

**Final Drainage Plan,  
Cherry Creek Crossing Filing No. 1 Lot 111  
El Paso County, Colorado**

Prepared for:  
Colorado Highway 382 Limited Partnership  
6070 North Camino Almonte  
Tucson, Arizona 85718

Prepared by:  
**Kiowa**  
Engineering Corporation  

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1604 South 21st Street  
Colorado Springs, Colorado 80904  
(719) 630-7342

Kiowa Project No. 14028  
August 3, 2017  
Revised September 20, 2017  
Revised July 19, 2018

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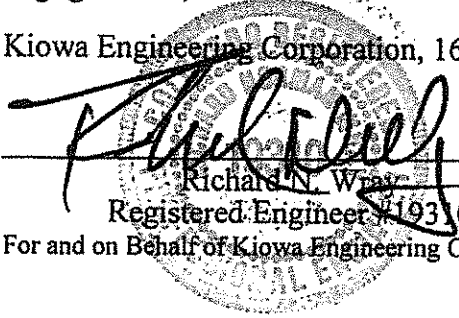
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### Appendix A – Hydraulic Calculations

**Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Kiowa Engineering Corporation, 1604 South 21<sup>st</sup> Street, Colorado Springs, Colorado 80904

  
Richard N. Wray  
Registered Engineer #19310  
For and on Behalf of Kiowa Engineering Corporation

8/3/18  
Date

**Developer's Statement:**

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Ibex Advisors, LLC, General Partner

BY: Nathan K. Miller, Managing Member 8/24/18  
Date

Nathan K. Miller  
Printed

ADDRESS: Colorado Springs Highway 382 Limited Partnership  
6070 North Camino Almonte  
Tucson, Arizona 85718

**El Paso County:**

Filed in accordance with the requirements of the Drainage Criteria Manual Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code, as amended.

Jennifer Irvine, P.E.  
County Engineer/ECM Administrator

                      
Date

## **I. General Location and Description of Project**

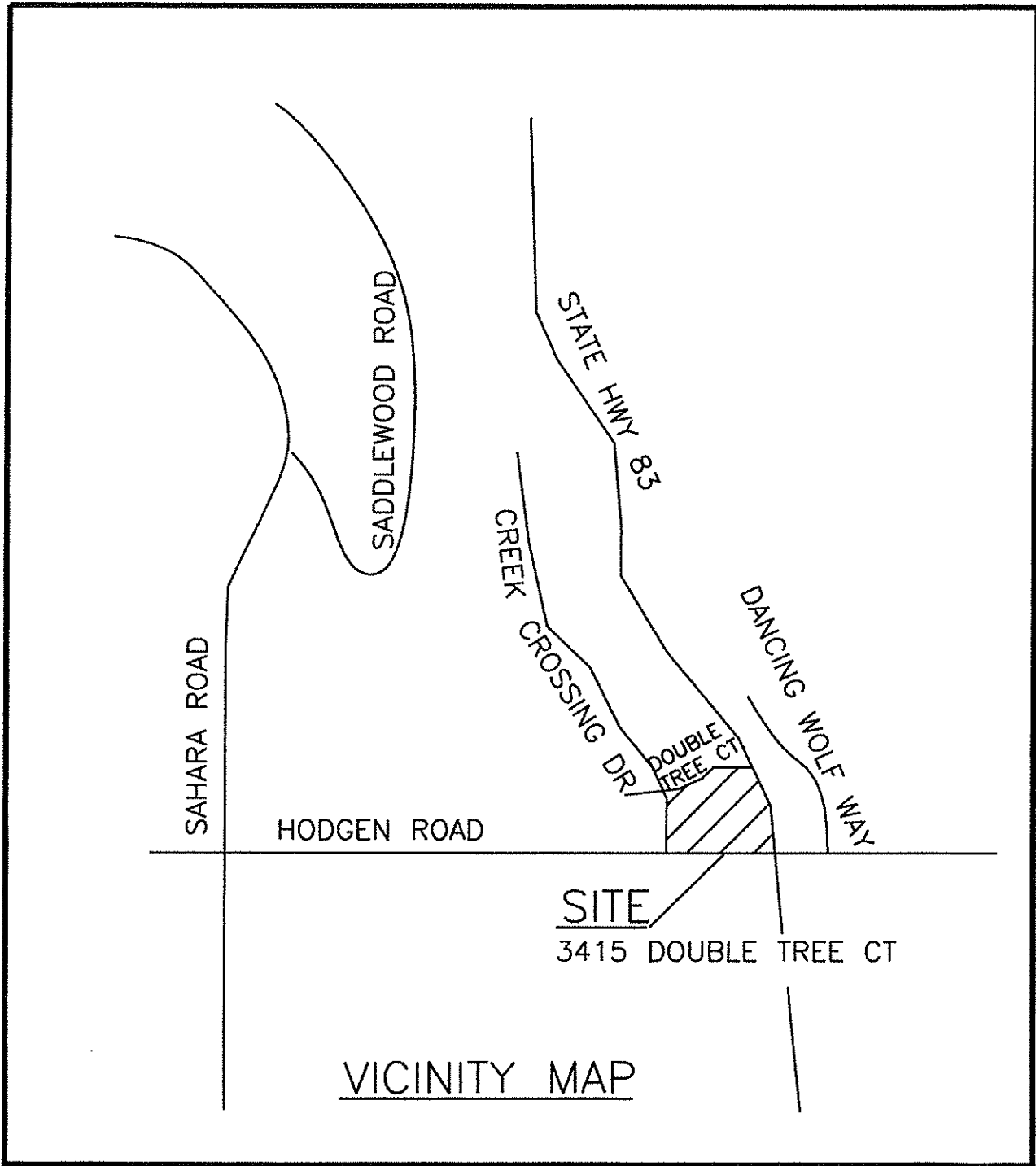
Cherry Creek Crossing Filing No. 1 is a platted subdivision in northern El Paso County that consists of 53 single family lots ranging in size from 2.5 to 5 acres, and one 8-acre commercial lot. The commercial lot, Lot 111, is located at the northwest corner of State Highway 83 and Hodgen Road. The owner of Lot 111 is proposing to carry out overlot grading in anticipation of a commercial use being established on the lot. The location of Lot 111 is shown on Figure 1.

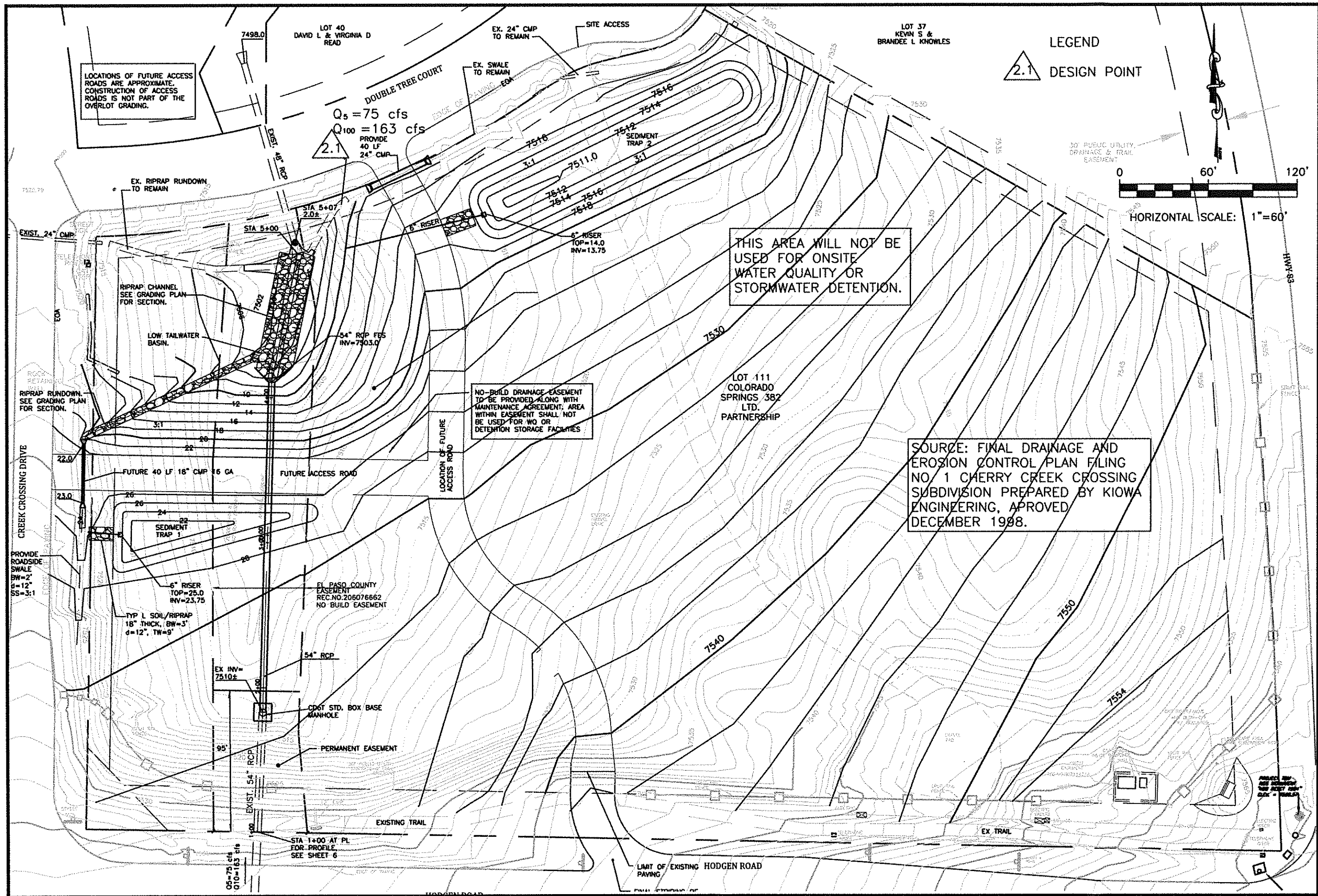
The final drainage report for Filing No. 1 was approved by the County in 1998. Since that time the single-family lots have all been developed while Lot 111 has remains undeveloped. The public roadways that serve the subdivision have all been built and are currently maintained by the County. An overlot grading and erosion control plan has been prepared to show the extent of grading that is proposed for Lot 111. In addition to the overlot grading operations, the existing 54-inch reinforced concrete pipe presently maintained by the County that conveys runoff from offsite watersheds into Lot 111 is proposed for extension approximately 200 feet to the north. The proposed extension to this culvert is shown on Figure 2. When Filing 1 was platted, a drainage, floodplain and no-build easement was shown. This easement was created for access to the drainageway for the purposes of maintenance by the individual property owner. The County has a dedicated permanent easement that extends into the property 95-feet from the Hodgen Road right-of-way for the purposes of maintenance access to the 54-inch RCP that was extended when Hodgen Road was widened. These easements are shown on Figure 2.

Prior to the final development of Lot 111 a site plan will have to be provided to the County for review and approval per the requirements of the approved development plan for Cherry Creek Crossing. A specific use has not been identified for Lot 111. It is anticipated that onsite drainage facilities as well as water quality storage will be installed at that time. There are no stormwater detention or water quality facilities proposed for construction as part of the overlot grading. Permanent water quality measures will be installed when the site is developed into its final use. Permanent water quality measures such as water quality storage basins will not be placed in the area bounded by Double Tree Court, Cherry Crossing Road and the future access drives shown on Figure 2. A temporary sediment basin will be installed as part of the overlot grading work.

## **II. Hydrology**

Onsite and offsite hydrology for Cherry Creek Crossing Filing 1 used to size the drainage facilities within the subdivision is summarized in the Filing 1 final drainage report. The hydrology work map from the Filing 1 final drainage plan showing the location of Lot 111 has been included within Appendix A. The overlot grading and eventual revegetation efforts will cause no change in the existing condition rates of runoff for Lot 111. The peak flow rates that are carried into the site by the existing 54-inch RCP under Hodgen Road are shown on Figure 2.





CHERRY CREEK CROSSING, FILING NO. 1 LOT 111  
AMENDED FINAL DRAINAGE PLAN

EL PASO COUNTY, COLORADO

Project No.:	14028
Date:	JULY 27, 2018
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	

FIG.2

### **III. Hydraulic Calculations**

The hydraulic capacity of the existing 48-inch CMP under Hodgen Road has been verified in its as-built condition. A field survey was conducted in 2014 whereby the as-built invert of the 54-inch RCP under Hodgen Road as well as for the 48-inch CMP culvert under Double Tree Court were confirmed. The overlot grading as proposed would not affect the culvert under Double Tree Court. The hydraulic capacity of the 54-inch RCP under Hodgen Road extended as shown on Figure 2 was reverified. Based upon the hydraulic calculations, extending the 54-inch into the site will not affect the hydraulic capacity of the culvert. The headwater-to-depth ratio is unchanged between the existing and extended condition. The culvert calculations have been included in Appendix A.

The outlet of the 54-inch will be stabilized by means of a standard CDOT headwall and wingwall. Due to the high outlet velocity in the 100-year condition (17.2 feet per second), and the anticipated super-critical flow condition, a low tailwater basin has been designed per UDFCD Volume 2. Based on the calculations a Type M soil/riprap low tailwater basin is required.

The present outlet condition of the 48-inch CMP under Double Tree Court was field checked and found to be stable and free of any scouring. The installation of the 54-inch RCP through Lot 111 will not affect the outlet hydraulics of the existing 48-inch CMP under Double Tree Court as this culvert functions under inlet control conditions.

### **IV. Floodplain Statement**

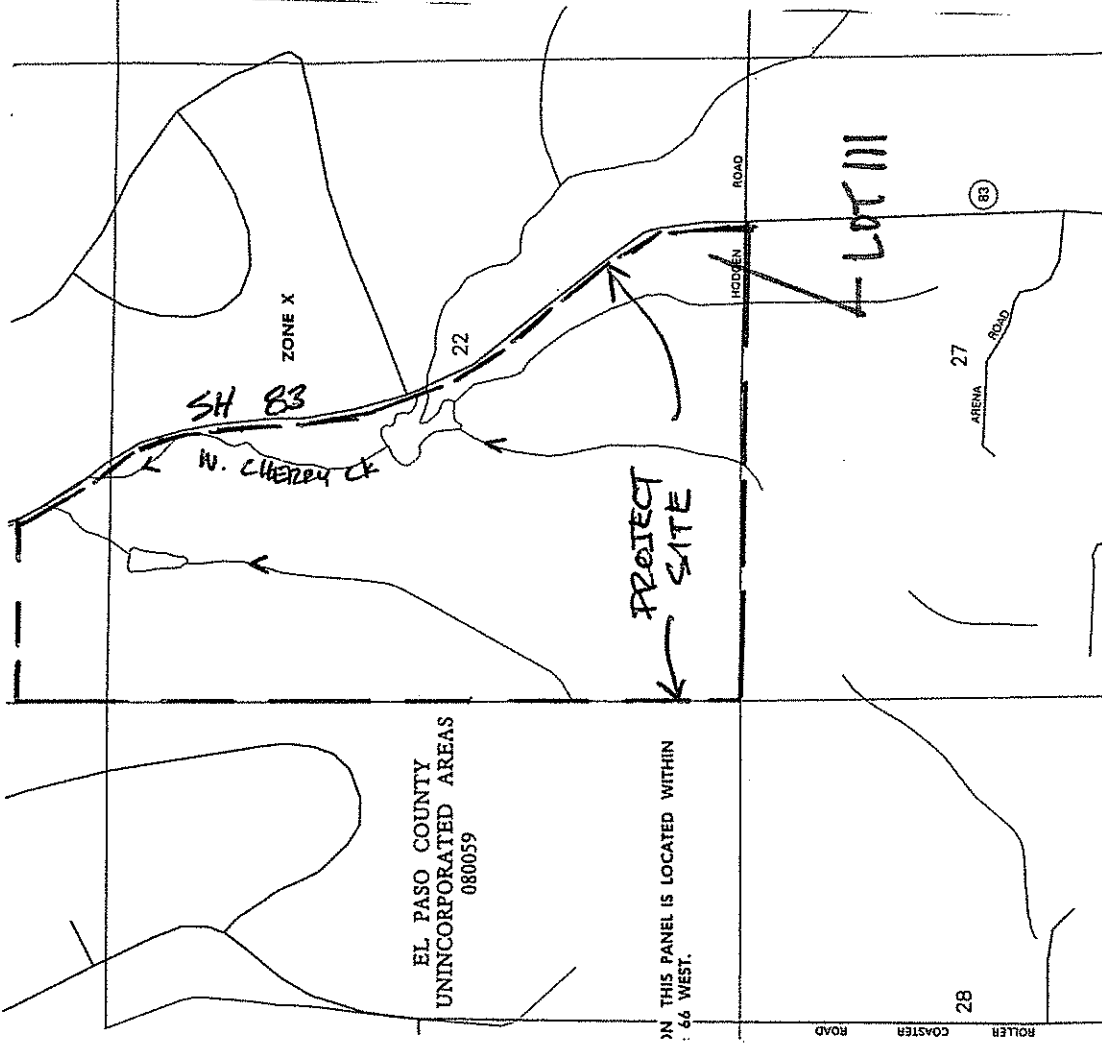
The Floodplain Insurance Rate Map (FIRM) for El Paso County Flood Insurance Study (FIS) panel 285 was reviewed to determine any potential regulatory floodplains within Lot 111. There is no land within the Filing 1 subdivision that is located within a 100-year floodplain as delineated in the FIS. A copy of the relevant portion of FIRM panel 285F is shown on Figure 3.

### **V. Drainage and Bridge Fees**

Drainage and bridge fees for Filing No.1 were determined in the Filing No. 1 final drainage report. The drainage and bridge fees were paid with the development of Filing 1. Therefore, there are no fees due for Lot 111.

### **VI. Economic Analysis**

Summarized on Table 1 is the cost estimate for the extension of the 54-inch culvert through Lot 111.



**NATIONAL FLOOD INSURANCE PROGRAM**

**FIRM**

**FLOOD INSURANCE RATE MAP**

**EL PASO COUNTY, COLORADO AND INCORPORATED AREAS**

**PANEL 285 OF 1300**  
(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:	NUMBER	PANEL	SUFFIX
EL PASO COUNTY, UNINCORPORATED AREAS	080059	0285	F

**MAP NUMBER 08041C0285 F**

**EFFECTIVE DATE: MARCH 17, 1997**

**Federal Emergency Management Agency**

**FIGURE 3**  
**NO SCALE**



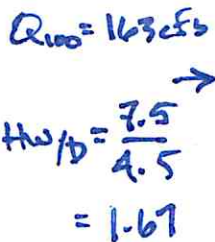
**Appendix A**  
**Hydraulic Calculations**

**TABLE 1: CHERRY CREEK CROSSING FILING 1 LOT 111**  
**DRAINAGE IMPROVEMENT COST ESTIMATE**  
**KIOWA PROJECT NUMBER 14028**

ITEM	UNIT COST	UNIT	QUANTITY	TOTAL
<b>PUBLIC DRAINAGE FACILITIES</b>				
54-INCH RCP	\$225	LF	215	\$48,375
CDoT std headwall/wingwall	\$5,000	EA	1	\$5,000
BOX BASE MANHOLE	\$7,500	EA	1	\$7,500
TYPE L SOIL/RIPRAP RUNDOWN	\$70	CY	50	\$3,500
TYPE M SOIL/RIPRAP	\$85	CY	160	\$13,600
SUBTOTAL				\$77,975.00
CONTINGENCY (5 %)				\$3,898.75
ENGINEERING (10 %)				\$7,797.50
<b>TOTAL</b>				<b>\$89,671.25</b>

**Appendix A**  
**Hydraulic Calculations**

Project: 14028 Cherry Creek Crossing Filing No. 1, Lot 111  
Basin ID: Hodgen Road culvert existing conditions  
Status:



## HY-8 Culvert Analysis Report

54" CULVERT EXTENSION

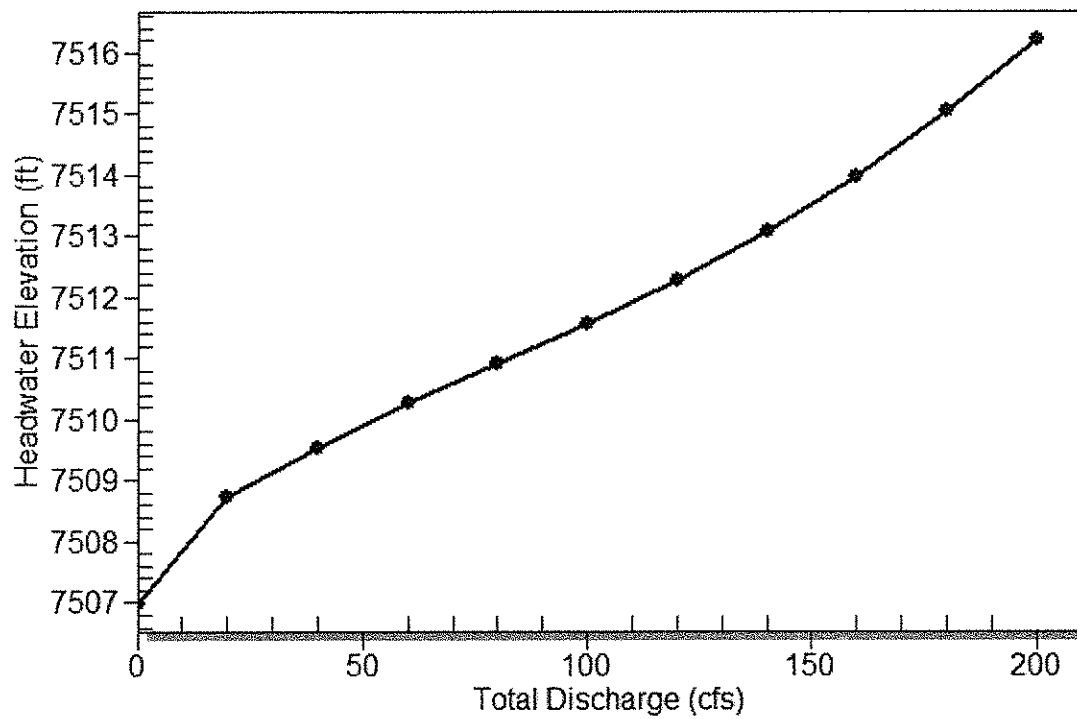
**Table 1 - Summary of Culvert Flows at Crossing: 54-inch rcp**

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
7507.00	0.00	0.00	0.00	1
7508.72	20.00	20.00	0.00	1
7509.55	40.00	40.00	0.00	1
7510.28	60.00	60.00	0.00	1
7510.93	80.00	80.00	0.00	1
7511.57	100.00	100.00	0.00	1
7512.26	120.00	120.00	0.00	1
7513.06	140.00	140.00	0.00	1
7513.97	160.00	160.00	0.00	1
7515.03	180.00	180.00	0.00	1
7516.22	200.00	200.00	0.00	1
7534.00	383.98	383.98	0.00	Overtopping

Rating Curve Plot for Crossing: 54-inch rcp

### Total Rating Curve

Crossing: 54-inch rcp



**Table 2 - Culvert Summary Table: Culvert 1**

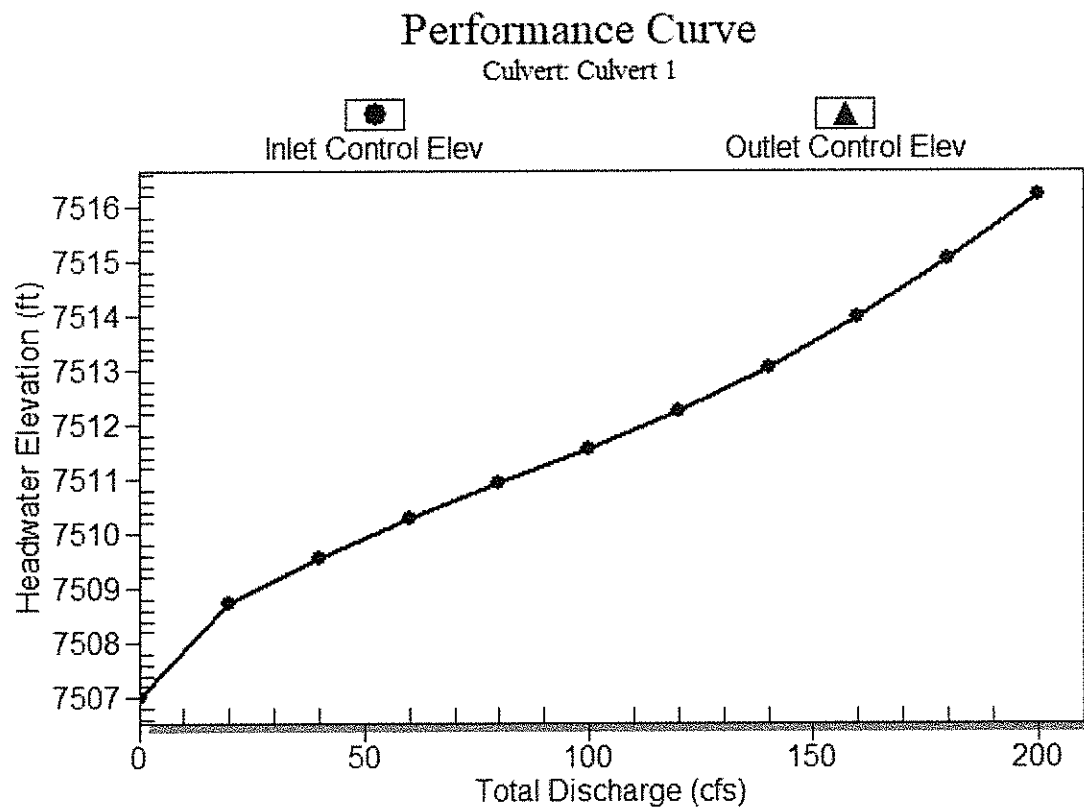
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	7507.00	0.000	0.0*	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
20.00	20.00	7508.72	1.721	0.0*	1-S2n	0.786	1.260	0.800	0.446	10.287	3.956
40.00	40.00	7509.55	2.547	0.0*	1-S2n	1.124	1.819	1.141	0.666	12.500	5.008
60.00	60.00	7510.28	3.282	0.0*	1-S2n	1.402	2.250	1.409	0.838	14.062	5.718
80.00	80.00	7510.93	3.928	0.0*	1-S2n	1.628	2.610	1.630	0.985	15.346	6.266
100.00	100.00	7511.57	4.568	0.0*	5-S2n	1.846	2.928	1.854	1.116	16.176	6.717
120.00	120.00	7512.26	5.263	0.0*	5-S2n	2.041	3.218	2.148	1.233	16.012	7.103
140.00	140.00	7513.06	6.056	0.0*	5-S2n	2.237	3.467	2.361	1.342	16.571	7.441
160.00	160.00	7513.97	6.972	0.0*	5-S2n	2.423	3.682	2.568	1.442	17.072	7.744
180.00	180.00	7515.03	8.025	0.0*	5-S2n	2.608	3.856	2.771	1.537	17.528	8.018
200.00	200.00	7516.22	9.219	0.0*	5-S2n	2.797	4.031	2.975	1.626	17.950	8.270



\* theoretical depth is impractical. Depth reported is corrected.

```
*****  
Inlet Elevation (invert): 7507.00 ft,   Outlet Elevation (invert): 7503.00 ft  
Culvert Length: 228.04 ft,   Culvert Slope: 0.0175  
*****
```

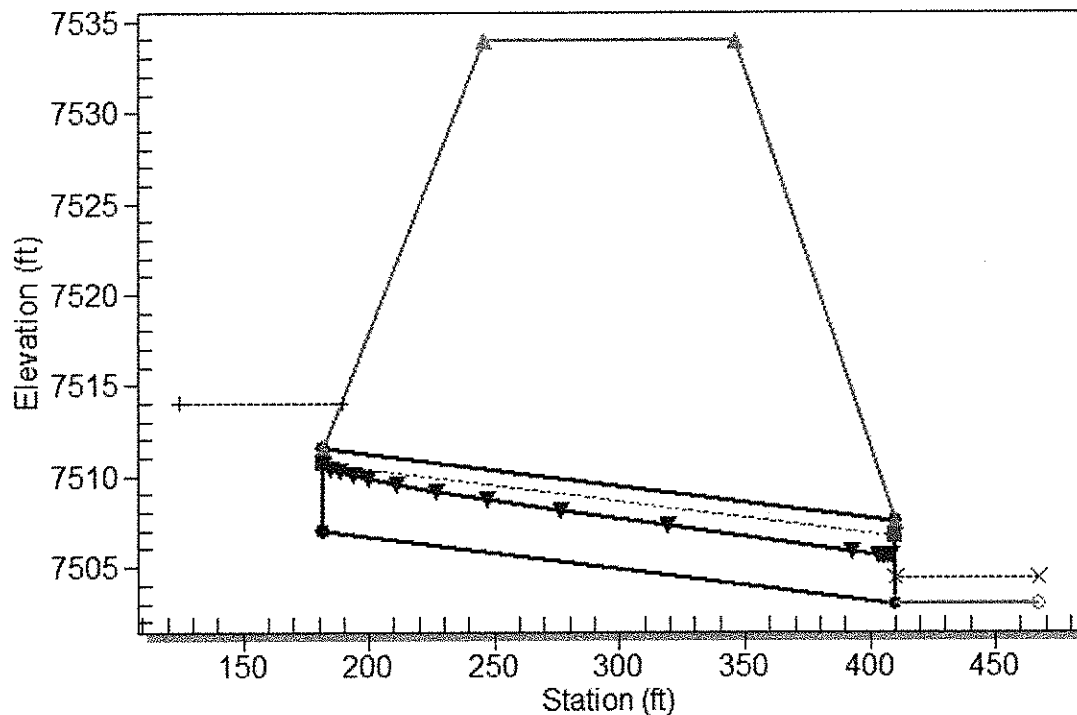
# Culvert Performance Curve Plot: Culvert 1



## Water Surface Profile Plot for Culvert: Culvert 1

Crossing - 54-inch rcp, Design Discharge - 160.0 cfs

Culvert - Culvert 1, Culvert Discharge - 160.0 cfs



### Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 182.00 ft

Inlet Elevation: 7507.00 ft

Outlet Station: 410.00 ft

Outlet Elevation: 7503.00 ft

Number of Barrels: 1

### Culvert Data Summary - Culvert 1

Barrel Shape: Circular

Barrel Diameter: 4.50 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Inlet Type: Conventional

Inlet Edge Condition: Square Edge with Headwall

Inlet Depression: NONE

**Table 3 - Downstream Channel Rating Curve (Crossing: 54-inch rcp)**

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	7503.00	0.00	0.00	0.00	0.00
20.00	7503.45	0.45	3.96	0.83	1.10
40.00	7503.67	0.67	5.01	1.25	1.17
60.00	7503.84	0.84	5.72	1.57	1.21
80.00	7503.99	0.99	6.27	1.84	1.23
100.00	7504.12	1.12	6.72	2.09	1.25
120.00	7504.23	1.23	7.10	2.31	1.27
140.00	7504.34	1.34	7.44	2.51	1.28
160.00	7504.44	1.44	7.74	2.70	1.30
180.00	7504.54	1.54	8.02	2.88	1.31
200.00	7504.63	1.63	8.27	3.04	1.32

**Tailwater Channel Data - 54-inch rcp**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 10.00 ft

Side Slope (H:V): 3.00 (1:1)

Channel Slope: 0.0300

Channel Manning's n: 0.0350

Channel Invert Elevation: 7503.00 ft

**Roadway Data for Crossing: 54-inch rcp**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft

Crest Elevation: 7534.00 ft

Roadway Surface: Paved

Roadway Top Width: 100.00 ft

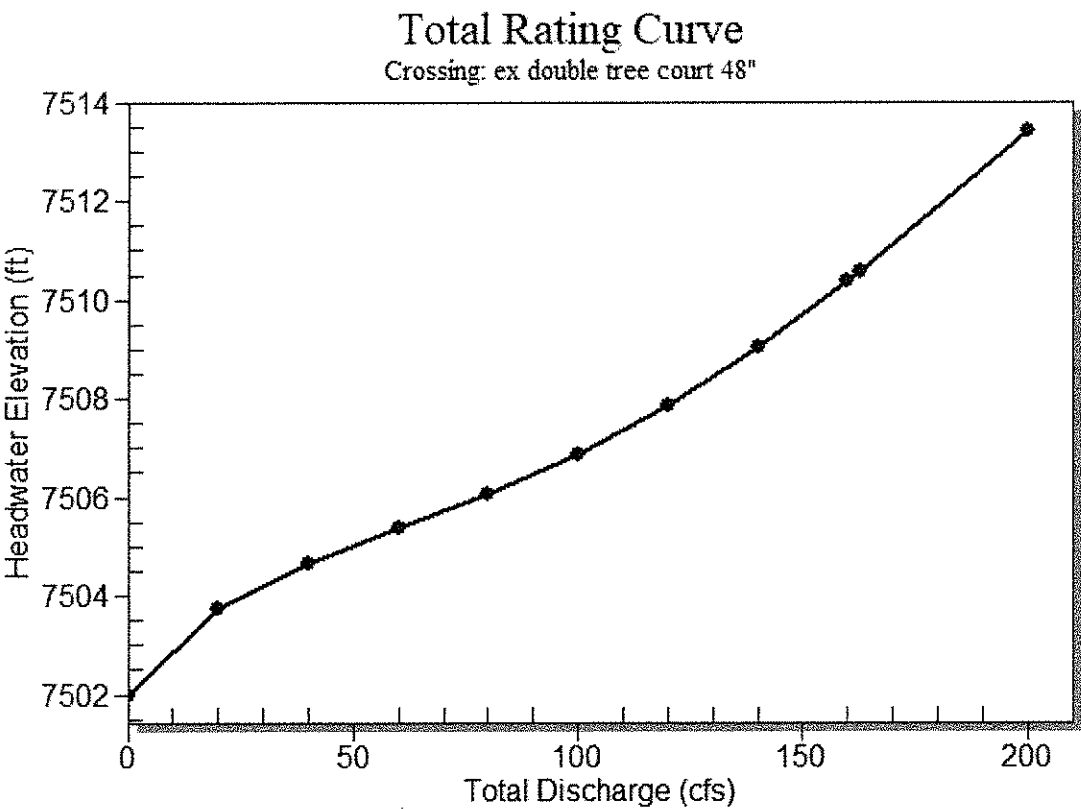
# HY-8 Culvert Analysis Report

EX 48" RCP DOUBLE TEE CE

**Table 1 - Summary of Culvert Flows at Crossing: ex double tree court 48"**

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
7502.00	0.00	0.00	0.00	1
7503.75	20.00	20.00	0.00	1
7504.64	40.00	40.00	0.00	1
7505.36	60.00	60.00	0.00	1
7506.06	80.00	80.00	0.00	1
7506.87	100.00	100.00	0.00	1
7507.86	120.00	120.00	0.00	1
7509.03	140.00	140.00	0.00	1
7510.36	160.00	160.00	0.00	1
7510.58	163.00	163.00	0.00	1
7513.44	200.00	200.00	0.00	1
7515.50	221.67	221.67	0.00	Overtopping

Rating Curve Plot for Crossing: ex double tree court 48"



**Table 2 - Culvert Summary Table: Culvert 1**

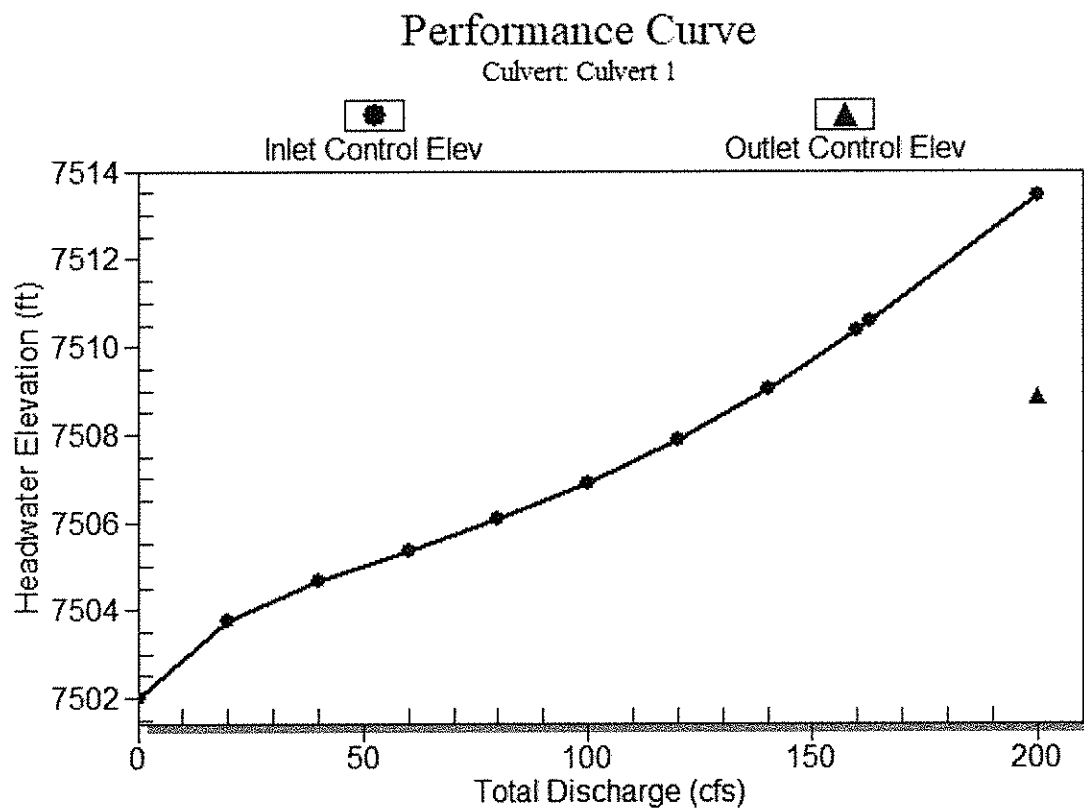
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	7502.00	0.000	0.0*	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
20.00	20.00	7503.75	1.751	0.0*	1-S2n	0.713	1.305	0.729	0.323	12.598	3.722
40.00	40.00	7504.64	2.643	0.0*	1-S2n	1.017	1.879	1.031	0.484	15.454	4.745
60.00	60.00	7505.36	3.359	0.0*	1-S2n	1.267	2.329	1.368	0.611	15.749	5.442
80.00	80.00	7506.06	4.060	0.0*	5-S2n	1.474	2.703	1.628	0.719	16.667	5.984
100.00	100.00	7506.87	4.872	0.0*	5-S2n	1.670	3.018	1.862	0.815	17.437	6.431
120.00	120.00	7507.86	5.857	0.0*	5-S2n	1.850	3.281	2.088	0.902	18.092	6.815
140.00	140.00	7509.03	7.027	0.0*	5-S2n	2.028	3.490	2.300	0.983	18.734	7.152
160.00	160.00	7510.36	8.365	0.0*	5-S2n	2.198	3.698	2.503	1.058	19.359	7.454
163.00	163.00	7510.58	8.578	0.0*	5-S2n	2.223	3.729	2.529	1.069	19.486	7.497
200.00	200.00	7513.44	11.438	6.856	6-FFc	2.544	4.000	4.000	1.195	15.915	7.980



\* theoretical depth is impractical. Depth reported is corrected.

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*****  
Inlet Elevation (invert): 7502.00 ft,   Outlet Elevation (invert): 7498.00 ft  
Culvert Length: 130.06 ft,   Culvert Slope: 0.0308  
*****
```

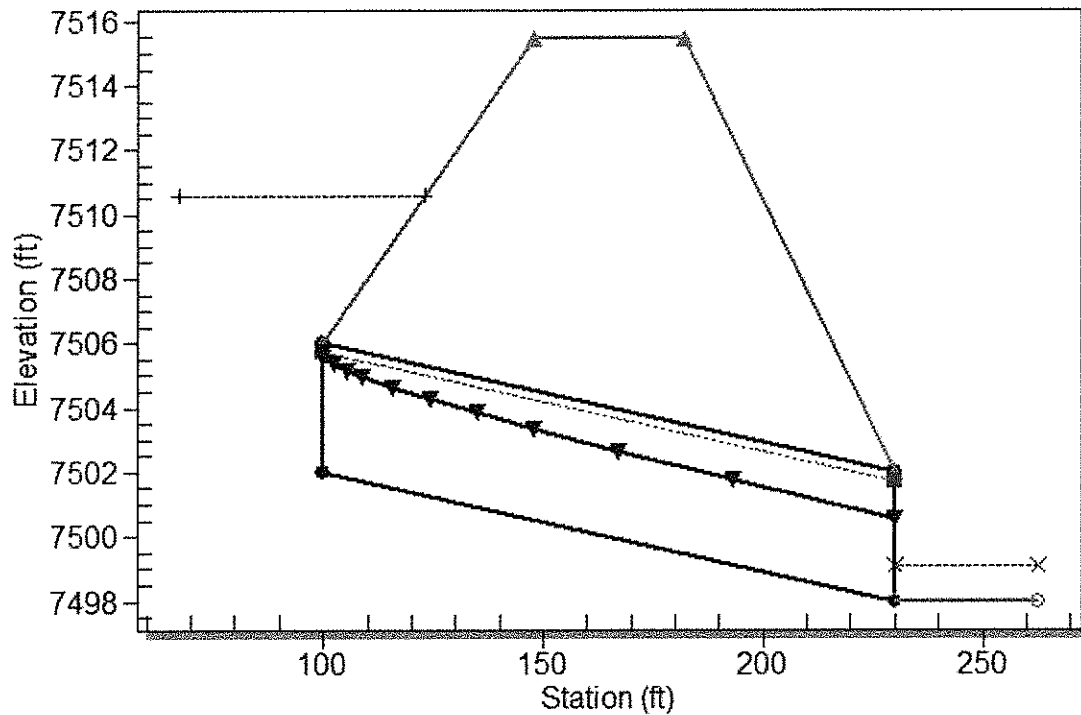
# Culvert Performance Curve Plot: Culvert 1



### Water Surface Profile Plot for Culvert: Culvert 1

Crossing - ex double tree court 48", Design Discharge - 163.0 cfs

Culvert - Culvert 1, Culvert Discharge - 163.0 cfs



### Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 100.00 ft

Inlet Elevation: 7502.00 ft

Outlet Station: 230.00 ft

Outlet Elevation: 7498.00 ft

Number of Barrels: 1

### Culvert Data Summary - Culvert 1

Barrel Shape: Circular

Barrel Diameter: 4.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Inlet Type: Conventional

Inlet Edge Condition: Beveled Edge (1:1)

Inlet Depression: NONE

**Table 3 - Downstream Channel Rating Curve (Crossing: ex double tree court 48")**

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	7498.00	0.00	0.00	0.00	0.00
20.00	7498.32	0.32	3.72	0.71	1.21
40.00	7498.48	0.48	4.75	1.06	1.28
60.00	7498.61	0.61	5.44	1.33	1.33
80.00	7498.72	0.72	5.98	1.57	1.36
100.00	7498.82	0.82	6.43	1.78	1.38
120.00	7498.90	0.90	6.81	1.97	1.40
140.00	7498.98	0.98	7.15	2.15	1.42
160.00	7499.06	1.06	7.45	2.31	1.43
163.00	7499.07	1.07	7.50	2.33	1.44
200.00	7499.19	1.19	7.98	2.61	1.46

**Tailwater Channel Data - ex double tree court 48"**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 15.00 ft

Side Slope (H:V): 5.00 (\_:1)

Channel Slope: 0.0350

Channel Manning's n: 0.0330

Channel Invert Elevation: 7498.00 ft

**Roadway Data for Crossing: ex double tree court 48"**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft

Crest Elevation: 7515.50 ft

Roadway Surface: Paved

Roadway Top Width: 34.00 ft

KIOWA ENGINEERING CORPORATION

JOB Cherry Creek Xing Lot III  
 SHEET NO. 1402B OF 1 of 3  
 CALCULATED BY \_\_\_\_\_ DATE 7-18-88  
 CHECKED BY \_\_\_\_\_ DATE 7-18-88  
 SCALE Hydraulics

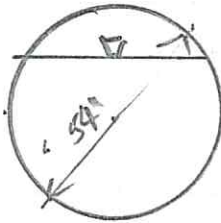
Outlet Velocity @ 54" RCP

$$Q_{100} = 163 \text{ cfs}$$

54" RCP free area = 15.4 sq'

Flowy full  $Q @ 100\% = 218 \text{ cfs}$   $V = 17.5 \text{ fps}$

Check @  $2/3$  full: Area = 10.3 sq'



$$Q = \frac{1.49}{n} S^{1/2} K D^{2/3}$$

$$A = 10.3 \quad R \approx .90$$

$$Q = \frac{1.49}{.013} \sqrt{.019} (10.3)(.9)^{2/3}$$

$$Q = 156 \text{ cfs: check Velocity}$$

$$V = \frac{156}{10.3} = 15.1 \text{ fps}$$

Per H&B Analysis:  $V @ \text{outlet} = 17.1 \text{ fps}$   
 Velocity:  $17.1 / 1.7 = 10.1 \text{ fps}$

KIOWA ENGINEERING CORPORATION

JOB Cherry Creek Crossing  
 SHEET NO. Lot 11 OF 2 of 3  
 CALCULATED BY HOB DATE 9/18/17  
 CHECKED BY BSW DATE Rev 2/12/17  
 SCALE Hydraulics

Proposed Sizing

Slope outlet of 54" to 48" under Double Tree  
 $S = .028' / ft$

$$\frac{VS^{.17}}{(Ss-1)^{.446}} = \frac{17.1 (.028)^{.17}}{(2.6-1)^{.446}} = \frac{9.31}{1.536} = 6.08$$

Per Table 10-6 DCM

Rock Size  $> 4H$  24" D<sub>50</sub> - lower end

probably super critical @ outlet  $\therefore$  10-6 does not apply;

Due to inlet control condition @ 48" under Double Tree, in 100-year flow would be stalled, @ 15 fps @ outlet of 54" is not reasonable. Continuous layer of Type H Gravel should suffice @ this location as velocity would be  $< 10$  fps. warranting Type M.

Since  $< 10$  fps  $VS^{.17}$   
 Check size of rock per UDFCD low tailwater basin requirements.

KIOWA ENGINEERING CORPORATION

JOB Cherry Creek Crossing  
 SHEET NO. Lot 111 OF 3 of 3  
 CALCULATED BY 14028 DATE 7/17/18  
 CHECKED BY David DATE \_\_\_\_\_  
 SCALE Hydraulics -

54" outlet Protection

use chapter 9. Low tailwater barrel.

per Fig 9-37

Rock Sizing: Figure 9-38

$$D = 4.5' \quad y_t =$$

assume critical flow depth in barrel

$$\begin{aligned} \therefore D_a &= \frac{D_c + y_n}{2} & D_c &= 3.73 \\ &= \frac{(3.73 + 2.51)}{2} & y_n &= 2.51 \\ &= 3.12 \end{aligned}$$

$$Q/1.5 \quad Q/D_a^{1.5} = \frac{163}{(3.12)^{1.5}} = 29.6$$

$$y_t/D_a = 2.5/3.12 = .80$$

per Figure 9-38: Type M (Soil Riprap)

$$\text{Thickness } 2 \times D_m = \underline{\underline{24"}}$$

### 3.2.2 Low Tailwater Basin

The design of low tailwater riprap basins is necessary when the receiving channel may have little or no flow or tailwater at time when the pipe or culvert is in operation. Figure 9-37 provides a plan and profile view of a typical low tailwater riprap basin.

By providing a low tailwater basin at the end of a storm drain conduit or culvert, the kinetic energy of the discharge dissipates under controlled conditions without causing scour at the channel bottom.

Low tailwater is defined as being equal to or less than  $\frac{1}{3}$  of the height of the storm drain, that is:

$$y_t \leq \frac{D}{3} \quad \text{or} \quad y_t \leq \frac{H}{3}$$

Where:

$y_t$  = tailwater depth at design flow (feet)

$D$  = diameter of circular pipe (feet)

$H$  = height of rectangular pipe (feet)

#### Rock Size

The procedure for determining the required riprap size downstream of a conduit outlet is in Section 3.2.3.

After selecting the riprap size, the minimum thickness of the riprap layer,  $T$ , in feet, in the basin is defined as:

$$T = 2D_{50} \quad \text{Equation 9-15}$$

#### Basin Geometry

Figure 9-37 includes a layout of a standard low tailwater riprap basin with the geometry parameters provided. The minimum length of the basin ( $L$ ) and the width of the bottom of the basin ( $W1$ ) are provided in a table at the bottom of Figure 9-37. All slopes in the low tailwater basin shall be 3(H):1(V), minimum.

#### Other Design Requirements

Extend riprap up the outlet embankment slope to the mid-pipe level, minimum. It is recommended that riprap that extends more than 1 foot above the outlet pipe invert be installed 6 inches below finished grade and buried with topsoil.

Provide pipe end treatment in the form of a pipe headwall or a flared-end section headwall. See Section 3.1 for options.



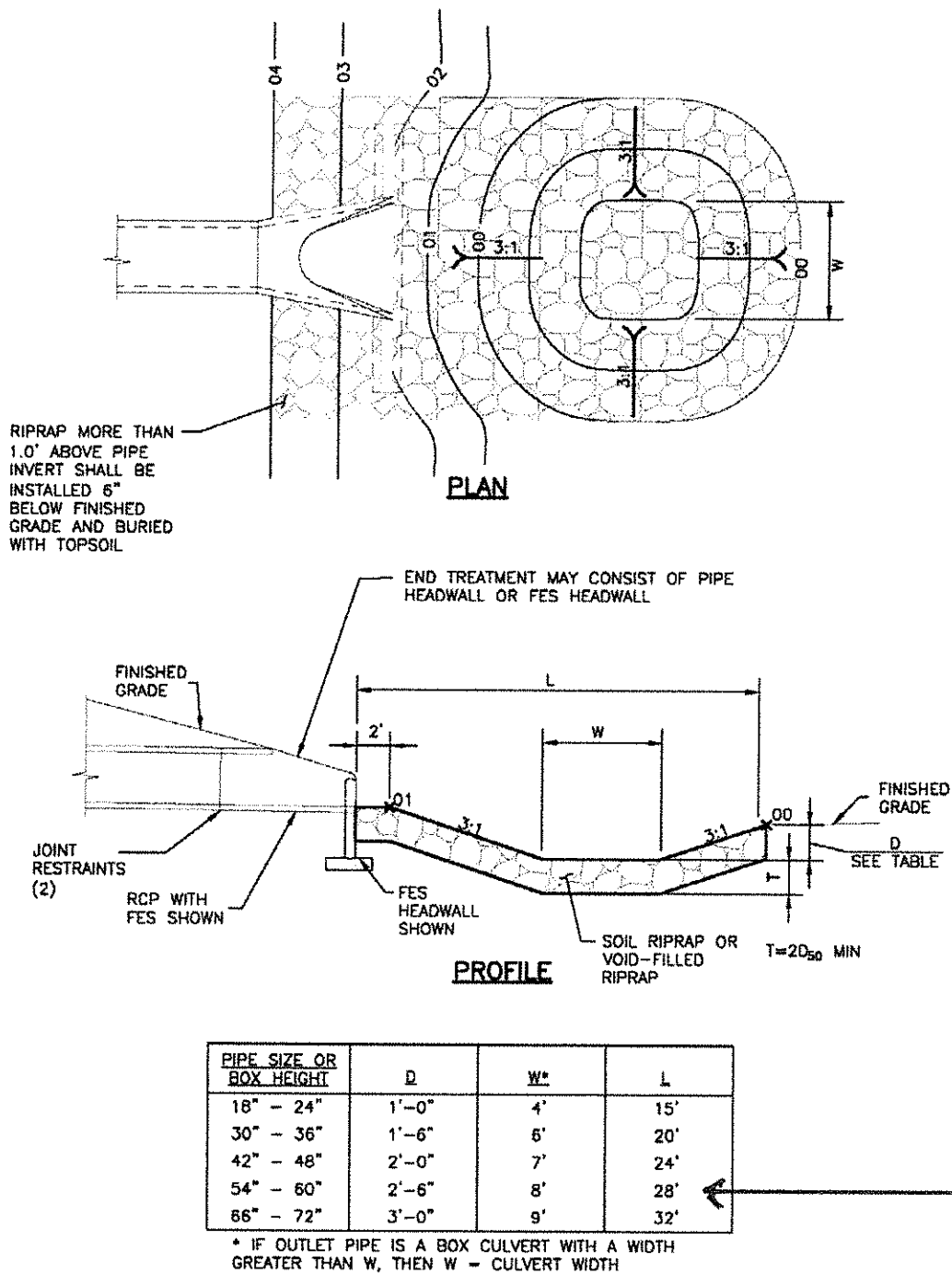


Figure 9-37. Low tailwater riprap basin

### 3.2.3 Rock Sizing for Riprap Apron and Low Tailwater Basin

Scour resulting from highly turbulent, rapidly decelerating flow is a common problem at conduit outlets. The following section summarizes the method for sizing riprap protection for both riprap aprons (Section 3.2.1) and low tailwater basins (Section 3.2.2).

Use Figure 9-38 to determine the required rock size for circular conduits and Figure 9-39 for rectangular conduits. Figure 9-38 is valid for  $Q/D_c^{2.5}$  of 6.0 or less and Figure 9-39 is valid for  $Q/WH^{1.5}$  of 8.0 or less. The parameters in these two figures are:

1.  $Q/D_c^{1.5}$  or  $Q/WH^{0.5}$  in which  $Q$  is the design discharge in cfs,  $D_c$  is the diameter of a circular conduit in feet, and  $W$  and  $H$  are the width and height of a rectangular conduit in feet.
2.  $Y_t/D_c$  or  $Y_t/H$  in which  $Y_t$  is the tailwater depth in feet,  $D_c$  is the diameter of a circular conduit in feet, and  $H$  is the height of a rectangular conduit in feet. In cases where  $Y_t$  is unknown or a hydraulic jump is suspected downstream of the outlet, use  $Y_t/D_c = Y_t/H = 0.40$  when using Figures 9-38 and 9-39.
3. The riprap size requirements in Figures 9-38 and 9-39 are based on the non-dimensional parametric Equations 9-16 and 9-17 (Steven, Simons, and Watts 1971 and Smith 1975).

Circular culvert:

$$d_{50} = \frac{0.023Q}{Y_t^{1.2} D_c^{0.3}} \quad \text{Equation 9-16}$$

Rectangular culvert:

$$d_{50} = \frac{0.014H^{0.5}Q}{Y_t W} \quad \text{Equation 9-17}$$

These rock size requirements assume that the flow in the culvert is subcritical. It is possible to use Equations 9-16 and 9-17 when the flow in the culvert is supercritical (and less than full) if the value of  $D_c$  or  $H$  is modified for use in Figures 9-38 and 9-39. Note that rock sizes referenced in these figures are defined in the *Open Channels* chapter. Whenever the flow is supercritical in the culvert, substitute  $D_a$  for  $D_c$  and  $H_a$  for  $H$ , in which  $D_a$  is defined as:

$$D_a = \frac{(D_c + Y_n)}{2} \quad \text{Equation 9-18}$$

Where the maximum value of  $D_a$  shall not exceed  $D_c$ , and

$$H_a = \frac{(H + Y_n)}{2}$$

Equation 9-19

Where the maximum value of  $H_a$  shall not exceed  $H$ , and:

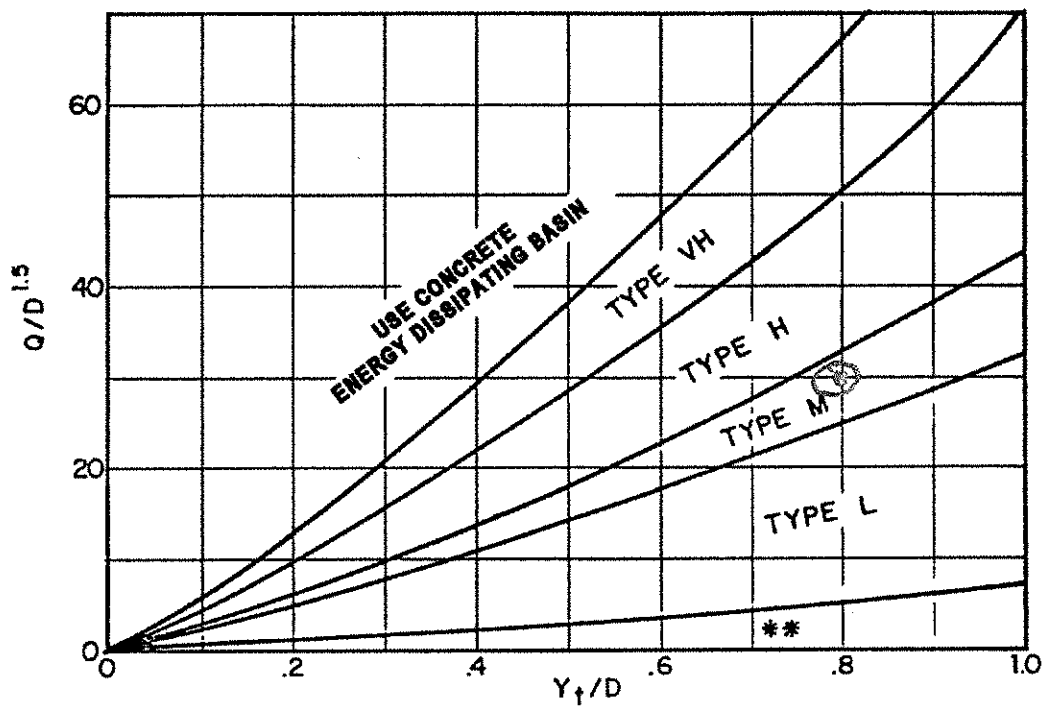
$D_a$  = parameter to use in place of  $D$  in Figure 9-38 when flow is supercritical (ft)

$D_c$  = diameter of circular culvert (ft)

$H_a$  = parameter to use in place of  $H$  in Figure 9-39 when flow is supercritical (ft)

$H$  = height of rectangular culvert (ft)

$Y_n$  = normal depth of supercritical flow in the culvert (ft)



Use  $D_a$  instead of  $D$  whenever flow is supercritical in the barrel.

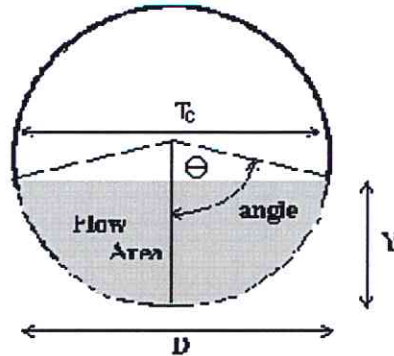
\*\* Use Type L for a distance of  $3D$  downstream.

Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for  $Q/D^{2.5} \leq 6.0$ )

## CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

Project: **14028 Cherry Creek Crossing Filing No. 1, Lot 111**

Pipe ID: **Hodgen Road Culvert- Extended Condition**



### Design Information (Input)

Pipe Invert Slope	So =	0.0190	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	54.00	inches
Design discharge	Q =	163.00	cfs

### Full-flow Capacity (Calculated)

Full-flow area	Af =	15.90	sq ft
Full-flow wetted perimeter	Pf =	14.14	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	271.79	cfs

### Calculation of Normal Flow Condition

Half Central Angle ( $0 < \text{Theta} < 3.14$ )	Theta =	1.69	radians
Flow area	An =	9.13	sq ft
Top width	Tn =	4.47	ft
Wetted perimeter	Pn =	7.59	ft
Flow depth	Yn =	2.51	ft
Flow velocity	Vn =	17.86	fps
Discharge	Qn =	163.01	cfs
Percent Full Flow	Flow =	60.0%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	2.20	supercritical

### Calculation of Critical Flow Condition

Half Central Angle ( $0 < \text{Theta-c} < 3.14$ )	Theta-c =	2.29	radians
Critical flow area	Ac =	14.09	sq ft
Critical top width	Tc =	3.39	ft
Critical flow depth	Yc =	3.73	ft
Critical flow velocity	Vc =	11.57	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	



NORTH  
1" = 1000'

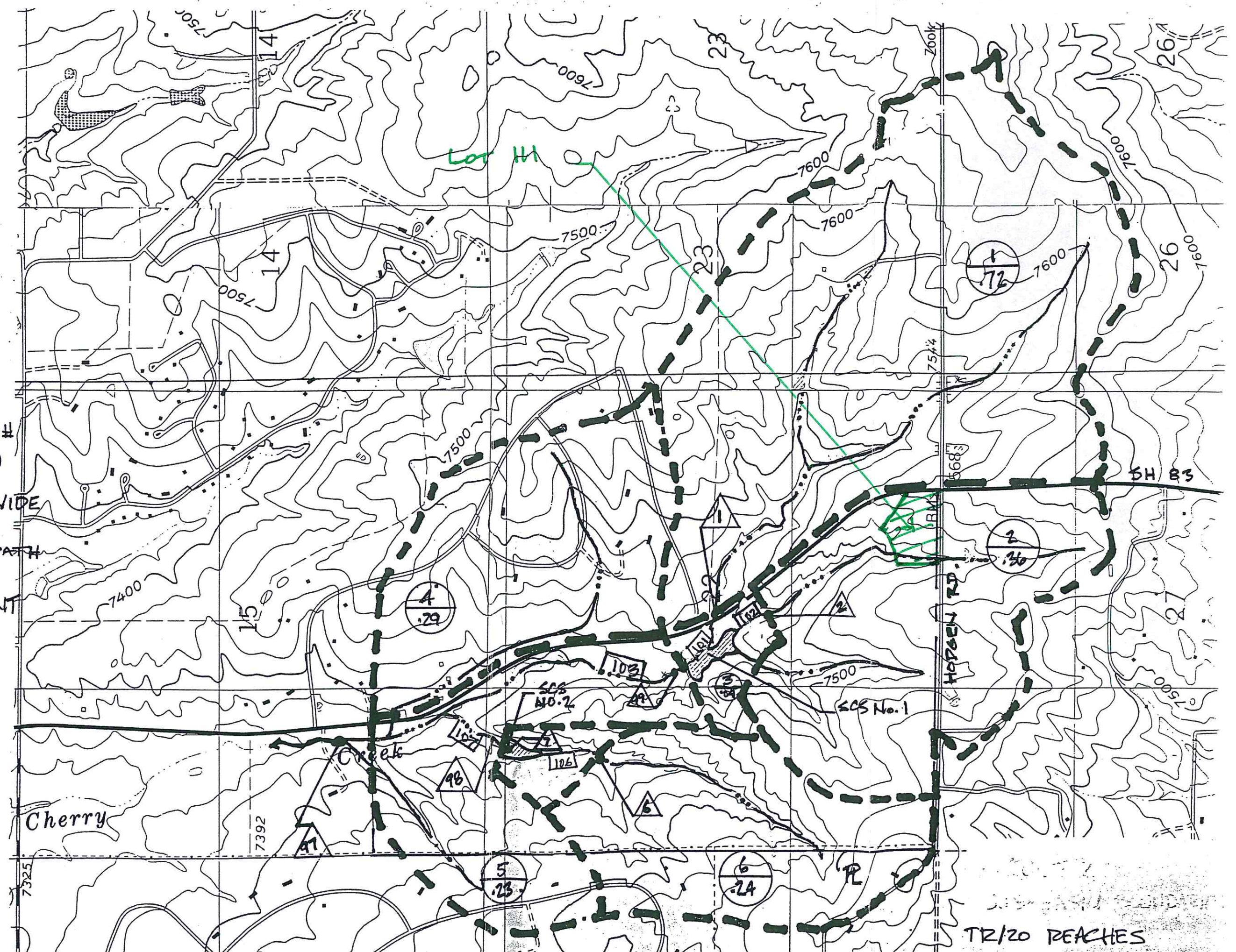
1  
72  
- GUB-BASIN #  
- AREA (SM)

--- BASIN DIVIDE

103 Tc FLOWPATH

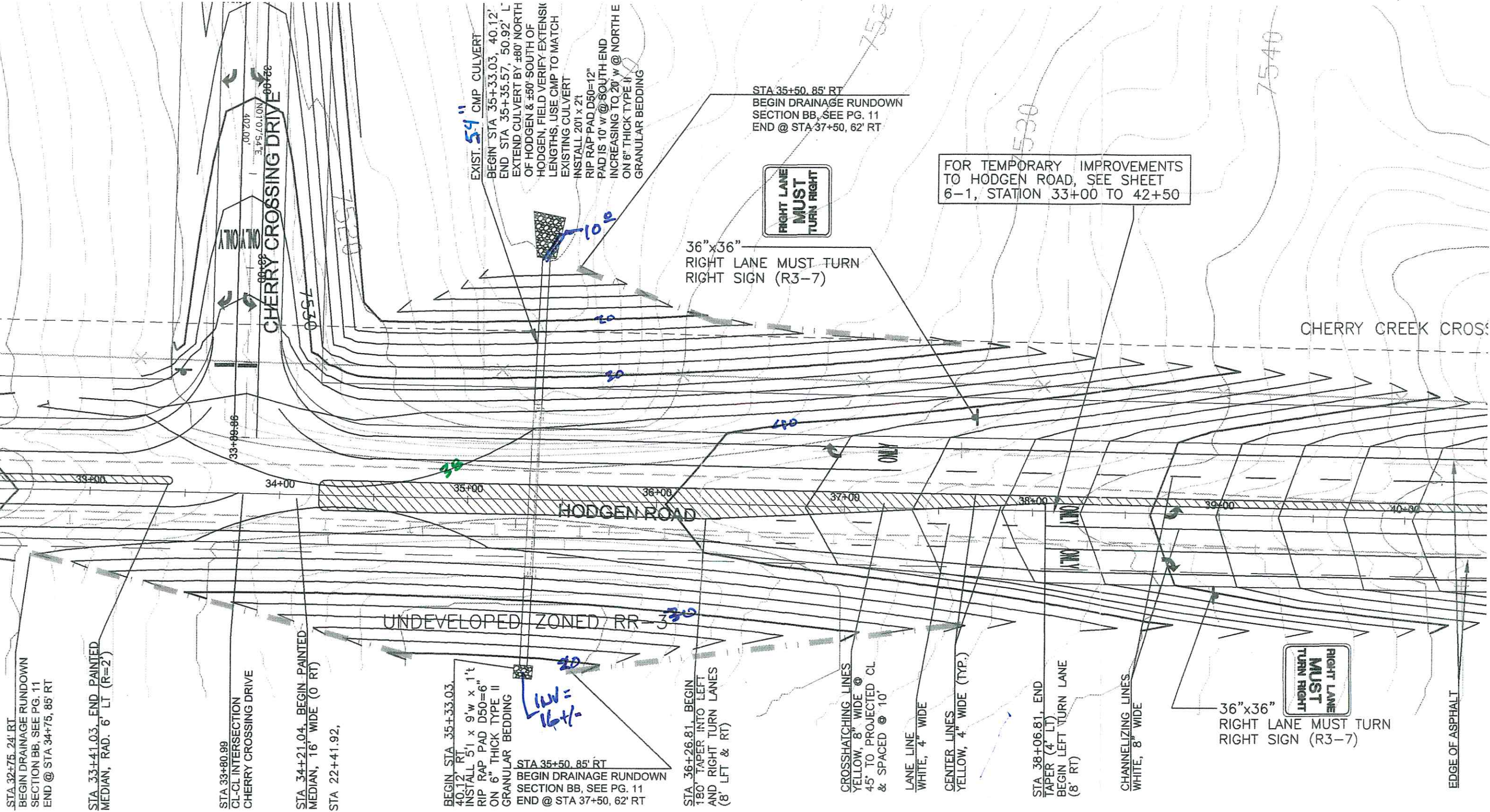
7 - DESIGN POINT

TR20 REACH  
ELEMENT



TR/20 REACHES





HODGEN ROAD

EXISTING 54" RCP  
1"=20'



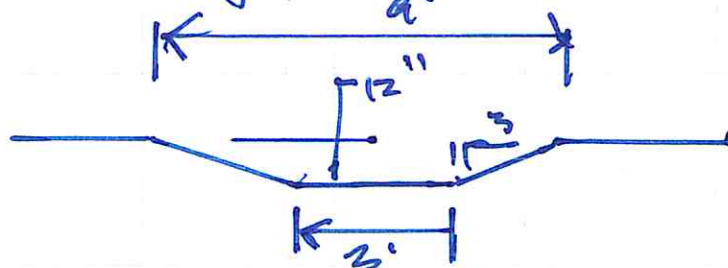
Spillways: Trap. Sediment Traps.

Sed. trap 1:  $DA = 1.4 \text{ ac}$  - round up to 2 ac

$\therefore$  per SB details SC-7

Riser pipe = 6" PVC

Spillway  $D_{50} = 9"$ : Crest length = 3'

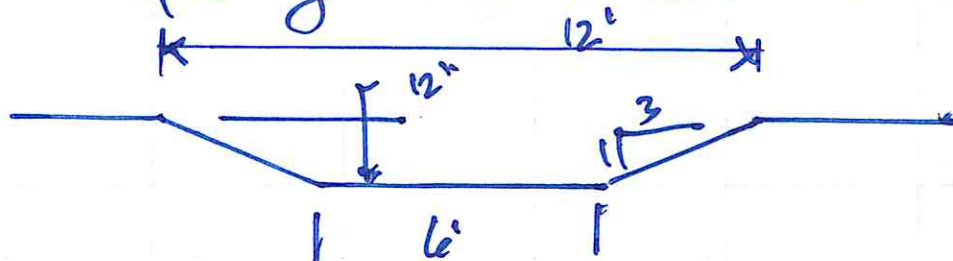


Sed. Trap # 2:  $DA = 5.3 \text{ ac}$  round to 5 ac.

$\therefore$  per SB details SC-7

Riser pipe = 6" PVC

Spillway  $D_{50} = 9"$  Crest length = 6'



Cherry Creek Crossing Lot 111  
Sedimentation Basin 1  
Volume Calculation

Stage	Elevation	Area sq. ft.	Area Acres	Avg. Area	Increment	Incremental Volume	Cumulative Volume
0	11	0	0.00				
				0.04	1	0.04	0.04
1	12	3,352	0.08				
				0.11	2	0.21	0.25
3	14	5,811	0.13				
				0.17	2	0.33	0.58
5	16	8,635	0.20				



Cherry Creek Crossing Lot 111  
Sedimentation Basin 2  
Volume Calculation

Stage	Elevation	Area sq. ft.	Area Acres	Avg. Area	Increment	Incremental Volume	Cumulative Volume
0	21	0	0.00				
				0.01	1	0.01	0.01
1	22	788	0.02				
				0.03	2	0.07	0.08
3	24	2,165	0.05				
				0.07	2	0.14	0.22
5	26	4,046	0.09				