub>i</sub> =	N/A	N/A	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet		GrateCoef =	N/A	N/A	
Clogging Factor for Multiple-unit Grate Inlet		GrateClog =	N/A	N/A	
Effective (unclogged) Length of Multiple-unit Grate Inlet		L <sub>e</sub> =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Actual Interception Capacity		Q <sub>s</sub> =	N/A	N/A	cfs
Carry-Over Flow = Q <sub>o</sub> - Q <sub>s</sub> (to be applied to curb opening or next d/s inlet)		Q <sub>b</sub> =	N/A	N/A	cfs
<b>Curb or Slotted Inlet Opening Analysis (Calculated)</b>		MINOR		MAJOR	
Equivalent Slope S <sub>e</sub> (based on grate carry-over)		S <sub>e</sub> =	0.090	0.059	ft/ft
Required Length L <sub>T</sub> to Have 100% Interception		L <sub>T</sub> =	16.13	45.96	ft
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L <sub>T</sub> )		L =	5.00	5.00	ft
Interception Capacity		Q <sub>i</sub> =	3.8	7.7	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient		CurbCoef =	1.00	1.00	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet		CurbClog =	0.10	0.10	
Effective (Unclogged) Length		L <sub>e</sub> =	4.50	4.50	ft
Actual Interception Capacity		Q <sub>s</sub> =	3.5	7.0	cfs
Carry-Over Flow = Q <sub>b(GRATE)</sub> - Q <sub>s</sub>		Q <sub>b</sub> =	4.3	39.1	cfs
<b>Summary</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	3.5	7.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q <sub>b</sub> =	4.3	39.1	cfs
Capture Percentage = Q <sub>s</sub> /Q <sub>o</sub> =		C% =	44	15	%

# INLET I6

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



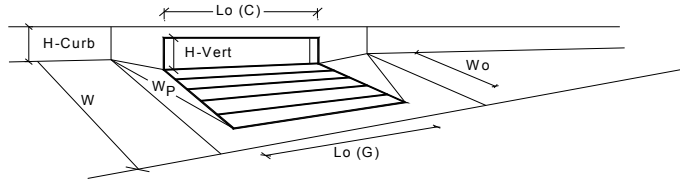
Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	6.0	7.8	inches
<b>Grate Information</b>			MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C <sub>r</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C <sub>o</sub> (G) =	N/A	N/A	
<b>Curb Opening Information</b>			MINOR	MAJOR	
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches		H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C <sub>r</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C <sub>o</sub> (C) =	0.67	0.67	
<b>Low Head Performance Reduction (Calculated)</b>			MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d <sub>Curb</sub> =	0.33	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF <sub>Combination</sub> =	0.57	0.74	
Curb Opening Performance Reduction Factor for Long Inlets		RF <sub>Curb</sub> =	0.93	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets		RF <sub>Grate</sub> =	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			MINOR	MAJOR	
		Q <sub>a</sub> =	8.3	15.5	cfs
		Q <sub>PEAK REQUIRED</sub> =	8.3	38.1	cfs

**WARNING: Inlet Capacity less than Q Peak for Minor and Major Storms**

# INLET I7

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



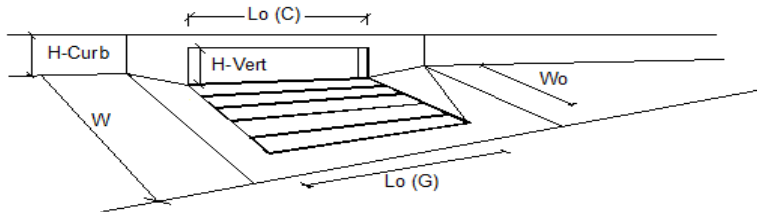
Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	4.6	7.8	inches
<b>Grate Information</b>		MINOR		MAJOR	
Length of a Unit Grate		L <sub>g</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate		W <sub>g</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C <sub>l</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C <sub>o</sub> (G) =	N/A	N/A	
<b>Curb Opening Information</b>		MINOR		MAJOR	
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	45.00	45.00	feet
Height of Vertical Curb Opening in Inches		H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C <sub>l</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C <sub>o</sub> (C) =	0.67	0.67	
<b>Grate Flow Analysis (Calculated)</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple Units		Coef =	N/A	N/A	
Clogging Factor for Multiple Units		Clog =	N/A	N/A	
<b>Grate Capacity as a Weir (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>all</sub> =	N/A	N/A	cfs
Interception with Clogging		Q <sub>we</sub> =	N/A	N/A	cfs
<b>Grate Capacity as an Orifice (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>or</sub> =	N/A	N/A	cfs
Interception with Clogging		Q <sub>or</sub> =	N/A	N/A	cfs
<b>Grate Capacity as Mixed Flow</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>mi</sub> =	N/A	N/A	cfs
Interception with Clogging		Q <sub>mi</sub> =	N/A	N/A	cfs
<b>Resulting Grate Capacity (assumes clogged condition)</b>		MINOR		MAJOR	
		Q <sub>Grate</sub> =	N/A	N/A	cfs
<b>Curb Opening Flow Analysis (Calculated)</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple Units		Coef =	1.33	1.33	
Clogging Factor for Multiple Units		Clog =	0.01	0.01	
<b>Curb Opening as a Weir (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>all</sub> =	11.8	52.1	cfs
Interception with Clogging		Q <sub>we</sub> =	11.6	51.3	cfs
<b>Curb Opening as an Orifice (based on Modified HEC22 Method)</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>or</sub> =	77.0	99.5	cfs
Interception with Clogging		Q <sub>or</sub> =	75.9	98.0	cfs
<b>Curb Opening Capacity as Mixed Flow</b>		MINOR		MAJOR	
Interception without Clogging		Q <sub>mi</sub> =	28.0	66.9	cfs
Interception with Clogging		Q <sub>mi</sub> =	27.6	65.9	cfs
<b>Resulting Curb Opening Capacity (assumes clogged condition)</b>		MINOR		MAJOR	
		Q <sub>Curb</sub> =	11.6	51.3	cfs
<b>Resultant Street Conditions</b>		MINOR		MAJOR	
Total Inlet Length		L =	45.00	45.00	feet
Resultant Street Flow Spread (based on street geometry from above)		T =	12.7	26.2	ft. > T-Crown
Resultant Flow Depth at Street Crown		d <sub>CROWN</sub> =	0.0	2.2	inches
<b>Low Head Performance Reduction (Calculated)</b>		MINOR		MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d <sub>Curb</sub> =	0.21	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF <sub>Combination</sub> =	0.43	0.74	
Curb Opening Performance Reduction Factor for Long Inlets		RF <sub>Curb</sub> =	0.68	0.88	
Grated Inlet Performance Reduction Factor for Long Inlets		RF <sub>Grate</sub> =	N/A	N/A	
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>		MINOR		MAJOR	
		Q <sub>s</sub> =	11.6	51.3	cfs
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		MINOR		MAJOR	
		Q <sub>PEAK REQUIRED</sub> =	5.0	50.7	cfs



# INLET J2

## INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

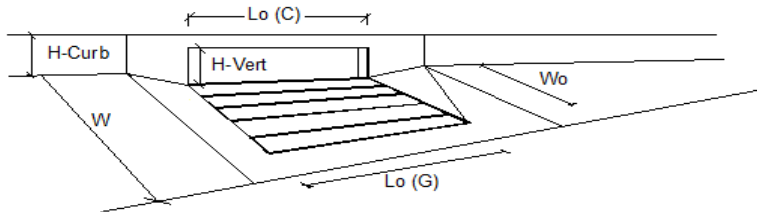


Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>T-G</sub> =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C <sub>T-C</sub> =	0.10	0.10	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>					
<b>Design Discharge for Half of Street (from Sheet Inlet Management)</b>		MINOR		MAJOR	
Water Spread Width		Q <sub>o</sub> =	1.1	2.2	cfs
Water Depth at Flowline (outside of local depression)		T =	5.0	7.5	ft
Water Depth at Street Crown (or at T <sub>MAX</sub> )		d =	2.7	3.3	inches
Ratio of Gutter Flow to Design Flow		d <sub>CROWN</sub> =	0.0	0.0	inches
Discharge outside the Gutter Section W, carried in Section T <sub>x</sub>		E <sub>o</sub> =	0.893	0.722	
Discharge within the Gutter Section W		Q <sub>s</sub> =	0.1	0.6	cfs
Discharge Behind the Curb Face		Q <sub>w</sub> =	1.0	1.6	cfs
Flow Area within the Gutter Section W		Q <sub>BACK</sub> =	0.0	0.0	cfs
Velocity within the Gutter Section W		A <sub>w</sub> =	0.28	0.39	sq ft
Water Depth for Design Condition		V <sub>w</sub> =	3.5	4.1	fps
		d <sub>LOCAL</sub> =	5.7	6.3	inches
<b>Grate Analysis (Calculated)</b>		MINOR		MAJOR	
Total Length of Inlet Grate Opening		L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow		E <sub>o-GRATE</sub> =	N/A	N/A	
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Interception Capacity		Q <sub>i</sub> =	N/A	N/A	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet		GrateCoef =	N/A	N/A	
Clogging Factor for Multiple-unit Grate Inlet		GrateClog =	N/A	N/A	
Effective (unclogged) Length of Multiple-unit Grate Inlet		L <sub>e</sub> =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Actual Interception Capacity		Q <sub>s</sub> =	N/A	N/A	cfs
Carry-Over Flow = Q <sub>o</sub> - Q <sub>s</sub> (to be applied to curb opening or next d/s inlet)		Q <sub>b</sub> =	N/A	N/A	cfs
<b>Curb or Slotted Inlet Opening Analysis (Calculated)</b>		MINOR		MAJOR	
Equivalent Slope S <sub>e</sub> (based on grate carry-over)		S <sub>e</sub> =	0.188	0.155	ft/ft
Required Length L <sub>T</sub> to Have 100% Interception		L <sub>T</sub> =	4.45	6.92	ft
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L <sub>T</sub> )		L =	4.45	5.00	ft
Interception Capacity		Q <sub>i</sub> =	1.1	2.0	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient		CurbCoef =	1.00	1.00	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet		CurbClog =	0.10	0.10	
Effective (Unclogged) Length		L <sub>e</sub> =	4.50	4.50	ft
Actual Interception Capacity		Q <sub>s</sub> =	1.1	1.9	cfs
Carry-Over Flow = Q <sub>b(Grate)</sub> - Q <sub>s</sub>		Q <sub>b</sub> =	0.0	0.3	cfs
<b>Summary</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	1.1	1.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q <sub>b</sub> =	0.0	0.3	cfs
Capture Percentage = Q <sub>s</sub> /Q <sub>o</sub> =		C% =	100	85	%

# INLET J4

## INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>T-G</sub> =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C <sub>T-C</sub> =	0.10	0.10	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>					
<b>Design Discharge for Half of Street (from Sheet Inlet Management)</b>		MINOR		MAJOR	
Water Spread Width		Q <sub>o</sub> =	8.6	19.2	cfs
Water Depth at Flowline (outside of local depression)		T =	13.9	17.0	ft
Water Depth at Street Crown (or at T <sub>MAX</sub> )		d =	4.9	6.1	inches
Ratio of Gutter Flow to Design Flow		d <sub>CROWN</sub> =	0.0	0.5	inches
Discharge outside the Gutter Section W, carried in Section T <sub>x</sub>		E <sub>o</sub> =	0.429	0.309	
Discharge within the Gutter Section W		Q <sub>s</sub> =	4.9	13.3	cfs
Discharge Behind the Curb Face		Q <sub>w</sub> =	3.7	5.9	cfs
Flow Area within the Gutter Section W		Q <sub>BACK</sub> =	0.0	0.0	cfs
Velocity within the Gutter Section W		A <sub>w</sub> =	0.64	0.86	sq ft
Water Depth for Design Condition		V <sub>w</sub> =	5.7	6.9	fps
		d <sub>LOCAL</sub> =	7.9	9.1	inches
<b>Grate Analysis (Calculated)</b>		MINOR		MAJOR	
Total Length of Inlet Grate Opening		L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow		E <sub>o-GRATE</sub> =	N/A	N/A	
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Interception Capacity		Q <sub>i</sub> =	N/A	N/A	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet		GrateCoef =	N/A	N/A	
Clogging Factor for Multiple-unit Grate Inlet		GrateClog =	N/A	N/A	
Effective (unclogged) Length of Multiple-unit Grate Inlet		L <sub>e</sub> =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins		V <sub>o</sub> =	N/A	N/A	fps
Interception Rate of Frontal Flow		R <sub>f</sub> =	N/A	N/A	
Interception Rate of Side Flow		R <sub>s</sub> =	N/A	N/A	
Actual Interception Capacity		Q <sub>s</sub> =	N/A	N/A	cfs
Carry-Over Flow = Q <sub>o</sub> - Q <sub>s</sub> (to be applied to curb opening or next d/s inlet)		Q <sub>b</sub> =	N/A	N/A	cfs
<b>Curb or Slotted Inlet Opening Analysis (Calculated)</b>		MINOR		MAJOR	
Equivalent Slope S <sub>e</sub> (based on grate carry-over)		S <sub>e</sub> =	0.100	0.078	ft/ft
Required Length L <sub>T</sub> to Have 100% Interception		L <sub>T</sub> =	16.97	28.69	ft
<b>Under No-Clogging Condition</b>		MINOR		MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L <sub>T</sub> )		L =	10.00	10.00	ft
Interception Capacity		Q <sub>i</sub> =	6.9	10.3	cfs
<b>Under Clogging Condition</b>		MINOR		MAJOR	
Clogging Coefficient		CurbCoef =	1.25	1.25	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet		CurbClog =	0.06	0.06	
Effective (Unclogged) Length		L <sub>e</sub> =	8.75	8.75	ft
Actual Interception Capacity		Q <sub>s</sub> =	6.6	9.9	cfs
Carry-Over Flow = Q <sub>b(Grate)</sub> - Q <sub>s</sub>		Q <sub>b</sub> =	2.0	9.3	cfs
<b>Summary</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	6.6	9.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q <sub>b</sub> =	2.0	9.3	cfs
Capture Percentage = Q <sub>s</sub> /Q <sub>o</sub> =		C% =	77	52	%

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## APPENDIX D – POND CALCULATIONS

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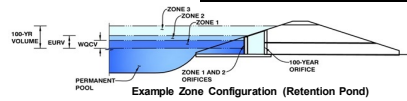
## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

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Project: Creekside South FDR

Basin ID: POND E2



#### Required Volume Calculation

Selected BMP Type =	<b>EDB</b>	
Watershed Area =	125.00	acres
Watershed Length =	2.900	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	35.00%	percent
Percentage Hydrologic Soil Group A =	0.00%	percent
Percentage Hydrologic Soil Group B =	40.0%	percent
Percentage Hydrologic Soil Groups C/D =	60.0%	percent
Desired Runoff Drain Time =	40.0	hours
Location for 1-hr Rainfall Depth =	User Input	
Water Quality Capture Volume (WCQV) =	1.732	acre-feet
Excess Urban Runoff Volume (EURV) =	4.222	acre-feet
2-yr Runoff Volume ( $P_1 = 1.19$ in.) =	3.945	acre-feet
5-yr Runoff Volume ( $P_1 = 1.75$ in.) =	6.556	acre-feet
10-yr Runoff Volume ( $P_1 = 1.75$ in.) =	7.847	acre-feet
25-yr Runoff Volume ( $P_1 = 2$ in.) =	12.045	acre-feet
50-yr Runoff Volume ( $P_1 = 2.25$ in.) =	14.974	acre-feet
100-yr Runoff Volume ( $P_1 = 2.52$ in.) =	18.724	acre-feet
50-yr Runoff Volume ( $P_1 + 0$ in.) =	0.000	acre-feet
Approximate 2-yr Detention Volume =	3.411	acre-feet
Approximate 5-yr Detention Volume =	5.233	acre-feet
Approximate 10-yr Detention Volume =	6.508	acre-feet
Approximate 25-yr Detention Volume =	7.293	acre-feet
Approximate 50-yr Detention Volume =	7.634	acre-feet
Approximate 100-yr Detention Volume =	9.039	acre-feet

Water Quality Capture Volume (WQCV) =	1.732	acre-feet	Optional User Override 1-hr Precipitation	
Excess Urban Runoff Volume (EVRV) =	4.232	acre-feet		
2-yr Runoff Volume (P1 = 1.19 in.) =	3.645	acre-feet		1.19 inches
5-yr Runoff Volume (P1 = 1.5 in.) =	5.556	acre-feet		1.50 inches
10-yr Runoff Volume (P1 = 1.75 in.) =	7.947	acre-feet		1.75 inches
25-yr Runoff Volume (P1 = 2 in.) =	12.045	acre-feet		2.00 inches
50-yr Runoff Volume (P1 = 2.25 in.) =	14.974	acre-feet		2.25 inches
100-yr Runoff Volume (P1 = 2.52 in.) =	18.724	acre-feet	2.52 inches	
500-yr Runoff Volume (P1 = 0 in.) =	0.000	acre-feet	inches	

### Stage-Storage Calculation

Zone 1 Volume ( $V_{QVC1}$ )	1,732	acre-feet
Zone 2 Volume ( $EURV - Zone 1$ )	2,500	acre-feet
Zone 3 (100yr + 1/2 $V_{QVC}$ - Zones 1 & 2)	5,673	acre-feet
Total Detention Basin Volume =	9,905	acre-feet
Initial Surcharge Volume ( $ISV$ )	user	ft <sup>3</sup>
Initial Surcharge Depth ( $ISD$ )	user	ft
Total Available Detention Depth ( $H_{DAV}$ )	user	ft
Depth of Trickle Channel ( $H_{TC}$ )	user	ft
Slope of Trickle Channel ( $S_{TC}$ )	user	ft/V
Slopes of Main Basin Sides ( $S_{MAIN}$ )	user	ft/V
Basin Length-to-Width Ratio ( $R_{L/W}$ )	user	
Initial Surcharge Area ( $A_{IS}$ )	user	ft <sup>2</sup>
Surcharge Volume Length ( $L_{IS}$ )	user	ft
Surcharge Volume Width ( $W_{IS}$ )	user	ft
Depth of Basin Floor ( $H_{1(100)}$ )	user	ft
Length of Basin Floor ( $L_{1(100)}$ )	user	ft
Width of Basin Floor ( $W_{1(100)}$ )	user	ft
Area of Basin Floor ( $A_{1(100)}$ )	user	ft <sup>2</sup>
Volume of Basin Floor ( $V_{1(100)}$ )	user	ft <sup>3</sup>
Depth of Main Basin ( $H_{MAIN}$ )	user	ft
Length of Main Basin ( $L_{MAIN}$ )	user	ft
Width of Main Basin ( $W_{MAIN}$ )	user	ft
Area of Main Basin ( $A_{MAIN}$ )	user	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ )	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{TOTAL}$ )	user	acre-feet

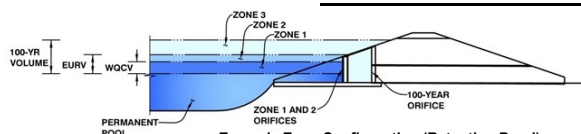
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## Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: Creekside South FDR

Basin ID: POND E2



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.13	1.732	Orifice Plate
Zone 2 (EURV)	4.80	2.500	Rectangular Orifice
(100+1/2WQCV)	8.18	5.673	Weir&Pipe (Restrict)
		9.905	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	3.12	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	12.00	inches
Orifice Plate: Orifice Area per Row =	5.25	sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row =	3.646E-02	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	2.00	3.00				
Orifice Area (sq. inches)	5.25	5.25	5.25	5.25				

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	3.50	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.80	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	4.00	N/A	inches
Vertical Orifice Width =	18.00		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.50	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.17	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.85	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	17.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	6.70	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H <sub>1</sub> =	5.85	N/A	feet
Over Flow Weir Slope Length =	6.70	N/A	feet
Grate Open Area / 100-yr Orifice Area =	6.34	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	79.73	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	39.87	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.10	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	48.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	48.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	12.57	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	2.00	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	8.20	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	55.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	0.50	feet

Calculated Parameters for Spillway

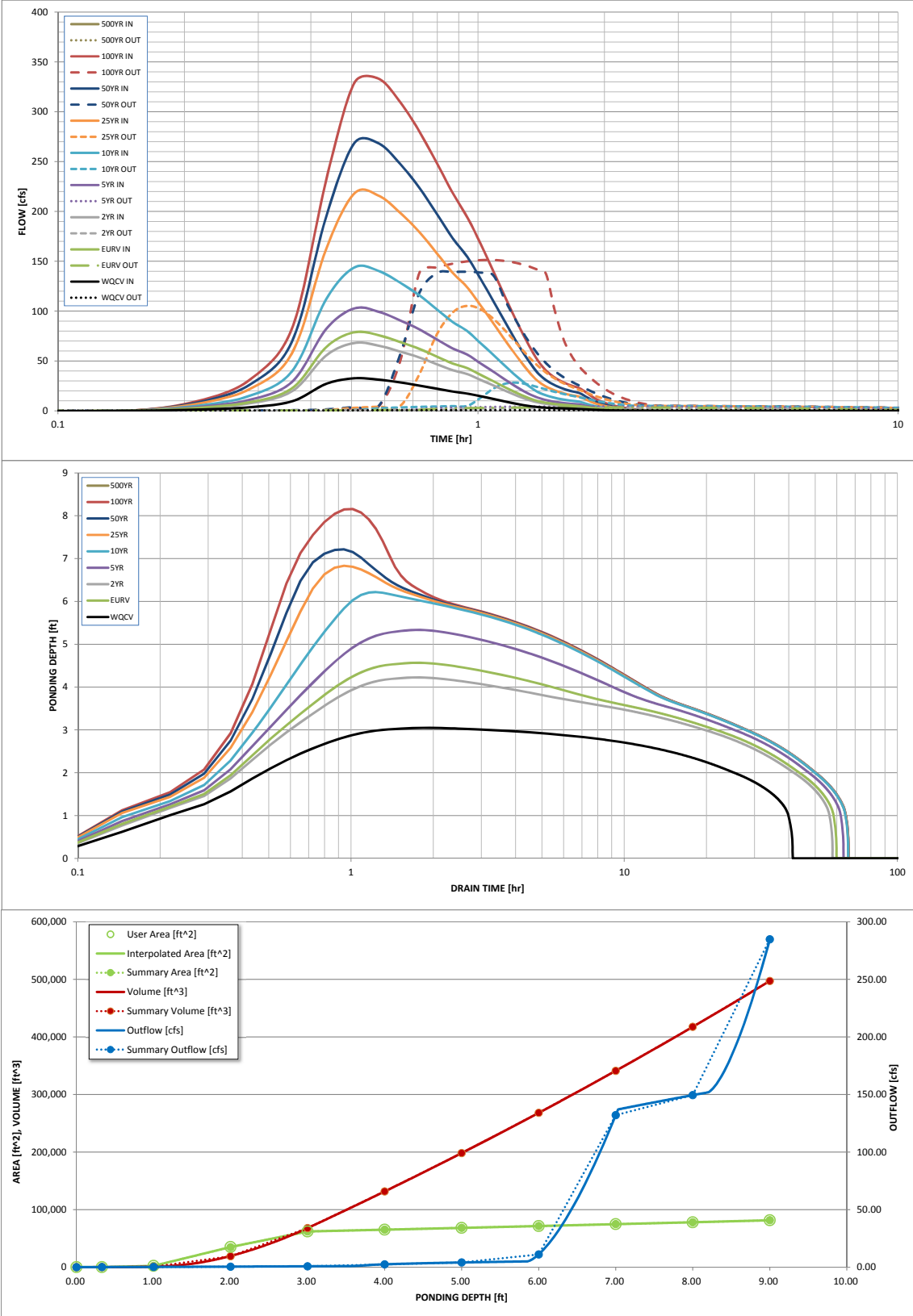
Spillway Design Flow Depth =	1.51	feet
Stage at Top of Freeboard =	10.21	feet
Basin Area at Top of Freeboard =	1.87	acres

### Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	1.732	4.232	3.645	5.556	7.847	12.045	14.974	18.724	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.732	4.233	3.646	5.554	7.843	12.049	14.970	18.731	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.10	0.34	0.87	1.17	1.53	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	2.0	12.4	42.6	108.8	146.0	191.3	0.0
Peak Inflow Q (cfs) =	32.7	78.8	68.1	102.8	143.9	218.1	268.6	333.2	#N/A
Peak Outflow Q (cfs) =	0.8	3.5	2.9	4.5	28.3	105.4	139.5	151.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.7	1.0	1.0	0.8	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.3	1.2	1.7	1.8	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	54	53	56	56	53	50	47	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	57	56	60	62	60	59	58	#N/A
Maximum Ponding Depth (ft) =	3.05	4.57	4.23	5.34	6.22	6.83	7.22	8.16	#N/A
Area at Maximum Ponding Depth (acres) =	1.43	1.54	1.51	1.59	1.66	1.70	1.73	1.80	#N/A
Maximum Volume Stored (acre-ft) =	1.617	3.868	3.351	5.072	6.500	7.541	8.194	9.855	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override

	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			



## Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

[illegible]



# Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.06, November 2016)

Sheet 1 of 4

**Designer:** Richard Schindler  
**Company:** Core Engineering Group  
**Date:** February 16, 2019  
**Project:** Lorson Ranch East 4 FDR - Pond E2 forebay design (ultimate)  
**Location:**

## 1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area,  $I_a$
- B) Tributary Area's Imperviousness Ratio ( $i = I_a / 100$ )
- C) Contributing Watershed Area
- D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- E) Design Concept  
(Select EURV when also designing for flood control)
- F) Design Volume (WQCV) Based on 40-hour Drain Time  
( $V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * \text{Area})$ )
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume  
( $V_{WQCV \text{ OTHER}} = (d_6 * (V_{DESIGN} / 0.43))$ )
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume  
(Only if a different WQCV Design Volume is desired)
- I) Predominant Watershed NRCS Soil Group
- J) Excess Urban Runoff Volume (EURV) Design Volume  
 For HSG A:  $EURV_A = 1.68 * i^{1.28}$   
 For HSG B:  $EURV_B = 1.36 * i^{1.08}$   
 For HSG C/D:  $EURV_{C/D} = 1.20 * i^{1.08}$

$I_a = 35.0$  %

$i = 0.350$

Area = 125.000 ac

$d_6 =$  in

Choose One

- ☒ Water Quality Capture Volume (WQCV)  
☐ Excess Urban Runoff Volume (EURV)

$V_{DESIGN} = 1.732$  ac-ft

$V_{DESIGN \text{ OTHER}} =$  ac-ft

$V_{DESIGN \text{ USER}} =$  ac-ft

Choose One

- ☐ A  
☐ B  
☐ C / D

WQCV selected. Soil group not required.

EURV = ac-ft

## 2. Basin Shape: Length to Width Ratio

(A basin length to width ratio of at least 2:1 will improve TSS reduction.)

$L : W = 2.0 : 1$

## 3. Basin Side Slopes

- A) Basin Maximum Side Slopes  
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

$Z = 0.33$  ft / ft **TOO STEEP (< 3)**

## 4. Inlet

- A) Describe means of providing energy dissipation at concentrated inflow locations:

# Design Procedure Form: Extended Detention Basin (EDB)

Sheet 2 of 4

**Designer:** Richard Schindler  
**Company:** Core Engineering Group  
**Date:** February 16, 2019  
**Project:** Lorson Ranch East 4 FDR - Pond E2 forebay design (ultimate)  
**Location:**

## 5. Forebay

A) Minimum Forebay Volume  
( $V_{FMIN} = 3\%$  of the WQCV)

B) Actual Forebay Volume

C) Forebay Depth  
( $D_F = 30$  inch maximum)

D) Forebay Discharge

i) Undetained 100-year Peak Discharge

ii) Forebay Discharge Design Flow  
( $Q_F = 0.02 * Q_{100}$ )

E) Forebay Discharge Design

F) Discharge Pipe Size (minimum 8-inches)

G) Rectangular Notch Width

$V_{FMIN} = 0.052$  ac-ft

$V_F = 0.055$  ac-ft

$D_F = 30.0$  in

$Q_{100} = 333.00$  cfs

$Q_F = 6.66$  cfs

Choose One  
☐ Berm With Pipe  
☒ Wall with Rect. Notch  
☐ Wall with V-Notch Weir

Calculated  $D_p =$  in

Calculated  $W_N = 12.1$  in

use 7" wide notch in this forebay. existing forebay has a 6" wide notch

## 6. Trickle Channel

A) Type of Trickle Channel

F) Slope of Trickle Channel

Choose One  
☒ Concrete  
☐ Soft Bottom

$S = 0.0050$  ft / ft

## 7. Micropool and Outlet Structure

A) Depth of Micropool (2.5-feet minimum)

B) Surface Area of Micropool (10 ft<sup>2</sup> minimum)

C) Outlet Type

D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing  
(Use UD-Detention)

E) Total Outlet Area

$D_M = 2.5$  ft

$A_M = 56$  sq ft

Choose One  
☒ Orifice Plate  
☐ Other (Describe):

$D_{orifice} = 2.30$  inches

$A_{ot} = 21.00$  square inches

# Design Procedure Form: Extended Detention Basin (EDB)

Sheet 3 of 4

Designer: Richard Schindler  
 Company: Core Engineering Group  
 Date: February 16, 2019  
 Project: Lorson Ranch East 4 FDR - Pond E2 forebay design (ultimate)  
 Location: \_\_\_\_\_

## 8. Initial Surge Volume

- A) Depth of Initial Surge Volume  
(Minimum recommended depth is 4 inches)
- B) Minimum Initial Surge Volume  
(Minimum volume of 0.3% of the WQCV)
- C) Initial Surge Provided Above Micropool

$$D_{IS} = \underline{4} \text{ in}$$

$$V_{IS} = \underline{226.3} \text{ cu ft}$$

$$V_s = \underline{18.7} \text{ cu ft}$$

## 9. Trash Rack

- A) Water Quality Screen Open Area:  $A_t = A_{ot} * 38.5 * (e^{-0.095D})$
- B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open area to the total screen area for the material specified.)

Other (Y/N): Y

- C) Ratio of Total Open Area to Total Area (only for type 'Other')
- D) Total Water Quality Screen Area (based on screen type)
- E) Depth of Design Volume (EURV or WQCV)  
(Based on design concept chosen under 1E)
- F) Height of Water Quality Screen ( $H_{TR}$ )
- G) Width of Water Quality Screen Opening ( $W_{opening}$ )  
(Minimum of 12 inches is recommended)

$$A_t = \underline{650} \text{ square inches}$$

Other (Please describe below)

well screen stainless steel

$$\text{User Ratio} = \underline{0.6}$$

$$A_{total} = \underline{1083} \text{ sq. in.} \quad \text{Based on type 'Other' screen ratio}$$

$$H = \underline{3} \text{ feet}$$

$$H_{TR} = \underline{64} \text{ inches}$$

$$W_{opening} = \underline{16.9} \text{ inches}$$

# Design Procedure Form: Extended Detention Basin (EDB)

Sheet 4 of 4

**Designer:** Richard Schindler  
**Company:** Core Engineering Group  
**Date:** February 16, 2019  
**Project:** Lorson Ranch East 4 FDR - Pond E2 forebay design (ultimate)  
**Location:**

## 10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

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---

B) Slope of Overflow Embankment  
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

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## 11. Vegetation

Choose One

- ☐ Irrigated  
☐ Not Irrigated

## 12. Access

A) Describe Sediment Removal Procedures

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Notes:

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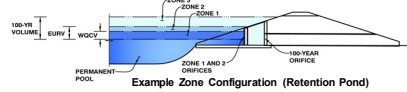
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## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Project: Creekside South at Lorson Ranch

Basin ID: Pond J



**POOL**      **Example Zone Configuration (Retention Pond)**

**Required Volume Calculation**

Selected BMP Type =	<b>EDB</b>	
Watershed Area =	54.00	acres
Watershed Length =	2.200	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	26.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	90.0%	percent
Percentage Hydrologic Soil Groups C/D =	10.0%	percent
Desired WQCV Rainfall Depth =	40.0	inches
Location for 1-yr Rainfall Depths =	User Input	
Water Quality Capture Volume (WQCV) =	0.623	acre-feet
Excess Urban Runoff Volume (EURV) =	1.408	acre-feet
2-yr Runoff Volume ( $P1 = 1.19$ ) =	1.084	acre-feet
5-yr Runoff Volume ( $P1 = 1.75$ ) =	1.502	inches
10-yr Runoff Volume ( $P1 = 1.75$ ) =	2.509	inches
25-yr Runoff Volume ( $P1 = 2.1$ ) =	4.406	acre-feet
50-yr Runoff Volume ( $P1 = 2.25$ ) =	5.648	acre-feet
100-yr Runoff Volume ( $P1 = 2.52$ ) =	7.267	acre-feet
500-yr Runoff Volume ( $P1 = 0$ ) =	0.000	acre-feet
Approximate 2-yr Detention Volume =	1.011	acre-feet
Approximate 5-yr Detention Volume =	1.495	acre-feet
Approximate 10-yr Detention Volume =	2.192	acre-feet
Approximate 25-yr Detention Volume =	2.587	acre-feet
Approximate 50-yr Detention Volume =	2.728	acre-feet
Approximate 100-yr Detention Volume =	3.285	acre-feet

### Stage-Storage Calculation

Zone 1 Volume ( $WQV_1$ )	0.623	acre-feet
Zone 2 Volume ( $EVR - Zone 1$ )	0.785	acre-feet
Zone 3 ( $100yr + 1/2 WQVC - Zones 1 \& 2$ )	2.188	acre-feet
Total Detention Basin Volume	3.556	acre-feet
Initial Surcharge Volume ( $ISV$ )	0.657	cu ft
Initial Surcharge Depth ( $ISD$ )	0.657	ft
Total Available Detention Depth ( $H_{TAD}$ )	0.657	ft
Depth of Trickle Channel ( $H_{TC}$ )	0.657	ft
Slope of Trickle Channel ( $S_{TC}$ )	0.657	ft/ft
Slopes of Main Basin Sides ( $S_{MB}$ )	0.657	H/V
Basin Length-to-Width Ratio ( $R_{LW}$ )	0.657	
Initial Surcharge Area ( $A_{IS}$ )	0.657	sq ft
Surcharge Volume Length ( $L_{SV}$ )	0.657	ft
Surcharge Volume Width ( $W_{SV}$ )	0.657	ft
Depth of Basin Floor ( $H_{BF}$ )	0.657	ft
Length of Basin Floor ( $L_{BF}$ )	0.657	ft
Width of Basin Floor ( $W_{BF}$ )	0.657	ft
Area of Basin Floor ( $A_{BF}$ )	0.657	sq ft
Volume of Basin Floor ( $V_{BF}$ )	0.657	cu ft
Length of Main Basin ( $L_{MB}$ )	0.657	ft
Length of Main Basin ( $L_{MB}$ )	0.657	ft
Width of Main Basin ( $W_{MB}$ )	0.657	ft
Area of Main Basin ( $A_{MB}$ )	0.657	sq ft
Volume of Main Basin ( $V_{MB}$ )	0.657	cu ft
Calculated Total Basin Volume ( $V_{TB}$ )	0.657	acre-feet

Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
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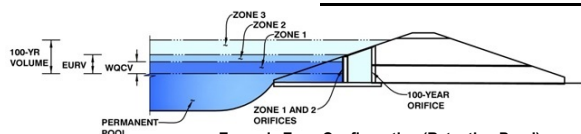
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## Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: Creekside South

Basin ID: Pond J



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.52	0.623	Orifice Plate
Zone 2 (EURV)	3.60	0.785	Rectangular Orifice
(100+1/2WQCV)	6.06	2.188	Weir&Pipe (Restrict)
		3.596	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  2.52 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  9.00 inches  
Orifice Plate: Orifice Area per Row =  2.15 sq. inches (diameter = 1-5/8 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row =  1.493E-02 ft<sup>2</sup>  
Elliptical Half-Width =  N/A feet  
Elliptical Slot Centroid =  N/A feet  
Elliptical Slot Area =  N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.80	1.60					
Orifice Area (sq. inches)	2.15	2.15	2.15					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.52	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.60	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	N/A	inches
Vertical Orifice Width =	12.13		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.17	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.70	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Slope =	6.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	6.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H <sub>1</sub> =	4.70	N/A	feet
Over Flow Weir Slope Length =	6.08	N/A	feet
Grate Open Area / 100-yr Orifice Area =	4.88	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	25.55	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	12.77	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	36.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	25.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	5.24	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	1.16	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.97	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  6.10 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  25.00 feet  
Spillway End Slopes =  4.00 H:V  
Freeboard above Max Water Surface =  1.00 feet

Calculated Parameters for Spillway

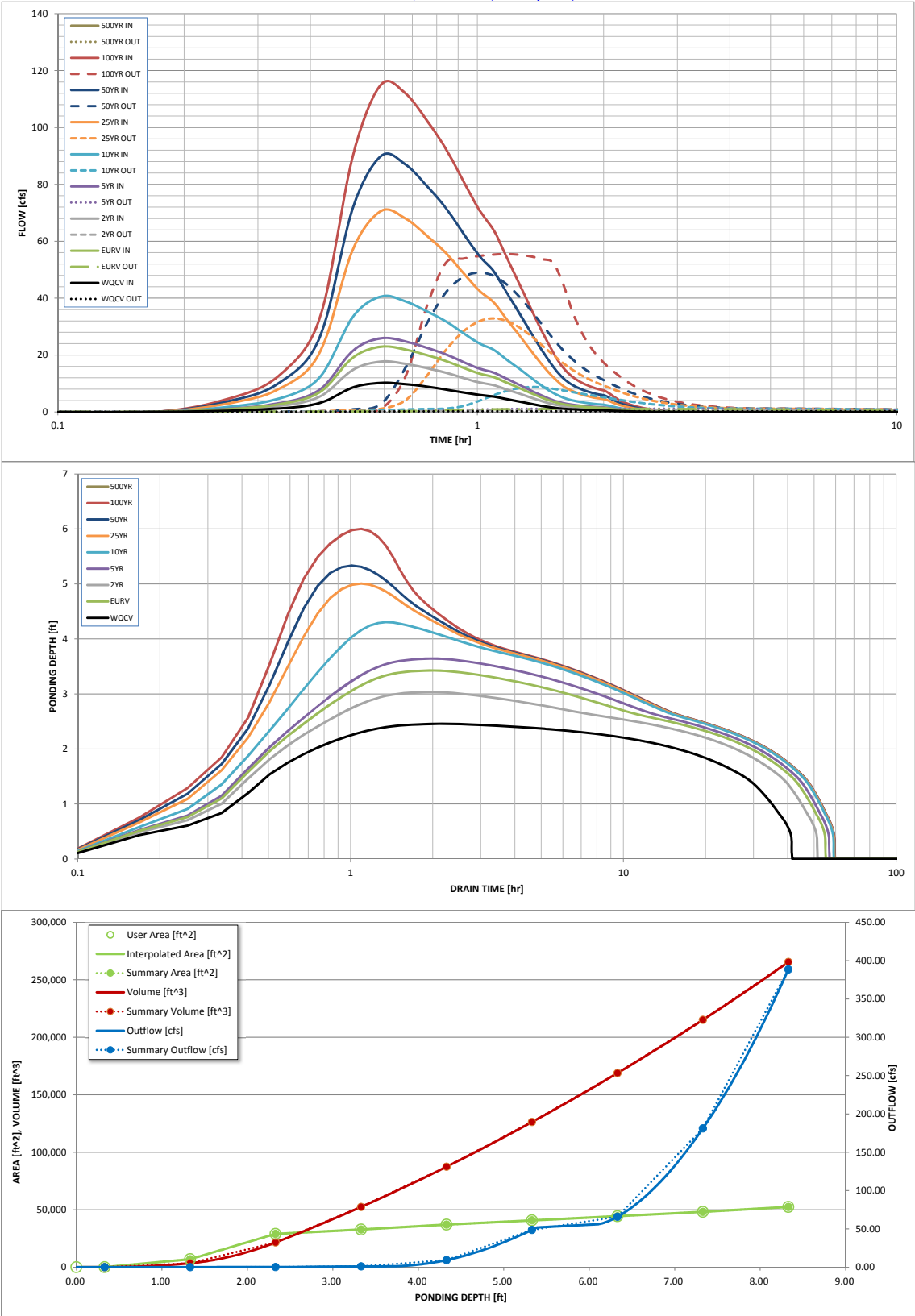
Spillway Design Flow Depth =  1.20 feet  
Stage at Top of Freeboard =  8.30 feet  
Basin Area at Top of Freeboard =  1.20 acres

### Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.623	1.408	1.084	1.592	2.509	4.406	5.648	7.267	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.622	1.409	1.084	1.593	2.510	4.409	5.647	7.267	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.03	0.21	0.67	0.92	1.24	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.7	1.7	11.4	36.1	49.8	66.7	0.0
Peak Inflow Q (cfs) =	10.2	23.0	17.7	25.9	40.6	70.6	90.0	115.1	#N/A
Peak Outflow Q (cfs) =	0.3	1.1	0.9	1.2	8.8	32.9	49.0	55.5	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.7	0.8	0.9	1.0	0.8	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.3	1.2	1.9	2.1	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	48	46	49	49	44	42	39	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	52	49	53	54	52	51	50	#N/A
Maximum Ponding Depth (ft) =	2.46	3.43	3.03	3.64	4.31	5.01	5.34	6.00	#N/A
Area at Maximum Ponding Depth (acres) =	0.68	0.76	0.73	0.78	0.85	0.91	0.93	0.99	#N/A
Maximum Volume Stored (acre-ft) =	0.575	1.272	0.982	1.442	1.981	2.596	2.899	3.545	#N/A

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			





## Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

	Stage	Area	Area	Volume	Volume	Total
--	-------	------	------	--------	--------	-------

[illegible]

# Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

**Designer:** Richard Schindler  
**Company:** Core Engineering Group  
**Date:** January 9, 2020  
**Project:** Creekside South at Lorson Ranch  
**Location:** Pond J

## 1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area,  $I_a$
- B) Tributary Area's Imperviousness Ratio ( $i = I_a / 100$ )
- C) Contributing Watershed Area
- D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- E) Design Concept  
(Select EURV when also designing for flood control)
- F) Design Volume (WQCV) Based on 40-hour Drain Time  
( $V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area)$ )
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume  
( $V_{WQCV\ OTHER} = (d_b * (V_{DESIGN} / 0.43))$ )
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume  
(Only if a different WQCV Design Volume is desired)
- I) NRCS Hydrologic Soil Groups of Tributary Watershed  
 i) Percentage of Watershed consisting of Type A Soils  
 ii) Percentage of Watershed consisting of Type B Soils  
 iii) Percentage of Watershed consisting of Type C/D Soils
- J) Excess Urban Runoff Volume (EURV) Design Volume  
 For HSG A:  $EURV_A = 1.68 * i^{1.28}$   
 For HSG B:  $EURV_B = 1.36 * i^{1.08}$   
 For HSG C/D:  $EURV_{C/D} = 1.20 * i^{1.08}$
- K) User Input of Excess Urban Runoff Volume (EURV) Design Volume  
(Only if a different EURV Design Volume is desired)

$I_a = 26.0$  %

$i = 0.260$

Area = 54.000 ac

$d_b =$  in

Choose One

- ☒ Water Quality Capture Volume (WQCV)  
☐ Excess Urban Runoff Volume (EURV)

$V_{DESIGN} = 0.623$  ac-ft

$V_{DESIGN\ OTHER} =$  ac-ft

$V_{DESIGN\ USER} =$  ac-ft

HSG A = %

HSG B = %

HSG C/D = %

$EURV_{DESIGN} =$  ac-ft

$EURV_{DESIGN\ USER} =$  ac-ft

## 2. Basin Shape: Length to Width Ratio

(A basin length to width ratio of at least 2:1 will improve TSS reduction.)

L : W = 2.0 : 1

## 3. Basin Side Slopes

- A) Basin Maximum Side Slopes  
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

Z = 3.00 ft / ft

DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE

## 4. Inlet

- A) Describe means of providing energy dissipation at concentrated inflow locations:

## 5. Forebay

- A) Minimum Forebay Volume  
( $V_{MIN} = 3\%$  of the WQCV)

$V_{MIN} = 0.019$  ac-ft

- B) Actual Forebay Volume

$V_F = 0.024$  ac-ft

- C) Forebay Depth  
( $D_F = 18$  inch maximum)

$D_F = 24.0$  in

DF > DF MAXIMUM

- D) Forebay Discharge

i) Undetained 100-year Peak Discharge

$Q_{100} = 115.00$  cfs

ii) Forebay Discharge Design Flow  
( $Q_F = 0.02 * Q_{100}$ )

$Q_F = 2.30$  cfs

- E) Forebay Discharge Design

Choose One

- ☐ Berm With Pipe  
☒ Wall with Rect. Notch  
☐ Wall with V-Notch Weir

Flow too small for berm w/ pipe

- F) Discharge Pipe Size (minimum 8-inches)

Calculated  $D_P =$  in

- G) Rectangular Notch Width

Calculated  $W_N = 7.7$  in

# Design Procedure Form: Extended Detention Basin (EDB)

Sheet 2 of 3

Designer: Richard Schindler  
 Company: Core Engineering Group  
 Date: January 9, 2020  
 Project: Creekside South at Lorson Ranch  
 Location: Pond J

## 6. Trickle Channel

A) Type of Trickle Channel

F) Slope of Trickle Channel

Choose One

☒ Concrete

☐ Soft Bottom

S = 0.0050 ft / ft

## 7. Micropool and Outlet Structure

A) Depth of Micropool (2.5-feet minimum)

B) Surface Area of Micropool (10 ft<sup>2</sup> minimum)

C) Outlet Type

D<sub>M</sub> = 2.5 ft

A<sub>M</sub> = 50 sq ft

Choose One

☒ Orifice Plate

☐ Other (Describe):

D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)

E) Total Outlet Area

D<sub>orifice</sub> = 1.63 inches

A<sub>orifice</sub> = 6.45 square inches

## 8. Initial Surge Volume

A) Depth of Initial Surge Volume (Minimum recommended depth is 4 inches)

B) Minimum Initial Surge Volume (Minimum volume of 0.3% of the WQCV)

C) Initial Surge Provided Above Micropool

D<sub>IS</sub> = 4 in

V<sub>IS</sub> = 81 cu ft

V<sub>s</sub> = 16.7 cu ft

## 9. Trash Rack

A) Water Quality Screen Open Area:  $A_t = A_{ot} * 38.5 * (e^{-0.095D})$

B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open area to the total screen area for the material specified.)

Other (Y/N): y

C) Ratio of Total Open Area to Total Area (only for type 'Other')

D) Total Water Quality Screen Area (based on screen type)

E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)

F) Height of Water Quality Screen (H<sub>TR</sub>)

G) Width of Water Quality Screen Opening (W<sub>opening</sub>) (Minimum of 12 inches is recommended)

A<sub>t</sub> = 213 square inches

Other (Please describe below)

wellscreen stainless

User Ratio = 0.6

A<sub>total</sub> = 355 sq. in. Based on type 'Other' screen ratio

H = 2.52 feet

H<sub>TR</sub> = 58.24 inches

W<sub>opening</sub> = 12.0 inches VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.

# Design Procedure Form: Extended Detention Basin (EDB)

Sheet 3 of 3

**Designer:** Richard Schindler  
**Company:** Core Engineering Group  
**Date:** January 9, 2020  
**Project:** Creekside South at Lorson Ranch  
**Location:** Pond J

## 10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

B) Slope of Overflow Embankment  
 (Horizontal distance per unit vertical, 4:1 or flatter preferred)

Ze =  ft / ft

## 11. Vegetation

Choose One

- ☐ Irrigated  
☐ Not Irrigated

## 12. Access

A) Describe Sediment Removal Procedures

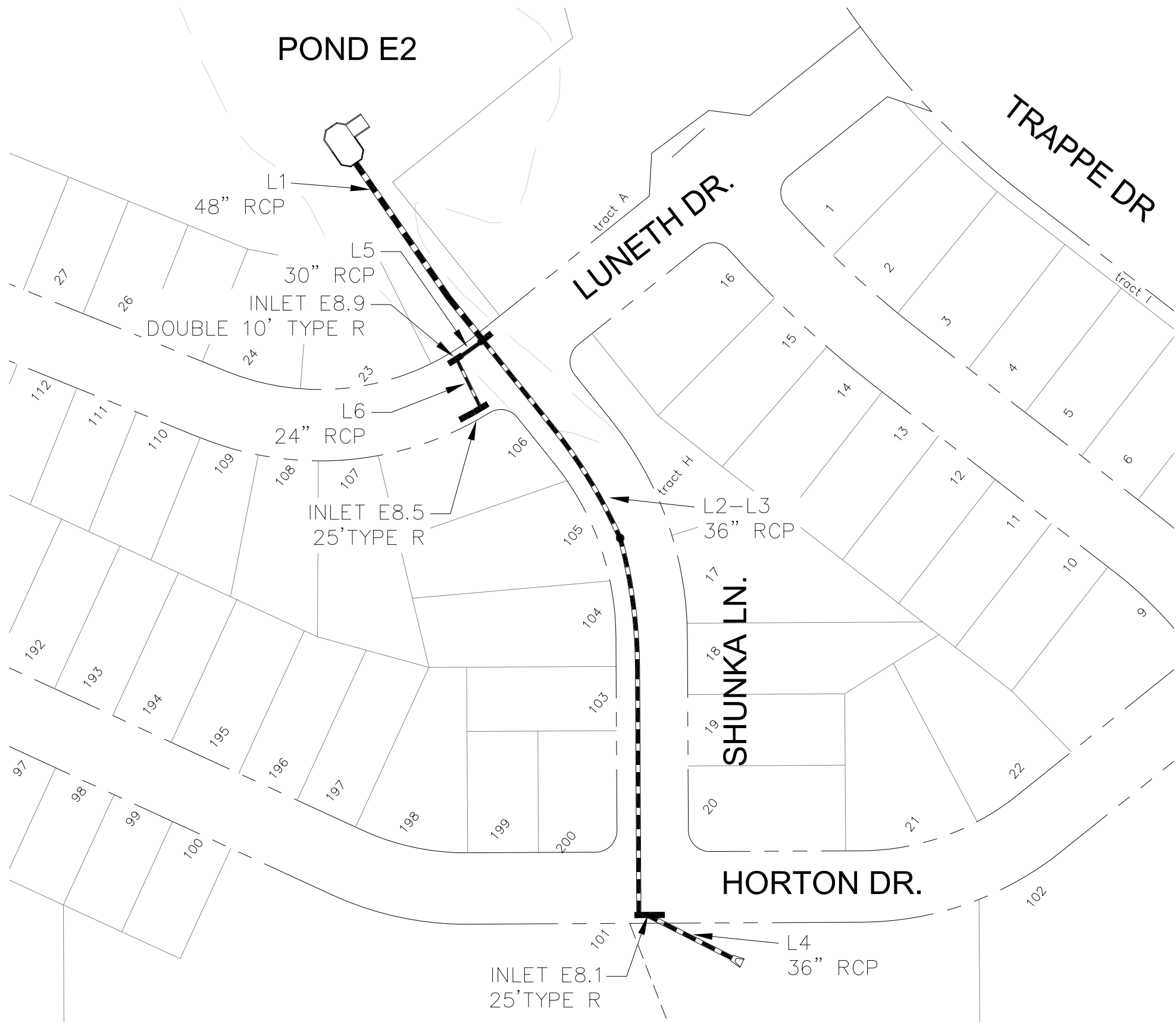
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Notes:

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_




BASIN 'E' STORM SCHEMATIC



DESCRIPTION		DATE
NO.		
PROJECT:		
CREEKSIDE SOUTH		
TRAPPE DR - HORTON DR		
EL PASO COUNTY, COLORADO		
PREPARED FOR:		
LORSON, LLC		
212 N. WAHSATCH AVE., SUITE 301		
COLORADO 80903		
CONTACT: JEFF MARK		

STORM SEWER SCHEMATIC  
BASIN E  
CREEKSIDE SOUTH AT LORSON RANCH

DATE	MAY 12, 2020
PROJECT NO.	100.051
SHEET NUMBER	1
TOTAL SHEETS:	1



**CORE**  
ENGINEERING GROUP  
15004 1ST AVE. S.  
BURNSVILLE, MN 55306  
PH: 719.570.1100  
CONTACT: RICHARD L. SCHINDLER, P.E.  
EMAIL: Rich@ceg1.com

# Storm Sewer Summary Report

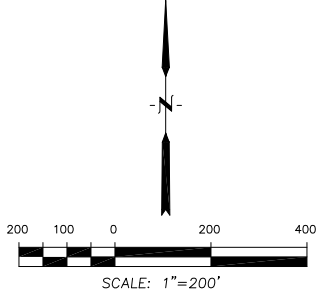
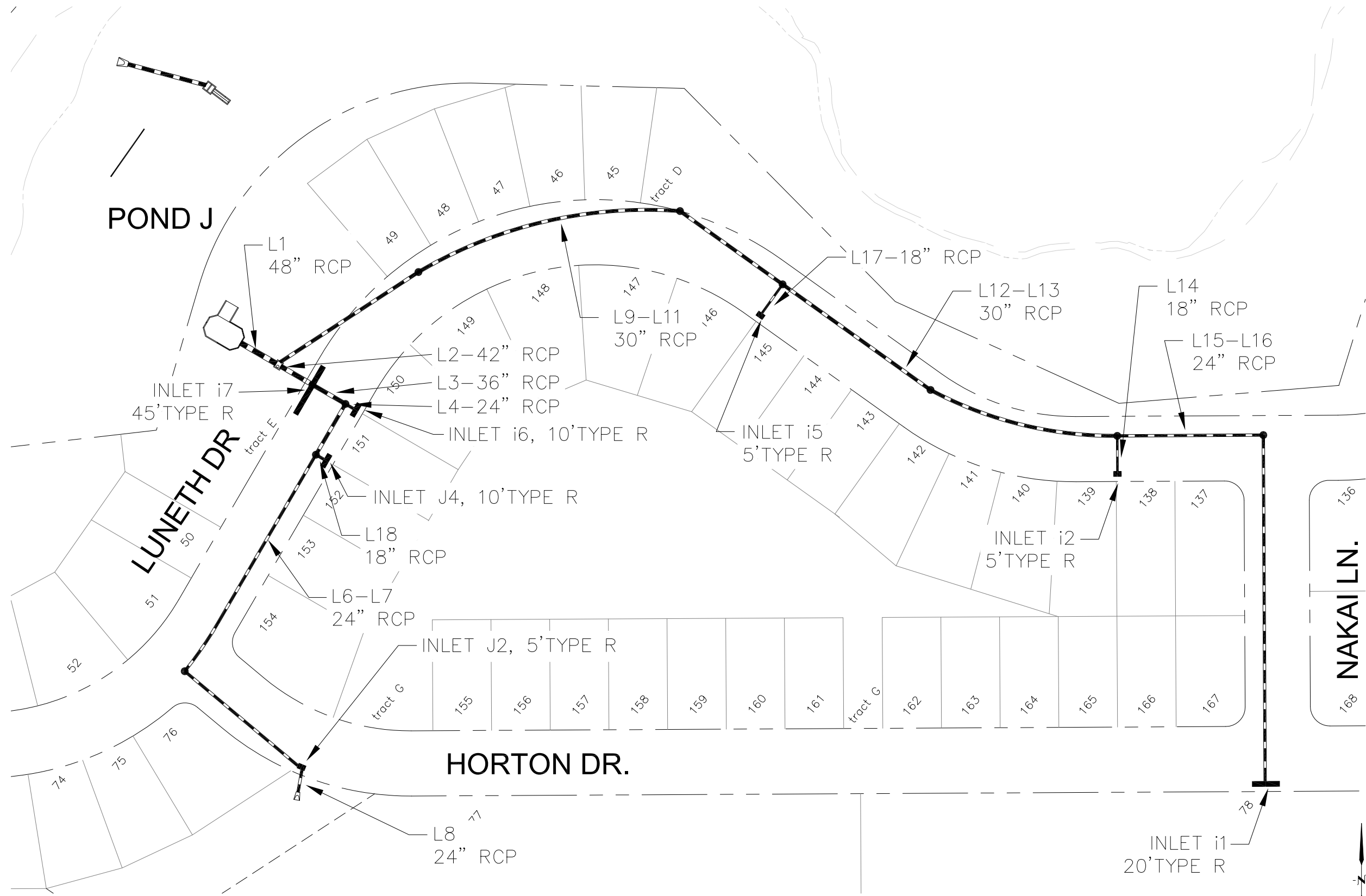
Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	L1-48"	43.30	48 c	151.0	5695.35	5699.40	2.682	5698.69	5701.35	n/a	5701.35 j	End
2	L2-36"	25.20	36 c	166.0	5700.40	5702.90	1.506	5701.94	5704.50	0.38	5704.50	1
3	L3-36"	25.20	36 c	264.0	5703.20	5709.07	2.223	5704.97	5710.67	n/a	5710.67 j	2
4	L4-36"	15.80	36 c	73.0	5709.40	5711.51	2.890	5711.26	5712.78	n/a	5712.78 j	3
5	L5-24"	18.10	30 c	17.0	5700.91	5701.76	4.998	5701.93	5703.18	n/a	5703.18	1
6	L6-24"	15.00	24 c	36.0	5703.26	5703.64	1.057	5704.43	5705.11	0.14	5705.25	5
Project File: 100.051 Basins E, 5yr flow.stm							Number of lines: 6			Run Date: 01-22-2020		
NOTES: c = cir; e = ellip; b = box; Return period = 5 Yrs. ; j - Line contains hyd. jump.												

# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	L1-48"	139.5	48 c	151.0	5695.35	5699.40	2.683	5698.87	5702.92	n/a	5702.92	End
2	L2-36"	85.50	36 c	166.0	5700.40	5702.90	1.506	5703.00	5705.73	1.33	5707.06	1
3	L3-36"	85.50	36 c	264.0	5703.20	5709.07	2.223	5707.17	5711.89	3.30	5711.89	2
4	L4-36"	70.00	36 c	73.0	5709.40	5711.51	2.890	5712.76	5714.18	1.73	5714.18	3
5	L5-24"	54.00	30 c	17.0	5700.91	5701.76	4.998	5703.24	5704.11	0.99	5704.11	1
6	L6-24"	32.00	24 c	36.0	5703.26	5703.64	1.057	5705.26*	5705.98*	0.40	5706.38	5




BASIN I & J STORM SCHEMATIC



STORM SEWER SCHEMATIC	
BASIN I & J	
CREEKSIDE SOUTH AT LORSON RANCH	
DATE	MAY 12, 2020
PROJECT NO.	100.051
SHEET NUMBER	1
TOTAL SHEETS: 1	

DESCRIPTION	
NO.	DATE
PROJECT: CREEKSIDE SOUTH TRAPPE DR - HORTON DR. EL PASO COUNTY, COLORADO	
PREPARED FOR: LORSON, LLC 212 N. WAHSATCH AVE., SUITE 301 COLORADO 80903 CONTACT: RICHARD L. SCHINDLER, P.E. EMAIL: Rich@ceg1.com	



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CONTACT: RICHARD L. SCHINDLER, P.E.  
EMAIL: Rich@ceg1.com

# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	L1	45.60	48 c	50.8	5684.60	5685.37	1.515	5688.06	5687.92	0.25	5688.17	End
2	L2	27.40	42 c	28.6	5687.29	5693.00	19.979	5688.50	5694.60	0.32	5694.60	1
3	L3	22.40	36 c	27.5	5695.20	5695.50	1.090	5696.37	5697.39	0.35	5697.75	2
4	L4	8.30	24 c	7.5	5696.50	5696.57	0.931	5697.86	5697.84	0.24	5698.08	3
5	L5	14.10	30 c	45.0	5696.00	5696.74	1.646	5697.97	5698.00	n/a	5698.00 j	3
6	L6	7.50	24 c	204.7	5697.24	5701.60	2.130	5698.41	5702.57	n/a	5702.57 j	5
7	L7	7.50	24 c	112.9	5701.71	5703.74	1.799	5702.86	5704.71	n/a	5704.71 j	6
8	L8	6.40	24 c	23.0	5703.90	5704.53	2.739	5705.03	5705.43	n/a	5705.43 j	7
9	L9	18.20	30 c	129.0	5690.55	5696.73	4.791	5691.31	5698.16	n/a	5698.16	1
10	L10	18.20	30 c	209.0	5696.83	5698.92	1.000	5698.56	5700.35	n/a	5700.35 j	9
11	L11	18.20	30 c	97.0	5699.02	5699.99	1.000	5700.75	5701.42	n/a	5701.42	10
12	L12	14.70	30 c	139.0	5700.39	5701.51	0.805	5701.89	5702.79	n/a	5702.79 j	11
13	L13	14.70	30 c	150.0	5701.88	5703.07	0.793	5703.18	5704.35	n/a	5704.35 j	12
14	L14	3.60	18 c	27.0	5703.98	5704.14	0.593	5704.81	5704.87	0.28	5705.15	13
15	L15	11.10	24 c	112.0	5703.58	5704.48	0.803	5704.68	5705.66	0.26	5705.66	13
16	L16	11.10	24 c	265.3	5704.65	5708.21	1.342	5705.98	5709.39	n/a	5709.39 j	15
17	L17	3.50	18 c	27.0	5700.92	5701.21	1.074	5701.97	5701.93	n/a	5702.20 j	11
18	L18	6.60	18 c	35.3	5697.72	5698.27	1.558	5698.47	5699.32	0.20	5699.51	5
Project File: 100.051 Basins I & J, 5yr flow.stm							Number of lines: 18			Run Date: 01-23-2020		
NOTES: c = cir; e = ellip; b = box; Return period = 5 Yrs. ; j - Line contains hyd. jump.												

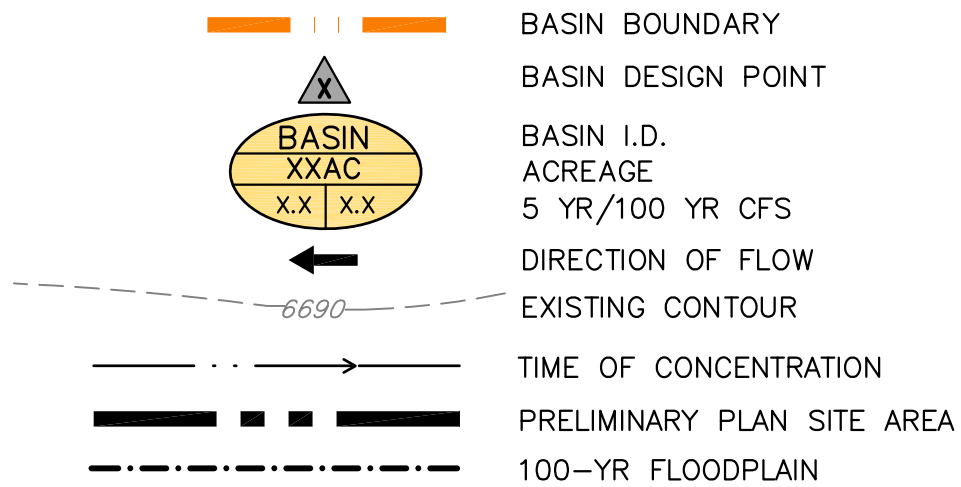
# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	L1	133.6	48 c	50.8	5684.60	5685.37	1.515	5688.06	5688.83	1.17	5688.83	End
2	L2	104.0	42 c	28.6	5687.29	5693.00	19.979	5689.09	5696.12	1.03	5696.12	1
3	L3	53.30	36 c	27.5	5695.20	5695.50	1.090	5697.29	5697.95	1.15	5699.11	2
4	L4	15.50	24 c	7.5	5696.50	5696.57	0.931	5699.88*	5699.92*	0.38	5700.30	3
5	L5	37.80	30 c	45.0	5696.00	5696.74	1.646	5699.34*	5699.72*	0.74	5700.46	3
6	L6	27.90	24 c	204.7	5697.24	5701.60	2.130	5700.46	5703.60	1.23	5704.83	5
7	L7	27.90	24 c	112.9	5701.71	5703.74	1.799	5704.83*	5706.54*	1.79	5708.33	6
8	L8	26.00	24 c	23.0	5703.90	5704.53	2.739	5708.50*	5708.80*	1.06	5709.86	7
9	L9	29.60	30 c	129.0	5690.55	5696.73	4.791	5691.54	5698.55	0.14	5698.55	1
10	L10	29.60	30 c	209.0	5696.83	5698.92	1.000	5698.91	5700.74	n/a	5700.74 j	9
11	L11	29.60	30 c	97.0	5699.02	5699.99	1.000	5701.10	5701.81	0.93	5701.81	10
12	L12	22.60	30 c	139.0	5700.39	5701.51	0.805	5702.41	5703.10	n/a	5703.10 j	11
13	L13	22.60	30 c	150.0	5701.88	5703.07	0.793	5703.50	5704.66	n/a	5704.66 j	12
14	L14	7.10	18 c	27.0	5703.98	5704.14	0.593	5705.14	5705.25	0.40	5705.65	13
15	L15	15.50	24 c	112.0	5703.58	5704.48	0.803	5705.01	5705.88	n/a	5705.88 j	13
16	L16	15.50	24 c	265.3	5704.65	5708.21	1.342	5706.18	5709.60	n/a	5709.60 j	15
17	L17	7.00	18 c	27.0	5700.92	5701.21	1.074	5702.39	5702.42	0.33	5702.75	11
18	L18	9.90	18 c	35.3	5697.72	5698.27	1.558	5700.89*	5701.21*	0.24	5701.45	5
Project File: 100.051 Basins I & J, 100yr flow.stm							Number of lines: 18			Run Date: 05-11-2020		
NOTES: c = cir; e = ellip; b = box; Return period = 100 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.												

# MAP POCKET



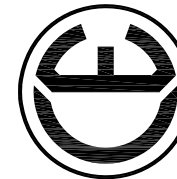
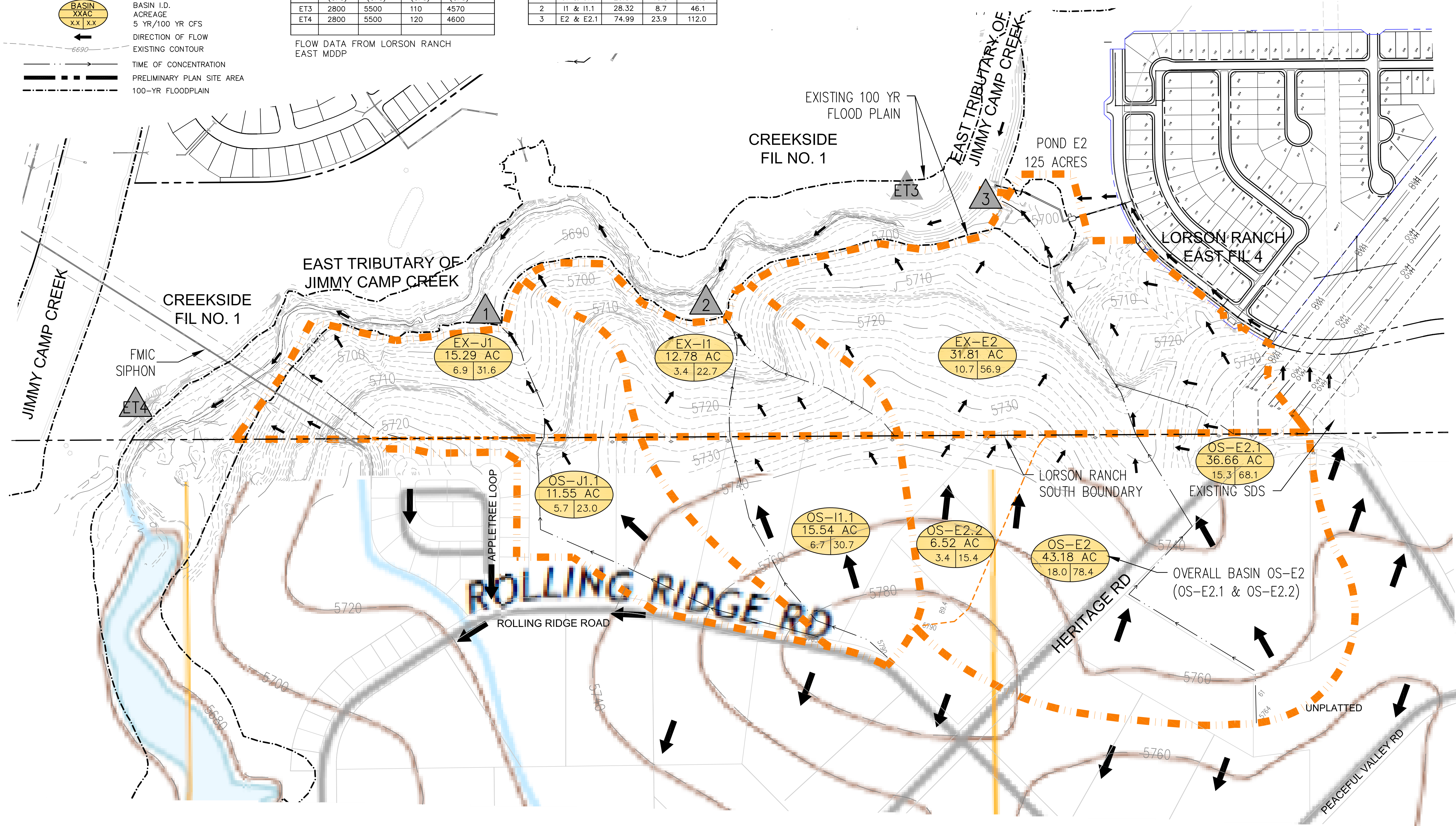
LEGEND



EAST TRIBUTARY FEMA FLOW DATA				EAST TRIBUTARY DBPS FLOW DATA			
DESIGN POINT	RUNOFF 10 YR (CFS)	RUNOFF 100 YR (CFS)		RUNOFF 2 YR (CFS)	RUNOFF 100 YR (CFS)		
ET3	2800	5500		110	4570		
ET4	2800	5500		120	4600		

FLOW DATA FROM LORSON RANCH  
EAST MDDP

DESIGN POINT SUMMARY TABLE					
DESIGN POINT	BASIN (EX & OS)	DRAINAGE AREA (AC)	RUNOFF 5 YR (CFS)	RUNOFF 100 YR (CFS)	
1	J1 & J1.1	26.84	10.8	46.6	
2	I1 & I1.1	28.32	8.7	46.1	
3	E2 & E2.1	74.99	23.9	112.0	



DATE:

DESCRIPTION:

NO.:

DRAWN:  
DESIGNED:  
CHECKED:

LAB  
LAB  
RLS

EXISTING CONDITIONS  
CREEKSIDE SOUTH AT LORSON RANCH

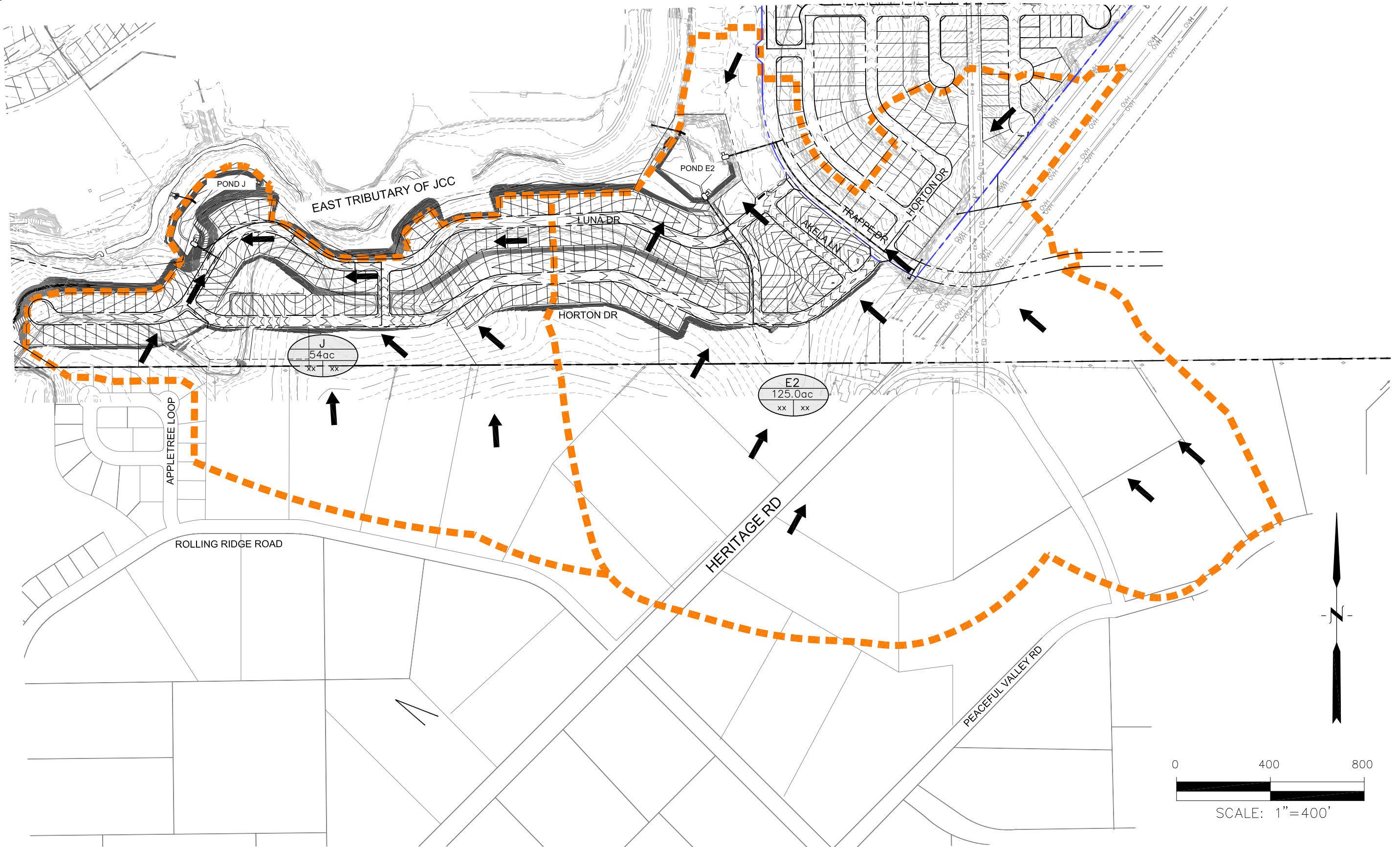
DATE:  
JANUARY 15, 2020

PROJECT NO.  
100.051

SHEET NUMBER  
1

TOTAL SHEETS: 1





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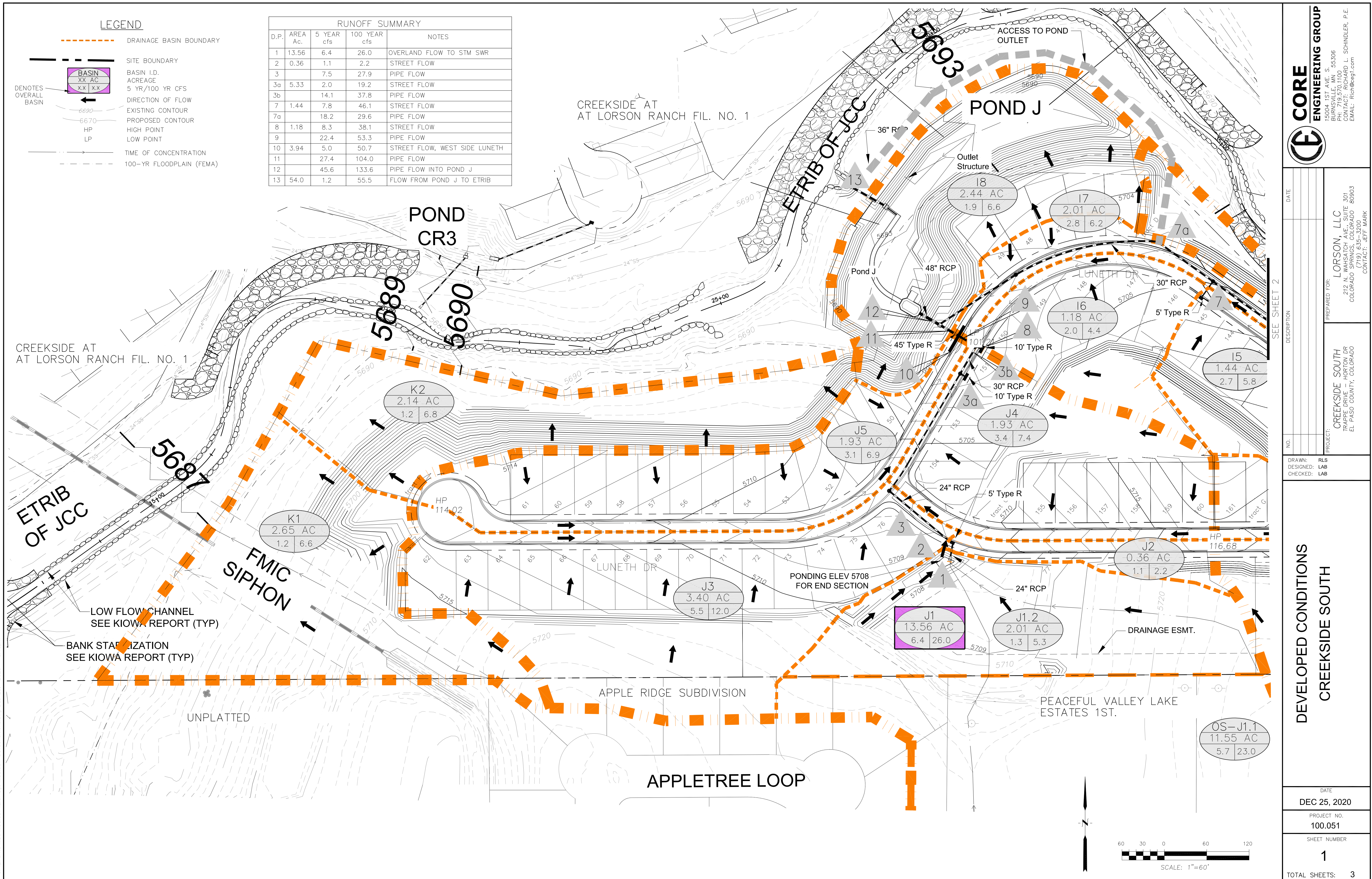
**CREEKSIDE SOUTH AT LORSON RANCH  
WATER QUALITY & POND TRIBUTARY AREAS**

SCALE:  
NTS

DATE:  
JANUARY 15, 2020

FIGURE NO.  
1



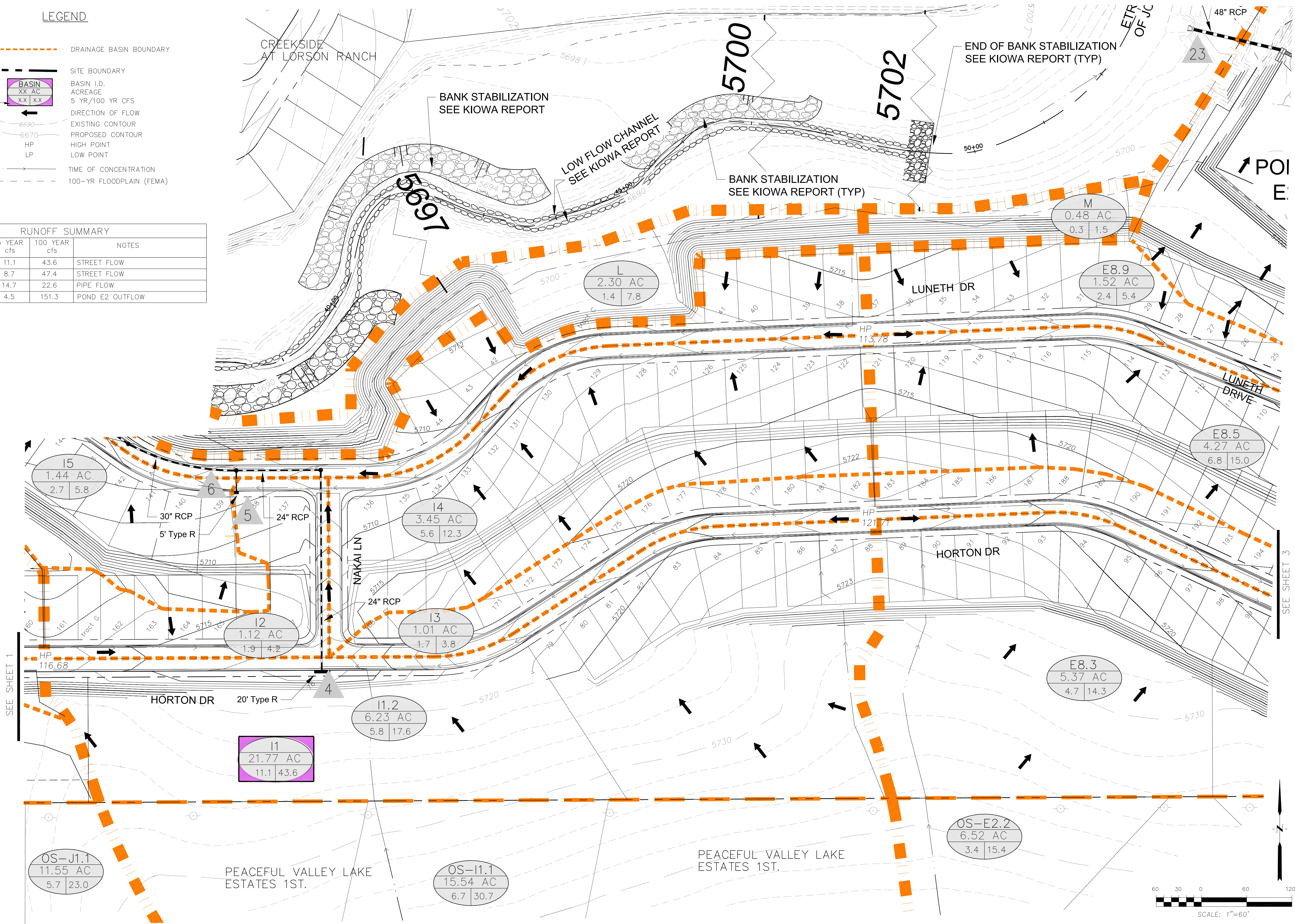




LEGEND

- DRAINAGE BASIN BOUNDARY
- SITE BOUNDARY
- BASIN I.D.  
ACREAGE  
5 YR/100 YR CFS  
DIRECTION OF FLOW
- 6690 --- EXISTING CONTOUR  
--- 6670 --- PROPOSED CONTOUR  
HP HIGH POINT  
LP LOW POINT
- TIME OF CONCENTRATION  
--- 100-YR FLOODPLAIN (FEMA)
- DENOTES OVERALL BASIN

RUNOFF SUMMARY				
D.P.	AREA Ac.	5 YEAR cfs	100 YEAR cfs	NOTES
4	21.77	11.1	43.6	STREET FLOW
5	5.58	8.7	47.4	STREET FLOW
6	14.7	22.6		PIPE FLOW
14	125	4.5	151.3	POND E2 OUTFLOW



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DATE

DESCRIPTION

NO.

PREPARED FOR:

PROJECT:

DRAWN: RLS  
DESIGNED: LAB  
CHECKED: LAB

DEVELOPED CONDITIONS  
CREEKSIDE SOUTH

DATE

PROJECT NO.

SHEET NUMBER

TOTAL SHEETS:

3

FOR:

PROJECT:

100.051

2

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CONTACT: JEFF MARK



