

# **FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 1**

## **EL PASO COUNTY, COLORADO**

April 2018

Prepared for:

**SR Land, LLC  
20 Boulder Crescent, Suite 210  
Colorado Springs, CO 80903**

Prepared by:



**20 Boulder Crescent, Suite 110  
Colorado Springs, CO 80903  
(719) 955-5485**

**Project #09-005  
DSD Project # SF-17-025**

**FINAL DRAINAGE REPORT FOR  
HOMESTEAD AT STERLING RANCH FILING NO. 1**

**DRAINAGE PLAN STATEMENTS**

**ENGINEERS STATEMENT**

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin.

\_\_\_\_\_  
Virgil A. Sanchez, P.E. #37160  
For and on Behalf of M&S Civil Consultants, Inc

**DEVELOPER'S STATEMENT**

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

BY: \_\_\_\_\_  
James F Morley

TITLE: \_\_\_\_\_  
DATE: \_\_\_\_\_

ADDRESS: SR Land, LLC  
20 Boulder Crescent, Suite 210  
Colorado Springs, CO 80903

**EL PASO COUNTY'S STATEMENT**

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
Jennifer Irvine, P.E.  
County Engineer / ECM Administrator

**FINAL DRAINAGE REPORT FOR  
HOMESTEAD AT STERLING RANCH FILING NO. 1**

**TABLE OF CONTENTS**

PURPOSE	4
GENERAL LOCATION AND DESCRIPTION	4
SOILS	4
PREVIOUS STUDIES	5
HYDROLOGIC CALCULATIONS	5
HYDRAULIC CALCULATIONS	5
FLOODPLAIN STATEMENT	5
DRAINAGE CRITERIA	5
EXISTING DRAINAGE CONDITIONS	5
PROPOSED DRAINAGE CHARACTERISTICS	9
EROSION CONTROL	9
CONSTRUCTION COST OPINION	10
DRAINAGE & BRIDGE FEES	10
SUMMARY	11
CONSTRUCTION COST OPINION	12
REFERENCES	13

**APPENDIX**

Vicinity Map  
Soils Map  
FIRM Panel W/ Revised LOMR  
Hydrologic Calculations  
Hydraulic Calculations  
Drainage Map

# **FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 1**

## **PURPOSE**

The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site and to downstream facilities in a safe manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual and any conditions set forth by the approved master drainage development plans.

## **GENERAL LOCATION AND DESCRIPTION**

Homestead at Sterling Ranch Filing No. 1 is located in the NE  $\frac{1}{4}$  of the NW  $\frac{1}{4}$  of Section 33, Township 12 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, and the SE  $\frac{1}{4}$  of the NW  $\frac{1}{4}$  of Section 33, Township 12 South, Range 65 West of the 6<sup>th</sup> Principal Meridian within unincorporated El Paso County, Colorado. The site is bound on the north by Dines Boulevard and platted Tract C, within the Sterling Ranch development. The property is bound to the east by Dines Boulevard and to the west by existing Vollmer Road. The property is bound to the south by the existing Barbarick Subdivision and Tract BB within the Sterling Ranch. Tract BB is planned for residential development and shall be henceforth referred to as Branding Iron Filing No. 1 at Sterling Ranch. Sterling Ranch lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

Homestead at Sterling Ranch Filing No. 1 consists of 19.574 acres and is presently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from northwest to south and southeast at grades that vary between 2% and 4%.

Prior to development Homestead at Sterling Ranch Filing No. 1 is presently zoned "AG for agricultural grazing land, but has been identified to contain residential lots within the Sterling Ranch Filing No. 1 Plat (Tract G) thereby conforming to the type of development approved Sterling Ranch Preliminary Plan. Improvements proposed for the site include paved, streets, trails, utilities, and storm drainage improvements, as normally required in constructed of a residential development. Onsite water quality is provided by the existing FSD Ponds 4, 8 and W-9 which were constructed with Sterling Ranch Filing No. 1 (see MDDPSR).

RS-5000?

## **SOILS**

The soils associated with the drainage area analyzed by this study consist of Pring Coarse Sandy Loam (71) as determined by the mapping provided by the Natural Resources Conservation Service Web Soil Survey. According the information available on the website, this soil has a Hydrologic Soil Group rating of "B". A map showing the proposed site, studied watershed and hydrologic soil group classification is included in the appendix of this report.

## **PREVIOUS STUDIES**

This area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area has been studied in the "Master

Development Drainage Report for Sterling Ranch Filing Nos. 1 & 2, and Final Drainage Report for Sterling Ranch Filing No.1” prepared by MS Civil Consultants, dated April 2017 (henceforth referred to as MDDPSR) and the Sterling Ranch MDDP revised April 2018.

## **HYDROLOGIC CALCULATIONS**

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

## **HYDRAULIC CALCULATIONS**

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

## **FLOODPLAIN STATEMENT**

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0535 F, effective date March 17, 1997 and revised to reflect LOMR, 08-08-O541P, dated July 23, 2009. An annotated FIRM Panel is included in the Appendix.

## **DRAINAGE CRITERIA**

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County’s Engineering Criteria Manual (ECM), 2008). In addition to the aforementioned ECMs, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates) have been utilized to aid in design of the Full Spectrum Detention Facilities when required.

## **EXISTING DRAINAGE CONDITIONS**

Homestead at Sterling Ranch Filing No. 1 site consists of 19.574 acres and is situated west of the Sand Creek Watershed. This area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area was studied in the “Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1” prepared by MS Civil Consultants, dated April 2017. Homestead at Sterling Ranch Filing No. 1 and the surrounding areas, with the exception of the existing Barbarick Subdivision, have recently overlot graded. Please refer to the MDDPSR and Sterling Ranch Early Onsite Grading Plan for information on historic conditions and overlot drainage patterns.

## PROPOSED DRAINAGE CHARACTERISTICS

### General Concept Drainage Discussion

The proposed drainage plan for Homestead at Sterling Ranch Filing No. 1 will mimic and formalize the grading patterns established with both the Sterling Ranch MDDP and the Master Development Drainage Report for Sterling Ranch Filing Nos. 1 & 2, and Final Drainage Report for Sterling Ranch Filing No.1 and with its approval allow for the constructing the internal subdivision roadways, utilities, sidewalks and ultimately the placement of homes. With the prior approval of the Sterling Ranch Filing Nos. 1 & 2, and Final Drainage Report for Sterling Ranch Filing No.1, construction plans have been recently approved by El Paso County which have allowed for the construction of the adjacent Dines Boulevard, Filing 1 Storm sewer infrastructure and the formalization of the adjacent Full Spectrum Detention Facilities (Pond Nos. 4, 8 and W-9) and the outlet structures which are needed to collect and convey the developed drainage to the existing channel. It should be noted that the construction of these facilities are occurring during the writing of this report. The following detailed drainage discussion provides an overview of the proposed development drainage analysis and ensures that no alternation of the planned improvements is necessary.

### Detailed Drainage Discussion

The following is a description of the onsite basins, offsite bypass flows and the overall drainage characteristics for the development of Homestead at Sterling Ranch Filing No. 1 and the Amendment to Master Development Drainage Report for Sterling Ranch Filing No. 1 & 2. The development of Homestead at Sterling Ranch Filing No. 1 consists only of the two cul-de-sacs, an eyebrow, roadways, and lots located within the filing boundary. The proposed development drainage patterns and flow values are generally the same as those recommended within the MDDPSR. The following design points and basin results were determined using the Rational Method. Developed surface flow is designated as Design Points (DP) and flow within the storm sewer as (Pipe Run (PR)). To allow for comparison, an **asterisk (\*)** symbol in the detailed drainage discussions below represents each Basin or Design Point as labeled in the Sterling Ranch Filing Nos. 1 & 2 MDDP.

### Detailed Drainage Discussion (Design Points)

**DP1**, 2.79 acres, consists of proposed residential lots and streets (Basin A) which have been assigned runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year events. Developed runoff of 3.6 cfs and 8.7 cfs has been calculated to reach DP1 as shallow overland and street flows in the 5 and 100 year events respectively. A proposed 15' CDOT type R at-grade inlet will intercept flows of  $Q_5=3.6$  cfs and  $Q_{100}=8.6$  cfs (PR1) and route them under Wheatland road via a proposed 30" RCP to DP2. Although not accounted for in the MDDP, the flow-by of approximately 0.1 cfs in the 100 year event (negligible) is not anticipated to adversely affect the downstream infrastructure.

**DP2**, 2.70 acres, consists of proposed residential lots and streets (Basin B) that have been assigned runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year storm events. Developed runoff of 3.6 cfs and 8.6 cfs has been calculated to reach DP2 as shallow overland and street flows in the two events respectively. A proposed 15' CDOT type R at-grade inlet will intercept flows of  $Q_5=3.6$  cfs and  $Q_{100}=8.5$  cfs will combine with flows from PR1 be routed via a 36" RCP (PR2) to an existing 36" RCP stub in the western

right of way of existing Dines Boulevard. The cumulative flows in PR2 (Q5=7.1 cfs and Q100=17.2 cfs) are just slightly less than the flows documented in the MDDPSR report (Q5=8.0 cfs and Q100=19.3 cfs) (Aka DP2\*). Similar to the inlet at DP1 flow-by of approximately 0.1 cfs in the 100 year event is anticipated to continue to existing Dines Boulevard. The negligible runoff is not anticipated to adversely affect the downstream infrastructure.

**DP3, (Aka DP3\*)**, 2.92 acres, consists of proposed residential lots and streets (Basin C) that have been assigned runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year events. Developed runoff of 4.2 cfs and 10.1 cfs has been calculated to reach DP3. A proposed 10' CDOT type R sump inlet and 18" RCP storm pipe will intercept and convey flood flows of Q5=4.2 cfs and Q100=10.1 cfs to an 18" RCP existing stub. The flows in PR3 are equivalent to the flows documented in the MDDPSR report of Q5=4.2 cfs and Q100=10.1 cfs.

**DP4, (Aka DP4\*)**, 9.36 acres, consists of proposed residential lots Basin D (2.9 ac) and Basin E (5.34 ac) with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and 1.12 acres of streets (Basin F, Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=16.1 cfs and Q100=36.7 cfs has been calculated to reach DP4. A proposed 15' CDOT type R at-grade inlet will intercepted flows of Q5=13.3 cfs and Q100=20.0 cfs prior to combining with flows from PR3 and routed east via an existing 30" RCP to existing FSD Pond 4. The flows at DP4 are equivalent to the flows documented in the MDDPSR report (Q5=16.1 cfs and Q100=36.7 cfs). Flow-by from DP4 will be routed to DP5.

**DP5, (Aka DP5\*)** 0.80 acres, consists of 0.61 acres proposed backyards of residential lots (Basin G) that have assigned runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, as well 0.19 acres of Dines Boulevard (Basin H) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year as well as flow by from DP4. Developed runoff of 4.2 and 19.7 cfs has been calculated to reach DP5 in the two events respectively. An existing 15' CDOT type R at-grade inlet at DP5 will intercept flows of Q5=4.2 cfs and Q100=14.7 cfs. These flows are equivalent to the flows documented in the MDDPSR report (Q5=4.2 cfs and Q100=19.7 cfs). An existing 36" RCP will carry the collected runoff under existing Dines Boulevard towards DP6, while flow-by from DP5 will continue south within Dines Boulevard.

**DP6, (Aka DP5\*)** 4.68 acres, consists backyards of residential lots of 0.43 and 0.61 acres in size (Basins OS3 and OS4) that have been assigned runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year events and 2.1 acre portion of Wheatland Drive and 1.54 acre portion of Dines Boulevard, both with assigned runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year events. Developed runoff of Q5=14.1 cfs and Q100=26.7 cfs has been calculated to reach DP6. An existing 15' CDOT type R at-grade inlet. These flows are equivalent to the flows documented in the MDDPSR report (Q5=14.1 cfs and Q100=26.7 cfs). Flow-by from DP6 will continue south within Dines Boulevard.

**DP7, (Aka DP9\*)** 9.73 acres, consists of proposed residential lots of the planned development located east of the subject site (Basin OS-6) that have been assigned runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year events. Developed runoff of Q5=12.6 cfs and Q100=30.5 cfs has been calculated to reach DP6. An existing 30" RCP will convey runoff to existing FSD Pond 4. The flows in PR7 are approximately equivalent to the flows documented in the MDDPSR report of Q5=12.5 cfs and Q100=30.4 cfs.

DP7?

**DP8,(Aka DP10\*)** 1.97 acres, consists of Basin S (Existing FSD Pond 4) with runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and runoff from PR4, PR6 and PR7. Based upon this drainage analysis the total combined developed runoff to reach DP10 at the existing pond will be  $Q_5=49.2$  cfs and  $Q_{100}=105.39$  cfs for the 5 and 100 year events respectively, which varies just slightly from the MDDPSR flows of  $Q_5=50.0$  cfs and  $Q_{100}=102.9$  cfs that the facility was designed for.

The existing privately maintained facility, as constructed, continues to provide full spectrum detention and water quality for the calculated runoff as planned. The pond will continue to treat approx 27.63 acres, and provide 0.46 ac-ft of water quality storage and 2.915 ac-ft of 100-year storage (refer to UD-Detention worksheet in appendix of this report). According to the updated UD detention worksheet, the slight inflow increase in results in only an increase in the ponding elevation of 0.03' and an increase of 0.6 cfs being released from the pond when compared to the initial design worksheets. Despite the minor increase the pond continues to meet the required drain times and pre-developed flow release rates as necessary with no negative impacts to downstream facilities.

In the event of clogging or total inlet failure, flows at DP8 will over top the existing emergency spillway and outfall into Sand Creek. The existing detention pond will be private and shall be maintained by the Sterling Ranch Metropolitan District (SRMD). Access has been granted to the SRMD and El Paso County for access and maintenance of the private detention pond.

**DP9,(Aka DP10\*)** 3.01 acres, consists of 2.71 acres of existing low density residential (Basin OS1A) that have assigned runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and 0.31 acres of existing west half of Vollmer Road (Basin V1A) with assigned runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of  $Q_5=1.6$  cfs and  $Q_{100}=7.0$  cfs has been calculated to reach an existing 12" CMP culvert (PR8) at DP9. The runoff shall continue south in its historic drainage pattern via an existing road side swale to DP10.

**DP10 (Aka DP63\*),** 9.35 acres, consists of 9.09 acres of existing low density residential (Basin OS1B) that have assigned runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and 0.31 acres of the existing west half of Vollmer Road (Basin V1B) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Runoff reaching DP10, including flows from DP9, are calculated to be  $Q_5=4.8$  cfs and  $Q_{100}=26.3$  cfs in the 5 and 100 year events respectively. Runoff reaching DP 10, is captured by an existing CDOT type D inlet and routed, under Vollmer Road via an existing 24" RCP (PR9). As discussed in the SRMDDP, in the event of clogging, runoff will overtop the local sump condition and the surface runoff shall be routed via historic drainage patterns and an existing road side swale to DP11.

**DP11 (Aka DP 64\*),** 5.85 acres, consists of 5.64 ac existing low density residential (Basin OS1C) with assigned runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and approximately 0.21 ac of the existing west half of Vollmer Road (Basin V1C) with assigned runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Runoff reaching DP11 has been calculated to be  $Q_5=2.2$  cfs and  $Q_{100}=12.3$  cfs for the 5 and 100 year events respectively. An existing CDOT type C inlet and existing 18" RCP (PR10) route the collected runoff under Vollmer Road. These flows combine with flows within the existing 24" 24" RCP (PR9) before continuing to the south via an existing 30" RCP, (PR11) at flow rates of  $Q_5=7.0$  cfs and  $Q_{100}=38.6$  cfs. In the event of clogging, runoff will overtop the sump condition and the surface runoff shall be routed via historic drainage patterns and an existing road side swale to DP12.

**DP12, (Aka DP 64\*),** 104.75 acres, consists of 94.3 and 10.0 acre basins of existing low density residential (Basin OS1D and Basin W-2), that have been assigned runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year storm events and 0.13 and 0.32 acre basins of the existing west half of Vollmer Road (Basin V1D and Basin V2) that have been assigned runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Runoff reaching DP12 has been calculated to be 18.9 cfs and 133.7 cfs in the 5 and 100 year events. An existing 4.0'x14.0' modified CDOT type D inlet will collect the runoff and route it under Vollmer Road, via an existing 54" RCP (PR12) to an existing manhole located within a tract east of the Vollmer Road right of way. **Complete the description of where this flow goes (undetained through the site to Sand Creek).**

**DP13,** 2.04 acres, consists of a portion of Vollmer Road and (Basin RP-2B) with runoff coefficients of 0.63 for the 5-year and 0.76 for the 100-year storm events. Developed runoff of Q5=2.8 cfs and Q100=5.6 cfs has been calculated to reach DP13. The collected surface runoff will be routed existing via curb and gutter to an existing 6.0' wide CDOT Type 5 embankment protector. An existing riprap apron placed at the bottom of the rundown provides to dissipate energy and prevent local scour. Runoff is conveyed southerly in an existing earthen swale that leads to existing Detention Pond W-9.

**DP14 (Aka DP61\*),** 4.03 acres, consists 1.15 acres of rear residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year and 1.60 acres of landscape area and an existing FSD pond (Basin M2) that has been assigned runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and 2.04 acres of the eastern half of existing Vollmer Road and adjacent landscaped areas, which have been assigned runoff coefficients of 0.63 and 0.76 for the 5 and 100 year events respectively as well as flows from DP13. Runoff reaching the existing pond at DP 14 is calculated to be Q5=8.9 cfs and Q100=21.2 cfs, which matches the MDDPSR flows of Q5=8.9 cfs and Q100=21.2 cfs that the facility was designed for.

The existing facility functions to provide full spectrum detention and water quality for runoff calculated to reach DP14. The existing pond will treat approx 5.87 acres, and provide 0.092 ac-ft of water quality storage and 0.638 ac-ft of 100-year storage. As described within the MDDPSR the detention facility is private and shall be maintained by the Sterling Ranch Metropolitan District. Access shall be granted to the owner and El Paso County for access and maintenance of the private detention pond. In the event of clogging or total inlet failure, flows at DP14 will over top the emergency spillway and outfall into a proposed swale which will route flows to an existing Vollmer Road side swale. The peak release rates from Pond W-9 (PR13, Q5=0.6 cfs and Q100=8.7 cfs) are conveyed within an existing 18" RCP to an existing 30" RCP (PR14) (Q5=7.6 cfs and Q100=47.2 cfs). These flows will be combine with flows from PR12 and be routed east, within the Homestead Sterling Ranch Filing No. 1 subdivision, via a 54" RCP, PR15 (Q5=23.8 cfs and Q100=164.1 cfs). These flows will combine with flows from PR16 (Q5=2.8 cfs and Q100=36.8 cfs, release rate Pond 4) and be routed south via a 60" RCP, PR12 (Q5=26.6 cfs and Q100=200.9 cfs). These flows are nearly equivalent to the SRMDDP runoff rates of (Q5=26.5 cfs and Q100=200.3 cfs) which the pipe was designed. The collected runoff will outfall into an existing low tailwater riprap basin at Sand Creek.

**Basin N** 2.08 acres, consists of proposed residential backyard lots and part of Tract L located along the south boundary of Homestead at Sterling Ranch Filing No. 1 with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year. Developed runoff of Q5=1.6 cfs and Q100=5.7 cfs have been calculated for the basin. Runoff from the proposed residential backyard lots will flow to an existing swale that falls along the east boundary of the Barbarick Subdivision. Basin N was part of a larger Basin YY\* that was as discussed

— shall. (Also add to plat note re swales.)

in the MDDPSR. The limited developed flows from Basin N that are discharged to the south are considerably less than the historic flows previously directed toward the Barbarick subdivision as can be seen by noting Basin EX-3A in the Sterling Ranch MDDP Existing Conditions Map. As the backyards are typically permeable, and roof drainage from the back of the house can be directed to the front of the lot water quality treatment is not required for this area. As such the proposed develop shall not adversely affect the downstream infrastructure.

is required unless there is an approved deviation request.

**Basin O** 0.57 acres, consists of planned residential backyard lots located along the south boundary of Homestead at Sterling Ranch Filing No. 1 that have been assigned runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year storm events. Developed runoff of, Q5=0.5 cfs and Q100=1.8 cfs is anticipated to be produced by the basin. Runoff from the proposed residential backyard lots will sheet flows towards the planned Branding Iron at Sterling Ranch Filing No. 1 as discussed in the MDDPSR. Basin O was part of a larger Basin GG\* in the MDDPSR. Runoff from basin O and the flow-by from DP1, 2, 5 and 6 will be collected within existing system within existing Dines Boulevard and detained and released at pre-developed flow rates from FSD Pond 4. Refer to Branding Iron at Sterling Ranch filing No.1 FDR for additional information.

## DETENTION PONDS

### Water Quality/Full Spectrum Detention Facilities

As discussed in the detained drainage summary, developed runoff from Branding Iron at Sterling Ranch Filing No. 1 is conveyed to existing Full Spectrum Detention Ponds No 4, 8 and W-9 in accordance with the Sterling Ranch Filing Nos. 1&2 MDDP. Based upon the provided analysis the ponds are adequate to server there intended purpose and require no modification. This is because this final drainage report and the SR Filing 1 and 2 MDDP were nearly concurrent. Thus the larger scale concept planning was very finite and thus allowed for the developed flow rates to align between the two documents and thereby not requiring modifications to facility which is often common between conceptual and final design. The information provided in this report regarding Ponds 8 and W-9 shall supersede the information presented in the MDDP and should be re-referenced with future design.

## EROSION CONTROL

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. EPC approved “Early Grading Plan for Sterling Ranch Phase I Onsite Grading & Erosion Control”, November 18, 2015. And “Early Grading Plan for Sterling Ranch Phase I Offsite Grading & Erosion Control”, December 3, 2015. Grading and Erosion control operations are currently underway (August 2016). Grading and Erosion Control will cease with the final development of the site in the next 12-36 months.

Address WQCV deviation (maintenance of vegetated buffer/swale to be addressed in deviation request)

## CONSTRUCTION COST OPINION – HOMESTEAD AT STERLING RANCH FILING NO. 1

### Drainage Facilities:

See Construction Cost Opinion for Alternative Sterling Ranch Filing No. 1 MDDP on the next page following the Summary paragraph.

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2017.

## DRAINAGE & BRIDGE FEES – HOMESTEAD AT STERLING RANCH FILING NO. 1

This site is within the Sand Creek Drainage Basin. The 2017 Drainage and Bridge Fees per El Paso County for the Homestead at Sterling Ranch Filing No. 1 site are as follows:

Item	Description	Quantity	Unit Cost	Cost
1	18" RCP	10	\$40 /LF	\$400.00
2	30" RCP	34	\$65 /LF	\$2,210.00
3	36" RCP	36	\$75 /LF	\$2,700.00
4	15' CDOT Type R At-Grade	2	\$6000 /EA	\$12,000.00
5	8' CDOT Type R Sump Inlet	1	\$4700 /EA	<u>\$4,700.00</u>
<b>Total</b>				<b>\$22,010.00</b>

Per Homestead at Sterling Ranch Filing No.1 Plat –

**Total Area**

**19.574 Acres**

### FILING NO. 1 FEES:

<b>Drainage Fees:</b>	19.574	x	42%	\$	16,270.00	=	\$	133756.97
<b>Bridge Fees:</b>	19.574	x	42%	\$	4,929.00	=	\$	<u>40,521.70</u>
<b>Total</b>								<b>\$ 174,275.67</b>

## SUMMARY

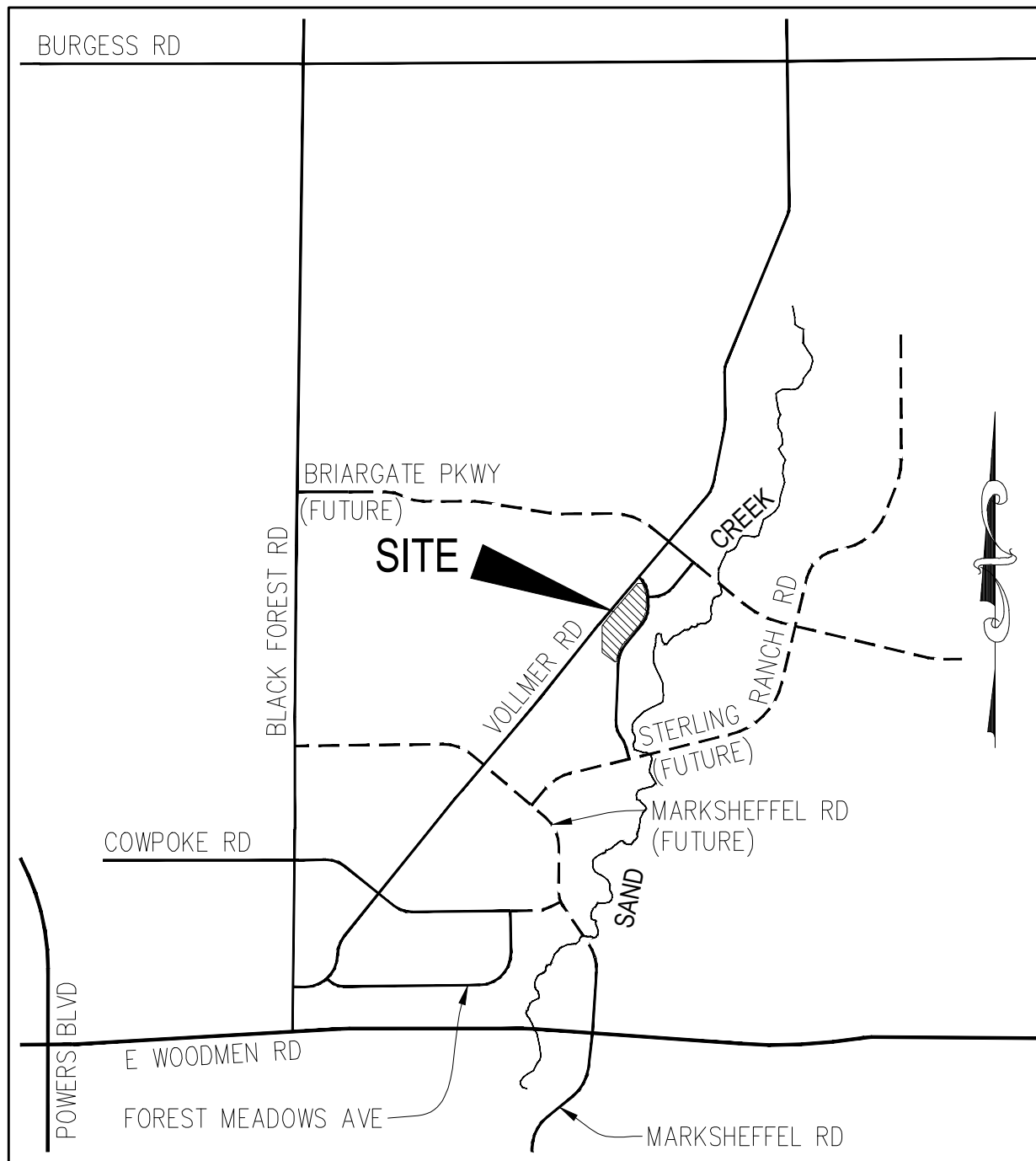
Developed runoff from Homestead at Sterling Ranch Filing No.1 will be conveyed into the existing and proposed drainage systems as shown on the enclosed Drainage Map. The majority of the stormwater will be conveyed to the south within the proposed rights of way and public storm sewer systems to the Existing Pond No. 4 which will provide full spectrum detention. A small portion of the site adjacent to Vollmer Road will drain to existing Full Spectrum Detention Facility W-9, while a small segment of the development adjacent to Branding Iron at Sterling Ranch Filing No.1 will be collected within existing Dines Boulevard and treated by Full Spectrum Detention Facility No.8. All facilities will discharge runoff to Sand Creek at rates that are equivalent or less than the pre-developed condition in patterns that concur with the both the Sterling Ranch MDDP and the Sterling Ranch filing No.1 and 2 MDDP. As such, the development of this site will not adversely affect the surrounding development and is anticipated to have no negative impact to downstream facilities. The detention facilities treating the runoff from Homestead at Sterling Ranch Filing No.1 and the surface and subsurface improvements to convey runoff located outside the public right of way shall be owned and maintained by the Sterling Ranch Metropolitan District..

## REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2.) "Urban Storm Drainage Criteria Manuals, Volumes 1-3"
- 3.) NRSC Web Soil Survey Map for El Paso County. <http://websoilsurvey.nrcs.usda.gov>
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date March 17, 1997.
- 5.) "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996
- 6.) "Preliminary Drainage Report for Sterling Ranch-Phase 1", dated May 2015, by M&S Civil Consultants, Inc.
- 7.) "Sterling Ranch-Phase 1 Offsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 8.) "Sterling Ranch-Phase 1 Onsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 9.) "Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3 & 4, by Matrix Design Group, dated June 2016.
- 10.) "Preliminary and Final Drainage Report, Barbarick Subdivision, A Replat of Lot "D", McClintock Subdivision", El Paso County, Revised August 15, 2007, prepared by Oliver E. Watts, Consulting Engineer, Inc.
- 11.) "Master Development Drainage Plan For Sterling Ranch", prepared by M&S Civil Consultants, Inc., dated July 2010 (Draft not approved)
- 12.) "Technical Memorandum Sand Creek Channel Study (North of Woodmen Road) Hydrologic Analysis" (TM-SCCS) prepared by M&S Civil Consultants, Inc., dated July 2016
- 13.) "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2 and Final Drainage Report for Sterling Ranch Filing No. 1", prepared by M&S Civil Consultants, Inc., dated April 2017
- 14.) "Master Development Drainage Report for Sterling Ranch, prepared by M&S Civil Consultants, Inc., dated April 2018

## **APPENDIX**

## **VICINITY MAP**

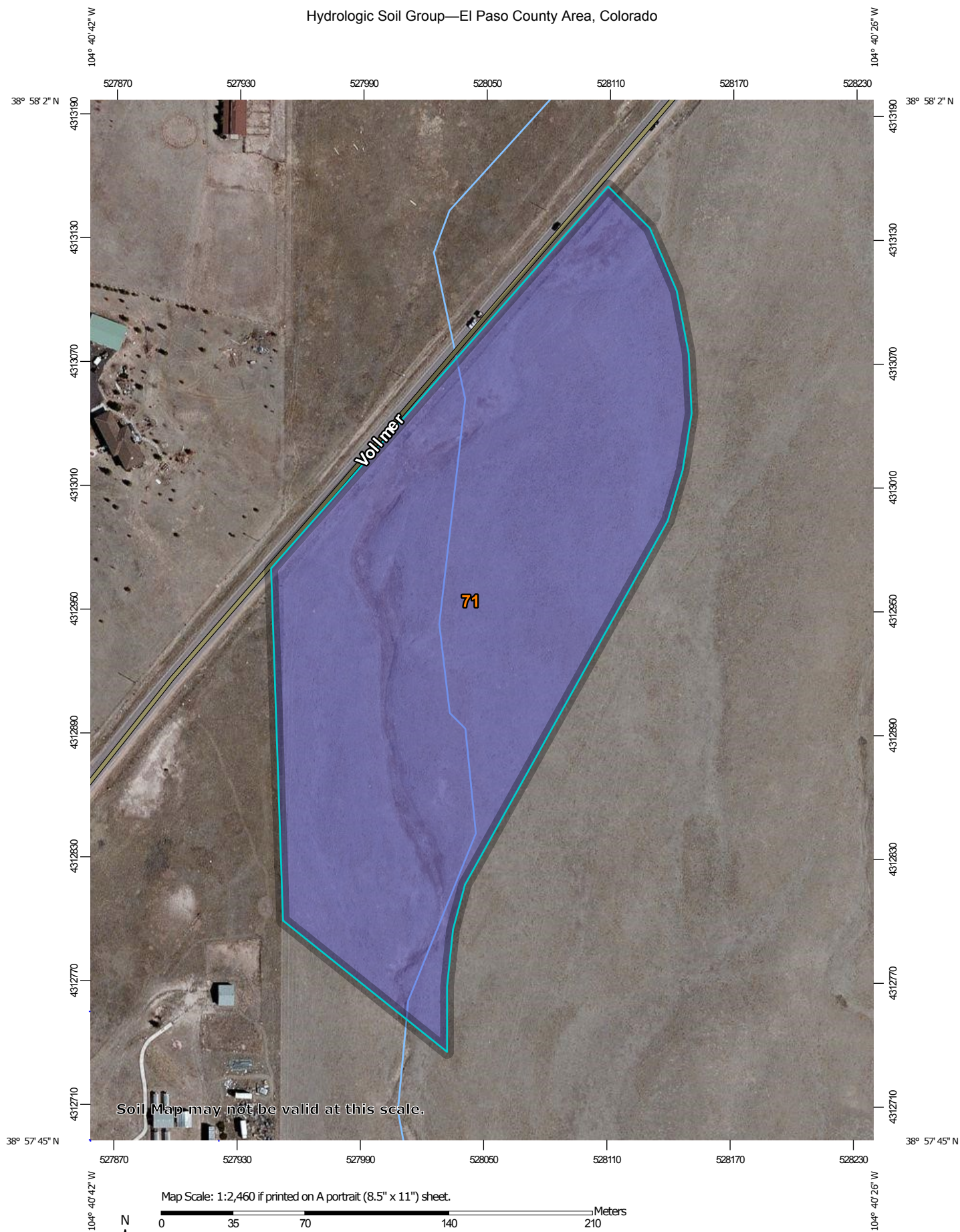


## VICINITY MAP

N.T.S.


## **SOILS MAP**

# Hydrologic Soil Group—El Paso County Area, Colorado



## MAP LEGEND

### Area of Interest (AOI)









 Area of Interest (AOI)

### Soils

#### Soil Rating Polygons





 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Lines

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Points






 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available


### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 14, Sep 23, 2016

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Apr 15, 2011—Sep 22, 2011

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — El Paso County Area, Colorado (CO625)				
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71	Pring coarse sandy loam, 3 to 8 percent slopes	B	11.3	100.0%
<b>Totals for Area of Interest</b>			<b>11.3</b>	<b>100.0%</b>

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

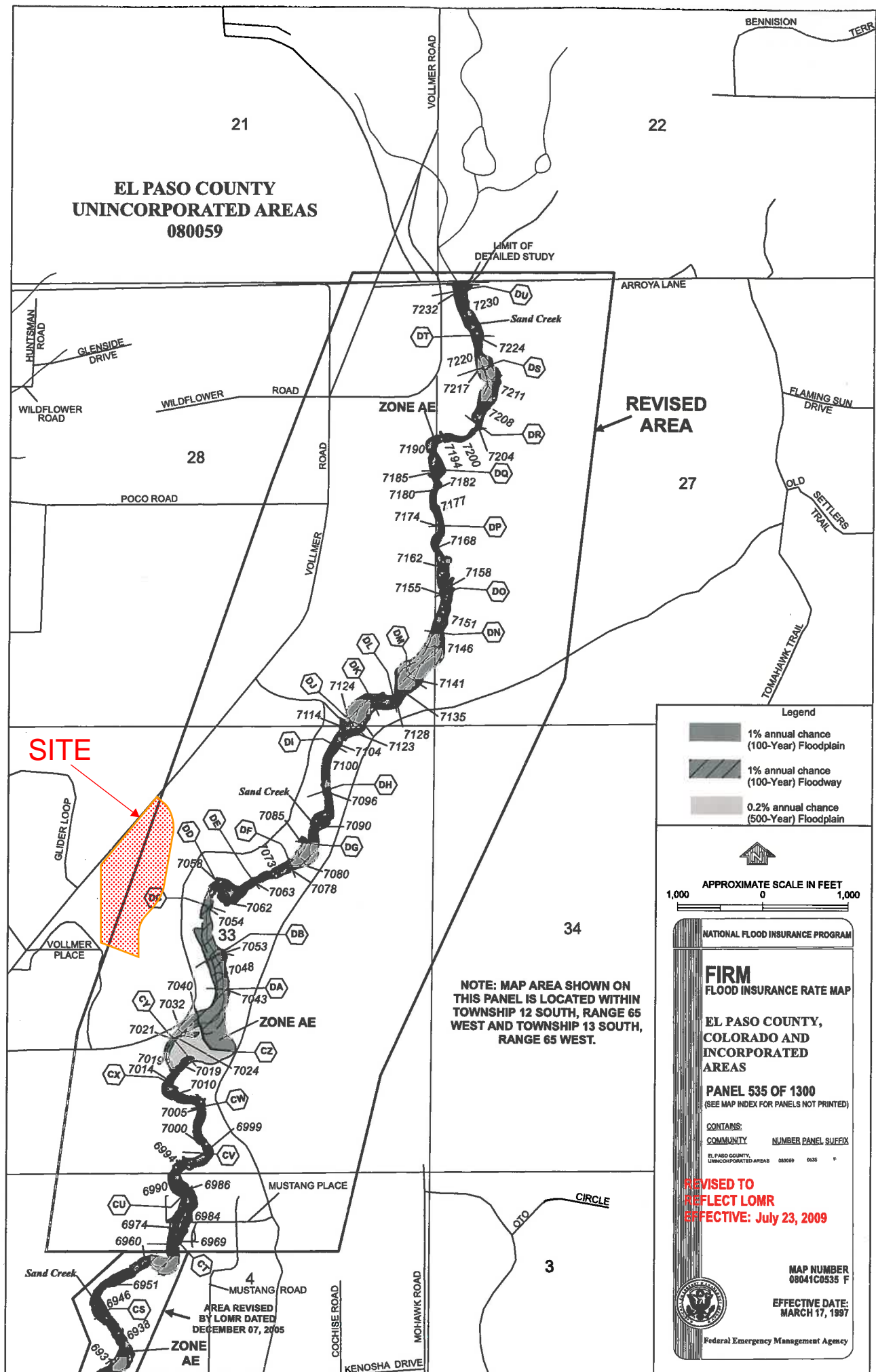
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

**FIRM PANEL W/ REVISED LOMR**

**EL PASO COUNTY  
UNINCORPORATED AREAS  
080059**



**Legend**

- 1% annual chance (100-Year) Floodplain
- 1% annual chance (100-Year) Floodway
- 0.2% annual chance (500-Year) Floodplain

**APPROXIMATE SCALE IN FEET**

1,000 0 1,000

**NATIONAL FLOOD INSURANCE PROGRAM**

**FIRM**  
FLOOD INSURANCE RATE MAP

**EL PASO COUNTY,  
COLORADO AND  
INCORPORATED  
AREAS**

**PANEL 535 OF 1300**  
(SEE MAP INDEX FOR PANELS NOT PRINTED)

**CONTAINS:**

COMMUNITY	NUMBER PANEL SUFFIX
EL PASO COUNTY, UNINCORPORATED AREAS 080059	0335 F

**REVISED TO  
REFLECT LOMR  
EFFECTIVE: July 23, 2009**

**MAP NUMBER  
08041C0535 F**

**EFFECTIVE DATE:  
MARCH 17, 1997**

Federal Emergency Management Agency

## **HYDROLOGIC CALCULATIONS**

# HOMESTEAD AT STERLING RANCH FILING NO.1

## FINAL DRAINAGE REPORT

### (Area Drainage Summary)

From Area Runoff Coefficient Summary				OVERLAND				STREET / CHANNEL FLOW				Time of Travel (T <sub>t</sub> )		INTENSITY *		TOTAL FLOWS		#REF!	#REF!	
BASIN	AREA TOTAL (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>C</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	CHECK (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)	CA <sub>5</sub>	Basin	CA <sub>100</sub>
Proposed Area Drainage Summary																				
OS2	2.1	0.90	0.96	0.90	10	0.2	0.9	1082	2.5%	3.0	5.9	6.9	16.1	4.7	7.9	8.9	15.9	1.89	OS2	2.02
OS3	0.43	0.22	0.46	0.22	90	1.8	12.0	0	0.0%	0.0	0.0	12.0	10.5	4.1	6.8	0.4	1.3	0.09	OS3	0.20
OS4	0.61	0.22	0.46	0.22	75	1.5	10.9	0	0.0%	0.0	0.0	10.9	10.4	4.1	6.8	0.5	1.9	0.13	OS4	0.28
OS5	1.54	0.90	0.96	0.90	10	0.2	0.9	1805	2.1%	3.0	9.9	10.8	20.1	4.0	6.7	5.6	10.0	1.39	OS5	1.48
OS6	9.73	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	12.5	30.4	3.70	OS6	5.35
OS7	1.97	0.08	0.35	0.08	60	10	5.6	270	0.5%	2.3	2.0	7.6	11.8	4.5	7.6	0.7	5.3	0.16	OS7	0.69
A	2.79	0.38	0.55	0.38	65	1.3	8.3	1449	2.8%	3.0	8.0	16.3	18.4	3.4	5.7	3.6	8.7	1.06	A	1.53
B	2.70	0.38	0.55	0.38	60	1.2	8.0	1381	2.8%	3.0	7.6	15.6	18.0	3.5	5.8	3.6	8.6	1.03	B	1.49
C	2.92	0.38	0.55	0.38	100	1.2	12.2	411	3.0%	3.0	2.3	14.5	12.8	3.8	6.3	4.2	10.1	1.11	C	1.61
D	2.9	0.38	0.55	0.38	100	2	10.3	245	2.1%	3.0	1.3	11.7	11.9	3.9	6.5	4.3	10.4	1.10	D	1.60
E	5.34	0.38	0.55	0.38	100	2	10.3	61	3.3%	3.0	0.3	10.7	10.9	4.0	6.8	8.2	19.9	2.03	E	2.94
F	1.12	0.90	0.96	0.90	10	0.2	0.9	1525	2.8%	3.0	8.4	9.3	18.5	4.2	7.1	4.3	7.7	1.01	F	1.08
G	0.61	0.22	0.46	0.22	100	2	12.6	0	2.2%	3.0	0.0	12.6	10.6	4.0	6.8	0.5	1.9	0.13	G	0.28
EX-H	0.19	0.90	0.96	0.90	10	0.2	0.9	280	2.1%	3.0	1.5	5.0	11.6	5.2	8.7	0.9	1.6	0.17	EX-H	0.18
M	1.15	0.22	0.46	0.22	100	2	12.6					12.6	10.6	4.0	6.8	1.0	3.6	0.25	M	0.53
M2	1.6	0.08	0.35	0.08	100	2	14.7	1015	2.4%	2.3	7.4	22.1	16.2	3.4	5.7	0.4	3.2	0.13	M2	0.56
N	2.08	0.22	0.46	0.22	75	1.5	10.9	818	2.9%	3.0	4.5	15.4	15.0	3.5	5.9	1.6	5.7	0.46	N	0.96
O	0.57	0.22	0.46	0.22	100	4	10.1	0	2.7%	3.0	0.0	10.1	10.6	4.1	6.9	0.5	1.8	0.13	O	0.26
W-2	10	0.08	0.35	0.08	100	2	14.7	1113	4.0%	2.3	8.2	22.8	16.7	3.4	5.6	2.7	19.7	0.80	W-2	3.50
OS1 Historic	111.7	0.08	0.35					FROM HISTORIC MDDP CALC AREA WEST OF VOLLMER ROAD								18.9	136.8	8.94	OS1 Historic	39.10
SUB-BASIN OS1A	2.7	0.08	0.35	0.08	100	0.57	22.2	1174	2.5%	1.5	12.9	35.1	17.1	3.3	5.6	0.7	5.3	0.22	SUB-BASIN OS1A	0.95
SUB-BASIN OS1B	9.09	0.08	0.35	0.08	100	0.57	22.2	1174	2.5%	2.3	8.6	30.8	17.1	3.3	5.6	2.4	17.8	0.73	SUB-BASIN OS1B	3.18
SUB-BASIN OS1C	5.64	0.08	0.35	0.08	300	9	22.2	907	3.3%	2.3	6.6	28.8	16.7	3.4	5.6	1.5	11.1	0.45	SUB-BASIN OS1C	1.97
SUB-BASIN OS1D	94.3	0.08	0.35	0.08	100	0.57	22.2	4800	3.0%	2.3	35.2	57.3	37.2	2.2	3.6	16.3	119.5	7.54	SUB-BASIN OS1D	33.01
V1A	0.31	0.90	0.96	0.90	20	0.4	1.3					5.0	10.1	5.2	8.7	1.4	2.6	0.28	V1A	0.30
V1B	0.26	0.90	0.96	0.90	20	0.4	1.3					5.0	10.1	5.2	8.7	1.2	2.2	0.23	V1B	0.25
V1C	0.21	0.90	0.96	0.90	20	0.4	1.3					5.0	10.1	5.2	8.7	1.0	1.7	0.19	V1C	0.20
V1D	0.13	0.90	0.96	0.90	20	0.4	1.3					5.0	10.1	5.2	8.7	0.6	1.1	0.12	V1D	0.12
V2	0.32	0.90	0.96	0.90	20	0.4	1.3					5.0	10.1	5.2	8.7	1.5	2.7	0.29	V2	0.31
RP-2B	2.04	0.63	0.76	0.63	50	1	4.8	1380	2.2%	3.0	7.6	12.4	17.9	3.8	6.4	4.9	9.9	1.29	RP-2B	1.55
RP-2C	1.28	0.74	0.84	0.74	50	1	3.7	692	2.2%	3.0	3.8	7.5	14.1	4.6	7.7	4.3	8.2	0.95	RP-2C	1.08

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: ET  
Date: 4/11/2018  
Checked by: VAS

# HOMESTEAD AT STERLING RANCH FILING NO.1

## FINAL DRAINAGE REPORT

### (Basin Routing Summary)

From Area Runoff Coefficient Summary				OVERLAND				PIPE / CHANNEL FLOW				Time of Travel (T <sub>t</sub> )	INTENSITY *		TOTAL FLOWS		COMMENTS
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>C</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)	
PROPOSED DRAINAGE BASIN ROUTING SUMMARY																	
1	A	1.06	1.53									16.3	3.4	5.7	3.6	8.7	15' AT-GRADE INLET
2	B	1.03	1.49									15.6	3.5	5.8	3.6	8.6	15' AT-GRADE INLET
3	C	1.11	1.61									12.8	3.8	6.3	4.2	10.1	6' SUMP INLET
4	D, E, F	4.14	5.61									11.7	3.9	6.5	16.1	36.7	EX 15' AT-GRADE INLET
5	G, EX-H, FLOWBY DP4	1.07	3.02									11.7	3.9	6.5	4.2	19.7	EX 15' AT-GRADE INLET
6	OS2, OS3, OS4, OS5	3.50	3.97									10.8	4.0	6.7	14.1	26.7	EX 15' AT-GRADE INLET
7	OS6	3.70	5.35									16.4	3.4	5.7	12.6	30.5	EX 18" RCP
8	OS7, PR4, PR6, PR7	14.52	18.52									16.4	3.4	5.7	49.2 50.0	105.3 102.9	EX FSD POND 4 (flows anticipated by MDDP 1&2)
9	OS1A, V1A	0.50	1.24									17.1	3.3	5.6	1.6	7.0	EX 12" CMP CULVERT
10	OS1B,V1B, DP6	1.46	4.67									17.1	3.3	5.6	4.8	26.3	EX 2.9x5.7' CDOT TYPE D INLET
11	OS1C, V1C	0.64	2.18									16.7	3.4	5.6	2.2	12.3	EX 2.9x2.9' CDOT TYPE C INLET
12	OS1D, V1D, W-2, V2	8.75	36.94									37.2	2.2	3.6	18.9	133.7	EX 4x14' MOD CDOT TYPE D INLET
13	RP-2B	1.29	1.55									12.4	2.2	3.6	2.8	5.6	EX CDOT EMBANKMENT PROTECTOR TYPE 5
14	M, M2, RP2C, DP13	2.61	3.71									16.2	3.4	5.7	8.9 8.9	21.2 21.2	EX FSD SAND FILTER POND W-9 (flows anticipated by MDDP 1&2)

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: ET  
Date: 4/11/2018  
Checked by: VAS

# HOMESTEAD AT STERLING RANCH FILING NO.1

## FINAL DRAINAGE REPORT

### (Storm Sewer Routing Summary)

PIPE RUN	Contributing Pipes/Design Points	Equivalent $CA_5$	Equivalent $CA_{100}$	Maximum $T_C$	Intensity*		Flow		PIPE SIZE
					$I_5$	$I_{100}$	$Q_5$	$Q_{100}$	
1	DP1 (Int)	1.06	1.53	16.3	3.4	5.7	3.6	8.7	30" RCP
2	DP2 (Int), PR1	2.09	3.02	16.3	3.4	5.7	7.1	17.2	36" RCP
3	DP3	1.11	1.61	12.8	3.8	6.3	4.2	10.1	18" RCP
4	DP4 (Int), PR3	4.48	4.66	12.8	3.8	6.3	16.8	29.4	30" RCP
5	DP5 (Int), PR2	3.17	5.27	16.3	3.4	5.7	10.8	30.0	36" RCP
6	DP6 (Int), PR5	6.18	7.82	16.3	3.4	5.7	21.0	44.6	36" RCP
7	DP7	3.70	5.35	16.4	3.4	5.7	12.6	30.5	30" RCP
8	DP9	0.50	1.24	17.1	3.3	5.6	1.6	7.0	12" CMP
9	DP10	1.46	4.67	17.1	3.3	5.6	4.8	26.3	24" RCP
10	DP11	0.64	2.18	16.7	3.4	5.6	2.2	12.3	18" RCP
11	PR9, PR10	2.10	6.85	17.1	3.3	5.6	7.0	38.6	30" RCP
12	DP12	8.75	36.94	37.2	2.2	3.6	18.9	133.7	54" RCP
13	OUTFLOW EDB POND W-9	0.18	1.53	16.2	3.4	5.7	0.6	8.7	18" RCP
14	PR11, PR13	2.28	8.38	17.1	3.3	5.6	7.6	47.2	30" RCP
15	PR12, PR14	11.03	45.32	37.2	2.2	3.6	23.8	164.1	54" RCP
16	OUTFLOW EDB POND 4	PEAK OUTFLOW FROM POND 4 UD DET v3.04					2.8	36.8	30" RCP
17	PR15, PR16	SUMMATION OF PR11 & PR18					26.6	200.9	60" RCP

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: ET

DP - Design Point

FB- Flow By from Design Point

Date: 4/11/2018

EX - Existing Design Point

INT- Intercepted Flow from Design Point

Checked by: VAS

## **HYDRAULIC CALCULATIONS**

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

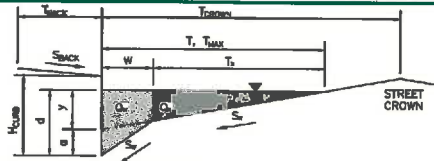
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Homestead at Sterling Ranch Filing No. 1

Inlet ID:

Inlet DP1

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 8.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.020$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 17.0$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.022$  ft/ft  
 $n_{STREET} = 0.020$

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	5.1	7.8	inches
	<input type="checkbox"/>	<input checked="" type="checkbox"/>	check = yes

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

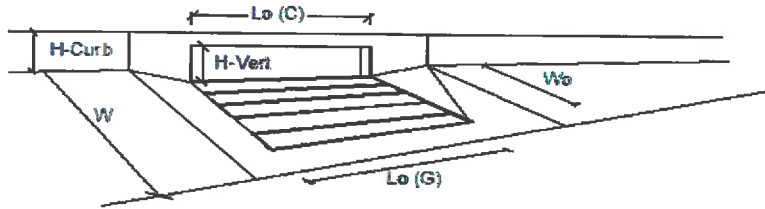
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

	Minor Storm	Major Storm	
$Q_{allow} =$	8.4	28.1	cfs

# INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	Type = CDOT Type R Curb Opening		
Total Number of Units in the Inlet (Grate or Curb Opening)	$B_{LOCAL} = 3.0$	$3.0$	inches
Length of a Single Unit Inlet (Grate or Curb Opening)	$N_0 = 3$	$3$	
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$L_0 = 5.00$	$5.00$	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$W_0 = N/A$	$N/A$	ft
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_T-G = N/A$	$N/A$	
Street Hydraulics: OK - $Q < \text{Allowable Street Capacity}$	$C_T-C = 0.10$	$0.10$	
Total Inlet Interception Capacity	MINOR MAJOR		
Total Inlet Carry-Over Flow (flow bypassing Inlet)	$Q = 3.6$	$8.8$	cfs
Capture Percentage = $Q_i/Q_a =$	$Q_b = 0.0$	$0.1$	cfs
	$C\% = 100$	$89$	%

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

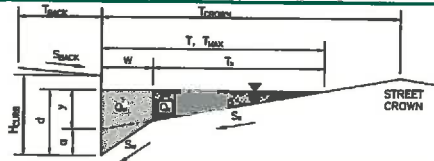
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

Homestead at Sterling Ranch Filing No. 1

Inlet ID:

Inlet DP2

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

T <sub>BACK</sub>	8.0	ft
S <sub>BACK</sub>	0.020	ft/ft
n <sub>BACK</sub>	0.020	

H <sub>CURB</sub>	6.00	Inches
T <sub>CROWN</sub>	17.0	ft
W	2.00	ft
S <sub>x</sub>	0.020	ft/ft
S <sub>w</sub>	0.083	ft/ft
S <sub>o</sub>	0.022	ft/ft
n <sub>STREET</sub>	0.020	

Max. Allowable Spread for Minor &amp; Major Storm

	Minor Storm	Major Storm	
T <sub>MAX</sub>	17.0	17.0	ft
d <sub>MAX</sub>	5.1	7.8	Inches

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☒ check = yes

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

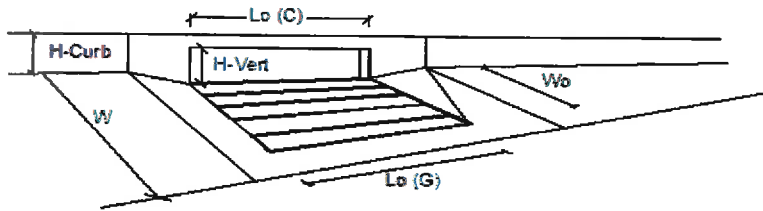
	Minor Storm	Major Storm	
Q <sub>allow</sub>	9.4	29.1	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

# INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL}$ =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o$ =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than $W$ , Gutter Width)		$W_o$ =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G$ =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C$ =	0.10	0.10	
<b>Street Hydraulics: OK - <math>Q &lt; \text{Allowable Street Capacity}</math></b>					
Total Inlet Interception Capacity		$Q$ =	3.6	8.5	cfs
Total Inlet Carry-Over Flow (flow bypassing Inlet)		$Q_b$ =	0.0	0.1	cfs
Capture Percentage = $Q/Q_b$ =		C% =	100	99	%

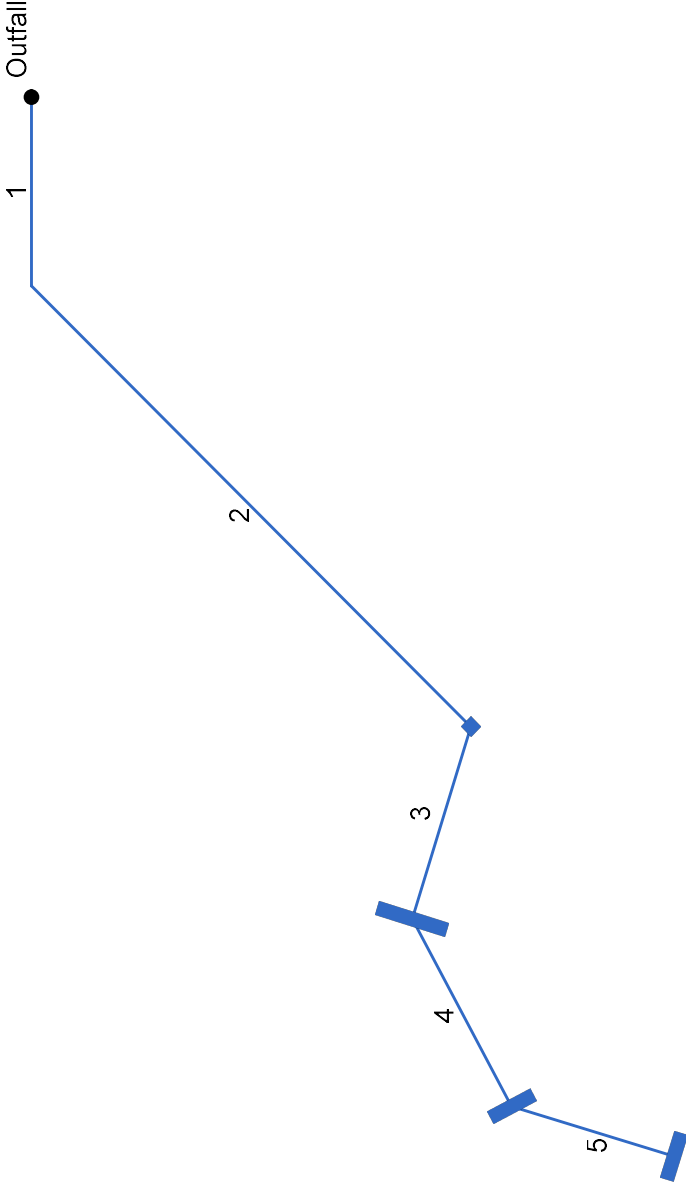
# HOMESTEAD AT STERLING RANCH FILING NO.1 FINAL DRAINAGE REPORT

## (CDOT Type R Inlet Calculations - Sump Condition)

Urban Local Roadway-50' ROW-30' Pavement-6" Vertical Curb Maximum allowable depth for MINOR (0.43') & MAJOR (0.66') storm						
Inlet Length	Storm	Depth	Eqn. 7-31 $Q_w = C_w N_w L_e D^{3/2}$	Eqn. 7-32 $Q_o = C_o N_o (L_e H_c) (2g(D - 0.5H_c))^{1/2}$	Eqn. 7-29 $Q_m = C_m (Q_w Q_o)^{1/2}$	
5	Q5	0.43	5.1	5.7	5.0	
5	Q100	0.66	9.7	8.6	8.5	
6	Q5	0.43	6.1	6.8	6.0	
6	Q100	0.66	11.6	10.3	10.2	
8	Q5	0.43	8.1	9.1	8.0	
8	Q100	0.66	15.4	13.8	13.6	
10	Q5	0.43	10.2	11.4	10.0	
10	Q100	0.66	19.3	17.2	17.0	
12	Q5	0.43	12.2	13.7	12.0	
12	Q100	0.66	23.2	20.7	20.3	
14	Q5	0.43	14.2	16.0	14.0	
14	Q100	0.66	27.0	24.1	23.7	
15	Q5	0.43	15.2	17.1	15.0	
15	Q100	0.66	29.0	25.8	25.4	
16	Q5	0.43	16.2	18.2	16.0	
16	Q100	0.66	30.9	27.5	27.1	

Table 7-7. Coefficients for various inlets in sumps

Inlet Type	Nw	Cw	No	Co	Cm
CDOT Type 13 Grate	0.7	3.3	0.43	0.6	0.93
Denver No. 16 Grate	0.73	3.6	0.31	0.6	0.9
Curb Opening for Type 13/No. 16 Combination	1	3.7	1	0.66	0.86
CDOT Type R Curb Opening	1	3.6	1	0.67	0.93

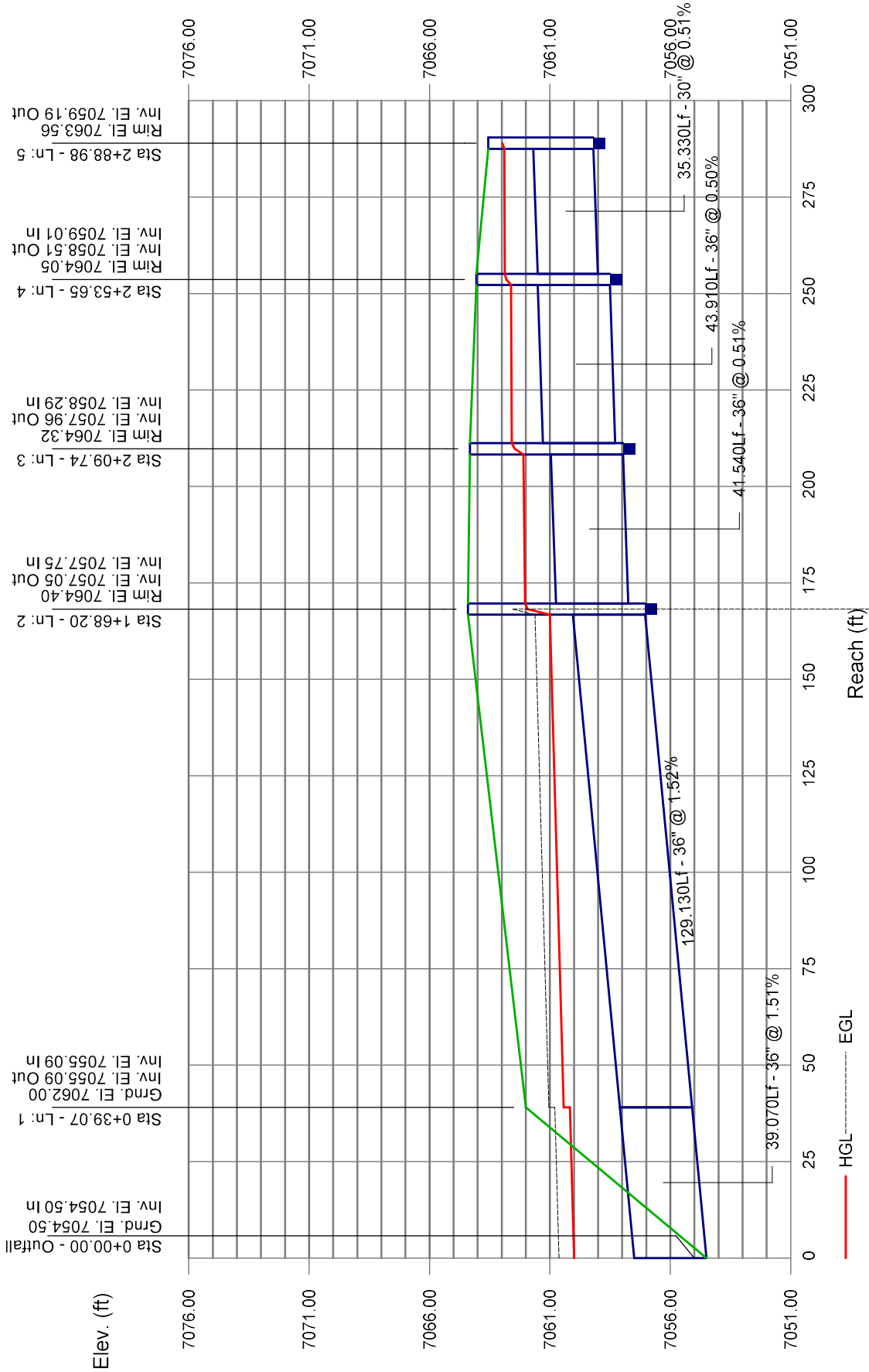


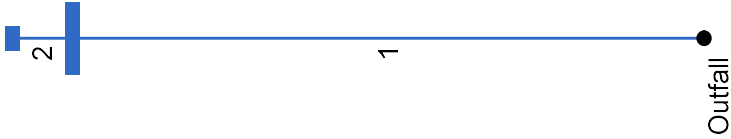
Project File: Storm 1 2 5 and 6.stm	Number of lines: 5	Date: 4/24/2018
-------------------------------------	--------------------	-----------------

# Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert EI Dn (ft)	Line Slope (%)	Invert EI Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim EI (ft)	
1	End	39.070	180.000	None	44.60	0.00	0.00	0.0	7054.50	1.51	7055.09	36	Cir	0.013	0.40	7062.00	
2	1	129.130	-45.000	Curb	44.60	0.00	0.00	0.0	7055.09	1.52	7057.05	36	Cir	0.013	1.50	7064.32	
3	2	41.540	62.000	Curb	30.00	0.00	0.00	0.0	7057.75	0.51	7057.96	36	Cir	0.013	1.50	7064.40	
4	3	43.910	-45.000	Curb	17.20	0.00	0.00	0.0	7058.29	0.50	7058.51	36	Cir	0.013	1.70	7063.55	
5	4	35.330	-45.000	Curb	8.70	0.00	0.00	0.0	7059.01	0.51	7059.19	30	Cir	0.013	1.50	7063.06	
Project File: Storm 1 2 5 and 6.stm										Number of lines: 5							Date: 4/24/2018

# Storm Sewer Profile



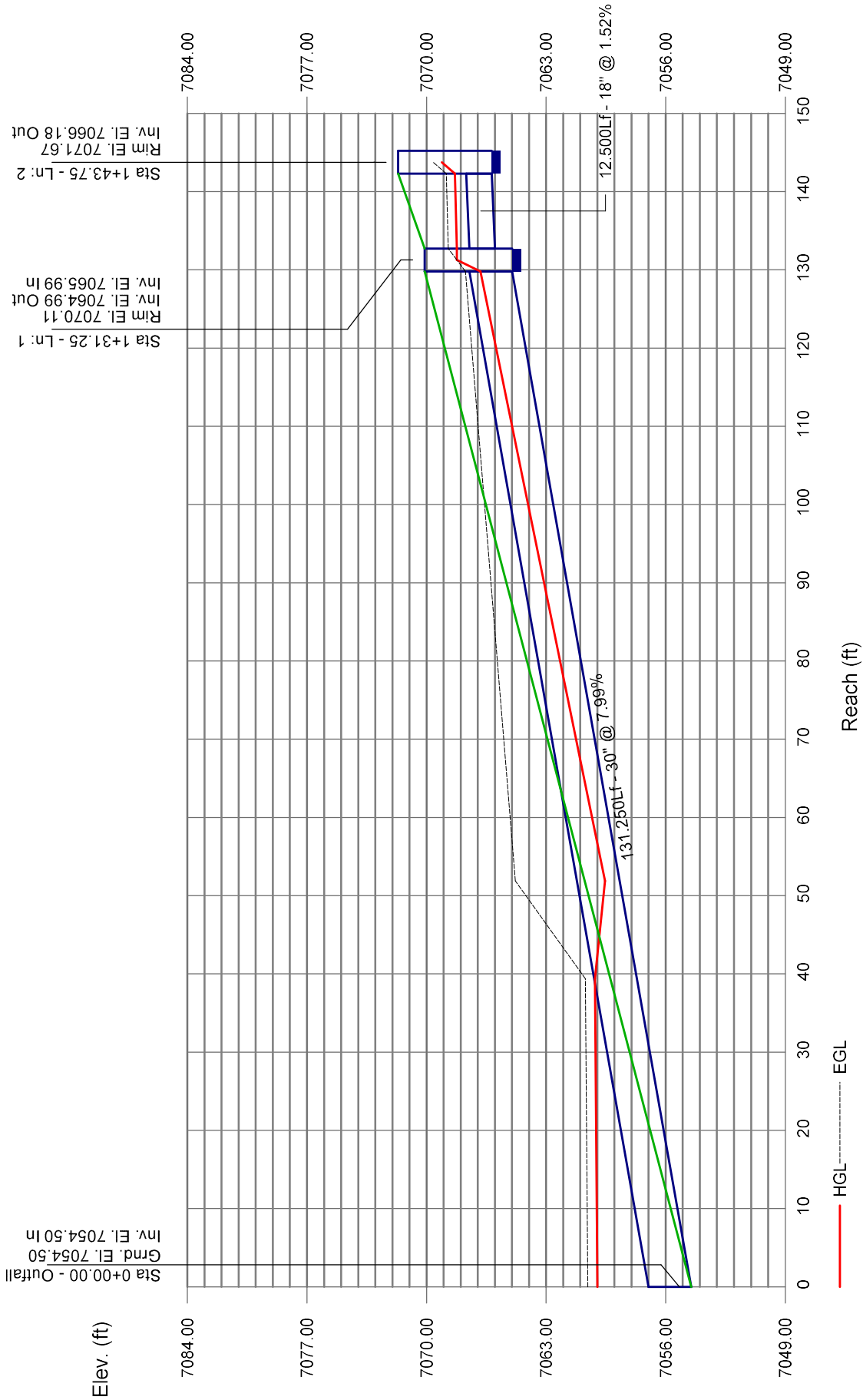


Project File: Storm 3 and 4.stm	Number of lines: 2	Date: 4/24/2018
---------------------------------	--------------------	-----------------

# Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data							Line ID		
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)		Inlet/ Rim El (ft)	
1	End	131.250	-90.000	Curb	29.40	0.00	0.00	0.0	7054.50	7.99	7064.99	30	Cir	0.013	1.50	7070.11	Storm 3	
2	1	12.500	0.000	Curb	10.10	0.00	0.00	0.0	7065.99	1.52	7066.18	18	Cir	0.013	1.50	7071.67	Storm 3	
Project File: Storm 3 and 4.stm																	Number of lines: 2	Date: 4/24/2018

# Storm Sewer Profile



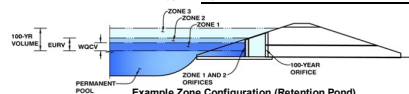
## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project: STERLING RANCH FILING NO. 1

---

Basin ID: POND 4

Basin ID: POND 4



**Example Zone Configuration (Retention Pond)**

### Required Volume Calculation

Selected BMP Type =	<b>EDB</b>	
Watershed Area =	27.63	acres
Watershed Length =	1,720	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	53.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Desired WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	Use Input	
Water Quality Capture Volume (WQCV) =	0.494	acre-feet
Excess Urban Runoff Volume (EURV) =	1.573	acre-feet
2-y Runoff Volume ( $P_1 = 1.19$ in.) =	1.312	acre-feet
2-y Runoff Volume ( $P_1 = 1.75$ in.) =	1.981	acre-feet
10-y Runoff Volume ( $P_1 = 1.75$ in.) =	2.542	acre-feet
25-y Runoff Volume ( $P_1 = 2.12$ in.) =	3.324	acre-feet
50-y Runoff Volume ( $P_1 = 2.25$ in.) =	3.977	acre-feet
100-y Runoff Volume ( $P_1 = 2.50$ in.) =	4.582	acre-feet
50-y Runoff Volume ( $P_1 = 6.53$ in.) =	13.003	acre-feet
Approximate 2-y Detention Volume =	1.241	acre-feet
Approximate 5-y Detention Volume =	1.821	acre-feet
Approximate 10-y Detention Volume =	1.991	acre-feet
Approximate 25-y Detention Volume =	2.082	acre-feet
Approximate 50-y Detention Volume =	2.317	acre-feet
Approximate 100-y Detention Volume =	2.781	acre-feet

Water Quality Capture Volume (WQCV)	0.494	acre-feet	Optional User Input 1-hr Precipitation	
Excess Urban Runoff Volume (EURV)	1.573	acre-feet		
2-hr Runoff Volume (P1 = 1.19 in.)	1.312	acre-feet		
5-hr Runoff Volume (P1 = 1.5 in.)	1.981	acre-feet		
10-hr Runoff Volume (P1 = 2.75 in.)	2.545	acre-feet		
25-hr Runoff Volume (P1 = 2 in.)	3.324	acre-feet		
50-hr Runoff Volume (P1 = 2.25 in.)	3.977	acre-feet		
100-hr Runoff Volume (P1 = 2.52 in.)	4.702	acre-feet	1.19	inches
500-hr Runoff Volume (P1 = 6.53 in.)	13.003	acre-feet	1.50	inches
			1.75	inches
			2.00	inches
			2.25	inches
			2.52	inches
			6.53	inches

### Stage-Storage Calculation

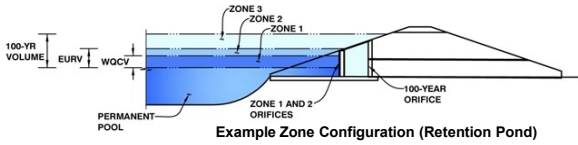
Zone 1 Volume ( $WQCV_1$ )	0.494	acre-feet
Zone 2 Volume ( $EURV - Zone 1$ )	1.079	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2)	1.209	acre-feet
Total Detention Basins ( $V_{DB}$ )	2.781	acre-feet
Initial Surcharge Volume ( $ISV$ )	USBF	H+3
Initial Surcharge Depth ( $ISD$ )	USBF	H
Total Available Detention Depth ( $H_{ADB}$ )	USBF	H
Depth of Trickle Channel ( $H_{TC}$ )	USBF	H
Slope of Trickle Channel ( $S_{TC}$ )	USBF	Hft
Slopes of Main Basin Sides ( $S_{MB}$ )	USBF	H:V
Basin Length-to-Width Ratio ( $R_{LWB}$ )	USBF	
Initial Surcharge Area ( $A_{ISB}$ )	USBF	H+2
Surcharge Volume Length ( $L_{SVL}$ )	USBF	H
Surcharge Volume Width ( $W_{SVL}$ )	USBF	H
Depth of Basin Floor ( $H_{BDF}$ )	USBF	H
Length of Basin Floor ( $L_{BDF}$ )	USBF	H
Width of Basin Floor ( $W_{BDF}$ )	USBF	H
Area of Basin Floor ( $A_{BDF}$ )	USBF	H+2
Volume of Basin Floor ( $V_{BDF}$ )	USBF	H+3
Depth of Main Basin ( $H_{MBD}$ )	USBF	H
Length of Main Basin ( $L_{MBD}$ )	USBF	H
Width of Main Basin ( $W_{MBD}$ )	USBF	H
Area of Main Basin ( $A_{MBD}$ )	USBF	H+2
Volume of Main Basin ( $V_{MBD}$ )	USBF	H+3
Calculated Total Basin Volume ( $V_{MBD}$ )	USBF	acre-feet

Depth Increment = 1 ft

[illegible]

## Detention Basin Outlet Structure Design

Project: **STERLING RANCH FILING NO. 1**  
Basin ID: **POND 4**



**Example Zone Configuration (Retention Pond)**

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.32	0.494	Orifice Plate
Zone 2 (EURV)	5.38	1.079	Orifice Plate
Zone 3 (100-year)	6.69	1.209	Weir&Pipe (Restrict)
		2.781	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  inches

Calculated Parameters for Plate

WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.79	3.58					
Orifice Area (sq. inches)	2.33	2.33	2.60					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =   ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =   ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =   inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area =   ft<sup>2</sup>  
Vertical Orifice Centroid =   feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Overflow Weir Front Edge Height, H<sub>o</sub> =   ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =   feet  
Overflow Weir Slope =   H:V (enter zero for flat grate)  
Horiz. Length of Weir Sides =   feet  
Overflow Grate Open Area % =   % grate open area/total area  
Debris Clogging % =   %

Calculated Parameters for Overflow Weir

Height of Grate Upper Edge, H<sub>t</sub> =   feet  
Over Flow Weir Slope Length =   feet  
Grate Open Area / 100-yr Orifice Area =   should be ≥ 4  
Overflow Grate Open Area w/o Debris =   ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris =   ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =   ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =   inches  
Restrictor Plate Height Above Pipe Invert =   inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Outlet Orifice Area =   ft<sup>2</sup>  
Outlet Orifice Centroid =   feet  
Half-Central Angle of Restrictor Plate on Pipe =   radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

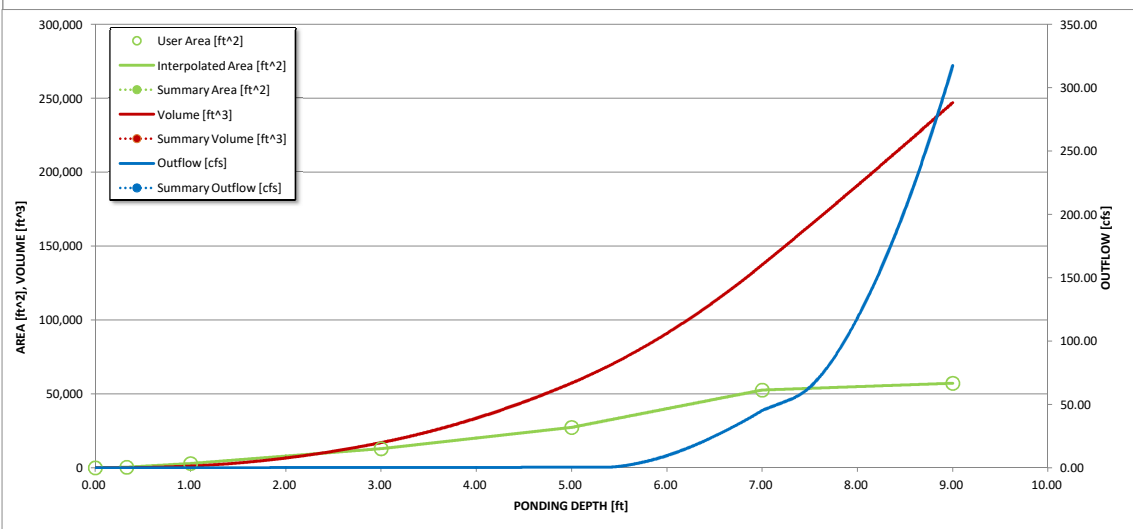
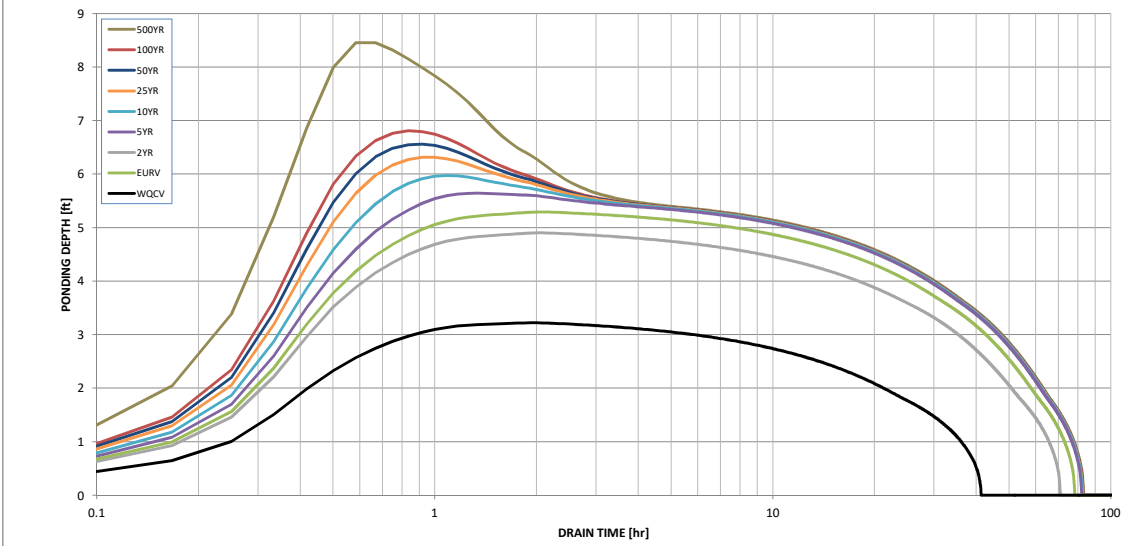
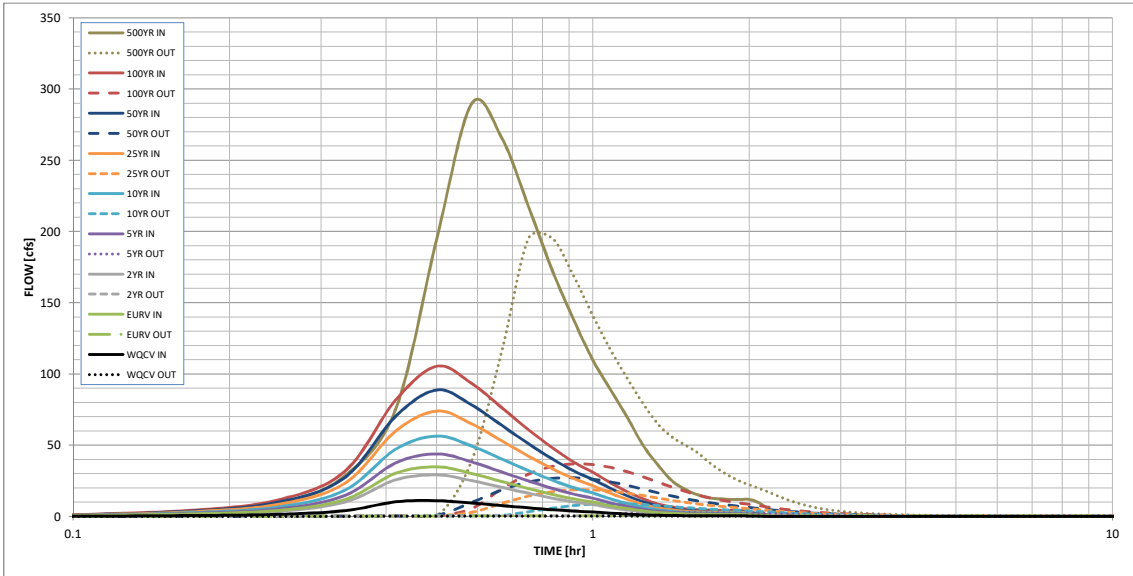
Calculated Parameters for Spillway

Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres

### Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	6.53
Calculated Runoff Volume (acre-ft) =	0.494	1.573	1.312	1.981	2.542	3.324	3.977	4.720	13.003
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.494	1.573	1.312	1.982	2.543	3.326	3.980	4.723	13.012
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.20	0.40	0.90	1.16	1.48	2.09
Predevelopment Peak Q (cfs) =	0.0	0.0	0.4	5.5	11.0	24.8	32.1	40.9	57.7
Peak Inflow Q (cfs) =	11.0	34.8	29.1	43.8	56.3	73.9	88.6	105.3	289.7
Peak Outflow Q (cfs) =	0.2	0.4	0.4	2.8	9.0	18.6	27.1	36.8	195.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.8	0.7	0.8	0.9	3.4
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	1.0	1.4	1.9	3.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	70	64	72	70	68	66	64	48
Time to Drain 99% of Inflow Volume (hours) =	40	75	68	78	77	76	76	75	65
Maximum Ponding Depth (ft) =	3.22	5.29	4.90	5.64	5.97	6.32	6.56	6.81	8.46
Area at Maximum Ponding Depth (acres) =	0.33	0.71	0.61	0.81	0.91	1.01	1.08	1.15	1.28
Maximum Volume Stored (acre-ft) =	0.460	1.510	1.253	1.776	2.060	2.386	2.647	2.915	4.956

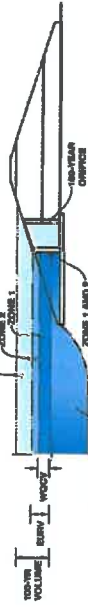
Detention Basin Outlet Structure Design



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

## UD-Detention, Version 3.07 (February 2017)

**Basin ID: East Vollmer Road, Homestead backyards and Landscape area 3:1 Pond slope**



### Example Zone Configuration (Retention Pond)

Selected BMP Type	SF
Watershed Area	5.87 acres
Watershed Length	575 ft
Watershed Slope	0.024 %
Watershed Imperviousness	70.00% percent
Percentage Hydrologic Soil Group A	0.0% percent
Percentage Hydrologic Soil Group B	100.0% percent
Percentage Hydrologic Soil Group C/D	0.0% percent
Desired WQCV Drain Time	12.0 hours

Location for 1-hr Rainfall Depths = User Input

Water Quality Capburo Volume (WQCV) =	0.106	acre-foot
Excess Urban Runoff Volume (EURV) =	0.451	acre-foot
2-yr Runoff Volume ( $P_1 = 1.19$ in.) =	0.376	acre-foot
5-yr Runoff Volume ( $P_1 = 1.5$ in.) =	0.500	acre-foot
10-yr Runoff Volume ( $P_1 = 1.75$ in.) =	0.634	acre-foot
25-yr Runoff Volume ( $P_1 = 2$ in.) =	0.799	acre-foot
50-yr Runoff Volume ( $P_1 = 2.25$ in.) =	0.922	acre-foot
100-yr Runoff Volume ( $P_1 = 2.52$ in.) =	1.083	acre-foot
500-yr Runoff Volume ( $P_1 = 0$ in.) =	0.000	acre-foot
Approximate 2-yr Detention Volume =	0.353	acre-foot
Approximate 5-yr Detention Volume =	0.470	acre-foot
Approximate 10-yr Detention Volume =	0.593	acre-foot
Approximate 25-yr Detention Volume =	0.637	acre-foot
Approximate 50-yr Detention Volume =	0.683	acre-foot
Approximate 100-yr Detention Volume =	0.710	acre-foot

Zone 1 Volume ( $WQCV =$	0.108	acre-foot
Zone 2 Volume ( $EURV - Zone 1 =$	0.344	acre-foot
Zone 3 Volume ( $100\text{-year} - Zones 1 \& 2 =$	0.259	acre-foot
Total Detention Basin Volume =	0.710	acre-foot
Initial Surcharge Volume ( $SV$ ) =	N/A	$ft^3$
Initial Surcharge Depth ( $ISD$ ) =	N/A	ft
Total Available Detention Depth ( $H_{avail}$ ) =	user	ft
Depth of Trickle Channel ( $H_{TC}$ ) =	N/A	ft
Slope of Trickle Channel ( $S_{TC}$ ) =	N/A	$ft/ft$
Slopes of Main Basin Sides ( $S_{main}$ ) =	user	H:V
Basin Length-to-Width Ratio ( $R_{L/W}$ ) =	user	

[illegible]

**Optional User Override  
1-hr Precipitation**

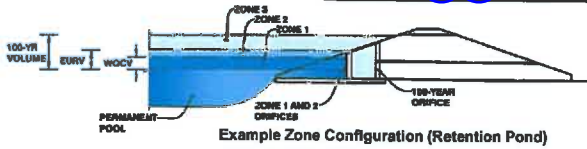
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
	inches

# Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: Revision to Road W-2 Stoning Ranch Filling No.1 MDDP

Basin ID: East Vollmer Road, Homestead Backyards and Landscape area 3:1 Pond slope



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.69	0.108	Filtration Media
Zone 2 (EURV)	2.21	0.344	Circular Orifice
Zone 3 (100-year)	3.07	0.259	Weir & Pipe (Restrict)
		0.710	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 3.30 ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter = 1.49 Inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = 0.0 ft<sup>2</sup>  
 Underdrain Orifice Centroid = 0.06 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft)  
 Orifice Plate: Orifice Vertical Spacing = N/A inches  
 Orifice Plate: Orifice Area per Row = N/A inches

Calculated Parameters for Plate

WQ Orifice Area per Row = N/A ft<sup>2</sup>  
 Elliptical Half-Width = N/A feet  
 Elliptical Slot Centroid = N/A feet  
 Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

Zone 2 Circular Not Selected  
 Invert of Vertical Orifice = 0.69 N/A ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Vertical Orifice = 2.21 N/A ft (relative to basin bottom at Stage = 0 ft)  
 Vertical Orifice Diameter = 3.92 N/A inches

Calculated Parameters for Vertical Orifice

Zone 2 Circular Not Selected  
 Vertical Orifice Area = 0.08 N/A ft<sup>2</sup>  
 Vertical Orifice Centroid = 0.16 N/A feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Zone 3 Weir Not Selected  
 Overflow Weir Front Edge Height, H<sub>o</sub> = 2.21 N/A ft (relative to basin bottom at Stage = 0 ft)  
 Overflow Weir Front Edge Length = 2.91 N/A feet  
 Overflow Weir Slope = 0.00 N/A H:V (enter zero for flat grate)  
 Horiz. Length of Weir Sides = 2.91 N/A feet  
 Overflow Grate Open Area % = 70% N/A %  
 Debris Clogging % = 50% N/A %

Calculated Parameters for Overflow Weir

Zone 3 Weir Not Selected  
 Height of Grate Upper Edge, H<sub>u</sub> = 2.21 N/A feet  
 Overflow Weir Slope Length = 2.91 N/A feet  
 Grate Open Area / 100-yr Orifice Area = 8.08 N/A  
 Overflow Grate Open Area w/o Debris = 5.93 N/A ft<sup>2</sup>  
 Overflow Grate Open Area w/ Debris = 2.96 N/A ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Restrictor Not Selected  
 Depth to Invert of Outlet Pipe = 3.55 N/A ft (distance below basin bottom at Stage = 0 ft)  
 Outlet Pipe Diameter = 18.00 N/A inches  
 Restrictor Plate Height Above Pipe Invert = 7.80 N/A inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Zone 3 Restrictor Not Selected  
 Outlet Orifice Area = 0.73 N/A ft<sup>2</sup>  
 Outlet Orifice Centroid = 0.38 N/A feet  
 Half-Central Angle of Restrictor Plate on Pipe = 1.44 N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 3.08 ft (relative to basin bottom at Stage = 0 ft)  
 Spillway Crest Length = 12.00 feet  
 Spillway End Slopes = 3.00 H:V  
 Freeboard above Max Water Surface = 0.67 feet

Calculated Parameters for Spillway

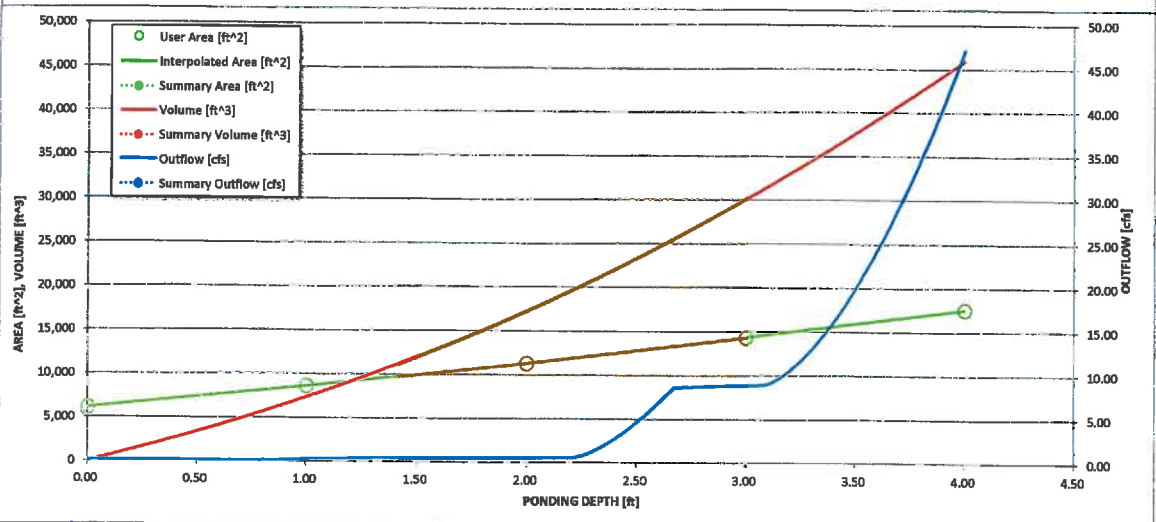
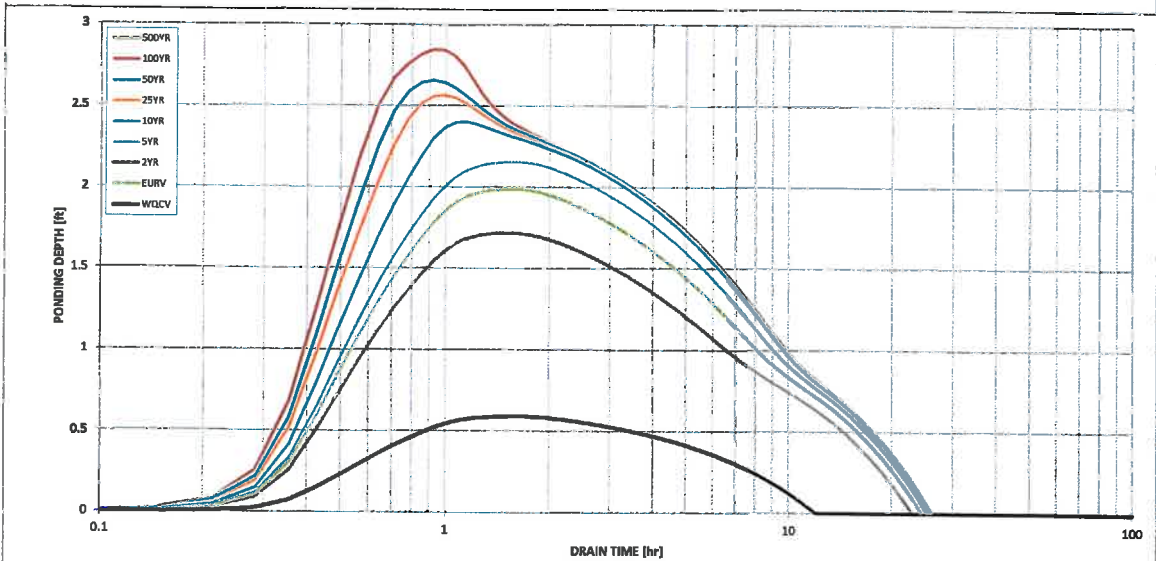
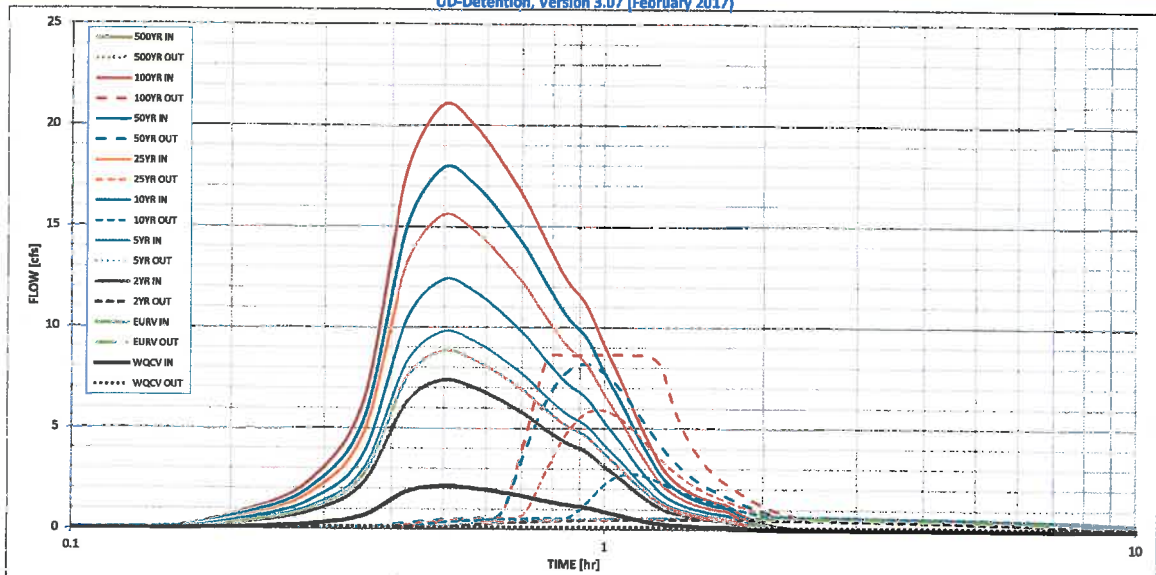
Spillway Design Flow Depth = 0.64 feet  
 Stage at Top of Freeboard = 4.39 feet  
 Basin Area at Top of Freeboard = 0.40 acres

## Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.108	0.451	0.376	0.500	0.634	0.799	0.922	1.083	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.107	0.451	0.376	0.500	0.634	0.800	0.923	1.083	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.03	0.25	0.81	1.11	1.49	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.1	0.2	1.5	4.7	6.5	8.7	0.0
Peak Inflow Q (cfs) =	2.1	8.8	7.4	9.8	12.4	15.5	17.9	21.0	#N/A
Peak Outflow Q (cfs) =	0.1	0.6	0.5	0.6	2.7	5.9	8.2	8.7	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	4.0	1.8	1.3	1.2	1.0	#N/A
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.4	0.9	1.3	1.3	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	23	22	24	24	23	23	23	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	24	23	25	25	25	25	25	#N/A
Maximum Ponding Depth (ft) =	0.59	1.99	1.72	2.15	2.40	2.56	2.66	2.84	#N/A
Area at Maximum Ponding Depth (acres) =	0.17	0.26	0.24	0.27	0.29	0.30	0.30	0.32	#N/A
Maximum Volume Stored (acre-ft) =	0.092	0.390	0.323	0.435	0.505	0.552	0.579	0.638	#N/A

# Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

## **DRAINAGE MAP**

## APRIL 2018

# FINAL DRAINAGE MAP

APRIL 2018

