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### Grandview Reserve Phase 2 Preliminary Drainage Report

July 2024

HR Green Project No: 201662.202

#### Prepared For:

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#### Prepared By:

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> EDARP Filing No.: PUDSP236



### Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Date

Ken Huhn, P.E.	
State of Colorado No. 54022	
For and on behalf of HR Green Development, LLC	

### Owner/Developer's Statement:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Authorized Signa	ture
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Address: D.R. Horton 9555 S. Kingston Court Englewood, CO

### El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

Joshua Palmer, P.E.

County Engineer/ECM Administrator

Conditions:

Date

Date



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## I. General Purpose, Location and Description

#### a. Purpose

The purpose of this Preliminary Drainage Report (PDR) for the Grandview Reserve Subdivision Phase 2 is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls.

#### b. Location

The Grandview Reserve Phase 2 site is located in unincorporated El Paso County, Colorado. The Phase 2 location (referred to as the site herein) is located northwest of Grandview Reserve Filings 1-4 and MST2, and southeast of the intersection of Eastonville Road & Rex Road.

The site lies within a tract of land within Sections 21 and 28, Township 12 South, Range 64 West of the 6<sup>th</sup> Principal Meridian, in El Paso County, State of Colorado. A Vicinity Map is included in **Appendix A**.

The site is bound by a segment of Rex Road to be developed with this project to the northeast and undeveloped land that has historically been used as ranching lands. The east of the site will be a future phase of the Grandview Reserve Subdivision. The south and west of the site is bound by Grandview Reserve Filings 1-4 and MST2. A vicinity map is presented in Appendix A.

The Gieck Ranch Tributary #2 "MST2" is a part of the Gieck Ranch Drainage Basin tributary to Black Squirrel Creek. The channel draining through the site is an ongoing project with associated CLOMR Report (PCD File No. is CDR228 with El Paso County). The Grandview Reserve improvements will follow any requirements of that report. There is another floodplain channel to the north of Rex Road that will not be disturbed by this phase of development and studied in a future project.

The existing surrounding platted developments include the Grandview Reserve Phase 1 Filings 1-4, and the Meridian Ranch Subdivision that is west of the site, on the west side of Eastonville Road.

### c. Description of Property

The site is approximately 68.61 acres of proposed residential development with associated right of way, open space tracts, public improvements, and stormwater treatment infrastructure.

The existing groundcover and topography of the site is native grasses/weeds and exposed soil on gently rolling hillside with slopes ranging from 2% to 4%.

Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam. Soils were hydraulically analyzed as 90% Type B to account for being disturbed in the proposed condition. The NRCS soil survey is presented in **Appendix A**.

There is one major drainageway through the site. The Gieck Ranch Tributary #2 (MST2 as referenced in the MDDP) traverses the site along its southwestern boundary and forms the southwest boundary for Phase 2. This drainageway generally flows from the northwest to the southeast towards Highway 24, before crossing through existing drainage infrastructure. The CLOMR report by HR Green for MST2 is ongoing and pending approval for this channel. Refer to the CLOMR report included in **Appendix E** for more specific design information regarding the MST2 channel. A tributary referred to as the East Fork Tributary (EFT) in the MDDP



traverses the site along its northeastern boundary and forms the northeast boundary for Phase 2 along Rex Road. The initial analysis of this drainage way has been performed by HR Green in conjunction with Phase 2. The analysis delineated the 100-yr floodplain and ensures the construction of Rex Road will not impact the floodplain. This channel will not be disturbed by this phase of development. A CLOMR report is not required by the County at this time.

There are no known irrigation facilities in the area.

There are no known existing utilities or other encumbrances on site.

### d. Floodplain Statement

Based on FEMA Firm map 08041C0552G & 08041C0556G (eff. 12/7/2018), the site contains flood Zone A through the site which is part of the Gieck Ranch Tributary #2. See FEMA Firm Maps in **Appendix A**. This floodplain is being studied and revised in the Gieck Ranch Tributary # 2 CLOMR report. A copy of the current revised floodplain map is also provided in **Appendix A**. There is a Zone A floodplain northeast of the site which will not be altered with this project's improvements.

### II. Drainage Design Criteria

### a. Drainage Criteria

Hydrologic data and calculations were performed using Drainage Criteria Manual Volume 1 of El Paso County (EPCDCM), with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual (CCSDCM), May 2014 revised January 2021.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Private, full spectrum Detention. Detention pond allowable release rate will be limited to less than historic rates.

Rainfall Depths per NOAA A	tlas 14	
Return Period (yr)	5	100
1-hr Rainfall Depth (in)	1.21	2.49

Storm sewer and inlet sizing shown is preliminary at this stage of the project. Calculations for the storm sewer system on site will be provided with the Final Drainage Report (FDR) for the project. The sizing methodology that will be used is per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer sizing was performed per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

This preliminary drainage report follows any recommendations and is in conformance with the previously approved MDDP for the site prepared by HR Green, "*Grandview Reserve Master Development Drainage Plan*", HR Green, August 2021 (MDDP).



### III. Drainage Basins and Subbasins

### a. Major Basin Description

The site is located within the Gieck Ranch Drainage Basin. The site's drainage characteristics were previously studied in the following reports:

- 1. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
- 2. "Grandview Reserve Master Development Drainage Plan" prepared by HR Green, August 2021.
- 3. "Grandview Reserve Filing No. 1 Preliminary Drainage Report" prepared by Galloway & Company, Inc., September 2022.
- 4. "Grandview Reserve CLOMR REPORT" prepared by HR Green, November 22 2023

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains to the Arkansas River. The majority of the basin is undeveloped and rolling range land of 2% - 4% slopes.

The Grandview Reserve MDDP divided the site into 8 major drainage basins (A-H), where each basin is tributary to a full spectrum detention pond facility. The Grandview Reserve Phase 2 improvements are located in subbasins B3 and C1 of the MDDP.

There are no known existing irrigation facilities or other obstructions that could influence or will be influenced by local drainage characteristics. Proposed local drainage characteristics will continue to follow historic patterns. Offsite flows entering Phase 2 from Phase 1 are accounted for in the drainage calculations.

### b. Existing Subbasin Description

The Grandview Reserve Phase 2 site drains from the northwest to the southeast slopes ranging from 2% - 4%. The site has historically drained into the Gieck Ranch Tributary #2 (the existing MST2).

The existing subbasins for the Grandview Reserve Phase 2 site were studied the approved MDDP for Grandview Reserve. This site is located within subbasins B3 and C1 of this report and are described as follows.

"Subbasin B3 is located between MS and EF and to the northeast of east of basin B2. The existing MST2 tributary runs through the basin. The site drains towards the southeast and towards Detention Pond B. Current planning documents call for high, medium-high, and medium density dwelling units along with a pocket park. The basin is 118.90 acres, with a composite impervious value of 49.42% and runoff rates for the 5 and 100 year of 92.76 cfs and 295.27 cfs respectively."

"Subbasin C1 is located to the northeast of east of basin B1 and the existing MST2 tributary runs through the middle of the basin. The basin drains towards the southeast and towards Detention Pond C. Current planning documents call for an institutional parcel, medium and high-density dwelling units and a pocket park. The basin is 77.83 acres, with a composite impervious value of 51.20% and runoff rates for the 5 and 100-year of 77.99 cfs and 238.03 cfs respectively."

A copy of the referenced pages of the approved MDDP has been included in **Appendix E** of this report. The proposed drainage conditions for this development will follow historic drainage patterns as described in the MDDP.





#### c. Proposed Subbasin Description

#### **Description of Proposed Project**

The proposed drainage conditions for the site generally follow historic drainage patterns. The site drains from the northwest to the southeast at slopes between 0.6% - 4%, into proposed public storm sewer systems via sheetflow/curb & gutter/channel flow which drain to proposed private extended detention basins for treatment and flood attenuation. The northwestern half of the site will drain to and be treated by "Pond A", and the southeastern half of the site will drain to and be treated by "Pond B". Both of these detention ponds will outfall into the rerouted channel MST2. Drainage from both ponds has been accounted for in the channel realignment design and is detailed in the CLOMR report.

There is no anticipated offsite flow that will enter the site.

#### Subbasins Tributary to and Treated by Pond A

Basin A1-A is 3.22 acres of landscaped area, townhome lot area, and the proposed full spectrum detention facility Pond A. Stormwater ( $Q_5 = 2.2$  cfs  $Q_{100} = 8.5$  cfs) is conveyed via grass swales in Tract A to the private detention facility, Pond A at DP16.1-A.

Basin A2-A is 1.23 acres of landscaped area and townhome lot area. Stormwater ( $Q_5 = 2.2 \text{ cfs } Q_{100} = 5.2 \text{ cfs}$ ) is conveyed via grass swales in a rear yard swale to the public 12" RCP & open grate sump inlet at DP10-A.

Basin B1-A is 0.26 acres of right-of-way (ROW) area, asphalt parking lot, and townhome lot area. Stormwater  $(Q_5 = 0.8 \text{ cfs } Q_{100} = 1.6 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin B2-A is 1.02 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater  $(Q_5 = 2.6 \text{ cfs } Q_{100} = 5.3 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to DP14-A, where flows combine with those of subbasin B1-A, B3-A, and B4-A. Runoff then follows patterns of subbasin B1-A and drains to a public type R sump inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin B3-A is 0.89 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater  $(Q_5 = 2.8 \text{ cfs } Q_{100} = 5.5 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to DP19-A, where flows combine with those of subbasin B1-A, B2-A, and B4-A. Runoff then follows patterns of subbasin B1-A and drains to a public type R inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin B4-A is 3. 67 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 8.2 \text{ cfs } Q_{100} = 17.8 \text{ cfs}$ ) is conveyed via curb and gutter in the public right-of-way to DP9-A, where flows combine with those of DP8-A and are captured by a public type R inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin C1-A is 0.63 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater  $(Q_5 = 1.6 \text{ cfs } Q_{100} = 3.4 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP15-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin D1-A is 0.70 acres of landscaped area, asphalt parking lot, and townhome lot area. Stormwater ( $Q_5 = 1.3 \text{ cfs } Q_{100} = 3.4 \text{ cfs}$ ) is conveyed via a swale to an open grate sump inlet at DP13-A, ultimately draining to Pond A via the proposed public storm sewer network.



Basin E1-A is 0.73 acres of right-of-way (ROW) area and landscaped area. Stormwater ( $Q_5 = 1.7$  cfs  $Q_{100} = 3.7$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP8-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin E2-A is 2.56 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 6.2$  cfs  $Q_{100} = 12.9$  cfs) is conveyed via curb and gutter in the public right-of-way to DP9-A, where flows drain to a public type R sump inlet at DP14-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin E3-A is 0.97 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater  $(Q_5 = 2.4 \text{ cfs } Q_{100} = 4.9 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to DP12-A, where flows combine with those of subbasin E4-A and are captured by a Type R sump inlet. Flows are ultimately conveyed to Pond A via the proposed public storm sewer network.

Basin E4-A is 1.02 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater  $(Q_5 = 2.5 \text{ cfs } Q_{100} = 5.2 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to DP11-A, where flows combine with those of subbasin E3-A and are captured by a Type R sump inlet. Flows are ultimately conveyed to Pond A via the proposed public storm sewer network.

Basin F1-A is 0.46 acres of right-of-way (ROW) area, asphalt parking lot, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.2$  cfs  $Q_{100} = 2.5$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP7-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin H1-A is 2.25 acres of right-of-way (ROW) area, landscaped area, and a small amount of townhome lot area. Stormwater ( $Q_5$  = 3.4 cfs  $Q_{100}$  = 8.4 cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP5-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin H2-A is 1.94 acres of right-of-way (ROW) area, asphalt parking lot, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 4.0$  cfs  $Q_{100} = 8.7$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP6-A, combining with DP6-A and ultimately draining to Pond A via the proposed public storm sewer network.

Basin H3-A is 2.80 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater ( $Q_5 = 6.5$  cfs  $Q_{100} = 13.5$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP6-A, combining with DP5-A and ultimately draining to Pond A via the proposed public storm sewer network.

Basin H4-A is 3.87 acres of right-of-way (ROW) area, landscaped area, and townhome lot area. Stormwater  $(Q_5 = 6.4 \text{ cfs } Q_{100} = 14.9 \text{ cfs})$  is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP2-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin J1-A is 1.50 acres of landscaped area, and townhome lot area. Stormwater ( $Q_5 = 1.6$  cfs  $Q_{100} = 4.7$  cfs) is conveyed via grass swale to an open grate inlet at DP4-A, ultimately draining to Pond A via the proposed public storm sewer network.

Basin K1-A is 1.75 acres of right-of-way (ROW) area, and landscaped area. Stormwater ( $Q_5 = 4.3$  cfs  $Q_{100} = 8.8$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP1-A, and ultimately draining to Pond A via the proposed public storm sewer network.

Basin EA6 is 0.70 acres of right-of-way (ROW) area, and landscaped area. Stormwater ( $Q_5 = 3.2$  cfs  $Q_{100} = 5.7$  cfs) is conveyed via curb and gutter into subbasin K1-A at DP 35.1. Runoff continues to drain via curb and



gutter in the public right-of-way to a public type R inlet at DP1-A, and ultimately draining to Pond A via the proposed public storm sewer network. This drainage basin is per the Grandview Reserve Filing 1 PDR.

Basin EA7 is 0.65 acres of right-of-way (ROW) area, and landscaped area. Stormwater ( $Q_5 = 2.6$  cfs  $Q_{100} = 4.8$  cfs) is conveyed via curb and gutter into subbasin H5-A at DP 35.2. Runoff continues to drain via curb and gutter in the public right-of-way to a public type R inlet at DP2-A, and ultimately draining to Pond A via the proposed public storm sewer network. This drainage basin is per the Grandview Reserve Filing 1 PDR.

#### Subbasins Tributary to and Treated by Pond B

Basin A-B is 6.56 acres of landscaped area, duplex lot area, townhome lot area, and right-of-way (ROW) area. Stormwater ( $Q_5$  = 8.5 cfs  $Q_{100}$  = 21.1 cfs) is conveyed via curb and gutter in the public right-of-way to a type R at grade inlet at DP4-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin B-B is 3.55 acres of landscaped area and duplex lot area. Stormwater ( $Q_5 = 2.9$  cfs  $Q_{100} = 9.4$  cfs) is conveyed via grassed swale to a private open grate inlet at DP11-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin C-B is 1.53 acres of landscaped area, duplex lot area, townhome lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 2.9$  cfs  $Q_{100} = 6.5$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R at grade inlet at DP5-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin D-B is 1.03 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5$  = 1.7 cfs  $Q_{100}$  = 4.1 cfs) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP2-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin E-B is 1.03 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 0.6$  cfs  $Q_{100} = 2.7$  cfs) is conveyed via swale to a private open grate sump inlet at DP19-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin F-B is 1.45 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 1.3 \text{ cfs } Q_{100} = 4.2 \text{ cfs}$ ) is conveyed via curb and gutter in the public right-of-way to a public type R at grade inlet at DP5-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin G-B is 2.15 acres of landscaped area and right-of-way (ROW) area. Stormwater ( $Q_5 = 4.0 \text{ cfs } Q_{100} = 8.7 \text{ cfs}$ ) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP8-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin H-B is 4.12 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 5.1$  cfs  $Q_{100} = 12.9$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R inlet at DP9-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin I-B is 0.76 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 1.5 \text{ cfs } Q_{100} = 3.3 \text{ cfs}$ ) is conveyed via curb and gutter in the public right-of-way to a public type R at grade inlet at DP12-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin J-B is 6.81 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 11.9 \text{ cfs } Q_{100} = 26.2 \text{ cfs}$ ) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP13-B, and ultimately draining to Pond B via the proposed public storm sewer network.



Basin K-B is 1.12 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 2.1$  cfs  $Q_{100} = 4.7$  cfs) is conveyed via curb and gutter in the public right-of-way to a public type R at grade inlet at DP1-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin L-B is 1.89 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5 = 1.5 \text{ cfs } Q_{100} = 5.3 \text{ cfs}$ ) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP13-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin M-B is 1.46 acres of landscaped area, duplex lot area, and right-of-way (ROW) area. Stormwater ( $Q_5$  = 2.7 cfs  $Q_{100}$  = 5.9 cfs) is conveyed via curb and gutter in the public right-of-way to a public type R sump inlet at DP15-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin N-B is 3.00 acres of landscaped area, and duplex lot area. Stormwater ( $Q_5 = 1.6$  cfs  $Q_{100} = 7.0$  cfs) is conveyed via rear yard swales to a private open grate sump inlet at DP17-B, ultimately draining to Pond B via the proposed public storm sewer network.

Basin O-B is 1.59 acres of landscaped area which contains the proposed full spectrum detention facility Pond B. Stormwater ( $Q_5 = 0.6$  cfs  $Q_{100} = 4.2$  cfs) is conveyed via sheet flow to DP21-B in Pond B.



### IV. Drainage Facility Design

### a. General Concept

The proposed improvements will generally follow historic drainage patterns. Inlets will be placed at low points and in the public ROW where the street capacity would be exceeded. Stormwater from the development will be routed via a proposed public storm sewer system to full spectrum detention ponds which release runoff into MST2. All ponds and water quality features will discharge the design storms at less than rates specified in the Grandview reserve MDDP. Per DCM Section 2.5.3., release rates will not exceed historic runoff rates.

### b. Water Quality & Detention

The proposed detention facility release rates for the minor and major storms have been taken from the approved Grandview Reserve MDDP. The Grandview Reserve Phase 2 project limits make up approximately 20.98 acres of subbasin C1 in the MDDP, and 41.54 acres of subbasin B3 in the MDDP. From the MDDP subbasin C1 was anticipated to drain to a future detention pond "C", and B3 to a future detention pond "B". Both of these ponds are planned to outfall into the MST2. The Grandview Reserve improvements propose two additional private full spectrum detention ponds at locations within subbasin C1 and B3 that outfall into the MST2. These detention ponds will provide water quality and stormwater detention for a portion of these two basins. The required minor (5 year storm) and major (100 year storm) storm release rates from these two ponds has been calculated as a portion of the total release rate from pond "B" and "C" per the MDDP based on the acreage of the site within these basins. The total tributary area to pond "C" in the MDDP is 77.63 acres and the minor and major release rates are 1.5 cfs & 120.2 cfs. Approximately 27% of the tributary area to pond "C" in the MDDP is comprised of phase two improvements that will drain to a separate detention pond on the phase 2 site, and outfall into the MST2. The calculated allowable release rate for the pond "C" portion of the site is 0.4 cfs & 32.5 cfs as a percentage of the total release rate. The total tributary area to pond "B" in the MDDP is 180.79 acres and the minor and major release rates are 2.6 cfs & 165.4 cfs. Approximately 23% of the tributary area to pond "B" in the MDDP is made up of phase two improvements that will drain to a separate detention pond on the phase 2 site. The calculated allowable release rate for the pond "B" portion of the site is 0.6 cfs & 38.0 cfs as a percentage of the total release rate.

The total allowable release rates for both proposed Ponds A & B on the Grandview Reserve Phase 2 Site is the sum of these two release rates. The result is a total allowable minor storm release rate of 1.0 cfs and an allowable major storm release of 70.5 cfs from the phase 2 improvements into the MST2 channel. These rates have been accounted for by the MDDP for release into the MST2.

The proposed release rate in the minor and major storm from the Grandview Reserve Pond A is 0.5 cfs and 11.5 cfs. The proposed release rate in the minor and major storm from the Grandview Reserve Pond B is 0.5 cfs and 18.2 cfs. The total release rate then from the Grandview Reserve Phase 2 site is 1.0 cfs in the minor storm and 19.7 cfs in the major storm. Both release rates in the minor and major storm events are less than or equal to the pre-development rates for the Grandview Reserve Phase 2 project.

#### Pond A (Full Spectrum Detention Basin)

Water quality and detention for Basins A-A through K-A is provided in Pond A; a private, full spectrum extended detention basin within Phase 2 of Grandview Reserve. A total of 31.95 acres at 49% composite imperviousness will be detained. The pond has been sized to provide water quality treatment, and detention for up to the 100-yr storm volume to be released at or below historic rates. The WQCV is 0.542 ac-ft, the EURV is 1.141 ac-ft, and the 100-year detention volume is 1.219 ac-ft. The WQCV, EURV and 100-year



storms are released in 41, 71 and 71 hours, respectively. A forebay is located at the outfall into the pond and a 4.0' trickle channel conveys flow towards the outlet structure. A 15' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 50' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Geick Ranch Tributary #2.

#### Pond B (Full Spectrum Detention Basin)

Water quality and detention for Basins A-B through O-B is provided in Pond B; a private, full spectrum extended detention basin within Phase 2 of Grandview Reserve. A total of 38.19 acres at 43% composite imperviousness will be detained. The pond has been sized to provide water quality treatment, and detention for up to the 100-yr storm volume to be released at or below historic rates. The WQCV is 0.597 ac-ft, the EURV is 1.410 ac-ft, and the 100-year detention volume is 1.410 ac-ft. The WQCV, EURV and 100-year storms are released in 40, 72 and 72 hours, respectively. A forebay is located at the outfall into the pond and a 4.0' trickle channel conveys flow towards the outlet structure. A 15' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 26' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Geick Ranch Tributary #2.

#### c. Channel Improvements

The Gieck Ranch Tributary #2 is proposed to be rerouted. As part of this rerouting of the channel, offsite upstream tributary flows will be captured upstream from the proposed Rex Road extension and be conveyed via culvert to the rerouted channel along the Grandview Reserve Phase 2 western boundary. An analysis has been done for the channel with both existing and future condition flows as described within the Grandview Reserve CLOMR Report, HR Green; September 2021; revised January 2022 (CLOMR). Both scenarios, throughout the channel fall within the channel stability criteria. Channel improvement construction plans have been submitted to El Paso County for review as a separate project (#CDR228).

#### d. Inspection and Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated that all drainage facilities within the public Right-of-Way are to be owned and maintained by El Paso County.

All private detention ponds are to be owned and maintained by the Grandview Reserve Metropolitan District NO. 2 (DISTRICT), once established, unless an agreement is reached stating otherwise. Maintenance access for all full spectrum detention facilities will be provided from public Right-of-Way. Maintenance access for the drainageways will be provided through the proposed tracts.

### V. Wetlands Mitigation

There is one existing wetlands on site associated with the Gieck Ranch Tributary #2. The wetlands are contained within the existing channel and classified as non-jurisdictional. The wetlands USACE determination will be provided with the Grandview Reserve CLOMR Report, HR Green; April 2022, which can be found in **Appendix E**. Wetlands maintenance will be the responsibility of the Grandview Reserve Metropolitan District No. 2.



# VI. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates. Rear and side yard swales are also being utilized in the design to promote infiltration from individual lot impervious areas. The Impervious Reduction Factor (IRF) method will be used in the final design and calculations provided with the FDR.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Onsite full spectrum detention pond provides water quality treatment for the site. The WQCV is released over a period of 40 hours while the EURV is released over a period of 68-72 hours.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

### VII. Drainage and Bridge Fees

Gieck Ranch drainage basin has not been established as a fee basin within El Paso County. Therefore, no drainage basin fees are due at time of platting.

### VIII. Opinion of Probable Cost

An engineer's opinion of probable cost will be provided with the Final Drainage Report (FDR) for the site.

### IX. Hydraulic Grade Line Analysis

Hydraulic grade line analysis and final pipe sizes will be provided with the FDR for the site.

### X. Summary

The Grandview Reserve Phase 2 site lies within the Gieck Ranch Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds. There is one major drainageway that traverses the site: Gieck Ranch Tributary #2. The water quality and detention features ponds will be maintained by the Grandview Reserve Metropolitan District No. 2 (DISTRICT). All drainage facilities were sized per the El Paso County Drainage Criteria Manuals.

The development of this project will not adversely affect adjacent or downstream properties.

### XI. Drawings

Refer to the appendices for vicinity and drainage basin maps.



### XII. References

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
- 3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
- 4. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
- 5. "Grandview Reserve Master Development Drainage Plan" prepared by HR Green, August 2021.
- 6. "Grandview Reserve Filing No. 1 Preliminary Drainage Report" prepared by Galloway & Company, Inc., September 2022.
- 7. "Grandview Reserve CLOMR REPORT" prepared by HR Green, March 2023



Grandview Reserve Phase 2 Preliminary Drainage Report Project No.: 201662.202

### APPENDIX A - VICINITY MAP, PHOTOS, SOIL MAP, FEMA MAP





USDA



### Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	254.0	66.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	127.8	33.5%
Totals for Area of Intere	st		381.8	100.0%

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





#### 104°33'44.61"W 38°58'N

### **FLOOD HAZARD INFORMATION**

#### SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR DRAFT FIRM PANEL LAYOUT



### **NOTES TO USERS**

For information and questions about this Flood Insurance Rate Map (FIRM), available products associated with this FIRM, including historic versions, the current map date for each FIRM panel, how to order products, or the National Flood Insurance Program (NFIP) in general, please call the FEMA Map Information eXchange at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA Flood Map Service Center website at https://msc.fema.gov. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the website.

Communities annexing land on adjacent FIRM panels must obtain a current copy of the adjacent panel as well as the current FIRM Index. These may be ordered directly from the Flood Map Service Center at the number listed above.

For community and countywide map dates, refer to the Flood Insurance Study Report for this jurisdiction.

To determine if flood insurance is available in this community, contact your Insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

Basemap information shown on this FIRM was provided in digital format by the United States Geological Survey (USGS). The basemap shown is the USGS National Map: Orthoimagery. Last refreshed October, 2020.

This map was exported from FEMA's National Flood Hazard Layer (NFHL) on 12/14/2023 3:20 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. For additional information, please see the Flood Hazard Mapping Updates Overview Fact Sheet at https://www.fema.gov/media-library/assets/documents/118418

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date.

### SCALE

Map Projection: GCS, Geodetic Reference System 1980; Vertical Datum: NAVD88

For information about the specific vertical datum for elevation features, datum conversions, or vertical monuments used to create this map, please see the Flood Insurance Study (FIS) Report for your community at https://msc.fema.gov



NATIONAL FLOOD INSURANCE PROGRAM National Flood Insurance Program **FEMA** FLOOD INSURANCE RATE MAP PANEL 552 OF 1275 ---

#### **Panel Contains:**

COMMUNITY EL PASO COUNTY NUMBER 080059

PANEL

0552

### MAP NUMBER 08041C0552G EFFECTIVE DATE December 07, 2018



#### 104°31'52.11"W 38°58'N

### **FLOOD HAZARD INFORMATION**

#### SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR DRAFT FIRM PANEL LAYOUT



### **NOTES TO USERS**

For information and questions about this Flood Insurance Rate Map (FIRM), available products associated with this FIRM, including historic versions, the current map date for each FIRM panel, how to order products, or the National Flood Insurance Program (NFIP) in general, please call the FEMA Map Information eXchange at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA Flood Map Service Center website at https://msc.fema.gov. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the website.

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For community and countywide map dates, refer to the Flood Insurance Study Report for this jurisdiction.

To determine if flood insurance is available in this community, contact your Insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

Basemap information shown on this FIRM was provided in digital format by the United States Geological Survey (USGS). The basemap shown is the USGS National Map: Orthoimagery. Last refreshed October, 2020.

This map was exported from FEMA's National Flood Hazard Layer (NFHL) on 12/14/2023 3:22 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. For additional information, please see the Flood Hazard Mapping Updates Overview Fact Sheet at https://www.fema.gov/media-library/assets/documents/118418

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date.

### SCALE

Map Projection: GCS, Geodetic Reference System 1980; Vertical Datum: No elevation features on this FIRM For information about the specific vertical datum for elevation features, datum conversions, or vertical monuments used to create this map, please see the Flood Insurance Study (FIS) Report for your community at https://msc.fema.gov



NATIONAL FLOOD INSURANCE PROGRAM National Flood Insurance Program **FEMA** FLOOD INSURANCE RATE MAP PANEL 556 OF 1275 and the second

#### **Panel Contains:**

COMMUNITY EL PASO COUNTY NUMBER 080059

PANEL

0556

### MAP NUMBER 08041C0556G **EFFECTIVE DATE** December 07, 2018









NOTES: 1. BASIS OF BEARINGS: THE EAST LINE OF SECTION 21, BEING MONUMENTED AT THE SOUTHEAST CORNER BY A 3-1/4" ALUMINUM SURVEYOR'S CAP STAMPED "PS INC PLS 30087 1996", BEING APPROPRIATELY MARKED, AND BEING MONUMENTED AT THE NORTHEAST CORNER BY A 3-1/4" ALUMINUM SURVEYOR'S CAP STAMPED "PS INC PLS 30087 1996", BEING APPROPRIATELY MARKED, BEING ASSUMED TO BEAR NORTH 00 DEGREES 52 MINUTES 26 SECONDS WEST, A DISTANCE OF 5290.17 FEET.

NAVD88



FLOODPLAIN EXHIBIT



Grandview Reserve Phase 2 Preliminary Drainage Report Project No.: 201662.202

### **APPENDIX B – HYDROLOGIC CALCULATIONS**

Precipitation Frequency Data Server



NOAA Atlas 14, Volume 8, Version 2 Location name: Peyton, Colorado, USA\* Latitude: 38.9877°, Longitude: -104.5596° Elevation: 6971 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### **PF** tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>												
Duration	Average recurrence interval (years)   1 2 5 10 25 50 100 500 500												
Duration	1	2	5	10	25	50	100	200	500	1000			
5-min	<b>0.239</b> (0.189-0.304)	<b>0.291</b> (0.230-0.371)	<b>0.382</b> (0.300-0.487)	<b>0.461</b> (0.360-0.591)	<b>0.576</b> (0.438-0.771)	<b>0.670</b> (0.497-0.906)	<b>0.769</b> (0.552-1.06)	<b>0.874</b> (0.602-1.24)	<b>1.02</b> (0.675-1.48)	<b>1.14</b> (0.731-1.67)			
10-min	<b>0.350</b> (0.276-0.446)	<b>0.427</b> (0.337-0.544)	<b>0.559</b> (0.439-0.714)	<b>0.675</b> (0.528-0.866)	<b>0.844</b> (0.642-1.13)	<b>0.982</b> (0.728-1.33)	<b>1.13</b> (0.808-1.56)	<b>1.28</b> (0.881-1.82)	<b>1.49</b> (0.989-2.17)	<b>1.66</b> (1.07-2.44)			
15-min	<b>0.427</b> (0.337-0.543)	<b>0.520</b> (0.410-0.663)	<b>0.681</b> (0.536-0.870)	<b>0.823</b> (0.643-1.06)	<b>1.03</b> (0.783-1.38)	<b>1.20</b> (0.888-1.62)	<b>1.37</b> (0.985-1.90)	<b>1.56</b> (1.07-2.22)	<b>1.82</b> (1.21-2.65)	<b>2.03</b> (1.30-2.98)			
30-min	<b>0.607</b> (0.480-0.773)	<b>0.740</b> (0.583-0.942)	<b>0.967</b> (0.761-1.24)	<b>1.17</b> (0.912-1.50)	<b>1.46</b> (1.11-1.95)	<b>1.69</b> (1.26-2.29)	<b>1.94</b> (1.39-2.68)	<b>2.20</b> (1.51-3.12)	<b>2.56</b> (1.70-3.73)	<b>2.85</b> (1.83-4.19)			
60-min	<b>0.774</b> (0.611-0.985)	<b>0.932</b> (0.735-1.19)	<b>1.21</b> (0.952-1.55)	<b>1.46</b> (1.14-1.88)	<b>1.84</b> (1.40-2.47)	<b>2.15</b> (1.60-2.92)	<b>2.49</b> (1.79-3.45)	<b>2.85</b> (1.96-4.05)	<b>3.35</b> (2.22-4.90)	<b>3.76</b> (2.42-5.54)			
2-hr	<b>0.941</b> (0.749-1.19)	<b>1.12</b> (0.894-1.42)	<b>1.46</b> (1.15-1.84)	<b>1.76</b> (1.39-2.24)	<b>2.22</b> (1.71-2.97)	<b>2.61</b> (1.96-3.52)	<b>3.03</b> (2.20-4.19)	<b>3.49</b> (2.43-4.94)	<b>4.14</b> (2.78-6.02)	<b>4.68</b> (3.04-6.84)			
3-hr	<b>1.03</b> (0.824-1.29)	<b>1.22</b> (0.973-1.53)	<b>1.57</b> (1.25-1.98)	<b>1.90</b> (1.50-2.40)	<b>2.41</b> (1.88-3.23)	<b>2.86</b> (2.16-3.85)	<b>3.34</b> (2.44-4.60)	<b>3.87</b> (2.72-5.47)	<b>4.64</b> (3.13-6.72)	<b>5.27</b> (3.44-7.67)			
6-hr	<b>1.19</b> (0.961-1.48)	<b>1.40</b> (1.12-1.74)	<b>1.78</b> (1.43-2.23)	<b>2.16</b> (1.72-2.71)	<b>2.76</b> (2.17-3.67)	<b>3.28</b> (2.50-4.40)	<b>3.86</b> (2.85-5.29)	<b>4.50</b> (3.19-6.33)	<b>5.44</b> (3.70-7.84)	<b>6.21</b> (4.10-8.98)			
12-hr	<b>1.38</b> (1.12-1.70)	<b>1.61</b> (1.30-1.98)	<b>2.05</b> (1.66-2.53)	<b>2.47</b> (1.99-3.07)	<b>3.14</b> (2.49-4.15)	<b>3.73</b> (2.87-4.96)	<b>4.38</b> (3.26-5.96)	<b>5.10</b> (3.64-7.12)	<b>6.14</b> (4.23-8.80)	<b>7.01</b> (4.67-10.1)			
24-hr	<b>1.59</b> (1.30-1.95)	<b>1.86</b> (1.52-2.28)	<b>2.37</b> (1.93-2.90)	<b>2.84</b> (2.30-3.50)	<b>3.58</b> (2.86-4.66)	<b>4.22</b> (3.27-5.55)	<b>4.92</b> (3.69-6.62)	<b>5.68</b> (4.09-7.86)	<b>6.79</b> (4.71-9.65)	<b>7.70</b> (5.17-11.0)			
2-day	<b>1.85</b> (1.53-2.24)	<b>2.17</b> (1.79-2.63)	<b>2.75</b> (2.26-3.34)	<b>3.28</b> (2.68-4.00)	<b>4.09</b> (3.28-5.26)	<b>4.78</b> (3.73-6.21)	<b>5.52</b> (4.17-7.36)	<b>6.33</b> (4.59-8.67)	<b>7.48</b> (5.23-10.5)	<b>8.42</b> (5.71-12.0)			
3-day	<b>2.02</b> (1.68-2.44)	<b>2.38</b> (1.97-2.86)	<b>3.01</b> (2.48-3.64)	<b>3.58</b> (2.94-4.35)	<b>4.45</b> (3.58-5.68)	<b>5.18</b> (4.06-6.69)	<b>5.97</b> (4.52-7.90)	<b>6.81</b> (4.97-9.28)	<b>8.02</b> (5.63-11.2)	<b>8.99</b> (6.13-12.7)			
4-day	<b>2.17</b> (1.81-2.61)	<b>2.55</b> (2.12-3.06)	<b>3.21</b> (2.66-3.86)	<b>3.81</b> (3.14-4.61)	<b>4.72</b> (3.80-6.00)	<b>5.48</b> (4.31-7.04)	<b>6.29</b> (4.79-8.30)	<b>7.17</b> (5.24-9.73)	<b>8.42</b> (5.93-11.8)	<b>9.42</b> (6.45-13.3)			
7-day	<b>2.57</b> (2.16-3.06)	<b>2.97</b> (2.48-3.54)	<b>3.67</b> (3.06-4.39)	<b>4.31</b> (3.58-5.17)	<b>5.27</b> (4.28-6.64)	<b>6.08</b> (4.81-7.76)	<b>6.94</b> (5.32-9.09)	<b>7.87</b> (5.80-10.6)	<b>9.20</b> (6.53-12.8)	<b>10.3</b> (7.08-14.4)			
10-day	<b>2.92</b> (2.46-3.46)	<b>3.35</b> (2.82-3.98)	<b>4.11</b> (3.44-4.89)	<b>4.79</b> (3.99-5.73)	<b>5.81</b> (4.73-7.28)	<b>6.66</b> (5.29-8.45)	<b>7.56</b> (5.82-9.85)	<b>8.53</b> (6.32-11.4)	<b>9.90</b> (7.06-13.7)	<b>11.0</b> (7.63-15.4)			
20-day	<b>3.90</b> (3.31-4.57)	<b>4.50</b> (3.81-5.28)	<b>5.51</b> (4.65-6.49)	<b>6.37</b> (5.36-7.55)	<b>7.61</b> (6.22-9.37)	<b>8.60</b> (6.87-10.8)	<b>9.62</b> (7.44-12.4)	<b>10.7</b> (7.95-14.1)	<b>12.1</b> (8.71-16.6)	<b>13.3</b> (9.28-18.4)			
30-day	<b>4.68</b> (3.99-5.46)	<b>5.42</b> (4.61-6.33)	<b>6.63</b> (5.63-7.76)	<b>7.64</b> (6.45-8.99)	<b>9.03</b> (7.39-11.0)	<b>10.1</b> (8.11-12.5)	<b>11.2</b> (8.70-14.3)	<b>12.3</b> (9.20-16.2)	<b>13.8</b> (9.95-18.7)	<b>14.9</b> (10.5-20.6)			
45-day	<b>5.64</b> (4.84-6.55)	<b>6.52</b> (5.58-7.58)	<b>7.94</b> (6.77-9.25)	<b>9.09</b> (7.71-10.6)	<b>10.6</b> (8.73-12.8)	<b>11.8</b> (9.49-14.5)	<b>13.0</b> (10.1-16.4)	<b>14.1</b> (10.6-18.4)	<b>15.6</b> (11.3-21.0)	<b>16.7</b> (11.8-22.9)			
60-day	<b>6.45</b> (5.55-7.46)	<b>7.42</b> (6.37-8.59)	<b>8.96</b> (7.68-10.4)	<b>10.2</b> (8.69-11.9)	<b>11.8</b> (9.74-14.2)	<b>13.1</b> (10.5-16.0)	<b>14.2</b> (11.1-17.9)	<b>15.4</b> (11.6-20.0)	<b>16.8</b> (12.2-22.6)	<b>17.9</b> (12.7-24.6)			

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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#### **PF** graphical







Duration												
5-min	2-day											
- 10-min	- 3-day											
— 15-min	- 4-day											
30-min	- 7-day											
- 60-min	— 10-day											
- 2-hr	— 20-day											
— 3-hr	— 30-day											
— 6-hr	— 45-day											
- 12-hr	- 60-day											
24-hr												

NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Tue Sep 5 16:10:04 2023

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Maps & aerials

Small scale terrain







Large scale aerial

Precipitation Frequency Data Server



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

**Disclaimer** 



<u>Calc'd by:</u>	cvw
Checked by:	КН

Date: 7/14/2024

SOIL TYPE:	HSG	A&B																				
			•						CON	ИРОЗ	SITE	'C' F	ACT	ORS	;							
								L	AND U	SE TY	(PE											
		Paved			Gra	vel		Lawns	;	Туріо	cal Tow Lots	nhome	Mine	or Arte Tyj	rial ROW 5.	Loc	al ROW	Тур.		С	OMPOSI	LE LOO O O
	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	С	5 <b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%	C,	<b>C</b> <sub>100</sub>	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>		IMPER	VIOUSNE	:55 & C
	100	0.90	0.96	80	0.5	9 0.70	0	0.08	0.35	53	0.48	0.64	68	0.6	3 0.76	90	0.82	0.90	TOTAL		FACTOR	1
BASIN		ACRES	;		ACR	ES		ACRES	;		ACRES	5		ACR	ES		ACRES	;	ACRES	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>
A1-A					0.1	4		2.42			0.66								3.22	14	0.18	0.42
A2-A								0.10			1.13								1.23	49	0.45	0.62
B1-A								0.03									0.23		0.26	79	0.73	0.83
B2-A								0.06			0.56						0.40		1.02	64	0.59	0.72
B3-A		0.09						0.04			0.39						0.37		0.89	71	0.65	0.77
B4-A								0.55			2.02						1.10		3.67	56	0.52	0.67
C1-A								0.00			0.44						0.19		0.63	64	0.58	0.72
D1-A								0.11			0.59								0.70	45	0.42	0.59
E1-A								0.03			0.55						0.15		0.73	59	0.54	0.68
E2-A								0.26			1.28						1.02		2.56	63	0.58	0.72
E3-A											0.68						0.29		0.97	64	0.58	0.72
E4-A											0.71						0.31		1.02	64	0.58	0.72
F1-A								0.00			0.32						0.14		0.46	64	0.58	0.72
H1-A								0.90			0.90						0.45		2.25	39	0.39	0.58
H2-A								0.19			1.26						0.49		1.94	57	0.53	0.68
H3-A											1.96						0.84		2.80	64	0.58	0.72
H4-A								0.97			1.35			1.5	5				3.87	46	0.44	0.62
J1-A								0.75			0.75								1.50	27	0.28	0.50
K1-A								0.00						1.7	5				1.75	68	0.63	0.76
EA6		0.70																	0.70	100	0.90	0.96
EA7		0.58						0.07											0.65	89	0.81	0.89
POND A		1.37			0.1	4		6.48			15.56			3.3	0		5.97		32.82	53	0.50	0.66

### **GRANDVIEW RESERVE (PHASE II-TOWNHOMES)** Calc'd by:

CVW



### PROPOSED CONDITIONS

Checked by:

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EL PASO COUNTY, CO

Date:

7/	14/	20	24
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KH

				TIME O	F CONCE	INTRATI	ON						
BAS	IN DATA		OVER	LAND TIM	E (T <sub>i</sub> )		TRAV	EL TIME (	(T <sub>t</sub> )		TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>V</sub>	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)	tc max	tc design (min)
A1-A	0.18	3.22	100	2.8	11.9	7	529	2.9	1.2	7.3	19.2	13.5	13.5
A2-A	0.45	1.23	68	4.9	5.8	15	630	2.2	2.2	4.8	10.5	13.9	10.5
B1-A	0.73	0.26	41	0.5	5.4	20	340	0.6	1.5	3.7	9.1	12.1	9.1
B2-A	0.59	1.02	32	0.7	6.1	20	614	2.9	3.4	3.0	9.2	13.6	9.2
B3-A	0.65	0.89	42	2.9	3.8	20	544	2.9	3.4	2.7	6.5	13.3	6.5
B4-A	0.52	3.67	43	4.8	4.1	20	970	2.7	3.3	4.9	9.0	15.6	9.0
C1-A	0.58	0.63	53	2.9	4.8	20	318	0.6	1.5	3.4	8.3	12.1	8.3
D1-A	0.42	0.70	100	4.6	7.5	15	196	2.3	2.3	1.4	9.0	11.6	9.0
E1-A	0.54	0.73	41	1.0	6.6	20	186	1.0	2.0	1.5	8.2	11.3	8.2
E2-A	0.58	2.56	38	2.0	4.7	20	970	2.8	3.3	4.9	9.6	15.6	9.6
E3-A	0.58	0.97	68	2.0	6.2	20	627	2.6	3.2	3.2	9.4	13.9	9.4
E4-A	0.58	1.02	66	2.0	6.1	20	627	2.4	3.1	3.4	9.5	13.9	9.5
F1-A	0.58	0.46	63	2.0	6.0	20	230	1.0	2.0	1.9	7.9	11.6	7.9
H1-A	0.39	2.25	79	2.0	9.2	20	284	0.6	1.5	3.0	12.2	12.0	12.0
H2-A	0.53	1.94	41	0.8	7.3	20	667	2.0	2.8	3.9	11.2	13.9	11.2
H3-A	0.58	2.80	41	2.8	4.3	20	1246	2.5	3.2	6.6	10.9	17.1	10.9
H4-A	0.44	3.87	62	2.5	7.0	20	1246	3.0	3.5	6.0	13.0	17.3	13.0
J1-A	0.28	1.50	100	4.5	9.1	15	550	2.4	2.3	3.9	13.0	13.6	13.0
K1-A	0.63	1.75	45	3.4	3.8	20	1409	2.4	3.1	7.6	11.4	18.1	11.4
EA6	0.90	0.70	26	2.0	1.5	20	630	1.7	2.6	4.0	5.5	13.6	5.5
EA7	0.81	0.65	24	2.0	2.1	20	630	1.7	2.6	4.0	6.1	13.6	6.1

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C<sub>v</sub>

Type of Land Surface	<i>C</i> <sub>v</sub>
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select Cv value based on type of vegetative cover



#### GRANDVIEW RESERVE (PHASE II-TOWNHOMES) PROPOSED CONDITIONS DESIGN STORM: 5-YEAR

<u>Calc'd by:</u> <u>Checked by:</u> <u>Date:</u> CVW KH 7/14/2024

				DI	RECT	RUNO	FF		т	DTAL	RUN	DFF	S	TREE	т		PI	PE		٦	RAV	EL .	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C <sub>5</sub>	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)		VEL. (FPS)	TRAVEL TIME (mir	
	35.1	EA6	0.70	0.90	5.5	0.63	5.02	2 3.2	5.5	0.63	5.02	3.2	3.2	0.63	2.4					145	54 1	.5	15.64	OFFSITE FLOWS FLOW TO DP 1-A
	35.2	EA7	0.65	0.81	6.1	0.53	4.88	3 2.6	6.1	0.53	4.88	2.6	2.6	0.53	2.4					144	13 1	.5	15.52	OFFSITE FLOWS FLOW TO DP 2-A
	1-A	K1-A	1.75	0.63	11.4	1.10	3.93	3 4.3	21.2	1.73	3.01	5.2				5.2	1.73	3 0.5	5 1.	5 85	5 2	.1	0.67	BASIN K1-A STORMWATER CAPTURED IN TYPE R INLET AT DP 1-A
	2-A	H4-A	3.87	0.44	13.0	1.70	3.74	6.4	21.6 4	2.23	2.97	6.6				6.6	2.23	3 0.5	5 1.	56	2	.1	0.04	BASIN H4-A STORMWATER CAPTURED IN TYPE R INLET AT DP 2-A
	2.1-A								21.8	3.96	2.96	11.7				11.7	3.96	6 0.5	5 2.	0 36	0 2	.9	2.04	DP 2.1A PIPED TO DP4.1A
	3-A	H3-A	2.80	0.58	10.9	1.63	4.01	6.5	10.9 5	1.63	4.01	6.5				F	PIPE TI	RAVE			IGNI	FICA	NT	BASIN H3-A STORMWATER CONVEYED VIA CURB AND GUTTER AT DP 3-A, FLOW TO DP 5.1-A
	3.1-A								10.9	1.63	4.01	6.5												DP 3.1A PIPED TO DP 5.1A
	4-A	J1-A	1.50	0.28	13.0	0.42	3.73	3 1.6	13.0	0.42	3.73	1.6				P		RAVE			IGNI		NT	BASIN J1-A STORMWATER CAPTURED IN OPEN GRATE INLET AT DP 4-A
	4.1-A								23.9	4.38	2.82	12.4				12.4	4.38	3 0.5	5 2.	0 63	3 2	.9	0.36	DP 4.1-A PIPED TO DP 5.1-A
	5-A		2.25	0.30	12.0	0.97	3.95	. 3/	12.0	0.87	3.85	3.4				F	PIPE TI	RAVE			IGNI	FICA	NT	BASIN H1-A CONVEYED VIA CURB AND GUTTER AT DP 5-A, CAPTURED IN
	5.1-A	111-75	2.25	0.00	12.0	0.07	0.00	, 3	12.0	0.87	3.85	3.4												
	6-A	H2-A	1.94	0.53	11.2	1.02	3.95	5 4.0	11.2	1.02	3.95	4.0				P	IPE TI	RAVE	L TIM	EINS	IGNI	FICA	NT	BASIN H2-A CAPTURED IN TYPE R SUMP INLET AT DP 6-A, FLOW TO DP 5.1A
	6.1-A		DP 4.1-4	TC + T	RAVEL	TIME U	JSED	1	24.2	7.90	2.80	22.1				22.1	7.90	0.5	5 3.	0 32	0 4	.7	1.13	
	7-A	F1-A	0.46	0.58	7.9	0.27	4.48	3 1.2	7.9	0.27	4.48	1.2				P	IPE TI	RAVE	L TIM	EINS	IGNI	FICA	NT	BASIN F1-A CAPTURED IN TYPE R SUMP INLET AT DP 7-A
	7.1-A								7.9	0.27	4.48	1.2												DP 7.1-A PIPED TO 9.1A
	8-A	E1-A	0.73	0.54	8.2	0.39	4.43	8 1.7	8.2 7	0.39	4.43	1.7												BASIN E1-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 9-A
	9-A	B4-A E2-A	3.67 2.56	0.52 0.58	9.0 9.6	1.92 1.47	4.28 4.20	8 8.2 0 6.2	2 9.6 2	3.39	4.20	14.2				P	PIPE TI	RAVE	L TIM	EINS	IGNI	FICA	NT	BASIN E2-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 9-A
	9.1-A		DP 6.1-4	A TC + T	RAVEL		JSED		25.4	11.95	2.73	32.7				32.7	11.95	5 0.5	5 3.	0 15	0 4	.7	0.53	DP 9.1A PIPED TO DP 13.1-A
	10-A	A2-A	1.23	0.45	10.5	0.55	4.05	5 2.2	10.5 2	0.55	4.05	2.2				10.5	0.55	5 0.5	5 1.	0 75	5 1	.3	0.95	BASIN E6-A STORMWATER CONVEYED VIA CURB AND GUTTER AT DP 10-A, FLOW TO DP5-A
	10.1A								11.5	0.55	3.92	2.2												DP 10.1A PIPED TO DP 12.1-A
	11-A	E4-A	1.02	0.58	9.5	0.59	4.21	2.5	9.5 5	0.59	4.21	2.5												BASIN E4-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 12-A, FLOW TO DP 14-A
	12-A	E3-A	0.97	0.58	9.4	0.56	4.22	2 2.4	9.4 4	0.56	4.22	2.4												BASIN E3-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 12-A, FLOW TO DP 13-A
	12.1-A			DP 10.1	-A TC U	ISED			11.5	1.71	3.92	6.7				6.7	1.71	1 0.5	5 2.	0 70	0 2	.9		DP 12.1A PIPED TO DP 14.1-A
	13-A	D1-A	0.70	0.42	9.0	0.29	4.29	1.3	9.0	0.29	4.29	1.3				P	PIPE TI	RAVE		EINS	IGNI	FICA	NT	BASIN D1-A STORMWATER CAPTURED IN OPEN GRATE MANHOLE AT DP 13-A, FLOW TO DP 13.1-A
	13.1-A								25.9	12.24	2.70	33.1				33.1	12.24	4 0.5	5 3.	5 14	0 5	.6	0.41	DP 13.1A PIPED TO DP 14.1-A
	14-A	B1-A B2-A B3-A	0.26 1.02 0.89	0.73 0.59 0.65	9.1 9.2 6.5	0.19 0.60 0.58	4.27 4.26 4.79	0.8 2.6 2.8	8 9.2 6 8	1.37	4.26	5.8				P	PIPE TI	RAVE		EINS	IGNI		NT	BASIN B1-A, B2-A, B3-A, & BASIN B4-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 14-A, FLOW TO DP 16.1-A



#### GRANDVIEW RESERVE (PHASE II-TOWNHOMES) PROPOSED CONDITIONS DESIGN STORM: 5-YEAR

<u>Calc'd by:</u> <u>Checked by:</u> <u>Date:</u> CVW KH 7/14/2024

																				_				
				DI	RECT	RUNO	FF		Т	OTAL	RUN	OFF	S	TREE	т		PI	PE		т	RAV	EL 1	ГІМЕ	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C <sub>5</sub>	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)			TRAVEL TIME (mir	
	14.1-A								26.3	13.95	2.68	37.4				26.3	13.95	0.5	5 3.	5 101	5	.6	0.30	DP 14.1A PIPED TO DP 16.1-A
	14.2-A								9.2	1.37	4.26	5.8				F	IPE T	RAVE	L TIM	E INS	GNIF	ICAI	NT	
																			1					DP 14.2A PIPED TO DP 16.1-A
	15-A	C1-A	0.63	0.58	8.3	0.37	7 4.42	2 1.0	8.3 6	0.37	4.42	1.6				1.6	0.37	0.5	5 1.	5 29	2	.1	0.23	BASIN C1-A STORMWATER CAPTURED IN TYPE R SUMP INILET AT DP 15-A
	15.1-A								8.3	0.37	4.42	1.6				F	PIPE T	RAVE	L TIM	E INS	GNIF	ICAI	NT	
																								DP 15.1A PIPED TO DP 16.1-A
	16.1-A	A1-A	3.22	0.18	13.5	0.59	3.68	3 2.1	26.3 2	16.28	3 2.68	43.6												TOTAL FLOW INTO POND A

1					G	RAN	IDVI	EW F	RESE	RVE	(PH	ASE	II-T	'OW	/NH	ОМ	ES)				Cal	c'd by:	CVW
	+ -	à						F	PROP	OSED	CON	DITI	DNS	_							Che	cked by	KH
								DE	SIGN	STO	RM:	100-1	(EAI	R							<u>C</u>	Date:	7/14/2024
HR	Gree	n																					
				DI	RECT	RUNO	FF		т	OTAL P	RUNO	FF	S	TREE	T		PI	PE		T	RAVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C100	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	35.1	EA6	0.70	0.96	5.5	0.67	7 8.43	5.7	5.5	0.67	8.43	5.7	5.7	0.67	2.4					1454	1.5	15.64	OFFSITE FLOWS FLOW TO DP 1-A
	35.2	EA7	0.65	0.89	6.1	0.58	8 8.19	4.8	6.1	0.58	8.19	4.8	4.8	0.58	2.4					1443	3 1.5	15.52	OFFSITE FLOWS FLOW TO DP 2-A
	1-A	K1-A	1.75	0.76	5 11.4	1.33	3 6.60	8.8	21.2	2.00	5.04	10.1				10.1	2.00	0.5	i 1.	5 85	2.1	0.67	BASIN K1-A STORMWATER CAPTURED IN TYPE R INLET AT DP 1-A
	2-A	H4-A	3.87	0.62	13.0	2.38	6.27	14.9	21.6	2.96	4.99	14.8				14.8	2.96	0.5	5 1.	56	2.1	0.04	BASIN H4-A STORMWATER CAPTURED IN TYPE R INLET AT DP 2-A
	2.1-A								21.8	4.97	4.97	24.7				24.7	4.97	0.5	5 2.0	0 360	2.9	2.04	DP 2.1A PIPED TO DP4.1A
	3-A	H3-A	2.80	0.72	10.9	2.0'	1 6.73	13.5	10.9	2.01	6.73	13.5				F	PIPE TR	RAVEI	і тімі І		GNIFIC	ANT	BASIN H3-A STORMWATER CONVEYED VIA CURB AND GUTTER AT DP 3-A. FLOW TO DP 5.1-A
	3.1-A								10.9	2.01	6.73	13.5											DP 3.1A PIPED TO DP 5.1A
	4-A	J1-A	1.50	0.50	13.0	0.74	4 6.26	4.7	13.0	0.74	6.26	4.7				F	PIPE TR	RAVEI	L ТІМІ		GNIFIC	ANT	BASIN J1-A STORMWATER CAPTURED IN OPEN GRATE INLET AT DP 4-A
	4.1-A								23.9	5.71	4.74	27.1				27.1	5.71	0.5	2.0	0 63	2.9	0.36	DP 4.1-A PIPED TO DP 5.1-A
	5-A	H1-A	2.25	0.58	12.0	1.30	6.47	8.4	12.0	1.30	6.47	8.4				F	PIPE TR	RAVEI	L ТІМІ		GNIFIC	ANT	BASIN H1-A CONVEYED VIA CURB AND GUTTER AT DP 5-A, CAPTURED IN TYPE R SUMP INLET AT DP 5-A, FLOW TO DP 5.1-A
	5.1-A								12.0	1.30	6.47	8.4											DP 5.1A PIPED TO DP 6.1A
	6-A	H2-A	1.94	0.68	11.2	1.3	1 6.64	8.7	, 11.2	1.31	6.64	8.7				F	PIPE TR	AVE	L ТІМІ		GNIFIC	ANT	BASIN H2-A CAPTURED IN TYPE R SUMP INLET AT DP 6-A, FLOW TO DP 5.1A
	6.1-A		DP 4.1-4	A TC + 1	RAVEL	TIME	USED	1	24.2	10.33	4.70	48.6				48.6	10.33	0.5	3.0	0 320	4.7	1.13	DP 6.1-A PIPED TO 9.1A
	7-A	Ε1-Δ	0.46	0.72	70	0.3	3 7 53	25	7.9	0.33	7.53	2.5				F	PIPE TF	RAVEI	L TIMI		GNIFIC	ANT	BASIN E1-A CADTURED IN TYPE R SUMP INI ET AT DR 7-A
	7.1-A		0.40	0.72	. 1.5	0.0	5 1.55	2.0	7.9	0.33	7.53	2.5											DP 7 1-A PIPED TO 9 1A
	8-A	F1-A	0.73	0.68	82	0.50	7 44	37	8.2	0.50	7.44	3.7											BASIN E1-A STORMWATER CAPTURED IN TYPE R SUMP IN ET AT DP 9-A
	9-A	B4-A E2-A	3.67	0.67	9.0	2.48	8 7.18 3 7.05	17.8	9.6	4.31	7.05	30.3				F	PIPE TR	RAVE	L ТІМІ		GNIFIC	ANT	BASIN E2-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 9-A
	9.1-A		DP 6.1-4	A TC + 1	RAVEL	TIME	USED		25.4	15.46	4.59	70.9				70.9	15.46	0.5	i 3.	0 150	4.7	0.53	DP 9.1A PIPED TO DP 13.1-A
	10-A	A2-A	1.23	0.62	2 10.5	0.76	6 6.80	5.2	10.5	0.76	6.80	5.2				5.2	0.76	0.5	i 1.	0 75	1.3	0.95	BASIN E6-A STORMWATER CONVEYED VIA CURB AND GUTTER AT DP 10-A, FLOW TO DP5-A
	10.1-A								11.5	0.76	6.58	5.0											DP 10.1A PIPED TO DP 12.1-A
	11-A	E4-A	1.02	0.72	9.5	0.73	3 7.06	5.2	9.5	0.73	7.06	5.2											BASIN E4-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 12-A, FLOW TO DP 14-A
	12-A	E3-A	0.97	0.72	9.4	0.70	0 7.08	4.9	9.4	0.70	7.08	4.9											BASIN E3-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 12-A, FLOW TO DP 13-A
	12.1-A			DP 10.1	-A TC U	SED			11.5	2.19	6.58	14.4				14.4	2.19	0.5	2.0	0 700	2.9	3.97	DP 12.1A PIPED TO DP 14.1-A
	13-A	D1-A	0.70	0.59	9.0	0.42	2 7.21	3.0	9.0	0.42	7.21	3.0				F	PIPE TR	RAVE			GNIFIC		BASIN D1-A STORMWATER CAPTURED IN OPEN GRATE MANHOLE AT DP 13-A, FLOW TO DP 13.1-A
	13.1-A								25.9	15.88	4.54	72.0				72.0	15.88	0.5	3.	5 140	5.6	0.41	DP 13.1A PIPED TO DP 14.1-A
	14-A	B1-A B2-A B3-A	0.26 1.02 0.89	0.83 0.72 0.77	9.1 9.2 6.5	0.22 0.74 0.68	2 7.17 4 7.15 8 8.04	1.6 5.3 5.5	9.2	1.64	7.15	11.7				F	PIPE TR	RAVEI			GNIFIC		BASIN B1-A, B2-A, B3-A, & BASIN B4-A STORMWATER CAPTURED IN TYPE R SUMP INLET AT DP 14-A, FLOW TO DP 16.1-A

					G	RAN	DVI	EW F	RESE	RVE	(PH	ASE	11-1	wo	NHC	ОМЕ	ES)				Cal	ic'd by:	CVW
								F	PROPO	DSED	CON	DITI	ONS	i							Che	cked by:	КН
		1						DE	SIGN	STO	RM:	100-`	YEA	R								Date:	7/14/2024
HR	Gree	n																					
				DI	RECT	RUNO	FF		тс	TAL R	NON	FF	S	TREE	г		PI	PE		TR	AVEL		REMARKS
STREET	DESIGN POINT 14.1-A	BASIN ID	AREA (ac)	C100	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	<b>t</b> e <b>(min)</b>	C100*A (ac)	<b>/ (in./ hr.)</b>	<b>o (cłs)</b> 81.2	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	<b>G</b> PIPE (cfs) 81.2	C <sup>100</sup> *A (ac)	0.5	DIPE SIZE (ft)	101	5.6	0.30	
																							DP 14.1A PIPED TO DP 16.1-A
	14.2-A								9.2	1.64	7.15	11.7				PI	IPE TR		TIME	INSIG	NIFIC		DP 14.2A PIPED TO DP 16.1-A
	15-A	C1-A	0.63	0.72	8.3	0.45	7.42	2 3.4	8.3	0.45	7.42	3.4	ŀ			3.4	0.45	0.5	1.5	29	2.1	0.23	BASIN C1-A STORMWATER CAPTURED IN TYPE R SUMP INILET AT DP 15-A
	15.1-A								8.3	0.45	7.42	3.4				PI	IPE TF	RAVEL	TIME	INSIG	NIFIC	ANT	
L	10.1.1									00.45			-									_	DP 15.1A PIPED TO DP 16.1-A
	16.1-A	A1-A	3.22	0.42	13.5	1.37	6.18	8 8.5	26.3	20.15	4.50	90.6	'										TOTAL FLOW INTO POND A

	GRANDVIEW RESERVE (PHASE II- DUPLEXES)	<u>Calc'd by:</u>	CVW
	PROPOSED CONDITIONS	Checked by:	КН
HRGreen	EL PASO COUNTY, CO	Date:	7/14/2024

	1100	AGB																	
							С	OMP	OSITI	E 'C'	FAC	TOR	S						
							LAN	) USE	TYPE										
	EP	PC LOC	AL		Duplex			Lawns	i	EI	PC MIN	OR Al	т	ownhor	ne		С	OMPOSI	re
	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>		IMPER	VIOUSNE	SS & C
	90	0.82	0.90	47	0.40	0.58	0	0.08	0.35	68	0.63	0.76	53	0.48	0.64	TOTAL		FACTOR	
BASIN		ACRES	;		ACRES	;		ACRES	;		ACRES	;		ACRES	;	ACRES	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>
A-B		0.66			3.94			1.31			0.00			0.66		6.56	43	0.39	0.57
B-B		0.00			1.78			1.78			0.00			0.00		3.55	24	0.24	0.47
C-B		0.38			1.07			0.08			0.00			0.08		1.53	58	0.51	0.68
D-B		0.41			0.21			0.41			0.00			0.00		1.03	45	0.44	0.62
E-B		0.00			0.26			0.77			0.00			0.00		1.03	12	0.16	0.41
F-B		0.00			0.73			0.73			0.00			0.00		1.45	24	0.24	0.47
G-B		0.00			0.00			0.38			1.77			0.00		2.15	56	0.53	0.69
H-B		0.00			1.65			1.24			1.24			0.00		4.12	39	0.37	0.57
I-B		0.15			0.61			0.00			0.00			0.00		0.76	56	0.48	0.64
J-B		1.70			5.11			0.00			0.00			0.00		6.81	58	0.51	0.66
K-B		0.22			0.90			0.00			0.00			0.00		1.12	56	0.48	0.64
L-B		0.19			0.38			1.32			0.00			0.00		1.89	18	0.22	0.45
M-B		0.29			1.17			0.00			0.00			0.00		1.46	56	0.48	0.64
N-B		0.00			0.75			2.25			0.00			0.00		3.00	12	0.16	0.41
O-B		0.00			0.00			1.59			0.00			0.00		1.18	0	0.11	0.47
Pond B		4.01			18.53			11.85			3.00			0.74		38.13	39		

	GRAN	IDVIEW	RESER	VE (PH	ASE II-	DUPLE	XES)	Calc'd b	y:	c	W		
	PROP	OSED (	CONDITI	ONS				Checked	by:	[	КН		
HRGreen	EL PAS		гү, со					Date:		7/14	4/2024		
				TIME OF		NTRATI	ON			1			
BAS	IN DATA		OVER		E (T <sub>i</sub> )		TRAV	EL TIME (	<b>T</b> <sub>t</sub> )		TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>V</sub>	LENGTH (ft)	SLOPE %	$\Sigma Q_5$ (cfs)	t <sub>t</sub> (min)	t <sub>c</sub> (min)	tc max	tc design (min)
A-B	0.39	6.56	100	2.0	10.4	20	1250	2.6	3.2	6.5	16.9	17.5	16.9
B-B	0.24	3.55	100	2.0	12.5	20	1030	2.6	3.2	5.3	17.8	16.3	16.3
C-B	0.51	1.53	100	2.0	8.5	20	930	2.6	3.2	4.8	13.3	15.7	13.3
D-B	0.44	1.03	100	2.0	9.6	20	540	2.6	3.2	2.8	12.4	13.6	12.4
E-B	0.16	1.03	100	2.0	13.7	15	225	2.9	2.6	1.5	15.1	11.8	11.8
F-B	0.24	1.45	100	2.0	12.5	20	430	2.0	2.8	2.5	15.0	12.9	12.9
G-B	0.53	2.15	30	2.0	4.5	20	1250	1.0	2.0	10.4	14.9	17.1	14.9
H-B	0.37	4.12	100	2.0	10.6	20	1250	1.0	2.0	10.4	21.0	17.5	17.5
I-B	0.48	0.76	100	2.0	9.0	20	385	2.3	3.0	2.1	11.1	12.7	11.1
J-B	0.51	6.81	100	2.0	8.7	20	1250	2.3	3.0	6.9	15.5	17.5	15.5
K-B	0.48	1.12	100	2.0	9.0	20	570	3.0	3.5	2.7	11.7	13.7	11.7
L-B	0.22	1.89	100	2.0	12.8	20	520	2.0	2.8	3.1	15.9	13.4	13.4
M-B	0.48	1.46	100	2.0	9.0	20	690	2.3	3.0	3.8	12.8	14.4	12.8
N-B	0.16	3.00	100	2.0	13.7	15	990	0.8	1.3	12.3	26.0	16.1	16.1
O-B	0.11	1.18	25	2.0	7.2	20	50	1.0	2.0	0.4	7.6	10.4	7.6
						n							

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

#### Table 6-7. Conveyance Coefficient, $C_{\nu}$

Type of Land Surface	$C_{\nu}$																							
Heavy meadow	2.5																							
Tillage/field	5																							
Riprap (not buried)*	6.5																							
Short pasture and lawns	7																							
Nearly bare ground	10																							
Grassed waterway	15																							
Paved areas and shallow paved swales	20																							
For buried riprap, select C <sub>v</sub> value based on type of v	vegetative cover																							
GRANDVIEW R		ESE	SERVE (PHASE II- DUPLEXES) Calc'd I											Ca	lc'd b	by: CVW								
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	$\neg$	, A						PRO	POS	6ED	CON	IDIT	ION	S							Che	cked	by:	КН
1 1		1						DE	SIGN	STO	RM:	5-YI	EAR								<u>[</u>	Date:		7/14/2024
HR	Gree	n																						
				DII	RECT	RUNO	FF			$\Sigma Q_5$	(cfs)		ST	REET		I	PIPE			TR	AVE	L TIM	E	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C <sub>5</sub>	t <sub>e</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac) SLOPE %	Q <sub>PIPE</sub> (cfs)		C <sub>5</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min		
	DP1-B	K-B	1.12	0.48	11.7	0.54	3.89	2.1	11.7	0.54	3.89	2.1		P					SIGN		NT	1		BASIN K-B CAPTURED IN TYPE R AT GRADE INLET
	DP2-B	D-B	1.03	0 44	12.4	0.45	3.81	17	12.4	0 45	3.81	1.7		P	IPE TR	AVE		AE INS	SIGN	IIFICA	NT	1		BASIN D-B CAPTURED IN TYPE R AT GRADE INLET
	DP3-B	00	1.00	DP1-B		Р2-В	0.01	1.7	12.4	1.00	3.81	3.8			12	.4 1	1.00	0.5	2.0	78	5.1	0.2	26	COMBINES DP1-B & DP2-B
	DP4-B	A-B	6 56	0.39	16.9	2 53	3 35	85	16.9	2 53	3 35	8 5		P		AVE		AE INS	SIGN	IIFICA	NT	1		BASIN A-B CAPTURED IN TYPE R AT GRADE INI ET
		C-B	1.53	0.51	13.3	0.79	3.70	2.9	10.0	2.00	0.00	0.0		Р		AVE			SIGN	IFICA	NT	1		
	DP5-B	F-R	1.45	0.24	12.9	0.35	3.74	1.3	13.3	1.14	3.70	4.2												BASIN C-B & BASIN F-B CAPTURED IN TYPE R AT GRADE INLET
	DP6-B			DP4-B	AND DF	Р5-В	-		16.9	3.67	3.35	12.3			12	.3 3	3.67	0.5	2.0	45	5.1	0.1	15	COMBINES DP4-B & DP5-B
	DP7-B		T	DP6-B	AND DF	3-B		1	17.0	4.66	3.33	15.5		P	15	.5 4	4.66		2.0	406	5.1	1.3	33	COMBINES DP3-B & DP6-B
	DP8-B	G-B	2.15	0.53	14.9	1.14	3.53	4.0	14.9	1.14	3.53	4.0			Ī							1		BASIN G-B CAPTURED IN TYPE R SUMP INLET
	DP9-B	Н-В	4.12	0.37	17.5	1.54	3.29	5.1	17.5	1.54	3.29	5.1	Ì	P					SIGN	IIFICA	NT	Ì		BASIN H-B CAPTURED IN TYPE R SUMP INLET
	DP10-B		I	DP8-B		Р9-В			17.5	2.68	3.29	8.8			8	.8 2	2.68	0.5	2.0	650	5.1	2.1	13	COMBINES DP8-B & DP9-B
			0.55							0.05	0.10			Р		AVE		AE INS	SIGN	IFICA	NT	1		
	DP11-B	B-B	3.55	0.24	16.3	0.85	3.40	2.9	16.3	0.85	3.40	2.9		P	IPE TR	AVE		IE INS	SIGN	IIFICA	NT			BASIN B-B CAPTURED IN OPEN GRATE SUMPTINLET
	DP12-B	I-B	0.76	0.48	11.1	0.37	3.98	1.5	11.1	0.37	3.98	1.5												BASIN I-B CAPTURED IN TYPE R AT GRADE INLET
	DP13-B	L-В J-В	6.81	0.22	13.4	0.41 3.44	3.69	1.5	15.5	3.85	3.47	13.4		P		AVE			SIGN					BASIN L-B & BASIN J-B CAPTURED IN TYPE R SUMP INLET
	DP14-B		DP7-	B, DP11	  -B, AN	D DP12	-В	I	18.3	5.88	3.22	18.9			18	.9 5	5.88	0.5	3.0	133	5.1	0.4	14	COMBINES DP7-B, DP11-B, & DP12-B
	DP15-B	M-B	1.46	0.48	12.8	0.71	3.76	2.7	12.8	0.71	3.76	2.7		P		AVE	L TIN		SIGN	IIFICA	NT	Í		BASIN M-B CAPTURED IN TYPE R SUMP INLET
	DP16-B			P13-B		215_B			15.5	1 56	3 / 7	15.8			15	8	1 56	0.5	3.0	120	67	0.3	30	COMBINES DP13.8 & DP15.8
						13-13			10.0	4.50	0.40	10.0		Р		AVE	L TIN		SIGN	IIFICA	NT	0.0	0	
	DP17-B	N-B	3.00	0.16	16.1	0.48	3.42	1.6	16.1	0.48	3.42	1.6		P	IPE TR	AVE		AE INS	SIGN	IIFICA	NT			BASIN N-B CAPTURED IN OPEN GRATE SUMP INLET
	DP18-B		<u> </u>	р14-В /	AND DF	Р17-В		I	18.3	6.36	3.22	20.5			_			$\rightarrow$				-		COMBINES DP17-B & DP14-B
	DP19-B	E-B	1.03	0.16	11.8	0.16	3.88	0.6	11.8	0.16	3.88	0.6									NT			BASIN E-B CAPTURED IN OPEN GRATE SUMP INLET
	DB20-B			р16-В /	AND DF	Р19-В		 	15.8	4.72	3.44	16.2		P		AVE			SIGN			1		COMBINES DP19-B & DP15-B
	DP21-B	DP18-B DP20-B O-B	1 18	0 11	18.3 15.8 7.6	6.36 4.72	4 53	0.6	18.3	11 21	3 22	36.1												TOTAL FLOW TO BE DETAINED BY POND B
L	D			0.71		0.10		0.0			J													

			GRANDVIEV			IEW	RESERVE (PHASE II- DUPLEXES)								S)				Calc'd by:					
		à						Р	ROPO	DSED	CON	IDITIO	ONS									Chec	ked by	КН
		7						DE	SIGN	STO	RM:	100-1	(EA	R								Da	ate:	7/14/2024
HR	Gree	en																						
				DI	RECT	RUNO	FF			$\Sigma Q_5$	(cfs)		S	TREE	т		PI	PE			TR/	AVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C100	f <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %		PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	DP1-B	K-B	1 12	0.64	11 7	0.72	6.54	47	117	0.72	6.54	4.7			PIP	E TRA	AVEL .	TIME	INSI	IGNIF	ICAN	т	1	BASIN K-B CAPTURED IN TYPE R AT GRADE INLET
	DITE	КВ	1.12	0.04		0.72	0.04			0.72	0.04				PIP	E TRA	VEL .	тіме	INSI	IGNIF	ICAN	IT		
-	DP2-B	D-B	1.03	0.62	12.4	0.63	6.39	4.1	12.4	0.63	6.39	4.1						_						BASIN D-B CAPTURED IN TYPE R AT GRADE INLET
	DP3-B		l	DP1-B	AND DF	Р2-В			12.4	1.36	6.39	8.7				8.7	1.36	6 0.5	5	2.0	78	5.1	0.26	COMBINES DP1-B & DP2-B
		A R	6 56	0.57	16.0	3.76	5.62	21 1	16.0	3 75	5.62	21 1			PIP	E TRA	AVEL .	TIME	INSI	IGNIF		ΙТ	1	BASIN A.B. CADTI IDED IN TYPE P. AT CRADE INI ET
	DF4-D	C-B	1.53	0.68	13.3	1.04	6.21	6.5	10.9	3.75	5.02	21.1			PIP	E TRA	VEL .	TIME	INSI	IGNIF	ICAN	т		
	DP5-B	F-B	1.45	0.47	12.9	0.67	6.28	4.2	13.3	1.72	6.21	10.7						_						BASIN C-B & BASIN F-B CAPTURED IN TYPE R AT GRADE INLET
	DP6-B			DP4-B	AND DF	Р5-В		1	16.9	5.47	5.62	30.7				30.7	5.47	7 0.5	5	2.0	45	5.1	0.15	COMBINES DP4-B & DP5-B
	DP7-B		I	DP6-B	AND DF	Р3-В		I	17.0	6.83	5.60	38.2				38.2	6.83	3 0.5	5	2.0	406	5.1	1.33	COMBINES DP3-B & DP6-B
	DP8-B	G-B	2.15	0.69	14.9	1.48	3 5.92	8.7	14.9	1.48	5.92	2 8.7			PIP	E TRA	VEL .	TIME	INSI	IGNIF		Т	1	BASIN G-B CAPTURED IN TYPE R SUMP INLET
			4.40	0.57	47.5	0.00		10.0	47.5	0.00	E E C	42.0			PIP	E TRA	AVEL .	TIME	INSI	IGNIF		Т	1	
-	DP9-B	п-в	4.12	0.57	17.5	2.33	5.52	12.9	17.S	2.33	5.52	2 12.9						-	-					DASIN H-D CAPTURED IN TTPER SUMP INLET
	DP10-B		-	DP8-B	AND DF	9-B	-	1	17.5	3.80	5.52	2 21.0				21.0	3.80	0 0.5	5	2.0	650	5.1	2.13	COMBINES DP8-B & DP9-B
	DP11-B	B-B	3.55	0.47	16.3	1.65	5.70	9.4	16.3	1.65	5.70	9.4			PIP	EIRA	AVEL		11131		ICAN		1	BASIN B-B CAPTURED IN OPEN GRATE SUMP INLET
	DD40 D		0.70	0.04		0.40	0.07			0.40	0.07				PIP	E TRA	VEL .	TIME	INSI	IGNIF	ICAN	IT	1	
	DP12-B	I-B L-B	0.76	0.64	11.1	0.49	6.67	5.3	11.1	0.49	6.67	3.3			PIP	E TRA	VEL .	TIME	INSI	IGNIF	ICAN	т		BASIN I-B CAPTURED IN TYPE R AT GRADE INLET
	DP13-B	J-B	6.81	0.66	15.5	4.49	5.82	26.2	15.5	5.35	5.82	2 31.1						_						BASIN L-B & BASIN J-B CAPTURED IN TYPE R SUMP INLET
	DP14-B		DP7-	 B, DP11	-B, ANI	D DP12	-В	I	18.3	8.97	5.41	48.5				48.5	8.9	7 0.5	5	3.0	133	6.7	0.33	COMBINES DP7-B, DP11-B, & DP12-B
	DP15-B	M-B	1.46	0.64	12.8	0.9/	1 6 32	5 9	12.8	0.94	6 32	5 9			PIP	E TRA	AVEL .	TIME	INSI	IGNIF	ICAN	IT	i	BASIN M-B CAPTURED IN TYPE R SUMP INLET
	DI 10 D	M D	1.40	0.04	12.0	0.0-	0.02	0.0	12.0	0.04	0.02	. 0.0												
	DP16-B			0P13-B /	AND DF	P15-B		<u> </u>	15.5	6.29	6.32	2 39.7			PIP	39.7	6.29	9 0.8 TIME	5 INSI	0.5		2.0	0.02	COMBINES DP13-B & DP15-B
	DP17-B	N-B	3.00	0.41	16.1	1.22	2 5.74	7.0	16.1	1.22	5.74	7.0				- 110-							1	BASIN N-B CAPTURED IN OPEN GRATE SUMP INLET
	DP18-B			р Р14-В <i>А</i>	AND DF	Р17-В			18.3	10.19	5.41	55.1			PIP	E TRA	AVEL .	TIME	INSI	IGNIF	ICAN	IT	1	COMBINES DP17-B & DP14-B
	DP19-B	E-B	1.03	0.41	11.8	0.42	2 6.51	2.7	11.8	0.42	6.51	2.7												BASIN E-B CAPTURED IN OPEN GRATE SUMP INLET
						10 P		ľ	15.0	6.74	E OT	20.0			PIP	ETRA	AVEL .	TIME	INSI	IGNIF	ICAN	IT	1	
	DP20-B	DP18-B		л- 10-В A	18.3	10.19	9		15.6	0.71	5.62	39.0						-	+	-+				
	0001 0	DP20-B		0.47	15.6	6.71	1		40.0	17.15														
	DP21-B	0-в	1.18	0.47	7.6	0.56	0 /.61	4.2	18.3	17.45	5.41	94.3												I OTAL FLOW TO BE DETAINED BY POND B



Grandview Reserve Phase 2 Preliminary Drainage Report Project No.: 201662.202

## APPENDIX C – HYDRAULIC CALCULATIONS (TO BE PROVIDED WITH FDR)



Grandview Reserve Phase 2 Preliminary Drainage Report Project No.: 201662.202

## **APPENDIX D – WATER QUALITY & DETENTION**

Note: Calculations provided are preliminary only and are subject to revisions and additional review at time of Final Drainage Report.

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project:	Grandview Reserve - Phase 2
Basin ID:	Pond A



es

Depth Increment = 1.00

ft

Ontional

Optional

Т

Т

T

POOL Example Zone C		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume			
					Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>+</sup> )	(acre)	(ft <sup>3</sup> )	(ac-ft)
Watershed Information				6965.67	Top of Micropool		0.00				10	0.000		
Selected BMP Type =	EDB				6966		0.33		-		592	0.014	99	0.002
Watershed Area -	21.05	20100					1 50				11 407	0.264	7 171	0.165
Watersneu Area =	51.95	acres					1.50				11,497	0.204	/,1/1	0.105
Watershed Length =	2,977	ft			-		2.50				24,552	0.564	25,196	0.578
Watershed Length to Centroid =	1,283	ft					3.50				34,874	0.801	54,909	1.261
Watershed Slope =	0.018	ft/ft					4.50				44.697	1.026	94,694	2.174
Watershed Impensiousness =	40.00%	porcont					5 50				52 979	1 227	142 092	2 205
watershed imperviousness -	49.00 %	percent					5.50				33,878	1.257	143,302	3.305
Percentage Hydrologic Soil Group A =	10.0%	percent			6,972.17		6.50				62,472	1.434	202,157	4.641
Percentage Hydrologic Soil Group B =	90.0%	percent												
Percentage Hydrologic Soil Groups C/D =	0.0%	percent												
Target WOCV Drain Time =	40.0	hours												
larger wood brain time -	-10.0	nours												
Location for 1-hr Rainfall Depths =	User Input													
After providing required inputs above incl	ludina 1-hour	rainfall												
depths, click 'Run CUHP' to generate rung	off hydrograph	s using												
the embedded Colorado Urban Hydro	graph Procedu	ire.	Ontional Lloo	r Ovorridoc										
		1	Optional Use	Tovernues										
water Quality Capture Volume (WQCV) =	0.542	acre-reet		acre-reet										
Excess Urban Runoff Volume (EURV) =	1.683	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 0.93 in.) =	1.097	acre-feet	0.93	inches										
5-vr Pupoff Volume (P1 = 1 21 in ) =	1 555	acro-foot	1 21	inches										
	1.555	dere rece	1.21											
10-yr Runon Volume (P1 = 1.46 In.) =	2.105	acre-reet	1.40	inches										
25-yr Runoff Volume (P1 = 1.84 in.) =	3.229	acre-feet	1.84	inches										
50-yr Runoff Volume (P1 = 2.15 in.) =	4.044	acre-feet	2.15	inches									7	T
100-vr Runoff Volume (P1 = 2.49 in ) =	5,086	acre-feet	2.49	inches										
$500_{\text{eV}}$ Rupoff Volume (P1 = 2.25 in) =	7 451	acre-foot	3.25	inches										
500 yr Rahon Volume (P1 = 5.55 (fl.) =	, .TJI	au cheel	5.55	Turces						-				
Approximate 2-yr Detention Volume =	0.975	acre-feet												
Approximate 5-yr Detention Volume =	1.377	acre-feet												
Approximate 10-yr Detention Volume =	1.878	acre-feet												
Approximate 25-yr Detention Volume -	2 203	acre-feet												
Approximate 20-yr Detention volume =	2.233	acroneet								-				
Approximate 50-yr Detention Volume =	2.506	acre-feet												
Approximate 100-yr Detention Volume =	2.902	acre-feet												
		-							1					
Define Zones and Basin Geometry														
Define Zones and Basin Geometry		1												
Zone 1 Volume (WQCV) =	0.542	acre-feet			-									
Zone 2 Volume (EURV - Zone 1) =	1.141	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	1.219	acre-feet							-					
Total Detention Basin Volume -	2 902	acro-foot												
Initial Sursharge Volume (ISV) -	21502	A 3												
	usei													
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft												
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft												
Slope of Trickle Channel $(S_{rc}) =$	user	ft/ft												
Classes of Main Desin Cides (C		11.37												
Slopes of Main Basin Sloes (Smain) =	usei	п.v												
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	]												
_		_												
Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>							-					
Surcharge Volume Length (Lucy) =	user	ft.												
Curcharge Volume Width (W)		A.												
	usei													
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	user	ft			-									
Length of Basin Floor (L <sub>FLOOR</sub> ) =	user	ft												
Width of Basin Floor (WFLOOR) =	user	ft							1					
Area of Basin Floor (Arease) =	usor	<b>⊕</b> <sup>2</sup>												
Victoria of Dasin Floor (Victoria)	usei	- 3												
volume or basin Hoor (V <sub>FLOOR</sub> ) =	user	rt -												
Depth of Main Basin $(H_{MAIN}) =$	user	nt												
Length of Main Basin (L <sub>MAIN</sub> ) =	user	ft											7	T
Width of Main Basin (Wmm) =	user	ft												
Area of Main Bacin (A	LICON	φ <sup>2</sup>												
	usel									-				
volume of Main Basin ( $V_{MAIN}$ ) =	user	π												
Calculated Total Basin Volume (V <sub>total</sub> ) =	user	acre-feet												

	DI	TENTION	BASIN OUT	LET STRU	CTURE DE	SIGN					
MHFD-Detention, Version 4.06 (July 2022)											
Project: Basin ID:	Grandview Reserv	e - Phase 2									
ZONE 3	- one A			Estimated	Estimated						
ZONE 2 ZONE 1				Stage (ft)	Volume (ac-ft)	Outlet Type					
			Zone 1 (WQCV)	2.44	0.542	Orifice Plate	1				
	100-YEAR		Zone 2 (EURV)	4.00	1.141	Orifice Plate	-				
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	5.17	1.219	Weir&Pipe (Restrict)	)				
POOL Example Zone	Configuration (Ret	ention Pond)		Total (all zones)	2.902	,	4				
User Input: Orifice at Underdrain Outlet (typically	used to drain WQC	V in a Filtration BM	<u>P)</u>			1	Calculated Parame	ters for Underdrain			
Underdrain Orifice Invert Depth =		ft (distance below	the filtration media	surface)	Under	drain Orifice Area =		ft <sup>2</sup>			
Underdrain Orifice Diameter =		inches			Underdrai	n Orifice Centroid =		feet			
User Input: Orifice Plate with one or more orifice	s or Elliptical Slot W	air (typically used t	o drain WOCV and/o	or FLIDV in a codime	ntation BMP)		Calculated Barama	tors for Plata			
Centroid of Lowest Orifice =	0.00	ft (relative to basir	n bottom at Stage =	0 ft)	WO Orif	ice Area per Row =	N/A	ft <sup>2</sup>			
Depth at top of Zone using Orifice Plate =	4.00	ft (relative to basir	h bottom at Stage =	0 ft)	Ell	iptical Half-Width =	N/A	feet			
Orifice Plate: Orifice Vertical Spacing =	16.10	inches			Ellipt	ical Slot Centroid =	N/A	feet			
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			E	Iliptical Slot Area =	N/A	ft <sup>2</sup>			
Licer Input: Stage and Total Area of Each Orifice	Bow (numbered fr	m lowest to higher	+)								
User input. Stage and rotal Area of Lach Onnee	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1		
Stage of Orifice Centroid (ft)	0.00	1.33	2.67					(spaced)			
Orifice Area (sq. inches)	2.60	4.00	4.00								
		r							-		
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)			
Stage of Orifice Centroid (ft)									-		
Orifice Area (sq. inches)											
User Input: Vertical Orifice (Circular or Rectangu	lar)						Calculated Parame	ters for Vertical Ori	ice		
	Not Selected	Not Selected	]				Not Selected	Not Selected	]		
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ve	rtical Orifice Area =	N/A	N/A	ft <sup>2</sup>		
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	I Orifice Centroid =	N/A	N/A	feet		
Vertical Orifice Diameter =	N/A	N/A	inches								
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and C	utlet Pipe OR Recta	angular/Trapezoidal	Weir and No Outlet	Pipe)		Calculated Parame	ters for Overflow W	eir		
	Zone 3 Weir	Not Selected	1				Zone 3 Weir	Not Selected	1		
Overflow Weir Front Edge Height, Ho =	4.02	N/A	ft (relative to basin l	bottom at Stage = 0 f	ft) Height of Grat	e Upper Edge, $H_t =$	4.02	N/A	feet		
Overflow Weir Front Edge Length =	5.00	N/A	feet		Overflow V	/eir Slope Length =	5.00	N/A	feet		
Overflow Weir Grate Slope =	0.00	N/A	H:V	G	irate Open Area / 10	00-yr Orifice Area =	7.41	N/A	~2		
Horiz. Length of Weir Sides =	5.00 Type C Grate	N/A	reet	Ľ	Overflow Grate Open	Area w/o Debris =	8 70	N/A	ft #2		
Debris Clogging % =	50%	N/A	%		overnow drate ope	in Alca wy Debits =	0.70	N/A	lir.		
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re	trictor Plate, or Re	ctangular Orifice)		<u>Ci</u>	alculated Parameter	rs for Outlet Pipe w/	Flow Restriction Pla	ate		
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected			
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below be	asin bottom at Stage	= 0 ft) 0	utlet Orifice Area =	2.35	N/A	ft <sup>2</sup>		
Outlet Pipe Diameter =	24.00	N/A	inches	Half-Con	Outle otral Angle of Pectric	t Orifice Centroid =	1.08	N/A	reet		
Restrictor Flate fleight Above Fipe invert -	10.00	I	linenes	Tidii-Cer	In a Angle of Result	tor riate on ripe -	1.50	N/A	radians		
User Input: Emergency Spillway (Rectangular or	Trapezoidal)						Calculated Parame	ters for Spillway			
Spillway Invert Stage=	5.16	ft (relative to basir	n bottom at Stage =	0 ft)	Spillway D	esign Flow Depth=	0.51	feet			
Spillway Crest Length =	50.00	feet			Stage at	Top of Freeboard =	6.67	feet			
Spillway End Slopes =	4.00	H:V			Basin Area at	Top of Freeboard =	1.43	acres			
Freeboard above Max water Surface =	1.00	reet			Basin volume at	top of Freeboard =	4.64	acre-ft			
Routed Hydrograph Results	The user can over	ide the default CUP	HP hydrographs and	runoff volumes by e	entering new values	in the Inflow Hydro	ographs table (Colur	nns W through AF).	E00 Voor		
One-Hour Rainfall Depth (in) =	N/A	N/A	0.93	1.21	1.46	1.84	2.15	2.49	3.35		
CUHP Runoff Volume (acre-ft) =	0.542	1.683	1.097	1.555	2.105	3.229	4.044	5.086	7.451		
Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak O (cfs) =	N/A N/A	N/A N/A	0.2	1.555	2.105	3.229	4.044	5.086	/.451 42.5		
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.00	0.12	0.12	0.55	0.01	1.00		
Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow O (cfs) =	N/A N/A	N/A N/A	0.01	0.03	0.13	0.42	0.60 46 3	0.84	1.33		
Peak Outflow Q (cfs) =	0.3	0.5	0.4	0.5	2.9	12.9	20.6	24.3	58.6		
Ratio Peak Outflow to Predevelopment Q =	N/A Plate	N/A Plate	N/A Plate	0.5 Plate	0.7 Overflow Wair 1	1.0 Overflow Weir 1	1.1 Overflow Weir 1	0.9 Outlet Plate 1	1.4 Spillway		
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.7	1.2	1.4	1.4		
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A		
Time to Drain 97% of Inflow Volume (hours) =	39 <b>41</b>	71	59	69	76	74	73	59 71	55		
Maximum Ponding Depth (ft) =	2.44	4.00	3.18	3.73	4.20	4.55	4.75	5.15	5.52		
Area at Maximum Ponding Depth (acres) =	0.55	0.91	0.72	0.85	0.96	1.03	1.08	1.16	1.24		
Maximum volume Stored (acre-rt) =	0.515	1.005	1.005	11101	11007	LILIU	21120	2.07 1	0.000		

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



Watershed Information

sileu Iniornation		
Selected BMP Type =	EDB	
Watershed Area =	38.19	acres
Watershed Length =	2,173	ft
Watershed Length to Centroid =	1,171	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	43.00%	percent
Percentage Hydrologic Soil Group A =	10.0%	percent
Percentage Hydrologic Soil Group B =	90.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Approximate 100-yr Detention Volume = 3.152

	1 C C C C C C C C C C C C C C C C C C C			
the embedded Colorado Urban Hydrog	graph Proced	ure.	Optional Use	r Overrides
Water Quality Capture Volume (WQCV) =	0.597	acre-feet		acre-feet
Excess Urban Runoff Volume (EURV) =	1.743	acre-feet		acre-feet
2-yr Runoff Volume (P1 = 0.93 in.) =	1.132	acre-feet	0.93	inches
5-yr Runoff Volume (P1 = 1.21 in.) =	1.625	acre-feet	1.21	inches
10-yr Runoff Volume (P1 = 1.46 in.) =	2.255	acre-feet	1.46	inches
25-yr Runoff Volume (P1 = 1.84 in.) =	3.602	acre-feet	1.84	inches
50-yr Runoff Volume (P1 = 2.15 in.) =	4.563	acre-feet	2.15	inches
100-yr Runoff Volume (P1 = 2.49 in.) =	5.816	acre-feet	2.49	inches
500-yr Runoff Volume (P1 = 3.35 in.) =	8.622	acre-feet	3.35	inches
Approximate 2-yr Detention Volume =	0.999	acre-feet		
Approximate 5-yr Detention Volume =	1.422	acre-feet		
Approximate 10-yr Detention Volume =	1.981	acre-feet		
Approximate 25-yr Detention Volume =	2.446	acre-feet		
Approximate 50-yr Detention Volume =	2.680	acre-feet		

acre-feet

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.597	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.145	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.410	acre-feet
Total Detention Basin Volume =	3.152	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR})$ =	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet

	Depth Increment =		θ.							
	bepar increment		Optional				Optional			
	Stage - Storage	Stage	Override Stage (ft)	Length	Width (ft)	Area	Override Area (ft <sup>2</sup> )	Area (acro)	Volume	Volume
6021.67	Top of Micropool		0.00				10	0.000	(10)	(dc-rt)
0951.07	6932		0.33				100	0.002	18	0.000
	6933		1 33				27 759	0.637	13 947	0.000
	6934		2 33				31 266	0.037	43.460	0.520
	6935		3.33				34.890	0.801	76,538	1.757
	6,936.00		4.33				38,648	0.887	113,306	2,601
	6937		5.50				42,535	0.976	160,799	3.691
	6,938.00		6.00				47,426	1.089	183,289	4.208
	6939		7.00				52,297	1.201	233,150	5.352
r Overrides										
acre-feet										
inches										
inches										
inches										
inches										
inches										
inches									· · · · · · · · · · · · · · · · · · ·	
inches										

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#### DETENTION BASIN OUTLET STRUCTURE DESIGN

Project	Grandview Becom	A Phace 2	1HFD-Detention, V	ersion 4.06 (July 2	2022)				
Basin ID:	Pond B	e Plidse 2							
ZONE 3				Ectimated	Ectimated				
ZONE 2 ZONE 1				Esumated	Estimated	Outlat Tura			
				Stage (IL)	volume (ac-it)	Outlet Type	1		
Leony Wacy			Zone 1 (WQCV)	1.76	0.597	Orifice Plate	-		
	100-YEAR ORIFICE		Zone 2 (EURV)	3.32	1.145	Orifice Plate			
PERMANENT ORIFICES			Zone 3 (100-year)	4.94	1.410	Weir&Pipe (Restrict)			
Example Zone	Configuration (Ret	ention Pond)		Total (all zones)	3.152		-		
User Input: Orifice at Underdrain Outlet (typically	used to drain WQC	V in a Filtration BMF	P)			1	Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =		ft (distance below	the filtration media	surface)	Under	drain Orifice Area =		ft <sup>2</sup>	
Underdrain Orifice Diameter =		inches		-	Underdrai	n Orifice Centroid =		feet	
								1	
User Input: Orifice Plate with one or more orifice	s or Elliptical Slot W	eir (typically used to	o drain WQCV and/o	or EURV in a sedime	entation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage =	0 ft)	WQ Orif	ice Area per Row =	2.785E-02	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	3.32	ft (relative to basin	bottom at Stage =	0 ft)	EI	iptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	13.30	inches			Ellipt	ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	4.01	sa. inches (use rec	tangular openings)			Elliptical Slot Area =	N/A	ft <sup>2</sup>	
			gg-,					Inc	
User Input: Stage and Total Area of Each Orifice	Row (numbered fro	m lowest to highest	t)						
ober input blage and total filed of Eden office	Row 1 (required)	Row 2 (ontional)	Row 3 (ontional)	Row 4 (ontional)	Row 5 (optional)	Row 6 (ontional)	Row 7 (ontional)	Row 8 (ontional)	1
Stage of Orifice Centroid (ft)	0.00	1 11	2 21	now r (optional)	now 5 (optional)	non o (optional)	(optional)	now o (optional)	
Orifice Area (cg. inches)	4.01	4.01	4.01						-
Office Area (sq. IIICHES)	1.01	1.01	1.01						J
	Dow 0 (optional)	Row 10 (ontional)	Dow 11 (optional)	Dow 12 (ontional)	Dow 12 (optional)	Dow 14 (optional)	Dow 1E (optional)	Dow 16 (optional)	1
Stage of Orifice Controld (#)	Row 9 (optional)	Row to (optional)	Row II (optional)	ROW 12 (Optional)	Row 15 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Online Centroid (It)									-
Urifice Area (sq. inches)									]
Haar Innuts Martinel Orifice (Circular or Destance)	(a.r.)						Calculated Davama	have fee Ventical Orif	
User input: vertical Onlice (Circular of Rectangu	ldr)	Not Colorised	1				Calculated Parame	Lers for vertical Oni	1
Truck (Mathed Offer	Not Selected	Not Selected	Q. (and all and a local second	h	0.01	1-1-0-15 A	Not Selected	Not Selected	e.2
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0π) ve	rtical Orifice Area =	N/A	N/A	π <sup>-</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	I Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and O	utlet Pipe OR Recta	ingular/Trapezoidal	Weir and No Outlet	Pipe)		Calculated Parame	ters for Overflow W	eir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	1
Overflow Weir Front Edge Height, Ho =	3.33	N/A	ft (relative to basin	bottom at Stage = 0	ft) Height of Grat	e Upper Edge, $H_t =$	3.33	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet		Overflow V	/eir Slope Length =	6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	0	Grate Open Area / 10	00-yr Orifice Area =	6.49	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet	C	Overflow Grate Oper	Area w/o Debris =	25.06	N/A	ft <sup>2</sup>
Overflow Grate Type =	Type C Grate	N/A			Overflow Grate Ope	n Area w/ Debris =	12.53	N/A	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%						
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Res	trictor Plate, or Rec	tangular Orifice)		<u>C</u>	alculated Parameter	rs for Outlet Pipe w/	Flow Restriction Pla	ate
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below b	asin bottom at Stage	= 0 ft) C	utlet Orifice Area =	3.86	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	30.00	N/A	inches		Outle	t Orifice Centroid =	1.02	N/A	feet
Restrictor Plate Height Above Pipe Invert =	22.00		inches	Half-Cer	ntral Angle of Restrie	tor Plate on Pipe =	2.06	N/A	radians
									-
User Input: Emergency Spillway (Rectangular or	Frapezoidal)						Calculated Parame	ters for Spillway	
Spillway Invert Stage=	4.80	ft (relative to basin	bottom at Stage =	0 ft)	Spillway [	esign Flow Depth=	0.92	feet	
Spillway Crest Length =	26.00	feet			Stage at	Top of Freeboard =	6.72	feet	
Spillway End Slopes =	4.00	H:V			Basin Area at	Top of Freeboard =	1.17	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at	Top of Freeboard =	5.02	acre-ft	
								-	
Routed Hydrograph Results	The user can overr	<i>ide the default CU</i> H	IP hydrographs and	runoff volumes by e	entering new values	in the Inflow Hydro	ographs table (Colum	nns W through AF).	500 V/
Design Storm Return Period =	N/A	EURV	2 Year	5 Year	10 Year	25 Year	2 15	100 Year	3 35
CLIHP Runoff Volume (acre-ft) =	0.597	1 743	1 132	1.21	2 255	3 602	4 563	5.816	8.622
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.132	1.625	2.255	3.602	4.563	5.816	8.622
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.3	1.6	6.5	20.7	29.1	40.4	63.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.04	0.17	0.54	0.76	1.00	1.67
rredevelopment unit Peak How, q (CTS/acre) = Peak Inflow Q (cfc) =	IN/A N/A	N/A N/Δ	0.01	0.04	0.1/	0.54 48.4	0./6	1.06	1.0/
Peak Outflow $O(cfs) =$	0.3	0.6	0.4	0.5	4.6	20.2	32.1	37.1	79.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.7	1.0	1.1	0.9	1.2
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.2	0.8	1.3	1.5	1.6
Max velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	IN/A 30	N/A 68	IN/A 56	N/A 66	N/A 70	N/A 67	N/A 64	N/A 61	IN/A 55
Time to Drain 99% of Inflow Volume (hours) =	40	72	59	70	75	74	73	72	69
Maximum Ponding Depth (ft) =	1.76	3.32	2.41	3.04	3.55	3.96	4.20	4.76	5.40
Area at Maximum Ponding Depth (acres) =	0.67	0.80	0.72	0.78	0.82	0.86	0.88	0.92	0.97
Maximum Volumo Storod (acro-ft) =	0.602	1 749	1.055	1 521	1.935	2 279	2.478	2,990	3 594

02-Pond\_B-.xlsm, Outlet Structure



Grandview Reserve Phase 2 Preliminary Drainage Report Project No.: 201662.202

**APPENDIX E – REFERENCES** 



Only relevant sheets from this report provided

## Grandview Reserve Master Development Drainage Plan

August 2021 HR Green Project No: 191850

#### **Prepared For:**

4 SITE INVESTMENTS, LLC Mr. Peter Martz or Paul Howard 1271 Kelly Johnson Blvd., Ste. 100 Colorado Springs, CO 80920 719-499-8416

#### **Prepared By:**

HR Green Development, LLC Contact: Chris McFarland, PE cmcfarland@hrgreen.com 720-602-4956 > HRGREEN.COM



## Subbasin Description

The entire site drains in a south easterly direction and is divided into 8 major drainage basins and a total of 18 subbasins together as described below.

- Subbasin A1 is located in the southwestern corner of the site, to the south and west of MS. The basin drains towards the southeast to proposed detention pond A. Current planning documents call for medium density dwelling units and a small pocket park. The basin is 37.00 acres, with a composite impervious value of 35.22% and runoff rates for the 5 and 100 year of 30.72 cfs and 100.64 cfs respectively. The pond will discharge at predevelopment rates and into MS via the ponds outlet structure.
- Subbasin B1 is located between MS and MST2 to the east of subbasin A1. The basin drains towards the southeast and towards subbasin B2. Current planning documents call for medium density dwelling units and some parkland area. The basin is 37.00 acres, with a composite impervious value of 45.00% and runoff rates for the 5 and 100 year of 29.46 cfs and 97.08 cfs respectively.
- Subbasin B2 is located between MS and MST2 to the northeast of subbasin A1. The basin drains towards the southeast and towards Detention Pond B. Current planning documents call for medium density dwelling units. The basin is 24.89 acres, with a composite impervious value of 43.26% and runoff rates for the 5 and 100 year of 12.02 cfs and 42.26 cfs respectively.
- Subbasin B3 is located between MS and EF and to the northeast of east of basin B2. The existing MST2 tributary runs through the basin. The site drains towards the southeast and towards Detention Pond B. Current planning documents call for high, medium-high, and medium density dwelling units along with a pocket park. The basin is 118.90 acres, with a composite impervious value of 49.42% and runoff rates for the 5 and 100 year of 92.76 cfs and 295.27 cfs respectively.
- Subbasin C1 is located to the northeast of east of basin B1 and the existing MST2 tributary runs through the middle of the basin. The basin drains towards the southeast and towards Detention Pond C. Current planning documents call for an institutional parcel, medium and high density dwelling units and a pocket park. The basin is 77.83 acres, with a composite impervious value of 51.20% and runoff rates for the 5 and 100 year of 77.99 cfs and 238.03 cfs respectively.
- Subbasin D1 is located between MS and MST2 to the east of Basin B3 and adjacent to the MST2 channel. The basin drains towards the southeast and towards drainage basin D2. Current planning documents call for medium density dwelling units along with a pocket park. The basin is 24.33 acres, with a composite impervious value of 53.89% and runoff rates for the 5 and 100 year of 24.15 cfs and 70.07 cfs respectively.
- Subbasin D2 is located between MS and MST2 to the south of basins D1 and B3. The basin drains towards the southwest and towards detention pond D. Current planning documents call for high density dwelling units along with a pocket park and a commercial parcel. The basin is 77.90 acres, with a composite impervious value of 62.10% and runoff rates for the 5 and 100 year of 98.47 cfs and 252.18 cfs respectively.
- Subbasin E1 is located just east of EFT along the northern portion of the site. The basin drains towards the southeast and towards basins F3 and F4. Current planning documents call for low



slope, length, shape, impervious area, pervious depression storage area, and various infiltration rates. Tabular hydrographs are then computed and can be used in EPA SWMM. The CUHP results are included within Appendix B.

EPA SWMM was used to determine flow routing via the kinematic wave method. Subbasins were routed to their respective design points and detention ponds for both the developed and predeveloped condition to determine peak runoff amounts for the 5-year and 100-year storm events. Information from these models along with information and calculations performed in the Colorado Springs BMP spreadsheets was used to determine pond sizing calculations and release rates.

## c. Basin Hydrology

A summary of the flows for both the predeveloped and developed cases for each basin, subbasin and Pond are found on next page along with the full computation found in Appendix B.

	SWMM Basin and Pond Summary								
			5 Year			100 Year			
	Basin		Peak	100 Year	5 Year Pond	Pond			
Basin	Area	%	Runoff	Peak Runoff	Volume (ac-	Volume (ac-			
Description	(ac)	Impervious	(cfs)	(cfs)	ft)	ft)			
A1	45.38	35.22%	30.72	100.64					
	-		Рс	ond A	1.83	3.50			
B1	37.00	45.00%	29.46	97.08					
B2	24.89	43.26%	12.02	42.26					
B3	118.90	49.42%	92.76	295.27					
	-		Рс	ond B	5.90	19.00			
C1	77.83	51.20%	77.99	238.03					
	-		Po	ond C	3.91	6.87			
D1	24.33	44.14%	24.15	70.07					
D2	77.90	62.10%	98.47	252.18					
	-		Рс	ond D	6.61	10.19			
E1	88.60	19.54%	46.88	178.04					
	-		Po	ond E	1.96	2.44			
F1	33.73	25.00%	16.28	58.95					
F2	67.64	51.39%	60.11	170.90					
F3	12.84	45.00%	11.36	32.93					
F4	51.81	46.54%	42.32	124.89					
	-		Po	ond F	7.38	12.62			
G1	20.13	36.52%	13.78	43.95					
G2	15.14	25.00%	6.55	23.95					
			Po	ond G	0.72	2.03			
H1	20.71	24.49%	5.68	27.62					
H2	18.55	43.68%	16.24	47.62					
Н3	6.01	40.57%	5.21	15.60					
H4	27.65	38.24%	20.93	64.71					
			Po	ond H	2.93	6.17			



## IV. Hydraulic Analysis

## a. Major Drainageways

In general, the site runoff flows towards the 4 major drainageways and in a southeasterly direction. These basins are described in more detail below:

#### Main Stem

The Main Stem (MS) is in the southwestern portion of the site. Offsite flows collect and are conveyed under Eastonville Road via a culvert. MS travels in a southeasterly direction and combines with the Main Stem Tributary #2 (MST2) just off site where it is then conveyed past Highway 24 via a culvert. An existing breached stock pond exists in the approximate center point of the channel within the site. Jurisdictional wetlands exist within this channel and the area is within a Zone A floodplain towards the southern portion of the site. This channel sees only intermittent flows at this time however once development occurs there may be a more constant baseflow.

Proposed improvements for MS include the removal of the breached stock pond berm and regrading of the affected stretch of channel to restore its historic state. Proposed flow rates through MS are not to exceed historic flowrates and as such, the remainder of the channel is to remain in its current state sans any preemptive check structures; modeling indicates the channel shall remain stable despite the removal of the existing berm.

### Main Stem Tributary #2

MST2 crosses Eastonville road via an existing culvert and flows through the site in a southeasterly direction. Portions of this channel are within a mapped floodplain as shown in the existing FIRM Panel. Per a July email from the USACE this drainage channel was preliminarily determined to be a non-jurisdictional waters/wetland.

Proposed improvements for MST2 include the realignment of the channel, generally shifting the channel towards the west to accommodate the proposed land plan. There is to be a dedicated 100' corridor in which the valley will meander. Preliminary analysis indicates the valley will have an average width of approximately 63' at the elevation necessary to meet freeboard requirements; initial sizing approximates the bankfull width to be 6.8'. The valley and channel thalweg will generally follow the same profile, with some deviation as the bankfull channel meanders through the valley in turn decreasing the low flow channels average slope. The average valley profile is to be approximately 1% with a series of grade control structures to both decrease elevation and dissipate energy to meet natural channel criteria as outline in El Paso County criteria and agreed upon channel parameters.

## East Fork Tributary

The East Fork tributary (EFT) crosses the north property line and flows are conveyed through the site via a natural channel. The channel has been mapped as a Zone A floodplain per the existing FIRM panel; it appears any hydraulic effects of the crossing at Eastonville Road was not accounted for in the floodplain delineation. While the current floodplain delineation shows the channel continuing through Highway 24, there is no existing crossing for this section of the drainage channel below Highway 24 and instead the flows are conveyed to the northeast towards the East Fork Upper (EF). Per a July email from the USACE this drainage channel was preliminarily determined to be a non-jurisdictional waters/wetland.



## VI. Selected Plan

## a. Plan Hydrology

This MDDP schematically addressed on-site and off-site drainage patterns using the existing topography and proposed land use plan for the overall drainage design. Individual preliminary and final drainage reports will better define the planning areas as the site is developed. These reports will include inlet design, storm sewer hydraulics, street design and other requirements typical of more detailed drainage reports.

The overall site is divided into 8 separate major basins, basins A-H and contribute to individual detention ponds for each major basin. Basin sizes range from 35 acres to 181 acres in size. Basins A, B, C and D drain and eventually discharge into the Main Stem and Main Stem Tributary #2. Basins E, F, G, and H drain towards the East Fork Drainage channel.

The sub-basins are described in additional detail above.

## **b.** Detention Ponds

The site plans propose the construction of 8 separate full spectrum detention facilities.

- Pond A is located in the southwest corner of the site and discharges into the Main Stem drainageway. The pond is planned to store a maximum of 4.05 ac-ft during the 100 year event and have a peak outflow of 55.9 cfs which is slightly below the pre development peak outflow of 57.1 cfs. The 5 year storage volume is 2.46 ac-ft with a peak outflow of 3.7 cfs.
- Pond B is located to the east of Pond A and the Main Stem and discharges into the Main Stem Tributary #2. The pond is planned to store a maximum of 16.60 ac-ft during the 100 year event and have a peak outflow of 165.4 cfs which is slightly above the pre development peak outflow of 164.2 cfs. The 5 year storage volume is 8.44 ac-ft with a peak outflow of 2.6 cfs.
- Pond C is located near the center of the western portion of the site near the existing Main Stem Tributary #2. The pond discharges into a revised open channel to be designed and discharges to the Main Stem Tributary #2 which merges with the Main Stem Tributary just off site. The pond is planned to store a maximum of 6.91 ac-ft during the 100 year event and have a peak outflow of 119.2 cfs which is slightly below the pre development peak outflow of 120.2 cfs. The 5 year storage volume is 4.07 ac-ft with a peak outflow of 1.5 cfs.
- Pond D is located near the southern portion of the site adjacent to Highway 24. The pond discharges into the Main Stem right after the Main Stem and Main Stem Tributary #2 merge. The pond is planned to store a maximum of 9.41 ac-ft during the 100 year event and have a peak outflow of 154.4 cfs which equals the predevelopment peak flow rate. The 5 year storage volume is 6.28 ac-ft with a peak outflow of 2.0 cfs.
- Pond E is located in the middle of the site just east of the East Fork drainage way. The pond discharges into the East Fork drainageway. The pond is planned to store a maximum of 2.40 ac-ft during the 100 year event and have a peak outflow of 163.4 cfs which is greater than the pre



ate





Basin	Design Point	5 Year P Devlopm
	67	231.47
G1	70	5.57
G2	71	3.87
	72	3.87
	73	3.87
	74	189.42
H1	80	1.85
H2	81	5.37
H3	82	1.92
H4	83	8.07
	84	7.22
	85	1.92
OS1	OS1	67.00
OS2	OS2	59.00
OS3	OS3	61.00
OS4	OS4	180.00
	Outfall1	80.03
	Outfall2	85.96
	Outfall3	30.00
	Outfall4	341.05

			i		i
		5 Year Pre	5 Year Post	100 Year Pre	100 Year Post
Basin	Design Point	Devlopment	Development	Development	Development
A1	10	13.03	30.72	66.80	100.64
B1	20	4.33	29.46	48.76	97.08
B2	21	1.66	12.02	20.74	42.26
	22	11.85	92.76	140.35	295.27
	23	5.99	40.92	68.56	136.17
B3	24	21.23	93.26	249.20	334.84
C1	30	9.95	77.99	110.70	238.03
	31	9.95	1.52	110.70	115.75
D1	40	8.12	24.15	40.00	70.07
D2	41	22.23	98.47	114.87	252.18
	42	8.12	24.15	40.00	70.07
E1	50	32.34	46.88	157.99	178.04
	51	93.34	85.04	374.99	381.75
F1	60	9.70	16.28	49.45	58.95
F2	61	16.46	60.11	86.73	170.90
F3	62	3.65	11.36	18.42	32.93
F4	63	12.98	42.32	67.82	124.89
	64	13.35	26.88	67.87	90.88
	65	26.04	69.12	135.62	215.63
	66	16.46	60.11	86.73	170.90



HR	Green	

Job No.:	191897.01
Prepared By:	TBI
Date:	04/14/2020











HRGreen DRAWING PATH:\\hrgreen.com\HRG\Data\2019\191897.01\CAD\Dwgs\Exhibits\00-Drainage Basins



Only relevant sheets from this report provided

> HRGREEN.COM

Eastonville Road – Londonderry Dr. to Rex Rd. Segment 2 Improvements Stationing 47+00.00 – 79+31.62

## **Final Drainage Report**

January 2024 HR Green Project No: 201662.08

#### Prepared For:

D.R. Horton Contact: Riley Hillen, P.E. 9555 S. Kingston Ct. Englewood, CO 80112

**Prepared By:** 

HR Green Development, LLC Contact: Colleen Monahan, P.E., LEED AP cmonahan@hrgreen.com

(719) 394-2433



pavement roadway with 4' wide sand shoulders and weedy swales located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts.

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). This includes Basins EA1-EA11.

Refer to the Eastonville Road Segment 1 improvements FDR for subbasin information and calculations south of subbasins EA10 & EA11.

#### Eastonville Road Basins

Basin EA1 is 0.22 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.7$  cfs  $Q_{100} = 1.3$  cfs) is conveyed in curb and gutter to DP2. Flows at DP2 are captured in a 5' Type R sump inlet (Public) and piped to Pond A Sand Filter. Basin EA1 will be detained Pond A Sand Filter.

Basin EA2 is 0.25 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.5$  cfs) is conveyed in curb and gutter to DP3. Flows at DP3 are captured in a 5' Type R sump inlet (Public) and piped to Pond A. Basin EA2 will be detained Pond A Sand Filter.

Basin EA3 is 0.20 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.7$  cfs  $Q_{100} = 1.4$  cfs) is conveyed in curb and gutter to DP5. Flows at DP5 are captured in a 10' Type R sump inlet (Public) and piped to DP9.1. Basin EA3 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch.

Basin EA4 is 0.17 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.5$  cfs  $Q_{100} = 1.1$  cfs) is conveyed in curb and gutter to DP6. Flows at DP6 are captured in a 5' Type R sump inlet (Public) and piped to DP9.1. Basin EA4 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch.

Basin EA5 is 0.16 acres of undeveloped area and includes Pond A Sand Filter. Stormwater ( $Q_5 = 0.1$  cfs  $Q_{100} = 0.4$  cfs) is flows directly into Pond A Sand Filter.

Basin EA6 is 0.70 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ( $Q_5 = 3.1$  cfs  $Q_{100} = 5.5$  cfs) is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA6. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA6 will be detained in TSB #1.

Basin EA7 is 0.65 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ( $Q_5 = 2.5$  cfs  $Q_{100} = 4.7$  cfs is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA7. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA7 will be detained in TSB #1.

Basin EA8 is 2.08 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 5.0 \text{ cfs } Q_{100} = 9.0 \text{ cfs}$ ) is conveyed in curb and gutter to DP14. Flows at DP14 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA8 will be detained Pond B Full Spectrum Detention Basin.

# HRGreen

**PROPOSED CONDITIONS** EL PASO COUNTY, CO

**EASTONVILLE ROAD SEG 2** SPC Calc'd by: СМ Checked by: 2/2/2024 Date:

SUMMARY RUNOFF TABLE												
BASIN	ASIN AREA (ac) % IMPERVIOUS $Q_5$ (cfs)											
EA1	0.22	73	0.8	1.5								
EA2	0.25	72	0.9	1.7								
EA3	0.20	70	0.7	1.3								
EA4	0.17	65	0.5	1.1								
EA5	0.16	0	0.1	0.4								
EA6	0.70	100	3.2	5.3								
EA7	0.65	89	2.6	4.8								
EA8	2.08	99	5.2	8.8								
EA9	2.99	63	5.0	10.4								
EA10	0.16	75	0.6	1.1								
EA11	0.15	67	0.5	1.0								
*G18	321.53	-	28.3	365.2								
*FG36	18.88	-	1.7	18.8								
OS3	1.00	2	0.3	2.2								
OS4	9.60	9	4.8	21.6								
*G16	131.26	-	6.1	112.1								
*G06	832.70	-	22.4	491.0								
OS7	11.42	2	3.6	24.4								

DESIGN CONTRIBUTING  $\Sigma Q_5$  (cfs)  $\Sigma Q_{100}$  (cfs) POINT BASINS G18 365.2 28.3 1 2 FG36 1.7 18.8 2.1 EA1 0.8 1.5 3 G16 6.1 112.1 3.1 EA2, DP2.1 1.6 3.2 22.4 491.0 4 G06 EA5, DP3.1 4.1 1.7 3.4 EA3 0.7 1.3 5 DP5, EA4 6 1.2 2.4 6.1 DP6, DP8 2.9 22.4 7 OS3 0.3 2.2 DP2, DP7 2.0 21.0 8 DP6.1 2.9 9 22.4 10 EA6, EA7 5.6 9.9 OS4, DP9 11 7.5 44.0 12 OS7 3.6 24.4 13 DP2, DP12 26.0 515.3 14 EA8 5.2 8.8 15 EA9 5.0 10.4 DP14, DP15 15.1 10.2 19.1 16.1 EA10 0.6 1.1 EA11 17.1 0.5 1.0

**DESIGN POINT SUMMARY TABLE** 

\* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

Pr\_Drainage\_Calcs3

RBM 2/2/2024 10:36 AM

	EASTONVILLE ROAD SEG 2	<u>Calc'd by:</u>	SPC
ヨゴス	PROPOSED CONDITIONS	Checked by:	СМ
HRGreen	EL PASO COUNTY, CO	Date:	11/27/2023

## SOIL TYPE: HSG A&B

	COMPOSITE 'C' FACTORS																				
							LAN	) USE	TYPE												
		Paved		Histor Green	ic Flow Ar belts, Agr	nalysis iculture		Lawns	i	Land	Use Und	defined	Land	Use Un	defined		С	COMPOSITE			
	%I	<b>C</b> 5	<b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	<b>C</b> 5	<b>C</b> <sub>100</sub>	%I	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	C₅	<b>C</b> <sub>100</sub>			VIOUSNE	:55 & C		
	100	0.90	0.96	2	0.09	0.36	0	0.08	0.35	0	0.00	0.00	0	0.00	0.00	TOTAL		FACTOR			
BASIN		ACRES	5		ACRES	5		ACRES	5		ACRES	5		ACRES	5	ACRES	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>		
EA1		0.16						0.06								0.22	73	0.68	0.79		
EA2		0.18						0.07								0.25	72	0.67	0.79		
EA3		0.14						0.06								0.20	70	0.65	0.78		
EA4		0.11						0.06								0.17	65	0.61	0.74		
EA5		0.00						0.16								0.16	0	0.08	0.35		
EA6		0.70						0.00								0.70	100	0.90	0.96		
EA7		0.58						0.07								0.65	89	0.81	0.89		
EA8		2.06						0.02								2.08	99	0.89	0.95		
EA9		1.88						1.11								2.99	63	0.60	0.73		
EA10		0.12						0.04								0.16	75	0.70	0.81		
EA11		0.10						0.05								0.15	67	0.63	0.76		
G18																321.53					
FG36																18.88					
OS3					1.00											1.00	2	0.09	0.36		
OS4		0.70			8.90											9.60	9	0.15	0.40		
G16																131.26					
G06																832.70					
OS7					11.42											11.42	2	0.09	0.36		
Pond A		0.34			0.00			0.29								0.63	54	0.52	0.68		

	EAST	ONVILI	E ROAD	SEG 2				Calc'd b	y:	ę	3PC			
ヨイコ	PROP	OSED (	CONDITI	ONS				Checked	by:	СМ				
HRGreen	EL PAS		Date:		2/2/2024									
				TIME OF	F CONCE	NTRATI	ON							
BAS	BASIN DATAOVERLAND TIME $(T_i)$ TRAVEL TIME $(T_t)$ TOTAL													
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	Cv	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)			
EA1	0.68	0.22	34	2.0	3.6	20	137	1.4	2.4	1.0	5.0			
EA2	0.67	0.25	34	2.0	3.6	20	60	1.4	2.4	0.4	5.0			
EA3	0.65	0.20	34	2.0	3.8	20	126	1.4	2.4	0.9	5.0			
EA4	0.61	0.17	34	2.0	4.2	20	126	3.8	3.9	0.5	5.0			
EA5	0.08	0.16	20	2.0	6.6	20	20	33.0	11.5	0.0	6.7			
EA6	0.90	0.70	26	2.0	1.5	20	630	1.7	2.6	4.0	5.5			
EA7	0.81	0.65	24	2.0	2.1	20	630	1.7	2.6	4.0	6.1			
EA8	0.89	2.08	26	2.0	1.5	20	2500	0.7	1.7	24.9	26.4			
EA9	0.60	2.99	26	2.0	3.7	20	2500	0.7	1.7	24.9	28.6			
EA10	0.70	0.16	26	2.0	3.0	20	157	0.6	1.5	1.7	5.0			
EA11	0.63	0.15	26	2.0	3.5	20	157	0.6	1.5	1.7	5.2			
G18			· · · ·	í										
FG36			· · ·	(										
OS3	0.09	1.00	220	2.1	21.4	10	345	2.3	1.5	3.8	25.2			
OS4	0.15	9.60	153	3.1	14.8	10	1124	2.5	1.6	11.8	26.6			
G16	1		ļ	()										
G06	1		ļ	()										
OS7	0.09	11.42	200	11.6	11.6	10	675	3.4	1.8	6.1	17.7			

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

## Table 6-7. Conveyance Coefficient, $C_{\nu}$

Type of Land Surface	$C_{\nu}$
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

\* For buried riprap, select  $C_v$  value based on type of vegetative cover.



## **Grandview Reserve CLOMR Report**

## Introduction

This report was prepared by HR Green to support the submission of MT-2 forms and documents in a request for a Conditional Letter of Map Revision (CLOMR) for channel improvements along Geick Ranch Tributary 2. This request impacts the current delineation of the 100-year boundary on Flood Insurance Rate Maps (FIRMs) 08041C0552G and 08041C0556G.

Grandview Reserve is located in Falcon, Colorado within El Paso County and contains approximately 776 acres within the south half of section 21 and 22 and the north half of section 27 and 28, Township 12 South, and Range 66 West of the Sixth Principal Meridian in Ela Paso County, Colorado.

Grandview Reserve (GVR) falls within the Gieck Ranch Drainage Basin which covers approximately 22 square miles. This drainage basin is tributary to Black Squirrel Creek and joins said creek just to the south of Ellicott, CO about 18 miles to the south. Black Squirrel Creek eventually drains to the Arkansas River in Pueblo Colorado. Much of the Gieck Ranch Drainage basin is undeveloped and consists of rural farmland. The Gieck Ranch Drainage basin lies north of the Haegler Ranch drainage basin. The channels through the Grandview property can all be described as gently sloping drainages that roll through the site towards the creeks to which they are tributary.

Per the NRCS web soil survey, the site is made up entirely of Type A and B soils. The majority of which are Type B soils. The vegetation found within Grandview Reserve consists of wetland communities in the floodplain with a transitional area to shortgrass prairie communities that dominate the site. The primary species found in the shortgrass prairie regions include little bluestem, blue grama, and buffalograss. The transitional area between the wetlands and shortgrass prairie includes patches of snowberry, and wood's rose. There are a few plains cottonwoods along the main channels. The area has historically been heavily grazed and there are weeds throughout the site. Weeds found onsite include Canada thistle, Russian thistle, common mullein and yellow toadflax spp.

Observations of the existing channels suggest that they are at equilibrium with their watershed flows; evidence including relatively stable bank full channels, adequate floodplain (above bank full channel elevations) and in-tact plant communities that would be expected in this type of reach support the notion that the reach is in equilibrium.

At present, the preliminary analysis and design of Geick Ranch Tributary 2 (GRT2) has been completed. Proposed improvements for Geick Ranch Tributary 2 include refinement of the existing channel alignment and a stabilizing natural stream design that will allow a more predictable floodplain. There is to be a dedicated 100' wide corridor in which the channel valley will meander. The valley is the area needed to fully contain the 100-year event. Preliminary analysis indicates the valley will have an average width of approximately 63'; initial sizing approximates the bank full width to be 8.8' – 13.8'. The valley and channel thalweg will generally follow the same profile, with some deviation as the bank full channel meanders through the valley in turn decreasing the low flow channels average slope. The average valley profile is to be approximately 0.9% with a series of grade control structures to both decrease elevation and dissipate energy to meet natural channel criteria as outlined in El Paso County criteria.

## Hydrology

El Paso County criteria states that all developments are required to detain storm flows down to their historic peaks. For this reason GRT2 has been designed using the flows that drain to it in the existing conditions.





LINE #/ URVE#         LENGTH         RADIUS         LINE/CHORD DIRECTION         CHORD LENGTH         LINE #/ URVE#         LENGTH         RADIUS         LINE #/ LENGTH         LENGTH         RADIUS         LINE #/ LENGTH         LENGTH         RADIUS         LINE #/ URVE#         LENGTH         RADIUS         LINE #/ LENGTH         LENGTH	CHORD LENGTH 15.75 19.72 13.38 13.10
L208       1.73       M 1° 53' 24.03"E       I       C114       23.32       13.00       N21° 15' 09.13"W       20.32       C129       17.56       25.25       N18° 38' 53.36"W       17.21       C146       18.13       10.00       N34° 01' 03.83"W         C99       17.18       11.42       N1° 13' 02.63"E       15.61       L222       8.89       N72° 38' 32.69"W       18.28       C130       12.52       34.40       N9° 02' 14.74"W       12.45       L248       13.71       N1° 55' 53.54"E         L209       6.08       N41° 50' 45.40"W       I       13.58       C115       18.57       30.00       S89° 37' 21.45"W       18.28       C131       24.08       11.98       N80° 39' 48.26"W       20.23       C147       28.09       10.00       N62° 32' 31.87"W         L210       14.93       10.00       N84° 36' 57.43"W       13.58       C116       23.85       10.00       N39° 46' 52.01"W       18.59       C132       24.70       11.00       N77° 33' 02.36"W       12.48       14.66       10.00       S78° 573.811"W         L210       24.26       11.00       N72° 01' 20 89"W       18.10       1224       7.78       N28° 32' 58 51"E       1237       5.56       N10' 21' 11' 24''W       1.250       1	15.75 19.72 13.38 13.10
C99       17.18       11.42       N1° 13' 02.63"E       15.61       L222       8.89       N72° 38' 32.69"W       C130       12.52       34.40       N9° 02' 14.74"W       12.45       L248       13.71       M1° 55' 53.54"E         L209       6.08       N41° 50' 45.40"W       I       C115       18.57       30.00       S89° 37' 21.45"W       18.28       C131       24.08       11.98       N80° 39' 48.26"W       20.23       C147       28.09       10.00       N62° 32' 31.87"W         C100       14.93       10.00       N84° 36' 57.43"W       13.58       L223       10.97       S71° 53' 15.59"W       18.28       C132       24.70       11.00       N77° 33' 02.36"W       24.30       12.48       13.71       M10° 55' 53.54"E         L210       8.40       0.40       S26° 36' 50.54"W       13.58       L223       10.00       N39° 46' 52.01"W       18.59       C132       24.70       11.00       N77° 33' 02.36"W       19.83       C148       14.66       10.00       S78° 58' 38.11"W         C101       21.26       11.00       N72° 01' 20.89"W       18.29       12.24       7.78       N198° 32' 58 51"E       5.56       N118° 12' 11 74"W       12.50       11.78       N 50° 01' 48 57"W	19.72 13.38 13.10
L209       6.08       N41° 50' 45.40"W       C115       18.57       30.00       S89° 37' 21.45"W       18.28       C131       24.08       11.98       N80° 39' 48.26"W       20.23       C147       28.09       10.00       N62° 32' 31.87"W         C100       14.93       10.00       N84° 36' 57.43"W       13.58       C115       18.57       30.00       S89° 37' 21.45"W       18.28       C131       24.08       11.98       N80° 39' 48.26"W       20.23       C147       28.09       10.00       N62° 32' 31.87"W         L210       8.40       S52° 36' 50.54"W       13.58       C116       23.85       10.00       N39° 46' 52.01"W       18.59       C132       24.70       11.00       N77° 33' 02.36"W       19.83       C147       28.09       10.00       N62° 32' 31.87"W         C101       21.26       11.00       N72° 00' 20.89"W       18.10       1234       7.78       N128° 32' 58 51"E       1237       5.56       N118° 12' 12' 12' 12' 12' 12' 12' 12' 12' 12'	19.72 13.38 13.10
C100       14.93       10.00       N84° 36' 57.43"W       13.58       L223       10.97       S71° 53' 15.59"W       L       L236       10.86       S38° 07' 07.02"W       L249       9.08       S36° 59' 02.72"W         L210       8.40       S52° 36' 50.54"W       C116       23.85       10.00       N39° 46' 52.01"W       18.59       C132       24.70       11.00       N77° 33' 02.36"W       19.83       C148       14.66       10.00       S78° 58' 38.11"W         C101       21.26       11.00       N72° 00' 20.89"W       18.10       1.224       7.78       N128° 32' 58 51"E       1.237       5.56       N143° 13' 14 74"W       1.250       17.98       N150° 01' 48 57"W	13.38
L210       8.40       S52° 36' 50.54"W       C116       23.85       10.00       N39° 46' 52.01"W       18.59       C132       24.70       11.00       N77° 33' 02.36"W       19.83       C148       14.66       10.00       S78° 58' 38.11"W         C101       21.26       11.00       N72° 00' 20.89"W       18.10       1.224       7.78       N128° 32' 58 51"E       1.237       5.56       N128° 13' 11 74"W       1.250       17.98       N150° 01' 48 57"W	13.38
C101 21 26 11 00 N72° 00' 20 89"W 18 10 1 224 7 78 N28° 32' 58 51"E 1 237 5 56 N12° 13' 11 74"N/ 1 250 17 08 N50° 01' 49 57"N/	13.10
	13.10
L211 6.02 N16° 37' 32.32"W C117 33.50 12.00 N51° 25' 50.20"W 23.63 C133 6.28 10.00 N4° 46' 29.57"E 6.18 C149 14.28 10.00 N18° 08' 03.26"W	
C102       19.50       30.00       N1° 59' 34.48"E       19.16       L225       6.48       S48° 35' 21.08"W       L238       4.58       N22° 46' 10.88"E       L251       9.68       N21° 32' 16.30"E	10.00
L212       6.39       N20° 36' 40.80"E       C118       11.32       14.00       S71° 45' 22.12"W       11.02       C134       29.21       10.00       N60° 55' 11.65"W       19.88       C150       24.93       10.00       N49° 52' 37.35"W	19.90
C103       26.57       10.00       N55° 30' 50.85"W       19.42       L226       6.19       N85° 04' 36.85"W       L239       11.08       S35° 23' 25.82"W       L252       16.41       S58° 42' 29.00"W	
L213 10.38 S48° 21' 37.51"W C119 16.12 10.01 N38° 54' 34.31"W 14.43 C135 16.69 10.00 S83° 12' 10.72"W 14.82 C151 23.51 10.00 N53° 56' 30.21"W	18.46
C104       19.05       10.00       N77° 03' 24.45"W       16.30       L227       18.94       N11° 39' 57.18"E       L240       22.46       N48° 59' 05.72"W       L253       10.05       N13° 24' 30.57"E	
L214       4.49       N22° 28' 26.42"W       C120       8.87       7.66       N28° 37' 10.59"W       8.39       C136       19.46       25.00       N26° 41' 15.43"W       18.97       C152       12.41       10.00       N22° 09' 24.69"W	11.63
C105       16.30       20.00       N0° 52' 04.01"E       15.85       L228       5.88       N57° 56' 20.06"W       L241       6.51       N4° 23' 25.15"W       L254       9.00       N57° 43' 19.96"W	
L215       7.35       N24° 12' 34.43"E       C121       19.07       15.00       S85° 38' 25.55"W       17.81       C137       18.49       10.00       N57° 22' 01.09"W       15.97       C153       24.24       30.00       N80° 52' 06.53"W	23.58
C106       12.68       10.00       N12° 07' 40.58"W       11.85       L229       7.91       S49° 13' 09.23"W       L242       9.62       S69° 39' 22.97"W       L255       13.93       S77° 44' 49.86"W	
L216 4.63 N48° 27' 55.60"W C122 28.76 10.00 N48° 23' 34.94"W 19.82 C138 6.95 20.00 S59° 42' 29.37"W 6.91 C154 19.03 10.00 N39° 33' 47.95"W	16.29
C107       14.10       12.00       N82° 08' 01.06"W       13.31       L230       7.92       N33° 59' 40.88"E       L243       6.80       S49° 45' 35.79"W       L256       13.71       N14° 57' 35.33"E	
L217       7.48       S64° 11' 53.48"W       C123       27.69       10.00       N45° 19' 19.11"W       19.65       C139       26.96       10.00       N52° 59' 53.73"W       19.51       C155       16.88       10.00       N33° 23' 36.03"W	14.95
C108       5.01       30.06       S68° 58' 34.98"W       5.00       L231       6.44       S55° 21' 40.89"W       L244       8.77       N24° 14' 35.42"E	
L218       8.03       S73° 31' 44.52"W       C124       5.15       20.00       S62° 44' 22.73"W       5.14       C140       19.62       10.00       N31° 58' 39.54"W       16.62	
C109       18.41       10.00       N53° 43' 58.80"W       15.92       L232       6.17       S70° 07' 03.81"W       L245       7.77       N88° 11' 54.49"W	
L219       10.16       N0° 59' 42.13"W       C125       21.42       10.00       N48° 30' 32.07"W       17.56       C141       11.68       10.00       S58° 20' 24.97"W       11.03	
C110       6.71       8.87       N15° 30' 59.41"E       6.55       L233       6.32       N12° 51' 50.87"E       L246       4.56       S24° 52' 44.43"W	
C111       15.56       12.49       N1° 33' 53.25"E       14.58       C126       14.36       17.00       N1° 20' 32.97"W       13.94       C142       20.88       8.44       S89° 22' 23.65"W       15.95	
C112       17.28       9.02       S88° 33' 46.47"W       14.76       L234       4.96       N35° 32' 56.81"W       L247       24.22       N12° 38' 45.62"W	
L220 6.95 S36° 36' 49.17"W C127 18.28 10.00 N87° 55' 40.41"W 15.84 C143 11.75 8.95 N44° 25' 39.16"W 10.92	
C113       30.29       10.00       N56° 37' 28.74"W       19.97       L235       11.09       S39° 41' 37.22"W       C144       14.21       17.19       S72° 27' 21.39"W       13.81	
L221       10.63       N30° 08' 14.43"E       C128       18.49       10.13       N87° 52' 25.26"W       16.03       C145       17.07       24.50       S74° 40' 14.78"W       16.72	
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CONSTRUCTION DOCUMENTS TRIBUTARY 2 BANKFULL



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LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH	LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH	LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH	LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH	LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH
C156	15.76	60.71	S82° 15' 15.94"W	15.72	L267	7.77		N72° 04' 21.48"W		C180	18.49	10.13	N71° 44' 52.25"W	16.03	C191	33.50	12.00	N24° 33' 51.04"W	23.63	C202	16.30	20.00	N36° 52' 50.66"E	15.85
C157	9.19	4.73	N48° 26' 22.95"W	7.81	C168	19.62	10.00	N15° 51' 06.52"W	16.62	L63	11.09		S55° 49' 10.23"W		L74	7.78		N55° 24' 57.68"E		L85	4.49		N13° 32' 20.24"E	
L257	3.58		N3° 04' 06.31"E		L268	8.77		N40° 22' 08.43"E		C181	18.28	10.00	N71° 48' 07.40"W	15.84	C192	23.85	10.00	N12° 54' 52.85"W	18.59	C203	19.05	10.00	N41° 02' 37.80"W	16.30
C158	19.37	10.00	N58° 30' 53.78"W	16.48	C169	26.96	10.00	N36° 52' 20.72"W	19.51	L64	4.96		N19° 25' 23.80"W		L75	10.97		N81° 14' 45.25"W		L86	10.38		S84° 22' 24.17"W	
L258	14.86		S68° 36' 16.40"W		L269	6.80		S65° 53' 08.80"W		C182	14.36	17.00	N4° 47' 00.04"E	13.94	C193	18.57	30.00	N63° 30' 39.38"W	18.28	C204	26.57	10.00	N19° 30' 04.19"W	19.42
C159	24.92	10.00	N36° 46' 43.51"W	18.95	C170	6.95	20.00	S75° 50' 02.38"W	6.91	L65	6.32		N28° 59' 23.88"E		L76	8.89		N45° 46' 33.52"W		L87	6.39		N56° 37' 27.46"E	
L259	8.54		N34° 36' 24.38"E		L270	9.62		S85° 46' 55.98"W		C183	21.42	10.00	N32° 22' 59.06"W	17.56	C194	23.32	13.00	N5° 36' 50.04"E	20.32	C205	19.50	30.00	N38° 00' 21.14"E	19.16
C160	14.25	10.00	N6° 12' 38.24"W	13.07	C171	18.49	10.00	N41° 14' 28.08"W	15.97	L66	6.17		S86° 14' 36.82"W		L77	10.63		N57° 00' 13.60"E		L88	6.02		N19° 23' 14.34"E	
L260	6.03		N47° 01' 39.20"W		L271	6.51		N11° 44' 07.86"E		C184	5.15	20.00	S78° 51' 55.74"W	5.14	C195	30.29	10.00	N29° 45' 29.57"W	19.97	C206	21.26	11.00	N35° 59' 34.23"W	18.10
C161	16.43	10.00	S85° 53' 35.89"W	14.65	C172	19.46	25.00	N10° 33' 42.42"W	18.97	L67	6.44		S71° 29' 13.91"W		L78	6.95		S63° 28' 48.34"W		L89	8.40		S88° 37' 37.20"W	
L261	9.89		S38° 48' 50.97"W		L272	22.46		N32° 51' 32.70"W		C185	27.69	10.00	N29° 11' 46.10"W	19.65	C196	29.92	10.00	N30° 47' 54.08"W	19.94	C207	14.93	10.00	N48° 36' 10.78"W	13.58
C162	27.21	10.00	N63° 13' 46.48"W	19.56	C173	16.69	10.00	N80° 40' 16.27"W	14.82	L68	7.92		N50° 07' 13.89"E		L79	4.15		N54° 55' 22.26"E		L90	6.08		N5° 49' 58.75"W	
L262	6.59		N14° 43' 35.02"E		L273	11.08		S51° 30' 58.83"W		C186	28.76	10.00	N32° 16' 01.93"W	19.82	C197	6.25	18.00	N44° 58' 12.97"E	6.22	C208	19.45	13.00	N37° 02' 16.06"E	17.69
C163	6.02	20.00	N6° 06' 03.29"E	6.00	C174	29.21	10.00	N44° 47' 38.64"W	19.88	L69	7.91		S65° 20' 42.25"W		L80	10.16		N35° 01' 04.53"E		L91	6.84		N79° 54' 30.86"E	
L263	7.20		N2° 31' 29.50"W		L60	4.58		N38° 53' 43.89"E		C187	19.07	15.00	N78° 14' 01.44"W	17.81	C198	18.41	10.00	N17° 43' 12.15"W	15.92	C209	27.37	13.00	N19° 35' 19.50"E	22.59
C164	23.46	10.00	N69° 43' 47.95"W	18.44	C175	6.28	10.00	N20° 54' 02.58"E	6.18	L70	5.88		N41° 48' 47.05"W		L81	8.03		N70° 27' 28.82"W		L92	3.27		N40° 43' 51.79"W	
L264	9.75		S43° 03' 53.60"W		L61	5.56		N2° 54' 21.27"E		C188	14.23	10.00	N1° 03' 38.55"W	13.06	C199	5.01	30.06	N75° 00' 38.36"W	5.00	C210	9.28	20.00	N54° 01' 48.85"W	9.20
C165	25.51	10.26	N64° 27' 12.24"W	19.43	C176	24.70	11.00	N61° 25' 29.35"W	19.83	L71	13.81		N39° 41' 29.96"E		L82	7.48		N79° 47' 19.86"W		L93	8.27		N67° 19' 45.91"W	
L265	24.22		N3° 28' 47.39"E		L62	10.86		S54° 14' 40.03"W		C189	16.83	10.01	N10° 00' 57.74"W	14.91	C200	14.10	12.00	N46° 07' 14.40"W	13.31	C211	35.19	13.00	N10° 12' 28.14"E	25.39
C166	20.88	8.44	N74° 30' 03.34"W	15.95	C177	24.08	11.98	N64° 32' 15.25"W	20.23	L72	6.19		N58° 12' 37.69"W		L83	4.63		N12° 27' 08.94"W		L94	7.78		N87° 44' 40.12"E	
L266	4.56		S41° 00' 17.45"W		C178	12.52	34.40	N7° 05' 18.27"E	12.45	C190	11.32	14.00	N81° 22' 38.72"W	11.02	C201	12.68	10.00	N23° 53' 06.07"E	11.85	C212	23.02	10.00	N21° 47' 21.49"E	18.26
C167	11.68	10.00	S74° 27' 57.98"W	11.03	C179	17.56	25.25	N2° 31' 20.35"W	17.21	L73	6.48		S75° 27' 20.25"W		L84	7.35		N60° 13' 21.09"E						
			-				•		•					•										
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CONSTRUCTION DOCUMENTS TRIBUTARY 2 BANKFULL GRADING



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UPSTREAMImage: CHORD LENGTHLINE #/ CURVE#LENGTHRADIUSLNE/CHORD DIRECTIONCHORD DIRECTIONLINE #/ CURVE#LENGTHRADIUSLNE/CHORD DIRECTIONN77° 32' 29.10"WImage: Chord Image: Chord Im	CHORE LENGTH 14.99 13.76
LNE/CHORD DIRECTIONCHORD LENGTHLINE #/ CURVE#LENGTHRADIUSLNE/CHORD DIRECTIONCHORD LENGTHLINE #/ CURVE#LENGTHRADIUSLNE/CHORD DIRECTIONN77° 32' 29.10"WLL1277.41N16° 10' 58.09"WL15227.44N26° 46' 26.58"WN38° 36' 17.81"W12.57C24718.3815.00N18° 55' 33.27"E17.25C25816.9510.00N21° 46' 36.50"EN0° 19' 53.48"EL1286.36N54° 02' 04.63"EL1383.84N70° 19' 39.57"E	CHORE LENGTF 14.99 13.76
N77° 32' 29.10"W         L127         7.41         N16° 10' 58.09"W         L152         27.44         N26° 46' 26.58"W           N38° 36' 17.81"W         12.57         C247         18.38         15.00         N18° 55' 33.27"E         17.25         C258         16.95         10.00         N21° 46' 36.50"E           N0° 19' 53.48"E         L128         6.36         N54° 02' 04.63"E         L138         3.84         N70° 19' 39.57"E	14.99 13.76
N38° 36' 17.81"W         12.57         C247         18.38         15.00         N18° 55' 33.27"E         17.25         C258         16.95         10.00         N21° 46' 36.50"E           N0° 19' 53.48"E         L128         6.36         N54° 02' 04.63"E         L138         3.84         N70° 19' 39.57"E	14.99 13.76
N0° 19' 53.48"E         L128         6.36         N54° 02' 04.63"E         L138         3.84         N70° 19' 39.57"E	13.76
	13.76
N40° 09' 12.75"E         15.37         C248         9.39         20.00         N40° 35' 03.09"E         9.30         C259         14.65         12.00         N35° 21' 09.72"E	
N79° 58' 33.23"E         L129         7.15         N27° 08' 01.54"E         L139         16.46         N0° 22' 41.14"E	
N27° 44' 22.92"E 18.97 C249 20.51 10.00 N31° 37' 14.85"W 17.10	
N24° 29' 46.28"W L130 9.76 S89° 37' 28.76"W	
N38° 08' 52.11"W 11.80 C250 27.90 10.00 N10° 27' 09.67"W 19.69	
N51° 47' 57.21"W L131 11.50 N69° 28' 12.96"E	
N1° 49' 28.09"E 22.51 C251 17.33 12.00 N28° 06' 25.18"E 15.86	
N66° 02' 17.32"E L132 8.67 N13° 15' 22.59"W	
N29° 12' 46.81"E 9.14 C252 9.13 10.00 N39° 24' 31.73"W 8.82	
N2° 00' 28.98"E L133 17.18 N77° 27' 43.71"W	
N33° 43' 31.88"W 29.20 C253 25.62 10.00 N9° 01' 06.61"E 19.17	
N69° 27' 32.74"W L134 9.39 N82° 24' 48.02"E	
N3° 49' 59.88"E 19.16 C254 26.62 10.00 N6° 09' 26.70"E 19.43	
N77° 07' 32.51"E L135 4.72 N70° 05' 54.62"W	
N40° 39' 52.64"E 11.89 C255 2.40 10.00 N76° 59' 14.73"W 2.40	
N4° 12' 10.94"E L136 7.28 N83° 52' 34.84"W	
N42° 20' 24.85"W 14.52 C256 28.51 10.00 N2° 12' 50.31"W 19.79	
N88° 53' 00.63"W L137 0.10 N79° 26' 54.22"E	
N52° 31' 59.36"W 11.85 C257 18.54 10.00 N26° 20' 13.82"E 16.00	



FALCON, COLORADO

SHEET		
SR18	22	



TRIBUTARY 2 UPSTREAM										
LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH						
C260	14.80	12.00	N34° 56' 39.85"W	13.88						
L140	10.77		N70° 15' 59.85"W							
C261	44.55	20.00	N6° 27' 33.85"W	35.89						
L141	8.98		N57° 20' 52.15"E							
C262	29.24	18.00	N10° 48' 15.97"E	26.13						
L142	16.23		N45° 31' 56.12"W							
C263	24.34	11.44	N9° 01' 06.38"E	20.00						
L143	11.94		N74° 50' 42.15"E							
C264	31.22	12.00	N0° 18' 44.36"E	23.13						
L144	8.82		N74° 13' 13.43"W							
C265	27.28	14.00	N18° 24' 07.71"W	23.16						
L145	7.63		N38° 57' 54.40"E							
C266	5.69	10.00	N55° 15' 07.16"E	5.61						
L146	6.73		N71° 32' 18.85"E							
C267	53.21	20.40	N5° 38' 58.70"E	39.35						
L147	5.41		N68° 39' 59.99"W							
C268	14.28	10.00	N27° 44' 59.82"W	13.10						
L148	4.50		N13° 10' 00.36"E							
C269	13.50	10.00	N51° 50' 51.43"E	12.50						
L149	10.57		S89° 28' 17.51"E							
C270	27.53	10.00	N11° 39' 24.20"E	19.62						

TRIBUTARY 2 UPSTREAM											
LINE #/ CURVE#	LENGTH	RADIUS	LNE/CHORD DIRECTION	CHORD LENGTH							
L150	7.19		N67° 12' 54.10"W								
C271	24.50	15.00	N20° 25' 45.98"W	21.86							
C272	14.98	18.00	N2° 31' 05.79"E	14.55							
L151	3.20		N21° 19' 11.62"W								

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CONSTRUCTION DOCUMENTS

TRIBUTARY 2 BANKFULL GRADING

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6918	00 5, 6920 00, 00, 00, 00, 00, 00, 00, 00, 00, 0	6921 (C)	6920 6920 4) 8' X 4' BO EE PP5 7269	DX CULVER 77+00000000	90400 975. 9052	6926	69 70×00 60	66029	6930		15+0	0 6930	6933	- 6933					6935 6935	
PVI STA = 10+32.43	PVI ELEV = 6921.46 PVI STA = 10+42.43 PVI ELEV = 6921.46 PVI STA = 10+67.43	PVI ELEV = 6923.96															/ 	//	TER -	
D+00	PRO	3.00' (TÝP) 10:00% POSED CI	) HANNEL TH	IALWEG	TING GR	ADE 	15+	 16+(	0.9	0%	18	+00	19+	+00	20+(		21+	-00	22	+00
		HRG	reen FA	R GREEN - 513 DTC PA ENVER CO HONE: 720 AX: 713.965	DENVE ARKWAY 80111 .602.499 5.0044	R ' SUITE 950 9			GRAN DR H FALCO	DVIEW ORTOI	<b>RES</b> N ORADC	ERVI	E							





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7010	PROPOS	S WEILANDS - ISDICTIONAL	RAIL
7000         6990         6980         0.91%         6980         6970         6960         6950         6950         6940         6930         6930         6930	<ul> <li>NOTES:</li> <li>1. BASIS OF BEARINGS: THE BEING MONUMENTED AT IBY A 3-1/4" ALUMINUM SUU "PS INC PLS 30087 1996", FMARKED, AND BEING MORTHEAST CORNER BY SURVEYOR'S CAP STAMP BEING APPROPRIATELY M TO BEAR NORTH 00 DEGR SECONDS WEST, A DISTA</li> <li>2. BENCHMARK: DESIGNATION = F 24 PID = JK0240 DESCRIPTION = DISK ON MONUMENT CONTROL POINT COORDINAVD88 NORTHING: 1421049.80 EASTING: 3273631.55 ELEVATION: 6866.33</li> <li>3. ALIGNMENT NOT FOR USE TO NORTHINGS AND EAST</li> <li>4. PLAN SET APPROVAL APP CONSTRUCTION. PLEASE NUMBER 1 PLAN SET FOR CHANNEL LIMITS OF CONS (AREA SOUTH OF TRIBUT/ CONSTRUCTED WITH FILL TRIBUTARY 1 TO BE CONS (AREA SOUTH OF TRIBUT/ CONSTRUCTED WITH FILL TRIBUTARY 1 AND SOUTH BOX CULVERTS/CROSSIN BE CONSTRUCTED WITH FILL AND AND AND AND AND AND AND AND AND AND</li></ul>	EAST LINE OF SECT THE SOUTHEAST CC RVEYOR'S CAP STAN BEING APPROPRIATE UMENTED AT THE A 3-1/4" ALUMINUM ED "PS INC PLS 3008 MRKED, BEING ASSI REES 52 MINUTES 26 NCE OF 5290.17 FEE NOT OF CONCRETE NATE SYSTEM: E IN CONSTRUCTION TINGS PLIES TO THE LIMITS SEE GRANDVIEW FI GRADING OUTSIDE STRUCTED WITH FILL ARY 1), TRIBUTARY 2 NG 2 (AREA NORTH WEST OF TRIBUTAR GS ALONG TRIBUTAR GS ALONG TRIBUTAR GS ALONG TRIBUTAR GS ALONG TRIBUTAR STRUCTED WITH FILL ARY 1), TRIBUTARY 2 NG 2 (AREA NORTH WEST OF TRIBUTAR GS ALONG TRI	ION 21, PRNER APED ELY 7 1996", JMED T. T. I. REFER OF LING OF THE NG 1 2 TO BE OF Y 2), RY 2 TO SMEALTS. 10 5
DRAINAGE TRIBUTARY 2 PLAN	AND PROFILE	PP3	32









![](_page_69_Picture_1.jpeg)

![](_page_69_Figure_2.jpeg)

![](_page_70_Figure_0.jpeg)

![](_page_70_Figure_2.jpeg)

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## **REX ROAD CULVERT CROSSING**

![](_page_70_Picture_6.jpeg)

HR GREEN - DENVER 5613 DTC PARKWAY SUITE 950 DENVER CO 80111 PHONE: 720.602.4999 HRGreen FAX: 713.965.0044

GRANDVIEW RESERVE DR HORTON FALCON, COLORADO

![](_page_70_Figure_9.jpeg)

![](_page_71_Figure_0.jpeg)

![](_page_71_Figure_5.jpeg)

![](_page_71_Figure_6.jpeg)

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![](_page_71_Figure_7.jpeg)

![](_page_71_Figure_9.jpeg)


















DRAWN BY: TBI APPROVED: GLP CAD DATE: 11/30/2023





Grandview Reserve Phase 2 Preliminary Drainage Report Project No.: 201662.202

**APPENDIX F – DRAINAGE MAPS** 



		5 Year Pre	100 Year Pre
Basin	Design Point	Devlopment	Development
A1	10	13.03	66.80
B1	20	4.33	48.76
B2	21	1.66	20.74
	22	11.85	140.35
	23	5.99	68.56
B3	24	21.23	249.20
C1	30	9.95	110.70
	31	9.95	110.70
D1	40	8.12	40.00
D2	41	22.23	114.87
	42	8.12	40.00
E1	50	32.34	157.99
	51	93.34	374.99
F1	60	9.70	49.45
F2	61	16.46	86.73
F3	62	3.65	18.42
F4	63	12.98	67.82
	64	13.35	67.87
	65	26.04	135.62

	66	16.46	86.73
	67	231.47	864.52
G1	70	5.57	28.46
G2	71	3.87	20.06
	72	3.87	20.06
	73	3.87	20.06
	74	189.42	643.48
H1	80	1.85	21.89
H2	81	5.37	27.12
H3	82	1.92	9.51
H4	83	8.07	40.86
	84	7.22	49.01
	85	1.92	9.51
OS1	OS1	67.00	413.00
OS2	OS2	59.00	280.00
OS3	OS3	61.00	217.00
OS4	OS4	180.00	595.00
	Outfall1	80.03	479.80
	Outfall2	85.96	597.41
	Outfall3	30.00	154.35
	Outfall4	341.05	1335.77



## V3\_Drainage Report.pdf Markup Summary

Highlight (12)		
for medium density of 43.26% and run Subbasin B3 is loc existing MST2 trib towards Detention	Subject: Highlight Page Label: 21 Author: cmarshall Date: 2/14/2024 2:53:33 PM Status: Color: Layer: Space:	
<ul> <li>impervious value respectively.</li> <li>Subbasin C1 is lo through the middle Pond C. Current</li> </ul>	Subject: Highlight Page Label: 21 Author: cmarshall Date: 2/14/2024 2:53:37 PM Status: Color: Layer: Space:	
<u>B2</u> B3	Subject: Highlight Page Label: 22 Author: cmarshall Date: 2/14/2024 2:54:23 PM Status: Color: Layer: Space:	B3
B2 B3	Subject: Highlight Page Label: 22 Author: cmarshall Date: 2/14/2024 2:54:29 PM Status: Color: Layer: Space:	
<u>C1</u>	Subject: Highlight Page Label: 22 Author: cmarshall Date: 2/14/2024 2:54:31 PM Status: Color: Layer: Space:	
<ul> <li>Be allered witch of classes is re- ary preengive check structures, m- of the existing berm.</li> <li>Main Stem Triblargy C</li> <li>Mittl concess Fastownile and via 1 detection. Portions of this channel and Per a Juy email from the USACE to jurisdictional waters/wetland.</li> </ul>	Subject: Highlight Page Label: 23 Author: cmarshall Date: 2/14/2024 2:55:12 PM Status: Color: Layer: Space:	

	Cristian de Lindelinde
some deviation as the banktu channels average slope. The	
control structures to both dec	Page Label: 23
outline in El Paso County criti	Author: cmarchall
East Fork Tributary	
The East Fork tributary (EFT) a natural channel. The chann	Date: 2/14/2024 2:55:15 PM
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EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer:
EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space:
EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space:
EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space:
EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space:
EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space:
EA5 EA6 EA7 EA8 EA5	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 33
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EA5 EA6 EA7 EA8 EA5 EA6 EA6	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 33 Author: khuhn
EA5 EA6 EA7 EA8 EA5 EA5 EA6 EA7	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 33 Author: khuhn Date: 3/8/2024 3:13:12 PM
EA5 EA6 EA7 EA8 EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 33 Author: khuhn Date: 3/8/2024 3:13:12 PM Status:
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EA5 EA6 EA7 EA8 EA8 EA5 EA6 EA7 EA8	Subject: Highlight Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:16 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 33 Author: khuhn Date: 3/8/2024 3:13:12 PM Status: Color: Layer: Space:

## Rectangle (8)

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	Subject: Rectangle Page Label: 21 Author: cmarshall Date: 2/14/2024 2:53:53 PM Status: Color: Color: Space:
	Subject: Rectangle Page Label: 22 Author: cmarshall Date: 2/14/2024 2:55:00 PM Status: Color: Color: Color: Space:
<text></text>	Subject: Rectangle Page Label: 24 Author: sean.callahan Date: 3/4/2024 1:52:58 PM Status: Color: Layer: Space:
	Subject: Rectangle Page Label: 30 Author: khuhn Date: 3/8/2024 1:35:42 PM Status: Color: Layer: Space:
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	Subject: Rectangle Page Label: 32 Author: khuhn Date: 3/8/2024 3:12:09 PM Status: Color: Layer: Space:

	Subject: Rectangle Page Label: 33 Author: khuhn Date: 3/8/2024 3:13:10 PM Status: Color: Layer: Space: Subject: Rectangle Page Label: 34 Author: khuhn Date: 3/8/2024 3:19:33 PM Status: Color: Layer: Space:	
Snapshot (2)		
LAND LISE LOW DOISTY HIGH DOISTY HIGH DOISTY HIGH DOISTY CANON A CLAMENTAY SOOD COMMENTY PARK	Subject: Snapshot Page Label: [4] 00-Drainage Basins-DR5 Author: chris.walton Date: 7/15/2024 10:23:11 AM Status: Color: Layer: Space:	
	Subject: Snapshot Page Label: [9] 00-Drainage Basins-DR10 Author: chris.walton Date: 7/15/2024 10:23:29 AM Status: Color: Layer: Space:	
Text Box (3)		
Only relevant sheets from this report provided	Subject: Text Box Page Label: 20 Author: khuhn Date: 3/8/2024 1:34:12 PM Status: Color: Layer: Space:	Only relevant sheets from this report provided
Only relevant sheets from this report provided Load – Londonderry Dr. to priment 2 Improvements	Subject: Text Box Page Label: 29 Author: khuhn Date: 3/8/2024 1:34:42 PM Status: Color: Layer: Space:	Only relevant sheets from this report provided



Subject: Text Box Page Label: [1] EX1 Author: Bret Date: 9/11/2024 1:11:03 PM Status: Color: Layer: Space:

Response acknowledged, however, please provide an existing drainage map, specifically for Phase 2. Include design points that will correspond to pond release locations, so historic flows can be compared to pond release rates.

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