FINAL DRAINAGE REPORT FOR SADDLEHORN RANCH – FILING 5 EARLY GRADING

Prepared For: ROI Property Group, LLC 2495 Rigdon Street Napa, CA 94558 (707) 365-6891

> August 17, 2023 Project No. 25142.07

Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

El Paso County PCD File No.: EGP226

Final Drainage Report Filing 5 - Saddlehorn Ranch Early Grading

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

25043 Bryan Law, Colorado P.E. # 25043 For and On Behalf of JR Engineering, LLC **DEVELOPER'S STATEMENT:** I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan. Business Name: ROI Property Group, LLC (BILL GUMAN By: REPRESENTATIVE Title: Address: 2495 Rigdon Street Napa, CA 94558 El Paso County: Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended. Joshua Palmer, P.E. Date County Engineer/ ECM Administrator



Conditions:

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PURPOSE

This document is the Final Drainage report for Filing 5 of Saddlehorn Ranch Early Grading. The purpose of this report is to:

- 1. Identify on-site and off-site drainage patterns.
- 2. Recommend storm water facilities to collect and convey storm runoff from the proposed development during early grading operations to appropriate discharge and/or detention locations.
- 3. Recommend water quality and detention facilities to control discharge release rates to below historic.
- 4. Demonstrate compliance with surrounding major drainage basin planning studies, master development drainage plans and flood insurance studies.

GENERAL LOCATION AND DESCRIPTION

Location

The proposed Saddlehorn Ranch Filing 5, known as "Filing 5" from herein, is a parcel of land located in Section 3 and 10, Township 13 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado. Saddlehorn Ranch is an 824 acre, rural, single family-development. Filing 5 is 126.73 acres and is comprised of 41 lots of the overall Saddlehorn Ranch development. Saddlehorn Ranch is bound by Judge Orr Road to the North and Curtis Road to the West. To the East, Saddlehorn Ranch is bound by undeveloped land owned by Brent Houser Enterprises, LLC. To the south, Saddlehorn Ranch is bound by undeveloped properties owned by Carolyn Gudzunas and Faye Reynolds. Filing 5 is bound by future Filing 4 to the north, Drainageway MS-06 to the west, and unplatted vacant land to the east and to the south. A vicinity map is presented in Appendix A.

Currently, there are two major Drainageway that will receive flows from Filing 5: Gieck Ranch (WF-R7A) and Haegler Ranch Main Stem 6 (MS-06). These Drainageways were analyzed, both hydrologically and hydraulically, in the following reports:

- Haegler Ranch Basin Drainage Basin Planning Study (DBPS), May 2009.
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision, June 2004.
- Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch, May 2020.
- Geick Ranch Drainage Basin Planning Study (DBPS), October 2007

The impact of these Drainageways and planning studies on the proposed development will be discussed later in the report.

Description of Property

Filing 5 is currently unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling range land condition. In general, Filing 5 slopes from south to southeast and the existing drainageways follow this topography.

Per a NRCS web soil survey of the area, Filing 5 is made up of Group A soils. Group A soils have a high infiltration rate when thoroughly wet. A NRCS soil survey map has been presented in Appendix A.

Floodplain Statement

Based on the FEMA FIRM Map number 08041C0558G, dated December 7, 2018, Filing 5 lies within Zone AE and Zone X. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. All proposed residential development within Filing 5 will occur in Zone X. The FIRM Map has been presented in Appendix A.

DRAINAGE BASINS AND SUB-BASINS

Unresolved:
Add statement regarding
CLOMR/LOMR requirements will be
completed with subsequent submittals
and no floodplain improvements to be
done with early grading.

Existing Major Basin Descriptions

Filing 5 lies within Haegler Ranch Drainage Basin based on the "*Haegler Ranch Drainage Basin Planning Study*" prepared by URS Corporation in May 2009.

The Haegler Ranch Drainage Basin covers approximately 16.6 square miles in unincorporated El Paso County, CO. The Haegler Ranch Drainage Basin is tributary to Black Squirrel Creek. In its existing condition, the basin is comprised of rolling rangeland with poor vegetative cover associated with Colorado's semi-arid climate. The natural Drainageways within the basin are typically shallow and wide with poorly defined flow paths in most areas. Anticipated land use for the basin includes residential and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

As part of its drainage research, JR Engineering reviewed the following drainage studies, reports and LOMRs:

- Haegler Ranch Drainage Basin Planning Study prepared by URS Corporation in May 2009
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision prepared by Tri-Core Engineering in June 2004.
- Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch, prepared by JR Engineering, May 2020.
- Gieck Ranch Drainage Basin Planning Study (DBPS), October 2007

The "Haegler Ranch Drainage Basin Planning Study" was used to establish a stormwater management plan for the existing and future stormwater infrastructure needs within the Haegler Ranch Drainage Basin. Based on provided drainage maps and analysis, in the existing condition Haegler Ranch contributes a total

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of 710 cfs onto the site. Of the 710 cfs, 590 cfs crosses Curtis Road in an existing 24" CMP onto the site. Major Drainageway MS-06 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. The remaining 210 cfs crosses Curtis Road in an existing 36" CMP onto the site. Major Drainageway T-6 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. Both Curtis Road culverts are undersized for existing and future flows and overtopping occurs locally near the culvert crossings.

Based on flood impacts, stream stability and cost effectiveness, this study recommended a sub-regional detention approach. This allows future development anywhere in the basin with the construction of an associated sub-regional pond. However, based on the *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch*, Filing 5 will utilize one on-site full spectrum water quality and detention ponds instead. This full spectrum detention pond will limit developed discharge into Drainageway MS-06 to less than historic rates.

The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR was executed on Haegler Ranch Tributary 2, 3, and 4. The LOMR revised the onsite effective flood zone from Zone A to Zone AE. See FIRM Map Panel 08041C0558G for limits of LOMR study and revised flood zones, presented in Appendix E.

The Gieck Ranch Drainage Basin covers approximately 22 square miles and begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. The Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains south to the Arkansas River near the city of Pueblo, Colorado. The majority of the area within the basin is undeveloped and is characterized as rolling range land typically associated with Colorado's semi-arid climates. Anticipated land use for the basin includes residential, industrial, agricultural and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

See Table 2 for comparison of Drainageway identification and the naming convention used within the context of this report. See Table 3 for a comparison of 100-year flows as calculated in the aforementioned DBPS and LOMR. An existing conditions drainage map is presented in Appendix E.

Table 1: Major Drainageway Naming Convention

	Major Dr	rainageway Naming Convention	ns
Saddlehorn Ranch MDDP/PDR:	Per Haegler Ranch DBPS:	Per Geick Ranch DBPS:	Per Sante Fe Springs LOMR:
MS-06	Main Stem (MS- 06)	N/A*	Haegler Ranch Tributary 3
WF-R7A	N/A*	West Fork (Middle)/WF-R7A	N/A*

Table 2: Major Drainageway – Ex. 100-Year Flow Comparison

	Major Drainag	geways: 100-Year Flo	ow Comparison	
Drainageway Name	Contributing Area (sq. mi.)	Q ₁₀₀ Per Haegler Ranch DBPS:	Q ₁₀₀ Per Geick Ranch DBPS:	Q ₁₀₀ Per Sante Fe Springs LOMR:
MS-06 @ Curtis Road	1.05	590 cfs	N/A*	505 cfs
WF-R7A @ Judge Orr Road	1.50	N/A*	1,017 cfs	N/A*

^{*}N/A: Flow regime outside limits of study.

The *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch* proposed the overall drainage facility design for Saddlehorn Ranch. Within the context of this report, onsite drainage basins the associated full spectrum water quality pond were established. As it pertains to Filing 5, two full spectrum water quality ponds are recommended. Roadside ditches and local street culverts will be utilized to capture and convey Filing 5's runoff to the water quality ponds. Both ponds A and B will discharge into Drainageway MS-06, while a portion of the proposed lots will release directly into Drainageway WF-R7A. All ponds are full spectrum and will release at less than historic rates.

Existing Sub-basin Drainage

On-site, existing sub-basin drainage patterns are generally from northeast to southwest, following the general slope of the existing grade. On-site areas flow directly into these drainageways, which also bypass off-site flows through the site.

On-site, existing drainage basins were established based upon existing topography and the limits of the 100-year floodplain. These existing sub-basins were analyzed in the *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch*. An existing drainage map has been provided in Appendix E.

Sub-basin H2 is comprised of rolling rangeland and runoff flows southwest to Drainageway MS-06 as represented by Design Point 4 (Q100=91.1 cfs).

Proposed Sub-basin Drainage

The proposed Filing 5 basin delineation is as follows;

Basin A consists solely of Basin A1 for a total of 15.08 acres. In its existing condition, Basin A is rolling rangeland and runoff generally flows southeast towards the southern property line where it will flow across adjacent property and ultimately outfall into Drainageway MS-06. In the proposed condition, Basin A will be rural 2.5 acre lots, paved roadway, and will include Pond A. In the early grading phase, runoff from this basin will be collected in roadside ditches and conveyed to Sediment Basin 2 in the southeast corner of the Filing 5 development. The watershed area of Pond A is 15.08 acres, and in the major event, the pond receives 10.4 cfs of flow. In the proposed condition, Sediment Basin 2 will be

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converted to Pond A. Pond A will be a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway MS-06.

B5

Basin B consists of Sub-basins B1-B6 combining for a total of 60.42 acres. In its existing condition, Basin B is rolling rangeland and runoff generally flows southwest to Drainageway MS-06. In the proposed condition, Basin B will be rural 2.5 acre lots and paved roadway, flowing ultimately to Pond B. In the early grading phase, runoff from this basin will be collected in roadside ditches and conveyed west to Sediment Basin 1 located in the south west corner of the Filing 5 development. In the proposed condition, Sediment Basin 1 will be converted to Pond B. The watershed area of Pond B is 60.42 acres, and in the major event the pond receives 34.3 cfs of flow. Pond B will be a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway MS-06.

Basin C consists of Sub-basins C1-C2 combining for a total of 5.45 acres. In its existing condition, Basin C is rolling rangeland and runoff generally flows south west towards Drainageway MS-06. In the proposed condition, Basin C will be rural 2.5 acre lots and paved roadway. Runoff from this basin will be collected in road side ditches and conveyed to the existing Pond C located in the southern portion of the Filing 4 development along Del Cambre Trail. Pond C is a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway MS-06. All calculations pertaining to Pond C can be found in the *Final Drainage Report for Saddlehorn Ranch – Filing 3*, prepared by JR Engineering, February 4, 2022.

46.99

Basin UD consists of Sub-basins UD1-UD4 combining for a total of 45.81 acres. In their existing condition, these basins are rolling rangeland. Runoff from Basins UD2, UD3, & UD 4 generally flows south and west to Drainageway MS-06. Basin UD1 flows east to Drainageway WF-R7A. In the proposed condition, these basins will be rural 2.5 acre lots with an Imperviousness = 6.2% and will be excluded from permanent stormwater quality management per Section I.7.1.B.5 of the ECM – Stormwater Quality Policy and Procedures.

Basin OS consists of Sub-basins OS1-OS4 combining for a total of 10.55 acres. These basins are offsite, and will remain undeveloped rangeland throughout the duration of the project. Runoff from sub-basins OS1-OS4 generally flows from northeast to southwest on to the Saddlehorn site. Runoff from Basin OS will not be treated by on-site water quality treatment per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures.

Finish basin name

A summary table of proposed basin parameters and flow rates are presented in Appendix B.

In the ultimate conditions, Basin A runoff will overland flow into Pond A, or be captured by roadside swales and conveyed to the proposed Pond A. In the ultimate conditions, Basin B will be captured in roadside swales and conveyed to the proposed Pond B. Both full spectrum ponds will release treated flows at less than historic rates to minimize adverse downstream impacts, and both will discharge into Drainageway MS-06.

See Table 3 below for proposed Filing 5 pond parameters.

Table 3: Pond Summary

Tributary Sub-Basin	Pond Name	Tributary Acres	WQ Volume (ac-ft)	Total Detention Volume (ac-ft)	Provided Volume (ac-ft)	Maximum 100-Year Discharge (cfs)
Α	Pond A	15.08	0.085	0.199	0.279	7.5
В	Pond B	60.42	0.382	1.144	1.295	21.6

Early Grading Drainage

During early grading operations, runoff will be captured in roadside ditches and conveyed into one of two sediment basins. Basin A runoff will be conveyed to Sediment Basin 2. Basin B runoff will be conveyed to Sediment Basin 1. Sediment Basin 1 is designed to treat a tributary area of 60.42 acre, 20.98 acre of disturbed area, and 39.44 acre of undisturbed area. The required volume of Sediment Basin 1 in order to treat the 60.42 acre is 1.320 Ac-ft. Sediment Basin 1 exceeds this with a provided volume of 2.315 Ac-ft. Sediment Basin 1 was designed to drain its entire volume within 40 hrs via a temporary outlet structure. This temporary outlet structure was designed as a singular column with five 1.25" dia holes allowing for water to drain.

Sediment Basin 2 is designed to treat a tributary area of 15.08 acre, 1.55 acre of disturbed area, and 13.53 acre of undisturbed area. The required volume of Sediment Basin 2 in order to treat the 15.08 acre is 0.219 Ac-ft. Sediment Basin 2 has a provided volume of 0.279 Ac-ft. Sediment Basin 2 was designed to drain its entire volume within 40 hrs via a temporary outlet structure. This temporary outlet structure was designed as a singular column with five 1.25" dia holes allowing for water to drain.

Once the project progresses past this early grading phase, both Sediment Basin 1 and Sediment Basin 2 will be converted to a full spectrum water quality detention ponds. Sediment Basin 1 will be converted to Pond B, and Sediment Basin 2 will be converted to Pond A. Each Pond will be fitted with a concrete forebay along with appropriately sized riprap. The water will then drain through a concrete trickle channel to the proposed permanent outlet structure. Both temporary outlet structures will be replaced with permanent outlet structures, each with appropriately sized riprap spreaders. Both ponds will release treated flows at less than historic rates to minimize adverse impacts downstream. Both ponds will discharge into Major Drainageway MS-06. The final design for both Pond A and Pond B will be included in the Final drainage Report.

See Table 4 below for proposed Filing 5 Early Grading sediment basin parameters

Table 4: Sediment Basin Summary

Tributary Sub-Basin	Sediment Basin Name	Tributary Acres	Total Detention Volume (ac- ft)	Provided Volume (ac- ft)	Maximum Discharge (cfs)
A	Sediment Basin 2	15.08	0.219	0.279	0.0331
В	Sediment Basin 1	60.42	1.320	2.315	0.1997

DRAINAGE DESIGN CRITERIA

Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "City of Colorado Spring/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual (CCSDCM), dated May 2014, as adopted by El Paso County.

Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Rational Method calculations were prepared, in accordance with Section 13.3.2.1. of the CCSDCM, for the sub-basins that directly impact the sizing of ditches and local street culverts. Rational method calculations are presented in Appendix B.

Urban Drainage and Flood Control District's UD-Detention, Version 4.06 workbook was used for pond sizing. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. Pond sizing spreadsheets are presented in Appendix D.

Hydraulic Criteria

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for roadside ditch design. Ditches were checked for velocity and capacity per the CCS/EPCDCM Section 12.3.2.2. In order to check both capacity and velocity, a cross section analysis was performed on the roadside swales using the basin's

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maximum runoff Q and the proposed uniform slope of the swale. Swale cross sections have been presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for local road crossing culvert design. Culvert size was determined based on 100-year flows and hydraulic criteria from EPCDCM Chapter 9 –Culvert Design. All local road crossing culvert design reports are presented in Appendix C.

DRAINAGE FACILITY DESIGN

General Concept

The proposed stormwater conveyance system was designed to convey the developed Filing 5 runoff during interim early grading to one of two Sediment Basins via roadside ditches and local street culverts. These Sediment Basins were designed to release at less than historic rates to minimize adverse impacts downstream during early grading.

The proposed early grading improvements are over designed for the current state of the project site. The roadside swales along with the proposed culverts are designed to treat runoff for the completed development. During early grading operations, the site will have minimal composite impervious surfaces without the proposed roads and vacant lots. This will allow more runoff to infiltrate the ground, reducing the amount of runoff that needs to be caught by the roadside swales and sediment basins.

Once the project progresses past early grading operations, Sediment Basin 1 and Sediment Basin 2 will each be converted into Pond B and Pond A respectively. The temporary outlet structures will be replaced with permanent outlet structures. Each Pond will have a concrete forebay and trickle channel. Both ponds will release treated flows at less than historic rates to minimize adverse impacts downstream. Both ponds will discharge into Major Drainageway MS-06. The final design for Ponds A and B will be included in the Final Drainage report.

Specific Details

Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume (WQCV), and consider the need for Industrial Commercial BMP's.

Step 1, Reducing Runoff Volumes: The development of the project site is proposed single family residential lots (2.5 ac. min.) with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roadways utilize soil riprap lined roadside ditches further disconnecting impervious areas. These practices will also allow for increased infiltration and reduce runoff volume.

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Step 2, Stabilize Drainageways: Filing 5 utilizes roadside ditches with culvert crossings throughout. These roadside ditches direct the on-site development flows to the proposed detention ponds within the project that releases at or below historic rates into Drainageway MS-06. Based upon the proposed reduction in released flows compared to the pre-developed flows, no impacts to downstream Drainageway MS-06 or Drainageway WF-R7A are anticipated.

Step 3, Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV in a full spectrum water quality and detention pond that is designed per current El Paso County drainage criteria.

Step 4 Consider the need for Industrial and Commercial BMP's: No industrial or commercial uses are proposed within this development. However, a site specific storm water quality and erosion control plan and narrative are prepared in conjunction with this report. Site specific temporary source control BMPs as well as permanent BMP's are detailed in this plan and narrative to protect receiving waters.

Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention are provided for all developed basins. Outlet structure release rates are limited to less than historic rates to minimize adverse impacts to downstream stormwater facilities. Complete pond and outlet structure designs are presented in Appendix D for information.

Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted since this project is disturbing more than 1 acre. The Early Erosion Control Plans for Filing 5 have been submitted concurrently with this report.

Operation & Maintenance

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within the any platted County ROW will be owned and maintained by El Paso County. All proposed drainage structures within easements or tracts will be owned and maintained by the Saddlehorn Ranch Metropolitan District. Vegetation in the natural and improved portions of Drainageway MS-06 with the Filing 5 improvements is the responsibility of the Saddlehorn Ranch Metropolitan District. This includes all mowing, seeding and weed control activities. An Inspection & Maintenance Plan is submitted concurrently with this drainage report that details the required maintenance activities and intervals to ensure proper function of all stormwater infrastructure in the future.

Drainage and Bridge Fees

Drainage and Bridge Fees are not due with the early grading permit application. An estimate of basin fees for the proposed development within Haegler Ranch drainage basin will be calculated and provided with the Filing 5 Final Drainage Report.

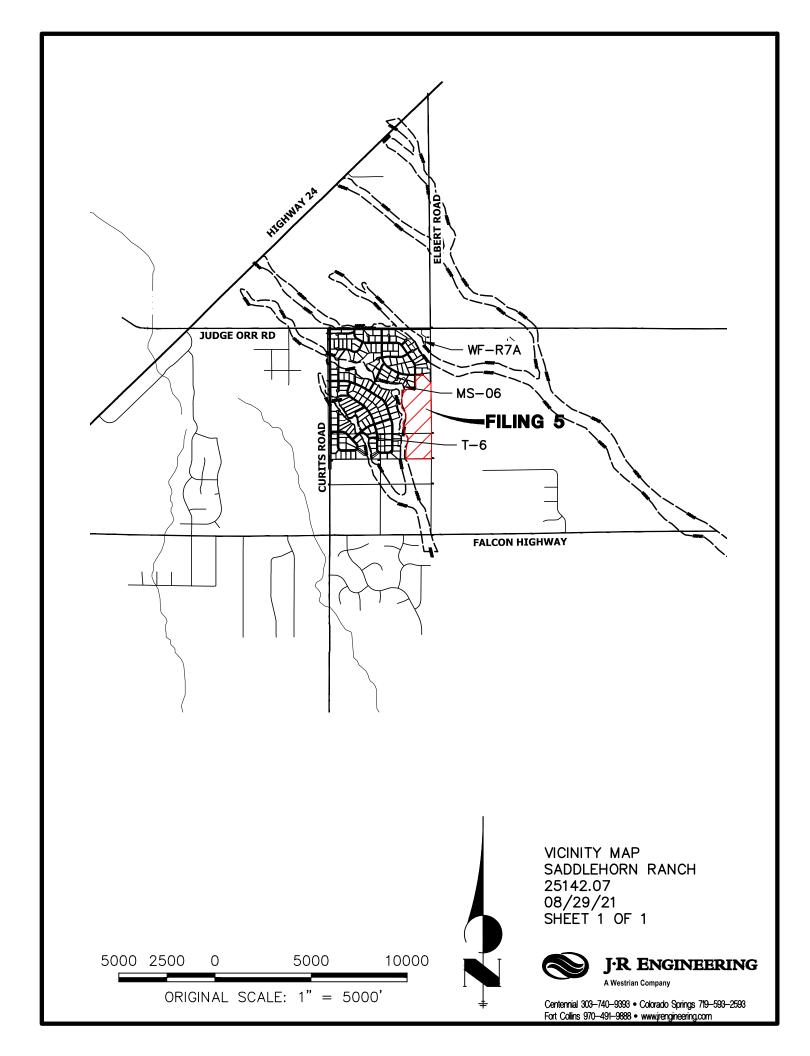
SUMMARY

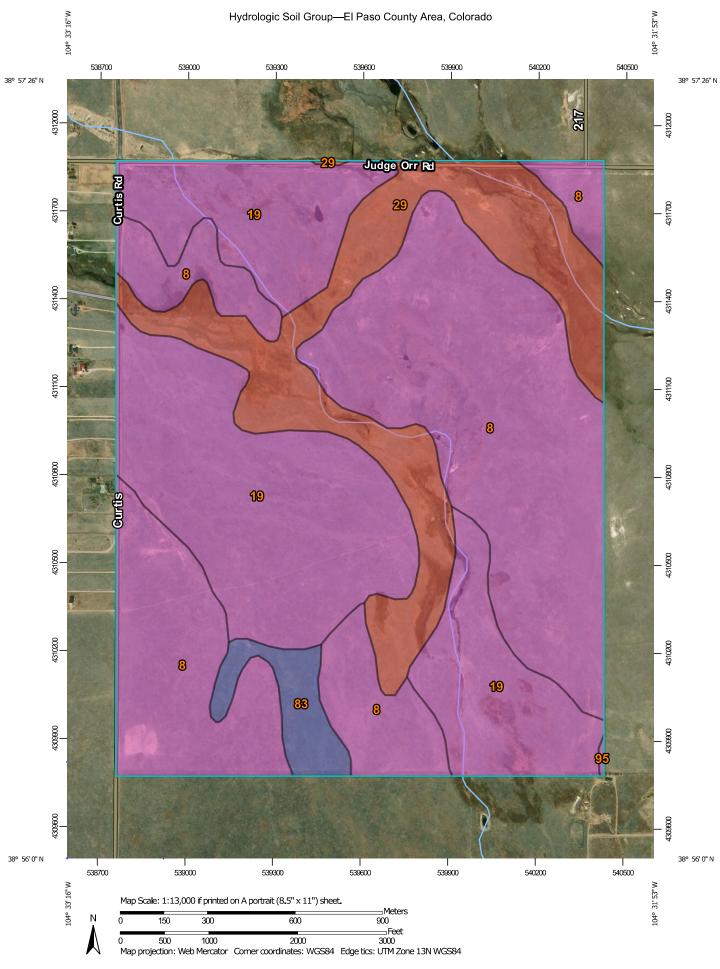
The proposed development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements, including ditches, culverts and detention ponds. The proposed development will not adversely affect the offsite major drainageways or surrounding development. This report meets the latest El Paso County Drainage Criteria requirements for this site and is in accordance with the PDR/MDDP for Saddlehorn Ranch.

REFERENCES:

- 1. <u>City of Colorado Springs Drainage Criteria Manual Volume 1</u>, City of Colorado Springs, CO, May 2014.
- 2. <u>Urban Storm Drainage Criteria Manual</u>, Urban Drainage and Flood Control District, Latest Revision.
- 3. <u>Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch</u>, JR Engineering, May 2020.
- 4. Haegler Ranch Drainage Basin Planning Study, URS Corporation, May 2009.
- 5. <u>The Santa Fe Springs Haegler Ranch Drainage Basin LOMR</u>, Federal Emergency Management Agency, October 20, 2004.
- 6. Final Drainage Report for Saddlehorn Ranch Filing 3, JR Engineering, February 4, 2022

APPENDIX A FIGURES AND EXHIBITS





This product is generated from the USDA-NRCS certified data as Date(s) aerial images were photographed: May 22, 2016—Aug distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background projection, which preserves direction and shape but distorts Soil map units are labeled (as space allows) for map scales Source of Map: Natural Resources Conservation Service imagery displayed on these maps. As a result, some minor Albers equal-area conic projection, should be used if more The soil surveys that comprise your AOI were mapped at Please rely on the bar scale on each map sheet for map accurate calculations of distance or area are required. Soil Survey Area: El Paso County Area, Colorado Coordinate System: Web Mercator (EPSG:3857) MAP INFORMATION shifting of map unit boundaries may be evident. Survey Area Data: Version 16, Sep 10, 2018 of the version date(s) listed below. Web Soil Survey URL: 1:50,000 or larger. measurements Not rated or not available Streams and Canals Interstate Highways Aerial Photography Major Roads Local Roads US Routes Rails C/D Water Features Transportation ပ Background MAP LEGEND ŧ Not rated or not available Not rated or not available Area of Interest (AOI) Soil Rating Polygons Area of Interest (AOI) Soil Rating Points Soil Rating Lines B/D ΑD B/D ΑD B/D ⋖

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	А	388.3	44.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	307.3	35.3%
29	Fluvaquentic Haplaquolls, nearly level	D	150.0	17.2%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	24.6	2.8%
95	Truckton loamy sand, 1 to 9 percent slopes	А	0.6	0.1%
Totals for Area of Inter	rest		870.8	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

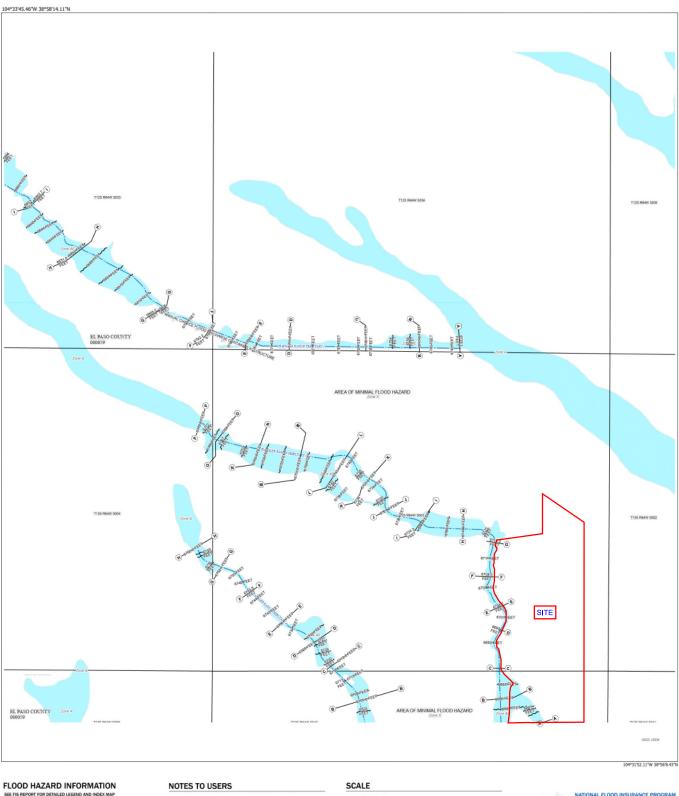
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher





1:6,000 1 inch = 500 feet





MAP NUMBER 08041C05580

APPENDIX B HYDROLOGIC CALCULATIONS

COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: Saddlehorn Ranch Filing 5 Early Grading Location: El Paso County

Project Name: Saddlehorn Ranch
Project No.: 25142.07
Calculated By: WKN
Checked By: TBD
Date: 8/22/23

	2.0%										137.31	TOTAL
The												
*Area based on 2												
Comp % Impervious												
U.212.U												
0.2124												
Area* (ac)												
nodus W/ nodu												
ocod/m speed												
	2.0%	2.0%	5.72	2%	0.0%	0.00	6.2%	0.0%	0.00	45%	5.72	084
	2.0%	2.0%	3.56	2%	0.0%	0.00	6.2%	%0:0	0.00	45%	3.56	083
mointain %	2.0%	2.0%	0.68	7%	0.0%	00'0	6.2%	%0:0	0.00	45%	0.68	082
	2.0%	2.0%	0.59	2%	0.0%	0.00	6.2%	0.0%	0.00	45%	0.59	051
2.50	2.0%	2.0%	2.68	7%	0.0%	0.00	6.2%	%0:0	0.00	45%	2.68	UD4
Total Area (ac)	2.0%	2.0%	11.03	7%	0.0%	00'0	6.2%	%0:0	0.00	45%	11.03	UD3
	2.0%	2.0%	25.14	7%	%0.0	00'0	6.2%	%0:0	0.00	45%	25.14	UD2
	2.0%	2.0%	8.14	7%	%0.0	00'0	%7'9	%0:0	0.00	45%	8.14	UD1
	2.0%	2.0%	4.19	7%	%0.0	00'0	%7'9	%0:0	0.00	45%	4.19	C2
Roofs 9	2.0%	2.0%	1.26	7%	%0.0	00'0	6.2%	%0:0	0.00	45%	1.26	C1
e la	2.0%	2.0%	14.04	7%	%0.0	00'0	6.2%	%0:0	0.00	45%	14.04	B5
Strunts Paved 10	2.0%	2.0%	9.16	7%	0.0%	00'0	6.2%	%0:0	0.00	45%	9.16	B4
landute to undefined	2.0%	2.0%	10.83	7%	%0.0	00'0	6.2%	%0:0	0.00	45%	10.83	B3
Engineed Rock 10	2.0%	2.0%	12.64	7%	%0.0	00'0	%7'9	%0:0	0.00	45%	12.64	B2
Gearbelts, Agriculture Pasture/Maxima	2.0%	2.0%	12.57	7%	%0.0	00:00	6.2%	%0:0	0.00	45%	12.57	B1
Understand Areas Heloric Flow Analysis	2.0%	2.0%	15.08	7%	%0.0	00:00	6.2%	%0:0	0.00	45%	15.08	A1
Rabrad Yard Areas												
Policy and Complaines	weignted % lmp.	weignted % Imp.	Area (ac)	% Imp.	weignted % Imp.	Area (ac)	% Imp.	weignted % Imp.	Area (ac)	% Imp.	Total Area (ac)	Basin ID
Light Apaz	Basins Total		Lawns		ots	2.5 Acre Rural Lots	2.5		Paved Roads			

and the same and and	-						Rundly Conflicients	efficients					
Danadaribles	Impersions	2.4	2-yaze	3.4	2 tests	ver.	13-year	Ń	S-year	08	50-year	907	100 year
		HIG ALE	HISCORD	MICABLE	HISTORIE	MICABLE	HISCORD	YEST A SAR	169 CBD	HIST AND	N3Q CIED	HOSE AND	NO CALO
Actions													
Commercial Areas	MI	20	030	130	0.30	BO	0.34	28.0	25.0	0.87	86.0	0.88	0.30
Neighborhood Aveza	92	57-0	11.49	0.45	1133	8.83	11.57	0.50	25.0	0.60	2510	73.0	0.55
esdential													
1/2 Acre or less	8	19-0	0.45	0.45	0.40	0.45	25.0	25.0	0.36	0.57	29'0	0.55	0.65
1/4.4570	9	20	0.38	0.30	0.35	95.0	D 43	242	05.0	0.46	150	050	200
1/3 400	R	N O	0.23	0.75	030	0.37	95.0	910	0.47	0.43	0.53	0.47	150
1/1 Acre	и	510	020	0.72	DJR	0.30	0.36	0.37	0.46	0.41	0.51	0.46	100
Lacra	30	0.0	0.17	0.70	0.25	0.77	1134	0.35	11.00	0.40	0.50	0.44	0.55
Schuttras													
Light Areas	8	0.57	0.60	0.55	0.63	9.63	970	0.00	0.70	0.68	0.72	0.70	0.74
Hequy Areas	06	0.71	0.75	0.73	0.75	0.75	0,77	0.75	DED	0.80	DETO	1810	0.35
and and Comettines	-	900	600	0.12	0.15	9.76	H 29	0.31	H.45	0.34	E.25	0.50	
approauds.	13	0.67	B.13	0.16	B 23	0.74	1131	0.52	E.42	0.37	0.43	0.45	133
altred had Areas	Ge .	6.0	0.28	0.81	036	95.0	1742	270	020	5770	150	0.20	920
Andrew Comments of the second		Ī	I	I		I	I				I		
Heloni Row Analysis			1	1					1	3	-	1	1
Samuel Manhain	0	0.00	non u	90.0	0.15	0.10	36.0	0.75	0.37	0.10	200	32.0	900
Forest	0	0.02	DOM	9000	51.0	51.0	0.25	0.75	0.37	0.40	11.43	0.35	030
Expressed Sock	100	0.85	0.30	050	0.30	25'0	0.82	200	100	950	0.00	3670	980
Official Row Analysis (when landuse is undefined)	18	0.36	0.31	0.22	1137	0.76	177	4	8.53	0.48	11.55	150	020
COURTS													
Payed	100	0.83	0.30	050	0.30	250	0.90	0.54	100	56.0	0.00	96'0	0.06
Gavel	Si.	50	090	950	59'0	98	99'0	390	0,70	0.68	0,77	02.0	其口
Colon need Market	101	80	0.30	0.00	98.0	0.62	0.00	200	100	30.0	900	20.00	8
Ago/s	98	12.0	0.73	0.73	0.75	0.75	0.77	0.78	0.30	0.80	0.87	0.81	11.65
	,	000		1	-	I	I		1	1		ŀ	

uo	Area (ac) - Lawns (2%)	2.39	
% Impervious Calculati	Area (ac)- Drives (100%)	0.046	6.20%
2.5 Acre Rural Lots - Comp. % Impervious Calculation	Area (ac) - Roofs (90%) Area (ac)- Drives (100%) Area (ac) - Lawns (2%)	890'0	
2.5 A	Total Area (ac)	2.50	Comp % Imperviousness

rvious Calculation	Area - Roads (100%)	0.0804	0.41
Roads w/ Roadside Ditches - Comp. % Impervious Calculation	Area - Ditch (5%)	0.1320	0
Roads w/ Roadside D	Area* (ac)	0.2124	Comp % Imperviousness

n 250 LF roadway from CL to outside edge of roadside ditch he above conservatively rounded to 45%.

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

bdivision: Saddlehorn Ranch Filing 5 Early Grading Location: El Paso County

Project Name: Saddlehorn Ranch
Project No.: 25142.07
Calculated By: WKN
Checked By: TBD
Date: 8/22/23

		Basins Total	Hydro	Hydrologic Soil Group	Group	Hydro	Hydrologic Soil Group	Group	Μin	Minor Coefficients	ents	Мај	Major Coefficients	ents		Basins Total
Basin ID	Total Area (ac)	Weighted %	Area A (ac)	Area B (ac)	Area C/D (ac)	% A (ac)	% B (ac)	% C/D (ac)	C _{5,A}	C _{5,8}	C _{5,C/D}	C _{100,A}	С _{100,В}	C _{100,C/D}	Basins Total Weighted C _s	Weighted C ₁₀₀
A1	15.08	2.0%	15.08	00:00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
B1	12.57	2.0%	12.57	00:00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
B2	12.64	2.0%	12.64	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
B3	10.83	2.0%	10.83	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
B4	9.16	2.0%	9.16	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
B5	14.04	2.0%	14.04	00'0	0.00	100%	%0	%0	0.01	0.01	90.0	0.13	0.44	0.49	0.01	0.13
C1	1.26	2.0%	1.26	00:00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
C2	4.19	2.0%	4.19	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
UD1	8.14	2.0%	8.14	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
UD2	25.14	2.0%	25.14	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
UD3	11.03	2.0%	11.03	00.0	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
UD4	2.68	2.0%	2.68	0.00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
051	0.59	2.0%	0.59	0.00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
082	0.68	2.0%	0.68	0.00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
053	3.56	2.0%	3.56	0.00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
054	5.72	2.0%	5.72	0.00	0.00	100%	%0	%0	0.01	0.01	0.05	0.13	0.44	0.49	0.01	0.13
TOTAL	137.31	2.0%	137.31	0.00	0.00	100%	%0	%0	-	-	-	-	-	-	0.01	0.13

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

	S Vans	10 Van	Storm Ret	Storm Return Period	100 Van	500 Vans
7-1 can	2-1 cal	10-1-01	73-1 cq	30-1 cat	100-1 ca	200-1 cal
	CA=	C _A =	CA=	CA=	C _A =	CA=
0.8471302	0.8671276	0.8771.232	0.841.124	0.857+0.025	0.85i+0.025 0.78i+0.110 0.65i+0.254	0.657+0.254
1	CB =	C _B =	C _B =	C _B =	C _B =	C _B =
0.8411169	0.86/1.088	0.817+0.057	0.81#+0.057 0.63#+0.249 0.56#+0.328 0.47#+0.426 0.37#+0.536	0.56+0.328	0.47#+0.426	0.37#+0.536
	C _{C/D} =	C _{CD} =	C _{CD} =	C _{CD} =	C _{CD} =	C _{CD} =
0.831122		0.821+0.035 0.747+0.132	0.567+0.319 0.497+0.393 0.417+0.484 0.327+0.588	0.491+0.393	0.417+0.484	0.321+0.588

t = % imperviousness (expressed as a decimal)

 C_d = Runoff coefficient for Natural Resources Conservation Service (NRCS) HSG A soils

 $C_B = \text{Runoff coefficient for NRCS HSG B soils}$

 C_{CD} = Runoff coefficient for NRCS HSG C and D soils.

TIME OF CONCENTRATION **STANDARD FORM SF-2**

Subdivision: Saddlehorn Ranch Filing 5 Early Grading Location: El Paso County

Project Name: Saddlehorn Ranch
Project No.: 25142.07
Calculated By: WKN
Checked By: TBD
Date: 8/22/23

		-SUB-I	SUB-BASIN			INITI	INITIAL/OVERLAND	AND		ľ	TRAVEL TIME				tc CHECK		
		D.	DATA				(T _i)				(¹L)			<u></u>	(URBANIZED BASINS)	ASINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	ڻ	C ₁₀₀	7	So	t,	1 t	S	К	VEL.	t,	COMP. t	TOTAL	Urbanized t_c	t
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	15.08	А	2%	0.01	0.13	300	4.8%	20.4	1330	2.9%	7.0	1.2	18.6	39.0	1630.0	39.7	39.0
B1	12.57	А	2%	0.01	0.13	282	4.9%	19.6	1160	1.3%	15.0	1.7	11.5	31.2	1442.0	44.3	31.2
B2	12.64	А	7%	0.01	0.13	20	20.0%	3.3	1561	4.6%	15.0	3.2	8.1	11.4	1581.0	38.7	11.4
B3	10.83	А	7%	0.01	0.13	300	2.0%	27.2	1117	3.1%	15.0	2.6	7.0	34.3	1417.0	37.1	34.3
B4	9.16	А	2%	0.01	0.13	300	3.3%	23.1	266	1.5%	15.0	1.8	9.0	32.1	1297.0	40.3	32.1
B5	14.04	А	2%	0.01	0.13	41	9.0%	6.1	3242	1.6%	15.0	1.9	28.9	35.1	3283.0	72.4	35.1
C1	1.26	А	2%	0.01	0.13	143	2.4%	17.7	184	1.0%	15.0	1.5	2.0	19.7	327.0	29.0	19.7
C2	4.19	А	2%	0.01	0.13	154	3.0%	17.1	455	1.0%	15.0	1.5	5.1	22.1	0.609	33.8	22.1
UD1	8.14	А	2%	0.01	0.13	300	3.6%	22.4	267	5.5%	7.0	1.6	2.7	25.1	567.0	7.72	25.1
UD2	25.14	А	2%	0.01	0.13	300	1.7%	28.7	367	4.1%	7.0	1.4	4.3	33.0	0.799	28.9	28.9
EGN	11.03	A	7%	0.01	0.13	300	1.8%	28.2	810	1.3%	7.0	0.8	16.7	8'47	1110.0	38.2	38.2
UD4	2.68	А	2%	0.01	0.13	300	5.1%	19.9	360	2.1%	7.0	1.0	5.9	25.8	0.099	30.1	25.8
051	0.59	А	2%	0.01	0.13	20	5.1%	8.1	029	7.1%	7.0	1.9	0.9	14.1	720.0	30.2	14.1
082	0.68	Α	2%	0.01	0.13	20	1.1%	13.5	345	7.4%	7.0	1.9	3.0	16.6	395.0	27.9	16.6
OS3	3.56	А	2%	0.01	0.13	20	4.0%	8.8	180	3.4%	7.0	1.3	2.3	11.2	230.0	27.4	11.2
084	5.72	А	2%	0.01	0.13	20	2.1%	10.9	180	3.2%	7.0	1.3	2.4	13.3	230.0	27.5	13.3
NOTES:																	
$t_c =$	$t_c = t_i + t_t$				Equation 6-2	1 6-2	$t_i = \frac{0.395(1)}{1}$	$0.395(1.1-C_5)\sqrt{L_i}$				Equation 6-3	5	Type of Land Surface	Surface	Table 0-2. NRCS Conveyance factors, K Land Surface Conveyance Factor.	actor. K
Where:								0						Heavy meadow	ndow	2.5	
$t_c = c c$	omputed time	$t_c =$ computed time of concentration (minutes)	(minutes)			Where:								Tillage/field	eld	5	
14	perland fenities	t = correctiond (initial) flow time (minutes)	toc)				$t_i = \text{overland}$	t_i = overland (initial) flow time (minutes)	ime (minutes)					Short pasture and lawns	nd lawns	7	
0 - 11	Verramo (mito	at) mow time (minut	rics)				$C_5 = \text{runoff}$ $L_i = \text{length o}$	$C_5 = \text{runoff coefficient for 5-yea}$ $L_i = \text{length of overland flow (ft)}$	$C_5 = \text{runoff coefficient for 5-year frequency (from Table 6-4)}$ $L_i = \text{length of overland flow (ft)}$	y (from Table	6-4)			Nearly bare ground	ground	10	
$t_t = cI$	nannelized fle	$t_r = \text{channelized flow time (minutes)}.$					So = average	slope along th	So = average slope along the overland flow path (ft/ft)	path (ft/ft).				Grassed waterway	terway	15	
$t_r = -\frac{1}{6}$	$t_t = \frac{L_t}{60K\sqrt{S_o}} =$	$r = \frac{L_t}{60V_t}$			Equation 6-4	$t_t = (26 - 17i) +$	17i)+	L_{r} $60(14i+9)\sqrt{S_{r}}$				Equation 6-5		Paved areas and shallow paved swales	ow paved swales	20	
Where:						Where:											
$t_t = \text{cha}$ $L_t = \text{wa}$ $S_0 = \text{wa}$ $V_t = \text{tra}$	t_t = channelized flow tim L_t = waterway length (ft) S_0 = waterway slope (ft/ft) V_t = travel time velocity (t_i = channelized flow time (travel time, min) L_i = waterway length (f) S_0 = waterway slope (f/f) V_i = travel time velocity (f/sec) = K_i / S_0	uin)			1. L.	= minimum 1 = length of c : impervious: = slone of the	t_e = minimum time of concentration for first L_i = length of channelized flow path (ff) i = imperviousness (expressed as a decimal) S_i = slone of the channelized flow anth (Hift)	t_e = minimum time of concentration for first design point when less than t_e from Equation 6-1. L_e = length of chamelized flow path (ff) L_e = inpervousness (sepressed as a decimal) L_e = show of the chamelized flow each (ff) L_e	design point w	rhen less than	c from Equatio	ո 6-1.				
A - INE	CCS conveyan	ce factor (see 1 anie	0-5).			Ī	- andag		and the								

Use a minimum tevalue of 5 minutes for urbanized areas and a minimum tevalue of 10 minutes for areas

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name: Saddlehorn Ranch Project No.: 25142.07 Calculated By: WKN Checked By: TBD Date: 8/22/23 Subdivision: Saddlehorn Ranch Filing 5 Early Grading Location: El Paso County
Design Storm: 5-Year

															Da	Date: 8/22/23	22/23			
			٥	DIRECT RUNOFF	UNOFF			Ĭ	TOTAL RUNOFF	JNOFF		SWALE	ш		PIPE		Ę	TRAVEL TIME	IME	
STREET	Jnio9 ngisəO	Ol nizs8	Area (Ac)	Runoff Coeff.	t _c (min) C*A (Ac)	(٦٩/ui) <i>1</i>	Q (cfs)	(nim) 23	(ac) A*O	(٦٩/ui) <i>\</i>	Q (cfs)	Ostreet (cfs) C*A (ac)	(%) ədols	Q _{pipe} (cfs)	(ac) A*O	Slope (%)	Pipe Size (inches) Length (ft)	Velocity (fps)	(nim) 32	REMARKS
	-			5								0.2 0.08	3 1.1				7.	791 2.1	.1 6.3	
	7	Tq.	17:27		31.2 0.0	75.7		_			1	0 0 0 0 0	111			+	$\frac{1}{1}$	21		Swale conveyance to DP 1.0
-	2	82	12.64 (0.01	11.4 0.08	3.94	4 0.3													Noadside Swale Swale conveyance to DP 1.0
												0.3 0.16	5 2.99	L			×	804 3.	3.5 3.9	3.9 Sum of DP 1 and DP 2
	1.0							37.4		0.16 2.15	0.3						+			Swale conveyance to DP 1.1
	ĸ	83	10.83	0.01	34.3 0.06	36 2.28	8 0.1					0.10								U.U Roadside Swale Swale conveyance to DP 1.1
	1.1							41.3	3 0.22	2.00	0.4	0.4 0.22	2 1.0				.5	513 2.	2.0 4.3	4.3 Sum of DP 1.0 & DP 3 Swale conveyance to DP 1.2
												0.1 0.05	5 1.9					0 2.7		0.0 Roadside Swale
	4	84	9.16	0.01	32.1 0.05	35 2.38	8 0.1										-			Swale conveyance to DP 1.2
	1.2							45.6	5 0.27	1.85	0.5	0.5 0.27	9.0	_			ŧ.	488	5.2 5.2	5.55 Sum of DP 1.1 & DP 4 Swale conveyance to DP 1.3
	u	ä	10.01	100	35 1 0.08	عر د عر		_				0.2 0.08	3 1.1					0 2.1		0.0 Swale
	,											0.6 0.35	5 0.5				46	466 1.	1.4 5.5	5.51 Sum of DP 1.3 and DP 5
	1.3							50.8	3 0.35	1.69	9.0									Sheet flow into Sediment Basin 1
-	5	ξ	1 26	100	10.7 7.01	2 11	0 0	~				0.03 0.01	1.9					2.7	۲.	Roadside Swale
	;	1										0.1 0.03	3 1.9				ł	2.7	7	Roadside Swale
	C2	C2	4.19 (0.01 2:	22.1 0.03	33 2.94	4 0.1	1												Swale conveyance to Pond C. See Filing 4 for calculations
	1	۵1	15.08	0.01	39.0 0.15	2 00	0.3	~												Overland Flow Shoot flow into Sodiment Basin 2
																	+			Overland Flow
	UD1	UD1	8.14 (0.01	25.1 0.05	35 2.75	5 0.1	_												Sheet flow into Drainageway WF-R7A
-	I CON	IID2	25.14 (0.01	28.9 0.15	15 2.54	4 0.4													Overland Flow Sheet flow into Drainapeway MS-D6
	-										H			l			-			Overland Flow
	nD3	UD3	11.03 (0.01	38.2 0.07	77 2.12	2 0.1	_												Sheet flow into Drainageway MS-06
	2	2	000	200	25.9 0.02	17.6	-													Overland Flow
	_	5															+			Street flow first Drainageway M3-06 Overland Flow from Off-Site Basin
	021	051	0.59	0.01	14.1 0.00	3.61	1 0.00	0												Sheet flows to Basin B2
	082	082	0.68	0.01	16.6 0.00	3.37	7 0.00													Overland Flow from Off-Site Basin Sheet flows to Basin B3
	083	083	3.56	0.01	11.2 0.02	3.96	6 0.1													Overland Flow from Off-Site Basin Sheet flows to Basin A1
	084	054	5.72 (0.01	13.3 0.03	33 3.70	0 0.1	1												Overland Flow from Off-Site Basin Sheet flows to Basin UD4

Notes: Street and Pipe C*A values are determined by Q/i using the catchment's intensity value. Street and Pipe C*A values

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE) STANDARD FORM SF-3

Subdivision: Saddlehorn Ranch Filing 5 Early Grading Location: El Paso County
Design Storm: 100-Year

Project Name: Saddlehorn Ranch Project No.: 25142.07 Calculated By: WKN Checked By: TBD Date: 8/22/23

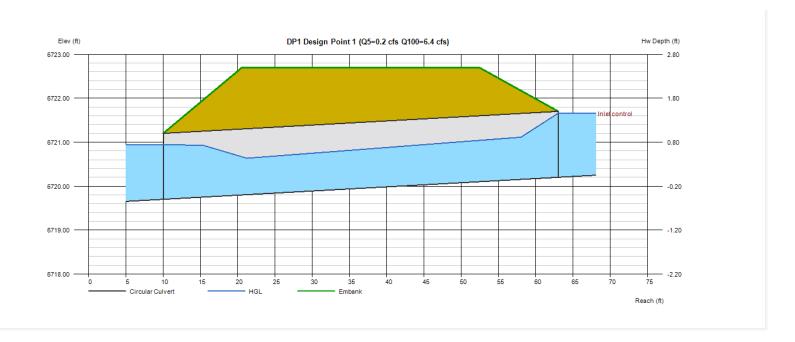
_		,						,																_					
	REMARKS	Roadside Swale	swale conveyance to DF 1.0 Roadside Swale	Swale conveyance to DP 1.0 Sum of DP 1 and DP 2	Swale conveyance to DP 1.1	Roadside Swale Swale conveyance to DP 1.1	Sum of DP 1.0 & DP 3 Swale conveyance to DP 1.2			Swale conveyance to DP 1.3	Swale Overland conveyance to DP 1.3	Sum of DP 1.3 and DP 5	Sheet flow into Sediment Basin 1	Roadside Swale Swale conveyance to Pond C. See Filing 4 for calculations	Roadside Swale	Swale conveyance to Pond C. See Filing 4 for calculations	Overland Flow Sheet flow into Sediment Basin 2	Overland Flow	Sheet flow into Drainageway WF-R7A	Overland Flow Sheet flow into Drainageway MS-06	Overland Flow	Sheet flow into Drainageway MS-06	Overland Flow	Sheet flow into Drainageway MS-U6	Overland Flow from Off-Site Basin Sheet flows to Basin B2	Overland Flow from Off-Site Basin	Sheet flows to Basin B3	Overland Flow from Off-Site Basin Sheet flows to Basin A1.	Overland Flow from Off-Site Basin Sheet flows to Basin UD4
	(nim) 1	3	0.0	3.9)	0.0	4.3	0.0	5.3		0.0	5.5																	
TIMI	Velocity (fps)	2.1	2.1	3.5		2.0	2.0	2.7	1.5		2.1	1.4		2.7	2.7									ı					
TRAVEL TIME	(17) d1gn9J	791	0	804		0	513	0	488		0	466																	
۲	Pipe Size (inches)																							T					
l	(%) ədolS																												
PIPE	(as) A*O																												
	Q _{pipe} (cfs)																							l					
F	(%) ədolS	1.1	1.1	2.99		1.0	1.0	1.9	9.0		1:1	0.5		1.9	1.9									ı					
SWALE	(ac) A*3	1.58	1.59	3.17		1.36	4.53	1.15	5.68		1.77	7.45		0.16	0.53														
2	Qstreet (cfs)	6.4	10.5	11.4		5.2	15.2	4.6	17.7		6.7	21.1		0.8	5.6														
_	Q (cfs)				11.4		15.2			17.7			21.1																
UNOF	(¹d/ni) \				3.61		3.36			3.11			2.83																
TOTAL RUNOFF	(ac) A*O				3.17		4.53			5.68			7.45																
ĭ	(nim) ɔɔ๋				37.4		41.3			45.6			50.8																
	Q (cfs)	·	0.4	10.5		5.2		4.6			6.7			0.8		2.6	6.9		4.7	13.5		4.9	,	T.0	0.4	L (0.5	3.0	4.5
	(14/ni) /			6.61		3.83		3.99			3.77			5.22		4.93	3.50		4.61	4.26		3.55		4.54	6.06		5.66	6.66	6.21
SPF.	(ac) A*O	, L	T.30	I.59		1.36		1.15			1.77			0.16		0.53	1.96		1.03	3.17		1.39		0.35	0.07	000	0.09	0.45	0.72
DIRECT RUNOFF	(nim) st		21.2	11.4		34.3		32.1			35.1			19.7		22.1	39.0		25.1	28.9		38.2	טב טר	72.8	14.1	400	16.6	11.2	13.3
DIRE	Runoff Coeff.	,	CT.O	0.13		0.13		0.13			0.13			0.13		0.13	0.13		0.13	0.13		0.13	,	U.T3	0.13		0.13	0.13	0.13
	Агеа (ас)]	12.37	17.64		10.83		9.16			14.04			1.26		4.19	15.08		8.14	25.14		11.03	0) (7.08	0.59	000	0.68	3.56	5.72
	Ol nize8			P7		B3		B4			85			C		C2	A1	1	UD1	UD2	_	UD3	2	UD4	051		052	083	054
r	Design Point	,	-	7	1.0	3	1.1	4		1.2	2		1.3	C1		C2	11		UD1	UD2		UD3	2	UD4	051		082	083	0S4
	STREET																												

Notes: Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

APPENDIX C HYDRAULIC CALCULATIONS

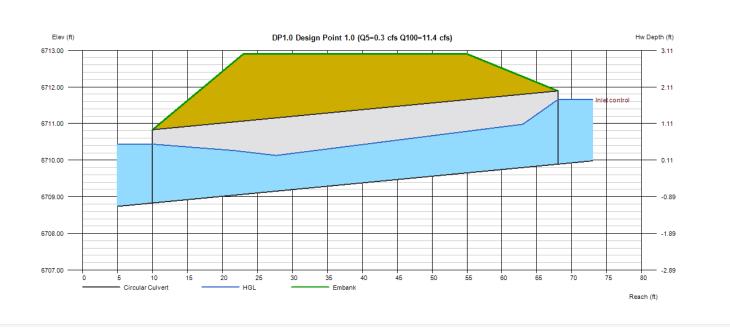
DP1 Design Point 1 (Q5=0.2 cfs Q100=6.4 cfs)

Invert Elev Dn (ft)	= 6719.70	Calculations	
Pipe Length (ft)	= 53.00	Qmin (cfs)	= 0.20
Slope (%)	= 0.94	Qmax (cfs)	= 6.40
Invert Elev Up (ft)	= 6720.20	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0		
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 6.40
No. Barrels	= 1	Qpipe (cfs)	= 6.40
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 4.10
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 5.25
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6720.94
		HGL Up (ft)	= 6721.18
Embankment		Hw Elev (ft)	= 6721.66
Top Elevation (ft)	= 6722.69	Hw/D (ft)	= 0.97
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



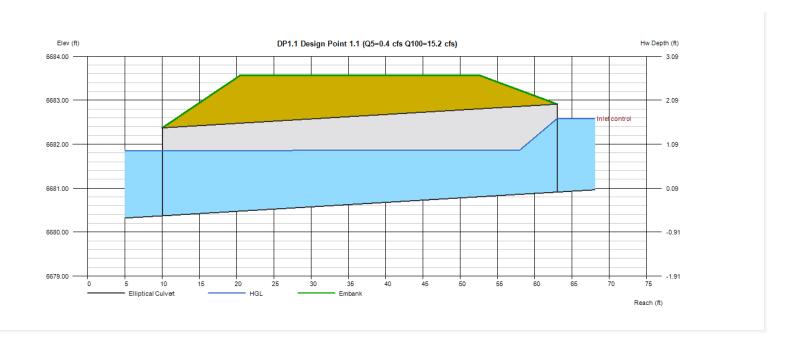
DP1.0 Design Point 1.0 (Q5=0.3 cfs Q100=11.4 cfs)

Invert Elev Dn (ft)	= 6708.83	Calculations	
Pipe Length (ft)	= 58.00	Qmin (cfs)	= 0.30
Slope (%)	= 1.83	Qmax (cfs)	= 11.40
Invert Elev Up (ft)	= 6709.89	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 11.40
No. Barrels	= 1	Qpipe (cfs)	= 11.40
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 4.22
Culvert Entrance	Groove end projecting (C)	Veloc Up (ft/s)	= 5.73
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6710.44
		HGL Up (ft)	= 6711.10
Embankment		Hw Elev (ft)	= 6711.65
Top Elevation (ft)	= 6712.90	Hw/D (ft)	= 0.88
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



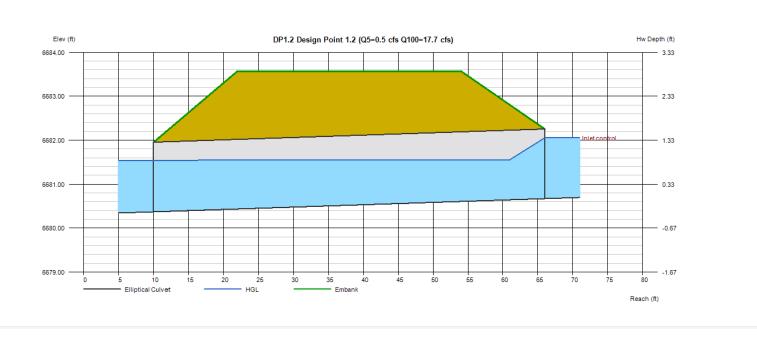
DP1.1 Design Point 1.1 (Q5=0.4 cfs Q100=15.2 cfs)

Invert Elev Dn (ft)	= 6680.37	Calculations	
Pipe Length (ft)	= 53.00	Qmin (cfs)	= 0.40
Slope (%)	= 1.02	Qmax (cfs)	= 15.20
Invert Elev Up (ft)	= 6680.91	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 38.0	Qtotal (cfs)	= 15.20
No. Barrels	= 1	Qpipe (cfs)	= 15.20
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 3.66
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 6.37
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6681.85
		HGL Up (ft)	= 6681.87
Embankment		Hw Elev (ft)	= 6682.58
Top Elevation (ft)	= 6683.57	Hw/D (ft)	= 0.84
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00	-	



DP1.2 Design Point 1.2 (Q5=0.5 cfs Q100=17.7 cfs)

Invert Elev Dn (ft)	= 6680.37	Calculations	
Pipe Length (ft)	= 56.00	Qmin (cfs)	= 0.50
Slope (%)	= 0.54	Qmax (cfs)	= 17.70
Invert Elev Up (ft)	= 6680.67	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 19.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 17.70
No. Barrels	= 2	Qpipe (cfs)	= 17.70
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 3.41
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 4.87
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6681.54
		HGL Up (ft)	= 6681.56
Embankment		Hw Elev (ft)	= 6682.05
Top Elevation (ft)	= 6683.57	Hw/D (ft)	= 0.87
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00	-	



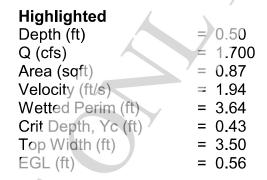
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

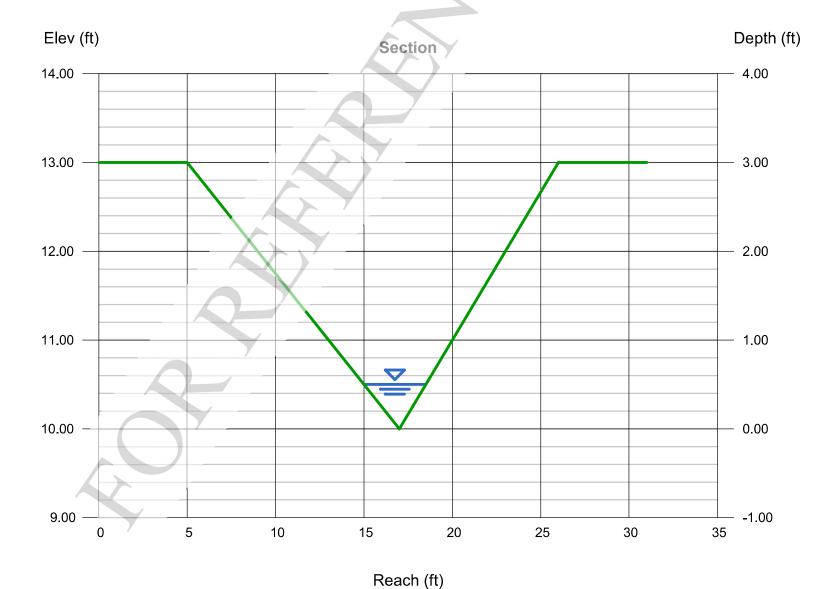
Friday, Jul 21 2023

DP 1 Swale (5-Year)(FR:0.48)

Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.09
N-Value	= 0.030

Calculations
Compute by: Known Q
Known Q (cfs) = 1.70





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Friday, Jul 21 2023

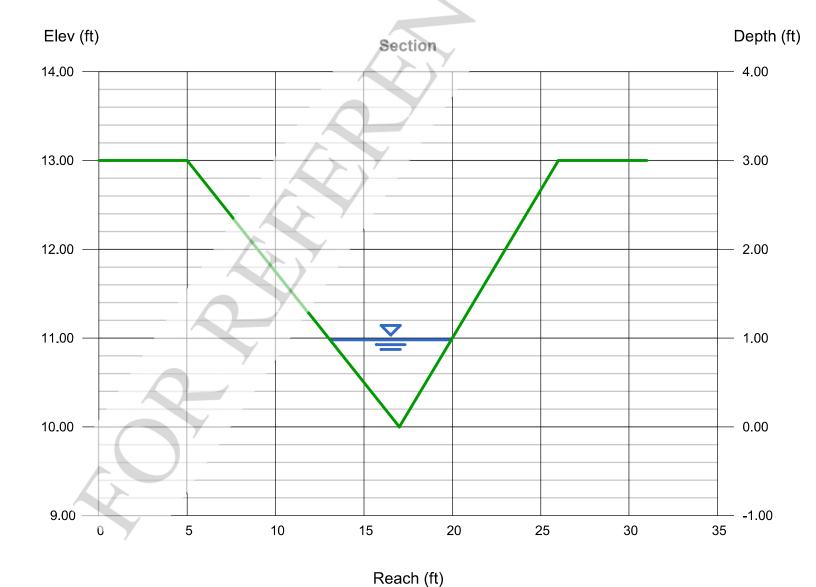
DP 1 Swale (100-Year)(FR:0.56)

Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Elev (ft) Slope (%)	= 10.00 = 1.09
N-Value	= 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 10.50





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Monday, May 8 2023

DP 1.0 Swale (5-Year)(FR:0.66)

Triangular

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

Invert Elev (ft) = 10.00Slope (%) = 2.01N-Value = 0.030

Calculations

Compute by: Known Q = 3.10Known Q (cfs)

Highlighted Depth (ft)

= 0.56Q (cfs) = 3.100 Area (sqft) = (1.10)Velocity (ft/s) 2.82 Wetted Perim (ft) = 4.08= 0.55Crit Depth, Yc (ft) Top Width (ft) = 3.92

EGL (ft)

= 0.68



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Monday, May 8 2023

DP 1.0 Swale (100-Year)(FR:0.76)

ia			

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

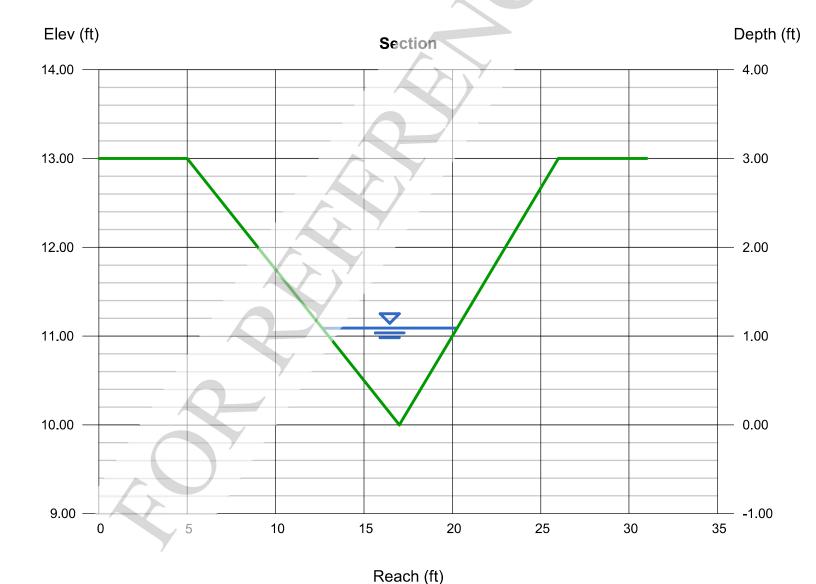
Invert Elev (ft) = 10.00 Slope (%) = 2.01 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 18.70

Highlighted

= 1.09Depth (ft) Q (cfs) = 18.70= 4.16Area (sqft) = 4.50Velocity (ft/s) Wetted Perim (ft) = 7.94 Crit Depth, Yc (ft) = 1.13 Top Width (ft) = 7.63 EGL (ft) = 1.40



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Monday, May 8 2023

DP 1.1 Swale (5-Year)(FR:0.50)

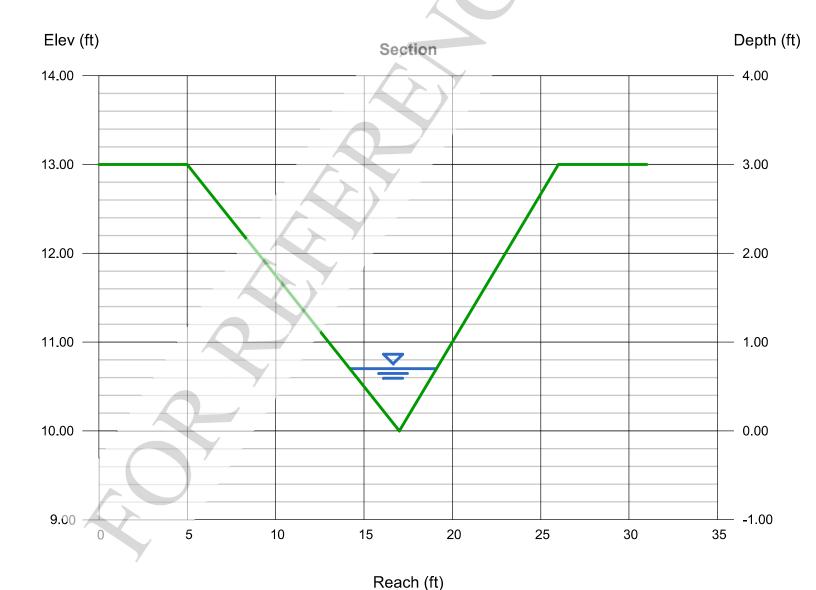
Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 4.10

Highlighted = 0.70Depth (ft) Q (cfs) = 4.100Area (sqft) = 1.71Velocity (ft/s) 2.39 Wetted Perim (ft) = 5.10 Crit Depth, Yc (ft) = 0.62Top Width (ft) = 4.90EGL (ft) = 0.79



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Monday, May 8 2023

DP 1.1 Swale (100-Year)(FR:0.56)

T	r	İ	a	n	g	u	a	r	

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

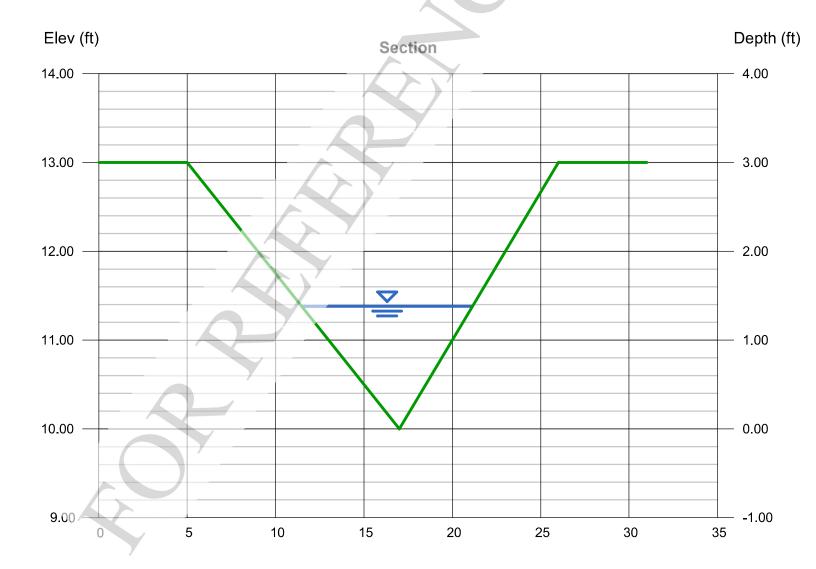
Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 24.90

Highlighted

= 1.38Depth (ft) Q (cfs) = 24.906.67 Area (sqft) Velocity (ft/s) = 3.74 Wetted Perim (ft) = 10.05Crit Depth, Yc (ft) = 1.26Top Width (ft) = 9.66EGL (ft) = 1.60



Reach (ft)

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Monday, May 8 2023

DP 1.2 Swale (5-Year)(FR:0.50)

Triangular

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 4.60

Highlighted Depth (ft)

= 0.74Depth (ft) Q (cfs) = 4.600= 1.92Area (sqft) = 2.40Velocity (ft/s) Wetted Perim (ft) = 5.39 Crit Depth, Yc (ft) = 0.65Top Width (ft) = 5.18 EGL (ft) = 0.83



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, May 8 2023

= 1.68

DP 1.2 Swale (100-Year)(FR:0.56)

Triangular

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

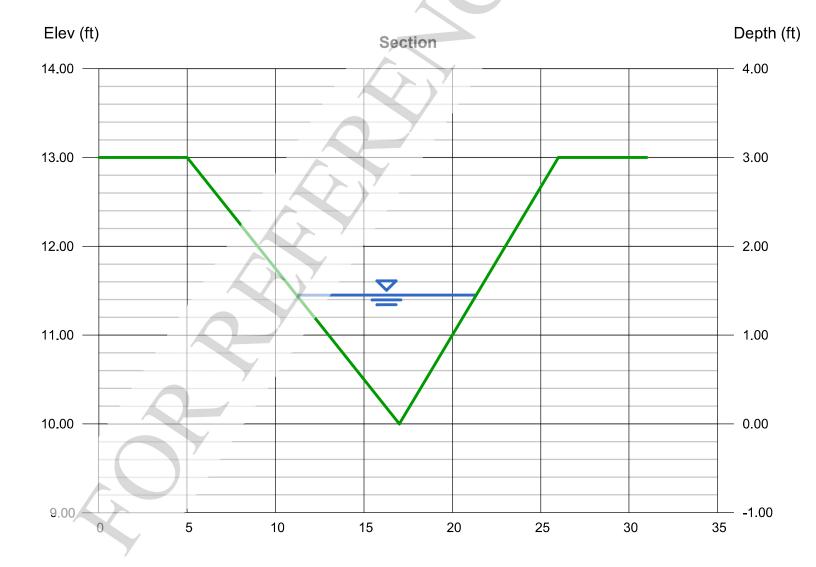
Calculations

Compute by: Known Q Known Q (cfs) = 28.40

Highlighted

EGL (ft)

Depth (ft) = 1.45
Q (cfs) = 28.40
Area (sqft) = 7.36
Velocity (ft/s) = 3.86
Wetted Perim (ft) = 10.56
Crit Depth, Yc (ft) = 1.33
Top Width (ft) = 10.15



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, May 8 2023

DP 1.3 Swale (5-Year)(FR:0.44)

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		а	u	G	_	u		u	а	п
-	-	•	_	_	_	_	-	•	•	•

Bottom Width (ft) = 4.00Side Slopes (z:1) = 4.00, 4.00Total Depth (ft) = 2.00 Invert Elev (ft) = 10.00Slope (%) = 0.50N-Value = 0.030

Calculations

Compute by: Known Q = 5.70Known Q (cfs)

Highlighted Depth (ft)

= 0.52Q (cfs) = 5.700Area (sqft) = 3.16Velocity (ft/s) = 1.80 Wetted Perim (ft) = 8.29Crit Depth, Yc (ft) = 0.36Top Width (ft) = 8.16EGL (ft) = 0.57



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, May 8 2023

DP 1.3 Swale (100-Year)(FR:0.46)

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114		11(1/4)
	2020	IGG

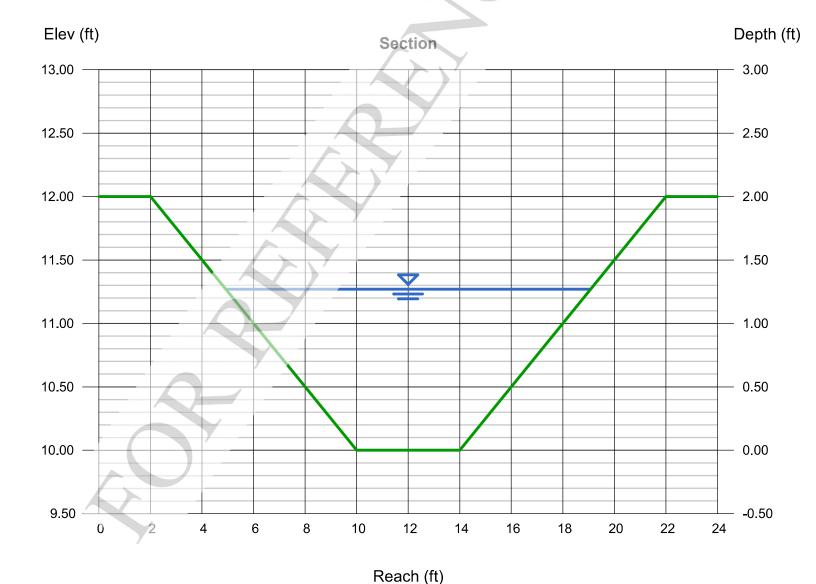
Bottom Width (ft) = 4.00 Side Slopes (z:1) = 4.00, 4.00 Total Depth (ft) = 2.00 Invert Elev (ft) = 10.00 Slope (%) = 0.50 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 34.30

Highlighted

= 1.27Depth (ft) Q (cfs) = 34.30Area (sqft) 11.53 Velocity (ft/s) = 2.97 Wetted Perim (ft) = 14.47 Crit Depth, Yc (ft) = 0.97Top Width (ft) = 14.16 EGL (ft) = 1.41



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Monday, May 8 2023

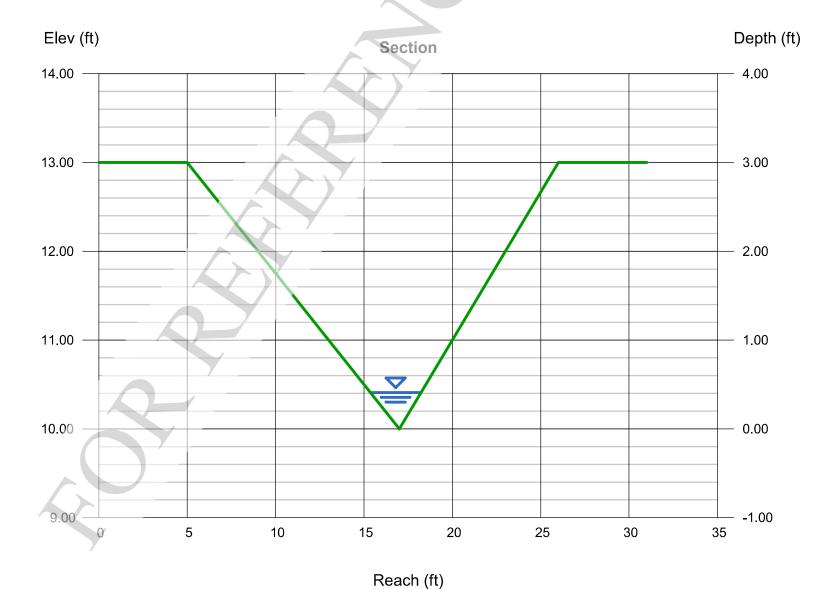
DP 11 Swale (5-Year)(FR:0.70)

Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 2.39
N-Value	= 0.030

Compute by: Known Q Known Q (cfs) = 1.50

Calculations





Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, May 8 2023

DP 11 Swale (100-Year)(FR:0.79)

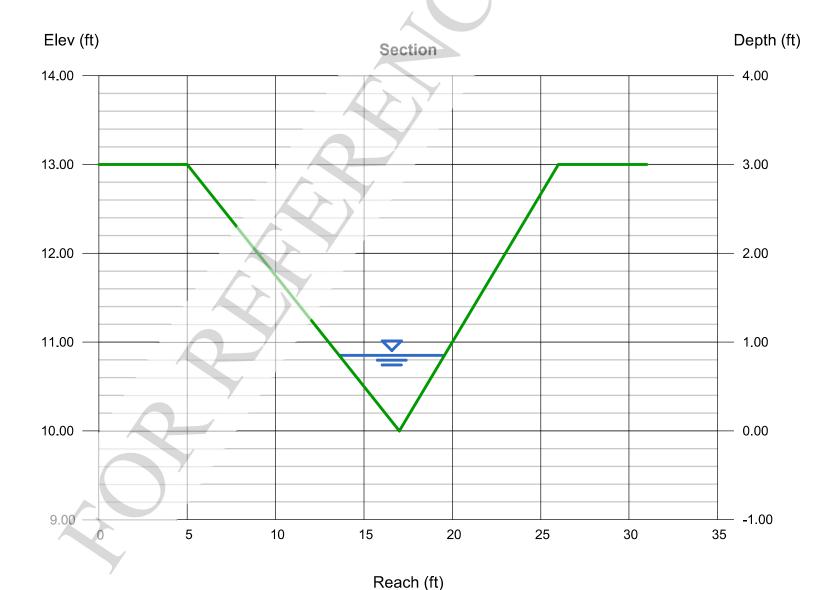
Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 2.39 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 10.40





Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Jul 21 2023

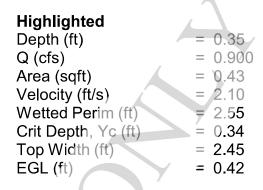
DP C2 Swale (5-Year)(FR:0.63)

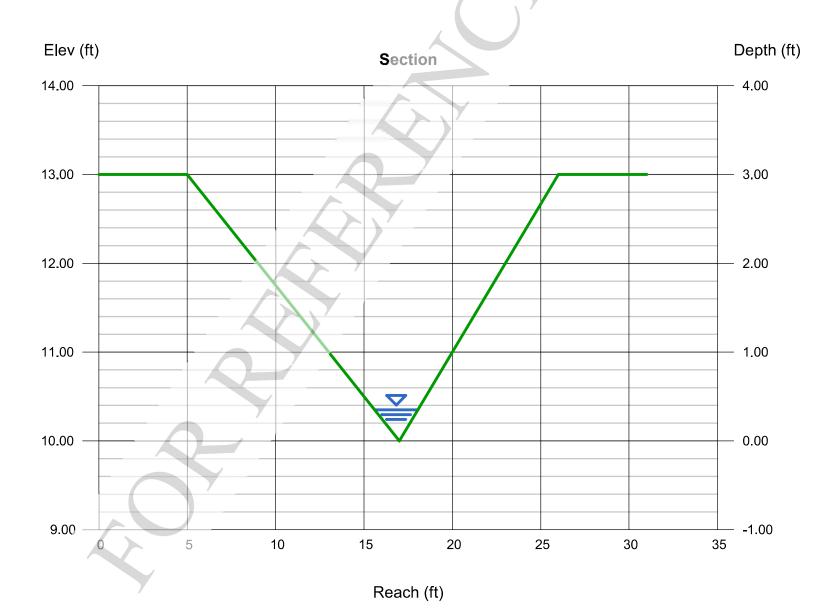
Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
Invert Flev (ft)	= 10.00

Invert Elev (ft) = 10.00 Slope (%) = 2.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 0.90





Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Jul 21 2023

DP C2 Swale (100-Year)(FR:0.68)

Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 2.00
N-Value	= 0.030

Calculations
Compute by: Known Q
Known Q (cfs) = 4.80





APPENDIX D WATER QUALITY AND DETENTION CALCULATIONS

Saddlehorn-2514207

Required Sediment Pond Volumes 8/29/2022

	Sediment Basin #1	(north)
Total Area =	60.42	acres
Developed Area =	20.98	acres
Undeveloped Area =	39.44	acres
Required Volume = (D	0ev. Area * 1800 ft^3/a	ac) + (Undev. Area * 500 ft^3/ac)
=	57,484	ft^3
	1.320	AC-FT
	0.660	1/2 VOLUME
L=2xW	196	L

98 W 19,161 pond bottom min (3' depth assumed)

	Sediment Basin #2	(South)	
Total Area =	15.08	acres	
Developed Area =	1.55	acres	
Undeveloped Area =	13.53	acres	
Required Volume =	(Dev. Area * 1800 ft^3/a	ac) + (Undev. Area * 500 ft^3/ac)	
=	9,555	ft^3	
·	0.219	AC-FT	
	0.110	1/2 VOLUME	
L=2xW	170	L	57800 ft3
	85	W	
	3,185	pond bottom min (3' depth assumed)	

Tributary Sub-Basin	Sediment Basin Name	Tributary Acres	Total Detention Volume (ac- ft)	Provided Volume (ac- ft)	Maximum Discharge (cfs)
A	Sediment Basin 2	15.08	0.219	0.279	0.0331
В	Sediment Basin 1	60.42	1.320	2.315	0.1997

76645.33 ft3

Saddlehorn (25142.07) Orifice Sizing

Sediment Basin #1

Basin Total Volume:	1.320	ac-ft	
Top 1/2	0.660	ac-ft	
	28750	cf	
Drain Time 40 hrs	0.1997	cfs	over 40 hrs
	Assuming	5	holes
	0.0399	cfs	per hole
Equates to a	1.25	diam. hole (in)	
Equates to a	1.23	sq. in. hole	
			_
Solution	5	1 Column - 5 holes	
	1.25	Inch diameter holes	

Saddlehorn (25142.07) Orifice Sizing

Sediment Basin #2

Solution	5	1 Column - 5 holes
Equates to a	1.23	sq. in. hole
Equates to a	1.25	diam. hole (in)
	0.0066	cfs
	Assuming	5
Drain Time 40 hrs	0.0331	cfs
	4770	cf
Top 1/2	0.110	ac-ft
Basin Total Volume:	0.219	ac-ft

1.25

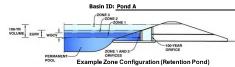
Inch diameter holes

over 40 hrs holes per hole

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Saddlehorn Filing 5



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	15.08	acres
Watershed Length =	1,659	ft
Watershed Length to Centroid =	794	ft
Watershed Slope =	0.048	ft/ft
Watershed Imperviousness =	10.10%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Rainfall Denths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Proced	dure.
Water Quality Capture Volume (WQCV) =	0.085	acre-feet
Excess Urban Runoff Volume (EURV) =	0.112	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.055	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.094	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.126	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.330	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.534	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.822	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	1.456	acre-feet
Approximate 2-yr Detention Volume =	0.067	acre-feet
Approximate 5-yr Detention Volume =	0.092	acre-feet
Approximate 10-yr Detention Volume =	0.121	acre-feet
Approximate 25-yr Detention Volume =	0.164	acre-feet
Approximate 50-yr Detention Volume =	0.221	acre-feet
Approximate 100-yr Detention Volume =	0.358	acre-feet
		_

Define Zones and Basin Geometry

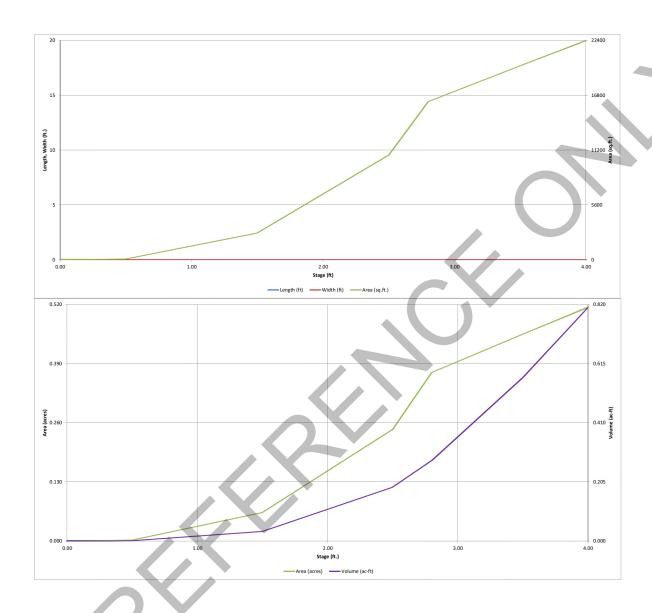
Zone 1 Volume (WQCV) =	0.085	acre-f
Zone 2 Volume (EURV - Zone 1) =	0.027	acre-f
Zone 3 Volume (100-year - Zones 1 & 2) =	0.245	acre-f
Total Detention Basin Volume =	0.358	acre-f
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (Htotal) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Calcula	ted Total Basin Volume (V_{total}) =	user	acre-fe
	Volume of Main Basin (V _{MAIN}) =	user	ft ³
	Area of Main Basin $(A_{MAIN}) =$	user	ft 2
	Width of Main Basin $(W_{MAIN}) =$	user	ft
	Length of Main Basin $(L_{MAIN}) =$	user	ft
	Depth of Main Basin $(H_{MAIN}) =$	user	ft
	Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
	Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
	Width of Basin Floor (W_{FLOOR}) =	user	ft
	Length of Basin Floor $(L_{FLOOR}) =$	user	ft
	Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
9	furcharge Volume Width $(W_{ISV}) =$	user	ft
5	furcharge Volume Length $(L_{ISV}) =$	user	ft
	Initial Surcharge Area $(A_{ISV}) =$	user	ft ²

Depth Increment =		ft							
Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
Top of Micropool		0.00				36	0.001		
6661.83		0.33		-		50	0.001	14	0.000
6662		0.50				75	0.002	25	0.001
6663		1.50				2,724	0.063	1,424	0.033
6664		2.50				10,676	0.245	8,124	0.187
6664.3		2.80				16,135	0.370	12,146	0.279
6665		3.50				19,821	0.455	24,730	0.568
6665.5		4.00				22,375	0.514	35,279	0.810

		6664		2.50	-			10.676	0.003	0.124	0.033
		6664		2.50				10,676	0.245	8,124	0.187
		6664.3		2.80				16,135	0.370	12,146	0.279
		6665		3.50				19,821	0.455	24,730	0.568
		6665.5		4.00				22,375	0.514	35,279	0.810
						-					
											4
Optional User	r Overrides										
	acre-feet										
	acre-feet										
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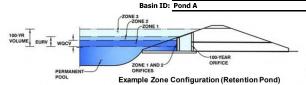
MHFD-Detention_v4-06 Pond A.xism, Basin 8/24/2022, 8:56 AM



MHFD-Detention_v4-06 Pond Axism, Basin

MHFD-Detention, Version 4.06 (July 2022)

Project: Saddlehorn Filing 5



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.99	0.085	Orifice Plate
Zone 2 (EURV)	2.16	0.027	Circular Orifice
Zone 3 (100-year)	3.01	0.245	Weir&Pipe (Restrict)
	Total (all zones)	0.358	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 1.99 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 8.00 inches

Orifice Plate: Orifice Area per Row = 0.33 sq. inches (diameter = 5/8 inch)

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.66	1.33					
Orifice Area (sq. inches)	0.33	0.33	0.33					

be district	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

(relative to basin bottom at Stage =

User Input: Vertical Orifice (Circular or Rectangular)

Depth at

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	1.99	N/A	ft (relative to basin bottom at Stage = 0 ft)
t top of Zone using Vertical Orifice =	2.16	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	0.38	N/A	inches

Calculated Parameters for Vertical Orifice				
Zone 2 Circular	Not Selected			
0.00	N/A	ft ²		
0.02	N/A	feet		
	Zone 2 Circular 0.00	Zone 2 Circular Not Selected 0.00 N/A		

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	2.17	N/A	ft (rel
Overflow Weir Front Edge Length =	3.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Grate Type =	Type C Grate	N/A	
Debris Clogging % =	0%	N/A	%

t Pipe	Pipe) Calculated Parameters for Overflow We			
		Zone 3 Weir	Not Selected	
= 0 ft	Height of Grate Upper Edge, $H_t =$	2.17	N/A	feet
	Overflow Weir Slope Length =	4.00	N/A	feet
	Grate Open Area / 100-yr Orifice Area =	8.28	N/A	
	Overflow Grate Open Area w/o Debris =	8.35	N/A	ft ²
	Overflow Grate Open Area w/ Debris =	8.35	N/A	ft ²
				_

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

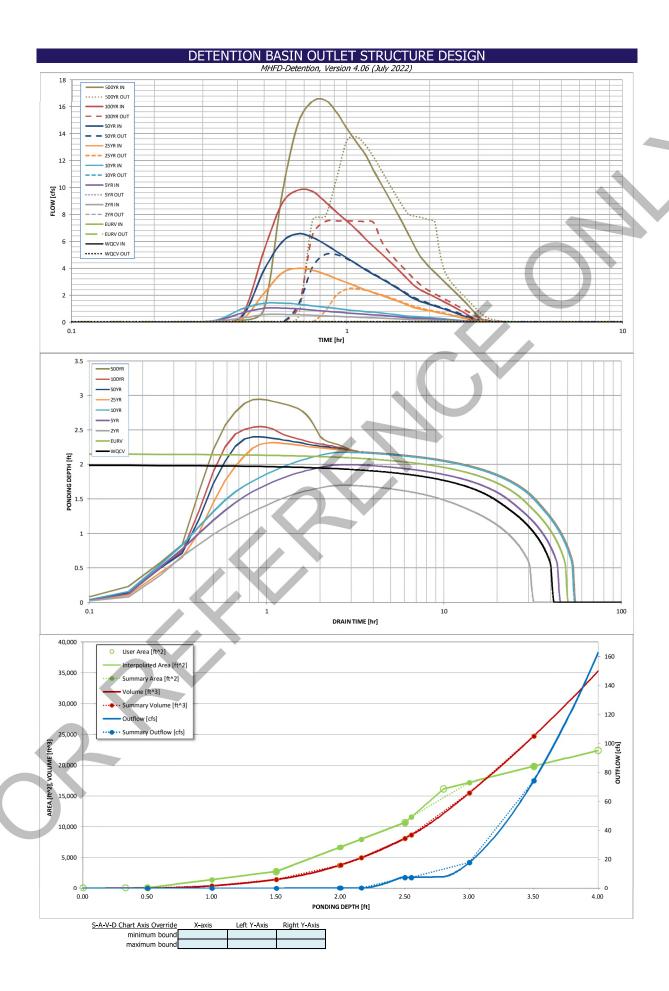
	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.33	N/A	☐ f
Outlet Pipe Diameter =	18.00	N/A	Īi
rictor Plate Height Above Pine Invert =	10.00		-i

Zone 3 Restrictor Not Selected Outlet Orifice Area 1.01 N/A ft (distance below basin bottom at Stage = 0 ft) inches Outlet Orifice Centroid 0.48 N/A feet Half-Central Angle of Restrictor Plate on Pipe : inches 1.68 N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	2.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	35.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF) Design Storm Return Period EURV 10 Year 25 Year 500 Year One-Hour Rainfall Depth (in) CUHP Runoff Volume (acre-ft) N/A N/A 1.19 1.50 1.75 2.00 2.25 2.52 3.14 0.822 0.055 0.534 0.085 0.094 0.126 0.330 1.456 0.112 Inflow Hydrograph Volume (acre-ft) 0.534 1.456 N/A N/A 0.055 0.094 0.126 0.330 0.822 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.1 0.2 0.3 5.0 8.1 14.7 OPTIONAL Override Predevelopment Peak O (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) 0.01 0.01 0.98 0.02 0.16 0.33 0.54 N/A N/A Peak Inflow Q (cfs) N/A N/A 0.6 1.0 1.4 4.0 6.6 9.8 16.5 Peak Outflow Q (cfs) 0.0 0.0 0.0 0.0 0.1 5.0 13.7 Ratio Peak Outflow to Predevelopment O N/A N/A N/A 0.2 0.3 1.0 1.0 0.9 0.9 Structure Controlling Flow Plate Vertical Orifice 1 Plate Plate Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Outlet Plate Spillway Max Velocity through Grate 1 (fps) N/A N/A N/A 0.0 0.3 0.6 Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (hours) N/A 50 N/A N/A N/A N/A N/A N/A N/A N/A 45 41 45 36 28 40 31 Time to Drain 99% of Inflow Volume (hours) 48 43 50 49 46 42 Maximum Ponding Depth (ft) 1,99 2,16 1,70 2,00 2,18 2,31 2,40 2,94 2,55 Area at Maximum Ponding Depth (acres) 0.15 0.18 0,10 0.15 0.18 0,26 0,39 Maximum Volume Stored (acre-ft) =



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	The user can ov	erride the calcul	lated inflow hydr	ographs from th	is workbook with	inflow hydrogra	phs developed i	n a separate prog	ram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval		70077								
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	0:15:00	0.00	0.00	0.02	0.04	0.05	0.03	0.04	0.04	0.06
30	0:20:00	0.00	0.00	0.08	0.11	0.13	0.08	0.10	0.10	0.14
	0:25:00	0.00	0.00	0.32	0.69	1.00	0.25	0.43	0.55	0.99
- 1	0:30:00	0.00	0.00	0.56	1.04	1.41	2.14	3.88	5.33	9.66
10	0:35:00	0.00	0.00		1.05	1.42	3.67		8.87	14.81
- 4	0:40:00	0.00	0.00	0.58 0.56	0.99	1.42	4.00	5.98 6.57	9.81	16.41
	0:45:00									
-4		0.00	0.00	0.51	0.90	1.21	3.85	6.29	9.70	16.50
	0:50:00	0.00	0.00	0.47	0.82	1.10	3.57	5.79	8.95	15.57
	0:55:00	0.00	0.00	0.44	0.76	1.01	3.23	5.24	8.17	14.37
	1:00:00	0.00	0.00	0.40	0.69	0.93	2.94	4.77	7.50	13.34
	1:05:00	0.00	0.00	0.38	0.64	0.85	2.66	4.33	6.87	12.44
1	1:10:00	0.00	0.00	0.35	0.60	0.79	2.40	3.90	6.19	11.26
- 4	1:15:00	0.00	0.00	0.33	0.55	0.75	2.19	3.55	5.61	10.24
	1:20:00	0.00	0.00	0.30	0.51	0.69	2.00	3.23	5.09	9.27
- 1	1:25:00	0.00	0.00	0.28	0.47	0.63	1.81	2.92	4.59	8.34
	1:30:00	0.00	0.00	0.25	0.42	0.56	1.63	2.61	4.10	7.45
1	1:35:00	0.00	0.00	0.23	0.38	0.50	1.44	2.31	3.63	6.58
	1:40:00	0.00	0.00	0.21	0.34	0.45	1.26	2.01	3.16	5.73
10	1:45:00	0.00	0.00	0.20	0.31	0.42	1.10	1.74	2.74	4.98
	1:50:00	0.00	0.00	0.19	0.30	0.39	0.99	1.57	2.44	4.46
10	1:55:00	0.00	0.00	0.18	0.28	0.37	0.91	1.44	2.23	4.06
	2:00:00	0.00	0.00	0.16	0.26	0.34	0.84	1.33	2.05	3.70
	2:05:00	0.00	0.00	0.15	0.24	0.31	0.77	1.21	1.87	3.36
"]	2:10:00	0.00	0.00	0.13	0.21	0.28	0.70	1.10	1.69	3.04
1.0	2:15:00	0.00	0.00	0.12	0.19	0.25	0.63	0.99	1.52	2.72
	2:20:00	0.00	0.00	0.12	0.16	0.22	0.56	0.88	1.35	2.42
16	2:25:00	0.00	0.00	0.09	0.14	0.19	0.49	0.77	1.19	2.13
- 1	2:30:00									
- 1	2:35:00	0.00	0.00	0.08	0.12	0.16	0.42	0.66	1.02	1.84
-4	2:40:00	0.00	0.00	0.07	0.10	0.13	0.35	0.55	0.86	1.55
1.3		0.00	0.00	0.05	0.08	0.11	0.29	0.45	0.70	1.26
-\	2:45:00	0.00	0.00	0.04	0.06	0.08	0.22	0.34	0.53	0.98
	2:50:00	0.00	0.00	0.03	0.04	0.05	0.16	0.24	0.37	0.69
	2:55:00	0.00	0.00	0.02	0.03	0.04	0.10	0.14	0.22	0.42
	3:00:00	0.00	0.00	0.02	0.02	0.03	0.05	0.07	0.12	0.24
	3:05:00	0.00	0.00	0.02	0.02	0.03	0.03	0.04	0.07	0.15
1-4	3:10:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.04	0.10
	3:15:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.03	0.07
	3:20:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.04
	3:25:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.03
	3:30:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02
3)	3:35:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:40:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
9	3:45:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
- 3	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
- 1	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
- 1	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
11	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-1	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow
Description	[ft]	[ft²]	[acres]	[ft³]	[ac-ft]	[cfs]
	0.50	75	0.002	25	0.001	0.01
	1.00	1,400	0.032	393	0.009	0.02
	1.50	2,724	0.063	1,424	0.033	0.03
WQCV	1.99	6,620	0.152	3,714	0.085	0.04
	2.00	6,700	0.154	3,780	0.087	0.04
EURV	2.16	7,972	0.183	4,954	0.114	0.04
2011	2.50	10,676	0.245	8,124	0.187	7.45
100-YR	2.55	11,586	0.266	8,681	0.199	7.53
	3.00	17,188	0.395	15,478	0.355	17.76
	3.50	19,821	0.455	24,730	0.568	74.32
						1
				 		
			l			

For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

POND A FOREBAY VOLUME REQUIREMENTS

Equation 3-1

WQCV= $a(0.91I^3-1.19I^2+0.781I)$ a=1 (40 hour drain time)

Proposed Forebay

I=.101

WQCV= 0.067578

Equation 3-3

V=(WQCV/12)A

Proposed Forebay

A= 15.08 Acres V= 0.085

3% OF WQCV

Forebay Total Volume = .03(V)

Volume Required For Proposed Forebay=

0.003 AC-FT

111 CF

Volume Provided For Proposed Forebay=

0.008 AC-FT

365 CF

Q₁₀₀ Discharges 2% OF Q₁₀₀

Q₁₀₀ Proposed Forebay =

.02*7.5 CFS= .15 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Mar 25 2022

= 0.20

Pond A Spillway

i rapezoidai vveir	
Crest	= Sharp
Bottom Length (ft)	= 35.00
Total Depth (ft)	= 1.20
Side Slope (z:1)	= 4.00

Calculations

Weir Coeff. Cw = 3.10 Compute by: Known Q Known Q (cfs) = 9.30

Highlighted Depth (ft)

Q (cfs) = 9.300 Area (sqft) = 7.16 Velocity (ft/s) = 1.30 Top Width (ft) = 36.60



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Known Q

= 0.15

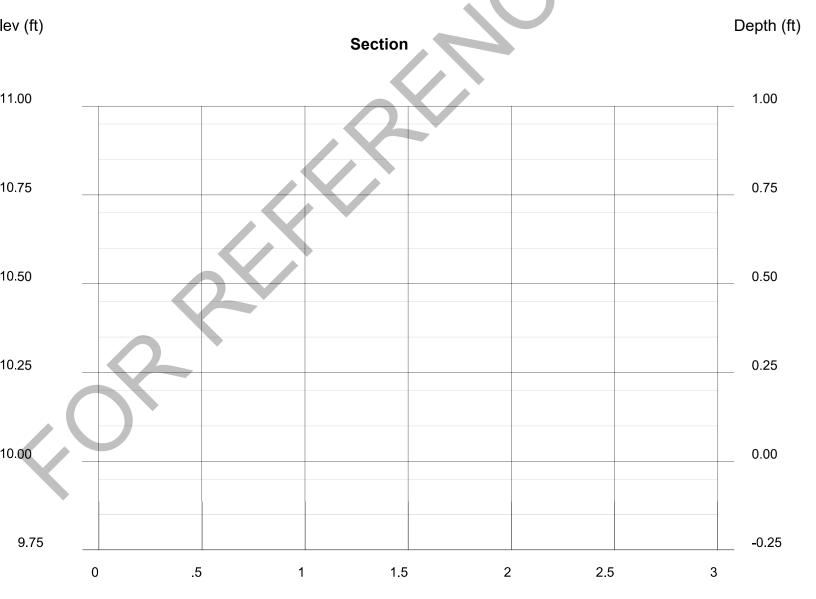
Wednesday, Aug 24 2022

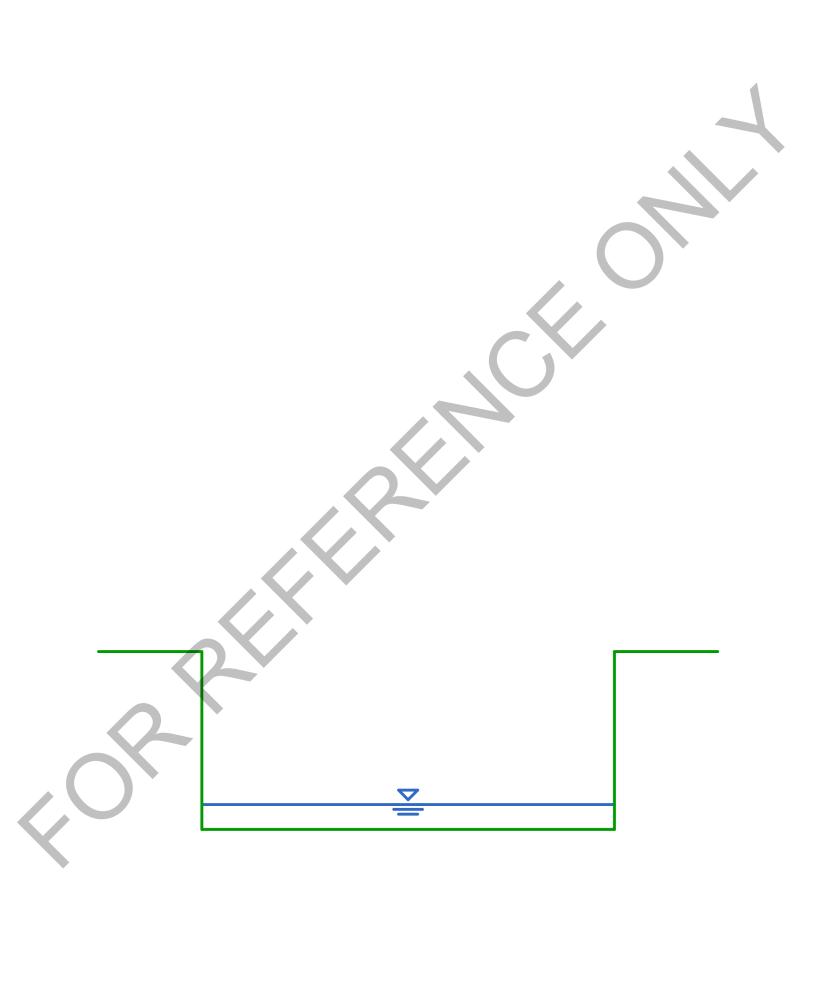
Pond A Trickle Channel

Compute by:

Known Q (cfs)

Rectangular		Highlighted	
Bottom Width (ft)	= 2.00	Depth (ft)	= 0.07
Total Depth (ft)	= 0.50	Q (cfs)	= 0.150
		Area (sqft)	= 0.14
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 1.07
Slope (%)	= 0.50	Wetted Perim (ft)	= 2.14
N-Value	= 0.013	Crit Depth, Yc (ft)	= 0.06
		Top Width (ft)	= 2.00
Calculations		EGL (ft)	= 0.09

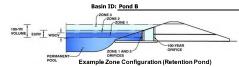




DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Saddehorn Filing 5



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	60.42	acres
Watershed Length =	3,478	ft
Watershed Length to Centroid =	1,805	ft
Watershed Slope =	0.023	ft/ft
Watershed Imperviousness =	11.50%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Painfall Donths =	Hear Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrog	graph Proced	ure.
Water Quality Capture Volume (WQCV) =	0.379	acre-feet
Excess Urban Runoff Volume (EURV) =	0.531	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.279	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.454	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.602	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	1.442	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	2.273	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.438	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	5.999	acre-feet
Approximate 2-yr Detention Volume =	0.320	acre-feet
Approximate 5-yr Detention Volume =	0.438	acre-feet
Approximate 10-yr Detention Volume =	0.572	acre-feet
Approximate 25-yr Detention Volume =	0.768	acre-feet
Approximate 50-yr Detention Volume =	1.006	acre-feet
Approximate 100-yr Detention Volume =	1.563	acre-feet
		-

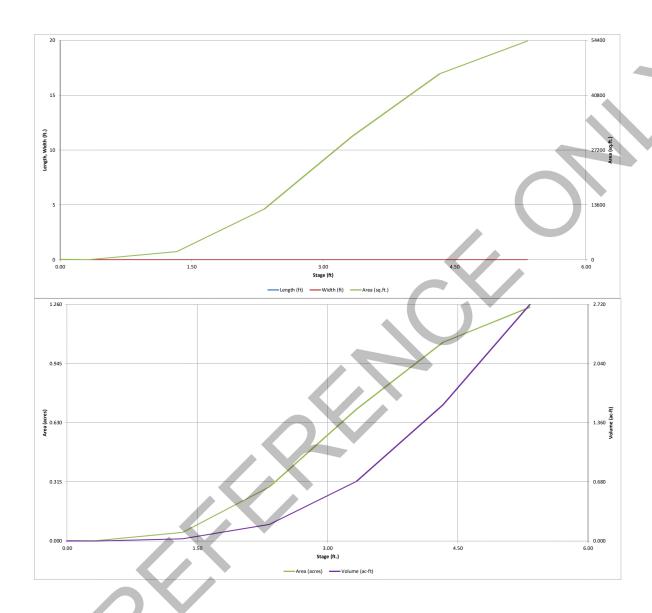
Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.379	acre-
Zone 2 Volume (EURV - Zone 1) =	0.152	acre-
ne 3 Volume (100-year - Zones 1 & 2) =	1.033	acre-
Total Detention Basin Volume =	1.563	acre-
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
tal Available Detention Depth (Htotal) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
Slopes of Main Basin Sides (S _{main}) =	user	

Initial Surcharge Area (A _{ISV}) =	user	ft²
Surcharge Volume Length (LISV) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (LFLOOR) =	user	ft
Width of Basin Floor (WFLOOR) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L _{MAIN}) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft 2
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-fe

				1.							
on Pond)		Depth Increment = Stage - Storage	Stage	ft Optional Override	Length	Width	Area	Optional Override	Area	Volume	Vo l ume
		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft²)	Area (ft 2)	(acre)	(ft ³)	(ac-ft)
		Top of Micropool		0.00		-		36	0.001		
		6675		0.33				50	0.001	14	0.000
		6676		1.33				1,986	0.046	1,032	0.024
		6677		2.33		-		12,572	0.289	8,311	0.191
		6678		3.33				30,573	0.702	29,884	0.686
		6679		4.33				46,107	1.058	68,223	1.566
		6680		5.33				54,237	1.245	118,395	2.718
						-					-
											-
					-	-					
						-					
					-	-					
ptional Use	er Overrides				-						
	acre-feet									-	
	acre-feet										
1.19	inches								7		
1.50	inches										
1.75	inches										
2.00	inches										
2.25	inches										
2.52	inches						-		,		
	inches					-					
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						-					
						-					

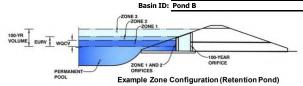
8/24/2022, 8:48 AM MHFD-Detention_v4-06 Pond B.xlsm, Basin



MHFD-Detention_v4-06 Pond B,xlsm, Basin

MHFD-Detention, Version 4.06 (July 2022)

Project: Saddehorn Filing 5



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.82	0.379	Orifice Plate
Zone 2 (EURV)	3.10	0.152	Circular Orifice
Zone 3 (100-year)	4.33	1.033	Weir&Pipe (Restrict)
_	Total (all zones)	1 563	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = N/A Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain Underdrain Orifice Area N/A Underdrain Orifice Centroid = N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate : ft (relative to basin bottom at Stage = 0 ft) 2.82 Orifice Plate: Orifice Vertical Spacing : 11.30 inches Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-3/16 inches) 1.19

Calculated Parameters for Plate WQ Orifice Area per Row 8.264E-03 Elliptical Half-Width = N/A Elliptical Slot Centroid feet N/A ln-² Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.94	1.88					
Orifice Area (sq. inches)	1.19	1.19	1.19					

araban cii	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.82	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.10	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	0.38	N/A	inches

Calculated Parameters for Vertical Orifice Zone 2 Circular Not Selected Vertical Orifice Area 0.00 N/A Vertical Orifice Centroid = 0.02 N/A feet

Calculated Parameters for Spillway

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.11	N/A	ft (rel
Overflow Weir Front Edge Length =	15.00	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V
Horiz. Length of Weir Sides =	5.00	N/A	feet
Overflow Grate Type =	Type C Grate	N/A	1
Debris Clogging % =	0%	N/A	%
_			_

t Pipe)	9	Calculated Parameters for Overflow Weir				
		Zone 3 Weir	Not Selected			
= 0 ft)	Height of Grate Upper Edge, $H_t =$	4.36	N/A	feet		
	Overflow Weir Slope Length =	5.15	N/A	feet		
Gra	ite Open Area / 100-yr Orifice Area =	17.13	N/A			
Ove	erflow Grate Open Area w/o Debris =	53.81	N/A	ft ²		
Overflow Grate Open Area w/ Debris =		53.81	N/A	ft ²		
				_		

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice. Restrictor Plat

Outlet Pipe w/ Flow Restriction Plate (C	Calculated Parameter	s for Outlet Pipe w/ F	-low Restriction Plat	<u>:e</u>			
	Zone 3 Restrictor	Not Selected		677.279.279	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	3.14	N/A	ft²
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	1.00	N/A	feet
trictor Plate Height Above Pipe Invert =	24.00		inches Half-Central Ang	le of Restrictor Plate on Pipe =	3.14	N/A	radians

(relative to basin bottom at Stage =

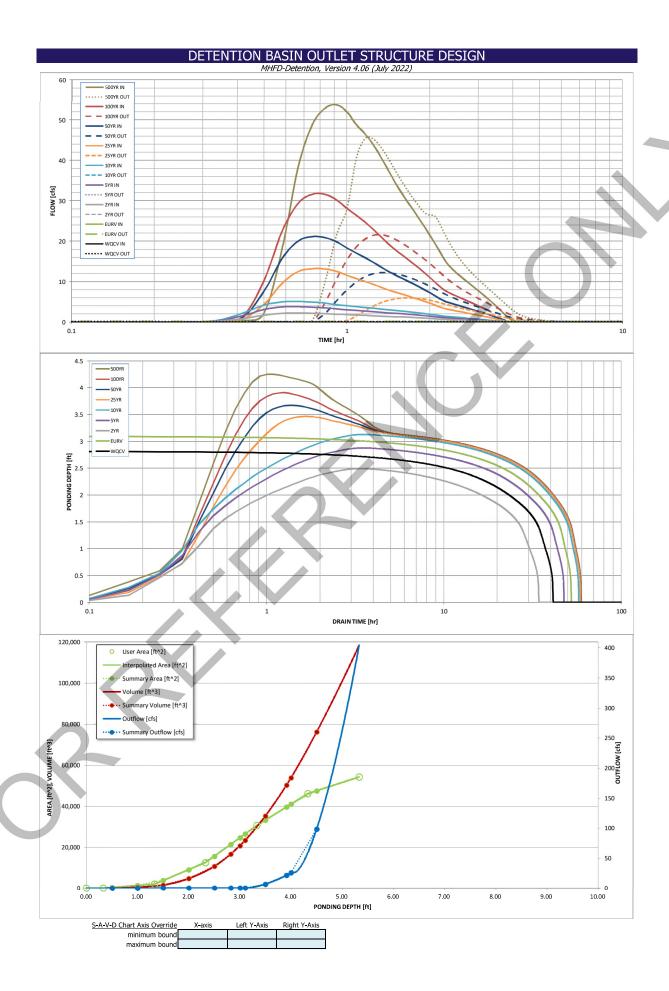
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Restri

Spillway Invert Stage=	4.08	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	85.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	4.00	feet

Spillway Design Flow Depth=	0.24	feet	
Stage at Top of Freeboard =	8.32	feet	
Basin Area at Top of Freeboard =	1.25	acres	
Basin Volume at Top of Freeboard =	2.72	acre-ft	
			t

Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF) Design Storm Return Period **EURV** 10 Year 25 Year 100 Year 500 Year One-Hour Rainfall Depth (in) CUHP Runoff Volume (acre-ft) 3.14 5.999 N/A N/A 1.19 1.50 1.75 2.00 2.25 2.52 0.379 3.438 0.454 0.531 0.279 0.602 2.273 1.442 Inflow Hydrograph Volume (acre-ft) 0.454 0.602 1.442 3.438 5.999 N/A N/A 0.279 2.273 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.3 0.6 0.8 15.1 25.1 46.6 OPTIONAL Override Predevelopment Peak O (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) 0.00 0.77 0.01 0.01 0.12 0.25 0.42 N/A N/A Peak Inflow Q (cfs) N/A N/A 2.3 3.8 5.1 21.2 31.6 53.8 Peak Outflow Q (cfs) 0.2 0.2 0.1 0.2 0.2 6.0 12.3 21.6 45.5 Ratio Peak Outflow to Predevelopment O N/A N/A N/A 0.3 0.3 0.8 0.8 0.9 1.0 Structure Controlling Flow Plate Vertical Orifice 1 Plate Vertical Orifice 1 Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Overflow Weir Spillway Max Velocity through Grate 1 (fps) N/A N/A N/A N/A 0.0 0.1 0.4 Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (hours) N/A 50 N/A N/A N/A N/A N/A N/A N/A N/A 31 43 42 40 33 55 53 51 Time to Drain 99% of Inflow Volume (hours) 50 46 48 Maximum Ponding Depth (ft) 2,88 2,82 3,10 2,49 3,13 3,46 3,67 3,91 4,25 Area at Maximum Ponding Depth (acres) 0.49 0.51 0.82 0.91 1.03 Maximum Volume Stored (acre-ft) =



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	The user can ov	erride the calcul	lated inflow hydr	ographs from th	is workbook with	inflow hydrogra	phs developed i	n a separate prog	ram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.02
1)	0:15:00	0.00	0.00	0.05	0.08	0.10	0.07	0.09	0.08	0.14
310	0:20:00	0.00	0.00	0.22	0.30	0.36	0.23	0.28	0.29	0.40
	0:25:00	0.00	0.00	0.85	1.57	2.17	0.72	1.10	1.32	2.23
- 1	0:30:00	0.00	0.00	1.73	3.13	4.24	4.42	7.67	10.34	18.52
40	0:35:00	0.00	0.00	2.18	3.76	5.02	9.68	15.88	22.71	38.59
- 1	0:40:00	0.00	0.00	2.26	3.82	5.10	12.56	20.11	29.50	48.94
10	0:45:00	0.00	0.00	2.22	3.73	4.97	13.23	21.17	31.65	52.96
-1	0:50:00	0.00	0.00	2.12	3.54	4.70	13.14	20.90	31.61	53.78
48	0:55:00									
	1:00:00	0.00	0.00	1.99	3.28	4.33	12.56	19.89	30.26	52.00
		0.00	0.00	1.87	3.07	4.06	11.59	18.33	28.16	48.82
- 1	1:05:00	0.00	0.00	1.78	2.91	3.83	10.76	17.06	26.39	46.45
	1:10:00	0.00	0.00	1.68	2.75	3.62	10.05	15.90	24.68	43.79
- 3	1:15:00	0.00	0.00	1.58	2.58	3.43	9.33	14.75	22.85	40.63
	1:20:00	0.00	0.00	1.49	2.42	3.24	8.61	13.59	21.01	37.41
- 1	1:25:00	0.00	0.00	1.41	2.29	3.07	7.95	12.51	19.30	34.39
	1:30:00	0.00	0.00	1.35	2.19	2.91	7.40	11.64	17.88	31.84
0.0	1:35:00	0.00	0.00	1.29	2.08	2.75	6.92	10.86	16.65	29.57
. 1	1:40:00	0.00	0.00	1.23	1.96	2.59	6.47	10.13	15.50	27.47
	1:45:00	0.00	0.00	1.16	1.84	2.43	6.02	9.41	14.37	25.44
1 1	1:50:00	0.00	0.00	1.10	1.72	2.27	5.58	8.70	13.26	23.44
-10	1:55:00	0.00	0.00	1.03	1.59	2.11	5.14	7.99	12.16	21.48
	2:00:00	0.00	0.00	0.95	1.47	1.94	4.70	7.28	11.07	19.54
	2:05:00	0.00	0.00	0.87	1.33	1.76	4.25	6.56	9.97	17.60
*1	2:10:00	0.00	0.00	0.79	1.21	1.60	3.79	5.84	8.87	15.68
1-1	2:15:00	150/200	0.00	0.73	1.12	1.49	3.42	5.27	100 (200	0.000
	2:20:00	0.00							8.00	14.19
68	2:25:00	0.00	0.00	0.68	1.05	1.39	3.15	4.87	7.38	13.08
- 1		0.00	0.00	0.63	0.98	1.30	2.95	4.55	6.88	12.16
	2:30:00	0.00	0.00	0.59	0.91	1.21	2.75	4.26	6.43	11.34
	2:35:00	0.00	0.00	0.54	0.84	1.12	2.57	3.98	6.01	10.57
	2:40:00	0.00	0.00	0.50	0.78	1.03	2.40	3.71	5.60	9.83
- 1	2:45:00	0.00	0.00	0.46	0.72	0.95	2.23	3.44	5.19	9.12
	2:50:00	0.00	0.00	0.43	0.66	0.87	2.06	3.18	4.81	8.44
0.3	2:55:00	0.00	0.00	0.39	0.60	0.80	1.89	2.92	4.42	7.77
70	3:00:00	0.00	0.00	0.36	0.55	0.72	1.73	2.67	4.04	7.11
	3:05:00	0.00	0.00	0.32	0.49	0.65	1.57	2.42	3.66	6.44
A -44	3:10:00	0.00	0.00	0.29	0.44	0.58	1.40	2.16	3.28	5.78
	3:15:00	0.00	0.00	0.25	0.39	0.51	1.24	1.91	2.91	5.12
	3:20:00	0.00	0.00	0.22	0.34	0.44	1.08	1.66	2.53	4.47
	3:25:00	0.00	0.00	0.19	0.28	0.37	0.93	1.41	2.15	3.81
- 1	3:30:00	0.00	0.00	0.16	0.23	0.30	0.77	1.16	1.78	3.15
- 1	3:35:00	0.00	0.00	0.13	0.18	0.24	0.61	0.92	1.40	2.50
- 4	3:40:00	0.00	A	0.10		0.17	19 79	100000	100000000000000000000000000000000000000	10 77 71 71
	3:45:00		0.00		0.14		0.45	0.67	1.03	1.85
		0.00	0.00	0.07	0.09	0.12	0.30	0.43	0.67	1.21
	3:50:00	0.00	0.00	0.05	0.07	0.09	0.17	0.23	0.37	0.71
	3:55:00	0.00	0.00	0.05	0.06	80.0	0.10	0.14	0.21	0.44
	4:00:00	0.00	0.00	0.04	0.05	0.07	0.08	0.10	0.14	0.29
	4:05:00	0.00	0.00	0.04	0.05	0.06	0.06	0.08	0.10	0.19
	4:10:00 4:15:00	0.00	0.00	0.03	0.04	0.05 0.04	0.05	0.06	0.07 0.05	0.13 0.09
	4:20:00	0.00	0.00	0.03	0.03	0.04	0.04	0.03	0.03	0.09
	4:25:00	0.00	0.00	0.02	0.03	0.04	0.03	0.04	0.04	0.03
	4:30:00	0.00	0.00	0.02	0.02	0.03	0.03	0.02	0.02	0.03
	4:35:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	4:40:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02
	4:45:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
~	4:50:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	4:55:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
*3	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
41	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
				U.UU	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage Stage Area Area (evit) (evit) (evit) (control control co
0.50 379 0.009 51 0.001 0.03 1.00 1,347 0.031 482 0.011 0.05 1.50 3,786 0.087 1,523 0.035 0.08 2.00 9,079 0.208 4,739 0.109 0.11 2.50 15,632 0.359 10,708 0.246 0.14 WQCV 2.82 21,392 0.491 16,632 0.382 0.16 3.00 24,633 0.565 20,775 0.477 0.17 EURV 3.10 26,433 0.607 23,328 0.536 0.17 3.50 33,214 0.762 35,305 0.811 6.96 100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
1.00
1.50 3,786 0.087 1,523 0.035 0.08 2.00 9,079 0.208 4,739 0.109 0.11 2.50 15,632 0.359 10,708 0.246 0.14 WQCV 2.82 21,392 0.491 16,632 0.382 0.16 3.00 24,633 0.565 20,775 0.477 0.17 EURV 3.10 26,433 0.607 23,328 0.536 0.17 3.50 33,214 0.762 35,305 0.811 6.96 100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
2.00 9,079 0.208 4,739 0.109 0.11
2.50 15,632 0.359 10,708 0.246 0.14
WQCV 2.82 21,392 0.491 16,632 0.382 0.16 3.00 24,633 0.565 20,775 0.477 0.17 EURV 3.10 26,433 0.607 23,328 0.536 0.17 3.50 33,214 0.762 35,305 0.811 6.96 100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
3.00 24,633 0.565 20,775 0.477 0.17 EURV 3.10 26,433 0.607 23,328 0.536 0.17 3.50 33,214 0.762 35,305 0.811 6.96 100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
EURV 3.10 26,433 0.607 23,328 0.536 0.17 3.50 33,214 0.762 35,305 0.811 6.96 100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
3.50 33,214 0.762 35,305 0.811 6.96 100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
100-YR 3.91 39,583 0.909 50,229 1.153 21.71 4.00 40,981 0.941 53,854 1.236 25.86
4.00 40,981 0.941 53,854 1.236 25.86
4.50 47,489 1.090 76,179 1.749 98.81

For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

POND B FOREBAY VOLUME REQUIREMENTS

WQCV= $a(0.91I^3-1.19I^2+0.781I)$ a=1 (40 hour drain time) Equation 3-1

Proposed Forebay I=.115 WQCV= 0.075346

> Equation 3-3 V=(WQCV/12)A

Proposed Forebay A= 60.42 Acres V= 0.379

3% OF WQCV

Forebay Total Volume= .03(V)

Volume Required For Proposed Forebay= 0.011 AC-FT 496 CF

620 CF Volume Provided For Proposed Forebay= 0.014 AC-FT

2% OF Q₁₀₀ Q₁₀₀ Discharges

 Q_{100} Proposed Forebay = .02*31.6 CFS= 0.63 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

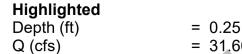
Tuesday, Mar 29 2022

Pond B Spillway

Trapezoidal Weir	
Crest	= Sharp
Bottom Length (ft)	= 85.00
Total Depth (ft)	= 1.25
Side Slope (z:1)	= 4.00

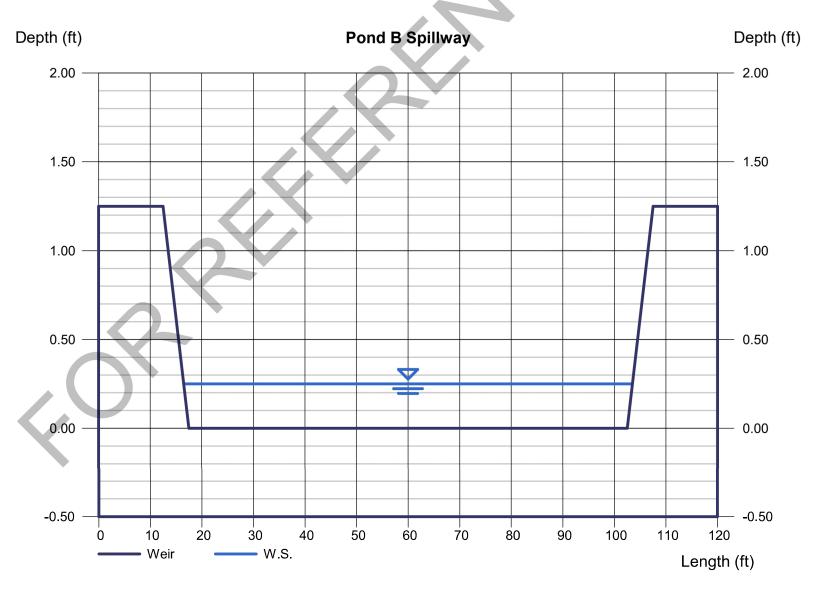
Calculations

Weir Coeff. Cw = 3.10 Compute by: Known Q Known Q (cfs) = 31.60



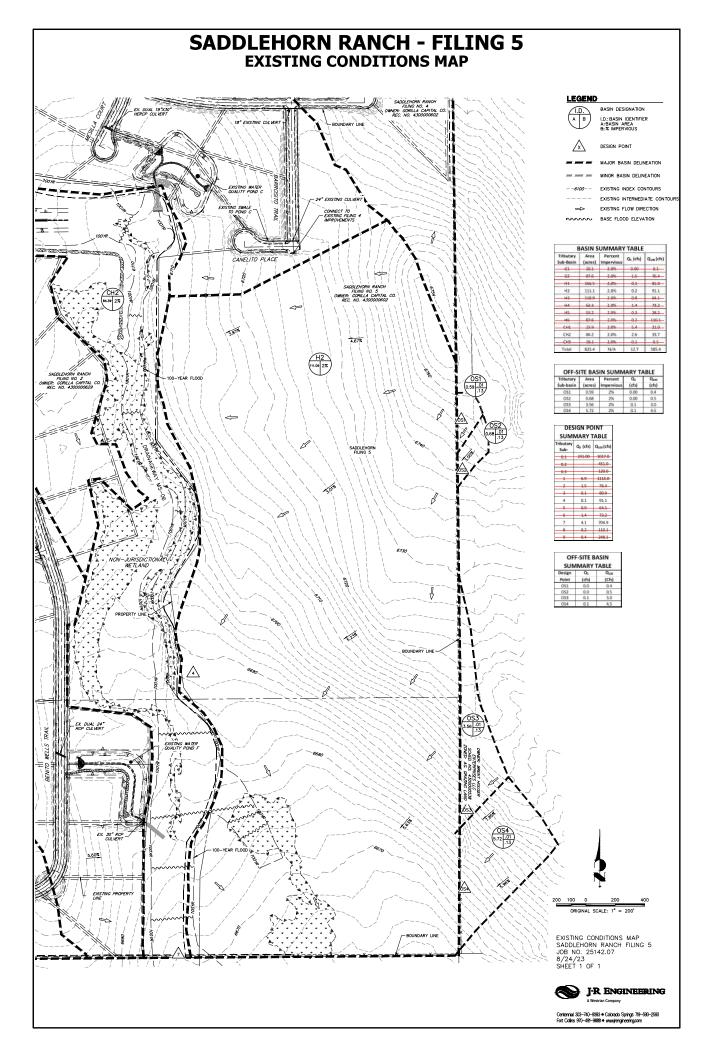
Q (cfs) = 31.60 Area (sqft) = 21.50 Velocity (ft/s) = 1.47

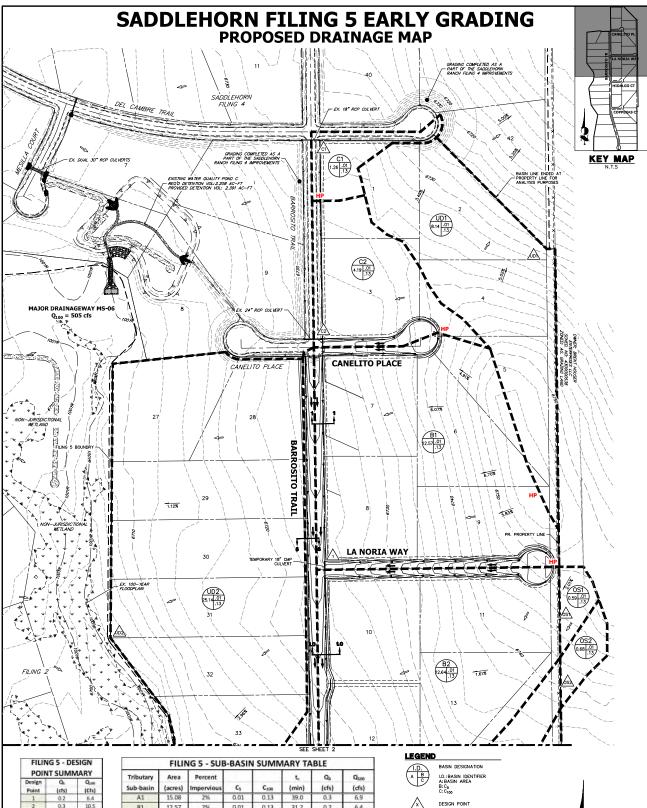
Top Width (ft) = 87.00



APPENDIX E REFERENCE MATERIALS

APPENDIX F DRAINAGE MAPS & PLANS





POINT SUMMARY					
Design	Qi	Qim			
Point	(rfs)	(Cfs)			
1	0.2	6.4			
2	0.3	10.5			
3	0.1	5.2			
4	0.1	4.6			
5	0.2	6.7			
11	E.0	6.9			
CI	0.02	0.6			
C2	0.1	2.6			
UDI	0.1	6.7			
UDZ	0.4	13.5			
UD3	0.1	4.9			
IJD4	0.1	1.6			
1.0	0.3	11.4			
1.1	0.4	15.2			
1.2	0.5	17.7			
1.3	0.6	21.1			
O51	0.00	0.4			
052	0.00	0.5			
053	0.1	3.0			
Q54	0.1	4.5			

Tributary	Area	Percent			t _c	Qs	Q ₁₀₀
Sub-basin	(acres)	Impervious	C ₅	C100	(min)	(cfs)	(cfs)
A1	15,08	2%	0,01	0.13	39.0	0.3	6,9
B1	12.57	2%	0.01	0.13	31.2	0.2	6.4
B2.	12.64	2%	0.01	0.13	11.4	0.3	10.5
B3	10.83	2%	0.01	0.13	34.3	0.1	5.2
B4	9.16	2%	0.01	0.13	32.1	0.1	4.6
B5	14,04	2%	0.01	0.13	35.1	0.2	6.7
C1	1.26	2%	0.01	0.13	19.7	0.02	0.8
C2	4.19	2%	0,01	0.13	22.1	0.1	2.6
UD1	8.14	2%	0,01	0.13	25.1	0.1	4.7
UD2	25.14	2%	0.01	0.13	28.9	0.4	13.5
UD3	11.03	2%	0.01	0.13	38.2	0.1	4.9
UD4	2.68	2%	0,01	0.13	25.8	0.1	1.5
051	0.59	2%	0,01	0.13	14.1	0.00	0,4
052	0.68	2%	0.01	0.13	16.6	0.00	0,5
053	3.56	2%	0.01	0.13	11.2	0.1	3,0
054	5.72	2%	0.01	0.13	13.3	0.1	4.5



PROPOSED INDEX CONTOURS PROPOSED INTERMEDIATE CONTOURS EXISTING FLOW DIRECTION

ΗР PROPOSED HIGH POINT LΡ PROPOSED LOW POINT WETLANDS HATCH

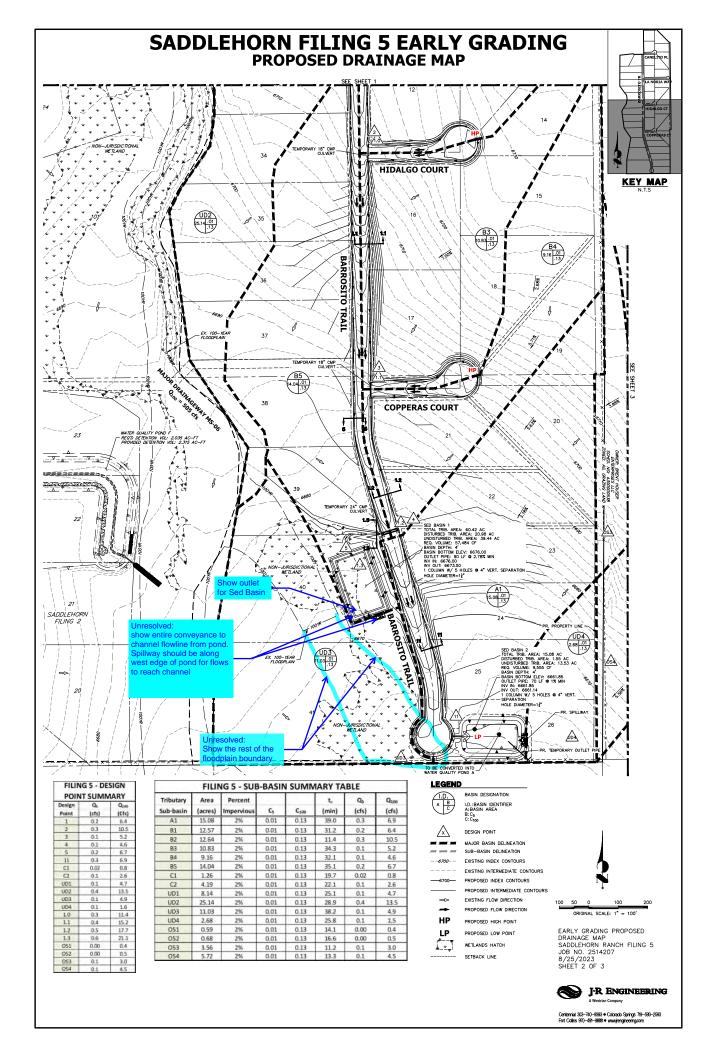
SETBACK LINE

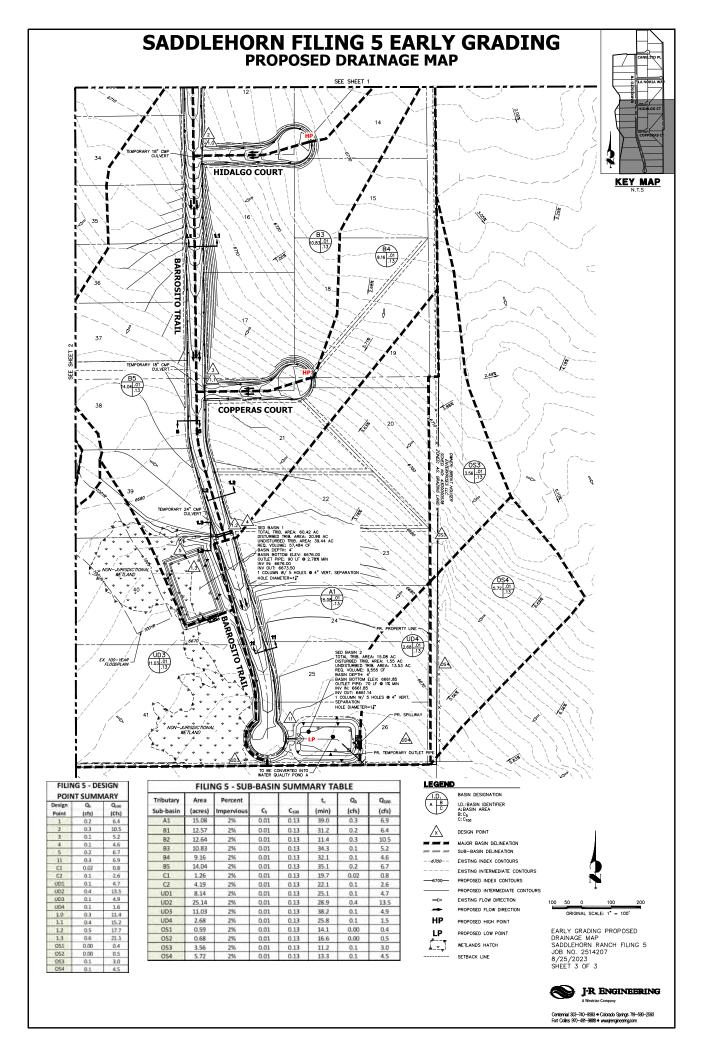


EARLY GRADING PROPOSED DRAINAGE MAP SADDLEHORN RANCH FILING 5 JOB NO. 2514207 8/25/2023 SHEET 1 OF 3

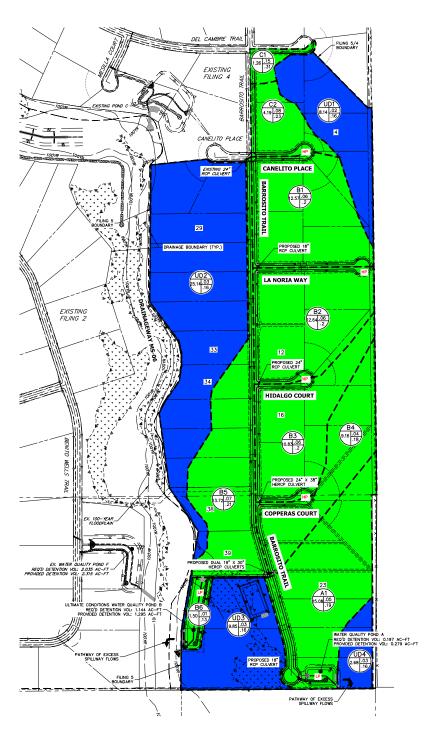


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SADDLEHORN RANCH - FILING 5 PERMANENT APPLICABILITY MAP



LEGEND BASIN DELINEATION

EXISTING INDEX CONTOURS

EXISTING INTERMEDIATE CONTOURS PROPOSED INDEX CONTOURS

PROPOSED INTERMEDIATE CONTOURS PROPOSED HIGH POINT

LP PROPOSED LOW POINT

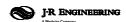
AREA NOT DETAINED IN PBMP PER SECTION 1.7.1.B.5 (RURAL 2.5+ ACRE LOTS W/ IMPERVIOUSNESS < 10%)



ORIGINAL SCALE: 1" = 200'

MS4 PERMIT EXCULSION AREAS SADDLEHORN RANCH FILING 5 JOB NO. 25142.07 5/02/2023 SHEET 1 OF 1

FOR INFORMATION ONLY



v3_Drainage Report - Final.pdf Markup Summary

Callout (5)



Subject: Callout Page Label: 8 Author: CDurham

Date: 10/30/2023 11:14:05 AM

Status: Color: Layer: Space: Finish basin name



Subject: Callout Page Label: 8 Author: CDurham

Date: 10/30/2023 11:15:32 AM

Status: Color: Layer: Space: 59.24 for Basins B1 to B5. Does this include OS1 & OS2? then include them in the discussion that OS1 & OS2 are also diverted to Sed Pond 1



Subject: Callout Page Label: 73

Author: CDurham

Date: 10/30/2023 11:27:29 AM

Status: Color: Layer: Space: Unresolved:

Show the rest of the floodplain boundary



Subject: Callout Page Label: 73

Author: CDurham **Date:** 10/30/2023 11:27:25 AM

Status: Color: Layer: Space: Show outlet for Sed Basin



Subject: Callout Page Label: 73 Author: CDurham

Date: 10/30/2023 11:27:50 AM

Status:
Color: Layer:
Space:

Unresolved:

show entire conveyance to channel flowline from

pond.

Spillway should be along west edge of pond for

flows to reach channel

Text Box (3)



Subject: Text Box Page Label: 5 Author: CDurham

Date: 10/30/2023 11:04:29 AM

Status: Color: Layer: Space: Unresolved:

Add statement regarding CLOMR/LOMR requirements will be completed with subsequent submittals and no floodplain improvements to be

done with early grading.

Subject: Text Box
Page Label: 8
Author: CDurham
Date: 10/30/2023 11:15:21 AM

DA ○ Status: Color: Layer: Space:

46.99

Subject: Text Box Page Label: 8 Author: CDurham

Date: 10/30/2023 11:15:47 AM

f 45.81 acı Status:
Color: Layer:
Space:

(1)



Subject: Page Label: 73 Author: CDurham

Date: 10/30/2023 11:23:33 AM

Status: Color: Layer: Space: