



## Grandview Reserve Phase 2 Preliminary Drainage Report

December 2023

HR Green Project No: 201662.202

**Prepared For:**

D.R. Horton

Contact: Riley Hillen, P.E.

9555 S. Kingston Ct.

Englewood, CO 80112

**Prepared By:**

HR Green Development, LLC

Contact: Ken Huhn, P.E.

[khuhn@hrgreen.com](mailto:khuhn@hrgreen.com)

(630) 602-4965

Add text:

EDARP Filing No.:  
PUDSP236

ADDRESSED.



### Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

\_\_\_\_\_

Ken Huhn, P.E.

\_\_\_\_\_

Date

State of Colorado No. 54022

For and on behalf of HR Green Development, LLC

### Owner/Developer's Statement:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By: \_\_\_\_\_

Authorized Signature

\_\_\_\_\_

Date

Address: D.R. Horton  
9555 S. Kingston Court  
Englewood, CO

### EI Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

\_\_\_\_\_

Joshua Palmer, P.E.

Date

County Engineer/ECM Administrator

Conditions:





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## I. General Purpose, Location and Description

### a. Purpose

The purpose of this Preliminary Drainage Report (PDR) for the Grandview Reserve Subdivision Phase 2 is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls.

### b. Location

The Grandview Reserve Phase 2 site is located in unincorporated El Paso County, Colorado. The Phase 2 location (referred to as the site herein) is located northwest of Grandview Reserve Filings 1-4 and MST2, and southeast of the intersection of Eastonville Road & Rex Road.

The site lies within a tract of land within Sections 21 and 28, Township 12 South, Range 64 West of the 6<sup>th</sup> Principal Meridian, in El Paso County, State of Colorado. A Vicinity Map is included in **Appendix A**.

The site is bound by a segment of Rex Road to be developed with this project to the northeast and undeveloped land that has historically been used as ranching lands. The east of the site will be a future phase of the Grandview Reserve Subdivision. The south and west of the site is bound by Grandview Reserve Filings 1-4 and MST2. A vicinity map is presented in Appendix A.

The Gieck Ranch Tributary #2 "MST2" is a part of the Gieck Ranch Drainage Basin tributary to Black Squirrel Creek. The channel draining through the site is an ongoing project with associated CLOMR Report and the PCD File No. is CDR228 with El Paso County. The Grandview Reserve improvements will follow any requirements of that report. There is another floodplain channel to the north of Rex Road that will not be disturbed by this phase of development and studies as a future project.

The existing surrounding platted developments include the Grandview Reserve Phase 1 Filings 1-4, and the Meridian Ranch Subdivision is west of the site on the west side of Eastonville Road.

### c. Description of Property

68.72 per other documents

ADDRESSED.

The site is approximately 70.67 acres of proposed residential development with associated right of way, open space tracts, public improvements, and stormwater treatment infrastructure.

The existing groundcover and topography of the site is native grasses/weeds and exposed soil on gently rolling hillside with slopes ranging from 2% to 4%.

Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam. The NRCS soil survey is presented in **Appendix A**.

There is one major drainageway through the site. The Gieck Ranch Tributary #2 (MST2 as referenced in the MDDP) traverses the site along its southwestern boundary and forms the southwest boundary for Phase 2. This drainageway generally flows from the northwest to the southeast towards Highway 24, before crossing through existing drainage infrastructure. The CLOMR report by HR Green for MST2 is ongoing and pending approval for this channel. Refer to the CLOMR report included in **Appendix E** for more specific design information regarding the MST2 channel. Gieck Ranch Tributary #3 traverses the site along its northeastern

boundary and forms the northeast boundary for Phase 2 along Rex Road. This channel will not be disturbed by this phase of development. Indicate when/what phase or filing this channel will be evaluated with.

There are no known irrigation facilities in the area.

There are no known existing utilities or other encumbrances on site.

**d. Floodplain Statement**

Based on FEMA Firm map 08041C0552G & 08041C0556G (eff. 12/7/2019) through the site which is part of the Gieck Ranch Tributary #2. See FEMA firm maps in **Appendix A**. The floodplain is being studied and revised in the Gieck Ranch Tributary # 2 CLOMR report. A copy of the current revised floodplain map is also provided in **Appendix A**. There is a Zone A floodplain northeast of the site which will not be altered with this projects improvements.

ADDRESSED. The initial HRG Analysis has established the 100 base flood elevation limits. This delineation is now shown on the Plans. Phase 2 proposed no fill within these limits or the FEMA Mapped limits.

## II. Drainage Design Criteria

### a. Drainage Criteria

Hydrologic data and calculations were performed using Drainage Criteria Manual Volume 1 of El Paso County (EPCDCM), with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual (CCSDCM), May 2014 revised January 2021.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Private, full spectrum Detention. Detention pond allowable release rate will be limited to less than historic rates.

Rainfall Depths per NOAA Atlas 14		
Return Period (yr)	5	100
1-hr Rainfall Depth (in)	1.21	2.49

Storm sewer and inlet sizing shown is preliminary at this stage of the project. Calculations for the storm sewer system on site will be provided with the Final Drainage Report (FDR) for the project. The sizing methodology that will be used is per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer sizing was performed per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

This preliminary drainage report follows any recommendations and is in conformance with the previously approved MDDP for the site prepared by HR Green, “Grandview Reserve Master Development Drainage Plan”, HR Green, November 2020 (MDDP).

## III. Drainage Basins and Subbasins

### a. Major Basin Description

The site is located within the Gieck Ranch Drainage Basin. The site’s drainage characteristics were previously studied in the following reports:

1. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
2. "Grandview Reserve Master Development Drainage Plan" prepared by HR Green, August 2021.
3. "Grandview Reserve Filing No. 1 Preliminary Drainage Report" prepared by Galloway & Company, Inc., September 2022.
4. "Grandview Reserve CLOMR REPORT" prepared by HR Green, March 2023

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains to the Arkansas River. The majority of the basin is undeveloped and rolling range land of 2% - 4% slopes.

The Grandview Reserve MDDP divided the site into 8 major drainage basins (A-H), where each basin is tributary to a full spectrum detention pond facility. The Grandview Reserve Phase 2 improvements are located in subbasins B3 and C1 of the MDDP.

There are no known existing irrigation facilities or other obstructions that could influence or will be influenced by local drainage characteristics. Proposed local drainage characteristics will continue to follow historic patterns. Indicate if there are any offsite flows entering the project site. **ADDRESSED.**

## b. Existing Subbasin Description

The Grandview Reserve Phase 2 site drains from the northwest to the southeast slopes ranging from 2% - 4%. The site has historically drained into the Gieck Ranch Tributary #2 (the existing MST2).

The existing subbasins for the Grandview Reserve Phase 2 site were studied the approved MDDP for Grandview Reserve. This site is located within subbasins B3 and C1 of this report and are described as follows.

"Subbasin B3 is located between MS and EF and to the northeast of east of basin B2. The existing MST2 tributary runs through the basin. The site drains towards the southeast and towards Detention Pond B. Current planning documents call for high, medium-high, and medium density dwelling units along with a pocket park. The basin is 118.90 acres, with a composite impervious value of 49.42% and runoff rates for the 5 and 100 year of 92.76 cfs and 295.27 cfs respectively."

"Subbasin C1 is located to the northeast of east of basin B1 and the existing MST2 tributary runs through the middle of the basin. The basin drains towards the southeast and towards Detention Pond C. Current planning documents call for an institutional parcel, medium and high density dwelling units and a pocket park. The basin is 77.83 acres, with a composite impervious value of 77.99% and runoff rates for the 5 and 100 year of 77.99 cfs and 238.03 cfs respectively." Only provide relevant sheets from the report. **ADDRESSED.**

A copy of the approved MDDP has been included in **Appendix E** of this report. The proposed drainage conditions for this development will follow historic drainage patterns as described in the MDDP.

## c. Proposed Subbasin Description

### Description of Proposed Project

The proposed drainage conditions for the site generally follow historic drainage patterns. The site drains from the northwest to the southeast at slopes between 0.6% - 4%, into proposed public storm sewer systems via sheetflow/curb & gutter/channel flow which drain to proposed private extended detention basins for treatment and flood attenuation. The northwestern half of the site will drain to and be treated by "Pond A", and the southeastern half of the site will drain to and be treated by "Pond B". Both of these detention ponds will outfall

into the rerouted channel MST2. Drainage from both of these ponds has been accounted for in the channel re-alignment design and is detailed in the CLOMR report.

There is no anticipated offsite flow that will enter the site.

Swales not shown on Drainage Map. Please clarify how flows will reach their intended design points and ultimately the pond. Or if any WQ exclusions are applicable.

**Subbasins Tributary to and Treated by Pond A**

**HR GREEN RESPONSE:**  
FLOWS ARE CONVEYED AT THE DP AND THEN FLOW TO THE INLET. WHILE FLOWING TO THE INLET THEY CAN COMBINE WITH THE FLOWS AT DIFFERENT A DIFFERENT DP THAN THEY WERE CONVEYED AT. FOR EXAMPLE: B1-A IS CONVEYED AT 18-A AND FLOWS TO 20-A. WHILE FLOWING TO THE INLET IT COMBINES WITH B2-1 AT 19-A.

es of landscaped area, townhome lot area, and the proposed full spect water ( $Q_5 = 2.2$  cfs  $Q_{100} = 8.5$  cfs) is conveyed via grass swales in Tract A at DP25-A.

ADDRESSED.

Per ECM Section 3.3.1.J.1 all public pipe must be RCP

es of landscaped area and townhome lot area. Stormwater ( $Q_5 = 1.7$  cfs  $Q_{100} = 4.6$  cfs) swales in a rear yard swale to the public 18" HDPE culvert crossing at DP23-A.

es of right-of-way (ROW) area, landscaped area, and townhome lot area ( $Q_5 = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at y draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

es of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.3$  cfs) is conveyed via curb and gutter in the public right-of-way to DP19-A, where flows subbasin B1-A, B3-A, and B4-A. Runoff then follows patterns of subbasin B1-A and R inlet at DP20-A, and ultimately draining to Pond A via the proposed public storm

From drainage map, Basin B4-A appears

ADDRESSED.

es of right-of-way (ROW) area, asphalt parking lot, landscaped area, ( $Q_5 = 2.6$  cfs  $Q_{100} = 5.2$  cfs) is conveyed via curb and gutter in the public right-of-way to

DP19-A, where flows combine with those of subbasin B1-A, B2-A and B4-A. Runoff then follows patterns of subbasin B1-A and drains to a public type R inlet at DP20-A, and ultimately draining to Pond A via the proposed public storm sewer network.

Basin B4-A is 0.86 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 2.3$  cfs  $Q_{100} = 4.9$  cfs) is conveyed via curb and gutter in the public right-of-way to DP18-A, where flows combine with those of subbasin B1-A. Runoff then follows patterns of subbasin B1-A and drains to DP19-A, then to a public type R inlet at DP20-A, and ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

Per routing spreadsheet, Basin B1-A combines at DP20-A

Basin C1-A is 0.56 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.5$  cfs  $Q_{100} = 3.1$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP21-A, and ultimately draining to Pond A via the proposed public storm sewer network.

Basin D1-A is 0.82 acres of landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.3$  cfs  $Q_{100} = 3.2$  cfs) is conveyed via a swale in Tract D to a public type C inlet at DP17-A, and ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

Basin E1-A is 0.18 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 0.6$  cfs  $Q_{100} = 1.2$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP14-A, and ultimately draining to Pond A via the proposed public storm sewer network.

Basin E2-A is 0.73 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.9$  cfs  $Q_{100} = 3.9$  cfs) is conveyed via curb and gutter in the public right-of-way to DP13-A, where flows combine with those of subbasin E1-A. Runoff then follows patterns of subbasin E1-A and drains to a public type R inlet at DP14-A, and ultimately draining to Pond A via the proposed public storm sewer network.

Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or

ADDRESSED.



ADDRESSED.

Basin E2-A is combined at DP 13-A according to spreadsheet. Revise report or spreadsheet to match

Basin E3-A is 0.95 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 2.7$  cfs  $Q_{100} = 5.4$  cfs) is conveyed via curb and gutter in the public right-of-way to DP12-A, where flows combine with those of subbasin E2-A, and E4-A. Runoff then follows patterns of subbasin E2-A draining to DP13-A and then drains to a public type R inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin E4-A is 1.12 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 3.0$  cfs  $Q_{100} = 6.1$  cfs) is conveyed via curb and gutter in the public right-of-way to DP12-A, where flows combine with those of subbasin E2-A, and E4-A. Runoff then follows patterns of subbasin E2-A draining to DP13-A and then drains to a public type R inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

Per routing spreadsheet combines with Basin E6-A. Revise report or spreadsheet to match

Basin E5-A is 1.23 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 3.3$  cfs  $Q_{100} = 6.7$  cfs) is conveyed via curb and gutter in the public right-of-way to DP11-A, where flows combine with those of subbasin E1-A. Runoff then follows patterns of subbasin E1-A draining to a public type R inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin E6-A is 0.96 acres of right-of-way (ROW) area, asphalt parking lot, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 2.3$  cfs  $Q_{100} = 4.8$  cfs) is conveyed via curb and gutter in the public right-of-way to DP10-A, where flows combine with those of subbasin E5-A. Runoff then follows patterns of subbasin E5-A draining to DP11-A, then to a public type R inlet at DP14-A, and ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

DP15-A per routing spreadsheet

Basin F1-A is 0.40 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.2$  cfs  $Q_{100} = 2.4$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP16-A, and ultimately draining to Pond A via the proposed public storm sewer network.

Area doesn't match with spreadsheet Please update.

Basin G1-A is 3.22 acres of landscaped area, and townhome lot area. Stormwater ( $Q_5 = 3.9$  cfs  $Q_{100} = 13.1$  cfs) is conveyed via grass swales in Tract AB to a public type R inlet at DP9-A, and ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

THERE IS A SLIGHT BIT OF TOWNHOME AREA IN THE BASIN.

Basin H1-A is 0.41 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.2$  cfs  $Q_{100} = 2.3$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP6-A, and ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

Basin H2-A is 1.05 acres of right-of-way (ROW) area, asphalt parking lot, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 2.8$  cfs  $Q_{100} = 5.6$  cfs) is conveyed via curb and gutter in the public right-of-way to DP5-A, where flows combine with those of subbasin H1-A. Runoff then follows patterns of subbasin H1-A draining to a public type R inlet at DP6-A, ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

Per routing spreadsheet, only Basins H3-A & H4-A are combined at DP3-A.

Basin H3-A is 0.70 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.9$  cfs  $Q_{100} = 4.0$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP6-A, ultimately draining to Pond A via the proposed public storm sewer network.

ADDRESSED.

ADDRESSED.

doesn't match with spreadsheet Please update.

Basin H4-A is 0.78 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 4.3$  cfs  $Q_{100} = 8.8$  cfs) is conveyed via curb and gutter in the public right-of-way to DP3-A, where flows combine with those of subbasin H1-A, H3-A, and H5-A. Runoff then follows patterns of subbasin H1-A



draining to a public type R inlet at DP6-A, ultimately draining to Pond A via the proposed public storm sewer network. **ADDRESSED.**

Area doesn't match with spreadsheet Please update.

Basin H5-A is 3.75 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 5.7$  cfs  $Q_{100} = 13.5$  cfs) is conveyed via curb and gutter in the public right-of-way to DP2-A, where flows combine with those of subbasin H1-A. Runoff then follows patterns of subbasin H1-A draining to DP3-A and then to a public type R inlet at DP6-A, ultimately draining to Pond A via the proposed public storm sewer network.

Per routing spreadsheet, Basin 5H-A combines with Basin H1-A at DP6-A. Please revise report or spreadsheet to match.

Basin I1-A is 0.63 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.3$  cfs  $Q_{100} = 2.9$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP7-A, and ultimately draining to Pond A via the proposed public storm sewer network. **ADDRESSED.**

Basin J1-A is 1.55 acres of landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.8$  cfs  $Q_{100} = 5.1$  cfs) is conveyed via grass swales in Tract O to a public type C inlet at DP4-A, and ultimately draining to Pond A via the proposed public storm sewer network. **ADDRESSED.**

Area doesn't match with spreadsheet Please update.

Basin K1-A is 0.63 acres of right-of-way (ROW) area, and landscaped area. Stormwater ( $Q_5 = 4.1$  cfs  $Q_{100} = 8.3$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP1-A, and ultimately draining to Pond A via the proposed public storm sewer network.

#### **Subbasins Tributary to and Treated by Pond B**

Please update all basin flows in this section to match with hydrology spreadsheet.

Basin A-B is 3.52 acres of landscaped area, duplex lot area, townhome lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP1-B, and ultimately draining to Pond B via the proposed public storm sewer network. **ADDRESSED.**

Basin B-B is 2.50 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP1-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin C-B is 0.85 acres of landscaped area, duplex lot area, townhome lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP2-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin D-B is 1.05 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP2-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin E-B is 4.05 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP6-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin F-B is 2.95 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP5-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin G-B is 2.15 acres of landscaped area and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP8-B, and ultimately draining to Pond B via the proposed public storm sewer network.



Swales not shown on Drainage Map. Please clarify how flows will reach their intended design points and ultimately the pond. Or if any WQ exclusions are applicable.

ADDRESSED.

Basin H-B is 4.77 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP9-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin I-B is 2.05 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP11-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin J-B is 2.77 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP13-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin K-B is 2.30 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP13-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin L-B is 2.14 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP13-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin M-B is 1.81 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP15-B, and ultimately draining to Pond B via the proposed public storm sewer network.

Basin N-B is 4.10 acres of landscaped area, and duplex lot area. Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.6$  cfs) is conveyed via rear yard swales to DP17-B in Pond B.

HR GREEN RESPONSE: TEXT UPDATED TO INDICATE Q RATIOS ARE MET THE FOR DESIGN STORMS.

THE DESIGN STORMS ARE THE WQCV, EURV, AND 100 YR STORM. THE DETENTION MEASURES ARE DESIGNED TO RELEASE THE WQCV & EURV OVER A SPECIFIC TIME DURATION FOR TREATMENT WHICH IS ACCOMPLISHED VIA THE ORIFICE PLATE. THE 100 YR STORM IS RELEASED AT LESS-THAN-HISTORIC RATES WHICH IS ACCOMPLISHED VIA THE RESTRICTOR PIPE. THE TEXT HAS BEEN UPDATED TO CLARIFY THE RELEASE RATE DESIGN STORMS.

HR GREEN RESPONSE:

Justification for 5-yr and 100-yr release rates has been provided in the "Water Quality & Detention" Section of the PDR. Per coordination with Glenn Reese on 02.27.24 we will not be required to meet pre-development flows for storms in between the 5-yr and 100-yr event.

at flow to DP17-B in Pond B

This statement conflicts with what is shown as the Q ratios on the two MHFD-Detention spreadsheet.

ge patterns. Inlets will be placed in the public ROW where the street capacity would be exceeded. Stormwater from the detention basin will be routed via a proposed public storm sewer system to a full spectrum detention pond which will discharge into MST2. All ponds and water quality features will discharge at less than historic rates.

THIS STATEMENT HAS BEEN REVISED.

b. Water Quality & Detention

Pond A (Full Spectrum Detention Basin)

Labeled on map as Gieck Ranch Trib #2. Please revise to reflect and/or to remove discrepancy.

ADDRESSED.

Water quality and detention for Basins A-A through K-A is provided in the "Water Quality & Detention" Section of the PDR. A total of 30.60 acres at 47% composite imperviousness will be detained. The pond has been sized to provide water quality treatment, and detention for up to the 100-yr storm volume to be released at or below historic rates. The WQCV is 0.505 ac-ft, the EURV is 1.630 ac-ft, and the 100-year detention volume is 2.603 ac-ft. The WQCV, EURV and 100-year storms are released in 43, 72 and 74 hours, respectively. A forebay is located at the outfall into the pond and a 4.0' trickle channel conveys flow towards the outlet structure. A 10' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 60' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate towards MST2.

ADDRESSED.

Per DCM Section 11.2.2 minimum width for access is 15'. Please revise





quality treatment for the site. The WQCV is released over a period of 40 hours while the EURV is release over a period of 72 hours.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

## VII. Drainage and Bridge Fees

Gieck Ranch drainage basin has not been established as a fee basin within El Paso County. Therefore, no drainage basin fees are due at time of platting.

## VIII. Opinion of Probable Cost

An engineer's opinion of probable cost will be provided with the Final Drainage Report (FDR) for the site.

## IX. Hydraulic Grade Line Analysis

Hydraulic grade line analysis and final pipe sizes will be provided with the FDR for the site.

## X. Summary

The Grandview Reserve Phase 2 site lies within the Gieck Ranch Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds. There is one major drainageway that traverses the site: Gieck Ranch Tributary #2. The water quality and detention features ponds will be maintained by the Grandview Reserve Metropolitan District No. 2 (DISTRICT). All drainage facilities were sized per the El Paso County Drainage Criteria Manuals.

The development of this project will not adversely affect adjacent or downstream properties.

## XI. Drawings

Refer to the appendices for vicinity and drainage basin maps.

## XII. References

1. City of Colorado Springs – Drainage Criteria Manual, May 2014, Revised January 2021.
2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
4. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
5. "Grandview Reserve Master Development Drainage Plan" prepared by HR Green, August 2021.
6. "Grandview Reserve Filing No. 1 Preliminary Drainage Report" prepared by Galloway & Company, Inc., September 2022.
7. "Grandview Reserve CLOMR REPORT" prepared by HR Green, March 2023

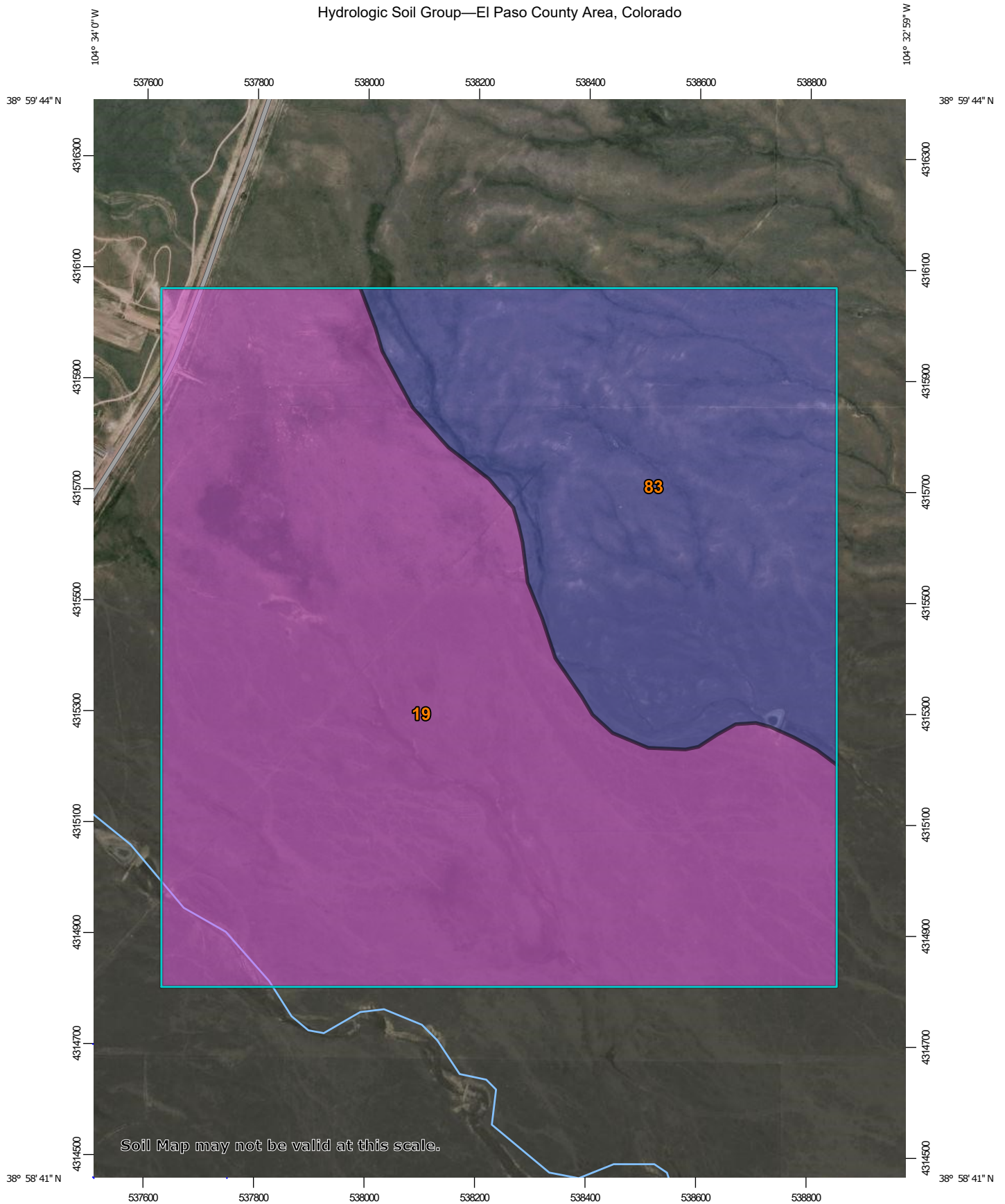
## **APPENDIX A – VICINITY MAP, PHOTOS, SOIL MAP, FEMA MAP**



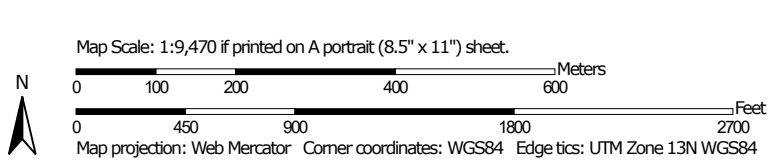




Hydrologic Soil Group—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



### MAP LEGEND

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 20, Sep 2, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Jun 12, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	254.0	66.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	B	127.8	33.5%
<b>Totals for Area of Interest</b>			<b>381.8</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method: Dominant Condition*

*Component Percent Cutoff: None Specified*

*Tie-break Rule: Higher*





**FLOOD HAZARD INFORMATION**

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR DRAFT FIRM PANEL LAYOUT

<b>SPECIAL FLOOD HAZARD AREAS</b>	Without Base Flood Elevation (BFE) Zone A, V, A99
	With BFE or Depth Zone AE, AO, AH, VE, AR
	Regulatory Floodway
<b>OTHER AREAS OF FLOOD HAZARD</b>	0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
	Future Conditions 1% Annual Chance Flood Hazard Zone X
	Area with Reduced Flood Risk due to Levee See Notes Zone X
	Area with Flood Risk due to Levee Zone D
<b>OTHER AREAS</b>	NO SCREEN Area of Minimal Flood Hazard Zone X
	Effective LOMRs
	Area of Undetermined Flood Hazard Zone D
<b>GENERAL STRUCTURES</b>	Channel, Culvert, or Storm Sewer
	Levee, Dike, or Floodwall
	20.2 Cross Sections with 1% Annual Chance
	17.5 Water Surface Elevation
	8 Coastal Transect
	Coastal Transect Baseline
	Profile Baseline
	Hydrographic Feature
<b>OTHER FEATURES</b>	Base Flood Elevation Line (BFE)
	Limit of Study
	Jurisdiction Boundary

**NOTES TO USERS**

For information and questions about this Flood Insurance Rate Map (FIRM), available products associated with this FIRM, including historic versions, the current map date for each FIRM panel, how to order products, or the National Flood Insurance Program (NFIP) in general, please call the FEMA Map Information eXchange at 1-877-FEMA-MAP (1-877-336-6627) or visit the FEMA Flood Map Service Center website at <https://msc.fema.gov>. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the website.

Communities annexing land on adjacent FIRM panels must obtain a current copy of the adjacent panel as well as the current FIRM Index. These may be ordered directly from the Flood Map Service Center at the number listed above.

For community and countywide map dates, refer to the Flood Insurance Study Report for this jurisdiction.

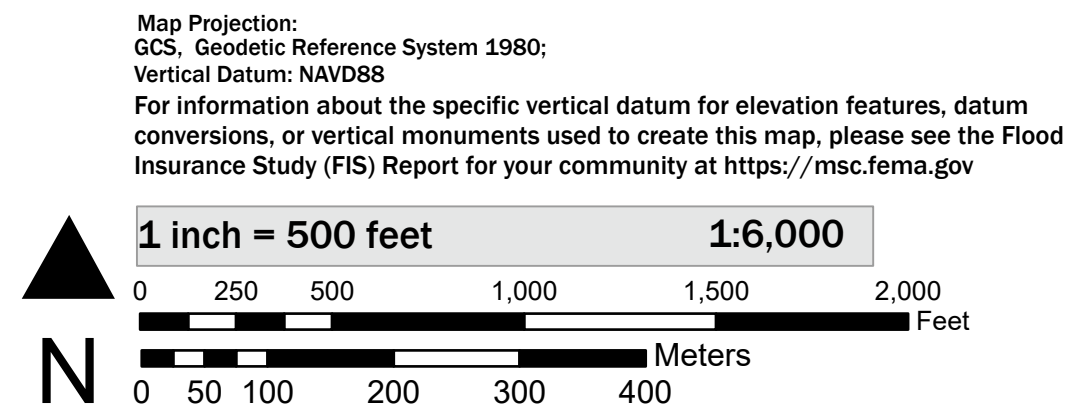
To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

Basemap information shown on this FIRM was provided in digital format by the United States Geological Survey (USGS). The basemap shown is the USGS National Map: Orthoimagery, Last refreshed October, 2020.

This map was exported from FEMA's National Flood Hazard Layer (NFHL) on 12/14/2023 3:20 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. For additional information, please see the Flood Hazard Mapping Updates Overview Fact Sheet at <https://www.fema.gov/media-library/assets/documents/118418>

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date.

**SCALE**



**NATIONAL FLOOD INSURANCE PROGRAM**  
FLOOD INSURANCE RATE MAP

PANEL 552 OF 1275

Panel Contains:  
**COMMUNITY** EL PASO COUNTY      **NUMBER** 080059      **PANEL** 0552





**FLOOD HAZARD INFORMATION**

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR DRAFT FIRM PANEL LAYOUT

<b>SPECIAL FLOOD HAZARD AREAS</b>		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
<b>OTHER AREAS OF FLOOD HAZARD</b>		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee See Notes Zone X
		Area with Flood Risk due to Levee Zone D
<b>OTHER AREAS</b>		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
		Area of Undetermined Flood Hazard Zone D
<b>GENERAL STRUCTURES</b>		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
		20.2 Cross Sections with 1% Annual Chance
		17.5 Water Surface Elevation
		8 Coastal Transect
		Coastal Transect Baseline
		Profile Baseline
		Hydrographic Feature
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		Limit of Study
		Jurisdiction Boundary

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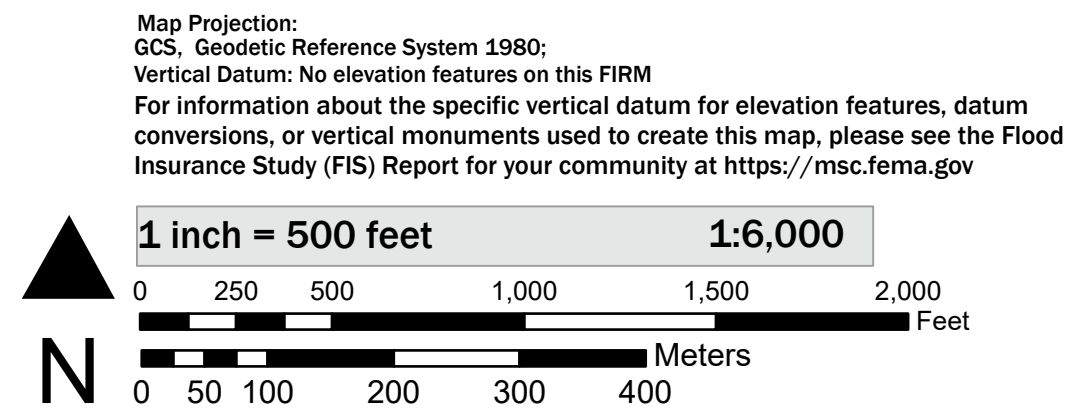
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This map was exported from FEMA's National Flood Hazard Layer (NFHL) on 12/14/2023 3:22 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. For additional information, please see the Flood Hazard Mapping Updates Overview Fact Sheet at <https://www.fema.gov/media-library/assets/documents/118418>

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date.

**SCALE**

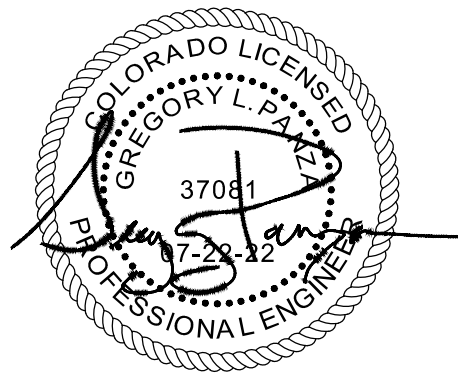
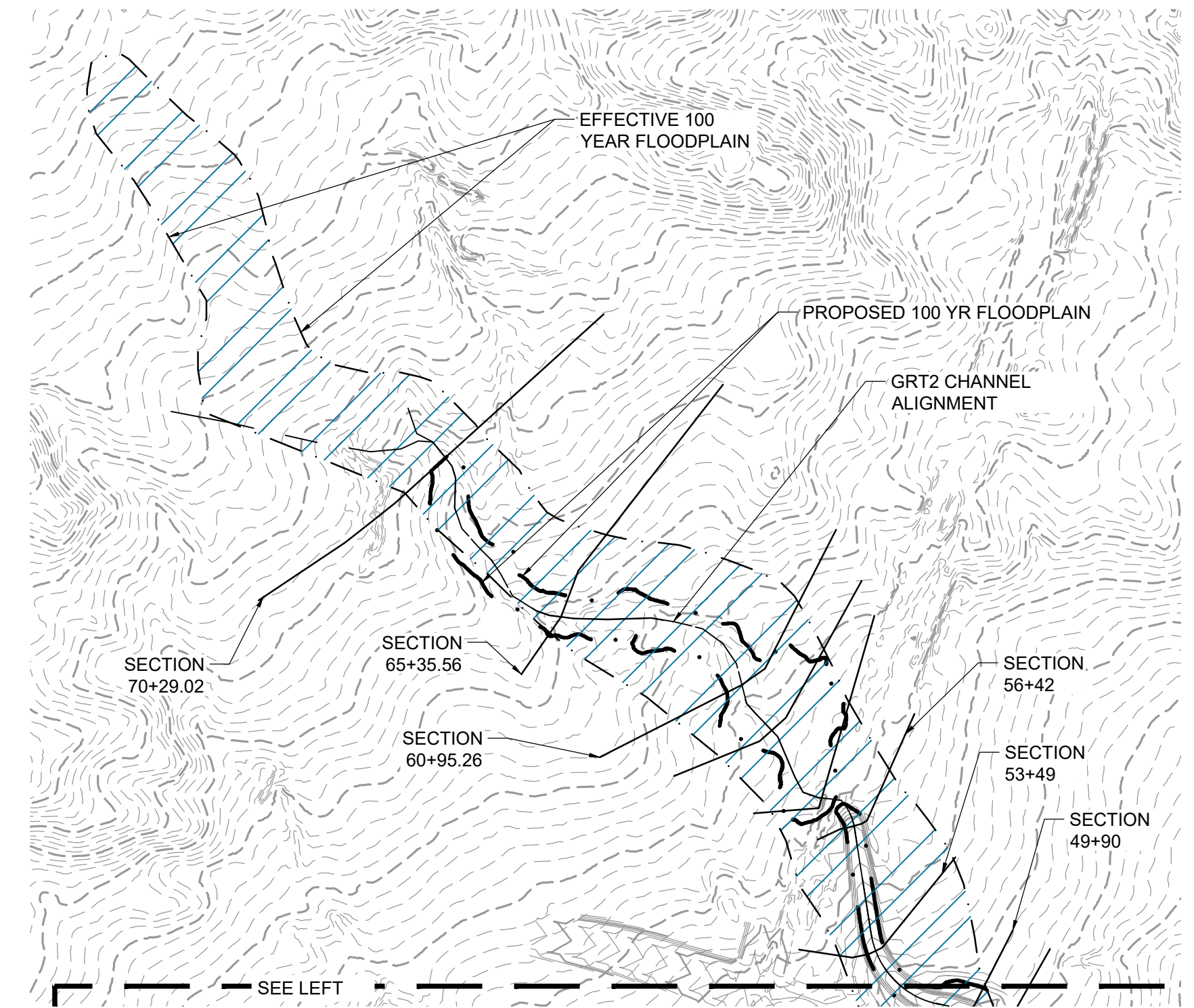
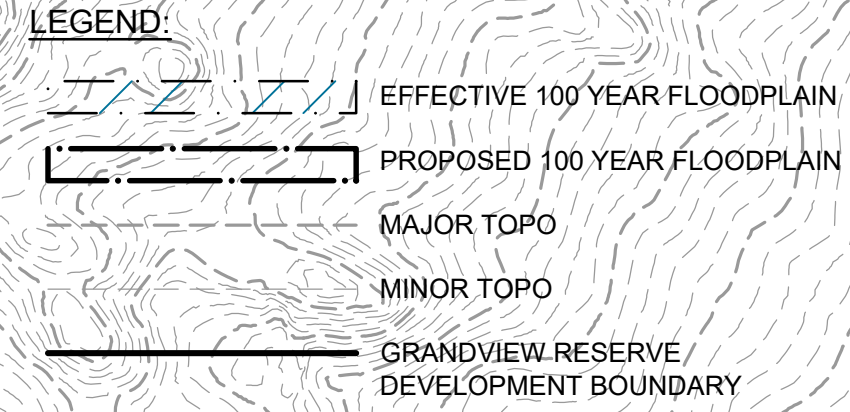
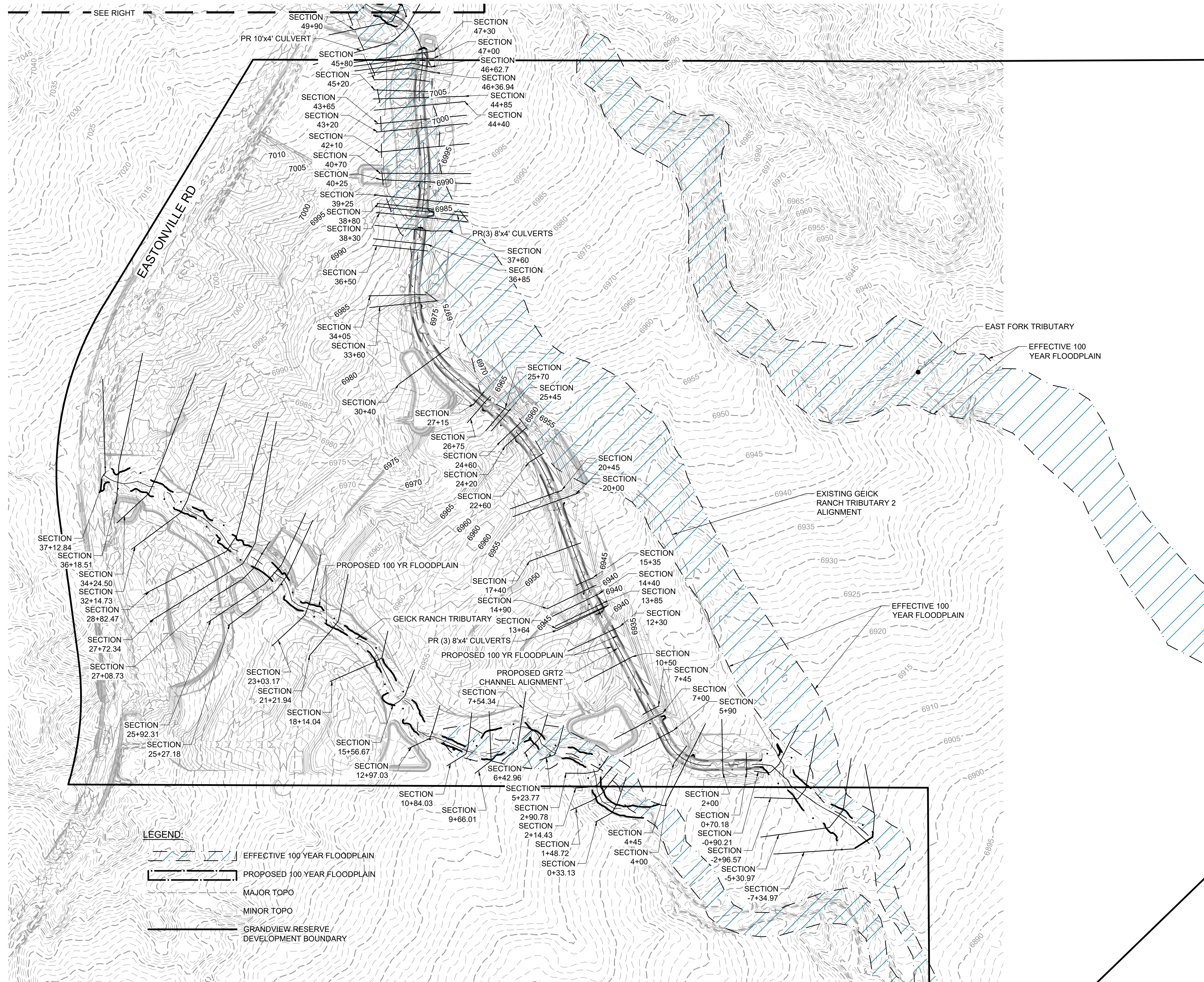


**NATIONAL FLOOD INSURANCE PROGRAM**  
FLOOD INSURANCE RATE MAP

PANEL 556 OF 1275

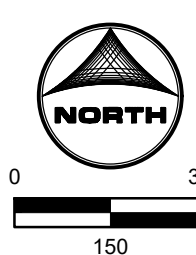
Panel Contains:  
**COMMUNITY** EL PASO COUNTY      **NUMBER** 080059      **PANEL** 0556





**NOTES:**  
 1. BASIS OF BEARINGS: THE EAST LINE OF SECTION 21, BEING MONUMENTED AT THE SOUTHEAST CORNER BY A 3-1/4" ALUMINUM SURVEYOR'S CAP STAMPED "PS INC PLS 30087 1998", BEING APPROPRIATELY MARKED, AND BEING MONUMENTED AT THE NORTHEAST CORNER BY A 3-1/4" ALUMINUM SURVEYOR'S CAP STAMPED "PS INC PLS 30087 1998", BEING APPROPRIATELY MARKED, BEING ASSUMED TO BEAR NORTH 00 DEGREES 52 MINUTES 26 SECONDS WEST, A DISTANCE OF 5290.17 FEET.

NAVD88



Job No.:	201662
Prepared By:	SJF
Date:	3/21/2023

FLOODPLAIN EXHIBIT



## **APPENDIX B – HYDROLOGIC CALCULATIONS**



**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Peyton, Colorado, USA\***  
**Latitude: 38.9877°, Longitude: -104.5596°**  
**Elevation: 6971 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps\\_&\\_aerials](#)

**PF tabular**

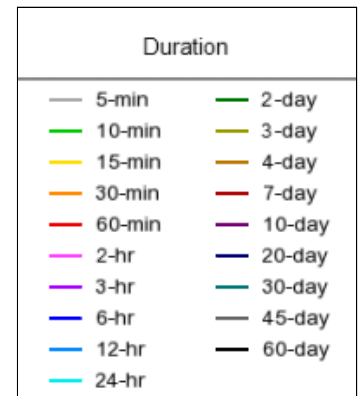
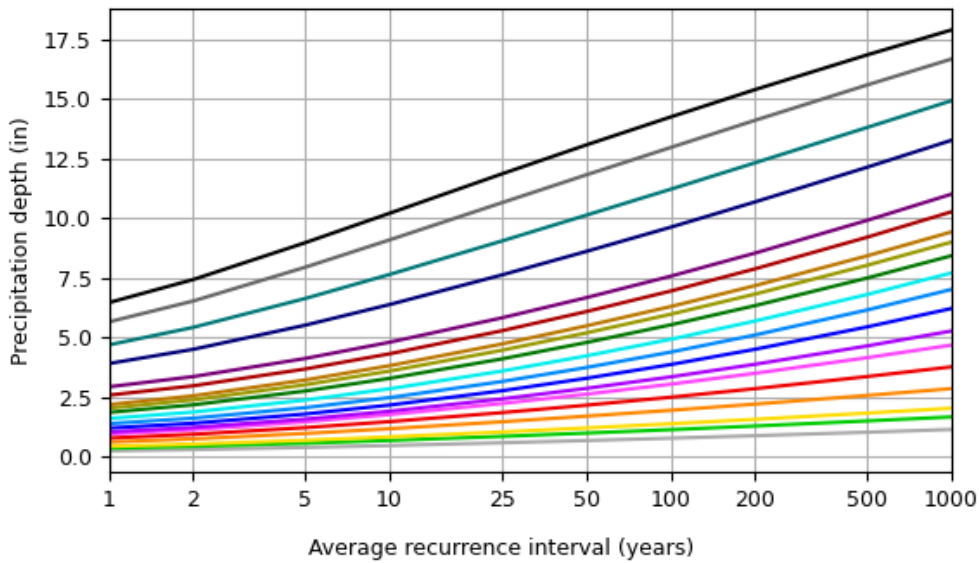
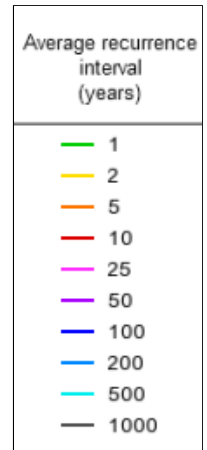
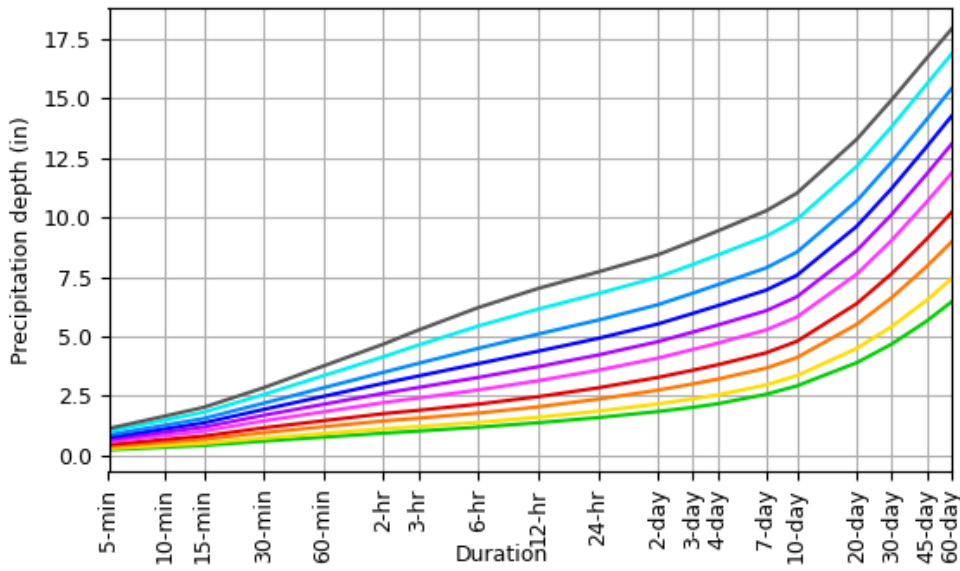
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.239</b> (0.189-0.304)	<b>0.291</b> (0.230-0.371)	<b>0.382</b> (0.300-0.487)	<b>0.461</b> (0.360-0.591)	<b>0.576</b> (0.438-0.771)	<b>0.670</b> (0.497-0.906)	<b>0.769</b> (0.552-1.06)	<b>0.874</b> (0.602-1.24)	<b>1.02</b> (0.675-1.48)	<b>1.14</b> (0.731-1.67)
<b>10-min</b>	<b>0.350</b> (0.276-0.446)	<b>0.427</b> (0.337-0.544)	<b>0.559</b> (0.439-0.714)	<b>0.675</b> (0.528-0.866)	<b>0.844</b> (0.642-1.13)	<b>0.982</b> (0.728-1.33)	<b>1.13</b> (0.808-1.56)	<b>1.28</b> (0.881-1.82)	<b>1.49</b> (0.989-2.17)	<b>1.66</b> (1.07-2.44)
<b>15-min</b>	<b>0.427</b> (0.337-0.543)	<b>0.520</b> (0.410-0.663)	<b>0.681</b> (0.536-0.870)	<b>0.823</b> (0.643-1.06)	<b>1.03</b> (0.783-1.38)	<b>1.20</b> (0.888-1.62)	<b>1.37</b> (0.985-1.90)	<b>1.56</b> (1.07-2.22)	<b>1.82</b> (1.21-2.65)	<b>2.03</b> (1.30-2.98)
<b>30-min</b>	<b>0.607</b> (0.480-0.773)	<b>0.740</b> (0.583-0.942)	<b>0.967</b> (0.761-1.24)	<b>1.17</b> (0.912-1.50)	<b>1.46</b> (1.11-1.95)	<b>1.69</b> (1.26-2.29)	<b>1.94</b> (1.39-2.68)	<b>2.20</b> (1.51-3.12)	<b>2.56</b> (1.70-3.73)	<b>2.85</b> (1.83-4.19)
<b>60-min</b>	<b>0.774</b> (0.611-0.985)	<b>0.932</b> (0.735-1.19)	<b>1.21</b> (0.952-1.55)	<b>1.46</b> (1.14-1.88)	<b>1.84</b> (1.40-2.47)	<b>2.15</b> (1.60-2.92)	<b>2.49</b> (1.79-3.45)	<b>2.85</b> (1.96-4.05)	<b>3.35</b> (2.22-4.90)	<b>3.76</b> (2.42-5.54)
<b>2-hr</b>	<b>0.941</b> (0.749-1.19)	<b>1.12</b> (0.894-1.42)	<b>1.46</b> (1.15-1.84)	<b>1.76</b> (1.39-2.24)	<b>2.22</b> (1.71-2.97)	<b>2.61</b> (1.96-3.52)	<b>3.03</b> (2.20-4.19)	<b>3.49</b> (2.43-4.94)	<b>4.14</b> (2.78-6.02)	<b>4.68</b> (3.04-6.84)
<b>3-hr</b>	<b>1.03</b> (0.824-1.29)	<b>1.22</b> (0.973-1.53)	<b>1.57</b> (1.25-1.98)	<b>1.90</b> (1.50-2.40)	<b>2.41</b> (1.88-3.23)	<b>2.86</b> (2.16-3.85)	<b>3.34</b> (2.44-4.60)	<b>3.87</b> (2.72-5.47)	<b>4.64</b> (3.13-6.72)	<b>5.27</b> (3.44-7.67)
<b>6-hr</b>	<b>1.19</b> (0.961-1.48)	<b>1.40</b> (1.12-1.74)	<b>1.78</b> (1.43-2.23)	<b>2.16</b> (1.72-2.71)	<b>2.76</b> (2.17-3.67)	<b>3.28</b> (2.50-4.40)	<b>3.86</b> (2.85-5.29)	<b>4.50</b> (3.19-6.33)	<b>5.44</b> (3.70-7.84)	<b>6.21</b> (4.10-8.98)
<b>12-hr</b>	<b>1.38</b> (1.12-1.70)	<b>1.61</b> (1.30-1.98)	<b>2.05</b> (1.66-2.53)	<b>2.47</b> (1.99-3.07)	<b>3.14</b> (2.49-4.15)	<b>3.73</b> (2.87-4.96)	<b>4.38</b> (3.26-5.96)	<b>5.10</b> (3.64-7.12)	<b>6.14</b> (4.23-8.80)	<b>7.01</b> (4.67-10.1)
<b>24-hr</b>	<b>1.59</b> (1.30-1.95)	<b>1.86</b> (1.52-2.28)	<b>2.37</b> (1.93-2.90)	<b>2.84</b> (2.30-3.50)	<b>3.58</b> (2.86-4.66)	<b>4.22</b> (3.27-5.55)	<b>4.92</b> (3.69-6.62)	<b>5.68</b> (4.09-7.86)	<b>6.79</b> (4.71-9.65)	<b>7.70</b> (5.17-11.0)
<b>2-day</b>	<b>1.85</b> (1.53-2.24)	<b>2.17</b> (1.79-2.63)	<b>2.75</b> (2.26-3.34)	<b>3.28</b> (2.68-4.00)	<b>4.09</b> (3.28-5.26)	<b>4.78</b> (3.73-6.21)	<b>5.52</b> (4.17-7.36)	<b>6.33</b> (4.59-8.67)	<b>7.48</b> (5.23-10.5)	<b>8.42</b> (5.71-12.0)
<b>3-day</b>	<b>2.02</b> (1.68-2.44)	<b>2.38</b> (1.97-2.86)	<b>3.01</b> (2.48-3.64)	<b>3.58</b> (2.94-4.35)	<b>4.45</b> (3.58-5.68)	<b>5.18</b> (4.06-6.69)	<b>5.97</b> (4.52-7.90)	<b>6.81</b> (4.97-9.28)	<b>8.02</b> (5.63-11.2)	<b>8.99</b> (6.13-12.7)
<b>4-day</b>	<b>2.17</b> (1.81-2.61)	<b>2.55</b> (2.12-3.06)	<b>3.21</b> (2.66-3.86)	<b>3.81</b> (3.14-4.61)	<b>4.72</b> (3.80-6.00)	<b>5.48</b> (4.31-7.04)	<b>6.29</b> (4.79-8.30)	<b>7.17</b> (5.24-9.73)	<b>8.42</b> (5.93-11.8)	<b>9.42</b> (6.45-13.3)
<b>7-day</b>	<b>2.57</b> (2.16-3.06)	<b>2.97</b> (2.48-3.54)	<b>3.67</b> (3.06-4.39)	<b>4.31</b> (3.58-5.17)	<b>5.27</b> (4.28-6.64)	<b>6.08</b> (4.81-7.76)	<b>6.94</b> (5.32-9.09)	<b>7.87</b> (5.80-10.6)	<b>9.20</b> (6.53-12.8)	<b>10.3</b> (7.08-14.4)
<b>10-day</b>	<b>2.92</b> (2.46-3.46)	<b>3.35</b> (2.82-3.98)	<b>4.11</b> (3.44-4.89)	<b>4.79</b> (3.99-5.73)	<b>5.81</b> (4.73-7.28)	<b>6.66</b> (5.29-8.45)	<b>7.56</b> (5.82-9.85)	<b>8.53</b> (6.32-11.4)	<b>9.90</b> (7.06-13.7)	<b>11.0</b> (7.63-15.4)
<b>20-day</b>	<b>3.90</b> (3.31-4.57)	<b>4.50</b> (3.81-5.28)	<b>5.51</b> (4.65-6.49)	<b>6.37</b> (5.36-7.55)	<b>7.61</b> (6.22-9.37)	<b>8.60</b> (6.87-10.8)	<b>9.62</b> (7.44-12.4)	<b>10.7</b> (7.95-14.1)	<b>12.1</b> (8.71-16.6)	<b>13.3</b> (9.28-18.4)
<b>30-day</b>	<b>4.68</b> (3.99-5.46)	<b>5.42</b> (4.61-6.33)	<b>6.63</b> (5.63-7.76)	<b>7.64</b> (6.45-8.99)	<b>9.03</b> (7.39-11.0)	<b>10.1</b> (8.11-12.5)	<b>11.2</b> (8.70-14.3)	<b>12.3</b> (9.20-16.2)	<b>13.8</b> (9.95-18.7)	<b>14.9</b> (10.5-20.6)
<b>45-day</b>	<b>5.64</b> (4.84-6.55)	<b>6.52</b> (5.58-7.58)	<b>7.94</b> (6.77-9.25)	<b>9.09</b> (7.71-10.6)	<b>10.6</b> (8.73-12.8)	<b>11.8</b> (9.49-14.5)	<b>13.0</b> (10.1-16.4)	<b>14.1</b> (10.6-18.4)	<b>15.6</b> (11.3-21.0)	<b>16.7</b> (11.8-22.9)
<b>60-day</b>	<b>6.45</b> (5.55-7.46)	<b>7.42</b> (6.37-8.59)	<b>8.96</b> (7.68-10.4)	<b>10.2</b> (8.69-11.9)	<b>11.8</b> (9.74-14.2)	<b>13.1</b> (10.5-16.0)	<b>14.2</b> (11.1-17.9)	<b>15.4</b> (11.6-20.0)	<b>16.8</b> (12.2-22.6)	<b>17.9</b> (12.7-24.6)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**PF graphical**

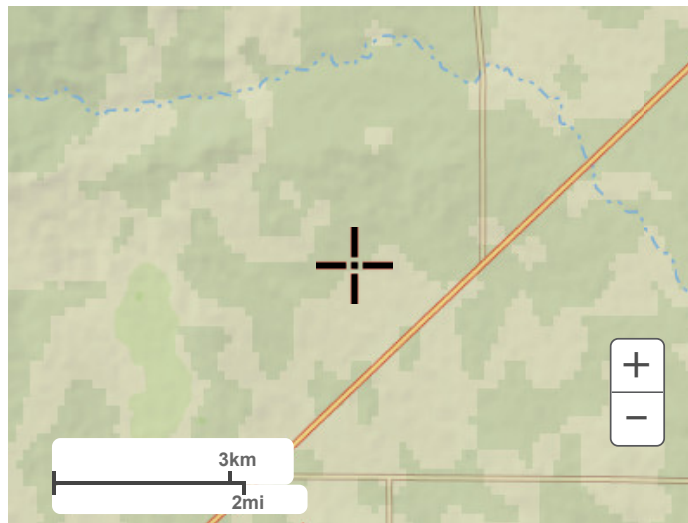
PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 38.9877°, Longitude: -104.5596°



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**Maps & aerials**

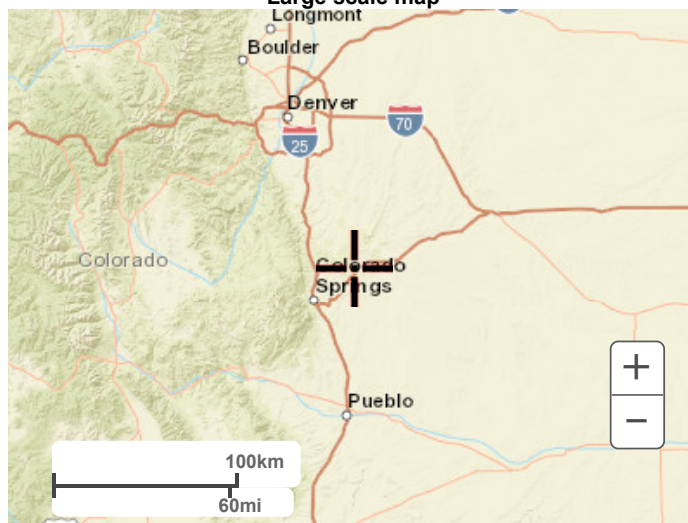
**Small scale terrain**



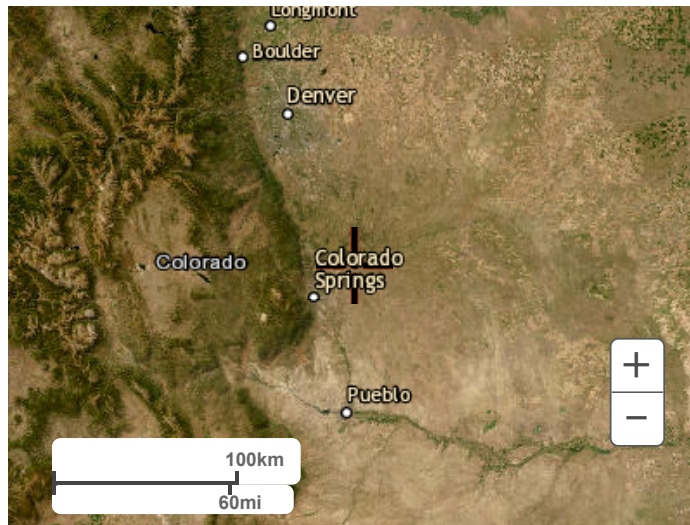
Large scale terrain



Large scale map



Large scale aerial



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[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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**GRANDVIEW RESERVE (PHASE II)**  
**PROPOSED CONDITIONS**  
**EL PASO COUNTY, CO**

**Calc'd by:** SPC  
**Checked by:** KH  
**Date:** 12/15/2023

SUMMARY RUNOFF TABLE				
BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
A1-A	3.22	14	2.2	8.5
A2-A	1.23	35	1.7	4.6
B1-A	0.26	79	0.8	1.6
B2-A	1.02	64	2.6	5.3
B3-A	0.87	69	2.6	5.2
B4-A	0.86	61	2.3	4.9
C1-A	0.56	67	1.5	3.1
D1-A	0.82	38	1.3	3.2
E1-A	0.18	77	0.6	1.2
E2-A	0.73	67	1.9	3.9
E3-A	0.95	69	2.7	5.4
E4-A	1.12	66	3.0	6.1
E5-A	1.23	68	3.3	6.7
E6-A	0.96	63	2.3	4.8
F1-A	0.40	68	1.2	2.4
G1-A	4.69	20	3.9	13.1
H1-A	0.41	70	1.2	2.3
H2-A	1.05	70	2.8	5.6
H3-A	0.70	63	1.9	4.0
H4-A	1.78	66	4.3	8.8
H5-A	3.72	44	5.7	13.5
I1-A	0.63	57	1.3	2.9
J1-A	1.55	28	1.8	5.1
K1-A	1.66	68	4.1	8.3

DESIGN POINT SUMMARY TABLE			
DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>5</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
1-A	K1-A	4.1	8.3
2-A	H5-A	5.7	13.5
2.1-A	DPS 1-A, 2-A	9.4	21.0
3-A	H3-A, H4-A	6.0	12.3
4-A	J1-A	1.8	5.1
4.1-A	DPS 2.1-A, 4-A	10.5	24.4
5-A	H2-A	2.8	5.6
6-A	H1-A, DPS 3-A, 5-A	8.7	17.8
7-A	I1-A	1.3	2.9
8-A	DPS 4.1-A, 6-A, 7-A	19.6	43.2
9-A	G1-A	3.9	13.1
9.1-A	DPS 8-A, 9-A	22.7	54.0
10-A	E6-A	2.3	4.8
11-A	E5-A, DPS 10-A	4.2	8.5
12-A	E3-A, E4-A	5.6	11.5
13-A	E2-A, DPS 12-A	6.4	12.9
14-A	E1-A, DPS 11-A, 13-A	8.9	18.2
15-A	F1-A	1.2	2.4
16-A	DPS 9.1-A, 14-A, 15-A	29.1	65.9
17-A	D1-A	1.3	3.2
17.1-A	DPS 16-A, 17-A	29.5	67.2
18-A	B4-A	2.3	4.9
19-A	B2-A, B3-A, DPS 18-A	6.3	12.9
20-A	B1-A, DPS 19-A	6.6	13.5
21-A	C1-A	1.5	3.1
22-A	DPS 17.1-A, 20-A, 21-A	34.9	78.0
23-A	A2-A	1.7	4.6
24-A	DPS 23-A	1.7	4.5
25-A	A1-A, DPS 22-A, 24-A	37.6	87.1



**GRANDVIEW RESERVE (PHASE II)**  
**PROPOSED CONDITIONS**  
 EL PASO COUNTY, CO

**Calc'd by:** SPC  
**Checked by:** KH  
**Date:** 12/15/2023

**SOIL TYPE:** HSG A&B

<b>COMPOSITE 'C' FACTORS</b>																						
<b>BASIN</b>	<b>LAND USE TYPE</b>																		<b>TOTAL</b>	<b>COMPOSITE IMPERVIOUSNESS &amp; C FACTOR</b>		
	<b>Paved</b>			<b>Gravel</b>			<b>Lawns</b>			<b>Typical Townhome Lots</b>			<b>Minor Arterial ROW Typ.</b>			<b>Local ROW Typ.</b>						
	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>				
	<b>100</b>	<b>0.90</b>	<b>0.96</b>	<b>80</b>	<b>0.59</b>	<b>0.70</b>	<b>0</b>	<b>0.08</b>	<b>0.35</b>	<b>53</b>	<b>0.48</b>	<b>0.64</b>	<b>68</b>	<b>0.63</b>	<b>0.76</b>	<b>90</b>	<b>0.82</b>	<b>0.90</b>				
<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	
A1-A				0.14			2.42			0.66								3.22	14	0.18	0.42	
A2-A							0.41			0.82								1.23	35	0.35	0.54	
B1-A							0.03								0.23			0.26	79	0.73	0.83	
B2-A							0.06			0.56					0.40			1.02	64	0.59	0.72	
B3-A	0.09						0.07			0.37					0.34			0.87	69	0.63	0.76	
B4-A							0.09			0.46					0.31			0.86	61	0.56	0.70	
C1-A							0.01			0.33					0.22			0.56	67	0.61	0.74	
D1-A							0.23			0.59								0.82	38	0.37	0.56	
E1-A							0.03								0.15			0.18	77	0.71	0.82	
E2-A							0.05			0.32					0.35			0.73	67	0.62	0.74	
E3-A							0.00			0.54					0.41			0.95	69	0.63	0.75	
E4-A							0.02			0.68					0.41			1.12	66	0.60	0.73	
E5-A	0.09						0.05			0.65					0.44			1.23	68	0.62	0.75	
E6-A	0.09						0.18			0.27					0.41			0.96	63	0.59	0.73	
F1-A							0.00			0.23					0.17			0.40	68	0.62	0.75	
G1-A							2.96			1.73								4.69	20	0.23	0.46	
H1-A							0.09								0.32			0.41	70	0.65	0.78	
H2-A	0.10						0.05			0.49					0.42			1.05	70	0.64	0.76	
H3-A							0.07			0.33					0.30			0.70	63	0.58	0.72	
H4-A							0.02			1.12					0.64			1.78	66	0.60	0.73	
H5-A							1.04			1.14			1.54					3.72	44	0.43	0.61	
I1-A							0.15			0.21					0.28			0.63	57	0.54	0.69	
J1-A							0.74			0.81								1.55	28	0.29	0.50	
K1-A							0.00						1.66					1.66	68	0.63	0.76	
POND A	0.38			0.14			8.76			12.31			3.20		5.80			30.60	47	0.45	0.62	



**GRANDVIEW RESERVE (PHASE II)**  
**PROPOSED CONDITIONS**  
**EL PASO COUNTY, CO**

Calc'd by: **SPC**  
 Checked by: **KH**  
 Date: **12/15/2023**

**TIME OF CONCENTRATION**

BASIN DATA			OVERLAND TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )					TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C <sub>s</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>v</sub>	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)	tc max	tc design (min)
A1-A	0.18	3.22	100	2.8	11.9	7	529	2.9	1.2	7.3	19.2	13.5	13.5
A2-A	0.35	1.23	68	4.9	6.7	15	470	2.2	2.2	3.5	10.2	13.0	10.2
B1-A	0.73	0.26	41	0.5	5.4	20	340	0.6	1.5	3.7	9.1	12.1	9.1
B2-A	0.59	1.02	32	0.7	6.1	20	614	2.9	3.4	3.0	9.2	13.6	9.2
B3-A	0.63	0.87	42	2.9	3.9	20	544	2.9	3.4	2.7	6.6	13.3	6.6
B4-A	0.56	0.86	43	4.8	3.8	20	480	2.7	3.3	2.4	6.3	12.9	6.3
C1-A	0.61	0.56	53	2.9	4.6	20	318	0.6	1.5	3.4	8.0	12.1	8.0
D1-A	0.37	0.82	100	4.6	8.1	15	196	2.3	2.3	1.4	9.5	11.6	9.5
E1-A	0.71	0.18	41	1.0	4.5	20	186	1.0	2.0	1.5	6.1	11.3	6.1
E2-A	0.62	0.73	38	0.6	6.4	20	570	2.8	3.3	2.9	9.2	13.4	9.2
E3-A	0.63	0.95	68	4.2	4.4	20	656	2.6	3.2	3.4	7.8	14.0	7.8
E4-A	0.60	1.12	66	4.5	4.5	20	656	2.4	3.1	3.5	8.1	14.0	8.1
E5-A	0.62	1.23	54	3.0	4.5	20	677	1.8	2.7	4.2	8.7	14.1	8.7
E6-A	0.59	0.96	74	1.0	8.0	20	495	3.5	3.7	2.2	10.2	13.2	10.2
F1-A	0.62	0.40	63	3.0	4.8	20	197	1.0	2.0	1.6	6.5	11.4	6.5
G1-A	0.23	4.69	100	10.0	7.4	15	822	2.0	2.1	6.5	13.9	15.1	13.9
H1-A	0.65	0.41	79	2.0	5.8	20	284	0.6	1.5	3.0	8.8	12.0	8.8
H2-A	0.64	1.05	41	0.8	5.9	20	667	2.0	2.8	3.9	9.8	13.9	9.8
H3-A	0.58	0.70	41	2.8	4.3	20	467	2.5	3.2	2.5	6.7	12.8	6.7
H4-A	0.60	1.78	62	2.5	5.3	20	1089	3.0	3.5	5.2	10.5	16.4	10.5
H5-A	0.43	3.72	100	4.8	7.3	20	1343	2.3	3.0	7.4	14.7	18.0	14.7
I1-A	0.54	0.63	81	0.6	11.0	20	114	0.6	1.5	1.2	12.2	11.1	11.1
J1-A	0.29	1.55	100	4.5	9.0	15	321	2.4	2.3	2.3	11.3	12.3	11.3
K1-A	0.63	1.66	45	3.4	3.8	20	1409	2.4	3.1	7.6	11.4	18.1	11.4

**FORMULAS:**

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S^{0.33}} \quad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C<sub>v</sub>

Type of Land Surface	C <sub>v</sub>
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

\*For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.



ADDRESSED.

Labels appear to be switched for these 2 columns

**GRANDVIEW RESERVE (PHASE II)**  
**PROPOSED CONDITIONS**  
**DESIGN STORM: 5-YEAR**

Calc'd by:

Checked by:

Date:

SPC

KH

12/15/2023

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE				TRAVEL TIME		REMARKS	
			AREA (ac)	C <sub>s</sub>	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)		VEL. (FPS)
	1-A	K1-A	0.63	1.66	11.4	1.05	3.93	4.1	11.4	1.05	3.93	4.1			4.1	1.05	0.5	1.5	85	2.1	0.67	
	2-A	H5-A	0.43	3.72	14.7	1.60	3.55	5.7	14.7	1.60	3.55	5.7			5.7	1.60	0.5	1.5	6	2.1	0.04	
	2.1-A								14.7	2.65	3.55	9.4			9.4	2.65	0.5	2.0	300	2.9	1.70	
	3-A	H3-A	0.58	0.70	6.7	0.41	4.72	1.9	10.5	1.47	4.05	6.0	6.0	1.47	0.6				160	0.8	3.44	
		H4-A	0.60	1.78	10.5	1.07	4.05	4.3														
	4-A	J1-A	0.29	1.55	11.3	0.45	3.94	1.8	11.3	0.45	3.94	1.8			1.8	0.45	0.5	1.5	26	2.1	0.21	
	4.1-A								16.4	3.09	3.39	10.5			10.5	3.09	0.5	2.0	46	2.9	0.26	
	5-A	H2-A	0.64	1.05	9.8	0.67	4.16	2.8	9.8	0.67	4.16	2.8	2.8	0.67	0.6				80	0.8	1.72	
	6-A	H1-A	0.65	0.41	8.8	0.27	4.32	1.2	14.0	2.41	3.63	8.7			8.7	2.41	0.5	1.5	3	2.1	0.02	
	7-A	I1-A	0.54	0.63	11.1	0.34	3.98	1.3	11.1	0.34	3.98	1.3			1.3	0.34	0.5	1.0	28	1.3	0.35	
	8-A								16.7	5.84	3.36	19.6			19.6	5.84	0.5	3.0	250	4.7	0.88	
	9-A	G1-A	0.23	4.69	13.9	1.07	3.64	3.9	13.9	1.07	3.64	3.9			3.9	1.07	0.5	1.0	24	1.3	0.31	
	9.1-A								17.6	6.91	3.28	22.7			22.7	6.91	0.5	3.0	86	4.7	0.30	
	10-A	E6-A	0.59	0.96	10.2	0.57	4.10	2.3	10.2	0.57	4.10	2.3	2.3	0.57	1.8				731	1.3	9.08	
	11-A	E5-A	0.62	1.23	8.7	0.76	4.34	3.3	19.3	1.33	3.14	4.2	4.2	1.33	0.6				217	0.8	4.67	
	12-A	E3-A	0.63	0.95	7.8	0.60	4.50	2.7	8.1	1.27	4.45	5.6	5.6	1.27	2.7				506	1.6	5.16	
		E4-A	0.60	1.12	8.1	0.67	4.45	3.0														
	13-A	E2-A	0.62	0.73	9.2	0.45	4.25	1.9	13.2	1.71	3.71	6.4	6.4	1.71	0.6				25	0.8	0.54	
	14-A	E1-A	0.71	0.18	6.1	0.13	4.88	0.6	24.0	3.17	2.82	8.9			8.9	3.17	0.5	2.0	6	2.9	0.03	
	15-A	F1-A	0.62	0.40	6.5	0.25	4.78	1.2	6.5	0.25	4.78	1.2			1.2	0.25	0.5	1.5	29	2.1	0.23	
	16-A								24.0	10.33	2.82	29.1			29.1	10.33	0.5	3.0	173	4.7	0.61	



**GRANDVIEW RESERVE (PHASE II)**  
**PROPOSED CONDITIONS**  
**DESIGN STORM: 5-YEAR**

**Calc'd by:**  
**Checked by:**  
**Date:**

**SPC**  
**KH**  
**12/15/2023**

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE				TRAVEL TIME			REMARKS				
			AREA (ac)	C <sub>s</sub>	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)	VEL. (FPS)		TRAVEL TIME (min)			
	17-A	D1-A	0.37	0.82	9.5	0.30	4.20	1.3	9.5	0.30	4.20	1.3						1.3	0.30	0.5	1.5	26	2.1	0.21		
	17.1-A								24.6	10.63	2.78	29.5			29.5	10.63	0.5	3.0	241	4.7	0.85					
	18-A	B4-A	0.56	0.86	6.3	0.48	4.83	2.3	6.3	0.48	4.83	2.3	2.3	0.48	0.6						268	0.8	5.77			
	19-A	B2-A	0.59	1.02	9.2	0.60	4.26	2.6	12.1	1.63	3.85	6.3	6.3	1.63	0.6						85	0.8	1.83			
		B3-A	0.63	0.87	6.6	0.55	4.75	2.6																		
	20-A	B1-A	0.73	0.26	9.1	0.19	4.27	0.8	13.9	1.82	3.64	6.6			6.6	1.82	0.5	1.5	6	2.1	0.04					
	21-A	C1-A	0.61	0.56	8.0	0.34	4.47	1.5	8.0	0.34	4.47	1.5			1.5	0.34	0.5	1.5	29	2.1	0.23					
	22-A								25.5	12.79	2.73	34.9			34.9	12.79	0.5	3.0	34	4.7	0.12					
	23-A	A2-A	0.35	1.23	10.2	0.43	4.10	1.7	10.2	0.43	4.10	1.7			1.7	0.43	0.5	1.5	80	2.1	0.63					
	24-A								10.9	0.43	4.01	1.7	1.7	0.43	2.0						400	1.4	4.71			
	25-A	A1-A	0.18	3.22	13.5	0.59	3.68	2.2	25.6	13.81	2.72	37.6														



**GRANDVIEW RESERVE (PHASE II)**

**PROPOSED CONDITIONS**

**DESIGN STORM: 100-YEAR**

Calc'd by:

SPC

Checked by:

KH

Date:

12/15/2023

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF						TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS
			AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	f (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	f (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	
	1-A	K1-A	1.66	0.76	11.4	1.26	6.60	8.3	11.4	1.26	6.60	8.3			8.3	1.26	0.5	1.5	85	2.1	0.67	
	2-A	H5-A	3.72	0.61	14.7	2.26	5.97	13.5	14.7	2.26	5.97	13.5			13.5	2.26	0.5	1.5	6	2.1	0.04	
	2.1-A				14.7	3.53	5.96	21.0	14.7	3.53	5.96	21.0			21.0	3.53	0.5	2.0	300	2.9	1.70	
	3-A	H3-A	0.70	0.72	6.7	0.50	7.92	4.0	10.5	1.81	6.80	12.3	12.3	1.81	0.6				160	0.8	3.44	
		H4-A	1.78	0.73	10.5	1.30	6.80	8.8														
	4-A	J1-A	1.55	0.50	11.3	0.78	6.62	5.1	11.3	0.78	6.62	5.1			5.1	0.78	0.5	1.5	26	2.1	0.21	
	4.1-A				16.4	4.30	5.68	24.4							24.4	4.30	0.5	2.0	46	2.9	0.26	
	5-A	H2-A	1.05	0.76	9.8	0.80	6.98	5.6	9.8	0.80	6.98	5.6	5.6	0.80	0.6				80	0.8	1.72	
	6-A	H1-A	0.41	0.78	8.8	0.32	7.25	2.3	14.0	2.92	6.09	17.8			17.8	2.92	0.5	1.5	3	2.1	0.02	
	7-A	I1-A	0.63	0.69	11.1	0.43	6.67	2.9	11.1	0.43	6.67	2.9			2.9	0.43	0.5	1.0	28	1.3	0.35	
	8-A				16.7	7.66	5.64	43.2							43.2	7.66	0.5	3.0	250	4.7	0.88	
	9-A	G1-A	4.69	0.46	13.9	2.14	6.11	13.1	13.9	2.14	6.11	13.1			13.1	2.14	0.5	1.0	24	1.3	0.31	
	9.1-A				17.6	9.80	5.51	54.0							54.0	9.80	0.5	3.0	86	4.7	0.30	
	10-A	E6-A	0.96	0.73	10.2	0.70	6.88	4.8	10.2	0.70	6.88	4.8	4.8	0.70	1.8				731	1.3	9.08	
	11-A	E5-A	1.23	0.75	8.7	0.92	7.29	6.7	19.3	1.62	5.28	8.5	8.5	1.62	0.6				217	0.8	4.67	
	12-A	E3-A	0.95	0.75	7.8	0.72	7.55	5.4	8.1	1.53	7.47	11.5	11.5	1.53	2.7				506	1.6	5.16	
		E4-A	1.12	0.73	8.1	0.82	7.47	6.1														
	13-A	E2-A	0.73	0.74	9.2	0.54	7.14	3.9	13.2	2.08	6.23	12.9	12.9	2.08	0.6				25	0.8	0.54	
	14-A	E1-A	0.18	0.82	6.1	0.15	8.19	1.2	24.0	3.84	4.73	18.2			18.2	3.84	0.5	2.0	6	2.9	0.03	
	15-A	F1-A	0.40	0.75	6.5	0.30	8.03	2.4	6.5	0.30	8.03	2.4			2.4	0.30	0.5	1.5	29	2.1	0.23	
	16-A				24.0	13.94	4.73	65.9							65.9	13.94	0.5	3.0	173	4.7	0.61	



**GRANDVIEW RESERVE (PHASE II)**

Calc'd by:

SPC

**PROPOSED CONDITIONS**

Checked by:

KH

**DESIGN STORM: 100-YEAR**

Date:

12/15/2023

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF					STREET			PIPE			TRAVEL TIME			REMARKS
			AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	
	17-A	D1-A	0.82	0.56	9.5	0.46	7.06	3.2	9.5	0.46	7.06	3.2			3.2	0.46	0.5	1.5	26	2.1	0.21	
	17.1-A								24.6	14.40	4.66	67.2			67.2	14.40	0.5	3.0	241	4.7	0.85	
	18-A	B4-A	0.86	0.70	6.3	0.60	8.10	4.9	6.3	0.60	8.10	4.9	4.9	0.60	0.6				268	0.8	5.77	
	19-A	B2-A	1.02	0.72	9.2	0.74	7.15	5.3	12.1	2.00	6.46	12.9	12.9	2.00	0.6				85	0.8	1.83	
		B3-A	0.87	0.76	6.6	0.66	7.98	5.2														
	20-A	B1-A	0.26	0.83	9.1	0.22	7.17	1.6	13.9	2.22	6.11	13.5			13.5	2.22	0.5	1.5	6	2.1	0.04	
	21-A	C1-A	0.56	0.74	8.0	0.41	7.50	3.1	8.0	0.41	7.50	3.1			3.1	0.41	0.5	1.5	29	2.1	0.23	
	22-A								25.5	17.03	4.58	78.0			78.0	17.03	0.5	3.0	34	4.7	0.12	
	23-A	A2-A	1.23	0.54	10.2	0.67	6.88	4.6	10.2	0.67	6.88	4.6			4.6	0.67	0.5	1.5	80	2.1	0.63	
	24-A								10.9	0.67	6.73	4.5	4.5	0.67	2.0				400	1.4	4.71	
	25-A	A1-A	3.22	0.42	13.5	1.37	6.18	8.5	25.6	19.07	4.57	87.1										



**GRANDVIEW RESERVE (PHASE II- DUPLEXES)**

**PROPOSED CONDITIONS**

**EL PASO COUNTY, CO**

**Calc'd by:**

**CBM**

**Checked by:**

**SPC**

**Date:**

**12/15/2023**

**SUMMARY RUNOFF TABLE**

BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
A-B	3.52	39	6.6	11.0
B-B	2.50	55	6.2	10.4
C-B	0.83	47	1.9	3.2
D-B	1.05	45	2.4	4.1
E-B	4.05	45	8.4	14.0
F-B	2.95	43	6.1	10.3
G-B	2.15	56	4.8	8.1
H-B	4.77	40	8.7	14.7
I-B	2.06	51	4.1	7.0
J-B	2.77	60	6.6	11.0
K-B	2.30	58	5.9	9.8
L-B	2.14	39	4.6	7.7
M-B	1.81	44	4.0	6.8
N-B	4.10	20	6.8	11.5
O-B	1.18	0	2	3.1

**DESIGN POINT SUMMARY TABLE**

DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>5</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
DP1-B	A,B	11.9	20.0
DP2-B	C,D	4.2	7.1
DP3-B	A,B,C,D	0.0	26.5
DP4-B	E	8.4	14.0
DP5-B	F	6.1	10.3
DP6-B	E,F	0.0	24.0
DP7-B	A,B,C,D,E,F	0.0	49.3
DP8-B	G	4.8	8.1
DP9-B	H	8.7	14.7
DP10-B	G,H	0.0	22.5
DP11-B	I	7.9	15.8
DP12-B	A,B,C,D,E,F,I	0.0	62.1
DP13-B	J,K,L	14.4	27.4
DP14-B	A-L	0.0	109.3
DP15-B	M	7.5	12.9
DP16-B	A-M	68.3	120.6





**GRANDVIEW RESERVE (PHASE II- DUPLEXES)**  
**PROPOSED CONDITIONS**  
 EL PASO COUNTY, CO

**Calc'd by:** CBM  
**Checked by:** SPC  
**Date:** 12/15/2023

<b>SOIL TYPE:</b>		<b>HSG A&amp;B</b>																	
<b>COMPOSITE 'C' FACTORS</b>																			
<b>BASIN</b>	<b>LAND USE TYPE</b>															<b>TOTAL</b>	<b>COMPOSITE IMPERVIOUSNESS &amp; C FACTOR</b>		
	<b>EPC LOCAL</b>			<b>Duplex</b>			<b>Lawns</b>			<b>EPC MINOR ARTERIAL</b>			<b>Townhome</b>						
	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>				
	<b>90</b>	<b>0.82</b>	<b>0.90</b>	<b>47</b>	<b>0.40</b>	<b>0.58</b>	<b>0</b>	<b>0.08</b>	<b>0.35</b>	<b>68</b>	<b>0.63</b>	<b>0.76</b>	<b>53</b>	<b>0.48</b>	<b>0.64</b>				
<b>ACRES</b>		<b>ACRES</b>		<b>ACRES</b>		<b>ACRES</b>		<b>ACRES</b>		<b>ACRES</b>		<b>ACRES</b>		<b>ACRES</b>		<b>%I</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	
A-B	0.48		1.51		1.09		0.00		0.44		3.52		39	0.37	0.56				
B-B	0.48		2.02		0.00		0.00		0.00		2.50		55	0.48	0.64				
C-B	0.26		0.25		0.25		0.00		0.08		0.83		47	0.44	0.62				
D-B	0.44		0.15		0.46		0.00		0.00		1.05		45	0.44	0.62				
E-B	0.71		2.26		0.83		0.00		0.25		4.05		45	0.41	0.59				
F-B	0.57		1.59		0.79		0.00		0.00		2.95		43	0.40	0.58				
G-B	0.00		0.00		0.38		1.77		0.00		2.15		56	0.53	0.69				
H-B	0.00		1.42		1.56		1.79		0.00		4.77		40	0.38	0.57				
I-B	0.22		1.80		0.03		0.00		0.00		2.06		51	0.44	0.61				
J-B	0.89		1.84		0.04		0.00		0.00		2.77		60	0.53	0.68				
K-B	0.84		1.24		0.22		0.00		0.00		2.30		58	0.52	0.67				
L-B	0.70		0.46		0.99		0.00		0.00		2.14		39	0.39	0.58				
M-B	0.50		0.73		0.58		0.00		0.00		1.81		44	0.41	0.59				
N-B	0.00		1.76		2.35		0.00		0.00		4.10		20	0.22	0.45				
O-B	0.00		0.00		1.18		0.00		0.00		1.18		0	0.08	0.35				
<b>Pond B</b>	<b>6.09</b>		<b>17.04</b>		<b>10.74</b>		<b>3.56</b>		<b>0.77</b>		<b>38.19</b>		<b>43</b>						



**GRANDVIEW RESERVE (PHASE II- DUPLEXES)**

Calc'd by:

**CBM**

**PROPOSED CONDITIONS**

Checked by:

**SPC**

**EL PASO COUNTY, CO**

Date:

**12/15/2023**

**TIME OF CONCENTRATION**

BASIN DATA			OVERLAND TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )					TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C <sub>s</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>v</sub>	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)	tc max	tc design (min)
A-B	0.37	3.52	100	2.0	10.7	20	1225	2.6	3.2	6.3	17.0	17.4	17.0
B-B	0.48	2.50	100	2.0	9.0	20	575	2.6	3.2	3.0	12.0	13.8	12.0
C-B	0.44	0.83	100	2.0	9.6	20	800	2.6	3.2	4.1	13.7	15.0	13.7
D-B	0.44	1.05	100	2.0	9.6	20	650	2.6	3.2	3.4	13.0	14.2	13.0
E-B	0.41	4.05	100	2.0	10.0	20	1100	2.9	3.4	5.4	15.4	16.7	15.4
F-B	0.40	2.95	100	2.0	10.3	20	830	2.9	3.4	4.1	14.3	15.2	14.3
G-B	0.53	2.15	30	2.0	4.5	20	1600	1.0	2.0	13.3	17.9	19.1	17.9
H-B	0.38	4.77	100	2.0	10.5	20	1450	1.0	2.0	12.1	22.5	18.6	18.6
I-B	0.44	2.06	100	2.0	9.6	20	1420	2.3	3.0	7.8	17.4	18.4	17.4
J-B	0.53	2.77	100	2.0	8.3	20	1290	2.3	3.0	7.1	15.4	17.7	15.4
K-B	0.52	2.30	100	2.0	8.4	20	890	3.0	3.5	4.3	12.7	15.5	12.7
L-B	0.39	2.14	100	2.0	10.3	20	520	2.0	2.8	3.1	13.4	13.4	13.4
M-B	0.41	1.81	100	2.0	10.0	20	520	2.3	3.0	2.9	12.8	13.4	12.8
N-B	0.22	4.10	100	2.0	12.8	20	460	0.8	1.8	4.3	17.1	13.1	13.1
O-B	0.08	1.18	25	2.0	7.4	20	50	1.0	2.0	0.4	7.8	10.4	7.8

**FORMULAS:**

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S^{0.33}} \quad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C<sub>v</sub>

Type of Land Surface	C <sub>v</sub>
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

\*For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.



**GRANDVIEW RESERVE (PHASE II- DUPLEXES)**

Calc'd by:

CBM

**PROPOSED CONDITIONS**

Checked by:

SPC

**DESIGN STORM: 5-YEAR**

Date:

12/15/2023

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF				TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS				
			AREA (ac)	C <sub>s</sub>	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	f (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	f (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	Q <sub>pipe</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)		LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
		A-B	3.52	0.56	17.0	1.97	3.33	6.6															BASIN A CAPTURED IN 15' TYPE R @ DP1	
	DP1-B	B-B	2.50	0.64	12.0	1.60	3.86	6.2	17.0	3.57	3.33	11.9	4.2	1.26	2.4					475	3.1	2.56	DP1 FLOWBY CAPTURED BY @ DP12	
																							BASIN B CAPTURED IN 15' TYPE R @ DP1, PIPED TO DP3	
		C-B	0.83	0.62	13.7	0.51	3.66	1.9															BASIN C CAPTURED IN 10' TYPE R @ DP2	
	DP2-B	D-B	1.05	0.62	13.0	0.65	3.74	2.4	13.7	1.16	3.66	4.2	0.1	0.04	2.4						3.1	0.00	BASIN D CAPTURED IN 10' TYPE R @ DP2, PIPED TO DP3	
																					8.4	0.05		
	DP3-B								17.0	4.73		0.0				0.0	4.73	2.0	1.5	58	8.4	0.11	DP3 FLOW TO DP7	
													1.9	0.54	0.8					640	1.8	5.96	FLOWBY CAPTURED @ DP15	
	DP4-B	E-B	4.05	0.59	15.4	2.40	3.48	8.4	15.4	2.40	3.48	8.4				6.5	1.87	2.0	1.5	27	8.4	0.05		
													3.2	0.90	0.8					675	1.8	6.29	FLOWBY CAPTURED @ DP15	
	DP5-B	F-B	2.95	0.58	14.3	1.71	3.59	6.1	14.3	1.71	3.59	6.1				2.9	0.81	2.0	1.5	7	8.4	0.01		
	DP6-B								15.4	4.11		0.0				0.0	0.00	2.0	1.5	62	8.4	0.12	PIPE TO DP7	
	DP7-B								17.1	8.85		0.0				0.0	8.85	2.0	2.0	420	10.2	0.69	PIPE TO DP12	
													0.3	0.10	0.8					1000	1.8	9.32	FLOWBY CAPTURED BY PHASE 3 STORM	
	DP8-B	G-B	2.15	0.69	17.9	1.48	3.26	4.8	17.9	1.48	3.26	4.8				4.5	1.38	2.0	1.5	19	8.4	0.04		
													3.1	0.98	0.8					1000	1.8	9.32	FLOWBY CAPTURED BY PHASE 3 STORM	
	DP9-B	H-B	4.77	0.57	18.6	2.73	3.20	8.7	18.6	2.73	3.20	8.7				5.6	1.75	2.0	1.5	34	8.4	0.07		
	DP10-B								18.7	4.21		0.0				0.0	4.21	2.0	2.0	650	10.2	1.06	PIPE TO DP14	
													0.2	0.06	2.4					215	3.1	1.16	FLOWBY CAPTURED @ DP13	
	DP11-B	I-B	2.06	0.61	17.4	1.26	3.30	4.1	19.5	2.52	3.12	7.9				7.7	2.46	2.0	1.5	7	8.4	0.01		
	DP12-B								19.6	11.37		0.0				0.0	11.37	2.0	2.5	58	11.8	0.08	PIPE TO DP14	
		J-B	2.77	0.68	15.4	1.88	3.48	6.6																
		K-B	2.30	0.67	12.7	1.55	3.77	5.9																
	DP13-B	L-B	2.14	0.58	13.4	1.24	3.69	4.6	20.7	4.73	3.04	14.4				14.4	4.73	2.0	2.0	7	10.2	0.01	SUMP INLET-PIPE TO DP14, OVERTOP CROWN AND CURB INTO POND	
	DP14-B								20.7	20.30		0.0				0.0	20.30	2.0	1.5	58	8.4	0.11	PIPE TO DP16	
	DP15-B	M-B	1.81	0.59	12.8	1.08	3.75	4.0	21.3	2.52	2.99	7.5				7.5	2.52	2.0	2.0	7	10.2	0.01	SUMP INLET, OVERTOP CURB INTO POND	
	DP16-B								21.3	22.82	2.99	68.3												PIPE TO POND X TO BE DETAINED AND RELEASED AT LESS THAN HISTORIC RATES
	DP17-B	N-B	4.10	0.45	13.1	1.84	3.72	6.8															BASIN N SWALE FLOW TO POND X	
		O-B	1.18	0.35	7.8	0.41	4.49	1.9															BASIN O SHEET FLOW INTO POND X	

Highlighted flows cannot be 0 cfs. Appears that intensity is missing. Please update. **ADDRESSED.**

Missing flow rate for design point **ADDRESSED.**



**APPENDIX C – HYDRAULIC CALCULATIONS  
(TO BE PROVIDED WITH FDR)**

## APPENDIX D – WATER QUALITY & DETENTION

Note that the pond calcs will be reviewed in more detail with the FDR and subsequent submission of CDs. Can't do a full review of these calcs without the pond details in the CDs.

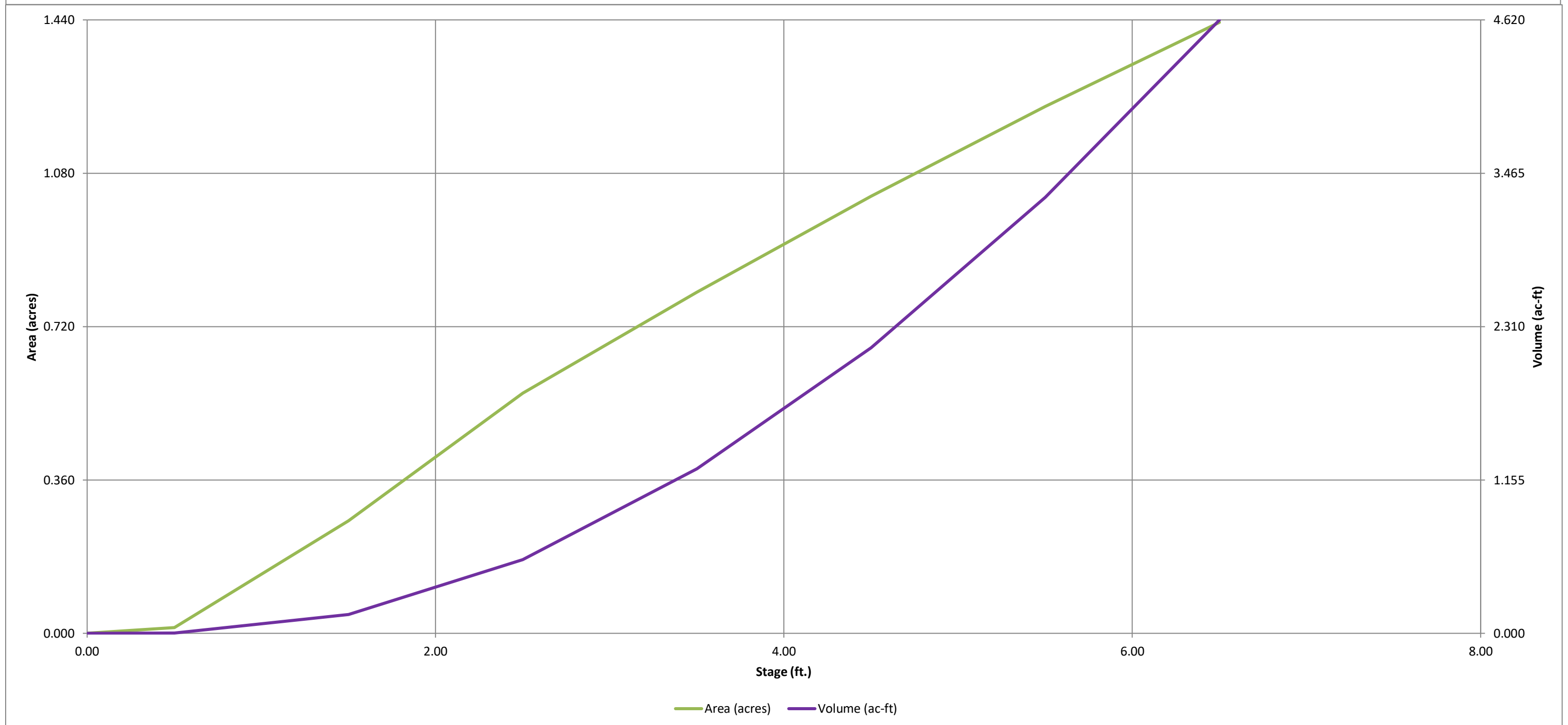
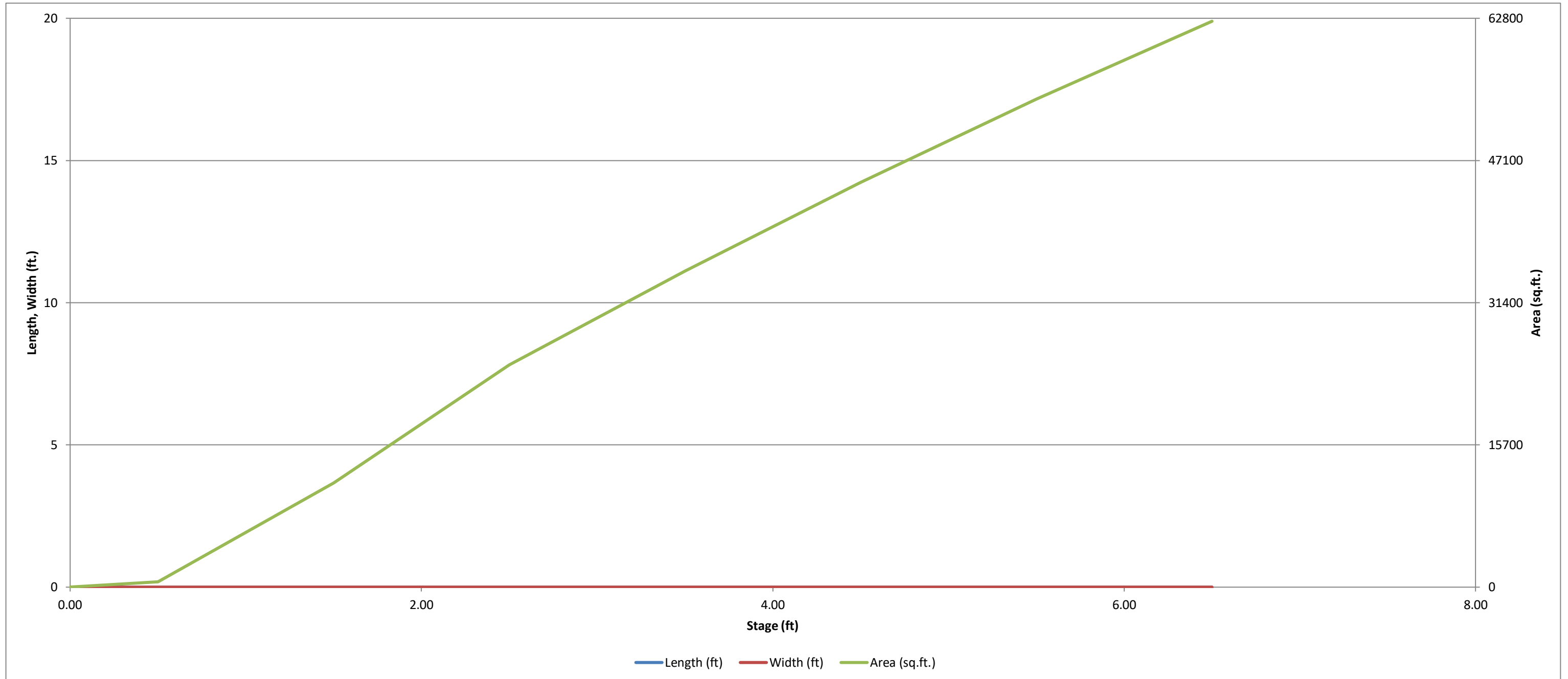
HR GREEN RESPONSE:  
NOTED.





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

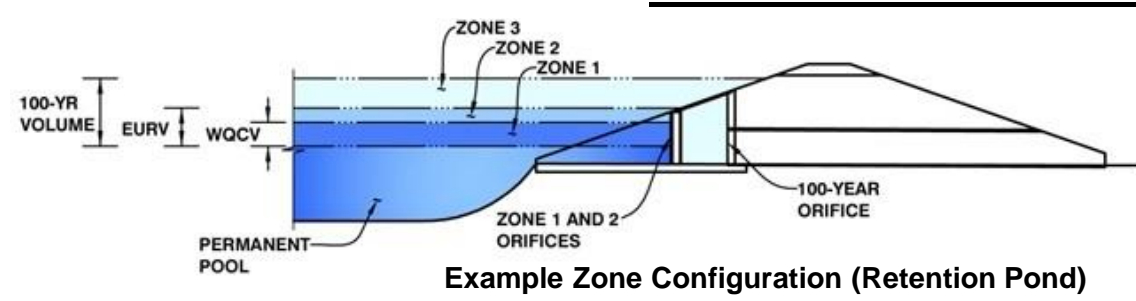
MHFD-Detention, Version 4.06 (July 2022)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

**Project: Grandview Reserve - Phase 2**  
**Basin ID: Pond A**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.41	0.505	Orifice Plate
Zone 2 (EURV)	3.96	1.124	Circular Orifice
Zone 3 (100-year)	4.93	0.973	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>2.603</b>	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =  ft<sup>2</sup>  
 Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =  0.00 ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Orifice Plate =  2.41 ft (relative to basin bottom at Stage = 0 ft)  
 Orifice Plate: Orifice Vertical Spacing =  N/A inches  
 Orifice Plate: Orifice Area per Row =  1.77 sq. inches (diameter = 1-1/2 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row =  1.229E-02 ft<sup>2</sup>  
 Elliptical Half-Width =  N/A feet  
 Elliptical Slot Centroid =  N/A feet  
 Elliptical Slot Area =  N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.80	1.60					
Orifice Area (sq. inches)	1.77	1.77	1.77					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.42	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.96	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	3.00	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.05	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.13	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	5.67	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	2.92	N/A	feet
Overflow Gate Type =	Type C Gate	N/A	
Debris Clogging % =	0%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>t</sub> =	4.00	N/A	feet
Overflow Weir Slope Length =	2.92	N/A	feet
Gate Open Area / 100-yr Orifice Area =	9.84	N/A	
Overflow Gate Open Area w/o Debris =	11.52	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	11.52	N/A	ft <sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	11.33	N/A	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.17	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.53	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.83	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	60.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.38	feet
Stage at Top of Freeboard =	6.38	feet
Basin Area at Top of Freeboard =	1.41	acres
Basin Volume at Top of Freeboard =	4.45	acre-ft

## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

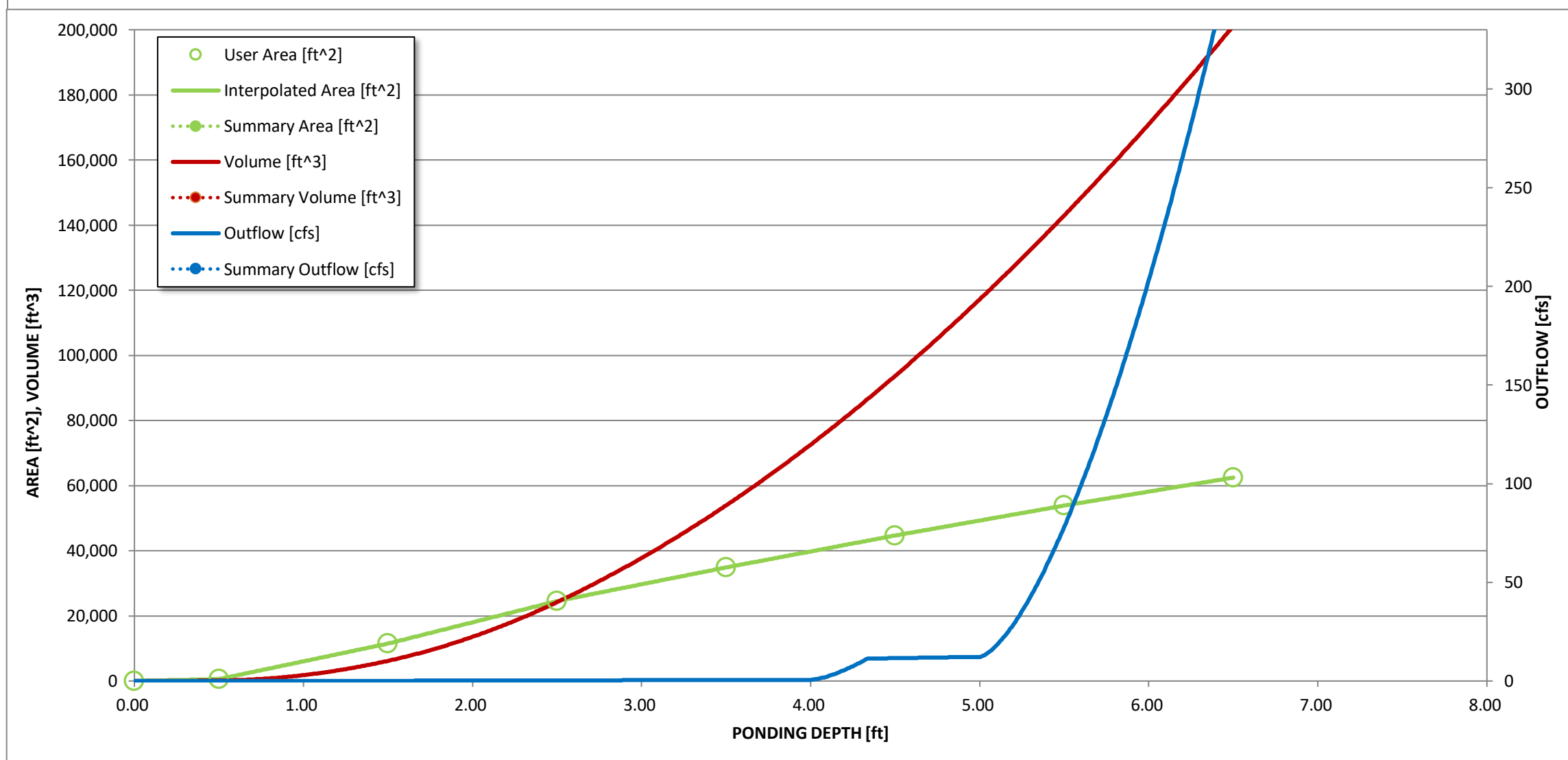
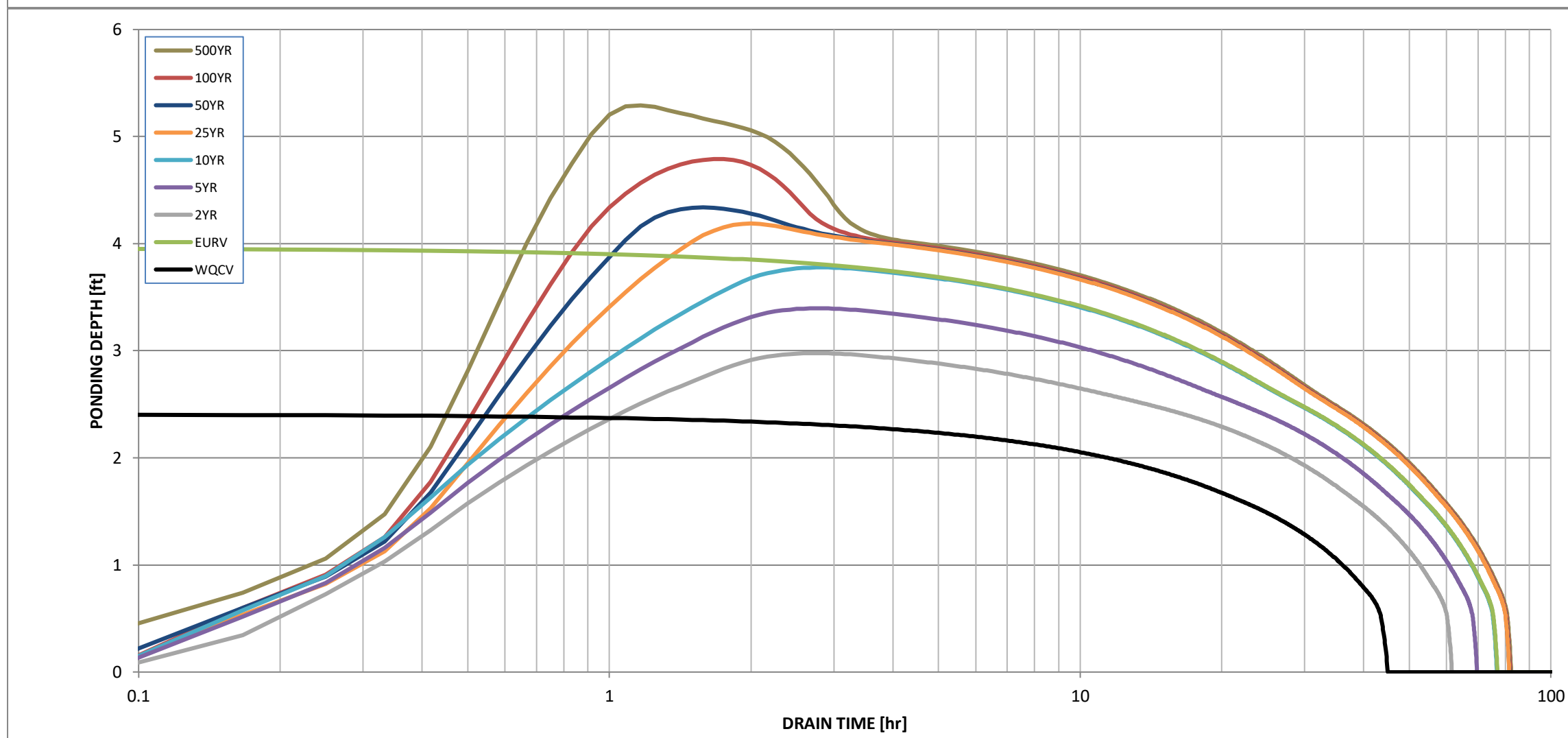
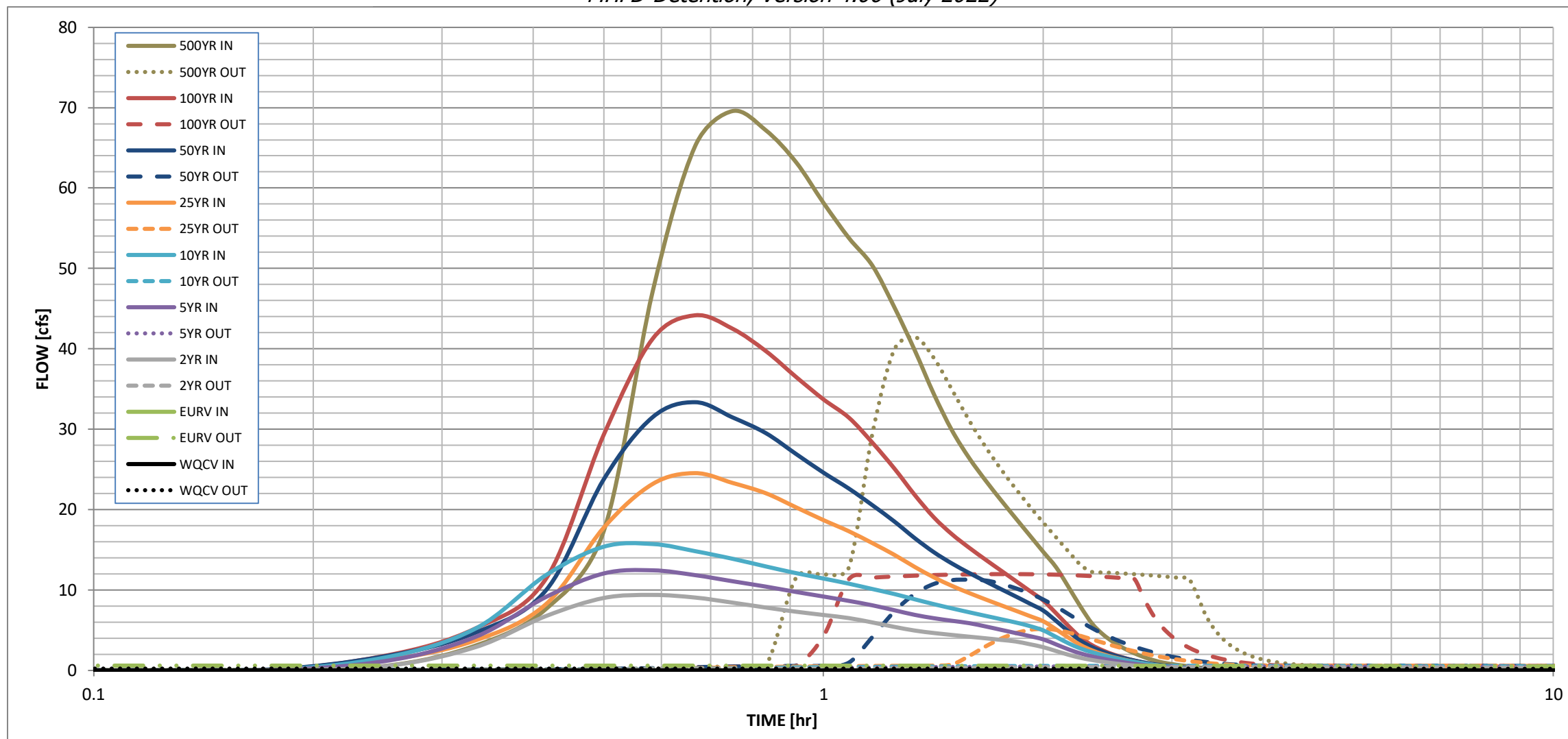
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	0.93	1.21	1.46	1.84	2.15	2.49	3.35
One-Hour Rainfall Depth (in) =	N/A	N/A	0.924	1.247	1.576	2.182	2.828	3.654	5.721
CUHP Runoff Volume (acre-ft) =	0.505	1.630	0.924	1.247	1.576	2.182	2.828	3.654	5.721
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.924	1.247	1.576	2.182	2.828	3.654	5.721
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.1	0.3	1.5	6.1	12.1	27.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.00	0.01	0.05	0.20	0.40	0.89
Peak Inflow Q (cfs) =	N/A	N/A	9.4	12.4	15.7	24.5	33.4	44.2	69.6
Peak Outflow Q (cfs) =	0.2	0.6	0.4	0.5	0.6	5.2	11.3	12.0	41.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	3.6	2.2	3.5	1.9	1.0	1.5
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.4	0.9	1.0	1.0
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	41	67	55	61	67	70	67	65	59
Time to Drain 99% of Inflow Volume (hours) =	43	72	59	66	72	76	75	74	71
Maximum Ponding Depth (ft) =	2.41	3.96	2.98	3.40	3.78	4.19	4.34	4.79	5.29
Area at Maximum Ponding Depth (acres) =	0.54	0.90	0.68	0.77	0.86	0.95	0.99	1.09	1.19
Maximum Volume Stored (acre-ft) =	0.506	1.630	0.847	1.151	1.462	1.835	1.980	2.447	3.028

Q ratios should be less than or equal to 1.

**HR GREEN RESPONSE:**  
 Justification for 5-yr and 100-yr release rates has been provided in the "Water Quality & Detention" Section of the PDR. Per coordination with Glenn Reese on 02.27.24 we will not be required to meet pre-development flows for storms in between the 5-yr and 100-yr event.

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			



## DETENTION BASIN OUTLET STRUCTURE DESIGN

*Outflow Hydrograph Workbook Filename:* \_\_\_\_\_

### Inflow Hydrographs

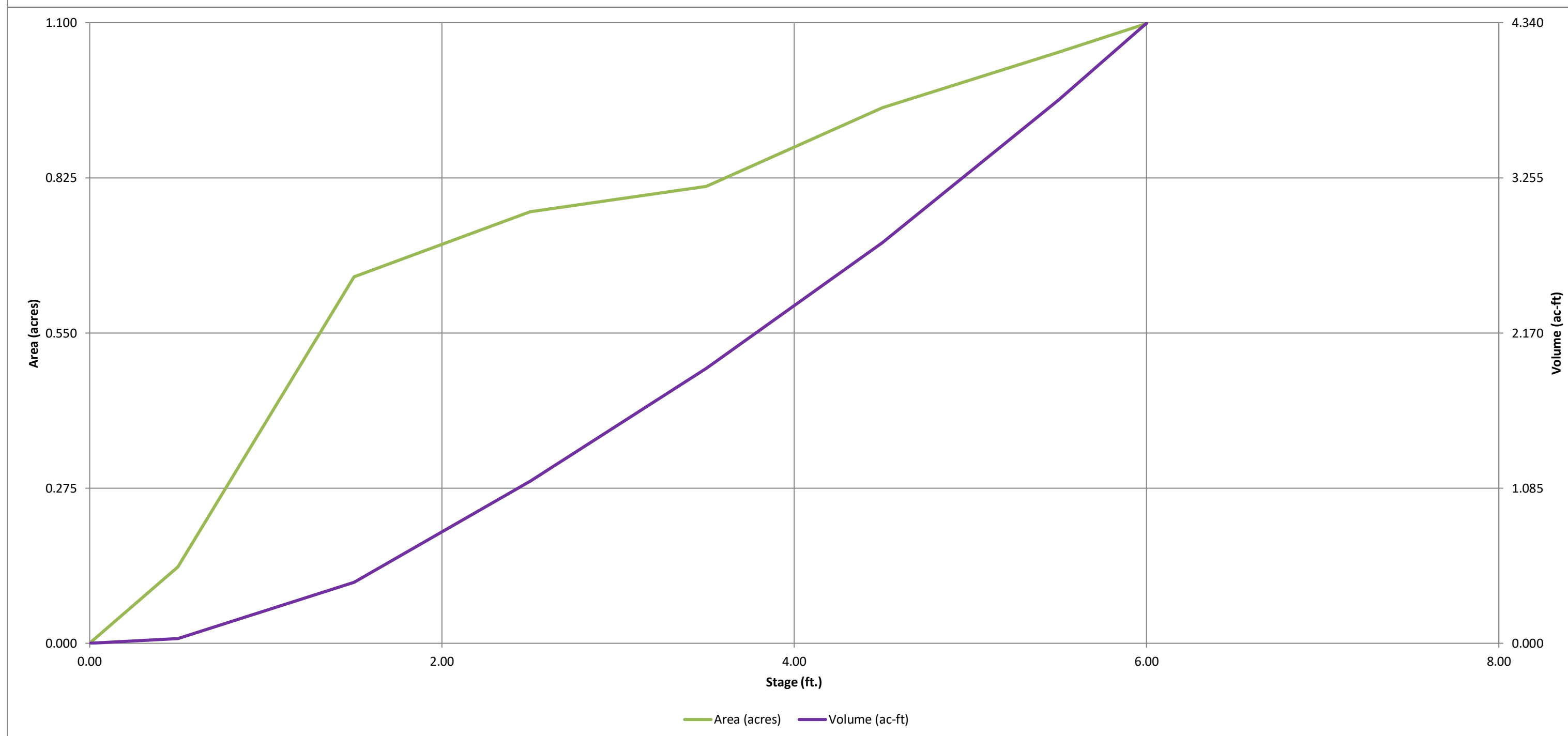
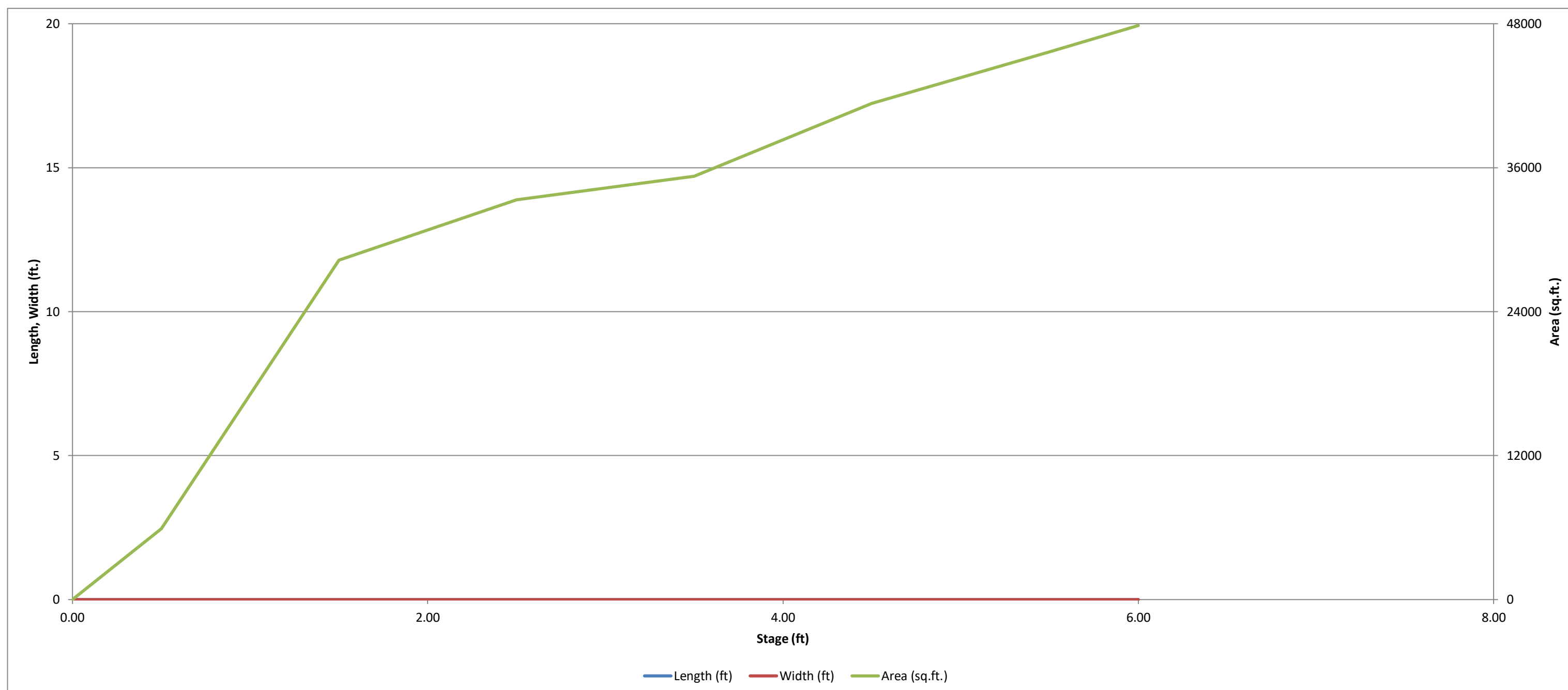
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.54
	0:15:00	0.00	0.00	0.52	1.14	1.58	1.25	1.74	1.79	3.07
	0:20:00	0.00	0.00	2.88	4.16	5.18	3.72	4.68	5.21	7.64
	0:25:00	0.00	0.00	6.76	9.13	11.85	8.24	9.96	11.41	17.34
	0:30:00	0.00	0.00	9.00	12.06	15.38	17.76	23.77	29.33	47.12
	0:35:00	0.00	0.00	9.39	12.44	15.72	23.19	31.50	41.25	65.17
	0:40:00	0.00	0.00	9.06	11.85	14.83	24.53	33.36	44.16	69.56
	0:45:00	0.00	0.00	8.43	11.09	13.88	23.32	31.48	42.51	67.19
	0:50:00	0.00	0.00	7.82	10.42	12.93	22.04	29.52	39.73	63.23
	0:55:00	0.00	0.00	7.30	9.76	12.10	20.29	26.93	36.51	58.14
	1:00:00	0.00	0.00	6.89	9.18	11.42	18.69	24.59	33.70	53.78
	1:05:00	0.00	0.00	6.50	8.64	10.78	17.30	22.61	31.44	50.35
	1:10:00	0.00	0.00	5.96	8.09	10.12	15.83	20.55	28.33	45.20
	1:15:00	0.00	0.00	5.41	7.48	9.50	14.38	18.53	25.13	39.83
	1:20:00	0.00	0.00	4.96	6.91	8.84	12.87	16.46	21.83	34.36
	1:25:00	0.00	0.00	4.64	6.49	8.24	11.57	14.69	19.03	29.84
	1:30:00	0.00	0.00	4.40	6.17	7.71	10.51	13.29	16.92	26.42
	1:35:00	0.00	0.00	4.19	5.87	7.23	9.62	12.12	15.26	23.64
	1:40:00	0.00	0.00	3.99	5.47	6.78	8.83	11.08	13.78	21.19
	1:45:00	0.00	0.00	3.79	5.05	6.36	8.11	10.11	12.42	18.93
	1:50:00	0.00	0.00	3.59	4.64	5.96	7.42	9.20	11.13	16.79
	1:55:00	0.00	0.00	3.25	4.26	5.51	6.76	8.31	9.89	14.75
	2:00:00	0.00	0.00	2.89	3.86	4.98	6.11	7.44	8.69	12.81
	2:05:00	0.00	0.00	2.40	3.23	4.16	5.10	6.15	7.10	10.36
	2:10:00	0.00	0.00	1.94	2.61	3.36	4.06	4.84	5.51	7.92
	2:15:00	0.00	0.00	1.56	2.11	2.72	3.15	3.69	4.09	5.82
	2:20:00	0.00	0.00	1.28	1.73	2.26	2.48	2.89	3.13	4.45
	2:25:00	0.00	0.00	1.06	1.44	1.88	2.00	2.31	2.46	3.47
	2:30:00	0.00	0.00	0.88	1.19	1.56	1.62	1.88	1.95	2.71
	2:35:00	0.00	0.00	0.73	0.99	1.29	1.32	1.52	1.55	2.12
	2:40:00	0.00	0.00	0.59	0.81	1.05	1.06	1.22	1.22	1.64
	2:45:00	0.00	0.00	0.48	0.65	0.85	0.85	0.98	0.95	1.26
	2:50:00	0.00	0.00	0.39	0.53	0.69	0.68	0.78	0.74	0.98
	2:55:00	0.00	0.00	0.32	0.42	0.55	0.54	0.62	0.59	0.78
	3:00:00	0.00	0.00	0.26	0.34	0.44	0.44	0.50	0.48	0.63
	3:05:00	0.00	0.00	0.21	0.27	0.35	0.35	0.40	0.38	0.50
	3:10:00	0.00	0.00	0.16	0.21	0.27	0.27	0.31	0.30	0.39
	3:15:00	0.00	0.00	0.12	0.15	0.21	0.21	0.23	0.23	0.29
	3:20:00	0.00	0.00	0.08	0.11	0.15	0.15	0.17	0.16	0.21
	3:25:00	0.00	0.00	0.05	0.07	0.10	0.10	0.11	0.11	0.14
	3:30:00	0.00	0.00	0.03	0.05	0.06	0.06	0.07	0.07	0.08
	3:35:00	0.00	0.00	0.02	0.03	0.03	0.04	0.04	0.03	0.04
	3:40:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
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5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.06 (July 2022)*

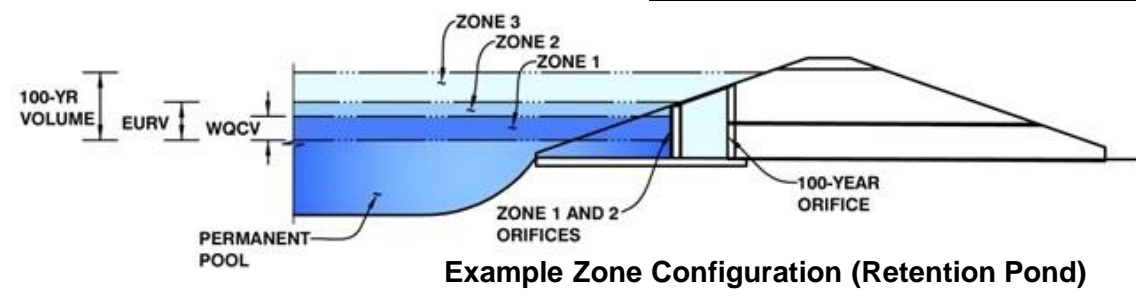


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

**Project: Grandview Reserve Phase 2**

**Basin ID: Pond B**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.76	0.597	Orifice Plate
Zone 2 (EURV)	3.37	1.218	Circular Orifice
Zone 3 (100-year)	4.68	1.158	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>2.974</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	1.76	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	2.95	sq. inches (diameter = 1-15/16 inches)

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	2.049E-02	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.60	1.20					
Orifice Area (sq. inches)	2.95	2.95	2.95					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	1.76	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.37	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	1.38	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.01	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.06	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)**

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.38	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	5.67	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	2.92	N/A	feet
Overflow Gate Type =	Type C Gate	N/A	
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H <sub>1</sub> =	3.38	N/A	feet
Overflow Weir Slope Length =	2.92	N/A	feet
Gate Open Area / 100-yr Orifice Area =	6.19	N/A	
Overflow Gate Open Area w/o Debris =	11.52	N/A	ft <sup>2</sup>
Overflow Gate Open Area w/ Debris =	5.76	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	13.75	N/A	inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.86	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.65	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.72	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage =	4.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	77.50	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.50	feet
Stage at Top of Freeboard =	6.00	feet
Basin Area at Top of Freeboard =	1.10	acres
Basin Volume at Top of Freeboard =	4.34	acre-ft

**Routed Hydrograph Results**

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	0.93	1.21	1.46	1.84	2.15	2.49	3.35
CUHP Runoff Volume (acre-ft) =	0.597	1.815	1.033	1.395	1.771	2.481	3.268	4.283	6.832
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.033	1.395	1.771	2.481	3.268	4.283	6.832
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.2	0.4	2.2	9.1	18.2	40.4
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.01	0.01	0.06	0.24	0.48	1.06
Peak Inflow Q (cfs) =	N/A	N/A	11.5	15.2	19.4	30.7	42.7	57.6	92.2
Peak Outflow Q (cfs) =	0.3	0.6	0.4	0.5	0.5	5.7	13.2	18.1	64.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.2	1.4	2.6	1.4	1.0	1.6
Structure Controlling Flow	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.4	1.1	1.5	1.6
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	66	51	59	66	68	66	63	58
Time to Drain 99% of Inflow Volume (hours) =	41	72	55	64	72	75	74	72	69
Maximum Ponding Depth (ft) =	1.76	3.37	2.27	2.72	3.19	3.70	3.97	4.46	4.83
Area at Maximum Ponding Depth (acres) =	0.68	0.80	0.74	0.77	0.80	0.84	0.88	0.94	0.98
Maximum Volume Stored (acre-ft) =	0.600	1.817	0.954	1.304	1.665	2.086	2.318	2.754	3.120

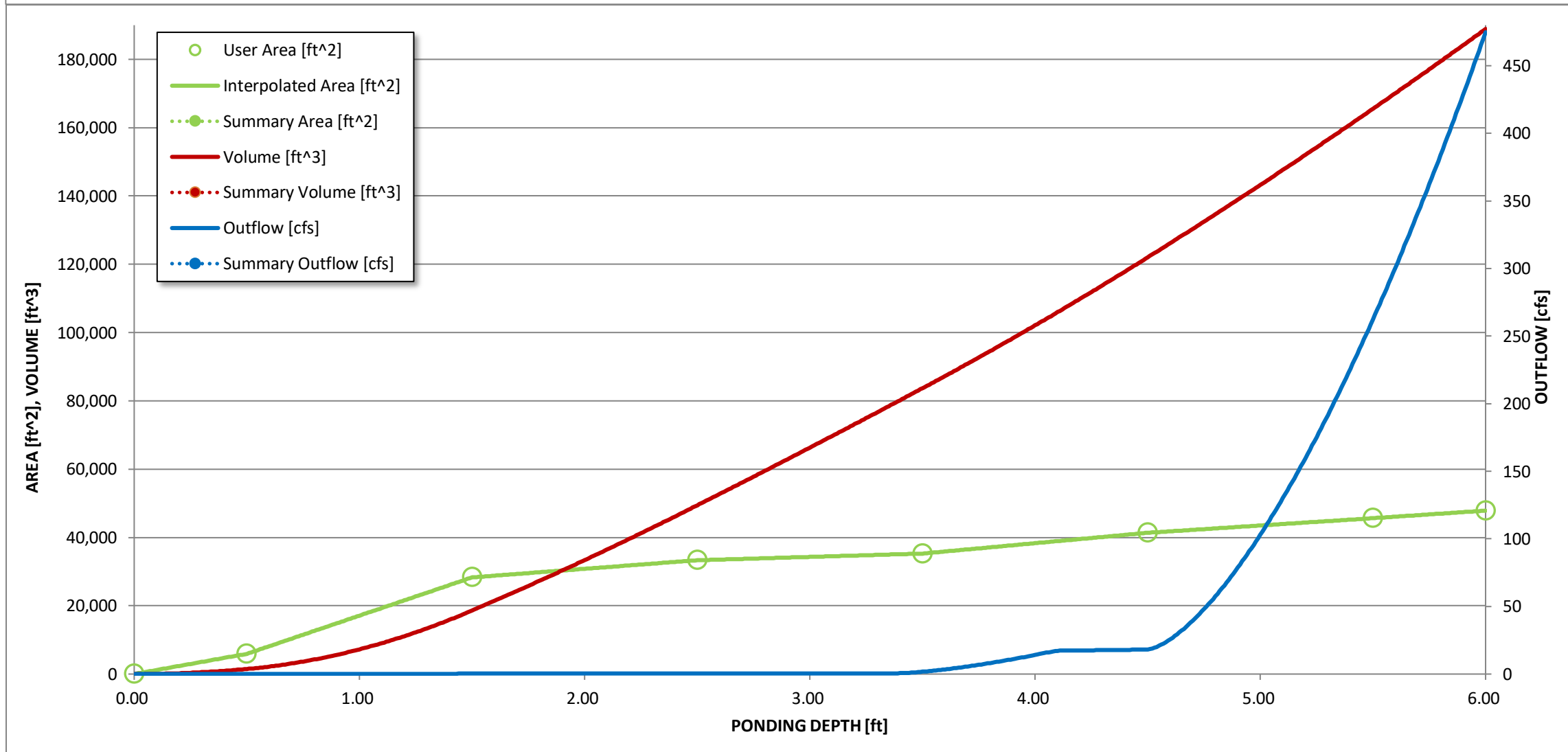
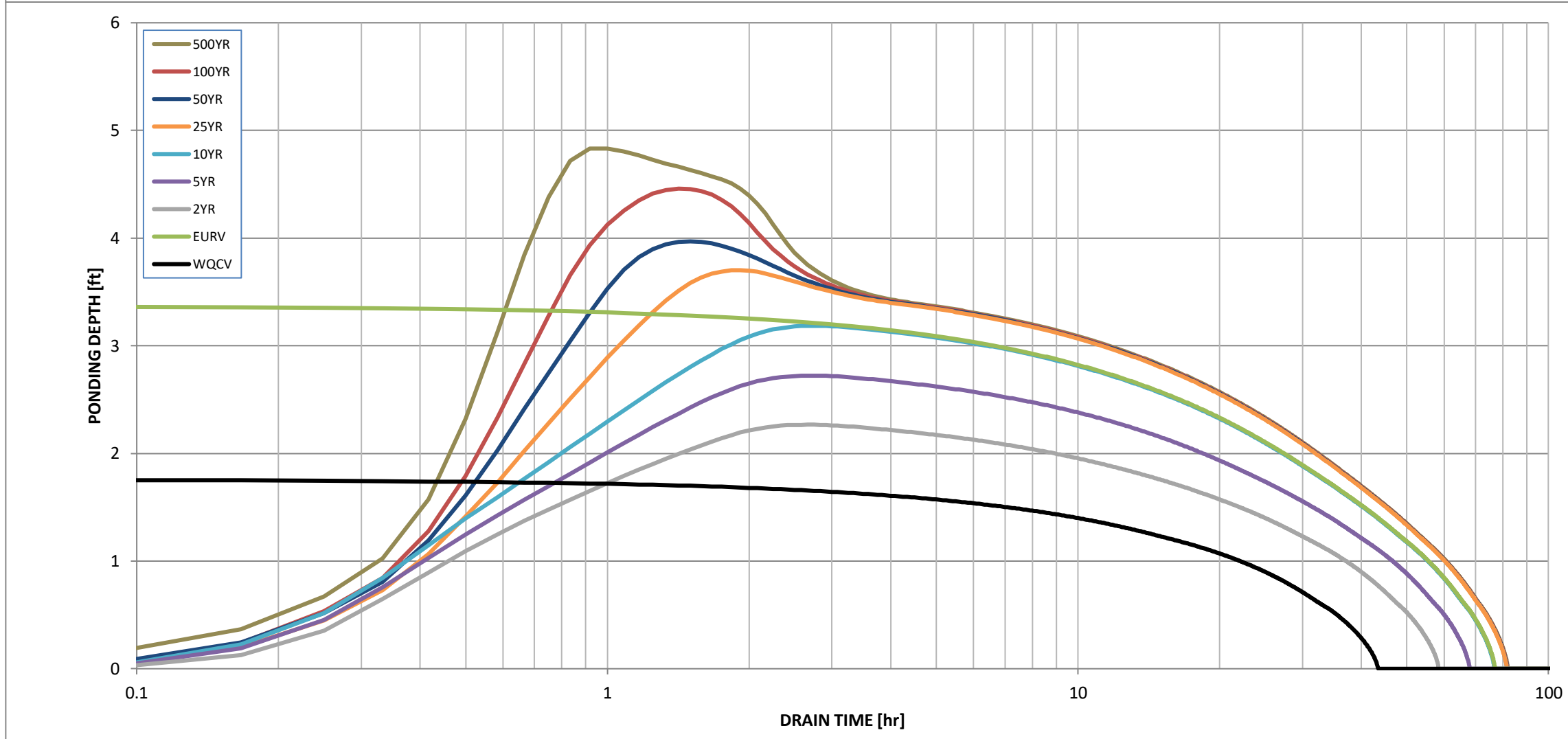
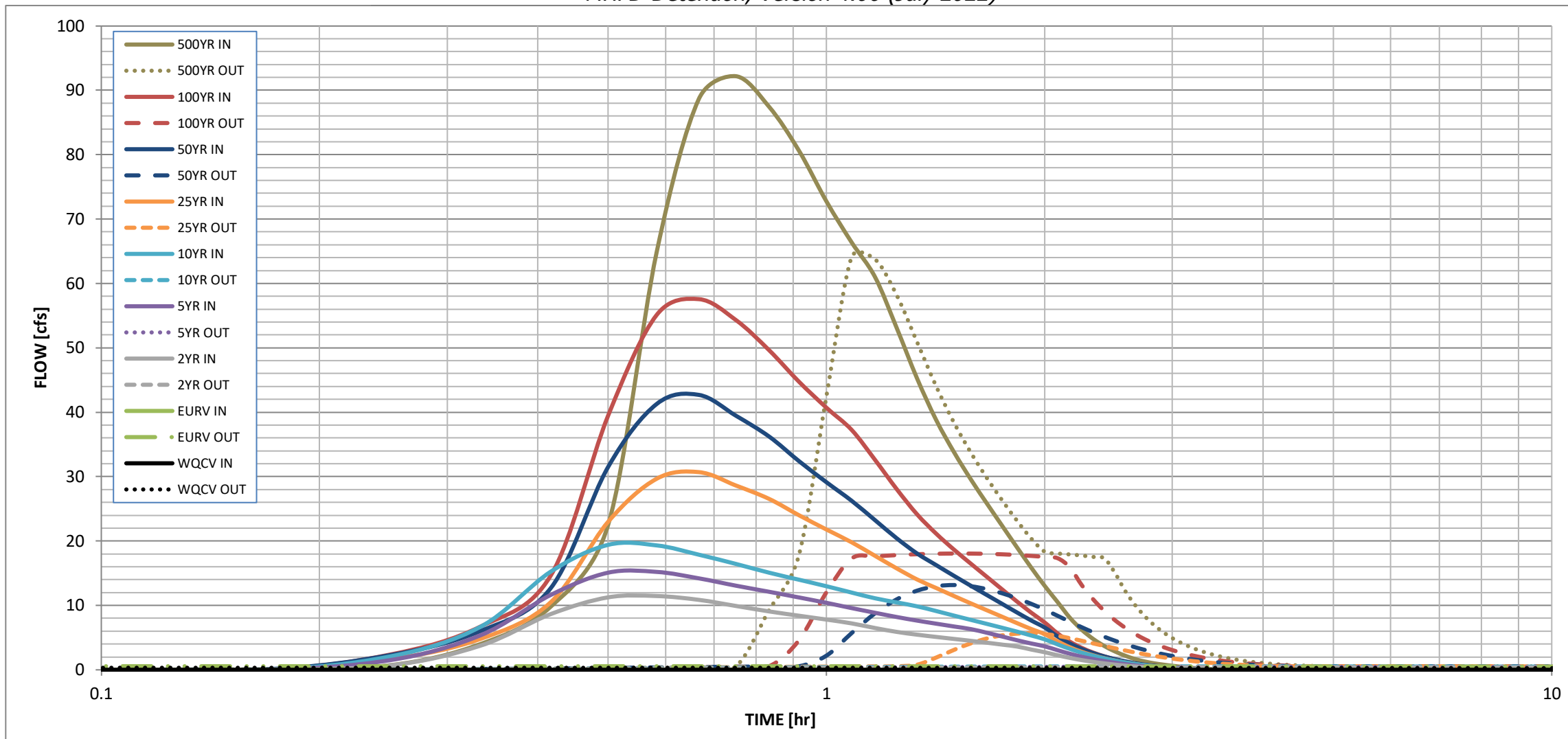
Q ratios should be less than or equal to 1.

**HR GREEN RESPONSE:**  
Justification for 5-yr and 100-yr release rates has been provided in the "Water Quality & Detention" Section of the PDR. Per coordination with Glenn Reese on 02.27.24 we will not be required to meet pre-development flows for storms in between the 5-yr and 100-yr event.



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.06 (July 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.00	0.71
	0:15:00	0.00	0.00	0.68	1.49	2.06	1.63	2.27	2.35	3.99
	0:20:00	0.00	0.00	3.75	5.36	6.67	4.79	6.02	6.71	9.81
	0:25:00	0.00	0.00	8.65	11.62	15.24	10.49	12.68	14.63	22.51
	0:30:00	0.00	0.00	11.25	15.08	19.40	22.98	31.51	39.48	64.89
	0:35:00	0.00	0.00	11.45	15.20	19.32	29.67	41.28	55.11	88.61
	0:40:00	0.00	0.00	10.86	14.20	17.88	30.70	42.69	57.56	92.18
	0:45:00	0.00	0.00	9.91	13.06	16.44	28.62	39.46	54.32	87.45
	0:50:00	0.00	0.00	9.07	12.12	15.08	26.54	36.23	49.65	80.59
	0:55:00	0.00	0.00	8.39	11.23	13.98	23.99	32.40	44.72	72.74
	1:00:00	0.00	0.00	7.80	10.40	12.98	21.78	29.13	40.70	66.38
	1:05:00	0.00	0.00	7.20	9.58	11.99	19.80	26.24	37.25	61.01
	1:10:00	0.00	0.00	6.48	8.85	11.11	17.70	23.24	32.61	53.09
	1:15:00	0.00	0.00	5.89	8.20	10.46	15.74	20.42	28.05	45.26
	1:20:00	0.00	0.00	5.45	7.64	9.85	14.03	18.06	24.15	38.81
	1:25:00	0.00	0.00	5.10	7.16	9.12	12.70	16.26	21.15	33.76
	1:30:00	0.00	0.00	4.79	6.72	8.41	11.45	14.58	18.64	29.49
	1:35:00	0.00	0.00	4.49	6.31	7.74	10.29	13.02	16.44	25.73
	1:40:00	0.00	0.00	4.19	5.73	7.11	9.21	11.57	14.38	22.25
	1:45:00	0.00	0.00	3.90	5.14	6.50	8.20	10.19	12.41	18.94
	1:50:00	0.00	0.00	3.60	4.58	5.91	7.23	8.87	10.56	15.84
	1:55:00	0.00	0.00	3.14	4.08	5.32	6.33	7.65	8.86	13.02
	2:00:00	0.00	0.00	2.73	3.64	4.73	5.53	6.56	7.34	10.52
	2:05:00	0.00	0.00	2.25	3.04	3.94	4.41	5.17	5.65	8.07
	2:10:00	0.00	0.00	1.84	2.49	3.24	3.49	4.07	4.36	6.20
	2:15:00	0.00	0.00	1.50	2.03	2.65	2.78	3.23	3.40	4.78
	2:20:00	0.00	0.00	1.23	1.65	2.17	2.24	2.59	2.66	3.69
	2:25:00	0.00	0.00	0.99	1.34	1.76	1.79	2.07	2.08	2.84
	2:30:00	0.00	0.00	0.80	1.09	1.42	1.44	1.65	1.62	2.18
	2:35:00	0.00	0.00	0.64	0.87	1.13	1.13	1.30	1.25	1.65
	2:40:00	0.00	0.00	0.51	0.68	0.89	0.89	1.02	0.97	1.28
	2:45:00	0.00	0.00	0.41	0.53	0.70	0.69	0.79	0.76	1.00
	2:50:00	0.00	0.00	0.32	0.42	0.55	0.55	0.63	0.60	0.79
	2:55:00	0.00	0.00	0.25	0.32	0.43	0.43	0.49	0.48	0.62
	3:00:00	0.00	0.00	0.19	0.24	0.33	0.33	0.37	0.36	0.47
	3:05:00	0.00	0.00	0.14	0.18	0.24	0.24	0.28	0.27	0.34
	3:10:00	0.00	0.00	0.09	0.12	0.17	0.17	0.19	0.18	0.23
	3:15:00	0.00	0.00	0.06	0.08	0.11	0.11	0.12	0.12	0.14
	3:20:00	0.00	0.00	0.03	0.05	0.06	0.06	0.07	0.06	0.08
	3:25:00	0.00	0.00	0.01	0.02	0.03	0.03	0.03	0.03	0.03
	3:30:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

## APPENDIX E – REFERENCES

For Reference Material, please only include sheets that are relevant to this portion of the project (Phase 2). Also, highlight specific information, such as basins & DP's being discussed within this report.

ADDRESSED.



# Grandview Reserve Master Development Drainage Plan

August 2021

HR Green Project No: 191850

**Prepared For:**

4 SITE INVESTMENTS, LLC  
Mr. Peter Martz or Paul Howard  
1271 Kelly Johnson Blvd., Ste. 100  
Colorado Springs, CO 80920  
719-499-8416

**Prepared By:**

HR Green Development, LLC  
Contact: Chris McFarland, PE  
[cmcfarland@hrgreen.com](mailto:cmcfarland@hrgreen.com)  
720-602-4956



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# Master Development Drainage Plan – Grandview Reserve

## I. General Purpose, Location and Description

### a. Purpose and Scope of study

The Purpose of this Master Development Drainage Plan (MDDP) is to describe the onsite and offsite drainage patterns, existing and proposed storm infrastructure as it relates to preliminary water quality and stormwater detention, areas tributary to the site and the planned storm water management for Grandview Reserve 2 development. The items discussed in this report are preliminary in nature and final drainage calculations and design will be required as development proceeds. This report provides a general drainage concept and guidance for future development of Grandview Reserve.

### b. DBPS Investigations

The Geick Ranch Drainage Basin Planning Study (DBPS) Preliminary Design Report prepared by Drexel, Barrell was reviewed to determine existing plans and constraints that would influence the design of Grandview Reserve. The proposed plans for Grandview Reserve are in general conformance with the DBPS.

The DBPS shows 4 reaches through Grandview Reserve. The Main Stem (MS) in the south western portion of the site, the Main Stem Tributary #2 (MST2) to the north and east of the Main Stem, the East Fork Tributary (EFT) in the middle of the site north and east of MST2, and the East Fork Upper (EF) at the north east side of the site. These drainageways have been reviewed in the following reports and further analysis will be completed of these major drainageways in future planning documents.

- Unnamed Tributary Black Squirrel Creek, Four Way Ranch Letter of Map Revisions, Kiowa Engineering, March 2004
- Haegler and Geick Drainage Basins Letter of Map Revision, Four Way Ranch Subdivision, Kiowa, March 2004
- Unnamed Tributary Black Squirrel Creek Drainage Basin, Letter of Map Revision, Elbert Road Site, Kiowa Engineering, February 2006
- Geick Ranch Drainage Basin Planning Study (DBPS), Drexel Barrell, October 2010 (not approved)
- Meridian Ranch Master Development Drainage Plan (MDDP), Tech Contractors, January 2018

### c. Agency Jurisdictions

Listed below are the jurisdictions that this project will conform to:

El Paso County

Falcon Colorado Municipal Code (where applicable)

Federal Emergency Management Agency



#### d. General Project Description

Grandview Reserve is located in Falcon, Colorado within El Paso County and contains approximately 776 acres within the south half of section 21 and 22 and the north half of section 27 and 28, Township 12 South, and Range 66 West of the Sixth Principal Meridian in El Paso County, Colorado. See below for approximate site location.



Figure 1 - Site Map

#### e. Data Sources

Listed Below are the technical resources reviewed in the preparation of this MDDP:

City of Colorado Springs Drainage Criteria Manual (DCM), Volumes 1 and 2

Mile High Flood District

NOAA Atlas 14

NRCS Soil Survey for El Paso County Area, Colorado

FEMA FIRM 08041C0556G and FIRM 08041C0552G (eff. 12/7/2018)

El Paso County Assessor Property Records

## **f. Applicable Criteria and Standards**

Per the DBPS, flows from the proposed site will be limited to historic flows in an effort to maintain the stability and of the existing channels with the drainage basin. The master plan follows the Drainage Criteria Manual for El Paso County which refers to the City of Colorado Springs Drainage Criteria Manuals as amended.

# **II. Project Characteristics**

## **a. Location in Drainage Basin, offsite flows, size**

Grandview Reserve is located within the Gieck Ranch Drainage Basin which covers approximately 22 square miles. This drainage basin is tributary to Black Squirrel Creek and joins said creek just to the south of Elicott, CO about 18 miles to the south. Black Squirrel Creek eventually drains to the Arkansas River in Pueblo Colorado. The majority of the Gieck Ranch Drainage basin is undeveloped consisting of rural farmland. The Gieck Ranch Drainage basin lies north of the Haegler Ranch drainage basin.

As part of the Fourway LOMR discussed above, the study reviewed the hydrology and hydraulics for the Main Stem Tributaries, however only a small portion of the site within Grandview was analyzed. The peak flows rates for the Main Stem for the 100 year event was 413 cfs and for the Main Stem Tributary (MST2) was 280 cfs.

For the East Fork tributaries (EF and EFT), the DBPS established 100 year flow rates of 595 cfs for the East Fork (EF) and 217 cfs for the East Fork Tributary (EFT)

Generally offsite flows are conveyed through the site via the 4 tributaries. Minor offsite basins may sheet flow onto the site. These flows will be routed through the site via the 4 tributaries.

## **b. Compliance with DBPS**

This MDDP is in general conformance with the guidelines outlined in the Gieck Ranch DBPS. Grandview Reserve will construct multiple full spectrum detention facilities to limit the effects of development and mimic natural flow patterns.

Existing downstream infrastructure is currently limited to the historic drainage channels and minimal downstream improvements exist. As such, the site follows the DBPS and restricts offsite flow rates to not exceed historic flow rates. The sites ultimate outfalls will generally be along the same historic tributaries. Although outfall rates will be at or below historic, the cumulative volume of runoff will increase and therefore downstream facilities may see an increase in the duration of flows. This may provide a net benefit to the downstream facilities by providing more water to assist with the sustenance of vegetation however it should be noted that increased volume may expedite potential erosion or channel movement.

## **c. Site Characteristic**

Per the NRCS web soil survey, the site is made up entirely of Type A and B soils. The majority of which are Type A soils. The predominate soils are Blakeland loamy sand, Columbine gravelly sandy loam, and Stapleton sandy loam. The first two soils are Type A soil and cover approximately 55.1% of the site and the later soil is a Type B soil and covers the remaining 44.9% of the site. See Appendix A for the NRCS soil map.

Current ground cover is predominantly short- to mid-grass prairie grasslands and former farmland which consists of nonnative weeds and grasses. The site has very few, if any, trees and a minimal number of shrubs are found on the site.

**d. Major drainage ways and structures**

As mentioned previously, 4 major drainage ways exist on the site. These convey existing on and off-site flows and current on-site flows through the site in a southeasterly direction. The drainageways eventually cross Highway 24 via culverts and other structures; further survey will be conducted to determine their effectiveness as the development of the site progresses.

A breached stock pond is located along the Main Stem; while it is breached, it still causes some ponding along the channel. As development occurs, this dam will be completely removed, and the region of the channel will be regraded to match the existing character of the remainder of the Main Stem channel. Improvements along the Main Stem Channel will be limited to the previously described reach.

Main Stem Tributary will be realigned through the site and will meander through a designated 100-foot corridor generally maintaining a 1% slope with a series of grade control structures. MST will be constructed to achieve a channel that is high functioning and will require low maintenance.

East Fork and East Fork Tributary improvements will be implemented to ensure the channels are high functioning low maintenance drainageway corridors.

**e. Existing and proposed land uses**

The existing site is open rangeland and farmland with no visible structures. The proposed development will consist of low, medium, and high density residential, along with two institutional sites, multiple pocket park sites, a large community park and a commercial area adjacent to Highway 24. The current land plan assumes approximately 3,261 dwelling units will be constructed on the site.

Land Use	MAX DU/AC
Low	2
Medium	4
Medium – High	8
High	12

### III. Hydrologic Analysis

**a. Major Basins and subbasins**

**Major Basin Description**

- Previous basin study: Gieck Ranch Drainage Basin Planning Study
- Per FEMA FIRM 08041C0556G and 08041C0552G (eff. 12/7/2018), Grandview Reserve has four mapped channels within its boundaries.
- Per aerial imaging, no major irrigation is in the vicinity that would affect Grandview Reserve.

The site has been divided into 8 major drainage basins per where each basin is tributary to a full spectrum detention pond facility. These basins and associated sub basins are described in more detail in the next section of this report.

## Subbasin Description

The entire site drains in a south easterly direction and is divided into 8 major drainage basins and a total of 18 subbasins together as described below.

- Subbasin A1 is located in the southwestern corner of the site, to the south and west of MS. The basin drains towards the southeast to proposed detention pond A. Current planning documents call for medium density dwelling units and a small pocket park. The basin is 37.00 acres, with a composite impervious value of 35.22% and runoff rates for the 5 and 100 year of 30.72 cfs and 100.64 cfs respectively. The pond will discharge at predevelopment rates and into MS via the ponds outlet structure.
- Subbasin B1 is located between MS and MST2 to the east of subbasin A1. The basin drains towards the southeast and towards subbasin B2. Current planning documents call for medium density dwelling units and some parkland area. The basin is 37.00 acres, with a composite impervious value of 45.00% and runoff rates for the 5 and 100 year of 29.46 cfs and 97.08 cfs respectively.
- Subbasin B2 is located between MS and MST2 to the northeast of subbasin A1. The basin drains towards the southeast and towards Detention Pond B. Current planning documents call for medium density dwelling units. The basin is 24.89 acres, with a composite impervious value of 43.26% and runoff rates for the 5 and 100 year of 12.02 cfs and 42.26 cfs respectively.
- Subbasin B3 is located between MS and EF and to the northeast of east of basin B2. The existing MST2 tributary runs through the basin. The site drains towards the southeast and towards Detention Pond B. Current planning documents call for high, medium-high, and medium density dwelling units along with a pocket park. The basin is 118.90 acres, with a composite impervious value of 49.42% and runoff rates for the 5 and 100 year of 92.76 cfs and 295.27 cfs respectively.
- Subbasin C1 is located to the northeast of east of basin B1 and the existing MST2 tributary runs through the middle of the basin. The basin drains towards the southeast and towards Detention Pond C. Current planning documents call for an institutional parcel, medium and high density dwelling units and a pocket park. The basin is 77.83 acres, with a composite impervious value of 51.20% and runoff rates for the 5 and 100 year of 77.99 cfs and 238.03 cfs respectively.
- Subbasin D1 is located between MS and MST2 to the east of Basin B3 and adjacent to the MST2 channel. The basin drains towards the southeast and towards drainage basin D2. Current planning documents call for medium density dwelling units along with a pocket park. The basin is 24.33 acres, with a composite impervious value of 53.89% and runoff rates for the 5 and 100 year of 24.15 cfs and 70.07 cfs respectively.
- Subbasin D2 is located between MS and MST2 to the south of basins D1 and B3. The basin drains towards the southwest and towards detention pond D. Current planning documents call for high density dwelling units along with a pocket park and a commercial parcel. The basin is 77.90 acres, with a composite impervious value of 62.10% and runoff rates for the 5 and 100 year of 98.47 cfs and 252.18 cfs respectively.
- Subbasin E1 is located just east of EFT along the northern portion of the site. The basin drains towards the southeast and towards basins F3 and F4. Current planning documents call for low

density dwelling units. The basin is 88.60 acres, with a composite impervious value of 19.54% and runoff rates for the 5 and 100 year of 46.88 cfs and 178.04 cfs respectively.

- Subbasin F1 is located east of basin E1 and between EFT and EF along the northern portion of the site. The basin drains towards the southeast and towards basin F3 and F4. Current planning documents call for a large community park, high density dwelling units, commercial site and an institution parcel. The basin is 33.73 acres, with a composite impervious value of 25.00% and runoff rates for the 5 and 100 year of 16.28 cfs and 58.95 cfs respectively.
- Subbasin F2 is located east of the existing drainage channel EFT. The basin drains towards the southwest and towards basin F4 and to the EFT drainage channel which runs parallel to the north east with Highway 24. Current planning documents call for high density dwelling units and commercial space. The basin is 67.64 acres, with a composite impervious value of 51.39% and runoff rates for the 5 and 100 year of 60.11 cfs and 170.90 cfs respectively.
- Subbasin F3 is located west of the existing drainage channel EF. The basin drains towards the southeast towards drainage channel EF but will be conveyed south towards subbasin F4. Current planning documents call for medium density dwelling units. The basin is 12.84 acres, with a composite impervious value of 45.00% and runoff rates for the 5 and 100 year of 11.36 cfs and 32.93 cfs respectively.
- Subbasin F4 is located west of the existing drainage channel EF and south of subbasins F1 and F3. The basin drains towards the southeast towards detention pond F. Current planning documents call for medium and medium-high density dwelling units. The basin is 51.81 acres, with a composite impervious value of 49.54% and runoff rates for the 5 and 100 year of 42.32 cfs and 124.89 cfs respectively.
- Subbasin G1 is located west of the existing drainage channel EFT along the northern property boundary. The basin drains towards the southeast towards detention pond G. Current planning documents call for medium density dwelling units and a park. The basin is 20.13 acres, with a composite impervious value of 36.52% and runoff rates for the 5 and 100 year of 13.78 cfs and 43.95 cfs respectively.
- Subbasin G2 is located east of the existing drainage channel EFT along the northern property boundary. The basin drains towards the southeast towards detention pond G. Current planning documents call for low density dwelling units. The basin is 15.14 acres, with a composite impervious value of 25.00% and runoff rates for the 5 and 100 year of 6.55 cfs and 23.95 cfs respectively.
- Subbasin H1 is located in the northeast corner of the site and east of the existing drainage channel EFT. The basin drains towards the south towards subbasin H4. Current planning documents call for low density dwelling units and a small park. The basin is 20.71 acres, with a composite impervious value of 24.49% and runoff rates for the 5 and 100 year of 5.68 cfs and 27.62 cfs respectively.
- Subbasin H2 is located south of basin G2 and east of the existing drainage channel EFT. The basin drains towards the south towards subbasin H4. Current planning documents call for medium density dwelling units and a small park. The basin is 18.55 acres, with a composite



impervious value of 46.68% and runoff rates for the 5 and 100 year of 16.24 cfs and 47.62 cfs respectively.

- Subbasin H3 is located south of basin H2 and east of the existing drainage channel EFT. The basin drains towards the southeast towards subbasin H4. Current planning documents call for medium density dwelling units and a small park. The basin is 6.01 acres, with a composite impervious value of 40.57% and runoff rates for the 5 and 100 year of 5.21 cfs and 15.60 cfs respectively.
- Subbasin H4 is located south of basin H2 and east of the existing drainage channel EFT and basin H3. The basin drains towards the south towards detention pond H. Current planning documents call for medium density dwelling units and park/open space area. The basin is 27.65 acres, with a composite impervious value of 38.24% and runoff rates for the 5 and 100 year of 20.93 cfs and 64.71 cfs respectively.

The above mentioned basins are large planning area basins and as drainage reports are developed for the individual developed parcels additional drainage reports and calculations will be required. It is expected that storm drainage infrastructure consisting of inlets, storm sewer and open drainage channels will be constructed as the property develops.

- Offsite Basins as shown in the Meridian Ranch MDDP include basins HG4, HG5, HG6A, HG6B, HG13, and HG14. Flow contributing to the site from these basins will be routed through the existing tributaries. Flow rates as shown in the MDDP Ranch report include the following flows and associated tributary areas.

Offsite Flow Summary					
Basin Description	Ultimate Design Point	Basin Area (ac)	Receiving Tributary	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)
HG4	G6	57	Main Stem	2	42
HG5	G6	72	Main Stem	3	52
HG6A	G6	88	Main Stem	3	51
HG6B	G6	66	Main Stem	2	35
HG13	G08	54	Main Stem Tributary 2	4	59
HG14	G08	147	Main Stem Tributary 2	5	83

Offsite Flow Summary				
Design Point	Basin Area (ac)	Receiving Tributary	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)
G6	760	Main Stem	36	628
G08	201	Main Stem Tributary 2	8	122



These basins along with the offsite basins which lie east of Eastonville Road contribute flows onto the site through the major tributaries. Estimate oncoming flows for each tributary are as follows:

Offsite Flow Summary		
Tributary	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)
Main Stem	36	628
Main Stem Tributary 2	8	122
East Fork Tributary*	56	116
East Fork*	175	357

\*Flows from Gieck Ranch  
DBPS, Oct 2010

As hydraulic analysis continues for the channels, these offsite flows will be used to size the channels for proper conveyance of the flow however it should be noted that the flows mentioned for the Main Stem and Main Stem Tributary 2 assume proper conveyance of the flow through (below or above) Eastonville Road. Due to the unknown nature of these conditions at the time of buildout, a probable scenario of the split flows will require analysis and agreed upon flow rates to each channel will be required. Currently some of the flow shown going to the Main Stem Tributary 2 may be diverted into the Main Stem. Previous analysis done by JR Engineering assumed approximately 160 additional cfs going to the Main Stem Tributary #2 during the 100-year event and as such it is recommended the following flows be used for analysis of the oncoming offsite flows:

Revised Offsite Flow Summary		
Tributary	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)
Main Stem**	67	413
Main Stem Tributary 2**	59	280
East Fork Tributary*	61	217
East Fork*	180	595

\*Flows from Gieck Ranch  
DBPS, Oct 2010

\*\*Flows from 4 Way Ranch LOMR, Mar 2004

Please note that the preliminary drainage reports will be required to reconcile any differences between the various reports done for these channels.

## b. Methodology

Design rainfall was determined utilizing figures from the NOAA Atlas 14, Volume 8, Version 2 to determine the 5-year and 100-year rainfall values for 1, 6 and 24-hour events. The 1-hour rainfall depths are 1.22 and 2.50 in/hr respectively, 6 hour 1.79 and 3.87 in/hr respectively and 2.36 and 4.90 in/hr for the 24 hour event. The rainfall values were then used as inputs into the Colorado Urban Hydrograph Procedure (CUHP) spreadsheets to determine runoff values for both pre-development and post-development site.

CUHP is an evolution of the Snyder unit hydrograph and is calibrated for use along the Colorado Front Range. 1 Hour rainfall amounts are input into the program to produce a storm hyetograph that is then used to calculate a storm hydrograph for each basin depending on the subbasins properties including

slope, length, shape, impervious area, pervious depression storage area, and various infiltration rates. Tabular hydrographs are then computed and can be used in EPA SWMM. The CUHP results are included within Appendix B.

EPA SWMM was used to determine flow routing via the kinematic wave method. Subbasins were routed to their respective design points and detention ponds for both the developed and predeveloped condition to determine peak runoff amounts for the 5-year and 100-year storm events. Information from these models along with information and calculations performed in the Colorado Springs BMP spreadsheets was used to determine pond sizing calculations and release rates.

### c. Basin Hydrology

A summary of the flows for both the predeveloped and developed cases for each basin, subbasin and Pond are found on next page along with the full computation found in Appendix B.

SWMM Basin and Pond Summary						
Basin Description	Basin Area (ac)	% Impervious	5 Year Peak Runoff (cfs)	100 Year Peak Runoff (cfs)	5 Year Pond Volume (ac-ft)	100 Year Pond Volume (ac-ft)
A1	45.38	35.22%	30.72	100.64		
<b>Pond A</b>					1.83	3.50
B1	37.00	45.00%	29.46	97.08		
B2	24.89	43.26%	12.02	42.26		
B3	118.90	49.42%	92.76	295.27		
<b>Pond B</b>					5.90	19.00
C1	77.83	51.20%	77.99	238.03		
<b>Pond C</b>					3.91	6.87
D1	24.33	44.14%	24.15	70.07		
D2	77.90	62.10%	98.47	252.18		
<b>Pond D</b>					6.61	10.19
E1	88.60	19.54%	46.88	178.04		
<b>Pond E</b>					1.96	2.44
F1	33.73	25.00%	16.28	58.95		
F2	67.64	51.39%	60.11	170.90		
F3	12.84	45.00%	11.36	32.93		
F4	51.81	46.54%	42.32	124.89		
<b>Pond F</b>					7.38	12.62
G1	20.13	36.52%	13.78	43.95		
G2	15.14	25.00%	6.55	23.95		
<b>Pond G</b>					0.72	2.03
H1	20.71	24.49%	5.68	27.62		
H2	18.55	43.68%	16.24	47.62		
H3	6.01	40.57%	5.21	15.60		
H4	27.65	38.24%	20.93	64.71		
<b>Pond H</b>					2.93	6.17

## IV. Hydraulic Analysis

### a. Major Drainageways

In general, the site runoff flows towards the 4 major drainageways and in a southeasterly direction. These basins are described in more detail below:

#### **Main Stem**

The Main Stem (MS) is in the southwestern portion of the site. Offsite flows collect and are conveyed under Eastonville Road via a culvert. MS travels in a southeasterly direction and combines with the Main Stem Tributary #2 (MST2) just off site where it is then conveyed past Highway 24 via a culvert. An existing breached stock pond exists in the approximate center point of the channel within the site. Jurisdictional wetlands exist within this channel and the area is within a Zone A floodplain towards the southern portion of the site. This channel sees only intermittent flows at this time however once development occurs there may be a more constant baseflow.

Proposed improvements for MS include the removal of the breached stock pond berm and regrading of the affected stretch of channel to restore its historic state. Proposed flow rates through MS are not to exceed historic flowrates and as such, the remainder of the channel is to remain in its current state sans any preemptive check structures; modeling indicates the channel shall remain stable despite the removal of the existing berm.

#### **Main Stem Tributary #2**

MST2 crosses Eastonville road via an existing culvert and flows through the site in a southeasterly direction. Portions of this channel are within a mapped floodplain as shown in the existing FIRM Panel. Per a July email from the USACE this drainage channel was preliminarily determined to be a non-jurisdictional waters/wetland.

Proposed improvements for MST2 include the realignment of the channel, generally shifting the channel towards the west to accommodate the proposed land plan. There is to be a dedicated 100' corridor in which the valley will meander. Preliminary analysis indicates the valley will have an average width of approximately 63' at the elevation necessary to meet freeboard requirements; initial sizing approximates the bankfull width to be 6.8'. The valley and channel thalweg will generally follow the same profile, with some deviation as the bankfull channel meanders through the valley in turn decreasing the low flow channels average slope. The average valley profile is to be approximately 1% with a series of grade control structures to both decrease elevation and dissipate energy to meet natural channel criteria as outline in El Paso County criteria and agreed upon channel parameters.

#### **East Fork Tributary**

The East Fork tributary (EFT) crosses the north property line and flows are conveyed through the site via a natural channel. The channel has been mapped as a Zone A floodplain per the existing FIRM panel; it appears any hydraulic effects of the crossing at Eastonville Road was not accounted for in the floodplain delineation. While the current floodplain delineation shows the channel continuing through Highway 24, there is no existing crossing for this section of the drainage channel below Highway 24 and instead the flows are conveyed to the northeast towards the East Fork Upper (EF). Per a July email from the USACE this drainage channel was preliminarily determined to be a non-jurisdictional waters/wetland.

Per SWMM modeling the current velocities will require channel stabilization. The EFT channel is to be engineered later in the design which will likely include a combination of channel widening, lowering of slope facilitated by the implementation of drop structures to meet non erosive velocity requirements. Bank stabilization, should it be necessary, may include coir rolls, erosion control blankets, live willow staking, soil lifts and/or other measures to ensure successful bank stabilization. The drainageway will require further analysis and design which will be completed as the project progresses.

### **East Fork Upper**

The EF crosses the north property line approximately 1500' east of the EFT crossing. The flow through the site is via a natural channel and travels in a southeasterly direction. The channel is mapped as a Zone A floodplain, and the channel crosses Highway 24 via an existing shallow bridge. The current floodplain delineation shows EF and EFT eventually merging approximately 1750' southeast of the site, however, as mentioned above Highway 24 blocks the flow of the EFT and flows are conveyed northeast to the EF bridge crossing.

Per SWMM modeling the current velocities will require channel stabilization. The EF channel is to be engineered later in the design which will likely include a combination of channel widening, lowering of slope facilitated by the implementation of drop structures to meet non erosive velocity requirements. Bank stabilization, should it be necessary, may include coir rolls, erosion control blankets, live willow staking, soil lifts and/or other measures to ensure successful bank stabilization. The drainageway will require further analysis and design which will be completed as the project progresses.

## **V. Environmental Evaluations**

### **a. Significant existing or potential wetland and riparian areas impacts**

As part of this work, the developer has engaged Ecosystem Services, LLC (ECOS) to perform environmental studies of the site that will be submitted with the planning documents. Major information from this report related to the wetlands shows that two of the tributaries through the site, the Main Stem and the East Fork contain jurisdictional wetlands and the other two tributaries, the East Fork Tributary and the Main Stem Tributary #2 are non-jurisdictional wetlands.

At this time, only minor improvements to the jurisdictional channels are proposed. These stream improvements will be made with keeping the natural habitat intact and the natural function of these channels as it is to maintain the wetland habitat. The non-jurisdictional channels will be modified, and the design of those channels is forthcoming.

### **b. Stormwater quality considerations and proposed practices**

As part of the development, full spectrum detention facilities will be installed to provide water quality for the development. The facilities will be designed using El Paso County criteria and provide stormwater quality by slowing the release of stormwater captured by the ponds and allowing solids to settle out. Additionally, when possible, the revised drainage channels, which were not jurisdictional wetlands, will be used to convey stormwater via a natural channel. Stormwater must be treated before entering the natural channels. The natural channel will provide a pervious means to transport stormwater and provide some water quality benefits as well.

On site practices for the homes, schools, churches, and other buildings should use means such that impervious areas drain across pervious area to allow for infiltration during the minor events. This would

include discharge of the gutters onto landscape areas vs. directly connecting to storm sewer and using natural ditches and swales where it is logical and makes sense to convey stormwater in lieu of storm sewer piping.

### **c. Permitting requirements**

When work infringes upon the wetlands or floodplain a 404 Permit will be required. If the work within the waterways is minimal, it will likely be covered under a nationwide 404 permit; it is however possible that an individual permits will be required.

The Colorado Department of Public Health and Environment will require permits for any disturbance that exceed 1 acre of land. Should groundwater be encountered, a dewatering permit will also be required.

El Paso County will require an Erosion and Stormwater Quality Control Permit and any other construction permits required to complete the construction of the site.

FEMA will require a permit for floodplain development prior to the commencement of any construction or development within any special flood hazard area (SFHA).

FEMA will require a letter of map revision (LOMR) should work alter the base flood elevation (BFE) of any area falling within the floodplain as shown in FEMA FIRM 08041C0556G and FIRM 08041C0552G (eff. 12/7/2018).

### **d. 4-Step Process**

In accordance with the Engineering Criteria Manual I.7.2.A and DCM V2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume, and considering the need for Industrial Commercial BMPs.

**Step 1 – Reducing Runoff Volumes:** The development of the project site includes a variety of land uses including open and vegetated areas interspersed to help disconnect impervious areas and reduce runoff volumes.

**Step 2 – Stabilize Drainageways:** Altered channels will be designed in a manner that provides water quality benefits through infiltration and the removal of pollutants via phytoremediation. Vegetation will also be selected to stabilize the channel by reducing the velocity of flows and decreasing any scour. Should the final channel require, grade control structures may be implemented to further reduce flow velocities and protect against erosion. These improvements will help stabilize drainageways.

**Step 3 – Provide WQCV:** Runoff from this development is treated through capture and slow release of the WQCV via detention ponds that are designed per current El Paso County DCM V2.

**Step 4 – Consider the need for Industrial and Commercial BMP's:** A site specific storm water quality and erosion control plan and narrative will be prepared with subsequent land use approvals prepared in conjunction with the report prior to any construction. Site specific temporary source control BMPs as well as permanent BMPs are detailed in this plan and narrative. Guidelines detailed in the El Paso DCM V2 4.2 pertaining to the covering and storage handline and spill containment and control shall be followed as necessary.

## VI. Selected Plan

### a. Plan Hydrology

This MDDP schematically addressed on-site and off-site drainage patterns using the existing topography and proposed land use plan for the overall drainage design. Individual preliminary and final drainage reports will better define the planning areas as the site is developed. These reports will include inlet design, storm sewer hydraulics, street design and other requirements typical of more detailed drainage reports.

The overall site is divided into 8 separate major basins, basins A-H and contribute to individual detention ponds for each major basin. Basin sizes range from 35 acres to 181 acres in size. Basins A, B, C and D drain and eventually discharge into the Main Stem and Main Stem Tributary #2. Basins E, F, G, and H drain towards the East Fork Drainage channel.

The sub-basins are described in additional detail above.

### b. Detention Ponds

The site plans propose the construction of 8 separate full spectrum detention facilities.

- Pond A is located in the southwest corner of the site and discharges into the Main Stem drainageway. The pond is planned to store a maximum of 4.05 ac-ft during the 100 year event and have a peak outflow of 55.9 cfs which is slightly below the pre development peak outflow of 57.1 cfs. The 5 year storage volume is 2.46 ac-ft with a peak outflow of 3.7 cfs.
- Pond B is located to the east of Pond A and the Main Stem and discharges into the Main Stem Tributary #2. The pond is planned to store a maximum of 16.60 ac-ft during the 100 year event and have a peak outflow of 165.4 cfs which is slightly above the pre development peak outflow of 164.2 cfs. The 5 year storage volume is 8.44 ac-ft with a peak outflow of 2.6 cfs.
- Pond C is located near the center of the western portion of the site near the existing Main Stem Tributary #2. The pond discharges into a revised open channel to be designed and discharges to the Main Stem Tributary #2 which merges with the Main Stem Tributary just off site. The pond is planned to store a maximum of 6.91 ac-ft during the 100 year event and have a peak outflow of 119.2 cfs which is slightly below the pre development peak outflow of 120.2 cfs. The 5 year storage volume is 4.07 ac-ft with a peak outflow of 1.5 cfs.
- Pond D is located near the southern portion of the site adjacent to Highway 24. The pond discharges into the Main Stem right after the Main Stem and Main Stem Tributary #2 merge. The pond is planned to store a maximum of 9.41 ac-ft during the 100 year event and have a peak outflow of 154.4 cfs which equals the predevelopment peak flow rate. The 5 year storage volume is 6.28 ac-ft with a peak outflow of 2.0 cfs.
- Pond E is located in the middle of the site just east of the East Fork drainage way. The pond discharges into the East Fork drainageway. The pond is planned to store a maximum of 2.40 ac-ft during the 100 year event and have a peak outflow of 163.4 cfs which is greater than the pre



development peak outflow of 157.99 cfs. The 5 year storage volume is 1.70 ac-ft with a peak outflow of 18.8 cfs.

- Pond F is located near the south east corner of the site just west of the East Fork Tributary drainageway. The pond discharges into the East Fork Tributary drainageway. The pond is planned to store a maximum of 12.40 ac-ft during the 100 year event and have a peak outflow of 235.5 cfs which is greater than the pre development peak outflow of 221.11 cfs. The 5 year storage volume is 8.07 ac-ft with a peak outflow of 14.5 cfs.
- Pond G is located near the north east corner of the site just west of the East Fork Tributary drainageway. The pond discharges into the East Fork Tributary drainageway at an upstream location within the site. The pond is planned to store a maximum of 2.54 ac-ft during the 100 year event and have a peak outflow of 50.7 cfs which is slightly greater than the pre development peak outflow of 48.48 cfs. The 5 year storage volume is 1.69 ac-ft with a peak outflow of 9.1 cfs.
- Pond H is located near the south east corner of the site just east of the East Fork Tributary drainageway and adjacent to Highway 24. The pond discharges into the East Fork Tributary drainageway. The pond is planned to store a maximum of 6.60 ac-ft during the 100 year event and have a peak outflow of 99.1 cfs which matches the pred development peak outflow. The 5 year storage volume is 4.03 ac-ft with a peak outflow of 1.3 cfs.

Overall runoff from the site will by and large match the predevelopment peak flows. The volume of water will increase however as the drainage channels are designs, continuous simulation models will be done to see the effects of prolonged runoff rates. Predevelopment and post development flows for the 5-year and 100-year events are summarized in the following table for the 4 site outfalls.

OUTFALL	Predevelopment		Postdevelopment*	
	5 year	100 year	5 year	100 year
1	80.03	479.80	67.69	466.95
2	85.96	597.41	61.68	536.11
3	30.00	154.35	8.58	160.70
4	341.05	1335.77	276.10	1291.25

\*Values to be refined with Preliminary and Final Drainage Reports for each filing

## VII. Drawings

Please refer to the appendices for vicinity maps and drainage basin maps.

## VIII. Summary

Grandview Reserve is a large master planned community consisting of various densities of dwelling units to include single family homes, multifamily homes, parks, institutional sites, and commercial areas. Due to development increased runoff will occur. To mitigate downstream impacts 8 large full spectrum detention facilities will be built to reduce the runoff rate to near historic levels. These detention facilities will provide water quality enhancements to account for the increased urbanization of the upstream catchment areas.

Additional analysis will be required and completed to review the hydraulics of the proposed major drainage channels and be included in future submittals. The proposed design, as described in this report, is not anticipated to cause any adverse impact to downstream properties however as noted previously due to the increased volume of water, downstream tributaries will see increases in the volume of flow. It is advised that low impact design be considered when designing and developing each filing. This shall include those items listed in the four-step process above and any additional measures that are within reason to disconnect impervious areas and increase infiltration. This will alleviate the additional volume of water due to development. Although the rate will remain at or below historic levels, the amount of time the channels will see water will increase which may cause more channel movement than historic. Downstream planning efforts should allow for the natural migration and movement of the channel by continuing to provide large floodplain areas to allow movement of the channel.

## IX. References

El Paso County – Drainage Criteria Manual, 2014

City of Colorado Springs – Drainage Criteria Manual, May 2014

Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018

Unnamed Tributary Black Squirrel Cree, Four Way Ranch Letter of Map Revisions, Kiowa Engineering, March 2004

Haegler and Geick Drainage Basins Letter of Map Revision, Four Way Ranch Subdivision, Kiowa, March 2004

Unnamed Tributary Black Squirrel Creek Drainage Basin, Letter of Map Revision, Elbert Road Site, Kiowa Engineering, February 2006

Geick Ranch Drainage Basin Planning Study (DBPS), Drexel Barrell, October 2010 (not approved)

EPC Engineering Criteria Manual (Appendix I updated July, 2019)

Meridian Ranch MDDP, January 2018

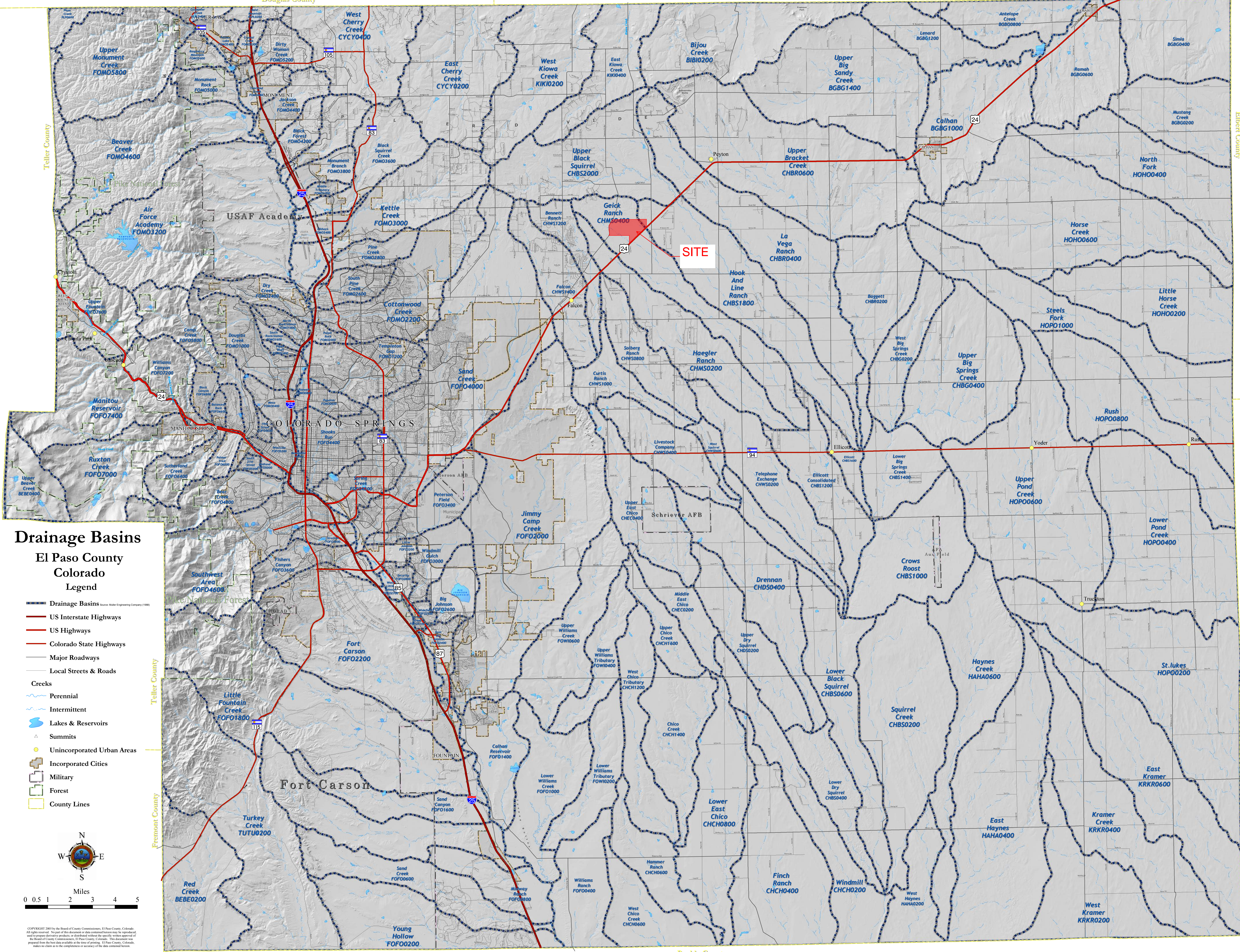


## Appendix A









Douglas County

Elbert County



### Drainage Basins

#### El Paso County Colorado Legend

-  Drainage Basins (source: Muler Engineering Company 1986)
-  US Interstate Highways
-  US Highways
-  Colorado State Highways
-  Major Roadways
-  Local Streets & Roads
- Creeks**
-  Perennial
-  Intermittent
-  Lakes & Reservoirs
-  Summits
-  Unincorporated Urban Areas
-  Incorporated Cities
-  Military
-  Forest
-  County Lines



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To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the **Flood Profiles and Floodway Data** and/or **Summary of Stillwater Elevations** tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations and are not necessarily the exact elevations. Floodway data and/or flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal base flood elevations are not provided in the Summary of Stillwater Elevations and Floodway Data tables. For information regarding the production of FIRM's for adjacent jurisdictions may result in slight, positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NNGS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel configurations that are different from those shown on this map. The Flood Profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile and Floodway Data Tables may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes are to emissions or operations may have occurred since the data were collected, users should contact appropriate community officials to verify current corporate limit locations.

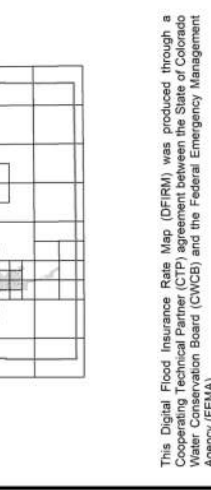
Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program details for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

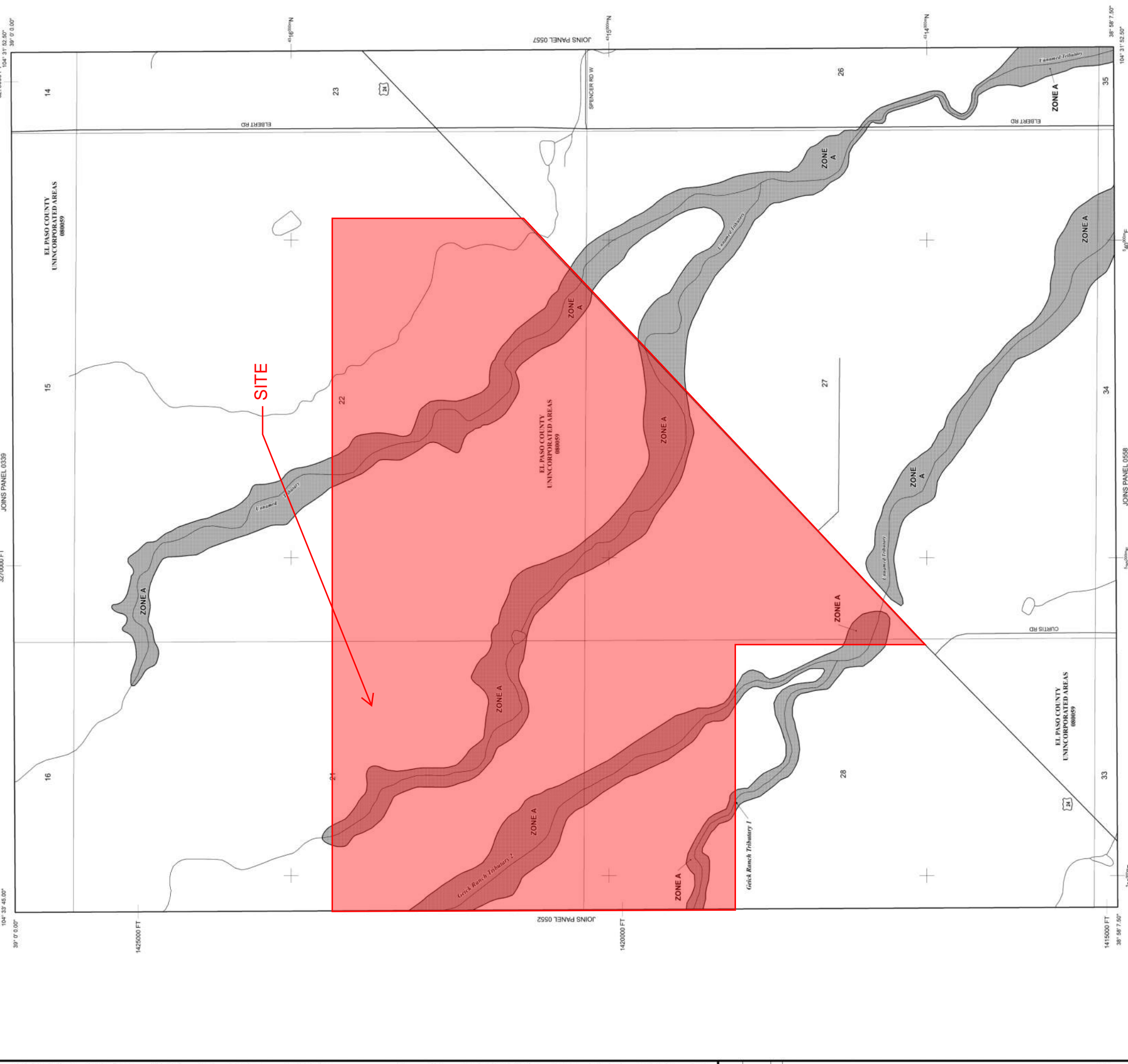
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP (1-877-336-2627)** or visit the FEMA website at <http://www.fema.gov/business/nfp>.

**El Paso County Vertical Datum Offset Table**

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperative Agreement between the El Paso County Office of Emergency Management, Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



**ZONE A**  
No Base Flood Elevations determined.

**ZONE AE**  
Base Flood Elevations determined.

**ZONE AH**  
Special Flood Hazard Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently abandoned. Zone boundaries are shown by a dashed line.

**ZONE AO**  
Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. For areas of abutment flooding, velocities also determined.

**ZONE AR**  
Special Flood Hazard Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently abandoned. Zone boundaries are shown by a dashed line.

**ZONE AW**  
Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

**OTHER AREAS**  
Areas determined to be outside the 0.2% annual chance floodplain.

**ZONE D**  
Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**  
CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

**OTHERWISE PROTECTED AREAS (OPAs)**  
Floodplain boundary  
Roadway boundary  
Zone D boundary  
CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.  
Base Flood Elevation line and value; elevation in feet\*  
Base Flood Elevation value where uniform within zone; elevation in feet\*  
\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line  
Transect line  
Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)  
97° 07' 30.00"  
32° 22' 30.00"  
579mN  
1000 meter Universal Transverse Mercator grid ticks, zone 13  
6000000 FT  
6000000 FT  
6000000 FT  
Datum: Colorado State Plane coordinate system, central zone (PROZONE 5000), Lambert Conformal Conic Projection  
Bench mark (see explanation in Notes to Users section of this FIRM panel)  
DX5519  
M1.5  
River Mile

MAP REPOSITORIES  
Refer to Map Repositories list on Map Index.  
EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP  
MARCH 17, 1997

**EFFECTIVE DATES OF REVISIONS TO THIS PANEL**  
Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map repository information, refer to the Community Map Repository table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-358-9620.

**FIRM**  
FLOOD INSURANCE RATE MAP  
EL PASO COUNTY,  
COLORADO  
AND INCORPORATED AREAS  
PANEL 556 OF 1300  
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:  
COMMUNITY NUMBER 080039  
EL PASO COUNTY PANEL 0556

MAP NUMBER 08041C0556G  
MAP REVISED

MAP REVISIONS

MAP SCALE 1" = 500'  
ELEVATION: 0, 50, 100, 150, 200, 250 FEET  
0, 100, 200 METERS

**NFIP**  
NATIONAL FLOOD INSURANCE PROGRAM



To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded, whole-foot values and are not necessarily exact. Floodway data is provided for informational purposes only and should not be used as the sole source of flood elevation information in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only to areas with a 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations and Floodway Data tables. Floodway data is provided for informational purposes only and floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with the floodway boundaries being defined by the 1% annual chance flood elevation and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones were used in the production of FIRMs for adjacent jurisdictions may result in slight, positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
 NOAA, NINGS12  
 National Geodetic Survey  
 SSMC-3, #9202  
 1315 East-West Highway  
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel configurations that are different from those shown on this map. Flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the flood profiles and floodway data may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes in the locations of or dimensions of structures may have occurred since the previous FIRM, users should contact appropriate community officials to verify current corporate limit locations.

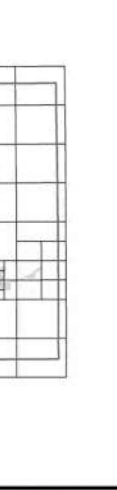
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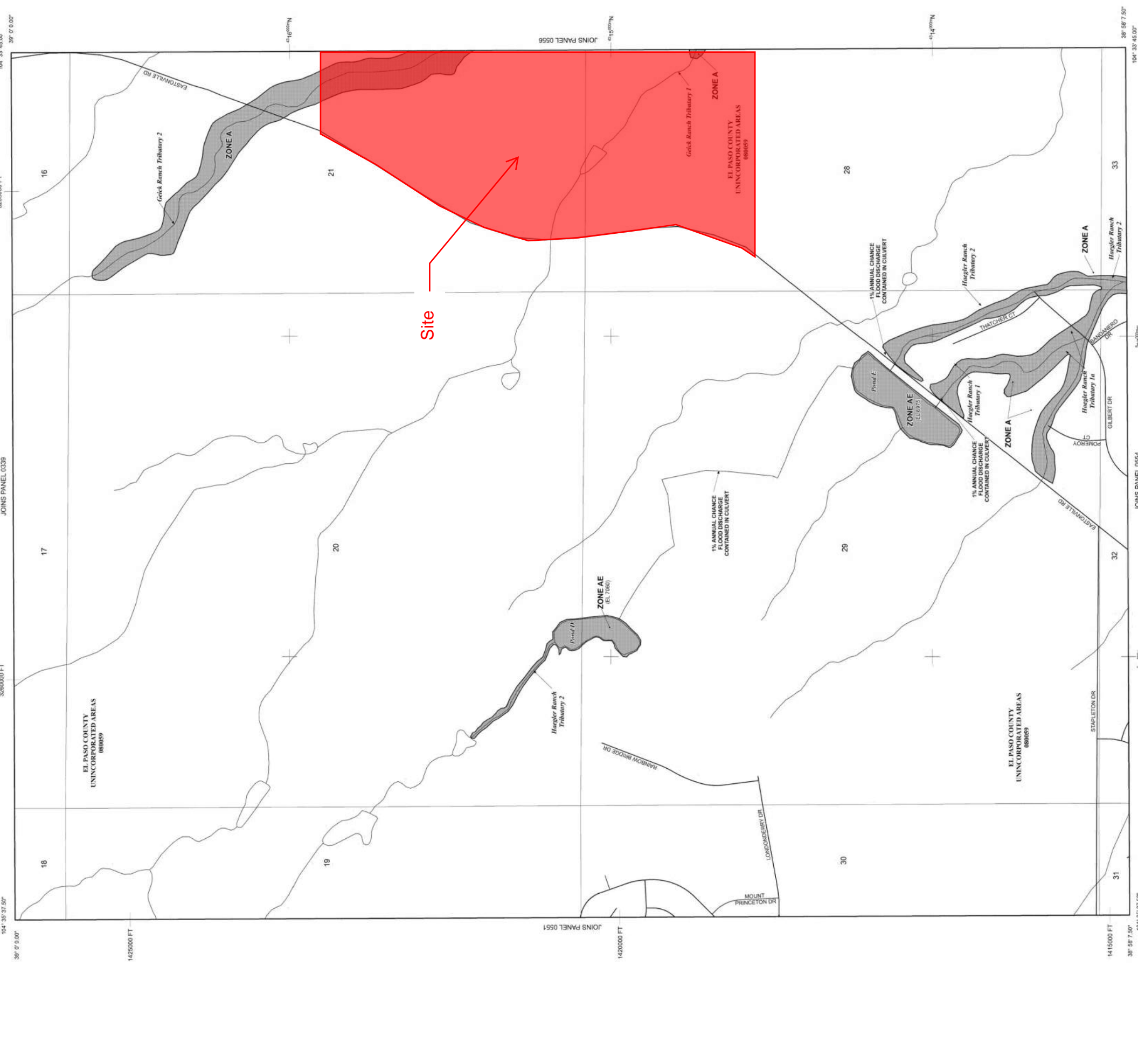
**El Paso County Vertical Datum Offset Table**

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	



**Panel Location Map**

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



**ZONE A** No Base Flood Elevations determined.

**ZONE AE** Base Flood Elevations determined.

**ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

**ZONE AO** Flood depths of 1 to 3 feet (usually areas of ponding); Average depths determined. For areas of shallow fan flooding, velocities also determined.

**ZONE AR** Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently described. Zone AR areas are shown in gray. Flood depths are determined by the 1% annual chance of greater flood protection system under construction; no Base Flood Elevations determined.

**ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

**ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE** The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

**OTHER FLOOD AREAS**

**ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

**OTHER AREAS**

**ZONE X** Areas determined to be outside the 0.2% annual chance floodplains.

**ZONE D** Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**

**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary  
 Floodway boundary  
 Zone D boundary  
 CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities  
 Base Flood Elevation line and value; elevation in feet\*  
 Base Flood Elevation value where uniform within zone;  
 elevation in feet\*

\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

Transect line

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)  
 97° 07' 30.00"  
 32° 22' 30.00"

416°00'N  
 415°00'N

600000 FT  
 5000-foot grid ticks. Coordinates shown in these coordinate systems are based on the North American Datum of 1983.  
 Lambert Conformal Conic Projection

Bench mark (see explanation in notes to Users section of this FIRM page)  
 River Mile

**MAP REPOSITORIES**  
 Refer to Map Repositories list on Map Index

**EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP**  
 MARCH 11, 1991

**EFFECTIVE DATES OF REVISIONS TO THIS PANEL**  
 DECEMBER 7, 2006  
 This panel was revised to incorporate the 1% Annual Chance Flood Insurance Study report for this jurisdiction, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.  
 To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

**FIRM**  
**FLOOD INSURANCE RATE MAP**  
**EL PASO COUNTY,**  
**COLORADO**  
**AND INCORPORATED AREAS**

**PANEL 552 OF 1300**  
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:  
 COMMUNITY  
 EL PASO COUNTY  
 NUMBER  
 0502  
 PANEL  
 552  
 SHEETS  
 6

**NATIONAL FLOOD INSURANCE PROGRAM**

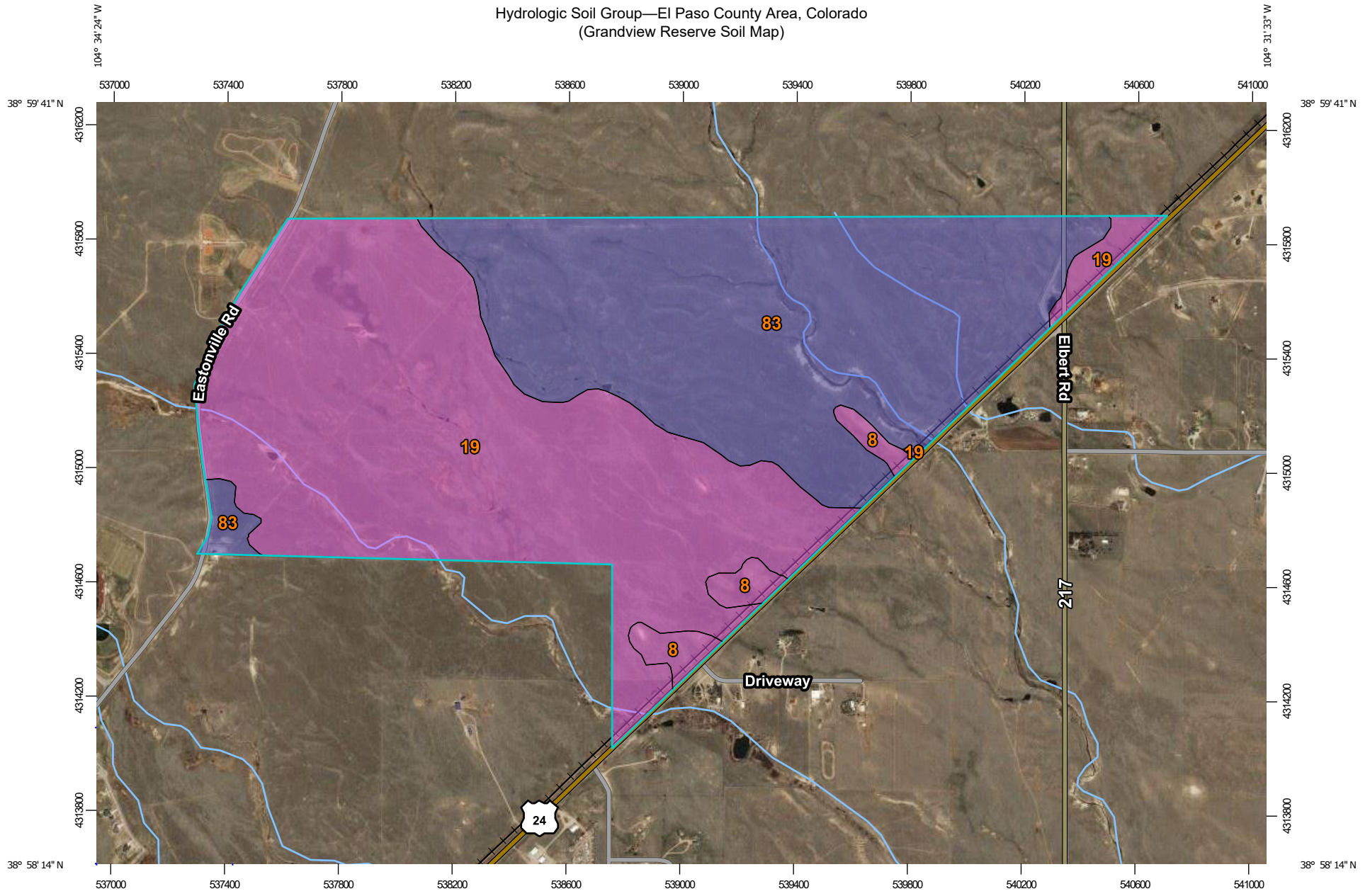
**MAP NUMBER**  
 08041C0552G  
**MAP REVISION**

MAP SCALE 1" = 500'

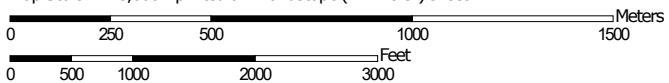
**PANEL 0552G**



Hydrologic Soil Group—El Paso County Area, Colorado  
(Grandview Reserve Soil Map)



Map Scale: 1:18,800 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84

Hydrologic Soil Group—El Paso County Area, Colorado  
(Grandview Reserve Soil Map)

**MAP LEGEND**

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available

**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

**MAP INFORMATION**

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
Survey Area Data: Version 17, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 8, 2018—May 26, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.4	2.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	450.7	52.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	B	385.4	44.9%
<b>Totals for Area of Interest</b>			<b>858.5</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher



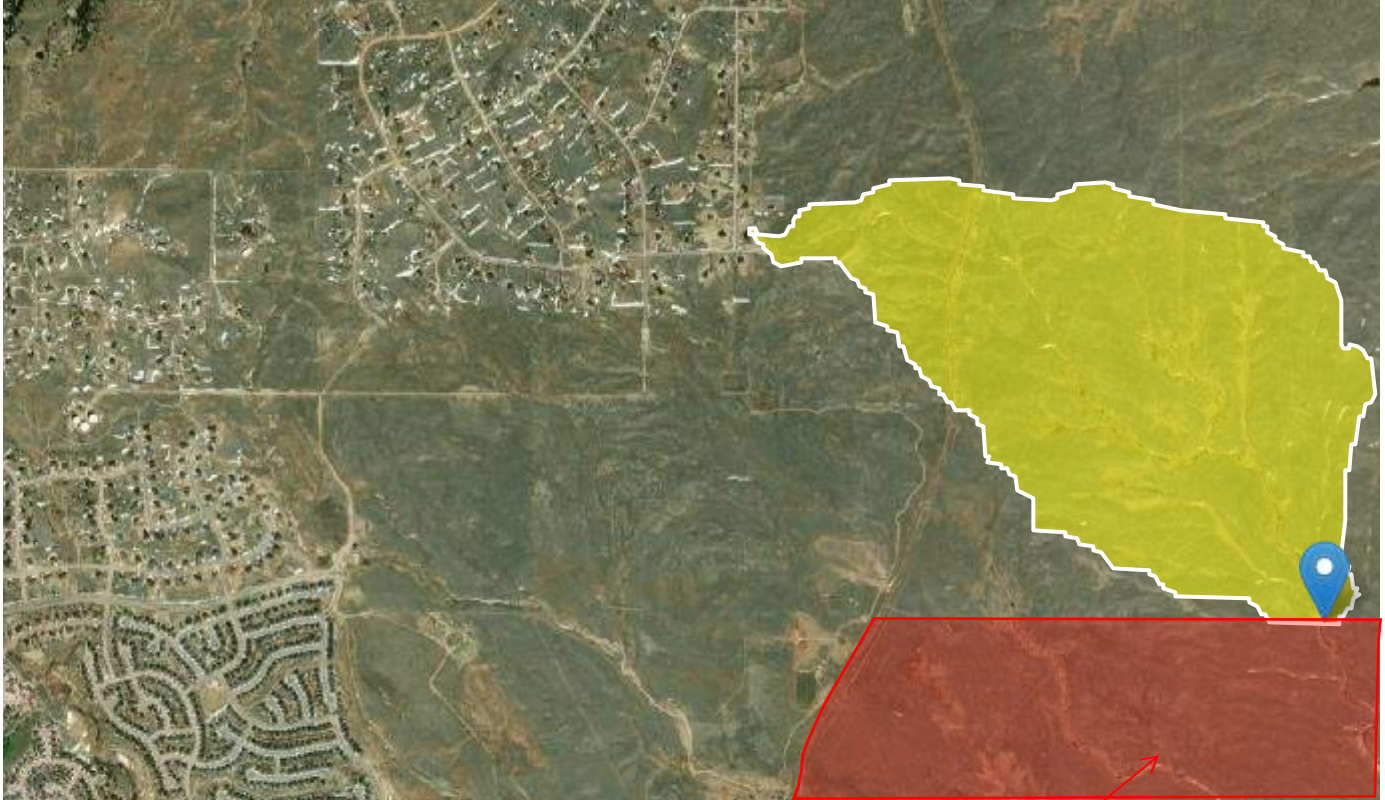
# EAST FORK

Region ID: CO

Workspace ID: CO20200817220340831000

Clicked Point (Latitude, Longitude): 38.99090, -104.54663

Time: 2020-08-17 16:03:57 -0600



Grandview Reserve

## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	4	percent
DRNAREA	Area that drains to a point on a stream	0.84	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4.9	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.86	inches



<b>Parameter Code</b>	<b>Parameter Description</b>	<b>Value</b>	<b>Unit</b>
RCN	Runoff-curve number as defined by NRCS ( <a href="http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba">http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba</a> )	58.28	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.22	dimensionless

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Application Version: 4.4.0

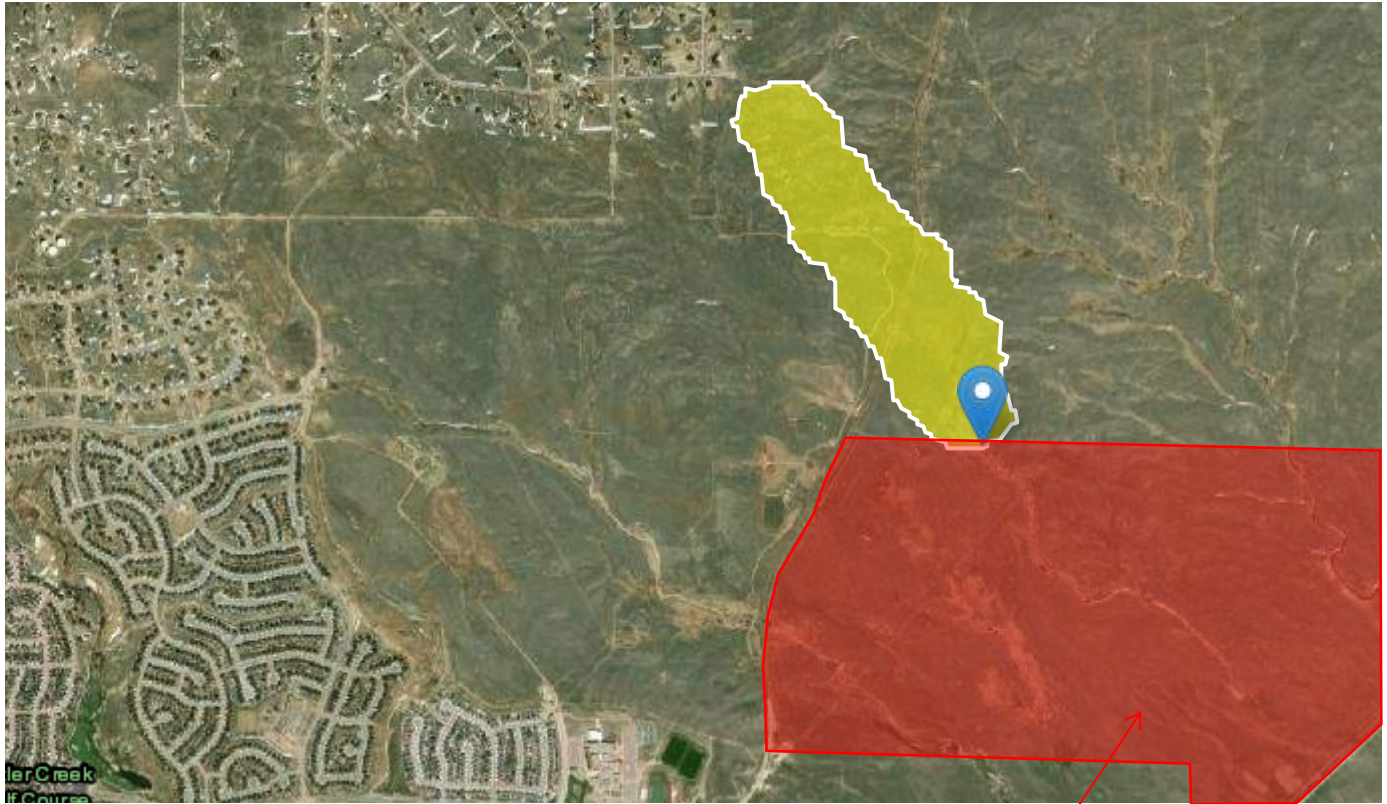
# EAST FORK TRIBUTARY BASIN DELINATION

**Region ID:** CO

**Workspace ID:** C020200817220732890000

**Clicked Point (Latitude, Longitude):** 38.99085, -104.55989

**Time:** 2020-08-17 16:07:50 -0600



Grandview Reserve

## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	3	percent
DRNAREA	Area that drains to a point on a stream	0.22	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4.92	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.86	inches

<b>Parameter Code</b>	<b>Parameter Description</b>	<b>Value</b>	<b>Unit</b>
RCN	Runoff-curve number as defined by NRCS ( <a href="http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba">http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba</a> )	54.53	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.23	dimensionless

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Application Version: 4.4.0

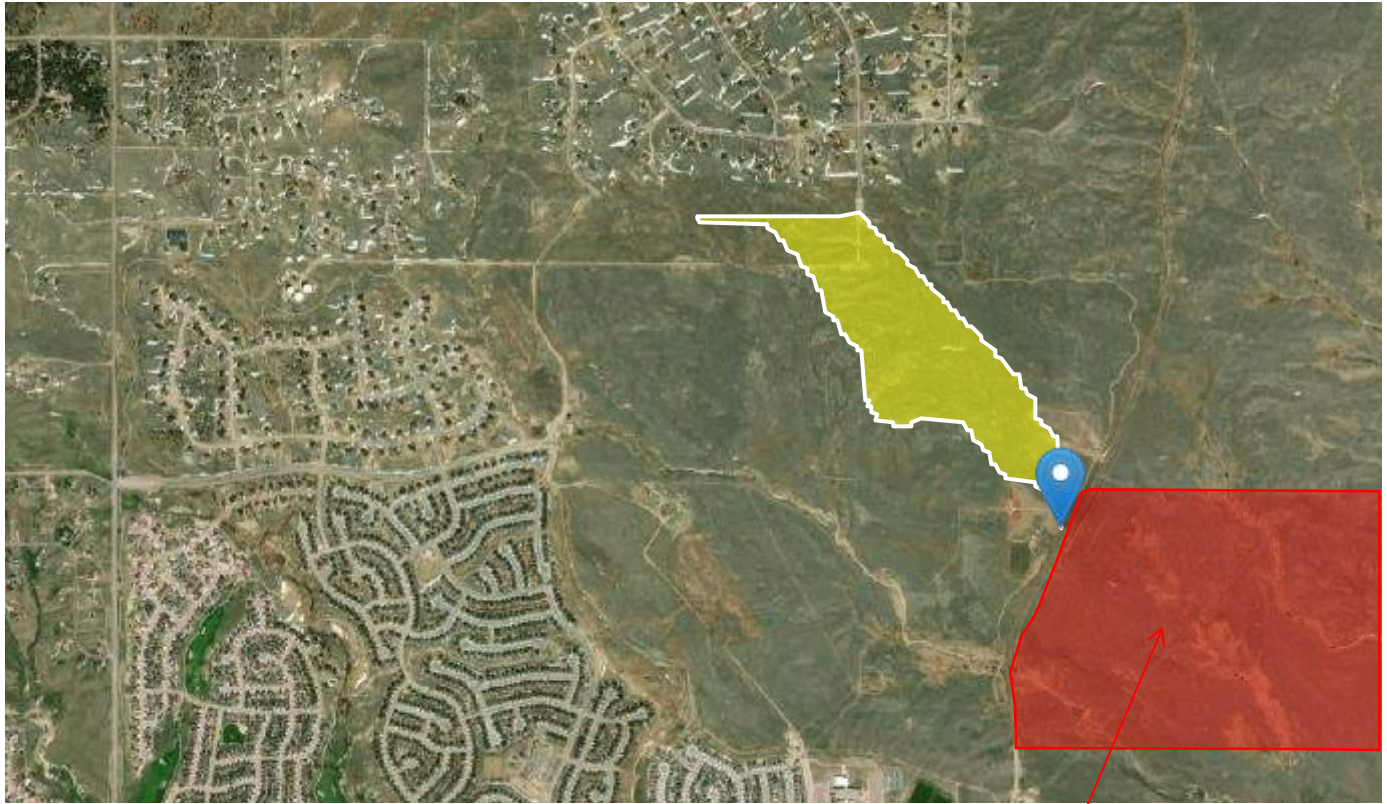
# MAIN STEM

Region ID: CO

Workspace ID: CO20200817221517278000

Clicked Point (Latitude, Longitude): 38.98969, -104.56703

Time: 2020-08-17 16:15:34 -0600



Grandview Reserve

## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	3	percent
DRNAREA	Area that drains to a point on a stream	0.17	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.87	inches

<b>Parameter Code</b>	<b>Parameter Description</b>	<b>Value</b>	<b>Unit</b>
RCN	Runoff-curve number as defined by NRCS ( <a href="http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba">http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba</a> )	55.04	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.22	dimensionless

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Application Version: 4.4.0



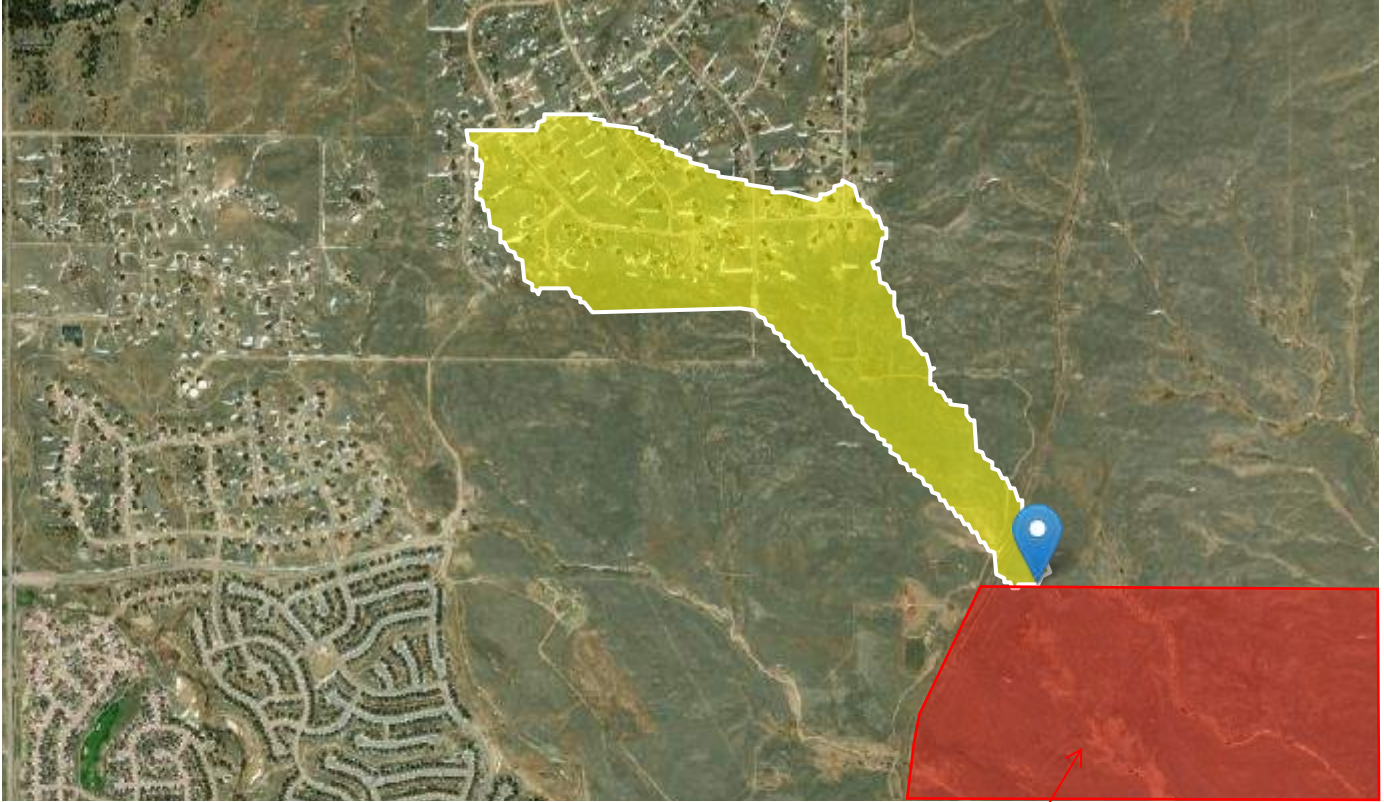
# MAIN STEM TRIBUTARY NUMBER 2

Region ID: CO

Workspace ID: C020200817221139984000

Clicked Point (Latitude, Longitude): 38.99101, -104.56354

Time: 2020-08-17 16:11:57 -0600



Basin Characteristics

Grandview Reserve

Parameter Code	Parameter Description	Value	Unit
BSLDEM10M	Mean basin slope computed from 10 m DEM	3	percent
DRNAREA	Area that drains to a point on a stream	0.44	square miles
I24H100Y	Maximum 24-hour precipitation that occurs on average once in 100 years	4.94	inches
I24H2Y	Maximum 24-hour precipitation that occurs on average once in 2 years - Equivalent to precipitation intensity index	1.87	inches



<b>Parameter Code</b>	<b>Parameter Description</b>	<b>Value</b>	<b>Unit</b>
RCN	Runoff-curve number as defined by NRCS ( <a href="http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba">http://policy.nrcs.usda.gov/OpenNonWebContent.aspx?content=17758.wba</a> )	56.49	dimensionless
RUNCO_CO	Soil runoff coefficient as defined by Verdin and Gross (2017)	0.23	dimensionless

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Application Version: 4.4.0



## Appendix B

Basin Description	Park/Open Space	High Density/Schools	Med/High Density	Med Density	Low Density	Commercial	Total Impervious	Total Acreage	Composite Percent Impervious	Predominant Soil Group	5 Year C Factor	100 Year C Factor
Impervious Percentage	10%	65%	55%	45%	25%	75%						
A1	12.68	0.00	0.00	32.70	0.00	0.00	15.98	45.38	35.22%	B	0.38	0.71
<b>Pond A</b>								<b>45.38</b>	<b>35.22%</b>			
B1	0.00	0.00	0.00	37.00	0.00	0.00	16.65	37.00	45.00%	A	0.4	0.61
B2	1.24	0.00	0.00	23.65	0.00	0.00	10.77	24.89	43.26%	A	0.38	0.59
B3	7.42	12.64	53.20	45.64	0.00	0.00	58.76	118.90	49.42%	A	0.36	0.5
<b>Pond B</b>								<b>180.79</b>	<b>47.66%</b>			
C1	4.19	30.61	1.70	41.33	0.00	0.00	39.85	77.83	51.20%	A	0.38	0.59
<b>Pond C</b>								<b>77.83</b>	<b>51.20%</b>			
D1	0.60	0.00	0.00	23.73	0.00	0.00	10.74	24.33	44.14%	A	0.39	0.6
D2	5.60	64.10	0.00	0.00	0.00	8.20	48.38	77.90	62.10%	A	0.39	0.6
<b>Pond D</b>								<b>102.23</b>	<b>57.82%</b>			
E1	32.26	0.00	0.00	0.00	56.34	0.00	17.31	88.60	19.54%	B	0.12	0.59
<b>Pond E</b>								<b>88.60</b>	<b>19.54%</b>			
F1	0.00	0.00	0.00	0.00	33.73	0.00	8.43	33.73	25.00%	B	0.15	0.61
F2	18.34	40.50	0.00	0.00	0.00	8.80	34.76	67.64	51.39%	B	0.36	0.7
F3	0.00	0.00	0.00	12.84	0.00	0.00	5.78	12.84	45.00%	B	0.45	0.74
F4	6.24	0.00	29.80	15.77	0.00	0.00	24.11	51.81	46.54%	B	0.37	0.64
<b>Pond F</b>								<b>166.02</b>	<b>44.02%</b>			
G1	4.88	0.00	0.00	15.25	0.00	0.00	7.35	20.13	36.52%	B	0.25	0.66
G2	0.00	0.00	0.00	0.00	15.14	0.00	3.79	15.14	25.00%	B	0.45	0.74
<b>Pond G</b>								<b>35.27</b>	<b>31.57%</b>			
H1	0.70	0.00	0.00	0.00	20.01	0.00	5.07	20.71	24.49%	A	0.38	0.75
H2	0.70	0.00	0.00	17.85	0.00	0.00	8.10	18.55	43.68%	B	0.43	0.75
H3	0.76	0.00	0.00	5.25	0.00	0.00	2.44	6.01	40.57%	B	0.4	0.72
H4	5.34	0.00	0.00	22.31	0.00	0.00	10.57	27.65	38.24%	B	0.37	0.7
<b>Pond H</b>								<b>72.92</b>	<b>35.91%</b>			

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results									Excess Precip.		Storm Hydrograph			
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.157	0.143	37.3	5.59	19.4	3.95	9.3	57	164,729	0.25	40,666	35.0	13	40,592	0.29
B1		0.158	0.131	33.0	4.82	17.2	3.41	8.0	53	134,310	0.08	11,390	35.0	4	11,363	0.12
B2		0.158	0.109	58.5	6.42	30.4	4.54	10.7	20	90,351	0.08	7,662	40.0	2	7,665	0.07
B3		0.158	0.221	39.1	8.15	20.3	5.76	13.6	142	431,607	0.08	36,602	40.0	12	36,572	0.10
C1		0.158	0.183	30.3	5.75	15.7	4.06	9.6	120	281,797	0.08	23,898	35.0	10	23,870	0.13
D1		0.157	0.108	31.5	4.11	16.4	2.91	6.9	36	88,318	0.25	21,803	35.0	8	21,721	0.33
D2		0.157	0.182	37.7	6.77	19.6	4.78	11.3	97	282,777	0.25	69,809	40.0	22	69,820	0.29
E1		0.157	0.193	28.9	5.77	15.0	4.08	9.6	144	321,618	0.25	79,397	35.0	32	79,287	0.37
F1		0.157	0.125	37.2	5.07	19.4	3.58	8.5	42	122,440	0.25	30,227	35.0	10	30,151	0.29
F2		0.157	0.171	45.1	7.42	23.5	5.24	12.4	70	245,533	0.25	60,614	40.0	16	60,563	0.24
F3		0.157	0.081	37.8	3.84	19.6	2.72	6.4	16	46,609	0.25	11,506	35.0	4	11,472	0.28
F4		0.157	0.151	43.2	6.52	22.5	4.61	10.9	56	186,981	0.25	46,160	40.0	13	46,174	0.25
G1		0.157	0.099	38.8	4.45	20.2	3.14	7.4	24	73,072	0.25	18,039	35.0	6	17,996	0.28
G2		0.157	0.087	42.3	4.33	22.0	3.06	7.2	17	54,958	0.25	13,567	35.0	4	13,536	0.26
H1		0.158	0.101	43.7	4.89	22.7	3.45	8.1	22	75,177	0.08	6,375	35.0	2	6,365	0.09
H2		0.157	0.095	37.0	4.21	19.2	2.97	7.0	24	67,337	0.25	16,623	35.0	5	16,581	0.29
H3		0.157	0.057	32.6	2.94	16.9	2.08	4.9	9	21,816	0.25	5,384	35.0	2	5,324	0.32
H4		0.157	0.114	36.7	4.72	19.1	3.33	7.9	35	100,370	0.25	24,778	35.0	8	24,718	0.29







**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results									Excess Precip.		Storm Hydrograph			
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.156	0.142	37.3	5.57	19.4	3.93	9.3	57	164,729	1.56	257,605	45.0	67	257,125	1.47
B1		0.157	0.130	33.0	4.80	17.2	3.39	8.0	53	134,310	1.17	157,714	40.0	49	157,336	1.32
B2		0.157	0.109	58.5	6.39	30.4	4.52	10.6	20	90,351	1.17	106,094	50.0	21	106,130	0.83
B3		0.157	0.220	39.1	8.11	20.3	5.73	13.5	142	431,607	1.17	506,815	45.0	140	506,418	1.18
C1		0.157	0.182	30.3	5.72	15.7	4.04	9.5	120	281,797	1.17	330,900	40.0	111	330,490	1.43
D1		0.156	0.107	31.5	4.10	16.4	2.90	6.8	36	88,318	1.56	138,112	40.0	40	137,590	1.64
D2		0.156	0.181	37.7	6.75	19.6	4.77	11.2	97	282,777	1.56	442,208	45.0	115	442,279	1.47
E1		0.156	0.192	28.8	5.76	15.0	4.07	9.6	144	321,618	1.56	502,948	40.0	158	502,220	1.78
F1		0.156	0.124	37.2	5.06	19.4	3.57	8.4	42	122,440	1.56	191,472	45.0	49	190,993	1.47
F2		0.156	0.170	45.1	7.40	23.5	5.23	12.3	70	245,533	1.56	383,966	50.0	87	383,641	1.28
F3		0.156	0.081	37.7	3.83	19.6	2.71	6.4	16	46,609	1.56	72,888	45.0	18	72,670	1.43
F4		0.156	0.150	43.2	6.50	22.5	4.59	10.8	56	186,981	1.56	292,403	45.0	68	292,494	1.32
G1		0.156	0.099	38.8	4.44	20.2	3.14	7.4	24	73,072	1.56	114,270	45.0	28	113,996	1.41
G2		0.156	0.087	42.3	4.31	22.0	3.05	7.2	17	54,958	1.56	85,944	45.0	20	85,743	1.32
H1		0.157	0.100	43.7	4.86	22.7	3.44	8.1	22	75,177	1.17	88,277	45.0	22	88,139	1.06
H2		0.156	0.095	37.0	4.20	19.2	2.97	7.0	24	67,337	1.56	105,301	45.0	27	105,031	1.46
H3		0.156	0.057	32.6	2.93	16.9	2.07	4.9	9	21,816	1.56	34,116	40.0	10	33,729	1.58
H4		0.156	0.114	36.7	4.70	19.1	3.32	7.8	35	100,370	1.56	156,958	45.0	41	156,578	1.48





**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results									Excess Precip.		Storm Hydrograph			
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.097	0.131	25.0	4.03	13.0	2.84	6.7	85	164,729	0.57	94,676	35.0	31	94,308	0.68
B1		0.092	0.139	18.2	3.44	9.5	2.43	5.7	95	134,310	0.58	77,837	30.0	29	77,220	0.80
B2		0.093	0.113	33.3	4.40	17.3	3.11	7.3	35	90,351	0.56	50,405	35.0	12	50,284	0.48
B3		0.109	0.171	35.1	6.09	18.2	4.30	10.2	159	431,607	0.31	135,184	35.0	37	135,109	0.31
C1		0.089	0.205	15.3	3.91	7.9	2.76	6.5	238	281,797	0.64	181,072	30.0	76	180,336	0.97
D1		0.092	0.115	17.3	3.03	9.0	2.14	5.1	66	88,318	0.67	59,557	30.0	24	58,560	0.99
D2		0.084	0.229	15.9	4.30	8.3	3.04	7.2	229	282,777	0.87	246,138	30.0	98	245,292	1.26
E1		0.114	0.151	26.8	4.61	13.9	3.25	7.7	155	321,618	0.41	131,675	35.0	47	131,227	0.53
F1		0.107	0.097	32.8	3.94	17.1	2.78	6.6	48	122,440	0.47	56,968	35.0	16	56,751	0.48
F2		0.088	0.198	21.9	4.83	11.4	3.41	8.1	145	245,533	0.75	184,862	35.0	60	183,986	0.89
F3		0.092	0.087	20.4	2.87	10.6	2.03	4.8	30	46,609	0.68	31,862	30.0	11	31,302	0.88
F4		0.121	0.121	41.5	5.37	21.6	3.79	8.9	58	186,981	0.36	67,763	35.0	17	67,675	0.34
G1		0.096	0.093	25.2	3.31	13.1	2.34	5.5	37	73,072	0.59	43,083	30.0	14	42,758	0.68
G2		0.107	0.067	37.3	3.43	19.4	2.42	5.7	19	54,958	0.47	25,571	35.0	7	25,468	0.43
H1		0.109	0.078	39.3	3.85	20.4	2.72	6.4	25	75,177	0.31	23,258	35.0	6	23,195	0.27
H2		0.092	0.101	20.5	3.09	10.6	2.18	5.2	42	67,337	0.67	45,076	30.0	16	44,528	0.88
H3		0.094	0.058	19.2	2.36	10.0	1.67	3.9	15	21,816	0.64	13,878	30.0	5	13,432	0.87
H4		0.095	0.111	22.8	3.45	11.9	2.44	5.7	57	100,370	0.61	61,173	30.0	21	60,592	0.76

5-Year Post Development CUHP Output

**Printouts for Unit Hydrographs**

flow in cfs

time in minutes	A1	B1	B2	B3	C1	D1	D2	E1	F1	F2	F3	F4	G1	G2	H1	H2	H3	H4
5	77.33	93.25	30.09	102.59	220.53	65.84	199.90	128.93	44.36	115.64	29.50	42.62	37.03	18.62	23.03	42.42	14.61	55.54
10	82.78	86.57	34.71	158.92	211.37	57.29	212.53	153.31	47.44	142.37	26.77	58.18	35.84	18.73	24.44	38.99	12.72	53.96
15	70.87	64.60	32.47	154.15	146.87	42.55	148.71	136.86	43.94	117.23	20.78	56.54	30.18	17.61	23.25	30.20	9.82	43.13
20	57.63	49.16	28.07	139.10	107.74	32.08	108.63	110.77	37.50	92.72	16.66	52.59	24.96	15.66	21.07	24.25	7.67	35.72
25	47.82	39.67	24.21	116.79	80.83	25.68	83.75	93.90	32.69	72.89	13.46	46.34	20.75	13.62	18.22	19.53	6.26	28.56
30	39.89	30.81	21.23	103.58	53.91	19.28	58.88	77.26	28.57	61.39	11.05	41.06	17.44	12.21	16.48	16.06	5.00	24.34
35	34.20	21.94	18.25	90.37	40.79	13.08	41.89	67.52	24.45	50.16	8.64	37.09	14.97	10.80	14.74	12.59	3.73	20.17
40	28.51	17.08	16.20	78.14	31.82	10.94	33.60	57.77	21.87	38.93	6.23	33.12	12.50	9.45	13.00	9.12	2.78	16.00
45	22.81	14.12	14.45	70.52	22.85	8.81	25.30	48.03	19.44	28.50	5.21	29.15	10.02	8.61	11.70	7.55	2.35	11.83
50	17.12	11.17	12.70	62.89	13.88	6.68	17.01	38.28	17.01	24.76	4.40	26.80	7.55	7.77	10.67	6.39	1.93	10.13
55	15.14	8.21	10.96	55.26	4.91	4.55	8.72	30.20	14.58	21.02	3.60	24.47	6.69	6.93	9.63	5.24	1.51	8.74
60	13.25	5.26	9.21	47.63	0.00	2.41	0.43	26.95	12.15	17.28	2.80	22.14	5.86	6.09	8.60	4.08	1.09	7.35
65	11.35	2.30	7.46	40.01		0.28	0.00	23.70	9.73	13.53	1.99	19.80	5.04	5.25	7.56	2.92	0.66	5.96
70	9.45	0.00	6.57	32.38		0.00		20.45	8.85	9.79	1.19	17.47	4.21	4.41	6.53	1.77	0.24	4.57
75	7.55		5.99	29.45				17.20	8.04	6.05	0.39	15.14	3.39	3.73	5.49	0.61	0.00	3.18
80	5.65		5.41	26.90				13.96	7.23	2.30	0.00	12.80	2.56	3.45	4.78	0.00		1.79
85	3.76		4.83	24.36				10.71	6.42	0.00		11.25	1.74	3.17	4.43			0.40
90	1.86		4.24	21.82				7.46	5.61			10.48	0.92	2.89	4.09			0.00
95	0.00		3.66	19.28				4.21	4.80			9.70	0.09	2.61	3.74			
100			3.08	16.73				0.96	3.99			8.92	0.00	2.33	3.40			
105			2.50	14.19				0.00	3.18			8.14		2.05	3.05			
110			1.91	11.65					2.37			7.37		1.77	2.71			
115			1.33	9.11					1.57			6.59		1.49	2.36			
120			0.75	6.57					0.76			5.81		1.21	2.02			
125			0.16	4.02					0.00			5.03		0.93	1.67			
130			0.00	1.48								4.25		0.65	1.33			
135				0.00								3.48		0.37	0.98			
140												2.70		0.09	0.64			
145												1.92		0.00	0.29			
150												1.14			0.00			
155												0.37						
160												0.00						





**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

Catchment Name/ID	User Comment for Catchment	Unit Hydrograph Parameters and Results									Excess Precip.		Storm Hydrograph			
		CT	Cp	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f.)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
A1		0.096	0.134	24.4	4.01	12.7	2.83	6.7	87	164,729	1.93	317,756	40.0	101	316,720	2.22
B1		0.091	0.141	17.8	3.42	9.2	2.42	5.7	98	134,310	1.82	243,813	35.0	97	241,630	2.62
B2		0.092	0.115	32.5	4.38	16.9	3.09	7.3	36	90,351	1.79	161,555	40.0	42	161,041	1.70
B3		0.089	0.250	19.5	5.26	10.2	3.72	8.8	285	431,607	1.88	813,554	40.0	295	807,930	2.48
C1		0.088	0.210	14.7	3.88	7.6	2.74	6.5	247	281,797	1.91	539,141	35.0	238	535,192	3.07
D1		0.092	0.116	17.1	3.02	8.9	2.14	5.0	67	88,318	2.03	179,570	35.0	70	176,587	2.88
D2		0.083	0.230	15.8	4.30	8.2	3.04	7.2	231	282,777	2.25	634,968	35.0	252	632,818	3.24
E1		0.113	0.150	26.5	4.56	13.8	3.23	7.6	157	321,618	1.75	563,176	40.0	178	561,356	2.01
F1		0.106	0.096	32.4	3.90	16.9	2.76	6.5	49	122,440	1.81	221,916	40.0	59	221,037	1.75
F2		0.088	0.199	21.7	4.82	11.3	3.40	8.0	146	245,533	2.12	520,116	40.0	171	517,601	2.53
F3		0.091	0.088	20.1	2.86	10.5	2.02	4.8	30	46,609	2.04	95,234	35.0	33	93,473	2.56
F4		0.090	0.168	22.4	4.39	11.7	3.10	7.3	108	186,981	2.06	385,413	40.0	125	383,174	2.42
G1		0.095	0.095	24.6	3.29	12.8	2.33	5.5	38	73,072	1.94	142,048	40.0	44	140,977	2.18
G2		0.106	0.067	36.8	3.40	19.2	2.41	5.7	19	54,958	1.81	99,609	45.0	24	99,196	1.58
H1		0.107	0.078	38.6	3.80	20.1	2.69	6.3	25	75,177	1.49	111,730	45.0	28	111,424	1.33
H2		0.092	0.102	20.2	3.08	10.5	2.18	5.1	43	67,337	2.03	136,549	35.0	48	134,796	2.57
H3		0.093	0.059	18.9	2.36	9.8	1.66	3.9	15	21,816	1.99	43,454	35.0	16	42,019	2.60
H4		0.094	0.113	22.3	3.44	11.6	2.43	5.7	58	100,370	1.96	197,106	35.0	65	195,054	2.34





CUHP 100-Year Post Development

**Printouts for Unit Hydrographs**

flow in cfs

time in minutes	A1	B1	B2	B3	C1	D1	D2	E1	F1	F2	F3	F4	G1	G2	H1	H2	H3	H4
5	79.48	95.51	30.93	212.33	229.82	66.81	201.50	131.02	45.09	117.17	29.92	92.63	37.90	18.89	23.57	43.06	14.85	56.70
10	84.67	87.92	35.54	282.68	215.27	57.76	213.46	154.59	47.98	143.83	27.05	104.96	36.56	18.95	24.84	39.42	12.85	54.86
15	71.63	65.18	33.09	218.45	147.65	42.75	148.95	137.43	44.32	117.53	20.92	85.95	30.43	17.77	23.57	30.43	9.89	43.38
20	58.21	48.97	28.30	170.33	107.98	32.20	108.75	111.17	37.59	92.99	16.68	69.02	25.18	15.74	21.25	24.29	7.66	35.92
25	47.87	39.61	24.48	132.75	78.94	25.61	83.53	93.98	32.85	72.85	13.48	54.84	20.77	13.71	18.39	19.57	6.27	28.68
30	40.08	30.32	21.34	107.50	49.89	19.02	58.31	77.43	28.63	61.37	11.00	46.28	17.51	12.26	16.59	16.00	4.96	24.34
35	34.09	21.04	18.21	82.24	39.94	13.05	41.79	67.50	24.41	49.89	8.52	38.16	14.92	10.82	14.79	12.42	3.65	20.00
40	28.10	16.93	16.26	57.04	30.26	10.85	33.38	57.58	21.90	38.40	6.04	30.04	12.33	9.48	12.98	8.85	2.77	15.66
45	22.11	13.83	14.43	48.62	20.58	8.66	24.98	47.65	19.41	28.45	5.18	21.93	9.74	8.62	11.74	7.51	2.33	11.51
50	16.99	10.74	12.59	40.20	10.90	6.46	16.57	37.72	16.92	24.63	4.35	18.95	7.50	7.76	10.67	6.32	1.89	10.06
55	15.00	7.64	10.76	31.78	1.22	4.26	8.16	30.14	14.43	20.80	3.52	16.25	6.63	6.90	9.60	5.12	1.46	8.61
60	13.00	4.55	8.92	23.36	0.00	2.07	0.00	26.83	11.95	16.97	2.70	13.54	5.77	6.04	8.53	3.93	1.02	7.17
65	11.00	1.45	7.15	14.94		0.00		23.53	9.65	13.14	1.87	10.83	4.91	5.18	7.46	2.74	0.58	5.72
70	9.01	0.00	6.53	6.53				20.22	8.82	9.32	1.04	8.13	4.04	4.32	6.39	1.55	0.15	4.27
75	7.01		5.92	0.00				16.91	7.99	5.49	0.22	5.42	3.18	3.72	5.32	0.36	0.00	2.82
80	5.01		5.31					13.60	7.16	1.66	0.00	2.72	2.31	3.43	4.76	0.00		1.38
85	3.02		4.70					10.29	6.33	0.00		0.01	1.45	3.15	4.41			0.00
90	1.02		4.09					6.98	5.50			0.00	0.59	2.86	4.05			
95	0.00		3.47					3.67	4.67				0.00	2.57	3.69			
100			2.86					0.36	3.84					2.29	3.34			
105			2.25					0.00	3.01					2.00	2.98			
110			1.64						2.18					1.71	2.62			
115			1.03						1.35					1.43	2.27			
120			0.41						0.52					1.14	1.91			
125			0.00						0.00					0.85	1.55			
130														0.57	1.19			
135														0.28	0.84			
140														0.00	0.48			
145															0.12			
150															0.00			





## Appendix C

SWMM Model Pre Development 5 Year

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

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SWMM Pre Development 5 Year

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NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS  
Process Models:  
  Rainfall/Runoff ..... NO  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Flow Routing Method ..... KINWAVE  
Starting Date ..... 01/01/2005 00:00:00  
Ending Date ..... 01/01/2005 06:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:05:00  
Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	12.024	3.918
External Outflow .....	12.024	3.918
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	0.000	0.000
Continuity Error (%) .....	-0.002	

SWMM Model Pre Development 5 Year

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.08	0.31	6945.31	0 00:35	0.30
24	JUNCTION	0.10	0.44	6934.44	0 00:40	0.44
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.10	0.48	6911.48	0 00:35	0.48
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.11	0.48	6900.48	0 00:35	0.48
65	JUNCTION	0.17	0.69	6880.69	0 00:36	0.69
66	JUNCTION	0.24	0.89	6868.89	0 00:40	0.89
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0 00:00	0.00
73	JUNCTION	0.11	0.43	6902.43	0 00:35	0.42



SWMM Model Pre Development 5 Year

80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.11	0.48	6872.48	0	00:35	0.47
85	JUNCTION	0.06	0.30	6874.30	0	00:35	0.30
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.11	0.44	6911.44	0	00:41	0.43
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.11	0.42	6900.42	0	00:36	0.42
PondH	JUNCTION	0.11	0.47	6866.47	0	00:36	0.47
PondF	JUNCTION	0.24	0.89	6866.89	0	00:41	0.88
PondD	JUNCTION	0.10	0.48	6881.48	0	00:37	0.47
Outfall12	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall11	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall14	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall13	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
31	OUTFALL	0.00	0.00	6953.00	0	00:00	0.00
51	OUTFALL	0.00	0.00	6920.00	0	00:00	0.00
74	OUTFALL	0.00	0.00	6897.00	0	00:00	0.00
67	OUTFALL	0.00	0.00	6865.50	0	00:00	0.00

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Inflow Volume gal	Flow Balance Error Percent	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal
10	0.304	JUNCTION	13.03	13.03	0 00:35	0.304
20	0.085	JUNCTION	4.33	4.33	0 00:35	0.085
21	0.0573	JUNCTION	1.66	1.66	0 00:40	0.0573

SWMM Model Pre Development 5 Year

22		JUNCTION	11.85	11.85	0	00:40	0.274
0.274	0.000						
23		JUNCTION	0.00	5.99	0	00:35	0
0.142	0.000						
24		JUNCTION	0.00	11.85	0	00:40	0
0.274	0.000						
30		JUNCTION	9.95	9.95	0	00:35	0.179
0.179	0.000						
40		JUNCTION	8.12	8.12	0	00:35	0.162
0.162	0.000						
41		JUNCTION	22.23	22.23	0	00:40	0.522
0.522	0.000						
42		JUNCTION	0.00	8.12	0	00:35	0
0.162	0.000						
50		JUNCTION	32.34	32.34	0	00:35	0.593
0.593	0.000						
60		JUNCTION	9.70	9.70	0	00:35	0.226
0.226	0.000						
61		JUNCTION	16.46	16.46	0	00:40	0.453
0.453	0.000						
62		JUNCTION	3.65	3.65	0	00:35	0.0858
0.0858	0.000						
63		JUNCTION	12.98	12.98	0	00:40	0.345
0.345	0.000						
64		JUNCTION	0.00	13.35	0	00:35	0
0.311	0.000						
65		JUNCTION	0.00	26.04	0	00:36	0
0.657	0.000						
66		JUNCTION	0.00	16.46	0	00:40	0
0.453	0.000						
70		JUNCTION	5.57	5.57	0	00:35	0.135
0.135	0.000						
71		JUNCTION	3.87	3.87	0	00:35	0.101
0.101	0.000						
72		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000						
73		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000						
80		JUNCTION	1.85	1.85	0	00:35	0.0476
0.0476	0.000						
81		JUNCTION	5.37	5.37	0	00:35	0.124
0.124	0.000						
82		JUNCTION	1.92	1.92	0	00:35	0.0398
0.0398	0.000						
83		JUNCTION	8.07	8.07	0	00:35	0.185
0.185	0.000						
84		JUNCTION	0.00	7.22	0	00:35	0
0.172	0.000						

SWMM Model Pre Development 5 Year

85		JUNCTION	0.00	1.92	0	00:35	0
0.0398	0.000						
PondC		JUNCTION	0.00	9.95	0	00:35	0
0.179	0.000						
PondA		JUNCTION	0.00	13.03	0	00:35	0
0.304	0.000						
PondB		JUNCTION	0.00	17.56	0	00:41	0
0.416	0.000						
PondE		JUNCTION	0.00	32.34	0	00:35	0
0.593	0.000						
PondG		JUNCTION	0.00	9.42	0	00:36	0
0.236	0.000						
PondH		JUNCTION	0.00	17.11	0	00:36	0
0.397	0.000						
PondF		JUNCTION	0.00	42.32	0	00:41	0
1.11	0.000						
PondD		JUNCTION	0.00	30.00	0	00:38	0
0.685	0.000						
Outfall2		OUTFALL	0.00	17.56	0	00:41	0
0.416	0.000						
Outfall1		OUTFALL	0.00	13.03	0	00:35	0
0.304	0.000						
Outfall4		OUTFALL	0.00	17.11	0	00:36	0
0.397	0.000						
Outfall3		OUTFALL	0.00	30.00	0	00:38	0
0.685	0.000						
31		OUTFALL	0.00	9.95	0	00:35	0
0.179	0.000						
51		OUTFALL	0.00	32.34	0	00:35	0
0.593	0.000						
74		OUTFALL	0.00	9.42	0	00:36	0
0.236	0.000						
67		OUTFALL	0.00	42.32	0	00:41	0
1.11	0.000						

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*



Outfall Node	SWMM Model Pre Development 5 Year			
	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall2	67.36	3.82	17.56	0.416
Outfall1	55.28	3.40	13.03	0.304
Outfall4	59.31	4.14	17.11	0.397
Outfall3	60.56	7.00	30.00	0.685
31	50.97	2.17	9.95	0.179
51	51.53	7.12	32.34	0.593
74	58.61	2.49	9.42	0.236
67	65.97	10.41	42.32	1.110
System	58.70	40.55	169.75	3.918

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	13.03	0 00:35			
200	DUMMY	4.33	0 00:35			
201	DUMMY	1.66	0 00:40			
202	CONDUIT	5.95	0 00:36	10.09	0.00	0.04
204	DUMMY	11.85	0 00:40			
205	CONDUIT	11.83	0 00:41	11.82	0.01	0.06
300	DUMMY	9.95	0 00:35			
400	DUMMY	8.12	0 00:35			
401	CONDUIT	8.03	0 00:37	8.38	0.02	0.10
402	DUMMY	22.23	0 00:40			
500	DUMMY	32.34	0 00:35			
601	DUMMY	16.46	0 00:40			
602	CONDUIT	16.42	0 00:41	6.99	0.07	0.18
603	DUMMY	9.70	0 00:35			
604	DUMMY	3.65	0 00:35			
605	CONDUIT	13.32	0 00:36	11.62	0.01	0.07
606	DUMMY	12.98	0 00:40			
607	CONDUIT	26.04	0 00:36	12.42	0.02	0.09
700	DUMMY	5.57	0 00:35			
701	DUMMY	3.87	0 00:35			
702	DUMMY	3.87	0 00:35			
703	CONDUIT	3.86	0 00:36	4.80	0.01	0.08
801	DUMMY	1.85	0 00:35			

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802	DUMMY	5.37	0	00:35			
803	CONDUIT	7.18	0	00:36	6.34	0.01	0.07
804	DUMMY	1.92	0	00:35			
806	DUMMY	8.07	0	00:35			
805	CONDUIT	1.91	0	00:37	4.00	0.01	0.06
301	DUMMY	9.95	0	00:35			
101	DUMMY	13.03	0	00:35			
206	DUMMY	17.56	0	00:41			
501	DUMMY	32.34	0	00:35			
704	DUMMY	9.42	0	00:36			
807	DUMMY	17.11	0	00:36			
608	DUMMY	42.32	0	00:41			
403	DUMMY	30.00	0	00:38			

\*\*\*\*\*

Conduit Surcharge Summary

\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Fri Apr 10 17:42:01 2020

Analysis ended on: Fri Apr 10 17:42:01 2020

Total elapsed time: < 1 sec

SWMM 5 Year Output Ex 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... NO  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/01/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	193.874	63.177
External Outflow .....	193.874	63.177
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	0.000	0.000
Continuity Error (%) .....	-0.000	



SWMM 5 Year Output Ex 9-21-20

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

Link 205 (1)  
 Link 206 (1)

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.08	0.31	6945.31	0 00:35	0.30
24	JUNCTION	0.13	0.58	6934.58	0 00:40	0.58
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.10	0.48	6911.48	0 00:35	0.48
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.11	0.48	6900.48	0 00:35	0.48
65	JUNCTION	0.17	0.69	6880.69	0 00:36	0.69
66	JUNCTION	0.24	0.89	6868.89	0 00:40	0.89
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0 00:00	0.00

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73	JUNCTION	0.11	0.43	6902.43	0	00:35	0.42
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.11	0.48	6872.48	0	00:35	0.47
85	JUNCTION	0.06	0.30	6874.30	0	00:35	0.30
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.13	0.58	6911.58	0	00:40	0.58
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.11	0.42	6900.42	0	00:36	0.42
PondH	JUNCTION	0.11	0.47	6866.47	0	00:36	0.47
PondF	JUNCTION	0.24	0.89	6866.89	0	00:41	0.88
PondD	JUNCTION	0.10	0.48	6881.48	0	00:37	0.47
31	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
51	JUNCTION	0.00	0.00	6920.00	0	00:00	0.00
67	JUNCTION	0.00	0.00	6865.50	0	00:00	0.00
74	JUNCTION	0.00	0.00	6897.00	0	00:00	0.00
OS1	JUNCTION	0.00	0.00	6950.00	0	00:00	0.00
OS2	JUNCTION	0.00	0.00	6924.00	0	00:00	0.00
OS3	JUNCTION	0.00	0.00	6930.00	0	00:00	0.00
OS4	JUNCTION	0.00	0.00	6905.00	0	00:00	0.00
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Inflow Volume		Flow Balance Error	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence	Lateral Inflow Volume
gal	Percent			CFS	CFS	days hr:min	10^6 gal
10			JUNCTION	13.03	13.03	0 00:35	0.304

SWMM 5 Year Output Ex 9-21-20

0.304	0.000						
20		JUNCTION	4.33	4.33	0	00:35	0.085
0.085	0.000						
21		JUNCTION	1.66	1.66	0	00:40	0.0573
0.0573	0.000						
22		JUNCTION	11.85	11.85	0	00:40	0.274
0.274	0.000						
23		JUNCTION	0.00	5.99	0	00:35	0
0.142	0.000						
24		JUNCTION	0.00	21.23	0	00:40	0
0.452	0.000						
30		JUNCTION	9.95	9.95	0	00:35	0.179
0.179	0.000						
40		JUNCTION	8.12	8.12	0	00:35	0.162
0.162	0.000						
41		JUNCTION	22.23	22.23	0	00:40	0.522
0.522	0.000						
42		JUNCTION	0.00	8.12	0	00:35	0
0.162	0.000						
50		JUNCTION	32.34	32.34	0	00:35	0.593
0.593	0.000						
60		JUNCTION	9.70	9.70	0	00:35	0.226
0.226	0.000						
61		JUNCTION	16.46	16.46	0	00:40	0.453
0.453	0.000						
62		JUNCTION	3.65	3.65	0	00:35	0.0858
0.0858	0.000						
63		JUNCTION	12.98	12.98	0	00:40	0.345
0.345	0.000						
64		JUNCTION	0.00	13.35	0	00:35	0
0.311	0.000						
65		JUNCTION	0.00	26.04	0	00:36	0
0.657	0.000						
66		JUNCTION	0.00	16.46	0	00:40	0
0.453	0.000						
70		JUNCTION	5.57	5.57	0	00:35	0.135
0.135	0.000						
71		JUNCTION	3.87	3.87	0	00:35	0.101
0.101	0.000						
72		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000						
73		JUNCTION	0.00	3.87	0	00:35	0
0.101	0.000						
80		JUNCTION	1.85	1.85	0	00:35	0.0476
0.0476	0.000						
81		JUNCTION	5.37	5.37	0	00:35	0.124
0.124	0.000						
82		JUNCTION	1.92	1.92	0	00:35	0.0398



SWMM 5 Year Output Ex 9-21-20

0.0398	0.000						
83		JUNCTION	8.07	8.07	0	00:35	0.185
0.185	0.000						
84		JUNCTION	0.00	7.22	0	00:35	0
0.172	0.000						
85		JUNCTION	0.00	1.92	0	00:35	0
0.0398	0.000						
PondC		JUNCTION	0.00	9.95	0	00:35	0
0.179	0.000						
PondA		JUNCTION	0.00	13.03	0	00:35	0
0.304	0.000						
PondB		JUNCTION	0.00	26.96	0	00:40	0
0.594	0.000						
PondE		JUNCTION	0.00	32.34	0	00:35	0
0.593	0.000						
PondG		JUNCTION	0.00	189.42	0	00:36	0
29.3	0.000						
PondH		JUNCTION	0.00	17.11	0	00:36	0
0.397	0.000						
PondF		JUNCTION	0.00	42.32	0	00:41	0
1.11	0.000						
PondD		JUNCTION	0.00	30.00	0	00:38	0
0.685	0.000						
31		JUNCTION	0.00	9.95	0	00:35	0
0.179	0.000						
51		JUNCTION	0.00	93.34	0	00:35	0
10.4	0.000						
67		JUNCTION	0.00	231.47	0	00:40	0
30.4	0.000						
74		JUNCTION	0.00	189.42	0	00:36	0
29.3	0.000						
OS1		JUNCTION	67.00	67.00	0	00:00	10.8
10.8	0.000						
OS2		JUNCTION	59.00	59.00	0	00:00	9.53
9.53	0.000						
OS3		JUNCTION	61.00	61.00	0	00:00	9.86
9.85	0.000						
OS4		JUNCTION	180.00	180.00	0	00:00	29.1
29.1	0.000						
Outfall2		OUTFALL	0.00	85.96	0	00:40	0
10.1	0.000						
Outfall1		OUTFALL	0.00	80.03	0	00:35	0
11.1	0.000						
Outfall4		OUTFALL	0.00	341.05	0	00:36	0
41.2	0.000						
Outfall3		OUTFALL	0.00	30.00	0	00:38	0
0.685	0.000						

SWMM 5 Year Output Ex 9-21-20

\*\*\*\*\*  
 Node Flooding Summary  
 \*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
 Outfall Loading Summary  
 \*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall12	100.00	62.68	85.96	10.120
Outfall11	100.00	68.88	80.03	11.121
Outfall14	100.00	255.45	341.05	41.246
Outfall13	60.56	7.00	30.00	0.685
System	90.14	394.01	536.81	63.172

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	13.03	0 00:35			
200	DUMMY	4.33	0 00:35			
201	DUMMY	1.66	0 00:40			
202	CONDUIT	5.95	0 00:36	10.09	0.00	0.04
204	DUMMY	11.85	0 00:40			
205	CONDUIT	21.20	0 00:40	14.13	0.01	0.08
300	DUMMY	9.95	0 00:35			
400	DUMMY	8.12	0 00:35			
401	CONDUIT	8.03	0 00:37	8.38	0.02	0.10
402	DUMMY	22.23	0 00:40			
500	DUMMY	32.34	0 00:35			
601	DUMMY	16.46	0 00:40			
602	CONDUIT	16.42	0 00:41	6.99	0.07	0.18
603	DUMMY	9.70	0 00:35			

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604	DUMMY	3.65	0	00:35			
605	CONDUIT	13.32	0	00:36	11.62	0.01	0.07
606	DUMMY	12.98	0	00:40			
607	CONDUIT	26.04	0	00:36	12.42	0.02	0.09
700	DUMMY	5.57	0	00:35			
701	DUMMY	3.87	0	00:35			
702	DUMMY	3.87	0	00:35			
703	CONDUIT	3.86	0	00:36	4.80	0.01	0.08
801	DUMMY	1.85	0	00:35			
802	DUMMY	5.37	0	00:35			
803	CONDUIT	7.18	0	00:36	6.34	0.01	0.07
804	DUMMY	1.92	0	00:35			
806	DUMMY	8.07	0	00:35			
805	CONDUIT	1.91	0	00:37	4.00	0.01	0.06
301	DUMMY	9.95	0	00:35			
101	DUMMY	13.03	0	00:35			
206	DUMMY	26.96	0	00:40			
501	DUMMY	32.34	0	00:35			
704	DUMMY	189.42	0	00:36			
807	DUMMY	17.11	0	00:36			
608	DUMMY	42.32	0	00:41			
403	DUMMY	30.00	0	00:38			
41	DUMMY	9.95	0	00:35			
42	DUMMY	93.34	0	00:35			
43	DUMMY	231.47	0	00:40			
44	DUMMY	189.42	0	00:36			
45	DUMMY	180.00	0	00:00			
46	DUMMY	67.00	0	00:00			
47	DUMMY	59.00	0	00:00			
48	DUMMY	61.00	0	00:00			

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:32:27 2020  
 Analysis ended on: Mon Sep 21 16:32:27 2020  
 Total elapsed time: < 1 sec



SWMM Model Pre Development 100 Year

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

-----  
SWMM 100 Year Pre Development

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS  
Process Models:  
  Rainfall/Runoff ..... NO  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Flow Routing Method ..... KINWAVE  
Starting Date ..... 01/01/2005 00:00:00  
Ending Date ..... 01/01/2005 06:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:05:00  
Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	82.644	26.931
External Outflow .....	82.609	26.919
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	0.000	0.000
Continuity Error (%) .....	0.043	

SWMM Model Pre Development 100 Year

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

Link 608 (1)

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.04  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.21	0.59	6945.59	0 00:45	0.58
24	JUNCTION	0.36	1.43	6935.43	0 00:45	1.42
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.24	1.05	6912.05	0 00:40	1.05
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.27	1.04	6901.04	0 00:45	1.03
65	JUNCTION	0.43	1.52	6881.52	0 00:45	1.52
66	JUNCTION	0.61	2.08	6870.08	0 00:50	2.08
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0 00:00	0.00
73	JUNCTION	0.27	0.94	6902.94	0 00:45	0.94

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80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.32	1.19	6873.19	0	00:45	1.18
85	JUNCTION	0.15	0.64	6874.64	0	00:40	0.64
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.39	1.43	6912.43	0	00:46	1.42
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.27	0.94	6900.94	0	00:46	0.94
PondH	JUNCTION	0.32	1.18	6867.18	0	00:46	1.18
PondF	JUNCTION	0.61	2.08	6868.08	0	00:51	2.08
PondD	JUNCTION	0.25	1.05	6882.05	0	00:42	1.05
Outfall12	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall11	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall14	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall13	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
31	OUTFALL	0.00	0.00	6953.00	0	00:00	0.00
51	OUTFALL	0.00	0.00	6920.00	0	00:00	0.00
74	OUTFALL	0.00	0.00	6897.00	0	00:00	0.00
67	OUTFALL	0.00	0.00	6865.50	0	00:00	0.00

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Flow		Maximum Lateral	Maximum Total	Time of Max Occurrence	Lateral Inflow Volume
Inflow Volume	Balance Error	Inflow CFS	Inflow CFS	days hr:min	10^6 gal
Node gal	Percent	Type			10^6
10	0.304	JUNCTION	13.03	0 00:35	0.304
20	0.085	JUNCTION	4.33	0 00:35	0.085
21	0.794	JUNCTION	20.74	0 00:50	0.794



		SWMM Model Pre Development 100 Year				
22		JUNCTION	140.35	140.35	0 00:45	3.79
3.79	0.000					
23		JUNCTION	0.00	23.90	0 00:45	0
0.879	0.000					
24		JUNCTION	0.00	140.35	0 00:45	0
3.79	0.000					
30		JUNCTION	110.70	110.70	0 00:40	2.47
2.47	0.000					
40		JUNCTION	40.00	40.00	0 00:40	1.03
1.03	0.000					
41		JUNCTION	114.87	114.87	0 00:45	3.31
3.31	0.000					
42		JUNCTION	0.00	40.00	0 00:40	0
1.03	0.000					
50		JUNCTION	157.99	157.99	0 00:40	3.76
3.76	0.000					
60		JUNCTION	49.45	49.45	0 00:45	1.43
1.43	0.000					
61		JUNCTION	86.73	86.73	0 00:50	2.87
2.87	0.000					
62		JUNCTION	18.42	18.42	0 00:45	0.544
0.544	0.000					
63		JUNCTION	67.82	67.82	0 00:45	2.19
2.19	0.000					
64		JUNCTION	0.00	67.87	0 00:45	0
1.97	0.000					
65		JUNCTION	0.00	135.62	0 00:45	0
4.16	0.000					
66		JUNCTION	0.00	86.73	0 00:50	0
2.87	0.000					
70		JUNCTION	28.46	28.46	0 00:45	0.853
0.853	0.000					
71		JUNCTION	20.06	20.06	0 00:45	0.641
0.641	0.000					
72		JUNCTION	0.00	20.06	0 00:45	0
0.641	0.000					
73		JUNCTION	0.00	20.06	0 00:45	0
0.641	0.000					
80		JUNCTION	21.89	21.89	0 00:45	0.659
0.659	0.000					
81		JUNCTION	27.12	27.12	0 00:45	0.786
0.786	0.000					
82		JUNCTION	9.51	9.51	0 00:40	0.252
0.252	0.000					
83		JUNCTION	40.86	40.86	0 00:45	1.17
1.17	0.000					
84		JUNCTION	0.00	49.01	0 00:45	0
1.44	0.000					

		SWMM Model Pre Development 100 Year					
85		JUNCTION	0.00	9.51	0	00:40	0
0.252	0.000						
PondC		JUNCTION	0.00	110.70	0	00:40	0
2.47	0.000						
PondA		JUNCTION	0.00	13.03	0	00:35	0
0.304	0.000						
PondB		JUNCTION	0.00	164.21	0	00:46	0
4.66	0.000						
PondE		JUNCTION	0.00	157.99	0	00:40	0
3.76	0.000						
PondG		JUNCTION	0.00	48.48	0	00:45	0
1.49	0.000						
PondH		JUNCTION	0.00	99.16	0	00:45	0
2.87	0.000						
PondF		JUNCTION	0.00	221.11	0	00:46	0
7.02	0.000						
PondD		JUNCTION	0.00	154.35	0	00:45	0
4.34	0.000						
Outfall2		OUTFALL	0.00	164.21	0	00:46	0
4.66	0.000						
Outfall1		OUTFALL	0.00	13.03	0	00:35	0
0.304	0.000						
Outfall4		OUTFALL	0.00	99.16	0	00:45	0
2.87	0.000						
Outfall3		OUTFALL	0.00	154.35	0	00:45	0
4.34	0.000						
31		OUTFALL	0.00	110.70	0	00:40	0
2.47	0.000						
51		OUTFALL	0.00	157.99	0	00:40	0
3.76	0.000						
74		OUTFALL	0.00	48.48	0	00:45	0
1.49	0.000						
67		OUTFALL	0.00	221.11	0	00:46	0
7.02	0.000						

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Outfall Node	SWMM Model Pre Development 100 Year			
	Flow Freq Pcmt	Avg Flow CFS	Max Flow CFS	Total Volume 10 <sup>6</sup> gal
Outfall2	76.53	37.73	164.21	4.665
Outfall11	55.28	3.40	13.03	0.304
Outfall4	67.08	26.46	99.16	2.867
Outfall3	67.92	39.52	154.35	4.336
31	53.89	28.39	110.70	2.472
51	58.47	39.76	157.99	3.757
74	67.08	13.78	48.48	1.494
67	74.31	58.49	221.11	7.022
System	65.07	247.53	962.28	26.917

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	13.03	0 00:35			
200	DUMMY	4.33	0 00:35			
201	DUMMY	20.74	0 00:50			
202	CONDUIT	23.89	0 00:46	15.49	0.01	0.08
204	DUMMY	140.35	0 00:45			
205	CONDUIT	140.32	0 00:46	24.86	0.09	0.20
300	DUMMY	110.70	0 00:40			
400	DUMMY	40.00	0 00:40			
401	CONDUIT	39.84	0 00:42	13.30	0.10	0.21
402	DUMMY	114.87	0 00:45			
500	DUMMY	157.99	0 00:40			
601	DUMMY	86.73	0 00:50			
602	CONDUIT	86.65	0 00:51	11.22	0.36	0.42
603	DUMMY	49.45	0 00:45			
604	DUMMY	18.42	0 00:45			
605	CONDUIT	67.80	0 00:45	19.12	0.05	0.15
606	DUMMY	67.82	0 00:45			
607	CONDUIT	135.63	0 00:46	20.33	0.08	0.19
700	DUMMY	28.46	0 00:45			
701	DUMMY	20.06	0 00:45			
702	DUMMY	20.06	0 00:45			
703	CONDUIT	20.04	0 00:46	7.87	0.08	0.19
801	DUMMY	21.89	0 00:45			



SWMM Model Pre Development 100 Year							
802	DUMMY	27.12	0	00:45			
803	CONDUIT	48.96	0	00:46	11.36	0.06	0.17
804	DUMMY	9.51	0	00:40			
806	DUMMY	40.86	0	00:45			
805	CONDUIT	9.46	0	00:42	6.45	0.04	0.13
301	DUMMY	110.70	0	00:40			
101	DUMMY	13.03	0	00:35			
206	DUMMY	164.21	0	00:46			
501	DUMMY	157.99	0	00:40			
704	DUMMY	48.48	0	00:45			
807	DUMMY	99.16	0	00:45			
608	DUMMY	221.11	0	00:46			
403	DUMMY	154.35	0	00:45			

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Fri Apr 10 13:11:18 2020  
 Analysis ended on: Fri Apr 10 13:11:18 2020  
 Total elapsed time: < 1 sec

SWMM 100 Year Output EX 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

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\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... NO  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/01/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	836.701	272.651
External Outflow .....	836.646	272.634
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	0.000	0.000
Continuity Error (%) .....	0.007	

SWMM 100 Year Output EX 9-21-20

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

Link 205 (1)  
 Link 608 (1)  
 Link 206 (1)

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.03  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.28	0.97	6945.97	0 00:45	0.97
24	JUNCTION	0.45	1.91	6935.91	0 00:45	1.91
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.24	1.05	6912.05	0 00:40	1.05
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.27	1.04	6901.04	0 00:45	1.03
65	JUNCTION	0.43	1.52	6881.52	0 00:45	1.52
66	JUNCTION	0.61	2.08	6870.08	0 00:50	2.08
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00



SWMM 100 Year Output EX 9-21-20

72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.27	0.94	6902.94	0	00:45	0.94
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.32	1.19	6873.19	0	00:45	1.18
85	JUNCTION	0.15	0.64	6874.64	0	00:40	0.64
PondC	JUNCTION	0.00	0.00	6956.00	0	00:00	0.00
PondA	JUNCTION	0.00	0.00	6949.00	0	00:00	0.00
PondB	JUNCTION	0.48	1.91	6912.91	0	00:45	1.90
PondE	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
PondG	JUNCTION	0.27	0.94	6900.94	0	00:46	0.94
PondH	JUNCTION	0.32	1.18	6867.18	0	00:46	1.18
PondF	JUNCTION	0.61	2.08	6868.08	0	00:51	2.08
PondD	JUNCTION	0.25	1.05	6882.05	0	00:42	1.05
31	JUNCTION	0.00	0.00	6953.00	0	00:00	0.00
51	JUNCTION	0.00	0.00	6920.00	0	00:00	0.00
67	JUNCTION	0.00	0.00	6865.50	0	00:00	0.00
74	JUNCTION	0.00	0.00	6897.00	0	00:00	0.00
OS1	JUNCTION	0.00	0.00	6950.00	0	00:00	0.00
OS2	JUNCTION	0.00	0.00	6924.00	0	00:00	0.00
OS3	JUNCTION	0.00	0.00	6930.00	0	00:00	0.00
OS4	JUNCTION	0.00	0.00	6905.00	0	00:00	0.00
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.00	0.00	6865.00	0	00:00	0.00
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

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Total	Flow		Maximum	Maximum		Lateral	
Inflow	Balance		Lateral	Total	Time of Max	Inflow	
Volume	Error		Inflow	Inflow	Occurrence	Volume	
Node	Percent	Type	CFS	CFS	days hr:min	10^6 gal	10^6
gal							

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SWMM 100 Year Output EX 9-21-20

10		JUNCTION	66.80	66.80	0	00:45	1.92
1.92	0.000						
20		JUNCTION	48.76	48.76	0	00:40	1.18
1.18	0.000						
21		JUNCTION	20.74	20.74	0	00:50	0.794
0.794	0.000						
22		JUNCTION	140.35	140.35	0	00:45	3.79
3.79	0.000						
23		JUNCTION	0.00	68.56	0	00:45	0
1.97	0.000						
24		JUNCTION	0.00	249.20	0	00:45	0
6.26	0.000						
30		JUNCTION	110.70	110.70	0	00:40	2.47
2.47	0.000						
40		JUNCTION	40.00	40.00	0	00:40	1.03
1.03	0.000						
41		JUNCTION	114.87	114.87	0	00:45	3.31
3.31	0.000						
42		JUNCTION	0.00	40.00	0	00:40	0
1.03	0.000						
50		JUNCTION	157.99	157.99	0	00:40	3.76
3.76	0.000						
60		JUNCTION	49.45	49.45	0	00:45	1.43
1.43	0.000						
61		JUNCTION	86.73	86.73	0	00:50	2.87
2.87	0.000						
62		JUNCTION	18.42	18.42	0	00:45	0.544
0.544	0.000						
63		JUNCTION	67.82	67.82	0	00:45	2.19
2.19	0.000						
64		JUNCTION	0.00	67.87	0	00:45	0
1.97	0.000						
65		JUNCTION	0.00	135.62	0	00:45	0
4.16	0.000						
66		JUNCTION	0.00	86.73	0	00:50	0
2.87	0.000						
70		JUNCTION	28.46	28.46	0	00:45	0.853
0.853	0.000						
71		JUNCTION	20.06	20.06	0	00:45	0.641
0.641	0.000						
72		JUNCTION	0.00	20.06	0	00:45	0
0.641	0.000						
73		JUNCTION	0.00	20.06	0	00:45	0
0.641	0.000						
80		JUNCTION	21.89	21.89	0	00:45	0.659
0.659	0.000						
81		JUNCTION	27.12	27.12	0	00:45	0.786
0.786	0.000						

SWMM 100 Year Output EX 9-21-20

82		JUNCTION	9.51	9.51	0	00:40	0.252
0.252	0.000						
83		JUNCTION	40.86	40.86	0	00:45	1.17
1.17	0.000						
84		JUNCTION	0.00	49.01	0	00:45	0
1.44	0.000						
85		JUNCTION	0.00	9.51	0	00:40	0
0.252	0.000						
PondC		JUNCTION	0.00	110.70	0	00:40	0
2.47	0.000						
PondA		JUNCTION	0.00	66.80	0	00:45	0
1.92	0.000						
PondB		JUNCTION	0.00	317.41	0	00:45	0
8.22	0.000						
PondE		JUNCTION	0.00	157.99	0	00:40	0
3.76	0.000						
PondG		JUNCTION	0.00	643.48	0	00:45	0
97.6	0.000						
PondH		JUNCTION	0.00	99.16	0	00:45	0
2.87	0.000						
PondF		JUNCTION	0.00	221.11	0	00:46	0
7.02	0.000						
PondD		JUNCTION	0.00	154.35	0	00:45	0
4.34	0.000						
31		JUNCTION	0.00	110.70	0	00:40	0
2.47	0.000						
51		JUNCTION	0.00	374.99	0	00:40	0
38.8	0.000						
67		JUNCTION	0.00	864.52	0	00:46	0
105	0.000						
74		JUNCTION	0.00	643.48	0	00:45	0
97.6	0.000						
OS1		JUNCTION	413.00	413.00	0	00:00	66.7
66.7	0.000						
OS2		JUNCTION	280.00	280.00	0	00:00	45.2
45.2	0.000						
OS3		JUNCTION	217.00	217.00	0	00:00	35.1
35	0.000						
OS4		JUNCTION	595.00	595.00	0	00:00	96.1
96.1	0.000						
Outfall2		OUTFALL	0.00	597.41	0	00:45	0
53.4	0.000						
Outfall1		OUTFALL	0.00	479.80	0	00:45	0
68.6	0.000						
Outfall4		OUTFALL	0.00	1335.77	0	00:45	0
146	0.000						
Outfall3		OUTFALL	0.00	154.35	0	00:45	0
4.34	0.000						



SWMM 100 Year Output EX 9-21-20

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10 <sup>6</sup> gal
Outfall2	100.00	330.89	597.41	53.430
Outfall1	100.00	424.90	479.80	68.605
Outfall4	100.00	905.71	1335.77	146.242
Outfall3	67.92	39.52	154.35	4.336
System	91.98	1701.02	2567.34	272.613

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	66.80	0 00:45			
200	DUMMY	48.76	0 00:40			
201	DUMMY	20.74	0 00:50			
202	CONDUIT	68.51	0 00:45	21.36	0.04	0.14
204	DUMMY	140.35	0 00:45			
205	CONDUIT	248.90	0 00:45	29.30	0.16	0.27
300	DUMMY	110.70	0 00:40			
400	DUMMY	40.00	0 00:40			
401	CONDUIT	39.84	0 00:42	13.30	0.10	0.21
402	DUMMY	114.87	0 00:45			
500	DUMMY	157.99	0 00:40			
601	DUMMY	86.73	0 00:50			
602	CONDUIT	86.65	0 00:51	11.22	0.36	0.42

SWMM 100 Year Output EX 9-21-20

603	DUMMY	49.45	0	00:45			
604	DUMMY	18.42	0	00:45			
605	CONDUIT	67.80	0	00:45	19.12	0.05	0.15
606	DUMMY	67.82	0	00:45			
607	CONDUIT	135.63	0	00:46	20.33	0.08	0.19
700	DUMMY	28.46	0	00:45			
701	DUMMY	20.06	0	00:45			
702	DUMMY	20.06	0	00:45			
703	CONDUIT	20.04	0	00:46	7.87	0.08	0.19
801	DUMMY	21.89	0	00:45			
802	DUMMY	27.12	0	00:45			
803	CONDUIT	48.96	0	00:46	11.36	0.06	0.17
804	DUMMY	9.51	0	00:40			
806	DUMMY	40.86	0	00:45			
805	CONDUIT	9.46	0	00:42	6.45	0.04	0.13
301	DUMMY	110.70	0	00:40			
101	DUMMY	66.80	0	00:45			
206	DUMMY	317.41	0	00:45			
501	DUMMY	157.99	0	00:40			
704	DUMMY	643.48	0	00:45			
807	DUMMY	99.16	0	00:45			
608	DUMMY	221.11	0	00:46			
403	DUMMY	154.35	0	00:45			
41	DUMMY	110.70	0	00:40			
42	DUMMY	374.99	0	00:40			
43	DUMMY	864.52	0	00:46			
44	DUMMY	643.48	0	00:45			
45	DUMMY	595.00	0	00:00			
46	DUMMY	413.00	0	00:00			
47	DUMMY	280.00	0	00:00			
48	DUMMY	217.00	0	00:00			

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:37:19 2020  
 Analysis ended on: Mon Sep 21 16:37:19 2020  
 Total elapsed time: < 1 sec

SWMM 5 Year Output

SWMM 5 Year Post Development

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... NO  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/02/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	39.629	12.914
External Outflow .....	23.957	7.807
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	15.654	5.101
Continuity Error (%) .....	0.045	



SWMM 5 Year Output

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*  
All links are stable.

\*\*\*\*\*  
Routing Time Step Summary  
\*\*\*\*\*  
Minimum Time Step : 30.00 sec  
Average Time Step : 30.00 sec  
Maximum Time Step : 30.00 sec  
Percent in Steady State : 0.00  
Average Iterations per Step : 1.01  
Percent Not Converging : 0.00

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.04	0.75	6945.75	0 00:30	0.74
24	JUNCTION	0.21	1.17	6935.17	0 00:30	1.16
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
31	JUNCTION	0.17	0.20	6953.20	0 02:23	0.20
67	JUNCTION	0.16	0.59	6866.09	0 01:57	0.59
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.03	0.82	6911.82	0 00:30	0.81
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
51	JUNCTION	0.03	0.21	6920.21	0 01:12	0.21
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.03	0.66	6900.66	0 00:35	0.66
65	JUNCTION	0.05	1.10	6881.10	0 00:35	1.10
66	JUNCTION	0.08	1.71	6869.71	0 00:35	1.71

SWMM 5 Year Output

70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.03	0.55	6902.55	0	00:35	0.54
74	JUNCTION	0.02	0.24	6897.24	0	01:15	0.24
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.04	0.80	6872.80	0	00:30	0.79
85	JUNCTION	0.02	0.48	6874.48	0	00:30	0.47
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.16	0.59	6865.59	0	01:57	0.59
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	5.89	6.37	6917.37	0	01:30	6.37
PondC	STORAGE	4.70	5.56	6961.56	0	02:23	5.56
PondA	STORAGE	4.01	4.67	6953.67	0	01:46	4.67
PondD	STORAGE	5.54	6.51	6887.51	0	02:25	6.51
PondE	STORAGE	4.04	4.77	6927.77	0	01:12	4.77
PondF	STORAGE	5.76	6.73	6872.73	0	02:02	6.73
PondG	STORAGE	0.11	1.20	6901.20	0	01:15	1.20
PondH	STORAGE	4.49	5.12	6871.12	0	02:09	5.12

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Inflow Volume gal	Flow Balance Error Percent	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal
10 0.705	0.000	JUNCTION	30.72	30.72	0 00:35	0.705
20 0.578	0.000	JUNCTION	29.46	29.46	0 00:30	0.578
21		JUNCTION	12.02	12.02	0 00:35	0.376

SWMM 5 Year Output

0.376	0.000						
22		JUNCTION	92.76	92.76	0	00:30	2.04
2.04	0.000						
23		JUNCTION	0.00	40.92	0	00:30	0
0.954	0.000						
24		JUNCTION	0.00	93.26	0	00:30	0
2.96	0.000						
30		JUNCTION	77.99	77.99	0	00:30	1.38
1.38	0.000						
31		JUNCTION	0.00	1.52	0	02:23	0
0.925	0.000						
67		JUNCTION	0.00	23.06	0	01:57	0
2.4	-0.000						
40		JUNCTION	24.15	24.15	0	00:30	0.438
0.438	0.000						
41		JUNCTION	98.47	98.47	0	00:30	1.83
1.83	0.000						
42		JUNCTION	0.00	24.15	0	00:30	0
0.438	-0.000						
50		JUNCTION	46.88	46.88	0	00:35	0.982
0.982	0.000						
51		JUNCTION	0.00	18.70	0	01:12	0
0.69	0.000						
60		JUNCTION	16.28	16.28	0	00:35	0.424
0.424	0.000						
61		JUNCTION	60.11	60.11	0	00:35	1.38
1.38	0.000						
62		JUNCTION	11.36	11.36	0	00:30	0.234
0.234	0.000						
63		JUNCTION	42.32	42.32	0	00:30	0.975
0.975	0.000						
64		JUNCTION	0.00	26.88	0	00:35	0
0.659	0.000						
65		JUNCTION	0.00	69.12	0	00:35	0
1.63	0.000						
66		JUNCTION	0.00	60.11	0	00:35	0
1.38	0.000						
70		JUNCTION	13.78	13.78	0	00:30	0.32
0.32	0.000						
71		JUNCTION	6.55	6.55	0	00:35	0.191
0.191	0.000						
72		JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000						
73		JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000						
74		JUNCTION	0.00	9.05	0	01:15	0
0.51	-0.000						
80		JUNCTION	5.68	5.68	0	00:35	0.173



SWMM 5 Year Output

0.173	0.000						
81		JUNCTION	16.24	16.24	0	00:30	0.333
0.333	0.000						
82		JUNCTION	5.21	5.21	0	00:30	0.1
0.1	0.000						
83		JUNCTION	20.93	20.93	0	00:30	0.453
0.453	0.000						
84		JUNCTION	0.00	21.67	0	00:30	0
0.507	0.000						
85		JUNCTION	0.00	5.21	0	00:30	0
0.1	0.000						
Outfall12		OUTFALL	0.00	34.45	0	01:30	0
2.22	0.000						
Outfall11		OUTFALL	0.00	5.43	0	01:46	0
0.441	0.000						
Outfall14		OUTFALL	0.00	35.27	0	01:51	0
3.71	0.000						
Outfall13		OUTFALL	0.00	2.52	0	02:25	0
1.43	0.000						
PondB		STORAGE	0.00	134.27	0	00:31	0
3.91	0.047						
PondC		STORAGE	0.00	77.99	0	00:30	0
1.38	0.005						
PondA		STORAGE	0.00	30.72	0	00:35	0
0.705	0.012						
PondD		STORAGE	0.00	120.96	0	00:30	0
2.27	0.003						
PondE		STORAGE	0.00	46.88	0	00:35	0
0.982	0.118						
PondF		STORAGE	0.00	129.20	0	00:35	0
3.01	0.014						
PondG		STORAGE	0.00	20.07	0	00:35	0
0.51	0.116						
PondH		STORAGE	0.00	47.25	0	00:32	0
1.06	0.001						

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

SWMM 5 Year Output

of Max Occurrence Storage Unit hr:min	Maximum Outflow Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time days
PondB 01:30	34.45	241.825	30	0	0	296.729	37	0
PondC 02:23	1.52	111.256	19	0	0	174.130	30	0
PondA 01:46	5.43	53.736	15	0	0	79.797	22	0
PondD 02:24	2.52	192.634	28	0	0	287.984	41	0
PondE 01:11	18.70	56.473	16	0	0	85.437	24	0
PondF 02:02	16.38	235.289	29	0	0	351.325	44	0
PondG 01:15	9.05	2.647	0	0	0	31.290	6	0
PondH 02:09	4.21	88.617	17	0	0	127.653	25	0

\*\*\*\*\*  
 Outfall Loading Summary  
 \*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall2	99.64	2.76	34.45	2.223
Outfall1	99.67	0.55	5.43	0.441
Outfall4	99.67	4.61	35.27	3.709
Outfall3	99.69	1.78	2.52	1.434
System	99.67	9.70	73.13	7.806

\*\*\*\*\*

SWMM 5 Year Output

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	30.72	0 00:35			
200	DUMMY	29.46	0 00:30			
201	DUMMY	12.02	0 00:35			
202	CONDUIT	40.84	0 00:31	18.27	0.02	0.11
203	CONDUIT	1.52	0 02:24	6.34	0.00	0.05
204	DUMMY	92.76	0 00:30			
205	CONDUIT	93.43	0 00:31	22.09	0.06	0.17
300	DUMMY	77.99	0 00:30			
400	DUMMY	24.15	0 00:30			
401	CONDUIT	23.53	0 00:32	11.46	0.06	0.16
402	DUMMY	98.47	0 00:30			
500	DUMMY	46.88	0 00:35			
601	DUMMY	60.11	0 00:35			
602	CONDUIT	60.09	0 00:35	10.17	0.25	0.34
603	DUMMY	16.28	0 00:35			
604	DUMMY	11.36	0 00:30			
605	CONDUIT	26.88	0 00:35	14.61	0.02	0.09
606	DUMMY	42.32	0 00:30			
607	CONDUIT	69.12	0 00:31	16.65	0.04	0.14
700	DUMMY	13.78	0 00:30			
701	DUMMY	6.55	0 00:35			
702	DUMMY	6.55	0 00:35			
703	CONDUIT	6.54	0 00:36	5.62	0.03	0.11
801	DUMMY	5.68	0 00:35			
802	DUMMY	16.24	0 00:30			
803	CONDUIT	21.49	0 00:32	8.87	0.03	0.11
804	DUMMY	5.21	0 00:30			
806	DUMMY	20.93	0 00:30			
805	CONDUIT	5.08	0 00:32	5.42	0.02	0.09
808	CONDUIT	23.06	0 01:57	2.25	0.00	0.06
800	CONDUIT	8.95	0 01:25	2.34	0.00	0.02
600	CONDUIT	18.26	0 01:17	5.75	0.00	0.03
101	DUMMY	5.43	0 01:46			
206	DUMMY	34.45	0 01:30			
301	DUMMY	1.52	0 02:23			
501	DUMMY	18.70	0 01:12			
704	DUMMY	9.05	0 01:15			
807	DUMMY	4.21	0 02:09			
608	DUMMY	16.38	0 02:02			
403	DUMMY	2.52	0 02:25			



SWMM 5 Year Output

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Apr 13 19:10:46 2020  
Analysis ended on: Mon Apr 13 19:10:46 2020  
Total elapsed time: < 1 sec

SWMM 5 Year Output 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... NO  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/02/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	949.387	309.372
External Outflow .....	930.375	303.177
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	20.095	6.548
Continuity Error (%) .....	-0.114	

SWMM 5 Year Output 9-21-20

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.04	0.75	6945.75	0 00:30	0.74
24	JUNCTION	0.21	1.17	6935.17	0 00:30	1.16
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
31	JUNCTION	0.17	0.20	6953.20	0 02:23	0.20
67	JUNCTION	1.87	1.97	6867.47	0 01:59	1.97
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.03	0.82	6911.82	0 00:30	0.81
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
51	JUNCTION	0.71	0.71	6920.71	0 00:32	0.71
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.03	0.66	6900.66	0 00:35	0.66
65	JUNCTION	0.05	1.10	6881.10	0 00:35	1.10
66	JUNCTION	0.08	1.71	6869.71	0 00:35	1.71
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00

SWMM 5 Year Output 9-21-20

71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.03	0.55	6902.55	0	00:35	0.54
74	JUNCTION	1.36	1.40	6898.40	0	01:15	1.40
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.04	0.80	6872.80	0	00:30	0.79
85	JUNCTION	0.02	0.48	6874.48	0	00:30	0.47
OS1	JUNCTION	0.45	0.45	6953.05	0	00:00	0.45
OS3	JUNCTION	0.71	0.71	6923.51	0	00:00	0.71
OS4	JUNCTION	1.21	1.21	6901.01	0	00:00	1.21
OS2	JUNCTION	0.42	0.42	6924.42	0	00:00	0.42
Outfall12	OUTFALL	0.42	0.42	6910.42	0	03:03	0.42
Outfall11	OUTFALL	0.45	0.45	6947.45	0	01:12	0.45
Outfall14	OUTFALL	1.87	1.97	6866.97	0	01:59	1.97
Outfall13	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.42	6.96	6917.96	0	02:52	6.96
PondC	STORAGE	4.70	5.56	6961.56	0	02:23	5.56
PondA	STORAGE	5.16	6.43	6955.43	0	02:35	6.43
PondD	STORAGE	5.57	6.66	6887.66	0	02:07	6.65
PondE	STORAGE	3.99	4.85	6927.85	0	01:03	4.85
PondF	STORAGE	5.76	6.72	6872.72	0	02:04	6.72
PondG	STORAGE	0.11	1.20	6901.20	0	01:15	1.20
PondH	STORAGE	4.38	5.01	6871.01	0	02:39	5.01

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Inflow Volume		Flow Balance Error	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence	Lateral Inflow Volume
gal	Percent			CFS	CFS	days hr:min	10^6 gal
10	0.705	0.000	JUNCTION	30.72	30.72	0 00:35	0.705



SWMM 5 Year Output 9-21-20

20		JUNCTION	29.46	29.46	0	00:30	0.578
0.578	0.000						
21		JUNCTION	12.02	12.02	0	00:35	0.376
0.376	0.000						
22		JUNCTION	92.76	92.76	0	00:30	2.04
2.04	0.000						
23		JUNCTION	0.00	40.92	0	00:30	0
0.954	0.000						
24		JUNCTION	0.00	93.26	0	00:30	0
2.96	0.000						
30		JUNCTION	77.99	77.99	0	00:30	1.38
1.38	0.000						
31		JUNCTION	0.00	1.52	0	02:23	0
0.925	0.000						
67		JUNCTION	0.00	201.42	0	01:59	0
147	0.000						
40		JUNCTION	24.15	24.15	0	00:30	0.438
0.438	0.000						
41		JUNCTION	98.47	98.47	0	00:30	1.83
1.83	0.000						
42		JUNCTION	0.00	24.15	0	00:30	0
0.438	-0.000						
50		JUNCTION	46.88	46.88	0	00:35	0.982
0.982	0.000						
51		JUNCTION	0.00	85.04	0	01:03	0
50	0.000						
60		JUNCTION	16.28	16.28	0	00:35	0.424
0.424	0.000						
61		JUNCTION	60.11	60.11	0	00:35	1.38
1.38	0.000						
62		JUNCTION	11.36	11.36	0	00:30	0.234
0.234	0.000						
63		JUNCTION	42.32	42.32	0	00:30	0.975
0.975	0.000						
64		JUNCTION	0.00	26.88	0	00:35	0
0.659	0.000						
65		JUNCTION	0.00	69.12	0	00:35	0
1.63	0.000						
66		JUNCTION	0.00	60.11	0	00:35	0
1.38	0.000						
70		JUNCTION	13.78	13.78	0	00:30	0.32
0.32	0.000						
71		JUNCTION	6.55	6.55	0	00:35	0.191
0.191	0.000						
72		JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000						
73		JUNCTION	0.00	6.55	0	00:35	0
0.191	0.000						

SWMM 5 Year Output 9-21-20

74		JUNCTION	0.00	189.05	0	01:15	0
146	0.000						
80		JUNCTION	5.68	5.68	0	00:35	0.173
0.173	0.000						
81		JUNCTION	16.24	16.24	0	00:30	0.333
0.333	0.000						
82		JUNCTION	5.21	5.21	0	00:30	0.1
0.1	0.000						
83		JUNCTION	20.93	20.93	0	00:30	0.453
0.453	0.000						
84		JUNCTION	0.00	21.67	0	00:30	0
0.507	0.000						
85		JUNCTION	0.00	5.21	0	00:30	0
0.1	0.000						
OS1		JUNCTION	67.00	67.00	0	00:00	54.1
54.1	0.000						
OS3		JUNCTION	61.00	61.00	0	00:00	49.3
49.3	0.000						
OS4		JUNCTION	180.00	180.00	0	00:00	145
145	0.000						
OS2		JUNCTION	59.00	59.00	0	00:00	47.7
47.7	0.000						
Outfall12		OUTFALL	0.00	61.68	0	02:52	0
49.4	0.000						
Outfall11		OUTFALL	0.00	67.69	0	02:35	0
54.5	0.000						
Outfall14		OUTFALL	0.00	276.10	0	01:07	0
198	0.000						
Outfall13		OUTFALL	0.00	8.58	0	02:07	0
1.45	0.000						
PondB		STORAGE	0.00	134.27	0	00:31	0
3.91	-0.000						
PondC		STORAGE	0.00	77.99	0	00:30	0
1.38	0.005						
PondA		STORAGE	0.00	30.72	0	00:35	0
0.705	0.003						
PondD		STORAGE	0.00	120.96	0	00:30	0
2.27	0.003						
PondE		STORAGE	0.00	46.88	0	00:35	0
0.982	0.190						
PondF		STORAGE	0.00	129.20	0	00:35	0
3.01	0.010						
PondG		STORAGE	0.00	20.07	0	00:35	0
0.51	0.116						
PondH		STORAGE	0.00	47.25	0	00:32	0
1.06	0.003						

SWMM 5 Year Output 9-21-20

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

of Max Occurrence hr:min	Maximum Outflow Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time days
PondB 02:51	2.68	321.956	38	0	0	389.908	46	0
PondC 02:23	1.52	111.256	19	0	0	174.130	30	0
PondA 02:35	0.69	59.417	29	0	0	88.970	44	0
PondD 02:07	8.58	184.527	30	0	0	278.950	45	0
PondE 01:03	24.04	46.471	16	0	0	72.497	25	0
PondF 02:03	15.59	238.240	29	0	0	353.902	43	0
PondG 01:15	9.05	2.647	0	0	0	31.289	6	0
PondH 02:39	1.11	86.593	14	0	0	132.766	21	0

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Flow Freq	Avg Flow	Max Flow	Total Volume
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SWMM 5 Year Output 9-21-20

Outfall Node	Pcnt	CFS	CFS	10^6 gal
Outfall2	99.97	61.16	61.68	49.385
Outfall1	99.97	67.44	67.69	54.456
Outfall4	99.89	245.24	276.10	197.866
Outfall3	99.69	1.80	8.58	1.447
System	99.88	375.63	407.24	303.154

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	30.72	0 00:35			
200	DUMMY	29.46	0 00:30			
201	DUMMY	12.02	0 00:35			
202	CONDUIT	40.84	0 00:31	18.27	0.02	0.11
203	CONDUIT	1.52	0 02:24	6.34	0.00	0.05
204	DUMMY	92.76	0 00:30			
205	CONDUIT	93.43	0 00:31	22.09	0.06	0.17
300	DUMMY	77.99	0 00:30			
400	DUMMY	24.15	0 00:30			
401	CONDUIT	23.53	0 00:32	11.46	0.06	0.16
402	DUMMY	98.47	0 00:30			
500	DUMMY	46.88	0 00:35			
601	DUMMY	60.11	0 00:35			
602	CONDUIT	60.09	0 00:35	10.17	0.25	0.34
603	DUMMY	16.28	0 00:35			
604	DUMMY	11.36	0 00:30			
605	CONDUIT	26.88	0 00:35	14.61	0.02	0.09
606	DUMMY	42.32	0 00:30			
607	CONDUIT	69.12	0 00:31	16.65	0.04	0.14
700	DUMMY	13.78	0 00:30			
701	DUMMY	6.55	0 00:35			
702	DUMMY	6.55	0 00:35			
703	CONDUIT	6.54	0 00:36	5.62	0.03	0.11
801	DUMMY	5.68	0 00:35			
802	DUMMY	16.24	0 00:30			
803	CONDUIT	21.49	0 00:32	8.87	0.03	0.11
804	DUMMY	5.21	0 00:30			
806	DUMMY	20.93	0 00:30			
805	CONDUIT	5.08	0 00:32	5.42	0.02	0.09



SWMM 5 Year Output 9-21-20								
808	CONDUIT	201.42	0	01:59	4.47	0.03	0.20	
800	CONDUIT	189.04	0	01:19	6.57	0.02	0.14	
600	CONDUIT	84.88	0	01:06	9.93	0.00	0.06	
EastForkTrib	CONDUIT	61.00	0	00:32	3.08	0.01	0.07	
EastFork	CONDUIT	180.00	0	00:24	4.29	0.03	0.15	
MainStem	CONDUIT	67.00	0	01:15	2.39	0.00	0.05	
MainStemTrib	CONDUIT	59.00	0	03:06	2.28	0.00	0.04	
101	DUMMY	0.69	0	02:35				
206	DUMMY	2.68	0	02:52				
301	DUMMY	1.52	0	02:23				
501	DUMMY	24.04	0	01:03				
704	DUMMY	9.05	0	01:15				
807	DUMMY	1.11	0	02:39				
608	DUMMY	15.59	0	02:04				
403	DUMMY	8.58	0	02:07				

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:22:13 2020  
 Analysis ended on: Mon Sep 21 16:22:14 2020  
 Total elapsed time: 00:00:01

SWMM 100 Year Output

SWMM 100 Year Post Development

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

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\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... NO  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/02/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	123.320	40.186
External Outflow .....	105.086	34.244
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	18.084	5.893
Continuity Error (%) .....	0.122	

SWMM 100 Year Output

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*  
 All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*  
 Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.02  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.06	1.35	6946.35	0 00:35	1.34
24	JUNCTION	0.27	2.22	6936.22	0 00:51	2.22
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
31	JUNCTION	0.24	1.68	6954.68	0 00:59	1.68
67	JUNCTION	0.24	2.30	6867.80	0 01:13	2.30
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.05	1.40	6912.40	0 00:35	1.38
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
51	JUNCTION	0.04	0.74	6920.74	0 00:49	0.74
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.06	1.19	6901.19	0 00:40	1.19
65	JUNCTION	0.09	1.92	6881.92	0 00:40	1.92

SWMM 100 Year Output

66	JUNCTION	0.13	3.12	6871.12	0	00:40	3.12
70	JUNCTION	0.00	0.00	6923.00	0	00:00	0.00
71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.06	1.02	6903.02	0	00:45	1.02
74	JUNCTION	0.05	0.60	6897.60	0	01:12	0.60
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.07	1.45	6873.45	0	00:40	1.45
85	JUNCTION	0.03	0.82	6874.82	0	00:35	0.81
Outfall2	OUTFALL	0.00	0.00	6910.00	0	00:00	0.00
Outfall1	OUTFALL	0.00	0.00	6947.00	0	00:00	0.00
Outfall4	OUTFALL	0.24	2.30	6867.30	0	01:13	2.30
Outfall3	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.72	9.85	6920.85	0	01:16	9.85
PondC	STORAGE	5.17	7.08	6963.08	0	00:59	7.08
PondA	STORAGE	5.81	8.60	6957.60	0	01:13	8.59
PondD	STORAGE	5.66	8.08	6889.08	0	01:04	8.08
PondE	STORAGE	4.04	5.84	6928.84	0	00:49	5.84
PondF	STORAGE	5.86	8.17	6874.17	0	01:09	8.17
PondG	STORAGE	0.20	2.69	6902.69	0	01:12	2.68
PondH	STORAGE	4.95	6.51	6872.51	0	01:12	6.51

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Inflow Volume		Flow Balance Error	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence	Lateral Inflow Volume
gal	Percent			CFS	CFS	days hr:min	10^6 gal
10			JUNCTION	100.64	100.64	0 00:40	2.37
2.37	0.000						
20			JUNCTION	97.08	97.08	0 00:35	1.81
1.81	0.000						



SWMM 100 Year Output

21		JUNCTION	42.26	42.26	0	00:40	1.2
1.2	0.000						
22		JUNCTION	295.27	295.27	0	00:40	6.04
6.04	0.000						
23		JUNCTION	0.00	136.17	0	00:35	0
3.01	0.000						
24		JUNCTION	0.00	334.84	0	00:51	0
9.43	-0.000						
30		JUNCTION	238.03	238.03	0	00:35	4
4	0.000						
31		JUNCTION	0.00	115.75	0	00:59	0
3.39	0.000						
67		JUNCTION	0.00	270.41	0	01:13	0
9.72	-0.000						
40		JUNCTION	70.07	70.07	0	00:35	1.32
1.32	0.000						
41		JUNCTION	252.18	252.18	0	00:35	4.73
4.73	0.000						
42		JUNCTION	0.00	70.07	0	00:35	0
1.32	0.000						
50		JUNCTION	178.04	178.04	0	00:40	4.2
4.2	0.000						
51		JUNCTION	0.00	164.75	0	00:49	0
3.95	0.000						
60		JUNCTION	58.95	58.95	0	00:40	1.65
1.65	0.000						
61		JUNCTION	170.90	170.90	0	00:40	3.87
3.87	0.000						
62		JUNCTION	32.93	32.93	0	00:35	0.699
0.699	0.000						
63		JUNCTION	124.89	124.89	0	00:40	2.87
2.87	0.000						
64		JUNCTION	0.00	90.88	0	00:40	0
2.35	0.000						
65		JUNCTION	0.00	215.63	0	00:40	0
5.22	0.000						
66		JUNCTION	0.00	170.90	0	00:40	0
3.87	0.000						
70		JUNCTION	43.95	43.95	0	00:40	1.05
1.05	0.000						
71		JUNCTION	23.95	23.95	0	00:45	0.742
0.742	0.000						
72		JUNCTION	0.00	23.95	0	00:45	0
0.742	0.000						
73		JUNCTION	0.00	23.95	0	00:45	0
0.742	0.000						
74		JUNCTION	0.00	42.13	0	01:12	0
1.79	-0.000						

SWMM 100 Year Output

80		JUNCTION	27.62	27.62	0	00:45	0.833
0.833	0.000						
81		JUNCTION	47.62	47.62	0	00:35	1.01
1.01	0.000						
82		JUNCTION	15.60	15.60	0	00:35	0.314
0.314	0.000						
83		JUNCTION	64.71	64.71	0	00:35	1.46
1.46	0.000						
84		JUNCTION	0.00	73.73	0	00:40	0
1.84	0.000						
85		JUNCTION	0.00	15.60	0	00:35	0
0.314	0.000						
Outfall12		OUTFALL	0.00	256.11	0	01:16	0
10.3	0.000						
Outfall11		OUTFALL	0.00	53.95	0	01:13	0
2.03	0.000						
Outfall14		OUTFALL	0.00	478.86	0	01:05	0
16.7	0.000						
Outfall13		OUTFALL	0.00	160.70	0	01:04	0
5.21	0.000						
PondB		STORAGE	0.00	447.00	0	00:49	0
12.4	0.062						
PondC		STORAGE	0.00	238.03	0	00:35	0
4	0.130						
PondA		STORAGE	0.00	100.64	0	00:40	0
2.37	0.096						
PondD		STORAGE	0.00	320.21	0	00:35	0
6.05	0.105						
PondE		STORAGE	0.00	178.04	0	00:40	0
4.2	0.178						
PondF		STORAGE	0.00	385.87	0	00:41	0
9.08	0.109						
PondG		STORAGE	0.00	67.73	0	00:40	0
1.8	0.079						
PondH		STORAGE	0.00	153.03	0	00:38	0
3.61	0.143						

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

SWMM 100 Year Output

of Max Occurrence Storage Unit hr:min	Maximum Outflow Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time days
PondB 01:15	256.11	363.135	43	0	0	827.701	97	0
PondC 00:58	115.75	146.763	26	0	0	299.338	52	0
PondA 01:12	53.95	75.030	37	0	0	152.554	76	0
PondD 01:04	160.70	192.591	31	0	0	418.291	67	0
PondE 00:48	164.75	48.028	17	0	0	106.230	37	0
PondF 01:09	229.20	250.108	31	0	0	549.589	67	0
PondG 01:11	42.13	5.811	1	0	0	88.594	16	0
PondH 01:12	80.17	131.315	21	0	0	268.983	42	0

\*\*\*\*\*  
 Outfall Loading Summary  
 \*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall2	99.64	12.77	256.11	10.280
Outfall1	99.69	2.53	53.95	2.035
Outfall4	99.67	20.76	478.86	16.717
Outfall3	99.69	6.47	160.70	5.209
System	99.67	42.53	924.48	34.241

SWMM 100 Year Output

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	100.64	0 00:40			
200	DUMMY	97.08	0 00:35			
201	DUMMY	42.26	0 00:40			
202	CONDUIT	136.36	0 00:36	26.17	0.08	0.19
203	CONDUIT	115.74	0 00:59	23.03	0.37	0.42
204	DUMMY	295.27	0 00:40			
205	CONDUIT	334.86	0 00:51	31.89	0.22	0.32
300	DUMMY	238.03	0 00:35			
400	DUMMY	70.07	0 00:35			
401	CONDUIT	69.37	0 00:36	15.63	0.17	0.28
402	DUMMY	252.18	0 00:35			
500	DUMMY	178.04	0 00:40			
601	DUMMY	170.90	0 00:40			
602	CONDUIT	170.58	0 00:41	13.26	0.71	0.62
603	DUMMY	58.95	0 00:40			
604	DUMMY	32.93	0 00:35			
605	CONDUIT	90.74	0 00:41	20.83	0.06	0.17
606	DUMMY	124.89	0 00:40			
607	CONDUIT	215.42	0 00:40	23.26	0.13	0.24
700	DUMMY	43.95	0 00:40			
701	DUMMY	23.95	0 00:45			
702	DUMMY	23.95	0 00:45			
703	CONDUIT	23.94	0 00:45	8.29	0.09	0.20
801	DUMMY	27.62	0 00:45			
802	DUMMY	47.62	0 00:35			
803	CONDUIT	73.66	0 00:40	12.80	0.09	0.21
804	DUMMY	15.60	0 00:35			
806	DUMMY	64.71	0 00:35			
805	CONDUIT	15.43	0 00:37	7.47	0.06	0.16
808	CONDUIT	270.40	0 01:13	4.87	0.04	0.23
800	CONDUIT	41.98	0 01:17	4.06	0.00	0.06
600	CONDUIT	164.38	0 00:51	12.48	0.01	0.09
101	DUMMY	53.95	0 01:13			
206	DUMMY	256.11	0 01:16			
301	DUMMY	115.75	0 00:59			
501	DUMMY	164.75	0 00:49			
704	DUMMY	42.13	0 01:12			
807	DUMMY	80.17	0 01:12			
608	DUMMY	229.20	0 01:09			





SWMM 100 Year Output 9-21-20

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... NO  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/02/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	3854.070	1255.906
External Outflow .....	3828.229	1247.485
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	28.186	9.185
Continuity Error (%) .....	-0.061	

SWMM 100 Year Output 9-21-20

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.02  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
10	JUNCTION	0.00	0.00	6975.00	0 00:00	0.00
20	JUNCTION	0.00	0.00	6982.00	0 00:00	0.00
21	JUNCTION	0.00	0.00	6953.00	0 00:00	0.00
22	JUNCTION	0.00	0.00	6936.00	0 00:00	0.00
23	JUNCTION	0.06	1.35	6946.35	0 00:35	1.34
24	JUNCTION	0.27	2.22	6936.22	0 00:51	2.22
30	JUNCTION	0.00	0.00	6985.00	0 00:00	0.00
31	JUNCTION	0.24	1.68	6954.68	0 00:59	1.68
67	JUNCTION	3.45	4.11	6869.61	0 01:12	4.11
40	JUNCTION	0.00	0.00	6918.00	0 00:00	0.00
41	JUNCTION	0.00	0.00	6888.00	0 00:00	0.00
42	JUNCTION	0.05	1.40	6912.40	0 00:35	1.38
50	JUNCTION	0.00	0.00	6945.00	0 00:00	0.00
51	JUNCTION	1.48	1.48	6921.48	0 00:21	1.48
60	JUNCTION	0.00	0.00	6942.00	0 00:00	0.00
61	JUNCTION	0.00	0.00	6893.00	0 00:00	0.00
62	JUNCTION	0.00	0.00	6908.00	0 00:00	0.00
63	JUNCTION	0.00	0.00	6882.00	0 00:00	0.00
64	JUNCTION	0.06	1.19	6901.19	0 00:40	1.19
65	JUNCTION	0.09	1.92	6881.92	0 00:40	1.92
66	JUNCTION	0.13	3.12	6871.12	0 00:40	3.12
70	JUNCTION	0.00	0.00	6923.00	0 00:00	0.00

SWMM 100 Year Output 9-21-20

71	JUNCTION	0.00	0.00	6908.00	0	00:00	0.00
72	JUNCTION	0.00	0.00	6904.00	0	00:00	0.00
73	JUNCTION	0.06	1.02	6903.02	0	00:45	1.02
74	JUNCTION	2.57	2.66	6899.66	0	01:12	2.66
80	JUNCTION	0.00	0.00	6890.00	0	00:00	0.00
81	JUNCTION	0.00	0.00	6896.00	0	00:00	0.00
82	JUNCTION	0.00	0.00	6886.00	0	00:00	0.00
83	JUNCTION	0.00	0.00	6878.00	0	00:00	0.00
84	JUNCTION	0.07	1.45	6873.45	0	00:40	1.45
85	JUNCTION	0.03	0.82	6874.82	0	00:35	0.81
OS1	JUNCTION	1.33	1.33	6953.93	0	00:00	1.33
OS3	JUNCTION	1.48	1.48	6924.28	0	00:00	1.48
OS4	JUNCTION	2.38	2.38	6902.18	0	00:00	2.38
OS2	JUNCTION	1.06	1.06	6925.06	0	00:00	1.06
Outfall12	OUTFALL	1.06	1.06	6911.06	0	01:47	1.06
Outfall11	OUTFALL	1.33	1.33	6948.33	0	00:39	1.33
Outfall14	OUTFALL	3.45	4.11	6869.11	0	01:12	4.11
Outfall13	OUTFALL	0.00	0.00	6880.00	0	00:00	0.00
PondB	STORAGE	6.72	9.85	6920.85	0	01:16	9.85
PondC	STORAGE	5.17	7.08	6963.08	0	00:59	7.08
PondA	STORAGE	5.81	8.60	6957.60	0	01:13	8.59
PondD	STORAGE	5.66	8.08	6889.08	0	01:04	8.08
PondE	STORAGE	4.04	5.84	6928.84	0	00:49	5.84
PondF	STORAGE	5.86	8.17	6874.17	0	01:09	8.17
PondG	STORAGE	0.20	2.69	6902.69	0	01:12	2.68
PondH	STORAGE	4.95	6.51	6872.51	0	01:12	6.51

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Total Flow		Maximum Lateral Inflow	Maximum Total Inflow	Time of Max Occurrence	Lateral Inflow Volume
Node	Balance Error Percent	Type	CFS	days hr:min	10^6 gal
10	2.37 0.000	JUNCTION	100.64	0 00:40	2.37



SWMM 100 Year Output 9-21-20

20		JUNCTION	97.08	97.08	0	00:35	1.81
1.81	0.000						
21		JUNCTION	42.26	42.26	0	00:40	1.2
1.2	0.000						
22		JUNCTION	295.27	295.27	0	00:40	6.04
6.04	0.000						
23		JUNCTION	0.00	136.17	0	00:35	0
3.01	0.000						
24		JUNCTION	0.00	334.84	0	00:51	0
9.43	-0.000						
30		JUNCTION	238.03	238.03	0	00:35	4
4	0.000						
31		JUNCTION	0.00	115.75	0	00:59	0
3.39	0.000						
67		JUNCTION	0.00	865.98	0	01:12	0
489	0.000						
40		JUNCTION	70.07	70.07	0	00:35	1.32
1.32	0.000						
41		JUNCTION	252.18	252.18	0	00:35	4.73
4.73	0.000						
42		JUNCTION	0.00	70.07	0	00:35	0
1.32	0.000						
50		JUNCTION	178.04	178.04	0	00:40	4.2
4.2	0.000						
51		JUNCTION	0.00	381.75	0	00:49	0
179	0.000						
60		JUNCTION	58.95	58.95	0	00:40	1.65
1.65	0.000						
61		JUNCTION	170.90	170.90	0	00:40	3.87
3.87	0.000						
62		JUNCTION	32.93	32.93	0	00:35	0.699
0.699	0.000						
63		JUNCTION	124.89	124.89	0	00:40	2.87
2.87	0.000						
64		JUNCTION	0.00	90.88	0	00:40	0
2.35	0.000						
65		JUNCTION	0.00	215.63	0	00:40	0
5.22	0.000						
66		JUNCTION	0.00	170.90	0	00:40	0
3.87	0.000						
70		JUNCTION	43.95	43.95	0	00:40	1.05
1.05	0.000						
71		JUNCTION	23.95	23.95	0	00:45	0.742
0.742	0.000						
72		JUNCTION	0.00	23.95	0	00:45	0
0.742	0.000						
73		JUNCTION	0.00	23.95	0	00:45	0
0.742	0.000						

SWMM 100 Year Output 9-21-20							
74		JUNCTION	0.00	637.13	0	01:12	0
482	0.000						
80		JUNCTION	27.62	27.62	0	00:45	0.833
0.833	0.000						
81		JUNCTION	47.62	47.62	0	00:35	1.01
1.01	0.000						
82		JUNCTION	15.60	15.60	0	00:35	0.314
0.314	0.000						
83		JUNCTION	64.71	64.71	0	00:35	1.46
1.46	0.000						
84		JUNCTION	0.00	73.73	0	00:40	0
1.84	0.000						
85		JUNCTION	0.00	15.60	0	00:35	0
0.314	0.000						
OS1		JUNCTION	413.00	413.00	0	00:00	334
334	0.000						
OS3		JUNCTION	217.00	217.00	0	00:00	175
175	-0.000						
OS4		JUNCTION	595.00	595.00	0	00:00	481
481	0.000						
OS2		JUNCTION	280.00	280.00	0	00:00	226
226	0.000						
Outfall2		OUTFALL	0.00	536.11	0	01:16	0
236	0.000						
Outfall1		OUTFALL	0.00	466.95	0	01:13	0
335	0.000						
Outfall4		OUTFALL	0.00	1291.25	0	01:05	0
671	0.000						
Outfall3		OUTFALL	0.00	160.70	0	01:04	0
5.21	0.000						
PondB		STORAGE	0.00	447.00	0	00:49	0
12.4	0.062						
PondC		STORAGE	0.00	238.03	0	00:35	0
4	0.130						
PondA		STORAGE	0.00	100.64	0	00:40	0
2.37	0.096						
PondD		STORAGE	0.00	320.21	0	00:35	0
6.05	0.105						
PondE		STORAGE	0.00	178.04	0	00:40	0
4.2	0.178						
PondF		STORAGE	0.00	385.87	0	00:41	0
9.08	0.109						
PondG		STORAGE	0.00	67.73	0	00:40	0
1.8	0.079						
PondH		STORAGE	0.00	153.03	0	00:38	0
3.61	0.143						

SWMM 100 Year Output 9-21-20

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

of Max Occurrence		Maximum Outflow Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time days
PondB	01:15	256.11	363.135	43	0	0	827.701	97	0
PondC	00:58	115.75	146.763	26	0	0	299.338	52	0
PondA	01:12	53.95	75.030	37	0	0	152.554	76	0
PondD	01:04	160.70	192.591	31	0	0	418.291	67	0
PondE	00:48	164.75	48.028	17	0	0	106.230	37	0
PondF	01:09	229.20	250.108	31	0	0	549.589	67	0
PondG	01:11	42.13	5.811	1	0	0	88.594	16	0
PondH	01:12	80.17	131.315	21	0	0	268.983	42	0

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Flow Freq	Avg Flow	Max Flow	Total Volume
-----------	----------	----------	--------------

SWMM 100 Year Output 9-21-20

Outfall Node	Pcnt	CFS	CFS	10 <sup>6</sup> gal
Outfall12	99.97	292.00	536.11	235.796
Outfall11	99.97	415.18	466.95	335.258
Outfall14	99.92	831.58	1291.25	671.130
Outfall13	99.69	6.47	160.70	5.209
System	99.89	1545.23	2428.13	1247.393

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
100	DUMMY	100.64	0 00:40			
200	DUMMY	97.08	0 00:35			
201	DUMMY	42.26	0 00:40			
202	CONDUIT	136.36	0 00:36	26.17	0.08	0.19
203	CONDUIT	115.74	0 00:59	23.03	0.37	0.42
204	DUMMY	295.27	0 00:40			
205	CONDUIT	334.86	0 00:51	31.89	0.22	0.32
300	DUMMY	238.03	0 00:35			
400	DUMMY	70.07	0 00:35			
401	CONDUIT	69.37	0 00:36	15.63	0.17	0.28
402	DUMMY	252.18	0 00:35			
500	DUMMY	178.04	0 00:40			
601	DUMMY	170.90	0 00:40			
602	CONDUIT	170.58	0 00:41	13.26	0.71	0.62
603	DUMMY	58.95	0 00:40			
604	DUMMY	32.93	0 00:35			
605	CONDUIT	90.74	0 00:41	20.83	0.06	0.17
606	DUMMY	124.89	0 00:40			
607	CONDUIT	215.42	0 00:40	23.26	0.13	0.24
700	DUMMY	43.95	0 00:40			
701	DUMMY	23.95	0 00:45			
702	DUMMY	23.95	0 00:45			
703	CONDUIT	23.94	0 00:45	8.29	0.09	0.20
801	DUMMY	27.62	0 00:45			
802	DUMMY	47.62	0 00:35			
803	CONDUIT	73.66	0 00:40	12.80	0.09	0.21
804	DUMMY	15.60	0 00:35			
806	DUMMY	64.71	0 00:35			
805	CONDUIT	15.43	0 00:37	7.47	0.06	0.16



SWMM 100 Year Output 9-21-20

808	CONDUIT	865.97	0	01:12	6.70	0.14	0.41
800	CONDUIT	637.10	0	01:15	9.35	0.06	0.27
600	CONDUIT	381.54	0	00:50	16.34	0.02	0.15
EastForkTrib	CONDUIT	217.00	0	00:21	4.75	0.02	0.15
EastFork	CONDUIT	595.00	0	00:16	6.34	0.10	0.30
MainStem	CONDUIT	413.00	0	00:40	4.75	0.03	0.13
MainStemTrib	CONDUIT	280.00	0	01:49	4.12	0.02	0.11
101	DUMMY	53.95	0	01:13			
206	DUMMY	256.11	0	01:16			
301	DUMMY	115.75	0	00:59			
501	DUMMY	164.75	0	00:49			
704	DUMMY	42.13	0	01:12			
807	DUMMY	80.17	0	01:12			
608	DUMMY	229.20	0	01:09			
403	DUMMY	160.70	0	01:04			

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Mon Sep 21 16:06:21 2020  
Analysis ended on: Mon Sep 21 16:06:21 2020  
Total elapsed time: < 1 sec



## Appendix D

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond A

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB) ▼

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	10	10
Orifice Spacing =	4.0	4.0
WQCV Ao =	0.61	0.61
Max Stage wqcv =	3.40	3.40
EURV Ao =	2.06	2.06
Max Stage EURV =	4.50	4.50
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	370.3	370.3
W <sub>PCM</sub> =	113.6	113.6
Stage at Top of Bench =	4.60	4.60
L <sub>Bench</sub> =	371.1	371.1
W <sub>Bench</sub> =	114.4	114.4
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
	13.03				57.08	

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		0.32				0.84	
0:10		2.12				2.93	
0:15		6.24				8.14	
0:20		19.45				26.66	
0:25		29.43				70.19	
0:30		30.68				95.65	
0:35		28.10				100.37	
0:40		24.84				96.25	
0:45		22.05				89.32	
0:50		19.61				81.43	
0:55		17.40				74.41	
1:00		15.33				68.04	
1:05		13.43				58.60	
1:10		11.93				49.54	
1:15		10.74				42.06	
1:20		9.68				35.93	
1:25		8.69				30.71	
1:30		7.74				26.07	
1:35		6.89				21.81	
1:40		6.13				17.82	
1:45		5.44				14.14	
1:50		4.81				10.94	
1:55		4.24				8.55	
2:00		3.72				6.51	
2:05		3.24				4.89	
2:10		2.80				3.64	
2:15		2.39				2.70	
2:20		2.00				1.98	
2:25		1.69				1.45	
2:30		1.41				1.07	
2:35		1.16				0.82	
2:40		0.94				0.64	
2:45		0.74				0.50	
2:50		0.57				0.39	
2:55		0.42				0.29	
3:00		0.30				0.20	
3:05		0.21				0.13	
3:10		0.15				0.07	
3:15		0.10				0.03	
3:20		0.07				0.01	
3:25		0.05				0.00	
3:30							
3:35							
3:40							
3:45							
3:50							
3:55							
4:00							
4:05							
4:10							
4:15							
4:20							
4:25							
4:30							
4:35							
4:40							
4:45							
4:50							
4:55							
5:00							
5:05							
5:10							
5:15							
5:20							
5:25							
5:30							
5:35							

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5.40								
5.45								
5.50								
5.55								
6.00								





Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond A

Date: April 6, 2020

Last Edited: April 13, 2020

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

	Input Parameters		
	User Input	COS DCM	
H <sub>weir front</sub> =	4.50	4.50	ft
L <sub>weir front</sub> =	8.00	9.00	ft
S <sub>weir sides</sub> =	0.00	0.00	ft / ft
Horizontal L <sub>weir sides</sub> =	8.00	5.00	ft
Grate Open Area =	70%	70%	%
Debris Clogging =	50%	50%	%
H <sub>grate top</sub> =	4.50	4.50	ft
Slope L <sub>weir sides</sub> =	8.00	5.00	ft
Open Area (No Clogging) =	44.80	31.50	sq ft
Open Area (Clogged) =	22.40	15.75	sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

	Input Parameters		
	User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50	ft
Pipe Diameter =	36.00	30.00	inches
Plate Height =	22.42	28.11	inches
Theta =	1.82	2.63	radians
Outlet Ao =	4.63	4.78	sq ft
Outlet <sub>centroid</sub> =	1.06	1.22	ft
Open Area Ratio =	9.68	6.59	

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

	Input Parameters		
	User Input	COS DCM	
H <sub>spillway invert</sub> =	5.90	6.00	ft
L <sub>spillway crest</sub> =	42.00	33.00	ft
S <sub>spillway ends</sub> =	4.00	4.00	ft / ft
Freeboard Depth =	1.00	1.00	ft
Flow Depth <sub>spillway</sub> =	0.80	1.00	ft
Freeboard Top Stage =	7.70	8.00	ft
Max Basin Area =	1.27	1.29	acres

9. Routed Hydrograph Results

	Results based on User Input								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.64	1.66		2.16				7.27	
Inflow Hydrograph Volume (ac-ft) =	N/A	N/A		13.0				57.1	
Predevelopment Peak Q (cfs) =	N/A	N/A		30.7				100.4	
Peak Inflow (cfs) =	0.3	0.5		4.6				56.3	
Peak Outflow (cfs) =	N/A	N/A		0.4				1.0	
Ratio (Outflow/Predevelopment) =	Orifice Plate	Orifice Plate		Overflow Grate				Outlet Pipe	
Structure Controlling Flow =	N/A	N/A		0.1				1.2	
Max Velocity through Grate =	39	69		73				61	
Time to Drain 97% of Volume (hr) =	41	72		77				72	
Time to Drain 99% of Volume (hr) =	3.40	4.50		4.70				5.90	
Maximum Ponding Depth (ft) =	0.80	0.97		0.98				1.09	
Area at Max Ponding Depth (ac) =	0.64	1.66		1.87				3.11	
Maximum Volume Stored (ac-ft) =									
	Results based on COS DCM Inputs								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.64	1.66		2.16				7.27	
Inflow Hydrograph Volume (ac-ft) =	N/A	N/A		13.0				57.1	
Predevelopment Peak Q (cfs) =	N/A	N/A		30.7				100.4	
Peak Inflow (cfs) =	0.3	0.5		4.3				57.5	
Peak Outflow (cfs) =	N/A	N/A		0.3				1.0	
Ratio (Outflow/Predevelopment) =	Orifice Plate	Orifice Plate		Overflow Grate				Outlet Pipe	
Structure Controlling Flow =	N/A	N/A		0.2				1.8	
Max Velocity through Grate =	39	69		73				61	
Time to Drain 97% of Volume (hr) =	41	72		77				72	
Time to Drain 99% of Volume (hr) =	3.40	4.50		4.70				5.90	
Maximum Ponding Depth (ft) =	0.80	0.97		0.98				1.09	
Area at Max Ponding Depth (ac) =	0.64	1.66		1.87				3.11	
Maximum Volume Stored (ac-ft) =									

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

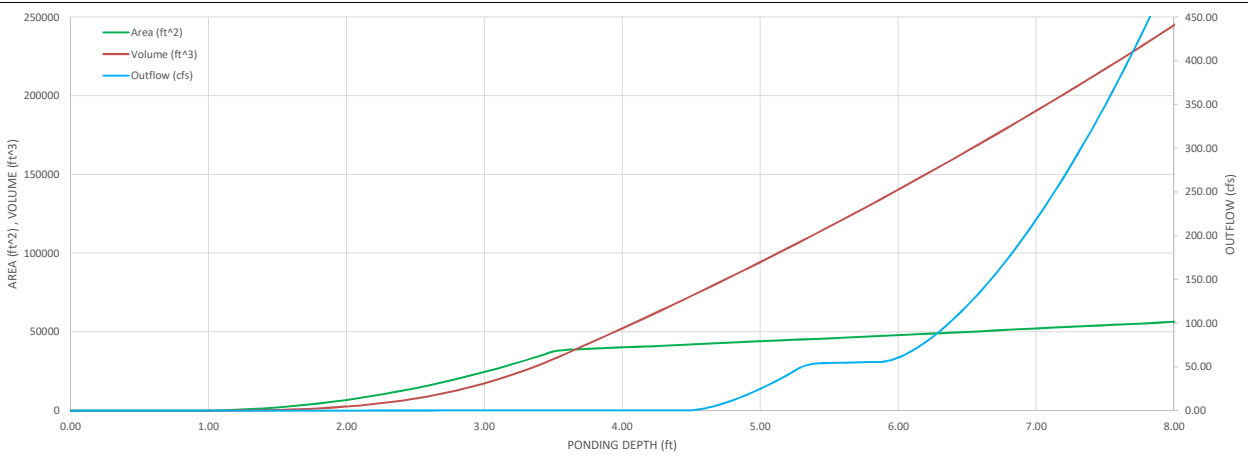
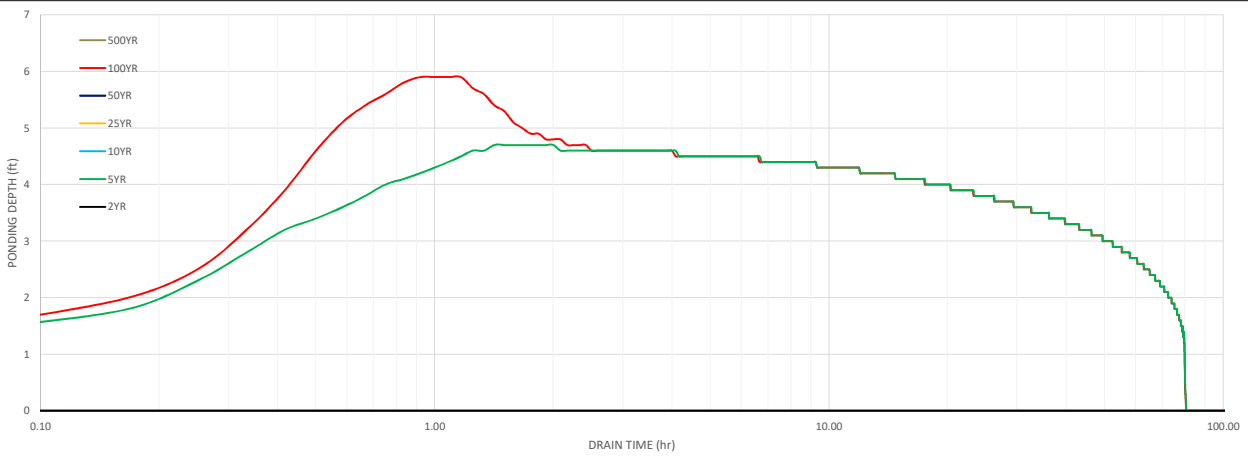
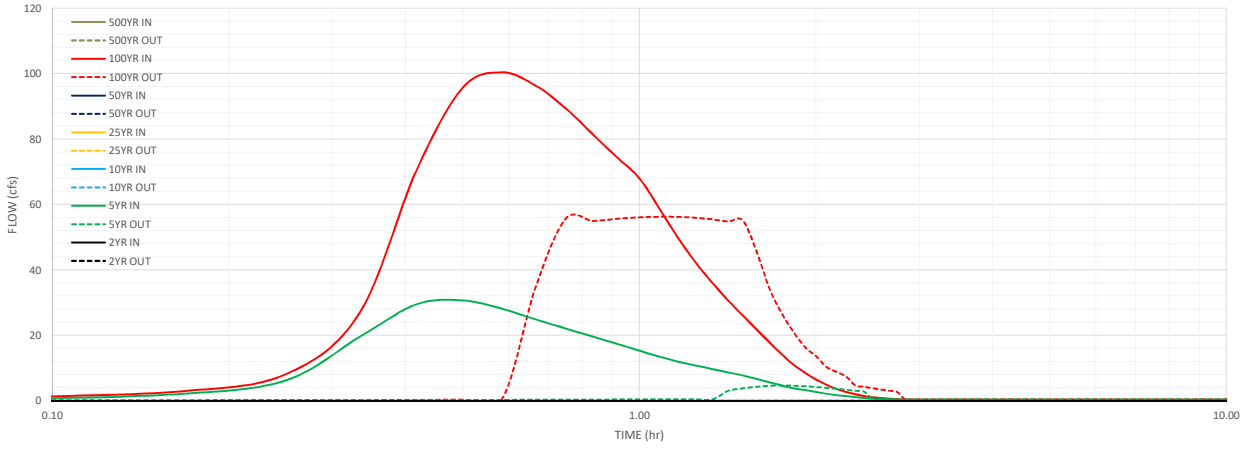


Designer: Chris McFarland

Project: Grandview Reserve Pond A

Date: April 6, 2020

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond B

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB) ▼

2. WQCV/EURV Outlet Details  
A) Average Infiltration Rate of WQCV  
B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface  
C) Underdrain Outlet Orifice Area  
D) Number of WQCV Orifice Rows  
E) Vertical Spacing between WQCV Orifice Rows  
F) WQCV Orifice Area (A<sub>o</sub>) per Row  
G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)  
H) EURV Orifice Area (A<sub>o</sub>) in Single Row  
I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)  
J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain A <sub>o</sub> =	N/A	N/A
# WQCV rows =	14	14
Orifice Spacing =	4.0	4.0
WQCV A <sub>o</sub> =	1.49	1.49
Max Stage wqcv =	4.70	4.70
EURV A <sub>o</sub> =	1.49	1.49
Max Stage EURV =	6.00	6.00
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

A) Length of Basin at Top of EURV  
B) Width of Basin at Top of EURV  
C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)  
D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)  
E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)  
F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	644.7	644.7
W <sub>PCM</sub> =	191.2	191.2
Stage at Top of Bench =	6.10	6.10
L <sub>Bench</sub> =	645.5	645.5
W <sub>Bench</sub> =	192.0	192.0
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
		17.56				164.21

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		0.69				2.08	
0:10		5.80				8.30	
0:15		16.64				20.58	
0:20		42.42				58.80	
0:25		68.16				179.82	
0:30		75.65				276.49	
0:35		71.78				307.62	
0:40		64.91				331.81	
0:45		58.24				366.22	
0:50		52.24				365.58	
0:55		47.02				346.26	
1:00		42.99				321.76	
1:05		39.68				290.00	
1:10		36.25				252.97	
1:15		32.60				216.52	
1:20		29.09				182.15	
1:25		26.07				152.09	
1:30		23.97				127.70	
1:35		22.28				109.78	
1:40		20.74				95.42	
1:45		19.35				83.46	
1:50		18.07				73.27	
1:55		16.77				63.53	
2:00		14.81				60.20	
2:05		12.66				51.42	
2:10		10.67				42.95	
2:15		8.88				35.32	
2:20		7.28				28.18	
2:25		5.90				21.64	
2:30		4.82				15.96	
2:35		4.08				11.89	
2:40		3.58				9.39	
2:45		3.19				7.53	
2:50		2.86				6.09	
2:55		2.60				4.98	
3:00		2.39				4.12	
3:05		2.22				3.47	
3:10		2.09				2.97	
3:15		1.97				2.55	
3:20		1.86				2.21	
3:25		1.77				2.08	
3:30		1.70				1.98	
3:35		1.63				1.88	
3:40		1.58				1.81	
3:45		1.54				1.75	
3:50		1.51				1.70	
3:55		1.49				1.67	
4:00		1.47				1.65	
4:05		1.46				1.64	
4:10		1.46				1.64	
4:15		1.46				1.64	
4:20		1.46				1.64	
4:25		1.45				1.64	
4:30		1.45				1.63	
4:35		1.45				1.63	
4:40		1.45				1.63	
4:45		1.45				1.63	
4:50		1.44				1.63	
4:55		1.44				1.63	
5:00		1.44				1.62	
5:05		1.44				1.62	
5:10		1.44				1.62	
5:15		1.43				1.62	
5:20		1.43				1.62	
5:25		1.43				1.61	
5:30		1.43				1.61	
5:35		1.43				1.61	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5.40		1.42				1.61	
5.45		1.42				1.61	
5.50		1.42				1.60	
5.55		1.42				1.60	
6.00							





Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond B

Date: April 6, 2020

Last Edited: April 13, 2020

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

	Input Parameters		
	User Input	COS DCM	
H <sub>weir front</sub> =	6.00	6.00	ft
L <sub>weir front</sub> =	17.00	17.00	ft
S <sub>weir sides</sub> =	0.00	0.00	ft / ft
Horizontal L <sub>weir sides</sub> =	17.00	7.00	ft
Grate Open Area =	70%	70%	%
Debris Clogging =	50%	50%	%
H <sub>grate top</sub> =	6.00	6.00	ft
Slope L <sub>weir sides</sub> =	17.00	7.00	ft
Open Area (No Clogging) =	202.30	83.30	sq ft
Open Area (Clogged) =	101.15	41.65	sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

	Input Parameters		
	User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50	ft
Pipe Diameter =	54.00	48.00	inches
Plate Height =	37.00	42.00	inches
Theta =	1.95	2.42	radians
Outlet Ao =	11.61	11.66	sq ft
Outlet <sub>centroid</sub> =	1.73	1.87	ft
Open Area Ratio =	17.42	7.14	

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

	Input Parameters		
	User Input	COS DCM	
H <sub>spillway invert</sub> =	9.50	9.30	ft
L <sub>spillway crest</sub> =	136.00	122.00	ft
S <sub>spillway ends</sub> =	4.00	4.00	ft / ft
Freeboard Depth =	1.00	1.00	ft
Flow Depth <sub>spillway</sub> =	0.90	1.00	ft
Freeboard Top Stage =	11.40	11.30	ft
Max Basin Area =	3.70	3.68	acres

9. Routed Hydrograph Results

	Results based on User Input								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	2.41	5.73		6.67					
Inflow Hydrograph Volume (ac-ft) =	2.41	5.73		6.67				31.72	
Predevelopment Peak Q (cfs) =	N/A	N/A		17.6				164.2	
Peak Inflow (cfs) =	N/A	N/A		75.7				366.2	
Peak Outflow (cfs) =	1.1	1.4		1.4				166.4	
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.1				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A		0.0				0.8	
Time to Drain 97% of Volume (hr) =	40	68		76				61	
Time to Drain 99% of Volume (hr) =	42	72		80				73	
Maximum Ponding Depth (ft) =	4.70	6.00		6.10				9.10	
Area at Max Ponding Depth (ac) =	1.92	2.83		2.85				3.32	
Maximum Volume Stored (ac-ft) =	2.41	5.73		6.04				15.28	

	Results based on COS DCM Inputs								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	2.41	5.73		6.67					
Inflow Hydrograph Volume (ac-ft) =	2.41	5.73		6.67				31.72	
Predevelopment Peak Q (cfs) =	N/A	N/A		17.6				164.2	
Peak Inflow (cfs) =	N/A	N/A		75.7				366.2	
Peak Outflow (cfs) =	1.1	1.4		1.4				166.5	
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.1				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A		0.0				2.0	
Time to Drain 97% of Volume (hr) =	40	68		76				61	
Time to Drain 99% of Volume (hr) =	42	72		80				73	
Maximum Ponding Depth (ft) =	4.70	6.00		6.10				9.20	
Area at Max Ponding Depth (ac) =	1.92	2.83		2.85				3.34	
Maximum Volume Stored (ac-ft) =	2.41	5.73		6.04				15.62	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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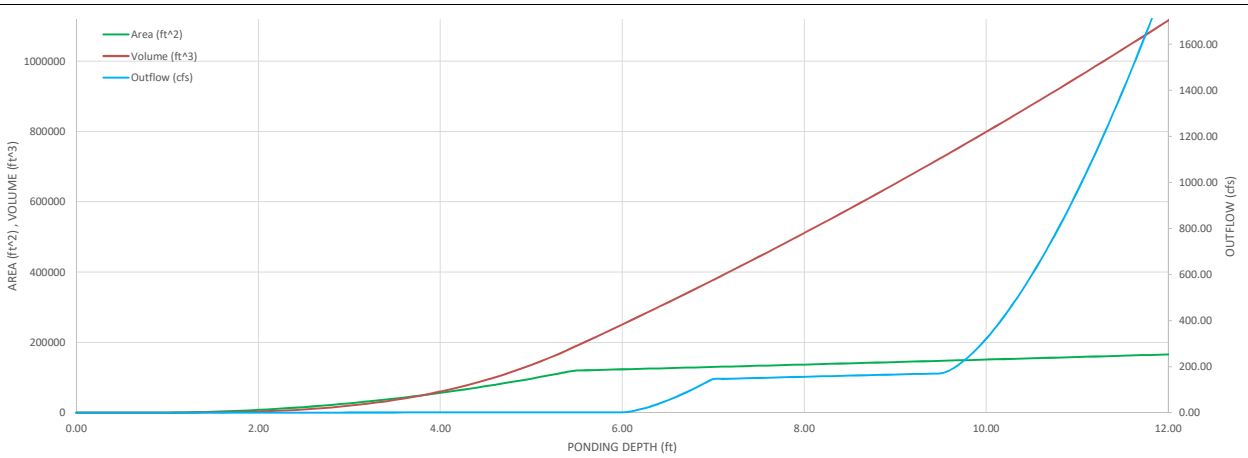
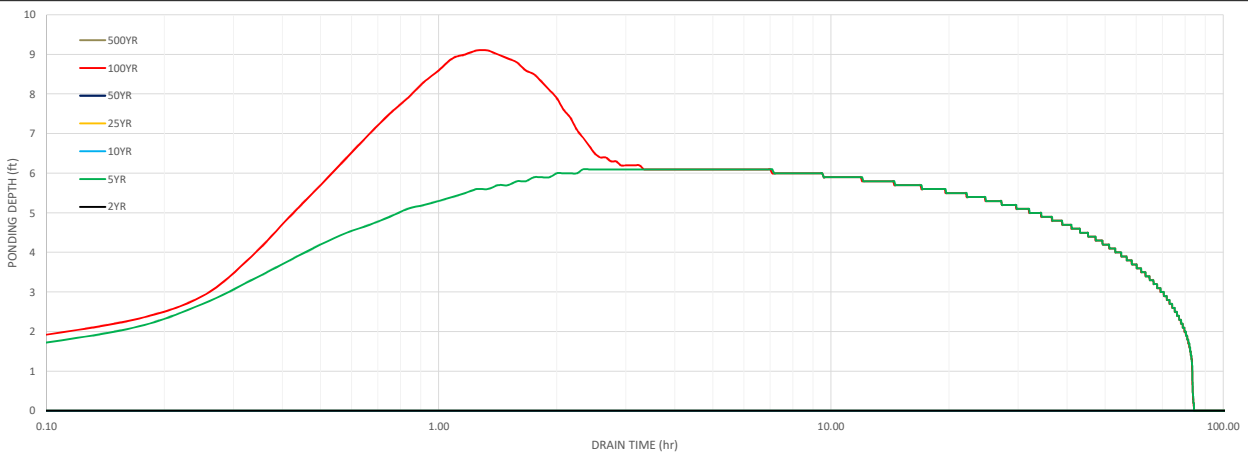
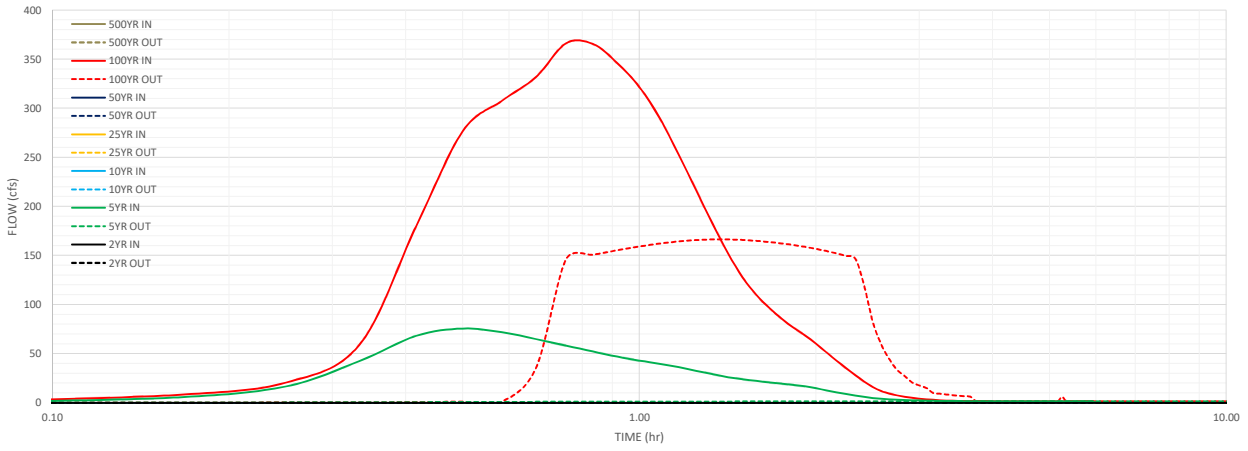


Designer: Chris McFarland

Project: Grandview Reserve Pond B

Date: April 6, 2020

Last Edited: April 13, 2020



Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond C

Date: April 6, 2020

Last Edited: April 08, 2020

1. Select QOCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB) ▼

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	12	12
Orifice Spacing =	4.0	4.0
WQCV Ao =	1.05	1.05
Max Stage wqcv =	4.00	4.00
EURV Ao =	17.07	17.07
Max Stage EURV =	6.00	6.00
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Slope at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	453.3	453.3
W <sub>PCM</sub> =	177.8	177.8
Stage at Top of Bench =	6.10	6.10
L <sub>Bench</sub> =	454.1	454.1
W <sub>Bench</sub> =	178.6	178.6
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
	9.95				120.21	

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		1.75				4.56	
0:10		11.33				15.20	
0:15		27.93				32.42	
0:20		61.14				76.70	
0:25		78.99				190.43	
0:30		71.29				238.04	
0:35		58.22				222.59	
0:40		47.28				193.29	
0:45		38.58				162.70	
0:50		32.22				131.89	
0:55		27.64				110.47	
1:00		23.60				95.05	
1:05		20.00				74.37	
1:10		16.49				54.92	
1:15		14.05				38.35	
1:20		12.80				27.93	
1:25		12.09				21.76	
1:30		11.62				18.07	
1:35		10.55				15.64	
1:40		9.55				14.06	
1:45		8.84				12.98	
1:50		8.33				12.35	
1:55		7.74				12.15	
2:00		5.88				9.32	
2:05		4.08				6.49	
2:10		2.79				4.48	
2:15		1.86				3.04	
2:20		1.21				1.99	
2:25		0.80				1.32	
2:30		0.49				0.80	
2:35		0.25				0.40	
2:40		0.09				0.14	
2:45		0.01				0.01	
2:50		0.00				0.00	
2:55							
3:00							
3:05							
3:10							
3:15							
3:20							
3:25							
3:30							
3:35							
3:40							
3:45							
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4:00							
4:05							
4:10							
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4:35							
4:40							
4:45							
4:50							
4:55							
5:00							
5:05							
5:10							
5:15							
5:20							
5:25							
5:30							
5:35							

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5.40								
5.45								
5.50								
5.55								
6.00								





Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond C

Date: April 6, 2020

Last Edited: April 08, 2020

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

	Input Parameters		
	User Input	COS DCM	
H <sub>weir front</sub> =	6.00	6.00	ft
L <sub>weir front</sub> =	12.00	11.00	ft
S <sub>weir sides</sub> =	0.00	0.00	ft / ft
Horizontal L <sub>weir sides</sub> =	12.00	11.00	ft
Grate Open Area =	70%	70%	%
Debris Clogging =	50%	50%	%
H <sub>grate top</sub> =	6.00	6.00	ft
Slope L <sub>weir sides</sub> =	12.00	11.00	ft
Open Area (No Clogging) =	100.80	84.70	sq ft
Open Area (Clogged) =	50.40	42.35	sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

	Input Parameters		
	User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50	ft
Pipe Diameter =	48.00	42.00	inches
Plate Height =	33.13	39.36	inches
Theta =	1.96	2.63	radians
Outlet Ao =	9.25	9.37	sq ft
Outlet <sub>centroid</sub> =	1.54	1.71	ft
Open Area Ratio =	10.90	9.04	

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

	Input Parameters		
	User Input	COS DCM	
H <sub>spillway invert</sub> =	8.00	999.00	ft
L <sub>spillway crest</sub> =	79.00	42.00	ft
S <sub>spillway ends</sub> =	4.00	4.00	ft / ft
Freeboard Depth =	1.00	1.00	ft
Flow Depth <sub>spillway</sub> =	1.00		ft
Freeboard Top Stage =	10.00		ft
Max Basin Area =	2.34		acres

9. Routed Hydrograph Results

	Results based on User Input								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	1.36	4.79		4.34				12.42	
Inflow Hydrograph Volume (ac-ft) =	1.36	4.79		4.34				12.42	
Predevelopment Peak Q (cfs) =	N/A	N/A		10.0				120.2	
Peak Inflow (cfs) =	N/A	N/A		79.0				238.0	
Peak Outflow (cfs) =	0.6	1.7		1.5				119.2	
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.2				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Orifice Plate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A		N/A				1.2	
Time to Drain 97% of Volume (hr) =	39	67		65				63	
Time to Drain 99% of Volume (hr) =	41	72		69				72	
Maximum Ponding Depth (ft) =	4.00	6.00		5.60				7.10	
Area at Max Ponding Depth (ac) =	1.32	1.85		1.80				1.98	
Maximum Volume Stored (ac-ft) =	1.36	4.79		4.07				6.91	

	Results based on COS DCM Inputs								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	1.36	4.79		4.34				12.42	
Inflow Hydrograph Volume (ac-ft) =	1.36	4.79		4.34				12.42	
Predevelopment Peak Q (cfs) =	N/A	N/A		10.0				120.2	
Peak Inflow (cfs) =	N/A	N/A		79.0				238.0	
Peak Outflow (cfs) =	0.6	1.7		1.5				116.8	
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.2				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Orifice Plate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A		N/A				1.3	
Time to Drain 97% of Volume (hr) =	39	67		65				63	
Time to Drain 99% of Volume (hr) =	41	72		69				72	
Maximum Ponding Depth (ft) =	4.00	6.00		5.60				7.10	
Area at Max Ponding Depth (ac) =	1.32	1.85		1.80				1.98	
Maximum Volume Stored (ac-ft) =	1.36	4.79		4.07				6.91	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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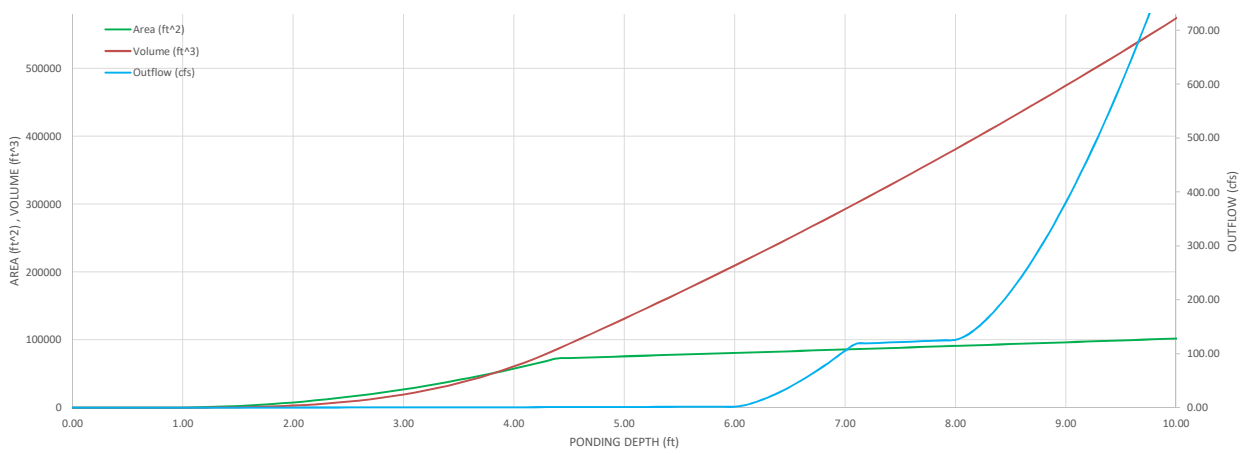
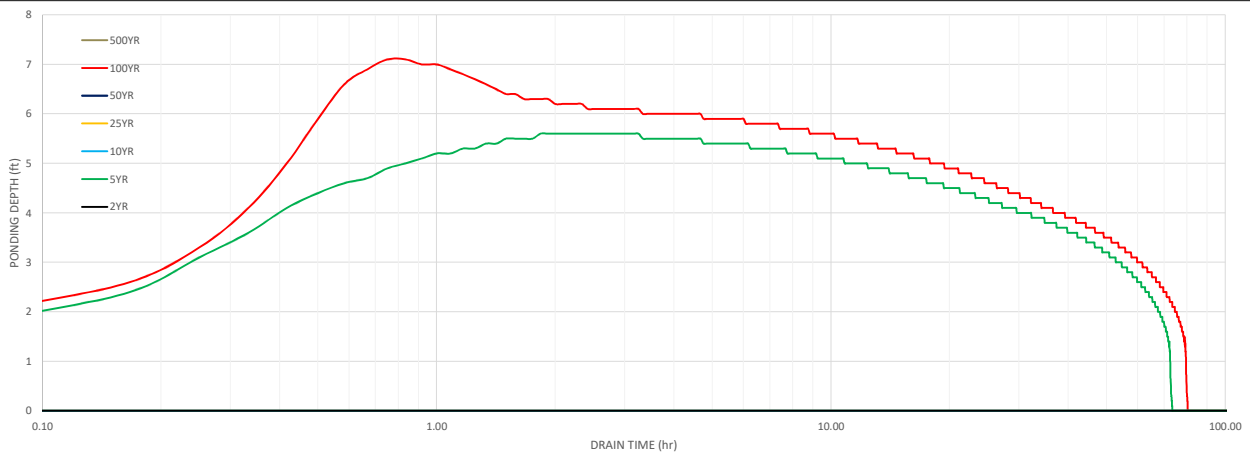
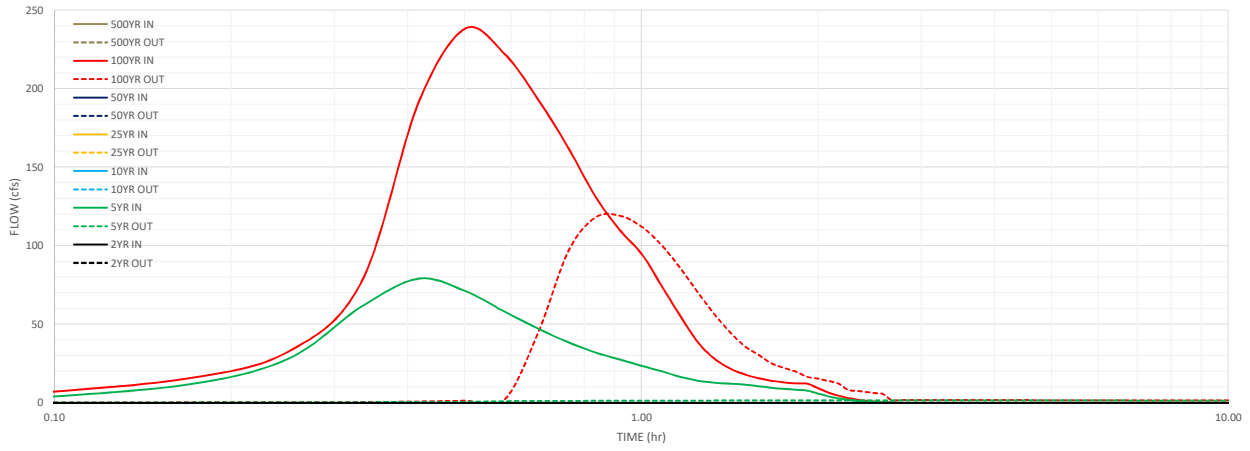


Designer: Chris McFarland

Project: Grandview Reserve Pond C

Date: April 6, 2020

Last Edited: April 08, 2020



Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond D

Date: April 6, 2020

Last Edited: April 13, 2020

1. Select WQCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB) ▼

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	13	13
Orifice Spacing =	4.0	4.0
WQCV Ao =	1.34	1.34
Max Stage wqcv =	4.50	4.50
EURV Ao =	20.83	20.83
Max Stage EURV =	6.50	6.50
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Slope at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	588.5	588.5
W <sub>PCM</sub> =	180.1	180.1
Stage at Top of Bench =	6.60	6.60
L <sub>Bench</sub> =	589.3	589.3
W <sub>Bench</sub> =	180.9	180.9
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)					
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
	30.00				154.35

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		1.91				5.05	
0:10		13.55				18.88	
0:15		36.44				44.44	
0:20		87.25				108.47	
0:25		118.48				244.10	
0:30		113.01				314.40	
0:35		95.70				305.49	
0:40		80.03				273.09	
0:45		67.12				239.63	
0:50		56.09				204.40	
0:55		48.05				175.96	
1:00		41.91				156.02	
1:05		36.47				129.55	
1:10		30.68				102.47	
1:15		25.11				77.55	
1:20		21.41				56.75	
1:25		19.34				42.46	
1:30		18.14				33.79	
1:35		16.52				28.16	
1:40		14.92				24.40	
1:45		13.77				21.60	
1:50		12.92				19.98	
1:55		12.02				18.83	
2:00		9.58				15.10	
2:05		6.95				10.86	
2:10		4.98				7.82	
2:15		3.53				5.61	
2:20		2.44				3.93	
2:25		1.66				2.73	
2:30		1.13				1.86	
2:35		0.72				1.18	
2:40		0.41				0.67	
2:45		0.20				0.31	
2:50		0.08				0.11	
2:55		0.04				0.05	
3:00		0.02				0.02	
3:05		0.01				0.01	
3:10		0.01				0.01	
3:15		0.00				0.00	
3:20						0.00	
3:25							
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5.40								
5.45								
5.50								
5.55								
6.00								





Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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Designer: Chris McFarland

Project: Grandview Reserve Pond D

Date: April 6, 2020

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
	User Input	COS DCM
H <sub>weir front</sub> =	6.50	6.50
L <sub>weir front</sub> =	11.00	9.00
S <sub>weir sides</sub> =	0.00	0.00
Horizontal L <sub>weir sides</sub> =	11.00	9.00
Grate Open Area =	70%	70%
Debris Clogging =	50%	50%
H <sub>grate top</sub> =	6.50	6.50
Slope L <sub>weir sides</sub> =	11.00	9.00
Open Area (No Clogging) =	84.70	56.70
Open Area (Clogged) =	42.35	28.35

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
	User Input	COS DCM
Pipe Invert Depth =	1.50	1.50
Pipe Diameter =	48.00	48.00
Plate Height =	44.00	44.00
Theta =	2.56	2.56
Outlet Ao =	12.07	12.07
Outlet <sub>centroid</sub> =	1.93	1.93
Open Area Ratio =	7.02	4.70

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
	User Input	COS DCM
H <sub>spillway invert</sub> =	8.00	999.00
L <sub>spillway crest</sub> =	105.00	42.00
S <sub>spillway ends</sub> =	4.00	4.00
Freeboard Depth =	1.00	1.00
Flow Depth <sub>spillway</sub> =	1.00	
Freeboard Top Stage =	10.00	
Max Basin Area =	2.95	

9. Routed Hydrograph Results

		Results based on User Input								
		WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =		1.96	6.56		6.97				18.57	
Inflow Hydrograph Volume (ac-ft) =		N/A	N/A		30.0				154.4	
Predevelopment Peak Q (cfs) =		N/A	N/A		118.5				314.4	
Peak Inflow (cfs) =		0.9	2.2		2.2				161.7	
Peak Outflow (cfs) =		N/A	N/A		0.1				1.0	
Ratio (Outflow/Predevelopment) =		Orifice Plate	Orifice Plate		Orifice Plate				Outlet Pipe	
Structure Controlling Flow =		N/A	N/A		N/A				1.8	
Max Velocity through Grate =		40	67		70				62	
Time to Drain 97% of Volume (hr) =		42	72		75				72	
Time to Drain 99% of Volume (hr) =		4.50	6.50		6.50				7.90	
Maximum Ponding Depth (ft) =		1.71	2.43		2.43				2.63	
Area at Max Ponding Depth (ac) =		1.96	6.56		6.59				10.13	
Maximum Volume Stored (ac-ft) =										
		Results based on COS DCM Inputs								
		WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =		1.96	6.56		6.97				18.57	
Inflow Hydrograph Volume (ac-ft) =		N/A	N/A		30.0				154.4	
Predevelopment Peak Q (cfs) =		N/A	N/A		118.5				314.4	
Peak Inflow (cfs) =		0.9	2.2		2.2				153.1	
Peak Outflow (cfs) =		N/A	N/A		0.1				1.0	
Ratio (Outflow/Predevelopment) =		Orifice Plate	Orifice Plate		Orifice Plate				Overflow Grate	
Structure Controlling Flow =		N/A	N/A		N/A				2.8	
Max Velocity through Grate =		40	67		70				63	
Time to Drain 97% of Volume (hr) =		42	72		75				72	
Time to Drain 99% of Volume (hr) =		4.50	6.50		6.50				8.10	
Maximum Ponding Depth (ft) =		1.71	2.43		2.43				2.66	
Area at Max Ponding Depth (ac) =		1.96	6.56		6.59				10.66	
Maximum Volume Stored (ac-ft) =										

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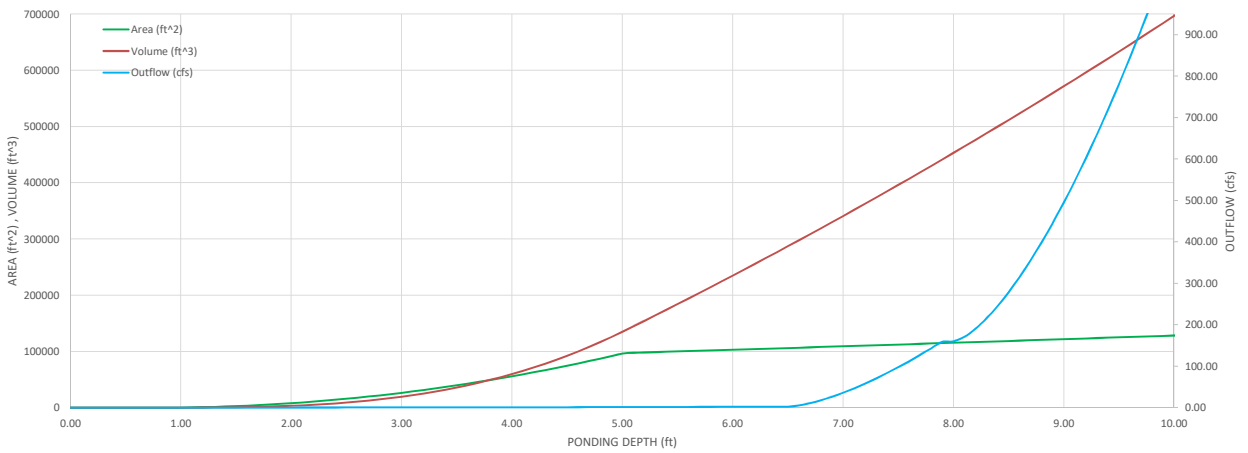
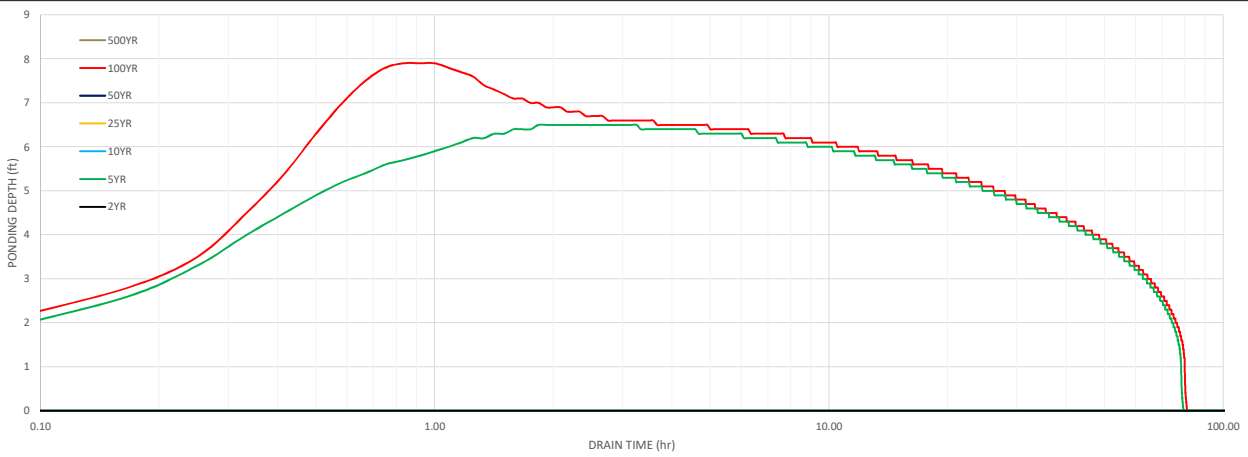
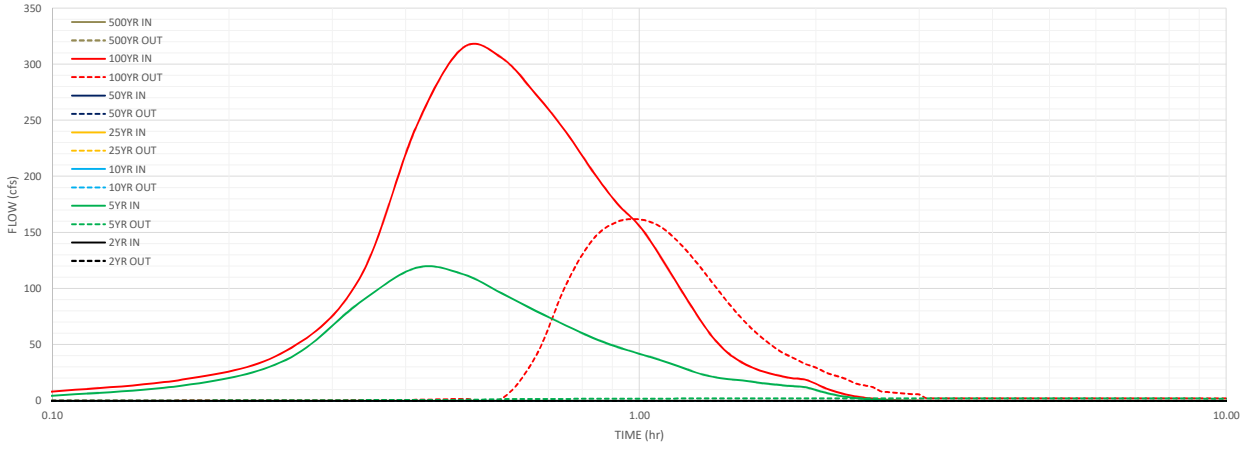


Designer: Chris McFarland

Project: Grandview Reserve Pond D

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Sheet 1 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond E

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1. Select WQCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	10	10
Orifice Spacing =	4.0	4.0
WQCV Ao =	0.67	0.67
Max Stage wqcv =	3.60	3.60
EURV Ao =	0.67	0.67
Max Stage EURV =	4.50	4.50
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	327.0	327.0
W <sub>PCM</sub> =	127.7	127.7
Stage at Top of Bench =	4.60	4.60
L <sub>Bench</sub> =	327.8	327.8
W <sub>Bench</sub> =	128.5	128.5
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
		32.34				157.99

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		0.16				0.43	
0:10		1.11				1.54	
0:15		5.07				7.00	
0:20		23.64				35.29	
0:25		41.87				110.52	
0:30		46.56				162.17	
0:35		43.13				176.94	
0:40		37.83				172.03	
0:45		33.03				161.08	
0:50		29.04				147.26	
0:55		25.75				135.35	
1:00		22.65				124.96	
1:05		19.67				109.31	
1:10		16.82				92.46	
1:15		14.63				77.36	
1:20		13.01				65.86	
1:25		11.61				56.57	
1:30		10.30				48.68	
1:35		8.90				41.54	
1:40		7.47				34.92	
1:45		6.08				28.67	
1:50		4.75				22.81	
1:55		3.50				17.32	
2:00		2.49				12.10	
2:05		1.86				8.45	
2:10		1.45				6.02	
2:15		1.16				4.29	
2:20		0.92				3.03	
2:25		0.73				2.11	
2:30		0.57				1.42	
2:35		0.44				0.96	
2:40		0.34				0.71	
2:45		0.26				0.55	
2:50		0.20				0.44	
2:55		0.15				0.34	
3:00		0.11				0.26	
3:05		0.07				0.19	
3:10		0.05				0.13	
3:15		0.03				0.08	
3:20		0.02				0.04	
3:25		0.01				0.02	
3:30		0.00				0.00	
3:35		0.00				0.00	
3:40		0.00					
3:45		0.00					
3:50		0.00					
3:55		0.00					
4:00		0.00					
4:05		0.00					
4:10		0.00					
4:15							
4:20							
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5:30							
5:35							

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5.40								
5.45								
5.50								
5.55								
6.00								





Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

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Designer: Chris McFarland

Project: Grandview Reserve Pond E

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

	Input Parameters		
	User Input	COS DCM	
H <sub>weir front</sub> =	4.50	4.50	ft
L <sub>weir front</sub> =	15.00	9.00	ft
S <sub>weir sides</sub> =	0.00	0.00	ft / ft
Horizontal L <sub>weir sides</sub> =	15.00	9.00	ft
Grate Open Area =	70%	70%	%
Debris Clogging =	50%	50%	%
H <sub>grate top</sub> =	4.50	4.50	ft
Slope L <sub>weir sides</sub> =	15.00	9.00	ft
Open Area (No Clogging) =	157.50	56.70	sq ft
Open Area (Clogged) =	78.75	28.35	sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

	Input Parameters		
	User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50	ft
Pipe Diameter =	60.00	54.00	inches
Plate Height =	43.00	50.00	inches
Theta =	2.02	2.59	radians
Outlet Ao =	15.06	15.37	sq ft
Outlet <sub>centroid</sub> =	1.99	2.18	ft
Open Area Ratio =	10.46	3.69	

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

	Input Parameters		
	User Input	COS DCM	
H <sub>spillway invert</sub> =	5.80	999.00	ft
L <sub>spillway crest</sub> =	100.00	42.00	ft
S <sub>spillway ends</sub> =	4.00	4.00	ft / ft
Freeboard Depth =	1.00	1.00	ft
Flow Depth <sub>spillway</sub> =	0.70		ft
Freeboard Top Stage =	7.50		ft
Max Basin Area =	1.22		acres

9. Routed Hydrograph Results

	Results based on User Input								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.81	1.70		3.01					
Inflow Hydrograph Volume (ac-ft) =								12.89	
Predevelopment Peak Q (cfs) =	N/A	N/A		32.3				158.0	
Peak Inflow (cfs) =	N/A	N/A		46.6				176.9	
Peak Outflow (cfs) =	0.3	0.4		18.0				164.2	
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.6				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Overflow Grate				Outlet Pipe	
Max Velocity through Grate =	N/A	N/A		0.1				1.0	
Time to Drain 97% of Volume (hr) =	44	69		71				54	
Time to Drain 99% of Volume (hr) =	46	72		76				69	
Maximum Ponding Depth (ft) =	3.60	4.50		4.80				5.70	
Area at Max Ponding Depth (ac) =	0.88	0.96		0.98				1.05	
Maximum Volume Stored (ac-ft) =	0.81	1.70		1.99				2.91	

	Results based on COS DCM Inputs								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.81	1.70		3.01					
Inflow Hydrograph Volume (ac-ft) =								12.89	
Predevelopment Peak Q (cfs) =	N/A	N/A		32.3				158.0	
Peak Inflow (cfs) =	N/A	N/A		46.6				176.9	
Peak Outflow (cfs) =	0.3	0.4		16.3				153.2	
Ratio (Outflow/Predevelopment) =	N/A	N/A		0.5				1.0	
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Overflow Grate				Overflow Grate	
Max Velocity through Grate =	N/A	N/A		0.3				2.3	
Time to Drain 97% of Volume (hr) =	44	69		71				54	
Time to Drain 99% of Volume (hr) =	46	72		76				69	
Maximum Ponding Depth (ft) =	3.60	4.50		4.90				6.10	
Area at Max Ponding Depth (ac) =	0.88	0.96		0.99				1.10	
Maximum Volume Stored (ac-ft) =	0.81	1.70		2.09				3.34	

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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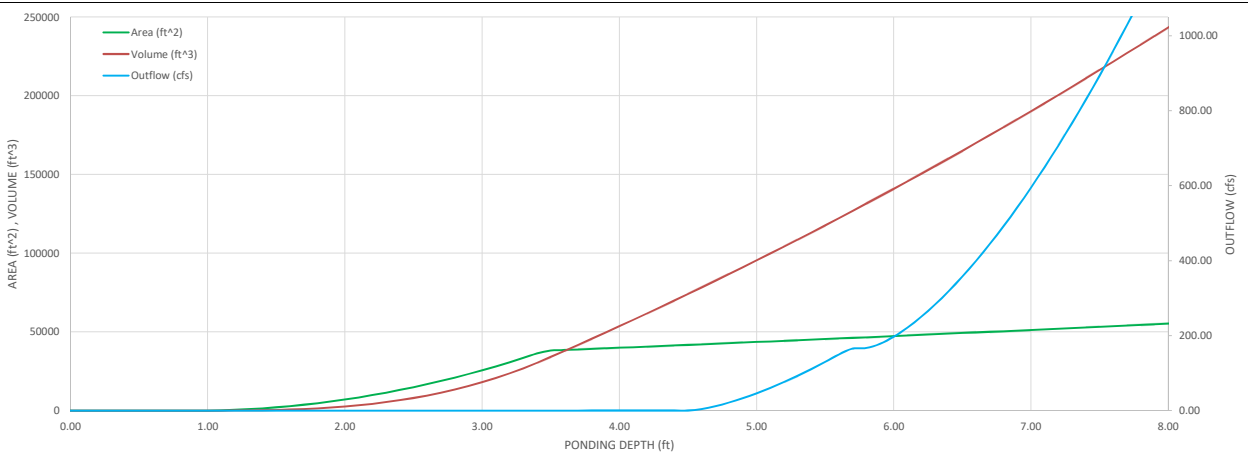
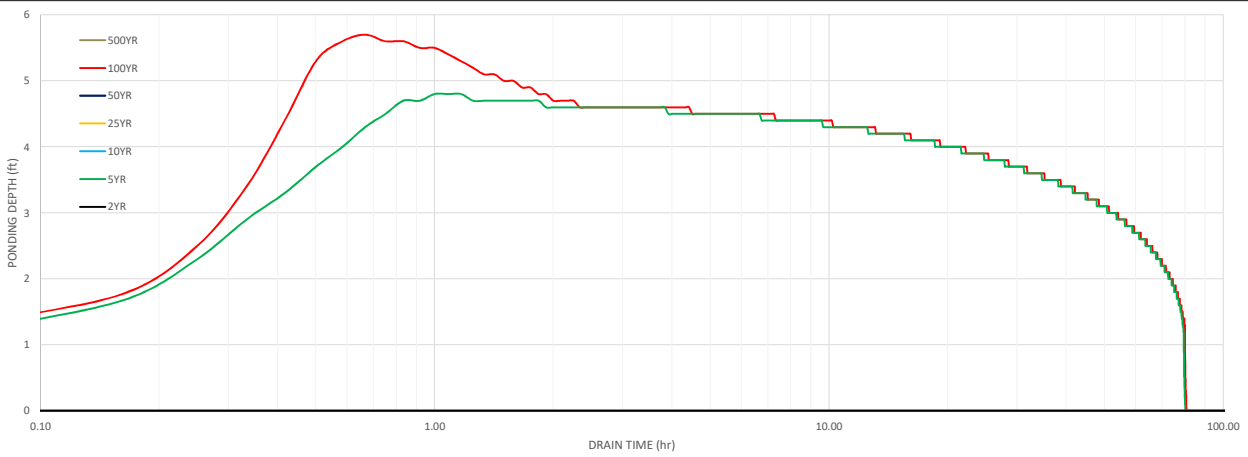
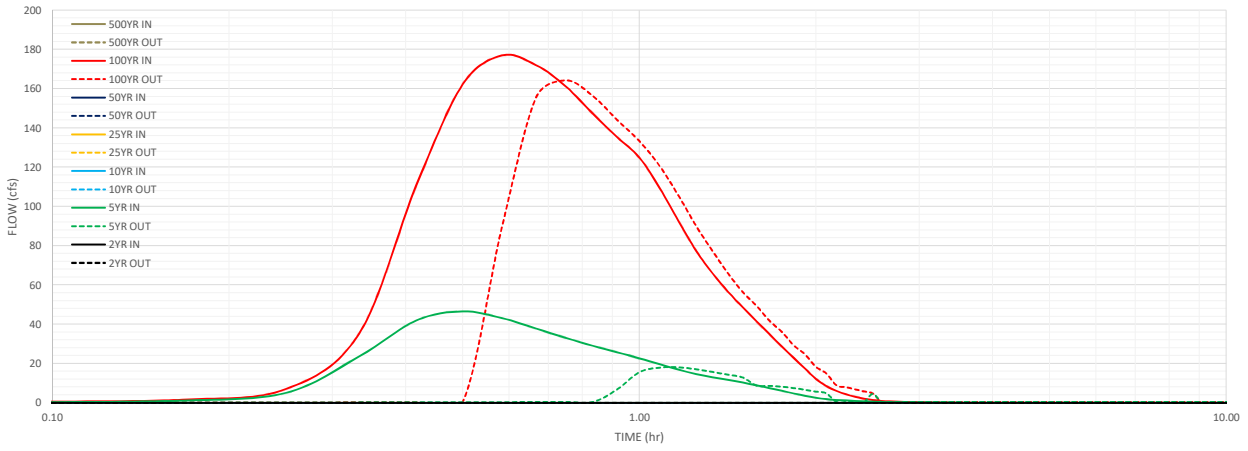


Designer: Chris McFarland

Project: Grandview Reserve Pond E

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

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Designer: Chris McFarland

Project: Grandview Reserve Pond F

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1. Select WQCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	14	13
Orifice Spacing =	4.0	4.0
WQCV Ao =	1.55	1.47
Max Stage wqcv =	4.80	4.50
EURV Ao =	1.55	7.84
Max Stage EURV =	6.00	6.00
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Slope at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	570.9	570.9
W <sub>PCM</sub> =	217.0	217.0
Stage at Top of Bench =	6.10	6.10
L <sub>Bench</sub> =	571.7	571.7
W <sub>Bench</sub> =	217.8	217.8
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
		42.34				221.11

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		0.52				1.80	
0:10		5.98				8.99	
0:15		19.71				25.32	
0:20		58.79				77.64	
0:25		94.74				207.48	
0:30		103.82				301.83	
0:35		97.47				329.97	
0:40		87.23				323.46	
0:45		77.84				304.34	
0:50		69.34				281.05	
0:55		61.26				257.82	
1:00		54.52				237.51	
1:05		49.46				211.11	
1:10		45.22				185.26	
1:15		40.70				161.15	
1:20		36.24				139.03	
1:25		32.06				119.17	
1:30		28.34				101.90	
1:35		24.61				86.26	
1:40		21.24				72.79	
1:45		19.05				62.33	
1:50		17.44				54.79	
1:55		16.04				48.91	
2:00		13.99				42.35	
2:05		11.69				35.81	
2:10		9.57				29.96	
2:15		7.79				24.91	
2:20		6.28				20.57	
2:25		5.03				16.95	
2:30		4.03				13.95	
2:35		3.21				11.42	
2:40		2.52				9.20	
2:45		1.92				7.18	
2:50		1.38				5.32	
2:55		0.95				3.69	
3:00		0.65				2.49	
3:05		0.46				1.70	
3:10		0.33				1.17	
3:15		0.24				0.81	
3:20		0.18				0.56	
3:25		0.14				0.38	
3:30		0.11				0.26	
3:35		0.08				0.18	
3:40		0.06				0.13	
3:45		0.05				0.10	
3:50		0.03				0.07	
3:55		0.02				0.05	
4:00		0.02				0.04	
4:05		0.01				0.03	
4:10		0.01				0.02	
4:15		0.00				0.01	
4:20						0.01	
4:25						0.00	
4:30							
4:35							
4:40							
4:45							
4:50							
4:55							
5:00							
5:05							
5:10							
5:15							
5:20							
5:25							
5:30							
5:35							

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5.40								
5.45								
5.50								
5.55								
6.00								





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Designer: Chris McFarland

Project: Grandview Reserve Pond F

Date: April 6, 2020

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
	User Input	COS DCM
H <sub>weir front</sub> =	6.00	5.00
L <sub>weir front</sub> =	13.00	10.00
S <sub>weir sides</sub> =	0.00	0.00
Horizontal L <sub>weir sides</sub> =	13.00	10.00
Grate Open Area =	70%	70%
Debris Clogging =	50%	50%
H <sub>grate top</sub> =	6.00	6.00
Slope L <sub>weir sides</sub> =	13.00	10.00
Open Area (No Clogging) =	118.30	70.00
Open Area (Clogged) =	59.15	35.00

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
	User Input	COS DCM
Pipe Invert Depth =	1.50	1.50
Pipe Diameter =	66.00	60.00
Plate Height =	46.05	54.00
Theta =	1.98	2.50
Outlet Ao =	17.70	18.61
Outlet <sub>centroid</sub> =	2.14	2.38
Open Area Ratio =	6.68	3.76

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
	User Input	COS DCM
H <sub>spillway invert</sub> =	7.60	999.00
L <sub>spillway crest</sub> =	126.00	42.00
S <sub>spillway ends</sub> =	4.00	4.00
Freeboard Depth =	1.00	1.00
Flow Depth <sub>spillway</sub> =	0.90	
Freeboard Top Stage =	9.50	
Max Basin Area =	3.37	

9. Routed Hydrograph Results

		Results based on User Input								
		WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =		2.62	5.94		7.80				26.37	
Inflow Hydrograph Volume (ac-ft) =		N/A	N/A		42.3				221.1	
Predevelopment Peak Q (cfs) =		N/A	N/A		103.8				330.0	
Peak Inflow (cfs) =		1.1	1.5		15.1				227.3	
Peak Outflow (cfs) =		N/A	N/A		0.4				1.0	
Ratio (Outflow/Predevelopment) =		Orifice Plate	Orifice Plate		Overflow Grate				Outlet Pipe	
Structure Controlling Flow =		N/A	N/A		0.2				1.9	
Max Velocity through Grate =		42	68		72				61	
Time to Drain 97% of Volume (hr) =		45	72		77				72	
Time to Drain 99% of Volume (hr) =		4.80	6.00		6.30				7.60	
Maximum Ponding Depth (ft) =		2.12	2.84		2.89				3.08	
Area at Max Ponding Depth (ac) =		2.62	5.94		6.82				10.70	
Maximum Volume Stored (ac-ft) =										
		Results based on COS DCM Inputs								
		WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =		2.21	5.94		7.80				26.37	
Inflow Hydrograph Volume (ac-ft) =		N/A	N/A		42.3				221.1	
Predevelopment Peak Q (cfs) =		N/A	N/A		103.8				330.0	
Peak Inflow (cfs) =		1.1	1.4		13.2				214.5	
Peak Outflow (cfs) =		N/A	N/A		0.3				1.0	
Ratio (Outflow/Predevelopment) =		Orifice Plate	Orifice Plate		Overflow Grate				Overflow Grate	
Structure Controlling Flow =		N/A	N/A		0.2				3.0	
Max Velocity through Grate =		36	69		74				63	
Time to Drain 97% of Volume (hr) =		38	73		78				73	
Time to Drain 99% of Volume (hr) =		4.50	6.00		6.30				7.80	
Maximum Ponding Depth (ft) =		1.81	2.84		2.89				3.11	
Area at Max Ponding Depth (ac) =		2.21	5.94		6.82				11.32	
Maximum Volume Stored (ac-ft) =										

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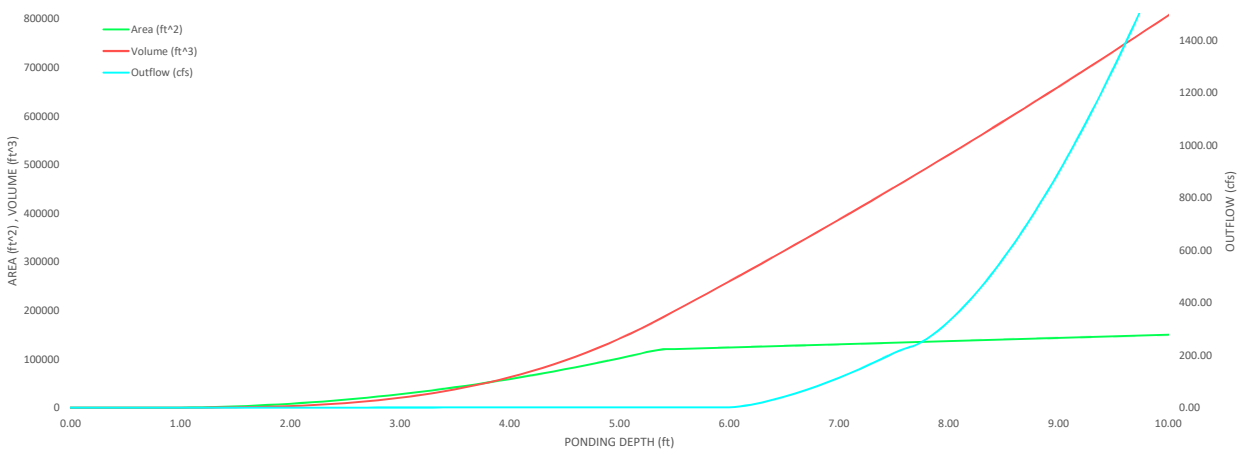
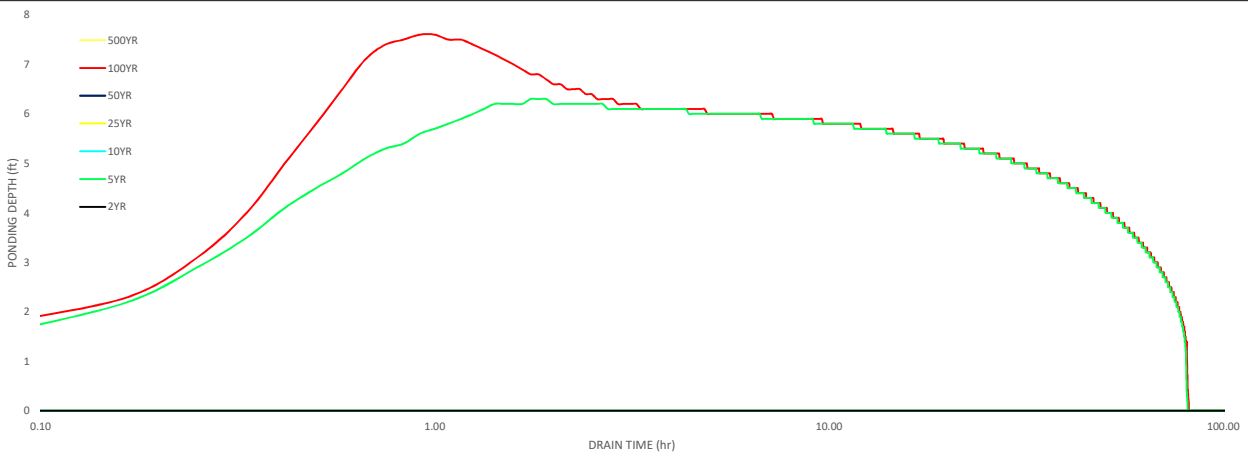
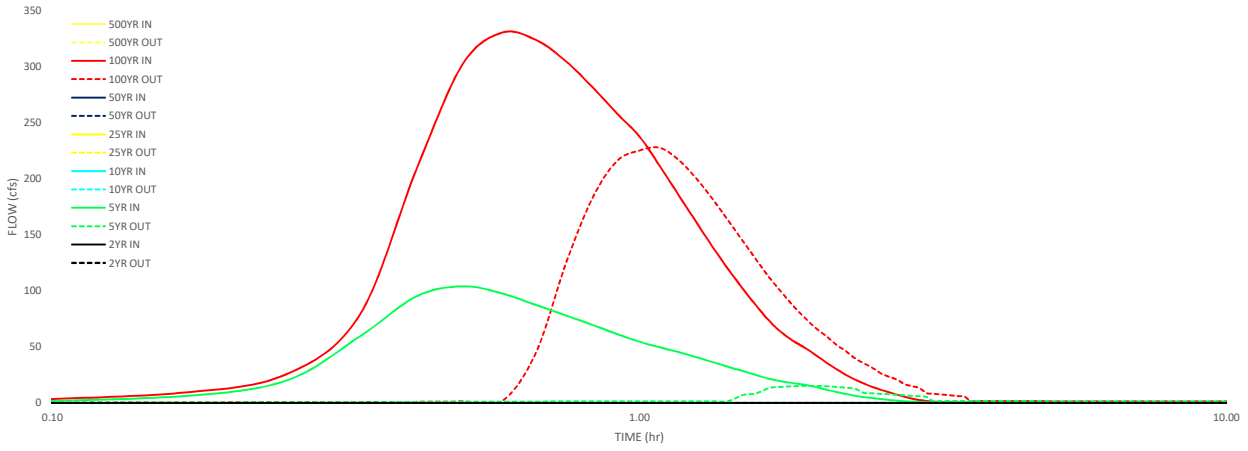


Designer: Chris McFarland

Project: Grandview Reserve Pond F

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Project: Grandview Reserve Pond G

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1. Select QWCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB) ▼

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	9	9
Orifice Spacing =	4.0	4.0
WQCV Ao =	0.49	0.49
Max Stage wqcv =	3.20	3.20
EURV Ao =	1.94	1.94
Max Stage EURV =	4.00	4.00
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Stage at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	349.7	349.7
W <sub>PCM</sub> =	105.4	105.4
Stage at Top of Bench =	4.10	4.10
L <sub>Bench</sub> =	350.5	350.5
W <sub>Bench</sub> =	106.2	106.2
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
	9.42				48.48	

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		0.18				0.49	
0:10		1.27				1.75	
0:15		3.86				5.05	
0:20		12.69				17.55	
0:25		19.21				47.38	
0:30		20.06				63.86	
0:35		18.72				67.51	
0:40		16.88				66.01	
0:45		15.24				62.38	
0:50		13.74				57.86	
0:55		12.37				53.71	
1:00		11.12				49.93	
1:05		10.01				44.10	
1:10		9.05				38.52	
1:15		8.20				33.58	
1:20		7.42				29.30	
1:25		6.67				25.48	
1:30		5.98				22.03	
1:35		5.28				18.97	
1:40		4.64				16.31	
1:45		4.05				13.93	
1:50		3.52				11.83	
1:55		3.12				10.10	
2:00		2.67				8.48	
2:05		2.26				7.10	
2:10		1.90				5.93	
2:15		1.58				4.93	
2:20		1.30				4.04	
2:25		1.05				3.25	
2:30		0.82				2.54	
2:35		0.62				1.90	
2:40		0.46				1.36	
2:45		0.35				0.99	
2:50		0.28				0.73	
2:55		0.22				0.54	
3:00		0.17				0.39	
3:05		0.13				0.28	
3:10		0.10				0.19	
3:15		0.07				0.13	
3:20		0.05				0.09	
3:25		0.04				0.07	
3:30		0.03				0.06	
3:35		0.02				0.04	
3:40		0.02				0.03	
3:45		0.01				0.03	
3:50		0.01				0.02	
3:55		0.01				0.01	
4:00		0.00				0.01	
4:05						0.00	
4:10							
4:15							
4:20							
4:25							
4:30							
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4:45							
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5:00							
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5:10							
5:15							
5:20							
5:25							
5:30							
5:35							

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5.40								
5.45								
5.50								
5.55								
6.00								



Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 2 of 3



Designer: Chris McFarland

Project: Grandview Reserve Pond G

Date: April 6, 2020

Last Edited: April 13, 2020

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

	Input Parameters		
	User Input	COS DCM	
H <sub>weir front</sub> =	4.00	4.00	ft
L <sub>weir front</sub> =	26.00	26.00	ft
S <sub>weir sides</sub> =	0.00	0.00	ft / ft
Horizontal L <sub>weir sides</sub> =	26.00	26.00	ft
Grate Open Area =	70%	70%	%
Debris Clogging =	50%	50%	%
H <sub>grate top</sub> =	4.00	4.00	ft
Slope L <sub>weir sides</sub> =	26.00	26.00	ft
Open Area (No Clogging) =	473.20	473.20	sq ft
Open Area (Clogged) =	236.60	236.60	sq ft

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

	Input Parameters		
	User Input	COS DCM	
Pipe Invert Depth =	1.50	1.50	ft
Pipe Diameter =	30.00	27.00	inches
Plate Height =	22.22	26.24	inches
Theta =	2.07	2.80	radians
Outlet Ao =	3.90	3.94	sq ft
Outlet <sub>centroid</sub> =	1.03	1.12	ft
Open Area Ratio =	121.39	119.97	

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

	Input Parameters		
	User Input	COS DCM	
H <sub>spillway invert</sub> =	5.40	4.90	ft
L <sub>spillway crest</sub> =	136.00	23.00	ft
S <sub>spillway ends</sub> =	4.00	4.00	ft / ft
Freeboard Depth =	1.00	1.00	ft
Flow Depth <sub>spillway</sub> =	0.30	0.90	ft
Freeboard Top Stage =	6.70	6.80	ft
Max Basin Area =	1.08	1.09	acres

9. Routed Hydrograph Results

	Results based on User Input								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.47	1.15		1.57					5.51
Inflow Hydrograph Volume (ac-ft) =	0.47	1.15		1.57					5.51
Predevelopment Peak Q (cfs) =	N/A	N/A		9.4					48.5
Peak Inflow (cfs) =	N/A	N/A		20.1					67.5
Peak Outflow (cfs) =	0.2	0.3		9.4					47.1
Ratio (Outflow/Predevelopment) =	N/A	N/A		1.0					1.0
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Overflow Grate					Outlet Pipe
Max Velocity through Grate =	N/A	N/A		0.0					0.1
Time to Drain 97% of Volume (hr) =	41	69		73					63
Time to Drain 99% of Volume (hr) =	43	72		78					74
Maximum Ponding Depth (ft) =	3.20	4.00		4.10					4.80
Area at Max Ponding Depth (ac) =	0.67	0.85		0.85					0.91
Maximum Volume Stored (ac-ft) =	0.47	1.15		1.24					1.85

	Results based on COS DCM Inputs								
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.47	1.15		1.57					5.51
Inflow Hydrograph Volume (ac-ft) =	0.47	1.15		1.57					5.51
Predevelopment Peak Q (cfs) =	N/A	N/A		9.4					48.5
Peak Inflow (cfs) =	N/A	N/A		20.1					67.5
Peak Outflow (cfs) =	0.2	0.3		9.4					47.1
Ratio (Outflow/Predevelopment) =	N/A	N/A		1.0					1.0
Structure Controlling Flow =	Orifice Plate	Orifice Plate		Overflow Grate					Outlet Pipe
Max Velocity through Grate =	N/A	N/A		0.0					0.1
Time to Drain 97% of Volume (hr) =	41	69		73					63
Time to Drain 99% of Volume (hr) =	43	72		78					74
Maximum Ponding Depth (ft) =	3.20	4.00		4.10					4.80
Area at Max Ponding Depth (ac) =	0.67	0.85		0.85					0.91
Maximum Volume Stored (ac-ft) =	0.47	1.15		1.24					1.85



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COS PCM-FSD Preliminary Design (Beta Version 1.00, September 2019)

Sheet 3 of 3

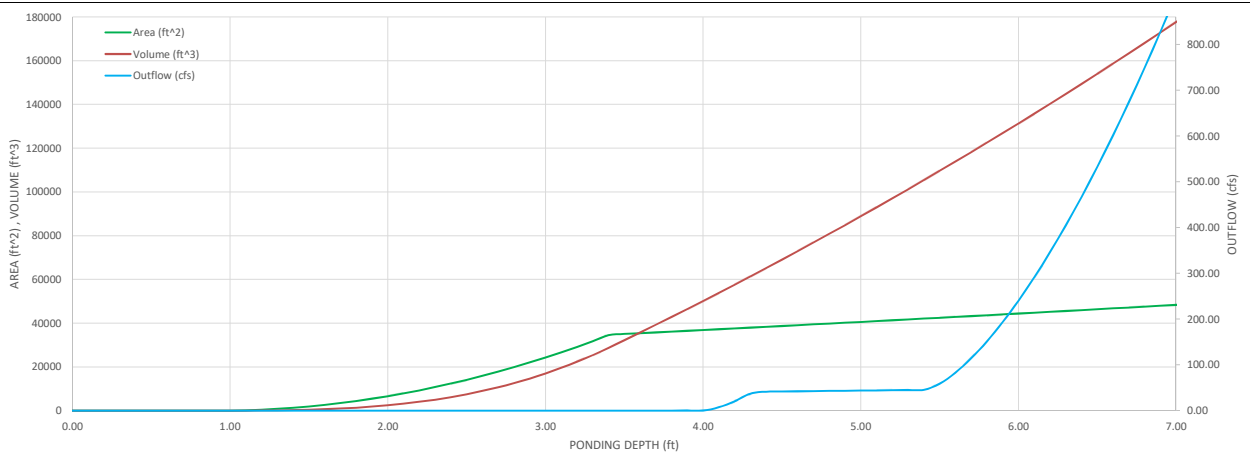
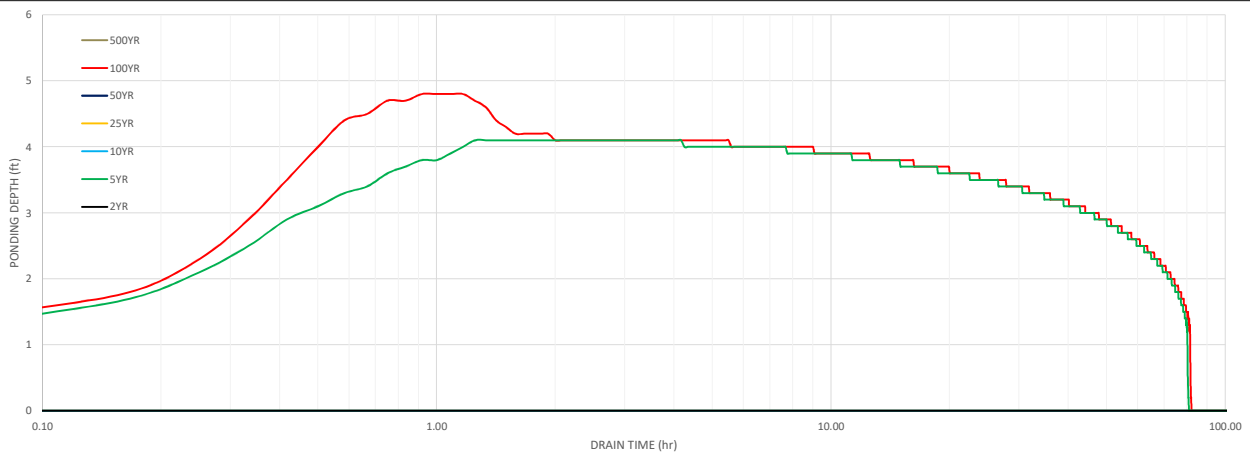
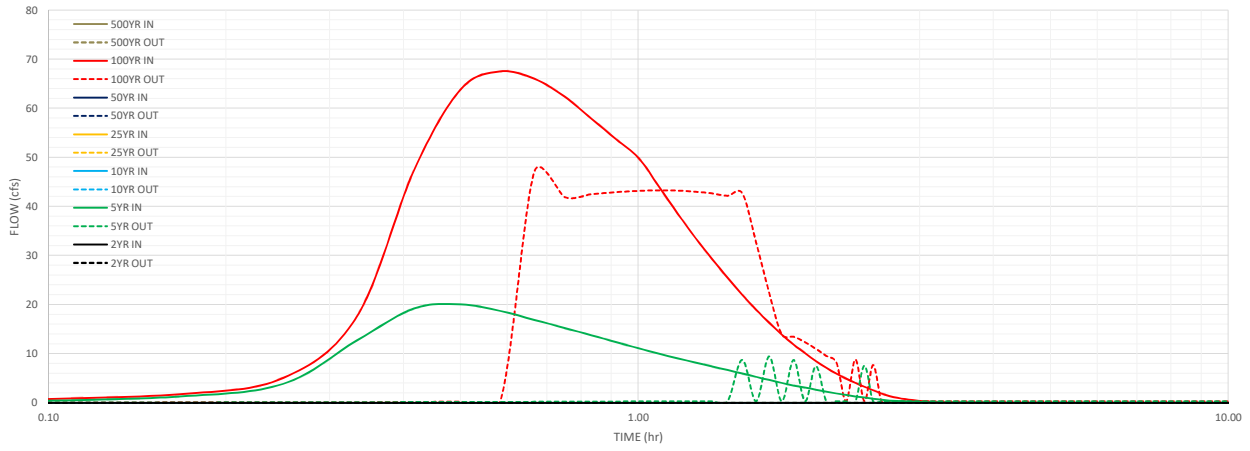


Designer: Chris McFarland

Project: Grandview Reserve Pond G

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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

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Project: Grandview Reserve Pond G

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1. Select QWCV/EURV PCM Type:  
Imports the Stage-Area-Volume-Discharge information from the corresponding PCM worksheet. The selected PCM worksheet must be completed before the import will work.

Extended Detention Basin (EDB)

2. WQCV/EURV Outlet Details

- A) Average Infiltration Rate of WQCV
- B) Depth to Centroid of Underdrain Outlet Orifice from filter media surface
- C) Underdrain Outlet Orifice Area
- D) Number of WQCV Orifice Rows
- E) Vertical Spacing between WQCV Orifice Rows
- F) WQCV Orifice Area (A<sub>o</sub>) per Row
- G) Maximum Stage of WQCV (includes ISD and Trickle Channel Depth)
- H) EURV Orifice Area (A<sub>o</sub>) in Single Row
- I) Maximum Stage of EURV (includes ISD and Trickle Channel Depth)
- J) Discharge Coefficient for all WQCV/EURV Outlet Orifice(s)

Input Parameters		
	User Input	COS DCM
i =	N/A	N/A
y =	N/A	N/A
Underdrain Ao =	N/A	N/A
# WQCV rows =	11	11
Orifice Spacing =	4.0	4.0
WQCV Ao =	0.66	0.66
Max Stage wqcv =	3.60	3.60
EURV Ao =	4.73	4.73
Max Stage EURV =	5.00	5.00
Cd =	0.60	0.60

3. Flood Control Surcharge Basin Geometry (above EURV) - See Figure  
Default Flood Surcharge Geometry inputs represent a continuation of the PCM Geometry in an upward direction without a transition bench.

- A) Length of Basin at Top of EURV
- B) Width of Basin at Top of EURV
- C) Slope at Top of Transition Bench (Bottom of Flood Control Surcharge)
- D) Length of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- E) Width of Basin at Top of Transition Bench (Bottom of Flood Control Surcharge)
- F) Average Side Slopes of Flood Control Surcharge above Transition Bench (Recommend no steeper than 3H:1V slope. Use zero for vertical walls.)

Input Parameters		
	User Input	COS DCM
L <sub>PCM</sub> =	468.4	468.4
W <sub>PCM</sub> =	141.1	141.1
Stage at Top of Bench =	5.10	5.10
L <sub>Bench</sub> =	469.2	469.2
W <sub>Bench</sub> =	141.9	141.9
Z <sub>Surcharge</sub> =	4.00	4.00

User can override default flood surcharge geometry inputs to create a transition bench between the top of the PCM and the Flood Surcharge Volume by entering larger dimensions in C), D), and E). See the Figure to the right.

Bench Slope is 4H:1V in length direction  
Bench Slope is 4H:1V in width direction

4. Tributary Watershed Hydrology

A) Input hydrology data (copy/paste) from model runs

Pre-Development Peak Flow (cfs)						
2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
	17.11				99.16	

B) Adjust "Time Interval" to match hydrograph data

5-yr and 100-yr Hydrology Required (Other Storms are Optional)

Post-Development Storm Inflow Hydrographs (cfs)							
Time (min)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
0:00		0.00				0.00	
0:05		0.41				1.20	
0:10		3.42				4.91	
0:15		10.22				13.16	
0:20		29.97				40.46	
0:25		45.35				109.08	
0:30		46.22				147.68	
0:35		41.85				152.97	
0:40		36.79				145.92	
0:45		32.51				134.77	
0:50		28.57				122.07	
0:55		24.90				110.10	
1:00		21.86				99.42	
1:05		19.69				85.33	
1:10		17.78				73.97	
1:15		15.86				63.12	
1:20		14.00				53.39	
1:25		12.24				44.73	
1:30		10.61				36.81	
1:35		9.00				29.60	
1:40		7.68				24.16	
1:45		6.80				19.99	
1:50		6.25				17.20	
1:55		5.79				15.20	
2:00		4.96				12.77	
2:05		4.07				10.46	
2:10		3.32				8.57	
2:15		2.70				7.04	
2:20		2.18				5.80	
2:25		1.75				4.76	
2:30		1.37				3.85	
2:35		1.07				3.04	
2:40		0.81				2.31	
2:45		0.60				1.65	
2:50		0.43				1.12	
2:55		0.31				0.76	
3:00		0.23				0.51	
3:05		0.17				0.34	
3:10		0.12				0.23	
3:15		0.09				0.16	
3:20		0.07				0.12	
3:25		0.06				0.09	
3:30		0.05				0.07	
3:35		0.04				0.06	
3:40		0.03				0.05	
3:45		0.03				0.04	
3:50		0.02				0.03	
3:55		0.01				0.02	
4:00		0.01				0.01	
4:05		0.01				0.01	
4:10		0.00				0.01	
4:15						0.00	
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5.40								
5.45								
5.50								
5.55								
6.00								



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Preliminary Design Procedure Form: Full Spectrum Detention (FSD) Routing

5. Flood Control Outlet Structure Type

A) Select Flood Control Outlet Structure Type

Overflow Weir/Grate, Outlet Pipe Restriction & Emergency Spillway

6. Overflow Weir (Dropbox) and Grate (Flat or Sloped)  
(Assumes that top of grate is flush with the top of the concrete dropbox)

- A) Overflow Weir Front Edge Height (relative to Stage = 0 ft)
- B) Overflow Weir Front Edge Length (inside edge of dropbox)
- C) Overflow Weir Grate Slope (H:V, enter zero for flat grate)
- D) Horizontal Length of Weir Sides (inside edge of dropbox)
- E) Overflow Grate Open Area % (grate open area / total grate area)
- F) Debris Clogging %
- G) Height of Grate Upper Edge (at back side of dropbox)
- H) Overflow Grate Slope Length (inside edge of dropbox)
- I) Overflow Grate Open Area (without debris)
- J) Overflow Grate Open Area (with debris)

Input Parameters		
	User Input	COS DCM
H <sub>weir front</sub> =	5.00	5.00
L <sub>weir front</sub> =	9.00	7.00
S <sub>weir sides</sub> =	0.00	0.00
Horizontal L <sub>weir sides</sub> =	9.00	7.00
Grate Open Area =	70%	70%
Debris Clogging =	50%	50%
H <sub>grate top</sub> =	5.00	5.00
Slope L <sub>weir sides</sub> =	9.00	7.00
Open Area (No Clogging) =	56.70	34.30
Open Area (Clogged) =	28.35	17.15

7. Outlet Pipe with Flow Restriction Plate

A) Select Type of Outlet Restriction  
(Circular Pipe w/ Restrictor Plate, Circular Orifice or Rectangular Orifice)

Circular Outlet Pipe w/ Restrictor Plate

- B) Depth to Invert of Outlet Pipe (relative to Stage = 0 ft)
- C) Outlet Pipe Diameter
- D) Restrictor Plate Height above Pipe Invert
- E) Half-Central Angle of Restrictor Plate on Pipe
- F) Outlet Orifice Area
- G) Height of Outlet Orifice Centroid above Outlet Pipe Invert
- H) Ratio of Grate Open Area / 100-yr Orifice Area (should be ≥ 4)

Input Parameters		
	User Input	COS DCM
Pipe Invert Depth =	1.50	1.50
Pipe Diameter =	42.00	42.00
Plate Height =	34.00	34.00
Theta =	2.24	2.24
Outlet Ao =	8.34	8.34
Outlet <sub>centroid</sub> =	1.54	1.54
Open Area Ratio =	6.80	4.11

8. Emergency Spillway (Rectangular or Trapezoidal)

- A) Spillway Invert Stage (relative to Stage = 0 ft)
- B) Spillway Crest Length
- C) Spillway End Slopes (H:V)
- D) Freeboard above Maximum Water Surface
- E) Spillway Design Flow Depth
- F) Stage at Top of Freeboard
- G) Basin Area at Top of Freeboard

Input Parameters		
	User Input	COS DCM
H <sub>spillway invert</sub> =	6.70	999.00
L <sub>spillway crest</sub> =	136.00	27.00
S <sub>spillway ends</sub> =	4.00	4.00
Freeboard Depth =	1.00	1.00
Flow Depth <sub>spillway</sub> =	0.50	
Freeboard Top Stage =	8.20	
Max Basin Area =	1.89	

9. Routed Hydrograph Results

		Results based on User Input							
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	1.03	2.73		3.25					11.08
Inflow Hydrograph Volume (ac-ft) =	N/A	N/A		17.1					99.2
Predevelopment Peak Q (cfs) =	N/A	N/A		46.2					153.0
Peak Inflow (cfs) =	0.4	0.7		4.2					101.9
Peak Outflow (cfs) =	N/A	N/A		0.2					1.0
Ratio (Outflow/Predevelopment) =	Orifice Plate	Orifice Plate		Overflow Grate					Outlet Pipe
Structure Controlling Flow =	N/A	N/A		0.0					1.7
Max Velocity through Grate =	39	68		73					62
Time to Drain 97% of Volume (hr) =	41	72		77					72
Time to Drain 99% of Volume (hr) =	3.80	5.00		5.10					6.20
Maximum Ponding Depth (ft) =	1.09	1.52		1.53					1.65
Area at Max Ponding Depth (ac) =	1.03	2.73		2.90					4.65
Maximum Volume Stored (ac-ft) =									
		Results based on COS DCM Inputs							
	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	1.03	2.73		3.25					11.08
Inflow Hydrograph Volume (ac-ft) =	N/A	N/A		17.1					99.2
Predevelopment Peak Q (cfs) =	N/A	N/A		46.2					153.0
Peak Inflow (cfs) =	0.4	0.7		3.6					98.1
Peak Outflow (cfs) =	N/A	N/A		0.2					1.0
Ratio (Outflow/Predevelopment) =	Orifice Plate	Orifice Plate		Overflow Grate					Overflow Grate
Structure Controlling Flow =	N/A	N/A		0.2					2.3
Max Velocity through Grate =	39	68		73					62
Time to Drain 97% of Volume (hr) =	41	72		77					73
Time to Drain 99% of Volume (hr) =	3.80	5.00		5.20					6.40
Maximum Ponding Depth (ft) =	1.09	1.52		1.54					1.68
Area at Max Ponding Depth (ac) =	1.03	2.73		3.05					4.98
Maximum Volume Stored (ac-ft) =									

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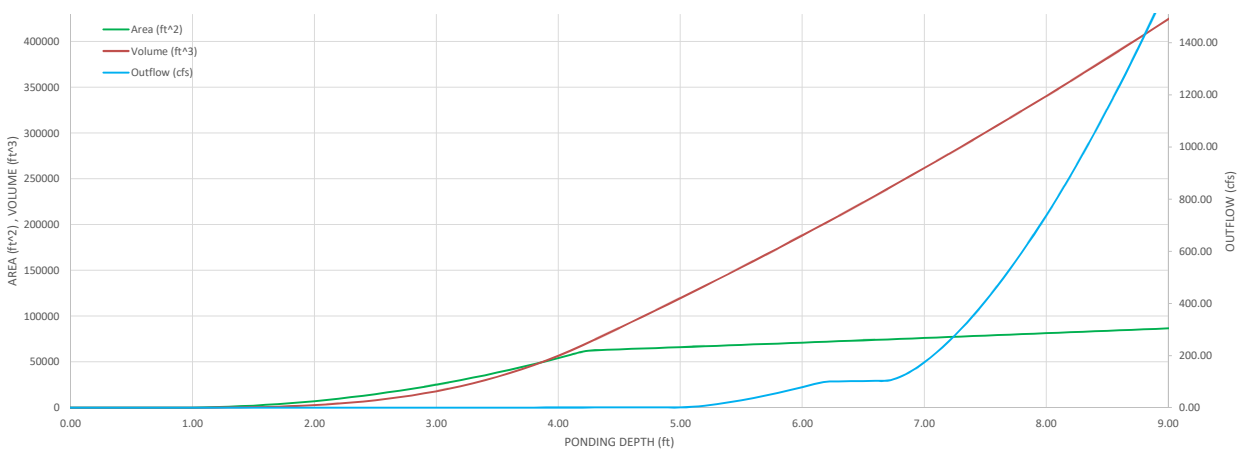
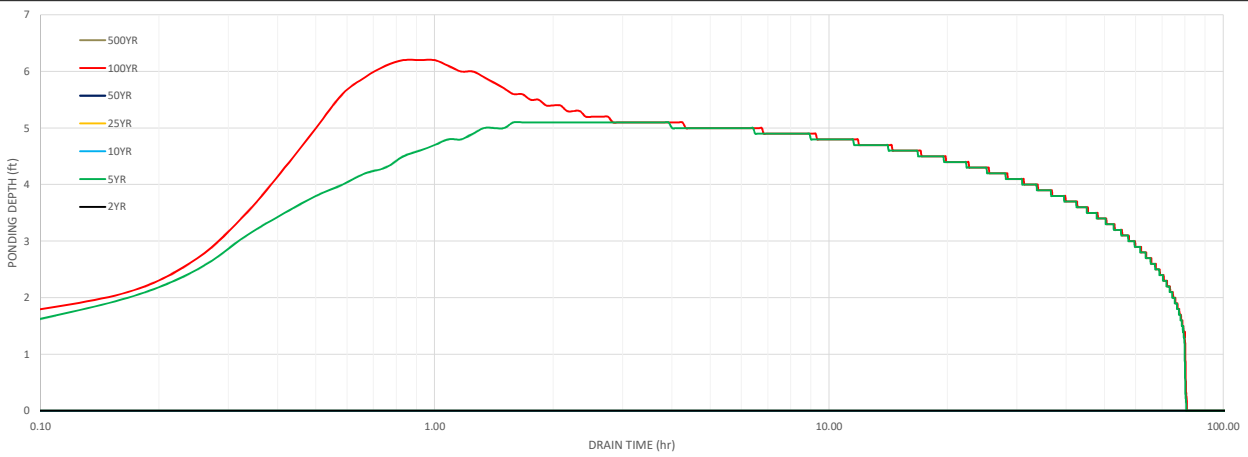
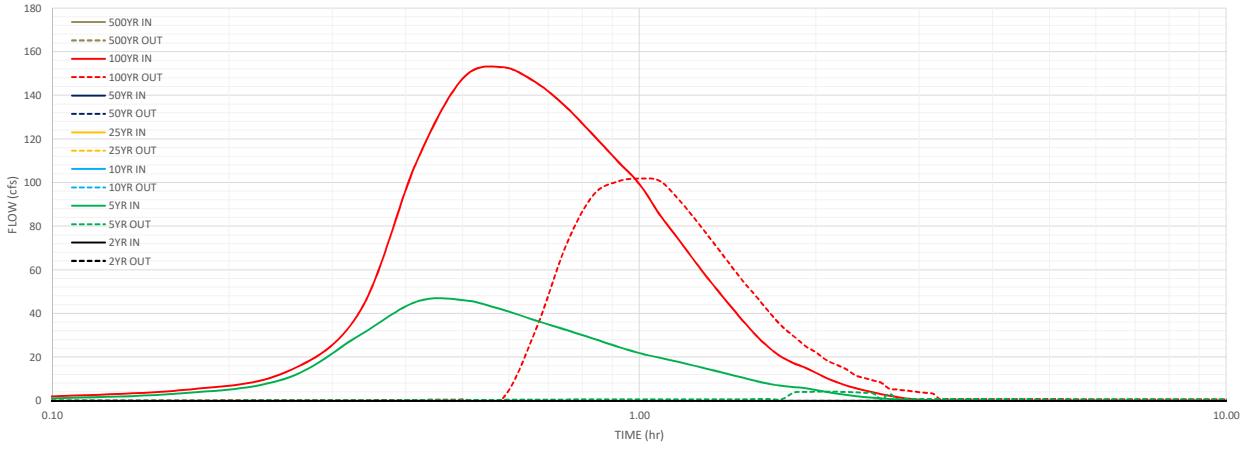


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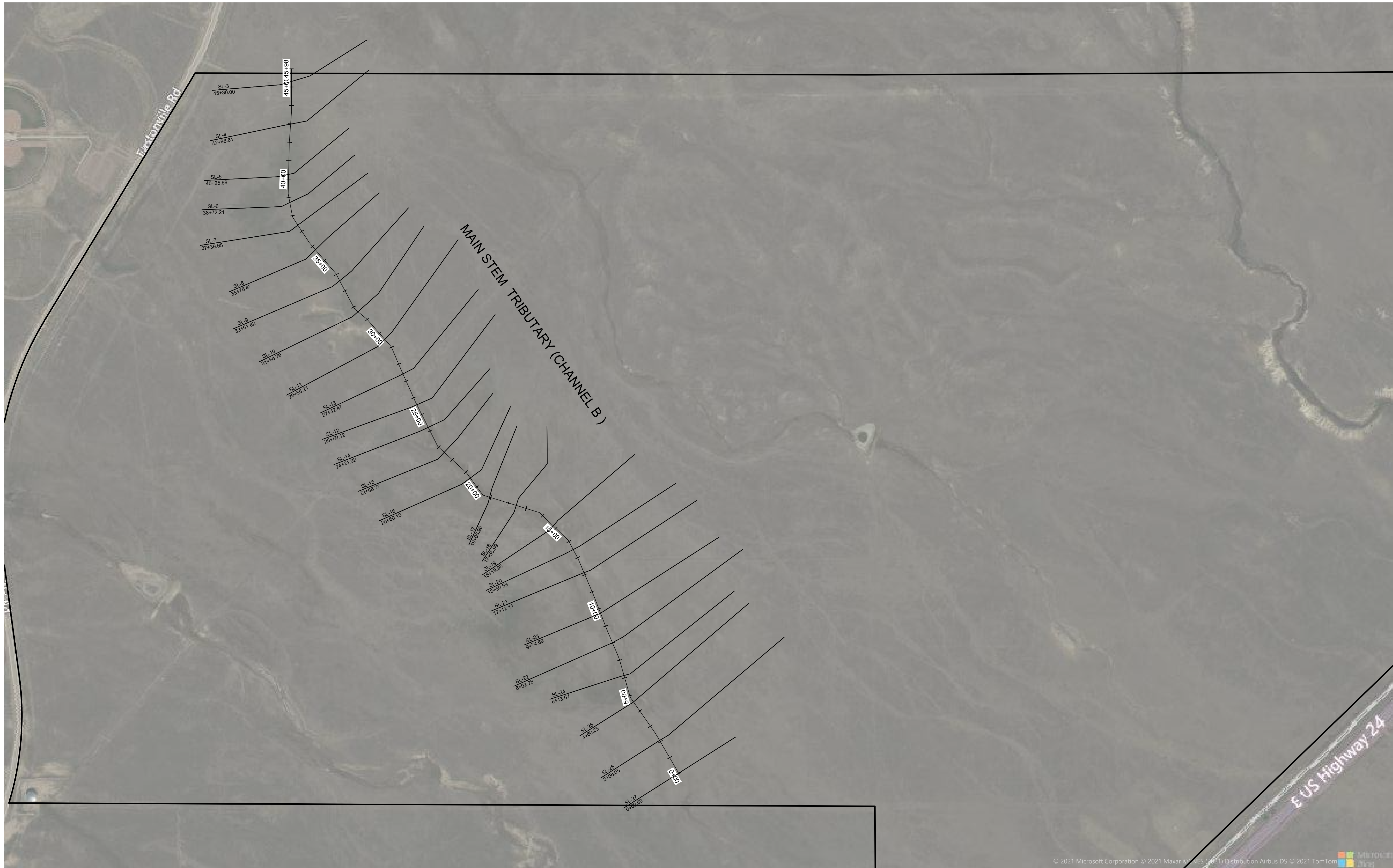


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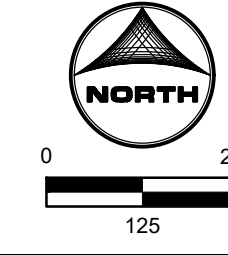




## Appendix E



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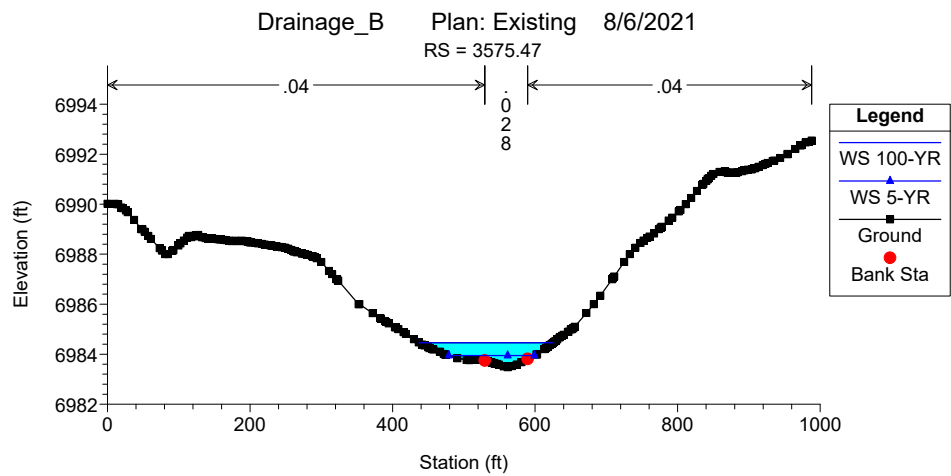
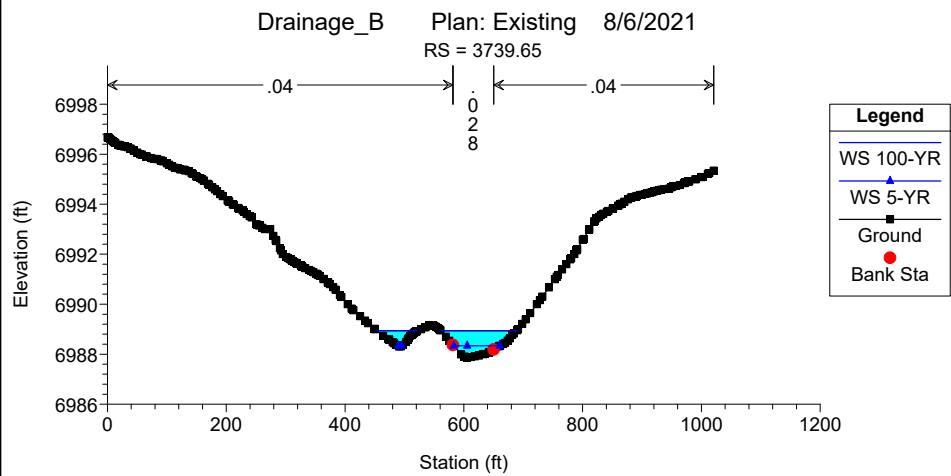
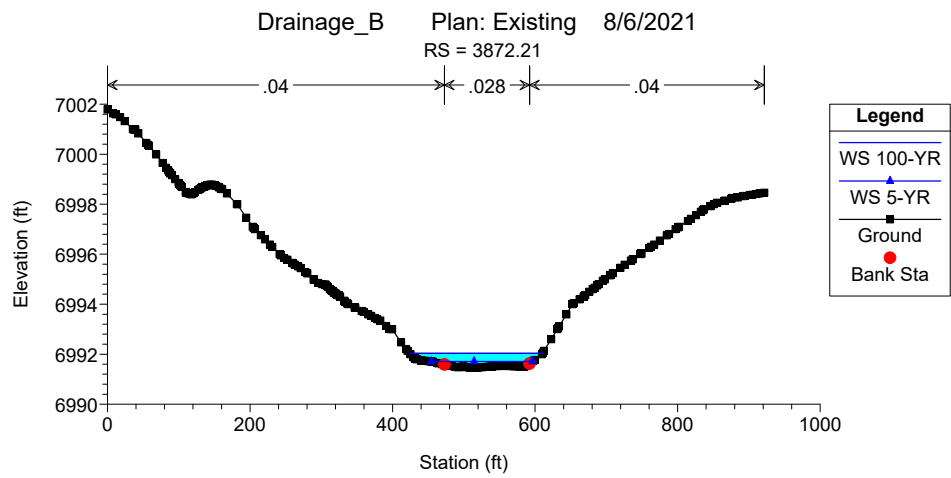
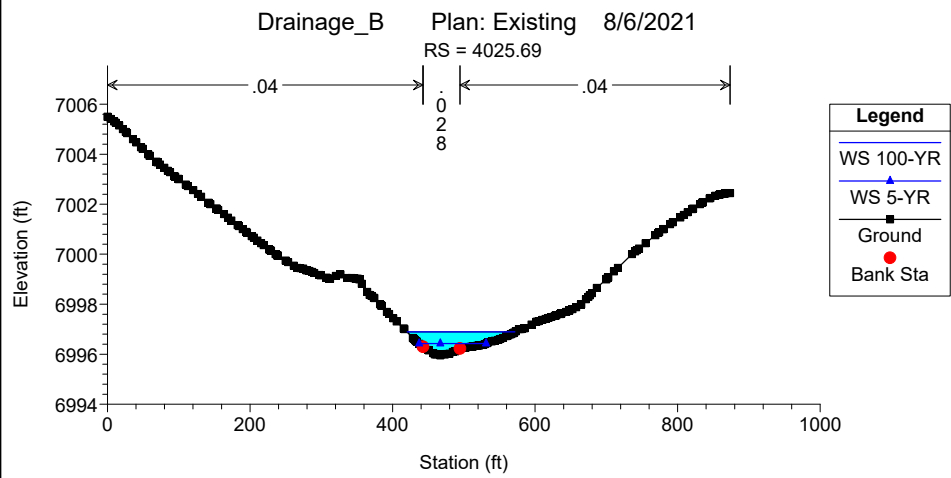
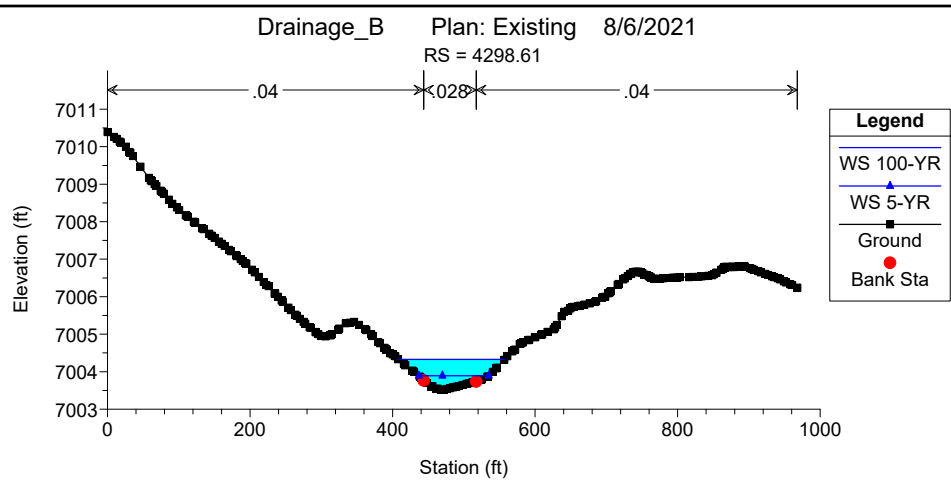
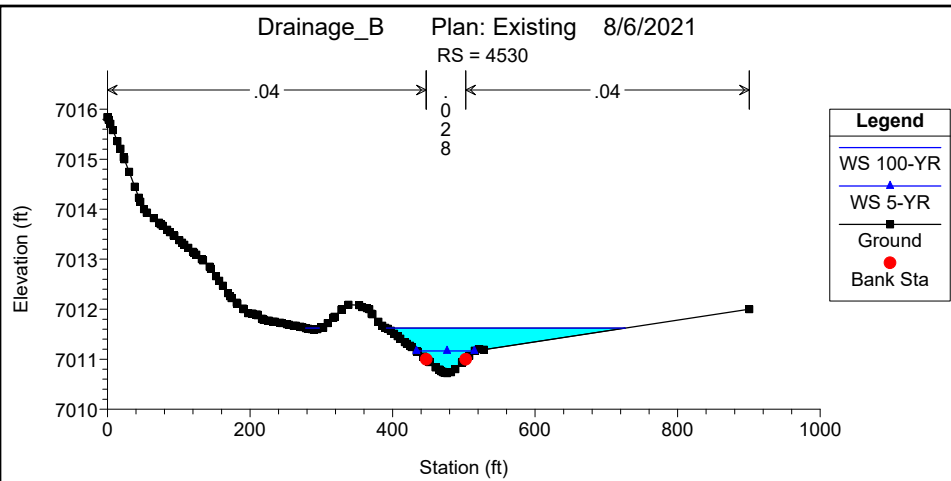


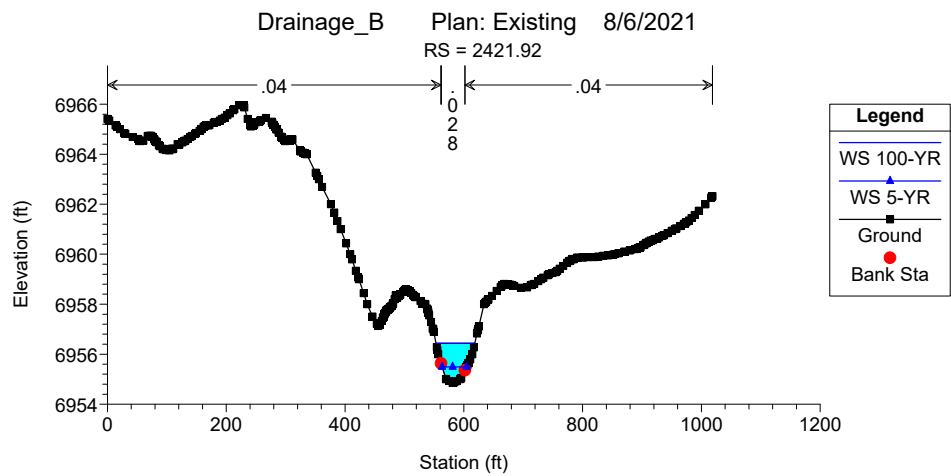
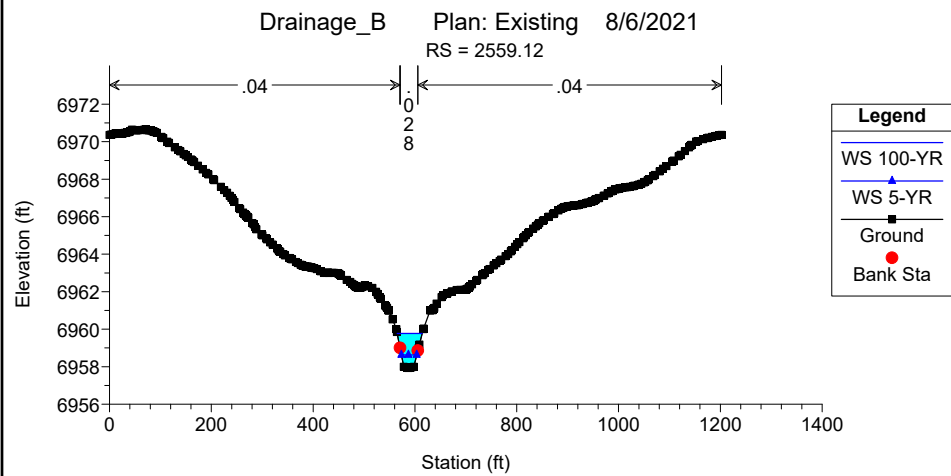
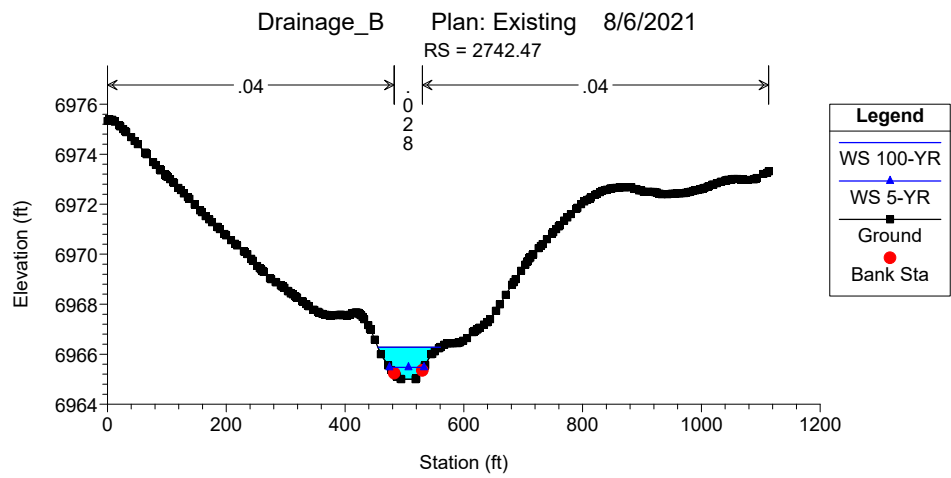
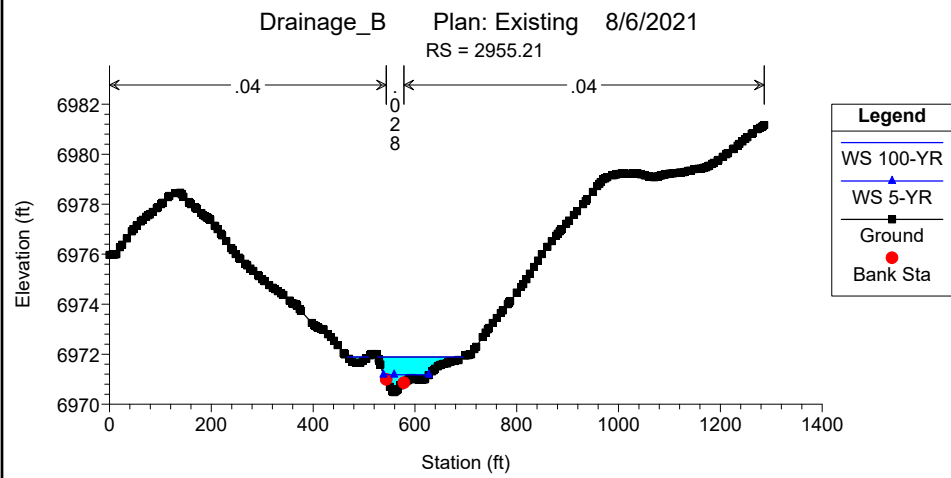
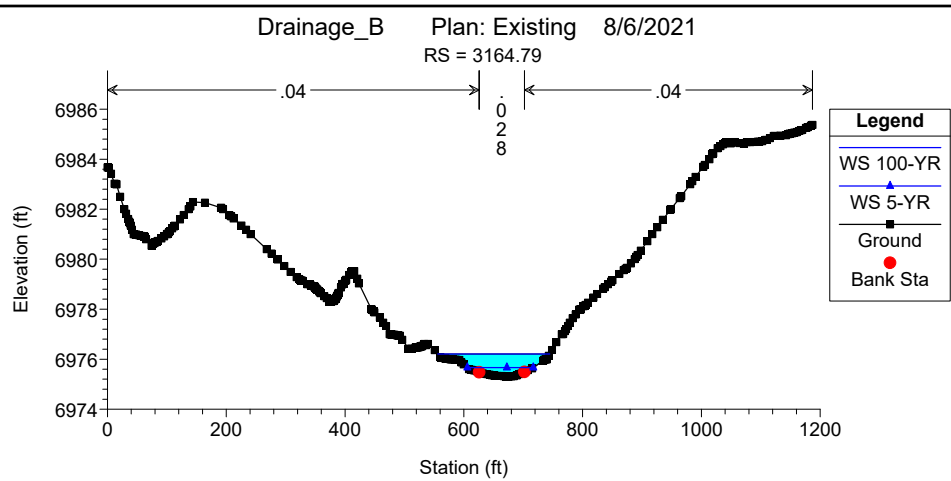
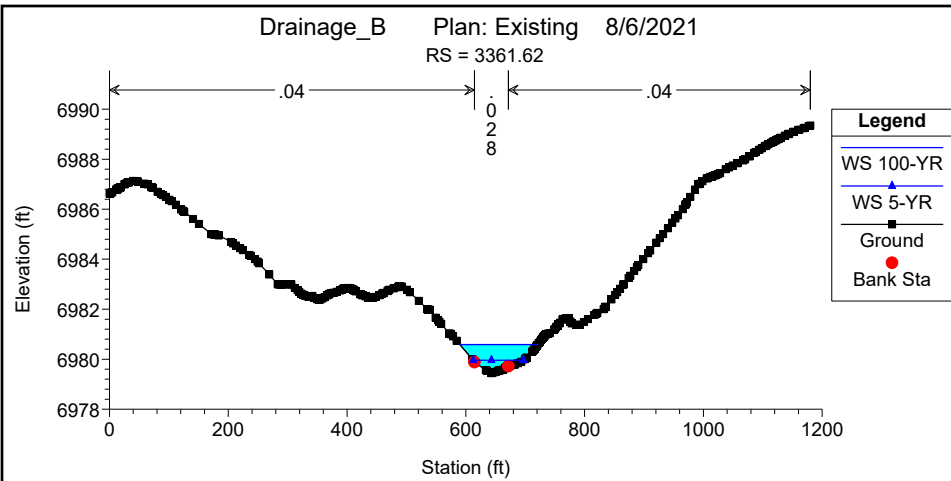
Job No.:	201662.03
Prepared By:	TBI
Date:	8/11/2021

EXISTING MODEL  
CROSS SECTIONS

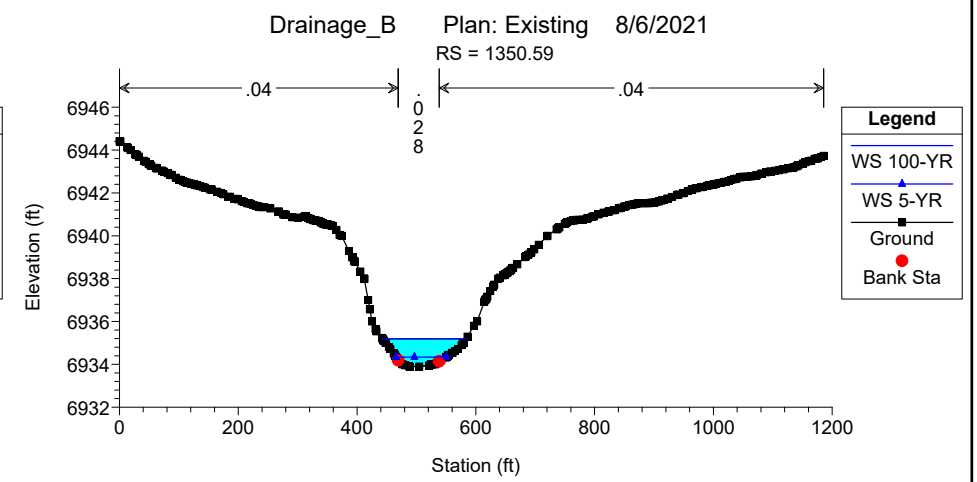
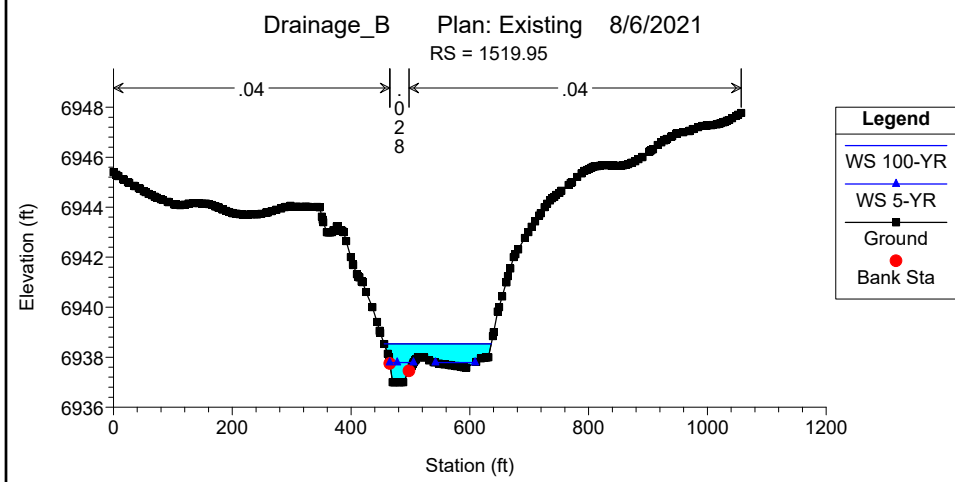
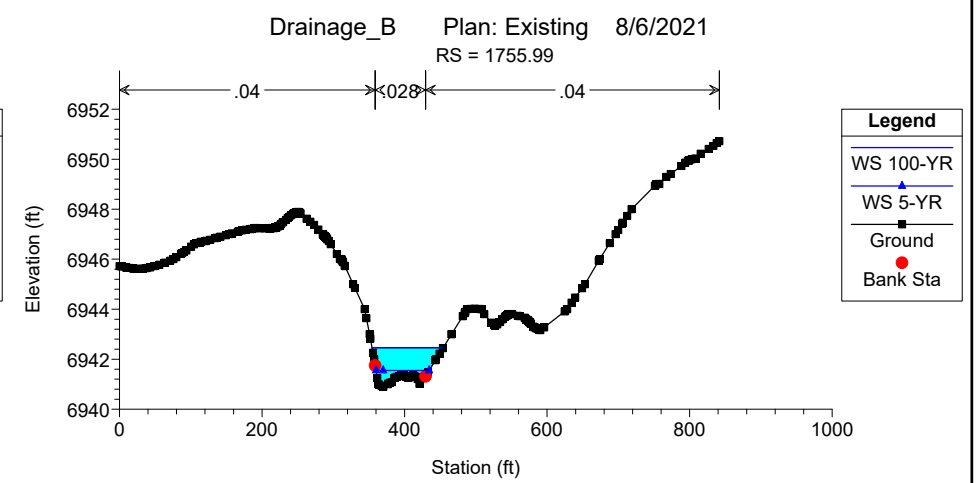
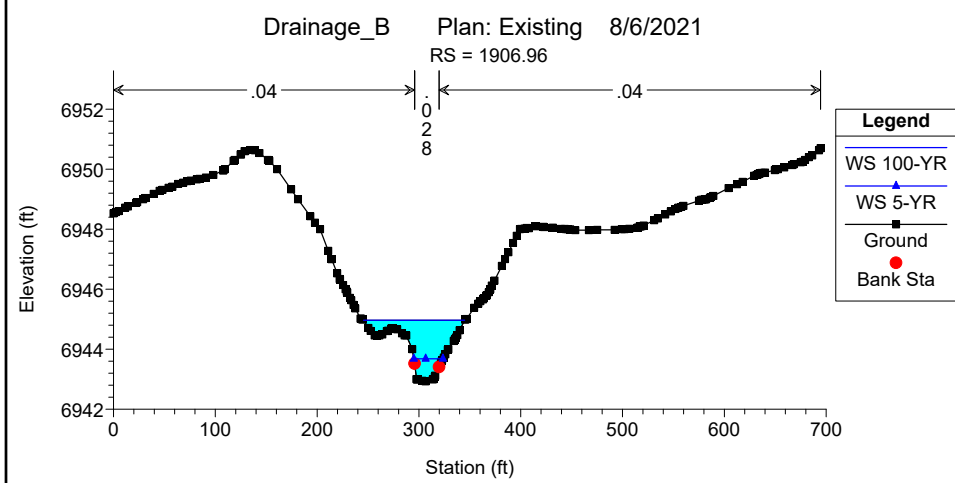
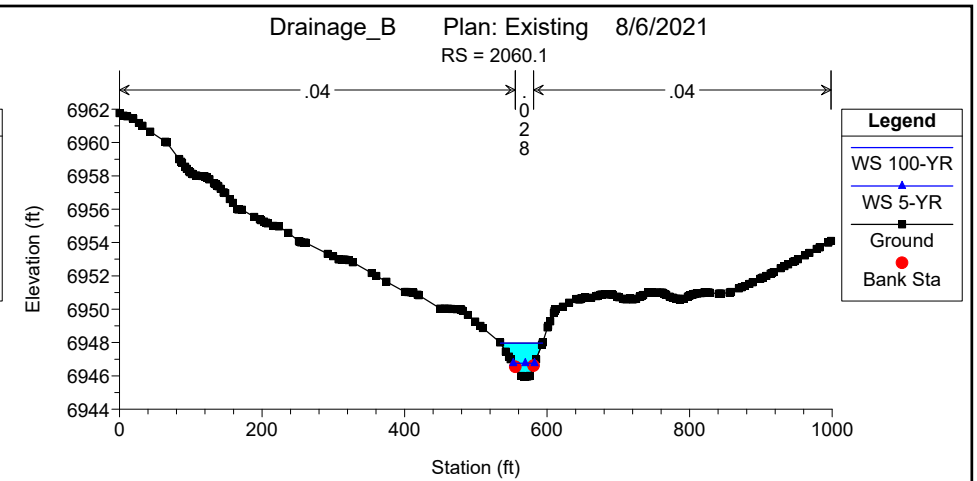
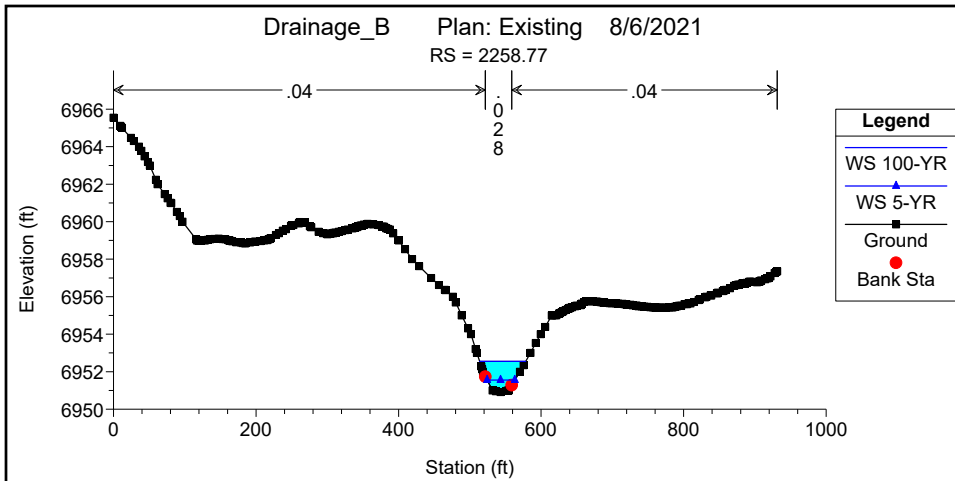
HEC-RAS Plan: Existing River: Drainage B Reach: Alignment - (2)

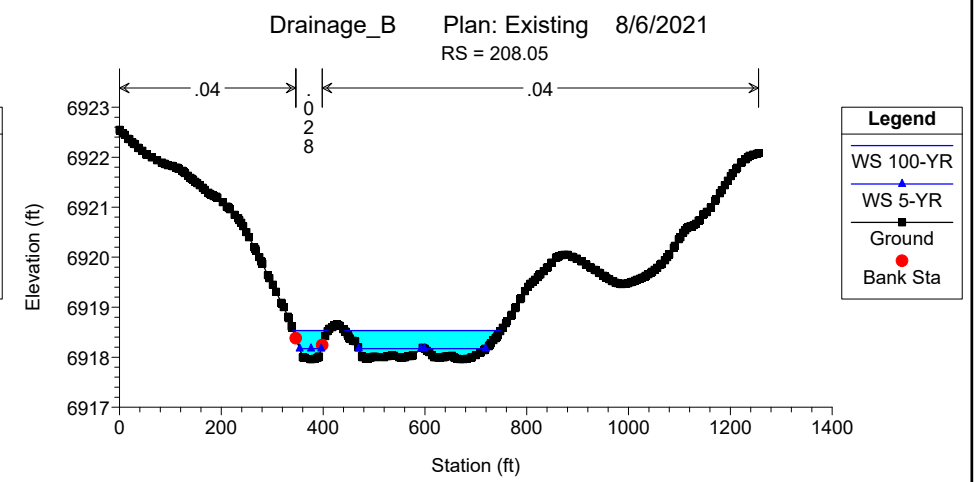
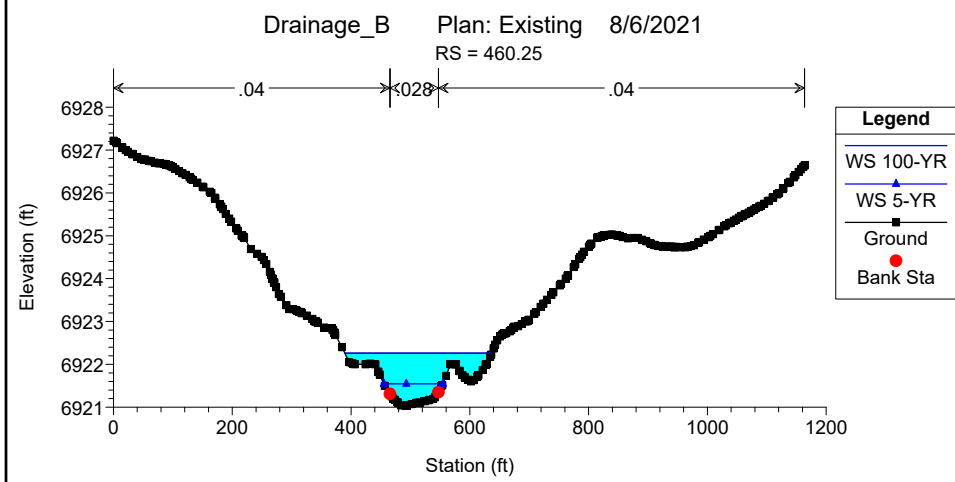
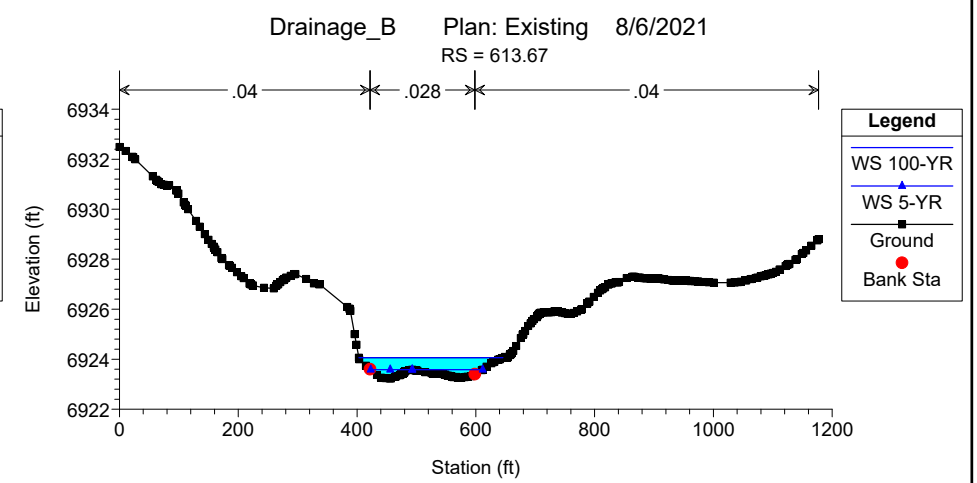
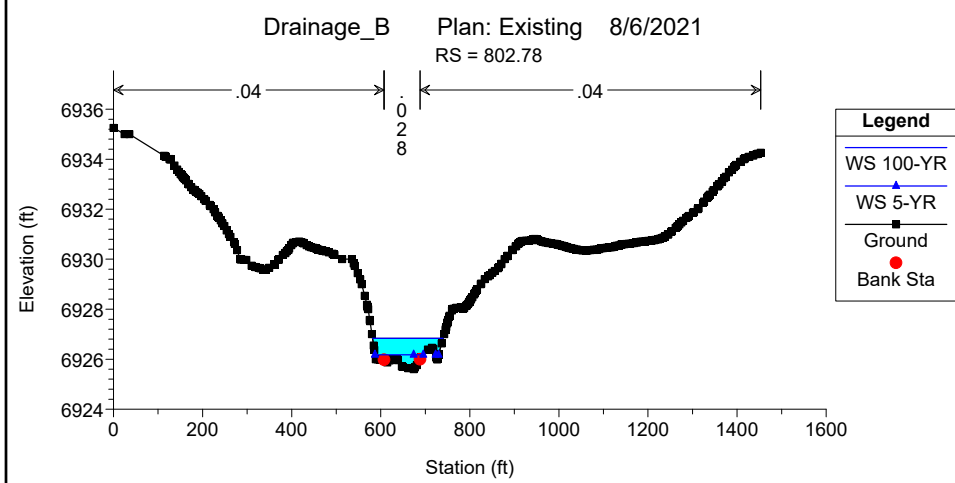
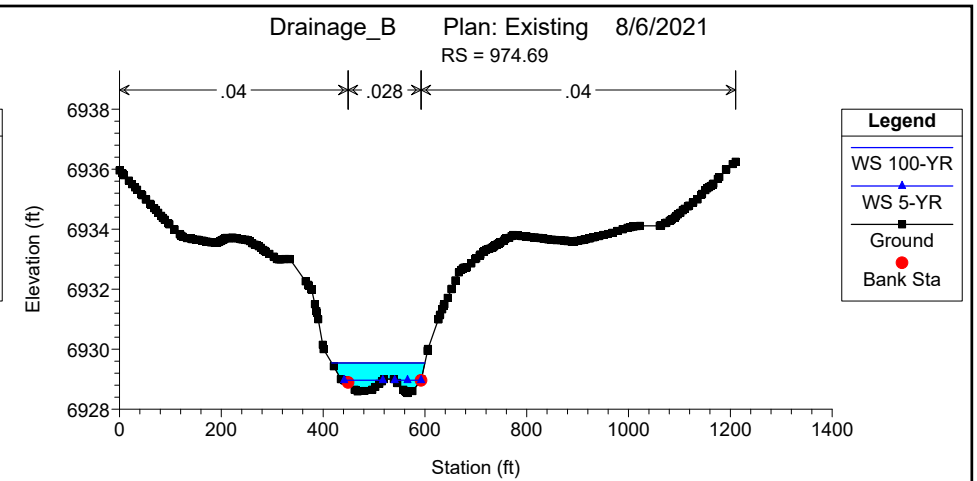
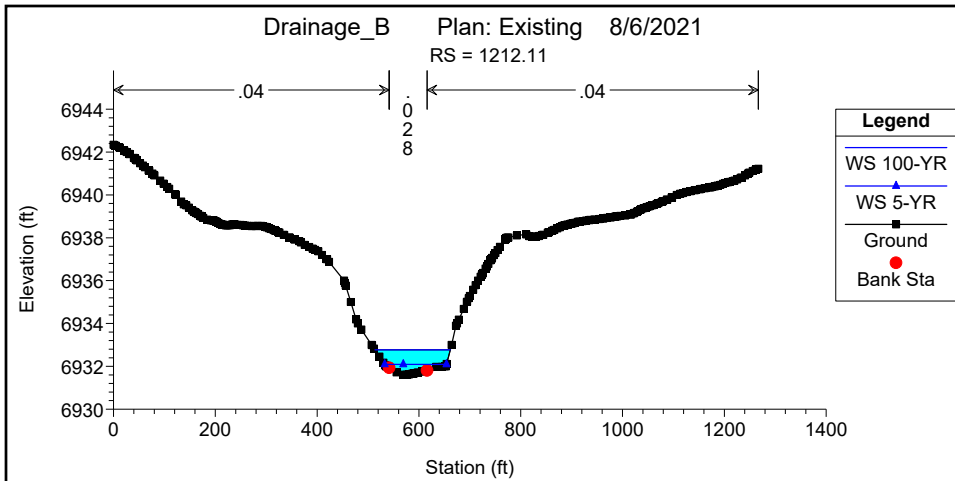
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Froude # Chl	Shear LOB (lb/sq ft)	Shear Chan (lb/sq ft)	Shear ROB (lb/sq ft)	Power LOB (lb/ft s)	Power Chan (lb/ft s)	Power ROB (lb/ft s)
Alignment - (2)	4530	100-YR	280.00	7010.72	7011.62	7011.62	7011.80	0.008420	4.14	115.80	0.82	0.12	0.41	0.13	0.18	1.71	0.17
Alignment - (2)	4530	5-YR	59.00	7010.72	7011.16	7011.16	7011.31	0.015603	3.15	20.24	0.97	0.08	0.32	0.08	0.07	1.00	0.07
Alignment - (2)	4298.61	100-YR	280.00	7003.52	7004.33	7004.33	7004.60	0.011446	4.51	75.98	0.95	0.19	0.51	0.25	0.32	2.29	0.50
Alignment - (2)	4298.61	5-YR	59.00	7003.52	7003.89	7003.89	7004.02	0.016302	2.85	22.00	0.96	0.06	0.28	0.09	0.04	0.79	0.08
Alignment - (2)	4025.69	100-YR	280.00	6995.96	6996.89	6996.89	6997.16	0.010606	4.76	80.74	0.93	0.21	0.54	0.27	0.37	2.57	0.57
Alignment - (2)	4025.69	5-YR	59.00	6995.96	6996.43	6996.43	6996.56	0.013192	3.02	22.56	0.90	0.06	0.29	0.09	0.04	0.87	0.09
Alignment - (2)	3872.21	100-YR	280.00	6991.45	6992.03	6992.03	6992.25	0.013013	3.94	80.99	0.96	0.24	0.43	0.18	0.45	1.68	0.27
Alignment - (2)	3872.21	5-YR	59.00	6991.45	6991.71	6991.71	6991.80	0.018167	2.44	25.07	0.96	0.07	0.23	0.05	0.05	0.55	0.03
Alignment - (2)	3739.65	100-YR	390.70	6987.86	6988.94	6988.94	6989.24	0.009468	4.89	107.95	0.90	0.19	0.55	0.25	0.31	2.67	0.52
Alignment - (2)	3739.65	5-YR	68.95	6987.86	6988.33	6988.33	6988.48	0.015568	3.13	22.67	0.97	0.02	0.32	0.07	0.01	0.99	0.05
Alignment - (2)	3575.47	100-YR	390.70	6983.48	6984.46	6984.46	6984.75	0.011370	5.06	107.93	0.97	0.34	0.60	0.15	0.83	3.04	0.50
Alignment - (2)	3575.47	5-YR	68.95	6983.48	6983.94	6983.94	6984.07	0.014396	3.04	27.39	0.93	0.12	0.30	0.06	0.14	0.90	0.05
Alignment - (2)	3361.62	100-YR	390.70	6979.44	6980.59	6980.59	6980.96	0.010660	5.41	92.08	0.96	0.23	0.65	0.37	0.43	3.54	0.97
Alignment - (2)	3361.62	5-YR	68.95	6979.44	6979.96	6979.96	6980.11	0.014781	3.22	23.64	0.96	0.04	0.33	0.13	0.02	1.05	0.15
Alignment - (2)	3164.79	100-YR	390.70	6975.30	6976.21	6976.21	6976.50	0.010031	4.74	107.61	0.91	0.23	0.53	0.27	0.43	2.50	0.56
Alignment - (2)	3164.79	5-YR	68.95	6975.30	6975.66	6975.66	6975.79	0.015475	2.92	25.80	0.95	0.10	0.28	0.08	0.10	0.83	0.08
Alignment - (2)	2955.21	100-YR	390.70	6970.48	6971.89	6971.89	6972.19	0.008109	5.43	119.58	0.87	0.13	0.61	0.27	0.21	3.33	0.61
Alignment - (2)	2955.21	5-YR	68.95	6970.48	6971.18	6971.18	6971.33	0.010373	3.40	26.43	0.85	0.09	0.32	0.11	0.09	1.10	0.13
Alignment - (2)	2742.47	100-YR	390.70	6965.00	6966.28	6966.28	6966.73	0.009026	5.74	84.97	0.92	0.33	0.68	0.21	0.82	3.93	0.38
Alignment - (2)	2742.47	5-YR	68.95	6965.00	6965.47	6965.47	6965.66	0.014494	3.51	20.49	0.97	0.12	0.37	0.05	0.13	1.29	0.04
Alignment - (2)	2559.12	100-YR	390.70	6957.93	6959.77	6959.77	6960.47	0.008921	6.81	61.70	0.95	0.21	0.88	0.25	0.40	6.00	0.52
Alignment - (2)	2559.12	5-YR	68.95	6957.93	6958.63	6958.63	6958.90	0.014366	4.22	16.34	1.01		0.48			2.05	
Alignment - (2)	2421.92	100-YR	390.70	6954.85	6956.44	6956.44	6957.02	0.009346	6.37	70.02	0.95	0.26	0.81	0.37	0.54	5.15	0.99
Alignment - (2)	2421.92	5-YR	68.95	6954.85	6955.49	6955.49	6955.72	0.014603	3.85	18.05	0.99		0.42	0.06		1.63	0.04
Alignment - (2)	2258.77	100-YR	390.70	6950.91	6952.55	6952.55	6953.14	0.009029	6.48	70.14	0.95	0.25	0.82	0.36	0.51	5.32	0.95
Alignment - (2)	2258.77	5-YR	68.95	6950.91	6951.55	6951.55	6951.79	0.013876	3.94	17.90	0.98		0.43	0.12		1.71	0.13
Alignment - (2)	2060.1	100-YR	390.70	6945.95	6947.97	6947.97	6948.64	0.007977	7.08	69.96	0.92	0.35	0.91	0.34	0.94	6.44	0.85
Alignment - (2)	2060.1	5-YR	68.95	6945.95	6946.75	6946.75	6947.05	0.012983	4.37	16.11	0.98	0.09	0.50	0.06	0.08	2.18	0.04
Alignment - (2)	1906.96	100-YR	390.70	6942.93	6944.96	6944.96	6945.50	0.006399	6.55	88.19	0.83	0.18	0.77	0.31	0.31	5.02	0.78
Alignment - (2)	1906.96	5-YR	68.95	6942.93	6943.68	6943.68	6943.98	0.012807	4.45	15.91	0.98	0.06	0.51	0.10	0.05	2.27	0.11
Alignment - (2)	1755.99	100-YR	597.69	6940.90	6942.46	6942.46	6943.03	0.010131	6.24	105.07	0.98	0.21	0.80	0.36	0.39	4.99	0.93
Alignment - (2)	1755.99	5-YR	86.00	6940.90	6941.55	6941.55	6941.73	0.016031	3.40	25.67	1.00		0.36	0.12		1.23	0.13
Alignment - (2)	1519.95	100-YR	597.69	6936.99	6938.53	6938.53	6938.92	0.009285	6.44	150.76	0.95	0.18	0.82	0.43	0.30	5.28	1.24
Alignment - (2)	1519.95	5-YR	86.00	6936.99	6937.78	6937.78	6937.98	0.008294	3.68	29.86	0.80		0.34	0.06		1.27	0.05
Alignment - (2)	1350.59	100-YR	597.69	6933.90	6935.19	6935.19	6935.65	0.009350	5.88	125.14	0.94	0.28	0.72	0.36	0.61	4.20	0.92
Alignment - (2)	1350.59	5-YR	86.00	6933.90	6934.33	6934.33	6934.50	0.014571	3.30	27.04	0.96	0.07	0.34	0.09	0.05	1.11	0.08
Alignment - (2)	1212.11	100-YR	597.69	6931.60	6932.77	6932.77	6933.20	0.011126	5.81	125.93	1.00	0.33	0.73	0.52	0.79	4.26	1.66
Alignment - (2)	1212.11	5-YR	86.00	6931.60	6932.09	6932.09	6932.21	0.010257	2.82	34.67	0.81	0.06	0.24	0.09	0.05	0.68	0.10
Alignment - (2)	974.69	100-YR	597.69	6928.54	6929.54	6929.54	6929.91	0.012309	5.01	127.84	1.00	0.31	0.60	0.23	0.71	3.02	0.41
Alignment - (2)	974.69	5-YR	86.00	6928.54	6928.96	6928.96	6929.09	0.017451	2.81	30.71	0.98	0.02	0.28		0.01	0.78	
Alignment - (2)	802.78	100-YR	597.69	6925.60	6926.84	6926.84	6927.25	0.011014	5.65	129.11	0.99	0.50	0.70	0.36	1.60	3.97	0.93
Alignment - (2)	802.78	5-YR	86.00	6925.60	6926.18	6926.18	6926.29	0.010327	2.74	34.35	0.80	0.12	0.23	0.06	0.15	0.64	0.04
Alignment - (2)	613.67	100-YR	597.69	6923.23	6924.06	6924.06	6924.39	0.013105	4.68	139.34	1.00	0.22	0.55	0.26	0.38	2.60	0.51
Alignment - (2)	613.67	5-YR	86.00	6923.23	6923.58	6923.58	6923.67	0.019440	2.49	35.29	0.99		0.24	0.11		0.59	0.11
Alignment - (2)	460.25	100-YR	597.69	6921.03	6922.26	6922.26	6922.59	0.007909	5.11	160.82	0.85	0.18	0.56	0.23	0.30	2.85	0.45
Alignment - (2)	460.25	5-YR	86.00	6921.03	6921.55	6921.46	6921.64	0.007343	2.52	35.52	0.69	0.06	0.19	0.04	0.04	0.48	0.03
Alignment - (2)	208.05	100-YR	597.69	6917.96	6918.53	6918.53	6918.76	0.025003	5.16	163.15	1.31	0.12	0.75	0.68	0.13	3.88	2.30
Alignment - (2)	208.05	5-YR	86.00	6917.96	6918.17	6918.17	6918.24	0.031904	2.87	42.68	1.24		0.33	0.29		0.95	0.54
Alignment - (2)	2.6	100-YR	597.42	6912.97	6914.97	6914.97	6915.51	0.010321	7.88	148.43	1.04	0.32	1.14	0.40	0.79	8.97	1.12
Alignment - (2)	2.6	5-YR	85.99	6912.97	6913.98	6913.98	6914.31	0.011008	4.72	20.88	0.94	0.16	0.54	0.16	0.25	2.54	0.24





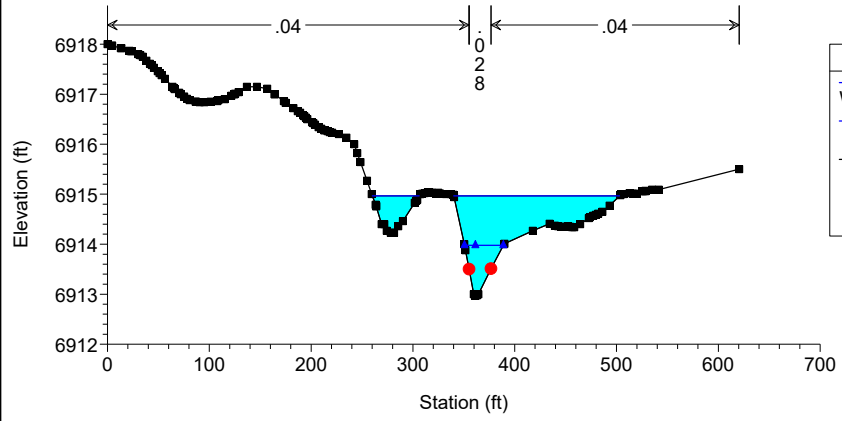






Drainage\_B Plan: Existing 8/6/2021

RS = 2.6



**Legend**

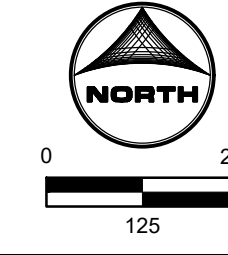
- WS 100-YR
- WS 5-YR
- Ground
- Bank Sta



## Appendix F



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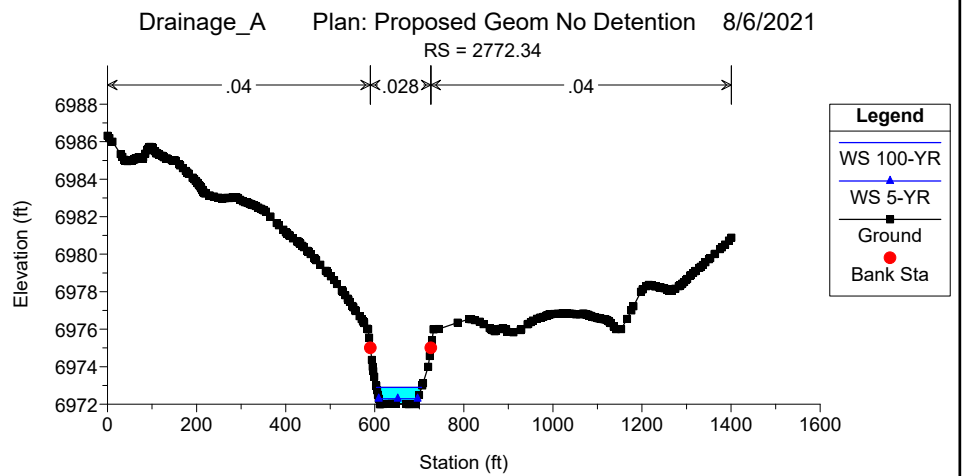
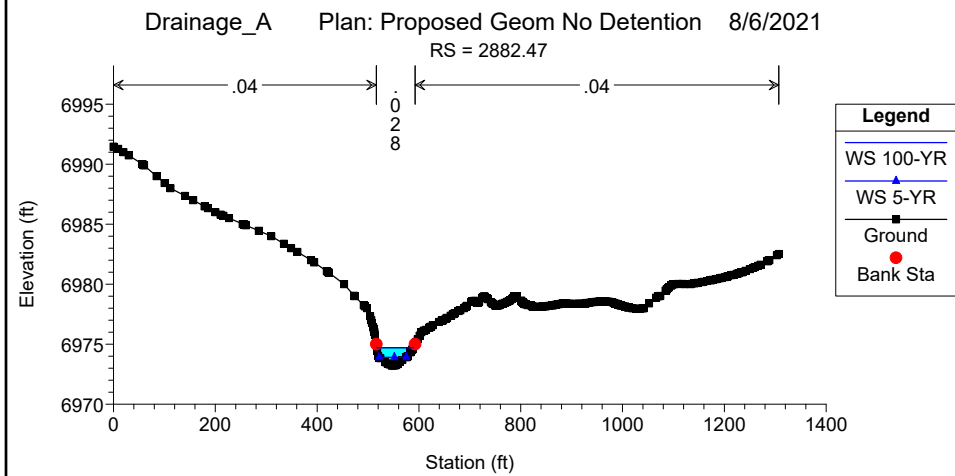
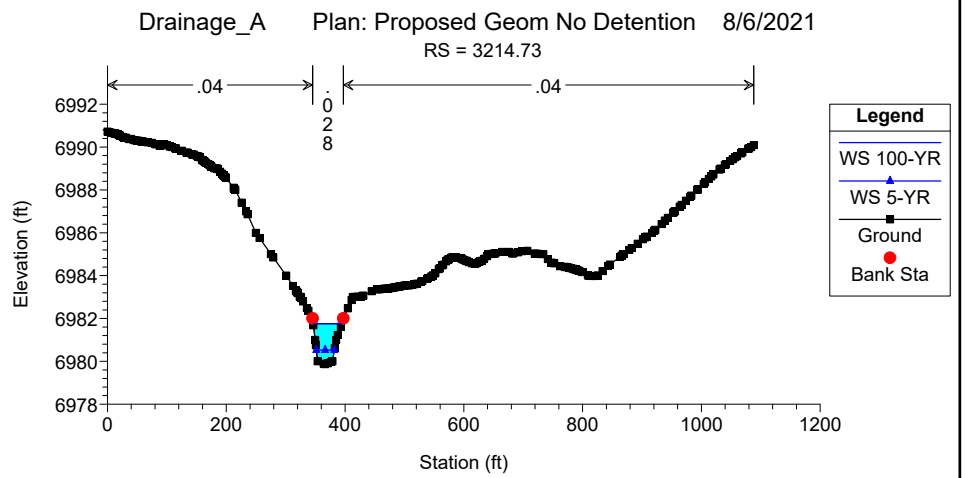
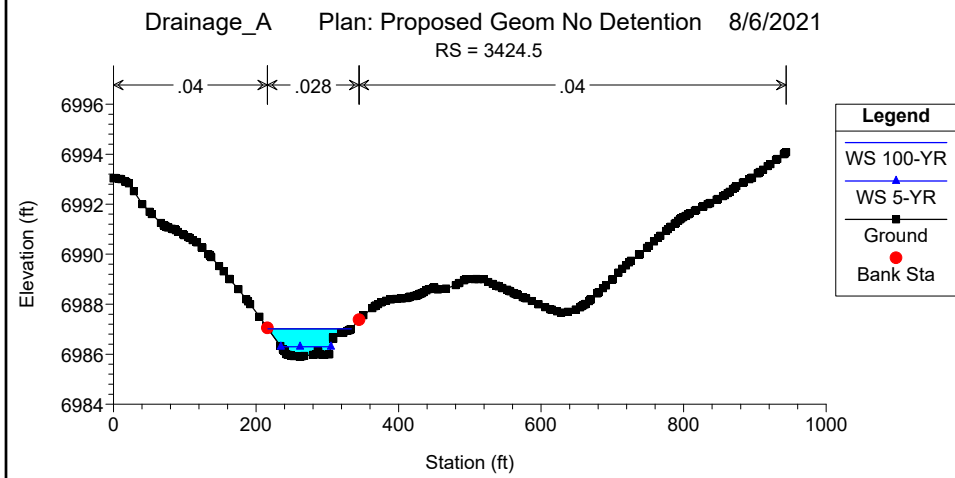
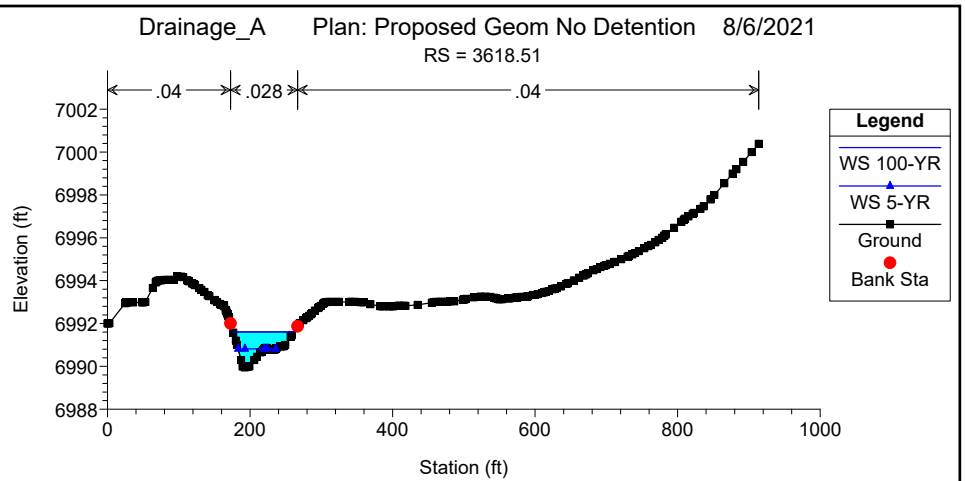
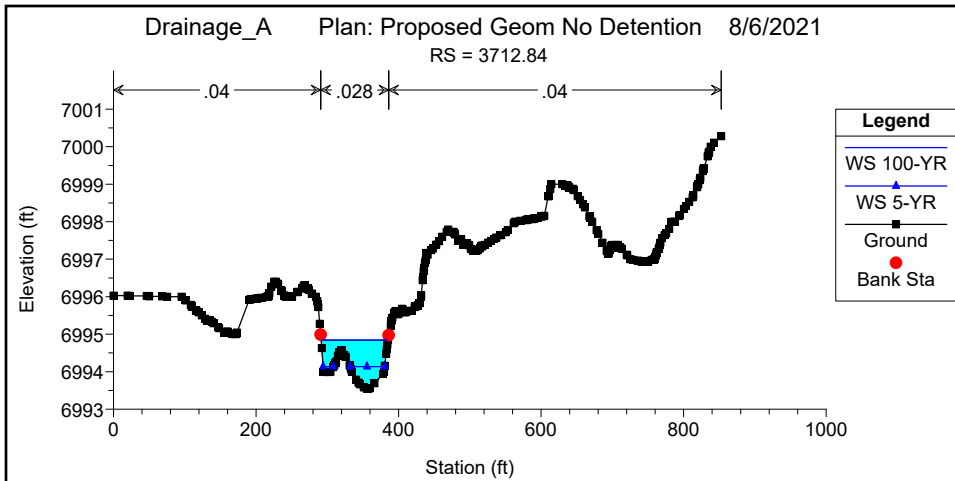


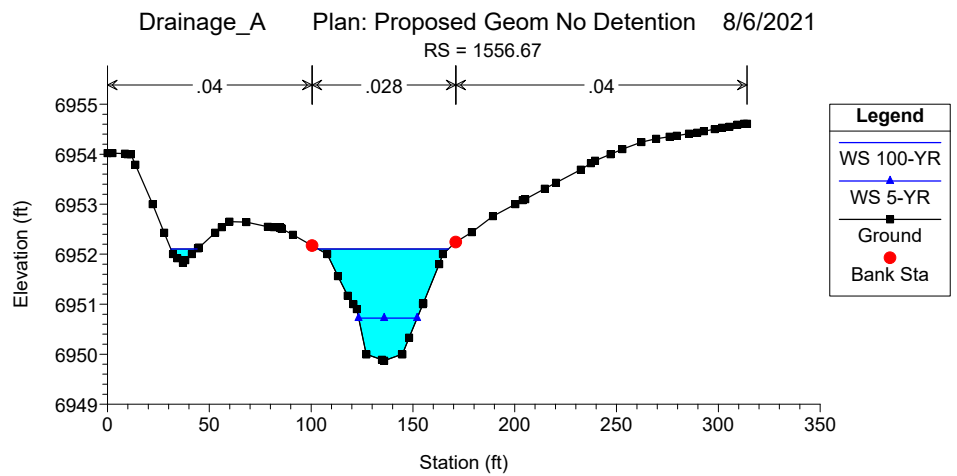
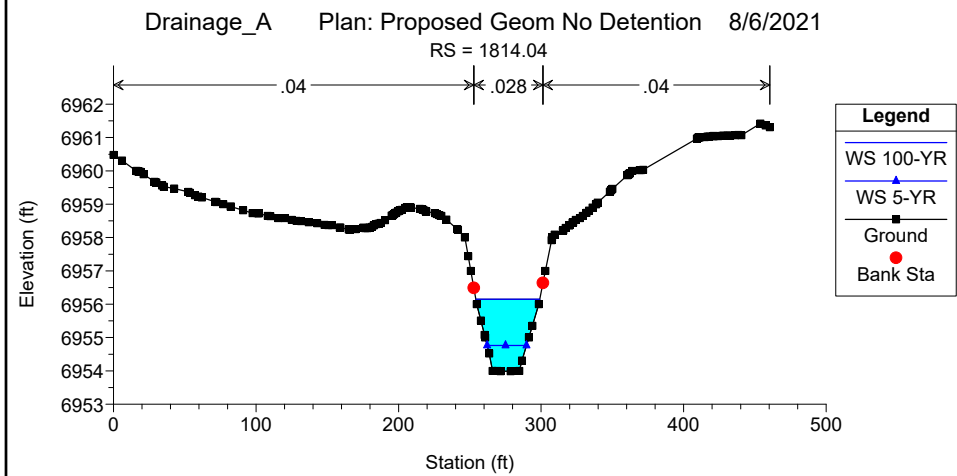
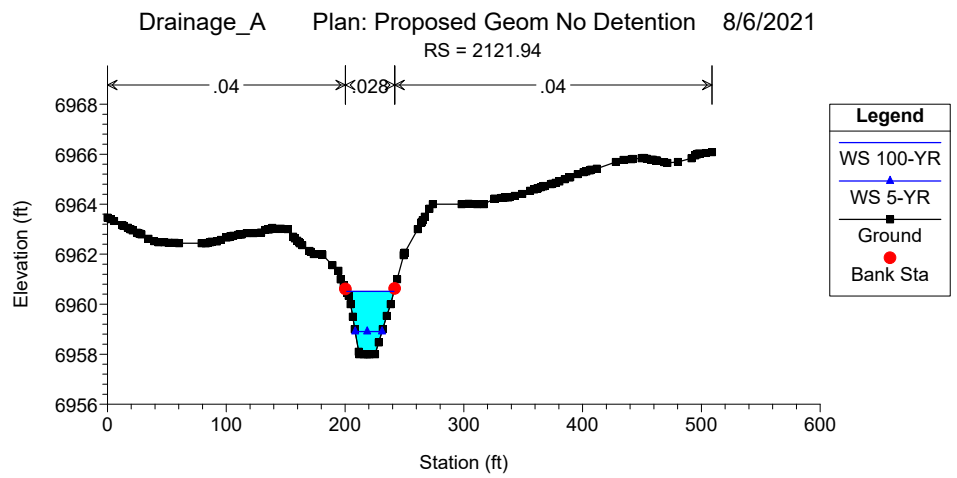
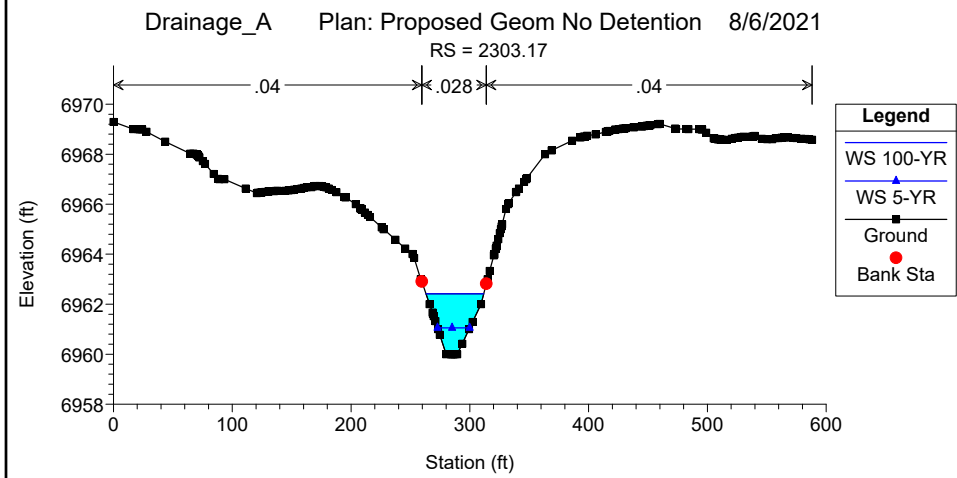
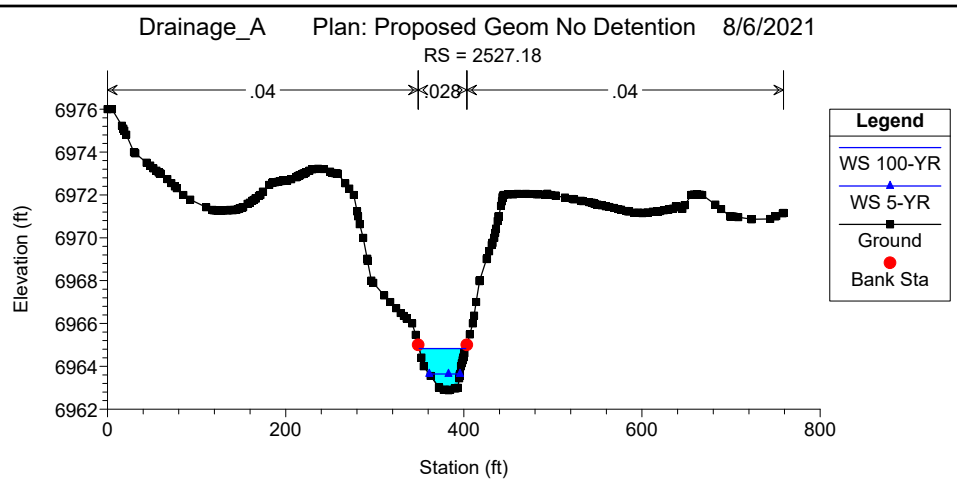
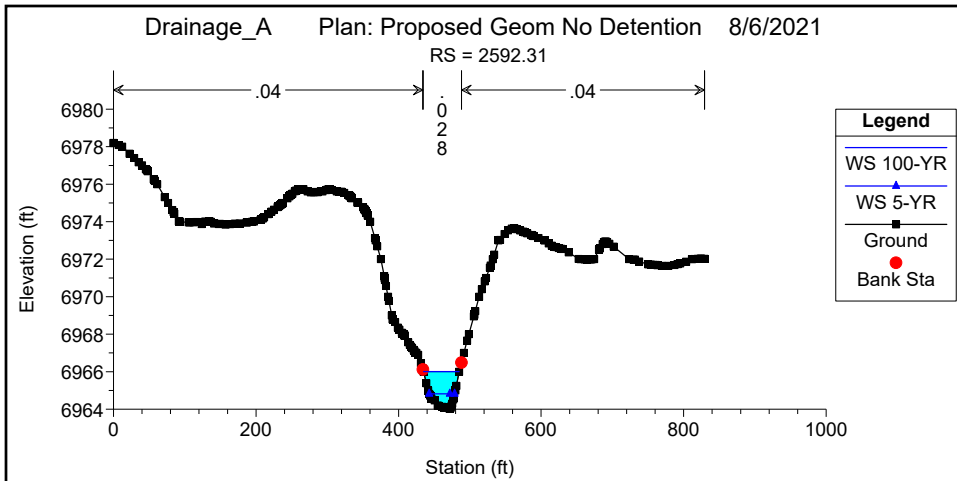
Job No.:	201662.02
Prepared By:	TBI
Date:	8/11/2021

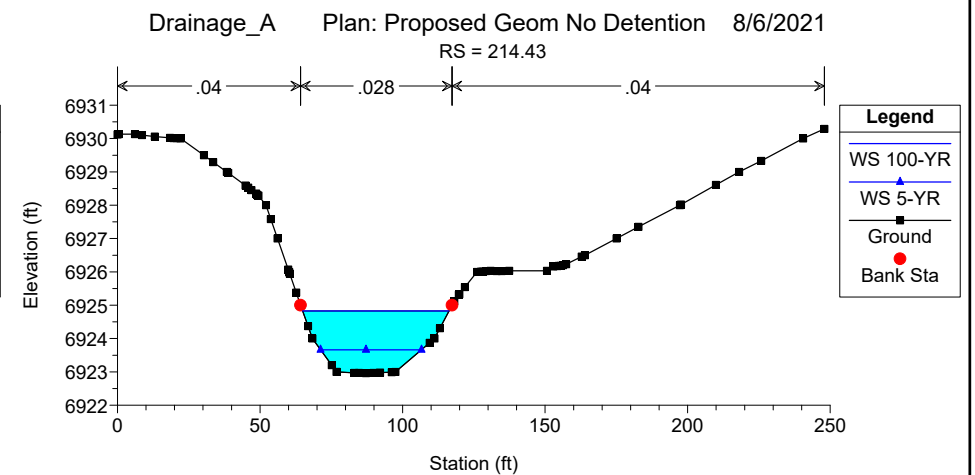
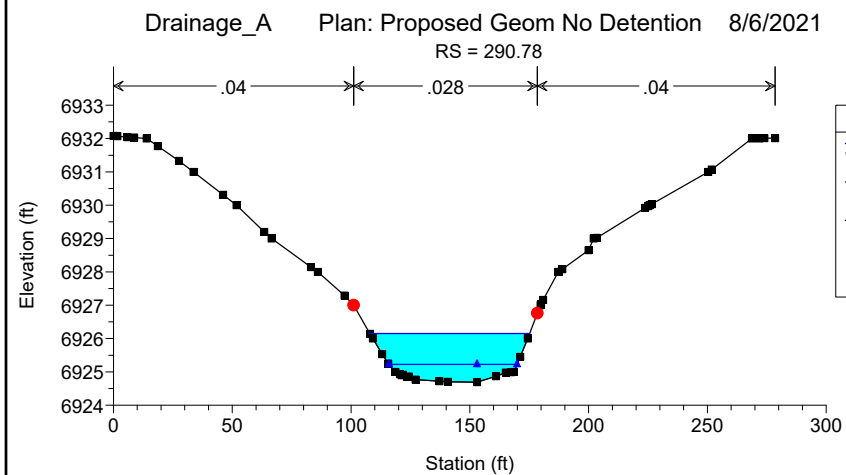
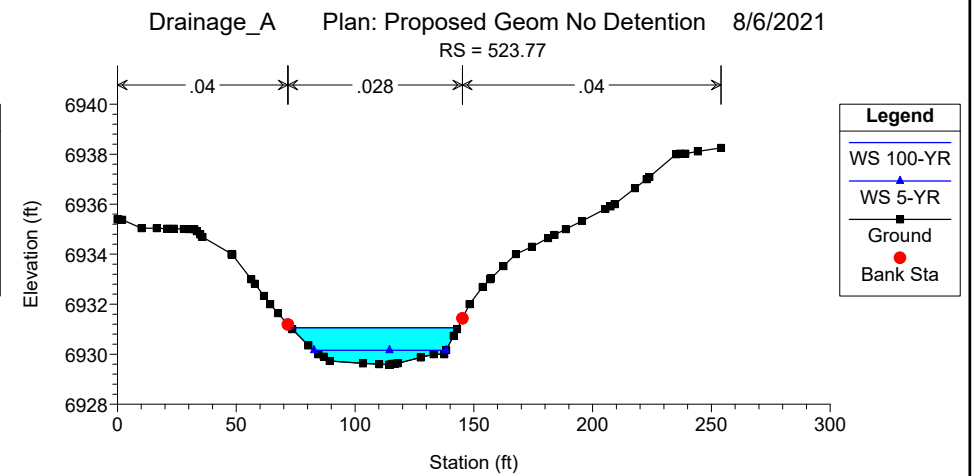
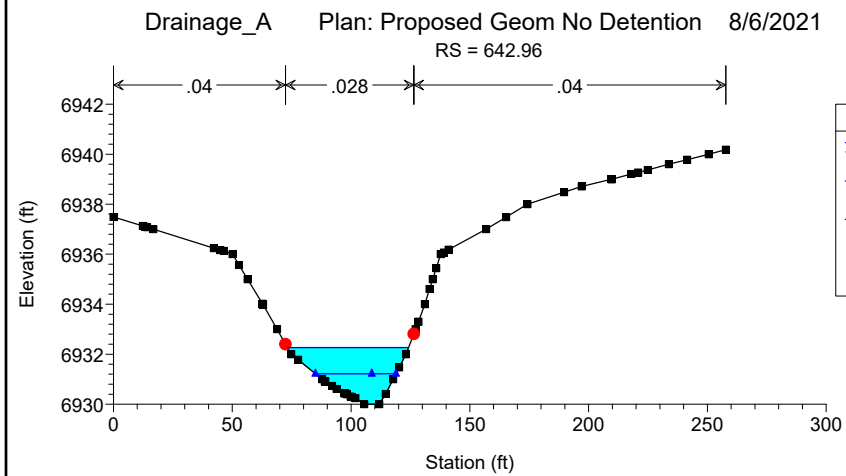
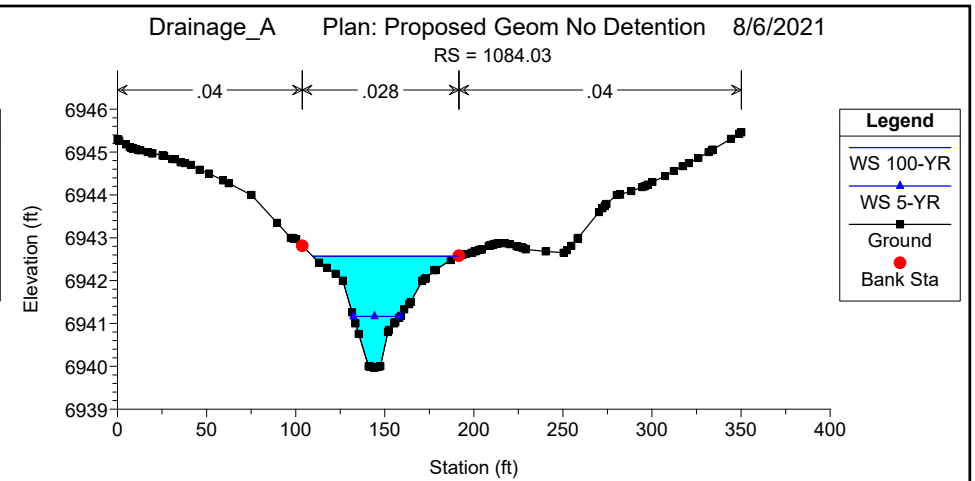
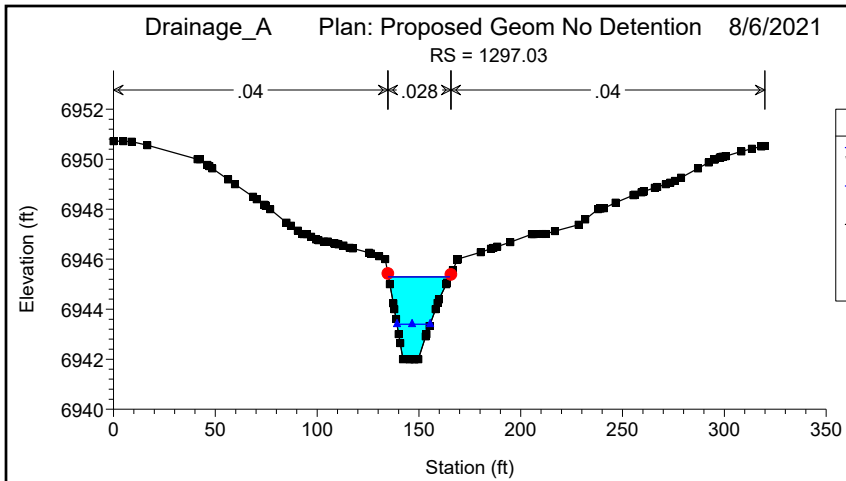
CHANNEL A MODEL CROSS SECTIONS



Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Froude # Chl	Shear LOB (lb/sq ft)	Shear Chan (lb/sq ft)	Shear ROB (lb/sq ft)	Power LOB (lb/ft s)	Power Chan (lb/ft s)	Power ROB (lb/ft s)
Alignment - (2)	3712.84	100-YR	413.00	6993.54	6994.84	6994.84	6995.27	0.012379	5.24	78.75	1.01		0.65			3.39	
Alignment - (2)	3712.84	5-YR	67.00	6993.54	6994.13	6994.13	6994.30	0.016774	3.26	20.58	1.00		0.34			1.11	
Alignment - (2)	3618.51	100-YR	413.00	6989.96	6991.61	6991.61	6992.06	0.012115	5.42	76.24	1.01		0.68			3.66	
Alignment - (2)	3618.51	5-YR	67.00	6989.96	6990.82	6990.82	6991.01	0.015635	3.54	18.93	1.00		0.38			1.35	
Alignment - (2)	3424.5	100-YR	413.00	6985.91	6987.02	6987.02	6987.39	0.013081	4.88	84.55	1.01		0.59			2.88	
Alignment - (2)	3424.5	5-YR	67.00	6985.91	6986.30	6986.30	6986.45	0.016765	3.12	21.47	0.99		0.32			1.00	
Alignment - (2)	3214.73	100-YR	413.00	6979.87	6981.76	6981.76	6982.42	0.010605	6.55	63.05	1.00		0.87			5.69	
Alignment - (2)	3214.73	5-YR	67.00	6979.87	6980.52	6980.52	6980.79	0.014361	4.16	16.10	1.01		0.47			1.97	
Alignment - (2)	2882.47	100-YR	413.00	6973.22	6974.71	6974.71	6975.21	0.011487	5.72	72.23	1.00		0.72			4.13	
Alignment - (2)	2882.47	5-YR	67.00	6973.22	6973.90	6973.87	6974.06	0.012544	3.19	21.03	0.90		0.31			0.98	
Alignment - (2)	2772.34	100-YR	413.00	6972.00	6972.90	6972.90	6973.31	0.012758	5.14	80.40	1.02		0.63			3.25	
Alignment - (2)	2772.34	5-YR	67.00	6972.00	6972.29	6972.29	6972.42	0.017777	2.91	23.04	1.00		0.29			0.85	
Alignment - (2)	2592.31	100-YR	479.80	6964.02	6966.01	6966.01	6966.73	0.010427	6.80	70.59	1.01		0.91			6.22	
Alignment - (2)	2592.31	5-YR	80.03	6964.02	6964.82	6964.82	6965.09	0.014202	4.17	19.19	1.00		0.47			1.98	
Alignment - (2)	2527.18	100-YR	479.80	6962.89	6964.83	6964.83	6965.52	0.010519	6.69	71.69	1.01		0.90			5.99	
Alignment - (2)	2527.18	5-YR	80.03	6962.89	6963.64	6963.64	6963.92	0.013864	4.20	19.05	1.00		0.48			2.00	
Alignment - (2)	2303.17	100-YR	479.80	6959.99	6962.42	6962.38	6963.11	0.009556	6.70	71.65	0.97		0.87			5.86	
Alignment - (2)	2303.17	5-YR	80.03	6959.99	6961.06	6960.97	6961.32	0.009677	4.15	19.30	0.87		0.43			1.77	
Alignment - (2)	2121.94	100-YR	479.80	6957.99	6960.51	6960.51	6961.34	0.009879	7.30	65.68	1.00		1.01			7.34	
Alignment - (2)	2121.94	5-YR	80.03	6957.99	6958.91	6958.91	6959.28	0.013151	4.88	16.40	1.01		0.59			2.88	
Alignment - (2)	1814.04	100-YR	479.80	6953.99	6956.15	6956.15	6956.82	0.010180	7.04	68.15	1.01		0.96			6.74	
Alignment - (2)	1814.04	5-YR	80.03	6953.99	6954.76	6954.76	6955.08	0.013386	4.54	17.62	1.00		0.53			2.41	
Alignment - (2)	1556.67	100-YR	479.80	6949.87	6952.10	6952.10	6952.67	0.009989	6.07	80.71	0.97	0.09	0.76		0.10	4.63	
Alignment - (2)	1556.67	5-YR	80.03	6949.87	6950.72	6950.72	6951.03	0.013371	4.47	17.92	1.00		0.52			2.31	
Alignment - (2)	1297.03	100-YR	479.80	6941.99	6945.29	6945.29	6946.29	0.009589	8.02	59.80	1.00		1.15			9.21	
Alignment - (2)	1297.03	5-YR	80.03	6941.99	6943.40	6943.27	6943.76	0.008428	4.83	16.57	0.84		0.52			2.51	
Alignment - (2)	1084.03	100-YR	479.80	6939.97	6942.57	6942.57	6943.09	0.011853	5.81	82.59	1.02		0.75			4.33	
Alignment - (2)	1084.03	5-YR	80.03	6939.97	6941.17	6941.17	6941.50	0.013605	4.64	17.26	1.01		0.55			2.55	
Alignment - (2)	642.96	100-YR	479.80	6930.00	6932.27	6932.27	6932.98	0.010616	6.78	70.78	1.01		0.91			6.20	
Alignment - (2)	642.96	5-YR	80.03	6930.00	6931.22	6931.22	6931.37	0.005127	3.14	25.52	0.84		0.24			0.75	
Alignment - (2)	523.77	100-YR	479.80	6929.58	6931.06	6931.06	6931.63	0.011302	6.09	78.84	1.01		0.79			4.81	
Alignment - (2)	523.77	5-YR	80.03	6929.58	6930.16	6930.16	6930.36	0.016078	3.63	22.05	1.02		0.40			1.44	
Alignment - (2)	290.78	100-YR	479.80	6924.69	6926.15	6926.15	6926.73	0.010915	6.13	78.32	1.00		0.79			4.85	
Alignment - (2)	290.78	5-YR	80.03	6924.69	6925.22	6925.22	6925.43	0.015614	3.64	21.97	1.01		0.40			1.45	
Alignment - (2)	214.43	100-YR	479.80	6922.96	6924.83	6924.83	6925.53	0.010512	6.74	71.18	1.01		0.90			6.10	
Alignment - (2)	214.43	5-YR	80.03	6922.96	6923.66	6923.66	6923.94	0.014503	4.21	16.99	1.01		0.48			2.04	
Alignment - (2)	148.72	100-YR	479.80	6920.98	6922.82	6922.82	6923.52	0.010380	6.71	71.47	1.00		0.90			6.02	
Alignment - (2)	148.72	5-YR	80.03	6920.98	6921.69	6921.69	6921.95	0.014036	4.11	19.47	1.00		0.46			1.90	
Alignment - (2)	33.13	100-YR	479.80	6918.00	6920.43	6920.43	6921.12	0.010447	6.63	72.42	1.00		0.88			5.83	
Alignment - (2)	33.13	5-YR	80.03	6918.00	6919.14	6919.14	6919.45	0.013835	4.53	17.68	1.01		0.53			2.41	

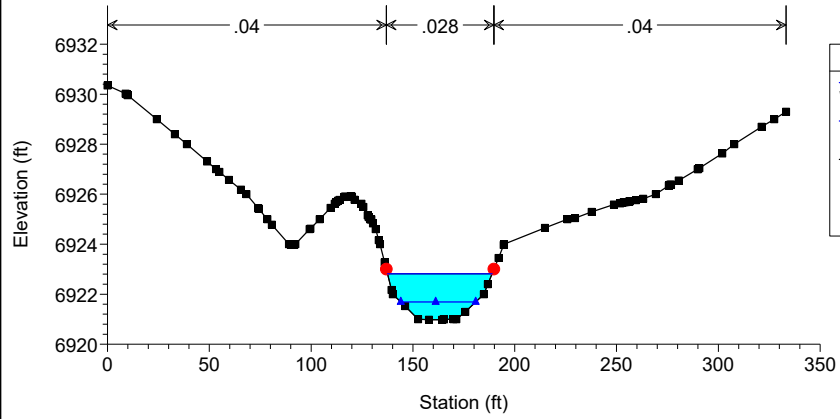






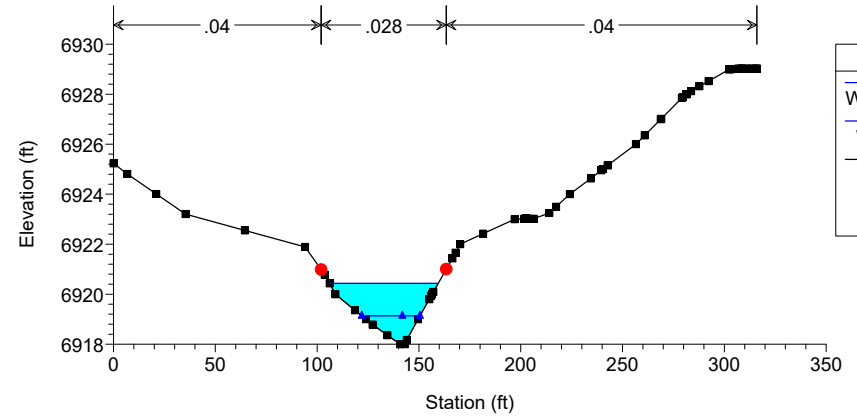
Drainage\_A Plan: Proposed Geom No Detention 8/6/2021

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Drainage\_A Plan: Proposed Geom No Detention 8/6/2021

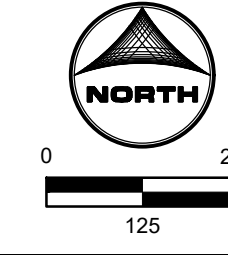
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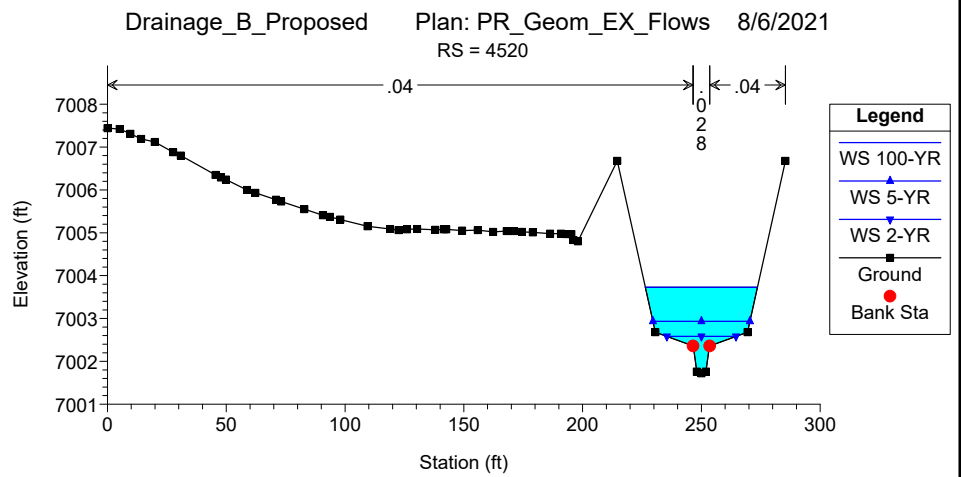
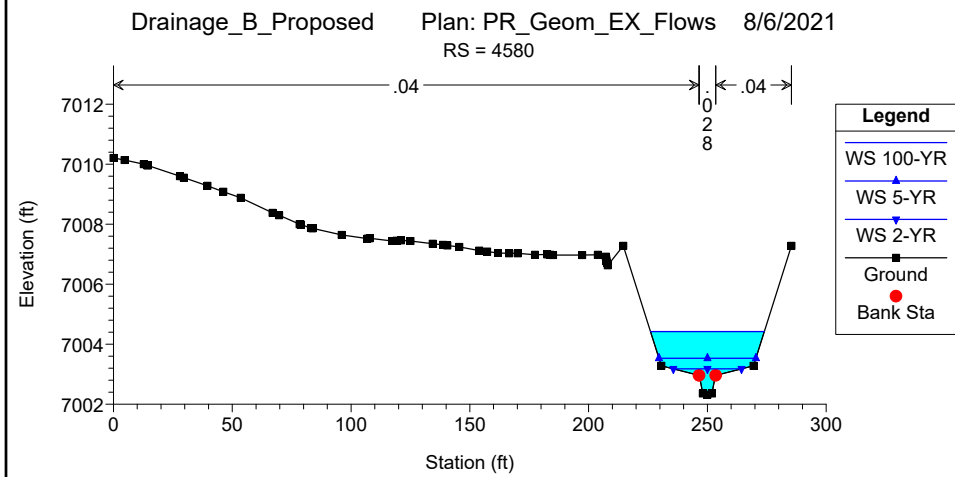
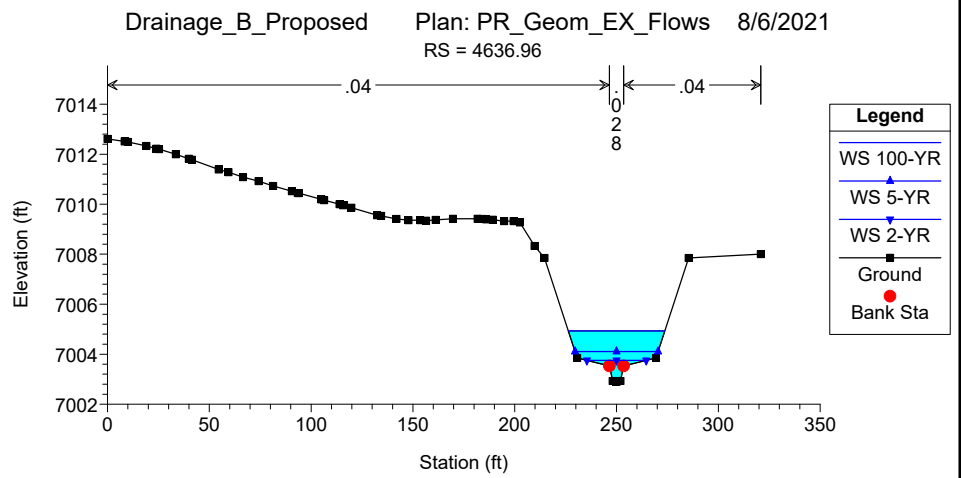
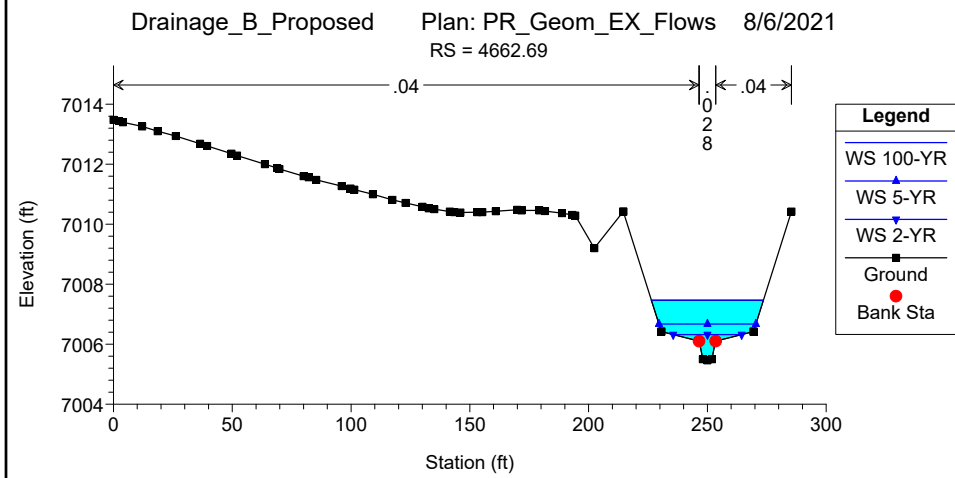
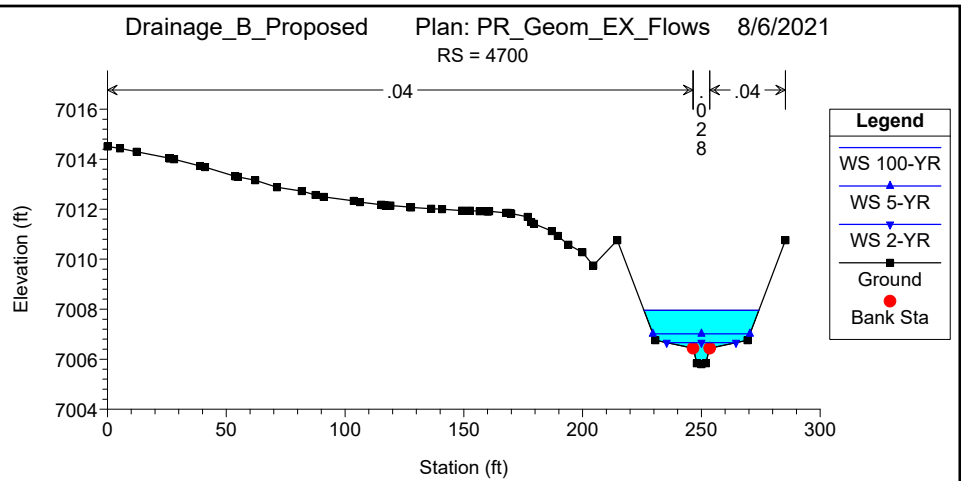
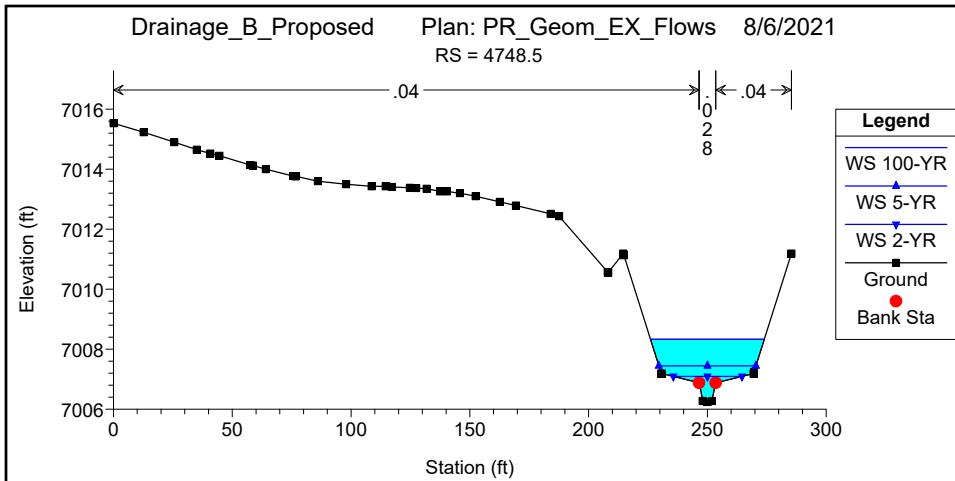
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Date:	8/12/2021

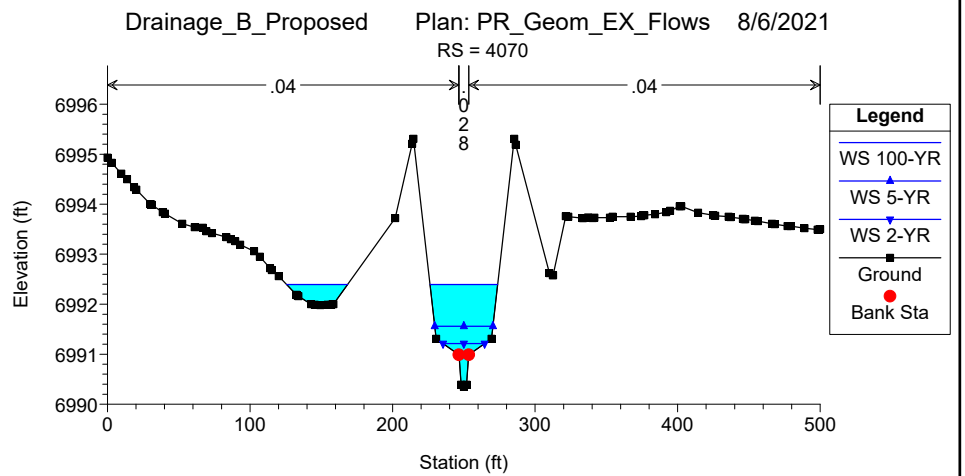
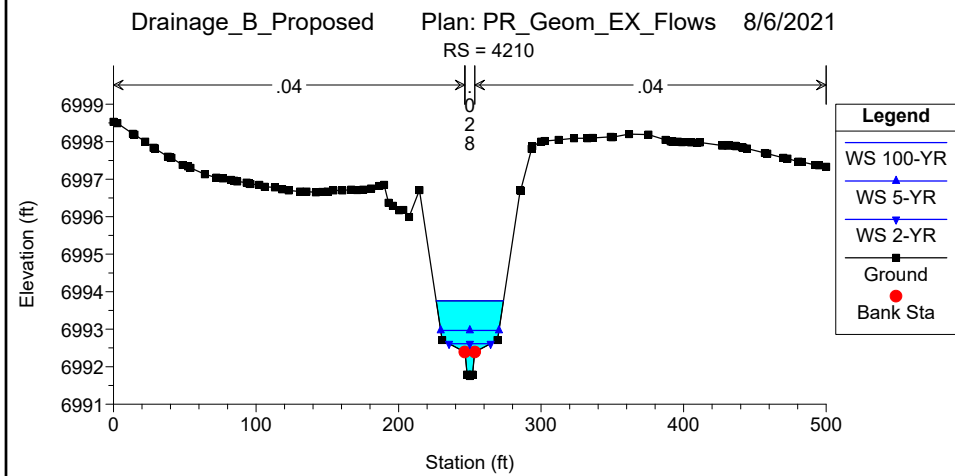
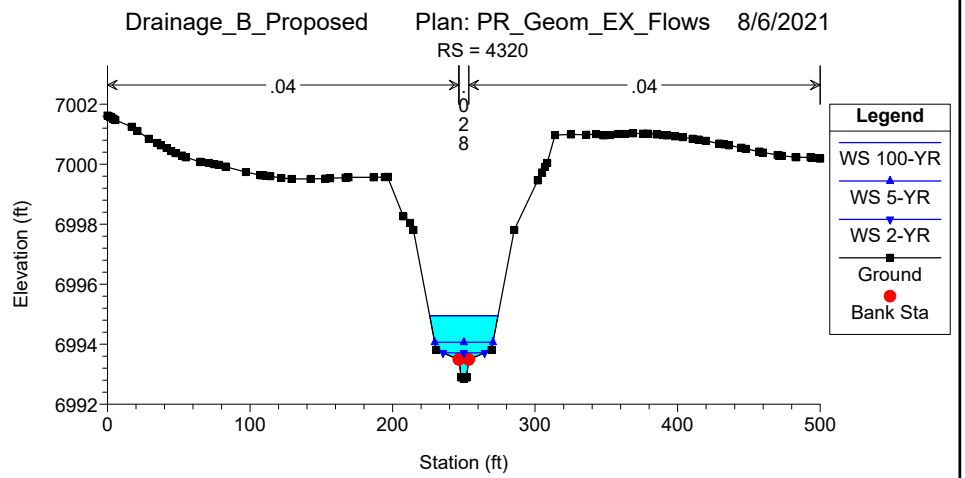
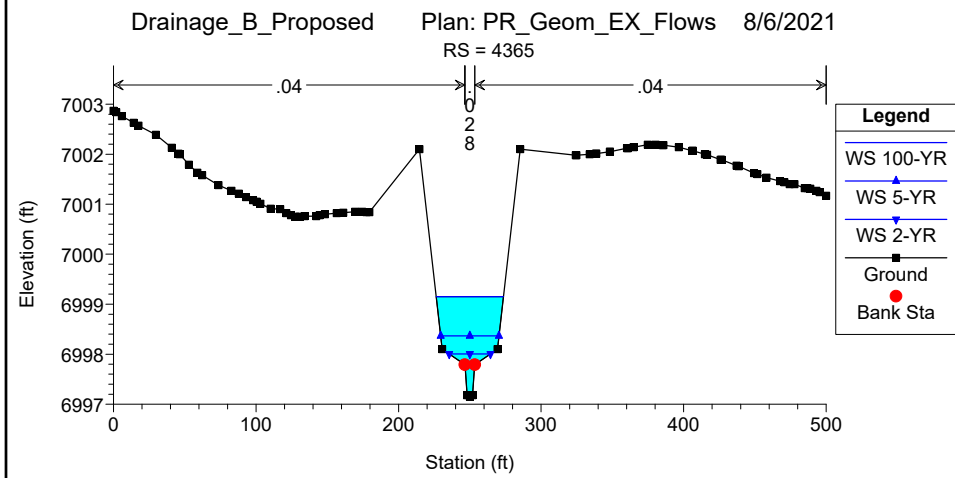
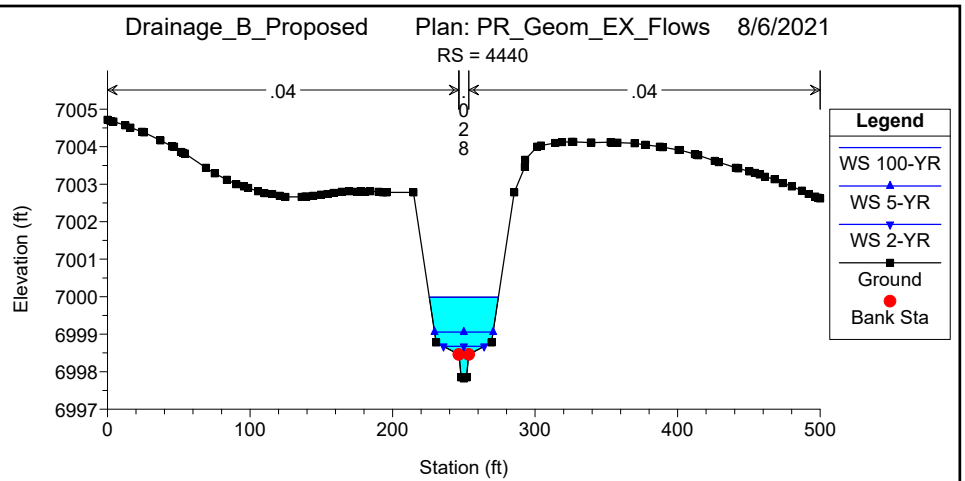
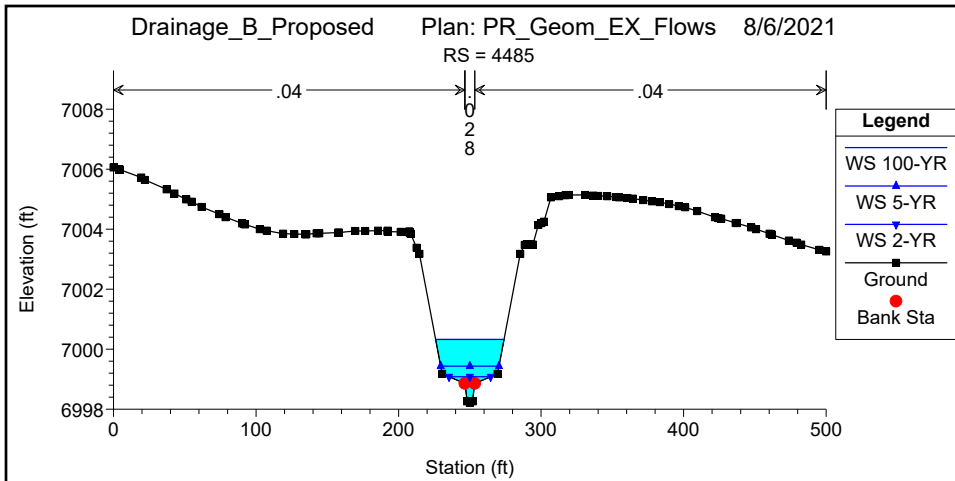
PROPOSED MODEL CROSS SECTIONS

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Froude # Chl	Shear LOB (lb/sq ft)	Shear Chan (lb/sq ft)	Shear ROB (lb/sq ft)	Power LOB (lb/ft s)	Power Chan (lb/ft s)	Power ROB (lb/ft s)
Alignment Channe	4748.5	100-YR	280.00	7006.24	7008.33	7008.24	7008.81	0.008996	7.62	59.94	0.97	0.63	1.05	0.63	2.41	7.97	2.42
Alignment Channe	4748.5	5-YR	59.00	7006.24	7007.45	7007.45	7007.68	0.008149	4.81	20.62	0.83	0.20	0.51	0.20	0.36	2.46	0.36
Alignment Channe	4700	100-YR	280.00	7005.80	7007.96		7008.39	0.007882	7.27	62.72	0.91	0.58	0.94	0.58	2.12	6.86	2.12
Alignment Channe	4700	5-YR	59.00	7005.80	7007.02	7007.02	7007.25	0.007985	4.77	20.79	0.82	0.20	0.50	0.20	0.36	2.40	0.36
Alignment Channe	4662.69	100-YR	280.00	7005.46	7007.47	7007.47	7008.02	0.011159	8.22	55.86	1.07	0.74	1.24	0.74	3.01	10.16	3.01
Alignment Channe	4662.69	5-YR	59.00	7005.46	7006.67	7006.67	7006.91	0.008170	4.81	20.61	0.83	0.20	0.51	0.20	0.36	2.46	0.36
Alignment Channe	4636.96	100-YR	280.00	7002.89	7004.93	7004.90	7005.46	0.010312	7.99	57.19	1.03	0.70	1.16	0.70	2.78	9.29	2.78
Alignment Channe	4636.96	5-YR	59.00	7002.89	7004.10	7004.10	7004.34	0.008058	4.78	20.72	0.83	0.20	0.51	0.20	0.36	2.42	0.36
Alignment Channe	4580	100-YR	280.00	7002.32	7004.42	7004.33	7004.89	0.008981	7.61	59.97	0.97	0.63	1.04	0.63	2.41	7.95	2.41
Alignment Channe	4580	5-YR	59.00	7002.32	7003.53	7003.53	7003.77	0.008191	4.81	20.59	0.83	0.20	0.51	0.20	0.36	2.47	0.36
Alignment Channe	4520	100-YR	280.00	7001.72	7003.73	7003.73	7004.29	0.011154	8.22	55.66	1.07	0.74	1.24	0.74	3.00	10.16	3.00
Alignment Channe	4520	5-YR	59.00	7001.72	7002.94	7002.94	7003.17	0.008055	4.78	20.72	0.83	0.20	0.51	0.20	0.36	2.42	0.36
Alignment Channe	4485	100-YR	280.00	6998.22	7000.33	7000.23	7000.79	0.008854	7.58	60.26	0.96	0.63	1.03	0.63	2.38	7.82	2.38
Alignment Channe	4485	5-YR	59.00	6998.22	6999.43	6999.43	6999.67	0.008075	4.79	20.70	0.83	0.20	0.51	0.20	0.36	2.43	0.36
Alignment Channe	4440	100-YR	280.00	6997.82	6999.99		7000.41	0.007644	7.20	63.37	0.90	0.56	0.92	0.56	2.05	6.64	2.05
Alignment Channe	4440	5-YR	59.00	6997.82	6999.06	6999.06	6999.27	0.007204	4.59	21.58	0.78	0.19	0.46	0.19	0.33	2.13	0.33
Alignment Channe	4365	100-YR	280.00	6997.15	6999.15	6999.15	6999.71	0.011185	8.23	55.62	1.07	0.74	1.24	0.74	3.01	10.20	3.01
Alignment Channe	4365	5-YR	59.00	6997.15	6998.37	6998.37	6998.59	0.007751	4.72	21.01	0.81	0.19	0.49	0.19	0.35	2.32	0.35
Alignment Channe	4320	100-YR	280.00	6992.85	6994.95	6994.86	6995.42	0.009001	7.62	59.92	0.97	0.63	1.05	0.63	2.42	7.97	2.42
Alignment Channe	4320	5-YR	59.00	6992.85	6994.07	6994.07	6994.30	0.008005	4.77	20.77	0.82	0.20	0.50	0.20	0.36	2.40	0.36
Alignment Channe	4210	100-YR	280.00	6991.75	6993.76	6993.76	6994.31	0.011161	8.22	55.65	1.07	0.74	1.24	0.74	3.01	10.16	3.01
Alignment Channe	4210	5-YR	59.00	6991.75	6992.97	6992.97	6993.20	0.007905	4.75	20.87	0.82	0.20	0.50	0.20	0.35	2.37	0.35
Alignment Channe	4070	100-YR	280.00	6990.35	6992.40	6992.40	6992.81	0.008921	7.44	69.51	0.96	0.30	1.01	0.61	0.89	7.50	2.24
Alignment Channe	4070	5-YR	59.00	6990.35	6991.56	6991.56	6991.80	0.008275	4.83	20.51	0.84	0.20	0.52	0.20	0.37	2.50	0.37
Alignment Channe	4025	100-YR	280.00	6985.85	6987.95	6987.86	6988.42	0.008940	7.60	60.06	0.97	0.63	1.04	0.63	2.40	7.91	2.40
Alignment Channe	4025	5-YR	59.00	6985.85	6987.06	6987.06	6987.30	0.008424	4.86	20.37	0.84	0.20	0.52	0.20	0.37	2.55	0.37
Alignment Channe	3925	100-YR	280.00	6984.85	6986.86	6986.86	6987.42	0.011256	8.24	55.49	1.07	0.74	1.24	0.74	3.03	10.26	3.03
Alignment Channe	3925	5-YR	59.00	6984.85	6986.06	6986.06	6986.30	0.008087	4.79	20.69	0.83	0.20	0.51	0.20	0.36	2.43	0.36
Alignment Channe	3880	100-YR	280.00	6980.35	6984.85		6984.89	0.002029	2.35	198.09	0.20	0.05	0.08	0.05	0.06	0.18	0.06
Alignment Channe	3880	5-YR	59.00	6980.35	6981.92		6981.99	0.001771	2.73	35.82	0.41	0.08	0.15	0.08	0.10	0.41	0.10
Alignment Channe	3830	100-YR	280.00	6979.90	6984.60	6982.19	6984.78	0.000681	3.73	87.49	0.30	0.17	0.19	0.17	0.42	0.70	0.42
Alignment Channe	3830	5-YR	59.00	6979.90	6981.49	6980.92	6981.59	0.001625	2.78	25.28	0.39	0.09	0.15	0.09	0.13	0.42	0.13
Alignment Channe	3825			Culvert													
Alignment Channe	3760	100-YR	280.00	6979.27	6981.78	6981.78	6982.88	0.008939	8.85	34.61	0.99	1.03	1.31	1.03	5.42	11.58	5.42
Alignment Channe	3760	5-YR	59.00	6979.27	6980.36	6980.28	6980.70	0.008018	4.77	13.40	0.82	0.21	0.50	0.21	0.41	2.40	0.41
Alignment Channe	3650	100-YR	390.70	6978.28	6980.80		6981.29	0.007384	7.87	80.68	0.91	0.66	1.05	0.66	2.70	8.22	2.70
Alignment Channe	3650	5-YR	68.95	6978.28	6979.56	6979.56	6979.80	0.007808	4.92	23.55	0.82	0.22	0.52	0.22	0.44	2.57	0.44
Alignment Channe	3405	100-YR	390.70	6976.08	6978.36	6978.36	6979.04	0.011518	9.17	69.24	1.11	0.92	1.47	0.92	4.29	13.49	4.29
Alignment Channe	3405	5-YR	68.95	6976.08	6977.34	6977.34	6977.59	0.008491	5.07	22.85	0.86	0.24	0.56	0.24	0.47	2.83	0.47
Alignment Channe	3360	100-YR	390.70	6971.58	6973.91	6973.86	6974.54	0.010411	8.86	71.69	1.06	0.85	1.36	0.85	3.86	12.05	3.86
Alignment Channe	3360	5-YR	68.95	6971.58	6972.83	6972.83	6973.09	0.008634	5.10	22.71	0.86	0.24	0.57	0.24	0.47	2.89	0.47
Alignment Channe	3040	100-YR	390.70	6968.69	6971.20	6970.99	6971.70	0.007461	7.90	80.40	0.91	0.67	1.05	0.67	2.73	8.32	2.73
Alignment Channe	3040	5-YR	68.95	6968.69	6969.96	6969.96	6970.21	0.008491	5.07	22.83	0.86	0.23	0.56	0.23	0.47	2.84	0.47
Alignment Channe	2715	100-YR	390.70	6965.77	6968.07	6968.07	6968.74	0.011236	9.10	69.82	1.10	0.90	1.44	0.90	4.18	13.14	4.18
Alignment Channe	2715	5-YR	68.95	6965.77	6967.04	6967.04	6967.29	0.008451	5.06	22.87	0.85	0.23	0.56	0.23	0.46	2.82	0.46
Alignment Channe	2675	100-YR	390.70	6961.77	6964.18	6964.07	6964.75	0.009096	8.46	75.09	1.00	0.77	1.23	0.77	3.36	10.38	3.36
Alignment Channe	2675	5-YR	68.95	6961.77	6963.04	6963.04	6963.29	0.008411	5.05	22.91	0.85	0.23	0.56	0.23	0.46	2.81	0.46
Alignment Channe	2570	100-YR	390.70	6960.72	6963.03	6963.03	6963.69	0.011094	9.06	70.19	1.09	0.84	1.43	0.89	3.89	12.95	4.12
Alignment Channe	2570	5-YR	68.95	6960.72	6961.98	6961.98	6962.24	0.008643	5.11	22.68	0.86	0.24	0.57	0.24	0.47	2.90	0.47
Alignment Channe	2545	100-YR	390.70	6958.22	6960.64	6960.51	6961.20	0.008854	8.38	75.79	0.99	0.76	1.20	0.76	3.26	10.07	3.26
Alignment Channe	2545	5-YR	68.95	6958.22	6959.51	6959.51	6959.74	0.007720	4.89	23.65	0.82	0.22	0.52	0.22	0.43	2.54	0.43
Alignment Channe	2460	100-YR	390.70	6957.37	6959.66	6959.66	6960.34	0.011438	9.16	69.39	1.11	0.91	1.46	0.91	4.25	13.41	4.25
Alignment Channe	2460	5-YR	68.95	6957.37	6958.63	6958.63	6958.89	0.008667	5.11	22.66	0.86	0.24	0.57	0.24	0.47	2.91	0.47
Alignment Channe	2420	100-YR	390.70	6953.37	6955.91		6956.39	0.007043	7.74	82.01	0.89	0.64	1.01	0.64	2.57	7.80	2.57
Alignment Channe	2420	5-YR	68.95	6953.37	6954.71		6954.90	0.006138	4.49	25.72	0.74	0.19	0.43	0.19	0.36	1.93	0.36
Alignment Channe	2260	100-YR	390.70	6951.93	6954.44	6954.22	6954.94	0.007451	7.89	80.43	0.91	0.67	1.05	0.67	2.73	8.31	2.73
Alignment Channe	2260	5-YR	68.95	6951.93	6953.19	6953.19	6953.45	0.008646	5.11	22.68	0.86	0.24	0.57	0.24	0.47	2.90	0.47
Alignment Channe	2045	100-YR	390.70	6950.00	6952.28	6952.28	6952.96	0.011523	9.18	69.23	1.11	0.92	1.47	0.92	4.29	13.50	4.29
Alignment Channe	2045	5-YR	68.95	6950.00	6951.25	6951.25	6951.51	0.008766	5.13	22.58	0.87	0.24	0.57	0.24	0.48	2.94	0.48
Alignment Channe	2000	100-YR	390.70	6945.50	6948.10		6948.53	0.006304	7.45	85.22	0.84	0.59	0.92	0.59	2.29	6.89	2.29
Alignment Channe	2000	5-YR	68.95	6945.50	6946.76	6946.76	6947.01	0.008518	5.07	22.83	0.86	0.24	0.56	0.24	0.47	2.84	0.47
Alignment Channe	1740	100-YR	597.69	6942.90	6945.81	6945.64	6946.52	0.008796	9.55	101.93	1.02	0.95	1.46	0.95	4.74	13.92	4.74
Alignment Channe	1740	5-YR	86.00	6942.90	6944.25	6944.25	6944.53	0.008827	5.45	26.46	0.88	0.29	0.63	0.29	0.64	3.43	0.64
Alignment Channe	1445	100-YR	597.69	6939.94	6942.69	6942.69	6943.55	0.011516	10.47	92.83	1.15	1.16	1.79	1.16	6.32	18.76	6.32
Alignment Channe	1445	5-YR	86.00	6939.94	6941.29	6941.29	6941.57	0.008918	5.46	26.37	0.89	0.29	0.63	0.29	0.65	3.46	0.65
Alignment Channe	1400	100-YR	597.69	6935.44	6938.21	6938.19	6939.05	0.011170	10.36	93.81	1.13	1.13	1.75	1.13	6.11		

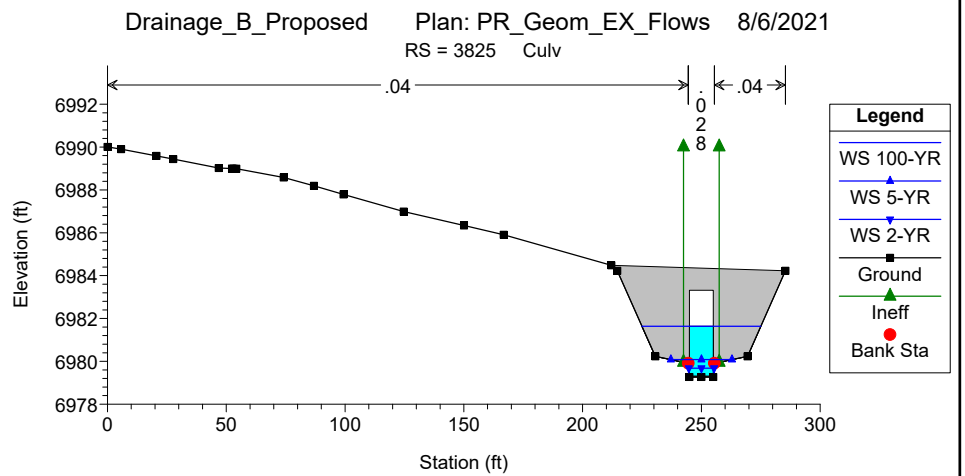
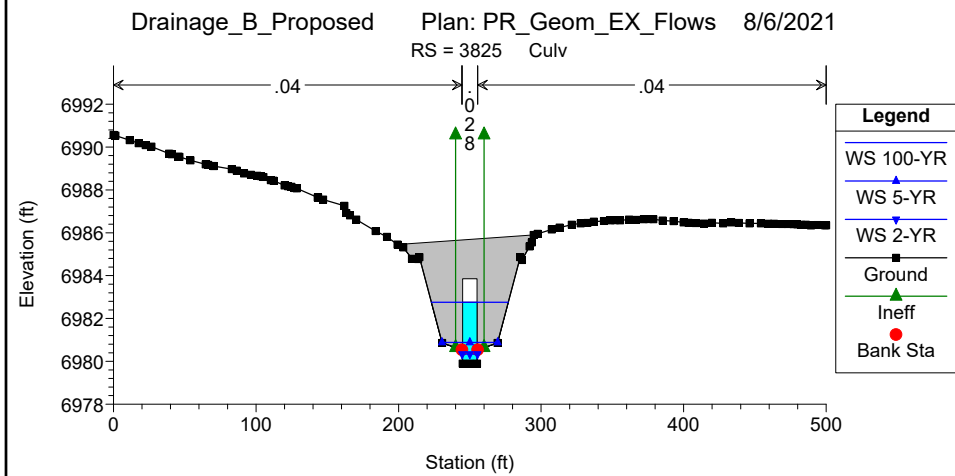
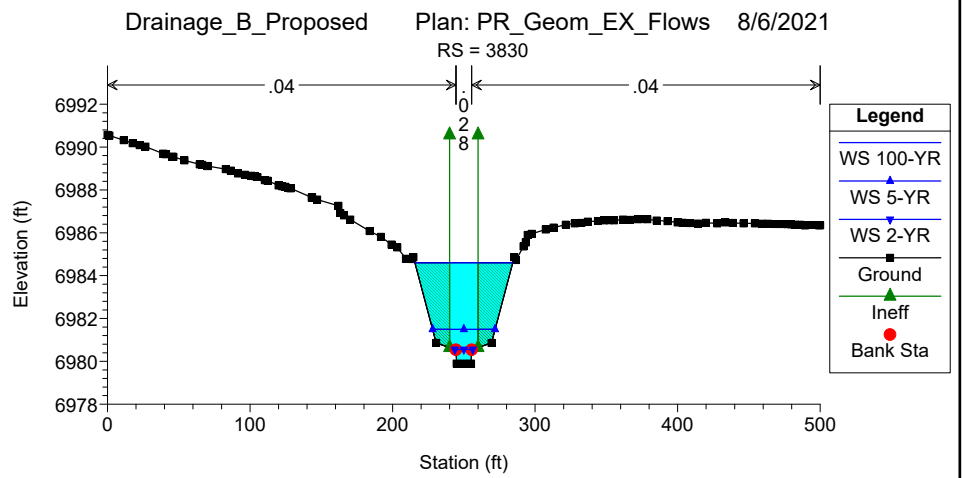
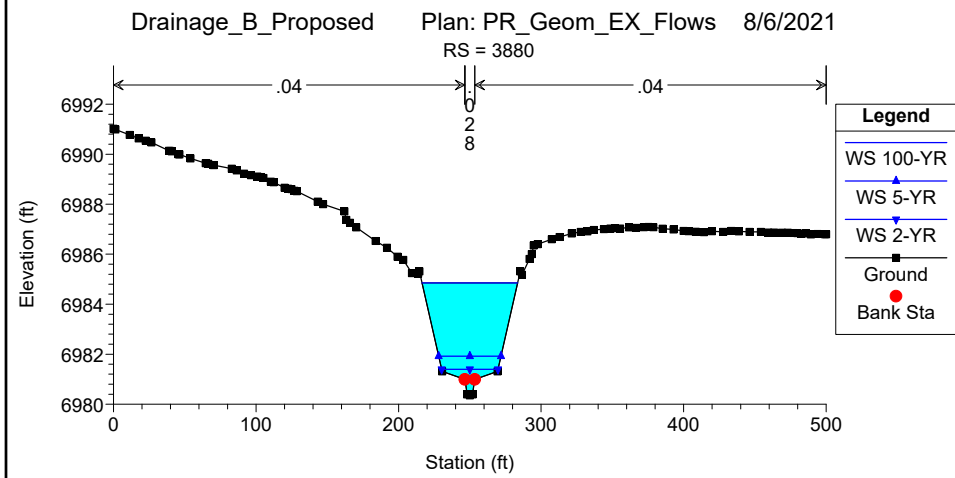
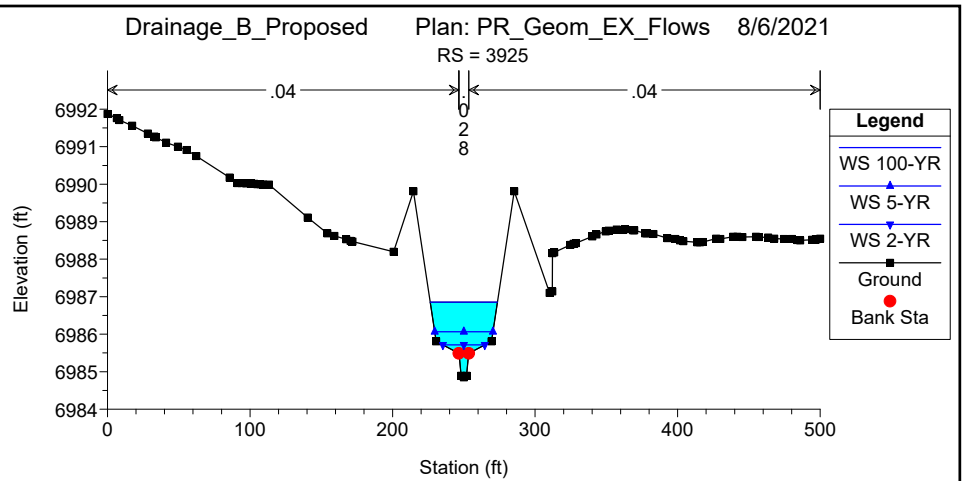
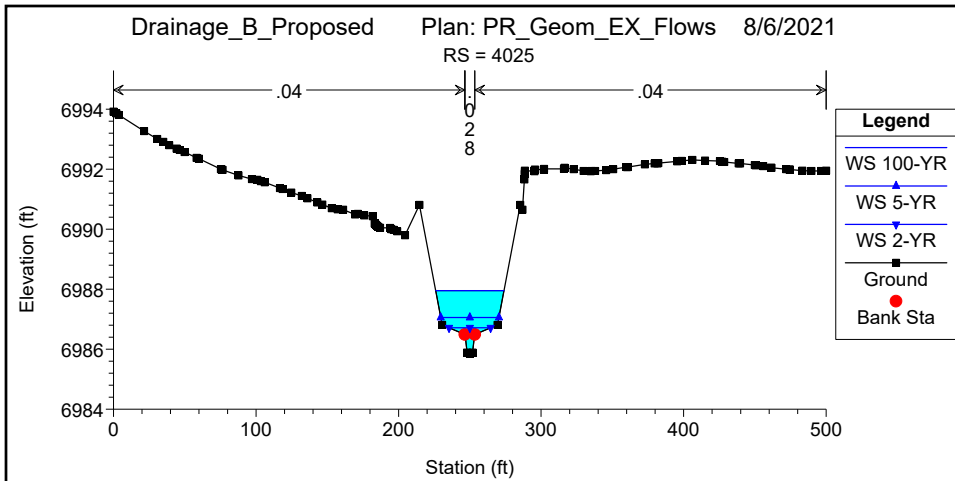
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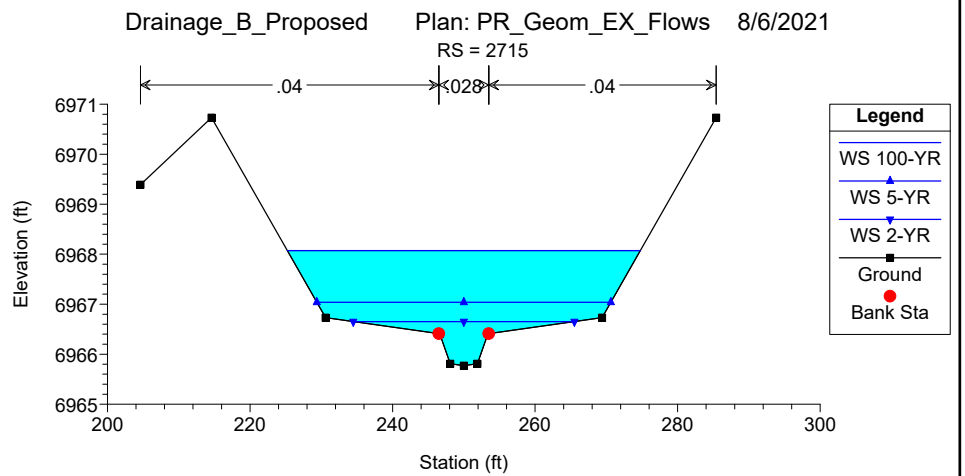
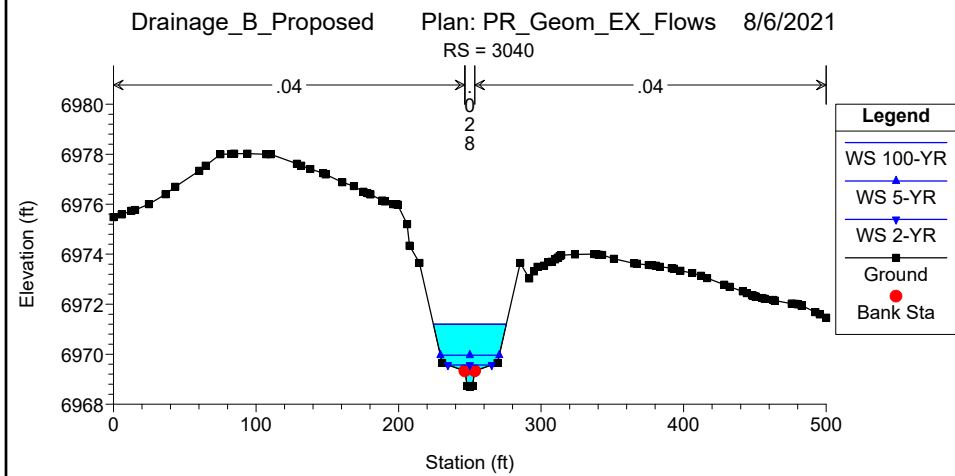
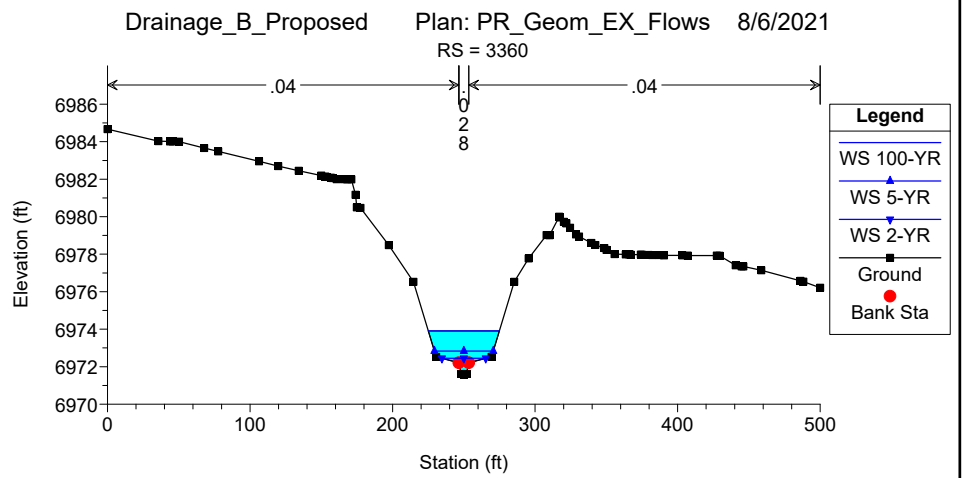
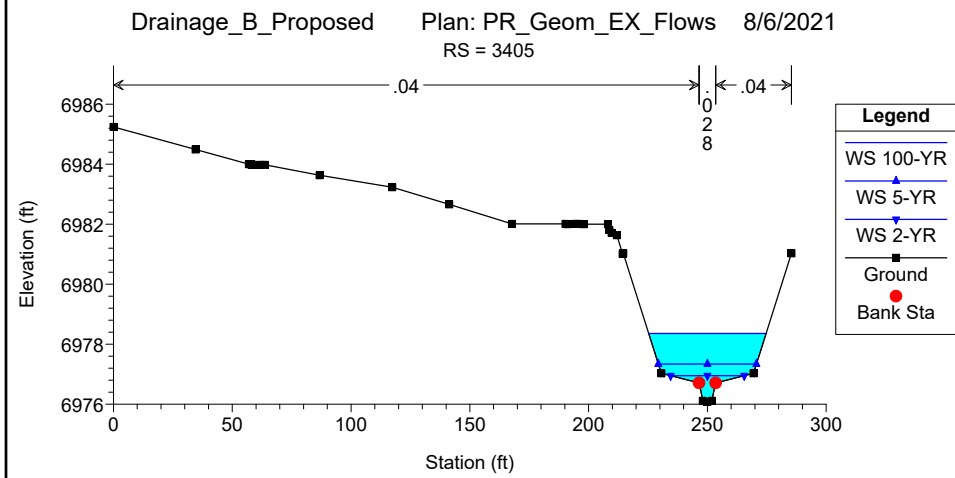
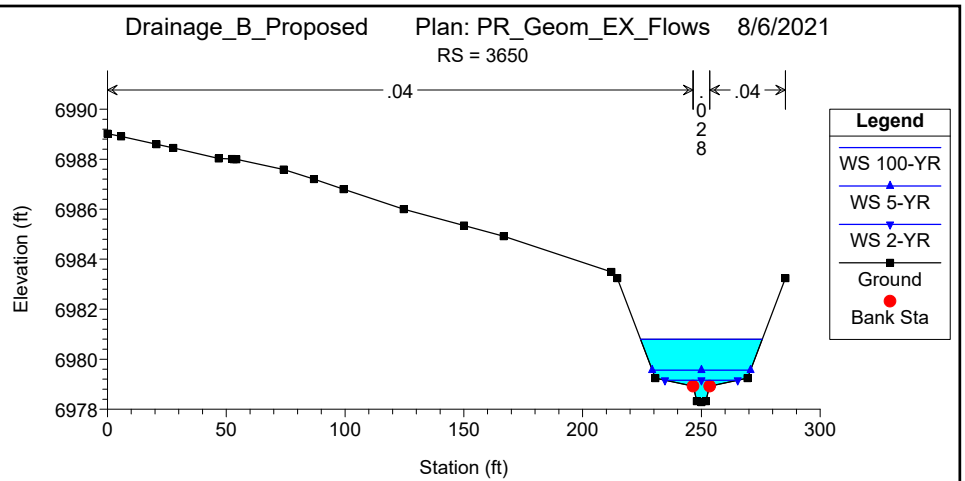
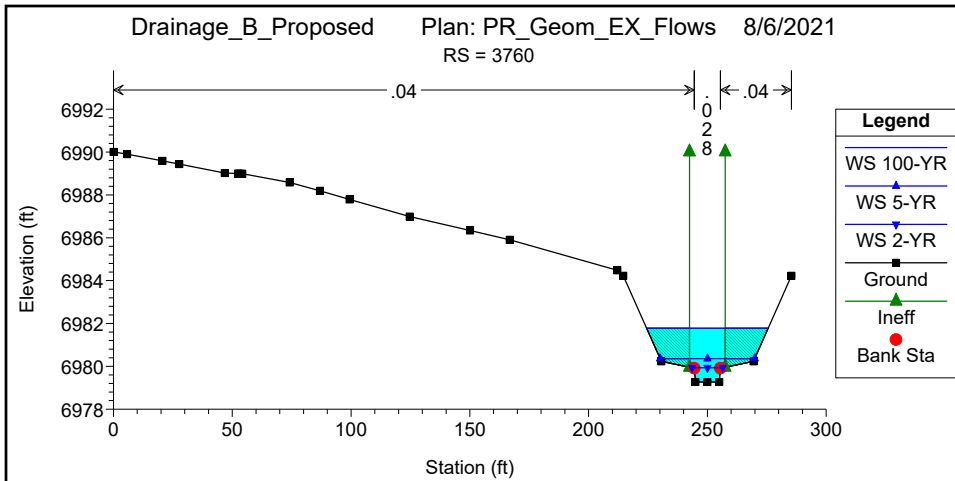
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Froude # Chl	Shear LOB (lb/sq ft)	Shear Chan (lb/sq ft)	Shear ROB (lb/sq ft)	Power LOB (lb/ft s)	Power Chan (lb/ft s)	Power ROB (lb/ft s)
Alignment Channe	590	100-YR	597.69	6923.40	6926.43		6927.06	0.007427	9.01	108.08	0.94	0.84	1.28	0.84	3.96	11.55	3.96
Alignment Channe	590	5-YR	86.00	6923.40	6924.75	6924.75	6925.03	0.008880	5.46	26.41	0.89	0.29	0.63	0.29	0.65	3.45	0.65
Alignment Channe	445	100-YR	597.69	6922.10	6924.85		6924.85	0.011516	10.47	92.83	1.15	1.16	1.79	1.16	6.32	18.76	6.32
Alignment Channe	445	5-YR	86.00	6922.10	6923.45	6923.45	6923.73	0.008918	5.46	26.37	0.89	0.29	0.63	0.29	0.65	3.46	0.65
Alignment Channe	400	100-YR	597.69	6917.60	6920.46		6920.35	0.009682	9.84	98.47	1.06	1.01	1.56	1.02	5.24	15.38	5.25
Alignment Channe	400	5-YR	86.00	6917.60	6918.95	6918.94	6919.23	0.008982	5.45	26.29	0.89	0.29	0.63	0.29	0.65	3.44	0.65
Alignment Channe	200	100-YR	597.69	6915.80	6918.80		6918.55	0.007830	9.17	106.11	0.96	0.87	1.33	0.87	4.19	12.24	4.19
Alignment Channe	200	5-YR	86.00	6915.80	6917.15	6917.15	6917.43	0.008995	5.48	26.29	0.89	0.29	0.64	0.29	0.66	3.50	0.66
Alignment Channe	70.18	100-YR	597.69	6914.63	6917.40		6917.40	0.011055	10.32	94.86	1.13	1.12	1.74	0.96	6.03	17.90	5.07
Alignment Channe	70.18	5-YR	86.00	6914.63	6915.98	6915.98	6916.26	0.009065	5.50	26.21	0.90	0.29	0.64	0.29	0.66	3.53	0.67

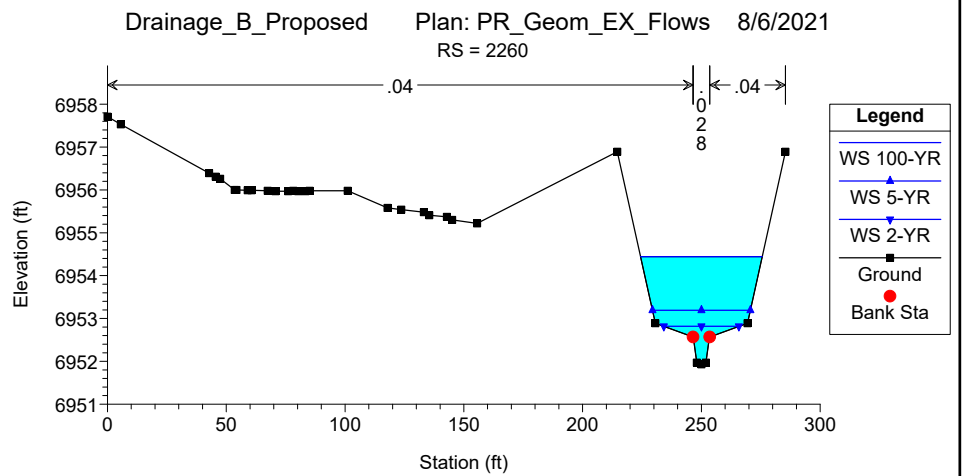
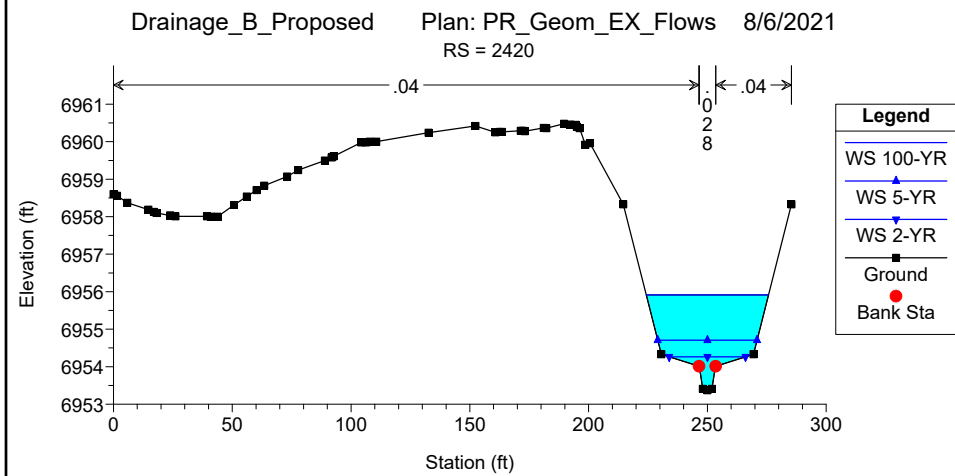
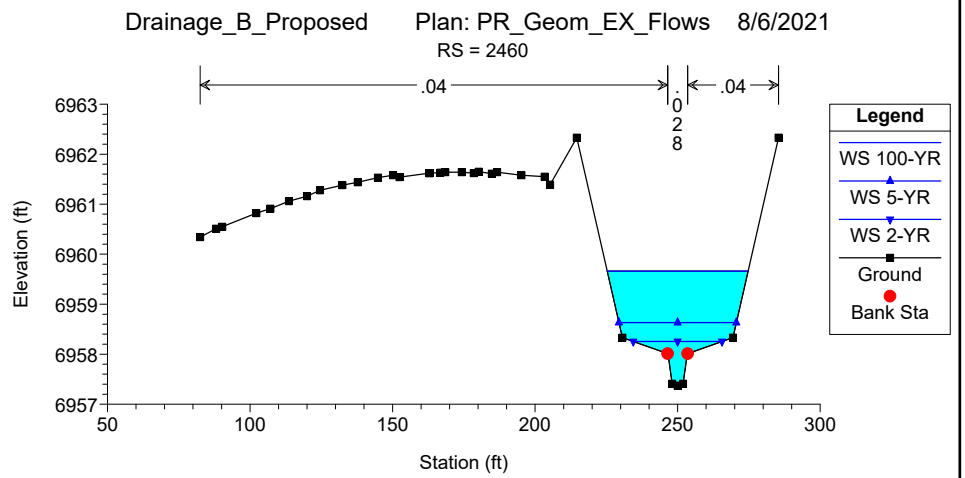
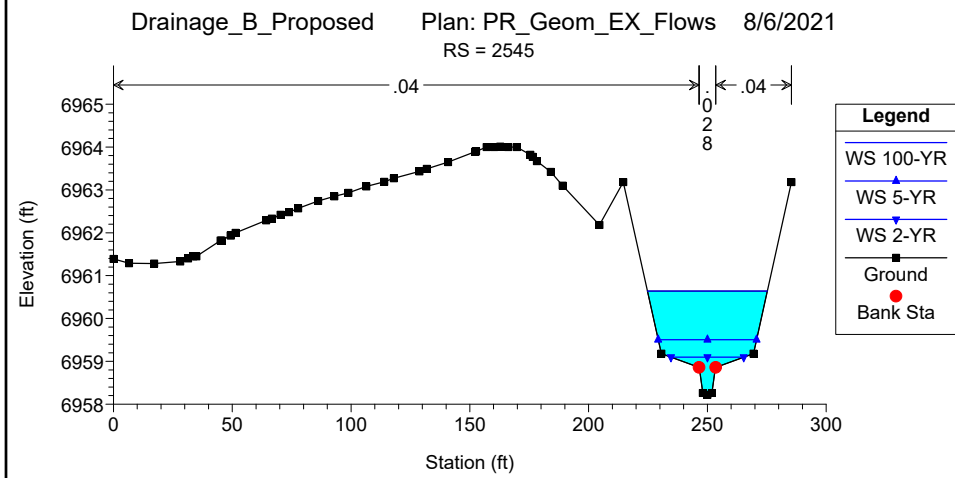
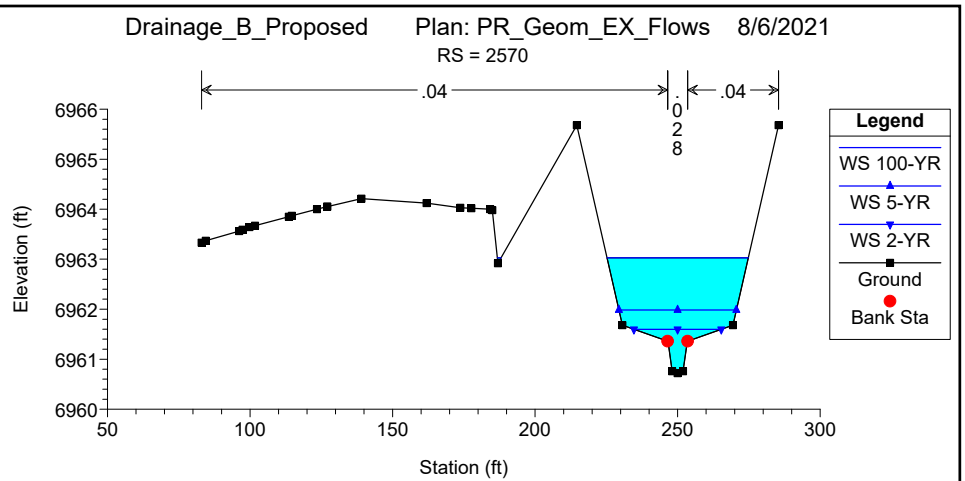
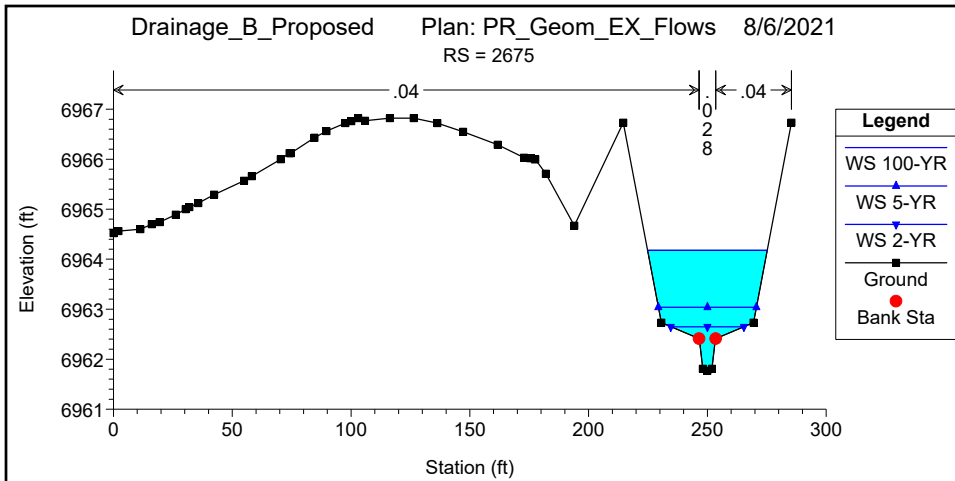


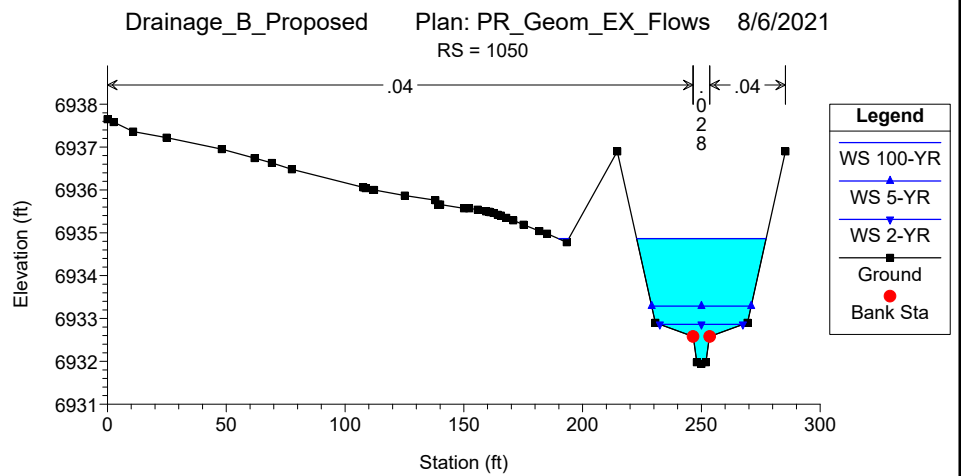
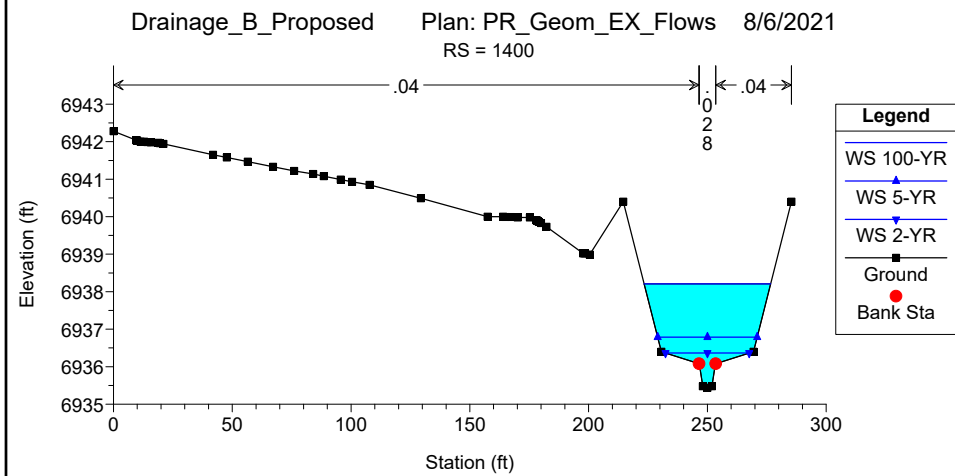
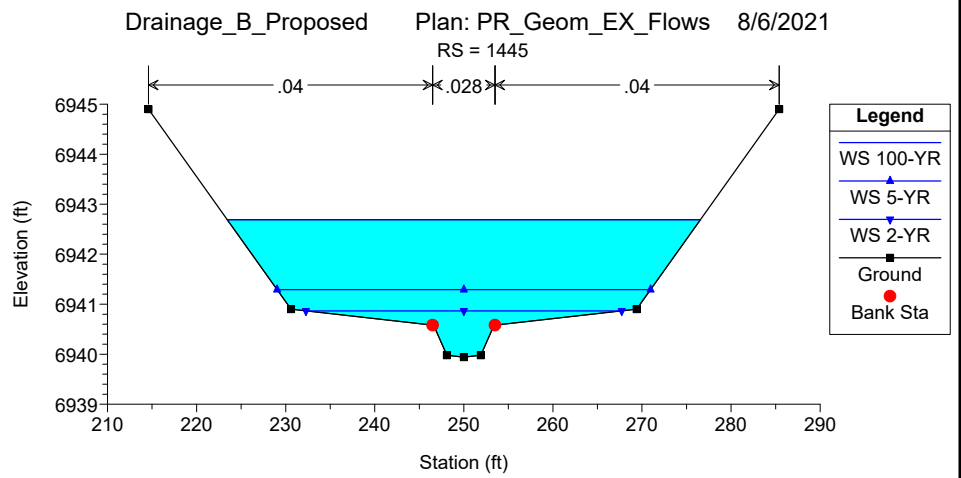
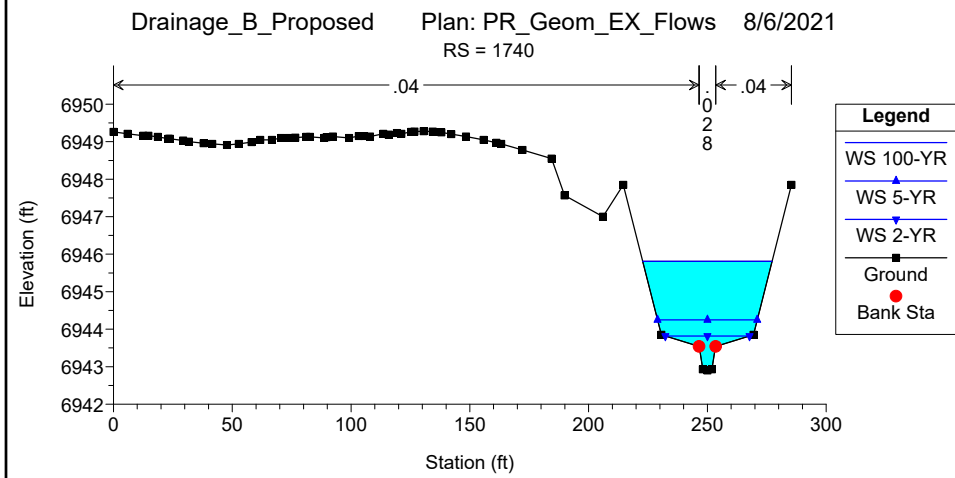
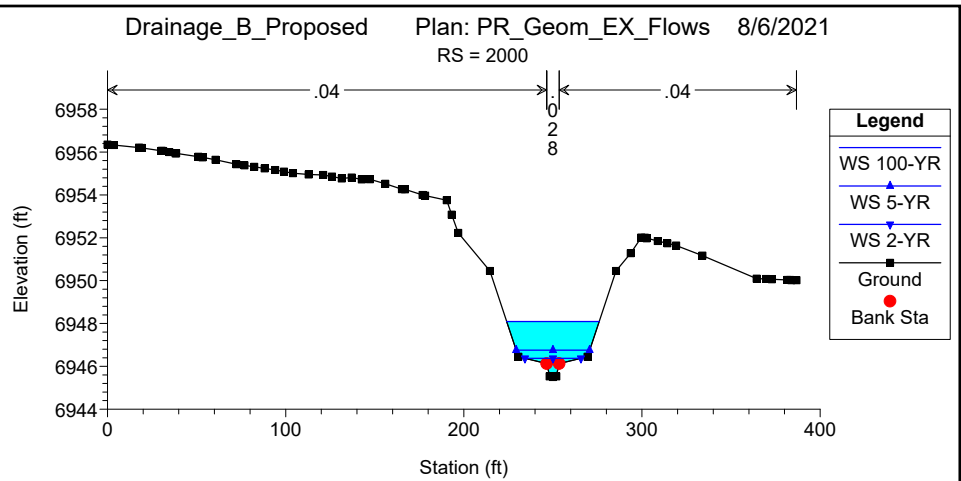
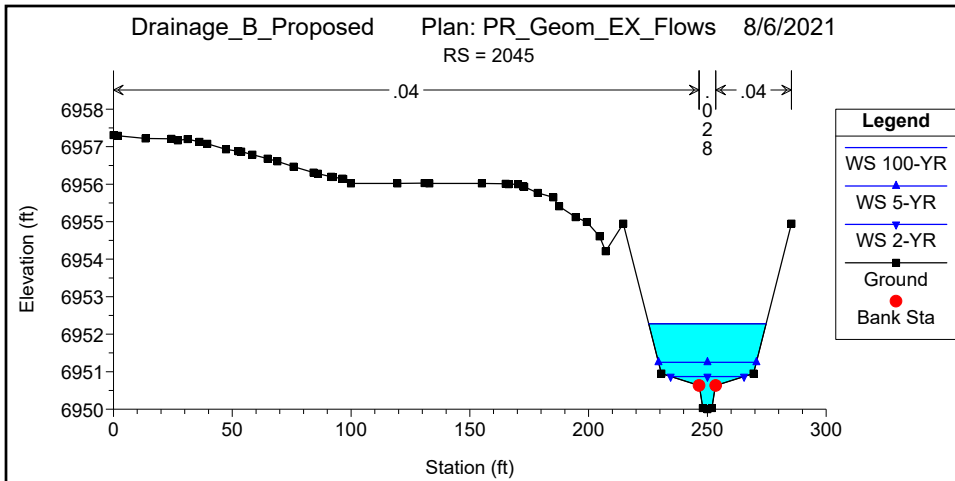


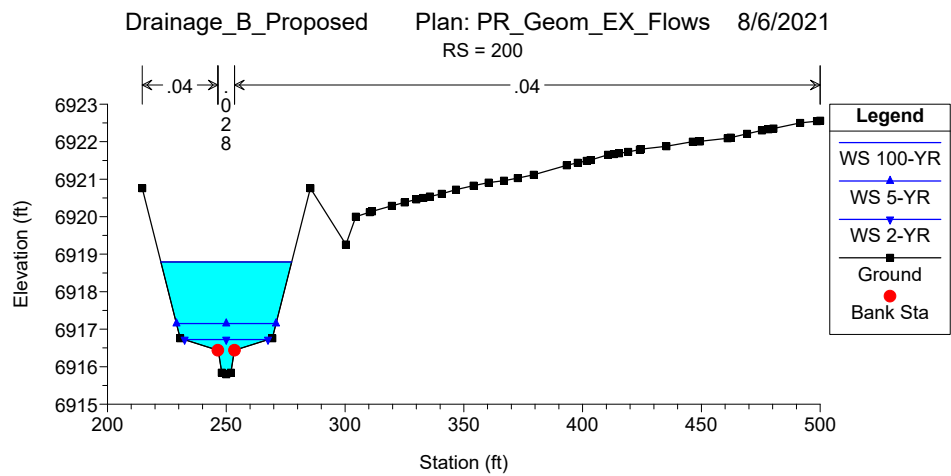
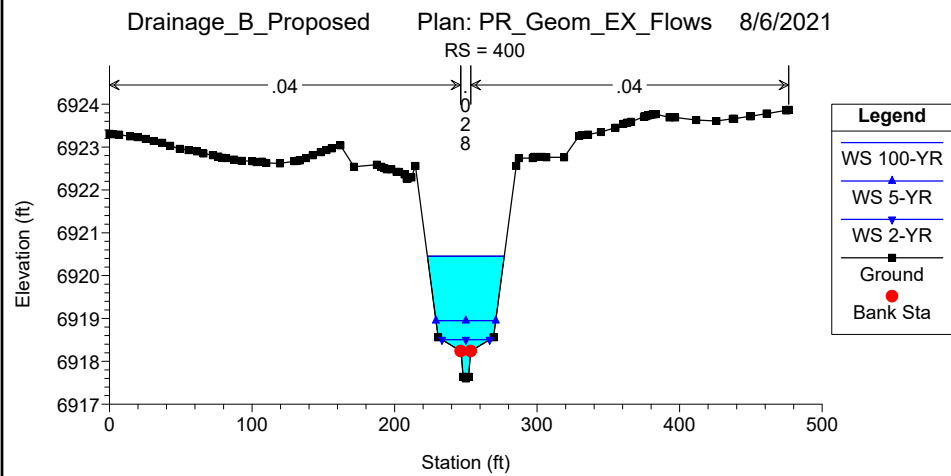
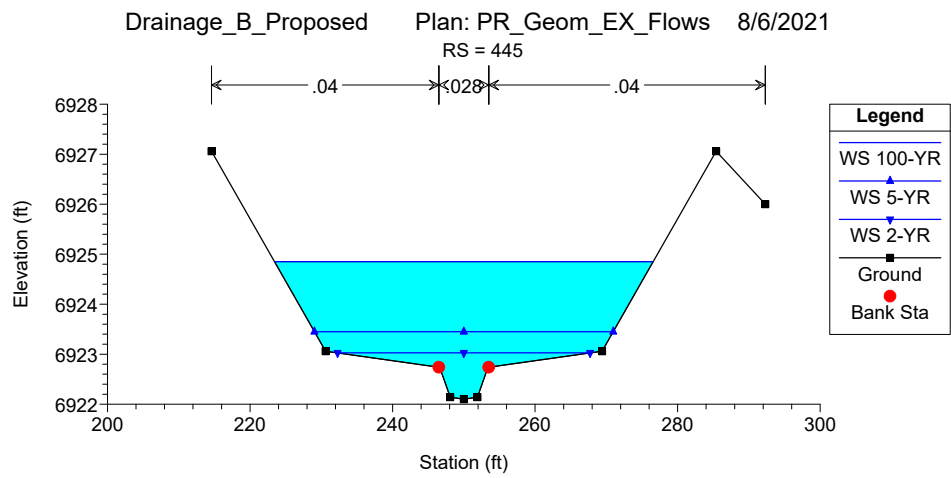
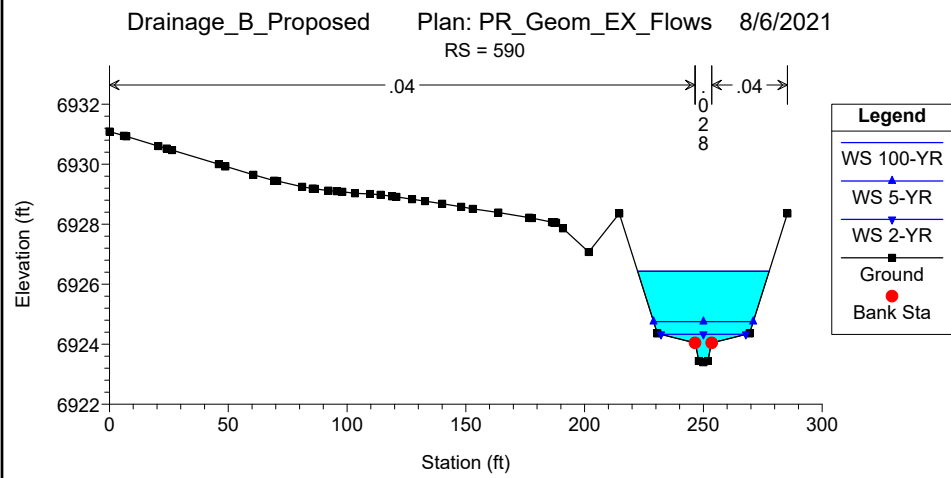
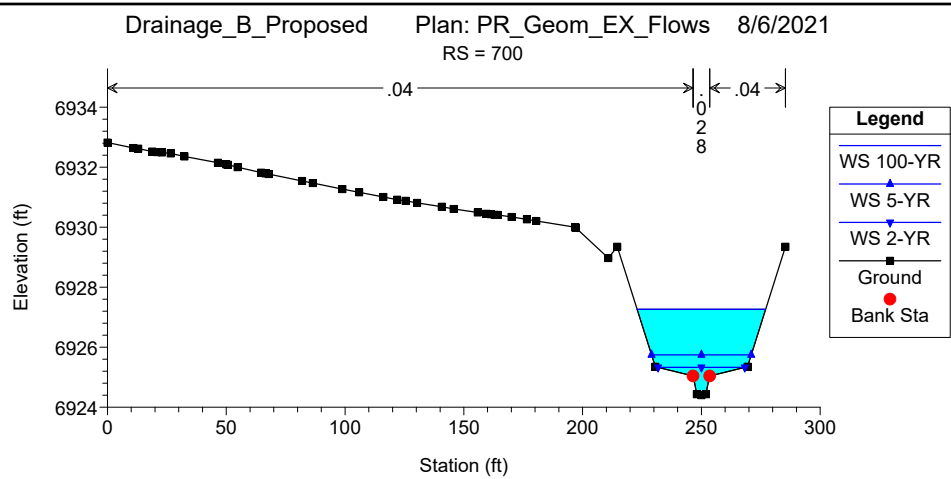
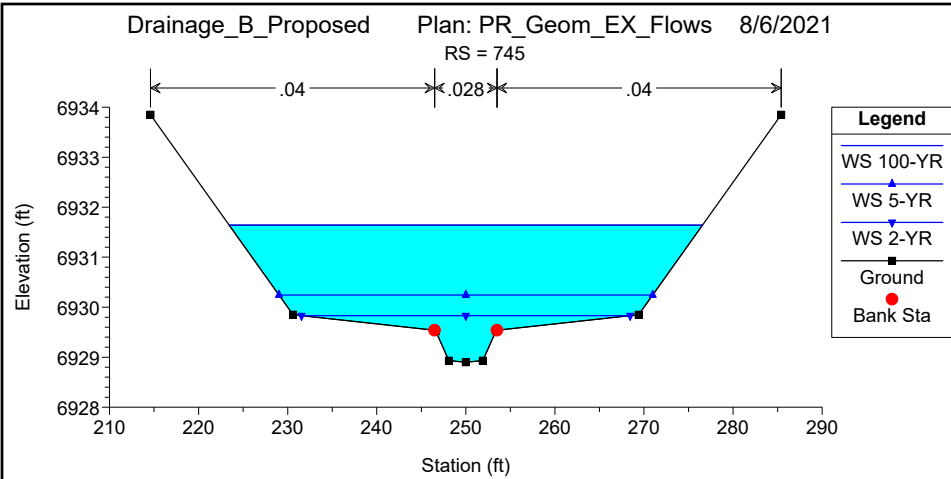






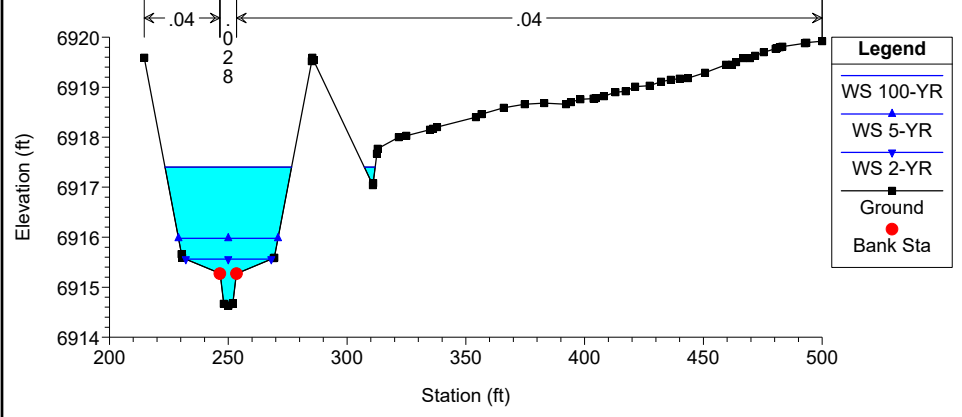








Drainage\_B\_Proposed Plan: PR\_Geom\_EX\_Flows 8/6/2021  
RS = 70.18





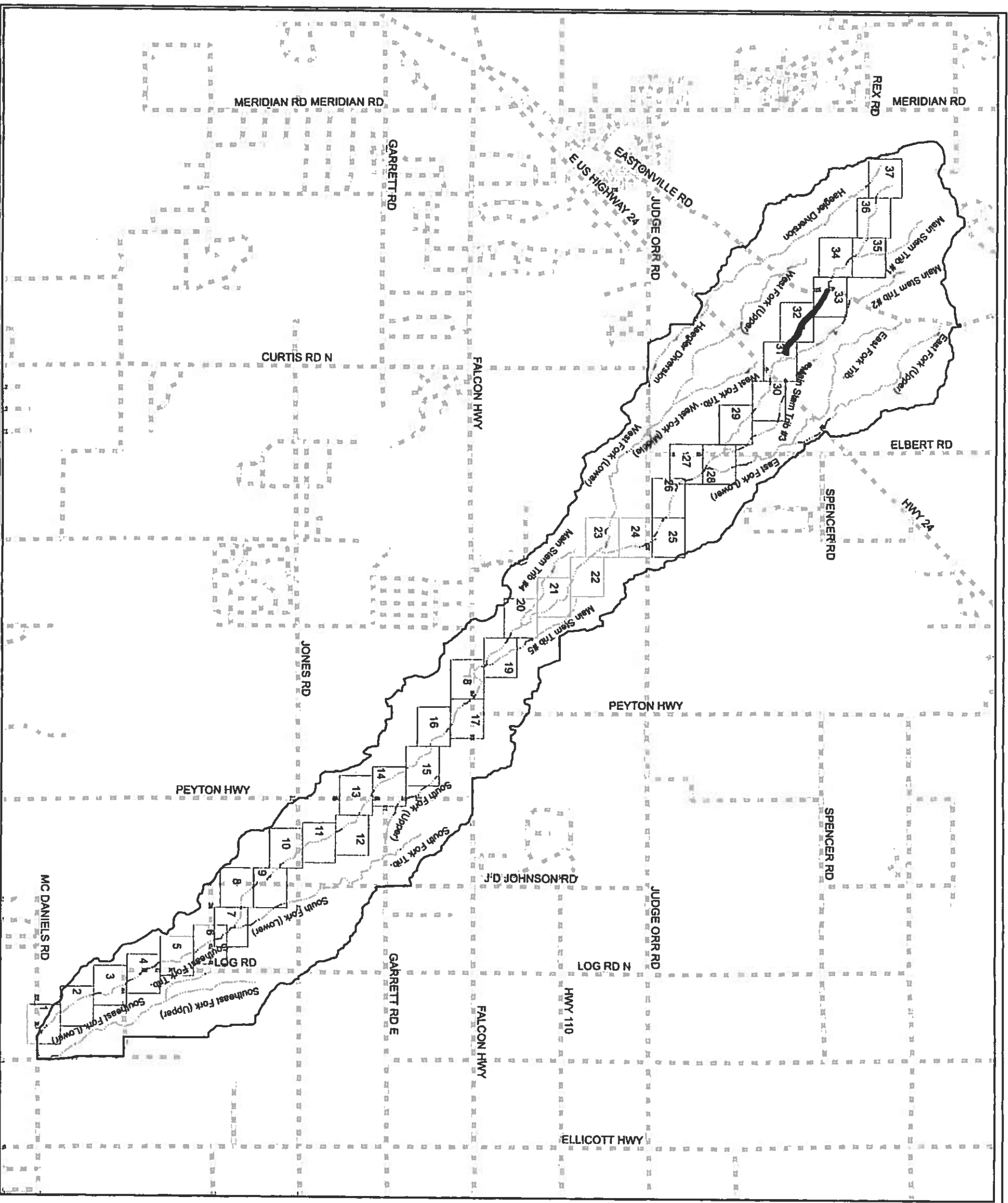
## Appendix G



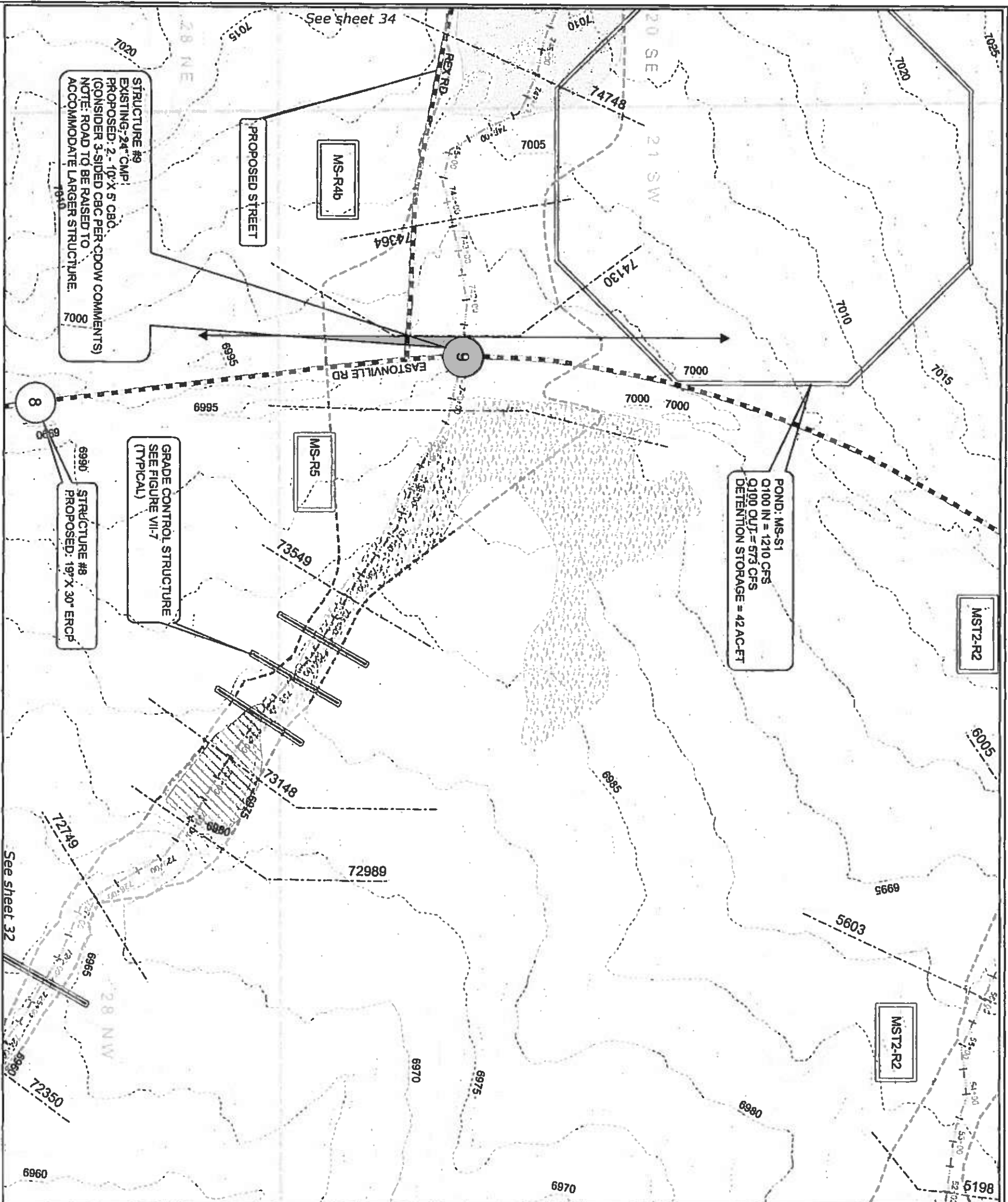
THIS DRAWING IS CONCEPTUAL IN NATURE AND IS NOT TO BE USED AS THE SOLE BASIS FOR FINAL DESIGN, CONSTRUCTION, OR REMEDIAL ACTION. FURTHER STUDIES UNDER EPC DOT'S DIRECTION SHOULD BE PERFORMED PRIOR TO SUCH DECISIONS.

**Legend**

- Streams
- Roads
- Basin Boundary
- Matchlines



<p><b>Drexel, Battell &amp; Co.</b> Engineers, Surveyors          1800 18TH STREET          315 7TH STREET          315 W. COLFAX STREET          COLORADO SPRINGS, COLORADO 80905 (719) 264-4444          GERRIT, COLORADO 80905 (719) 261-9444</p>	<p><b>REALTY DEVELOPMENT SERVICES</b>          25 NORTH TULSA STREET, SUITE 200          COLORADO SPRINGS, COLORADO 80905          CONTACT: NAY O'SULLIVAN (719) 277-1822</p>	<p><b>GIECK RANCH</b>          DRAINAGE BASIN PLANNING STUDY          EL PASO COUNTY, COLORADO</p>	<p>DATE: _____</p>
			<p>DESIGNED BY: RJB</p> <p>CHECKED BY: SLE</p> <p>DATE: _____</p>
<p><b>GIECK RANCH KEY MAP MAIN STEM</b></p>			<p>DATE: _____</p>
<p>SCALE: 1" = 5000'</p>	<p>DATE: AUGUST 2007</p>	<p>PROJECT NO: C7706-1</p>	<p>PLANT: PL</p>
<p>PROJECT NO: 6D 038</p>	<p>DATE: _____</p>	<p>PROJECT NO: _____</p>	<p>PLANT: K1</p>



POND: MS-S1  
 Q100 IN = 1210 CFS  
 Q100 OUT = 573 CFS  
 DETENTION STORAGE = 42 AC-FT

STRUCTURE #9  
 EXISTING-24" CMP  
 PROPOSED: 2-10' X 5' CBO  
 (CONSIDER 3-SIDED CBO PER CDOW COMMENTS)  
 NOTE: ROAD TO BE RAISED TO  
 ACCOMMODATE LARGER STRUCTURE.

STRUCTURE #8  
 PROPOSED: 19' X 30' ERCS

GRADE CONTROL STRUCTURE  
 SEE FIGURE VII-7  
 (TYPICAL)

**Drexel, Bartell & Co.** Engineers, Surveyors  
 1800 S. W. 10th Street  
 Suite 100, Colorado Springs, CO 80904  
 CONTACT: ROBERT BENNETT, P.E., CEM

**REALTY DEVELOPMENT SERVICES**  
 25 NORTH TEJON STREET, SUITE 300  
 COLORADO SPRINGS, COLORADO 80905  
 CONTACT: TONY O'NEILL, (719) 277-7122

**GIECK RANCH**  
 DRAINAGE BASIN PLANNING STUDY  
 EL PASO COUNTY, COLORADO

DATE	REVISION/DESCRIPTION	BY	CHKD BY
08/01/07	PRELIMINARY PLAN	RB	RB
08/01/07	REVISED PLAN	RB	RB
08/01/07	REVISED PLAN	RB	RB

**GIECK RANCH DBPS**  
 PLAN VIEW  
 MAIN STEM #33

DATE: AUGUST 2007  
 SCALE: 1" = 200'  
 SHEET: 6D 038  
 TOTAL SHEETS: 33

### Environmental Key

- Ponds
- Riparian: Good
- Riparian: Poor
- Potential Wetlands

The channel is considered dry unless shown as one of the above environmental categories.

### Legend

- Proposed Future Conditions 100-yr Flood Limits
- Streams
- Reaches
- Reach Breaklines
- Cross-sections
- Roads
- Structures
- Section Lines
- 5-ft contours
- 2-ft contours

### RECOMMENDED PLAN IMPROVEMENTS





Reach	Slope (%)	Q <sub>100</sub> (cfs)	V <sub>100</sub> (ft/s)
MS-R4b	1.76	1094	4.24
MS-R5	1.88	573	5.00

**Note:**  
 See Technical Addenda for grade control data.

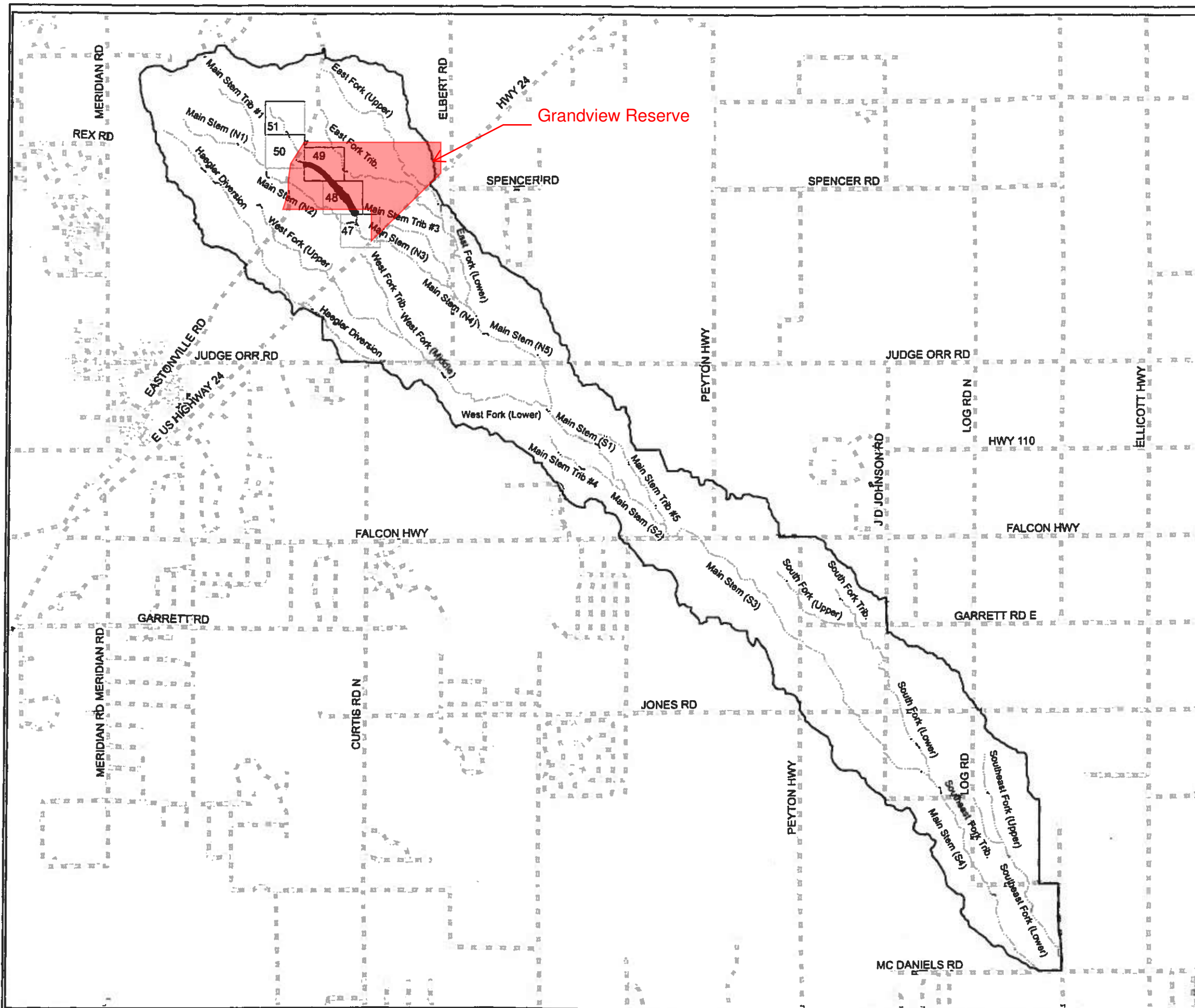
THIS DRAWING IS CONCEPTUAL IN NATURE AND IS NOT TO BE USED AS THE SOLE BASIS FOR FINAL DESIGN, CONSTRUCTION, OR REMEDIAL ACTION. FURTHER STUDIES UNDER EPC DOT'S DIRECTION SHOULD BE PERFORMED PRIOR TO SUCH DECISIONS.



# Legend

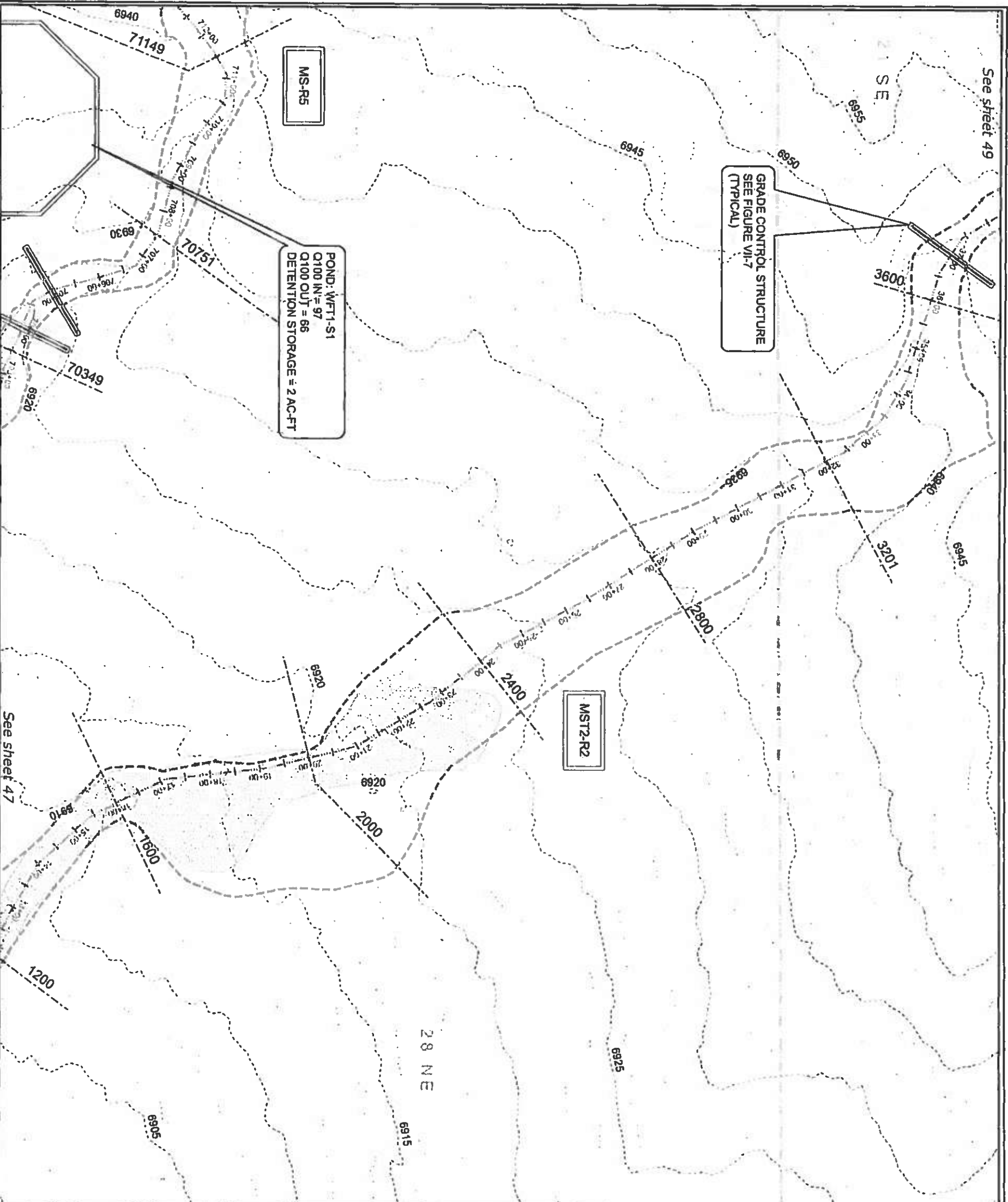
-  Streams
-  Roads
-  Basin Boundary
-  Matchlines

THIS DRAWING IS CONCEPTUAL IN NATURE AND IS NOT TO BE USED AS THE SOLE BASIS FOR FINAL DESIGN, CONSTRUCTION, OR REMEDIAL ACTION. FURTHER STUDIES UNDER EPC DOT'S DIRECTION SHOULD BE PERFORMED PRIOR TO SUCH DECISIONS.





See sheet 49



**Environmental Key**

- Ponds
- Riparian: Good
- Riparian: Poor
- Potential Wetlands

**Legend**

- Proposed Future Conditions 100-yr Flood Limits
- Streams
- Reaches
- Reach Breaklines
- Cross-sections
- Roads
- Structures
- Section Lines
- 5-ft contours
- 2-ft contours

The channel is considered dry unless shown as one of the above environmental categories.



Reach	Slope (%)	Q <sub>100</sub> (cfs)	V <sub>100</sub> (ft/s)
MST2-R2	1.93	271	3.16

**RECOMMENDED PLAN IMPROVEMENTS**  
 Reach MST2-R2 Vegetation Augmentation

**Note:**  
 See Technical Addenda for grade control data.  
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**Drexel Bartell & Co. Engineers - Surveyors**  
 1889 SPRING STREET  
 2517 W 11TH STREET  
 COLORADO SPRING, COLORADO 80904  
 CONTACT: ROBERT SEMNETT, P.E., CEM

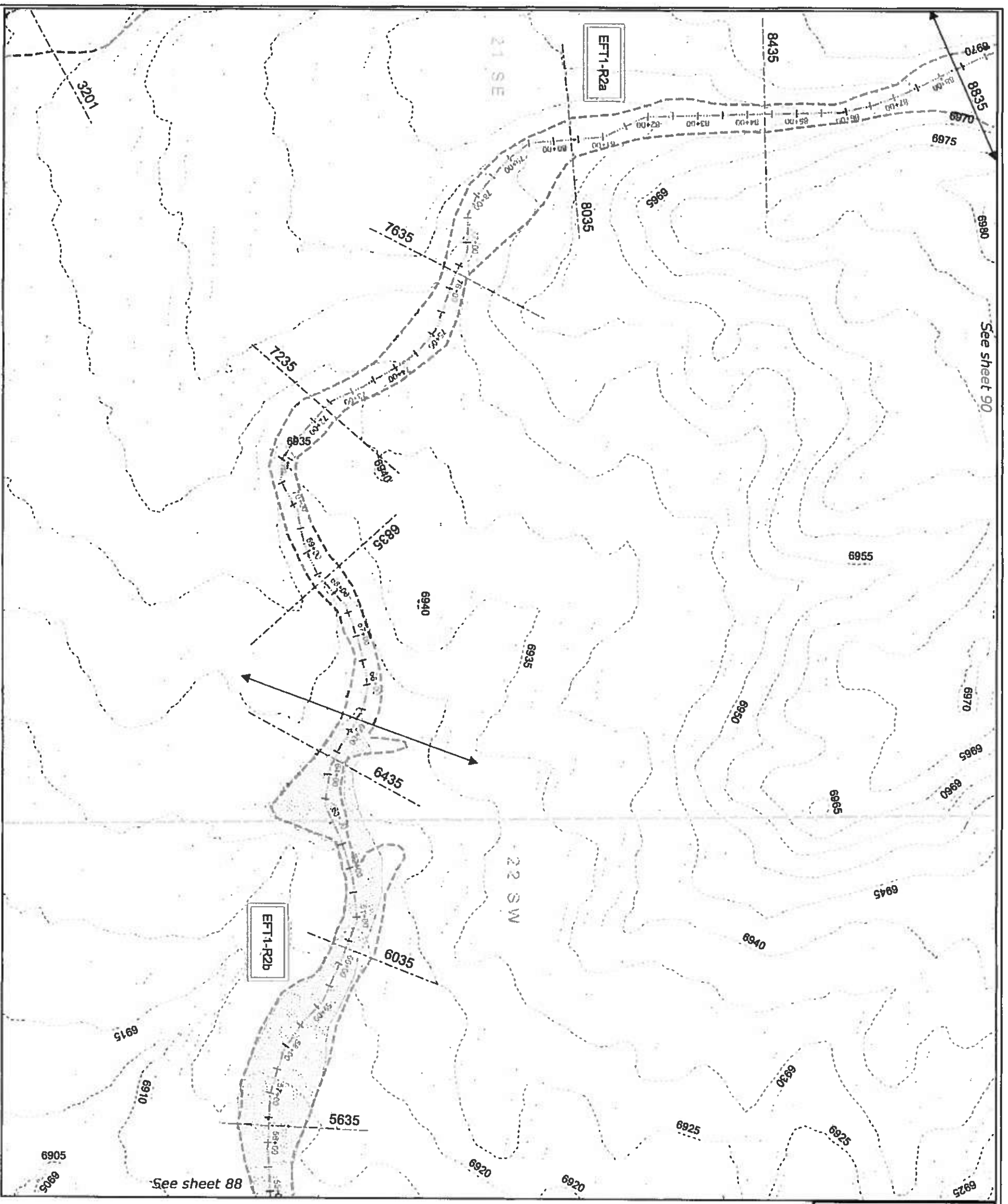
**REALTY DEVELOPMENT SERVICES**  
 25 HIGHLAND TERRACE, SUITE 200  
 COLORADO SPRING, COLORADO 80905  
 CONTACT: PAUL O'ROURKE, (719) 277-1822

**GIECK RANCH DRAINAGE BASIN PLANNING STUDY**  
 EL PASO COUNTY, COLORADO

DATE	REVISIONS	BY	FOR
JANUARY 2010	REGULAR UPDATE	R/S	FOR EPC DOT COUNTY
	THE EPC DOT CENTER	BUTSALAI	
			FOR EPC DOT CENTER
			FOR EPC DOT CENTER

**GIECK RANCH DBPS PLAN VIEW**  
 MAIN STEM TRIBUTARY-2 #2  
 DATE: AUGUST 2007  
 SCALE: 1" = 200'  
 DRAWING NO.: C7706-2  
 SHEET NO.: 48





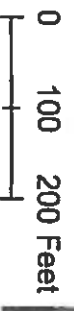
**Environmental Key**

- Ponds
- Riparian: Good
- Riparian: Poor
- Potential Wetlands

**Legend**

- Proposed Future Conditions 100-yr Flood Limits
- Streams
- Reaches
- Reach Breaklines
- Cross-sections
- Roads
- Structures
- Section Lines
- 5-ft contours
- 2-ft contours

The channel is considered dry unless shown as one of the above environmental categories.



Reach	Slope (%)	Q <sub>100</sub> (cfs)	V <sub>100</sub> (ft/s)
EFT1-R2a	1.83	217	3.73
EFT1-R2b	1.60	217	2.68

**RECOMMENDED PLAN IMPROVEMENTS**

- Reach EFT1-R2a As-needed Improvements
- Reach EFT1-R2b As-needed Improvements

THIS DRAWING IS CONCEPTUAL IN NATURE AND IS NOT TO BE USED AS THE SOLE BASIS FOR FINAL DESIGN, CONSTRUCTION, OR REMEDIAL ACTION. FURTHER STUDIES UNDER EPC DOT'S DIRECTION SHOULD BE PERFORMED PRIOR TO SUCH DECISIONS.

**Drexel, Bartell & Co. Engineers - Surveyors**  
 1315 NORTH STREET  
 SUITE 400  
 DENVER, CO 80202  
 CONTACT: ROBERT BENNETT, P.E. CFPS

**REALTY DEVELOPMENT SERVICES**  
 23 NORTH TEALON STREET, SUITE 200  
 COLORADO SPRING, COLORADO 80905  
 CONTACT: TONY SULLIVAN (719) 527-1022

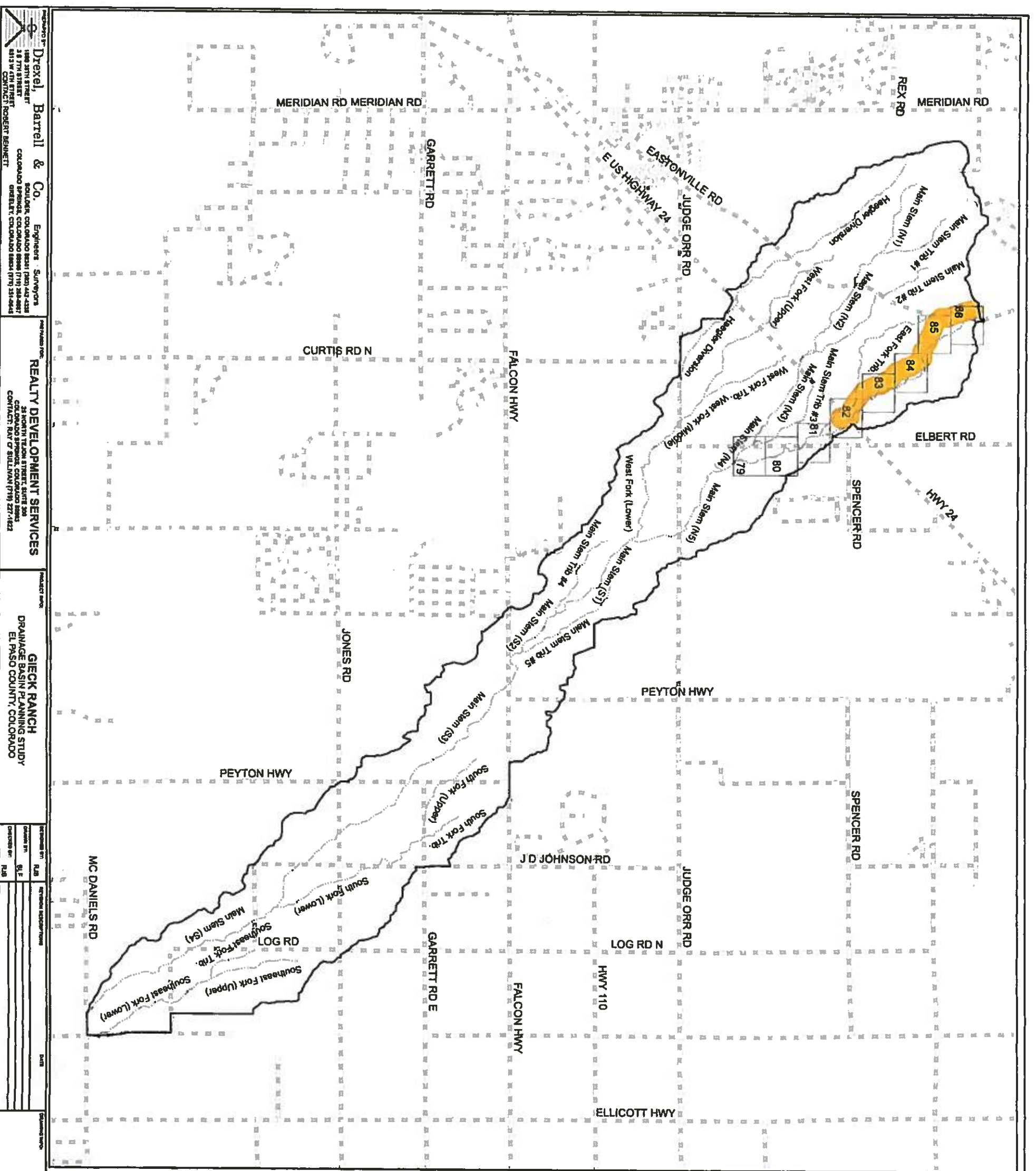
**GIECK RANCH**  
 DRAINAGE BASIN PLANNING STUDY  
 EL PASO COUNTY, COLORADO

DATE	BY	REVISION
JANUARY 2010	RJB	NETWORK REVISIONS
	ALJ	FINAL PLAN
	RJB	REVISION

**GIECK RANCH DBPS**  
 PLAN VIEW  
 EAST FORK TRIBUTARY #3

DATE: AUGUST 2007  
 SCALE: 1" = 200'  
 DRAWING NO: C7706-2  
 SHEET NO: 6D 038  
 TOTAL SHEETS: 89





**Drexel, Bartell & Co.** Engineers, Surveyors  
 1800 37th STREET  
 30 37th STREET  
 813 W 7th STREET  
 CONTACT: ROBERT BENNETT

**REALTY DEVELOPMENT SERVICES**  
 30 NORTH TULSA STREET, SUITE 200  
 COLORADO SPRINGS, COLORADO 80905  
 CONTACT: RAY C. SULLIVAN (719) 277-1622

**GIECK RANCH**  
 DRAINAGE BASIN PLANNING STUDY  
 EL PASO COUNTY, COLORADO

DATE	BY	REVISION

**GIECK RANCH**  
 KEY MAP  
 EAST FORK

DATE: AUGUST 2007  
 SCALE: 1" = 6000'  
 DRAWING NO.: C7706-1  
 SHEET NO.: 6D\_038  
 PROJECT NO.: K10

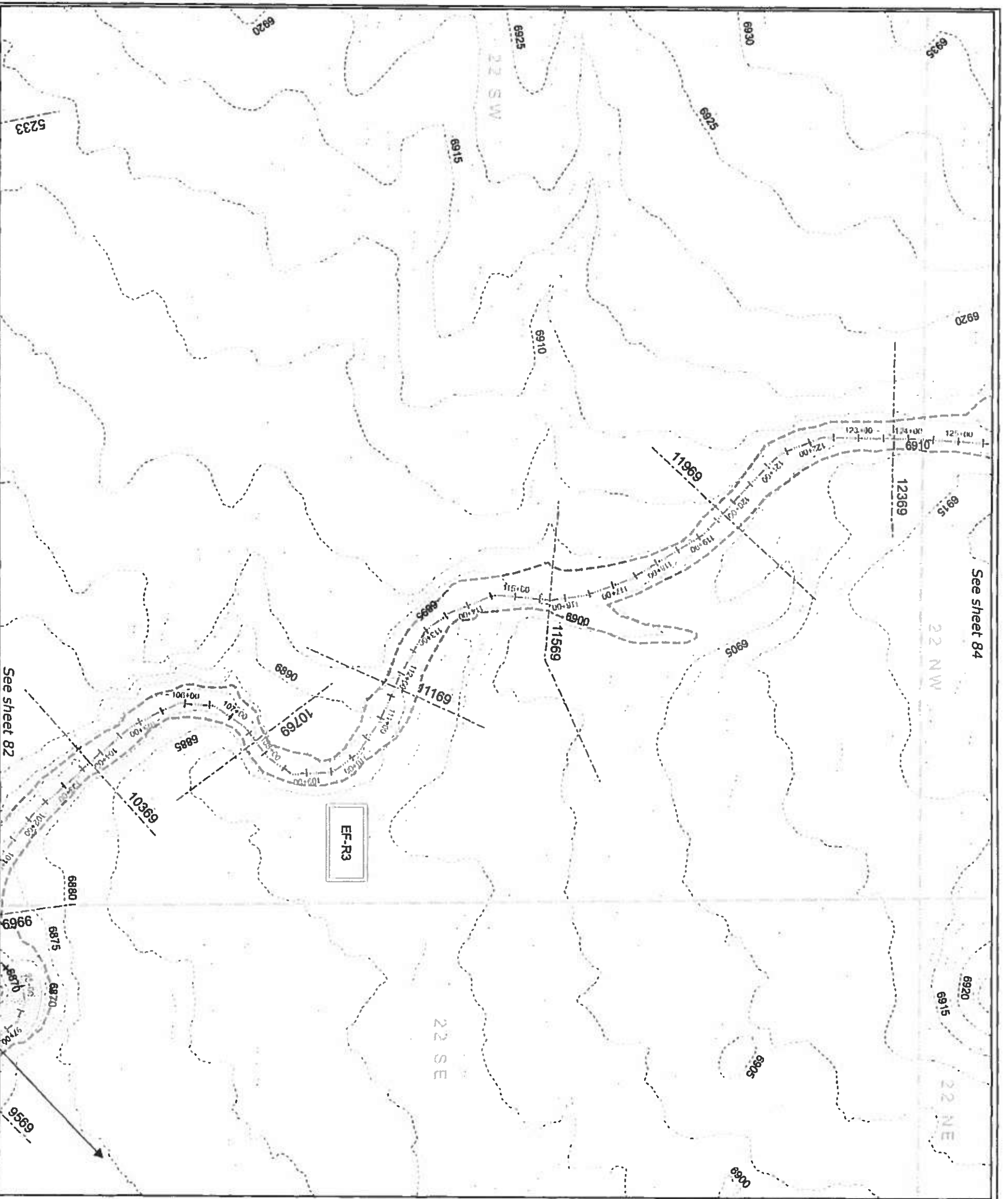


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**Legend**

- Roads
- Streams
- Basin Boundary
- Matchlines





**Environmental Key**

- Ponds
- Riparian: Good
- Riparian: Poor
- Potential Wetlands

The channel is considered dry unless shown as one of the above environmental categories.

**Legend**

- Proposed Future Conditions 100-yr Flood Limits
- Streams
- Reaches
- Reach Breaklines
- Cross-sections
- Roads
- Structures
- Section Lines
- 5-ft contours
- 2-ft contours

0 100 200 Feet

Reach	Slope (%)	Q <sub>100</sub> (cfs)	V <sub>100</sub> (ft/s)
EF-R3	1.53	595	5.09

**RECOMMENDED PLAN IMPROVEMENTS**

Reach EF-R3 As-needed Improvements

THIS DRAWING IS CONCEPTUAL IN NATURE AND IS NOT TO BE USED AS THE SOLE BASIS FOR FINAL DESIGN, CONSTRUCTION, OR REMEDIAL ACTION. FURTHER STUDIES UNDER EPC DOT'S DIRECTION SHOULD BE PERFORMED PRIOR TO SUCH DECISIONS.

**GIECK RANCH DBPS**  
PLAN VIEW  
EAST FORK #5

DATE: AUGUST 2007  
SCALE: 1" = 200'  
DRAWING NO.: C7706-2  
SHEET NO.: 6D 038

**Drexel, Bartell & Co.** Engineers - Surveyors  
1840 27TH STREET  
313 7TH STREET  
813 9TH STREET  
COLORADO SPRINGS, COLORADO 80905 (719) 285-0887  
CONTACT: ROBERT BENNETT, P.E.

**REALTY DEVELOPMENT SERVICES**  
20 NORTH TIAHO STREET, SUITE 200  
COLORADO SPRINGS, COLORADO 80905  
CONTACT: RAY O'SULLIVAN (719) 227-1022

**GIECK RANCH**  
DRAINAGE BASIN PLANNING STUDY  
EL PASO COUNTY, COLORADO

DESIGNED BY: RLB  
DRAWN BY: SLM/MLM  
CHECKED BY: RLB/MLM

DATE: AUGUST 2007  
SCALE: 1" = 200'  
DRAWING NO.: C7706-2  
SHEET NO.: 6D 038

DATE: AUGUST 2007  
SCALE: 1" = 200'  
DRAWING NO.: C7706-2  
SHEET NO.: 6D 038



# Channel Report

## East Fork Tributary 1 Reach 3 - Proposed Channel\_Capacity

### Trapezoidal

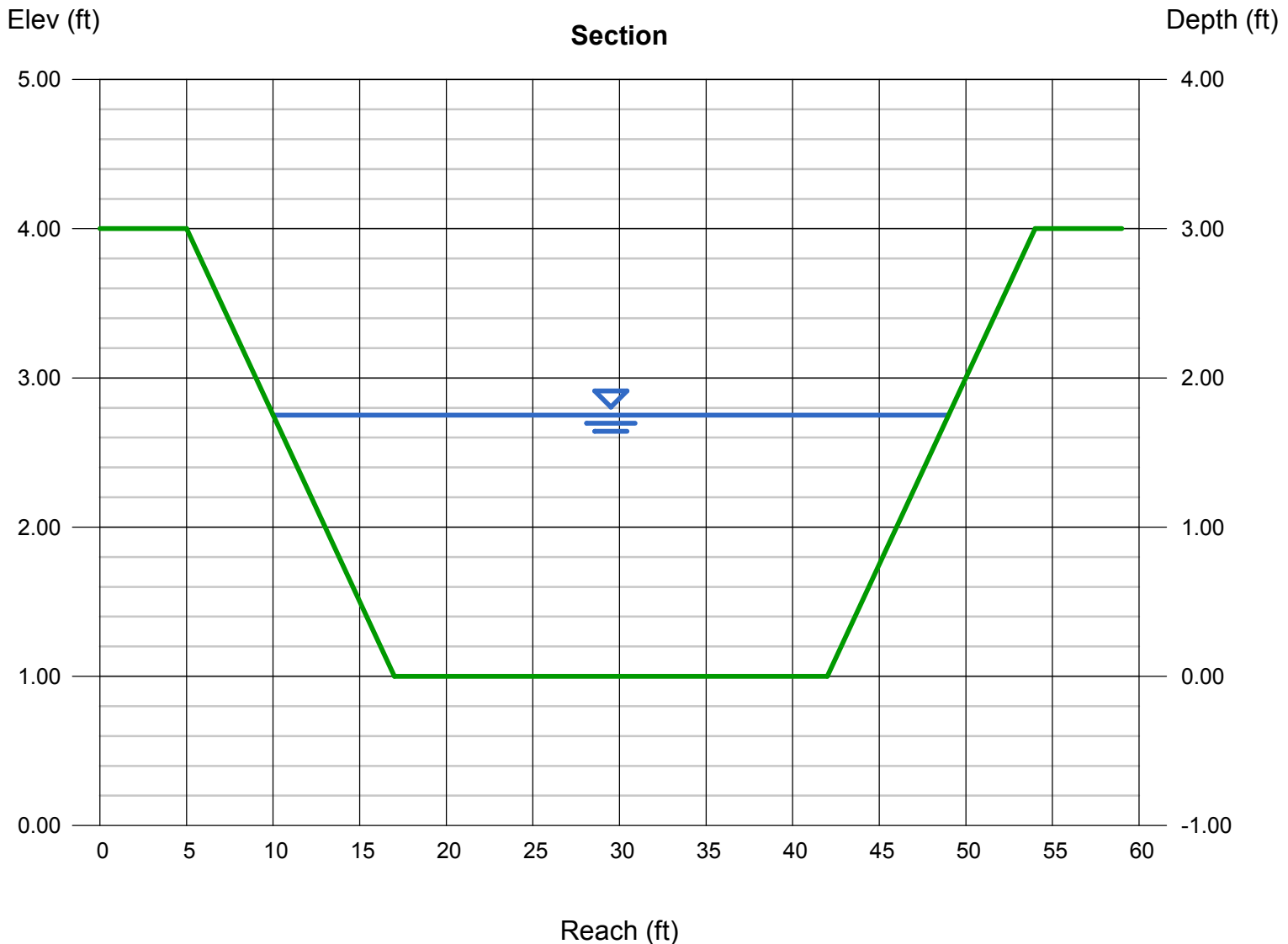
Bottom Width (ft) = 25.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 3.00  
Invert Elev (ft) = 1.00  
Slope (%) = 0.69  
N-Value = 0.040

### Highlighted

Depth (ft) = 1.75  
Q (cfs) = 217.00  
Area (sqft) = 56.00  
Velocity (ft/s) = 3.88  
Wetted Perim (ft) = 39.43  
Crit Depth, Yc (ft) = 1.24  
Top Width (ft) = 39.00  
EGL (ft) = 1.98

### Calculations

Compute by: Known Q  
Known Q (cfs) = 217.00



# Channel Report

## East Fork Tributary 1 Reach 3 - Proposed Channel\_Velocity

### Trapezoidal

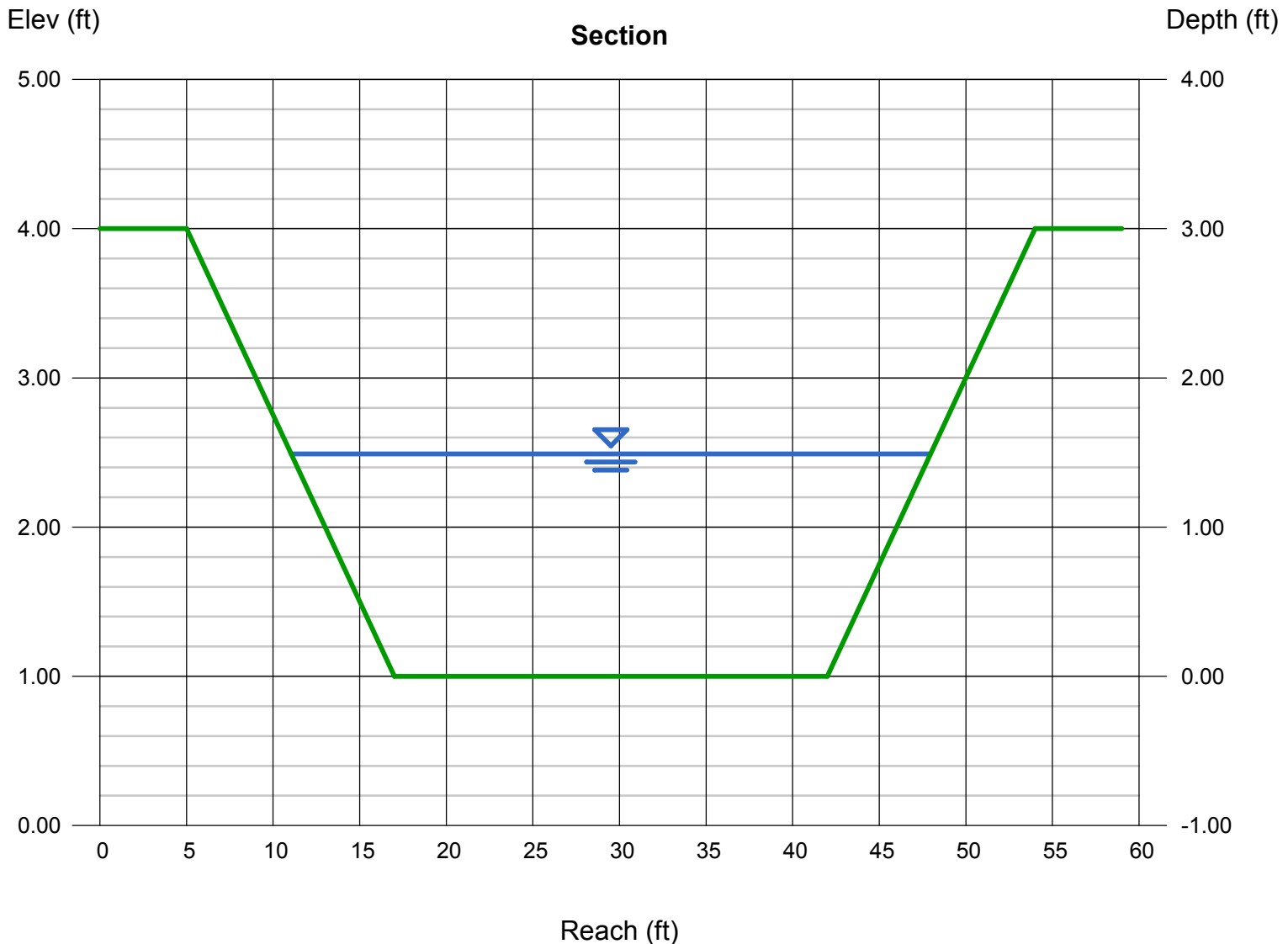
Bottom Width (ft) = 25.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 3.00  
Invert Elev (ft) = 1.00  
Slope (%) = 0.69  
N-Value = 0.030

### Highlighted

Depth (ft) = 1.49  
Q (cfs) = 217.00  
Area (sqft) = 46.13  
Velocity (ft/s) = 4.70  
Wetted Perim (ft) = 37.29  
Crit Depth, Yc (ft) = 1.24  
Top Width (ft) = 36.92  
EGL (ft) = 1.83

### Calculations

Compute by: Known Q  
Known Q (cfs) = 217.00



# Channel Report

## East Fork Tributary 1 Reach 2 - Proposed Channel\_Capacity

### Trapezoidal

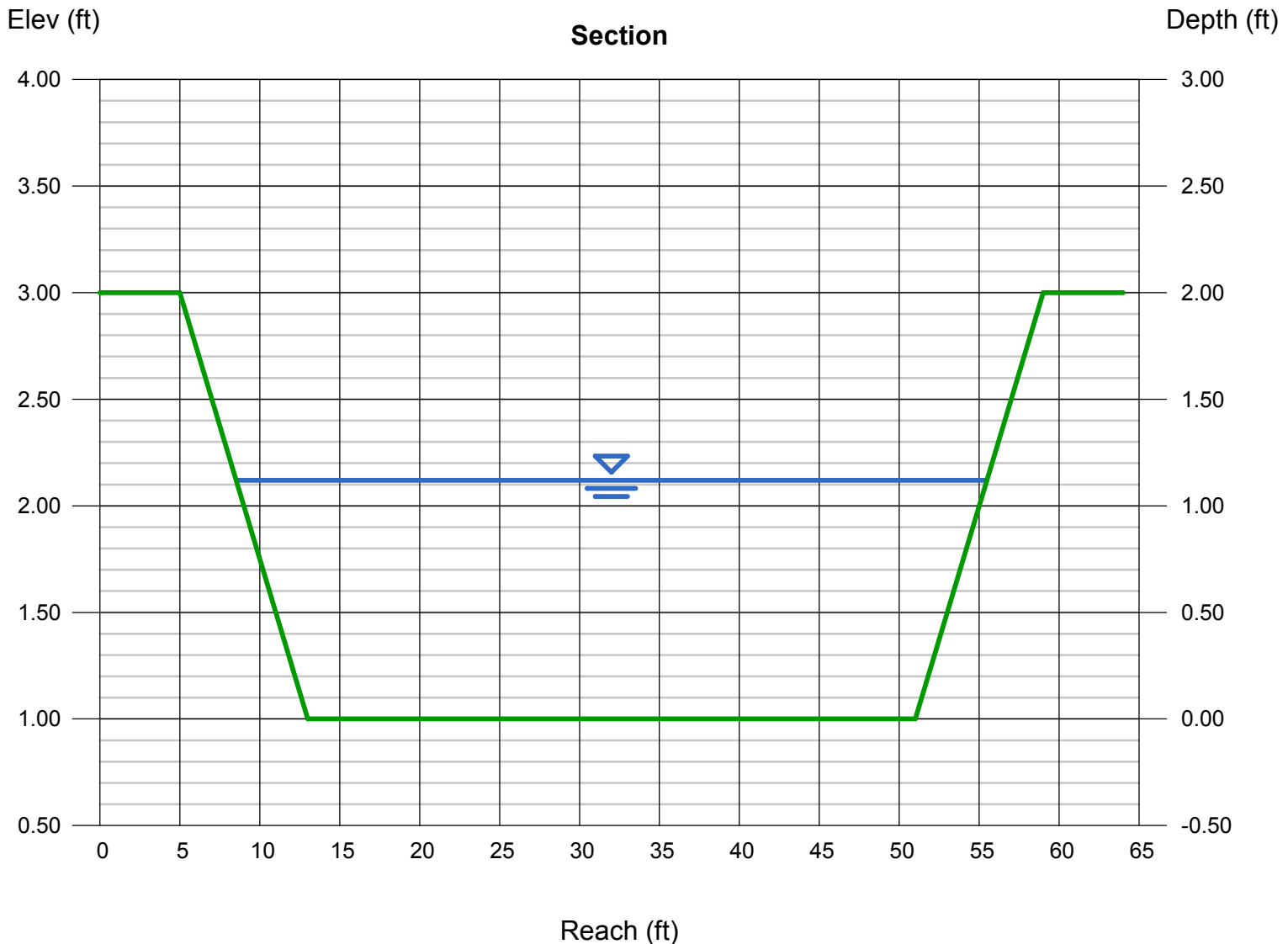
Bottom Width (ft) = 38.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 1.58  
N-Value = 0.050

### Highlighted

Depth (ft) = 1.12  
Q (cfs) = 177.00  
Area (sqft) = 47.58  
Velocity (ft/s) = 3.72  
Wetted Perim (ft) = 47.24  
Crit Depth, Yc (ft) = 0.86  
Top Width (ft) = 46.96  
EGL (ft) = 1.34

### Calculations

Compute by: Known Q  
Known Q (cfs) = 177.00



# Channel Report

## East Fork Tributary 1 Reach 2 - Proposed Channel\_Velocity

### Trapezoidal

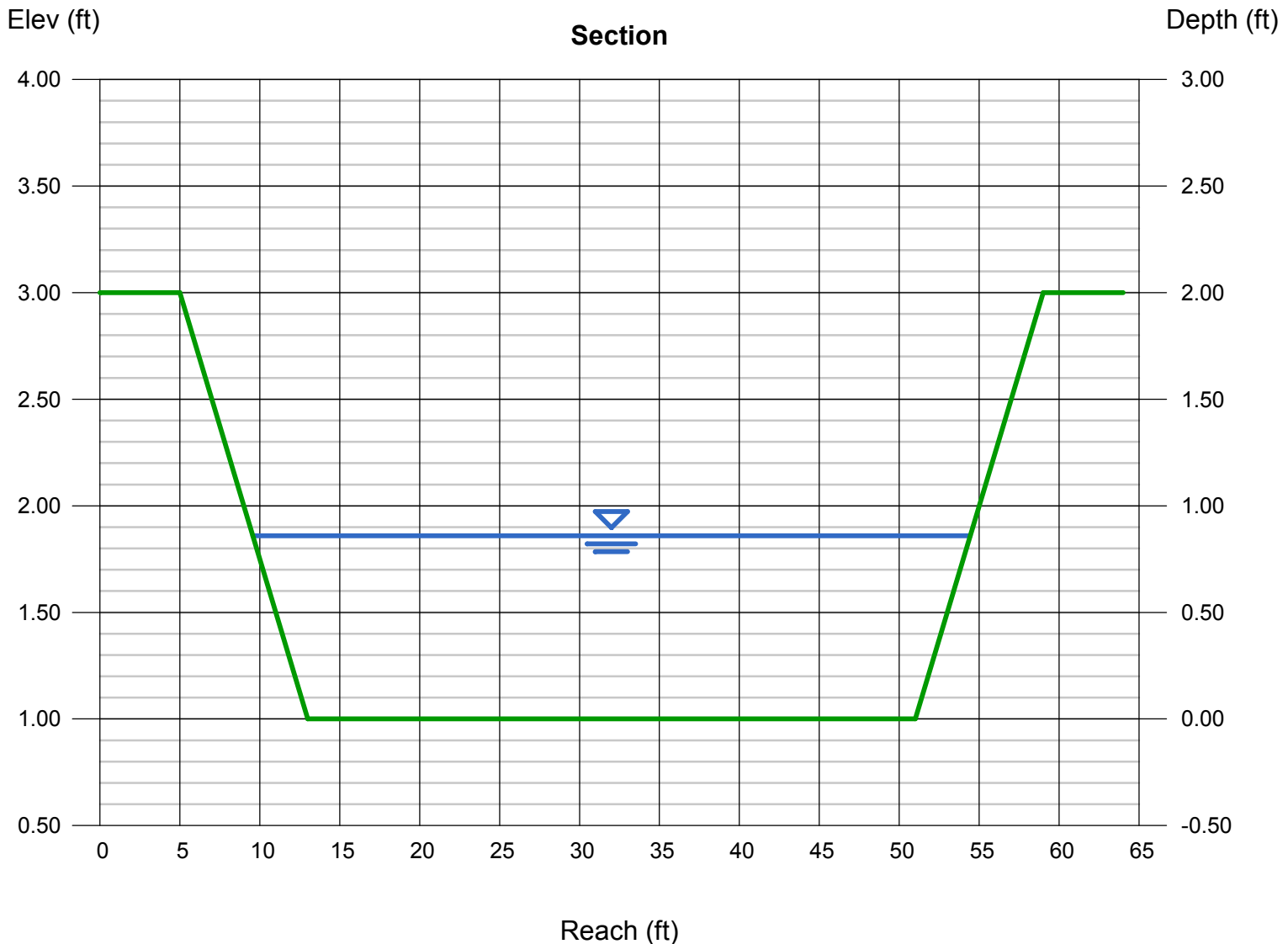
Bottom Width (ft) = 38.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 1.58  
N-Value = 0.032

### Highlighted

Depth (ft) = 0.86  
Q (cfs) = 177.00  
Area (sqft) = 35.64  
Velocity (ft/s) = 4.97  
Wetted Perim (ft) = 45.09  
Crit Depth, Yc (ft) = 0.86  
Top Width (ft) = 44.88  
EGL (ft) = 1.24

### Calculations

Compute by: Known Q  
Known Q (cfs) = 177.00



# Channel Report

Main Stem Trib 2

## Gieck Ranch Tributary 2 - Proposed Channel Section Capacity Check

### Trapezoidal

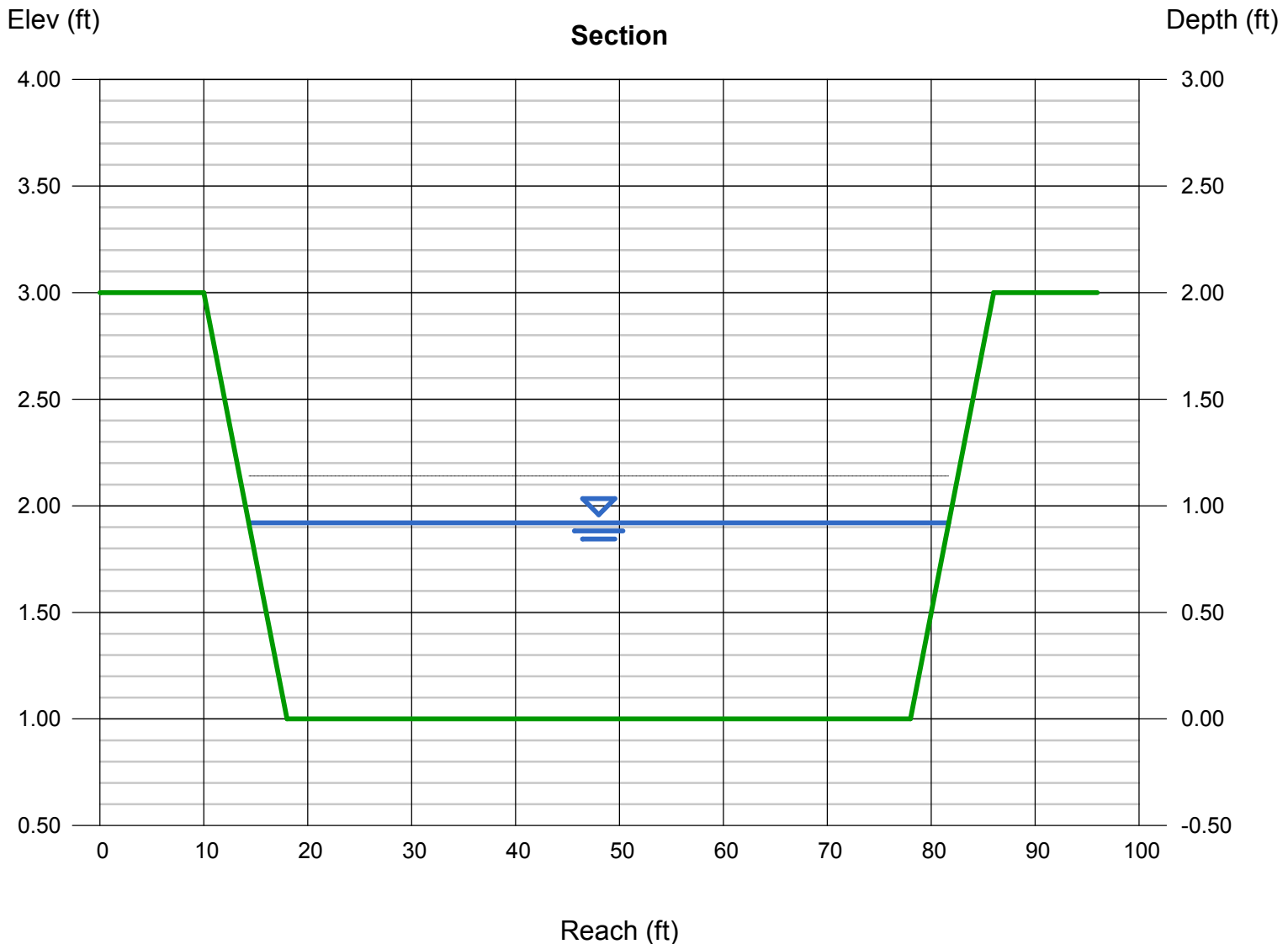
Bottom Width (ft) = 60.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 2.00  
N-Value = 0.050

### Highlighted

Depth (ft) = 0.92  
Q (cfs) = 220.00  
Area (sqft) = 58.59  
Velocity (ft/s) = 3.76  
Wetted Perim (ft) = 67.59  
Crit Depth, Yc (ft) = 0.74  
Top Width (ft) = 67.36  
EGL (ft) = 1.14

### Calculations

Compute by: Known Q  
Known Q (cfs) = 220.00





# Channel Report

Main Stem Trib 2

## Gieck Ranch Tributary 2 - Proposed Channel Section Velocity Check

### Trapezoidal

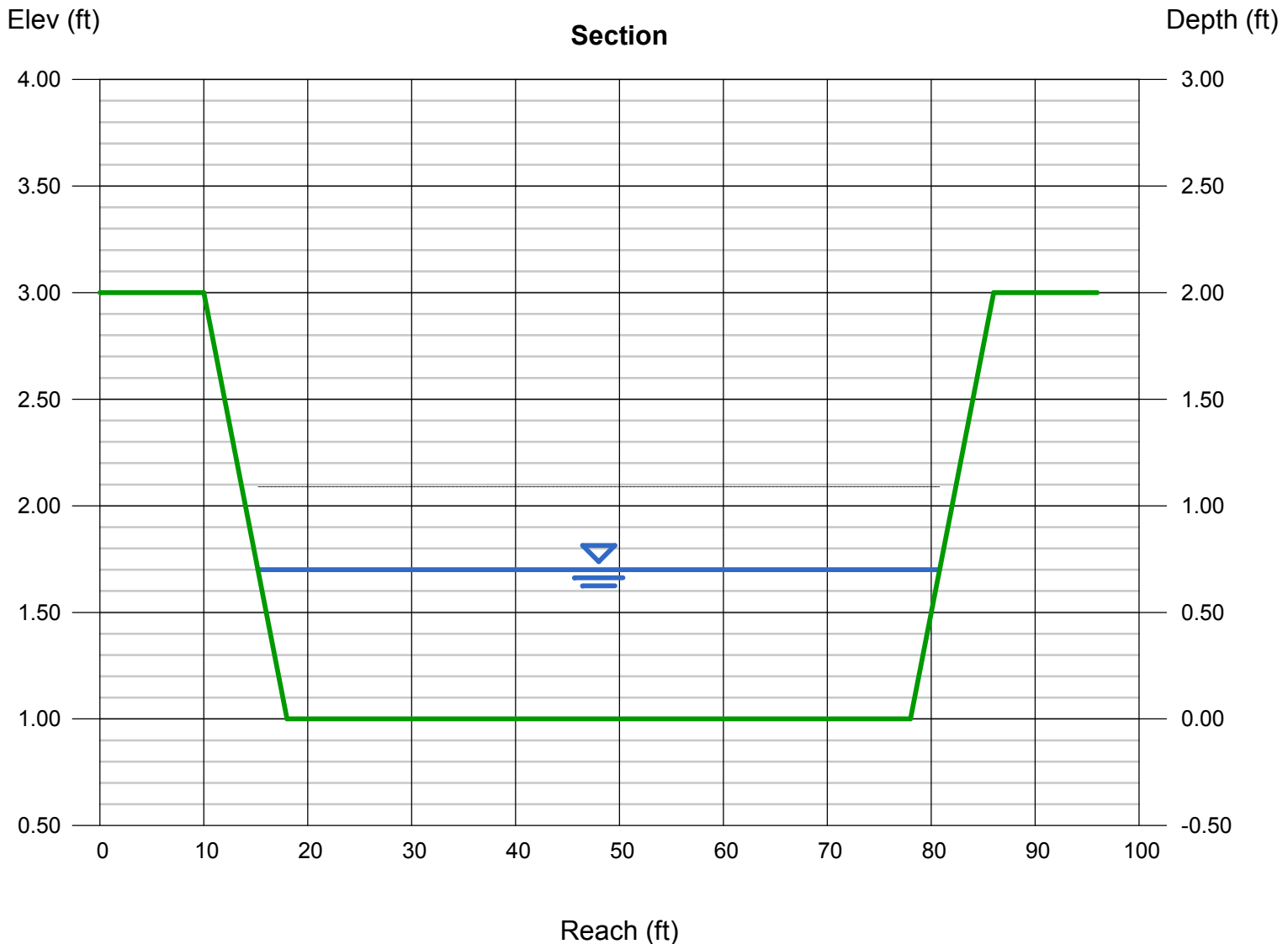
Bottom Width (ft) = 60.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 2.00  
N-Value = 0.032

### Highlighted

Depth (ft) = 0.70  
Q (cfs) = 220.00  
Area (sqft) = 43.96  
Velocity (ft/s) = 5.00  
Wetted Perim (ft) = 65.77  
Crit Depth, Yc (ft) = 0.74  
Top Width (ft) = 65.60  
EGL (ft) = 1.09

### Calculations

Compute by: Known Q  
Known Q (cfs) = 220.00



# Channel Report

## Gieck Ranch Tributary 2 Reach 1 - Proposed Channel Section Capacity Check

Main Stem

### Trapezoidal

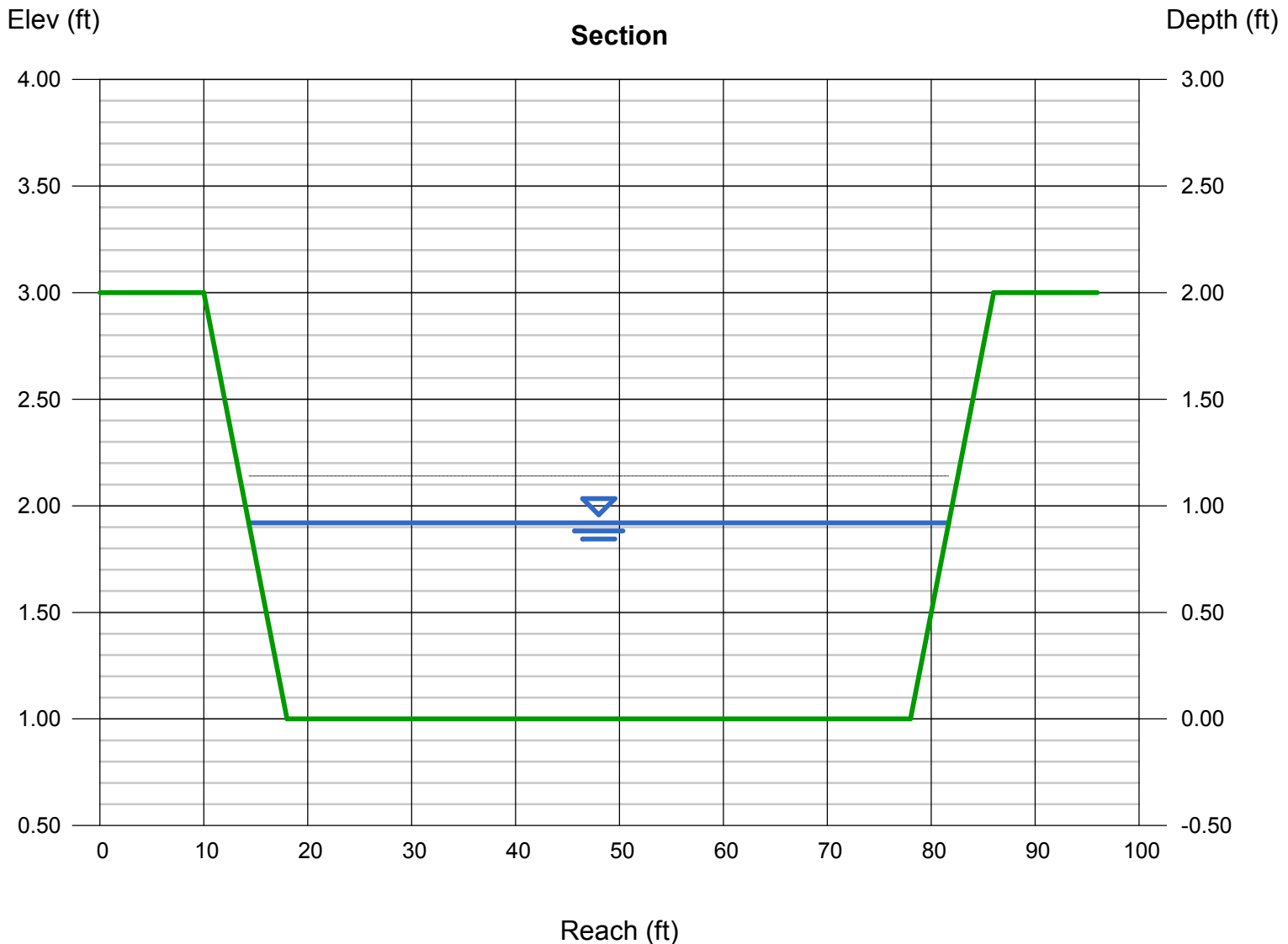
Bottom Width (ft) = 60.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 2.00  
N-Value = 0.050

### Highlighted

Depth (ft) = 0.92  
Q (cfs) = 220.00  
Area (sqft) = 58.59  
Velocity (ft/s) = 3.76  
Wetted Perim (ft) = 67.59  
Crit Depth, Yc (ft) = 0.74  
Top Width (ft) = 67.36  
EGL (ft) = 1.14

### Calculations

Compute by: Known Q  
Known Q (cfs) = 220.00



# Channel Report

## Gieck Ranch Tributary 2 Reach 1 - Proposed Channel Section Velocity Check

Main Stem

### Trapezoidal

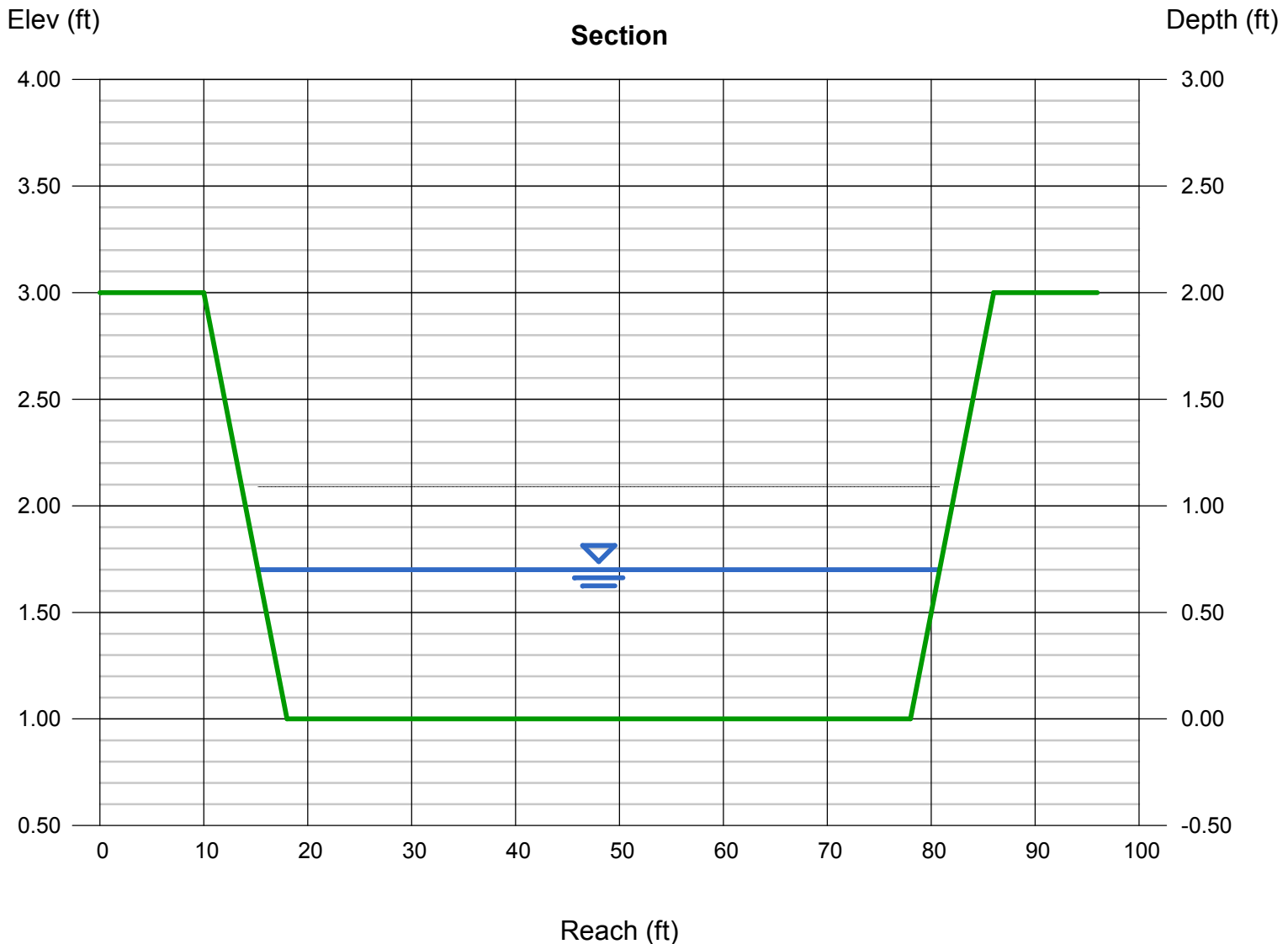
Bottom Width (ft) = 60.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 2.00  
N-Value = 0.032

### Highlighted

Depth (ft) = 0.70  
Q (cfs) = 220.00  
Area (sqft) = 43.96  
Velocity (ft/s) = 5.00  
Wetted Perim (ft) = 65.77  
Crit Depth, Yc (ft) = 0.74  
Top Width (ft) = 65.60  
EGL (ft) = 1.09

### Calculations

Compute by: Known Q  
Known Q (cfs) = 220.00



# Channel Report

## Gieck Ranch Tributary 2 Reach 2 - Proposed Channel Section Capacity Check

Main Stem

### Trapezoidal

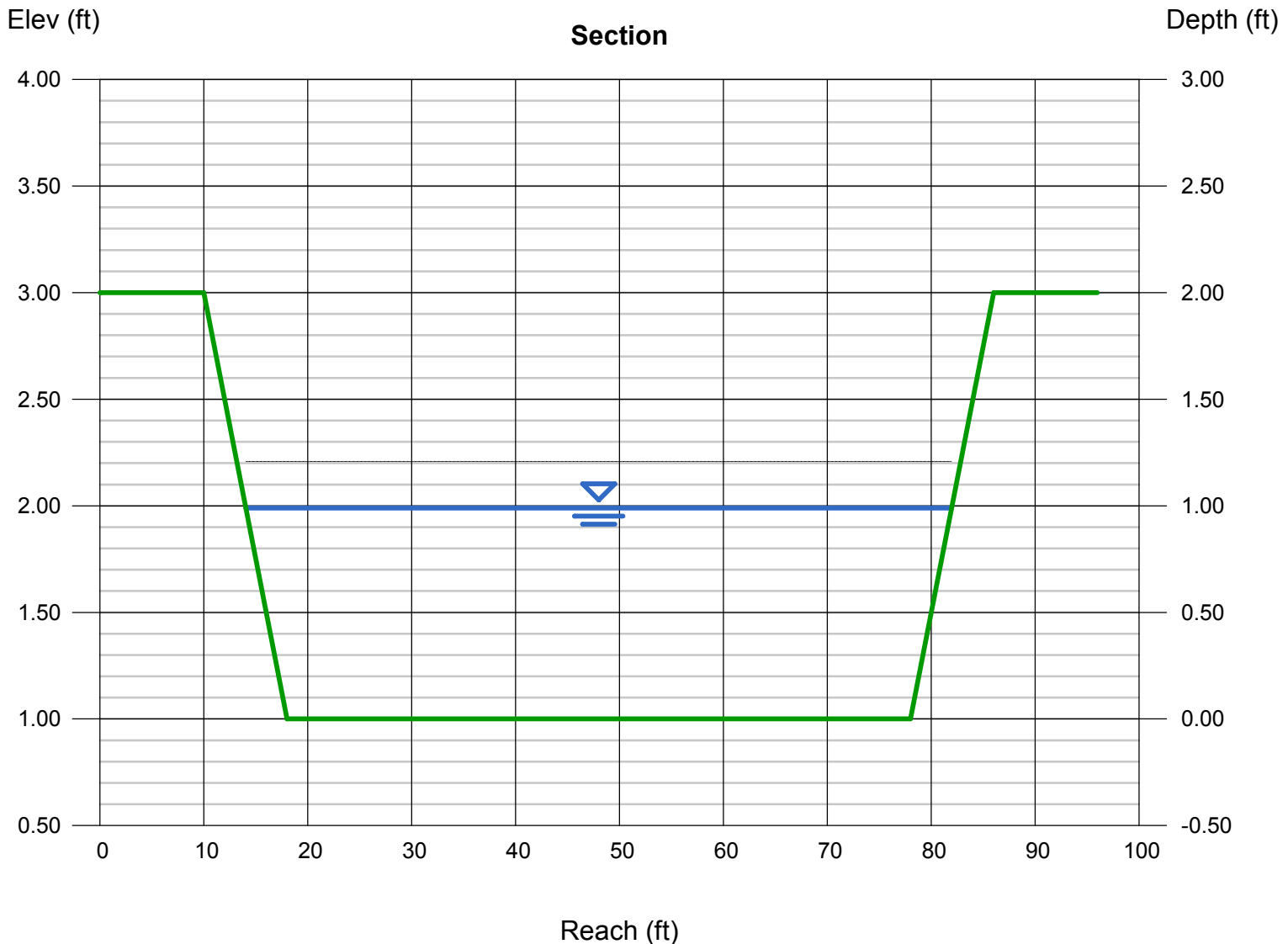
Bottom Width (ft) = 60.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 1.80  
N-Value = 0.050

### Highlighted

Depth (ft) = 0.99  
Q (cfs) = 237.00  
Area (sqft) = 63.32  
Velocity (ft/s) = 3.74  
Wetted Perim (ft) = 68.16  
Crit Depth, Yc (ft) = 0.78  
Top Width (ft) = 67.92  
EGL (ft) = 1.21

### Calculations

Compute by: Known Q  
Known Q (cfs) = 237.00



# Channel Report

## Gieck Ranch Tributary 2\_Reach 2 - Proposed Channel Section Velocity Check

### Trapezoidal

Main Stem

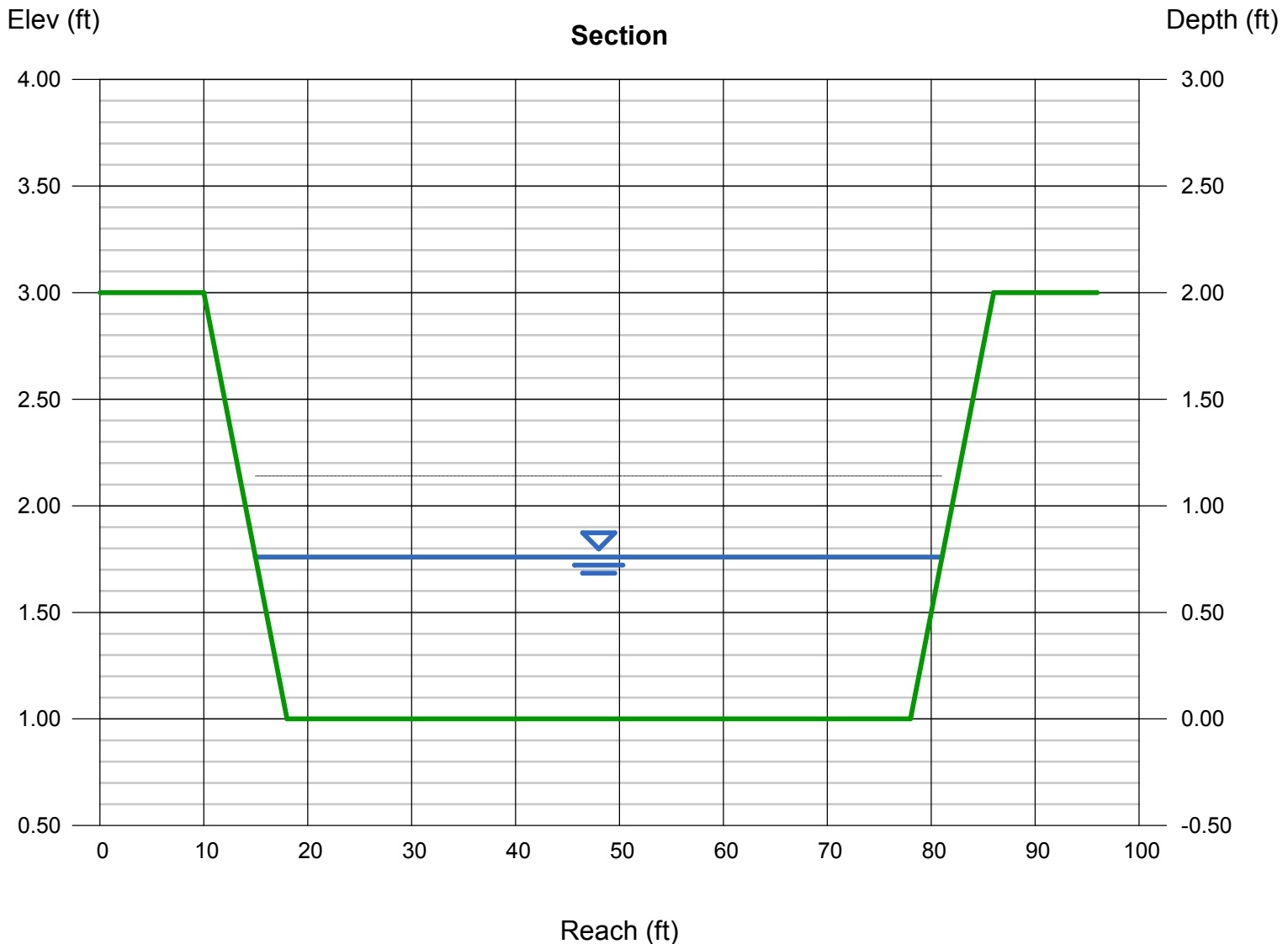
Bottom Width (ft) = 60.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 1.00  
Slope (%) = 1.80  
N-Value = 0.032

### Highlighted

Depth (ft) = 0.76  
Q (cfs) = 237.00  
Area (sqft) = 47.91  
Velocity (ft/s) = 4.95  
Wetted Perim (ft) = 66.27  
Crit Depth, Yc (ft) = 0.78  
Top Width (ft) = 66.08  
EGL (ft) = 1.14

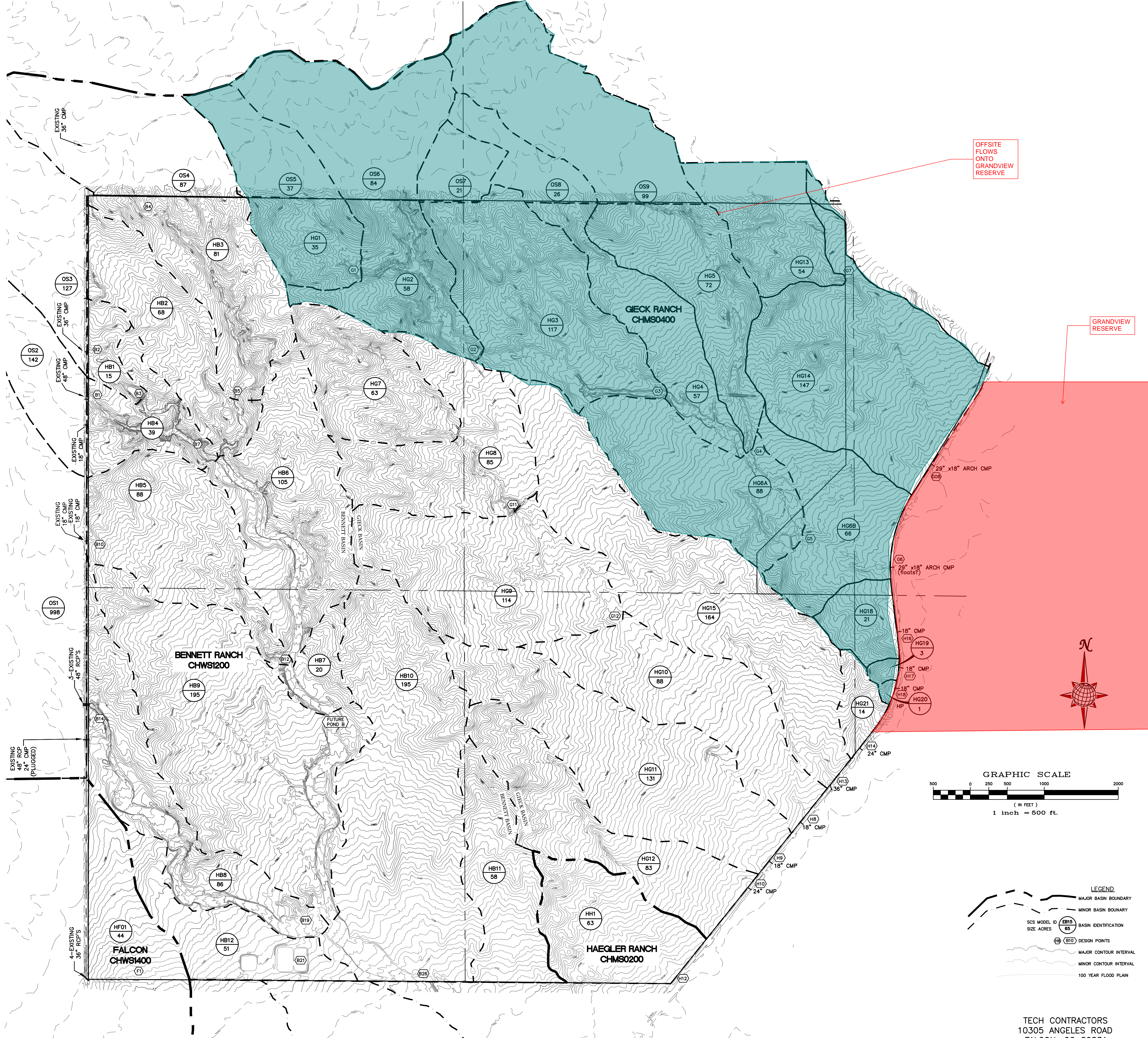
### Calculations

Compute by: Known Q  
Known Q (cfs) = 237.00



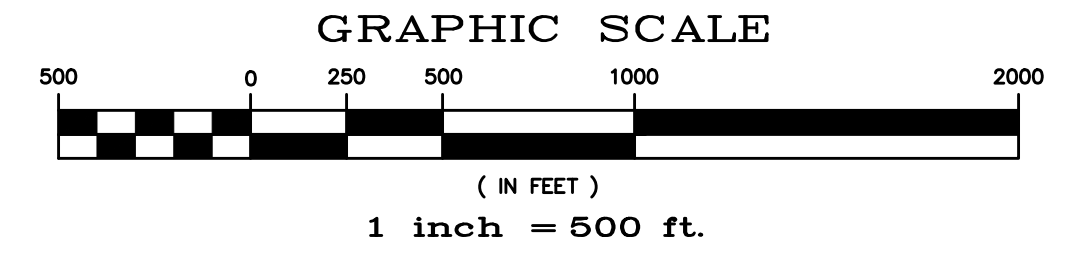


# MASTER DEVELOPMENT DRAINAGE PLAN MERIDIAN RANCH



OFFSITE  
FLOWS  
ONTO  
GRANDVIEW  
RESERVE

GRANDVIEW  
RESERVE



**LEGEND**

- MAJOR BASIN BOUNDARY
- MINOR BASIN BOUNDARY
- SCS MODEL ID (EB15 65) BASIN IDENTIFICATION  
SIZE ACRES
- (B10) DESIGN POINTS
- MAJOR CONTOUR INTERVAL
- MINOR CONTOUR INTERVAL
- 100 YEAR FLOOD PLAIN

TECH CONTRACTORS  
10305 ANGELES ROAD  
FALCON, CO 80831  
TELEPHONE: 719.495.7444  
FAX: 719.495.7608

**HISTORIC CONDITIONS - SCS MAP**

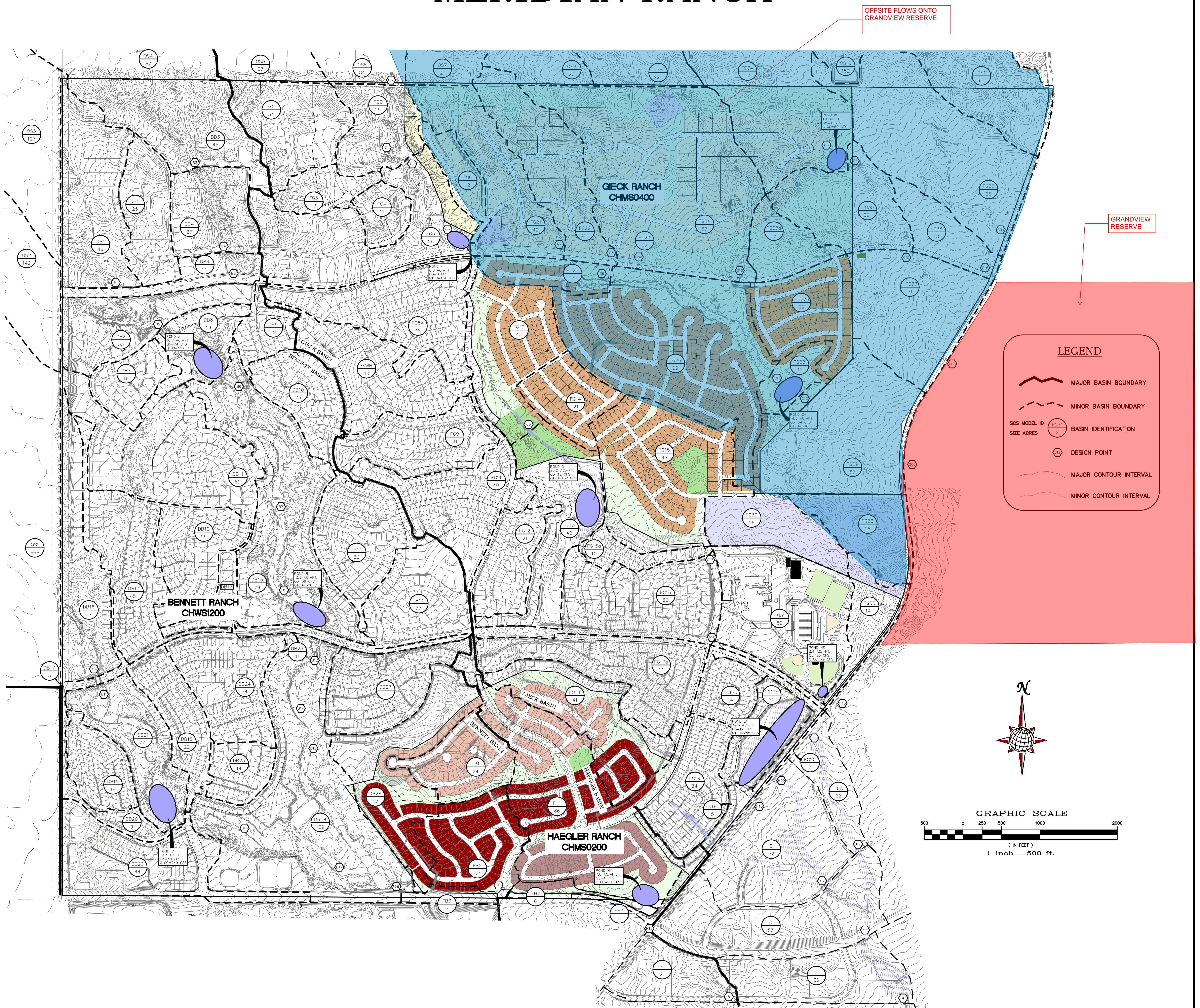
AUG 2017

FIGURE 4

S:\Chp\Proj\Meridian Ranch\_MDDP.dwg; Plan Sheets\2017\_ADDP\_HIST.dwg; IRS\_SCS\_MAP\_8/17/2017 10:59:19 AM



# MASTER DEVELOPMENT DRAINAGE PLAN MERIDIAN RANCH



\*NOTE: PRELIMINARY STORAGE VOLUMES AND OUTFLOW QUANTITIES HAVE BEEN PROVIDED FOR EACH OF THE FUTURE DETENTION FACILITIES LOCATED WITHIN THE DEVELOPMENT. THE ACTUAL STORAGE VOLUMES AND DISCHARGE RATES WILL BE DETERMINED UPON A COMPLETE ANALYSIS FOR EACH DETENTION FACILITY PRIOR TO CONSTRUCTION. THE VALUES GIVEN FOR DISCHARGE AND VOLUME ARE ESTIMATES FOR PLANNING PURPOSES ONLY.

## DEVELOPED CONDITIONS - SCS MAP

TECH CONTRACTORS  
10305 ANGELES ROAD  
FALCON, CO 80831  
TELEPHONE: 719.495.7444  
FAX: 719.495.7608

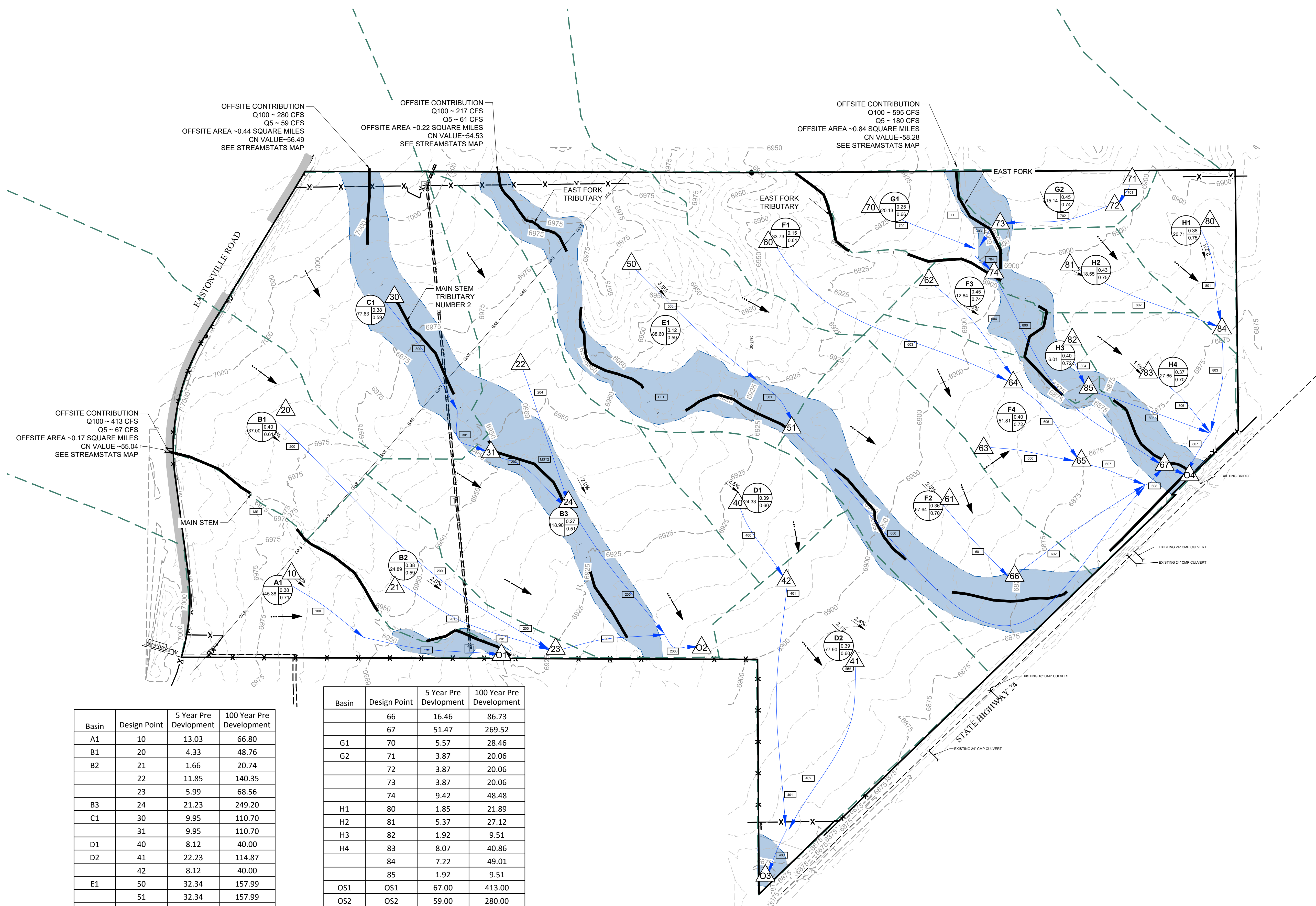
NOV 2017

FIGURE 5





## Appendix H



OFFSITE CONTRIBUTION  
Q100 ~ 280 CFS  
Q5 ~ 59 CFS  
OFFSITE AREA ~0.44 SQUARE MILES  
CN VALUE ~56.49  
SEE STREAMSTATS MAP

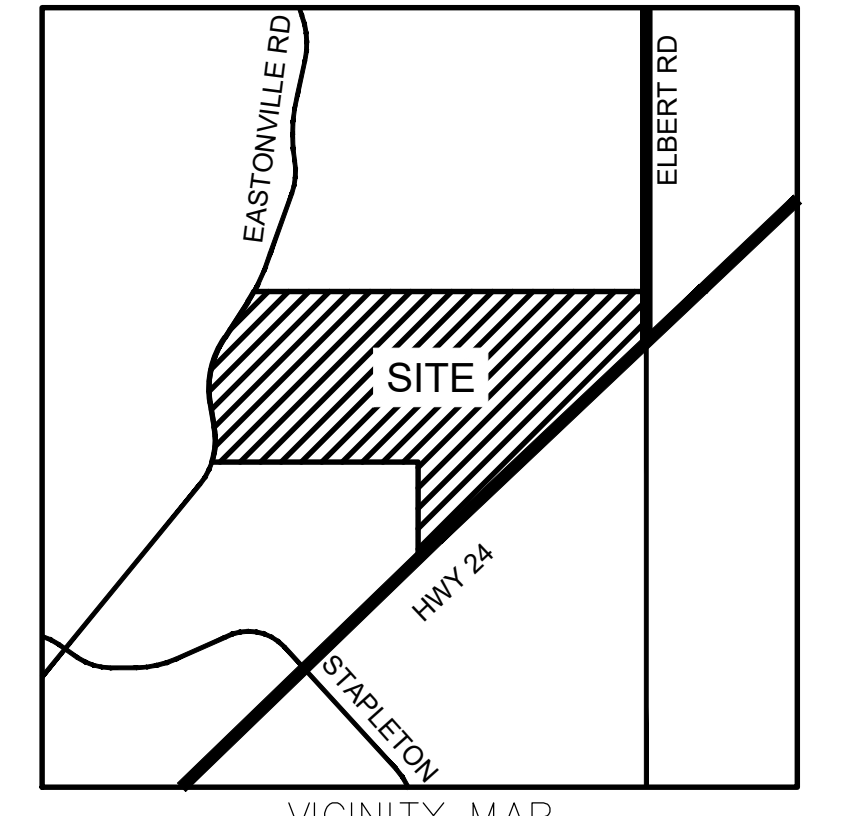
OFFSITE CONTRIBUTION  
Q100 ~ 217 CFS  
Q5 ~ 61 CFS  
OFFSITE AREA ~0.22 SQUARE MILES  
CN VALUE ~54.53  
SEE STREAMSTATS MAP

OFFSITE CONTRIBUTION  
Q100 ~ 595 CFS  
Q5 ~ 180 CFS  
OFFSITE AREA ~0.84 SQUARE MILES  
CN VALUE ~58.28  
SEE STREAMSTATS MAP

OFFSITE CONTRIBUTION  
Q100 ~ 413 CFS  
Q5 ~ 67 CFS  
OFFSITE AREA ~0.17 SQUARE MILES  
CN VALUE ~55.04  
SEE STREAMSTATS MAP

Basin	Design Point	5 Year Pre Development	100 Year Pre Development
A1	10	13.03	66.80
B1	20	4.33	48.76
B2	21	1.66	20.74
	22	11.85	140.35
	23	5.99	68.56
B3	24	21.23	249.20
C1	30	9.95	110.70
	31	9.95	110.70
D1	40	8.12	40.00
D2	41	22.23	114.87
	42	8.12	40.00
E1	50	32.34	157.99
	51	32.34	157.99
F1	60	9.70	49.45
F2	61	16.46	86.73
F3	62	3.65	18.42
F4	63	12.98	67.82
	64	13.35	67.87
	65	26.04	135.62

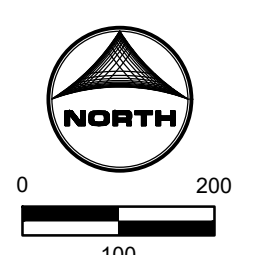
Basin	Design Point	5 Year Pre Development	100 Year Pre Development
	66	16.46	86.73
	67	51.47	269.52
G1	70	5.57	28.46
G2	71	3.87	20.06
	72	3.87	20.06
	73	3.87	20.06
	74	9.42	48.48
H1	80	1.85	21.89
H2	81	5.37	27.12
H3	82	1.92	9.51
H4	83	8.07	40.86
	84	7.22	49.01
	85	1.92	9.51
OS1	OS1	67.00	413.00
OS2	OS2	59.00	280.00
OS3	OS3	61.00	217.00
OS4	OS4	180.00	595.00
	Outfall1	80.03	479.80
	Outfall2	85.96	597.41
	Outfall3	30.00	154.35
	Outfall4	341.05	1335.77



**LEGEND:**

- PROPOSED MAJOR CONTOUR: 5250
- PROPOSED MINOR CONTOUR: 5250
- EXISTING MAJOR CONTOUR: 5250
- EXISTING MINOR CONTOUR: 5250
- PROPOSED STORM DRAIN PIPE: (Symbol)
- EXISTING STORM DRAIN PIPE: (Symbol)
- PROPOSED DRAINAGE CHANNEL: (Symbol)
- PROPOSED ROAD: (Symbol)
- PROPERTY LINE: (Symbol)
- DIRECTIONAL FLOW ARROW: (Symbol)
- EMERGENCY OVERFLOW ARROW: (Symbol)
- EXISTING 100-YR FLOODWAY: (Symbol)
- EXISTING 100-YR FLOODPLAIN: (Symbol)
- PROPOSED 100-YR FLOODPLAIN: (Symbol)
- WATERSHED BOUNDARY: (Symbol)
- MAJOR BASIN LINE: (Symbol)
- 100YR ZONE A FLOODPLAIN: (Symbol)
- PROPOSED DETENTION LOCATION: (Symbol)
- POTENTIAL WATER QUALITY LOCATION: (Symbol)
- SWMM CONVEYANCE ELEMENT: (Symbol)
- PROPOSED PEAK FLOW RATE (CFS): 850
- DESIGN POINT: (Symbol)
- PROPOSED BASIN LABEL: (Symbol)
- AREA (AC): (Symbol)
- LAND USE: LOW DENSITY, MEDIUM DENSITY, HIGH/MED DENSITY, HIGH DENSITY, CHURCH, COMMERCIAL, ELEMENTARY SCHOOL, COMMUNITY PARK

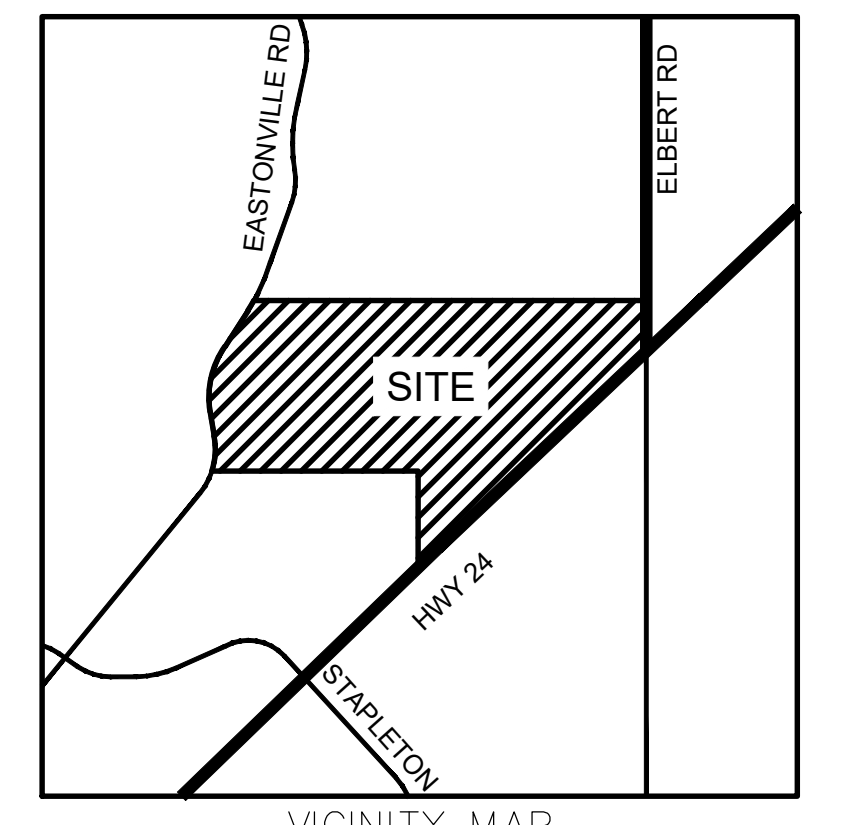
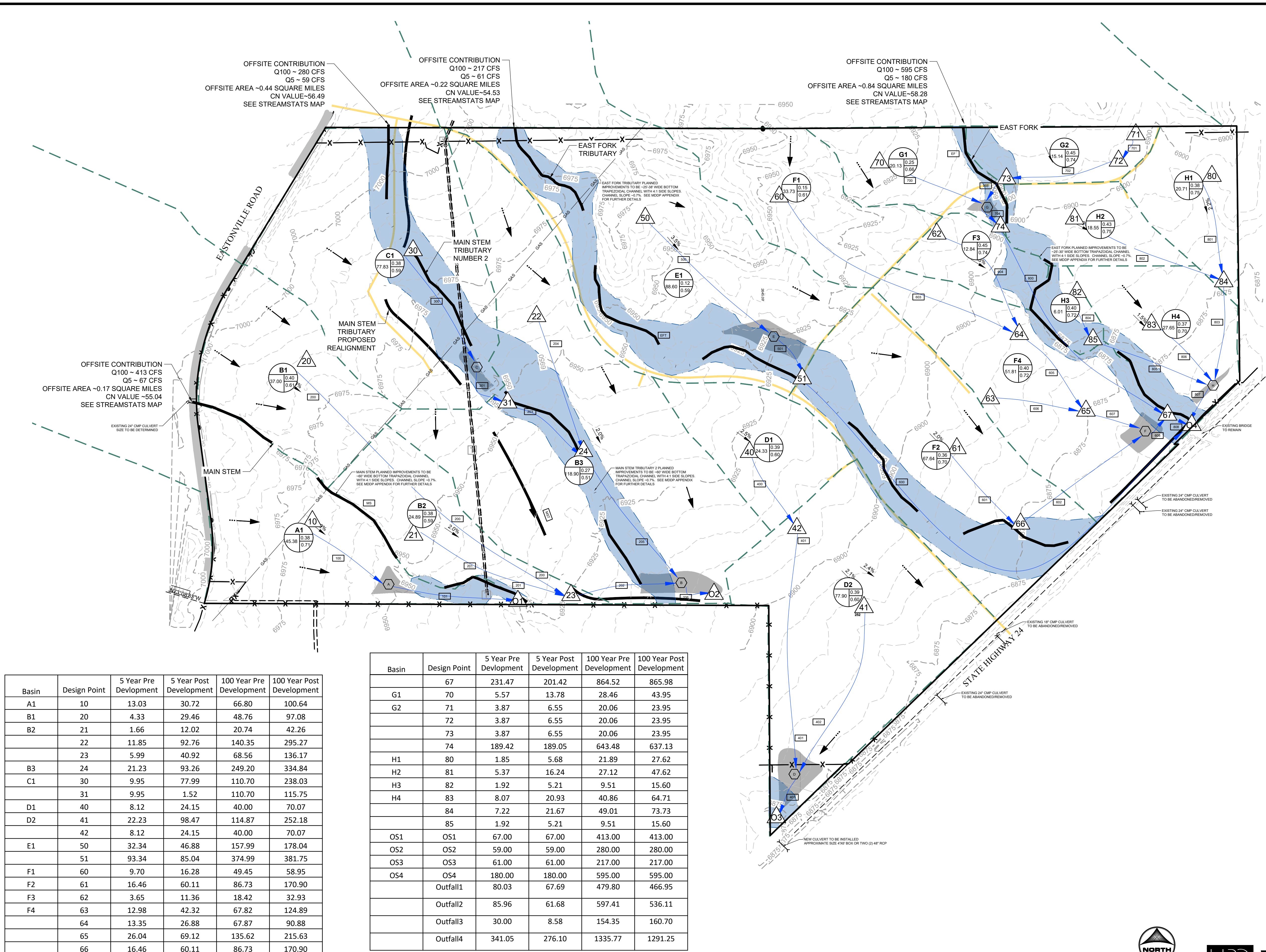
NOTES:



Job No.: 191897.01  
Prepared By: TBI  
Date: 04/14/2020

EXISTING EX1





**LEGEND:**

- PROPOSED MAJOR CONTOUR — 5250
- PROPOSED MINOR CONTOUR —
- EXISTING MAJOR CONTOUR - - - 5250
- EXISTING MINOR CONTOUR - - -
- PROPOSED STORM DRAIN PIPE —
- EXISTING STORM DRAIN PIPE —
- PROPOSED DRAINAGE CHANNEL —
- PROPOSED ROAD —
- PROPERTY LINE - - -
- DIRECTIONAL FLOW ARROW →
- EMERGENCY OVERFLOW ARROW ↶
- EXISTING 100-YR FLOODWAY —
- EXISTING 100-YR FLOODPLAIN - - -
- PROPOSED 100-YR FLOODPLAIN - - -
- WATERSHED BOUNDARY - - -
- MAJOR BASIN LINE - - -
- 100YR ZONE A FLOODPLAIN ■
- PROPOSED DETENTION LOCATION A
- POTENTIAL WATER QUALITY LOCATION WQ
- SWM CONVEYANCE ELEMENT SWM
- PROPOSED PEAK FLOW RATE (CFS) 850
- DESIGN POINT 10
- PROPOSED BASIN LABEL XX BASIN DESIGNATION  
XX C5  
XX C100
- LAND USE  
 LOW DENSITY  
 MEDIUM DENSITY  
 HIGH/MED DENSITY  
 HIGH DENSITY  
 CHURCH  
 COMMERCIAL  
 ELEMENTARY SCHOOL  
 COMMUNITY PARK

**NOTES:**

PRELIMINARY CHANNEL GEOMETRY (BY OTHERS)  
 MAIN STEM  
 BOTTOM WIDTH: 60'  
 SIDE SLOPES: 4:1

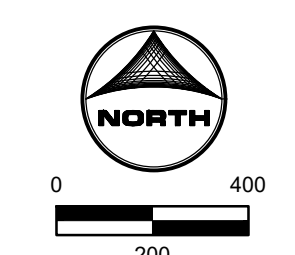
MAIN STEM TRIBUTARY 2  
 BOTTOM WIDTH: 60'  
 SIDE SLOPES: 4:1

EAST FORK TRIBUTARY 1 REACH 2  
 BOTTOM WIDTH: 38'  
 SIDE SLOPES: 4:1

EAST FORK TRIBUTARY 1 REACH 1  
 BOTTOM WIDTH: 25'  
 SIDE SLOPES: 4:1

Basin	Design Point	5 Year Pre Development	5 Year Post Development	100 Year Pre Development	100 Year Post Development
A1	10	13.03	30.72	66.80	100.64
B1	20	4.33	29.46	48.76	97.08
B2	21	1.66	12.02	20.74	42.26
B2	22	11.85	92.76	140.35	295.27
B3	23	5.99	40.92	68.56	136.17
B3	24	21.23	93.26	249.20	334.84
C1	30	9.95	77.99	110.70	238.03
C1	31	9.95	1.52	110.70	115.75
D1	40	8.12	24.15	40.00	70.07
D2	41	22.23	98.47	114.87	252.18
E1	50	32.34	46.88	157.99	178.04
E1	51	93.34	85.04	374.99	381.75
F1	60	9.70	16.28	49.45	58.95
F2	61	16.46	60.11	86.73	170.90
F3	62	3.65	11.36	18.42	32.93
F4	63	12.98	42.32	67.82	124.89
	64	13.35	26.88	67.87	90.88
	65	26.04	69.12	135.62	215.63
	66	16.46	60.11	86.73	170.90

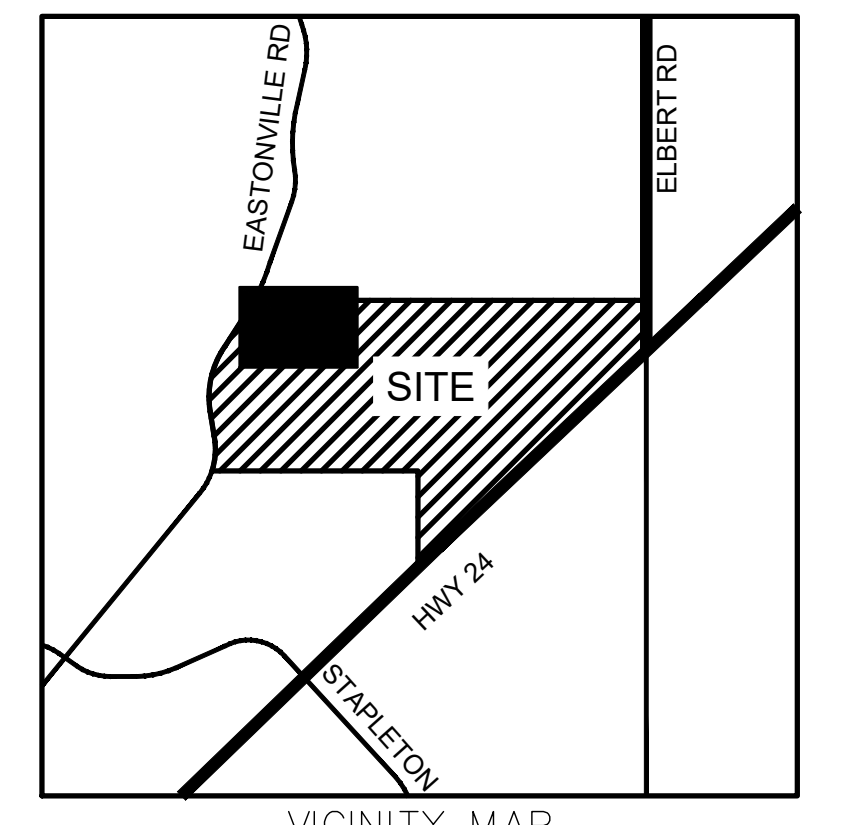
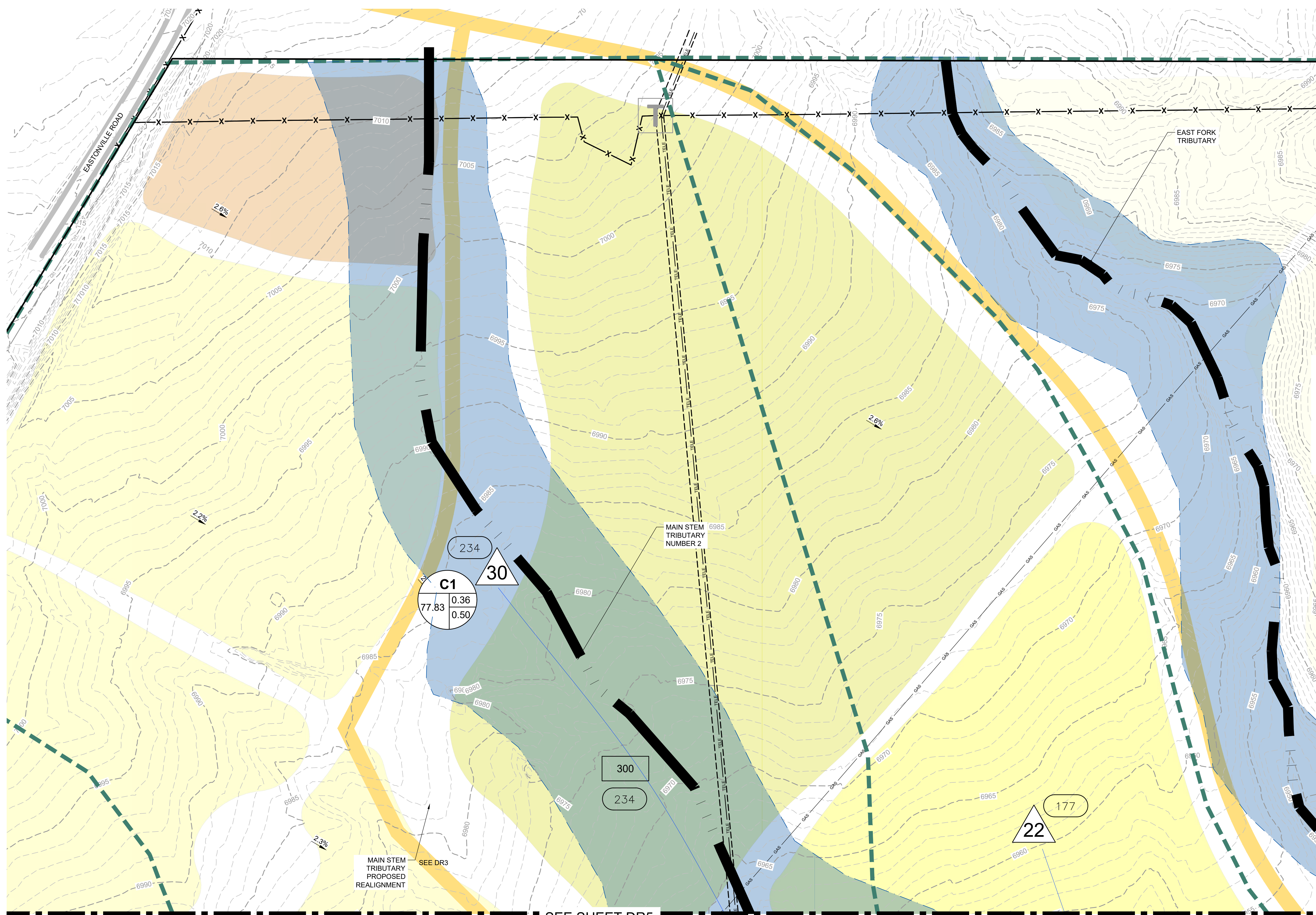
Basin	Design Point	5 Year Pre Development	5 Year Post Development	100 Year Pre Development	100 Year Post Development
G1	70	5.57	13.78	28.46	43.95
G2	71	3.87	6.55	20.06	23.95
	72	3.87	6.55	20.06	23.95
	73	3.87	6.55	20.06	23.95
	74	189.42	189.05	643.48	637.13
H1	80	1.85	5.68	21.89	27.62
H2	81	5.37	16.24	27.12	47.62
H3	82	1.92	5.21	9.51	15.60
H4	83	8.07	20.93	40.86	64.71
	84	7.22	21.67	49.01	73.73
	85	1.92	5.21	9.51	15.60
OS1	OS1	67.00	67.00	413.00	413.00
OS2	OS2	59.00	59.00	280.00	280.00
OS3	OS3	61.00	61.00	217.00	217.00
OS4	OS4	180.00	180.00	595.00	595.00
	Outfall1	80.03	67.69	479.80	466.95
	Outfall2	85.96	61.68	597.41	536.11
	Outfall3	30.00	8.58	154.35	160.70
	Outfall4	341.05	276.10	1335.77	1291.25



Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

PROPOSED DR1



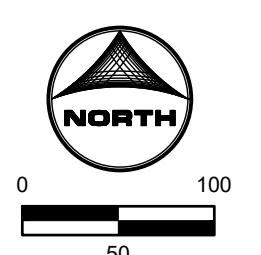


- LEGEND:**
- PROPOSED MAJOR CONTOUR ——— 5250 ———
  - PROPOSED MINOR CONTOUR ———
  - EXISTING MAJOR CONTOUR - - - - - 5250 - - - - -
  - EXISTING MINOR CONTOUR - - - - -
  - PROPOSED STORM DRAIN PIPE ———
  - EXISTING STORM DRAIN PIPE ———
  - PROPOSED DRAINAGE CHANNEL ———
  - PROPOSED ROAD ———
  - PROPERTY LINE ———
  - DIRECTIONAL FLOW ARROW ↖
  - EMERGENCY OVERFLOW ARROW ↗
  - EXISTING 100-YR FLOODWAY ———
  - EXISTING 100-YR FLOODPLAIN ———
  - PROPOSED 100-YR FLOODPLAIN ———
  - WATERSHED BOUNDARY ———
  - MAJOR BASIN LINE ———
  - 100YR ZONE A FLOODPLAIN ———
  - PROPOSED DETENTION LOCATION (A)
  - POTENTIAL WATER QUALITY LOCATION (WQ)
  - SWM CONVEYANCE ELEMENT (SWM)
  - PROPOSED PEAK FLOW RATE (CFS) (850)
  - DESIGN POINT (XX)
  - PROPOSED BASIN LABEL (XX) BASIN DESIGNATION
  - AREA (AC.) (XX XX) % IMPERVIOUSNESS

- LAND USE**
- LOW DENSITY
  - MEDIUM DENSITY
  - HIGH/MED DENSITY
  - HIGH DENSITY
  - CHURCH
  - COMMERCIAL
  - ELEMENTARY SCHOOL
  - COMMUNITY PARK

**NOTES:**

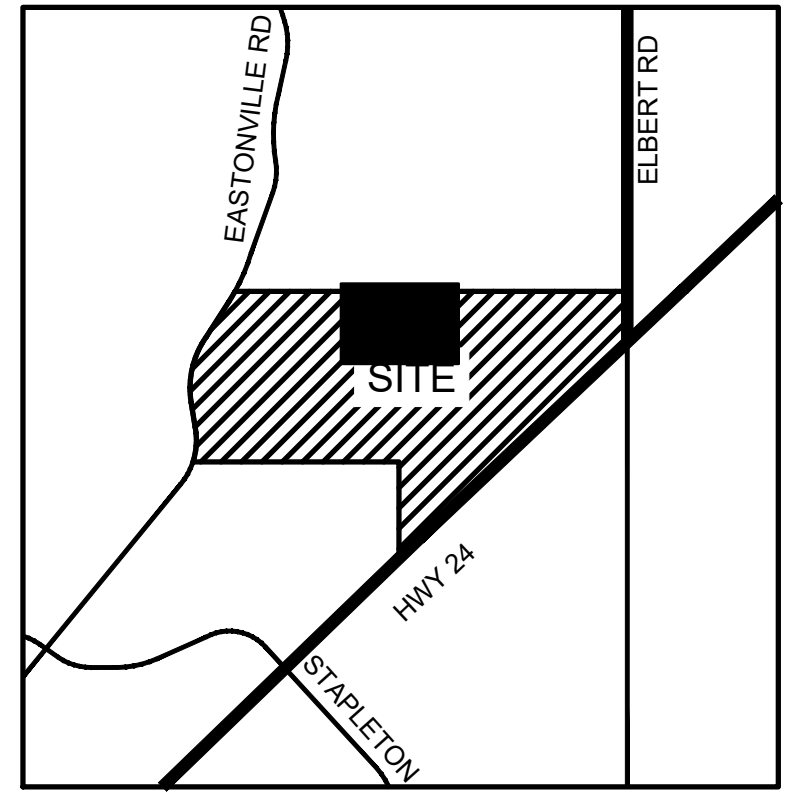
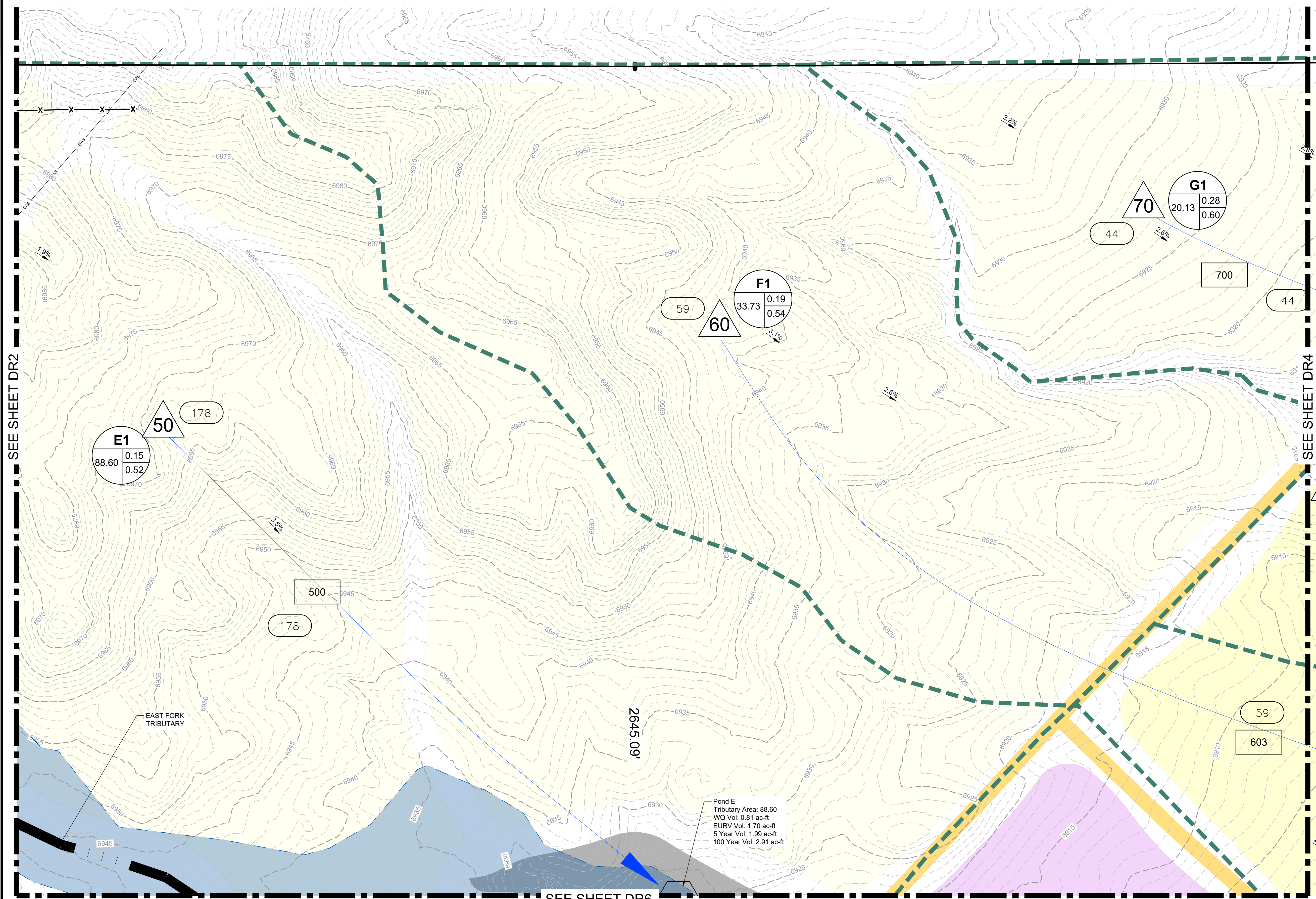
Is this Land Use legend supposed to be in color for the colors (like yellow and orange) shown on this map? Either way, please provide a Legend for all of the shaded colors show on these maps.



Job No.: 191897.01  
 Prepared By: CMM  
 Date: 4/9/2020

PROPOSED DR2





VICINITY MAP

- LEGEND:**
- PROPOSED MAJOR CONTOUR: 5250
  - PROPOSED MINOR CONTOUR: 5250
  - EXISTING MAJOR CONTOUR: 5250
  - EXISTING MINOR CONTOUR: 5250
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWMM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS)
  - DESIGN POINT
  - PROPOSED BASIN LABEL: XX BASIN DESIGNATION, XX XX % IMPERVIOUSNESS

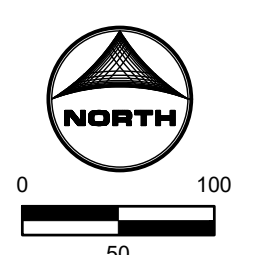
- LAND USE**
- LOW DENSITY
  - MEDIUM DENSITY
  - HIGH/MED DENSITY
  - HIGH DENSITY
  - CHURCH
  - COMMERCIAL
  - ELEMENTARY SCHOOL
  - COMMUNITY PARK

NOTES:

SEE SHEET DR2

SEE SHEET DR4

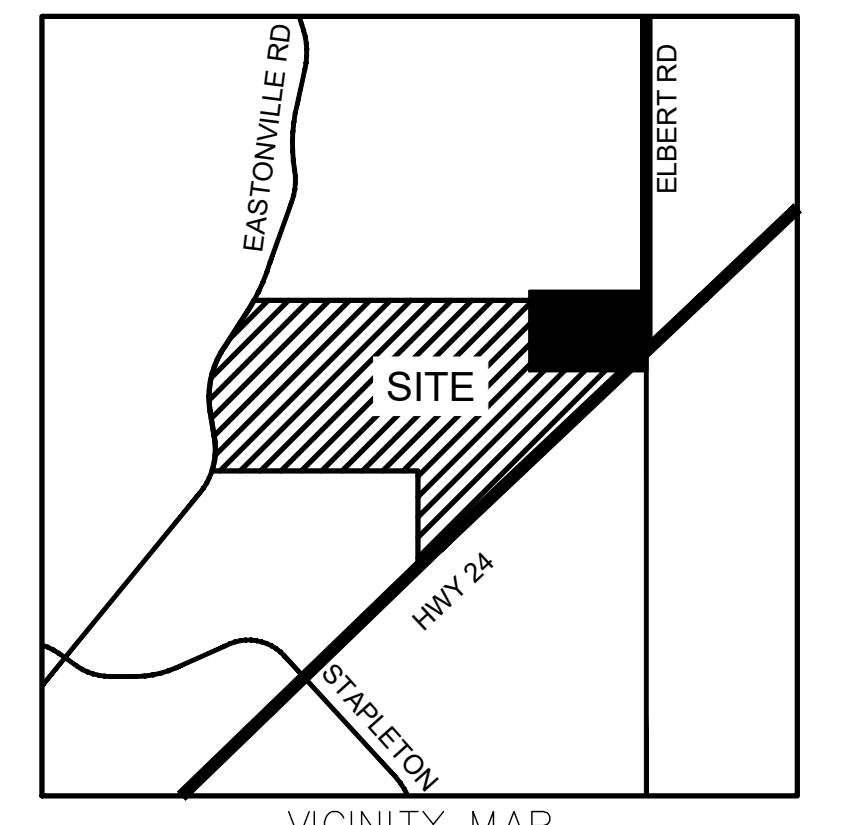
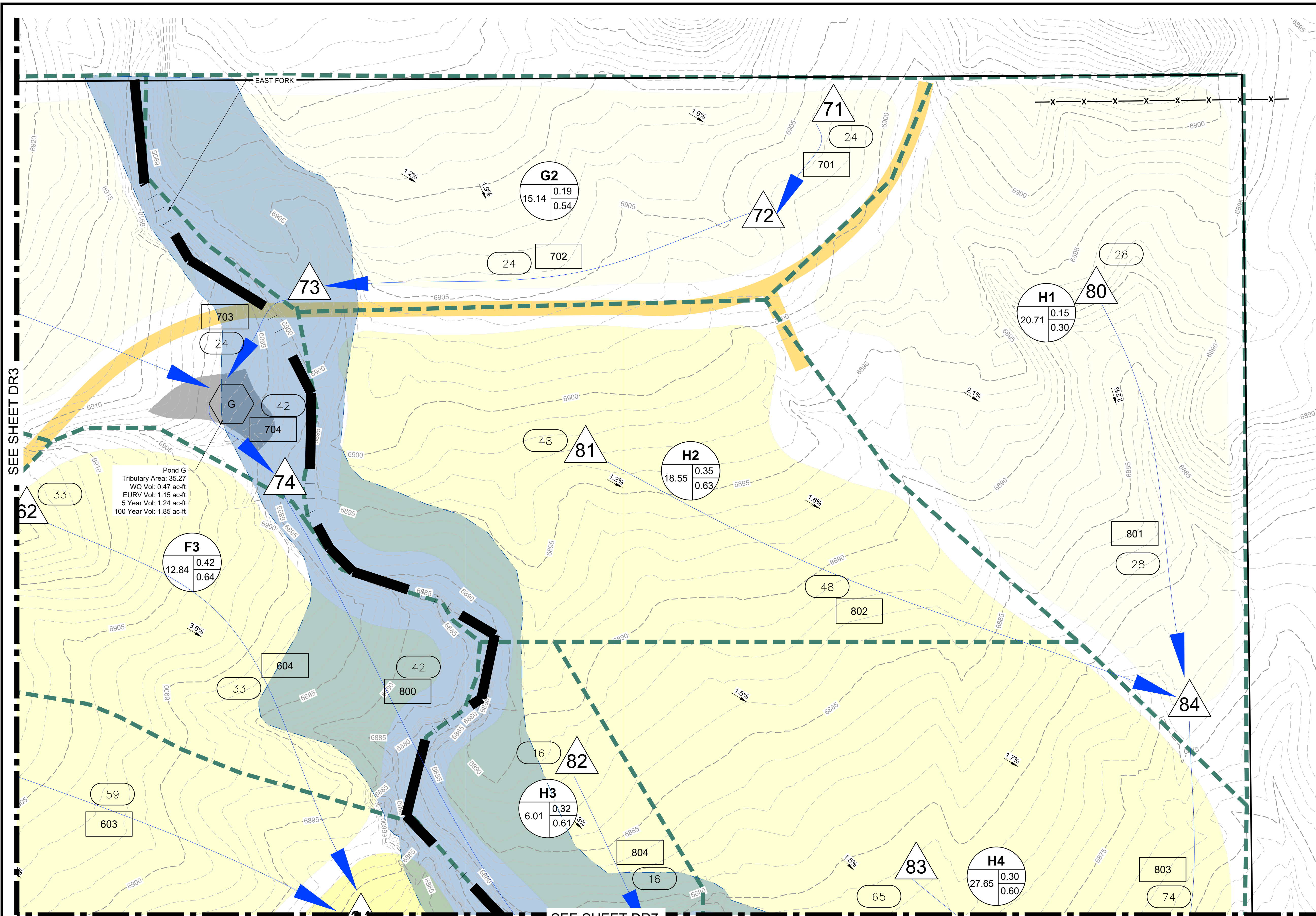
SEE SHEET DR6



Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

PROPOSED DR3



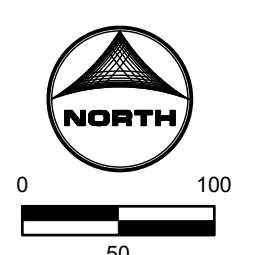


- LEGEND:**
- PROPOSED MAJOR CONTOUR: 5250
  - PROPOSED MINOR CONTOUR
  - EXISTING MAJOR CONTOUR: 5250
  - EXISTING MINOR CONTOUR
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWMM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS)
  - DESIGN POINT
  - PROPOSED BASIN LABEL: XX BASIN DESIGNATION, XX XX % IMPERVIOUSNESS
  - LAND USE: LOW DENSITY, MEDIUM DENSITY, HIGH/MED DENSITY, HIGH DENSITY, CHURCH, COMMERCIAL, ELEMENTARY SCHOOL, COMMUNITY PARK

NOTES:

SEE SHEET DR3

SEE SHEET DR7



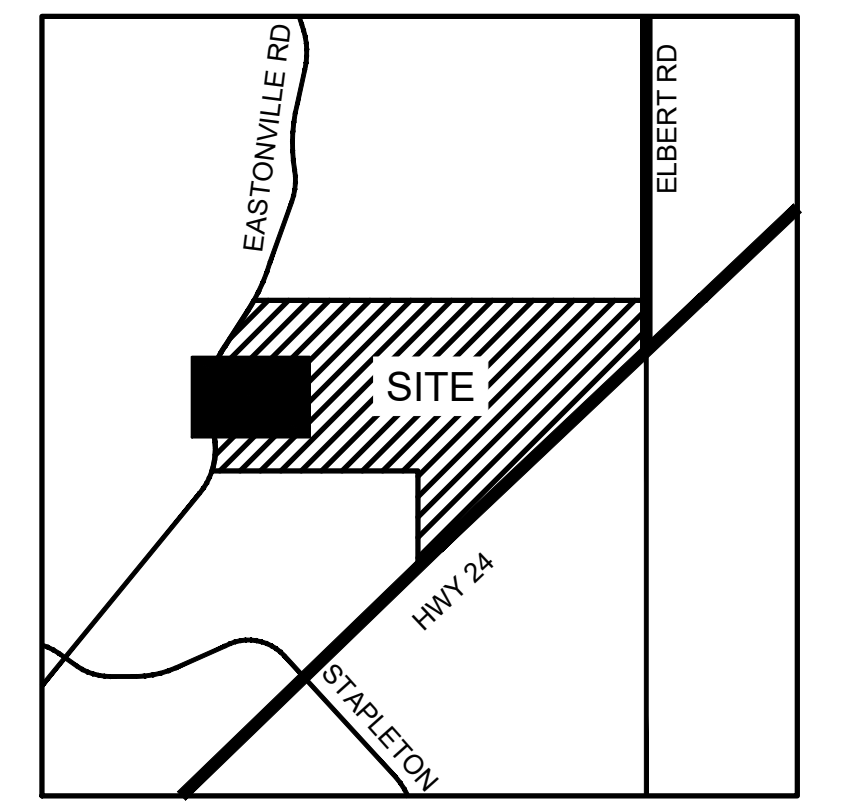
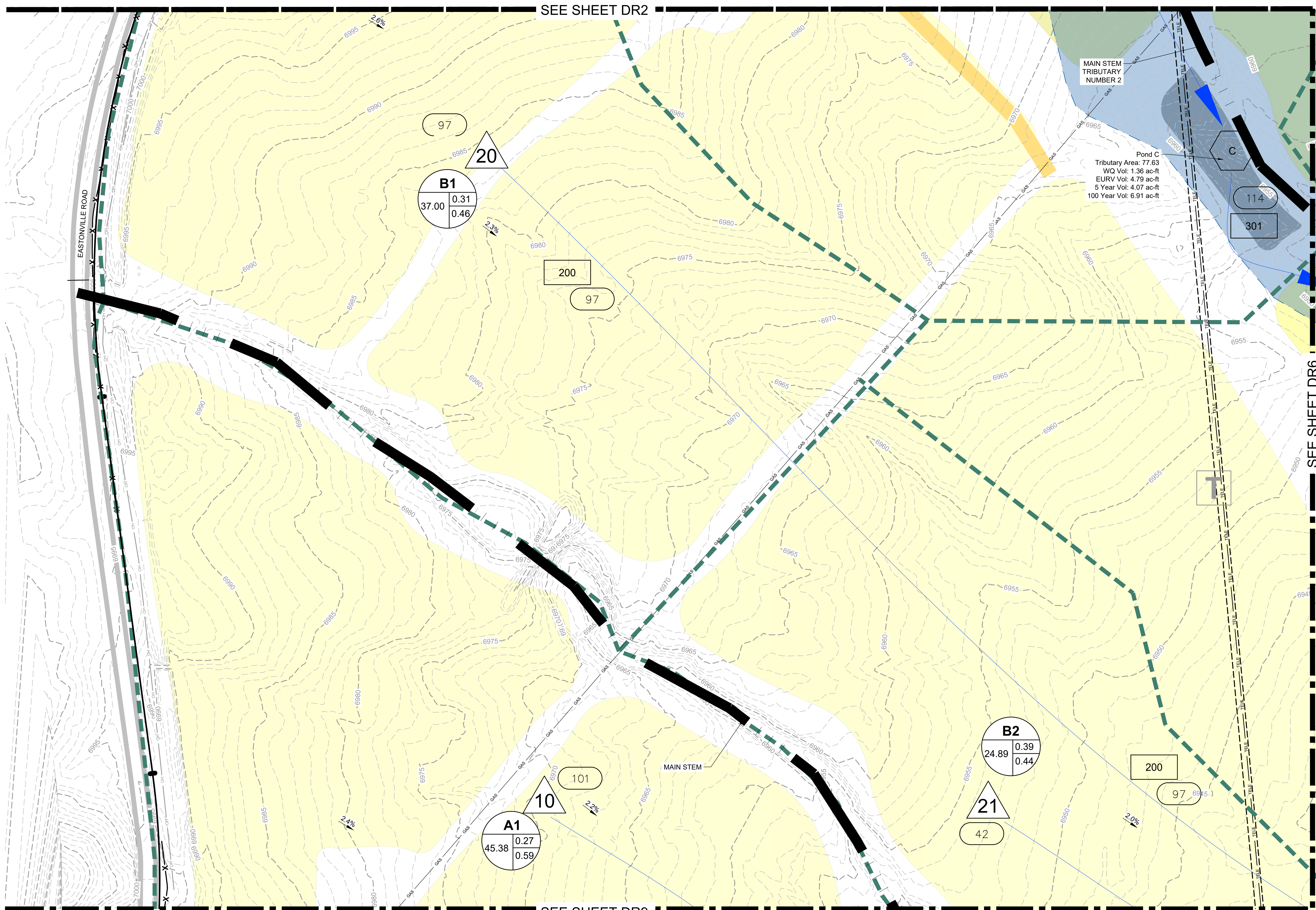
Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

PROPOSED DR4



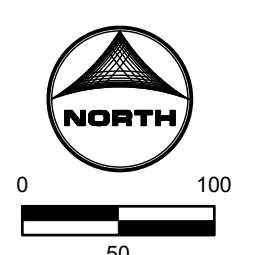
SEE SHEET DR2

SEE SHEET DR9



- LEGEND:**
- PROPOSED MAJOR CONTOUR: 5250
  - PROPOSED MINOR CONTOUR: 5250
  - EXISTING MAJOR CONTOUR: 5250
  - EXISTING MINOR CONTOUR: 5250
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS)
  - DESIGN POINT
  - PROPOSED BASIN LABEL
- LAND USE**
- LOW DENSITY
  - MEDIUM DENSITY
  - HIGH/MED DENSITY
  - HIGH DENSITY
  - CHURCH
  - COMMERCIAL
  - ELEMENTARY SCHOOL
  - COMMUNITY PARK

NOTES:



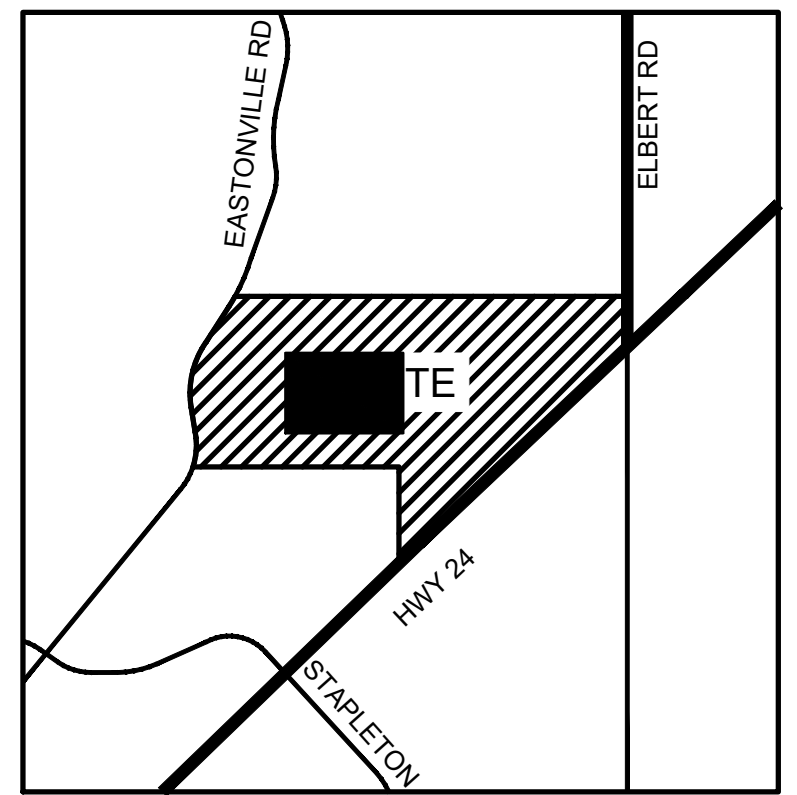
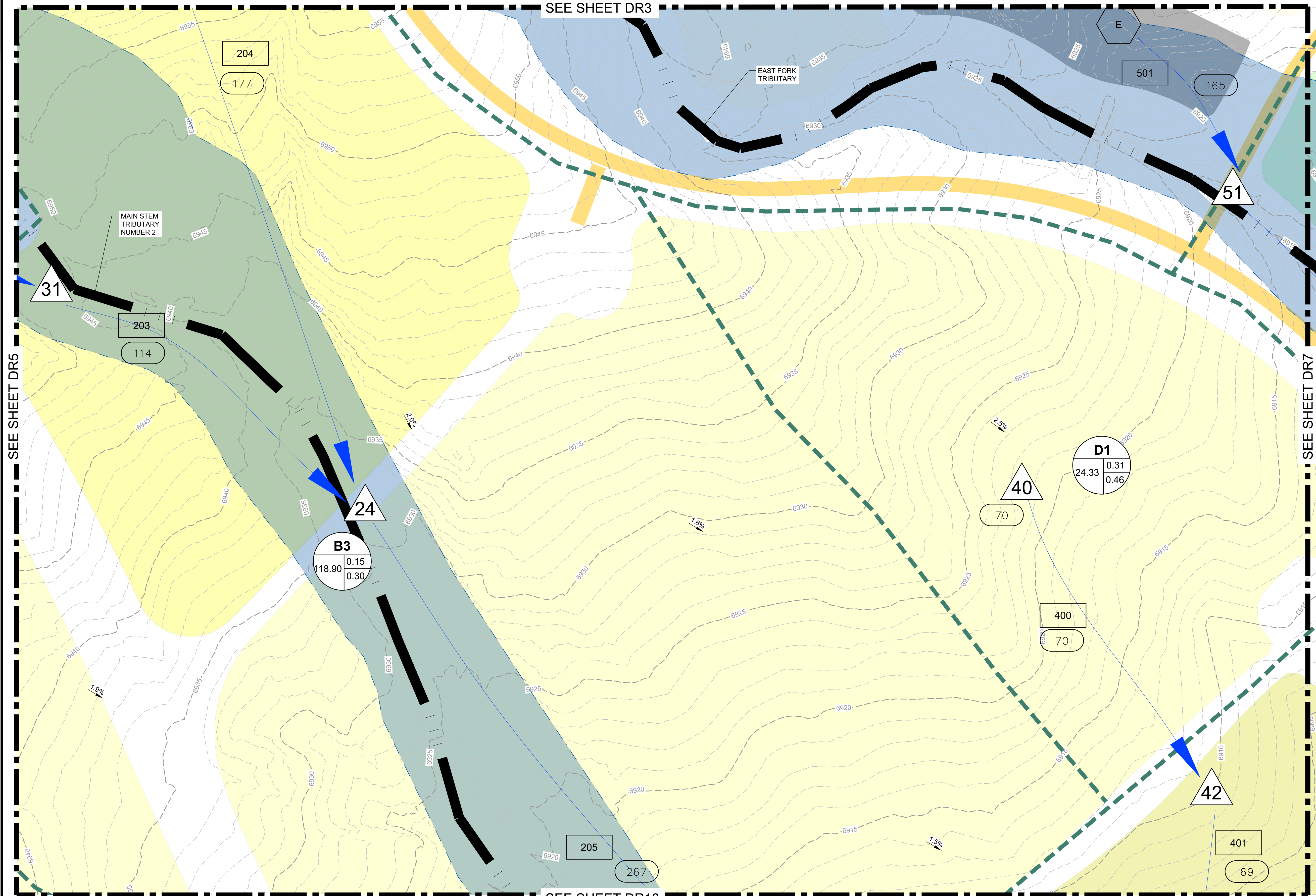
Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

PROPOSED DR5



SEE SHEET DR3

SEE SHEET DR10

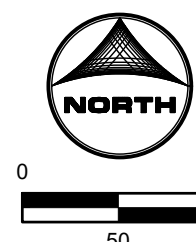


VICINITY MAP

LEGEND:

- PROPOSED MAJOR CONTOUR ——— 5250 ———
- PROPOSED MINOR CONTOUR ——— ———
- EXISTING MAJOR CONTOUR - - - - - 5250 - - - - -
- EXISTING MINOR CONTOUR - - - - -
- PROPOSED STORM DRAIN PIPE ———
- EXISTING STORM DRAIN PIPE ———
- PROPOSED DRAINAGE CHANNEL ———
- PROPOSED ROAD ———
- PROPERTY LINE ———
- DIRECTIONAL FLOW ARROW ———
- EMERGENCY OVERFLOW ARROW ———
- EXISTING 100-YR FLOODWAY ———
- EXISTING 100-YR FLOODPLAIN ———
- PROPOSED 100-YR FLOODPLAIN ———
- WATERSHED BOUNDARY ———
- MAJOR BASIN LINE ———
- 100YR ZONE A FLOODPLAIN ———
- PROPOSED DETENTION LOCATION ———
- POTENTIAL WATER QUALITY LOCATION ———
- SWMM CONVEYANCE ELEMENT ———
- PROPOSED PEAK FLOW RATE (CFS) 850
- DESIGN POINT ———
- PROPOSED BASIN LABEL ———
- AREA (AC.) XX XX % IMPERVIOUSNESS
- LAND USE
  - LOW DENSITY
  - MEDIUM DENSITY
  - HIGH/MED DENSITY
  - HIGH DENSITY
  - CHURCH
  - COMMERCIAL
  - ELEMENTARY SCHOOL
  - COMMUNITY PARK

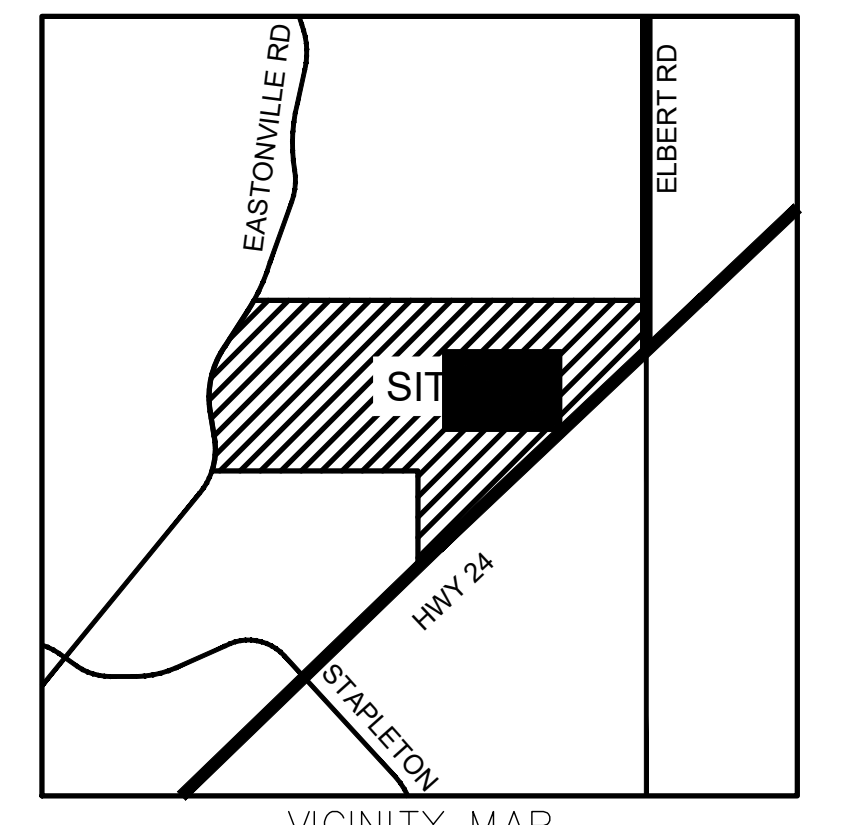
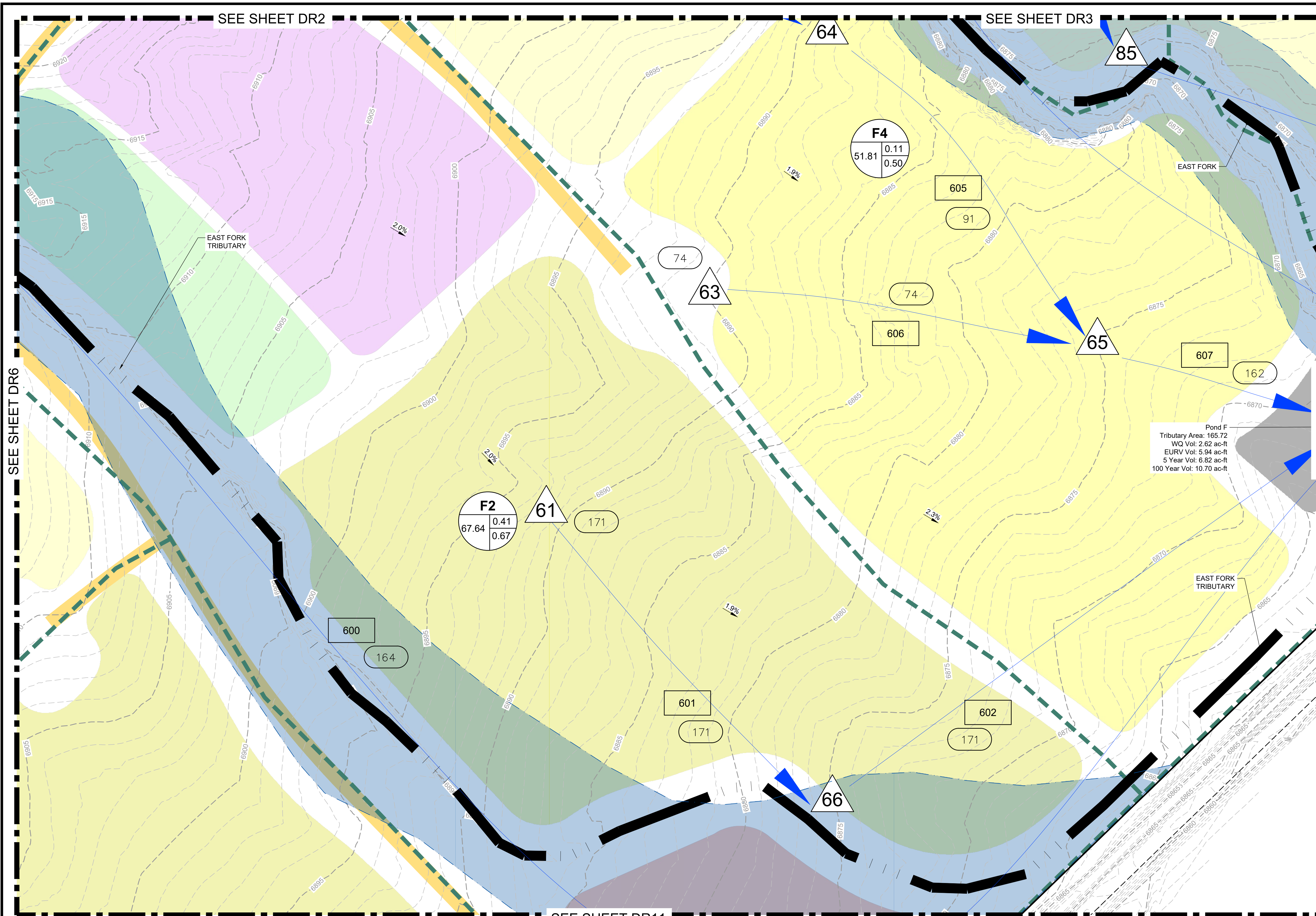
NOTES:



Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

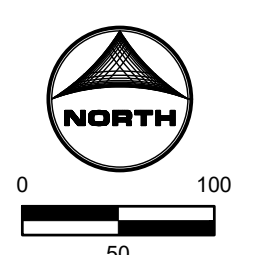
PROPOSED DR6





- LEGEND:**
- PROPOSED MAJOR CONTOUR: 5250
  - PROPOSED MINOR CONTOUR
  - EXISTING MAJOR CONTOUR: 5250
  - EXISTING MINOR CONTOUR
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWMM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS)
  - DESIGN POINT
  - PROPOSED BASIN LABEL: XX BASIN DESIGNATION
  - AREA (AC.): XX XX % IMPERVIOUSNESS
  - LAND USE:
    - LOW DENSITY
    - MEDIUM DENSITY
    - HIGH/MED DENSITY
    - HIGH DENSITY
    - CHURCH
    - COMMERCIAL
    - ELEMENTARY SCHOOL
    - COMMUNITY PARK

NOTES:



Job No.: 191897.01  
Prepared By: TBI  
Date: 04/14/2020

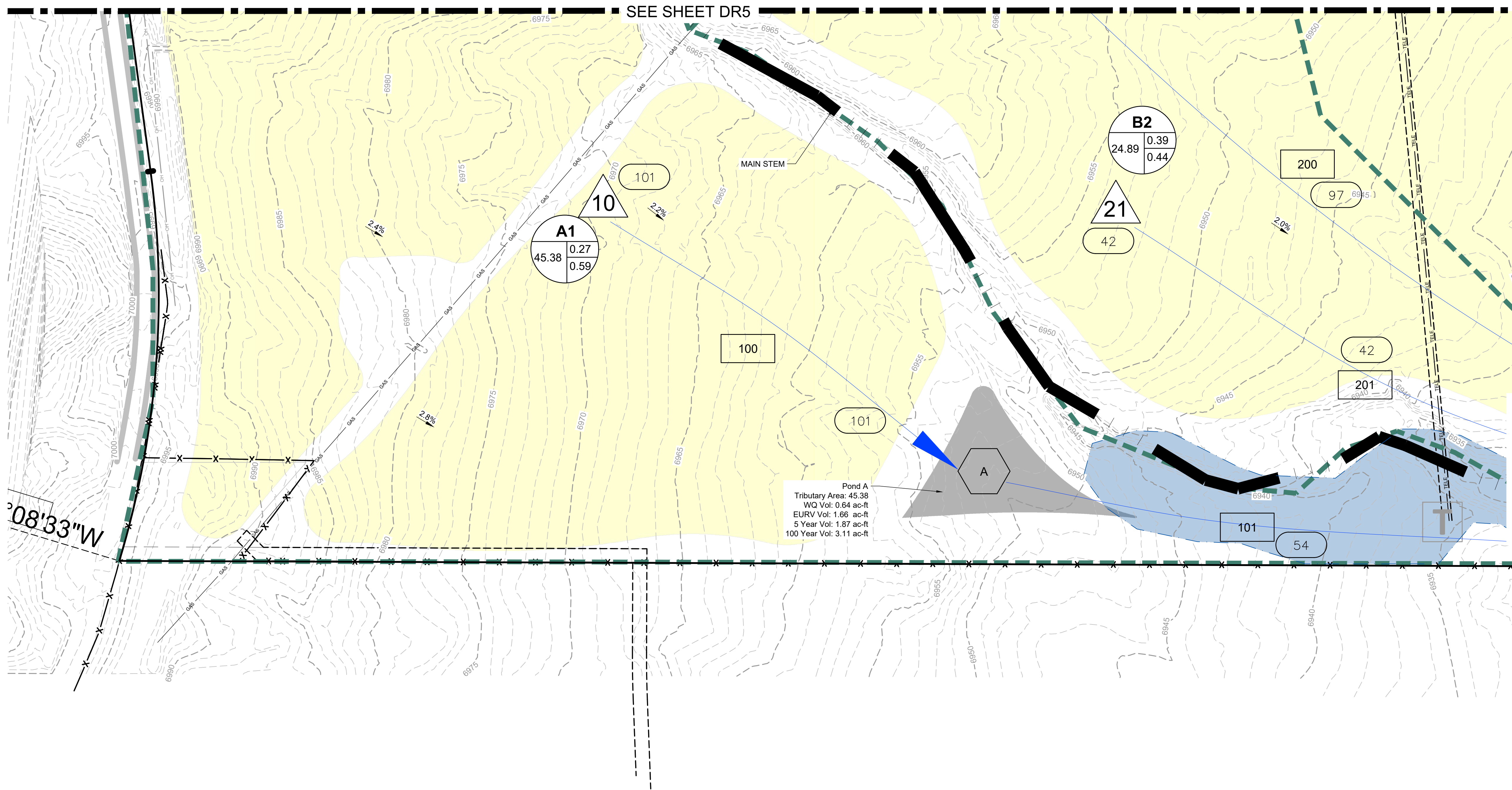
PROPOSED DR7





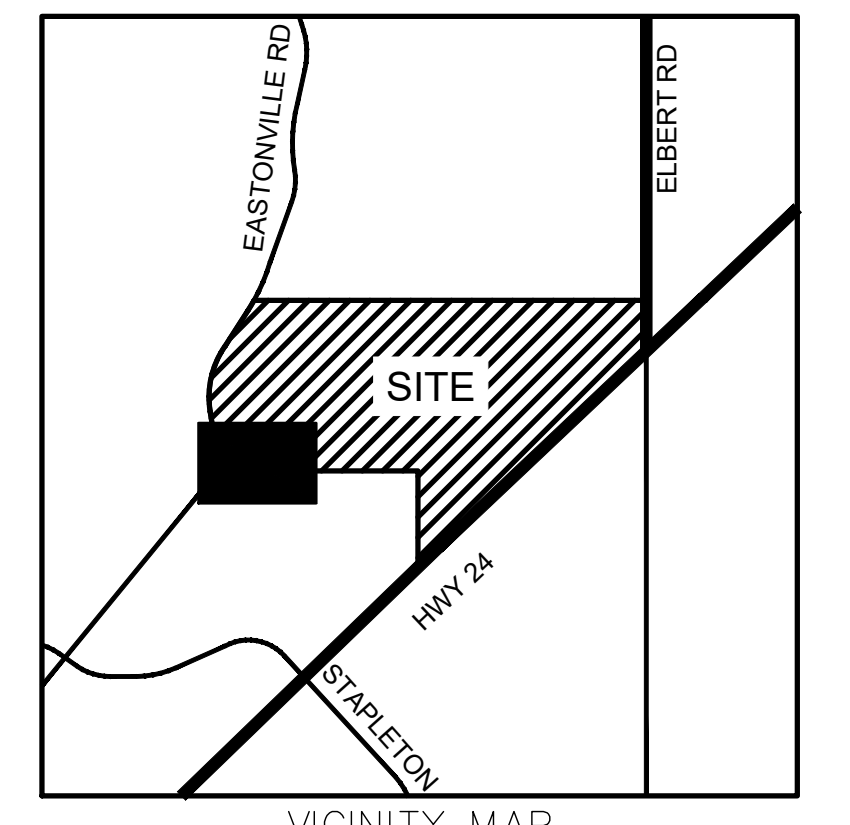


SEE SHEET DR5



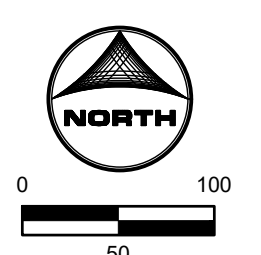
08'33"W

Pond A  
 Tributary Area: 45.38  
 WQ Vol: 0.64 ac-ft  
 EURV Vol: 1.66 ac-ft  
 5 Year Vol: 1.87 ac-ft  
 100 Year Vol: 3.11 ac-ft



- LEGEND:**
- PROPOSED MAJOR CONTOUR: 5250
  - PROPOSED MINOR CONTOUR: 5250
  - EXISTING MAJOR CONTOUR: 5250
  - EXISTING MINOR CONTOUR: 5250
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWMM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS) 850
  - DESIGN POINT
  - PROPOSED BASIN LABEL: XX BASIN DESIGNATION
  - AREA (AC.) XX XX % IMPERVIOUSNESS
- LAND USE**
- LOW DENSITY
  - MEDIUM DENSITY
  - HIGH/MED DENSITY
  - HIGH DENSITY
  - CHURCH
  - COMMERCIAL
  - ELEMENTARY SCHOOL
  - COMMUNITY PARK

NOTES:



Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

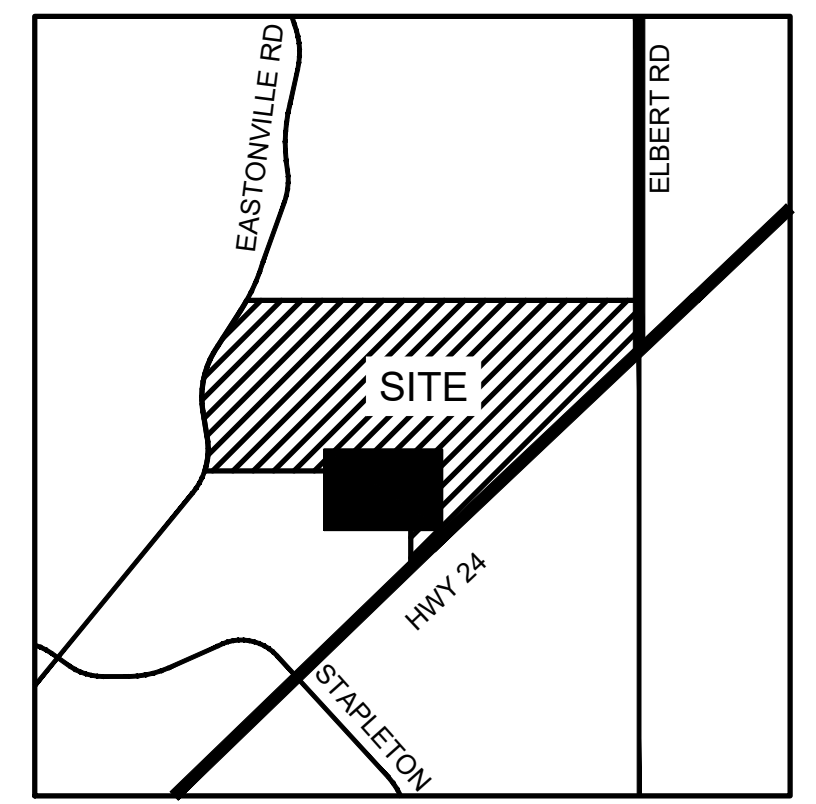
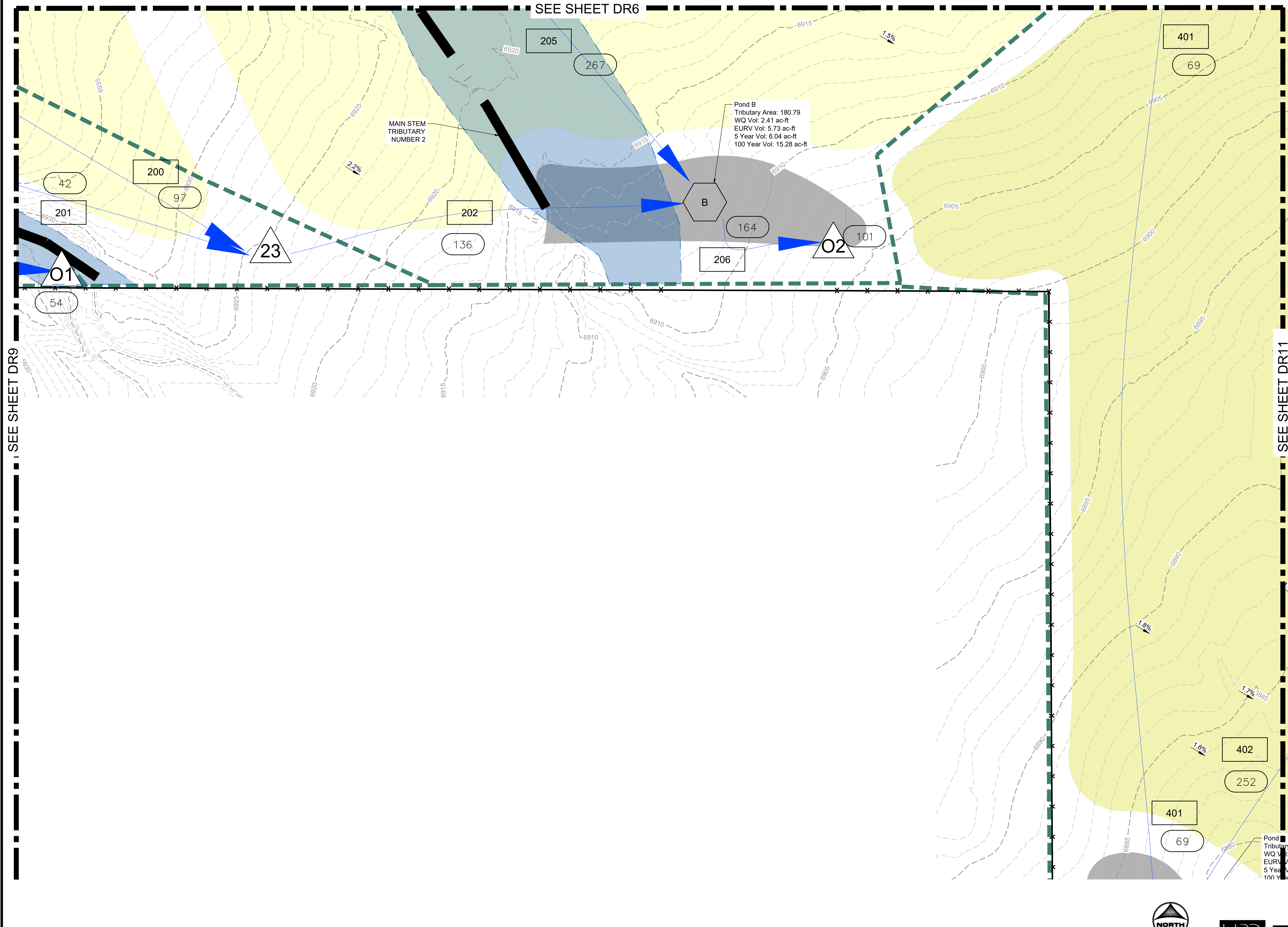
PROPOSED DR9



SEE SHEET DR6

SEE SHEET DR9

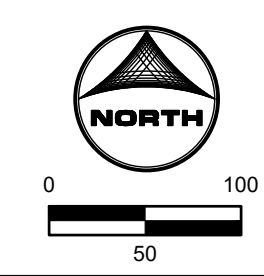
SEE SHEET DR11



LEGEND:

- PROPOSED MAJOR CONTOUR ——— 5250 ———
- PROPOSED MINOR CONTOUR ——— ———
- EXISTING MAJOR CONTOUR - - - - - 5250 - - - - -
- EXISTING MINOR CONTOUR - - - - -
- PROPOSED STORM DRAIN PIPE ———
- EXISTING STORM DRAIN PIPE ———
- PROPOSED DRAINAGE CHANNEL ———
- PROPOSED ROAD ———
- PROPERTY LINE ———
- DIRECTIONAL FLOW ARROW ———
- EMERGENCY OVERFLOW ARROW ———
- EXISTING 100-YR FLOODWAY ———
- EXISTING 100-YR FLOODPLAIN ———
- PROPOSED 100-YR FLOODPLAIN ———
- WATERSHED BOUNDARY ———
- MAJOR BASIN LINE ———
- 100YR ZONE A FLOODPLAIN ———
- PROPOSED DETENTION LOCATION ———
- POTENTIAL WATER QUALITY LOCATION ———
- SWMM CONVEYANCE ELEMENT ———
- PROPOSED PEAK FLOW RATE (CFS) 850
- DESIGN POINT ———
- PROPOSED BASIN LABEL XX BASIN DESIGNATION  
AREA (AC.) XX XX % IMPERVIOUSNESS
- LAND USE  
LOW DENSITY  
MEDIUM DENSITY  
HIGH/MED DENSITY  
HIGH DENSITY  
CHURCH  
COMMERCIAL  
ELEMENTARY SCHOOL  
COMMUNITY PARK

NOTES:

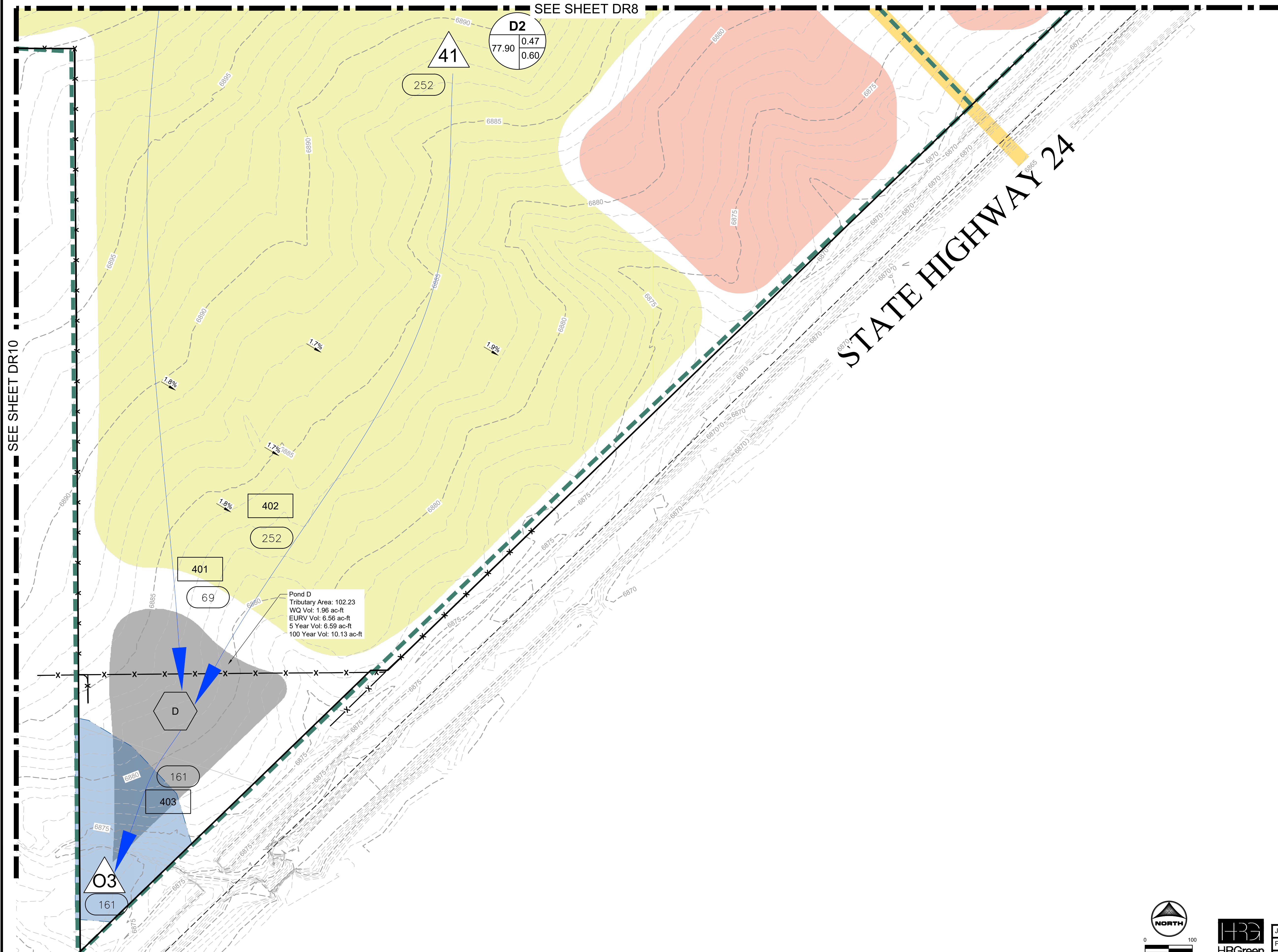


Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

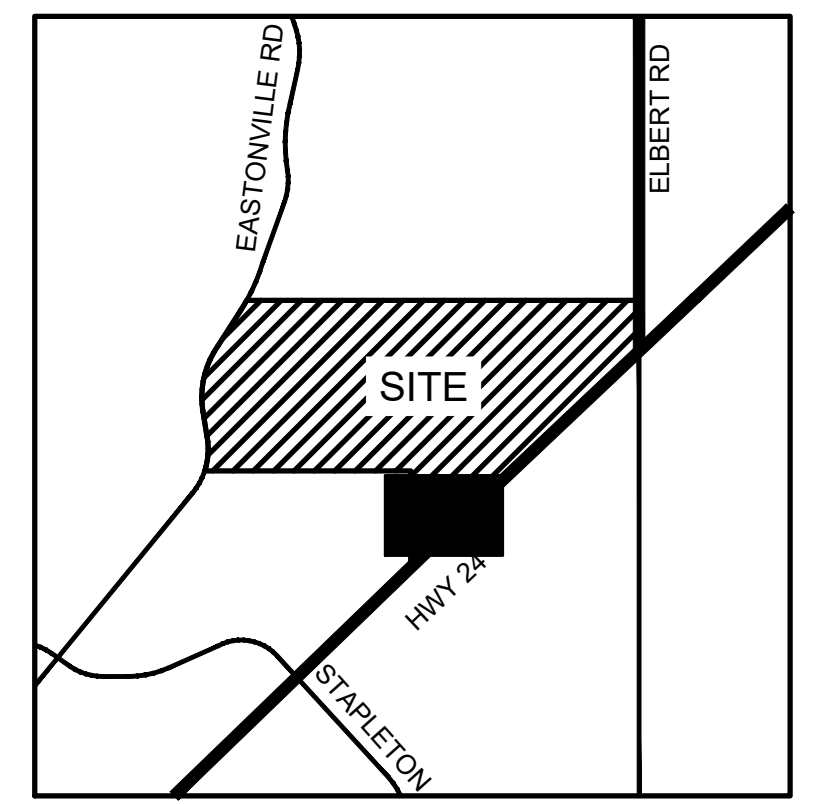
PROPOSED DR10



SEE SHEET DR8



SEE SHEET DR10

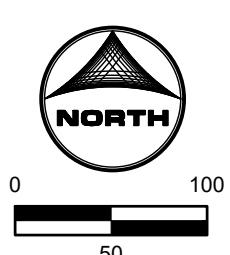


VICINITY MAP

LEGEND:

- PROPOSED MAJOR CONTOUR
  - PROPOSED MINOR CONTOUR
  - EXISTING MAJOR CONTOUR
  - EXISTING MINOR CONTOUR
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWMM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS)
  - DESIGN POINT
  - PROPOSED BASIN LABEL
  - AREA (AC.)
  - % IMPERVIOUSNESS
- LAND USE**
- LOW DENSITY
  - MEDIUM DENSITY
  - HIGH/MED DENSITY
  - HIGH DENSITY
  - CHURCH
  - COMMERCIAL
  - ELEMENTARY SCHOOL
  - COMMUNITY PARK

NOTES:

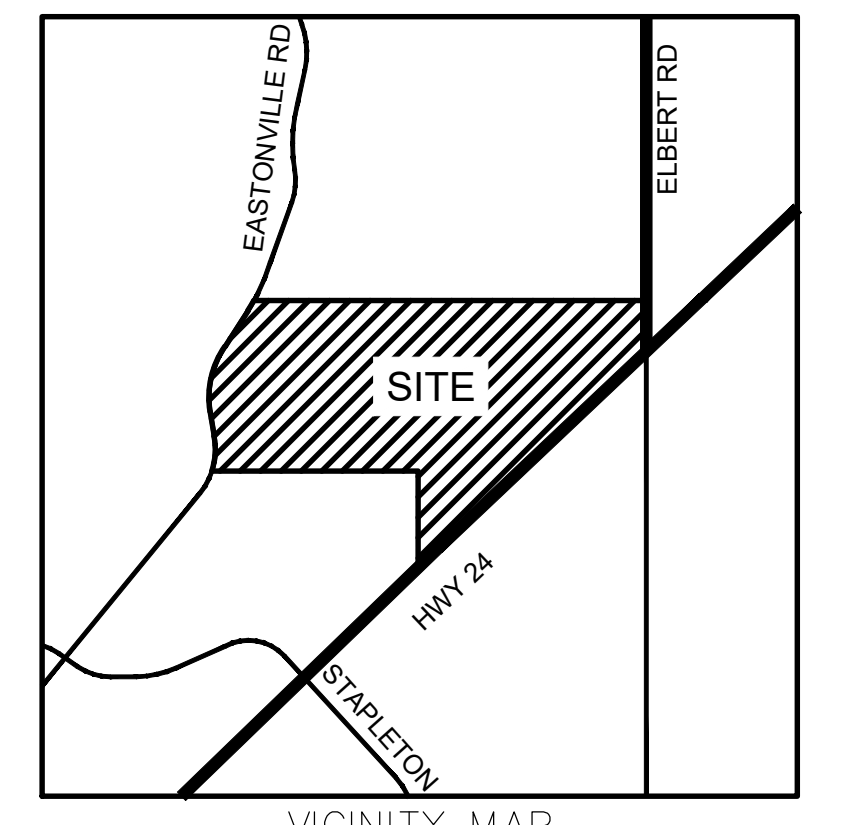
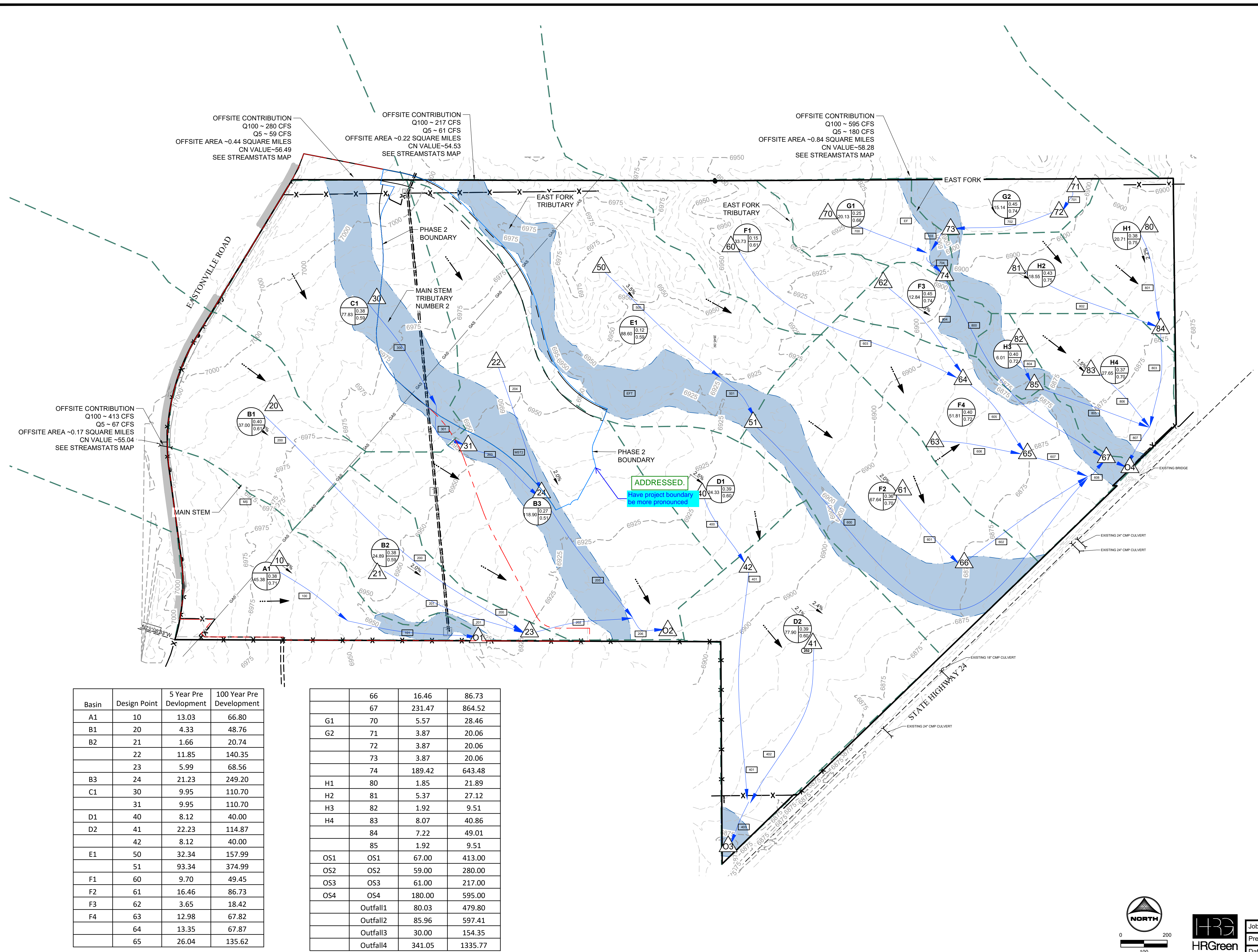


Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

PROPOSED DR11

## APPENDIX F – DRAINAGE MAPS





**LEGEND:**

- PROPOSED MAJOR CONTOUR: 5250
- PROPOSED MINOR CONTOUR: 5250
- EXISTING MAJOR CONTOUR: 5250
- EXISTING MINOR CONTOUR: 5250
- PROPOSED STORM DRAIN PIPE
- EXISTING STORM DRAIN PIPE
- PROPOSED DRAINAGE CHANNEL
- PROPOSED ROAD
- PROPERTY LINE
- DIRECTIONAL FLOW ARROW
- EMERGENCY OVERFLOW ARROW
- EXISTING 100-YR FLOODWAY
- EXISTING 100-YR FLOODPLAIN
- PROPOSED 100-YR FLOODPLAIN
- WATERSHED BOUNDARY
- MAJOR BASIN LINE
- 100YR ZONE A FLOODPLAIN
- PROPOSED DETENTION LOCATION
- POTENTIAL WATER QUALITY LOCATION
- SWMM CONVEYANCE ELEMENT
- PROPOSED PEAK FLOW RATE (CFS)
- DESIGN POINT
- PROPOSED BASIN LABEL

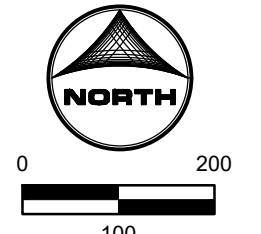
**LAND USE**

- LOW DENSITY
- MEDIUM DENSITY
- HIGH/MED DENSITY
- HIGH DENSITY
- CHURCH
- COMMERCIAL
- ELEMENTARY SCHOOL
- COMMUNITY PARK

NOTES:

Basin	Design Point	5 Year Pre Development	100 Year Pre Development
A1	10	13.03	66.80
B1	20	4.33	48.76
B2	21	1.66	20.74
	22	11.85	140.35
	23	5.99	68.56
B3	24	21.23	249.20
C1	30	9.95	110.70
	31	9.95	110.70
D1	40	8.12	40.00
D2	41	22.23	114.87
	42	8.12	40.00
E1	50	32.34	157.99
	51	93.34	374.99
F1	60	9.70	49.45
F2	61	16.46	86.73
F3	62	3.65	18.42
F4	63	12.98	67.82
	64	13.35	67.87
	65	26.04	135.62

	66	16.46	86.73
	67	231.47	864.52
G1	70	5.57	28.46
G2	71	3.87	20.06
	72	3.87	20.06
	73	3.87	20.06
	74	189.42	643.48
H1	80	1.85	21.89
H2	81	5.37	27.12
H3	82	1.92	9.51
H4	83	8.07	40.86
	84	7.22	49.01
	85	1.92	9.51
OS1	OS1	67.00	413.00
OS2	OS2	59.00	280.00
OS3	OS3	61.00	217.00
OS4	OS4	180.00	595.00
	Outfall1	80.03	479.80
	Outfall2	85.96	597.41
	Outfall3	30.00	154.35
	Outfall4	341.05	1335.77



Job No.: 191897.01  
 Prepared By: TBI  
 Date: 04/14/2020

EXISTING EX1



Please add both on and offsite drainage flow arrows to this map. Also add scale and north arrow. ADDRESSED.

The report narrative above states that this whole basin is tributary to design point 23-A via grass swales. But I don't see any swales. Everything appears to flow to Gieck Ranch Trib #2. Please clarify/revise to remove discrepancy.

HR GREEN RESPONSE: SWALES ADDED TO SURFACE AND INDICATED ON MAP WITH SWALE LINETYPE. ADDRESSED.

Fix all overlapping text. ADDRESSED.

ADDRESSED. Property owner information.

ADDRESSED. DP labels are hard to read. Please make a little larger.

Information in this column matches with CS value in spreadsheet. Please revise table or spreadsheet accordingly to match. ADDRESSED.

Provide street names. ADDRESSED.

ADDRESSED. Label storm infrastructure (MH, inlet, pipes, culverts, swales, etc) and include if it's public/private. States do not need to be provided at this time.

Use Design Point designations, as done on other DP Table, such as "DPs 1-B, 2-B" instead of "A,B,C,D". ADDRESSED.

Show and label Phase 2 boundary. ADDRESSED.

Update flows in these tables. Several do not match hydrology spreadsheet. ADDRESSED.

**SUMMARY RUNOFF TABLE**

BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
A1-A	3.22	14	2.2	8.5
A2-A	1.23	35	1.7	4.6
B1-A	0.26	79	0.8	1.6
B2-A	1.02	64	2.6	5.3
B3-A	0.87	69	2.6	5.2
B4-A	0.86	61	2.3	4.9
C1-A	0.56	67	1.5	3.1
D1-A	0.82	38	1.3	3.2
E1-A	0.18	77	0.6	1.2
E2-A	0.73	67	1.9	3.9
E3-A	0.95	69	2.7	5.4
E4-A	1.12	68	3.0	6.1
E5-A	1.23	68	3.3	6.7
E6-A	0.96	63	2.3	4.8
F1-A	0.40	68	1.2	2.4
G1-A	4.69	20	3.9	13.1
H1-A	0.41	70	1.2	2.3
H2-A	1.05	70	2.8	5.6
H3-A	0.70	63	1.9	4.0
H4-A	1.78	66	4.3	8.8
H5-A	3.72	44	5.7	13.5
I1-A	0.63	57	1.3	2.9
J1-A	1.55	28	1.8	5.1
K1-A	1.66	68	4.1	8.3

**DESIGN POINT SUMMARY TABLE**

DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>s</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
1-A	K1-A	4.1	8.3
2-A	H5-A	5.7	13.5
2.1-A	DPS 1-A, 2-A	9.4	21.0
3-A	H3-A, H4-A	6.0	12.3
4-A	J1-A	1.8	5.1
4.1-A	DPS 2.1-A, 4-A	10.5	24.4
5-A	H2-A	2.8	5.6
6-A	H1-A, DPS 3-A, 5-A	8.7	17.8
7-A	I1-A	1.3	2.9
8-A	DPS 4.1-A, 6-A, 7-A	19.6	43.2
9-A	G1-A	3.9	13.1
9.1-A	DPS 8-A, 9-A	22.7	54.0
10-A	E6-A	2.3	4.8
11-A	E5-A, DPS 10-A	4.2	8.5
12-A	E3-A, E4-A	5.6	11.5
13-A	E2-A, DPS 12-A	6.4	12.9
14-A	E1-A, DPS 11-A, 13-A	8.9	18.2
15-A	F1-A	1.2	2.4
16-A	DPS 9.1-A, 14-A, 15-A	29.1	65.9
17-A	D1-A	1.3	3.2
17.1-A	DPS 16-A, 17-A	29.5	67.2
18-A	B4-A	2.3	4.9
19-A	B2-A, B3-A, DPS 18-A	6.3	12.9
20-A	B1-A, DPS 19-A	6.6	13.5
21-A	C1-A	1.5	3.1
22-A	DPS 17.1-A, 20-A, 21-A	34.9	78.0
23-A	A2-A	1.7	4.6
24-A	DPS 23-A	1.7	4.5
25-A	A1-A, DPS 22-A, 24-A	37.6	87.1

**SUMMARY RUNOFF TABLE**

BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
A-B	3.52	39	6.6	11.0
B-B	2.50	55	6.2	10.4
C-B	0.83	47	1.9	3.2
D-B	1.05	45	2.4	4.1
E-B	4.05	45	8.7	14.6
F-B	2.95	43	6.1	10.3
G-B	2.15	56	4.8	8.1
H-B	4.77	40	8.7	14.7
I-B	2.06	51	4.1	7.0
J-B	2.77	60	6.6	11.0
K-B	2.30	58	5.9	9.8
L-B	2.14	39	4.6	7.7
M-B	1.81	44	4.0	6.8
N-B	4.10	20	6.8	11.5
O-B	1.18	0	2	3.1

**DESIGN POINT SUMMARY TABLE**

DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>s</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
DP1-B	A, B	11.9	20.0
DP2-B	C, D	4.2	7.1
DP3-B	A, B, C, D	0.0	26.5
DP4-B	E	8.7	14.6
DP5-B	F	6.1	10.3
DP6-B	E, F	0.0	24.6
DP7-B	A, B, C, D, E, F	0.0	49.8
DP8-B	G	4.8	8.1
DP9-B	H	8.7	14.7
DP10-B	G, H	0.0	22.5
DP11-B	I	7.9	15.8
DP12-B	A, B, C, D, E, F, I	0.0	62.6
DP13-B	J, K, L	14.4	27.4
DP14-B	A-L	0.0	109.7
DP15-B	M	7.8	13.4
DP16-B	A-M	68.9	121.7

**LEGEND:**

- PROPOSED MAJOR CONTOUR: — 5250
- PROPOSED MINOR CONTOUR: - - - 5250
- EXISTING MAJOR CONTOUR: — 5250
- EXISTING MINOR CONTOUR: - - - 5250
- PROPOSED STORM SEWER: —
- PROPOSED DRAINAGE SWALE: —
- PROPERTY LINE: —
- PROPOSED FLOW DIRECTION: —
- EXISTING FLOW DIRECTION: —
- PROPOSED DRAINAGE BASIN: —
- DESIGN POINT: —
- PROPOSED BASIN LABEL: —

We need to know how much of the proposed area of disturbance (not just the impervious surfaces) is treated vs untreated and if there are any exclusions that apply to the untreated areas. So please create a basic overview map (or modify an existing drainage map) with color shading/hatching that shows areas tributary to each PBMP (pond, runoff reduction, etc.) and those disturbed areas that are not treated by a PBMP, with the applicable exclusion listed in ECM App 1.7.1.B.#. An accompanying map would also be very helpful (two examples).

HR GREEN RESPONSE: THERE ARE NO EXCLUDED AREAS. HATCHING HAS BEEN ADDED TO DELINEATE WHICH BASINS ARE TRIBUTARY TO WHICH POND, HOWEVER.

**Water Quality Treatment Summary Table**

Basin ID	Total Area (ac)	Proposed Disturbed Area (ac)	Area Trib to Pond A (ac)	Disturbed Area Treated via Runoff Reduction (ac)	Disturbed Area Excluded from WQ per ECM App 1.7.1.C.1 (ac)	Disturbed Area Excluded from WQ per ECM App 1.7.1.B.# (ac)	Applicable WQ Exclusions (App 1.7.1.B.#)
A	4.50	4.50	4.50				
B	1.25	1.25		1.25			
C	6.00	4.00				4.00	ECM App 1.7.1.B.5
D	2.50	2.50	1.00		0.50		ECM App 1.7.1.B.7
E	3.00		3.00				
F	8.25	12.25	8.50	1.25	0.50		
Total	25.50	12.25	8.50	1.25	0.50	5.00	

**PBMP SUMMARY TABLE**

BASINS	PBMP TRIBUTARY AREA (AC)	PBMP
A1,1	1.43	RG-A1.1
A3,1	1.87	RG-A3.1
B1,B2	8.60	EDB-B
OA2,A2	0.95	EXCLUDED*

\* EXCLUDED BASED ON < 1-ACRE OF DEVELOPED ROADWAY AREA PER ECM APP. 17.C.1.g

Unless this maintenance path acts as a berm with a swale on the north side (which I'm not seeing from the topo), then these orange areas are not actually tributary to the ponds as stated in the report narrative above. ADDRESSED.

Add north arrow and scale. ADDRESSED.

DRAWN BY: CBM JOB DATE: ---  
APPROVED: KMH JOB NUMBER: 201662  
CAD DATE: 12/15/2023  
CAD FILE: J:\2020\201662\CAD\DWG\CIPUD\_Phase\_2\_662.202\Drainage\_02-DR

**NO. DATE BY REVISION**

NO.	DATE	BY	REVISION

PHASE 2  
**D-R-HORTON**  
America's Builder

####  
PROPOSED DRAINAGE CONDITIONS  
SHEET DRN 1



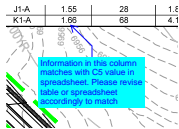
# V1\_Drainage Report - Preliminary Review 1.pdf Markup Summary

## Callout (32)



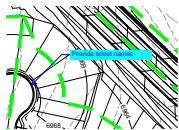
**Subject:** Callout  
**Page Label:** [1] EX1  
**Author:** CDurham  
**Date:** 1/30/2024 5:32:13 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Have project boundary be more pronounced



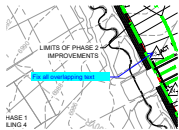
**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/31/2024 9:10:08 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Information in this column matches with C5 value in spreadsheet. Please revise table or spreadsheet accordingly to match



**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:34:54 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Provide street names



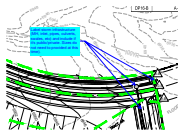
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**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:35:24 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Fix all overlapping text



**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:37:52 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Use Design Point designations, as done on other DP Table, such as "DPs 1-B, 2-B" instead of "A,B,C,D"



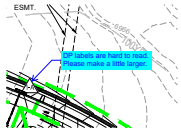
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**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/31/2024 9:28:09 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Label storm infrastructure (MH, inlet, pipes, culverts, swales, etc) and include if it's public/private. Sizes do not need to provided at this time).

NO.	Flow	Intensity
1	1.0	1.0
2	1.0	1.0
3	1.0	1.0
4	1.0	1.0
5	1.0	1.0
6	1.0	1.0
7	1.0	1.0
8	1.0	1.0
9	1.0	1.0
10	1.0	1.0
11	1.0	1.0
12	1.0	1.0
13	1.0	1.0
14	1.0	1.0
15	1.0	1.0
16	1.0	1.0
17	1.0	1.0
18	1.0	1.0
19	1.0	1.0
20	1.0	1.0

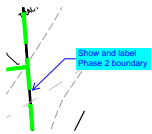
**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:40:12 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Update flows in these tables. Several do not match hydrology spreadsheet



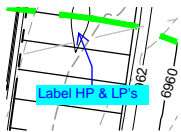
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**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:40:46 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

DP labels are hard to read. Please make a little larger.



**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:41:23 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Show and label Phase 2 boundary



**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:43:49 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Label HP & LP's

NO.	Flow	Intensity
1	1.0	1.0
2	1.0	1.0
3	1.0	1.0
4	1.0	1.0
5	1.0	1.0
6	1.0	1.0
7	1.0	1.0
8	1.0	1.0
9	1.0	1.0
10	1.0	1.0
11	1.0	1.0
12	1.0	1.0
13	1.0	1.0
14	1.0	1.0
15	1.0	1.0
16	1.0	1.0
17	1.0	1.0
18	1.0	1.0
19	1.0	1.0
20	1.0	1.0

**Subject:** Callout  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:49:59 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Highlighted flows cannot be 0 cfs. Appears that intensity is missing. Please update.

NO.	Flow	Intensity
1	1.0	1.0
2	1.0	1.0
3	1.0	1.0
4	1.0	1.0
5	1.0	1.0
6	1.0	1.0
7	1.0	1.0
8	1.0	1.0
9	1.0	1.0
10	1.0	1.0
11	1.0	1.0
12	1.0	1.0
13	1.0	1.0
14	1.0	1.0
15	1.0	1.0
16	1.0	1.0
17	1.0	1.0
18	1.0	1.0
19	1.0	1.0
20	1.0	1.0

**Subject:** Callout  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:50:25 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Missing flow rate for design point

ort. There is another floodplain channel to the north of development and studies as a future project. g planned developments include the Grandview Res sion to west of the site on the west side of Easton Property. 70.6% of proposed residential development rovements, and stormwater treatment infrastructure and topography of the site is native grasses/vee s ranging from 2% to 4%.

**Subject:** Callout  
**Page Label:** 4  
**Author:** CDurham  
**Date:** 1/31/2024 8:43:19 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

68.72 per other documents

f basin B1 and the existing MST2 tributary run t southeast towards Detention Pond C. C. , medium and high density dwelling units and a vious value of 51.20% and runoff rates for the t  
Only provide relevant sheets from the report.

**Subject:** Callout  
**Page Label:** 6  
**Author:** CDurham  
**Date:** 1/31/2024 9:03:51 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Only provide relevant sheets from the report.

**Subject:** Callout  
**Page Label:** 23  
**Author:** CDurham  
**Date:** 1/31/2024 9:09:41 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Labels appear to be switched for these 2 columns

a, and the proposed full spectrum detention yed via grade separated DP23-A, 12' x 12' area. Stormwater (Q<sub>10</sub> = 1.7 cfs Q<sub>100</sub> = 4.6 cfs) 18' HDPE culvert crossing at DP23-A. sd area, and townhome lot area. Stormwater to public right-of-way to a public type B inlet at 31c storm sewer network.

**Subject:** Callout  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:27:24 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per ECM Section 3.3.1.J.1 all public pipe must be RCP

2' inside the public 18' HDPE culvert crossing at DP23-A. DP23 area, landscaped area, and townhome lot area. Stormwater is conveyed via curb and gutter in the public right-of-way to go to DP23-A. DP23 area, landscaped area, and townhome lot area. Stormwater is conveyed via curb and gutter in the public right-of-way to go to DP23-A. DP23 area, landscaped area, and townhome lot area. Stormwater is conveyed via curb and gutter in the public right-of-way to go to DP23-A.

**Subject:** Callout  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:34:28 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

From drainage map, Basin B4-A appears to go towards DP 18-A

a public type B inlet at DP20-A, and ultimately draining to I network. ight-of-way (ROW) area, landscaped area, and townhome s conveyed via curb and gutter in the public right-of-way to go to DP20-A. DP20 area, landscaped area, and townhome lot area. Stormwater is conveyed via curb and gutter in the public right-of-way to go to DP20-A. DP20 area, landscaped area, and townhome lot area. Stormwater is conveyed via curb and gutter in the public right-of-way to go to DP20-A.

**Subject:** Callout  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:37:04 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per routing spreadsheet, Basin B1-A combines at DP20-A



is 0.73 acres of right-of-way (ROW) area, landscaped area, and treatment area, and treatment to DP12-A. Runoff then follows pattern of subbasin E1-A. Runoff then follows pattern of DP14-A, and ultimately draining to Pond A via the gutter.

**Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.**

**Subject:** Callout  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:42:51 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.

is 0.73 acres of right-of-way (ROW) area, landscaped area, and treatment to DP12-A. Runoff then follows pattern of subbasin E1-A. Runoff then follows pattern of DP14-A, and ultimately draining to Pond A via the gutter.

**Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.**

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 9:44:51 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Basin E2-A is combined at DP 13-A according to spreadsheet. Revise report or spreadsheet to match

is 0.73 acres of right-of-way (ROW) area, landscaped area, and treatment to DP12-A. Runoff then follows pattern of subbasin E1-A. Runoff then follows pattern of DP14-A, and ultimately draining to Pond A via the gutter.

**Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.**

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:38:24 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per routing spreadsheet combines with Basin E6-A. Revise report or spreadsheet to match

is 0.73 acres of right-of-way (ROW) area, landscaped area, and treatment to DP12-A. Runoff then follows pattern of subbasin E1-A. Runoff then follows pattern of DP14-A, and ultimately draining to Pond A via the gutter.

**Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.**

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:16:56 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

DP15-A per routing spreadsheet

is 0.73 acres of right-of-way (ROW) area, landscaped area, and treatment to DP12-A. Runoff then follows pattern of subbasin E1-A. Runoff then follows pattern of DP14-A, and ultimately draining to Pond A via the gutter.

**Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.**

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:18:40 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Area doesn't match with spreadsheet Please update.

is 0.73 acres of right-of-way (ROW) area, landscaped area, and treatment to DP12-A. Runoff then follows pattern of subbasin E1-A. Runoff then follows pattern of DP14-A, and ultimately draining to Pond A via the gutter.

**Per routing spreadsheet, this basin combines with Basins E3-A & E4-A at DP 13-A. Basin E1-A combines at BP 14-A. Verify and update report or spreadsheet accordingly.**

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:47:13 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per routing spreadsheet, only Basins H3-A & H4-A are combined at DP3-A.

network.  
Basin H3-A is 0.70 acres or  
(C<sub>o</sub> = 1.9 cfs C<sub>100</sub> = 4.0 cfs  
Area doesn't match with  
note of sube  
network.  
Basin H4-A is 0.78 acres or  
(C<sub>o</sub> = 4.3 cfs C<sub>100</sub> = 8.8 cfs  
combines with those of sube

**Subject:** Callout  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:47:41 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Area doesn't match with spreadsheet Please update.

1. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
2. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
3. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
4. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
5. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
6. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
7. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
8. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
9. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
10. A public right-of-way (ROW) area, substantially matching to Point A via the proposed

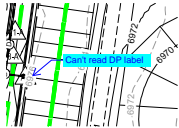
**Subject:** Callout  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:48:02 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Area doesn't match with spreadsheet Please update.

1. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
2. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
3. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
4. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
5. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
6. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
7. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
8. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
9. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
10. A public right-of-way (ROW) area, substantially matching to Point A via the proposed

**Subject:** Callout  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:52:11 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per routing spreadsheet, Basin 5H-A combines with Basin H1-A at DP6-A. Please revise report or spreadsheet to match.



**Subject:** Callout  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/31/2024 10:53:27 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Can't read DP label

1. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
2. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
3. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
4. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
5. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
6. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
7. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
8. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
9. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
10. A public right-of-way (ROW) area, substantially matching to Point A via the proposed

**Subject:** Callout  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:54:53 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Area doesn't match with spreadsheet Please update.

1. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
2. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
3. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
4. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
5. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
6. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
7. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
8. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
9. A public right-of-way (ROW) area, substantially matching to Point A via the proposed  
10. A public right-of-way (ROW) area, substantially matching to Point A via the proposed

**Subject:** Callout  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 11:06:52 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Please update all basin flows in this section to match with hydrology spreadsheet.

hours, respectively. A forebay is located a  
rds the outlet structure. A 10' access an  
facilitate maintenance of the pond facilities  
developed, peak 100-yr flow rate with 1.0'

Per DCM Section 11.2.2  
minimum width for access  
is 15'. Please revise

**Subject:** Callout  
**Page Label:** 10  
**Author:** CDurham  
**Date:** 1/31/2024 11:12:45 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Per DCM Section 11.2.2 minimum width for access  
is 15'. Please revise

twice water quality treatment, and detention  
toxic rates. The WQCV is 0.597 ac-ft, the  
4 ac-ft. The WQCV, EBRV and 100-year  
bay is located at the outlet into the pond and  
A 15' access and maintenance road is  
the pond facilities. A 77.5' emergency overflow  
we rate with 1% of the peak 100-yr flow rate.  
Per DCM Section 11.2.2  
minimum width for access  
is 15'. Please revise

all of this resulting in the drainage, closed  
posed River Road extension and be conveyed  
a Phase 2 western boundary. An analysis has  
is shown as described within the Grading  
formulas 9079 873 (MARI). Both scenarios

**Subject:** Callout  
**Page Label:** 11  
**Author:** CDurham  
**Date:** 1/31/2024 11:14:33 AM  
**Status:**  
**Color:** ■  
**Layer:**  
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Per DCM Section 11.2.2 minimum width for access  
is 15'. Please revise

### Highlight (18)

0.0  
1

**Subject:** Highlight  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:48:42 PM  
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0.0

0.0

**Subject:** Highlight  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:48:55 PM  
**Status:**  
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0.0

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**Subject:** Highlight  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:48:57 PM  
**Status:**  
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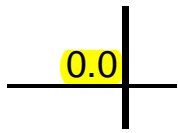
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0.0  
0

**Subject:** Highlight  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:48:59 PM  
**Status:**  
**Color:** ■  
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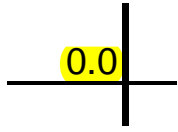
0.0






**Subject:** Highlight  
**Page Label:** 30  
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**Date:** 1/30/2024 5:49:01 PM  
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0.0



**Subject:** Highlight  
**Page Label:** 30  
**Author:** CDurham  
**Date:** 1/30/2024 5:49:03 PM  
**Status:**  
**Color:**   
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0.0

3 acres of right-of-way (ROW) = 3.9 cfs) is conveyed via use of subbasin E1-A. Runoff from subbasin E1-A, and ultimately drain


**Subject:** Highlight  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:41:35 AM  
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subbasin E1-A.

is conveyed via subbasin E1-A. Runoff from subbasin E1-A, and ultimately draining to


**Subject:** Highlight  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 9:45:46 AM  
**Status:**  
**Color:**   
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is 3.22 acres conveyed via a

**Subject:** Highlight  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:17:03 AM  
**Status:**  
**Color:**   
**Layer:**  
**Space:**

3.22


of right-of-way (ROW) area, landscape is conveyed via curb and gutter in subbasin H1-A, H4-A, and H5-A. Runoff from subbasin H1-A, H4-A, and H5-A, ultimately draining to inlet at DP6-A.

**Subject:** Highlight  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:39:36 AM  
**Status:**  
**Color:**   
**Layer:**  
**Space:**

H1-A, H4-A, and H5-A.


of right-of-way (ROW) area, landscape

Area is 0.78 ac  
fs Q<sub>100</sub> = 8.

**Subject:** Highlight  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:46:28 AM  
**Status:**  
**Color:**   
**Layer:**  
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0.78

of right-of-way (ROW) area, landscaped areas) is conveyed via curb and gutter into subbasin H1-A, H3-A, and H5-A. Runoff

**Subject:** Highlight  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:47:21 AM  
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H1-A, H3-A, and H5-A.

Area is 3.75 ac  
fs Q<sub>100</sub> = 1;

**Subject:** Highlight  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:48:08 AM  
**Status:**  
**Color:**   
**Layer:**  
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3.75



**Subject:** Highlight  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:50:47 AM  
**Status:**  
**Color:**   
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Runoff then follows patterns of subbasin H1-A draining to DP3-A and then to a public type R inlet at DP6-A

Area is 0.63 ac  
conveyed via

**Subject:** Highlight  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:54:56 AM  
**Status:**  
**Color:**   
**Layer:**  
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0.63

draining to Pond A via the proposed public  
**Tributary to and Treated by Pond B**  
3.52 acres of landscaped area, duplex  
water (Q<sub>10</sub> = 0.8 cfs Q<sub>100</sub> = 1.6 cfs) is con  
R inlet at DP1-B, and ultimately draining  
2.50 acres of landscaped area, duplex  
= 1.6 cfs) is conveyed via curb and gutter  
ultimately drain to Pond B via the proposed

**Subject:** Highlight  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:56:20 AM  
**Status:**  
**Color:**   
**Layer:**  
**Space:**

to provide water quality treatment, and d  
w historic rates. The WQCV is 0.505 ac-ft  
; 2.603 ac-ft. The WQCV, EURV and 100-  
A forebay is located at the outfall into the f  
ture. A 10' access and maintenance road  
e of the pond facilities. A 50' emergency c  
-yr flow rate with 1.0' of freeboard towards

**Subject:** Highlight  
**Page Label:** 10  
**Author:** CDurham  
**Date:** 1/31/2024 11:12:15 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

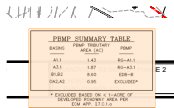
10' access and maintenanc

sserve. A total of 38.19 acres at 43% composite  
d to provide water quality treatment, and deterr  
w historic rates. The WQCV is 0.597 ac-ft, the  
s 2.974 ac-ft. The WQCV, EURV and 100-year  
A forebay is located at the outfall into the pond  
cture. A 10' access and maintenance road is  
se of the pond facilities. A 77.5' emergency ovr  
>-yr flow rate with 1.0' of freeboard towards MS

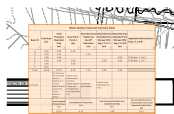
**Subject:** Highlight  
**Page Label:** 11  
**Author:** CDurham  
**Date:** 1/31/2024 11:14:14 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

10' access and maintenance ro

## Image (2)



**Subject:** Image  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 9:45:59 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**



**Subject:** Image  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 9:47:08 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

## Line (9)

3a. Stormwater (Q<sub>s</sub> = 1.7 cfs Q<sub>100</sub> =  
HDPE culvert crossing at DP23-A  
area, and townhome lot area. Ston  
public right-of-way to a public type  
storm sewer network.

**Subject:** Line  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:29:34 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

area, and townhome lot area. Ston

nveyed via (B1-A, B3  
sin B1-A, B3  
t DP20-A, a

**Subject:** Line  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:31:10 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**



conveyed  
in B1-A, B:  
at DP20-A,

**Subject:** Line  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:31:46 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

rea. Stormwater (Q<sub>5</sub> = 1.3 cfs Q<sub>100</sub> =  
-A, and ultimately draining to Pond  
area, ~~end-townhome-lot-area~~. Storm  
public right-of-way to a public type I  
storm sewer network.

**Subject:** Line  
**Page Label:** 7  
**Author:** CDurham  
**Date:** 1/31/2024 9:39:12 AM  
**Status:**  
**Color:** ■  
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**Space:**

right-of-way (ROW)  
s conveyed via cu  
sin E2-A, and E4-  
public type R inle

**Subject:** Line  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 9:44:46 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

ea. Stormwater (Q<sub>5</sub> = 3.9 cfs Q<sub>100</sub> =  
st at DP9-A, and ultimately drainin  
area, ~~and-townhome-lot-area~~. Storm  
ublic right-of-way to a public type  
orm sewer network.  
ng lot, landscaped area, and town

**Subject:** Line  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:29:53 AM  
**Status:**  
**Color:** ■  
**Layer:**  
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02) is conveyed via grass swales in 1-foot rise to a public type R, meet  
Pond A via the proposed public storm sewer network.  
Block 01-A is 0.41 acres of right-of-way (ROW) area, landscaped as  
Q<sub>5</sub> = 2.09 cfs Q<sub>100</sub> = 2.3 cfs) is conveyed via curb and gutter in the pu  
DP3-A, and ultimately draining to Pond A via the proposed public sto  
Block 02-A is 1.05 acres of right-of-way (ROW) area, asphalt parking  
area. Stormwater (Q<sub>5</sub> = 2.49 cfs Q<sub>100</sub> = 2.6 cfs) is conveyed via curb an  
DP3-A, ~~where the stormwater is conveyed to Pond A via the proposed~~ to Pond A  
draining to a public type R inlet at DP3-A, ultimately draining to Pond  
network.

**Subject:** Line  
**Page Label:** 8  
**Author:** CDurham  
**Date:** 1/31/2024 10:31:18 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

sa. Stormwater  
-A, ~~where flows~~  
to DP3-A and  
orm sewer

**Subject:** Line  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:50:31 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

draining to a public type R inlet at DP6-A, ultimate network.  
Basin 105-A is 3.75 acres of right-of-way (ROW) (Q<sub>10</sub> = 5.7 cfs Q<sub>100</sub> = 13.5 cfs) is conveyed via ~~conduit~~ with those of subbasin #111A. Runoff then to a public type R inlet at DP6-A, ultimate network.  
Basin 111-A is 0.63 acres of right-of-way (ROW) (Q<sub>10</sub> = 1.3 cfs Q<sub>100</sub> = 2.9 cfs) is conveyed via DP7-A, and ultimately draining to Pond A via 1

**Subject:** Line  
**Page Label:** 9  
**Author:** CDurham  
**Date:** 1/31/2024 10:50:37 AM  
**Status:**  
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**Layer:**  
**Space:**

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### Polygon (2)



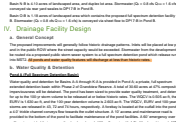
**Subject:** Polygon  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:11:15 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**



**Subject:** Polygon  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:14:02 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

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### SW - Highlight (1)

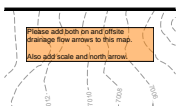


**Subject:** SW - Highlight  
**Page Label:** 10  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:39:48 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

All ponds and water quality features will discharge at less than historic rates.

---

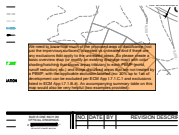
### SW - Textbox (4)



**Subject:** SW - Textbox  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:05:23 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

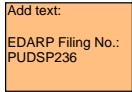
Please add both on and offsite drainage flow arrows to this map.

Also add scale and north arrow.



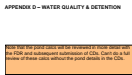
**Subject:** SW - Textbox  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 9:45:30 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

We need to know how much of the proposed area of disturbance (not just the impervious surfaces) is treated vs untreated and if there are any exclusions that apply to the untreated areas. So please create a basic overview map (or modify an existing drainage map) with color shading/hatching that shows areas tributary to each PBMP (pond, runoff reduction, etc.) and those disturbed areas that are not treated by a PBMP, with the applicable exclusion labeled (ex: 20% up to 1ac of development can be excluded per ECM App I.7.1.C.1 and exclusions listed in ECM App I.7.1.B.#). An accompanying summary table on this map would also be very helpful (two examples provided):



**Subject:** SW - Textbox  
**Page Label:** 1  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:53:07 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Add text:  
 EDARP Filing No.: PUDSP236



**Subject:** SW - Textbox  
**Page Label:** 33  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 3:32:23 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Note that the pond calcs will be reviewed in more detail with the FDR and subsequent submission of CDs. Can't do a full review of these calcs without the pond details in the CDs.

SW - Textbox with Arrow (10)



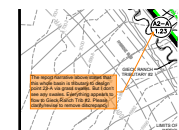
**Subject:** SW - Textbox with Arrow  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:25:00 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Unless this maintenance path acts as a berm with a swale on the north side (which I'm not seeing from the topo), then these orange areas are not actually tributary to the ponds as stated in the report narrative above.



**Subject:** SW - Textbox with Arrow  
**Page Label:** 7  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:17:42 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

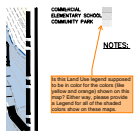
Swales not shown on Drainage Map. Please clarify how flows will reach their intended design points and ultimately the pond. Or if any WQ exclusions are applicable.



**Subject:** SW - Textbox with Arrow  
**Page Label:** [1] DRAINAGE MAP  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:24:26 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

The report narrative above states that this whole basin is tributary to design point 23-A via grass swales. But I don't see any swales. Everything appears to flow to Gieck Ranch Trib #2. Please clarify/revise to remove discrepancy.





**Subject:** SW - Textbox with Arrow  
**Page Label:** [1] 00-Drainage Basins-DR2  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:28:34 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Is this Land Use legend supposed to be in color for the colors (like yellow and orange) shown on this map? Either way, please provide a Legend for all of the shaded colors show on these maps.



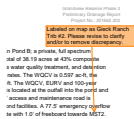
**Subject:** SW - Textbox with Arrow  
**Page Label:** 10  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:29:29 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Swales not shown on Drainage Map. Please clarify how flows will reach their intended design points and ultimately the pond. Or if any WQ exclusions are applicable.



**Subject:** SW - Textbox with Arrow  
**Page Label:** 10  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:40:11 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Labeled on map as Gieck Ranch Trib #2. Please revise to clarify and/or to remove discrepancy.



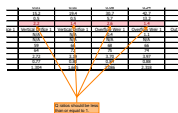
**Subject:** SW - Textbox with Arrow  
**Page Label:** 11  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:40:01 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Labeled on map as Gieck Ranch Trib #2. Please revise to clarify and/or to remove discrepancy.



**Subject:** SW - Textbox with Arrow  
**Page Label:** 36  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:39:12 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Q ratios should be less than or equal to 1.



**Subject:** SW - Textbox with Arrow  
**Page Label:** 41  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:38:41 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Q ratios should be less than or equal to 1.

for area Stormwater (Q = 0.8 cfs/ft<sup>2</sup> × 1.6 cfs/ft<sup>2</sup>) is  
in the proposed full spectrum detention facility Pond  
is shown for DP 17-B in Pond B.  
This statement conflicts with what is shown  
in the Q ratios on the two MHFD-Detention  
spreadsheet.  
drainage patterns. Sites will be placed at low points  
as indicated. Stormwater from the development will  
full spectrum detention pond which release runoff  
temporarily to area from basins/cases.  
is provided in Pond A. is provided. full spectrum

**Subject:** SW - Textbox with Arrow  
**Page Label:** 10  
**Author:** Glenn Reese - EPC Stormwater  
**Date:** 1/29/2024 10:41:21 AM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

This statement conflicts with what is shown as the Q ratios on the two MHFD-Detention spreadsheet.

## Text Box (9)

### APPENDIX E - REFERENCES

For Reference Material, please only include sheets that are relevant to this portion of the project (Phase 2). Also, highlight specific information, such as basins & DP's being discussed within this report.

**Subject:** Text Box  
**Page Label:** 44  
**Author:** CDurham  
**Date:** 1/30/2024 5:10:55 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

For Reference Material, please only include sheets that are relevant to this portion of the project (Phase 2). Also, highlight specific information, such as basins & DP's being discussed within this report.



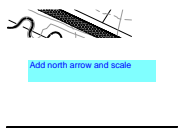
**Subject:** Text Box  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:33:33 PM  
**Status:**  
**Color:** ■  
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**Space:**

Property owner information



**Subject:** Text Box  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:38:17 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Missing DP 17-B



**Subject:** Text Box  
**Page Label:** [1] DRAINAGE MAP  
**Author:** CDurham  
**Date:** 1/30/2024 5:42:03 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Add north arrow and scale

ortheast boundary for Phase 2 along Res Road. This  
note. Indicate when/what phase or filing  
this channel will be evaluated with.  
son facilities in the area.  
ing utilities or other encumbrances on site.  
ement  
p 08041C0552G & 08041C0566G (eff. 12/7/2018), p

**Subject:** Text Box  
**Page Label:** 5  
**Author:** CDurham  
**Date:** 1/31/2024 8:45:34 AM  
**Status:**  
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