FINAL DRAINAGE REPORT FOR SADDLEHORN RANCH – FILING 3

Prepared For: ROI Property Group, LLC 2495 Rigdon Street Napa, CA 94558 (707) 365-6891

> February 4, 2022 Project No. 25142.05

Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

El Paso County PCD File No.: SF-XX-XXX SF234 23-003

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Bryan Law, Colorado P.E. # 25043 For and On Behalf of JR Engineering, LLC Date

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

ROI Property Group, LLC

By:

Title: Address:

2495 Rigdon Street Napa, CA 94558

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E. change to Joshua Palmer, P.E. County Engineer/ ECM Administrator Date

Conditions:



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Purpose

This document is the Final Drainage report for Filing 3 of Saddlehorn Ranch. The purpose of this report is to:

- 1. Identify on-site and off-site drainage patterns.
- 2. Recommend storm water facilities to collect and convey storm runoff from the proposed development to appropriate discharge and/or detention locations.
- 3. Recommend water quality and detention facilities to control discharge release rates to below historic.
- 4. Demonstrate compliance with surrounding major drainage basin planning studies, master development drainage plans and flood insurance studies.

GENERAL LOCATION AND DESCRIPTION

Location

Documents report either 175 or 179 acres, but it is not consistent. Verify total acreage and update throughout all documents.

The proposed Saddlehorn Ranch Filing 3, known as "Filing 3" from herein, is a parcel of land located in Section 3 and 10, Township 13 South, Range 64 West of the 6th Principal Meridian in El Raso County, Colorado. Saddlehorn Ranch is an 824 acre, rural, single family-development. Filing 3 is 175.43 acres and is comprised of 44 lots of the overall Saddlehorn Ranch development. Saddlehorn Ranch is bound by Judge Orr Road to the North and Curtis Road to the West. To the East, Saddlehorn Ranch is bound by undeveloped land owned by Brent Houser Enterprises, LLC. To the south, Saddlehorn Ranch is bound by undeveloped properties owned by Carolyn Gudzunas and Faye Reynolds. Filing 3 is bound by future Filing 4 to the east, Filing 2 to the south, Judge Orr Road to the north, and by Curtis Road to the west. A vicinity map is presented in Appendix A.

Currently, there are two major Drainageway that will receive flows from Filing 3: Gieck Ranch (WF-R7A) and Haegler Ranch Main Stem 6 (MS-06). These Drainageways were analyzed, both hydrologically and hydraulically, in the following reports:

- Haegler Ranch Basin Drainage Basin Planning Study (DBPS), May 2009.
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision, June 2004.
- Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch, May 2020.
- Geick Ranch Drainage Basin Planning Study (DBPS), October 2007

The impact of these Drainageways and planning studies on the proposed development will be discussed later in the report.

Description of Property

Filing 3 is currently unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling range land condition. In general, Filing 3 slopes from south to southeast and the existing drainageways follows this topography.

Per a NRCS web soil survey of the area, Filing 3 is made up of Type A and D soils. Type A soils cover roughly 76% of Filing 3 while Type D soils cover 24% of Filing 3. Group A soils have a high infiltration rate when thoroughly wet. Type D soils have a very slow infiltration when thoroughly wet. A NRCS soil survey map has been presented in Appendix A.

Floodplain Statement

Based on the FEMA FIRM Map number 08041C0558G, dated December 7, 2018, Filing 3 lies within Zone AE and Zone X. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. All proposed residential development within Filing 3 will occur in Zone X. The FIRM Map has been presented in Appendix A.

DRAINAGE BASINS AND SUB-BASINS

Existing Major Basin Descriptions

Filing 3 lies within Haegler Ranch Drainage Basin based on the "*Haegler Ranch Drainage Basin Planning Study*" prepared by URS Corporation in May 2009.

The Haegler Ranch Drainage Basin covers approximately 16.6 square miles in unincorporated El Paso County, CO. The Haegler Ranch Drainage Basin is tributary to Black Squirrel Creek. In its existing condition, the basin is comprised of rolling rangeland with poor vegetative cover associated with Colorado's semi-arid climate. The natural Drainageways within the basin are typically shallow and wide with poorly defined flow paths in most areas. Anticipated land use for the basin includes residential and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

As part of its drainage research, JR Engineering reviewed the following drainage studies, reports and LOMRs:

- Haegler Ranch Drainage Basin Planning Study prepared by URS Corporation in May 2009
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision prepared by Tri-Core Engineering in June 2004.
- Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch, prepared by JR Engineering, May 2020.
- Gieck Ranch Drainage Basin Planning Study (DBPS), October 2007

The "*Haegler Ranch Drainage Basin Planning Study*" was used to establish a stormwater management plan for the existing and future stormwater infrastructure needs within the Haegler Ranch Drainage Basin. Based on provided drainage maps and analysis, in the existing condition Haegler Ranch contributes a total of 710 cfs onto the site. Of the 710 cfs, 590 cfs crosses Curtis Road in an existing 24" CMP onto the site. Major Drainageway MS-06 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. The remaining 210 cfs crosses Curtis Road in an existing 36" CMP onto the

site. Major Drainageway T-6 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. Both Curtis Road culverts are undersized for existing and future flows and overtopping occurs locally near the culvert crossings. The overtopping culvert at the intersection of MS-06 and Curtis Road is not contained within the 100-year floodplain limits. Therefore, berming will be provided in order to protect proposed lots from overtopping flows. Verify berms will be able to withstand the flows and velocity from the

The existing 24" CMP culvert will not be upsized within the context of this report and development. The culvert is owned by El Paso County and timing of improvements, if any, will be controlled by the County.

Furthermore, the *Haegler Ranch DBPS* recommends channel improvements within Drainageway MS-06. Per the *Haegler Ranch DBPS*, all recommended channel sections are trapezoidal with side slopes of 4:1 and a maximum depth of five feet. Within the limits of the site, three (3) channel bottom widths are recommended for MS-06. The first reach, from station 0+00 - 31+34, is proposed with a 15' bottom width, the second reach from 31+34 to 74+61, MS-06 is proposed with a 30' bottom width, and the last reach from station 74+61 - 103+62 is proposed with a 20' channel bottom. The portion of the MS-06 channel improvements along Filing 3 has been analyzed with the Engineer's Certification of No Impact Letter. This letter shows the proposed Drainageway MS-06 sections and flow depths. This letter can be found in Appendix E.

Based on flood impacts, stream stability and cost effectiveness, this study recommended a sub-regional detention approach. This allows future development anywhere in the basin with the construction of an associated sub-regional pond. However, based on the *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch*, Filing 3 will utilize three on-site full spectrum water quality and detention ponds instead. These full spectrum detention ponds will limit developed discharge into the MS-06 and WF-R7A Drainageways to less than historic rates.

The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR was executed on Haegler Ranch Tributary 2, 3, and 4. The LOMR revised the onsite effective flood zone from Zone A to Zone AE. See FIRM Map Panel 08041C0558G for limits of LOMR study and revised flood zones, presented in Appendix E.

The Gieck Ranch Drainage Basin covers approximately 22 square miles and begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. The Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains south to the Arkansas River near the city of Pueblo, Colorado. The majority of the area within the basin is undeveloped and is characterized as rolling range land typically associated with Colorado's semi-arid climates. Anticipated land use for the basin includes residential, industrial, agricultural and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

Based upon provided drainage maps and analysis, Gieck Ranch discharges a total of 1,017 cfs onto the site within Major Drainageway Gieck Ranch West Fork Reach 7A (WF-R7A). An existing 66" CMP and 36" CMP convey the offsite flow across Judge Orr Road onto the site. The existing culverts at Judge Orr Road are undersized for existing and future flows resulting in localized overtopping. The DBPS recommends the culvert be upsized to four -12' x 5' box culverts. The culvert will not be upsized within

the context of this report and development. The culvert is owned by El Paso County and timing of the recommended improvements will be controlled by the County. The overtopping at the intersection of WF-R7A is not contained within the 100-year floodplain. Therefore, at time of Final Drainage Report for Filing 4, berming will be provided that will protect proposed lots from overtopping flows.

See Table 2 for comparison of Drainageway identification and the naming convention used within the context of this report. See Table 3 for a comparison of 100-year flows as calculated in the aforementioned DBPS and LOMR. An existing conditions drainage map is presented in Appendix E. Table 1: Major Drainageway Naming Convention

	Major Dr	rainageway Naming Conventior	ns
Saddlehorn Ranch MDDP/PDR:	Per Haegler Ranch DBPS:	Per Geick Ranch DBPS:	Per Sante Fe Springs LOMR:
MS-06	Main Stem (MS- 06)	N/A*	Haegler Ranch Tributary 3
WF-R7A	N/A*	West Fork (Middle)/WF-R7A	N/A*

Table 2.	Major Dra	inageway_	$\mathbf{Fr} = 1$	00-Vear	Flow (Comparison
1 auto 2.	Major Dia	mageway – I	LA. I	00-1 cai	110w v	Comparison

Major Drainageways: 100-Year Flow Comparison												
Drainageway Name	Contributing Area (sq. mi.)	Q ₁₀₀ Per Haegler Ranch DBPS:	Q ₁₀₀ Per Geick Ranch DBPS:	Q ₁₀₀ Per Sante Fe Springs LOMR:								
MS-06 @ Curtis Road	1.05	590 cfs	N/A*	505 cfs								
WF-R7A @ Judge Orr Road	1.50	N/A*	1,017 cfs	N/A*								

*N/A: Flow regime outside limits of study.

The *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch* proposed the overall drainage facility design for Saddlehorn Ranch. Within the context of this report, onsite drainage basins the associated full spectrum water quality pond were established. As it pertains to Filing 3, three full spectrum water quality ponds are recommended. Roadside ditches and local street culverts will be utilized to capture and convey Filing 3's runoff to the water quality ponds. Saddlehorn Filing 4 will also utilize the same three ponds. Thus, the ponds were sized for both the Filing 3 and Filing 4 improvements. Pond C and Pond E will discharge into Drainageway MS-06, while Pond D will release into Drainageway WF-R7A. All ponds are full spectrum and will release at less than historic rates.

Existing Sub-basin Drainage

On-site, existing sub-basin drainage patterns are generally from northwest to southeast by way of Drainageway MS-06 and Drainageway WF-R7A. On-site areas flow directly into these drainageways, which also bypass off-site flows through the site.

On-site, existing drainage basins were established based upon existing topography and the limits of the 100-year floodplain. These existing sub-basins were analyzed in the *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch*. An existing drainage map has been provided in Appendix E.

Also provide copy of existing basin calculations in appendix.

Proposed Sub-basin Drainage

The proposed Filing 3 basin delineation is as follows;

Basin C consists of Sub-Basins C1-C10 combining for a total of 93.77 acres. In its existing condition, Basin C is rolling rangeland and runoff generally flows southeast towards Drainageway MS-06. In the proposed condition, Basin C will be rural 2.5 acre lots, paved roadway, and will include Pond C. Runoff from this basin will be collected in road side ditches and conveyed to Pond C located in the southeast corner of the future Filing 4 development. Pond C will be a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway MS-06.

Basin D consists of Sub-basins D1-D7 combining for a total of 74.66 acres. In its existing condition, Basin D is rolling rangeland and runoff generally flows east to Drainageway WF-R7A. In the proposed condition, Basin D will be rural 2.5 acre lots, paved roadway, and will include Pond D. Runoff from this basin will be collected in road side ditches and conveyed west to Pond D located in the northeast corner of the future Filing 4 development. Pond D is a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway WF-R7A.

Basin E consists of Sub-basins E1-E4 combining for a total of 18.37 acres. In its existing condition, Basin E is rolling rangeland and runoff generally flows south towards Drainageway MS-06. In the proposed condition, Basin E will be rural 2.5 acre lots, paved roadway, and will include Pond E. Runoff from this basin will be collected in road side ditches and conveyed to Pond E located in the southern portion of the Filing 3 development along San Isidro Trail. Pond E will be a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway MS-06.

Basin UD consists of Sub-basins UD1-UD5 combining for a total of 74.27 acres. In their existing condition, these basins are rolling rangeland. Runoff from Basins UD1-UD3 generally flows south and east to Drainageway MS-06. Basin UD5 flows east to Drainageway MS-06. Basin UD4 represents Drainageway MS-06 and the runoff generated along the Filing 3 boundary. In the proposed condition, Basins UD1, UD2, UD3, and UD5 will be rural 2.5 acre lots with an Imperviousness = 6.2% and will be excluded from permanent stormwater quality management per Section I.7.1.B.5 of the ECM – Stormwater Quality Policy and Procedures.

Basin OS consists of Sub-basins OS1-OS5 combining for a total of 9.35 acres of offsite area. In their existing condition, these basins are paved roadway (Curtis Road & Judge Orr Road) and undeveloped

area. In the proposed condition, these basins will be improved with 8' of pavement width for both the Curtis Road and Judge Orr Road stretches. Basins OS1-OS4 will flow on-site prior to being captured in a roadside swale and conveyed to a proposed full spectrum detention pond prior to being released into Drainageway MS-06 or Drainageway WF-R7A. Basin OS5 will not be detained by a pond due to its location relative to the site. The improvements along Curtis Road within Basin OS5 will follow historic patterns and drain directly into Drainageway MS-06.

A summary table of proposed basin parameters and flow rates are presented in Appendix B.

Basin C runoff along with runoff from Sub-Basins OS1 and OS2 will be captured in roadside swales and conveyed to the proposed Pond C. This full spectrum pond will release treated flows at less than historic rates to minimize adverse impacts downstream. Basin D along with runoff from Sub-Basins OS3 and OS4 will be captured in roadside swales and conveyed to the proposed Pond D. Basin E will be captured in roadside swales and conveyed to the proposed Pond E. Pond C and Pond E will discharge into Drainageway MS-06. Pond D will discharge into Drainageway WF-R7A.

See Table 3 below for proposed Filing 3 pond parameters.

Tributary Sub-Basin	Pond Name	Tributary Acres	WQ Volume (ac-ft)	Total Detention Volume (ac-ft)	Provided Volume (ac-ft)	Maximum 100-Year Discharge (cfs)
С	POND C	96.84	0.745	2.208	2.391	41.2
D	POND D	78.02	0.621	2.051	2.315	60.1
E	POND E	18.37	0.087	0.303	0.424	9.6

Table 3: Pond Summary

DRAINAGE DESIGN CRITERIA

Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "*City of Colorado Spring/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual (CCSDCM), dated May 2014, as adopted by El Paso County.

Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Rational Method calculations were prepared, in accordance with Section 13.3.2.1. of

the CCSDCM, for the sub-basins that directly impact the sizing of ditches and local street culverts. Rational method calculations are presented in Appendix B.

Urban Drainage and Flood Control District's UD-Detention, Version 4.04 workbook was used for pond sizing. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. Pond sizing spreadsheets are presented in Appendix D.

Hydraulic Criteria

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for roadside ditch design. Ditches were checked for velocity and capacity per the CCS/EPCDCM Section 12.3.2.2. In order to check both capacity and velocity, a cross section analysis was performed on the roadside swales using the basin's maximum runoff Q and the proposed uniform slope of the swale. Swale cross sections have been presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for local road crossing culvert design. Culvert size was determined based on 100-year flows and hydraulic criteria from EPCDCM Chapter 9 –Culvert Design. All local road crossing culvert design reports are presented in Appendix C.

DRAINAGE FACILITY DESIGN

General Concept

The proposed stormwater conveyance system was designed to convey the developed Filing 3 runoff to one of three full spectrum detention ponds via roadside ditches and local street culverts. These full spectrum ponds were designed to release at less than historic rates to minimize adverse impacts downstream.

Improvements to Drainageway MS-06 are proposed within the Saddlehorn Filing 3 improvements. A no rise study has been conducted on the proposed Drainageway MS-06 improvements to ensure no rises to the floodplain occur as a result of the Filing 3 development. All proposed drainageway improvements, including the San Isidro culvert crossing and channel sections can be found in Appendix E. All improvements aforementioned to Drainageway WF-R7A are proposed with the Saddlehorn Filing 4 improvements. Outfall protection from Pond D is the only improvement to Drainageway WF-R7A proposed with the Filing 3 improvements. The remaining improvements to Drainageway MS-06 shall be implemented with the Filing 5 improvements.

Specific Details

Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume (WQCV), and consider the need for Industrial Commercial BMP's.

Channel stability still needs to be addressed as part of the overall subdivision.

Step 1, Reducing Runoff Volumes: The development of the project site is proposed single family residential lots (2.5 ac. min.) with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roadways utilize soil riprap lined roadside ditches further disconnecting impervious areas. These practices will also allow for increased infiltration and reduce runoff volume.

Step 2, Stabilize Drainageways: Filing 3 utilizes roadside ditches with culvert crossings throughout. These roadside ditches direct the on-site development flows to the proposed detention ponds within the project that releases at or below historic rates into Drainageways MS-06 and WF-R7A. Based upon the proposed reduction in released flows compared to the pre-developed flows, no impacts to downstream Drainageway MS-06 or Drainageway WF-R7A are anticipated.

Step 3, Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV in a full spectrum water quality and detention pond that is designed per current El Paso County drainage criteria.

Step 4 Consider the need for Industrial and Commercial BMP's: No industrial or commercial uses are proposed within this development. However, a site specific storm water quality and erosion control plan and narrative are prepared in conjunction with this report. Site specific temporary source control BMPs as well as permanent BMP's are detailed in this plan and narrative to protect receiving waters.

Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention are provided for all developed basins. Outlet structure release rates are limited to less than historic rates to minimize adverse impacts to downstream stormwater facilities. Complete pond and outlet structure designs are presented in Appendix D.

Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted with each Final Drainage Report. The Erosion Control Plans for Filing 3 have been submitted concurrently with this report.

Operation & Maintenance

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within the any platted County ROW will be owned and maintained by El Paso County. All proposed drainage structures within easements or tracts will be owned and maintained by the 824 Acre Metropolitan No. 1. Vegetation in the natural and improved portions of Drainageway MS-06 with the Filing 3 improvements is the responsibility of 824 Acre Metropolitan District No. 1. This includes all mowing, seeding and weed control activities. An Inspection & Maintenance Plan is submitted concurrently with this drainage report that details the required maintenance activities and intervals to ensure proper function of all stormwater infrastructure in the future.



The open space tract can be subtracted

Drainage and Bridge Fees

Drainage and Bridge Fees are due at time of final platting. An estimate of basin fees for the proposed development within Haegler Ranch drainage basin is provided below. Fee reduction for low density lots are applied to the overall basin fees in the next section. Additionally, reimbursable expenses are detailed % impervious for 2.5 acresses % in the formation of the section of th

Total Filing 3 Platted Acres: 175.43 ac Total Filing 3 Impervious Acres = 17.5 ac (175.43 ac x 10%)

Filing 3 Fee Totals (Prior to Reductions):

Based on average lot - size and plat restriction, 10% is okay.

Bridge Fees \$ 1,640/ac x 17.5 ac = \$28,700 \$1,916 Drainage Fees \$11,113/ac x 17.5 ac = \$194,478 \$12,985

Table 3-1 is 11%

Filing 3 Drainage Fee Reduction: 25% Reduction for Low Density Lots: \$194,478 x 25% = \$48,619

Filing 3 Fee Totals (After Reductions):

Bridge Fees \$ 1,640/ac x 17.5 ac = \$28,700 **Drainage Fees** \$194,478 - \$48,619 = \$145,859

Construction Cost Opinion

Cost opinion has been presented in Appendix A.

SUMMARY

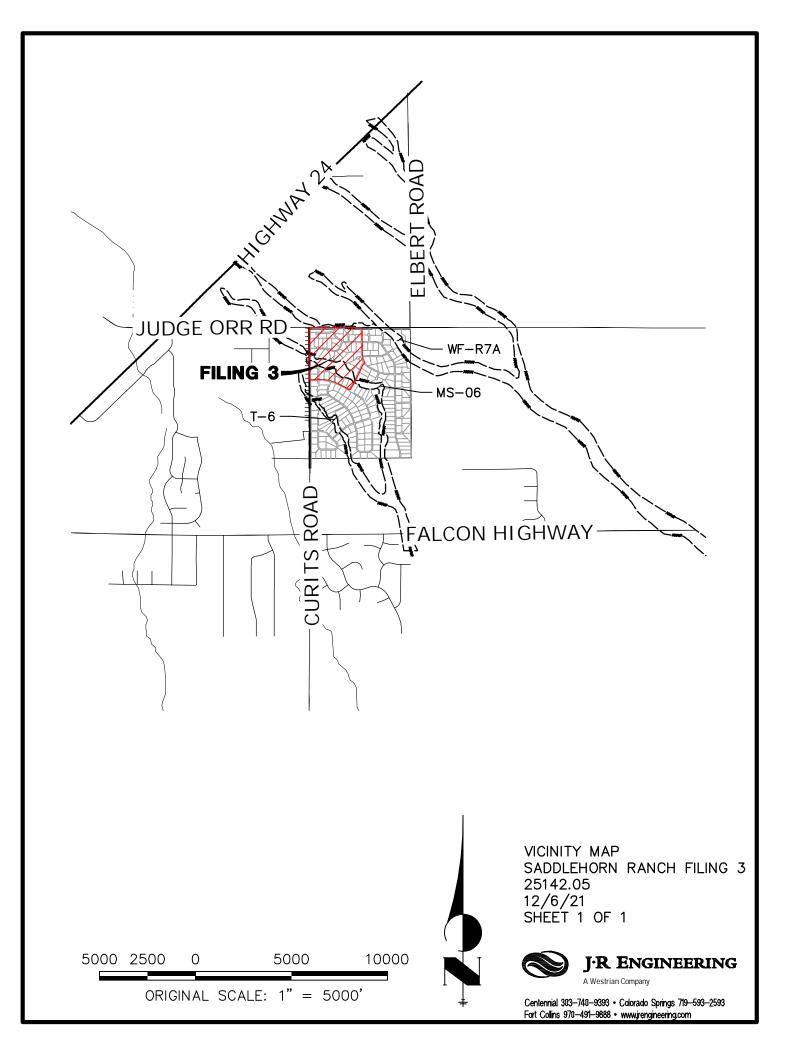
The proposed development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements, including ditches, culverts, detention ponds and drainage channel improvements. The proposed development will not adversely affect the offsite major drainageways or surrounding development. This report meets the latest El Paso County Drainage Criteria requirements for this site and is in accordance with the PDR/MDDP for Saddlehorn Ranch.

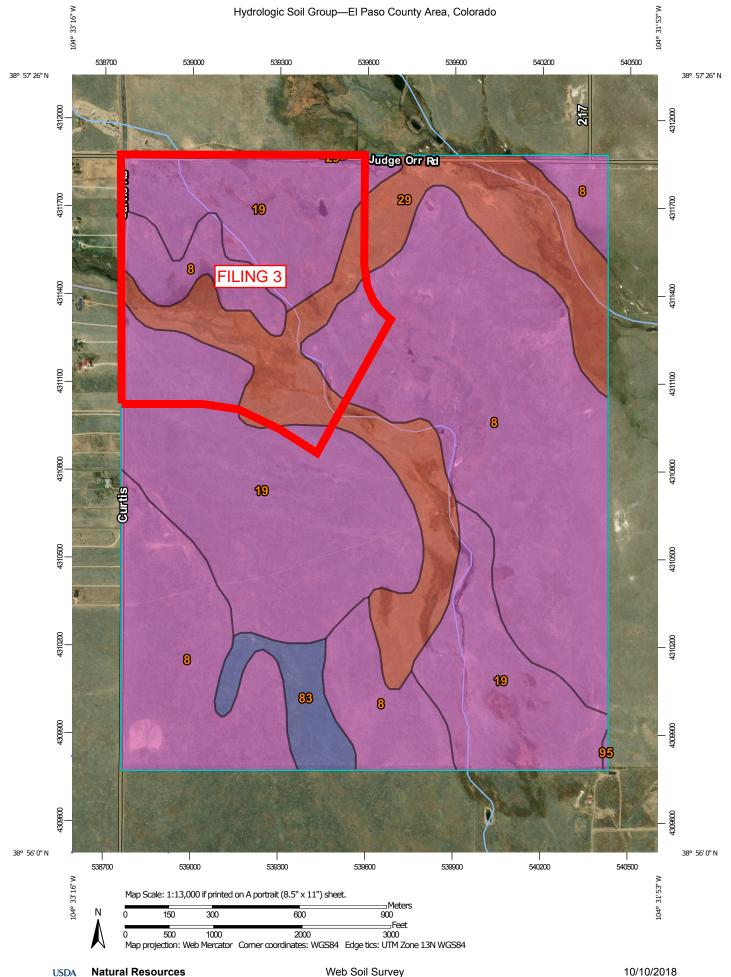
REFERENCES:

- 1. <u>City of Colorado Springs Drainage Criteria Manual Volume 1</u>, City of Colorado Springs, CO, May 2014.
- 2. <u>Urban Storm Drainage Criteria Manual</u>, Urban Drainage and Flood Control District, Latest Revision.
- <u>Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch</u>, JR Engineering, May 2020.
- 4. <u>Haegler Ranch Drainage Basin Planning Study</u>, URS Corporation, May 2009.
- 5. <u>The Santa Fe Springs Haegler Ranch Drainage Basin LOMR</u>, Federal Emergency Management Agency, October 20, 2004.
- 6. <u>Final Drainage Report for Saddlehorn Ranch Filing 2</u>, JR Engineering, January 4, 2022

APPENDIX A

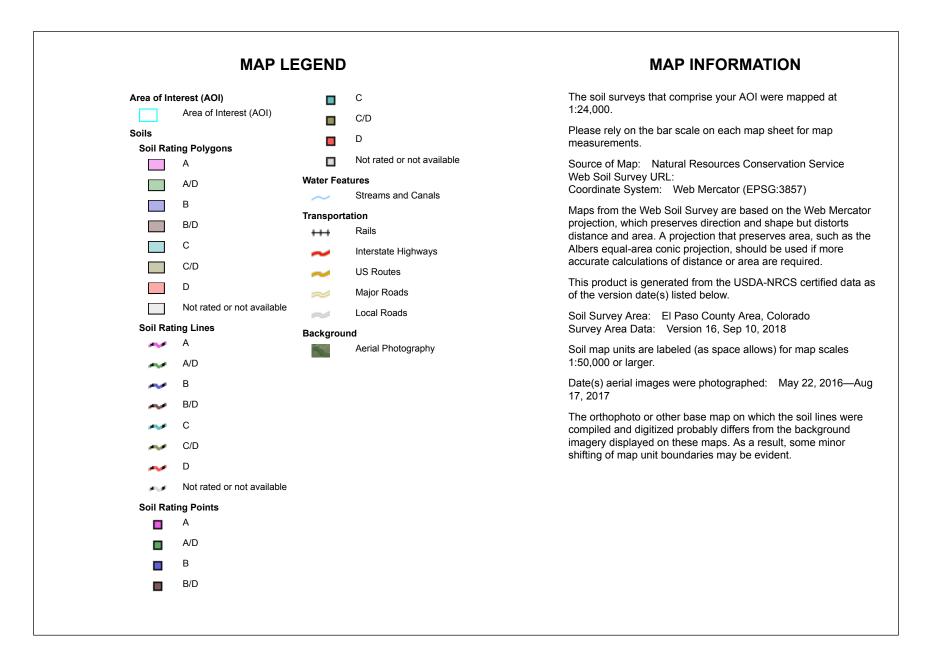
FIGURES AND EXHIBITS





Conservation Service

Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	388.3	44.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	307.3	35.3%
29	Fluvaquentic Haplaquolls, nearly level	D	150.0	17.2%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	24.6	2.8%
95	Truckton loamy sand, 1 to 9 percent slopes	A	0.6	0.1%
Totals for Area of Inter	est		870.8	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or loodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services

NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation ind may appear outside of the floodplain

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

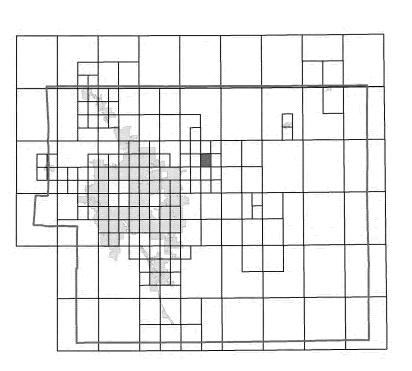
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

> El Paso County Vertical Datum Offset Table **Vertical Datum**

Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

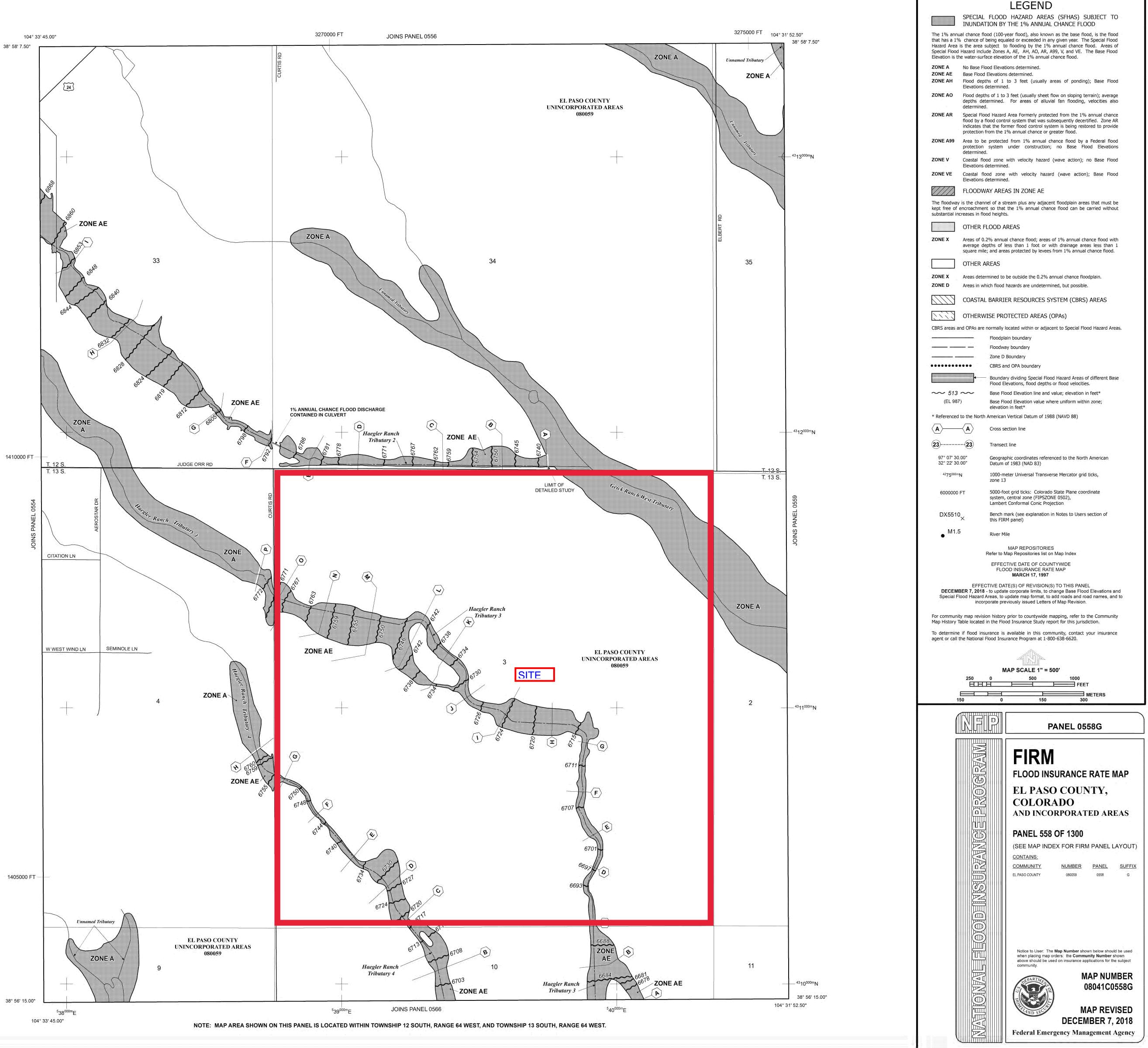
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



2022 Financial Assurance Estimate Form

(with pre-plat construction)

Updated: 12/22/2020

		RUJECTI	NFORMATI				
roject Name: Saddlehorn Filing 3	_		Date		_	PCD File No.	
			Unit			· ·	Plat Construction)
Description	Quantity	Units	Cost		Total	% Complete	Remaining
ECTION 1 - GRADING AND EROSION CONT	ROL (Constructio	<mark>n and Perm</mark>	anent BMPs)				
* Earthwork							
less than 1,000; \$5,300 min		CY	\$ 8.00	=	\$ -		\$ -
1,000-5,000; \$8,000 min		CY	\$ 6.00	=	\$ -		\$-
5,001-20,000; \$30,000 min		CY	\$ 5.00	=	\$ -		\$-
20,001-50,000; \$100,000 min		CY	\$ 3.50	=	\$ -		\$-
50,001-200,000; \$175,000 min	147,182	CY	\$ 2.50	=	\$ 367,955.		\$ 367,955.0
greater than 200,000; \$500,000 min		CY	\$ 2.00	=	\$ -		\$ -
* Permanent Seeding (inc. noxious weed mgmnt.)	26	AC	\$ 828.00	=	\$ 21,528.		\$ 21,528.0
* Mulching	26	AC	\$ 777.00	=	\$ 20,202.	00	\$ 20,202.0
* Permanent Erosion Control Blanket	11,656	SY	\$ 6.00	=	\$ 69,936.	00	\$ 69,936.0
* Permanent Pond/BMP Construction		CY	\$ 21.00	=	\$ -		\$ -
* Permanent Pond/BMP (provide engineer's estimate)		EA		=	\$-		\$-
					\$ -		\$-
*Detention Outlet Structure	1	EA	\$ 5,000.00	=	\$ 5,000.	00	\$ 5,000.0
*Concrete/Riprap Forebay	3	EA	\$ 3,000.00	=	\$ 9,000.	00	\$ 9,000.0
*Concrete Trickle Channel	704	CY	\$ 95.00	=	\$ 66,880.	00	\$ 66,880.0
*Detention Emergency Spillway	3	EA	\$ 4,000.00		\$ 12,000.	00	\$ 12,000.0
*Drainageway riprap, d50 size from 6" to 24"	1,609	Tons	\$ 83.00		\$ 133,547.	00	\$ 133,547.0
*Permanent WQ Feature (EDB)	3	EA	\$ 5,000.00		\$ 15,000.	00	\$ 15,000.0
*Gravel Maintenance Access Road	3,486	SY	\$ 45.00		\$ 156,870.	00	\$ 156,870.0
					\$ -		\$ -
Stabilized Staging Area	2,000	SY	\$ 2.00	=	\$ 4,000.	00	\$ 4,000.0
Safety Fence	11,960	LF	\$ 3.00	=	\$ 35,880.	00	\$ 35,880.0
Temporary Erosion Control Blanket		SY	\$ 3.00	-	\$ -		\$ -
Vehicle Tracking Control	4	EA	\$ 2,453.00	-	\$ 9,812.	00	\$ 9,812.0
Silt Fence	22,874	LF	\$ 2.60	=	\$ 59.472.	40	\$ 59,472,4
Temporary Seeding		AC	\$ 650.00	=	\$ -		\$ -
Temporary Slope Drain	96	LF	\$ 30.00		\$ 2.880.		\$ 2.880.0
Temporary Mulch		AC	\$ 777.00	=	\$ -		\$ -
Erosion Bales		EA	\$ 26.00	=	\$ -		\$ -
Erosion Logs/Straw Waddle	1,640	LF	\$ 5.00	=	\$ 8,200.		\$ 8,200.0
Reinforced Rock Berm	530	LF	\$ 9.00		\$ 4,770.		\$ 4,770.0
Rock Check Dams	107	EA	\$ 518.00	=	\$ 55,426.		\$ 55,426.0
Outlet Protection	107	EA	\$ 153.00	_	\$ 2,907.		\$ 2,907.0
Inlet Protection	19	EA	\$ 173.00	=	\$ 3,287.		\$ 3,287.0
Sediment Basin	3	EA	\$ 1,824.00	=	\$ 5,472.		\$ 5,472.0
Concrete Washout Basin	1	EA	\$ 932.00	_	\$ 932.		\$ 932.0
		LA	ψ 332.00	=	\$ 932.		\$
[insert items not listed but part of construction plans]				=	\$ - \$		s -
	AINTENANCE (359	6 of Constru	iction BMPc)	=	\$ 53,605.		- \$ 53.605.
- Subject to defect warranty financial assurance. A minimum of 20% shal a retained until final acceptance (MAXIMUM OF 80% COMPLETE LLOWED)			n 1 Subtotal	=	\$ 1,124,561.8		\$ 1,124,561.8

oject Name: Saddlehorn Filing 3				Date		_		PCD File No.	
ojoot namor oddaronom ning o				buto					
escription		Quantity	Units	Unit Cost			Total	(with Pre-P % Complete	lat Construction) Remaining
ECTION 2 - PUBLIC IMPROVEME	NTS *								
DADWAY IMPROVEMENTS			1.0	A 50 000 00			50.000.00		50.000
Mobilization/Construction Traffic Control		1	LS SY	\$ 50,000.00	=	\$	50,000.00	\$	
Removal of Asphalt (Full Depth) Removal of Asphalt (Planing-2")		515 2,354	SY	\$ 10.00 \$ 5.00		\$ \$	5,150.00	3	
Removal of Striping		3,117	LF	\$ 5.00		\$	3,117.00	3	
Removal of Fencing		3,021	LF	\$ 5.00		\$	15,105.00	\$	
Aggregate Base Course (135 lbs/cf)	10" Thick	2,086	Tons	\$ 29.00	-	\$	60,494.00	\$	
Aggregate Base Course (135 lbs/cf)		2,000	CY	\$ 52.00		\$	-	\$	
Asphalt Pavement (3" thick)			SY	\$ 14.50		\$	-	\$	-
Asphalt Pavement (4" thick)			SY	\$ 20.00		\$	-	\$	-
Asphalt Pavement (6" thick)			SY	\$ 30.00		\$	-	\$	
Asphalt Pavement (147 lbs/cf)	<u>7</u> " thick	23,267	Tons	\$ 91.00	=	\$	2,117,287.90	\$	
Raised Median, Paved			SF	\$ 8.30	=	\$	-	\$	
Regulatory Sign/Advisory Sign		22	EA	\$ 311.00	=	\$	6,842.00	\$	
Guide/Street Name Sign		22	EA	\$ 250.00	=	\$	5,500.00	\$	
Epoxy Pavement Marking		9,005	SF	\$ 14.00	=	\$	126,063.84	\$	
Thermoplastic Pavement Marking Barricade - Type 3		93 3	SF EA	\$ 24.00	=	\$	2,232.00	\$	
Delineator - Type I		3	EA	\$ 207.00 \$ 25.00	=	\$ \$	621.00	3	
Electrical Conduit, Size =				\$ 25.00	=	\$		3	
			LF	\$ 17.00	=	\$		4	
insert items not listed but part of construction	n plansl				-	\$		\$	
ORM DRAIN IMPROVEMENTS	. []					÷			
Concrete Box Culvert (M Standard), Size (NxH)		LF		=	\$	-	\$	-
8" Reinforced Concrete Pipe	,	443	LF	\$ 67.00	-	\$	29,651.52	ş	
4" Reinforced Concrete Pipe		226	LF	\$ 81.00	=	\$	18,306.00	\$	18,306.
0" Reinforced Concrete Pipe		99	LF	\$ 100.00	=	\$	9,939.00	\$	9,939.0
6" Reinforced Concrete Pipe		38	LF	\$ 124.00	=	\$	4,712.00	\$	4,712.
2" Reinforced Concrete Pipe			LF	\$ 166.00	=	\$	-	\$	-
8" Reinforced Concrete Pipe			LF	\$ 202.00	=	\$	-	\$	
4" Reinforced Concrete Pipe			LF	\$ 254.00	=	\$	-	ş	
0" Reinforced Concrete Pipe			LF	\$ 298.00	=	\$	-	\$	
6" Reinforced Concrete Pipe			LF	\$ 344.00	=	\$	-	\$	
2" Reinforced Concrete Pipe 9" x 30" HERCP		224	LF LF	\$ 393.00 \$ 100.00	=	\$	-	\$	
2' x 4' RCBC		224 160		\$ 100.00 \$ 1,100.00	=	\$ \$	22,400.00 176,000.00	\$	
8" Corrugated Steel Pipe		100	LF	\$ 1,100.00	-	\$	170,000.00	4	
24" Corrugated Steel Pipe			LF	\$ 99.00	=	\$		\$	
30" Corrugated Steel Pipe			LF	\$ 126.00	=	\$	-	4	
36" Corrugated Steel Pipe			LF	\$ 152.00	-	\$	-	\$	
2" Corrugated Steel Pipe			LF	\$ 174.00	=	\$	-	\$	
18" Corrugated Steel Pipe			LF	\$ 184.00	=	\$	-	ş	
54" Corrugated Steel Pipe			LF	\$ 269.00	=	\$	-	\$	-
0" Corrugated Steel Pipe			LF	\$ 290.00	=	\$	-	\$	-
6" Corrugated Steel Pipe			LF	\$ 352.00	=	\$	-	\$	-
2" Corrugated Steel Pipe			LF	\$ 414.00		\$	-	\$	
8" Corrugated Steel Pipe			LF	\$ 476.00	-	\$	-	\$	
34" Corrugated Steel Pipe Flared End Section (FES) RCP Size =	401 505		LF	\$ 569.00	=	\$	-	\$	-
unit cost = 6x pipe unit cost)	18" RCP	16	EA	\$ 402.00	=	\$	6,432.00	\$	6,432.0
lared End Section (FES) CSP Size =		10		¢ 407.00		*	4.0/0.00	s	4.0/07
unit cost = 6x pipe unit cost)	24" RCP	10	EA	\$ 486.00	=	\$	4,860.00	3	4,860.0
lared End Section (FES) CSP Size = unit cost = 6x pipe unit cost)	30" RCP	5	EA	\$ 600.00	=	\$	3,000.00	\$	3,000.0
lared End Section (FES) CSP Size =			LA	A 100 5					
unit cost = 6x pipe unit cost)	19" X 30" HE	4	EA	\$ 100.00	=	\$	400.00	\$	
nd Treatment- Headwall/Wingwall		2	EA	\$ 10,000.0	=	\$	20,000.00	\$	
nd Treatment - Cutoff Wall			EA		=	\$	-	\$	
eotextile (Erosion Control)			SY	\$ 6.20		\$	-	\$	
ip Rap, d50 size from 6" to 24"		1,402	Tons	\$ 83.00	=	\$	116,357.70	\$	
tip Rap, Grouted			Tons	\$ 98.00		\$	-	\$	
Drainage Channel Construction			LF	¢	=	\$	-	\$	
Prainage Channel Lining, Concrete	(Lou: Elaur)	1.050	CY	\$ 590.00		\$	-	\$	
Drainage Channel Lining, Rip Rap	(Low Flow)	1,250	CY AC	\$ 116.00 \$ 1,520.00		\$	145,000.00	\$	
rainage Channel Lining, Grass rainage Channel Lining, Other Stabilization			AC	φ 1,520.00	=	\$		\$	
Tamage Ghannel Linnig, Other Stabilization					=	\$	-	3	
							-		
nsert items not listed but part of construction	n nlansl					\$	-	\$	

Project Name: Saddlehorn Filing 3 Description Quantit SECTION 3 - COMMON DEVELOPMENT IMPROVEMENTS ROADWAY IMPROVEMENTS STORM DRAIN IMPROVEMENTS (Exception: Permaner) WATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6" Water Main Pipe (PVC), Size 8" 10,				Unit Cost Ct and N	= = = = = = er Section 1)	\$ \$ \$ \$ \$	Total by EPC)** - - - - - - - -	PCD File No. (with Pre % Complete	-Plat (\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	Construction) Remaining - - - - - -
STORM DRAIN IMPROVEMENTS STORM DRAIN IMPROVEMENTS WATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"		ate or Dis		Cost ct and N	= = = = = = er Section 1)	\$ \$ \$ \$ \$	by EPC)** - - - - -	•	\$ \$ \$ \$ \$	Remaining - - - -
STORM DRAIN IMPROVEMENTS COADWAY IMPROVEMENTS COADWAY IMPROVEMENTS CEXCEPTION : Permaner STORM DRAIN IMPROVEMENTS WATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"		ate or Dis		ct and N	= = = = = = er Section 1)	\$ \$ \$ \$ \$	by EPC)** - - - - -	% Complete	\$ \$ \$ \$	-
STORM DRAIN IMPROVEMENTS (Exception: Permaner NATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"					= = = = = = er Section 1)	\$ \$ \$ \$ \$	- - - - - - - -		\$ \$ \$ \$	-
TORM DRAIN IMPROVEMENTS (Exception: Permaner VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e iter	mized unde	= = = = = er Section 1)	\$ \$ \$ \$ \$	- - - -		\$ \$ \$ \$	-
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e itel	mized unde	= = = = = er Section 1)	\$ \$ \$ \$ \$	- - - -		\$ \$ \$ \$	-
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e iter	mized unde	= = = er Section 1)	\$ \$ \$ \$			\$ \$ \$	-
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e iter	mized unde	= = = er Section 1)	\$ \$ \$	-		\$ \$	-
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e itei	mized unde	= = er Section 1)	\$ \$	-		\$	
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e ite	mized unde	= er Section 1)	\$				
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"	t Pond/B	3MP shall b	e ite	mized unde	er Section 1)					-
VATER SYSTEM IMPROVEMENTS Water Main Pipe (PVC), Size 6"									÷	
Water Main Pipe (PVC), Size 6"					=	\$	-		\$	-
Water Main Pipe (PVC), Size 6"					=	\$	-		\$	-
Water Main Pipe (PVC), Size 6"					=	\$	-		\$	-
Water Main Pipe (PVC), Size 6"					=	\$	-		\$	-
Water Main Pipe (PVC), Size 6"					=	\$	-		\$	-
Water Main Pipe (PVC), Size 6"					=	\$	-		\$	-
Water Main Pipe (PVC), Size 8" 10,	313	LF	\$	64.00	=	\$	20,032.00		\$	20,032.
	279	LF	\$	66.00	=	\$	678,414.00		\$	678,414
Water Main Pipe (Ductile Iron), Size 8"		LF	\$	78.00	=	\$	-		\$	-
Gate Valves, 8"	35	EA		1,923.00	=	\$	67,305.00		\$	67,305.
Fire Hydrant Assembly, w/ all valves	24	EA		6,828.00	=	\$	163,872.00		\$	163,872.
Water Service Line Installation, inc. tap and valves	44	EA EA	\$	1,370.00	=	\$ \$	60,280.00		\$	60,280.
Fire Cistern Installation, complete		EA			=	⇒ \$			\$ \$	-
[insert items not listed but part of construction plans]					=	\$			\$	
ANITARY SEWER IMPROVEMENTS						Φ	-		φ	-
Sewer Main Pipe (PVC), Size 8"		LF	\$	66.00	=	\$	-		\$	-
Sanitary Sewer Manhole, Depth < 15 feet		EA		4,540.00	=	\$	-		\$	-
Sanitary Service Line Installation, complete		EA		1,451.00	=	\$	-		\$	-
Sanitary Sewer Lift Station, complete		EA			=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction plans]					=	\$	-		\$	-
ANDSCAPING IMPROVEMENTS (For subdivisio	n specifi	ic condition	of a	pproval, or	PUD)					
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
Section 3 is not subject to defect warranty requirements		EA		Subtotal	=	\$	- 989,903.00		\$ \$	- 989,903.0
		Section	130	Subiolai		D	989,903.00		Þ	989,903.0
S-BUILT PLANS (Public Improvements inc. Permanent WQCV BMPs)		LS			=	\$	-		\$	-
OND/BMP CERTIFICATION (inc. elevations and volume calculations)		LS			=	\$	-		\$	-
					Total	Const	ruction Financia	I Assurance	\$	5,075,705.8
			(Su	m of all sec	tion subtota	als plus a	as-builts and pond/BI	MP certification)		
Tetel Dev										
	-	-					(with Pre-Plat C	-	\$	5,075,705.8
(Sum	of all sec	stion totals I	ess	credit for ite	ems comple	te plus a	s-builts and pond/B	VIP certification)		
					Total De	foct W	arranty Financia		\$	768,631.7
	(200/	of all itama	ida	otified on (*			d at time of prelimina		φ	700,031.7
	(2070	or an items	luci	nuncu as (). TO DE COI	ateralize	d at time of prelimina	ary acceptance)		

Approved by Owner / Applicant

Date

Approved by El Paso County Engineer / ECM Administrator

Date

APPENDIX B

HYDROLOGIC CALCULATIONS

COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: Saddlehorn Ranch Filing 3 Location: El Paso County

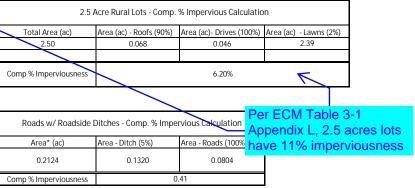
Project Name: <u>Saddlehorn Ranch</u> Project No.: <u>25142.05</u>

Calculated By: AAM Checked By: TBD

Date: 1/4/22

			Paved Roads	S	2.5	Acre Rural I	ots		Lawns		Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
C1	6.04	45%	1.07	8.0%	6.2%	4.97	5.1%	2%	0.00	0.0%	13.1%
C2	3.35	45%	1.50	20.1%	6.2%	1.85	3.4%	2%	0.00	0.0%	23.6%
C3	23.44	45%	1.63	3.1%	6.2%	21.81	5.8%	2%	0.00	0.0%	8.9%
C4	10.94	45%	3.40	14.0%	6.2%	7.54	4.3%	2%	0.00	0.0%	18.3%
C5	2.35	45%	0.83	15.9%	6.2%	1.52	4.0%	2%	0.00	0.0%	19.9%
C6	3.95	45%	1.59	18.1%	6.2%	2.36	3.7%	2%	0.00	0.0%	21.8%
C7	2.14	45%	1.00	21.0%	6.2%	1.14	3.3%	2%	0.00	0.0%	24.3%
C8	22.55	45%	2.21	4.4%	6.2%	20.34	5.6%	2%	0.00	0.0%	10.0%
С9	2.63	45%	1.98	33.9%	6.2%	0.65	1.5%	2%	0.00	0.0%	35.4%
C10	16.38	45%	2.47	6.8%	6.2%	11.85	4.5%	2%	2.06	0.3%	11.5%
D1	9.11	45%	1.51	7.5%	6.2%	7.60	5.2%	2%	0.00	0.0%	12.6%
D2	8.49	45%	1.49	7.9%	6.2%	7.00	5.1%	2%	0.00	0.0%	13.0%
D3	3.21	45%	0.19	2.7%	6.2%	3.02	5.8%	2%	0.00	0.0%	8.5%
D4	10.01	45%	0.35	1.6%	6.2%	8.21	5.1%	2%	1.45	0.3%	6.9%
D5	9.56	45%	2.78	13.1%	6.2%	6.78	4.4%	2%	0.00	0.0%	17.5%
D6	0.34	45%	0.34	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
D7	33.94	45%	7.65	10.1%	6.2%	24.05	4.4%	2%	2.24	0.1%	14.7%
E1	17.12	45%	0.71	1.9%	6.2%	13.22	4.8%	2%	3.19	0.4%	7.0%
E2	0.37	45%	0.37	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
E3	0.20	45%	0.20	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
E4	0.68	45%	0.00	0.0%	6.2%	0.19	1.7%	2%	0.49	1.4%	3.2%
UD1	7.48	45%	0.00	0.0%	6.2%	7.48	6.2%	2%	0.00	0.0%	6.2%
UD2	9.17	45%	0.00	0.0%	6.2%	9.17	6.2%	2%	0.00	0.0%	6.2%
UD3	2.23	45%	0.00	0.0%	6.2%	2.23	6.2%	2%	0.00	0.0%	6.2%
UD4	34.90	45%	0.00	0.0%	6.2%	0.00	0.0%	2%	34.90	2.0%	2.0%
UD5	20.49	45%	0.00	0.0%	6.2%	20.49	6.2%	2%	0.00	0.0%	6.2%
OS1	2.37	100%	1.35	57.0%	6.2%	0.00	0.0%	2%	1.02	0.9%	57.8%
OS2	0.70	100%	0.21	30.0%	6.2%	0.00	0.0%	2%	0.49	1.4%	31.4%
OS3	2.28	100%	1.35	59.2%	6.2%	0.00	0.0%	2%	0.93	0.8%	60.0%
OS4	1.08	100%	0.58	53.7%	6.2%	0.00	0.0%	2%	0.50	0.9%	54.6%
OS5	2.92	100%	0.59	20.2%	6.2%	0.94	2.0%	2%	1.39	1.0%	23.2%
F1	1.35	100%	0.53	39.3%	6.2%	0.00	0.0%	2%	0.82	1.2%	40.5%
F2	7.67	45%	0.98	5.7%	6.2%	6.69	5.4%	2%	0.00	0.0%	11.2%
F3	2.37	45%	2.37	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
F4	2.93	45%	2.93	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
TOTAL	284.74	1		1			1				12.4%

Land Use or Surface	Percent	Runoff Coefficients												
Characteristics	Impervious	2.4	ear	51	ear .	10-1	year	3	rear	50-year		100-	year	
		HSG A&B	HSG CAD	HIGASO	HSG C&D	HSG A&B	HIG CED							
Business												6		
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89	
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68	
Residential								-				-	-	
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65	
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58	
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57	
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56	
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55	
Industrial		-		-		-		-		-			-	
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74	
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52	
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54	
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58	
Undeveloped Areas	-			-			-	-	-					
Historic Flow Analysis-	2								-					
Greenbelts, Agriculture		0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51	
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	
Forest					0.15	0.15	0.25	0.25						
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Offsite Row Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59	
Streets														
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74	
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96	
Roofs	90	0.71	0.73	0,73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Lawins	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	



*Area based on 250 LF roadway from CL to outside edge of roadside ditch

The above conservatively rounded to 45%.

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

bdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name: Saddlehorn Ranch Project No.: 25142.05

Calculated By: AAM

Checked By: TBD

Date: 1/4/22

		Basins Total	Hydro	ologic Soil (Group	Hydro	ologic Soil (Group	Mir	nor Coeffici	ents	Maj	or Coefficie	ents		Basins Total
Basin ID	Total Area (ac)	Weighted % Imp.	Area A (ac)	Area B (ac)	Area C/D (ac)	% A (ac)	% B (ac)	% C/D (ac)	C _{5,A}	C _{5,B}	C _{5,C/D}	C _{100,A}	C _{100,B}	C _{100,C/D}	Basins Total Weighted C_5	Weighted C ₁₀₀
C1	6.04	13.1%	6.04	0.00	0.00	100%	0%	0%	0.06	0.09	0.14	0.21	0.49	0.54	0.06	0.21
C2	3.35	23.6%	3.35	0.00	0.00	100%	0%	0%	0.14	0.18	0.23	0.29	0.54	0.58	0.14	0.29
C3	23.44	8.9%	23.44	0.00	0.00	100%	0%	0%	0.04	0.06	0.11	0.18	0.47	0.52	0.04	0.18
C4	10.94	18.3%	5.12	0.00	5.82	47%	0%	53%	0.10	0.14	0.19	0.25	0.51	0.56	0.14	0.42
C5	2.35	19.9%	2.35	0.00	0.00	100%	0%	0%	0.11	0.15	0.20	0.26	0.52	0.57	0.11	0.26
C6	3.95	21.8%	3.95	0.00	0.00	100%	0%	0%	0.12	0.16	0.21	0.28	0.53	0.57	0.12	0.28
C7	2.14	24.3%	1.55	0.00	0.59	72%	0%	28%	0.14	0.19	0.23	0.30	0.54	0.58	0.17	0.38
C8	22.55	10.0%	22.55	0.00	0.00	100%	0%	0%	0.05	0.07	0.12	0.19	0.47	0.52	0.05	0.19
С9	2.63	35.4%	2.63	0.00	0.00	100%	0%	0%	0.23	0.28	0.32	0.39	0.59	0.63	0.23	0.39
C10	16.38	11.5%	16.38	0.00	0.00	100%	0%	0%	0.05	0.08	0.13	0.20	0.48	0.53	0.05	0.20
D1	9.11	12.6%	9.11	0.00	0.00	100%	0%	0%	0.06	0.09	0.14	0.21	0.49	0.54	0.06	0.21
D2	8.49	13.0%	7.40	0.00	1.09	87%	0%	13%	0.06	0.09	0.14	0.21	0.49	0.54	0.07	0.25
D3	3.21	8.5%	3.21	0.00	0.00	100%	0%	0%	0.04	0.06	0.10	0.18	0.47	0.52	0.04	0.18
D4	10.01	6.9%	3.16	0.00	6.85	32%	0%	68%	0.03	0.05	0.09	0.16	0.46	0.51	0.07	0.40
D5	9.56	17.5%	3.76	0.00	5.80	39%	0%	61%	0.09	0.13	0.18	0.25	0.51	0.56	0.14	0.43
D6	0.34	45.0%	0.17	0.00	0.17	50%	0%	50%	0.31	0.36	0.40	0.46	0.64	0.67	0.36	0.57
D7	33.94	14.7%	24.82	0.00	9.12	73%	0%	27%	0.07	0.11	0.16	0.22	0.50	0.54	0.10	0.31
E1	17.12	7.0%	14.17	0.00	2.95	83%	0%	17%	0.03	0.05	0.09	0.17	0.46	0.51	0.04	0.22
E2	0.37	45.0%	0.37	0.00	0.00	100%	0%	0%	0.31	0.36	0.40	0.46	0.64	0.67	0.31	0.46
E3	0.20	45.0%	0.18	0.00	0.02	90%	0%	10%	0.31	0.36	0.40	0.46	0.64	0.67	0.32	0.48
E4	0.68	3.2%	0.67	0.00	0.01	99%	0%	1%	0.01	0.02	0.06	0.14	0.44	0.50	0.01	0.14
UD1	7.48	6.2%	7.48	0.00	0.00	100%	0%	0%	0.03	0.04	0.09	0.16	0.46	0.51	0.03	0.16
UD2	9.17	6.2%	9.14	0.00	0.03	100%	0%	0%	0.03	0.04	0.09	0.16	0.46	0.51	0.03	0.16
UD3	2.23	6.2%	1.71	0.00	0.52	77%	0%	23%	0.03	0.04	0.09	0.16	0.46	0.51	0.04	0.24
UD4	34.90	2.0%	9.50	0.00	25.40	27%	0%	73%	0.01	0.01	0.05	0.13	0.44	0.49	0.04	0.39

UD5	20.49	6.2%	12.32	0.00	8.17	60%	0%	40%	0.03	0.04	0.09	0.16	0.46	0.51	0.05	0.30
OS1	2.37	57.8%	2.37	0.00	0.00	100%	0%	0%	0.43	0.47	0.51	0.56	0.70	0.72	0.43	0.56
OS2	0.70	31.4%	0.70	0.00	0.00	100%	0%	0%	0.20	0.24	0.29	0.35	0.57	0.61	0.20	0.35
OS3	2.28	60.0%	2.28	0.00	0.00	100%	0%	0%	0.45	0.49	0.53	0.58	0.71	0.73	0.45	0.58
OS4	1.08	54.6%	0.51	0.00	0.57	47%	0%	53%	0.40	0.44	0.48	0.54	0.68	0.71	0.44	0.63
OS5	2.92	23.2%	1.61	0.00	1.31	55%	0%	45%	0.13	0.17	0.22	0.29	0.54	0.58	0.17	0.42
F1	1.35	40.5%	1.35	0.00	0.00	100%	0%	0%	0.27	0.32	0.37	0.43	0.62	0.65	0.27	0.43
F2	7.67	11.2%	7.67	0.00	0.00	100%	0%	0%	0.05	0.08	0.13	0.20	0.48	0.53	0.05	0.20
F3	2.37	45.0%	2.00	0.00	0.37	84%	0%	16%	0.31	0.36	0.40	0.46	0.64	0.67	0.32	0.49
F4	2.93	45.0%	2.12	0.00	0.81	72%	0%	28%	0.31	0.36	0.40	0.46	0.64	0.67	0.34	0.52
TOTAL	284.74	12.4%	215.14	0.00	69.60	76%	0%	24%							0.08	0.29

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

NRCS				Storm Re	turn Period		
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year
A	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =
	0.84 <i>i</i> ^{1.302}	0.86 <i>i</i> ^{1.276}	0.87 <i>i</i> ^{1.232}	0.84 <i>i</i> ^{1.124}	0.85 <i>i</i> +0.025	0.78 <i>i</i> +0.110	0.65 <i>i</i> +0.254
В	C _B =	C _B =	C _B =	C _B =	C _B =	C _B =	C _B =
	0.84 <i>i</i> ^{1.169}	0.86 <i>i</i> ^{1.088}	0.81 <i>i</i> +0.057	0.63 <i>i</i> +0.249	0.56 <i>i</i> +0.328	0.47 <i>i</i> +0.426	0.37 <i>i</i> +0.536
C/D	C _{C/D} =	C _{CD} =	C _C D =	C _{C/D} =	C _{CD} =	C _{C/D} =	C _{C/D} =
	0.83 <i>i</i> ^{1.122}	0.82 <i>i</i> +0.035	0.74 <i>i</i> +0.132	0.56 <i>i</i> +0.319	0.49 <i>i</i> +0.393	0.41 <i>i</i> +0.484	0.32 <i>i</i> +0.588

Where:

i = % imperviousness (expressed as a decimal)

 C_{A} = Runoff coefficient for Natural Resources Conservation Service (NRCS) HSG A soils

CB = Runoff coefficient for NRCS HSG B soils

 C_{CD} = Runoff coefficient for NRCS HSG C and D soils.

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name: Saddlehorn Ranch Project No.: 25142.05 Calculated By: AAM Checked By: TBD

Date: 1/4/22

		SUB-E	BASIN			INITI	AL/OVER	LAND		Т	RAVEL TIM	E			tc CHECK		
		DA	TA				(T _i)				(T _t)			(U	RBANIZED BA	(SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t,	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
C1	6.04	А	13%	0.06	0.21	300	2.1%	25.4	940	1.0%	15.0	1.5	10.4	35.8	1240.0	38.2	35.8
C2	3.35	А	24%	0.14	0.29	155	1.9%	17.5	1661	1.8%	15.0	2.0	14.0	31.5	1816.0	39.0	31.5
C3	23.44	А	9%	0.04	0.18	268	2.5%	23.2	1620	1.0%	15.0	1.5	18.0	41.2	1888.0	50.8	41.2
C4	10.94	D	18%	0.14	0.42	26	33.0%	2.8	3375	1.0%	15.0	1.5	37.5	40.3	3401.0	71.6	40.3
C5	2.35	А	20%	0.11	0.26	300	2.7%	22.3	190	2.1%	15.0	2.2	1.5	23.8	490.0	24.5	23.8
C6	3.95	А	22%	0.12	0.28	97	1.4%	15.5	997	1.0%	15.0	1.5	11.1	26.6	1094.0	36.1	26.6
C7	2.14	А	24%	0.17	0.38	52	7.5%	6.2	689	1.0%	15.0	1.5	7.7	13.9	741.0	31.1	13.9
C8	22.55	А	10%	0.05	0.19	300	1.9%	26.7	630	1.0%	15.0	1.5	7.0	33.7	930.0	34.4	33.7
C9	2.63	А	35%	0.23	0.39	136	1.2%	17.2	1374	1.5%	15.0	1.8	12.5	29.6	1510.0	33.4	29.6
C10	16.38	А	12%	0.05	0.20	147	3.7%	14.9	1406	1.5%	15.0	1.8	12.8	27.6	1553.0	42.1	27.6
D1	9.11	А	13%	0.06	0.21	300	2.7%	23.4	448	1.3%	15.0	1.7	4.4	27.8	748.0	30.0	27.8
D2	8.49	А	13%	0.07	0.25	300	2.7%	23.1	1095	1.1%	15.0	1.6	11.6	34.7	1395.0	39.9	34.7
D3	3.21	А	8%	0.04	0.18	100	1.0%	19.2	170	1.0%	15.0	1.5	1.9	21.1	270.0	27.3	21.1
D4	10.01	D	7%	0.07	0.40	300	1.8%	26.5	1201	1.0%	15.0	1.5	13.3	39.8	1501.0	44.9	39.8
D5	9.56	D	17%	0.14	0.43	266	2.3%	21.4	1463	1.0%	15.0	1.5	16.3	37.6	1729.0	44.3	37.6
D6	0.34	А	45%	0.36	0.57	46	8.0%	4.6	332	1.0%	15.0	1.5	3.7	8.3	378.0	22.0	8.3
D7	33.94	А	15%	0.10	0.31	300	3.9%	20.0	1645	1.0%	15.0	1.5	18.3	38.3	1945.0	48.3	38.3
E1	17.12	А	7%	0.04	0.22	300	1.3%	30.4	1486	1.3%	7.0	0.8	31.0	61.4	1786.0	46.6	46.6
E2	0.37	А	45%	0.31	0.46	24	9.7%	3.3	402	1.0%	15.0	1.5	4.5	7.8	426.0	22.7	7.8
E3	0.20	А	45%	0.32	0.48	24	9.7%	3.3	185	1.1%	15.0	1.6	2.0	5.2	209.0	20.3	5.2
E4	0.68	А	3%	0.01	0.14	95	3.3%	12.9	97	1.8%	7.0	0.9	1.7	14.6	192.0	26.7	14.6
UD1	7.48	А	6%	0.03	0.16	300	1.9%	27.2	683	1.8%	7.0	0.9	12.1	39.3	983.0	33.5	33.5
UD2	9.17	А	6%	0.03	0.16	300	1.8%	27.7	445	1.9%	7.0	1.0	7.7	35.4	745.0	30.4	30.4
UD3	2.23	А	6%	0.04	0.24	300	2.0%	26.4	171	2.0%	7.0	1.0	2.9	29.3	471.0	27.0	27.0
UD4	34.90	D	2%	0.04	0.39	300	1.1%	32.2	2602	1.7%	15.0	2.0	22.2	54.3	2902.0	61.5	54.3
UD5	20.49	А	6%	0.05	0.30	300	1.7%	27.6	1230	1.5%	7.0	0.9	23.9	51.5	1530.0	41.9	41.9
OS1	2.37	А	58%	0.43	0.56	59	2.0%	7.4	1216	1.1%	15.0	1.6	12.9	20.3	1275.0	27.5	20.3
OS2	0.70	А	31%	0.20	0.35	59	3.3%	8.5	421	1.0%	15.0	1.5	4.7	13.1	480.0	25.9	13.1
OS3	2.28	А	60%	0.45	0.58	66	8.5%	4.7	1326	1.0%	15.0	1.5	14.7	19.5	1392.0	28.5	19.5
OS4	1.08	D	55%	0.44	0.63	66	8.5%	4.8	636	1.0%	15.0	1.5	7.1	11.8	702.0	23.1	11.8
OS5	2.92	А	23%	0.17	0.42	55	3.4%	8.3	857	1.0%	15.0	1.5	9.5	17.8	912.0	33.7	17.8

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name:	Saddlehorn Ranch
Project No.:	25142.05
Calculated By:	AAM
Checked By:	TBD
Date:	1/4/22

		SUB-E	BASIN			INITI	AL/OVER	LAND		Т	RAVEL TIM	E			tc CHECK		
		DA	ATA				(T _i)				(T _t)			(U	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t i	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
F1	1.35	А	40%	0.27	0.43	55	3.4%	7.4	754	2.5%	15.0	2.4	5.3	12.7	809.0	24.5	12.7
F2	7.67	А	11%	0.05	0.20	300	1.7%	27.5	690	1.0%	15.0	1.5	7.7	35.2	990.0	35.0	35.0
F3	2.37	А	45%	0.32	0.49	48	2.0%	7.7	2354	1.4%	15.0	1.8	22.1	29.8	2402.0	40.0	29.8
F4	2.93	А	45%	0.34	0.52	12	22.0%	1.7	3016	1.2%	15.0	1.6	30.6	32.3	3028.0	48.3	32.3

NOTES:

Table 6-2. NRCS Conveyance factors, K $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.03}}$ $t_c = t_i + t_t$ Equation 6-2 Equation 6-3 Type of Land Surface Conveyance Factor, K Where: Heavy meadow 2.5 Where: Tillage/field 5 te = computed time of concentration (minutes) ti = overland (initial) flow time (minutes) Short pasture and lawns 7 ti = overland (initial) flow time (minutes) C_5 = runoff coefficient for 5-year frequency (from Table 6-4) L_i = length of overland flow (ft) Nearly bare ground 10 t_t = channelized flow time (minutes). S_o = average slope along the overland flow path (ft/ft). Grassed waterway 15 Paved areas and shallow paved swales 20 $t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$ L, $t_r = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$ Equation 6-4 Equation 6-5 Where: Where: t_t = channelized flow time (travel time, min) t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1. t_t = chambridge how time (tayler time, time) L_t = waterway length (ft) S_0 = waterway slope (ft/ft) V_t = travel time velocity (ft/sec) = K $\sqrt{S_0}$ K = NRCS conveyance factor (see Table 6-2). $L_t = \text{length of channelized flow path (ft)}$ i = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$

Use a minimum te value of 5 minutes for urbanized areas and a minimum te value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Project Name: Saddlehorn Ranch

Subdivision:	Saddle	ehorn H	Ranch H	·iling 3	<u> </u>												Project			2.05			
Location: Design Storm:	El Paso	nuoù c	ty														culated Checked						
Design Storm:	5-rear															U				2			
																	L	Date:	1/4/2	2			
					CT RUN				Τſ	DTAL F		C C	(SWAL		I	PIF	DE		TRAVE		E	
			-	DIKL	CIKU	NOLL								JVVALI	-		FIE	- L		TRAVI		L	
	t			÷.															iches)		s)		
STREET	Design Point	۵I ر	Area (Ac)	Runoff Coeff	(min)	(Ac)	(in/hr)	S)	(min)	(ac)	(in/hr)	S)	O _{street} (cfs)	(ac)	Slope (%)	Q _{pipe} (cfs)	(ac)	Slope (%)	Pipe Size (inches)	Length (ft)	/elocity (fps)	(min)	REMARKS
	Desi	Basin ID	Area	Runc	t _c (m	C*A (Ac)	l (in,	Q (cfs)	tc (n	C*A (ac)	l (in	Q (cfs)	Ostree	C*A (ac)			C*A (ac)	Slop	Pipe	Leng	/	t _t (m	
	OS1	OS1	2.37	0.43	20.3	1.01	3.07	3.1					3.1	1.01	2.5					114	3.2	0.6	Roadside Swale Swale conveyance to DP 1.0
	1	C1	6.04										0.9	0.39	1.0					0	2.0	0.0	Swale conveyance to DP 1.0
	1.0	01	0.01	0.00	33.5	0.07	L.LL	0.7		1.40	2 22	3.1	3.1	1.40	2.1					752	2.9		Swale conveyance to DP 1.
			0.05						30.0	1.40	L.LL	3.1	1.1	0.46	1.0					0	2.0		Roadside Swale
	2	C2	3.35			0.46		1.1					1.8	0.91	1.0					0	2.0	0.0	Swale conveyance to DP 1.1 Roadside Swale
	3	C3	23.44	0.04	41.2	0.91	2.01	1.8					5.6	2.77	1.0					1716	2.0	14.3	Swale conveyance to DP 1.1 Sum of DP 1.0, DP 2, & DP 3
	1.1				\mid	┝──┤	$\left - \right $		41.2	2.77	2.01	5.6	3.2	1.58	0.5					0	1.4		Swale conveyance to DP 1.2 Roadside Swale
	4	C4	10.94	0.14	40.3	1.58	2.04	3.2						4.35						344	2.0		Swale conveyance to DP 1.2 Sum of DP 1.1 and DP 4
	1.2				\mid	\vdash	$\left - \right $		55.5	4.35	1.56	6.8		0.26						0	2.0		Roadside Swale conveyance to DP 1.3 Roadside Swale
	5	C5	2.35	0.11	23.8	0.26	2.83	0.7						4.61						1147	2.0		Swale conveyance to DP 1.3 Swale conveyance to DP 1.3 Swm of DP 1.2 and DP 5
	1.3					$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			58.3	4.61	1.48	6.8								0			Culvert conveyance to DP 1.4
	6	C6	3.95	0.12	26.6	0.49	2.66	1.3					1.3	0.49	1.0					U	2.0		Roadside Swale Swale conveyance to DP 1.4
	1.4								58.3	5.10	1.48	7.6					5.10	1.0	24	59	6.5		Sum of DP 1.3 and DP 6 Culvert conveyance to DP 1.6
	7	C7	2.14	0.17	13.9	0.36	3.64	1.3						0.36						1214			Roadside Swale Swale conveyance to DP 1.5
	8	C8	22.55	0.05	33.7	1.04	2.31	2.4	[2.4	1.04	1.0					0	2.0		Roadside Swale Swale conveyance to DP 1.5
	1.5								33.7	1.40	2.31	3.2	3.2	1.40	1.0					278	2.0	2.3	Sum of DP 7 and DP 8 Swale conveyance to DP 1.6
	9	C9	2.63	0.23	29.6	0.60	2.50	1.5					1.5	0.60	1.0					0	2.0		Roadside Swale Swale conveyance to DP 1.6
	1.6								58.5	7.10	1.48	10.5	10.5	7.10	0.75					388	1.7		Sum of DP 1.4, DP 1.5, and DP 9 Swale/ Pond conveyance to DP 1.7
	10	C10	16.38	0.05	27.6	0.90	2.61	2.3					2.3	0.90	1.0					0	2.0	0.0	Proposed Pond C, future Filing 4 Lots, and Filing 4 roadways Overland flow, future road swales, and pond conveyance to DP 1.7
	1.7								62.2	8.00	1.39	11 1											Sum of DP 1.6 and DP 10 Outlet structure release into Drainageway MS-06
	11	D1	9.11	0.06	27.8	0.56	2.59	1.5		0.00			1.5	0.56	1.0					682	2.0		Soadside Swale Swale conveyance to DP 2.0
	11		7.11	0.00	27.0	0.50	2.37	1.5															swale conveyance to be 2.0

																				ehorn	Ranch	ı	
Subdivision:				Filing 3	}												Project			2.05			
Location:			ty														culated						
Design Storm:	5-Year	-														C	hecked			0			
																	L	Date:	1/4/2	2			
					CT RUI				TC		RUNO	C C		SWAL			PIF	DE		TRAVE		IE	
		<u> </u>		DIKL		NOLL				/IAL r		FF	<u> </u>	JVVALI			F II	PE		IKAVL	LINV	IE	
																			es)				
	+			<u>ب</u>															lch,		()		
STREET	oin			oef									s)					\sim	(jr	£	(fp:		REMARKS
JINELI	Design Point	₽	Area (Ac)	Runoff Coeff.	С С	C*A (Ac)) L	0	Ê	ac)	L)	_	(cf:	ac)	(%)	cfs	ac)	%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Ê	NEW/INIO
l	sigr	sin	ea (nof	(min)	A (/	(in/hr)	cfs	(min)	A (ŝ	(in/hr)	cfs)	reet	A (ŝ	pe	pe (A (ĉ	pe	e S	lgtl	oci	(min)	
1	Def	Basin ID	Are	Rur	t _c (C*1	I (i	Q (cfs)	tc	C*A (ac)	I (j	Q (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pip	Ler	Vel	t _t	
													1.4							0	2.0	0.0	Roadside Swale
l	12	D2	8.49	0.07	34.7	0.63	2.26	1.4															Swale conveyance to DP 2.0
													2.7	1.19	1.0					1492	2.0	12.4	Sum of DP 11 & DP 12
	2.0								34.7	1.19	2.26	2.7											Swale conveyance to DP 2.3
													3.2	1.02	1.0					0	2.0	0.0	Roadside Swale
	OS3	OS3	2.28	0.45	19.5	1.02	3.13	3.2															Swale conveyance to DP 1.0
1													0.4	0.12	1.0					0	2.0	0.0	Roadside Swale
1	13	D3	3.21	0.04	21.1	0.12	3.01	0.4						1.1.4	1.0					700	2.0	(1	Swale conveyance to DP 1.0
1	2.1								21.1	1 1 4	2 01	2.4	3.4	1.14	1.0					730	2.0	6. I	Sum of DP OS3 and DP 13
	2.1								21.1	1.14	3.01	3.4	1.0	0.49	1.0					0	2.0	0.0	Swale conveyance to DP 2.2
	OS4	OS4	1.08	0.44	11.8	0.48	3.88	1.9					1.7	0.48	1.0					U	2.0	0.0	Roadside Swale Swale conveyance to DP 2.2
	034	034	1.00	0.47	11.0	0.40	3.00	1.7					43	1.62	1.0					895	2.0	75	Swale conveyance to DP 2.2 Sum of DP 2.1 and DP OS4
	2.2								27.2	1.62	2.63	4.3	4.5	1.02	1.0					075	2.0	1.5	Swale conveyance to DP 2.4
	2.2								21.2	1.02	2.00	1.5	3.0	1.38	1.0					0	2.0	0.0	Roadside Swale
	15	D5	9.56	0.14	37.6	1.38	2.14	3.0					0.2								2.0	0.2	Swale conveyance to DP 2.3
						-		-					0.5	0.12	1.0					59	2.0	0.5	
	16	D6	0.34	0.36	8.3	0.12	4.41	0.5															Roadside Swale Swale conveyance to DP 2.3
													4.8	2.69	1.0					117	2.0		Sum of DP 2.0, DP 15 and DP 16
	2.3								47.2	2.69	1.80	4.8											Swale conveyange to DP 2.4 2.4
													1.5	0.72	1.0					0	2.0	0.0	Roadside Swale
	14	D4	10.01	0.07	39.8	0.72	2.06	1.5															Swale conveyance to DP 2.3
										7.00			8.9	5.03	1.0					623	2.0	5.2	Sum of DP 14, DP 2.2 and DP 2.3
	2.4								48.1	5.03	1.//	8.9	()	2.25	1.0						2.0	2.0	Swale/ Pond conveyance to DP 2.5
	17	D7	22.04	0 10	20.2	2.25	2.11	()			1	7	0.9	3.25	1.0					0	2.0	0.0	Proposed Pond D, future Filing 4 Lots, and Filing 4 roadways
	17	D7	33.94	0.10	38.3	3.ZD	2.11	6.9					12 /	8.28	1.0					1147	2.0	0.6	Overland flow, future road swales, and pond conveyance to DP 2.5 Sum of DP 2.4 and DP 17
	2.5								52.2	8.28	1.60	13.4	13.4	0.20	1.0					1147	2.0	9.0	Sum of DP 2.4 and DP 17 Outlet structure release into Drainageway WF-R7A
	2.J								55.5	0.20	1.92												Roadside Swale
	21	E1	17.12	0.04	46.6	0.69	1.82	1.3				/'				1.3	0.69	1.0	24	48	3.9	0.2	Culvert conveyance to DP 3.0
											11	, 	0.5	0.11	1.0					185	2.0		Roadside Swale
	22	E2	0.37	0.31	7.8	0.11	4.51	0.5			/ /		-										Swale conveyance to DP 3.0
										/	1		0.3	0.06	1.0					0	2.0	0.0	Roadside Swale
	23	E3	0.20	0.32	5.2	0.06	5.10	0.3															Swale conveyance to DP 3.0
										17			1.6	0.86	2.1					217	2.9	1.2	Sum of DP 21, DP 22, and DP 23
	3.0								46.8	Ø .86	1.82	1.6											Swale/ Pond conveyance to DP 3.1
										//			0.04	0.01	0.5					0	1.4	0.0	Overland Flow
	24	E4	0.68	0.01	14.6	0.01	3.56	0.04					1.5	2.07	1.0					11.17	2.0	2.4	Pond Conveyance
													1.5	0.87	1.0					1147	2.0		Sum of DP 3.0 and DP 24
	3.1								48.0	0.87	1.78	1.5											Outlet structure release into Drainageway WF-R7A

Subdivision: Location: Design Storm:	El Paso	so Coun		iling 3												Pro I Calı C	oject Na Project Iculated Checked E	d By:	Saddl 25142 AAM TBD 1/4/2		Rancl	n	
i				DIRE	CT RUN	NOFF		<u> </u>	TC	otal r	RUNO	FF	5	SWALE	Ê I		Pľ	IPE	· · · ·	TRAV	VEL TIN	ЛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	UD1	UD1	7.48	0.03	33.5	0.19	2.31	0.4								1							Overland Flow Sheet flow into Drainageway MS-06
		UD2					2.46		, 🗖							Ī							Overland Flow Sheet flow into Drainageway MS-06
	UD3	UD3	2.23	0.04	27.0	0.09	2.64	0.2															Overland Flow Sheet flow into Drainageway MS-06
	UD4	UD4	34.90	0.04	54.3	1.35	1.59	2.1					Γ^{\top}			1							Overland Flow Sheet flow into Drainageway MS-06

Sheet flow into Drainageway MS-06

Sheet flow into Drainageway MS-06

Overland Flow

Overland Flow

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

2.92

UD5 UD5 20.49 0.05

2.0

1.7

41.9 1.01 1.98

0.17 17.8 0.51 3.26

Missing Basins OS2 & F1 thru F4 and corresponding design points

OS5 OS5

> It appears this basin should be made into 2, one running to north in roadside ditch to DP UD5 and one to the south in roadside ditch to join with Basin F3. See additional notes on drainage map.

Subdivision: Location: Design Storm:	: El Pas	o Cour	Ranch hty	Filing 3	3											Cal	oject N Projec Iculate Checke	t No.: d By: d By:	25142 AAM	2.05	Ranc	h	
	I	I		DIRE	CT RUI	NOFF			T	OTAL RU	NOFF		S	SWALE		[PI	PE		TRAV	EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (In/nr) O (cfe)		O _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
													6.8	1.33	2.5					114	3.2	0.6	Roadside Swale
	OS1	OS1	2.37	0.56	20.3	1.33	5.15	6.8						1.00	1.0								Swale conveyance to DP 1.0
	1	C1	6.04	0.21	35.8	1.28	3.72	4.8					4.8	1.28	1.0					0	2.0	0.0	Roadside Swale Swale conveyance to DP 1.0
	· ·	01	0.04	0.21	55.0	1.20	3.72	4.0				-	9.7	2.61	2.1					752	2.9	4.3	Swale Conveyance to DF 1.0
	1.0								35.8	2.61 3	.72	9.7											Swale conveyance to DP 1.1
													4.0	0.98	1.0					0	2.0	0.0	Roadside Swale
	2	C2	3.35	0.29	31.5	0.98	4.04	4.0					1 4 1	4.00	1.0					0	2.0	0.0	Swale conveyance to DP 1.1
	3	C3	23.44	0.10	41.2	4.20	3.37	14.1					14.1	4.20	1.0					0	2.0	0.0	Roadside Swale Swale conveyance to DP 1.1
	3	03	23.44	0.10	41.Z	4.20	3.37	14.1					26.2	7.79	1.0					1716	2.0	14.3	Swale conveyance to DP 1.1 Sum of DP 1.0, DP 2, & DP 3
	1.1								41.2	7.79 3	.37 20												Swale conveyance to DP 1.2
													15.5	4.54	0.5					0	1.4	0.0	Roadside Swale
-	4	C4	10.94	0.42	40.3	4.54	3.42	15.5				_											Swale conveyance to DP 1.2
	1.2								55.5	12.33 2	61 2		32.2	12.33	1.0					344	2.0	2.9	Sum of DP 1.1 and DP 4 Swale conveyance to DP 1.3
	1.2								55.5	12.33 2	.01 3.	2.2	2.9	0.62	1.0					0	2.0	0.0	Roadside Swale
	5	C5	2.35	0.26	23.8	0.62	4.75	2.9					2.7	0.02	1.0					Ŭ	2.0	0.0	Swale conveyance to DP 1.3
													32.2	12.95	1.0					1147	2.0	9.6	Sum of DP 1.2 and DP 5
	1.3								58.3	12.95 2	.49 32	2.2											Culvert conveyance to DP 1.4
	,	~ ~ ~	2.05	0.00	24.4			F 0					5.0	1.11	1.0					0	2.0	0.0	Roadside Swale
	6	C6	3.95	0.28	26.6	1.11	4.46	5.0				_											Swale conveyance to DP 1.4 Sum of DP 1.3 and DP 6
	1.4								58.3	14.06 2	49 3	5.0				35.0	14.06	1.0	24	59	11.1	0.1	Culvert conveyance to DP 1.6
									00.0	11100 2		0.0	4.9	0.81	1.0	0010	1.100		~ .	1214			Roadside Swale
	7	C7	2.14	0.38	13.9	0.81	6.10	4.9															Swale conveyance to DP 1.5
													16.4	4.24	1.0					0	2.0	0.0	Roadside Swale
	8	C8	22.55	0.19	33.7	4.24	3.87	16.4				_	19.6	5.05	1.0					278	2.0	1.2	Swale conveyance to DP 1.5 Sum of DP 7 and DP 8
	1.5								337	5.05 3	87 19		19.0	5.05	1.0					270	2.0	2.3	Sum of DP 7 and DP 8 Swale conveyance to DP 1.6
									0017	0.00 0		,	4.3	1.02	1.0					0	2.0	0.0	Roadside Swale
	9	C9	2.63	0.39	29.6	1.02	4.19	4.3															Swale conveyance to DP 1.6
													50.0	20.13	0.75					388	1.7	3.7	Sum of DP 1.4, DP 1.5, and DP 9
	1.6								58.4	20.13 2	.48 50		14.3	2 20	1.0					0	2.0	0.0	Swale/ Pond conveyance to DP 1.7
	10	C10	16.38	0.20	27.6	3.28	4.37	14.3					14.3	3.28	1.0					U	2.0	0.0	Proposed Pond C, future Filing 4 Lots, and Filing 4 roadways Overland flow, future road swales, and pond conveyance to DP 1.7
	1	0.0		0.20		0.20																	Sum of DP 1.6 and DP 10
	1.7								58.4	23.41 2	.48 58	8.1											Outlet structure release into Drainageway MS-06
													8.3	1.90	1.0					682	2.0	5.7	Roadside Swale
	11	D1	9.11	0.21	27.8	1.90	4.35	8.3	1	1								1				1	Swale conveyance to DP 2.0

Project Name: Saddlehorn Ranch Project No.: 25142.05 Calculated By: AAM Checked By: TBD Date: 1/4/22

Subdivision: Saddlehorn Ranch Filing 3 Location: El Paso County Design Storm: 100-Year

																		Date:	., ., _	-			
				DIRE	CT RUI	NOFF			T) DTAL F	RUNOF	F	9	SWALE			PI	PE		TRAV	'EL TIN	/IE	
																			les)				
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	c (min)	C*A (ac)	(in/hr)	Q (cfs)	tc (min)	C*A (ac)	(in/hr)	Q (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	^o ipe Size (inches)	-ength (ft)	Velocity (fps)	t (min)	REMARKS
							_			0		0	8.2	2.15				0,		0	~	0.0	Roadside Swale
	12	D2	8.49	0.25	34.7	2.15	3.80	8.2					45.4	4.05	1.0					4 4 0 0		40.4	Swale conveyance to DP 2.0
	2.0								34.7	4.05	3 80	15.4	15.4	4.05	1.0					1492	2.0	12.4	Sum of DP 11 & DP 12 Swale conveyance to DP 2.3
	2.0								01.7	1.00	0.00	10.1	6.9	1.32	1.0					0	2.0	0.0	Roadside Swale
	OS3	OS3	2.28	0.58	19.5	1.32	5.26	6.9												-			Swale conveyance to DP 1.0
													2.8	0.56	1.0					0	2.0	0.0	Roadside Swale
	13	D3	3.21	0.18	21.1	0.56	5.05	2.8															Swale conveyance to DP 1.0
													9.5	1.88	1.0					730	2.0	6.1	Sum of DP OS3 and DP 13
	2.1								21.1	1.88	5.05	9.5											Swale conveyance to DP 2.2
	001	OS4	1.00	0 ()	11.8	0.40	(51						4.4	0.68	1.0					0	2.0	0.0	Roadside Swale
	054	054	1.08	0.63	11.8	0.68	6.51	4.4					11.3	2.56	1.0					895	2.0	75	Swale conveyance to DP 2.2 Sum of DP 2.1 and DP OS4
	2.2								27.2	2.56	4 4 1	11 3	11.5	2.50	1.0					090	2.0	7.5	Sun of DP 2.1 and DP 054 Swale conveyance to DP 2.4
	2.2								21.2	2.00	1. 1.1	11.0	14.9	4.15	1.0					0	2.0	0.0	Roadside Swale
	15	D5	9.56	0.43	37.6	4.15	3.59	14.9												-			Swale conveyance to DP 2.3
													1.4	0.19	1.0					59	2.0	0.5	Roadside Swale
	16	D6	0.34	0.57	8.3	0.19	7.41	1.4															Swale conveyance to DP 2.3
													30.1	8.39	1.0					117	2.0	1.0	Sum of DP 2.0, DP 15 and DP 16
	2.3								37.6	8.39	3.59	30.1	12.0	4.00	1.0					0	2.0	0.0	Swale conveyance to DP 2.4
	14	D4	10.01	0.40	39.8	4.02	3.45	13.9					13.9	4.03	1.0					0	2.0	0.0	Roadside Swale
	14	D4	10.01	0.40	39.0	4.03	3.40	13.9					51.7	1/ 08	1.0					623	2.0	5.2	Swale conveyance to DP 2.3 Sum of DP 2.2 and DP 2.3
	2.4								39.8	14.98	3 4 5	517	51.7	14.70	1.0					025	2.0	J.Z	Swale/ Pond conveyance to DP 2.5
	2.1								07.0	11170	0.10	0111	37.3	10.52	1.0					0	2.0	0.0	Proposed Pond D, future Filing 4 Lots, and Filing 4 roadways
	17	D7	33.94	0.31	38.3	10.52	3.55	37.3							-								Overland flow, future road swales, and pond conveyance to DP 2.5
													80.1	25.50	1.0					1147	2.0	9.6	Sum of DP 2.4 and DP 17
	2.5								45.0	25.50	3.14	80.1										-	Outlet structure release into Drainageway WF-R7A
		54	47.45	0.05		0.0-											0.67						Roadside Swale
	21	E1	17.12	0.22	46.6	3.85	3.06	11.8					1.0	0.17	1.0	11.8	3.85	1.0	24				Culvert conveyance to DP 3.0
	22	E2	0.37	0.46	7.8	0.17	7.57	1.3					1.3	0.17	1.0					185	2.0	1.5	Roadside Swale Swale conveyance to DP 3.0
	~~~		0.57	00	7.0	0.17	1.51	1.5					0.9	0.10	1.0					0	2.0	0.0	Roadside Swale
	23	E3	0.20	0.48	5.2	0.10	8.57	0.9					0.7	0.10						Ū		0.0	Swale conveyance to DP 3.0
													12.6	4.12	2.1					217	2.9	1.2	Sum of DP 21, DP 22, and DP 23
	3.0								46.7	4.12	3.05	12.6											Swale/ Pond conveyance to DP 3.1
													0.6	0.10	0.5					0	1.4	0.0	Overland Flow
	24	E4	0.68	0.14	14.6	0.10	5.97	0.6					127	4 2 2	1.0					11/7	2.0	0 /	Pond Conveyance
	3.1								17.0	4.22	2 00	12.4	12.0	4.22	1.0					1147	2.0	9.6	Sum of DP 3.0 and DP 24
	3.1					I			47.9	4.ZZ	2.98	12.0					I						Outlet structure release into Drainageway WF-R7A

Project Name: Saddlehorn Ranch Project No.: 25142.05 Calculated By: AAM Checked By: TBD Date: 1/4/22

Subdivision: Saddlehorn Ranch Filing 3 Location: El Paso County Design Storm: 100-Year

																		Date:	1/ 4/ 2	2			
				DIRE	CT RU	NOFF			TC	)TAL F	RUNO	F		SWAL			PII	PE		TRAV	'EL TIN	ИE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	$t_c$ (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	UD1	UD1	7.48	0.16	33.5	1.18	3.88	4.6															Overland Flow Sheet flow into Drainageway MS-06
	UD2	UD2	9.17	0.16	30.4	1.46	4.13	6.0															Overland Flow Sheet flow into Drainageway MS-06
	UD3	UD3	2.23	0.24	27.0	0.53	4.43	2.3															Overland Flow Sheet flow into Drainageway MS-06
	UD4	UD4	34.90	0.39	54.3	13.69	2.67	36.5															Overland Flow Sheet flow into Drainageway MS-06
	UD5	UD5	20.49	0.30	41.9	6.11	3.32	20.3															Overland Flow Sheet flow into Drainageway MS-06
	OS5	OS5	2.92	0.42	17.8	1.23	5.48	6.7															Overland Flow Sheet flow into Drainageway MS-06

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

# **APPENDIX C**

# HYDRAULIC CALCULATIONS

Provide riprap sizing calculations for all culvert outlet protection.

Provide channel calculations for channels from all pond outlets major drainageways.

Need calculations for roadside swales along Badito Place, Estacado Place and San Isidro south of drainageway MS-06 and along Judge Orr Road between Curtis Road and Barrosito Trail

Provide design calculations for major channel crossing at San Isidro.

Provide HEC-RAS (channel analysis for channel improvements), including design of low flow.

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### DP01 Design Point 1.0 (Q5=3.1 cfs Q100=9.7 cfs)

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6759.75 = 62.81 = 1.58 = 6760.74 = 18.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 3.10 = 9.70 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 9.70
No. Barrels	= 1	Qpipe (cfs)	= 9.70
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 5.79
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 6.40
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6761.10
		HGL Up (ft)	= 6761.94
Embankment		Hw Elev (ft)	= 6762.72
Top Elevation (ft)	= 6763.64	Hw/D (ft)	= 1.32
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control

=	6763.64
=	32.00
=	20.00

ft)					DP01 De	sign Poir	nt 1.0 (Q5=	3.1 cfs C	2100=9.7	cfs)						Hw Dep	
																	- 3.26
														_			
																	- 2.26
													<u> </u>		Inle contro	bl	
													$\rightarrow$				
														-		_	- 1.26
														-			
		 												-			- 0.26
													╶┯╼╼┸╼				
						_								_			
																	- 0.7
	+																
				_		_	_										
			-			_	_		_	_							1.74
																_	2.74
0 5	10	15	20	25	30	35	40 nbank	45	50	55	60	65	70	75	80	85	

6743.00

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-1.50

80

Reach (ft)

75

## DP02 Design Point 1.1 (Q5=5.6 cfs Q100=26.2 cfs)

20

10

Circular Culvert

15

25

HGI

30

35

Embank

Invert Ele Pipe Leng Slope (%) Invert Ele Rise (in)	gth (ft) )	,	= = =	6744.^ 56.00 0.55 6744.{ 24.0	-					<b>Calcul</b> Qmin ( Qmax Tailwa	cfs) (cfs)	-		=	5.60 26.20 (dc+D)/2
Shape Span (in) No. Barre n-Value Culvert T Culvert E Coeff. K,N	ype ntranc		= = = =	Circula 24.0 1 0.012 Circula Groov 0.004	ar Coi e end	l proj	ecting		2	Highlin Qtotal Qpipe Qovert Veloc HGL D HGL D	(cfs) (cfs) op (cf Dn (ft/ Up (ft/ n (ft)	s)		= = = =	26.20 26.14 0.06 8.49 8.32 6746.08 6746.72
Embankr Top Eleva Top Widtl Crest Wid	ation (f n (ft)	ťt)	=	6748.( 32.00 20.00	)5					Hw Ele Hw/D ( Flow F	ev (ft) (ft)			= = =	6748.07 1.78 Inlet Control
													CM Ta		as allowed 5.5.
Elev (ft)															
					DP02	Design P	oint 1.1 (0	Q5=5.6 cfs (	Q100=26.2 d	cfs)				Н	w Depth (ft)
6749.00					DP02	Design P	oint 1.1 (0	Q5=5.6 cfs (	Q100=26.2 d	cfs)				H	w Depth (ft) 4.50
					DP02	Design P	oint 1.1 (0	25=5.6 cfs (	Q100=26.2 (	cfs)			Iniet con	H	
6749.00					DP02	Design P	oint 1.1 (0	25=5.6 cfs (	Q100=26.2 d	cfs)			Iniet con	Hi trol	4.50
6749.00					DP02	Design P	oint 1.1 (C	25=5.6 cfs (	Q100-26.2 d					trol	4.50
6749.00 6748.00 6747.00					DP02	Design P	oint 1.1 (C	25=5.6 cfs (	Q100-26.2 «	-fs)				trol	4.50 3.50 2.50

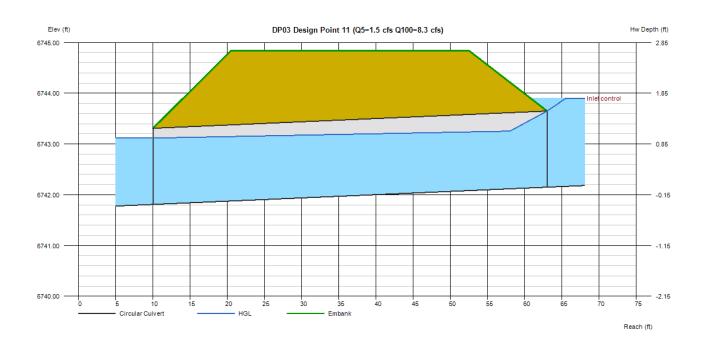
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### DP03 Design Point 11 (Q5=1.5 cfs Q100=8.3 cfs)

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 6741.81 = 53.00 = 0.64 = 6742.15	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.50 = 8.30 = (dc+D)/2
Rise (in)	= 18.0		
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 8.30
No. Barrels	= 1	Qpipe (cfs)	= 8.30
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 5.08
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 5.87
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6743.12
		HGL Up (ft)	= 6743.27
Embankment		Hw Elev (ft)	= 6743.90
Top Elevation (ft)	= 6744.84	Hw/D (ft)	= 1.17

=	6744.84
=	32.00
=	20.00

		0.00
Qpipe (cfs)	=	8.30
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	5.08
Veloc Up (ft/s)	=	5.87
HGL Dn (ft)	=	6743.12
HGL Up (ft)	=	6743.27
Hw Elev (ft)	=	6743.90
Hw/D (ft)	=	1.17
Flow Regime	=	Inlet Control



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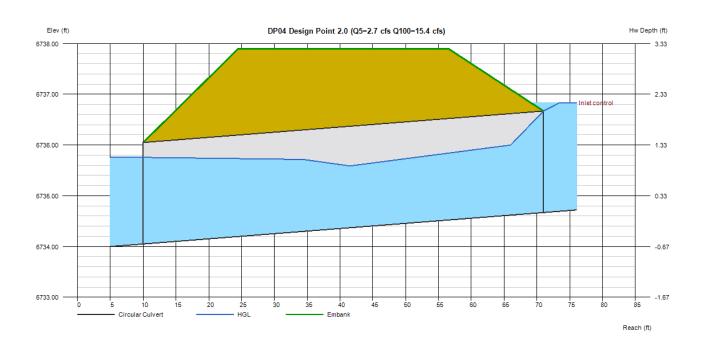
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### DP04 Design Point 2.0 (Q5=2.7 cfs Q100=15.4 cfs)

Invert Elev Dn (ft)	= 6734.05	Calculations	
Pipe Length (ft)	= 61.00	Qmin (cfs)	= 2.70
Slope (%)	= 1.02	Qmax (cfs)	= 15.40
Invert Elev Up (ft)	= 6734.67	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 24.0	. ,	, , , , , , , , , , , , , , , , , , ,
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 15.40
No. Barrels	= 1	Qpipe (cfs)	= 15.40
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 5.39
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 6.49
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6735.76
		HGL Up (ft)	= 6736.08
Embankment		Hw Elev (ft)	= 6736.84
Top Elevation (ft)	= 6737.90	Hw/D (ft)	= 1.08
<b>T</b>	~~~~		

=	6737.90	
=	32.00	
=	20.00	

Qpipe (cfs)	= 15.40
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 5.39
Veloc Up (ft/s)	= 6.49
HGL Dn (ft)	= 6735.76
HGL Up (ft)	= 6736.08
Hw Elev (ft)	= 6736.84
Hw/D (ft)	= 1.08
Flow Regime	= Inlet Control
-	



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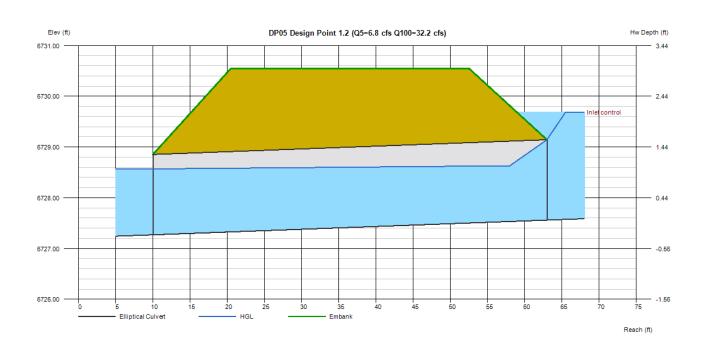
### DP05 Design Point 1.2 (Q5=6.8 cfs Q100=32.2 cfs)

Invert Elev Dn (ft)	= 6727.27	Calculations	
Pipe Length (ft)	= 52.98	Qmin (cfs)	= 6.80
Slope (%)	= 0.55	Qmax (cfs)	= 32.20
Invert Elev Up (ft)	= 6727.56	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 19.0	( )	( <i>'</i>
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 32.20
No. Barrels	= 2	Qpipe (cfs)	= 32.20
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Horizontal Ellipse Concrete	Veloc Dn (ft/s)	= 5.72
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 6.90
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6728.57
		HGL Up (ft)	= 6728.64
Embankment		Hw Elev (ft)	= 6729.69
Top Elevation (ft)	= 6730.55	Hw/D (ft)	= 1.34
_ '		` ′ .	

Top Width (ft) Crest Width (ft)

=	6730.55
=	32.00
=	20.00

	OEIEO
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 5.72
Veloc Up (ft/s)	= 6.90
HGL Dn (ft)	= 6728.57
HGL Up (ft)	= 6728.64
Hw Elev (ft)	= 6729.69
Hw/D (ft)	= 1.34
Flow Regime	= Inlet Control



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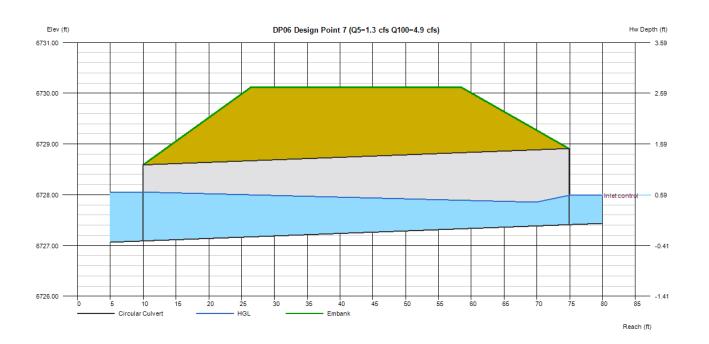
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### DP06 Design Point 7 (Q5=1.3 cfs Q100=4.9 cfs)

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6727.09 = 64.87 = 0.49 = 6727.41 = 18.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.30 = 4.90 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 1.30
No. Barrels	= 1	Qpipe (cfs)	= 1.30
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= 1.08
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 3.14
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6728.05
		HGL Up (ft)	= 6727.84
Embankment		Hw Elev (ft)	= 6727.99
Top Elevation (ft)	= 6730.12	Hw/D (ft)	= 0.39

=	6730.12
=	32.00
=	20.00

	Veloc Dn (ft/s)	= 1.08
	Veloc Up (ft/s)	= 3.14
2	HGL Dn (ft)	= 6728.05
	HGL Up (ft)	= 6727.84
	Hw Elev (ft)	= 6727.99
	Hw/D (ft)	= 0.39
	Flow Regime	= Inlet Control



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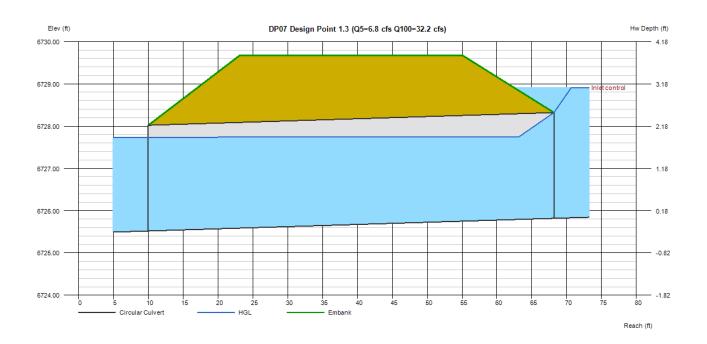
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### DP07 Design Point 1.3 (Q5=6.8 cfs Q100=32.2 cfs)

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 6725.52 = 58.18 = 0.52 = 6725.82	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 6.80 = 32.20 = (dc+D)/2
Rise (in)	= 30.0		(00.0)/2
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 32.20
No. Barrels	= 1	Qpipe (cfs)	= 32.20
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.00
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 7.92
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6727.74
		HGL Up (ft)	= 6727.75
Embankment		Hw Elev (ft)	= 6728.91
Top Elevation (ft)	= 6729.67	Hw/D (ft)	= 1.24
			-

=	6729.67
=	32.00
=	20.00

Qpipe (cfs)	= 32.20
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 7.00
Veloc Up (ft/s)	= 7.92
HGL Dn (ft)	= 6727.74
HGL Up (ft)	= 6727.75
Hw Elev (ft)	= 6728.91
Hw/D (ft)	= 1.24
Flow Regime	= Inlet Control



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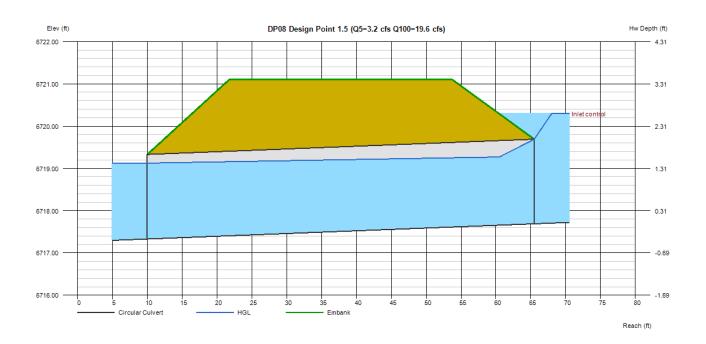
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### DP08 Design Point 1.5 (Q5=3.2 cfs Q100=19.6 cfs)

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6717.33 = 55.50 = 0.65 = 6717.69 = 24.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 3.20 = 19.60 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 19.60
No. Barrels	= 1	Qpipe (cfs)	= 19.60
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= 6.59
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 7.30
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6719.13
		HGL Up (ft)	= 6719.28
Embankment		Hw Elev (ft)	= 6720.30
Top Elevation (ft)	= 6721.10	Hw/D (ft)	= 1.30

=	6721.10
=	32.00
=	20.00

Veloc Dn (ft/s)	= 6.59
Veloc Up (ft/s)	= 7.30
HGL Dn (ft)	= 6719.13
HGL Up (ft)	= 6719.28
Hw Elev (ft)	= 6720.30
Hw/D (ft)	= 1.30
Flow Regime	= Inlet Control



Top Width (ft)

Crest Width (ft)

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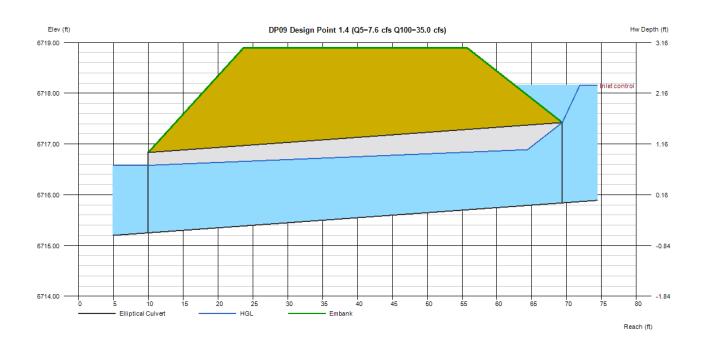
### DP09 Design Point 1.4 (Q5=7.6 cfs Q100=35.0 cfs)

= 32.00

= 20.00

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6715.25 = 59.38 = 0.99 = 6715.84 = 19.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 7.60 = 35.00 = (dc+D)/2
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 35.00
No. Barrels	= 2	Qpipe (cfs)	= 35.00
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Horizontal Ellipse Concrete	Veloc Dn (ft/s)	= 6.02
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 7.51
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6716.58
		HGL Up (ft)	= 6716.92
Embankment		Hw Elev (ft)	= 6718.15
Top Elevation (ft)	= 6718.90	Hw/D (ft)	= 1.46

- Flow Regime
- = Inlet Control



Crest Width (ft)

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### DP10 Design Point 22 (Q5=0.5 cfs Q100=1.3 cfs)

= 15.00

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6727.04 = 35.77 = 0.95 = 6727.38 = 18.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 0.50 = 1.30 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 1.30
No. Barrels	= 1	Qpipe (cfs)	= 1.30
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= 1.08
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 3.14
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6728.00
		HGL Up (ft)	= 6727.81
Embankment		Hw Elev (ft)	= 6727.96
Top Elevation (ft)	= 6729.50	Hw/D (ft)	= 0.39
Top Width (ft)	= 18.00	Flow Regime	= Inlet Control

DP10 Design Point 22 (Q5=0.5 cfs Q100=1.3 cfs) Elev (ft) Hw Depth (ft) 6730.00 - 2.62 - 2.12 6729.50 6729.00 1.62 6728.50 1.12 6728.00 0.62 let contr 6727.50 0.12 6727.00 -0.38 -0.88 6726.50 -35 15 25 45 55 60 ò 5 10 20 30 . 40 50 HGL Embank Circular Culvert Reach (ft)

Crest Width (ft)

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### DP11 Design Point 21 (Q5=1.3 cfs Q100=11.8 cfs)

= 20.00

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6724.11 = 47.04 = 1.04 = 6724.60 = 24.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.30 = 11.80 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 11.80
No. Barrels	= 1	Qpipe (cfs)	= 11.80
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= 4.34
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 5.81
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6725.73
		HGL Up (ft)	= 6725.83
Embankment		Hw Elev (ft)	= 6726.49
Top Elevation (ft)	= 6727.84	Hw/D (ft)	= 0.94
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control

DP11 Design Point 21 (Q5=1.3 cfs Q100=11.8 cfs) Hw Depth (ft) Elev (ft) 6728.00 - 3.40 6727.00 -- 2.40 Inlet control 6726.00 1.40 6725.00 0.40 6724.00 -0.60 6723.00 -- -1.60 15 20 45 50 70 0 25 30 35 40 55 60 65 5 10 HGL - Embank Circular Culvert Reach (ft)

Crest Width (ft)

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Tuesday, Dec 21 2021

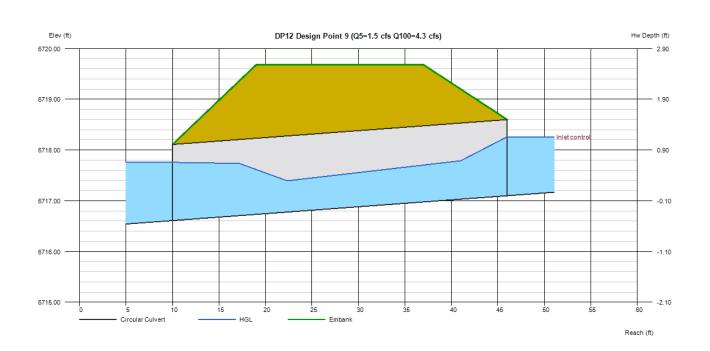
### DP12 Design Point 9 (Q5=1.5 cfs Q100=4.3 cfs)

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6716.61 = 36.00 = 1.36 = 6717.10 = 18.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.50 = 4.30 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 4.30
No. Barrels	= 1	Qpipe (cfs)	= 4.30
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 2.97
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 4.53
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6717.76
		HGL Up (ft)	= 6717.90
Embankment		Hw Elev (ft)	= 6718.26
Top Elevation (ft)	= 6719.68	Hw/D (ft)	= 0.77
Top Width (ft)	= 18.00	Flow Regime	= Inlet Contro

= 18.00

= 15.00

Hw/D (ft)
Flow Regime



Crest Width (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP13 Design Point 16 (Q5=0.5 cfs Q100=1.4 cfs)

= 15.00

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 6715.05 = 36.00 = 1.97 = 6715.76 = 18.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 0.50 = 1.40 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 1.40
No. Barrels	= 1	Qpipe (cfs)	= 1.40
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= 1.16
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 3.21
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6716.02
		HGL Up (ft)	= 6716.20
Embankment		Hw Elev (ft)	= 6716.35
Top Elevation (ft)	= 6718.75	Hw/D (ft)	= 0.40
Top Width (ft)	= 18.00	Flow Regime	= Inlet Control

DP13 Design Point 16 (Q5=0.5 cfs Q100=1.4 cfs) Hw Depth (ft) Elev (ft) 6719.00 - 3.24 6718.00 -- 2.24 6717.00 -1.24 Inlet contro 6716.00 0.24 6715.00 - -0.76 6714.00 -- -1.76 35 40 45 55 60 0 15 25 30 50 5 10 20 HGL Embank Circular Culvert Reach (ft)

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### DP15 Design Point 2.1 (Q5=3.4 cfs Q100=9.5 cfs)

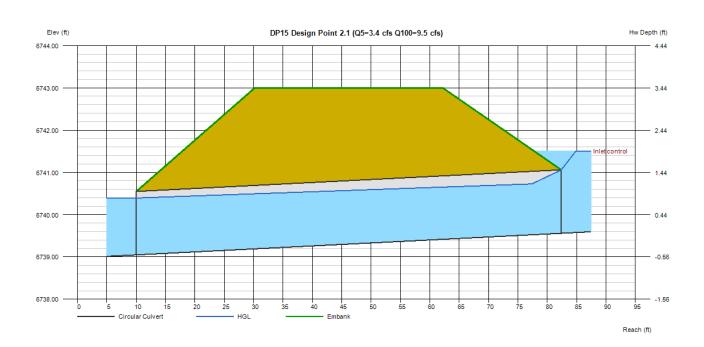
Invert Elev Dn (ft)	= 6739.05	Calculations	
Pipe Length (ft)	= 72.38	Qmin (cfs)	= 3.40
Slope (%)	= 0.70	Qmax (cfs)	= 9.50
Invert Elev Up (ft)	= 6739.56	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 18.0		, , , , , , , , , , , , , , , , , , ,
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 9.50
No. Barrels	= 1	Qpipe (cfs)	= 9.50
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 5.69
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 6.31
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6740.40
		HGL Up (ft)	= 6740.75
Embankment		Hw Elev (ft)	= 6741.51
Top Elevation (ft)	= 6743.00	Hw/D (ft)	= 1.30

I op Elevation (ft) Top Width (ft)

Crest Width (ft)

=	6743.00
=	32.00
=	20.00

5 5	
Qtotal (cfs)	= 9.50
Qpipe (cfs)	= 9.50
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 5.69
Veloc Up (ft/s)	= 6.31
HGL Dn (ft)	= 6740.40
HGL Up (ft)	= 6740.75
Hw Elev (ft)	= 6741.51
Hw/D (ft)	= 1.30
Flow Regime	= Inlet Control



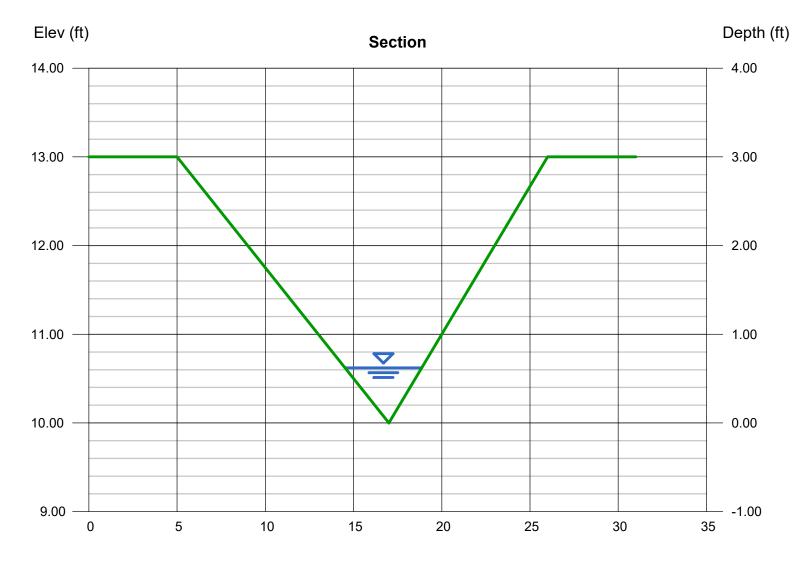
For all swales: verify depth and ensure it matches the GEC Plans, CD's, and all other locations. GEC plans state a min depth of 3', CD's state a min depth of 2'-3', and these reports show a depth of 3'-4'.

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#### DP 1.0 Swale (5-Year)(FR:0.73)

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.62
Total Depth (ft)	= 3.00	Q (cfs)	= 3.100
		Area (sqft)	= 1.35
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.30
Slope (%)	= 1.12	Wetted Perim (ft)	= 4.52
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.55
		Top Width (ft)	= 4.34
Calculations		EGL (ft)	= 0.70
Compute by:	Known Q		
Known Q (cfs)	= 3.10		

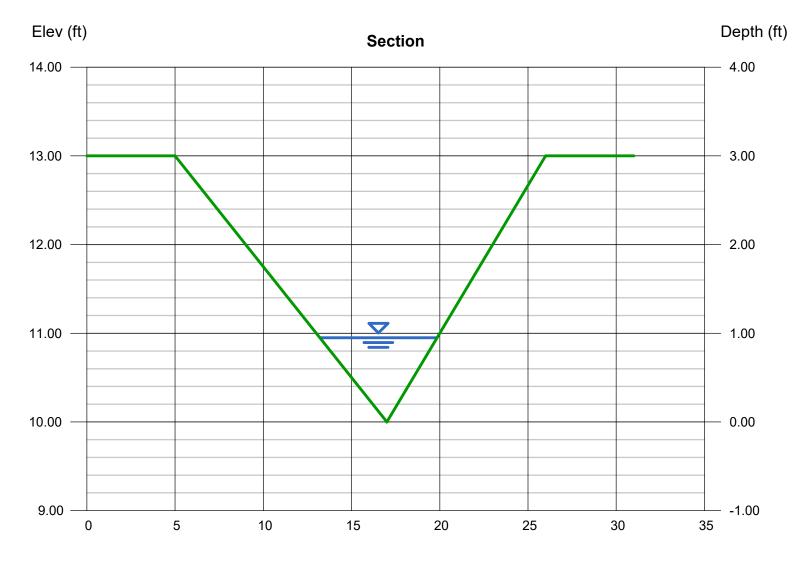


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### DP 1.0 Swale (100-Year)(FR:0.79)

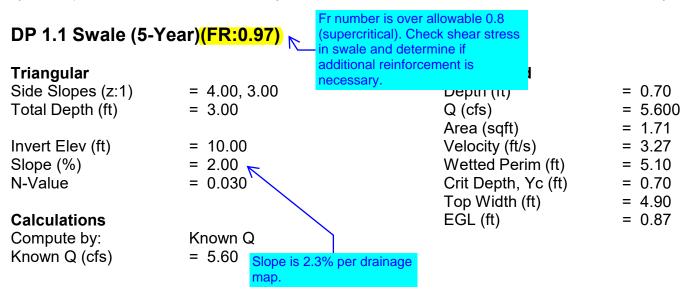
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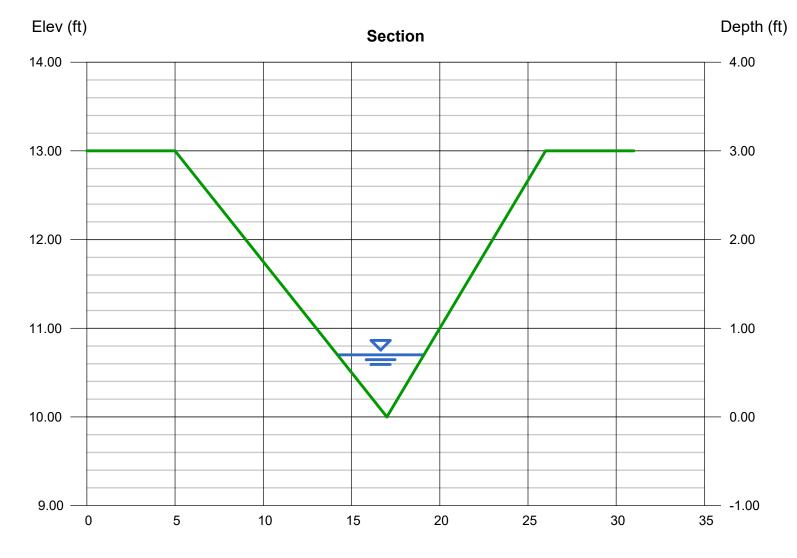
Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.95
Total Depth (ft)	= 3.00	Q (cfs)	= 9.700
		Area (sqft)	= 3.16
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.07
Slope (%)	= 1.12	Wetted Perim (ft)	= 6.92
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.87
		Top Width (ft)	= 6.65
Calculations		EGL (ft)	= 1.10
Compute by:	Known Q		
Known Q (cfs)	= 9.70		



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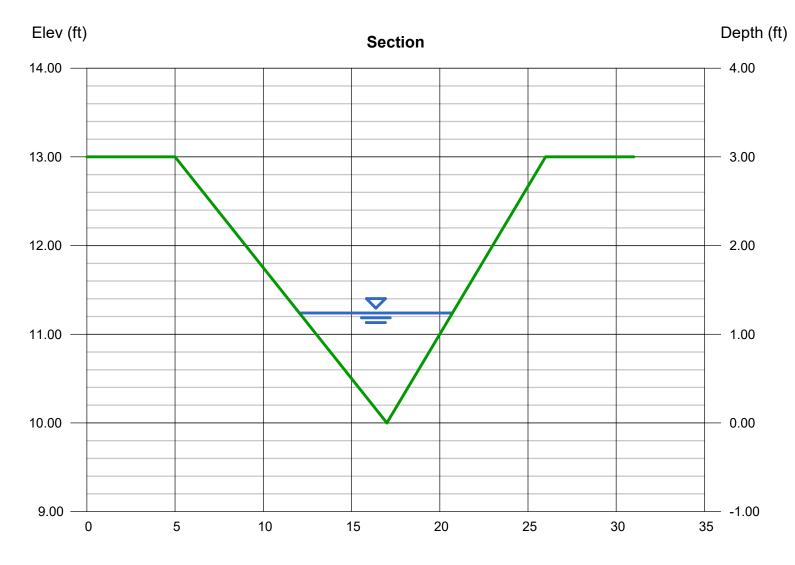


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### DP 1.1 Swale (100-Year)(FR:1.09)

#### Triangular

	Highlighted	
= 4.00, 3.00	Depth (ft)	= 1.24
= 3.00	Q (cfs)	= 26.20
	Area (sqft)	= 5.38
= 10.00	Velocity (ft/s)	= 4.87
= 2.00	Wetted Perim (ft)	= 9.03
= 0.030	Crit Depth, Yc (ft)	= 1.29
	Top Width (ft)	= 8.68
	EGL (ft)	= 1.61
Known Q		
= 26.20		
	= 3.00 = 10.00 = 2.00 = 0.030 Known Q	= 4.00, 3.00 Depth (ft) = 3.00 Q (cfs) Area (sqft) = 10.00 Velocity (ft/s) = 2.00 Wetted Perim (ft) = 0.030 Crit Depth, Yc (ft) Top Width (ft) EGL (ft)

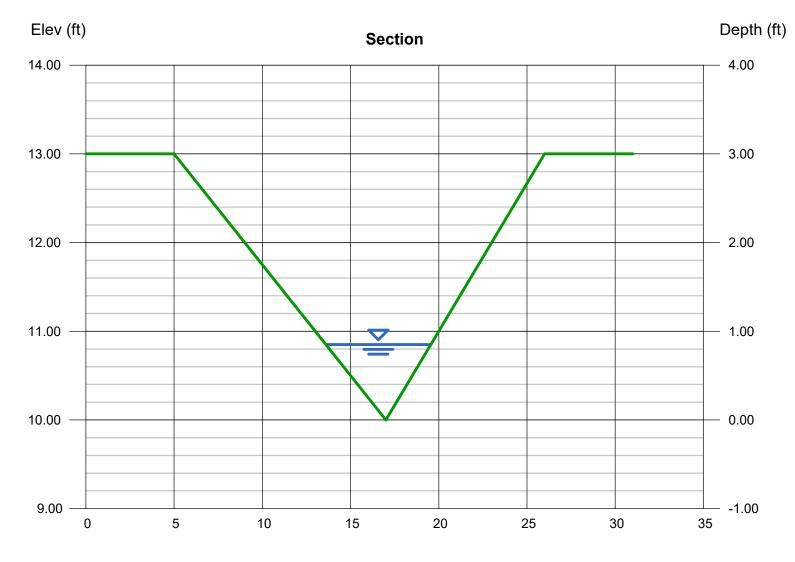


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### DP 1.2 Swale (5-Year)(FR:0.73)

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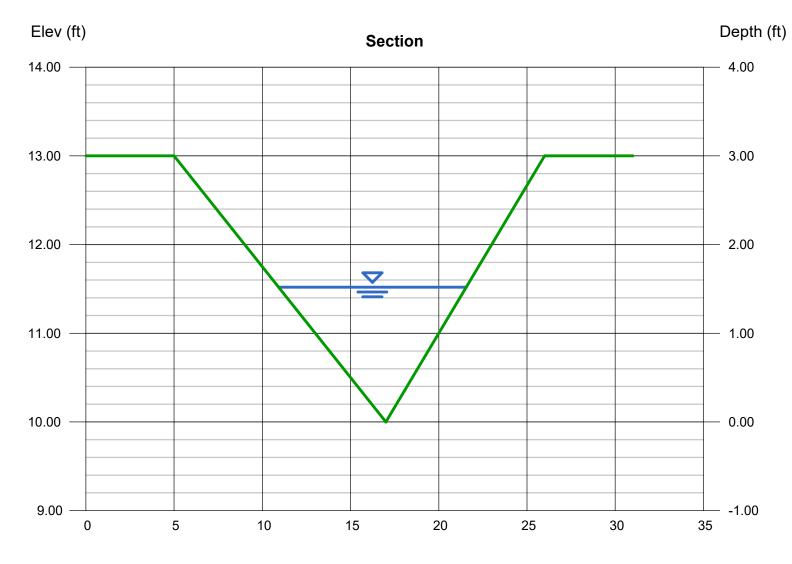
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### DP 1.2 Swale (100-Year)(FR:0.80)

Tria	na	ular

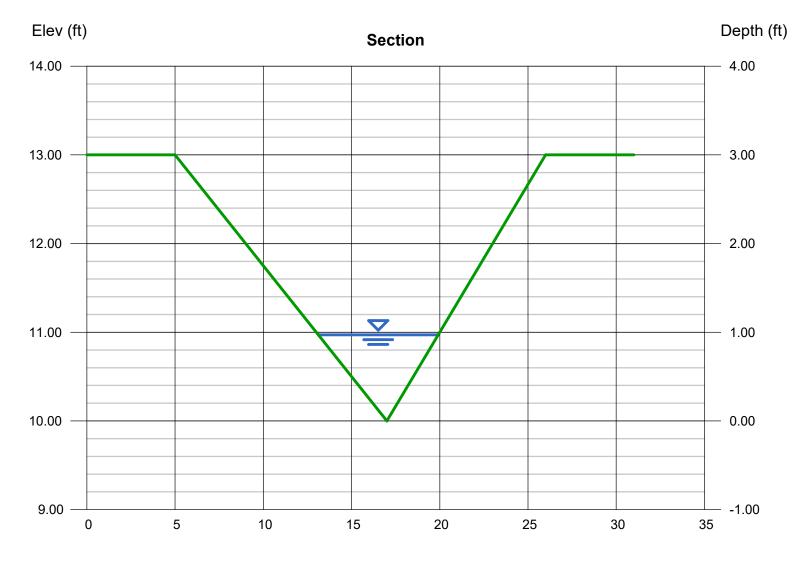
Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.52
Total Depth (ft)	= 3.00	Q (cfs)	= 32.20
		Area (sqft)	= 8.09
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.98
Slope (%)	= 1.00	Wetted Perim (ft)	= 11.07
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.40
		Top Width (ft)	= 10.64
Calculations		EGL (ft)	= 1.77
Compute by:	Known Q		
Known Q (cfs)	= 32.20		



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#### DP 1.3 Swale (5-Year)(FR:0.52)

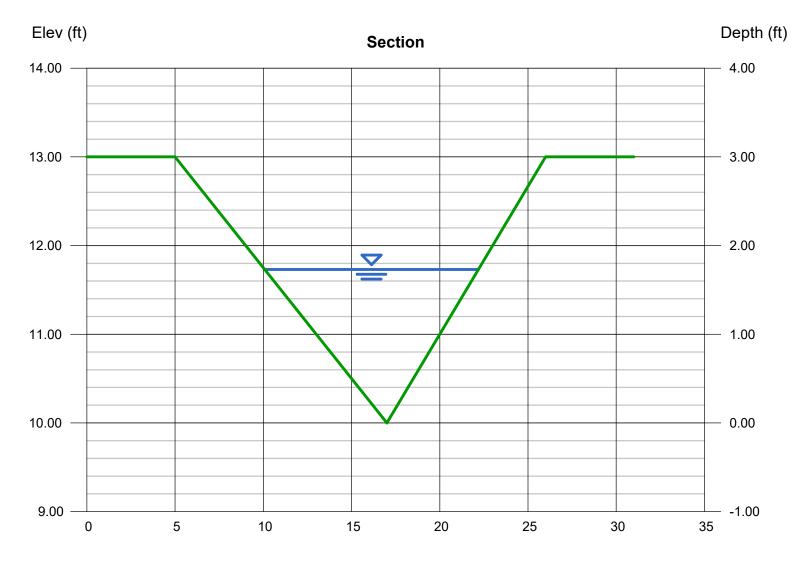
Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.97
Total Depth (ft)	= 3.00	Q (cfs)	= 6.800
		Area (sqft)	= 3.29
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.06
Slope (%)	= 0.50	Wetted Perim (ft)	= 7.07
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.75
		Top Width (ft)	= 6.79
Calculations		EGL (ft)	= 1.04
Compute by:	Known Q		
Known Q (cfs)	= 6.80		



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### DP 1.3 Swale (100-Year)(FR:0.58)

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.73
Total Depth (ft)	= 3.00	Q (cfs)	= 32.20
		Area (sqft)	= 10.48
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.07
Slope (%)	= 0.50	Wetted Perim (ft)	= 12.60
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.40
		Top Width (ft)	= 12.11
Calculations		EGL (ft)	= 1.88
Compute by:	Known Q		
Known Q (cfs)	= 32.20		

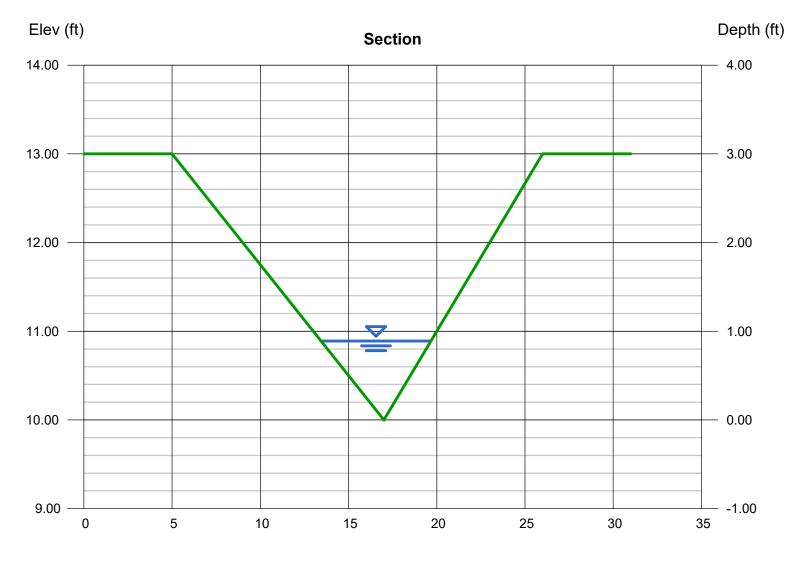


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### DP 1.4 Swale (5-Year)(FR:0.72)

Tria	na	ular

	Highlighted	
= 4.00, 3.00	Depth (ft)	= 0.89
= 3.00	Q (cfs)	= 7.600
	Area (sqft)	= 2.77
= 10.00	Velocity (ft/s)	= 2.74
= 1.00	Wetted Perim (ft)	= 6.48
= 0.030	Crit Depth, Yc (ft)	= 0.79
	Top Width (ft)	= 6.23
	EGL (ft)	= 1.01
Known Q		
= 7.60		
	= 3.00 = 10.00 = 1.00 = 0.030 Known Q	= 4.00, 3.00 Depth (ft) = 3.00 Q (cfs) Area (sqft) = 10.00 Velocity (ft/s) = 1.00 Wetted Perim (ft) = 0.030 Crit Depth, Yc (ft) Top Width (ft) EGL (ft)



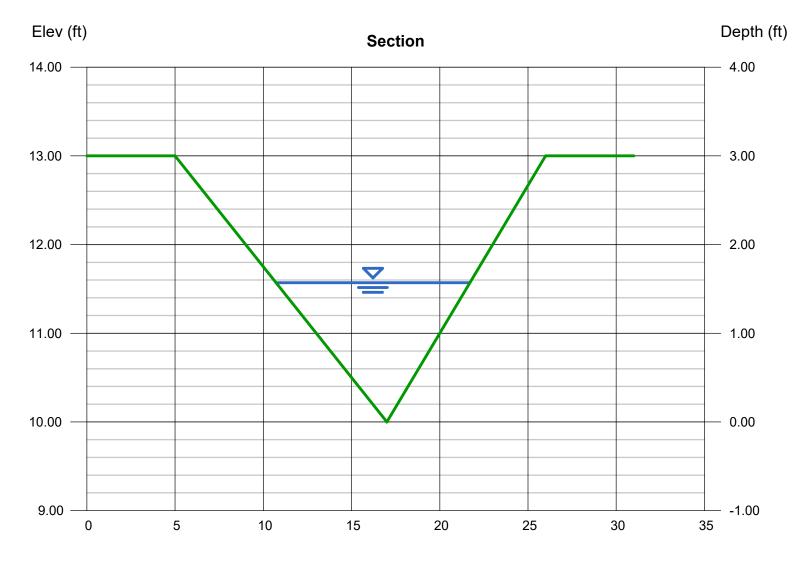
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### DP 1.4 Swale (100-Year)(FR:0.81)

Tria	na	ular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.57
Total Depth (ft)	= 3.00	Q (cfs)	= 35.00
		Area (sqft)	= 8.63
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 4.06
Slope (%)	= 1.00	Wetted Perim (ft)	= 11.44
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.45
		Top Width (ft)	= 10.99
Calculations		EGL (ft)	= 1.83
Compute by:	Known Q		
Known Q (cfs)	= 35.00		

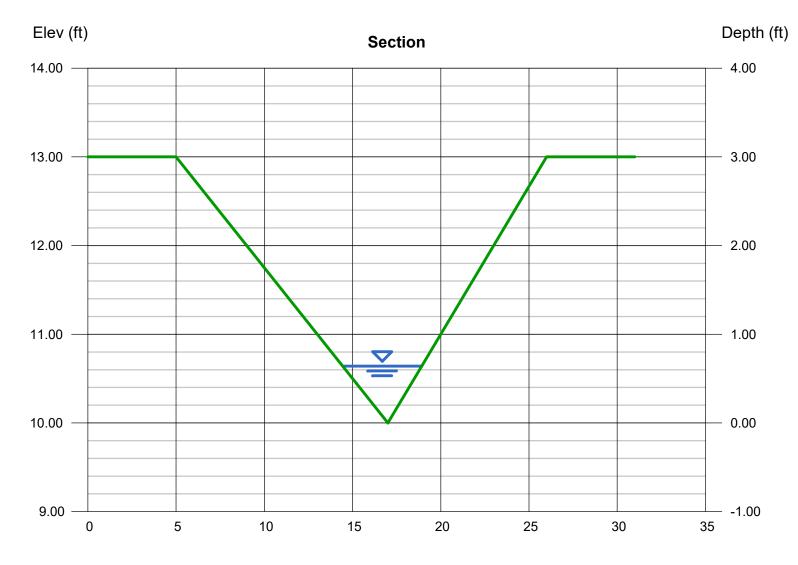


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#### DP 1.5 Swale (5-Year)(FR:0.69)

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TTTU	ngu	u

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.64
Total Depth (ft)	= 3.00	Q (cfs)	= 3.200
		Area (sqft)	= 1.43
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.23
Slope (%)	= 1.00	Wetted Perim (ft)	= 4.66
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.56
		Top Width (ft)	= 4.48
Calculations		EGL (ft)	= 0.72
Compute by:	Known Q		
Known Q (cfs)	= 3.20		

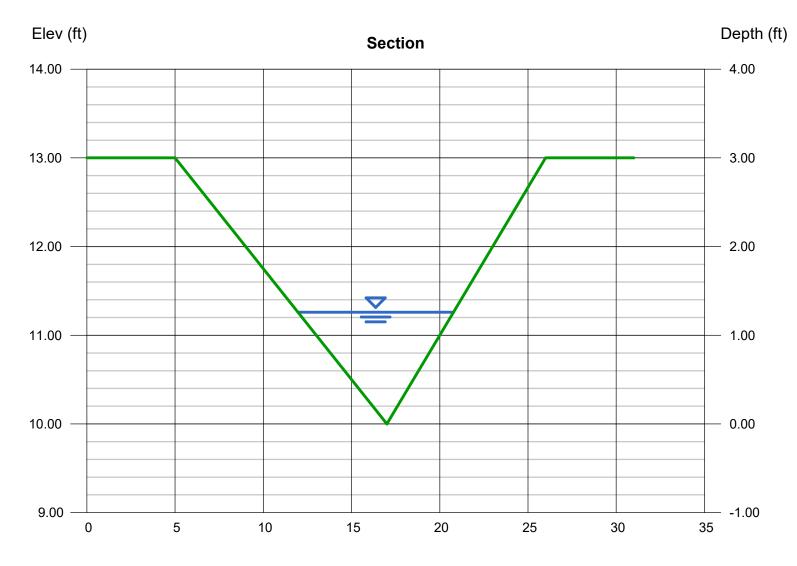


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#### DP 1.5 Swale (100-Year)(FR:0.78)

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.26
Total Depth (ft)	= 3.00	Q (cfs)	= 19.60
		Area (sqft)	= 5.56
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.53
Slope (%)	= 1.00	Wetted Perim (ft)	= 9.18
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.15
		Top Width (ft)	= 8.82
Calculations		EGL (ft)	= 1.45
Compute by:	Known Q		
Known Q (cfs)	= 19.60		



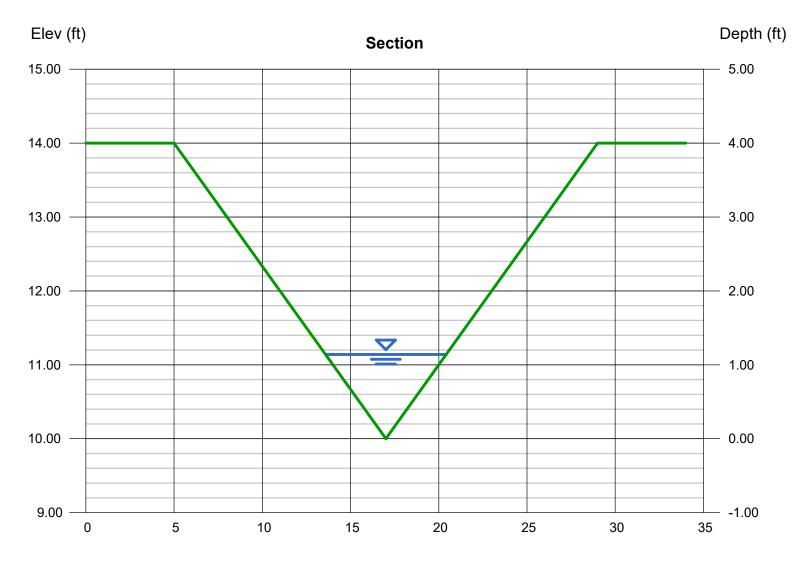
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#### DP 1.6 Swale (5-Year)(FR:0.63)

#### Triangular

Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 1.14
Total Depth (ft)	= 4.00 to avoid ponding and promote positive	Q (cfs) Area (sqft)	= 10.50 = 3.90
Invert Elev (ft)	= 10.00 drainage	Velocity (ft/s)	= 2.69
Slope (%)	= 0.70 Slope to be 1%	Wetted Perim (ft)	= 7.21
N-Value	= 0.030 minimum.	Crit Depth, Yc (ft)	= 0.95
		Top Width (ft)	= 6.84
Calculations		EGL (ft)	= 1.25
Compute by:	Known Q		
Known Q (cfs)	= 10.50		

Highlighted



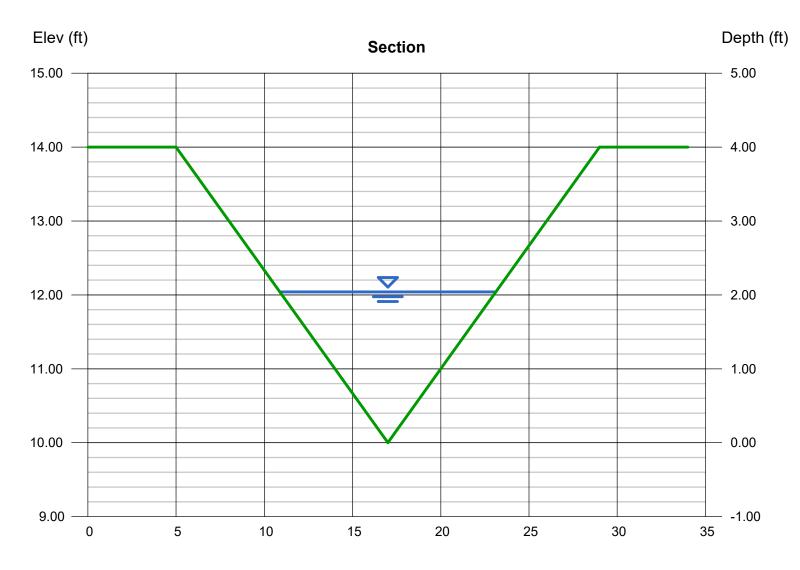
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#### DP 1.6 Swale (100-Year)(FR:0.70)

#### Triangular

Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 2.04
Total Depth (ft)	= 4.00	Q (cfs)	= 50.00
		Area (sqft)	= 12.48
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 4.00
Slope (%)	= 0.70 Slope to be 1%	Wetted Perim (ft)	= 12.90
N-Value	= 0.030 minimum.	Crit Depth, Yc (ft)	= 1.77
		Top Width (ft)	= 12.24
Calculations		EGL (ft)	= 2.29
Compute by:	Known Q		
Known Q (cfs)	= 50.00		

Highlighted

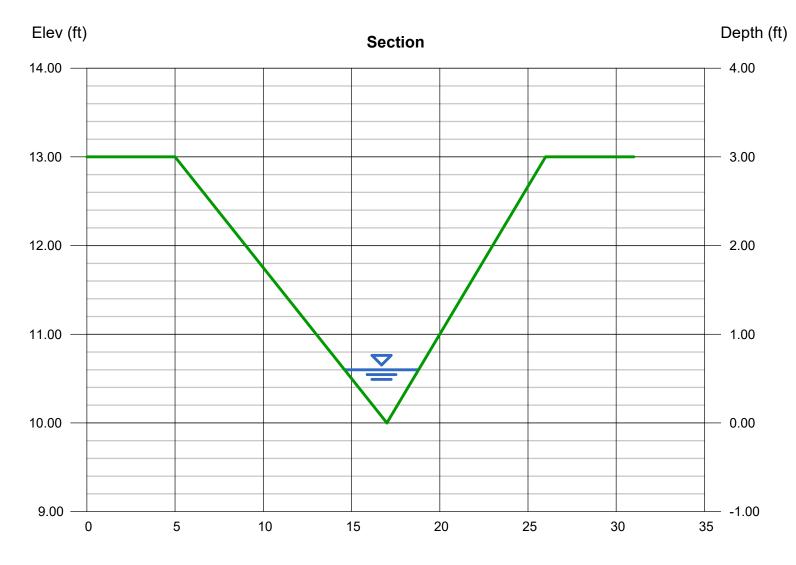


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#### DP 2.0 Swale (5-Year)(FR:0.71)

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.60
Total Depth (ft)	= 3.00	Q (cfs)	= 2.700
		Area (sqft)	= 1.26
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.14
Slope (%)	= 1.00	Wetted Perim (ft)	= 4.37
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.52
		Top Width (ft)	= 4.20
Calculations		EGL (ft)	= 0.67
Compute by:	Known Q		
Known Q (cfs)	= 2.70		

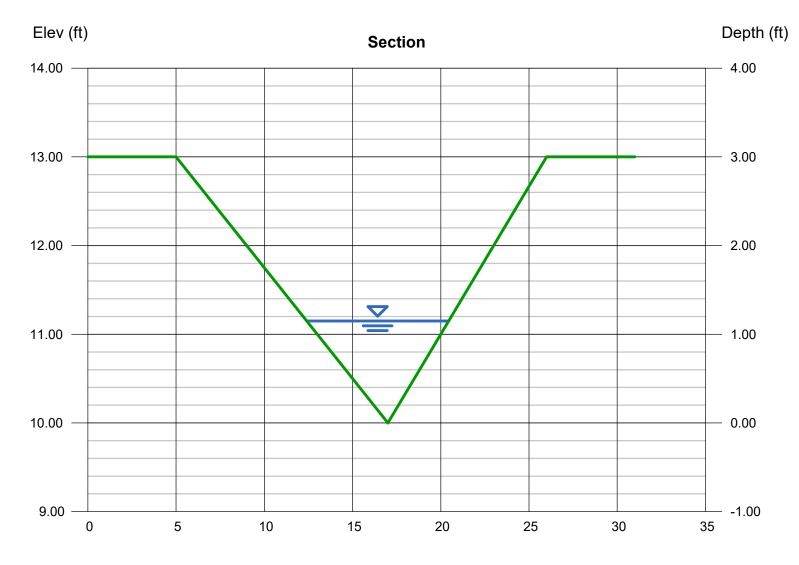


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#### DP 2.0 Swale (100-Year)(FR:0.77)

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.15
Total Depth (ft)	= 3.00	Q (cfs)	= 15.40
		Area (sqft)	= 4.63
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.33
Slope (%)	= 1.00	Wetted Perim (ft)	= 8.38
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.04
		Top Width (ft)	= 8.05
Calculations		EGL (ft)	= 1.32
Compute by:	Known Q		
Known Q (cfs)	= 15.40		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc in swale and determine if

### DP 2.1 Swale (5-Year)(FR:0.95)

#### Triangular

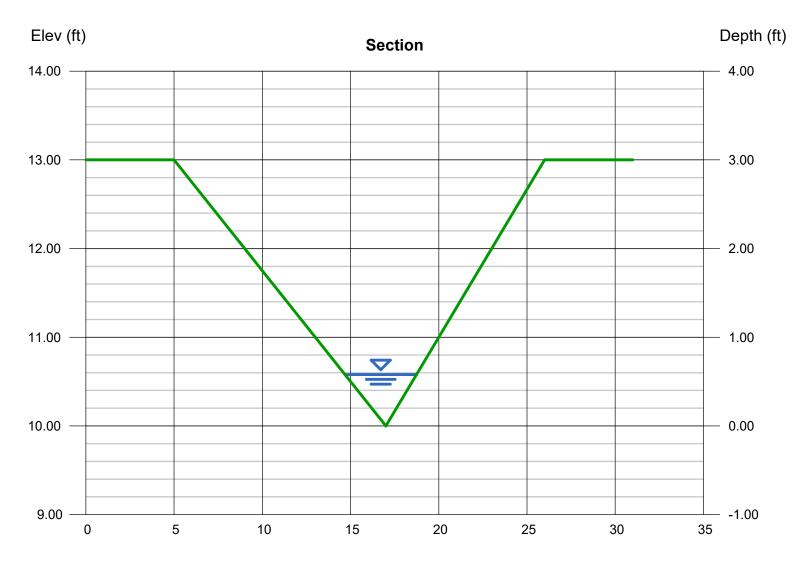
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.93
N-Value	= 0.030
Calculations	

Compute by:	Known Q
Known Q (cfs)	= 3.40

Fr number is over allowable 0.8 (supercritical). Check shear stress additional reinforcement is necessary.

#### Highlighted

Depth (ft)	= 0.58
Q (cfs)	= 3.400
Area (sqft)	= 1.18
Velocity (ft/s)	= 2.89
Wetted Perim (ft)	= 4.23
Crit Depth, Yc (ft)	= 0.57
Top Width (ft)	= 4.06
EGL (ft)	= 0.71



Reach (ft)

Friday, Dec 31 2021

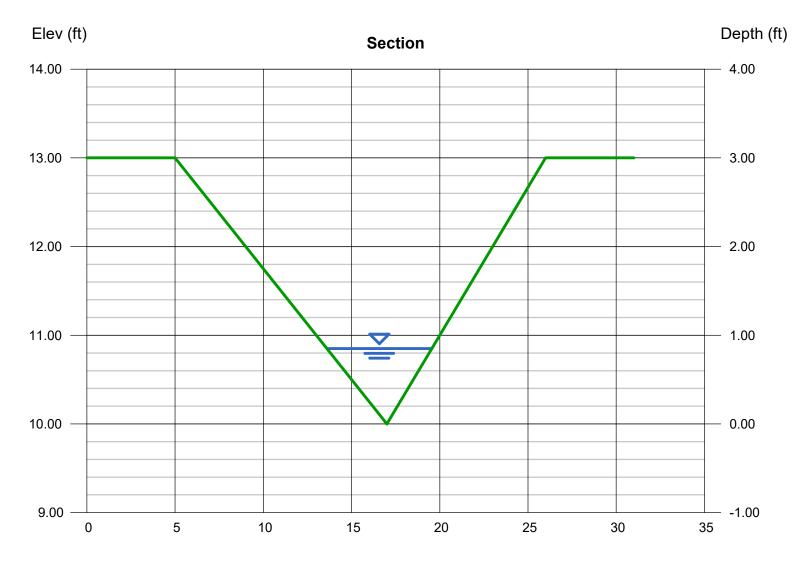
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

0.85 9.500 2.53 3.76 6.19 0.86 5.95 1.07

### DP 2.1 Swale (100-Year)(FR:1.01)

Tria	0.011	lar
IIIai	iyu	ai

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= (
Total Depth (ft)	= 3.00	Q (cfs)	= 9
		Area (sqft)	= 2
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= ;
Slope (%)	= 1.93	Wetted Perim (ft)	= (
N-Value	= 0.030	Crit Depth, Yc (ft)	= (
		Top Width (ft)	= ;
Calculations		EGL (ft)	=
Compute by:	Known Q		
Known Q (cfs)	= 9.50		



 Griatiner Report
 Fr number is over allowable 0.8

 Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Ine
 in swale and determine if

 additional reinforcement is
 necessary.

#### Friday, Dec 31 2021

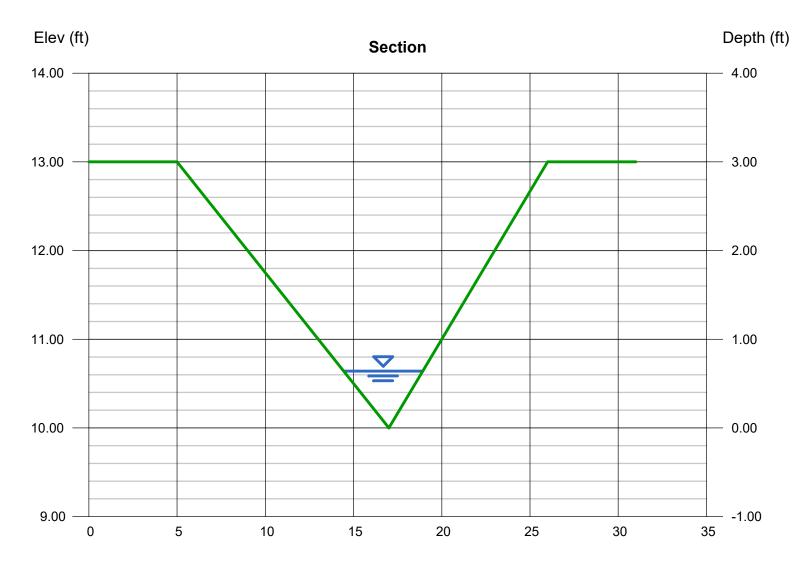
## Triangular

Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.83
N-Value	= 0.030
<b>Calculations</b> Compute by: Known Q (cfs)	Known Q = 4.30

DP 2.2 Swale (5-Year)(FR:0.93)

#### Highlighted

Depth (ft)	= 0.64
Q (cfs)	= 4.300
Area (sqft)	= 1.43
Velocity (ft/s)	= 3.00
Wetted Perim (ft)	= 4.66
Crit Depth, Yc (ft)	= 0.63
Top Width (ft)	= 4.48
EGL (ft)	= 0.78

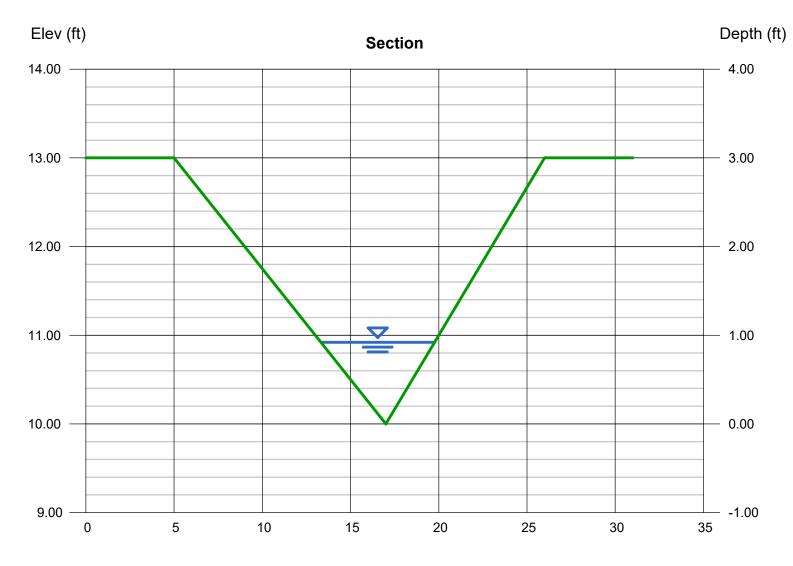


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### DP 2.2 Swale (100-Year)(FR:0.99)

Tria	ทศม	lar
I I I G	naa	iai

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.92
Total Depth (ft)	= 3.00	Q (cfs)	= 11.30
		Area (sqft)	= 2.96
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.81
Slope (%)	= 1.83	Wetted Perim (ft)	= 6.70
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.92
		Top Width (ft)	= 6.44
Calculations		EGL (ft)	= 1.15
Compute by:	Known Q		
Known Q (cfs)	= 11.30		

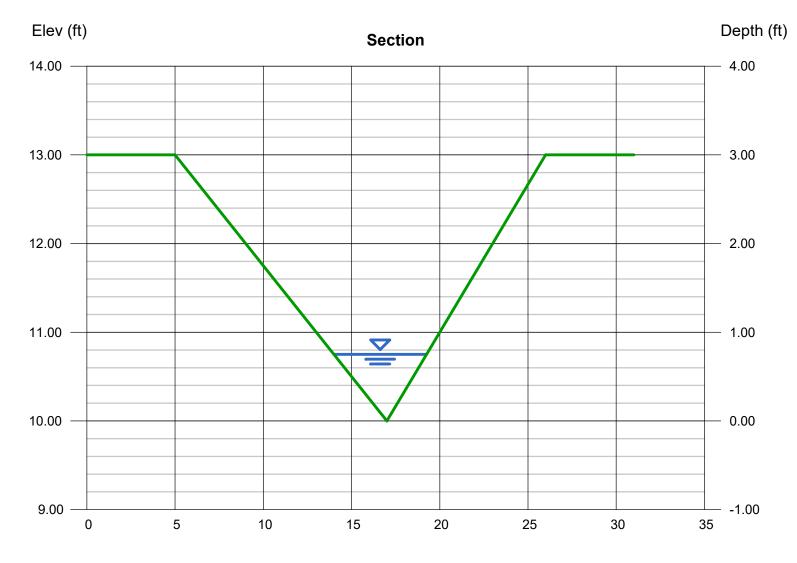


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### DP 2.3 Swale (5-Year)(FR:0.70)

In	ana	jular	•
	ung	juiui	

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.75
Total Depth (ft)	= 3.00	Q (cfs)	= 4.800
		Area (sqft)	= 1.97
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.44
Slope (%)	= 1.00	Wetted Perim (ft)	= 5.46
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.66
		Top Width (ft)	= 5.25
Calculations		EGL (ft)	= 0.84
Compute by:	Known Q		
Known Q (cfs)	= 4.80		

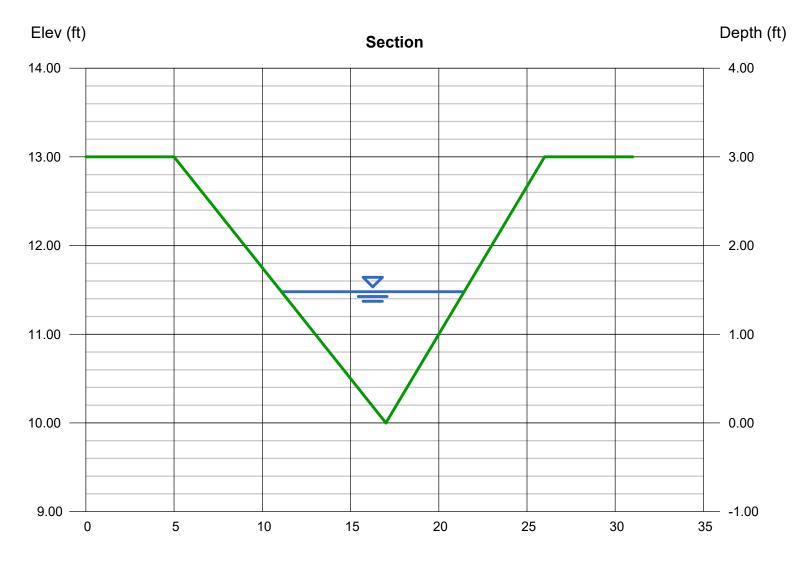


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### DP 2.3 Swale (100-Year)(FR:0.81)

Tria	ang	ular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.48
Total Depth (ft)	= 3.00	Q (cfs)	= 30.10
		Area (sqft)	= 7.67
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.93
Slope (%)	= 1.00	Wetted Perim (ft)	= 10.78
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.36
		Top Width (ft)	= 10.36
Calculations		EGL (ft)	= 1.72
Compute by:	Known Q		
Known Q (cfs)	= 30.10		

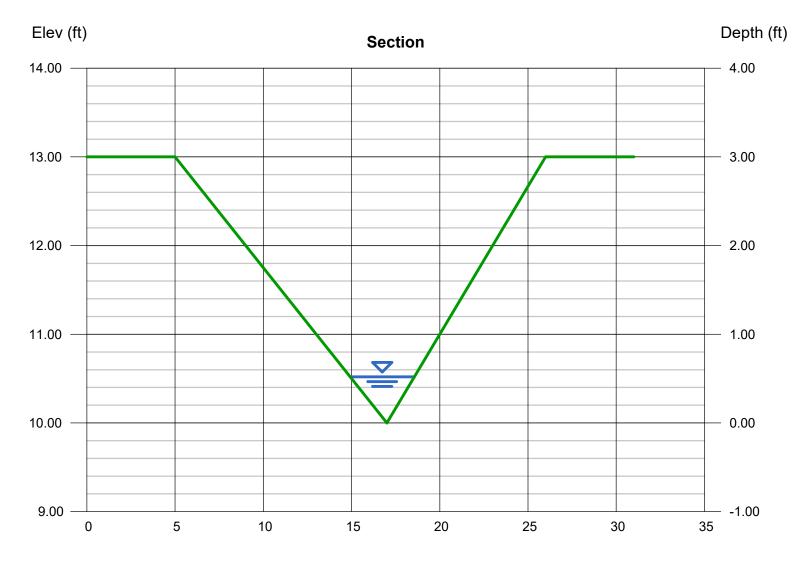


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP 3 Swale (5-Year)(FR:0.66)

Tri	an	an	lar
	un	gu	u

	Highlighted	
= 4.00, 3.00	Depth (ft)	= 0.52
= 3.00	Q (cfs)	= 1.800
	Area (sqft)	= 0.95
= 10.00	Velocity (ft/s)	= 1.90
= 1.00	Wetted Perim (ft)	= 3.79
= 0.030	Crit Depth, Yc (ft)	= 0.44
	Top Width (ft)	= 3.64
	EGL (ft)	= 0.58
Known Q		
= 1.80		
	= 3.00 = 10.00 = 1.00 = 0.030 Known Q	= 4.00, 3.00 Depth (ft) = 3.00 Q (cfs) Area (sqft) = 10.00 Velocity (ft/s) = 1.00 Wetted Perim (ft) = 0.030 Crit Depth, Yc (ft) Top Width (ft) EGL (ft)

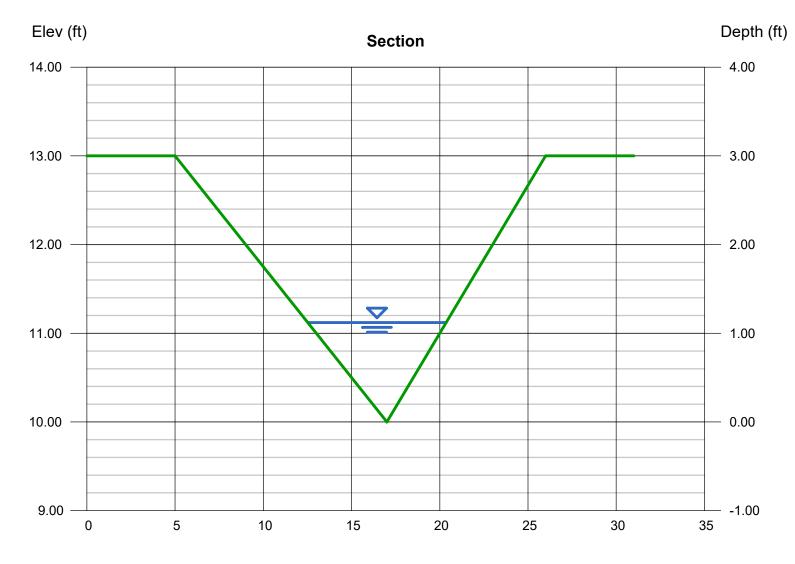


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP 3 Swale (100-Year)(FR:0.76)

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.12
Total Depth (ft)	= 3.00	Q (cfs)	= 14.10
		Area (sqft)	= 4.39
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.21
Slope (%)	= 1.00	Wetted Perim (ft)	= 8.16
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.01
		Top Width (ft)	= 7.84
Calculations		EGL (ft)	= 1.28
Compute by:	Known Q		
Known Q (cfs)	= 14.10		

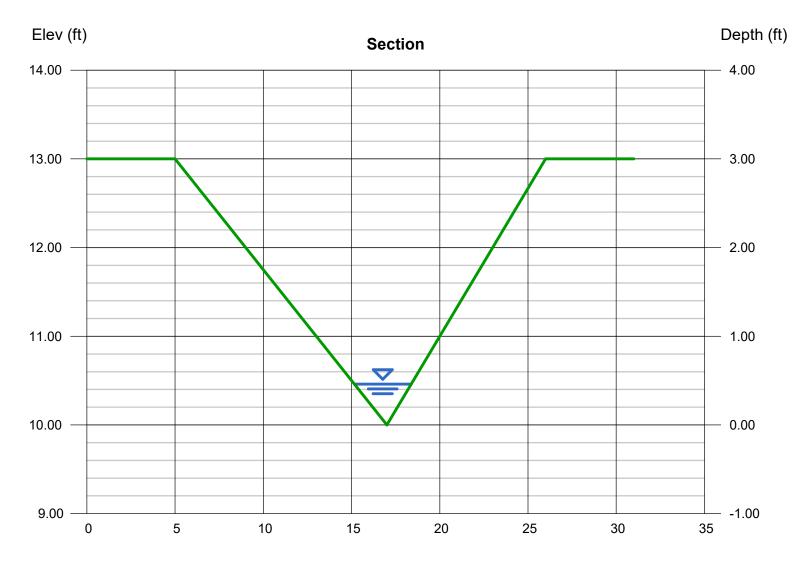


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP 7 Swale (5-Year)(FR:0.65)

Tri	an	an	lar
	un	gu	u

	Highlighted	
= 4.00, 3.00	Depth (ft)	= 0.46
= 3.00	Q (cfs)	= 1.300
	Area (sqft)	= 0.74
= 10.00	Velocity (ft/s)	= 1.76
= 1.00	Wetted Perim (ft)	= 3.35
= 0.030	Crit Depth, Yc (ft)	= 0.39
	Top Width (ft)	= 3.22
	EGL (ft)	= 0.51
Known Q		
= 1.30		
	= 3.00 = 10.00 = 1.00 = 0.030 Known Q	= 4.00, 3.00 Depth (ft) = 3.00 Q (cfs) Area (sqft) = 10.00 Velocity (ft/s) = 1.00 Wetted Perim (ft) = 0.030 Crit Depth, Yc (ft) Top Width (ft) EGL (ft)



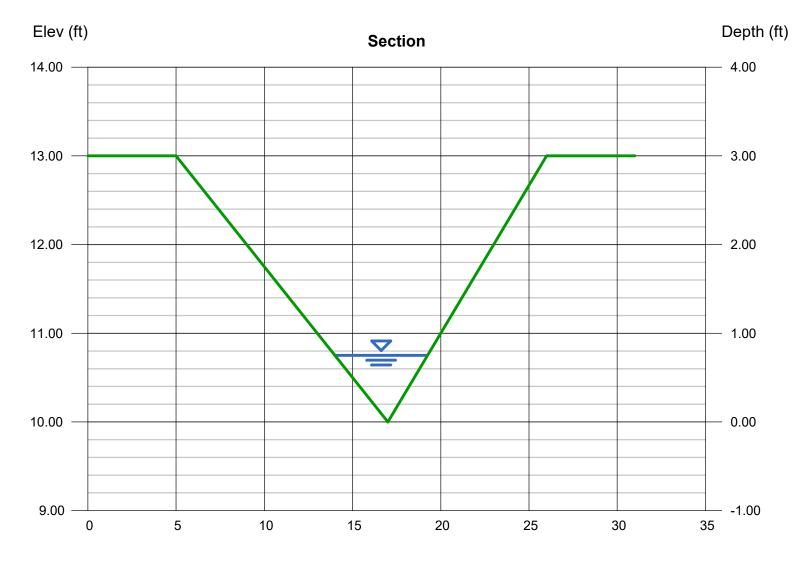
Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

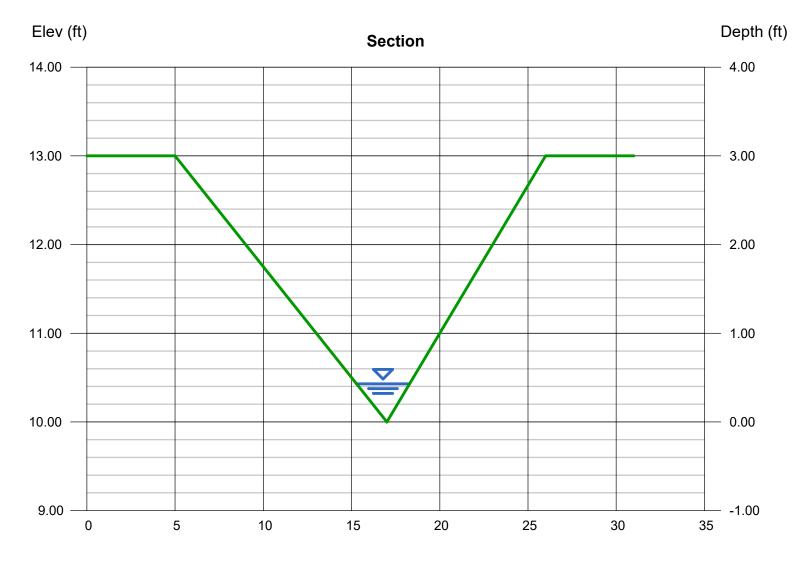
### DP 7 Swale (100-Year)(FR:0.72)

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.75
Total Depth (ft)	= 3.00	Q (cfs)	= 4.900
		Area (sqft)	= 1.97
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.49
Slope (%)	= 1.00	Wetted Perim (ft)	= 5.46
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.66
		Top Width (ft)	= 5.25
Calculations		EGL (ft)	= 0.85
Compute by:	Known Q		
Known Q (cfs)	= 4.90		



utodesk® Civil 3D® by Autodesk, Inc.	Fr number is over allowable 0.8 (supercritical). Check shear stress in swale and determine if additional reinforcement is necessary.	Friday, Dec 31 2021
4 00 0 00	Highlighted	0.40
,		= 0.43
= 3.00	Q (cfs)	= 1.500
	Area (sqft)	= 0.65
= 10.00	Velocity (ft/s)	= 2.32
= 2.00	Wetted Perim (ft)	= 3.13
	Crit Depth, Yc (ft)	= 0.41
dianage map	Top Width (ft)	= 3.01
	EGL (ft)	= 0.51
Known Q	ζ,	
= 1.50		
	<pre>e 4.00, 3.00 = 3.00 = 10.00 = 2.00 = 0.030 Slope is 2.3% p drainage map</pre>	<ul> <li>(supercritical). Check shear stress in swale and determine if additional reinforcement is necessary.</li> <li>= 4.00, 3.00</li> <li>= 3.00</li> <li>= 10.00</li> <li>= 2.00</li> <li>= 0.030</li> <li>Slope is 2.3% per drainage map</li> <li>Slope is 2.3% per drainage map</li> <li>Slope is 2.3% per drainage map</li> <li>Known Q</li> </ul>



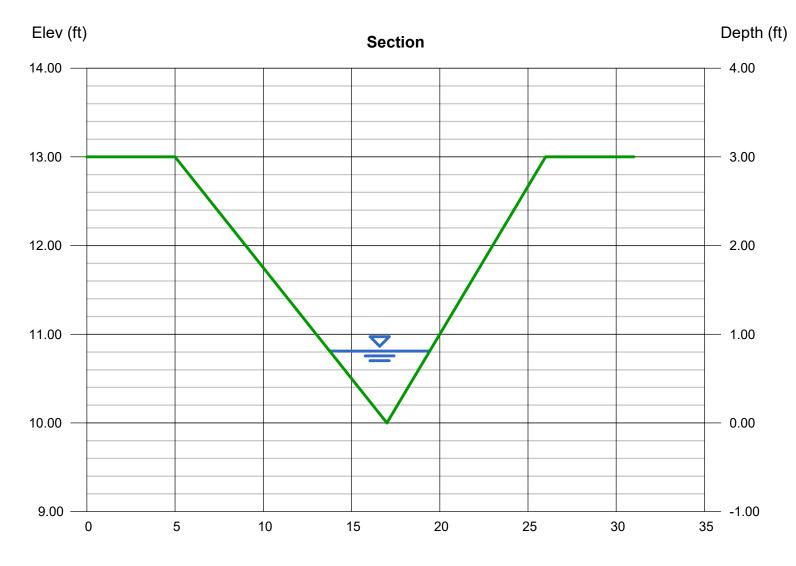
Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

## DP 11 Swale (100-Year)(FR:1.00)

Tri	an	qu	lar

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.81
Total Depth (ft)	= 3.00	Q (cfs)	= 8.300
		Area (sqft)	= 2.30
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 3.61
Slope (%)	= 2.00	Wetted Perim (ft)	= 5.90
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.82
		Top Width (ft)	= 5.67
Calculations		EGL (ft)	= 1.01
Compute by:	Known Q		
Known Q (cfs)	= 8.30		

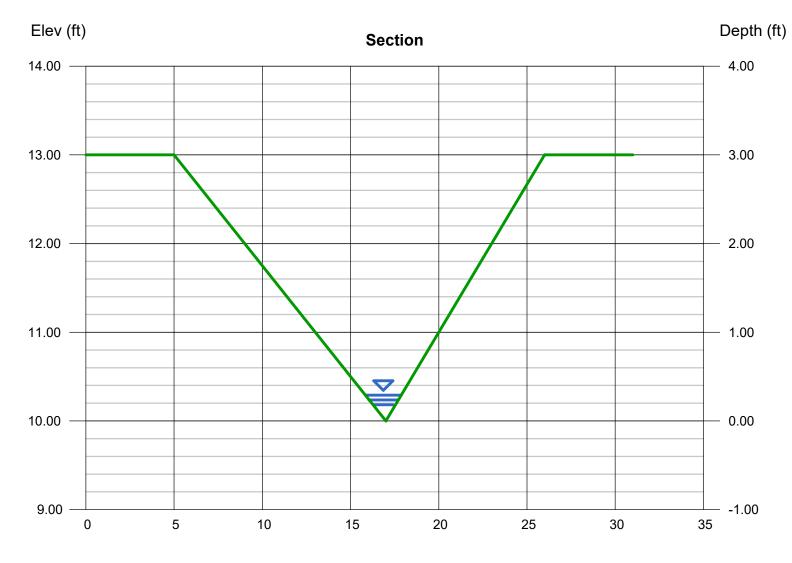


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP 16 Swale (5-Year)(FR:0.79)

Tria	ทศม	lar
I I I G	naa	iai

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.29
Total Depth (ft)	= 3.00	Q (cfs)	= 0.500
		Area (sqft)	= 0.29
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 1.70
Slope (%)	= 1.74	Wetted Perim (ft)	= 2.11
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.27
		Top Width (ft)	= 2.03
Calculations		EGL (ft)	= 0.33
Compute by:	Known Q		
Known Q (cfs)	= 0.50		

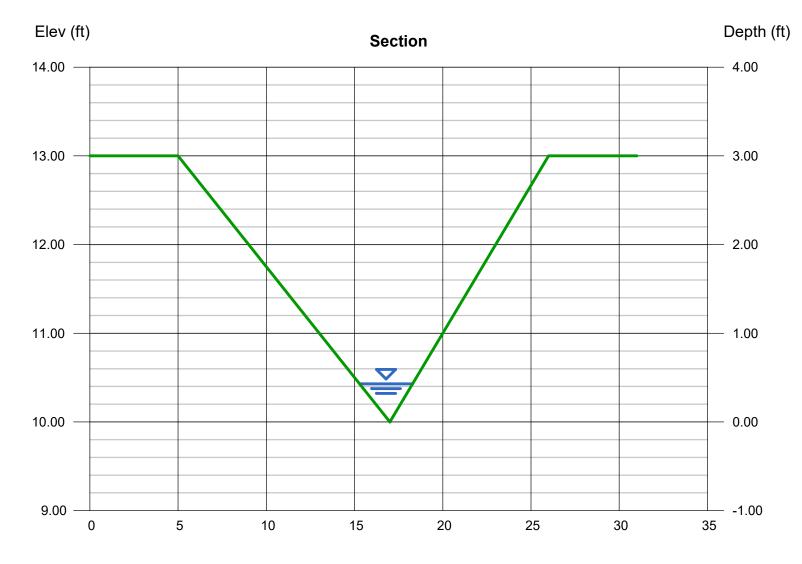


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP 16 Swale (100-Year)(FR:0.82)

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 0.43
Total Depth (ft)	= 3.00	Q (cfs)	= 1.400
		Area (sqft)	= 0.65
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 2.16
Slope (%)	= 1.74	Wetted Perim (ft)	= 3.13
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.40
		Top Width (ft)	= 3.01
Calculations		EGL (ft)	= 0.50
Compute by:	Known Q		
Known Q (cfs)	= 1.40		



Reach (ft)

Final Drainage Report Filing 3 - Saddlehorn Ranch

## **APPENDIX D**

## WATER QUALITY AND DETENTION CALCULATIONS

Provide tables each pond listing tributary basins, area and % impervious, to show total area & % impervious for each pond.

Provide calculations for sizing of spillway embankment riprap.

Provide calculations for sizing of riprap for rundowns into ponds.

Provide calculations for sizing of riprap at forebay berms

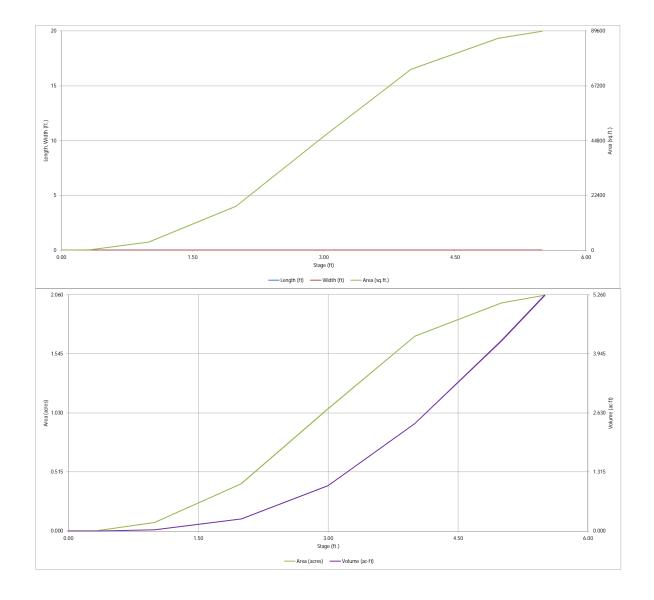
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

	Saddlehorn	Filing 3			etention, Version		-							
Basin I D:					page 5 c			ort,						
		1			in C is a									
VOLUME EURY WOCV	-	100-YE	AR	93.7	7 ac. U	odate	₽.							
PERMANENT ZONE POOL Example Zon	L1 AND 2		/		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Example 201	e comgura		nuon Ponu)		Description Top of Micropool	(ft)	Stage (ft) 0.00	(ft)	(ft)	(ft 2)	Area (ft ² ) 32	(acre) 0.001	(ft 3)	(ac-ft)
Watershed Information Selected BMP Type =	EDB			6710.67	6711		0.33				50	0.001	14	0.000
Watershed Area	96.84	acres			6712		1.00				3,260	0.075	1,122	0.026
Watershed Length = Watershed Length to Centroid =	5,370 1,383	ft ft			6713 6714		2.00				17,980 46,439	0.413	11,742 43,952	0.270
Watershed Slope =	0.012	ft/ft			6715		4.00				73,964	1.698	104,153	2.391
Watershed Imperviousness = Percentage Hydrologic Soil Group A =	14.60% 93.0%	percent percent			6716 6716.5		5.00 5.50				86,681 89,520	1.990 2.055	184,476 228,526	4.235 5.246
Percentage Hydrologic Soil Group B =	0.0%	percent			0710.0		0.00				07,520	2.000	210,020	0.210
Percentage Hydrologic Soil Groups C/D = Target WQCV Drain Time =	7.0%	percent hours												
Location for 1-hr Rainfall Depths =		nours				-				-				
After providing required inputs above in depths, click 'Run CUHP' to generate run	cluding 1-hour	rainfall												
the embedded Colorado Urban Hydro			Optional Use	er Overrides		1		1						
Water Quality Capture Volume (WQCV) = Excess Urban Runoff Volume (EURV) =	0.737	acre-feet acre-feet		acre-feet acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) =	0.711	acre-feet	1.19	inches		-		-						
5-yr Runoff Volume (P1 = 1.5 in.) = 10-yr Runoff Volume (P1 = 1.75 in.) =	1.074	acre-feet	1.50 1.75	inches										
25-yr Runoff Volume (P1 = 1.75 in.) =	3.279	acre-feet acre-feet	2.00	inches inches				1						
50-yr Runoff Volume (P1 = 2.25 in.) =	4.653	acre-feet	2.25	inches										
100-yr Runoff Volume (P1 = 2.52 in.) = 500-yr Runoff Volume (P1 = 3.14 in.) =	6.705 11.187	acre-feet acre-feet	2.52	inches inches										
Approximate 2-yr Detention Volume =	0.724	acre-feet		-				-						
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	1.034	acre-feet acre-feet												
Approximate 25-yr Detention Volume =	1.735	acre-feet												
Approximate 50-yr Detention Volume = Approximate 100-yr Detention Volume =	2.136 3.064	acre-feet acre-feet												
Define Zones and Basin Geometry Zone 1 Volume (WQCV) =	0.737	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	0.422	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	1.906	acre-feet acre-feet												
Initial Surcharge Volume (ISV) =	user	ft 3												
Initial Surcharge Depth (ISD) =	user	ft ft												
Total Available Detention Depth $(H_{total}) =$ Depth of Trickle Channel $(H_{TC}) =$	user	π ft												
Slope of Trickle Channel ( $S_{TC}$ ) =	user	ft/ft												
Slopes of Main Basin Sides $(S_{main}) =$ Basin Length-to-Width Ratio $(R_{L/W}) =$	user	H:V						-						
		-												
Initial Surcharge Area $(A_{ISV}) =$ Surcharge Volume Length $(L_{ISV}) =$	user	ft 2 ft												
Surcharge Volume Width (WISV) =	user	ft						-						
Depth of Basin Floor $(H_{FLOOR})$ = Length of Basin Floor $(L_{FLOOR})$ =	user	ft												
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	ft						-						
Area of Basin Floor (A _{FLOOR} ) = Volume of Basin Floor (V _{FLOOR} ) =	user	ft ² ft ³												
Depth of Main Basin (H _{MAIN} ) =	user	ft												
Length of Main Basin ( $L_{MAIN}$ ) = Width of Main Basin ( $W_{MAIN}$ ) =	user user	ft ft												
Area of Main Basin (A _{MAIN} ) =	user	ft ²												
Volume of Main Basin ( $V_{MAIN}$ ) = Calculated Total Basin Volume ( $V_{total}$ ) =	user user	ft ³												
carculated Total basili Volume (V _{total} ) =	usel	acre-feet												
								-						
								-						
						-								
												-		

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



#### DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021 Project: Saddlehorn Filing 3 Basin ID: Pond C Estimated Estimated Stage (ft) Volume (ac-ft) Outlet Type EURV W Orifice Plate Zone 1 (WQCV 2.73 0.737 Orifice Plate 100-YEAR Zone 2 (FURV 0.422 3.14 ZONE 1 AND 2 Zone 3 (100-year) 4.39 1.906 Weir&Pipe (Restrict) Example Zone Configuration (Retention Pond) Total (all zones) 3.064 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface) Underdrain Orifice Area N/A Underdrain Orifice Diameter N/A nches Underdrain Orifice Centroid N/A eet User Input: Orlfice Plate with one or more orlfices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row 1 694E-02 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width N/A Depth at top of Zone using Orifice Plate 3.14 feet Orifice Plate: Orifice Vertical Spacing N/A Elliptical Slot Centroid N/A feet inches 2.44 N/A ft² Orifice Plate: Orifice Area per Row sq. inches (diameter = 1-3/4 inches) Elliptical Slot Area User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ff 0.00 0.91 1.82 Orifice Area (sg. inches) 2 44 2.44 2 4 4 Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sq. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice N/A N/A N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area Depth at top of Zone using Vertical Orifice N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid N/A N/A feet Vertical Orifice Diameter N/A N/A nches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Wei Zone 3 Weir Not Selected Zone 3 Weir Not Selected Overflow Weir Front Edge Height, Ho 3.17 N/A t (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, Ht N/A 3.17 eet Overflow Weir Front Edge Length 6.00 N/A feet Overflow Weir Slope Length 5.00 N/A feet Overflow Weir Grate Slope 0.00 N/A H:V Grate Open Area / 100-yr Orifice Area 4.25 N/A Horiz. Length of Weir Sides 5.00 N/A eet Overflow Grate Open Area w/o Debris 20.88 N/A Overflow Grate Type Overflow Grate Open Area w/ Debris 20.88 N/A Type C Grate N/A Debris Clogging % = 0% N/A User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected N/A Depth to Invert of Outlet Pipe 0.39 N/A (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area 4.91 Outlet Pipe Diameter 30.00 N/A Spillway detail show spillway rifice Centroid 1.25 N/A feet Restrictor Plate Height Above Pipe Invert = inc Plate on Pipe : N/A 30.00 invert at 4.33 ft. Please revise 3.14 radians spreadsheet or details to match. User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= 4.00 Left (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.47 feet Spillway Crest Length 60.00 Stage at Top of Freeboard 5.47 feet feet Spillway End Slopes 4 00 н∙∨ Basin Area at Top of Freeboard 2 05 acres Freeboard above Max Water Surface 1.00 eet Basin Volume at Top of Freeboard 5.18 acre-ft Routed Hydrograph Results nle (Coli s W/th $uah \Delta F$ Design Storm Return Period WOC FUR\ 50 Year 100 Yea 500 Year 5 Ve 25 Ve One-Hour Rainfall Depth (in) N/A N/A 1.19 1.50 2.00 2.25 2.52 3.14 1.75 CUHP Runoff Volume (acre-ft) 0.737 1.159 0.71 1.074 1.450 3.279 4.653 6.705 11.187 3.279 Inflow Hydrograph Volume (acre-ft) N/A N/A 0.711 1.074 1 4 5 0 4.653 6.705 11.187 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.6 1.0 1.4 17.2 29.1 46.2 81.5 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.01 0.01 0.01 0.18 0.30 0.48 0.84 Peak Inflow Q (cfs) N/A N/A 8.8 29.2 41.8 60.2 97.1 Peak Outflow Q (cfs) 79.1 0.3 0.4 0.3 0.3 1.5 15.3 26.2 41.2 Ratio Peak Outflow to Predevelopment Q N/A N/A N/A 0.3 1.1 0.9 0.9 0.9 1.0 Plate Plate Plate Overflow Weir 1 Outlet Plate Structure Controlling Flow Overflow Weir 1 Overflow Weir 1 Spillway Plate Max Velocity through Grate 1 (fps) N/A N/A N/A N/A 07 21 1 2 20 Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) 51 38 49 57 53 50 46 39 38 Time to Drain 99% of Inflow Volume (hours) 40 54 40 60 58 57 52 52 Maximum Ponding Depth (ft) 273 3 14 2 5 9 2 97 3 52 3.68 3 90 4 33 3 23 0.89 1.15 0.80 1.05 1.21 1.39 1.49 1.63 1.79

0.977

1.27

1.649

1.86

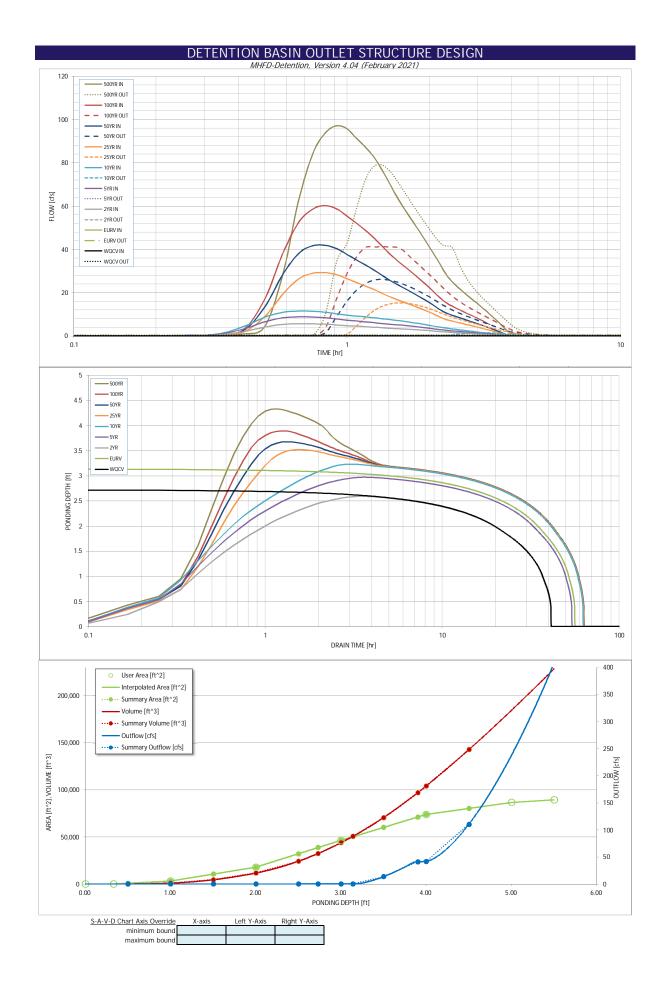
Area at Maximum Ponding Depth (acres) Maximum Volume Stored (acrest)

Fix drain time to be 40 hours

0.745

1.164

2.967



Outflow Hydrograph Workbook Filename:

[	The user can ov SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00 min	0:05:00						0.00		0.00	
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.04
	0:20:00	0.00	0.00	0.49	0.68	0.82	0.53	0.64	0.66	0.91
	0:25:00	0.00	0.00	1.97	3.17	4.25	1.80	2.42	2.78	4.35
	0:30:00	0.00	0.00	4.09	6.54	8.67	8.92	13.39	17.00	28.89
	0:35:00	0.00	0.00	5.34	8.37	10.93	19.40	28.58	38.34	63.01
	0:40:00	0.00	0.00	5.67	8.81	11.51	26.43	38.22	52.58	84.28
	0:45:00	0.00	0.00	5.63	8.71	11.43	28.97	41.67	58.62	93.78
	0:50:00	0.00	0.00	5.41	8.36	10.97	29.22	41.84	60.17	97.06
	1:00:00	0.00	0.00	5.09 4.78	7.81	10.24 9.62	28.29	40.33	58.73 55.34	95.68 91.22
	1:05:00	0.00	0.00	4.78	6.90	9.62	26.48 24.70	37.63 35.08	52.05	87.27
	1:10:00	0.00	0.00	4.30	6.53	8.80	23.10	32.81	48.89	82.89
	1:15:00	0.00	0.00	4.05	6.16	8.46	21.54	30.61	45.46	77.40
	1:20:00	0.00	0.00	3.80	5.77	8.05	19.95	28.35	41.94	71.50
	1:25:00	0.00	0.00	3.60	5.48	7.67	18.40	26.11	38.52	65.69
	1:30:00	0.00	0.00	3.45	5.23	7.28	17.12	24.29	35.66	60.79
	1:35:00	0.00	0.00	3.29	4.98	6.89	16.01	22.68	33.19	56.44
	1:40:00	0.00	0.00	3.14	4.72	6.50	14.98	21.19	30.91	52.44
	1:45:00	0.00	0.00	2.98	4.45	6.11	13.97	19.72	28.72	48.62
	1:50:00	0.00	0.00	2.83	4.16	5.72	12.98	18.28	26.58	44.92
	1:55:00 2:00:00	0.00	0.00	2.66	3.88	5.34	12.00	16.85	24.45	41.27
	2:00:00	0.00	0.00	2.46	3.59	4.94	11.02	15.43	22.36	37.68
	2:10:00	0.00	0.00	2.25	3.28	4.51	8.98	13.99 12.52	20.25	34.12 30.57
	2:15:00	0.00	0.00	1.88	2.97	3.78	8.07	12.52	16.13	27.54
	2:20:00	0.00	0.00	1.75	2.56	3.53	7.40	10.34	14.92	25.29
	2:25:00	0.00	0.00	1.63	2.39	3.28	6.89	9.63	13.86	23.44
	2:30:00	0.00	0.00	1.52	2.22	3.05	6.43	9.00	12.92	21.80
	2:35:00	0.00	0.00	1.41	2.06	2.83	6.01	8.41	12.06	20.29
	2:40:00	0.00	0.00	1.30	1.91	2.62	5.60	7.83	11.24	18.86
	2:45:00	0.00	0.00	1.20	1.77	2.41	5.20	7.27	10.44	17.49
	2:50:00	0.00	0.00	1.11	1.62	2.21	4.81	6.73	9.67	16.20
	2:55:00	0.00	0.00	1.02	1.49	2.03	4.44	6.20	8.92	14.95
	3:00:00	0.00	0.00	0.93	1.36	1.85	4.07	5.67	8.18	13.71
	3:05:00 3:10:00	0.00	0.00	0.84	1.23	1.67	3.70	5.16	7.44	12.48
	3:15:00	0.00	0.00	0.75	1.10 0.97	1.50 1.33	3.33 2.97	4.64	6.71 5.97	11.26 10.03
	3:20:00	0.00	0.00	0.59	0.85	1.17	2.61	3.62	5.24	8.81
	3:25:00	0.00	0.00	0.51	0.73	1.00	2.25	3.11	4.51	7.60
	3:30:00	0.00	0.00	0.43	0.61	0.84	1.89	2.61	3.79	6.38
	3:35:00	0.00	0.00	0.35	0.49	0.68	1.54	2.10	3.06	5.17
	3:40:00	0.00	0.00	0.27	0.38	0.53	1.19	1.60	2.34	3.96
	3:45:00	0.00	0.00	0.20	0.27	0.39	0.85	1.12	1.63	2.78
	3:50:00	0.00	0.00	0.16	0.21	0.30	0.53	0.66	0.96	1.70
	3:55:00	0.00	0.00	0.13	0.17	0.25	0.33	0.41	0.58	1.10
	4:00:00	0.00	0.00	0.11	0.15	0.21	0.23	0.29	0.39	0.75
	4:05:00	0.00	0.00	0.10	0.13 0.11	0.18	0.18	0.22 0.17	0.27	0.52
	4:10:00	0.00	0.00	0.08	0.11	0.16	0.14	0.17	0.20	0.35
	4:20:00	0.00	0.00	0.06	0.08	0.10	0.09	0.11	0.10	0.15
ļ	4:25:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.07	0.10
	4:30:00 4:35:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.06	0.08
	4:35:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	4:45:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
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	4:55:00 5:00:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	5:05:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
ļ	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Stage Description [ft]	Area [ft ² ]	Area [acres]	Volume [ft ³ ]	Volume	Outflow	1
1043				[ac-ft]	[cfs]	
		0.020	91	0.002	0.06	
0.50						For best results, include the
1.00		0.075	1,122	0.026	0.11	stages of all grade slope changes (e.g. ISV and Floor)
1.50		0.244	4,592	0.105	0.16	from the S-A-V table on
2.00		0.413	11,742	0.270	0.24	Sheet 'Basin'.
2.50		0.739	24,289	0.558	0.30	
WQCV 2.73		0.890	32,450	0.745	0.32	Also include the inverts of all
3.00		1.066	43,952	1.009	0.35	outlets (e.g. vertical orifice, overflow grate, and spillway,
EURV 3.14		1.155	50,723	1.164	0.36	where applicable).
3.50		1.382	70,612	1.621	13.83	
100-YR 3.90		1.635	96,894	2.224	41.21	-
4.00		1.698	104,153	2.391	41.88	-
4.50	80,322	1.844	142,725	3.277	110.43	-
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## POND C FOREBAY VOLUME REQUIREMENTS

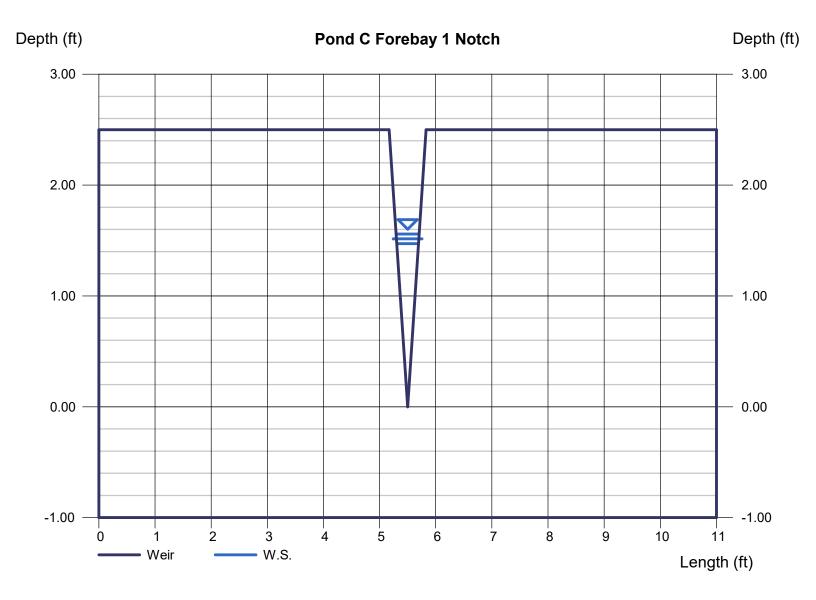
Equation 3-1	² +0.781/)			
PROPOSED FOREBAY FUTURE FOREBAY	I=.153	WQCV=	0.094743	
	I=.115	WQCV=	0.075346	
Equation 3-3	•			
PROPOSED FOREBAY	A= 80.46 Acres	V=	0.611	
FUTURE FOREBAY	A= 16.38 Acres	V=	0.103	
FOREB	3% OF WC AY TOTAL VOLUN		.03(V)	
VOLUME REQUIRED FOR PROPO	SED FOREBAY =		0.018 AC-FT	798 CF
VOLUME REQUIRED FOR FUTURE	E FOREBAY=		0.003 AC-FT	134 CF
VOLUME PROVIDED FOR PROPO	SED FOREBAY =		0.023 AC-FT	993 CF
Q ₁₀₀ DISCHARGES	2% OF Q ₁₀₀			
Q ₁₀₀ PROPOSED FOREBAY=	.02*50.0 CFS= 1.0	0 CES		
100				

Q₁₀₀ FUTURE FOREBAY= .02*14.3 CFS= 0.29 CFS

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### Pond C Forebay 1 Notch

	Highlighted	
= Sharp	Depth (ft)	= 1.56
= 15	Q (cfs)	= 1.000
= 2.50	Area (sqft)	= 0.32
	Velocity (ft/s)	= 3.13
	Top Width (ft)	= 0.41
= 0.33		
Known Q		
= 1.00		
	= 15 = 2.50 = 0.33 Known Q	= Sharp Depth (ft) = 15 Q (cfs) = 2.50 Area (sqft) Velocity (ft/s) Top Width (ft) = 0.33 Known Q

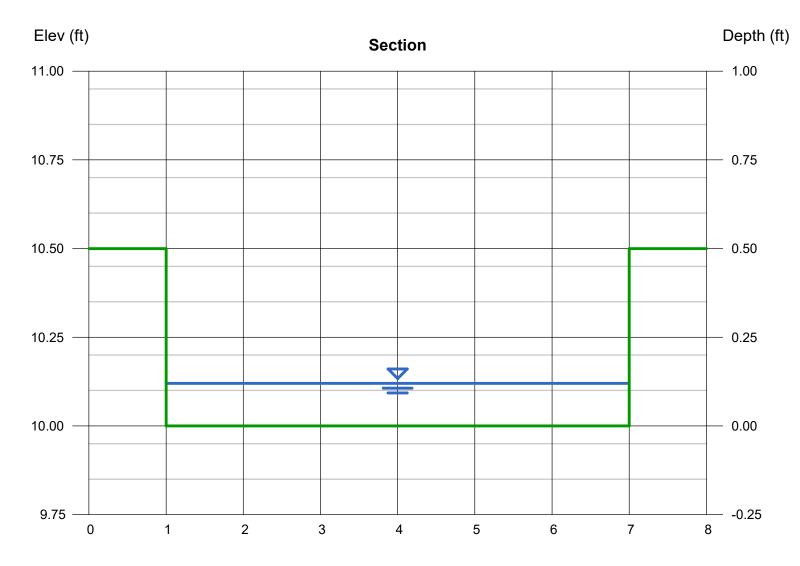


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

## Pond C Trickle Channel

Rectangular		Highlighted	
Bottom Width (ft)	= 6.00	Depth (ft)	= 0.12
Total Depth (ft)	= 0.50	Q (cfs)	= 1.290
		Area (sqft)	= 0.72
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 1.79
Slope (%)	= 0.50	Wetted Perim (ft)	= 6.24
N-Value	= 0.013	Crit Depth, Yc (ft)	= 0.12
		Top Width (ft)	= 6.00
Calculations		EGL (ft)	= 0.17
Compute by:	Known Q		
Known Q (cfs)	= 1.29		



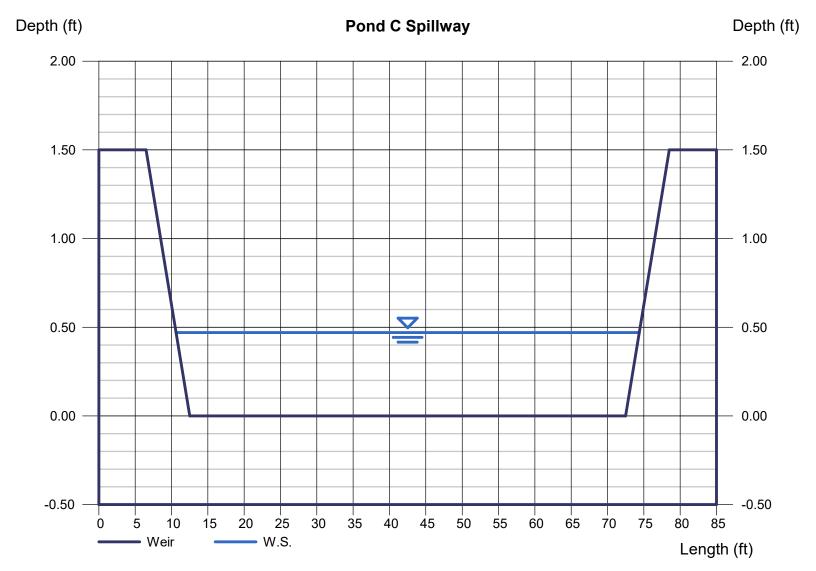
Reach (ft)

## Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### Pond C Spillway

.47
0.20
9.08
.07
3.76
(



#### Tuesday, Dec 14 2021

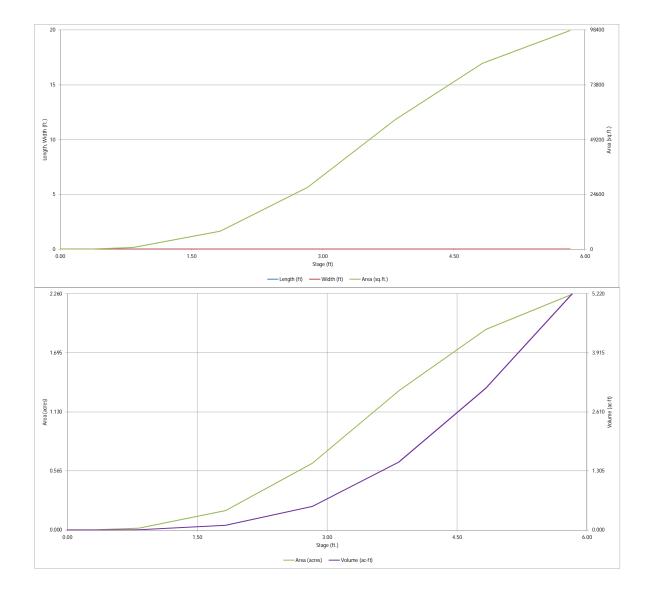
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention,	Version	4.04	(February	2021)
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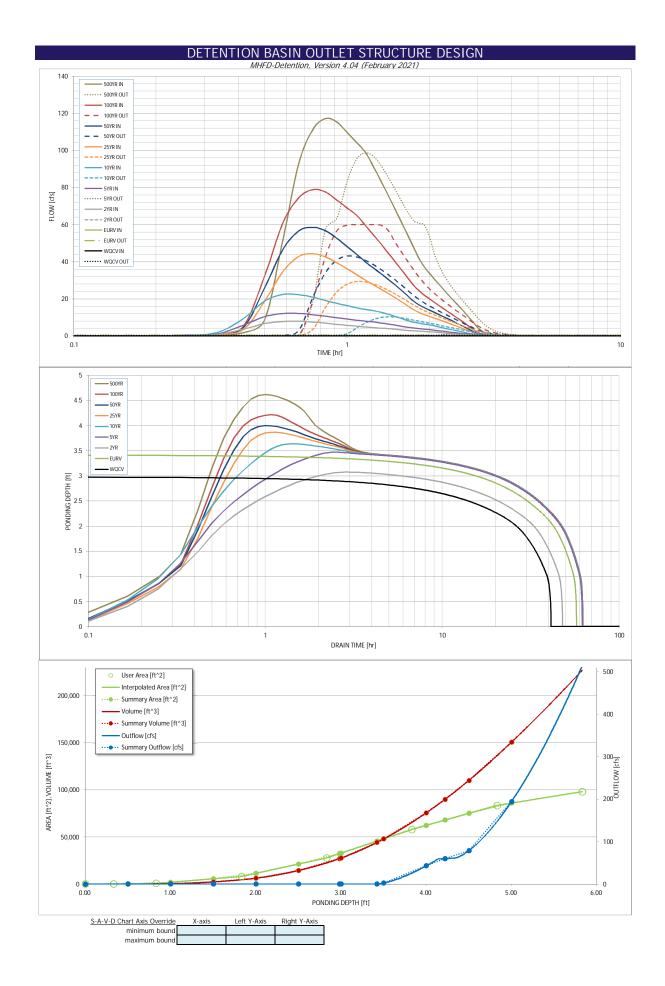
MHFD-Detention, Version 4.04 (February 2021) Project: Saddlehorn Filing 3														
Project: Basin I D:		Filing 3		On	page 5 c	of the	rend	ort						
ZONE 3	2							лц,						
		1			in D is a									
VOLUMET EDHAT MOCA		100-YE	AR	of74	1.66 ac.	Upda	ate.							
	I AND 2	0RIFIC	/		Depth Increment =	•	Ω Optional				Optional			
POOL Example Zon	e Configura	tion (Rete	ntion Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ² )	Override Area (ft ² )	Area (acre)	Volume (ft 3)	Volume (ac-ft)
Watershed Information		/		6709.17			0.00				32	0.001		
Selected BMP Type = Watershed Area =	EDB 78.02	acres			6709.5 6710		0.33				50 699	0.001	14 201	0.000
Watershed Length =	3,473	ft			6711		1.83				8,089	0.186	4,595	0.105
Watershed Length to Centroid =	970	ft			6712		2.83				27,770	0.638	22,524	0.517
Watershed Slope = Watershed Imperviousness =	0.012	ft/ft percent			6713 6714		3.83 4.83				58,037 83,546	1.332	65,427 136,219	1.502 3.127
Percentage Hydrologic Soil Group A =		percent			6715		5.83				98,172	2.254	227,078	5.213
Percentage Hydrologic Soil Group B =	0.0%	percent												
Percentage Hydrologic Soil Groups C/D = Target WQCV Drain Time =	30.0% 40.0	percent hours												
Location for 1-hr Rainfall Depths =	1	nours												
After providing required inputs above in	cluding 1-hour	rainfall												
depths, click 'Run CUHP' to generate run the embedded Colorado Urban Hydr			Optional Use	r Ouerridee										
Water Quality Capture Volume (WQCV) =		acre-feet	Optional 036	acre-feet										
Excess Urban Runoff Volume (EURV) =	1.007	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) = 5-yr Runoff Volume (P1 = 1.5 in.) =	0.755	acre-feet acre-feet	1.19	inches inches										
10-yr Runoff Volume (P1 = 1.5 in.) =	2.116	acre-feet	1.50	inches										
25-yr Runoff Volume (P1 = 2 in.) =	3.929	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) = 100-yr Runoff Volume (P1 = 2.52 in.) =	5.225	acre-feet acre-feet	2.25	inches inches							-			
500-yr Runoff Volume (P1 = 2.52 in.) =	11.183	acre-feet	2.02	inches										
Approximate 2-yr Detention Volume =	0.683	acre-feet												
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	1.098	acre-feet acre-feet												
Approximate 10-yr Detention Volume = Approximate 25-yr Detention Volume =	1.393	acre-feet												
Approximate 50-yr Detention Volume =	2.024	acre-feet												
Approximate 100-yr Detention Volume =	2.808	acre-feet												
Define Zones and Basin Geometry														
Zone 1 Volume (WQCV) =	0.619	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	0.388	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	1.800 2.808	acre-feet acre-feet												
Initial Surcharge Volume (ISV) =	user	ft ³												
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth ( $H_{total}$ ) = Depth of Trickle Channel ( $H_{TC}$ ) =	user	ft ft												
Slope of Trickle Channel ( $S_{TC}$ ) =	user	ft/ft												
Slopes of Main Basin Sides (S _{main} ) =	user	H:V												
Basin Length-to-Width Ratio (R _{L/W} ) =	user													
Initial Surcharge Area (A _{ISV} ) =	user	ft 2												
Surcharge Volume Length (LISV) =		ft												
Surcharge Volume Width $(W_{ISV})$ = Depth of Basin Floor $(H_{FLOOR})$ =	user	ft ft												
Length of Basin Floor $(L_{FLOOR}) =$		ft												
Width of Basin Floor ( $W_{FLOOR}$ ) =		ft												
Area of Basin Floor (A _{FLOOR} ) = Volume of Basin Floor (V _{FLOOR} ) =	user	ft ² ft ³												
Depth of Main Basin (H _{MAIN} ) =		ft												
Length of Main Basin ( $L_{MAIN}$ ) =	user	ft												
Width of Main Basin (W _{MAIN} ) =	user	ft ft ²												
Area of Main Basin $(A_{MAIN}) =$ Volume of Main Basin $(V_{MAIN}) =$	user	ft ² ft ³												
Calculated Total Basin Volume (V _{total} ) =	user	acre-feet												
									1				1	

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



N/A N/A N/A or Elliptical Slot We 0.00 3.42 13.70 2.05 Now 1 (required) 0.00 2.05 Row 9 (optional) 200 Zone 2 Circular 2.98 3.42 0.38 oped Grate and Or Zone 3 Weir (3.42) 10.00 0.00	etention Pond) V in a Filtration BMP) ft (distance below inches eir (typically used to c ft (relative to basin ft (relative to basin inches sq. inches (diamete m lowest to highest)	the filtration media si drain WQCV and/or E b bottom at Stage = ( b bottom at Stage = ( c bottom at Stage = ( c er = 1-5/8 inches) Row 3 (optional) 2.28 2.05 Row 11 (optional) ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	3.42 4.66 Total (all zones) urface) URV in a sedimental 0 ft) 0 ft) Row 4 (optional) Row 12 (optional) bottom at Stage = (	Underdra	Outlet Type Orifice Plate Circular Orifice Weir&Pipe (Restrict) drain Orifice Area = in Orifice Centroid = fice Area per Row = liptical Half-Width = tical Slot Centroid = Elliptical Slot Area = Row 6 (optional) Row 14 (optional) control = ertical Orifice Area = al Orifice Centroid =	Zone 2 Circular 0.00 0.02 Calculated Paramet	ft ² feet feet feet ft ² Row 8 (optional) Row 16 (optional) rers for Vertical Orific Not Selected N/A N/A	re ft² feet
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2.05 <u>www (numbered from</u> Row 1 (required) 0.00 2.05 Row 9 (optional) Zone 2 Circular 2.98 3.42 0.38 <u>oped Grate and O</u> Zone 3 Weir (3.42) 10.00 0.00	sq. inches (diameter m lowest to highest) Row 2 (optional) 1.14 2.05 Row 10 (optional) Row 10 (optional) Not Selected N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	Row 3 (optional) 2.28 2.05 Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b ft (relative to basin b) ft (r	Row 12 (optional)	Row 5 (optional) Row 13 (optional) Row 13 (optional) D ft) Vertic	Elliptical Slot Area = Row 6 (optional) Row 14 (optional) ertical Orifice Area =	N/A Row 7 (optional) Row 15 (optional) Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	ft ² Row 8 (optional) Row 16 (optional) ers for Vertical Orlfic Not Selected N/A N/A	ft ²
2.05 Row 1 (required) 0.00 2.05 Row 9 (optional) 2.05 2.05 Zone 2 Circular 2.98 3.42 0.38 2.98 3.42 0.38 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2.05 2	m lowest to highest) Row 2 (optional) 1.14 2.05 Row 10 (optional) Row 10 (optional) Not Selected N/A N/A N/A N/A N/A N/A	Row 3 (optional) 2.28 2.05 Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b ft (relative to basin b) ft (r	Row 12 (optional)	Row 5 (optional) Row 13 (optional) Row 13 (optional) D ft) D ft) V( D ft) Vertic D ft)	Row 6 (optional) Row 14 (optional)	Row 7 (optional) Row 15 (optional) Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	Row 8 (optional) Row 16 (optional) Not Selected N/A N/A	ft ²
Row 1 (required) 0.00 2.05 Row 9 (optional) Zone 2 Circular 2.98 3.42 0.38 oped Grate and Or Zone 3 Weir (3.42) 10.00 0.00	Row 2 (optional)       1.14       2.05       Row 10 (optional)       Not Selected       N/A	2.28 2.05 Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	Row 12 (optional)	Row 13 (optional) Row 13 (opti	Row 14 (optional)	Row 15 (optional) Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	Row 16 (optional)	ft ²
Row 1 (required) 0.00 2.05 Row 9 (optional) Zone 2 Circular 2.98 3.42 0.38 oped Grate and Or Zone 3 Weir (3.42) 10.00 0.00	Row 2 (optional)       1.14       2.05       Row 10 (optional)       Not Selected       N/A	2.28 2.05 Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	Row 12 (optional)	Row 13 (optional) Row 13 (opti	Row 14 (optional)	Row 15 (optional) Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	Row 16 (optional)	ft ²
Row 1 (required) 0.00 2.05 Row 9 (optional) Zone 2 Circular 2.98 3.42 0.38 oped Grate and Or Zone 3 Weir (3.42) 10.00 0.00	Row 2 (optional)       1.14       2.05       Row 10 (optional)       Not Selected       N/A	2.28 2.05 Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	Row 12 (optional)	Row 13 (optional) Row 13 (opti	Row 14 (optional)	Row 15 (optional) Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	Row 16 (optional)	ft ²
2.05 Row 9 (optional) Zone 2 Circular 2.98 3.42 0.38 0.98 0.38 0.00 2.09 3.42 0.38 0.00 0.00	2.05       Row 10 (optional)       Not Selected       N/A       N/A       N/A       Not Selected       N/A       N/A       Not Selected       N/A	2.05 Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( bottom at Stage = ( ir (and No Outlet Pip	D ft) Vo D ft) Vertic	ertical Orifice Area =	Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	ers for Vertical Orific Not Selected N/A N/A	ft ²
Row 9 (optional) Zone 2 Circular 2.98 3.42 0.38 Oped Grate and Or Zone 3 Weir 3.42 10.00 0.00	Row 10 (optional)  Not Selected N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A N/A	Row 11 (optional) ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( bottom at Stage = ( ir (and No Outlet Pip	D ft) Vo D ft) Vertic	ertical Orifice Area =	Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	ers for Vertical Orific Not Selected N/A N/A	ft ²
2) Zone 2 Circular 2.98 3.42 0.38 0 20ne 3 Weir 3.42 10.00 0.00	Not Selected N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( bottom at Stage = ( ir (and No Outlet Pip	D ft) Vo D ft) Vertic	ertical Orifice Area =	Calculated Paramet Zone 2 Circular 0.00 0.02 Calculated Paramet	ers for Vertical Orific Not Selected N/A N/A	ft ²
2) Zone 2 Circular 2.98 3.42 0.38 0 20ne 3 Weir 3.42 10.00 0.00	Not Selected N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	ft (relative to basin ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( bottom at Stage = ( ir (and No Outlet Pip	D ft) Vo D ft) Vertic	ertical Orifice Area =	Calculated Paramet	ers for Vertical Orific Not Selected N/A N/A	ft ²
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Zone 2 Circular 2.98 3.42 0.38 00000 Grate and Or Zone 3 Weir 3.42 10.00 0.00	N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( ir (and No Outlet Pip	D ft) Vertic		Zone 2 Circular 0.00 0.02 Calculated Paramet	Not Selected N/A N/A	ft ²
Zone 2 Circular 2.98 3.42 0.38 00000 Grate and Or Zone 3 Weir 3.42 10.00 0.00	N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( ir (and No Outlet Pip	D ft) Vertic		Zone 2 Circular 0.00 0.02 Calculated Paramet	Not Selected N/A N/A	ft ²
Zone 2 Circular 2.98 3.42 0.38 00000 Grate and Or Zone 3 Weir 3.42 10.00 0.00	N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( ir (and No Outlet Pip	D ft) Vertic		Zone 2 Circular 0.00 0.02 Calculated Paramet	Not Selected N/A N/A	ft ²
2.98 3.42 0.38 00000 Grate and Or Zone 3 Weir 3.42 10.00 0.00	N/A N/A N/A Utlet Pipe OR Rectang Not Selected N/A N/A	ft (relative to basin inches gular/Trapezoidal We ft (relative to basin b feet	bottom at Stage = ( ir (and No Outlet Pip	D ft) Vertic		0.00 0.02 Calculated Paramet	N/A N/A	
0.38 oped Grate and Or Zone 3 Weir (3.42) 10.00 0.00	N/A utlet Pipe OR Rectang Not Selected N/A N/A	gular/Trapezoidal We ft (relative to basin b feet	ir (and No Outlet Pip	be)	al Orifice Centroid =	Calculated Paramet		feet
oped Grate and Or Zone 3 Weir (3.42) 10.00 0.00	utlet Pipe OR Rectang Not Selected N/A N/A	gular/Trapezoidal We ft (relative to basin b feet					ers for Overflow We	
Zone 3 Weir 3.42 10.00 0.00	Not Selected N/A N/A	ft (relative to basin b					ers for Overflow We	
Zone 3 Weir 3.42 10.00 0.00	Not Selected N/A N/A	ft (relative to basin b					iers for Overflow We	
Zone 3 Weir 3.42 10.00 0.00	Not Selected N/A N/A	ft (relative to basin b						-
3.42 10.00 0.00	N/A N/A	feet	ottom at Stage = 0 ft					<u>r</u> 1
10.00 0.00	N/A	feet	ottom at stage – o n		te Upper Edge, H _t =	Zone 3 Weir 3.42	Not Selected N/A	feet
0.00				•	Weir Slope Length =	5.00	N/A	feet
		H:V		Grate Open Area / 1		4.92	N/A	1001
5.00	N/A	feet		Overflow Grate Ope		34.80	N/A	ft ²
Type C Grate	N/A			Overflow Grate Op		34.80	N/A	ft ²
0%	N/A	%						-
		angular Orifice)		<u>(</u>	Calculated Parameter	-		te T
		6 ( //						ft ²
			isin bottom at Stage =					
	IN/A		Half-Ce					feet radians
30.00		incres		shirtar virigie or restr		3.14	10/11	
apezoidal)						Calculated Paramet	ers for Spillway	
4.33	ft (relative to basin	n bottom at Stage = 0	D ft)	Spillway	Design Flow Depth=	0.49	feet	
75.00	feet			0		5.82	feet	
4.00	H:V					2.25	acres	
1.00	feet			Basin Volume at	Top of Freeboard =	5.19	acre-ft	
The user can over		P hydrographs and ru	inoff volumes by ent	tering new values in	the Inflow Hydrogra	phs table (Columns	W through AF).	
WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500
								3. 11.
N/A	N/A	0.755	1.188	2.116	3.929	5.225	7.358	11.
N/A	N/A	0.9	2.0	11.4	32.5	46.1	66.0	10
		0.01	0.03	0.15	0.42	0.50	0.85	1.3
N/A N/A	N/A N/A	7.9	12.1	22.4	44.2	58.5	78.8	11
0.3	0.3	0.3	1.4	10.3	29.3	43.1	60.1	98
N/A Diata	N/A Overflow Weir 1	N/A	0.7 Overflow Mair 1	0.9 Overflew Weir 1	0.9 Overflow Weir 1	0.9 Overflew Weir 1	0.9 Outlot Dista 1	1 Spil
								Spil 1
N/A N/A	N/A N/A	N/A	0.0 N/A	0.3 N/A	0.8 N/A	N/A	N/A	N/
38	53	44	56	54	49	47	42	3
								5 4.
0.74	1.05	0.80	3.47	3.64	3.87	4.00	4.22 1.55	4.
0.621	1.014	0.690	1.067	1.261	1.542	1.737	2.051	2.7
Highlighte	ed depths do	o not match						
	dia and a la aver							
with eleva	ations snowi	n on bond						
with eleva								
	ion drawings							
7	Vicular Orifice, Res           Zone 3 Restricto           0.40           36.00           36.00           36.00           0.40           36.00           0.40           36.00           0.40           36.00           0.00           4.00           1.00           1.00           WOCV           N/A	Visual Contraction         Visual Contraction           Cone 3 Restrictor         Not Selected           0.40         N/A           36.00         N/A           9         General Contraction Content Contraction Content	rcular Orifice, Restrictor Plate, or Rectangular Orifice)           Zone 3 Restrictor         Not Selected           0.40         N/A         ft (distance below be           36.00         N/A         inches           36.00         N/A         inches           36.00         N/A         inches           36.00         inches         inches           36.00         inches         inches           9         4.33         ft (relative to basin bottom at Stage = 0           75.00         feet         4.00           4.00         H:V         1.00           1.00         feet         2 Year           N/A         N/A         1.19           0.619         1.007         0.755           N/A         N/A         0.9           N/A         N/A         0.9           N/A         N/A         0.9           N/A         N/A         0.9           N/A         N/A         7.9           0.3         0.3         0.3           N/A         N/A         N/A           N/A         N/A         N/A           N/A         N/A         N/A           N/A <td>rcular Orifice, Restrictor Plate, or Rectangular Orifice)Zone 3 RestrictorNot Selected0.40N/Aft (distance below basin bottom at Stage - inches36.00N/Ainches36.00inchesHalf-Copezoidal)ft (relative to basin bottom at Stage = 0 ft)4.33ft (relative to basin bottom at Stage = 0 ft)75.00feet4.00H:V1.00feetWOCVEURV2 YearVAN/A1.191.500.6191.0070.7551.188N/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/A</td> <td>cular Orifice, Restrictor Plate, or Rectangular Orifice)         Construction           Zone 3 Restrictor         Not Selected         ft (distance below basin bottom at Stage = 0 ft)         Construction           36.00         N/A         inches         Outle         Outle           36.00         N/A         inches         Half-Central Angle of Restri           pezoidal)         feet         Stage at         Stage at           1.00         feet         Basin Nolume at         Basin Volumes at           The user can override the default CUHP hydrographs and runoff volumes by entering new values in         N/A         N/A           N/A         N/A         1.19         1.50         1.75           0.619         1.007         0.755         1.188         2.116           N/A         N/A         0.9         2.0         11.4</td> <td>cular Orifice, Restrictor Plate, or Rectangular Orifice)         Calculated Paramete           Zone 3. Restrictor         Not Selected         0.40         N/A         ft (distance below basin bottom at Stage = 0 ft)         Outlet Orifice Area =           36.00         N/A         inches         Outlet Orifice Centroid =           36.00         inches         Outlet Orifice Centroid =           action         inches         Outlet Orifice Centroid =           action         inches         Basin Area at Top of Freeboard =           pezoidal)         ft (relative to basin bottom at Stage = 0 ft)         Spillway Design Flow Depth =           75.00         feet         Stage at Top of Freeboard =           4.00         H:V         Basin Area at Top of Freeboard =           1.00         feet         Basin Volume at Top of Freeboard =           7he user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrograph         N/A           N/A         N/A         0.755         1.188         2.116         3.929           N/A         N/A         0.9         2.0         11.4         32.5           N/A         N/A         0.01         0.03         0.15         0.42           N/A         N/A         0.7         0.9</td> <td>cular Orifice, Restrictor Plate, or Rectangular Orifice)Calculated Parameters for Outlet Pipe w/ Zone 3 RestrictorZone 3 RestrictorNot Selected notesTCalculated Parameters for Outlet Pipe w/ Dutlet Orifice Area = 0utlet Orifice Centroid =Zone 3 Restrictor36.00N/A inchesinchesDutlet Orifice Centroid = 1.50T.0736.00inchesHalf-Central Angle of Restrictor Plate on Pipe =3.14ezcidal)Calculated ParameterCalculated Parameter4.33ft (relative to basin bottom at Stage = 0 ft)Spillway Design Flow Depth= Stage at Top of Freeboard = Basin Area at Top of Freeboard = 5.191.00feetStage at Top of Freeboard = 5.195.19The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns WOCVEURV2 Year5 YearWOCVEURV2 Year5 Year10.752.002.25N/AN/A1.191.501.752.002.25N/AN/A0.751.1882.1163.9295.225N/AN/A0.70.90.90.9N/AN/A0.10.030.150.420.59N/AN/AN/A0.70.90.90.9N/AN/AN/A0.70.90.90.9N/AN/AN/A0.00.30.81.2N/AN/AN/A0.00.30.81.2N/A</td> <td>Calculated Parameters for Outlet Pipe w/ Flow Restriction Pla           Calculated Parameters for Outlet Pipe w/ Flow Restriction Pla           Zone 3 Restrictor         Not Selected           0.40         N/A         ft (distance below basin bottom at Stage = 0 ft)         Outlet Orifice Area         Zone 3 Restrictor         Not Selected           36.00         N/A         Inches         Outlet Orifice Area         Zone 3 Restrictor         NA           36.00         Inches         Half-Central Angle of Restrictor Plate on Pipe         Zane 3 Restrictor         NA           36.00         Inches         Half-Central Angle of Restrictor Plate on Pipe         Zane 3 Restrictor         NA           4.33         ft (relative to basin bottom at Stage = 0 ft)         Spillway Design Flow Depart=         0.49         feet           75.00         feet         Stage at Top of Freeboart =         5.82         feet           4.00         H·V         Basin Area at Top of Freeboart =         5.19         acres           1.00         feet         Stage at Top of Freeboart =         5.19         acres           1.00         feet         Stage at Top of Freeboart =         5.19         acres           N/A         N/A         1.188         2.116         3.929</td>	rcular Orifice, Restrictor Plate, or Rectangular Orifice)Zone 3 RestrictorNot Selected0.40N/Aft (distance below basin bottom at Stage - inches36.00N/Ainches36.00inchesHalf-Copezoidal)ft (relative to basin bottom at Stage = 0 ft)4.33ft (relative to basin bottom at Stage = 0 ft)75.00feet4.00H:V1.00feetWOCVEURV2 YearVAN/A1.191.500.6191.0070.7551.188N/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/AN/A	cular Orifice, Restrictor Plate, or Rectangular Orifice)         Construction           Zone 3 Restrictor         Not Selected         ft (distance below basin bottom at Stage = 0 ft)         Construction           36.00         N/A         inches         Outle         Outle           36.00         N/A         inches         Half-Central Angle of Restri           pezoidal)         feet         Stage at         Stage at           1.00         feet         Basin Nolume at         Basin Volumes at           The user can override the default CUHP hydrographs and runoff volumes by entering new values in         N/A         N/A           N/A         N/A         1.19         1.50         1.75           0.619         1.007         0.755         1.188         2.116           N/A         N/A         0.9         2.0         11.4	cular Orifice, Restrictor Plate, or Rectangular Orifice)         Calculated Paramete           Zone 3. Restrictor         Not Selected         0.40         N/A         ft (distance below basin bottom at Stage = 0 ft)         Outlet Orifice Area =           36.00         N/A         inches         Outlet Orifice Centroid =           36.00         inches         Outlet Orifice Centroid =           action         inches         Outlet Orifice Centroid =           action         inches         Basin Area at Top of Freeboard =           pezoidal)         ft (relative to basin bottom at Stage = 0 ft)         Spillway Design Flow Depth =           75.00         feet         Stage at Top of Freeboard =           4.00         H:V         Basin Area at Top of Freeboard =           1.00         feet         Basin Volume at Top of Freeboard =           7he user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrograph         N/A           N/A         N/A         0.755         1.188         2.116         3.929           N/A         N/A         0.9         2.0         11.4         32.5           N/A         N/A         0.01         0.03         0.15         0.42           N/A         N/A         0.7         0.9	cular Orifice, Restrictor Plate, or Rectangular Orifice)Calculated Parameters for Outlet Pipe w/ Zone 3 RestrictorZone 3 RestrictorNot Selected notesTCalculated Parameters for Outlet Pipe w/ Dutlet Orifice Area = 0utlet Orifice Centroid =Zone 3 Restrictor36.00N/A inchesinchesDutlet Orifice Centroid = 1.50T.0736.00inchesHalf-Central Angle of Restrictor Plate on Pipe =3.14ezcidal)Calculated ParameterCalculated Parameter4.33ft (relative to basin bottom at Stage = 0 ft)Spillway Design Flow Depth= Stage at Top of Freeboard = Basin Area at Top of Freeboard = 5.191.00feetStage at Top of Freeboard = 5.195.19The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns WOCVEURV2 Year5 YearWOCVEURV2 Year5 Year10.752.002.25N/AN/A1.191.501.752.002.25N/AN/A0.751.1882.1163.9295.225N/AN/A0.70.90.90.9N/AN/A0.10.030.150.420.59N/AN/AN/A0.70.90.90.9N/AN/AN/A0.70.90.90.9N/AN/AN/A0.00.30.81.2N/AN/AN/A0.00.30.81.2N/A	Calculated Parameters for Outlet Pipe w/ Flow Restriction Pla           Calculated Parameters for Outlet Pipe w/ Flow Restriction Pla           Zone 3 Restrictor         Not Selected           0.40         N/A         ft (distance below basin bottom at Stage = 0 ft)         Outlet Orifice Area         Zone 3 Restrictor         Not Selected           36.00         N/A         Inches         Outlet Orifice Area         Zone 3 Restrictor         NA           36.00         Inches         Half-Central Angle of Restrictor Plate on Pipe         Zane 3 Restrictor         NA           36.00         Inches         Half-Central Angle of Restrictor Plate on Pipe         Zane 3 Restrictor         NA           4.33         ft (relative to basin bottom at Stage = 0 ft)         Spillway Design Flow Depart=         0.49         feet           75.00         feet         Stage at Top of Freeboart =         5.82         feet           4.00         H·V         Basin Area at Top of Freeboart =         5.19         acres           1.00         feet         Stage at Top of Freeboart =         5.19         acres           1.00         feet         Stage at Top of Freeboart =         5.19         acres           N/A         N/A         1.188         2.116         3.929



Outflow Hydrograph Workbook Filename:

	SOURCE	verride the calcul CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00 min	0:05:00		0.00						0.00	
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.30	0.38	0.00	0.02	0.00	0.07
	0:20:00	0.00	0.00	0.78	1.07	1.80	0.23	0.96	1.01	1.78
	0:25:00	0.00	0.00	3.62	5.77	9.24	3.35	4.42	5.02	8.89
	0:30:00	0.00	0.00	6.66	10.45	18.82	18.82	26.04	32.56	52.15
	0:35:00	0.00	0.00	7.84	12.08	22.42	34.80	46.75	61.06	93.07
	0:40:00	0.00	0.00	7.93	12.12	22.20	42.88	56.63	74.53	111.26
	0:45:00	0.00	0.00	7.48	11.45	20.90	44.25	58.54	78.84	117.15
	0:50:00	0.00	0.00	6.83	10.62	19.13	42.61	56.69	77.56	115.33
	1:00:00	0.00	0.00	6.26 E 74	9.86 9.14	17.62	39.50	52.70 48.27	73.29 68.97	109.78 104.24
	1:05:00	0.00	0.00	5.76 5.28	9.14	16.34 15.15	36.17 33.11	48.27	65.06	99.07
	1:10:00	0.00	0.00	4.89	7.99	14.25	30.04	39.97	59.68	91.26
	1:15:00	0.00	0.00	4.55	7.50	13.58	27.49	36.59	54.41	83.33
	1:20:00	0.00	0.00	4.22	6.95	12.74	25.14	33.49	49.45	75.69
	1:25:00	0.00	0.00	3.89	6.38	11.68	22.87	30.48	44.61	68.20
	1:30:00	0.00	0.00	3.56	5.81	10.53	20.61	27.48	40.05	61.16
	1:35:00	0.00	0.00	3.24	5.25	9.39	18.42	24.52	35.69	54.45
	1:40:00	0.00	0.00	2.93	4.70	8.31	16.26	21.61	31.44	47.94
	1:45:00	0.00	0.00	2.69	4.26	7.48	14.20	18.83	27.41	41.84
	1:50:00	0.00	0.00	2.54	3.96	6.91	12.64	16.78	24.37	37.36
	1:55:00 2:00:00	0.00	0.00	2.39	3.70	6.44	11.50	15.25	22.06	33.85
	2:00:00	0.00	0.00	2.23	3.45	5.96	10.59	13.99	20.09	30.81
	2:10:00	0.00	0.00	2.04	3.15 2.84	5.44	9.68 8.78	12.77 11.58	18.25 16.49	27.94 25.21
	2:15:00	0.00	0.00	1.65	2.64	4.90	7.91	10.44	14.82	23.21
	2:20:00	0.00	0.00	1.46	2.34	3.86	7.07	9.32	13.24	20.17
	2:25:00	0.00	0.00	1.28	1.96	3.37	6.25	8.23	11.74	17.88
	2:30:00	0.00	0.00	1.11	1.70	2.90	5.45	7.17	10.28	15.64
	2:35:00	0.00	0.00	0.94	1.44	2.45	4.66	6.12	8.83	13.43
	2:40:00	0.00	0.00	0.78	1.19	2.02	3.88	5.09	7.40	11.24
	2:45:00	0.00	0.00	0.62	0.95	1.60	3.12	4.07	5.97	9.05
	2:50:00	0.00	0.00	0.47	0.72	1.19	2.36	3.06	4.55	6.89
	2:55:00	0.00	0.00	0.33	0.50	0.82	1.62	2.08	3.16	4.80
	3:00:00	0.00	0.00	0.25	0.39	0.60	0.98	1.26	2.00	3.10
	3:05:00 3:10:00	0.00	0.00	0.20	0.32	0.50	0.63	0.81	1.31	2.10
	3:10:00	0.00	0.00	0.17	0.26	0.41	0.43	0.56	0.89	1.46
	3:20:00	0.00	0.00	0.13	0.22	0.34	0.32	0.41	0.81	0.67
	3:25:00	0.00	0.00	0.12	0.15	0.20	0.24	0.23	0.28	0.44
	3:30:00	0.00	0.00	0.09	0.12	0.17	0.15	0.18	0.18	0.28
	3:35:00	0.00	0.00	0.07	0.09	0.13	0.11	0.14	0.12	0.19
	3:40:00	0.00	0.00	0.06	0.07	0.10	0.09	0.10	0.09	0.14
	3:45:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.07	0.11
	3:50:00	0.00	0.00	0.04	0.05	0.06	0.05	0.06	0.06	0.09
	3:55:00	0.00	0.00	0.03	0.03	0.04	0.04	0.05	0.04	0.07
	4:00:00	0.00	0.00	0.02	0.03	0.03	0.03	0.03	0.03	0.05
	4:05:00	0.00	0.00	0.01 0.01	0.02	0.02	0.02	0.02	0.02	0.04
	4:10:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

he user should graphically co	ompare the summa	ary S-A-V-D table	e to the full S-A-	V-D table in the	chart to confirm		y transition points.
Stage - Storage Description	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft ² ]	[acres]	[ft ³ ]	[ac-ft]	[cfs]	
	0.00	32	0.001	0	0.000	0.00	For best results, include the
	0.50	271	0.006	41	0.001	0.05	stages of all grade slope changes (e.g. ISV and Floor)
	1.00	1,955	0.045	426	0.010	0.07	from the S-A-V table on
	1.50	5,650 11,435	0.130	2,328 6,254	0.053	0.13	Sheet 'Basin'.
	2.00	21,275	0.488	14,432	0.331	0.18	Also include the inverts of all
WQCV	2.30	32,310	0.742	27,030	0.621	0.22	outlets (e.g. vertical orifice,
	3.00	32,915	0.756	27,682	0.635	0.27	overflow grate, and spillway,
EURV	3.42	45,628	1.047	44,176	1.014	0.31	where applicable).
	3.50	48,049	1.103	47,923	1.100	2.50	
	4.00	62,374	1.432	75,662	1.737	43.04	
100-YR	4.22	67,986	1.561	90,002	2.066	60.12	
	4.50	75,128 86,032	1.725 1.975	110,038 150,633	2.526 3.458	78.64 194.14	
	5.00	00,032	1.7/J	130,033	3.430	174.14	
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	_						
				1	1		
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		I	I	I	I	1	I

## POND D FOREBAY VOLUME REQUIREMENTS

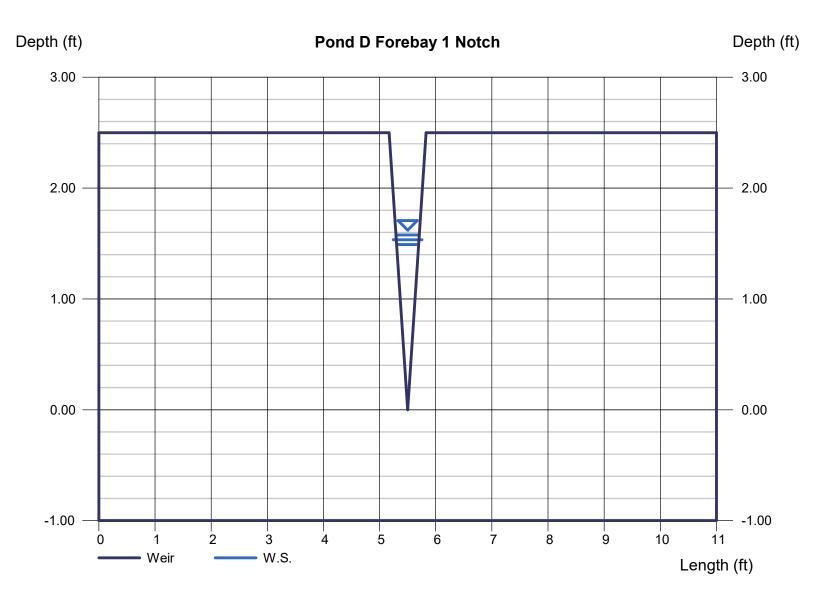
Equation 3-1	+0.781/)				
Proposed Forebay	0.080158				
Future Forebay	I=.147	WQC	V=	0.091836	
Equation 3-3	V=(WQCV	//12)A			
Proposed Forebay	A= 40.72 Acre	S	V=	0.272	
Future Forebay	0.260				
FOI	.03(V)				
VOLUME REQUIRED FOR PRO		0.008 AC-FT	355 CF		
VOLUME REQUIRED FOR FUTURE FOREBAY =				0.008 AC-FT	339 CF
VOLUME PROVIDED FOR PRO	0.015 AC-FT	642 CF			
Q ₁₀₀ Discharges Q ₁₀₀ Proposed Forebay 1=	2% OF Q ₁₀₀ .02*51.7 CFS= 1.0	03 CFS			

 $Q_{100}$  Future Forebay= .02*37.3 CFS= 0.75 CFS

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### Pond D Forebay 1 Notch

V-Notch Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 1.58
Angle (Deg)	= 15	Q (cfs)	= 1.030
Total Depth (ft)	= 2.50	Area (sqft)	= 0.33
		Velocity (ft/s)	= 3.15
Calculations		Top Width (ft)	= 0.42
Weir Coeff. Cw	= 0.33		
Compute by:	Known Q		
Known Q (cfs)	= 1.03		

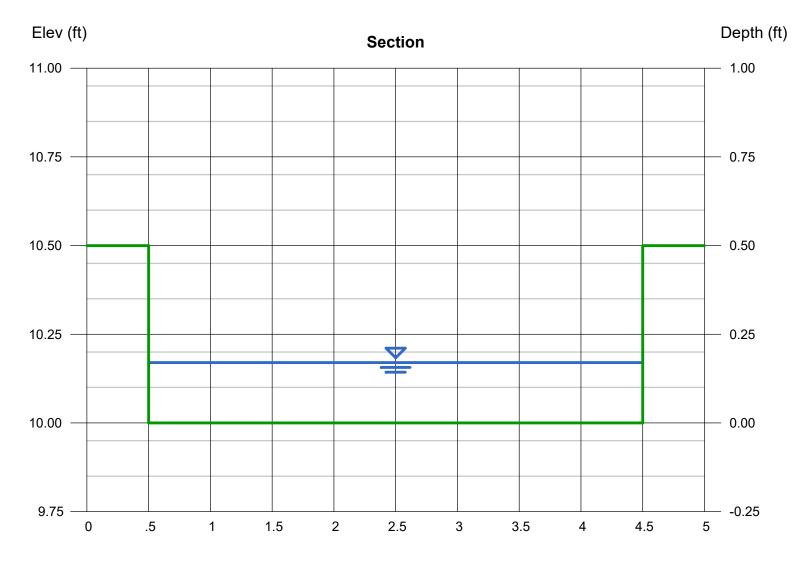


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

### **Pond D Trickle Channel**

Rectangular		Highlighted	
Bottom Width (ft)	= 4.00	Depth (ft) = 0	0.17
Total Depth (ft)	= 0.50	Q (cfs) = 1	1.520
		Area (sqft) = (	0.68
Invert Elev (ft)	= 10.00	Velocity (ft/s) = $2$	2.24
Slope (%)	= 0.50	Wetted Perim (ft) = 4	4.34
N-Value	= 0.013	Crit Depth, Yc (ft) = 0	0.17
		Top Width (ft) = $2$	4.00
Calculations		EGL(ft) = 0	0.25
Compute by:	Known Q		
Known Q (cfs)	= 1.52		



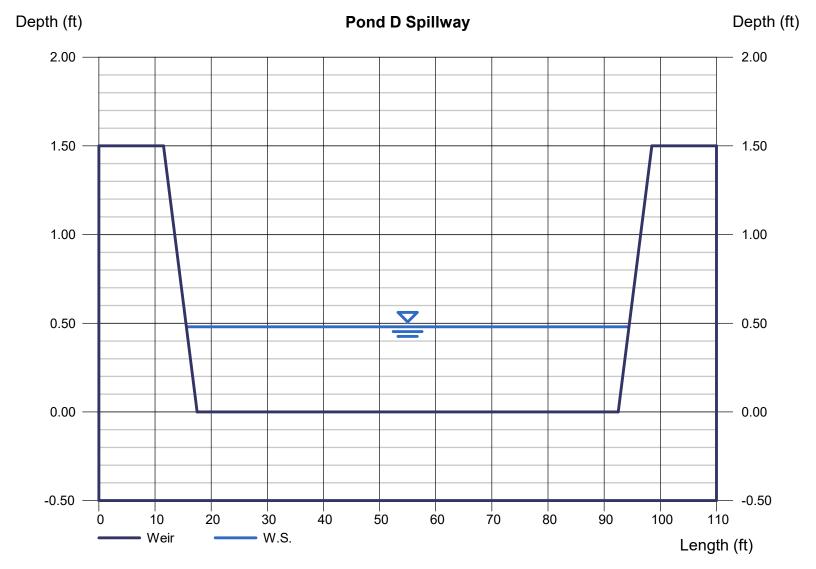
Reach (ft)

## Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### **Pond D Spillway**

Trapezoidal Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 0.48
Bottom Length (ft)	= 75.00	Q (cfs)	= 78.80
Total Depth (ft)	= 1.50	Area (sqft)	= 36.92
Side Slope (z:1)	= 4.00	Velocity (ft/s)	= 2.13
		Top Width (ft)	= 78.84
Calculations			
Weir Coeff. Cw	= 3.10		
Compute by:	Known Q		
Known Q (cfs)	= 78.80		



#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project: Saddlehorn Filing 3
Basin ID: Pond E
ZONE 2 ZONE 2 ZONE 1

____ Depth Increment = ft ORIFICE ZONE 1 AND 2 ORIFICE Example Zone Configuration (Retention Pond)

#### Watershed Information

PERMA

Selected BMP Type =	EDB	
Watershed Area =	18.37	acres
Watershed Length =	1,810	ft
Watershed Length to Centroid =	803	ft
Watershed Slope =	0.012	ft/ft
Watershed Imperviousness =	8.10%	percent
Percentage Hydrologic Soil Group A =	83.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	17.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded oblorddo orban nyare	graphinoceae	
Water Quality Capture Volume (WQCV) =	0.086	acre-feet
Excess Urban Runoff Volume (EURV) =	0.106	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.065	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.106	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.204	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.592	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.859	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.292	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	2.174	acre-feet
Approximate 2-yr Detention Volume =	0.067	acre-feet
Approximate 5-yr Detention Volume =	0.113	acre-feet
Approximate 10-yr Detention Volume =	0.153	acre-feet
Approximate 25-yr Detention Volume =	0.199	acre-feet
Approximate 50-yr Detention Volume =	0.254	acre-feet
Approximate 100-yr Detention Volume =	0.419	acre-feet

	'v
Define Zones and Basin Geometr	

0.086	acre-feet
0.021	acre-feet
0.313	acre-feet
0.419	acre-feet
user	ft ³
user	ft
user	ft
user	ft
user	ft/ft
user	H:V
user	
	0.021 0.313 0.419 user user user user user user

Initial Surcharge Area (A _{ISV} ) =	user	ft ²
Surcharge Volume Length ( $L_{ISV}$ ) =	user	ft
Surcharge Volume Width ( $W_{ISV}$ ) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR})$ =	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =		ft
Area of Basin Floor $(A_{FLOOR}) =$		ft ²
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft ³
Depth of Main Basin (H _{MAIN} ) =	user	ft
Length of Main Basin ( $L_{MAIN}$ ) =	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin (A _{MAIN} ) =	user	ft ²
Volume of Main Basin (V _{MAIN} ) =	user	ft ³

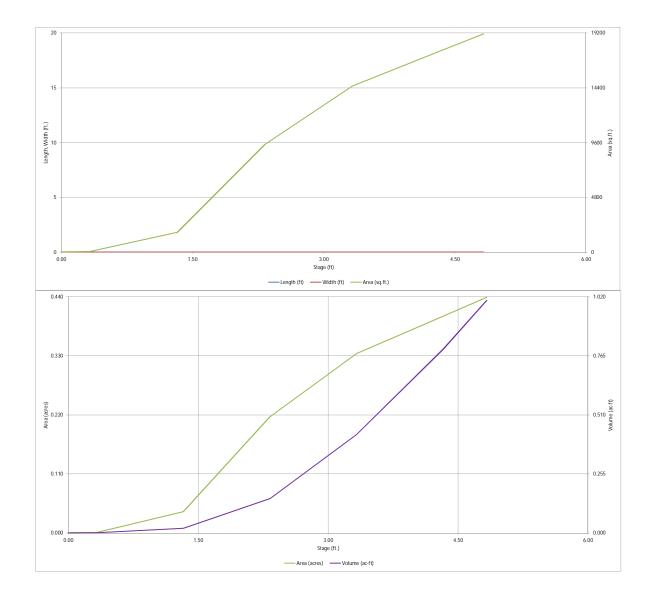
Calculated Total Basin Volume (Vtotal) = user acre-feet

AR E		Depth Increment =		ft Optional	-	-	1	Optional		1	-
ntion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft ² )	(acre)	(ft 3)	(ac-ft)
	6720.67			0.00	-			32	0.001	4.4	0.000
		6721		0.33				50	0.001	14	0.000
		6722		1.33				1,723	0.040	900	0.021
		6723		2.33				9,446 14,566	0.217	6,484 18,490	0.149 0.424
		6724 6725		3.33 4.33				14,500	0.334	34,573	0.424
		6725.5		4.83				19,121	0.439	43,754	1.004
								,			
Optional Use	r Overrides acre-feet										
	acre-feet										
1.19	inches										
1.50	inches										
1.75	inches										
2.00	inches										
2.25	inches										
2.52	inches										
	inches										
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#### MHFD-Detention_v4 04_Pond E.xlsm, Basin

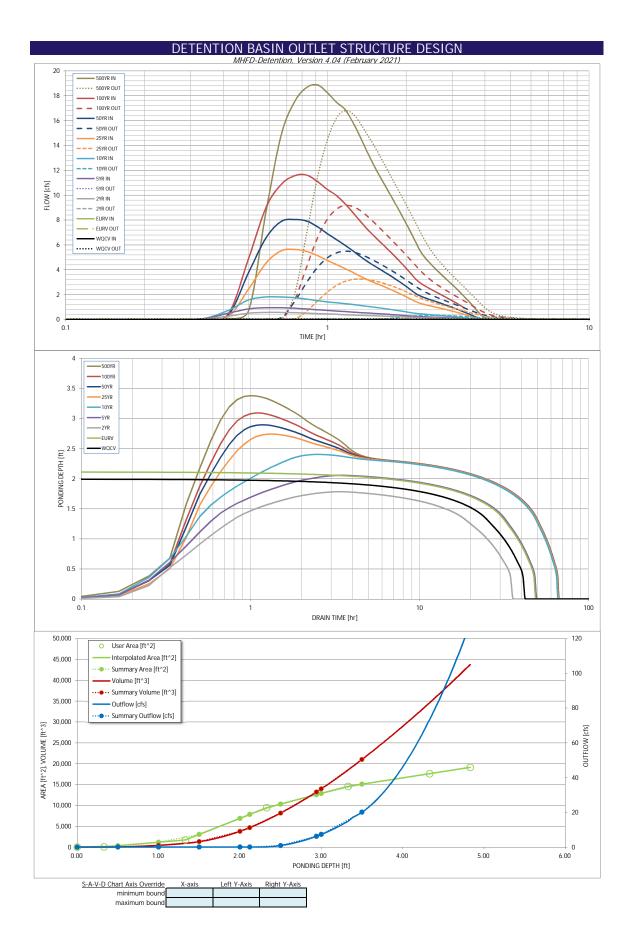
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN									
Decised	Saddlehorn Filing		FD-Detention, Vers	tion 4.04 (Februar	ry 2021)				
Basin ID:		3							
ZONE 3 ZONE 2	T OHA E			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
VOLUME EURY WOCY			Zone 1 (WQCV)	2.00	0.086	Orifice Plate	1		
			2				-		
ZONE 1 AND 2	0RIFICE		Zone 2 (EURV)	2.12	0.021	Orifice Plate	-		
PERMANENT ORIFICES	Configuration (Re	tention Dand)	Zone 3 (100-year)	3.32	0.313	Weir&Pipe (Restrict)			
-				Total (all zones)	0.419				
User Input: Orifice at Underdrain Outlet (typical								ters for Underdrain	
Underdrain Orifice Invert Depth = $N/A$ ft (distance below the filtration media surface) Underdrain Orifice Area = $N/A$ ft ²									
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orific							Calculated Parame		
Invert of Lowest Orifice =	0.00		n bottom at Stage =			ce Area per Row =	2.153E-03	ft ²	
Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing =	2.12 N/A	inches	n bottom at Stage =	01()		ptical Half-Width = cal Slot Centroid =	N/A N/A	feet feet	
Orifice Plate: Orifice Area per Row =	0.31	sq. inches (diamet	for = E/2 inch)			lliptical Slot Area =	N/A N/A	ft ²	
Office Plate. Office Area per Row =	0.31	sq. inches (diamer	ler = 5/8 mcm		L	iliptical Slot Alea =	IN/A	n	
User Input: Stage and Total Area of Each Orific	a Row (numbered fr	om lowest to high	act)						
oser input. Stage and rotal fired of Each office	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.60	1.20	non r (optional)	non o (optional)	non o (optional)	(optional)	now o (optional)	
Orifice Area (sq. inches)		0.31	0.31						
Chine Area (aq. IIIcites)	0.01	0.01	0.01						1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
User Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	ters for Vertical Ori	fice
	Not Selected	Not Selected	]				Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ver	tical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid =				N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
			_						
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoida	I Weir (and No Out	let Pipe)		Calculated Parame	ters for Overflow W	<u>eir</u>
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	2.30	N/A	ft (relative to basin b	oottom at Stage = 0 f		e Upper Edge, H _t =	3.55	N/A	feet
Overflow Weir Front Edge Length =	5.00	N/A	feet			eir Slope Length =	5.15	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V		rate Open Area / 10		10.15	N/A	
Horiz. Length of Weir Sides =	5.00	N/A	feet		verflow Grate Open		17.94	N/A	ft ²
Overflow Grate Type =	Type C Grate	N/A	-	(	Overflow Grate Ope	n Area w/ Debris =	17.94	N/A	ft ²
Debris Clogging % =	0%	N/A	%						
User Input: Outlet Pipe w/ Flow Restriction Plate	· · · · · · · · · · · · · · · · · · ·		Rectangular Orifice)		<u>Ca</u>	Iculated Parameter	· · · ·	Flow Restriction Pl	<u>ate</u>
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected	2
Depth to Invert of Outlet Pipe =	1.15	N/A	ft (distance below ba	isin bottom at Stage	,	utlet Orifice Area =	1.77	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches			Orifice Centroid =	0.75	N/A	feet
Restrictor Plate Height Above Pipe Invert =	18.00	-	inches	Half-Cen	tral Angle of Restric	tor Plate on Pipe =	3.14	N/A	radians
User Input: Emergency Spillway (Dectorgular or	Tranazoidal)						Calculated Parame	tors for Spillwov	
User Input: Emergency Spillway (Rectangular or Spillway Invert Stage-	3.33	ft (relative to basis	n bottom at Stage =	0 ft)	Snillway D	esian Flow Denth-	0.38	feet	
Spillway Invert Stage= Spillway Crest Length =	15.00	feet	socioni al staye =	0117		esign Flow Depth= Fop of Freeboard =	4.71	feet	
Spillway End Slopes =	4.00	H:V				op of Freeboard =	0.43	acres	
Freeboard above Max Water Surface =	1.00	feet				op of Freeboard =	0.95	acre-ft	
Trosseard above max water suitable =	1.00				Sashi volume di l		0.75	1-210	
Routed Hydrograph Results			HP hydrographs and						
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	N/A 0.086	N/A 0.106	1.19 0.065	1.50 0.106	1.75 0.204	2.00 0.592	2.25 0.859	2.52	3.14 2.174
Inflow Hydrograph Volume (acre-it) =	0.088 N/A	0.108 N/A	0.065	0.106	0.204	0.592	0.859	1.292	2.174
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.005	0.2	0.9	4.6	7.0	10.5	17.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.05	0.25	0.38	0.57	0.96
Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	N/A 0.0	N/A 0.0	0.6	1.0	1.8 0.3	5.6	8.0 5.5	11.6 9.2	18.9 16.8
Ratio Peak Outflow to Predevelopment Q =	0.0 N/A	0.0 N/A	0.0 N/A	0.0	0.3	3.3 0.7	0.8	9.2	0.9
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.2	0.3	0.5	0.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	44	32	44	58	51	47	42	32
Time to Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ft) =	40	46 2.12	34 1.78	47 2.06	62 2.40	59 2.74	57 2.90	54 3.09	49 3.38
Area at Maximum Ponding Depth (acres) =	0.16	0.18	0.12	0.17	0.23	0.27	0.28	0.31	0.34
Maximum Volume Stored (acre-ft)	0.087	0.107	0.056	0.095	0.164	0.248	0.289	0.348	0.438
· · · · · · · · · · · · · · · · · · ·									

# Fix drain time to be 40 hours



## DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

#### Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	The user can o	verride the calcu	lated inflow hyd	lrographs from t	this workbook w	ith inflow hydro	graphs develope	ed in a separate p	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	0:20:00	0.00	0.00	0.04	0.06	0.07	0.04	0.05	0.06	0.07
	0:25:00	0.00	0.00	0.27	0.50	0.72	0.23	0.34	0.41	0.72
	0:30:00	0.00	0.00	0.51	0.86	1.57	2.46	3.79	4.91	8.73
	0:35:00	0.00	0.00	0.57	0.95	1.81	4.55	6.58	9.03	14.87
	0:40:00	0.00	0.00	0.57	0.95	1.81	5.53	7.89	10.87	17.53
	0:45:00	0.00	0.00	0.55	0.91	1.75	5.64	8.05	11.57	18.66
	0:55:00	0.00	0.00	0.52	0.85	1.64 1.52	5.48	7.92	11.61 11.09	18.87
	1:00:00	0.00	0.00	0.48	0.78	1.52	5.14 4.75	7.46 6.90	10.46	18.24 17.47
	1:05:00	0.00	0.00	0.43	0.73	1.42	4.73	6.43	9.97	16.90
	1:10:00	0.00	0.00	0.39	0.64	1.28	4.11	5.98	9.32	15.88
	1:15:00	0.00	0.00	0.37	0.60	1.21	3.80	5.54	8.62	14.71
	1:20:00	0.00	0.00	0.34	0.56	1.14	3.49	5.08	7.92	13.52
	1:25:00	0.00	0.00	0.32	0.53	1.06	3.22	4.69	7.30	12.46
	1:30:00	0.00	0.00	0.31	0.50	1.00	2.99	4.36	6.76	11.55
	1:35:00	0.00	0.00	0.29	0.47	0.93	2.79	4.06	6.28	10.72
	1:40:00	0.00	0.00	0.27	0.44	0.87	2.60	3.77	5.83	9.94
	1:45:00	0.00	0.00	0.26	0.41	0.81	2.41	3.49	5.40	9.19
	1:50:00 1:55:00	0.00	0.00	0.24	0.38	0.74	2.22	3.22	4.97	8.45
	2:00:00	0.00	0.00	0.22	0.35	0.68	2.03	2.94	4.54	7.72
	2:05:00	0.00	0.00	0.20	0.28	0.55	1.65	2.38	3.70	6.31
	2:10:00	0.00	0.00	0.16	0.26	0.50	1.46	2.11	3.29	5.61
	2:15:00	0.00	0.00	0.15	0.24	0.47	1.32	1.92	2.99	5.12
	2:20:00	0.00	0.00	0.14	0.22	0.44	1.23	1.78	2.77	4.73
	2:25:00	0.00	0.00	0.13	0.21	0.41	1.15	1.67	2.57	4.40
	2:30:00	0.00	0.00	0.12	0.20	0.38	1.08	1.56	2.40	4.09
	2:35:00	0.00	0.00	0.12	0.18	0.35	1.01	1.46	2.24	3.81
	2:40:00	0.00	0.00	0.11	0.17	0.33	0.94	1.36	2.09	3.54
	2:45:00	0.00	0.00	0.10	0.16	0.30	0.87	1.27	1.94	3.28
	2:50:00	0.00	0.00	0.09	0.14	0.28	0.81	1.17	1.80	3.04
	2:55:00 3:00:00	0.00	0.00	0.08	0.13	0.25	0.74	0.98	1.65	2.80
	3:05:00	0.00	0.00	0.08	0.12	0.23	0.61	0.98	1.51	2.37
	3:10:00	0.00	0.00	0.06	0.09	0.18	0.55	0.89	1.23	2.09
	3:15:00	0.00	0.00	0.05	0.08	0.16	0.48	0.70	1.09	1.85
	3:20:00	0.00	0.00	0.04	0.07	0.14	0.42	0.60	0.95	1.62
	3:25:00	0.00	0.00	0.04	0.06	0.11	0.35	0.51	0.81	1.38
	3:30:00	0.00	0.00	0.03	0.05	0.09	0.29	0.42	0.67	1.14
	3:35:00	0.00	0.00	0.02	0.03	0.07	0.22	0.32	0.53	0.91
	3:40:00	0.00	0.00	0.02	0.02	0.05	0.16	0.23	0.39	0.67
	3:45:00	0.00	0.00	0.01	0.01	0.03	0.10	0.14	0.25	0.44
	3:50:00	0.00	0.00	0.01	0.01	0.02	0.05	0.07	0.14	0.27
	3:55:00 4:00:00	0.00	0.00	0.01	0.01	0.02	0.03	0.04	0.08	0.17
	4:05:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.05	0.11 0.07
	4:10:00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.03	0.07
	4:15:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.02
	4:20:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

# DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft ² ]	[acres]	[ft ³ ]	[ac-ft]	Outflow [cfs]	
	0.00	32	0.001	0	0.000	0.00	For best results, include the
	0.50	334	0.008	46	0.001	0.01	stages of all grade slope changes (e.g. ISV and Floor)
	1.00	1,171	0.027	423	0.010	0.02	from the S-A-V table on
	1.50	3,036	0.070	1,304	0.030	0.03	Sheet 'Basin'.
WQCV	2.00	6,897	0.158	3,788	0.087	0.04	
EURV	2.12	7,824	0.180	4,671	0.107	0.04	Also include the inverts of all
	2.50	10,316	0.237	8,164	0.187	0.91	outlets (e.g. vertical orifice,
100-YR	2.94	12,569	0.289	13,199	0.303	6.22	overflow grate, and spillway, where applicable).
	3.00	12,876	0.296	13,962	0.321	7.30	where applicable).
	3.50	15,082	0.346	21,011	0.482	20.07	
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### POND E FOREBAY VOLUME REQUIREMENTS

Equation 3-1	WQCV= a(0.91/ ³ -1.19/ ² +0.781/)
	a=1 (40 hour drain time)

Forebay 1 *I=.082 WQCV=* 0.05646

Equation 3-3	V=(WQCV/12)A		
Forebay 1	A= 17.69 Acres	V=	0.083

#### 3% OF WQCV FOREBAY TOTAL VOLUME= .03(V)

VOLUME REQUIRED FOR FOREBAY 1 =	0.002 AC-FT	109 CF

VOLUME PROVIDED FOR FOREBAY 1 = 0.005 AC-FT 230 CF

Q ₁₀₀ Discharges	2% OF Q ₁₀₀
Q ₁₀₀ Forebay 1=	.02*12.6 CFS= 0.25 CFS

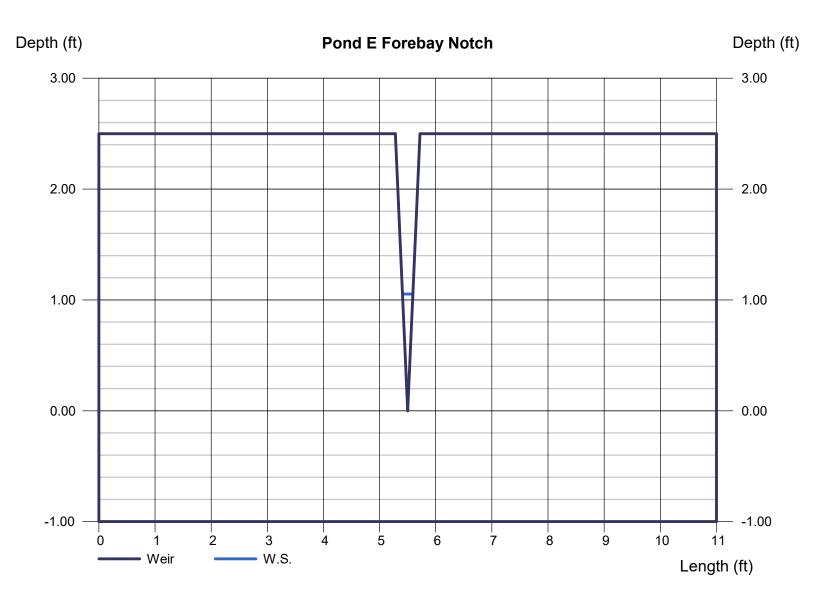
# Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

# Pond E Forebay Notch

V-Notch Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 1.05
Angle (Deg)	= 10	Q (cfs)	= 0.250
Total Depth (ft)	= 2.50	Area (sqft)	= 0.10
		Velocity (ft/s)	= 2.58
Calculations		Top Width (ft)	= 0.18
Weir Coeff. Cw	= 0.22		
Compute by:	Known Q		
Known Q (cfs)	= 0.25		



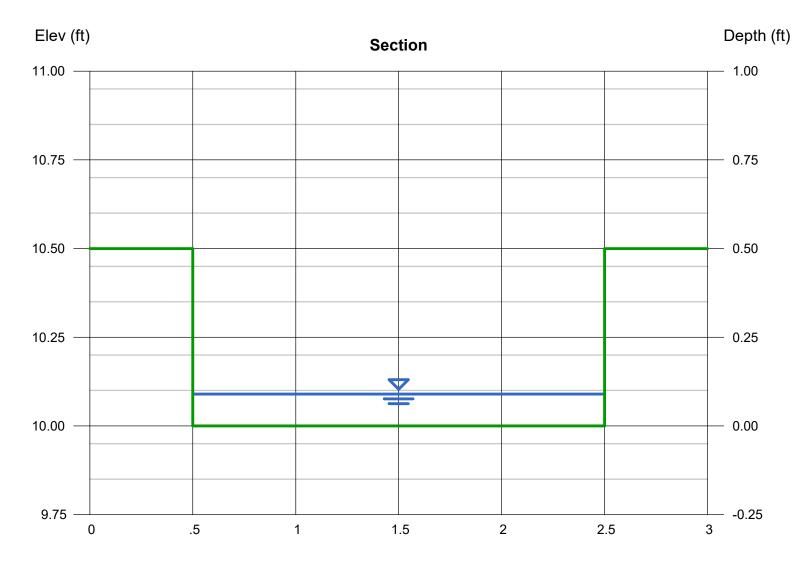
# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

# Pond E Trickle Channel

Rectangular		Highlighted	
Bottom Width (ft)	= 2.00	Depth (ft)	= 0.09
Total Depth (ft)	= 0.50	Q (cfs)	= 0.250
		Area (sqft)	= 0.18
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 1.39
Slope (%)	= 0.50	Wetted Perim (ft)	= 2.18
N-Value	= 0.013	Crit Depth, Yc (ft)	= 0.08
		Top Width (ft)	= 2.00
Calculations		EGL (ft)	= 0.12
Compute by:	Known Q		
Known Q (cfs)	= 0.25		

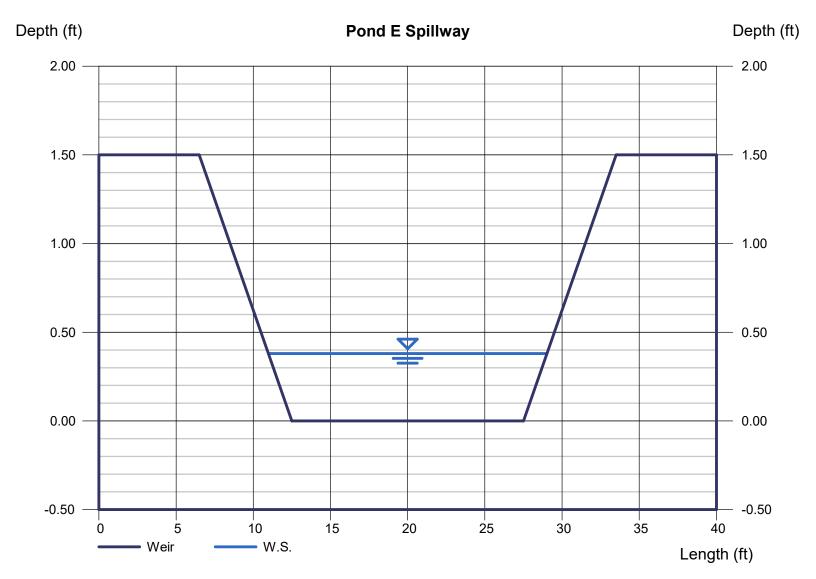


# Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# Pond E Spillway

Trapezoidal Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 0.38
Bottom Length (ft)	= 15.00	Q (cfs)	= 11.60
Total Depth (ft)	= 1.50	Area (sqft)	= 6.28
Side Slope (z:1)	= 4.00	Velocity (ft/s)	= 1.85
		Top Width (ft)	= 18.04
Calculations			
Weir Coeff. Cw	= 3.10		
Compute by:	Known Q		
Known Q (cfs)	= 11.60		



Update calculations if updates are made to the detention basin design spreadsheet

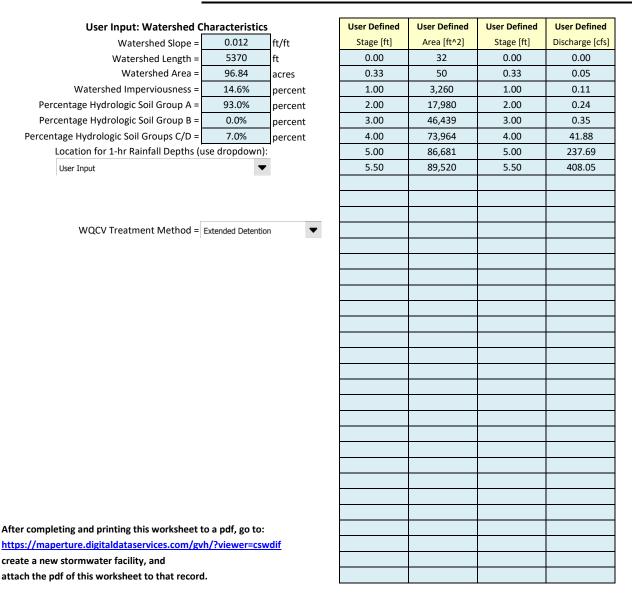
# **Stormwater Detention and Infiltration Design Data Sheet**

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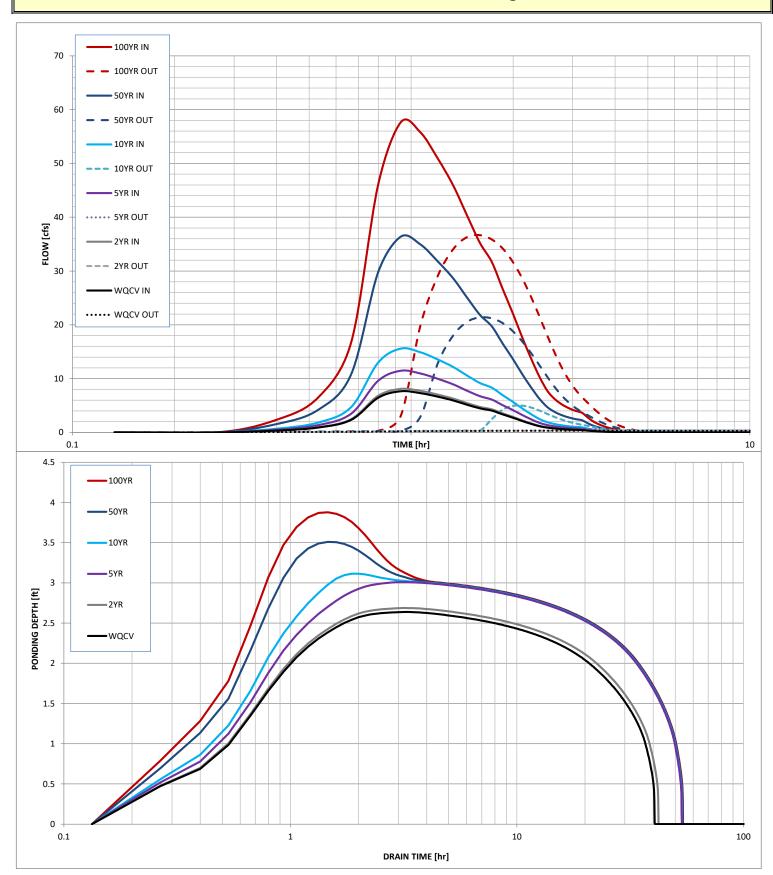
Stormwater Facility Name: Saddlehorn Filing 3 - Pond C

### Facility Location & Jurisdiction: El Paso County - Saddlehorn Ranch Metropolitan District



	Routed Hydro	graph Results					<b>_</b>
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in
Calculated Runoff Volume =	0.737	0.780	1.110	1.513	3.577	5.724	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.736	0.779	1.109	1.513	3.577	5.722	acre-ft
Time to Drain 97% of Inflow Volume =	37.4	38.9	49.0	48.1	43.7	39.8	hours
Time to Drain 99% of Inflow Volume =	39.3	40.9	51.6	51.2	49.4	47.7	hours
Maximum Ponding Depth =	2.64	2.69	3.01	3.11	3.51	3.88	ft
Maximum Ponded Area =	0.83	0.86	1.07	1.13	1.38	1.62	acres
Maximum Volume Stored =	0.662	0.702	1.014	1.127	1.624	2.180	acre-ft

SDI_Pond C.xlsm, Design Data

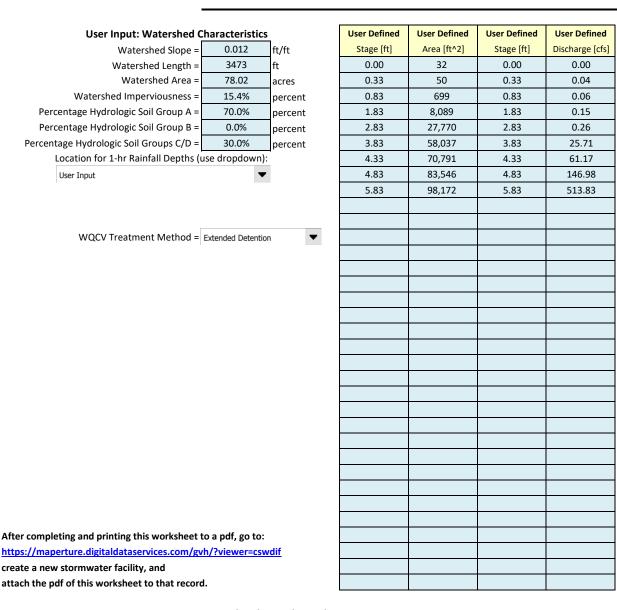


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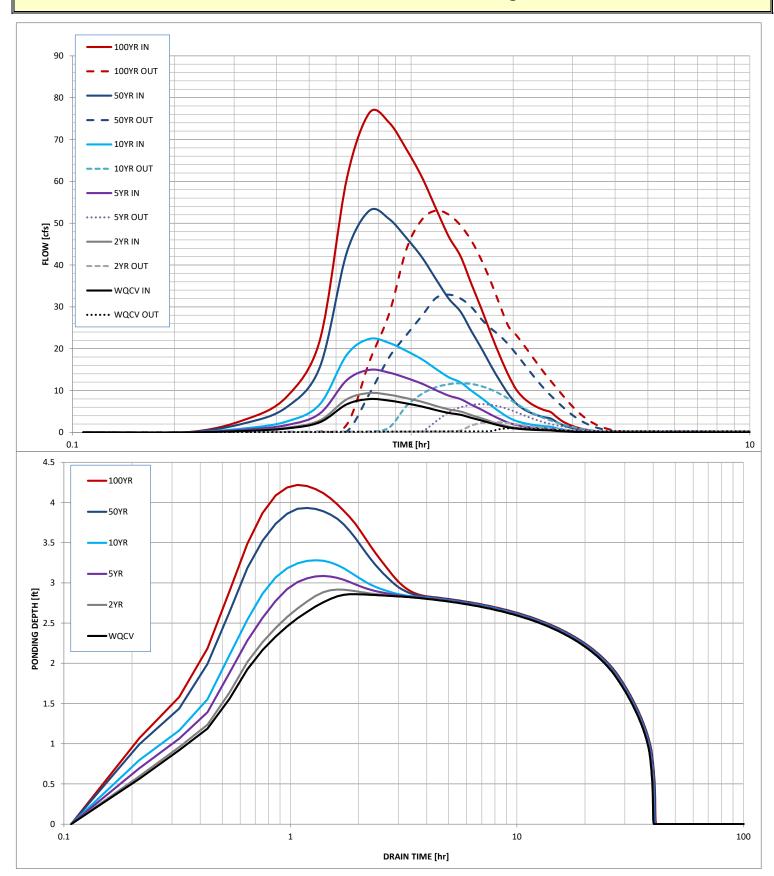
Stormwater Facility Name: Saddlehorn Ranch Filing 3 - Pond D

### Facility Location & Jurisdiction: El Paso County - Saddlehorn Ranch Metropolitan District



	<b>Routed Hydro</b>	graph Results					_
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in
Calculated Runoff Volume =	0.619	0.733	1.170	1.758	4.226	6.144	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.619	0.733	1.170	1.758	4.226	6.142	acre-ft
Time to Drain 97% of Inflow Volume =	36.5	36.0	34.5	32.7	26.5	22.5	hours
Time to Drain 99% of Inflow Volume =	38.5	38.3	37.8	37.0	34.2	32.4	hours
Maximum Ponding Depth =	2.86	2.92	3.09	3.28	3.93	4.22	ft
Maximum Ponded Area =	0.65	0.70	0.81	0.95	1.39	1.56	acres
Maximum Volume Stored =	0.533	0.573	0.701	0.872	1.637	2.055	acre-ft

### SDI_Pond D.xlsm, Design Data

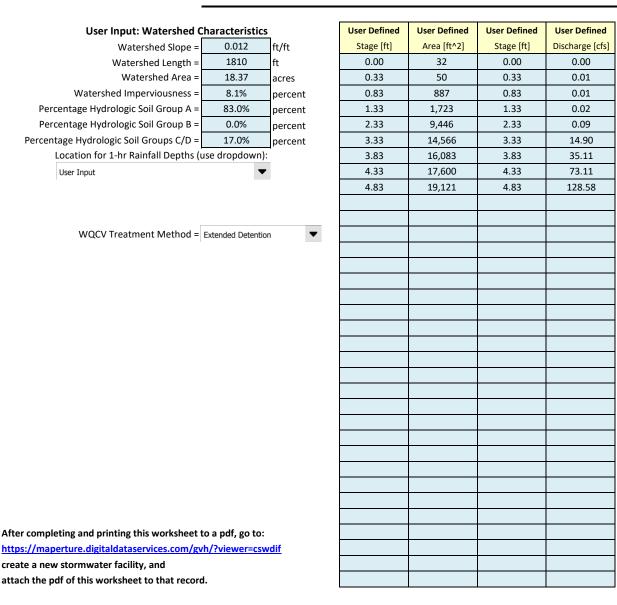


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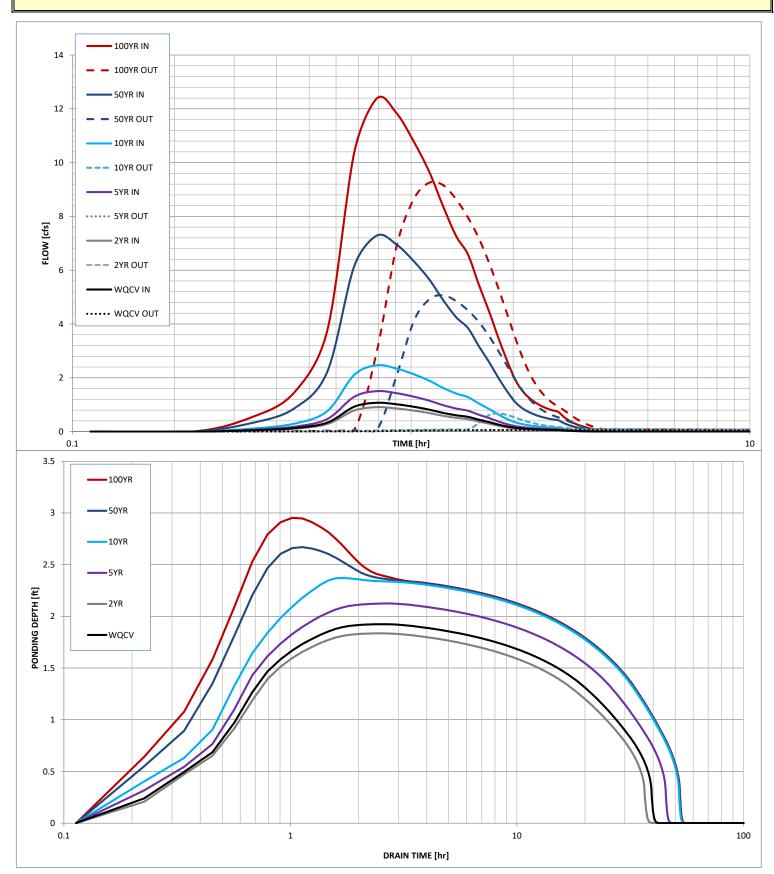
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Stormwater Facility Name: Saddlehorn Ranch Filing 3 - Pond E

### Facility Location & Jurisdiction: El Paso County - Saddlehorn Ranch Metropolitan District



	Routed Hydro	graph Results					_
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in
Calculated Runoff Volume =	0.086	0.073	0.121	0.199	0.596	1.019	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.085	0.072	0.120	0.199	0.596	1.019	acre-ft
Time to Drain 97% of Inflow Volume =	35.7	33.6	40.3	43.9	34.3	28.1	hours
Time to Drain 99% of Inflow Volume =	38.3	35.9	43.8	49.1	44.3	40.2	hours
Maximum Ponding Depth =	1.92	1.84	2.12	2.37	2.67	2.95	ft
Maximum Ponded Area =	0.14	0.13	0.18	0.22	0.26	0.29	acres
Maximum Volume Stored =	0.075	0.063	0.107	0.157	0.228	0.305	acre-ft



Final Drainage Report Filing 3 - Saddlehorn Ranch

# APPENDIX E

# **REFERENCE MATERIALS**



Issue Date: OCT 2 0 2004

Federal Emergency Management Agency

Case No.: 04-08-0587P

LOMR-APP

Washington, D.C. 20472

Effective Date: FEB 1 6 2005

# LETTER OF MAP REVISION **DETERMINATION DOCUMENT (CONTINUED)**

# PUBLIC NOTIFICATION OF REVISION

Within 90 days of the second publication in the local newspaper, a citizen may request that we reconsider this determination. Any request for reconsideration must be based on scientific or technical data. Therefore, this letter will be effective only after the 90-day appeal period has elapsed and we have resolved any appeals that we receive during this appeal period. Until this LOMR is effective, the revised BFEs presented in this LOMR may be changed.

A notice of changes will be published in the Federal Register. This information also will be published in your local newspaper on or about the dates listed below.

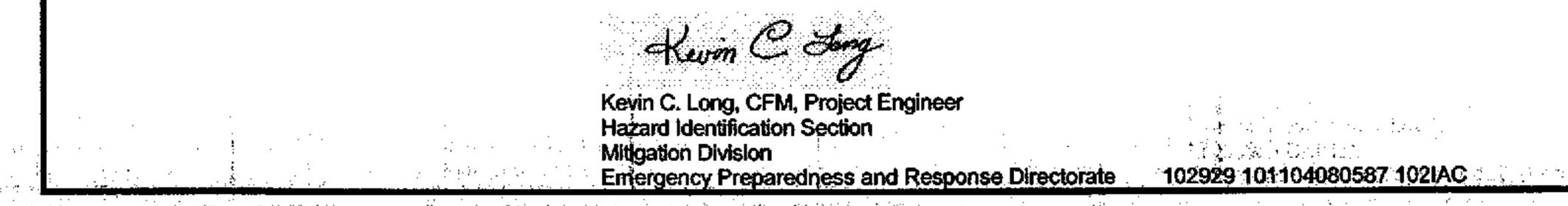
LOCAL NEWSPAPER

Page 4 of 4

Name: El Paso County News Dates: 11/10/2004 11/17/2004

		BFE (FEE		MAP PANEL
FLOODING SOURCE	LOCATION OF REFERENCED ELEVATION	EFFECTIVE	REVISED	NUMBER(S)
Haegler Ranch Tributary 2	Approximately 310 feet upstream of confluence with Geick Ranch West Tributary	None	6,735	08041C0575 F
naegiei Nancii Inibulary z	Approximately 3,140 feet upstream of confluence with Geick Ranch West Tributary	None	6,779	08041C0575 F
Haegler Ranch Tributary 3	Approximately 8,100 feet downstream of Curtis Road	None	6,672	08041C0575 F
naegiei Nanoi muutary 5	Approximately 300 feet upstream of Curtis Road	None	6,769	08041C0575 F
Haegler Ranch Tributary 4	Approximately 4,000 feet downstream of Curtis Road	None	6,688	08041C0575 F
Tacylet Ivanor Tribuvary 4	Approximately 300 feet upstream of Curtis Road	None	6,758	08041C0575 F
	· •			

# you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2677 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional information about the NFIP is available on our website at http://www.fema.gov/nfip.



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# CHANGES ARE MADE IN DETERMINATIONS OF BASE FLOOD ELEVATIONS FOR THE UNINCORPORATED AREAS OF EL PASO COUNTY, COLORADO, UNDER THE NATIONAL FLOOD INSURANCE PROGRAM

On March 17, 1997, the Department of Homeland Security's Federal Emergency Management Agency identified Special Flood Hazard Areas (SFHAs) in the unincorporated areas of El Paso County, Colorado, through issuance of a Flood Insurance Rate Map (FIRM). The Mitigation Division has determined that modification of the elevations of the flood having a 1-percent chance of being equaled or exceeded in any given year (base flood) for certain locations in this community is appropriate. The modified Base Flood Elevations (BFEs) revise the FIRM for the community.

The changes are being made pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (Public Law 93-234) and are in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, Public Law 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65.

A hydraulic analysis was performed to incorporate new hydrologic, hydraulic, and topographic data for Haegler Ranch Tributary 2 from approximately 310 feet upstream to approximately 3,140 feet upstream of the confluence with Geick Ranch West Tributary; for Haegler Ranch Tributary 3 from approximately 8,100 feet downstream to approximately 400 feet upstream of Curtis Road; and for Haegler Ranch Tributary 4 from approximately 4,100 feet downstream to approximately 400 feet upstream of Curtis Road. This has resulted in increases and decreases in SFHA width and increased BFEs for the above-mentioned tributaries. The table below indicates existing and modified BFEs for selected locations along the affected lengths of the flooding source(s) cited above.

	Existing BFE	'Modified BFE
Location	(feet)*	(feet)*
Haegler Ranch Tributary 2:		
Approximately 310 feet upstream of confluence with		
Geick Ranch West Tributary	None	6,735
Approximately 3,140 feet upstream of confluence with		
Geick Ranch West Tributary	None	6,779
Haegler Ranch Tributary 3:		
Approximately 8,100 feet downstream of Curtis Road	None	6,672
Approximately 300 feet upstream of Curtis Road	None	6,769
Haegler Ranch Tributary 4:		
Approximately 4,000 feet downstream of Curtis Road	None	6,688
Approximately 300 feet upstream of Curtis Road	None	6,758

*National Geodetic Vertical Datum, rounded to nearest whole foot

Under the above-mentioned Acts of 1968 and 1973, the Mitigation Division must develop criteria for floodplain management. To participate in the National Flood Insurance Program (NFIP), the community must use the modified BFEs to administer the floodplain management measures of the NFIP. These modified BFEs will also be used to calculate the appropriate flood insurance premium rates for new buildings and their contents and for the second layer of insurance on existing buildings and contents.

Upon the second publication of notice of these changes in this newspaper, any person has 90 days in which he or she can request, through the Chief Executive Officer of the community, that the Mitigation Division reconsider the determination. Any request for reconsideration must be based on knowledge of changed conditions or new scientific or technical data. All interested parties are on notice that until the 90-day period elapses, the Mitigation Division's determination to modify the BFEs may itself be changed.

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Any person having knowledge or wishing to comment on these changes should immediately notify:

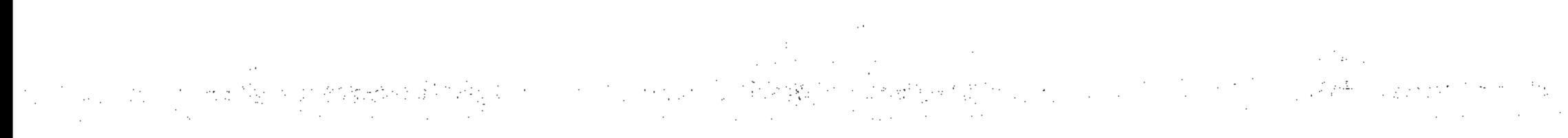
The Honorable Chuck Brown Chairman, El Paso County Board of Commissioners 27 Vermijo Avenue Colorado Springs, CO 80903-2208

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Flooding Source and Location	Drainage Area (square miles)	Pea <u>10-Year</u>	k Discharges (cu 50-Year	bic feet per second 100-Year	nd) <u>500-Y</u> e
Haegler Ranch Tributary 2 At the confluence with Geick Ranch West Tributary	1.47	1	1	592	1
Haegler Ranch Tributary 3 At approximately 2,300 feet upstream of the confluence with Haegler Ranch Tributary 4	1.09	1	1	505	1
Haegler Ranch Tributary 4 At approximately 3,700 feet upstream of the confluence with Haegler Ranch Tributary 3	0.60	1	1	1 <b>30</b>	1

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1 Data Not Available

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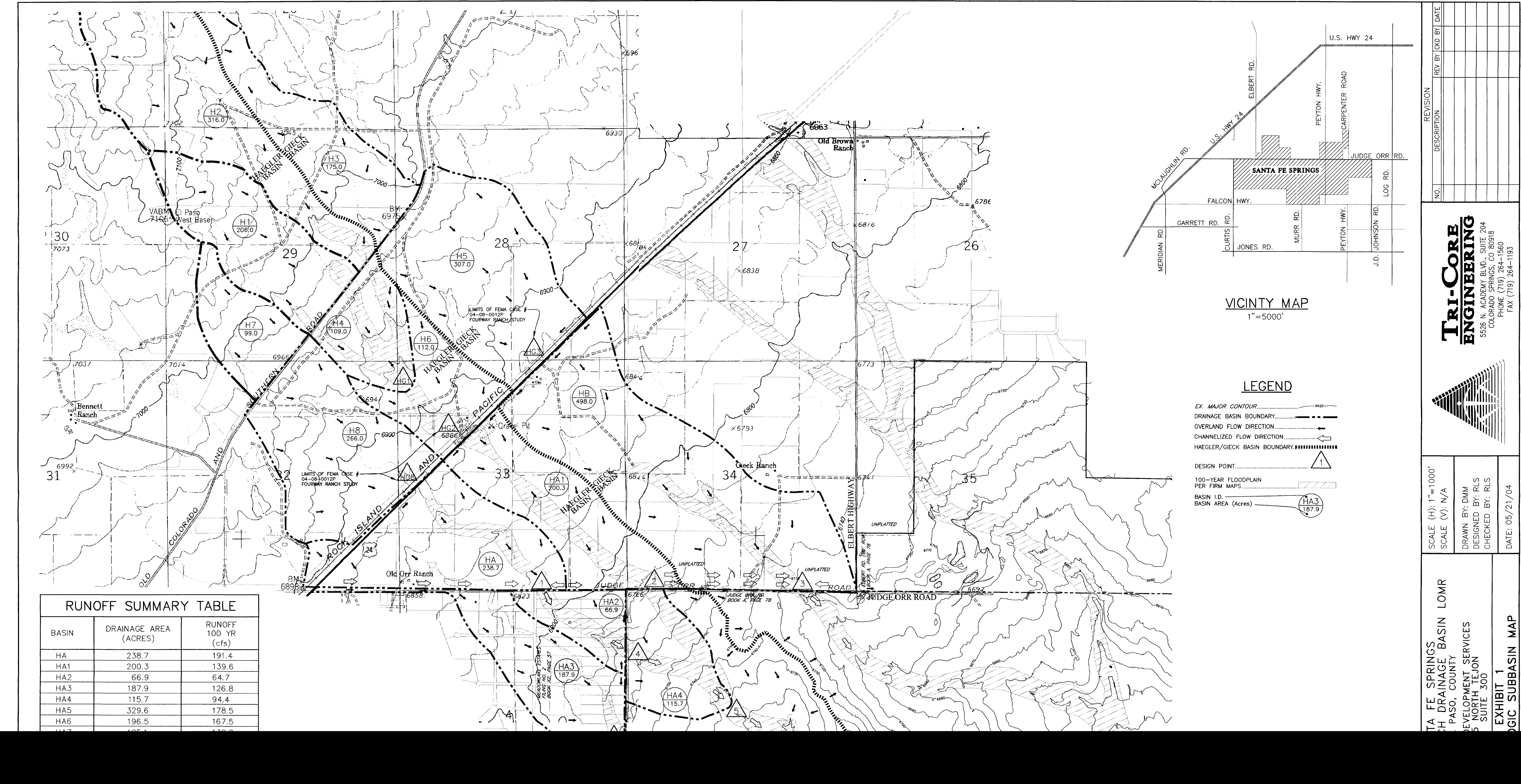
# Table 3. Summary of Discharges

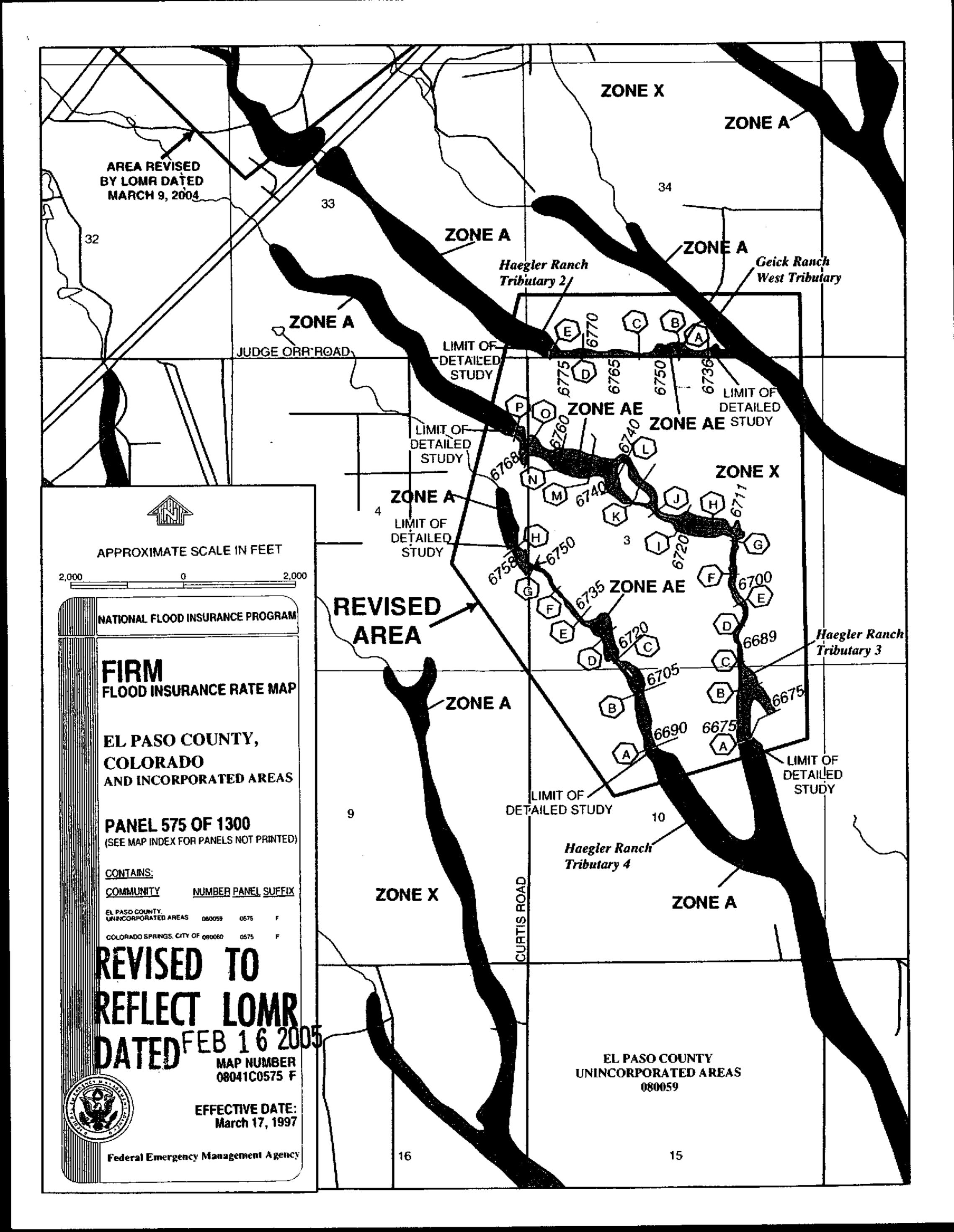
# **REVISED** TO REFLECT LOMR Dated Feb 1 6 2005

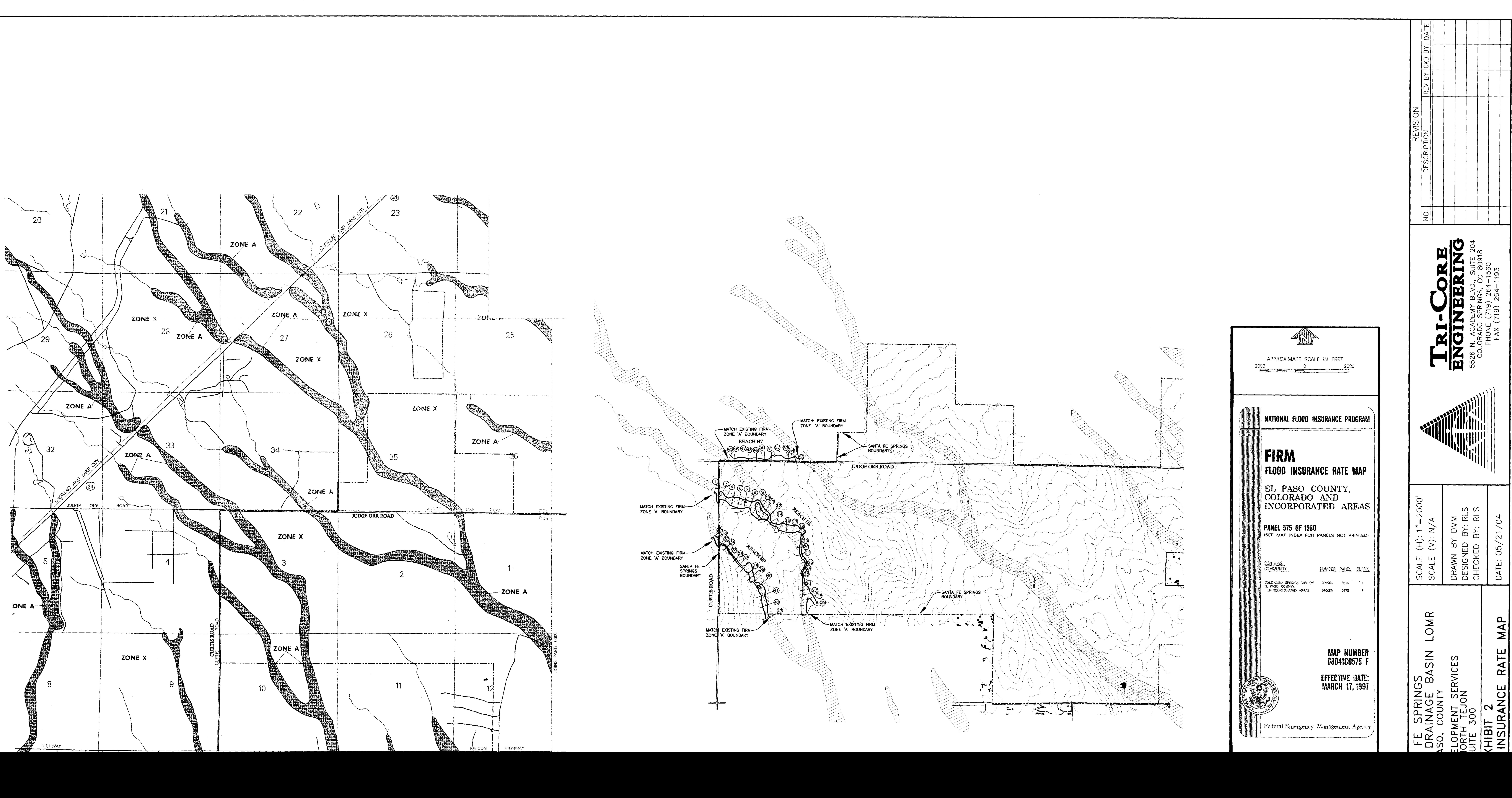
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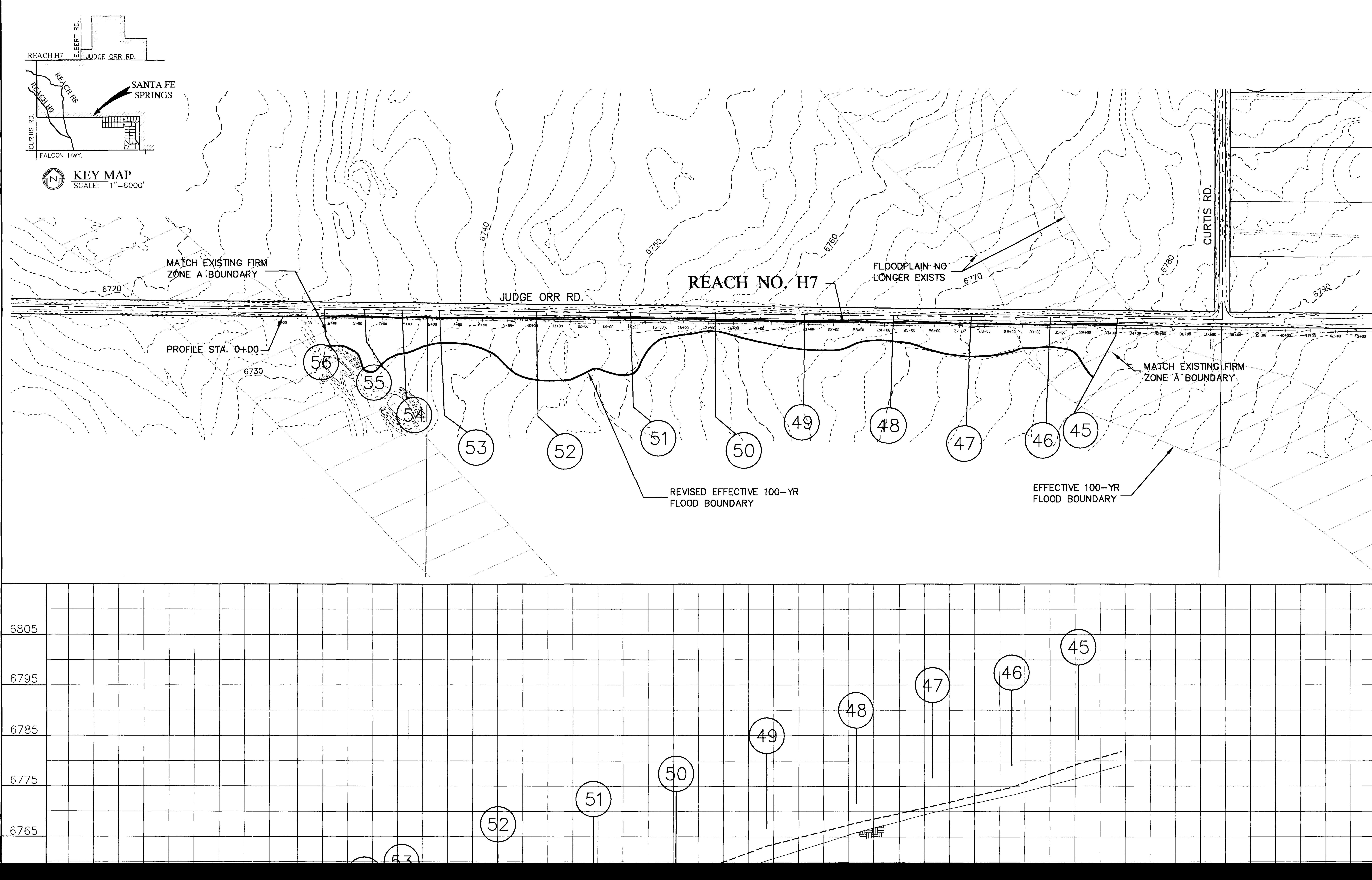




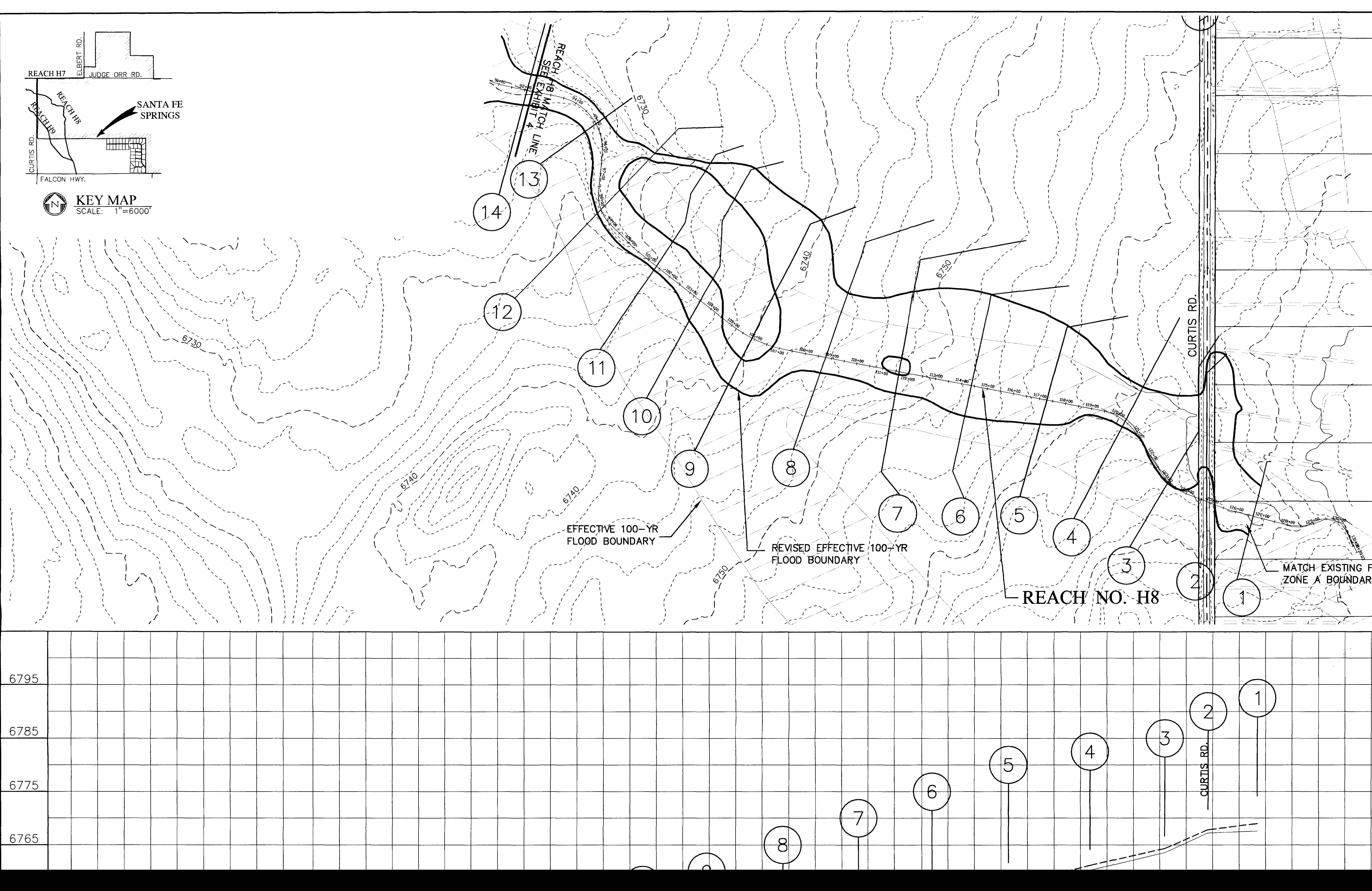




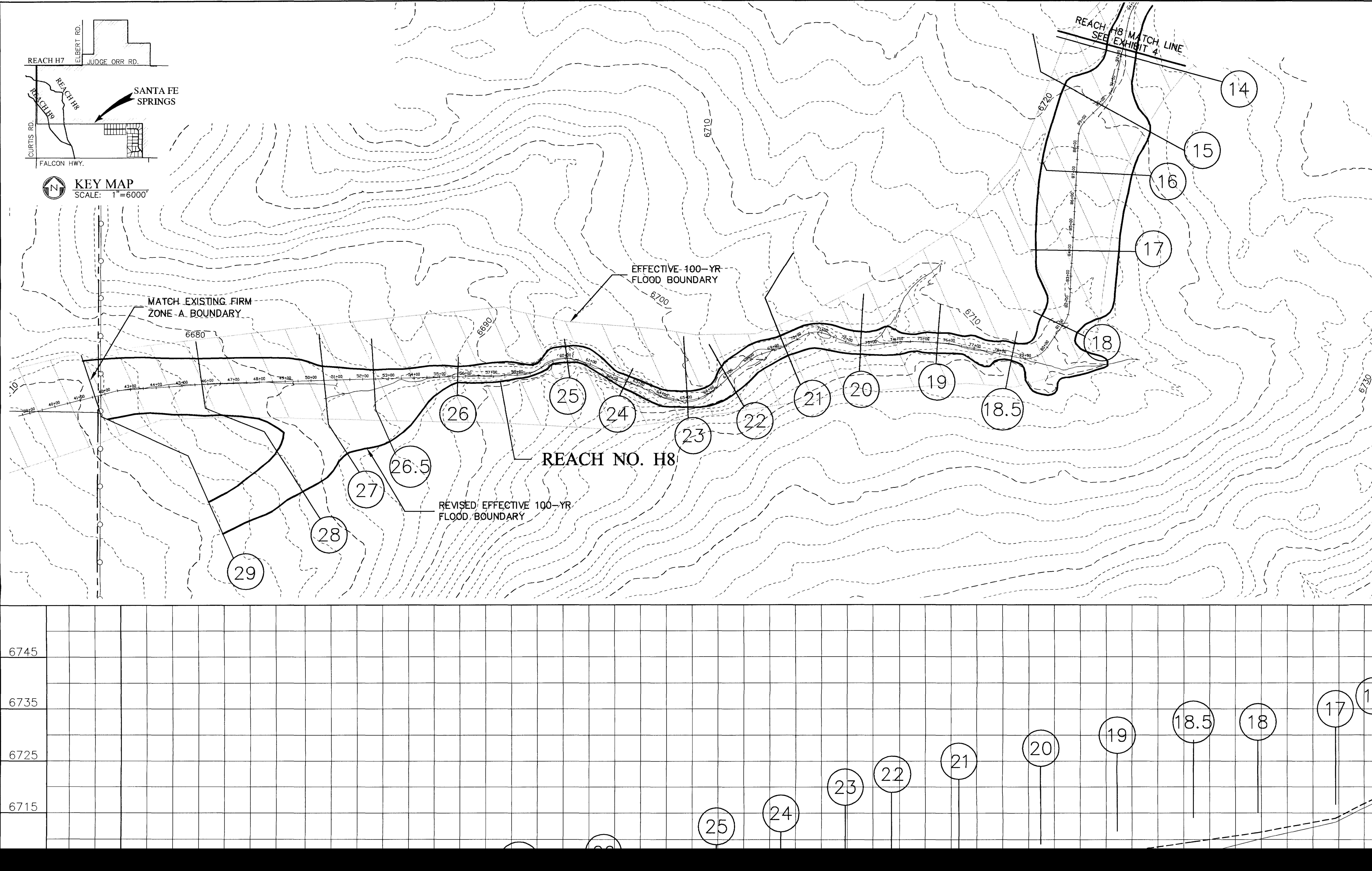




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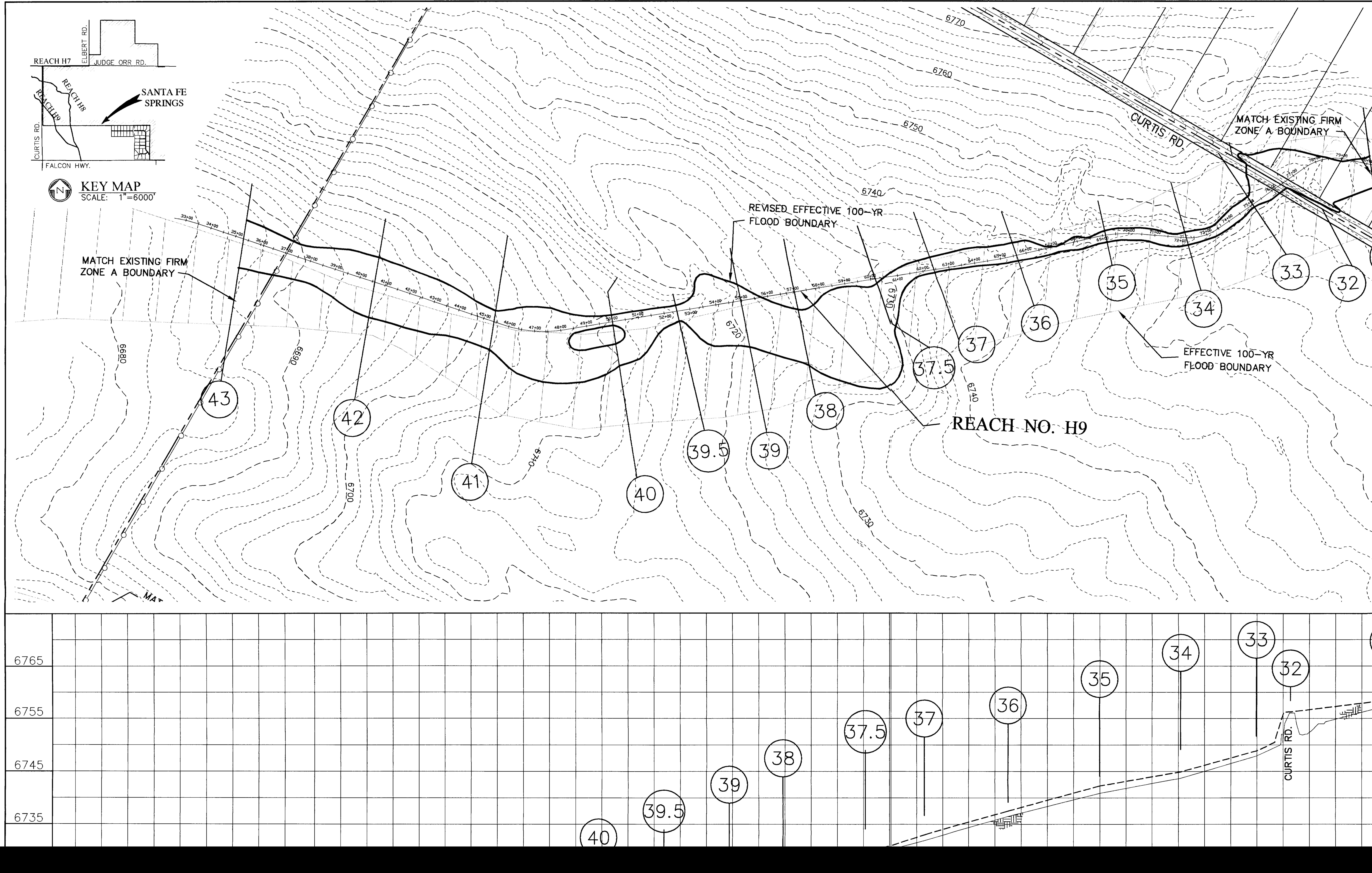


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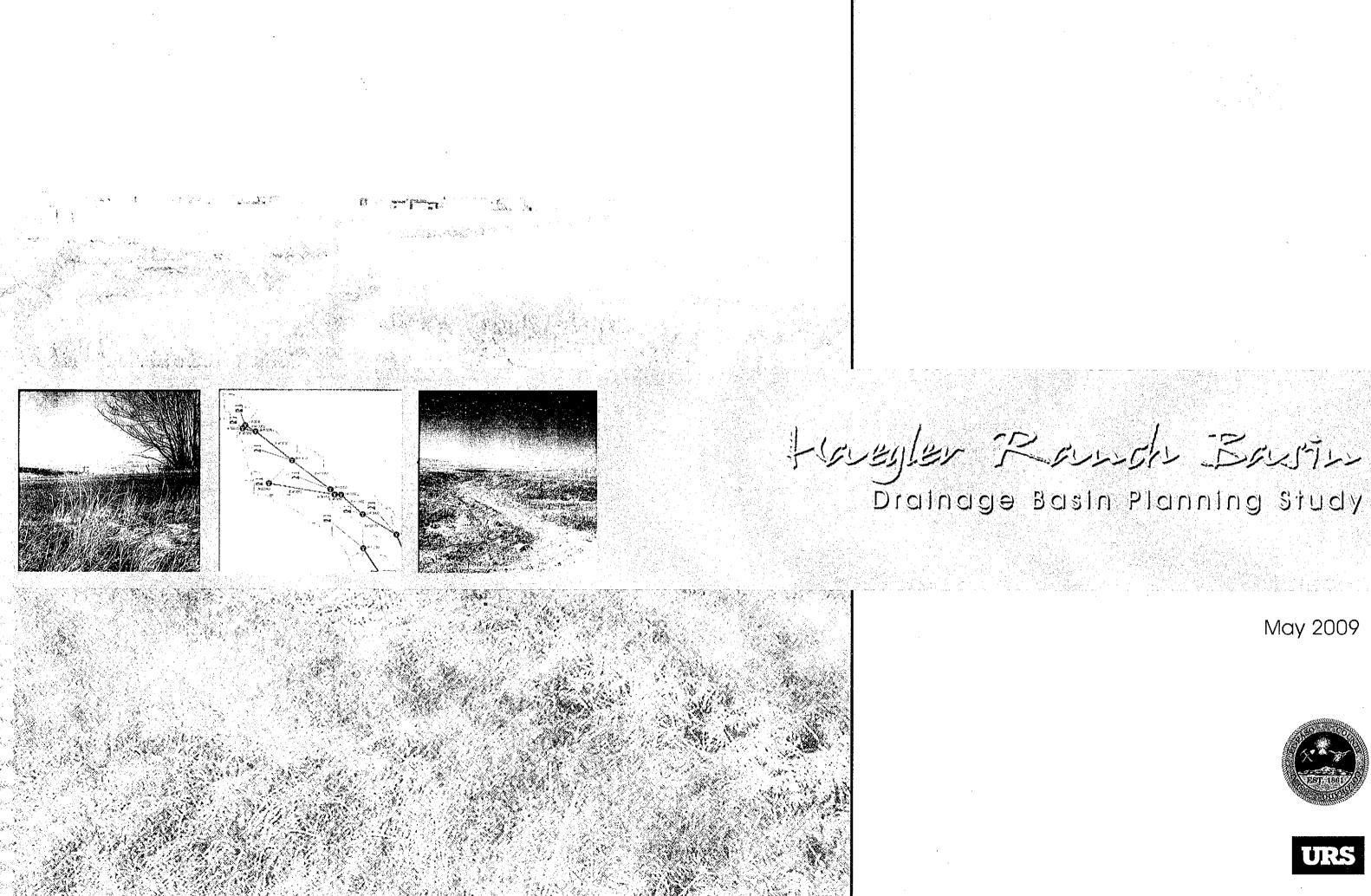


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I	REVISION         NO.       DESCRIPTION       REV BY       CKD BY       DATE         NO.       DESCRIPTION       REV BY       CKD BY       DATE
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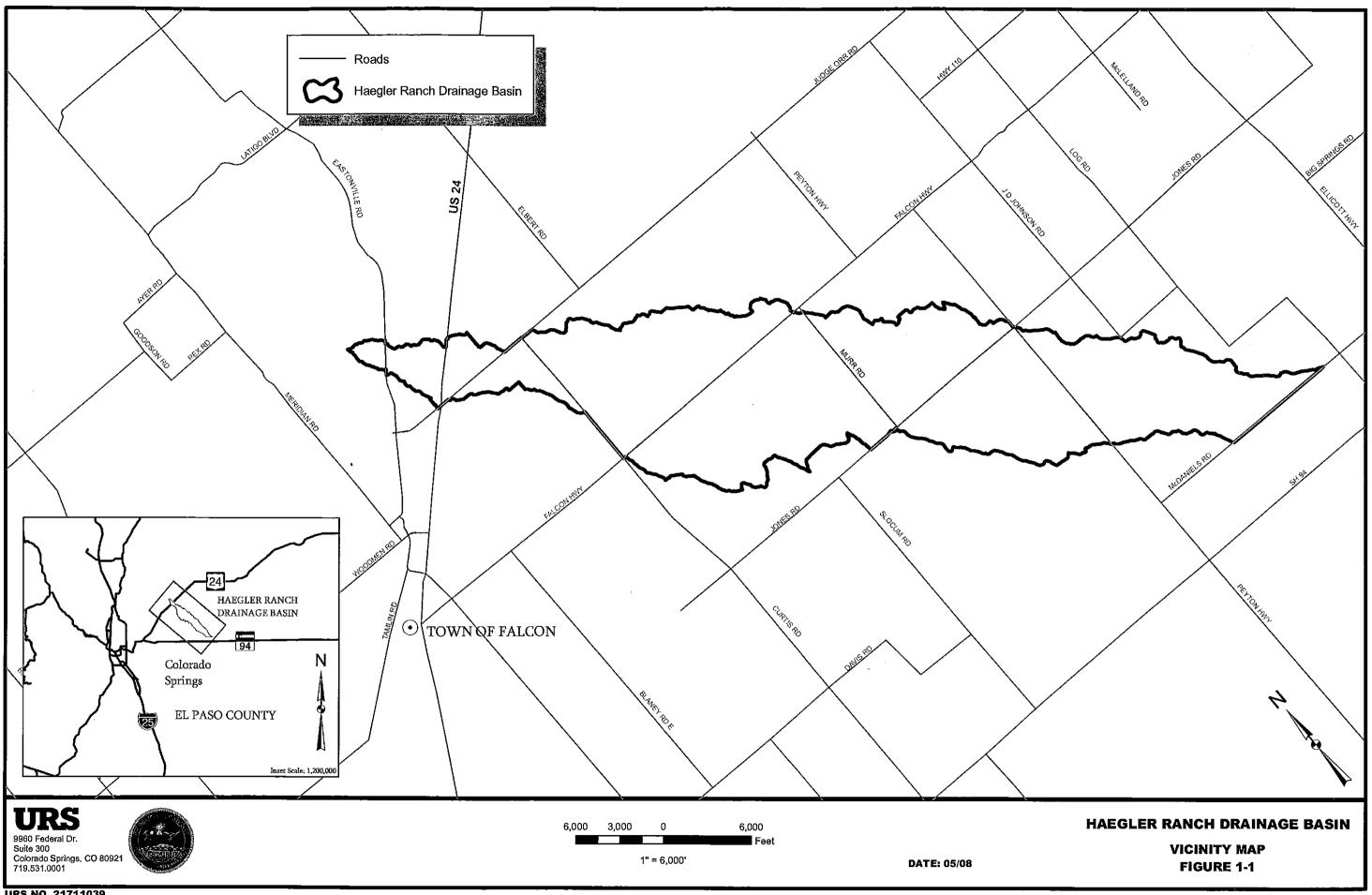
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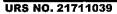


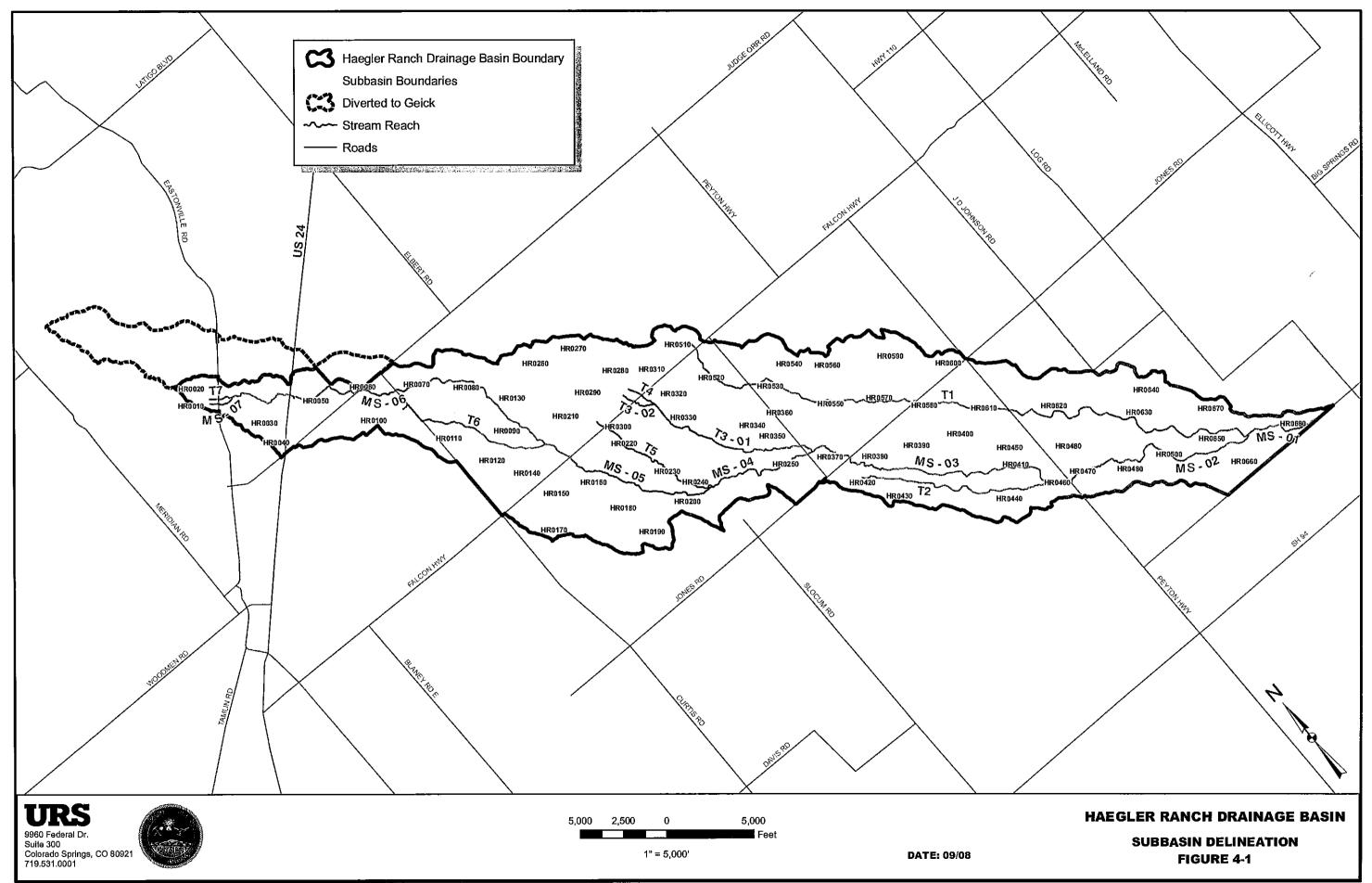
# May 2009











Facility Number	Road Crossing	Channel	Existing Size	Existing 100-yr Flow (cfs)	Deficiency
633	Sagecreek Road	N/A	24" CMP	N/A	N/A
634	Sagecreek Road	N/A	24" CMP	N/A	N/A
701	Curtis Road	N/A	18" CMP	N/A	N/A
702	Curtis Road	Tributary 6 (T6)	36" CMP	120	Overtops
703	Curtis Road	Main Stem (MS-06)	24" CMP	590	Overtops
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	540	Overtops
705	Judge Orr Road	N/A	18" CMP	N/A	N/A
706	US 24	N/A	20" Steel Pipe	N/A	N/A
707	US 24	N/A	24" CMP	N/A	N/A
801	Pedestrain Bridge	Main Stem (MS-06)	Bridge	350	Meets Capacity
802	US24	Main Stem (MS-06)	2-66" CMPs	350	Meets Capacity
803	Eastonville Road	Main Stem (MS-07)	27"X21" CMP	25	Overtops
804	Eastonville Road	Tributary 7 (T7)	18" CMP	99	Overtops

 Table 5-3 Existing Hydraulic Deficiencies

Note: 69 Structures were cataloged and located. N/A indicates that the structure was not analyzed because it was not on one of the main channels.

# 5.14. Results

Hydraulic conditions from the hydraulic model results are summarized in Table 5-4. This includes channel velocity, flow depth, and top width for existing conditions at key locations. Water surface profiles for Haegler Ranch Drainage Basin for the 100-year recurrence interval flood for the existing conditions are presented in Figure 5-4 the HEC-RAS model for Haegler Ranch Drainage Basin for the existing conditions is provided in Appendix B.

The approximate 100-year floodplain as seen in Figure 5-4 varies from a contained floodplain with in a defined channel to a wide floodplain with shallow flooding. Three areas were designated as flooding: 1) the approximate 100-year floodplain as delineated by HEC-RAS, 2) split flow flooding that was estimated from HEC-RAS elevation upstream and contours, and 3) shallow areas connected to the floodplain with less than 1 foot of flooding.

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Key Location	Reach and	HEC-RAS Result	Recurrence Intervals			
Key Location	Station	HLC-KAJ Kesut	2-yr	5-уг	10-yr	10
	MS-06 72276	Channel velocity (ft/sec)	1.1	1.63	1.98	2
Main stem at US 24		Water surface depth in channel (ft)	1.36	2.44	3.24	6
		Top width (ft)	18.23	24.85	29.7	25
	MS-06 67666	Channel velocity (ft/sec)	3.33	4.09	1.76	3
Main stem at Judge Orr Road		Water surface depth in channel (ft)	0.52	1.04	1.05	1
		Top width (ft)	174.53	534.34	535.52	56
		Channel velocity (ft/sec)	1.05	1.6	2.04	3
Main stem at Falcon Highway	MS-05 52353	Water surface depth in channel (ft)	1.79	3.69	4.96	5
		Top width (ft)	31.42	83.76	556.41	59
	MS-03 33189	Channel velocity (ft/sec)	2.45	3.7	1.27	2
Main stem at Jones Road		Water surface depth in channel (ft)	3.2	5.83	9.25	1(
		Top width (ft)	47.98	105.51	580.28	66
· · · · · · · · · · · · · · · · · · ·	MS-02 18474	Channel velocity (ft/sec)	0.16	0.4	0.59	1
Main stem at Peyton Highway		Water surface depth in channel (ft)	4.14	4.35	4.51	5
		Top width (ft)	813.21	871.68	882.22	92
Southeast Tributary at Jones Road	T1 22297	Channel velocity (ft/sec)	0.62	1.02	1.47	
		Water surface depth in channel (ft)	2.45	3.52	3.59	3
		Top width (ft)	197.35	345.68	351.74	37
Southeast Tributary at Peyton Highway	T1 16611	Channel velocity (ft/sec)	1.67	2.25	2.65	4
		Water surface dcpth in channel (ft)	0.08	0.17	0.24	0
		Top width (ft)	239.82	241.36	242.51	24
Southeast Tributary at Confluencc with Main stem		Channel velocity (ft/sec)	3.44	0.11	0.18	0
	T1 410	Water surface depth in channel (ft)	1.69	2.01	2.01	2
confluence with Main stem	410	Top width (ft)	31.89	1169.3	1169.3	11
· ·	L	Channel velocity (ft/sec)	2.68	3.85	19.89	1
At Confluence with Geick Basin	MS-01 82	Water surface depth in channel (ft)	1.45	2.17	1.11	2
zaom	02	Top width (ft)	75.88	255.32	60.67	2

# Table 5-4 Existing Conditions HEC-RAS Model

100-yr
2.92 6.49
255.62
3.48
1.35 569.34
3.59
5.74
592.33
2.51
10.46
667.17
1.43 5.15
925.27
3.2
3.82
372.17
4.05
0.51 247.41
0.67
2.01
1169.3
17.33
2.36
262.84

Grass channels are designed for depths and velocities to be within the limits of allowable shear stress. Grass lined channels are limited to 1.0 psf shear stress. If calculated shear stress is above this, drop structures must be added to flatten the natural slope of the channel.

Using these criteria, several channel sections were developed to accommodate a range of future flow rates from 100 cfs to 3500 cfs, as shown in Table 6-2. The approximate channel sections were used in the alternatives to accommodate future flows as necessary,

A.		Grass	
(cfs)	Sideslope	Bottom	Depth
	(h:v)	( <b>ft</b> )	(ft)
300	4	6	5
500	4	8	5
600	4	15	5
800	4	20	5
900	4	25	5
1000	4	30	5
1500	4	50	5
2000	4	80	5
3000	4	120	5
3500	4	140	5

# Table 6-2 Channel Dimensions based on Flow Rates

# 6.2.2. Culvert Design

Culvert sizes for use in alternative evaluation were estimated based on full flow capacity of reinforced concrete pipe with a minimum slope of 0.50% and concrete end sections. For flows up to 300 cfs single RC pipe culverts with a maximum of 72" diameter were used. For greater flows, multiple RC pipes or 6-foot by 6-foot concrete box culverts with headwalls and flared wingwalls were used. Proposed culverts sizes based on existing flow rates are listed in Table 6-3.

Facility Number	Road Crossing	Channel	Existing Size	Existing 100-yr Flow (cfs)	Deficiency	Necessary Facility
N/A	Peyton Highway	Tributary 1 (T1)	No Culvert	500	Overtops	2-72" RCPs
N/A	Falcon Highway	Tributary 1 (T1)	No Culvert	33	Overtops	36" RCP
301	Peyton Highway	Main Stem (MS-02)	2-33"X48" CMPs	2,500	Overtops	7-6'X6' RCBs
401	Jones Road	Tributary 1 (T1)	2-24" CMPs	370	Overtops	6'X6' RCB
403	Jones Road	Main Stem (MS-03)	3-60" CMPs	2,300	Overtops	6-6'X6' RCBs

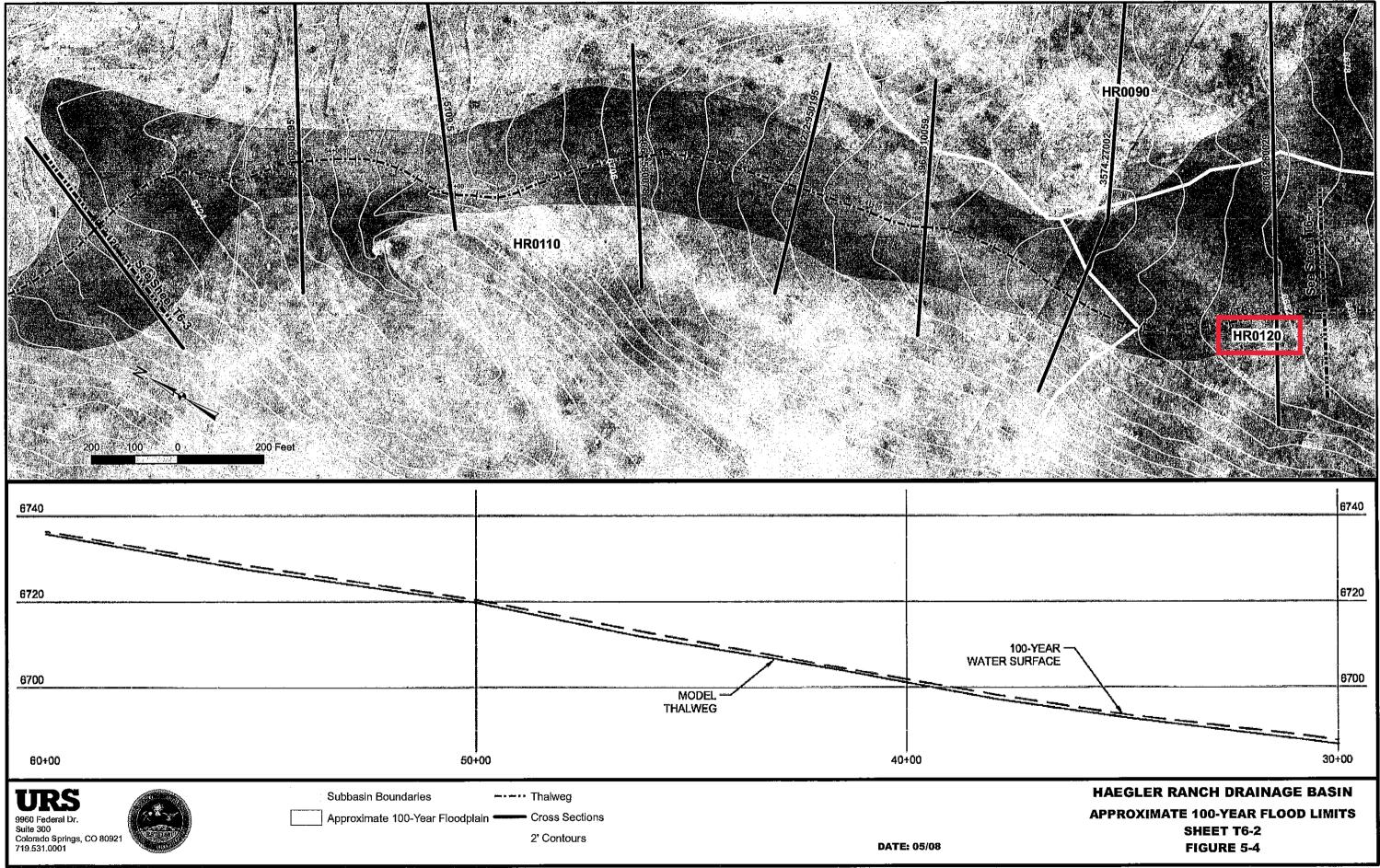
Facility Number	Road Crossing	Channel	Existing Size	Existing 100-yr Flow (cfs)	Deficiency	Necessary Facility
405	Murr Road	Main Stem (MS-04)	66" RCP	1,700	Overtops	5-6'X6' RCBs
407	Murr Road	Tributary 3 (T3-01)	66" RCP	670	Overtops	2-6'X6' RCBs
507	Peerless Farms Road	Tributary 3 (T3-01)	60'' CMP	600	Overtops	2-6'X6' RCBs
509	Murr Road	Tributary 1 (T1)	2-15" RCPs	220	Overtops	66" RCP
601	Whiting Way	Tributary 1 (T1)	24" CMP	220	Overtops	66" RCP
604	, Max Road	Tributary 1 (T1)	18" CMP	220	Overtops	66" RCP
609	Falcon Highway	Tributary 3 (T3-02)	18" CMP	180	Overtops	66" RCP
610	Falcon Highway	Tributary 4 (T4)	24" CMP	200	Overtops	66" RCP
612	Falcon Highway	Tributary 5 (T5)	24" CMP	150	Overtops	60" RCP
628	Falcon Highway	Main Stem (MS-05)	2-60" CMPs	1,000	Overtops	3-6'X6' RCBs
702	Curtis Road	Tributary 6 (T6)	36" CMP	120	Overtops	54" RCP
703	Curtis Road	Main Stem (MS-06)	24" CMP	590	Overtops	2-6'X6' RCBs
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	540	Overtops	2-72" RCPs
801	Pedestrain Bridge	Main Stem (MS-06)	Bridge	350	Meets Capacity	Existing Bridge
802	US24	Main Stem (MS-06)	2-66'' CMPs	350	Meets Capacity	Existing Culvert
803	Eastonville Road	Main Stem (MS-07)	27"X21" CMP	25	Overtops	30" RCP
804	Eastonville Road	Tributary 7 (T7)	18" CMP	99	Overtops	48" RCP

# 6.2.3. Detention Design

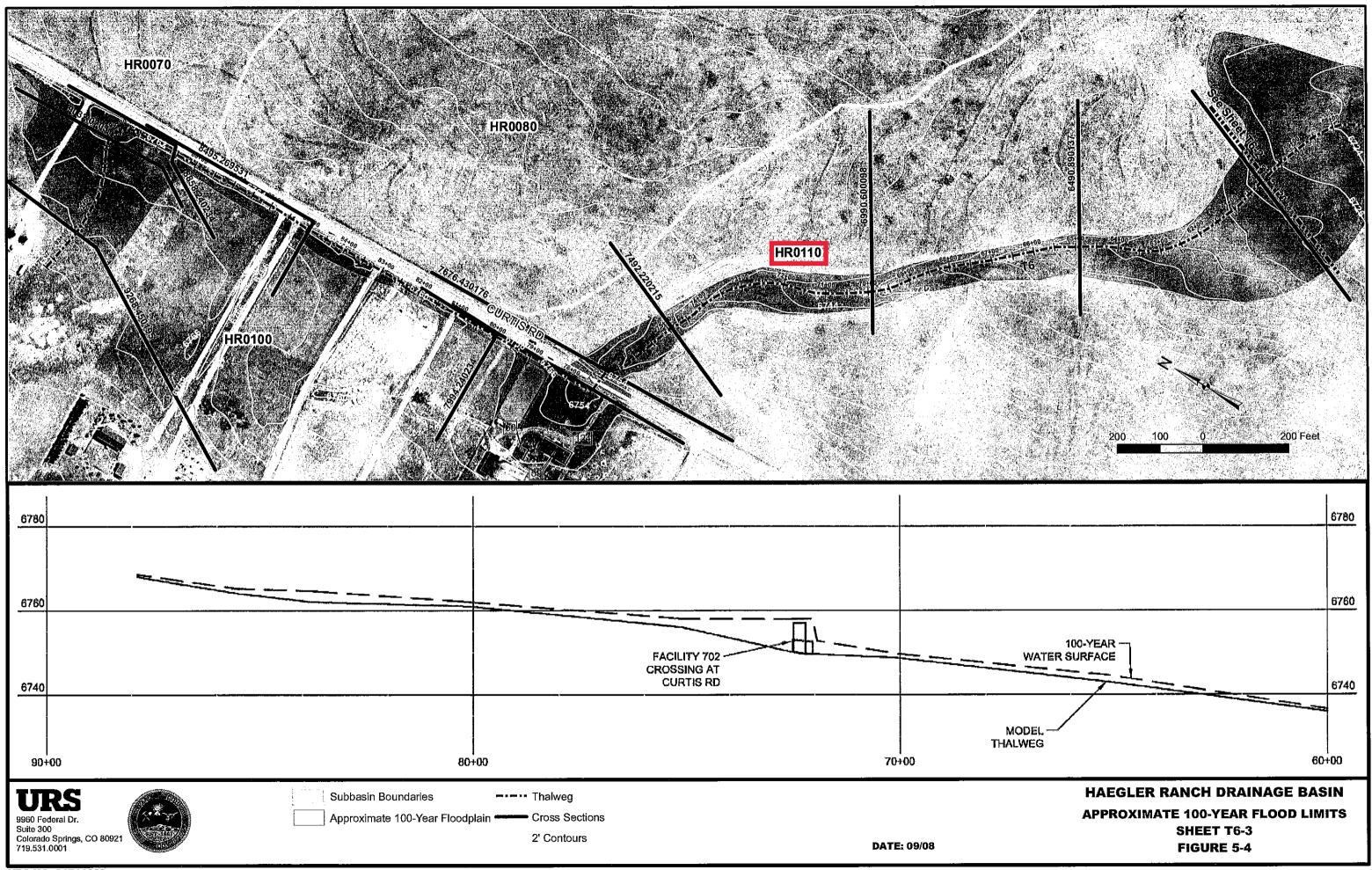
All detention pond design is based on Chapter 10, Storage, of the UDFCD SDCM. All ponds were assumed to be "full spectrum" per the SDCM. For final design to be performed later, some of the ponds may be separated into a water quality pond and an off-line major detention pond.

For the Regional Detention Alternative, either the simplified full spectrum sizing method or the hydrograph method was used to size the facility. If the contributing area is less than 160 acres and no

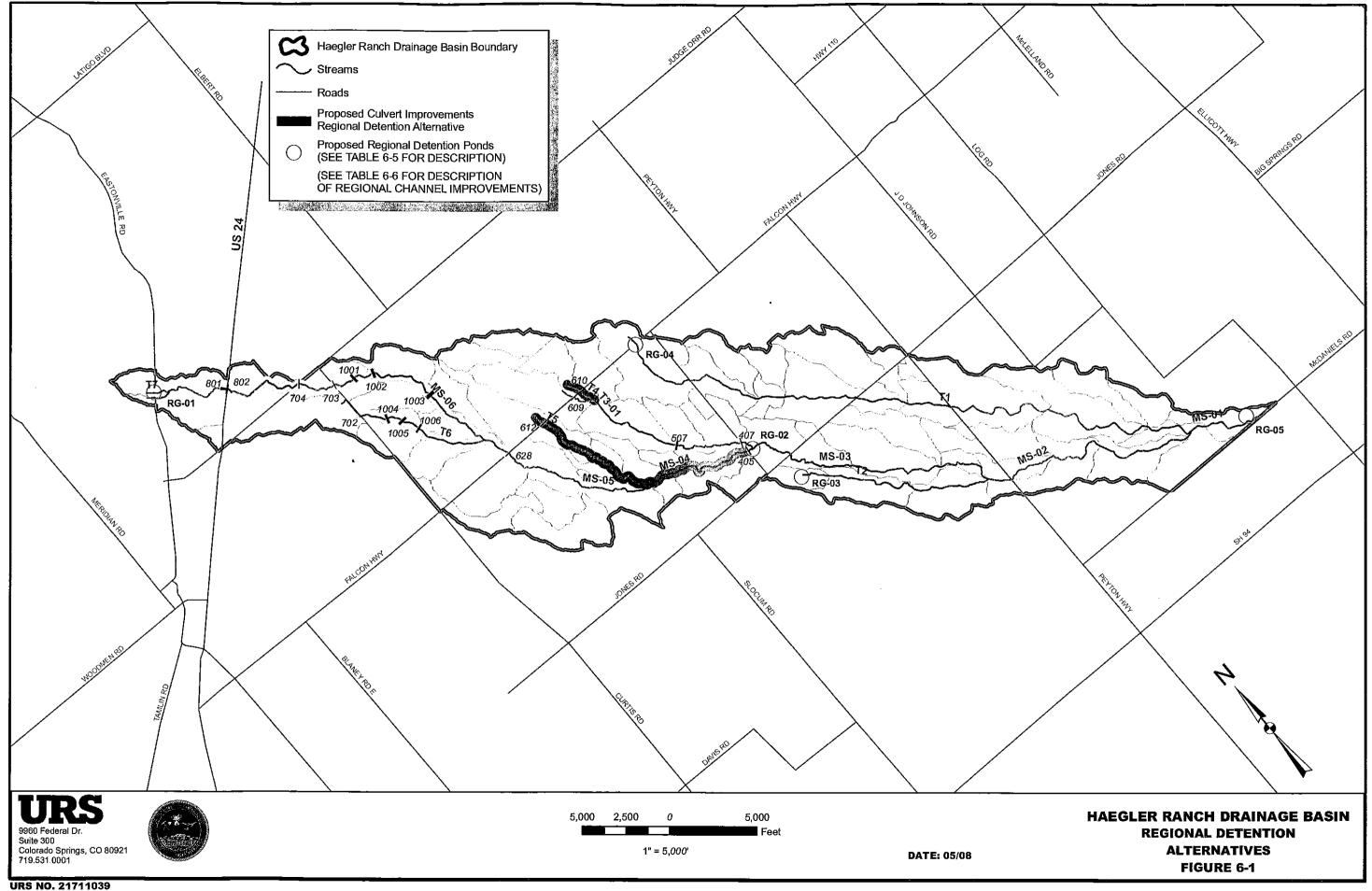
Haegler Ranch Drainage Basin Planning Study

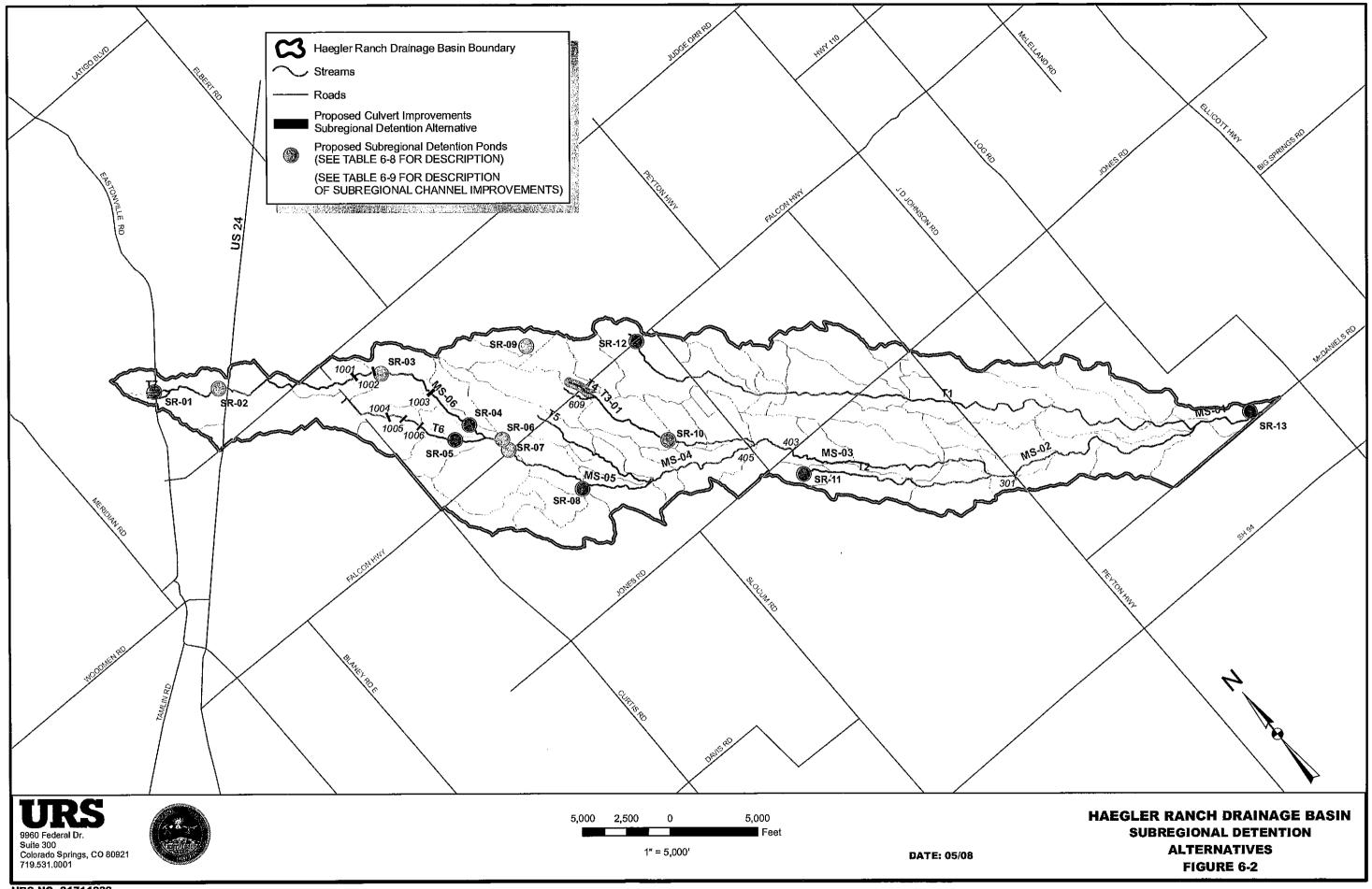


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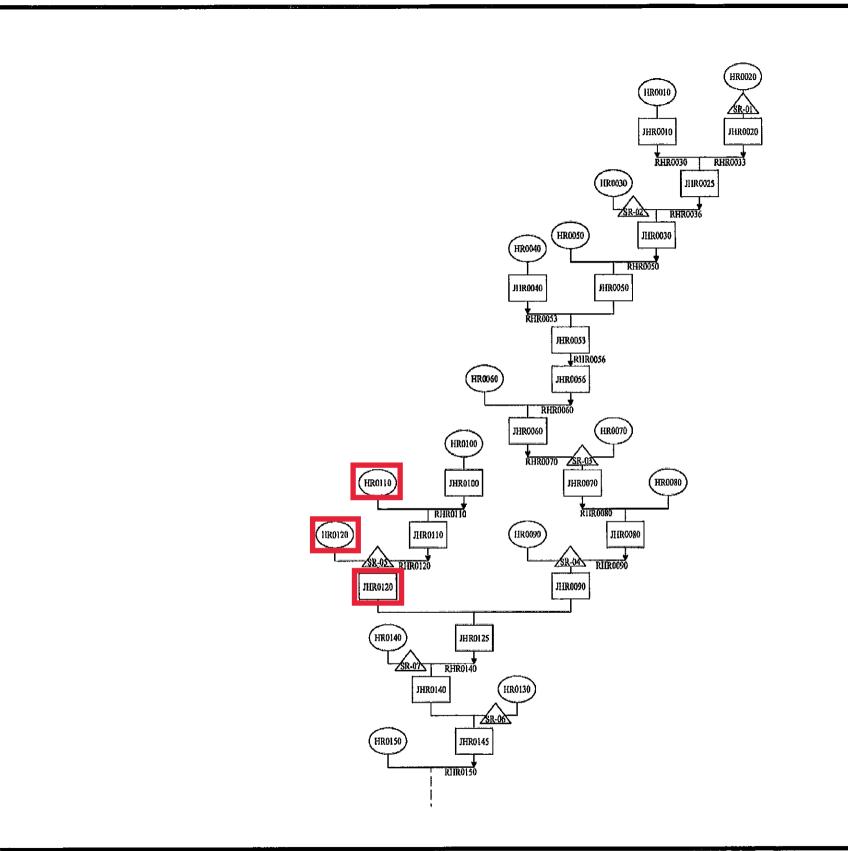


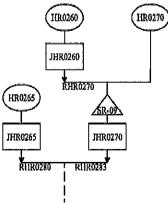
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# URS

9960 Federal Dr. Sulte 300 Colorado Springs, CO 80921 719.531.0001



URS NO. 21711039

DATE: 05/08

# HAEGLER RANCH DRAINAGE BASIN SUBREGIONAL DETENTION ALTERNATIVE SHEET 1 FIGURE 6-3

# 6.4.1. Channel & Culvert Costs

Channel costs for each alternative are based on cubic yards of excavation, plus the cost of the channel lining and drop structures. These costs are presented in Table 6-13 and Table 6-14.

<b>Table 6-13</b>	<b>Regional Detention</b>	Alternative Channel	Cost Estimates

tructure Cost
none
2,539,000
589,000
268,000
548,000
636,000
,302,000
127,000
\$36,000
370,000
222,000
253,000
5,888,000
,066,000
,033,000
,988,000

(See Tables C6 and C7 in Appendix C for details)

# Table 6-14 Sub-Regional Detention Alternative Channel Cost Estimates

Channel	Design Flow (cfs)	Channel Length (ft)	Total Cost	Drop Structure Cost
Main Stem (MS-05)	2,000	1,560	\$224,000	\$367,000
Main Stem (MS-06)	600	3,120	\$162,000	\$295,000
Main Stem (MS-06)	1,000	4,535	\$331,000	\$375,000
Main Stem (MS-06)	800	3,190	\$188,000	\$368,000
Tributary 3 (T3-01)	600	5,000	\$259,000	\$422,000
Tributary 3 (T3-02)	500	420	\$18,000	\$37,000
Tributary 4 (T4)	500	940	\$40.000	\$74.000
Tributary 6 (T6)	500	4,280	\$179,000	\$333,000
Tributary 6 (T6)	300	1,400	\$55,000	\$107,000
Sub-Total			\$1,456,000	\$2,374,000
30% Construction Con	itingency		\$430,000	\$712,000
15% Engineering Cont	tingency		\$218,000	\$356,000
Total			\$2,111,000	\$3,442,000

Culverts costs are based on a per linear foot of pipe with two flared end sections or two wing walls, as appropriate, complete-in-place. Culvert costs for each alternative are presented in Table 6-15 and Table 6-16.

## Table 6-15 Regional Detention Alternative Roadway Crossing Cost Estimate Sumary

Facility Number	Road Crossing	Channel	Existing Size	Proposed 100-yr Flow (cfs)	Necessary Facility for Proposed 100- year Flow	Estimated Cost
405	Murr Road	Main Stem (MS-04)	66" RCP	3,400	9-6'X6' RCBs	\$256,000
507	Peerless Farms Road	Tributary 3 (T3-01)	60" CMP	1200	4-6'X6' RCBs	\$139,000
609	Falcon Highway	Tributary 3 (T3-02)	18" CMP	460	2-66" RCPs	\$51,600
610	Falcon Highway	Tributary 4 (T4)	24" CMP	570	2-72" RCPs	\$51,000
612	Falcon Highway	Tributary 5 (T5)	24" CMP	240	72" RCP	\$26,000
628	Falcon Highway	Main Stem (MS-05)	2-60" CMPs	2,200	6-6'X6' RCBs	\$243,000
702	Curtis Road	Tributary 6 (T6)	36" CMP	140	60" RCP	\$29,000
703	Curtis Road	Main Stem (MS-06)	24" CMP	890	3-6'X6' RCBs	\$142,000
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	830	3-6'X6' RCBs	\$185,000
1001	Future Pastura Street	Main Stem (MS-06)	N/A	930	3-6'X6' RCBs	\$99,000
1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	N/A	930	3-6'X6' RCBs	\$99,000
1003	Future Arroyo Hondo Blvd. N	Main Stem (MS-06)	N/A	1500	4-6'X6' RCBs	\$143,000
1004	Future Pastura Street	Tributary 6 (T6)	N/A	440	2-66" RCPs	\$43,000
1005	Future El Vado Road	Tributary 6 (T6)	N/A	440	2-66" RCPs	\$43,000
1006	Future Socorro Trail	Tributary 6 (T6)	N/A	· 440	2-66" RCPs	\$43,000
Sub-Total						\$1,591,000
30% Construction Contingency						\$477,000
15% Engineering Contingency						\$239,000
Total	· · · · · ·					\$2,307,000

(See Table C4 in Appendix C for details)

(See Tables C6 and C8 in Appendix C for details)

Facility Number	Road Crossing	Channel	Proposed 100-yr Flow (cfs)	Necessary Facility for Proposed 100-year Flow	Estimated Cost
301	Peyton Highway	Main Stem (MS-02)	3,370 .	9-6'X6' RCBs	\$402,000
403	Jones Road	Main Stem (MS-03)	2,970	8-6'X6' RCBs	\$358,000
405	Murr Road	Main Stem (MS-04)	2,870	8-6'X6' RCBs	\$283,000
609	Falcon Highway	Tributary 3 (T3-02)	460	2-6'X6' RCBs	\$106,000
N/A	Falcon Highway	Tributary 1 (T1)	110	2 - 36" RCP	\$20,000
1001	Future Pastura Street	Main Stem (MS-06)	610	2-6'X6' RCBs	\$107,000
1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	610	2-6'X6' RCBs	\$87,000
1003	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	530	2-6'X6' RCBs	\$87,000
1004	Future Pastura Street	Tributary 6 (T6)	440	2-66" RCPs	\$43,000
1005	Future El Vado Road	Tributary 6 (T6)	440	2-66" RCPs	\$43,000
1006	Future Socorro Trail	Tributary 6 (T6)	440	2-66" RCPs	\$43,000
Sub-Total	· · · · · · · · · · · · · · · · · · ·	\$1,582,000			
30% Constru	<del>.</del>	\$475,000			
15% Engine	· · · · · · ·	\$237,000			
Total		\$2,294,000			

# Table 6-16 Sub-Regional Detention Roadway Crossing Cost Estimate Summary

Table 6-18 Sub-Regional Detent Facility Storage (AF) **Including Construc** SR-01 10 SR-02 5 SR-03 16 SR-04 25 24 SR-05 SR-06 9 SR-07 5 SR-08 5 SR-09 20 23 SR-10 2 SR-11 SR-12 9 SR-13 3 Total

(See Table C1 in Appendix C for details)

# 6.4.3. Other Costs

Design Engineering costs are also included as 15% of the construction costs. Construction contingencies (30%) include such items as utility relocations, mobilization, temporary erosion control, and construction engineering.

# 6.4.4. Conceptual Alternative Costs

The total estimated capital costs for each alternative are based on the sum of the cost of the proposed facilities, plus costs for engineering and construction contingencies. These costs are listed in Table 6-19.

Table 6-19 Conceptual Alternative Costs						
	Regional Alternative	Subregional Alternative				
Detention Ponds	\$5,048,000	\$9,780,000				
Channel Improvements	\$10,737,000	\$2,110,000				
Drop Structures	\$9,988,000	\$3,442,000				
Roadway Crossing Culverts	\$2,307,000	\$2,294,000				
Total	\$28,080,000	\$17,627,000				

(See Tables C5 in Appendix C for details)

# 6.4.2. Detention Pond Costs

The cost of detention ponds, both regional and subregional, is based on the cubic yards of excavation, an estimated outlet structure, and the cost of the land required for the facility. These costs are presented in Table 6-17 and Table 6-18.

Table 6-17	Regional	Detention	Pond	Cost Summary

Facility	Storage (AF)	Total Cost Including Construction and Engineering Contingencies
RG-01 9.02	9.02	\$542,000
RG-02 64.52	64.52	\$4,053,000
RG-03 0.04	0.04	\$146,000
RG-04 1.07	1.07	\$160,000
RG-05 0.03	0.03	\$146,000
Total		\$5,048,000

(See Tables C1 in Appendix C for details)

tion Pond Cost Summary					
Total Cost					
ction and Engineering Contingencies					
\$899,000					
\$640,000					
\$868,000					
\$1,453,000					
\$1,557,000					
\$547,000					
\$524,000					
\$326,000					
\$861,000					
\$1,069,000					
\$182,000					
\$477,000					
\$376,000					
\$9,780,000					

# . .

May 2009 Page 65 impacted by site development, utility, roadway and landscape construction activities have in some cases negatively affected downstream areas.

El Paso County has enacted an erosion control ordinance to address these problems. In general, it is the responsibility of the entity conducting any land disturbance activity to properly control surface runoff, erosion and sedimentation during and after the activity. Technical criteria identifying measures which help mitigate the impacts of erosion and sedimentation are available and being used throughout the region. Minimum requirements must be developed to properly control erosion.

Erosion control is necessary to prevent environmental degradation caused by wind or water-borne soil. The following minimum criteria and standards are intended to prevent excessive erosion. El Paso County as well as other affected agencies will enforce the Clean Water Act standards if the planned erosion control measures fail to perform satisfactorily. Proper installation and maintenance is necessary to achieve the desired function of erosion control measures. By paying attention to quality, reinstallation can be avoided. General requirements for erosion control are as follows:

- 1. Any land disturbing activity shall be conducted so as to effectively reduce unacceptable erosion and resulting sedimentation.
- 2. All land disturbing activities shall be designed, constructed, and completed in such a manner that the exposure time of disturbed land shall be limited to the shortest possible period of time.
- 3. Sediment caused by accelerated soil erosion and runoff shall be intercepted by erosion control measures such as hay bales, silt fences and / or sediment ponds, and contained within the site.
- 4. Any facility designed and constructed to convey storm runoff shall be designed to be non-erosive.
- 5. Erosion control measures will be used prior to and during construction.

Temporary erosion control measures are required during construction, and permanent erosion control measures are required for all developments. Maintenance of erosion control measures is the responsibility of the property owner.

Various structures have been proposed in this plan to help control localized erosion and sedimentation problems. It is important that the erosion control plan for any land disturbing activity be strictly adhered to and maintained so that the above minimum criteria can be achieved in the Haegler Ranch Basin.

# 7.4. Operations and Maintenance

Maintenance of drainage way facilities is essential in preventing long term degradation of the creek and overbank areas. Along the drainageway, clearing of debris and dead vegetation should be considered within the low flow area of the creek and its tributaries. On the overbanks, limited maintenance of the existing vegetative cover is recommended. Semi-annual clearing of trash and debris at roadway crossings is also recommended to increase the effectiveness of the crossings. Sediments cleared from the channel or culvert should not be left on the overbank. This disturbs the native vegetation, creates a potential water quality concern if the dredgings are subsequently washed into the drainageway by natural erosion, and reduces the capacity of the overbank. In those reaches designated to be selectively

lined and the floodplain preserved, maintenance activities should be carried out with the least disturbances to native vegetation that is practical.

Similar practices should be employed when removing sediment from detention basins. Although some channels degrade and others agrade, all detention basins will collect sediment and agrade. The use of an easily accessible concrete lined forebay in the final design of a detention facility can make the cleaning of the larger debris and trash more easily accomplished with motorized equipment. If forebays are provided, they will need clearing semi-annually and after major storm events. More frequent routine maintenance may be required depending on the type of development upstream and the access provided to the public. Plan for annual removal of sediment and debris from the detention area of a facility with a forebay.

Deposition in drainage facilities of wind-blown trash and debris, should be expected in this region. This means that regular maintenance, even without rainfall events, should be performed.

# 7.5. Drainage and Bridge Fee Calculations

The cost estimates and basin fee calculation for the major drainageways, tributary drainageways, roadway culverts, regional detention basins, and related improvements for the Sub-Regional Detention Facilities are presented in Table 7-2. The sub-regional detention capital construction cost estimates include the cost for the construction of the embankment, water quality, and outlet structures. Bridges in the Sub-Regional Detention Alternative are presented in Table 7-3. The cost estimates include engineering and construction costs for the entire Haegler Ranch Basin as presented on the Conceptual Design Drawings in Appendix D. These estimates do not include costs for local or initial systems, and therefore no costs attributable to local or minor drainage systems have been computed in the estimation of the drainage basin fee. These systems are expected to be provided with proposed development. Costs associated with utility relocations have not been estimated but would be included in construction contingencies. A review of utility maps indicates that the majority of the potential relocations occur at the roadway crossings. Land acquisition costs for the detention facilities were not included for calculation of fees per Appendix L of the El Paso County Criteria Manual.

Unplatted acreage within Haegler Ranch was obtained from El Paso County, and is shown in Figure 7-1. A total of 8,953 acres is estimated to be currently unplatted and subject to future development. This unplatted land is projected to have an average imperviousness of approximately 15%, corresponding to approximately 1,343 unplatted impervious acres. All drainage and bridge fees are calculated per *impervious* acre. (See Appendix D for an unplatted area breakdown by subbasin and average imperviousness calculations.)

Reimbursable costs calculated for the Haegler Ranch Basin are listed in Table 7-4. These costs are based on improvements required under existing conditions. The term "reimbursable costs" used on Table 7-4 means those costs that have been used in estimation of drainage basin fees. Costs considered "non-reimbursable" are costs for the replacement of existing, undersized culverts, or costs to rehabilitate or maintain an existing lined segment of drainageway. For the most part, all of the drainageway costs for Haegler Ranch Basin are considered reimbursable.

The calculated drainage basin fee presented in Table 7-2 is \$7,633 per impervious acre, and the bridge fee is \$1,126 per impervious acre, as shown in Table 7-3.

# Table 7-2 Drainage Basin Fec Calculations

		Channel Improvemen			
Channel	Basins	Channel Construction Cost	Drop Structure Construction Cost	Contingency Cost	Total Cost
Main Stem (MS-05)	HR0200	\$224,000	\$363,600	\$264,420	\$852,020
Main Stem (MS-06)	HR0070	\$162,000	\$295,400	\$205,830	\$633,230
Main Stem (MS-06)	HR0080	\$331,000	\$374,500	\$317,475	\$1,022,975
Main Stem (MS-06)	HR0090	\$188,000	\$368,000	\$250,200	\$806,200
Tributary 3 (T3-01)	HR0330	\$259,000	\$422,000	\$306,450	\$987,450
Tributary 3 (T3-02)	HR0300	\$18,000	\$37,000	\$24,750	\$79,750
Tributary 4 (T4)	HR0300	\$40,000	\$74,000	\$51,300	\$165,300
Tributary 6 (T6)	HR0110	\$179,000	\$333,000	\$230,400	\$742,400
Tributary 6 (T6)	HR0120	\$55,000	\$106,500	\$72,675	\$234,175
Subtotal Channel Cost	<u>s</u>				\$5,553,500
		<b>Culvert Improvement</b>	5		
Culvert	Road Crossing	Channel	Culvert Construction Cost	Contingency Cost	Total Cost
609	Falcon Highway	Tributary 3 (T3-02)	\$106,301	\$47,836	\$154,137
N/A	Falcon Highway	Tributary 1 (T1)	\$19,500	\$8,775	\$28,275
1001	Future Pastura Street	Main Stem (MS-06)	\$106,301	\$47,836	\$154,137
- 1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	\$87,301	\$39,286	\$126,587
1003	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	\$87,301	\$39,286	\$126,587
1004	Future Pasture Street	Tributary 6 (T6)	\$51,000	\$22,950	\$73,950
1005	Future El Vado Road	Tributary 6 (T6)	\$19,500	\$8,775	\$28,275
1006	Future Socorro Trail	Tributary 6 (T6)	\$42,800	\$19,260	\$62,060
Subtotal Culvert Costs					\$754,007
		Detention Improvemen	nts		
				Contingency	
Facility	Storage (AF)	<b>Construction Cost</b>		Cost	Total Cost
SR-01	10	\$296,701		\$133,516	\$430,217
SR-02	5	\$207,949		\$93,577	\$301,525
SR-03	16	\$186,252		\$83,814	\$270,066
SR-04	25	\$390,182		\$175,582	\$565,764
SR-05	24	\$455,235		\$204,856	\$660,091
SR-06	9	\$140,670		\$63,301	\$203,971
SR-07	5	\$162,046		\$72,921	\$234,967
SR-08	5	\$87,489		\$39,370	\$126,860
SR-09	20	\$188,250		\$84,713	\$272,963
SR-10	23	\$331,635		\$149,236	\$480,871
SR-11	2	\$56,880		\$25,596	\$82,476
SR-12	9	\$108,987		\$49,044	\$158,031
SR-13	3	\$107,812		\$48,515	\$156,327
Subtotal Detention Co	sts		· · · · · · · · · · · · · · · · · · ·		\$3,944,129
Total Cost	<u> </u>				\$10,251,636
Total Unplatted Impo	ervious Acres	··· ··· ··· ···	· · · · · · · · · · · · · · · · · · ·	<u> </u>	1,343
Fee Per Impervious A					\$7,633

# Table 7-3 Bridge Fce Calculation

301	Peyton Highway	Main Stem (MS-02)	401,710	\$180,770	\$582,480
403	Jones Road	Main Stem (MS-03)	358,123	\$161,155	\$519,278
405	Murr Road	Main Stem (MS-04)	282,941	\$127,323	\$410,264
Subtotal		\$1,512,022			
Total Co		\$1,512,022			
Total Un		1,343			
Bridge F		\$1,126			

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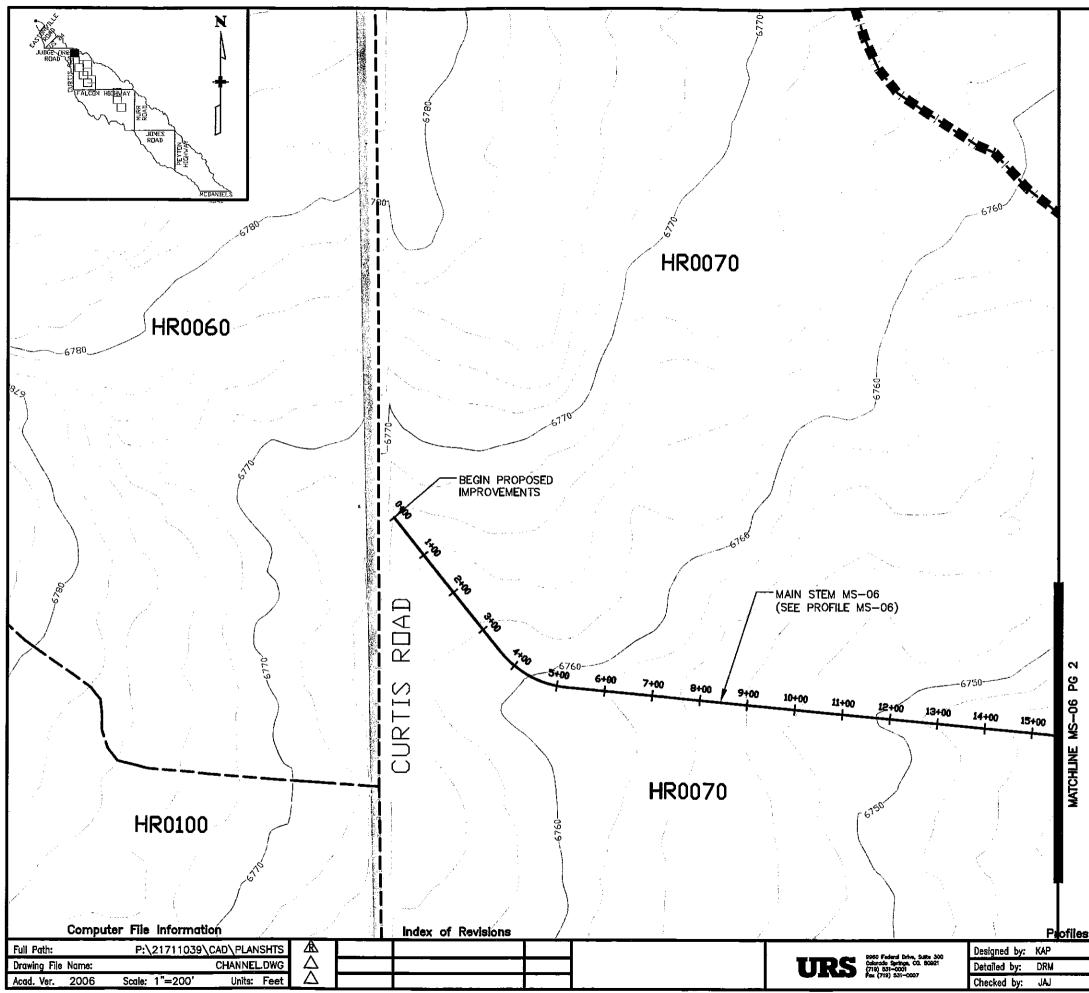
May 2009 Page 69

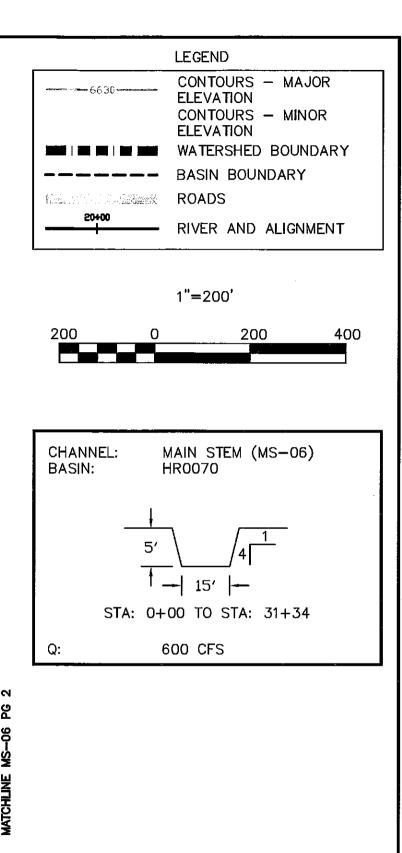
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		7-4 Reimbursable			
	Keimbi	irsable Culvert Impro	vements Culvert		
			Construction	Contingency	
Culvert	Road Crossing	Channel	Cost	Cost	Total Cost
N/A	Peyton Highway	Tributary 1 (T1)	\$51,000	\$22,950	\$73,950
N/A	Falcon Highway	Tributary 1 (T1)	\$9,7580	\$4,388	\$14,138
301	Peyton Highway	Main Stem (MS-02)	\$314,535	\$141,541	\$456,076
401	Jones Road	Tributary 1 (T1)	\$53,111	\$23,900	\$77,011
403	Jones Road	Main Stem (MS-03)	\$270,947	\$121,926	\$392,874
405	Murr Road	Main Stem (MS-04)	\$180,371	\$81,167	\$261,538
407	Murr Road	Tributary 3 (T3-01)	\$77,801	\$35,011	\$112,812
507	Peerless Farms Road	Tributary 3 (T3-01)	\$115,801	\$52,111	\$167,912
509	Murr Road	Tributary 1 (T1)	\$19,300	\$8,685	\$27,985
601	Whiting Way	Tributary 1 (T1)	\$23,500	\$10,575	\$34,075
604	Max Road	Tributary 1 (T1)	\$19,300	\$8,685	\$27,985
609	Falcon Highway	Tributary 3 (T3-02)	\$25,600	\$11,520	\$37,120
610	Falcon Highway	Tributary 4 (T4)	\$23,500	\$10,575	\$34,075
612	Falcon Highway	Tributary 5 (T5)	\$21,200	\$9,540	\$30,740
628	Falcon Highway	Main Stem (MS-05)	\$154,741	\$69,633	\$30,740 \$224,375
702	Curtis Road	Tributary 6 (T6)			
703	Curtis Road	Main Stem (MS-06)	\$23,150	\$10,418	\$33,568
704	· · · · · · · · · · · · · · · · · · ·		\$125,301	\$56,386	\$181,687
	Judge Orr Road	Main Stem (MS-06)	\$83,200	\$37,440	\$120,640
803	Eastonville Road	Main Stem (MS ¹ 07)	\$9,680	\$4,356	\$14,036
804	Eastonville Road	Tributary 7 (T7)	\$14,980	\$6,741	\$21,721
Subtotal Channel Costs					\$2,344,315
	Reimbu	sable Detention Impr	ovements		
Facility	Cfarman (ATD)			Contingency	
SR-01	Storage (AF)	Construction Cost		Cost	Total Cost
SR-01 SR-02	5	\$296,701 \$207,949		\$133,516	\$430,217
<u>SR-02</u>	16	\$186,252		\$93,577 \$83,814	\$301,525 \$270,066
SR-04	25	\$390,182		\$175,582	\$565,764
SR-05	24	\$455,235		\$204,856	\$660,091
SR-06	9	\$140,670		\$63,301	\$203,971
SR-07	5	\$162,046		\$72,921	\$234,967
SR-08	5	\$87,489		\$39,370	\$126,860
SR-09	20	\$188,250		\$84,713	\$272,963
SR-10	23	\$331,635		\$149,236	\$480,871
SR-11	2	\$56,880		\$25,596	\$82,476
SR-12	9	\$108,987		\$49,044	\$158,031
SR-13	3	\$107,812	<u> </u>	\$48,515	\$156,327
Subtotal Detention Cos		<u> </u>	····		\$3,944,129
Total Reimbursable C	ost				\$6,288,444

Table 7-4 Reimbursable Costs

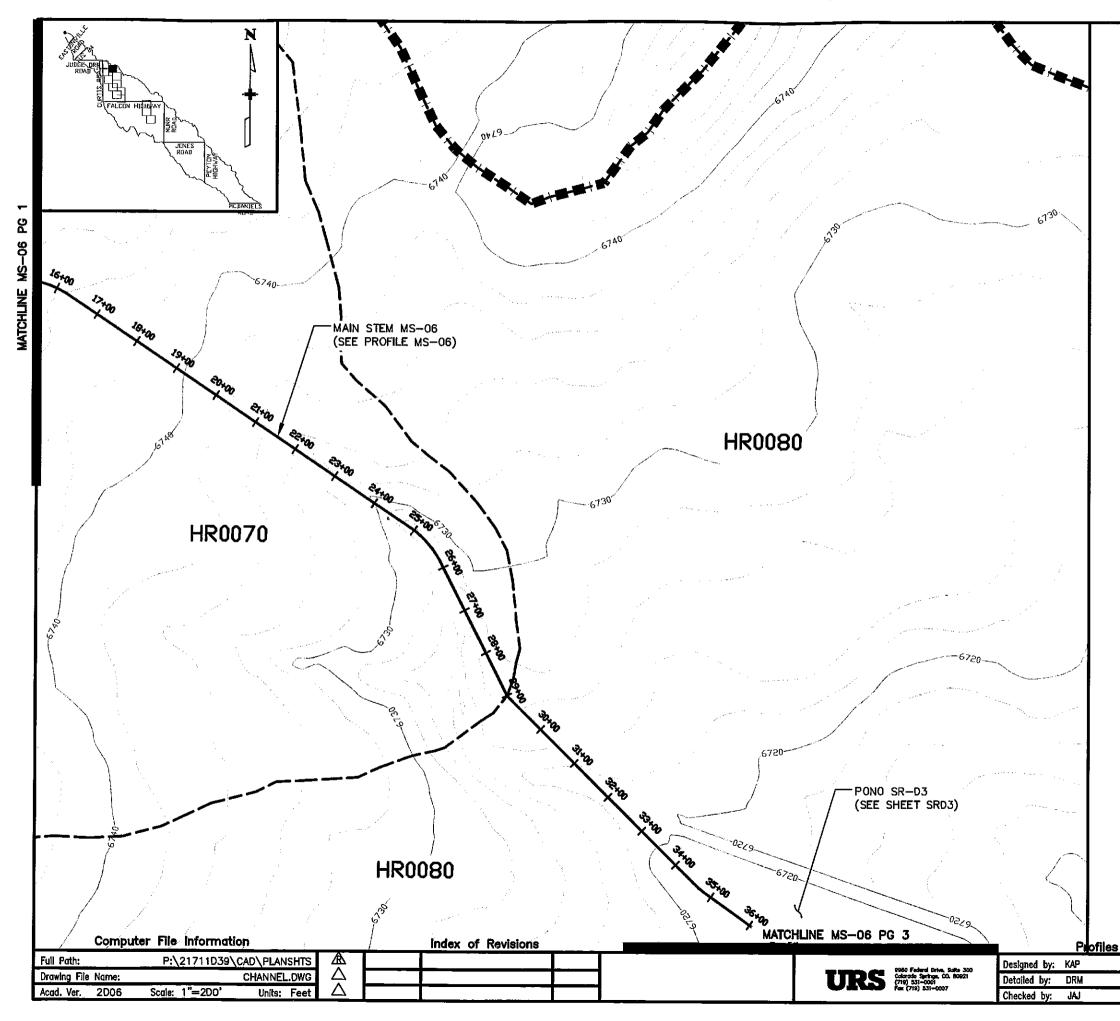
Haegler Ranch Drainage Basin Planning Study .

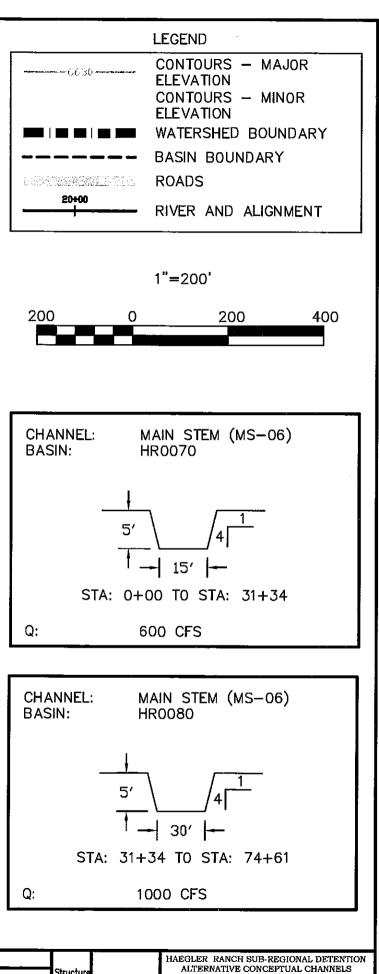




HAEGLER RANCH SUB-REGIONAL DETENTION ALTERNATIVE CONCEPTUAL CHANNELS Structur lumbe MAIN STEM PG Sheet Number

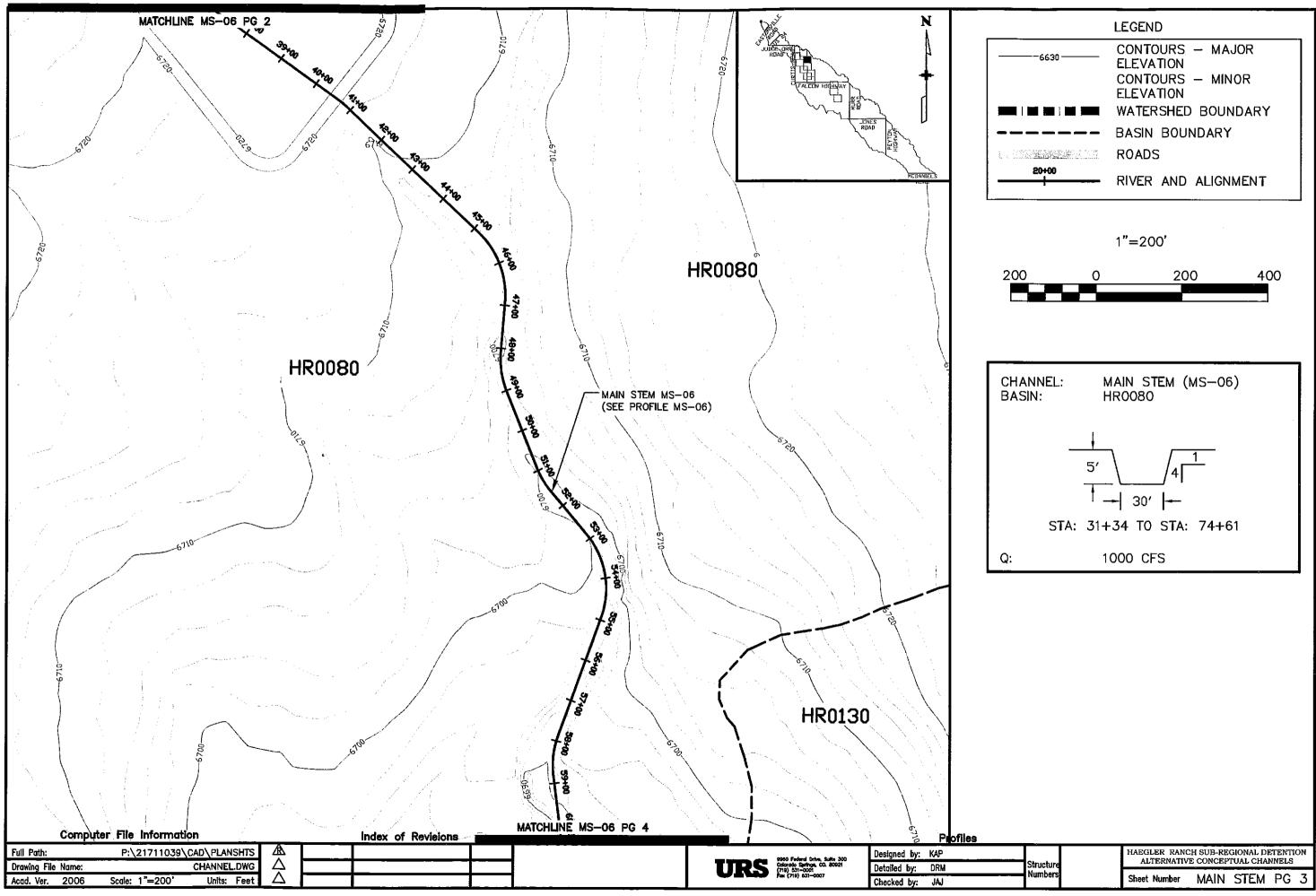
g 90 Ś MATCHLINE

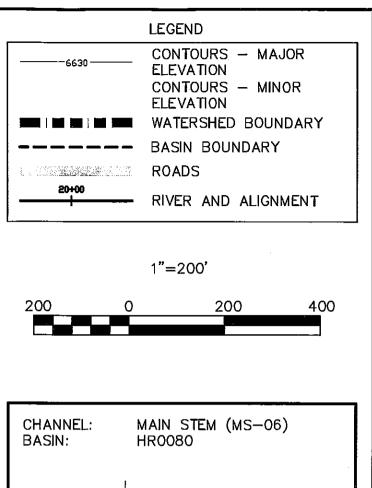


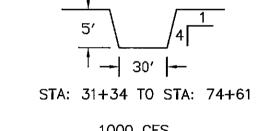


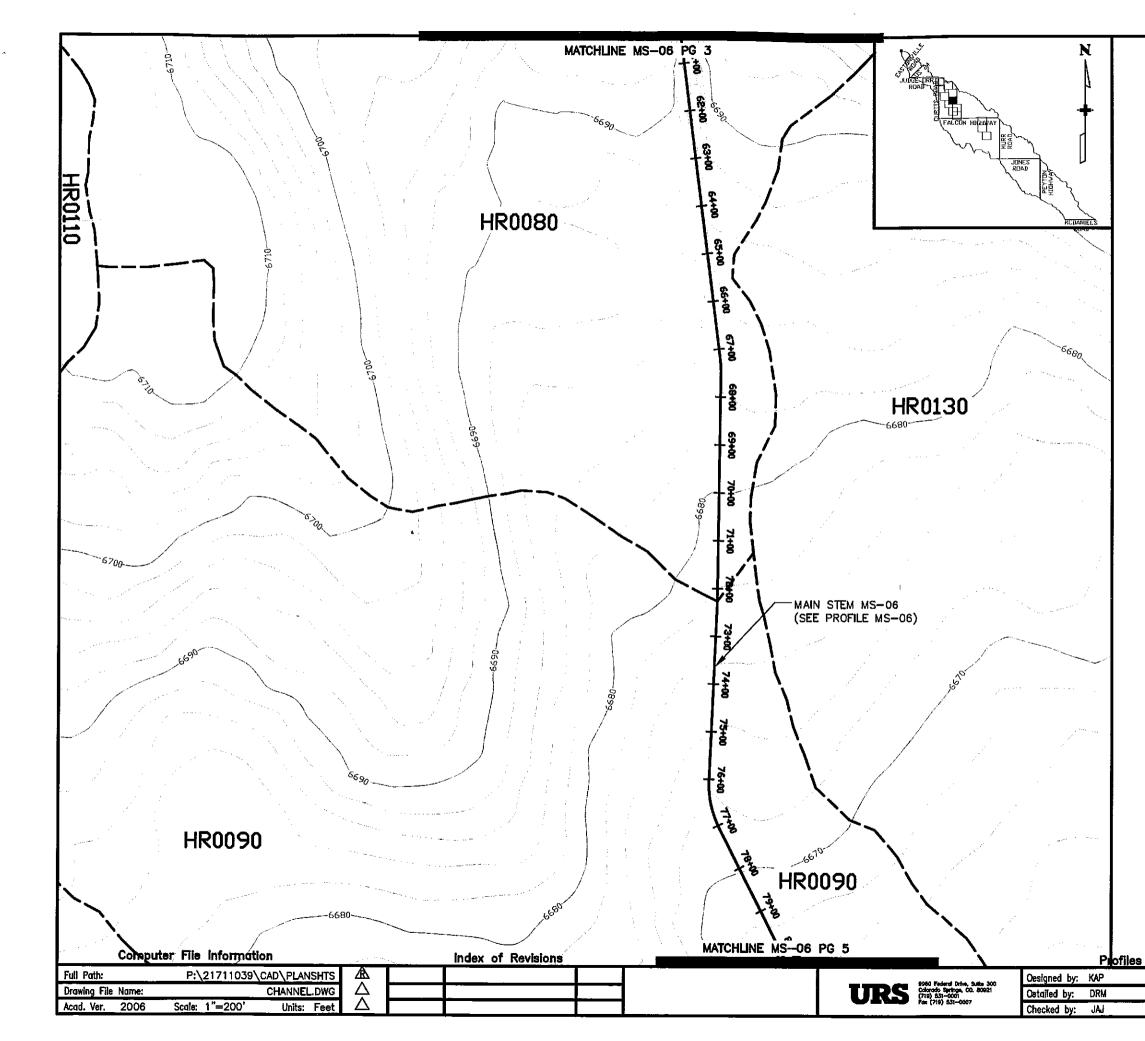
Structure ALTERNATIVE CO Numbers Sheet Number M

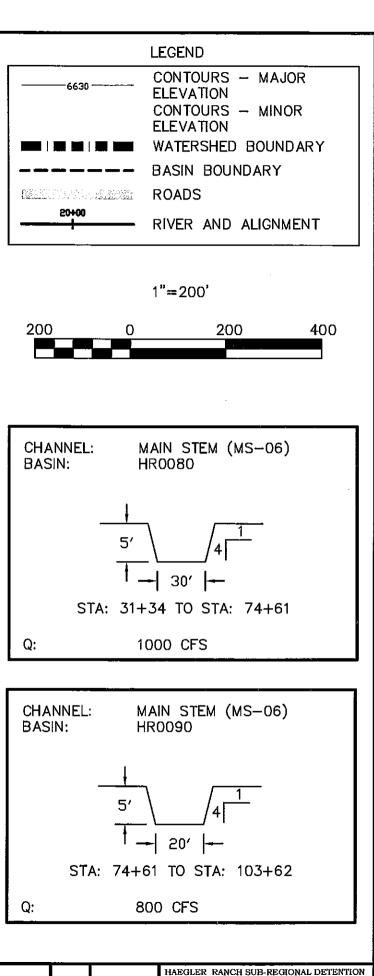
ALTERNATIVE CONCEPTUAL CHANNELS Sheet Number MAIN STEM PG 2



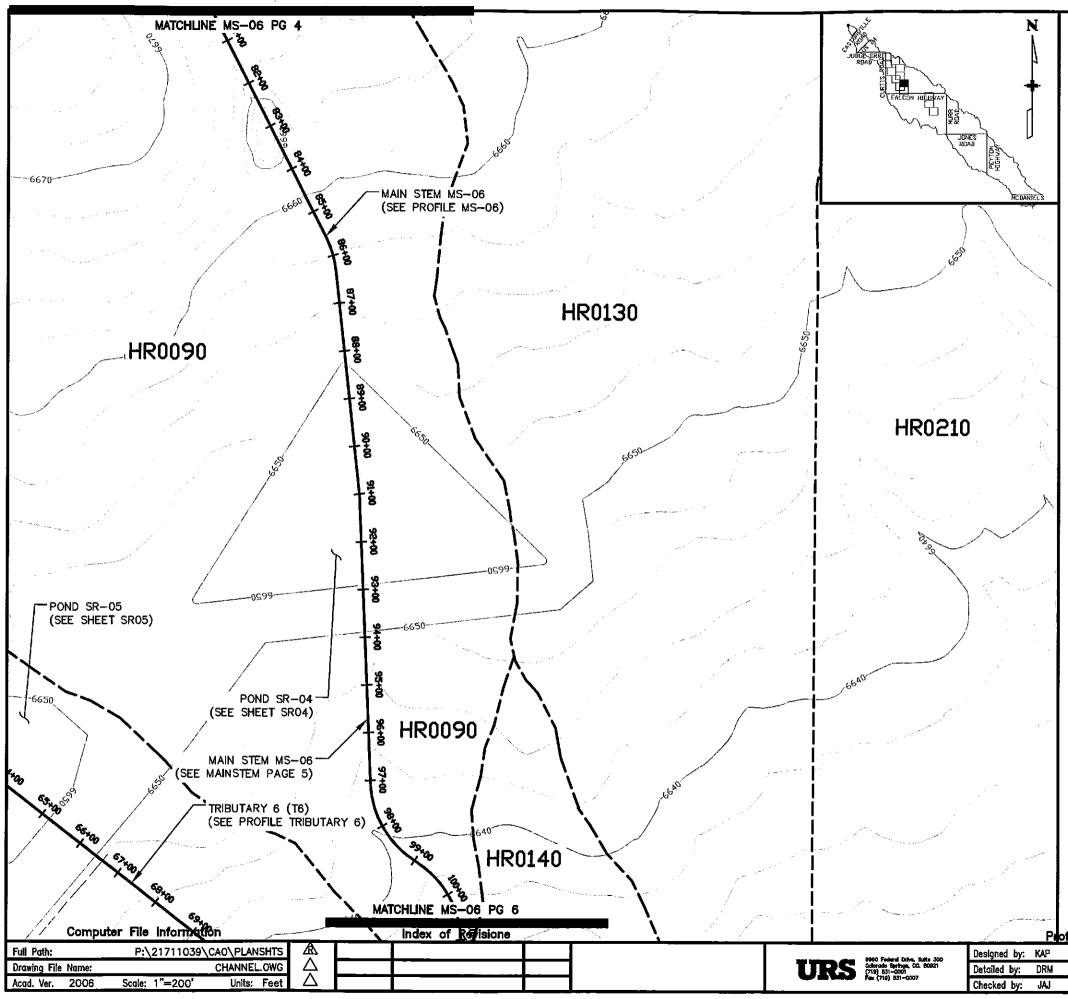


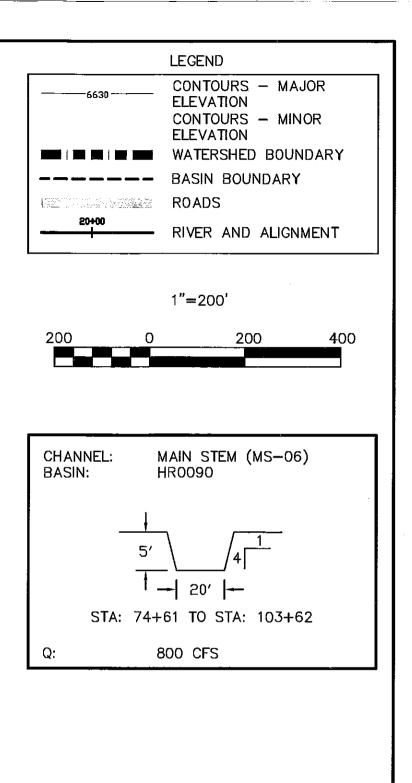




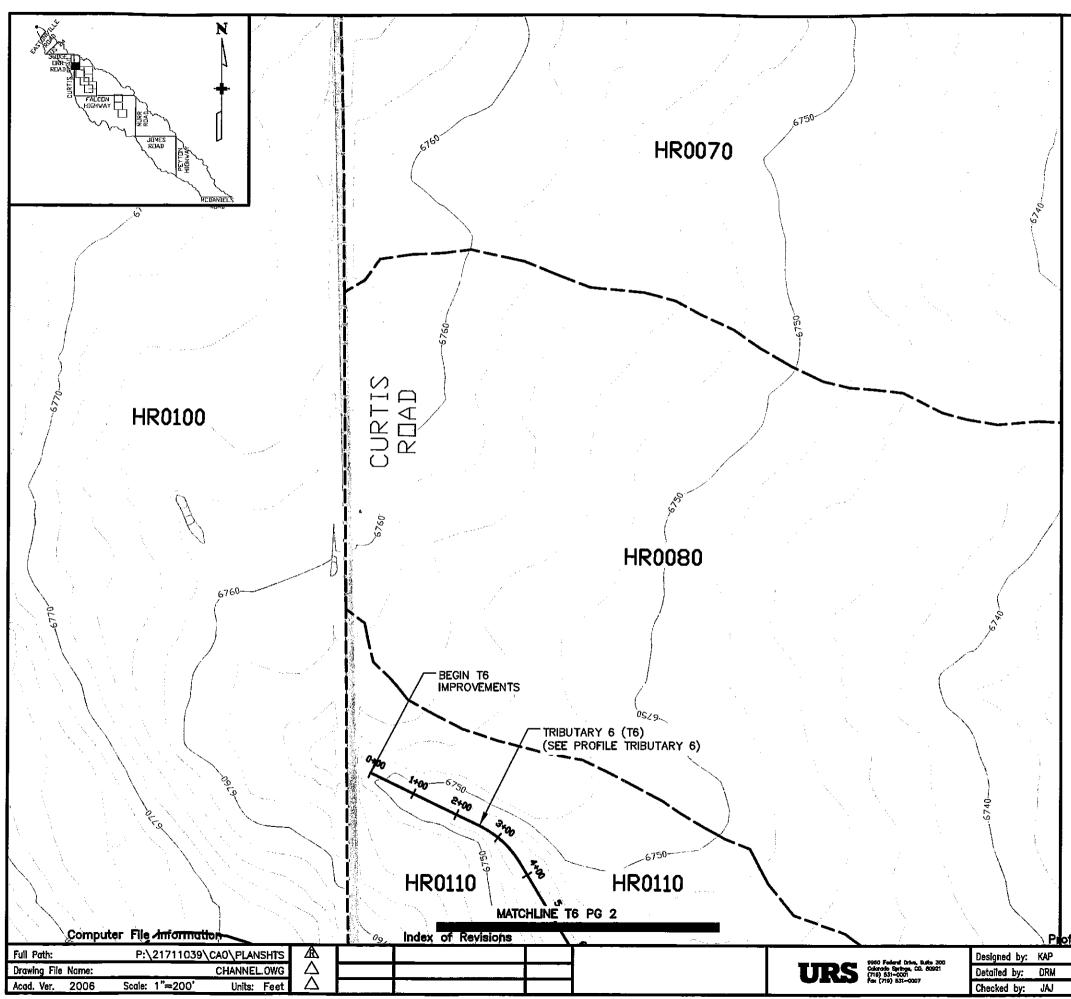


Structure Numbers Sheet Number MAIN STEM PG 4

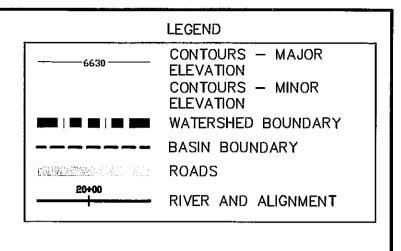




Structure	HAEGLER RANCH SUB-REGIONAL DETENTION ALTERNATIVE CONCEPTUAL CHANNELS				
irs	Sheet Number	MAIN	STEM	PG	5
		AL'TERNATIV	ALTERNATIVE CONCEP	ALTERNATIVE CONCEPTUAL CHAR	ALTERNATIVE CONCEPTUAL CHANNELS

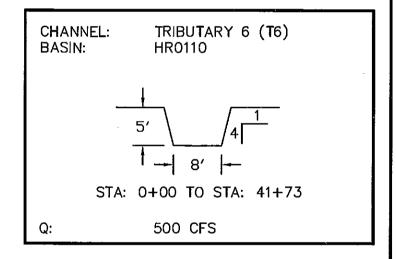




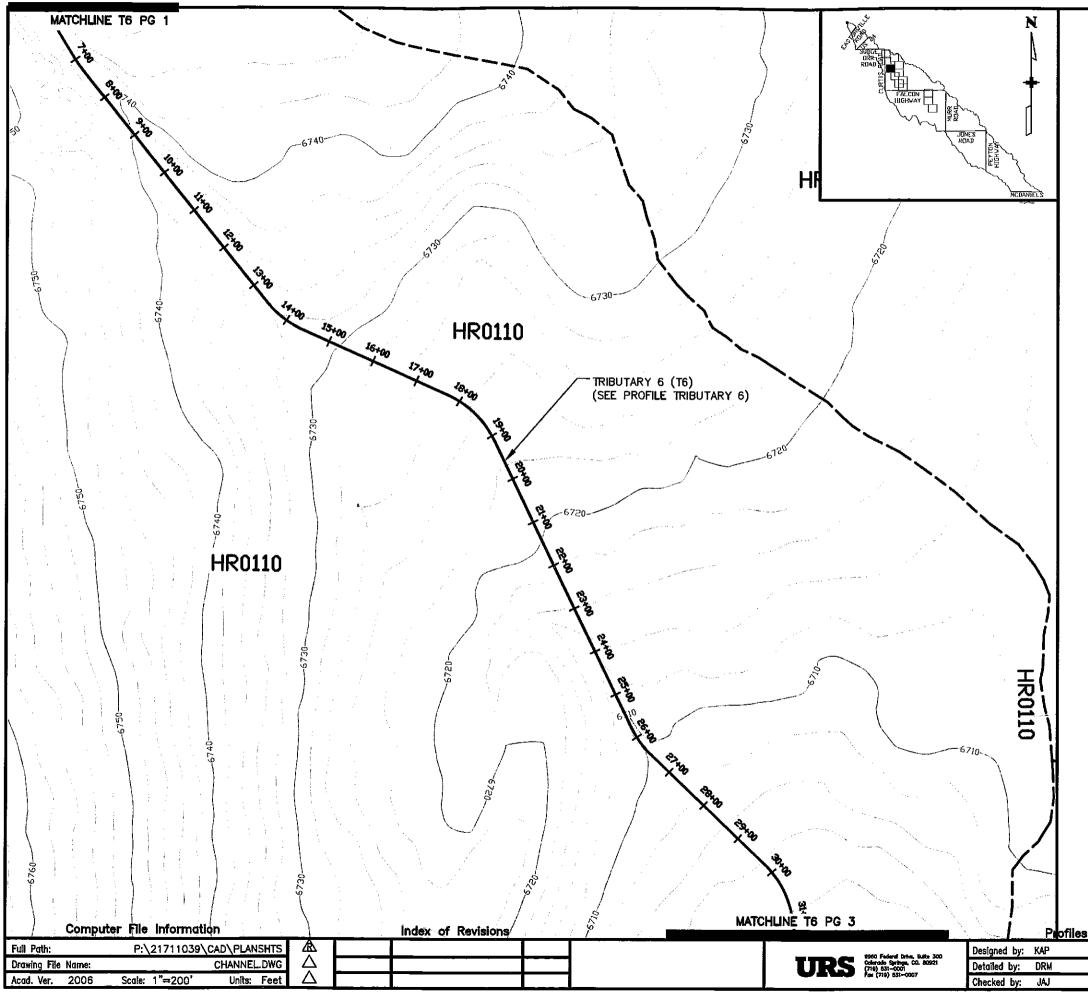


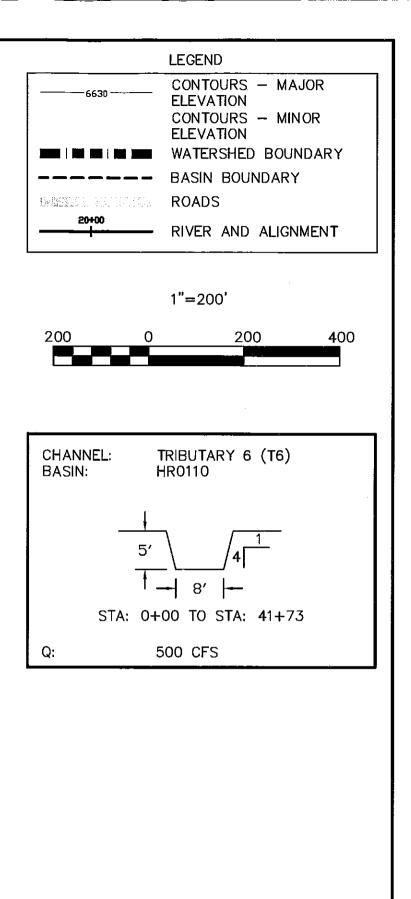
1"=200'





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HAEGLER RANCH SUB-REGIONAL ALTERNATIVE CONCEPTUAL CH		NC
Numbers Sheet Number TRIBUTARY	6 PG	1

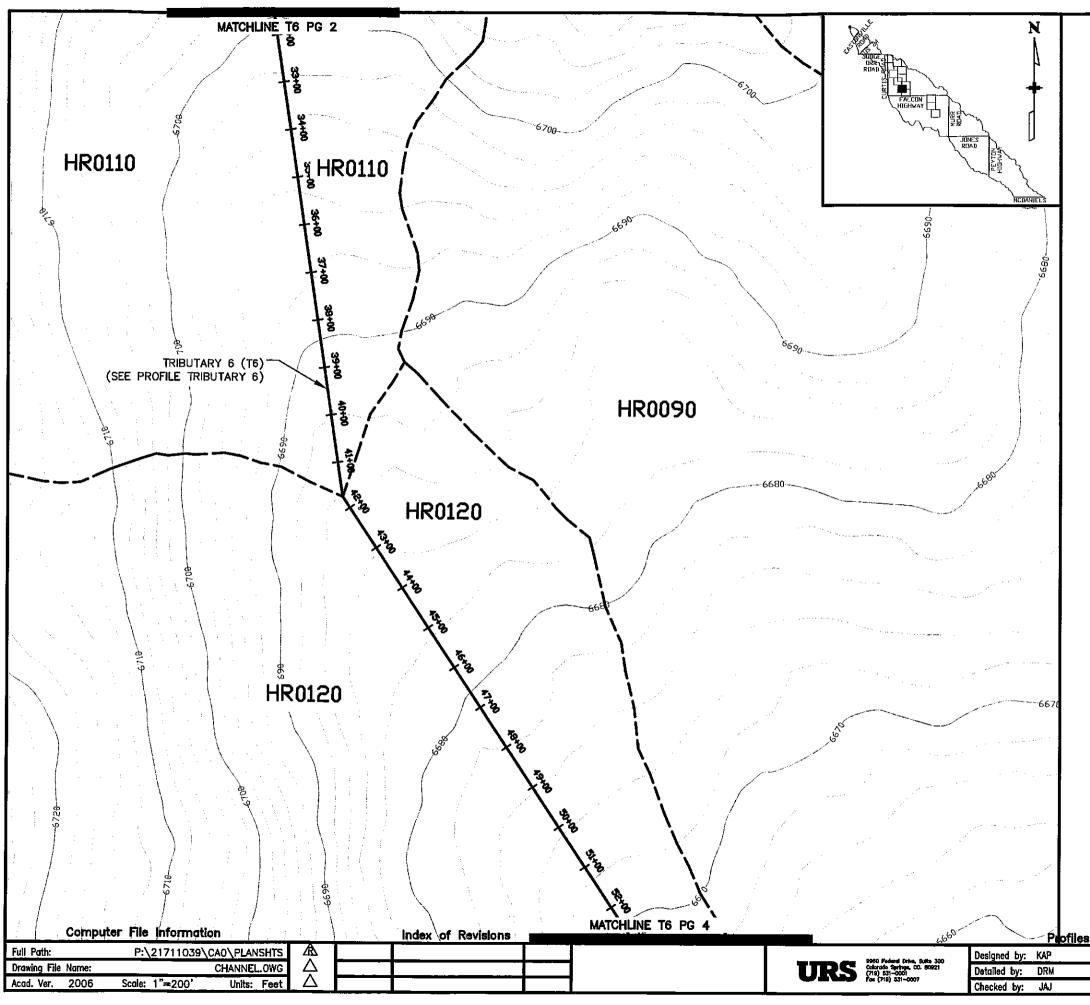


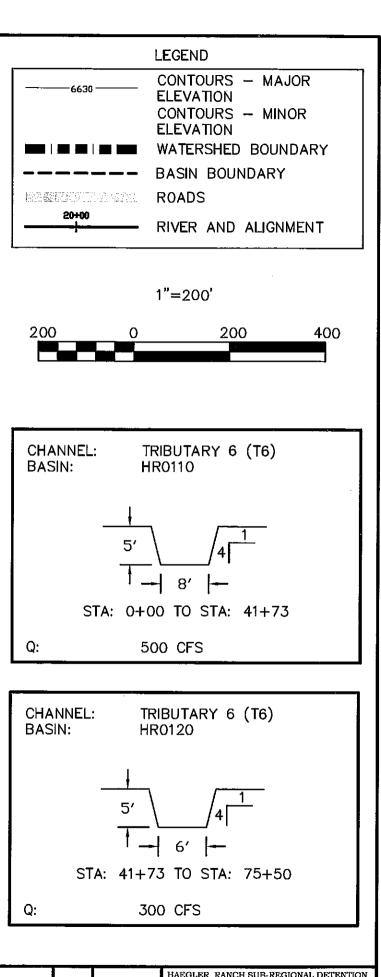


 Structure
 HAEGLER RANCH SUB-REGIONAL DETENTION

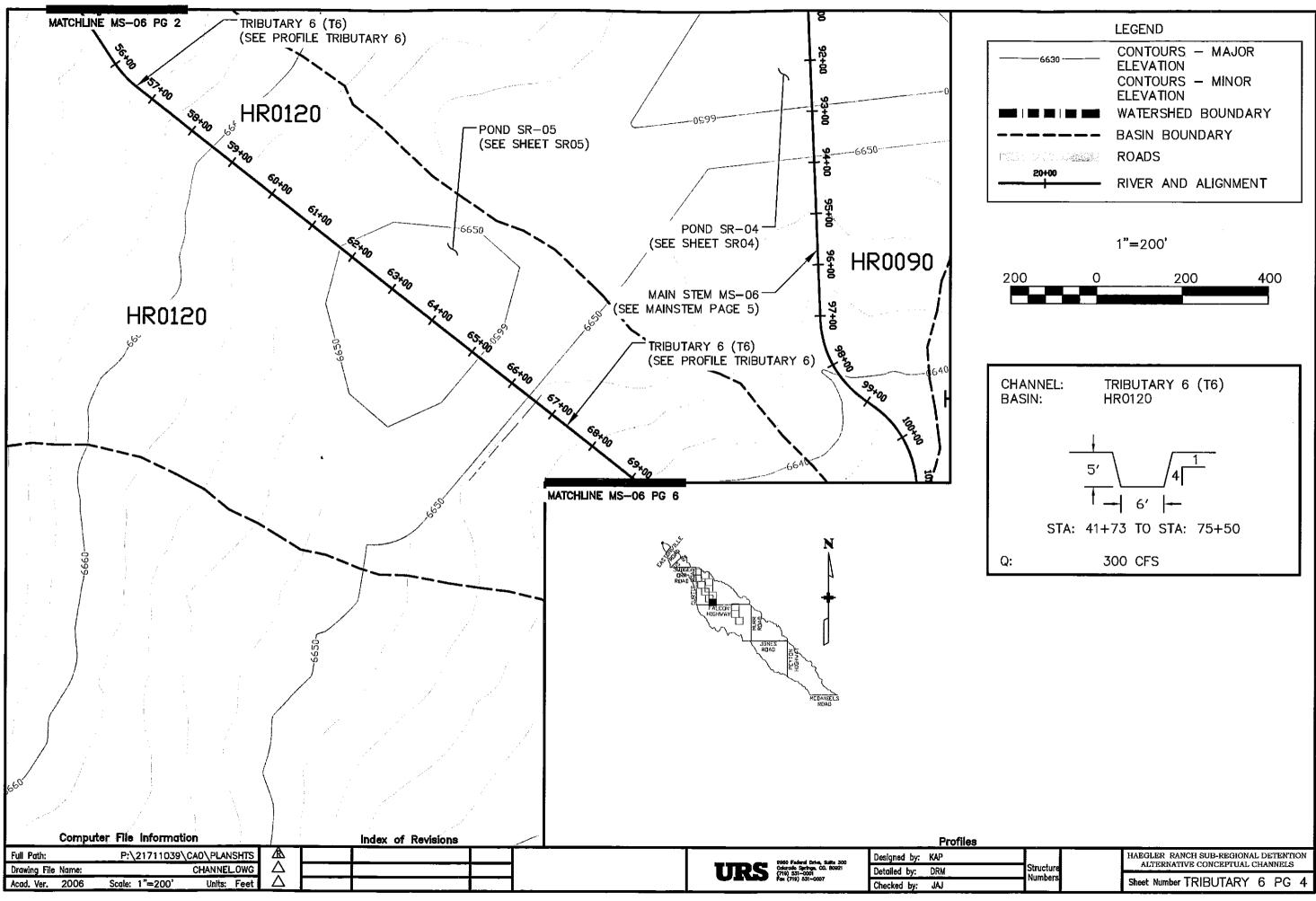
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 ALTERNATIVE CONCEPTUAL CHANNELS

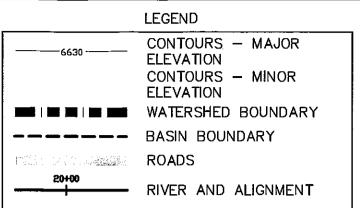
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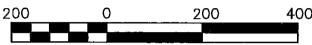


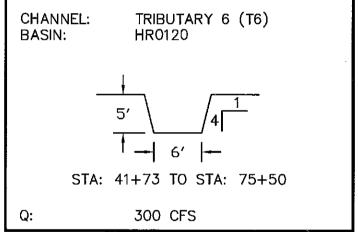


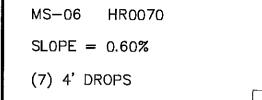
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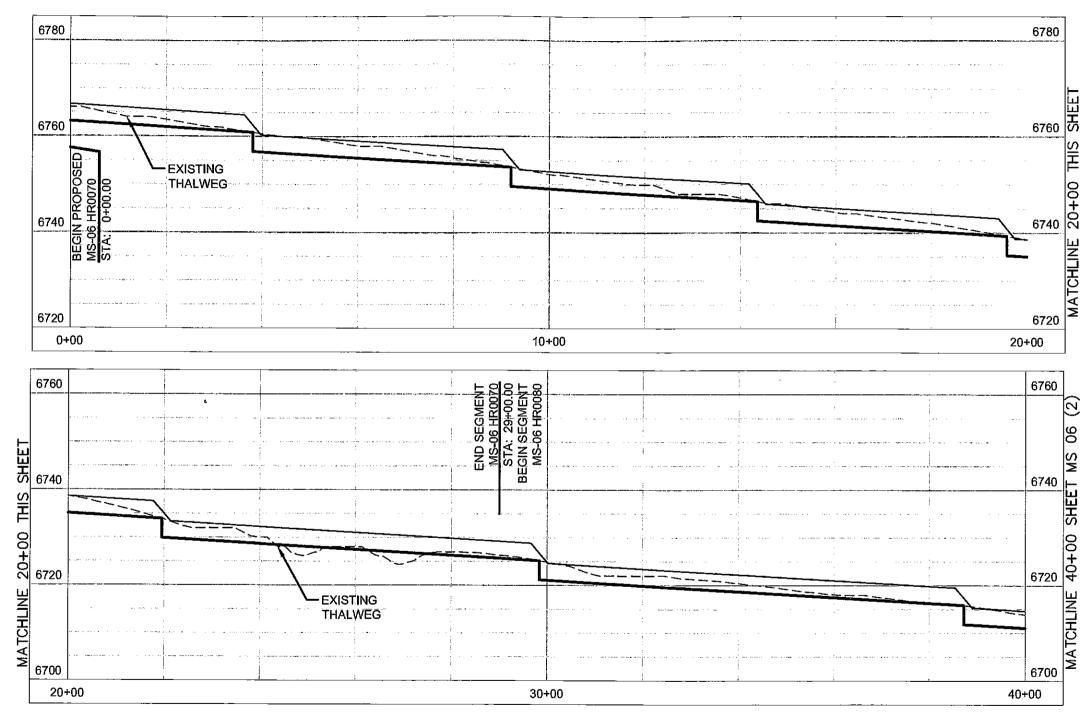




MS-06 HR0080

SLOPE = 0.60%

(7) 4' DROPS



PROFILE MAIN STEM (MS-06 & MS-05)

Computer File Information	Index of Revisions		Profiles	
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Acad. Ver. 20D6 Scale: 1"=2D' Units: Feet		DEPARTMENT OF RANSPORTATION DEPARTMENT OF RANSPORTATION Created Stream C (710) 331-0001 Par (710) 331-0001	Detailed by: DRM Structure The checked by:	Sheet Number MS 06

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 PROPOSED DROP STRUCTURE
 EXISTING THALWEG
 HYDRAULIC GRADE LINE



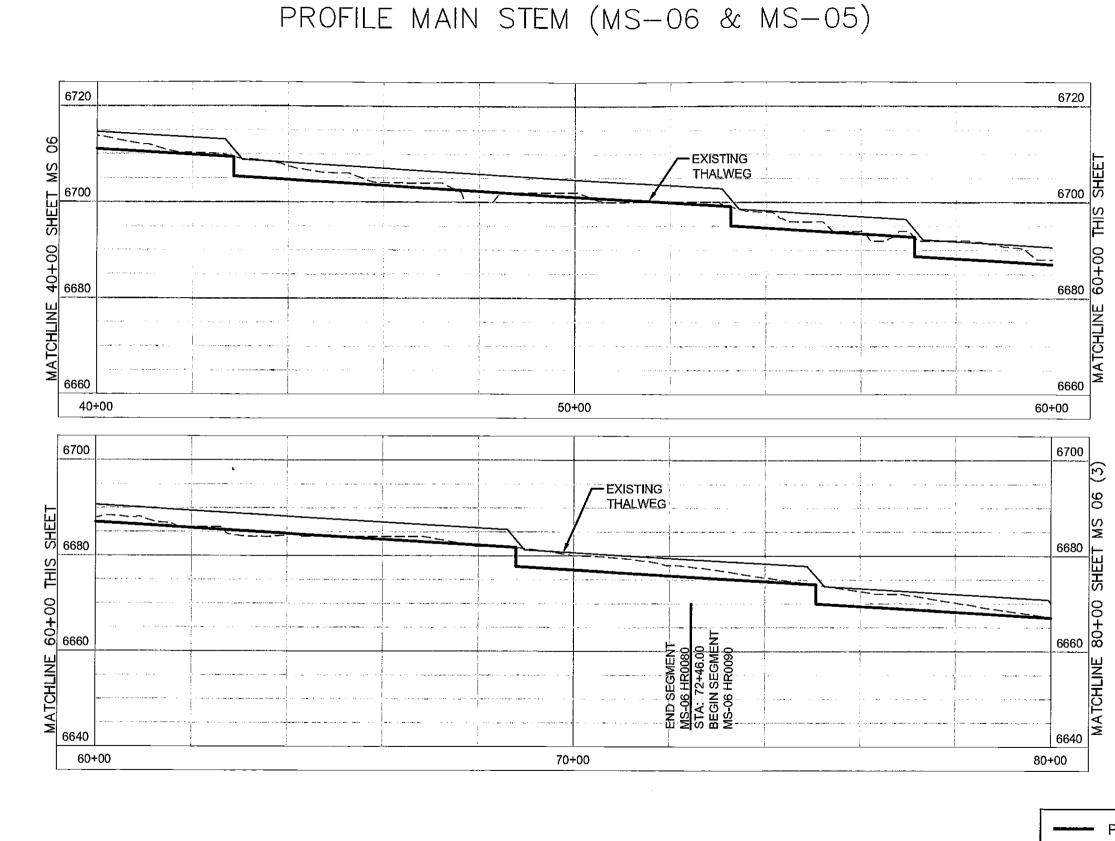
SLOPE = 0.60%

(7) 4' DROPS

MS-06 HR0090

SLOPE = 0.60%

(8) 4' DROPS



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Acad. Ver. 2006 Scale: 1"=20' Units: Feet		(715) S31-0001 Detailed by: Ditm	Sheet Number MSO6 (2)

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----- PROPOSED DROP STRUCTURE ---- EXISTING THALWEG ------ HYDRAULIC GRADE LINE



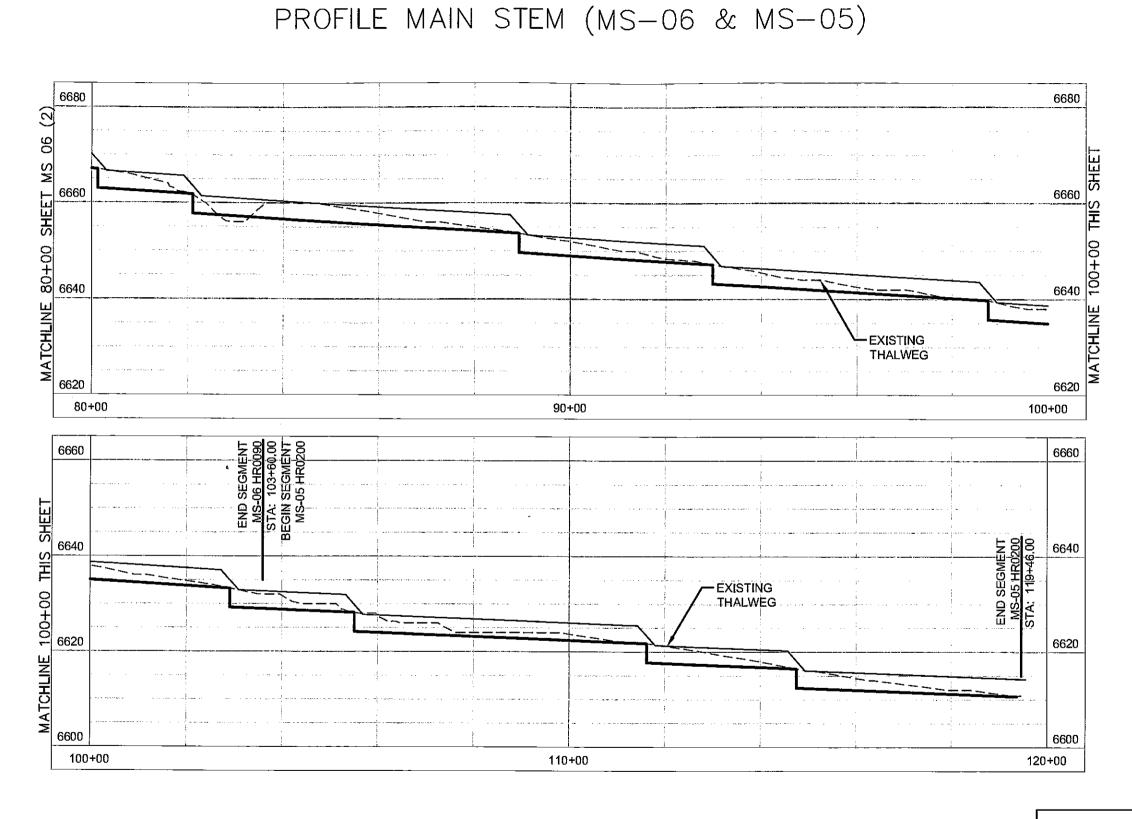
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(8) 4' DROPS

MS-05 HR0200

SLOPE = 0.40%

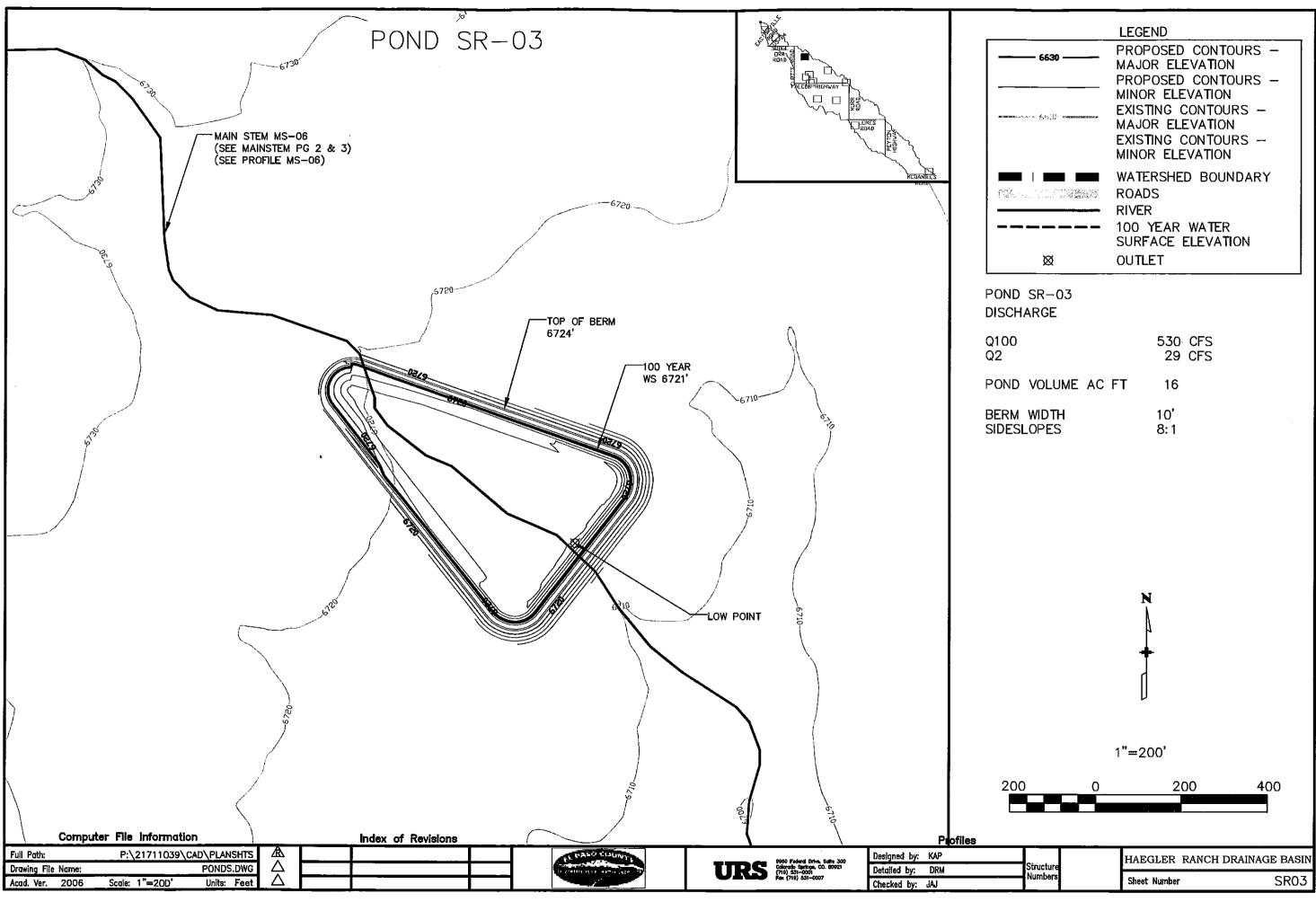
(4) 4' DROPS

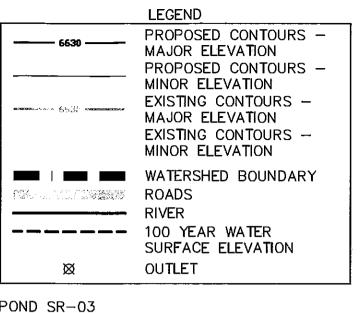


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Drawing File Name: MAINSTEM PROFILES_PROPOSED.DWG Acad. Ver. 2006 Scale: 1"=20' Units: Feet		URS CONTRACTOR STORE	Detailed by: DRM Structure Numbers	Sheet Number MS06 & MS05 (3)
Acad. Ver. 2006 Scale: 1 = 20 Units: Feet			Checked by:	

### LEGEND

PROPOSED DROP STRUCTURE
 EXISTING THALWEG
 HYDRAULIC GRADE LINE

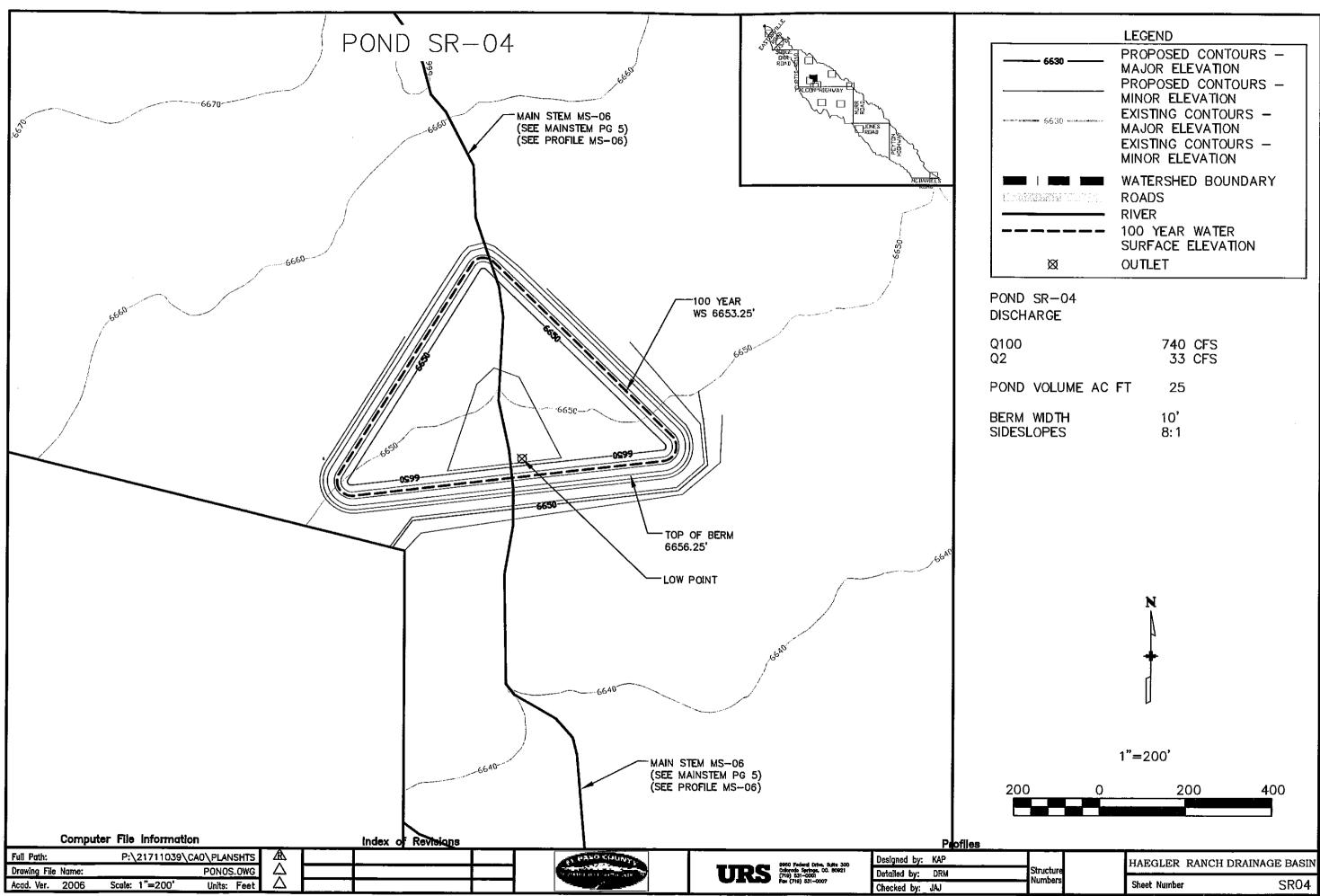


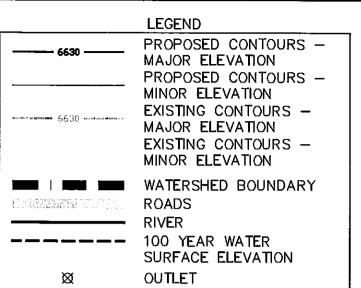


Q100	530 CFS
Q2	29 CFS
POND VOLUME AC FT	16
BERM WIDTH	10'
SIDESLOPES	8:1

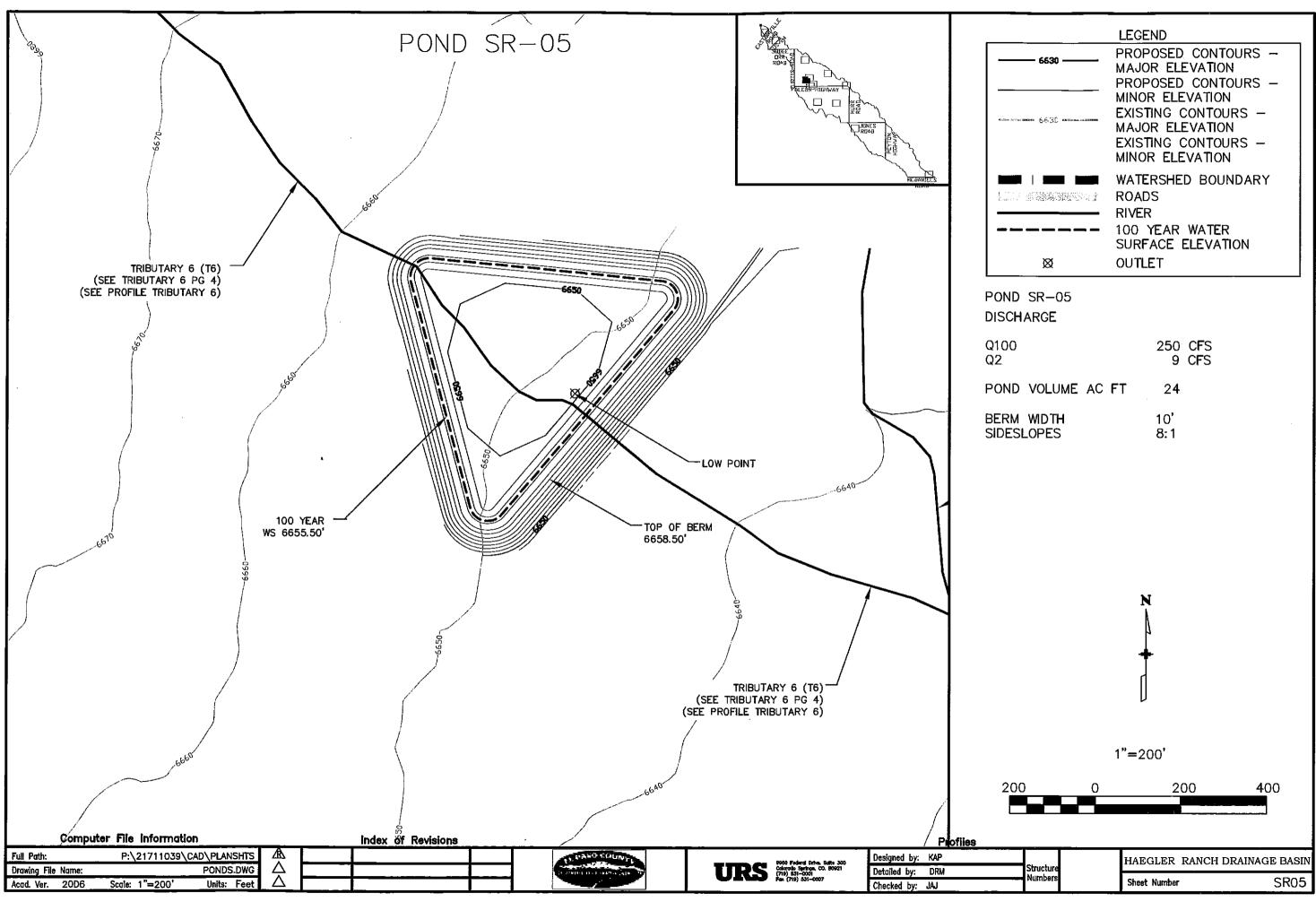


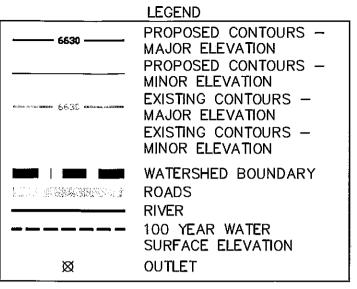






Q100	740 CFS
Q2	33 CFS
POND VOLUME AC FT	25
BERM WIDTH	10'
SIDESLOPES	8:1





Q100	250 CFS
Q2	9 CFS
POND VOLUME AC FT	24
BERM WIDTH	10'
SIDESLOPES	8:1



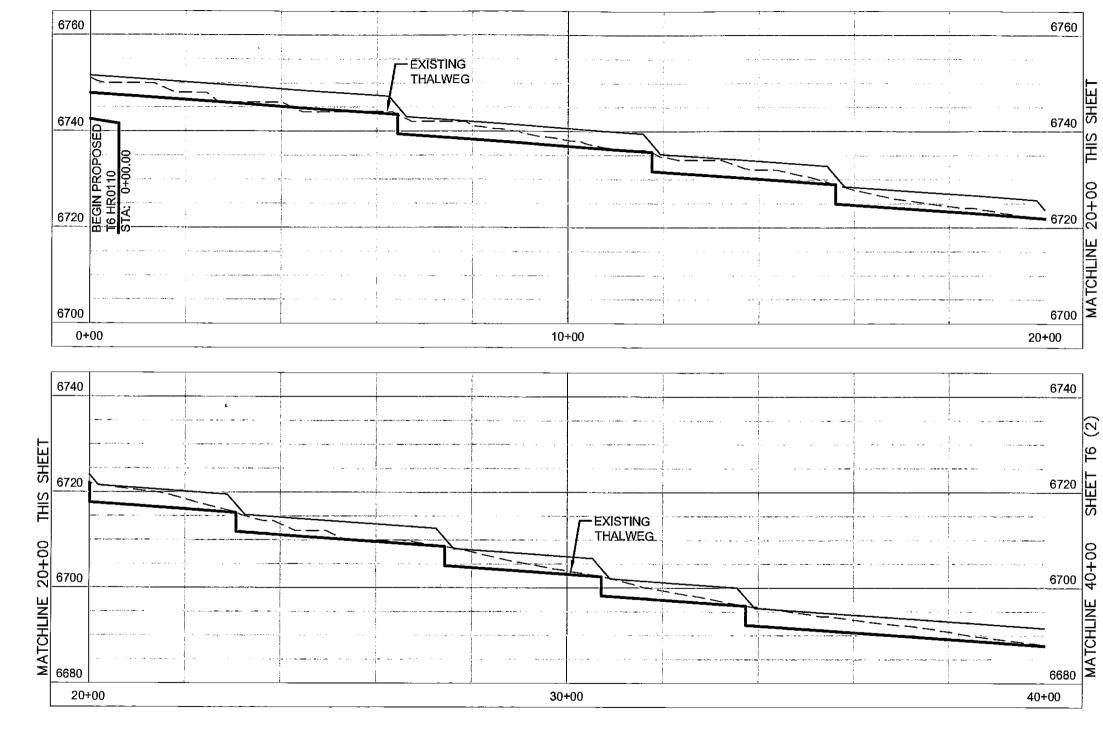


#### T6 HR0110

#### SLOPE = 0.70%

(9) 4' DROPS

# PROFILE TRIBUTARY 6 (T6)



Computer File information	index of Revisions	Profilee	
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Acad. Ver. 2006 Scale: 1"⇔20' Units: Feet 🛆		re (ne) as1-0007 Checked by:	Sheet Number T6

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### LEGEND

PROPOSED DROP STRUCTURE ---- EXISTING THALWEG HYDRAULIC GRADE LINE

#### T6 HR0110

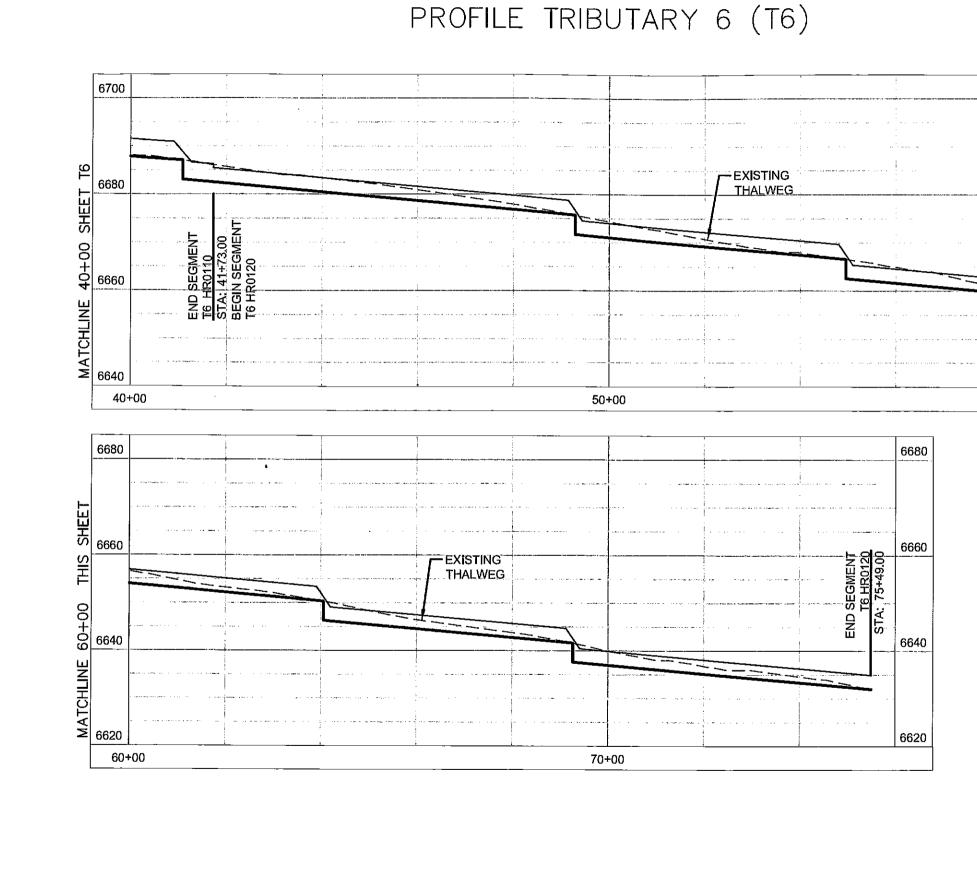
SLOPE = 0.70%

(9) 4' OROPS

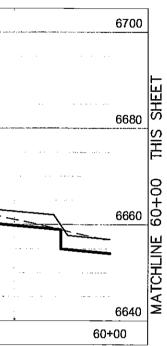
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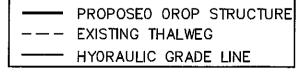
(6) 4' DROPS



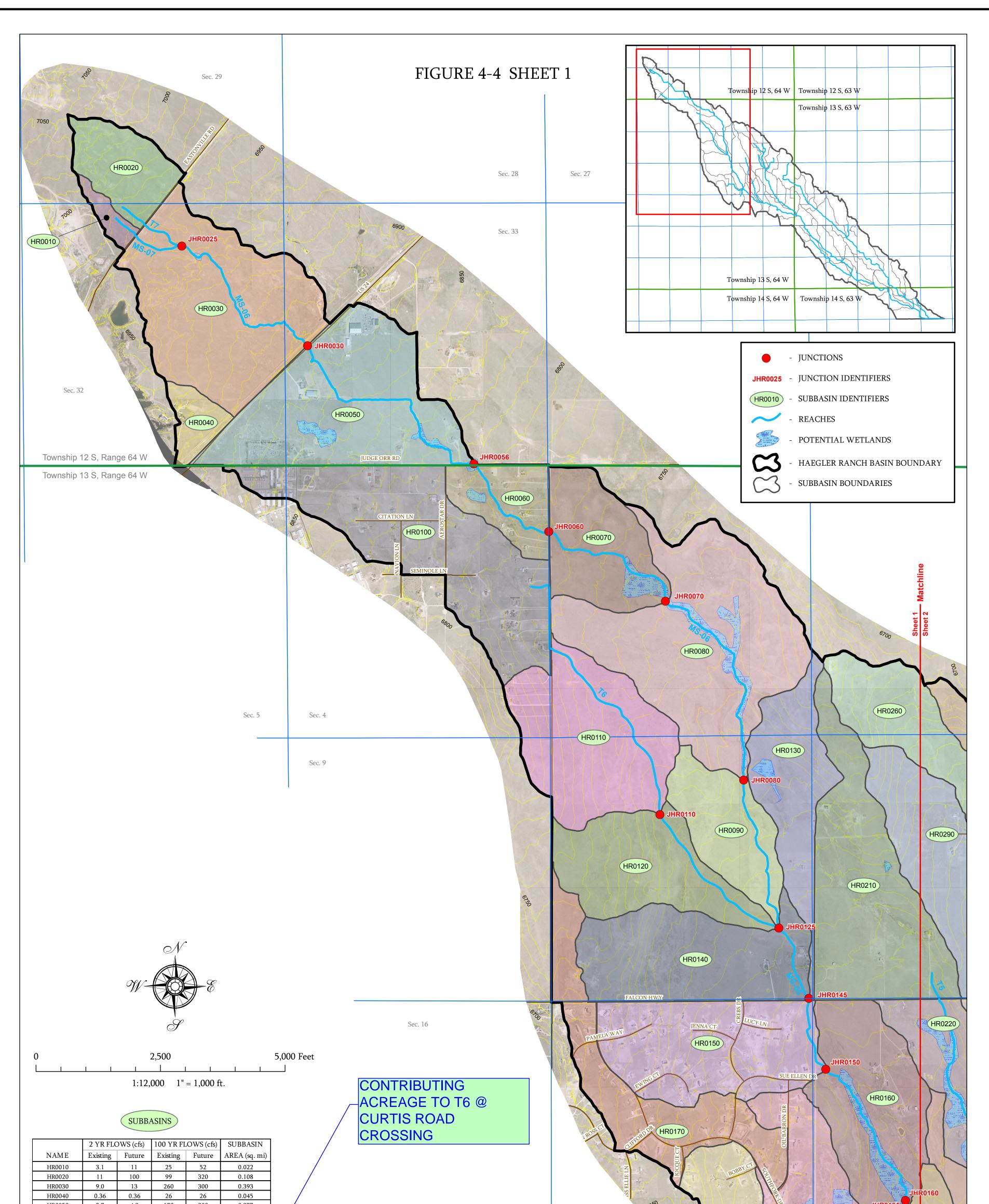
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### LEGEND



Structure Numbers T6 (2)

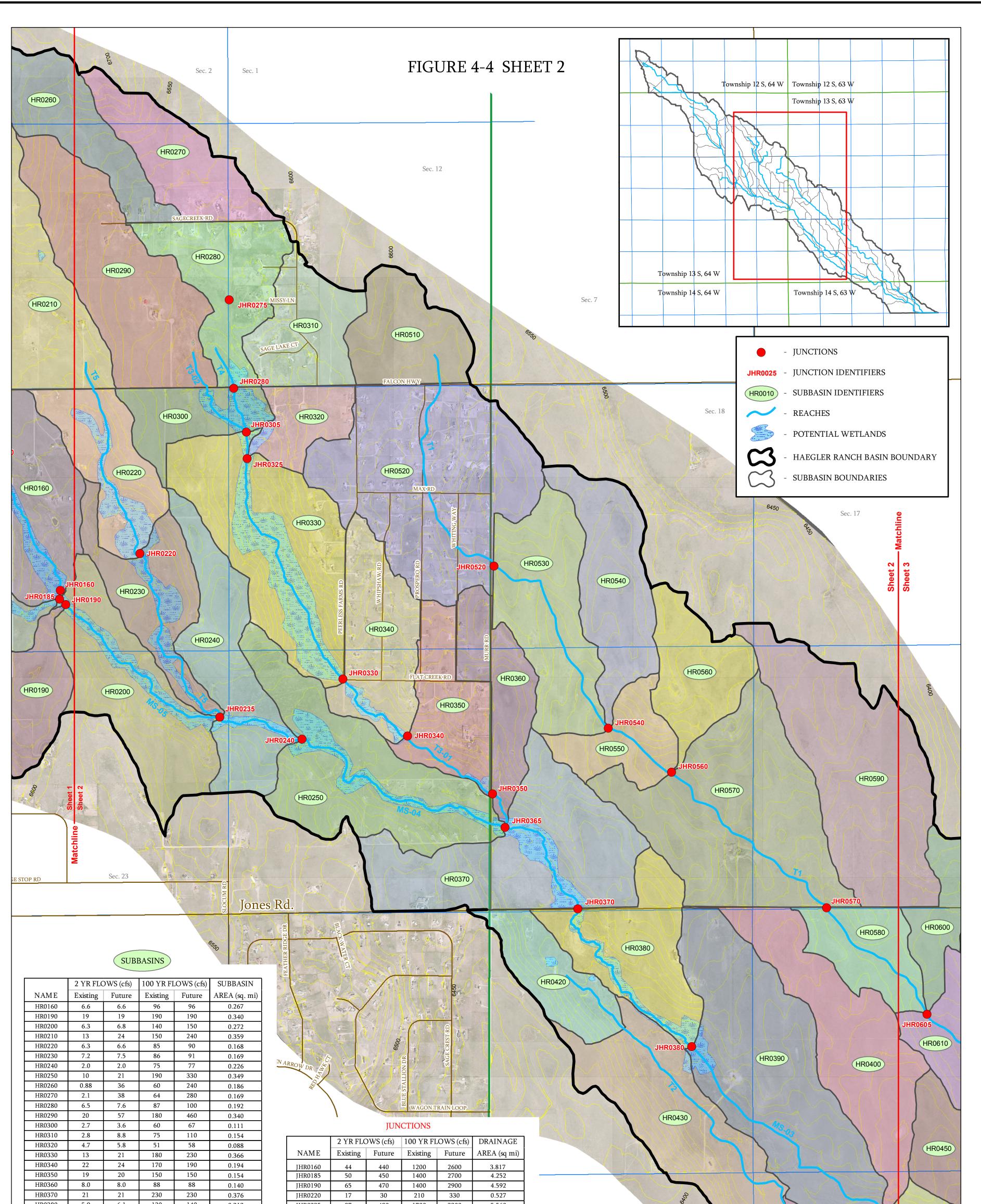


HR0050	2.7	4.3	170	200	0.377									6650	E P T	JHR0185	JHR0190
HR0060	2.0	3.5	54	66	0.101	_ /	, ,										
HR0070	5.4	210	99	580	0.180				II INI	CTIONS					HF	R0180	
HR0080	2.5	190	87	970	0.482				JUIN					Sec. 15	CALLEY CT		All and a set
HR0090	0.95	11	44	160	0.154	K		2 YR FLO	DWS (cfs)	100 YR FI	LOWS (cfs)	DRAINAGE	]				
HR0100	4.3	5.8	120	140	0.394		NAME	Existing	Future	Existing	Future	AREA (sq. mi)					
HR0110	1.9	72	84	420	0.310	I		0				-					
HR0120	2.0	4.0	73	150	0.226		JHR0025	14	110	120	370	0.130	4			$\langle \cdot \rangle$	
HR0130	0.27	15	29	180	0.185		JHR0030	21	120	350	630	0.523	1				
HR0140	3.5	6.4	110	140	0.283		JHR0056	24	120	540	830	0.945		Sec 22			
HR0150	21	21	210	210	0.290		JHR0060	25	120	590	890	1.046		CONTRIBUTING		R0190	HR0200
HR0160	6.6	6.6	96	96	0.267		JHR0070	28	210	660	930	1.226					
HR0170	15	17	130	150	0.241		JHR0080	29	340	720	1500	1.708		ACREAGE TO			
HR0180	6.4	6.4	85	85	0.194		JHR0110	6.1	72	200	440	0.704					125
HR0190	19	19	190	190	0.340		JHR0125	37	410	980	2100	2.792		MS-06 @			
HR0200	6.3	6.8	140	150	0.272		JHR0145	39	420	1100	2400	3.260		CURTIS ROAD	A A A		
HR0210	13	24	150	240	0.359		JHR0150	42	440	1100	2600	3.550					
HR0220	6.3	6.6	85	90	0.168		JHR0160	44	440	1200	2600	3.817		CROSSING	Т		$( \land ( \land \land \land \land \land \land \land \land \land \land \land \land \land \land \land \land \land$
HR0260	0.88	36	60	240	0.186		JHR0185	50	450	1400	2700	4.252	]				
HR0290	20	57	180	460	0.340		JHR0190	65	470	1400	2900	4.592	J				
																00	



URS NO. 21711039

DATE: 09/08

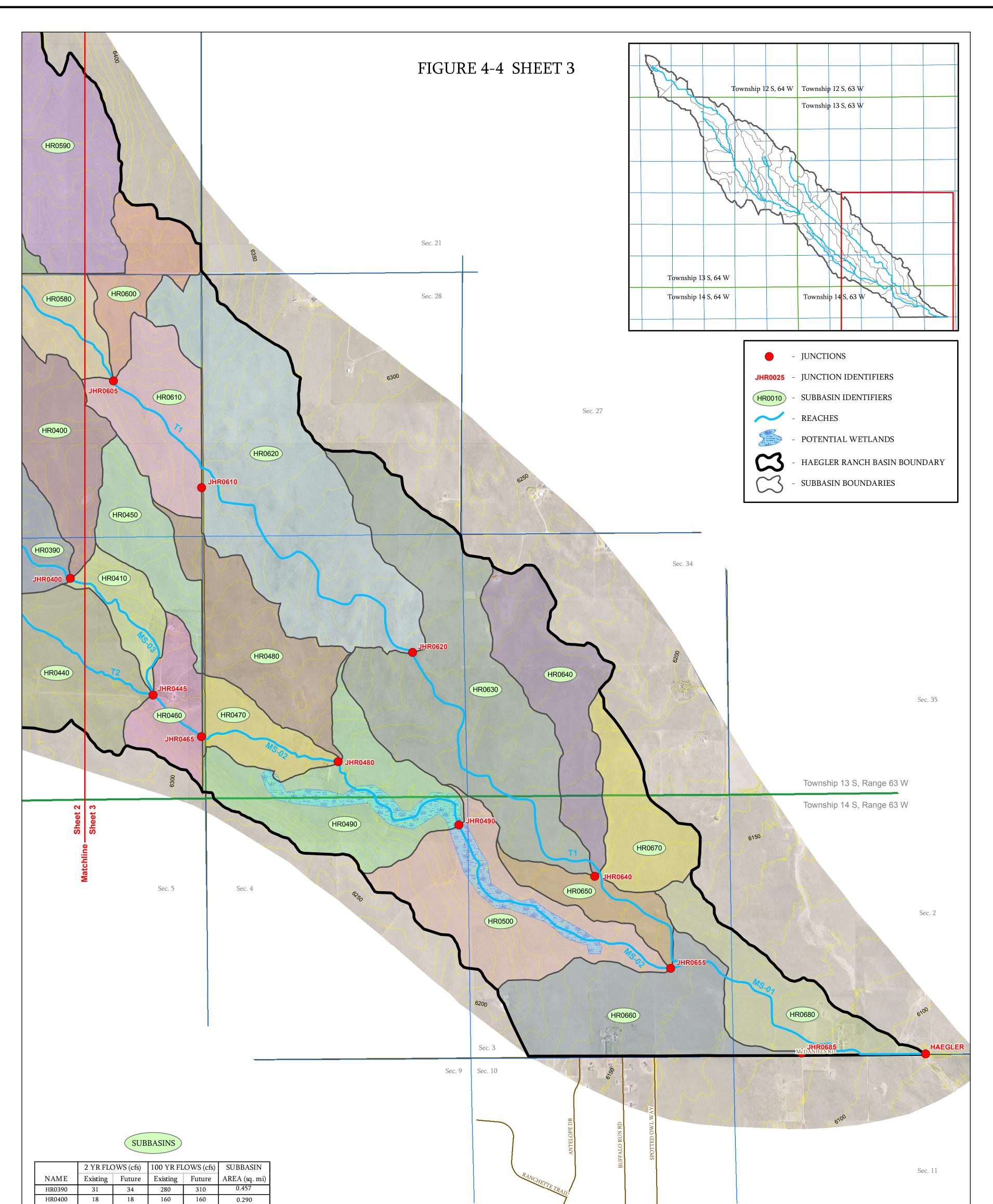


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HR0390	31	34	280	310	0.457	JHR0240	88	470	1700	3400	5.786	JHR0430 JHR0400 H
HR0400	18	18	160	160	0.290	JHR0275	2.9	69	120	480	0.355	Sec. 31
HR0410	7.4	8.4	68	77	0.084	JHR0280	6.5	75	200	570	0.547	
HR0420	1.8	2.5	59	70	0.124	JHR0305	29	96	400	870	0.998	
HR0430	4.7	4.7	90	90	0.295	JHR0325	36	110	490	1000	1.240	
HR0440	5.5	5.5	130	130	0.357	JHR0330	44	120	600	1200	1.606	
HR0450	9.5	9.5	85	85	0.140	JHR0340	49	130	640	1300	1.800	
HR0510	0.35	19	33	140	0.157	JHR0350	52	130	670	1400	1.954	
HR0520	23	24	200	210	0.488	JHR0365	150	600	2200	4800	8.229	W E E HR0440
HR0530	1.2	1.2	76	80	0.258	JHR0370	150	600	2300	5000	8.605	
HR0540	0.30	0.30	37	37	0.206	JHR0380	150	600	2300	5000	8.817	
HR0550	0.56	0.57	50	51	0.110	JHR0400	170	600	2400	5300	9.564	
HR0560	0.22	0.22	25	25	0.150	JHR0430	5.6	6.7	150	150	0.419	La 123 La la
HR0570	8.6	8.9	170	180	0.453	JHR0520	23	43	220	350	0.645	0 2,500 5,000
HR0580	10	11	96	98	0.124	JHR0540	24	44	270	420	1.109	
HR0590	2.2	2.2	84	84	0.408	JHR0560	25	44	300	460	1.369	Feet
HR0600	1.4	1.4	41	41	0.128	JHR0570	29	48	370	520	1.822	1:12,000 1" = 1,000 ft.
HR0610	5.7	5.8	100	110	0.202	JHR0605	33	52	480	630	2.482	



URS NO. 21711039

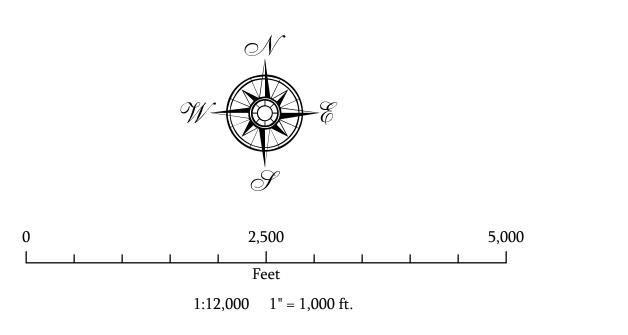
DATE: 09/08



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HR0440	5.5	5.5	130	130	0.357
HR0450	9.5	9.5	85	85	0.140
HR0460	4.0	4.0	76	76	0.109
HR0470	7.3	7.6	73	77	0.102
HR0480	0.86	0.86	34	34	0.244
HR0490	9.2	9.8	210	220	0.312
HR0500	3.3	3.4	140	150	0.326
HR0580	10	11	96	98	0.124
HR0590	2.2	2.2	84	84	0.408
HR0600	1.4	1.4	41	41	0.128
HR0610	5.7	5.8	100	110	0.202
HR0620	1.9	1.9	110	120	0.647
HR0630	2.2	2.2	86	86	0.616
HR0640	0.88	0.88	37	37	0.237
HR0650	4.2	4.3	45	46	0.092
HR0660	0.87	0.87	52	52	0.296
HR0670	0.63	0.63	31	31	0.153
HR0680	11	12	110	120	0.206

### JUNCTIONS

	2 YR FLOWS (cfs)		100 YR FL	OWS (cfs)	DRAINAGE
NAME	Existing	Future	Existing	Future	AREA (sq. mi)
JHR0400	170	600	2400	5300	9.564
JHR0445	180	590	2500	5400	10.424
JHR0465	180	570	2600	5400	10.673
JHR0480	180	570	2600	5400	11.019
JHR0490	180	570	2600	5500	11.331
JHR0605	33	52	480	630	2.482
JHR0610	34	52	500	650	2.684
JHR0620	35	53	560	700	3.331
JHR0640	38	54	670	780	4.184
JHR0655	190	570	3200	5600	15.933
JHR0685	190	550	3200	5600	16.588
HAEGLER	190	550	3200	5600	16.588





URS NO. 21711039

DATE: 09/08

#### MASTER DEVELOPMENT DRAINAGE PLAN and PRELIMINARY DRAINAGE REPORT FOR SADDLEHORN RANCH

Prepared For: ROI Property Group, LLC 2495 Rigdon Street Napa, CA 94558 (707) 365-6891

> May 8, 2020 Project No. 25142.00

Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

El Paso County PCD File No. SP-19-006

 $X:\2510000.all\2514200\Word\Reports\Drainage\Saddlehorn\ Ranch\ MDDP.PDR.docx$ 

#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. # 32314	
For and On Behalf of JR Engineering, LLC	

Date

#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

ROI Property Group, LLC

By:

Title: Address:

2495 Rigdon Street Napa, CA 94558

#### **El Paso County:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E. County Engineer/ ECM Administrator Date

Conditions:



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# Purpose

This document is the Master Development Drainage Plan (MDDP)/Preliminary Drainage Report (PDR) for the proposed Saddlehorn Ranch. The purpose of this report is to:

- 1. Identify on-site and off-site drainage patterns.
- 2. Recommend preliminary storm water facilities to collect and convey storm runoff from the proposed development to appropriate discharge and/or detention locations.
- 3. Recommend preliminary water quality and detention facilities to control discharge release rates to below historic.
- 4. Demonstrate compliance with surrounding major drainage basin planning studies, master plan and flood insurance studies.

# GENERAL LOCATION AND DESCRIPTION

# Location

The proposed Saddlehorn Ranch, known as "the site" from herein, is a parcel of land located in Section 3 and 10, Township 13 South, Range 65 West of the 6th Principal Meridian in El Paso County, Colorado. The proposed 824 acre, rural, single family-development is bound by Judge Orr Road to the North and Curtis Road to the West. To the East, the site is bound by undeveloped land owned by Brent Houser Enterprises, LLC. To the south, the site is bound by undeveloped properties owned by 7120 Sudiev, LLC and Faye Reyonlds. A vicinity map and property owner map is presented in Appendix A.

Currently, there are three major drainageways that run through the site: Haegler Ranch Main Stem 6 (MS-06), Haegler Ranch Tributary 6 (T-6), and Gieck Ranch West Fork – Reach 7A (WF-R7A). These drainageways were analyzed, both hydrologically and hydraulically, in the following reports:

- 1. Geick Ranch Drainage Basin Planning Study (DBPS), October 2007
- 2. Haegler Ranch Basin DBPS, May 2009
- 3. Sante Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision (LOMR), October 2004

The impact of these drainageways and planning studies on the proposed development will be discussed later in the report.

# Description of Property

The proposed development contains approximately 824 acres and will be comprised of 227 rural 2.5 – 5 acre lots. The site is currently unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling range land condition. In general, the site slopes from northwest to southeast and the existing drainageways follow this topography.

Per a NRCS web soil survey of the area, the site is made up of Type A, B and D soils. Type A soils cover roughly 80% of the site while Type B soils cover 3% and Type D cover the remaining 17% of the site. Group A soils have a high infiltration rate when thoroughly wet. Type B soils have a moderate infiltration when thoroughly wet. Type D soils have a very slow infiltration rate when thoroughly wet and have a high shrink-swell potential. A NRCS soil survey map has been presented in Appendix A.

Two existing wells are located in the southwest corner of the site. A 12" Cherokee Metropolitan District waterline runs through the site just south of the northern property line. Approximately a mile south of the Curtis Road and Judge Orr Road intersection, a two lane dirt road proceeds from Curtis Road east towards approximate center of the site. A water tank, pond and windmill are located within Major Drainageway MS-06 at the end of the dirt road.

## Floodplain Statement

Based on the FEMA FIRM Map number 08041C0558G, dated December 7, 2018, the site lies within Zone A, Zone AE, and Zone X. Zone A is defined as areas subject to inundation by the 1-percent-annual-chance flood determined using approximate methodologies because BFEs have not been established. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. All proposed development within the site will occur in Zone X.

In the northeast corner of the site, proposed development borders the Zone A boundary of the Geick Ranch West Tributary (WF-R7). At time of Final Drainage Report for this future phase of the development, a LOMR will be presented to establish base flood elevations (BFEs) for all lots that border the current Zone A boundary. The current FIRM Map has been presented in Appendix A.

# DRAINAGE BASINS AND SUBBASINS

# Major Basin Descriptions

The site lies within two major drainage basins: the Gieck Ranch Drainage Basin based on the "*Gieck Ranch Drainage Basin Planning Study*" (DBPS) prepared by Drexel, Barrell & Co. in October, 2007 and revised in February 2010 and the Haegler Ranch Drainage Basin based on the "*Haegler Ranch Drainage Basin Planning Study*" prepared by URS Corporation in May 2009.

The Gieck Ranch Drainage Basin covers approximately 22 square miles and begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. The Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains south to the Arkansas River near the city of Pueblo, Colorado. The majority of the area within the basin is undeveloped and is characterized as rolling range land typically associated with Colorado's semi-arid climates.

Anticipated land use for the basin includes residential, industrial, agricultural and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

The Haegler Ranch Drainage Basin covers approximately 16.6 square miles in unincorporated El Paso County, CO. The Haegler Ranch Drainage Basin is tributary to Black Squirrel Creek. In its existing condition, the basin is comprised of rolling rangeland with poor vegetative cover associated with Colorado's semi-arid climate. The natural drainageways within the basin are typically shallow and wide with poorly defined flow paths in most areas. Anticipated land use for the basin includes residential and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

As part of its drainage research, JR Engineering reviewed the following drainage studies, reports and LOMRs:

- Gieck Ranch Drainage Basin Planning Study prepared by Drexel, Barrell & Co. in October, 2007 and revised in February 2010. (Not adopted by El Paso County as of July 2019)
- Haegler Ranch Drainage Basin Planning Study prepared by URS Corporation in May 2009
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision prepared by Tri-Core Engineering in June 2004.

#### Existing Gieck Ranch Drainage Basin

The "*Gieck Ranch Drainage Basin Planning Study*" evaluated existing and future drainage conditions, identified future improvements, and established basin and bridge fees for the Gieck Ranch Drainage Basin. It should be noted that as of today the "*Gieck Ranch Drainage Basin Planning Study*" has not yet been approved and adopted by the County. All referenced information from the aforementioned report is presented for information purposes only.

Based upon provided drainage maps and analysis, Gieck Ranch discharges a total of 1,017 cfs onto the site within Major Drainageway Gieck Ranch West Fork Reach 7A (WF-R7A). An existing 66" CMP and 36" CMP convey the offsite flow across Judge Orr Road onto the site. The existing culverts at Judge Orr Road are undersized for existing and future flows resulting in localized overtopping. The DBPS recommends the culvert be upsized to four -12' x 5' box culverts. The culvert will not be upsized within the context of this report and development. The culvert is owned by El Paso County and timing of the recommended improvements will be controlled by the County. The overtopping at the intersection of WF-R7A is not contained within the 100-year floodplain. Therefore, at time of Final Drainage Report, berming will be provided that will protect proposed lots from overtopping flows. An overtopping analysis is presented in Appendix D and the limits of overtopping are presented on the existing and proposed drainage maps in Appendix F.

Based on existing channel analysis, the *Gieck Ranch DBPS* recommends WF-R7A channel improvements approximately 200' upstream and 300' downstream of the culvert crossing at Judge Orr Road (50' bottom width, 10:1 side slopes and vegetative augmentation). The recommended

channel improvements result from upsizing the culvert at Judge Orr Road, requiring the channel to be lowered. The channel improvements were not recommended due to existing channel instability. Existing velocities in the channel were found to be 2.19 ft/s, as presented in Appendix E. Per the MS4 permit requirements, the onsite reach of WF-R7A will be analyzed for channel stability with the corresponding Final Drainage Report for that phase of the development. At the time of Final Drainage Report, any necessary improvements to WF-R7A to satisfy the MS4 permit will be evaluated. It should be noted that the onsite reach of WF-R7A, where the aforementioned channel improvements were recommended, is comprised of jurisdictional wetlands which will limit the allowable improvements. Coordination with the Army Corps of Engineers will be required to grant permission to disturb the jurisdictional wetlands. Recommended channel improvements from the *Gieck Ranch DBPS* are presented in Appendix E.

#### Existing Haegler Ranch Drainage Basin

The "*Haegler Ranch Drainage Basin Planning Study*" was used to establish a stormwater management plan for the existing and future stormwater infrastructure needs within the Haegler Ranch Drainage Basin. Based on provided drainage maps and analysis, in the existing condition Haegler Ranch contributes a total of 710 cfs onto the site. Of the 710 cfs, 590 cfs crosses Curtis Road in an existing 24" CMP onto the site. Major Drainageway MS-06 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. The remaining 210 cfs crosses Curtis Road in an existing 36" CMP onto the site. Major Drainageway MS-05. Both Curtis Road culverts are undersized for existing and future flows and overtopping occurs locally near the culvert crossings. Overtopping at the intersection of Curtis Road and T-6 is contained within the 100-year floodplain and will not affect proposed lots. The overtopping at the intersection of MS-06 and Curtis Road is not contained within the 100-year floodplain limits. Therefore, at time of Final Drainage Report, berming will be provided that will protect proposed lots from overtopping flows. An overtopping analysis is presented in Appendix D and the limits of overtopping are presented on the existing and proposed drainage maps in Appendix F.

The culverts are not proposed to be upsized within the context of this report and development. The culverts are owned by El Paso County and timing of the recommended improvements will be controlled by the County.

Furthermore, the *Haegler Ranch DBPS* recommends channel improvements within drainageways MS-06 and T-6. Per the *Haegler Ranch DBPS*, all recommended channel sections are trapezoidal with side slopes of 4:1 and a maximum depth of five feet. Within the limits of the site, three (3) channel bottom widths are recommended for MS-06. The first reach, from station 0+00 - 31+34, is proposed with a 15' bottom width, the second reach from 31+34 to 74+61, MS-06 is proposed with a 30' bottom width, and the last reach from station 74+61 - 103+62 is proposed with a 20' channel bottom. The *Haegler Ranch DBPS* recommends Major Drainageway T-6 be improved to a trapezoidal channel with an 8' bottom width, 4:1 side slopes and depth of 5'. Drop structures have

also been recommended within MS-06 and T-6. These improvements will not occur within the context of this report or development. However, due to the addition of culvert crossings within MS-06 and T-6, channel improvements are anticipated up and downstream of the proposed culverts. The extent of these channel improvements will be addressed with corresponding Final Drainage Reports for those phases of the development. At that time, channel stability will be evaluated and any necessary improvements will be proposed. Recommended channel improvements from the *Haegler Ranch DBPS* are presented in Appendix E.

Based on flood impacts, stream stability and cost effectiveness, this study recommended a subregional detention approach. This allows future development anywhere in the basin with the construction of an associated sub-regional pond. Within the boundary of Saddlehorn Ranch, the DBPS recommended a total of three (3) sub-regional ponds. Based on discussion with El Paso County, the site will utilize full spectrum water quality and detention ponds instead. These full spectrum detention ponds will limit developed discharge into the drainageways to less than historic rates. Future, upstream development will also require full spectrum detention in accordance with current El Paso County criteria, which is an effective alternative to the sub-regional pond approach.

*The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR* was executed on Haegler Ranch Tributary 2, 3, and 4. The LOMR revised the onsite effective flood zones from Zone A to Zone AE for the three drainageways. Upstream stretches of Tributary 3 and 4 are classified Zone A but those channel reaches are off site. All stretches of Tributary 3 and 4 onsite are Zone AE. See FIRM Map Panel 080059-0575G for limits of LOMR study and revised flood zones, presented in Appendix E.

## Existing Sub-basin Drainage

On-site, existing drainage patterns are generally from northwest to southeast by way of existing, natural drainageways (MS-06, T-6, WF-R7A). On-site areas flow directly into these drainageways which also bypass off-site flows through the site. Offsite flows within the major drainageways that pass through the site will influence the on-site culvert designs and any channel improvements.

On-site, existing drainage basins were established based upon existing topography and the limits of 100-year floodplain. The site was divided into eleven existing sub-basins. See Table 1 below for summary of existing drainage sub-basins and corresponding peak flows. An existing drainage map is provided in Appendix F.

EXISTING BASIN SUMMARY TABLE									
Tributary Sub-Basin	Area (acres)	Percent Impervious	Q ₅ (cfs)	Q ₁₀₀ (cfs)					
G1	10.1	2.0%	0.00	0.1					
G2	87.6	2.0%	1.5	76.4					
H1	166.5	2.0%	0.1	81.0					
H2	111.1	2.0%	0.2	91.1					
H3	118.9	2.0%	0.9	64.1					
H4	63.3	2.0%	1.4	73.2					
H5	53.2	2.0%	0.3	28.2					
H6	87.6	2.0%	0.2	110.1					
CH1	23.9	2.0%	5.4	21.0					
CH2	84.2	2.0%	2.6	33.7					
CH3	19.1	2.0%	0.1	6.5					
Total	825.4	N/A	12.7	585.4					

Table 1: Existing Drainage Basin Summary

The existing condition of the three major drainageways are discussed below;

#### Existing Geick Ranch West Fork Reach 7A (WF-R7A)

The first major drainageway is the Gieck Ranch West Fork Reach 7A (WF-R7A), per the *Gieck Ranch DBPS*. WF-R7A crosses onto the site along Judge Orr Road, approximately ¹/₄ mile west of the intersection with Elbert Road. Discharge from the developed site into this drainageway will be limited to historic rates via a full spectrum detention pond prior to discharge. This drainageway includes jurisdictional wetlands and the entire drainageway onsite is classified Zone A. Access to the drainage way will be provided from internal roadways and along an equestrian trail will be constructed adjacent to the drainageway. The equestrian train can be utilized for maintenance equipment as well.

#### Existing Haegler Ranch Main Stem (MS-06)

The second drainageway is the Haegler Ranch Main Stem (MS-06), per the *Haegler Ranch DBPS*, which crosses onto the site along Curtis Road, approximately 1,600' south of the intersection with Judge Orr Road. MS-06 flows south towards its offsite confluence with Black Squirrel Creek. MS-06 exits the site along the southern property line. Discharge from the developed site into this drainageway will be limited to historic rates via a full spectrum detention pond prior to discharge. This drainageway includes non-jurisdiction wetlands and the entire drainageway is classified Zone AE. Access to the channel will be provided at the culvert crossing of MS-06 and San Isidro Trail via

a 15' wide maintenance and access road that will proceed from San Isidro trail to the channel bottom. From here, access through the channel is achievable with existing grades within the channel. Furthermore, an equestrian trail will be constructed adjacent to the drainageway that can be utilized for maintenance equipment as well. The road alignments are displayed on the proposed drainage map presented in Appendix F.

#### Existing Haegler Ranch Tributary 6 (T-6)

The third drainageway is the Haegler Ranch Tributary 6 (T-6), per the *Haegler Ranch DBPS*, which crosses onto the site along Curtis Road, approximately ³/₄ mile south of the intersection with Judge Orr Road. T-6 conveys flows south through the site and towards its off-site confluence with Black Squirrel Creek. Discharge from the developed site into this drainageway will be limited to historic rates via a full spectrum detention pond prior to discharge. This drainageway is absent of any on-site wetlands and the entire drainageway is classified Zone AE. Access to the channel will be provided at the culvert crossing of T-6 and Del Cerro Trail via a 15' wide maintenance and access road that will proceed from Del Cerro Trail to the channel bottom. From here, access through the channel is achievable with existing grades within the channel. Furthermore, an equestrian trail will be constructed adjacent to the drainageway that can be utilized for maintenance equipment as well. The road alignments are displayed on the proposed drainage map presented in Appendix F.

*The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR* was executed on three Haegler Ranch basin drainageways. Two of the drainageways that were evaluated pass through the proposed development. These drainageways are the: Haegler Ranch Tributary 3 & 4. Within the boundary of the proposed development, Haegler Ranch Tributary 3 and 4 are synonymous with Main Stem 6 and Tributary 6 from the *Haegler Ranch DBPS*. The purpose of the LOMR was to revise the flood hazard depicted in the current Flood Insurance Study. Additionally, the LOMR provided existing, 100-year velocities within the drainageways that will be utilized in the design of any potential channel improvements. A FIRM panel with the limits of the detailed study as well as BFEs has been presented in Appendix E.

See Table 2 for comparison of drainageway identification and the naming convention used within the context of this report. See Table 3 for a comparison of 100-year flows as calculated in the aforementioned DBPS' and LOMR. An existing conditions drainage map is presented in Appendix F.

#### Table 2: Major Drainageways

Major Drainageway Naming Conventions									
Saddlehorn Ranch MDDP/PDR:	Per Haegler Ranch DBPS:	Per Geick Ranch DBPS:	Per Sante Fe Springs LOMR:						
WF-R7A	N/A*	West Fork (Middle)/WF- R7A	N/A*						
MS-06	Main Stem (MS- 06)	N/A*	Haegler Ranch Tributary 3						
T-6	Tributary 6 (T-6)	N/A*	Haegler Ranch Tributary 4						

#### Table 3: Major Drainageways - Ex. 100-Year Flow Comparison

Major Drainageways: 100-Year Flow Comparison										
Drainageway Name	Contributing Area (sq. mi.)	Q ₁₀₀ Per Haegler Ranch DBPS:	Q ₁₀₀ Per Geick Ranch DBPS:	Q ₁₀₀ Per Sante Fe Springs LOMR:						
WF-R7A @ Judge Orr Road	1.50	N/A*	1,017 cfs	N/A*						
MS-06 @ Curtis Road	1.05	451 cfs	N/A*	505 cfs						
T-6 @ Curtis Road	0.39	120 cfs	N/A*	130 cfs						

*N/A: Flow regime outside limits of study.

# Proposed Sub-basin Drainage

The proposed basin delineation is as follows;

Basin A is approximately 9.2 acres and in its existing condition is rolling rangeland. Runoff generally flows southeast away from Drainageway MS-06. In the proposed condition, Basin A will be rural 2.5 acre lots and roadway. Runoff from this basin will be collected in road side swales and conveyed south along Barrosito Drive to Pond A. Pond A, while considered temporary in this MDDP, will need to meet Full Spectrum Detention Criteria unless deviations are approved in the Final Drainage Report for this future filing. It is anticipated that Barrosito Drive will be extended south as part of the development of the adjacent parcel to the south. The most logical place for a permanent Full Spectrum pond is located approximately 1,000 feet south at the future road crossing with MS-06. When that pond is constructed, the Saddlehorn Metropolitan District No. 1 will remove Pond A. The peak flow rate for Basin A in the 5 and 100-year storm are 9.5 cfs and 20.7 cfs, respectively. However, Pond A will discharge at less than historic rates.

Basin B is approximately 60.4 acres and in its existing condition is rolling rangeland. Runoff generally flows southwest across the basin towards Drainageway MS-06. In the proposed condition, Basin B will be rural 2.5 acre lots, paved roadway and will include Pond B. Runoff from this basin will be collected in road side swales and conveyed south along Barrosito Drive to Pond B. The peak flow rate for Basin B in the 5 and 100-year storm are 9.9 cfs and 46.3 cfs, respectively. However, Pond B will discharge at less than historic rates. A portion of Basin B is inundated by the existing 100-year floodplain, however; at time of final platting berming will be constructed to reduce the floodplain limits within the drainageway tract and a corresponding LOMR will be executed on this stretch of channel to establish the revised floodplain.

Basin C is approximately 102.5 acres and in its existing condition is rolling rangeland. Runoff generally flows southwest across the basin towards Drainageway MS-06. In the proposed condition, Basin C will be rural 2.5 acre lots, paved roadway and will include Pond C. Runoff from this basin will be collected in road side swales and conveyed south along Barrosito Drive and Del Cambre Drive to Pond C. The peak flow rate for Basin C in the 5 and 100-year storm are 15.8 cfs and 69.4 cfs, respectively. However, Pond C will discharge at less than historic rates.

Basin D is approximately 99.2 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway WF-R7A. In the proposed condition, Basin D will be rural 2.5 acre lots, paved roadway and will include Pond D. Runoff from this basin will be collected in road side swales and conveyed east along Barrosito drive to Pond D. The peak flow rate for Basin D in the 5 and 100-year storm are 29.4 cfs and 95.4 cfs, respectively. However, Pond D will discharge at less than historic rates. A portion of Basin D is inundated by the existing 100-year floodplain, however; at time of final platting berming will be constructed to reduce the floodplain limits within the drainageway tract and a corresponding LOMR will be executed on this stretch of channel to establish the base flood elevations.

Basin E is approximately 11.6 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway MS-06. In the proposed condition, Basin E will be rural 2.5 acre lots, paved roadway and will include Pond E. Runoff from this basin will be collected in road side swales and conveyed southwest along San Isidro Trail to Pond E. The peak flow rate for Basin E in the 5 and 100-year storm are 2.0 cfs and 9.9 cfs, respectively. However, Pond E will discharge at less than historic rates.

Basin F is approximately 117.4 acres and in its existing condition is rolling rangeland. Runoff generally flows southeast across the basin towards Drainageway MS-06. In the proposed condition, Basin F will be rural 2.5 acre lots, paved roadway and will include Pond F. Runoff from this basin will be collected in road side swales and conveyed southwest along Benito Wells Trail to Pond F. The peak flow rate for Basin F in the 5 and 100-year storm are 17.0 cfs and 69.9 cfs, respectively. However, Pond F will discharge at less than historic rates.

Basin G is approximately 39.9 acres and in its existing condition is rolling rangeland. Runoff generally flows south across the basin towards Drainageway T-6. In the proposed condition, Basin G will be rural 2.5 acre lots, paved roadway and will include Pond G. Runoff from this basin will be collected in road side swales and conveyed southwest along El Raiceno Trail to Pond G. The peak flow rate for Basin G in the 5 and 100-year storm are 6.1 cfs and 25.3, respectively. However, Pond G will discharge at less than historic rates.

Basin H is approximately 30.7 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway T-6. In the proposed condition, Basin H will be rural 2.5 acre lots, paved roadway and will include Pond H. Runoff from this basin will be collected in road side swales and conveyed north along Rosalia Place to Pond H. The peak flow rate for Basin H in the 5 and 100-year storm are 3.7 cfs and 17.9 cfs, respectively. However, Pond H will discharge at less than historic rates.

Basin I is approximately 46.6 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway T-6. In the proposed condition, Basin I will be rural 2.5 acre lots, paved roadway and will include Pond I. Runoff from this basin will be collected in road side swales and conveyed south down Carrizo Springs Trail and east down Zaragoza Trail to Pond I. The peak flow rate for Basin I in the 5 and 100-year storm are 15.9 cfs and 63.1 cfs, respectively. However, Pond I will discharge at less than historic rates.

Basin J is approximately 10.1 acres and in its existing condition is rolling rangeland. This basin will not be developed and will remain in its existing condition, per Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedures this basin will not be detained in a full spectrum water quality and detention pond. Runoff generally flows east across the basin towards Drainageway T-6. In the proposed condition, Basin J will be an undeveloped tract. Undeveloped runoff from this basin will follow existing drainage patterns and sheet flow into Drainageway WF-R7A. The peak flow rate for Basin J in the 5 and 100-year storm are 3.0 cfs and 10.5 cfs, respectively.

Basins CH1, CH2 and CH3 are existing drainageway basins that will remain undeveloped in the proposed condition. There will be no development within Basin CH1-CH3, however; Basin CH2 & CH3 will require channel grading to accommodate proposed culverts. The scope of this grading will leave the channels in an undeveloped condition per Section I.7.1.B.7 and therefore will be excluded from permanent stormwater management. Basin CH1 contains jurisdictional wetlands. Basin CH2 contains non-jurisdictional wetlands. There are no wetlands located in Basin CH3. Peak flow rates for proposed undeveloped basins are presented in Appendix B.

Basins UD1-UD11 acre comprised of rural 2.5+ acre residential lots and will follow existing drainage patterns in the proposed condition. Development in these basins will be limited to a maximum of 10% impervious development via a plat covenant. Therefore, these basins can be excluded from permanent stormwater detention per Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedures (2.5+ acre lots with imperviousness less than 10% can be excluded from

permanent stormwater management practices). Therefore, Basins UD1-UD11 will not be included in the developments permanent stormwater management facilities. A Permanent BMP applicability form is presented in Appendix D to justify these exclusions. A map detailing each development site and any exclusion is presented in Appendix F. Basin UD1 flows directly into Major Drainageway WF-R7A. Basins UD2, UD2.1, UD2.2, UD3, UD4, UD5 and UD8 flow directly into Major Drainageway MS-06. Basins UD6, UD7, UD9, and UD9.1 flow directly into Major Drainageway T-6. Basins UD8.1, UD10, and UD11 follow existing drainage patterns as well but flow directly off-site prior to being captured in major drainageways. A portion of Basin UD2.2 is inundated by the existing 100-yr floodplain. However, at time of final drainage report, lot lines will be adjusted outside floodplain limits. Furthermore, a portion of Basin UD10 is inundated by the existing 100-year floodplain, however; at time of final platting berming will be constructed to reduce the floodplain limits within the drainageway tract and a corresponding LOMR will be executed on this stretch of channel to establish the revised floodplain.

In addition to undeveloped lot areas, a small portion of Del Cerro Trail (portion of Basins UD9 & UD9.1) and San Isidro Trail (a portion of Basin UD5) will be allowed to directly discharge into Drainageway T-6 and MS-06, respectively, and excluded from the developments permanent stormwater management facilities. Per Section I.7.1.C.1, the County may exclude up to 20 percent, not to exceed 1 acre, of the applicable development site area from permanent stormwater management. Approximately, 16,240 ft² of Del Cerro Drive and 14,000 ft² square feet of San Isidro Trail, totaling 0.08% of the total development area, will be excluded from stormwater management, which is significantly less than the 20% limit.

A summary of all basin parameters has been presented in Appendix B.

Developed basin's runoff will be captured in roadside ditches and conveyed to a full spectrum water quality and detention pond per El Paso County DCM Volume 1. Each full spectrum pond will release treated flows at less than historic rates to minimize adverse impacts downstream. Pond D will discharge into Major Drainageway WF-7A, Pond B, C, E, and F will discharge into Major Drainageway T-6. Due to existing topography, Pond A will discharge into open space south of the site. Based on existing topography in the area, this flow will eventually be captured off-site by Major Drainageway MS-06.

See Table 4 for comparison of proposed pond parameters including a comparison of proposed basin discharge versus existing discharge.

Table 4: Pond Summary	1
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POND SUMMARY TABLE							
Tributary Sub- Basin	Pond Name	Tributary Acres	WQ Volume (ac-ft)	100-Year Volume (ac-ft)	Provided Volume (ac-ft)	100-Year Peak Discharge (cfs)	Ex. 100- Year Peak Discharge (cfs)
А	POND A	9.2	0.20	1.14	1.14	2.5	2.8
В	POND B	60.4	0.35	1.46	2.17	18.9	21.0
С	POND C	102.5	0.64	2.69	2.77	26.0	28.9
D	POND D	99.2	0.59	2.86	2.97	47.7	53.0
E	POND E	11.6	0.05	0.23	0.39	4.7	5.2
F	POND F	117.4	0.65	3.20	3.35	50.7	56.3
G	POND G	39.9	0.34	1.36	1.62	10.1	11.2
Н	POND H	30.7	0.16	0.70	1.18	10.5	11.7
I	POND I	46.6	0.25	1.09	1.41	26.8	29.8

# DRAINAGE DESIGN CRITERIA

# Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "*City of Colorado Spring/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual (CCSDCM), dated May 2014, as adopted by El Paso County, as well as the July 2019 El Paso County Engineering Criteria Manual update.

## Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using CUHP Version 2.0.0, developed by Urban Drainage and Flood Control District. The model utilizes the raingage classified as "a design storm by temporal distribution of one-hour rain depths with area correction factors". The following Colorado Springs rainfall depths were utilized in the model: 2.52 inches for 1-hour 100-year depth and 3.5 inches for 6-hour 100-year depth. EPA SWMM 5.1 was utilized to route runoff flow rates for the sizing of stormwater storage facilities. The CUHP calculations and SWMM model are presented in Appendix B.

Urban Drainage and Flood Control District's UD-Detention, Version 3.07 workbook was used for preliminary pond sizing. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. Pond sizing spreadsheets are presented in Appendix D.

### Hydraulic Criteria

The Federal Highway Administration's HY-8 program (Volume 7.50) was used to analyze the proposed box culvert within Major Drainageways MS-06 and T-6. Per Section 14.3.2 of the CCS/EPCDCM, a maximum headwater-to-rise ratio of 1.5 was used for the sizing of box culverts. Furthermore, box culverts will be designed in conjunction with channel improvements to maintain the current floodplain and base flood elevations. Culvert sizing and corresponding channel improvements will be revised as roadway geometry becomes better defined. Preliminary culvert design sheets are presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for preliminary roadside ditch design. For the purposes of this PDR/MDDP, the maximum roadside ditch size was determined based on peak 100-year flows and minimum roadway slopes within each basin. Swales were checked for velocity and Froude number per the EPC DCM Chapter 10, Section 10-7 and Table 10-4. Swale cross sections with a 100-year velocity greater than 5 ft/s or a Froude number greater than 0.9 will be lined with erosion control blanket and native grasses, or another approved method of stabilization, to limit erosive potential. Final swale designs and cross section details will be included with the Final Drainage Report. Preliminary swale design sheets are presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) will be used for final local road crossing culvert design with in the Final Drainage Report. All onsite, local road crossing culverts are assumed to be 18" or 24" CMP based on preliminary calculations. Culvert size was determined based on 100-year flows and hydraulic criteria from EPCDCM Chapter 9 –Culvert Design. The Final Drainage Report will provide final local road crossing culvert designs.

# DRAINAGE FACILITY DESIGN

### General Concept

The proposed stormwater conveyance system was designed to convey the developed Saddlehorn Ranch flows to full spectrum water quality and detention ponds. Water quality and detention ponds will be designed to release at less than historic rates to minimize adverse impacts downstream. All full spectrum water quality and detention ponds have been sized such that State Engineer review or approval is not required. Undeveloped basins are allowed to follow existing drainage patterns and discharge directly into major drainageways or off-site.

The undeveloped portion of developed lots will be allowed to discharge directly into Drainageways MS-06, T-6 and WF-R7A. Per the "Jurisdictional Determination Request for the 824 Acres Curtis Road subdivision Project" completed by Ecosystem System Services in October 2018, MS-06 and T-

6 are not waters of the state and WF-R7A is a water of the state however, any direct discharge into this drainageway will be historic, undeveloped flows. The direct discharge into drainageway situation occurs anywhere a lot naturally drains toward a drainageway rather than the street. It was determined for these lots that all development (i.e. house and driveway) will occur in the first 200' of the lot, measured from the street into the lot. The 200' developed region of the lot will drain towards the road and be conveyed to a full spectrum water quality pond, however; the remainder of the lot (undeveloped) will be allowed to follow historic drainage patterns and flow directly into the drainageways. Furthermore, at time of platting, a covenant will be established for the development that will limit imperviousness to 10% for areas draining directly to the drainageways in order to satisfy Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedures.

A box culvert will be proposed within Major Drainageway MS-06 and T-6 to convey existing, off site and developed, on-site flows underneath proposed roadways and through the site, in accordance with the *Haegler Ranch DBPS*. Culverts will not be required in Major Drainageway WF-R7A to maintain the drainage patterns established in the *Gieck Ranch DBPS*.

Channel improvements will be proposed immediately up and downstream of culvert improvements in order to maintain the current floodplain. Further channel improvements may be required within the major drainageways and the need for these potential improvements will be evaluated in the Final Drainage Report for each Filing. Access roads will be provided from local roadways down into the drainageways to provide culvert and drainageway maintenance access. A proposed drainage map is presented in Appendix F showing locations of culvert improvements, approximate channel improvements and access roads.

### Specific Details

### Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual, Volume 2 this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes; stabilizing drainageways, treating the water quality capture volume (WQCV), and consider the need for Industrial Commercial BMP's.

Step 1, Reducing Runoff Volumes: The development of the project site is proposed as single family residential (2.5 ac. min.) with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roadways will utilize roadside ditches further disconnecting impervious areas. These practices will also allow for increased infiltration and reduce runoff volume.

Step 2, Stabilize Drainageways: This site will utilize roadside ditches with culvert crossings throughout the site. These roadside ditches will then direct the on-site development flows to the multiple detention ponds within the project that will be designed to release at or below historic rates in the natural channels. The natural channels will be stabilized in reaches with high velocity by the

use of drop structures incorporated at each roadway culvert crossing and isolated grade control structures where warranted. Based upon the proposed reduction in released flows compared to the pre-developed flows, no impact to downstream drainageways is anticipated.

Step 3, Provide WQCV: Runoff from this development will be treated through capture and slow release of the WQCV in multiple permanent detention basins that will be designed per current El Paso County drainage criteria.

Step 4 Consider the need for Industrial and Commercial BMP's: No industrial or commercial uses are proposed within this development. However, a site specific storm water quality and erosion control plan and narrative will be prepared for each future Filing. Site specific temporary source control BMPs as well as permanent BMP's will be detailed in this plan and narrative to protect receiving waters.

### Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention will be provided for all of the development site not meeting exclusions present in the ECM - Stormwater Quality Policy and Procedures Section I.7.1.B and C. Any areas of the development site not being included in the site's permeant stormwater management are presented on the MS4 Development Site Map with their specific exclusion, presented in Appendix F. Outlet structure release rates will be limited to less than historic rates to minimize adverse impacts to downstream stormwater facilities. Complete pond and outlet structure designs will be provided with the Final Drainage Report. Preliminary pond design parameters are presented in Appendix D.

### Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted with each Final Drainage Report. We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plans and construction assurances posted prior to obtaining a grading permit.

### **Operation & Maintenance**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within the any platted County ROW (roadside ditches and local road culverts) will be owned and maintained by El Paso County. All proposed drainage structures within easements or tracts (full spectrum water quality ponds, drainageway culverts and drainageway improvements) will be owned and maintained by the Saddlehorn Ranch Metropolitan District No.1. Inspection access for El Paso County will be provided through a maintenance easement.

### Drainage and Bridge Fees

An estimate of total basin fees for the proposed development within Haegler Ranch Drainage Basin is provided in Table 6. A portion of Saddlehorn Ranch (Basin J and CH1) is not within an approved

drainage basin, therefore; no drainage or bridge fees will be required for this area. Drainage and Bridge fees are for informational purposes only and do not include reductions for rural lots, permanent water quality facilities or reimbursable channel improvements. Final drainage reports for each phase of development will establish official drainage and bridge fees to be paid at time of platting.

Total Site Composite % Impervious for Basin Fees									
Desin	Area	%	(Area) *						
Basin	(ac)	Imperviousness	(% Imp.)						
Α	9.2	67%	6.13						
В	60.4	10%	6.28						
С	102.5	11%	11.69						
D	99.2	11%	10.71						
E	11.6	12%	1.35						
F	117.4	10%	11.62						
G	39.9	17%	6.70						
Н	30.7	9%	2.89						
I	46.6	9%	4.38						
J	10.1	9%	0.89						
UD1	12.4	2%	0.25						
UD2	12.8	2%	0.26						
UD2.1	14.8	2%	0.30						
UD2.2	7.2	2%	0.14						
UD3	13.4	2%	0.27						
UD4	4.8	2%	0.10						
UD5	36.4	2%	0.73						
UD6	22.1	2%	0.44						
UD7	9.3	2%	0.19						
UD8	4.6	2%	0.09						
UD8.1	5.3	2%	0.11						
UD9	4.8	2%	0.10						
UD9.1	6.4	2%	0.13						
UD10	10.4	2%	0.21						
UD11	6.0	2%	0.12						
CH1	23.9	2%	0.48						
CH2	84.2	2%	1.68						
CH3	19.0	2%	0.38						
Total	825.4	-	68.59						
Com	p. % Imp. =	= 68.59%*ac/825.4	Comp. % Imp. = $68.59\%$ *ac/825.4 ac = $8.31\%$						

### Table 6: Drainage Basin Fees

	El Paso County - Haegler Ranch Drainage Basin Fees							
Area (acre)	Composite % Impervious	Total Impervious Acreage	2019 Drainage Fee (per Impervious Acre)	2019 Bridge Fee (per Impervious Acre)	Saddlehorn Ranch Drainage Fee	Saddlehorn Ranch Bridge Fee		
825.4	8.31%	68.59	\$10,324	\$1,524	\$708,123	\$104,531		

### Construction Cost Opinion

(For Information Only / Non-Reimbursable) Cost opinion to be provided with Final Drainage Report.

### SUMMARY

The proposed development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements, including ditches, culverts, detention ponds and drainage channel improvements. The proposed development will not adversely affect the offsite major drainageways or surrounding development. This report meets the latest El Paso County Drainage Criteria requirements for this site.

### **R**EFERENCES:

- <u>City of Colorado Springs Drainage Criteria Manual Volume 1</u>, City of Colorado Springs, CO, May 2014.
- 2. <u>Urban Storm Drainage Criteria Manual</u>, Urban Drainage and Flood Control District, Latest Revision.
- 3. <u>Gieck Ranch Drainage Basin Planning Study</u>, Drexel, Barrell & Co., October 2007 and revised in February 2010.
- 4. <u>Haegler Ranch Drainage Basin Planning Study</u>, URS Corporation, May 2009.
- <u>The Santa Fe Springs Haegler Ranch Drainage Basin LOMR</u>, Federal Emergency Management Agency, October 20, 2004.

### APPENDIX A

### FIGURES AND EXHIBITS

### **APPENDIX B**

### HYDROLOGIC CALCULATIONS

### APPENDIX C

### HYDRAULIC CALCULATIONS

### APPENDIX D

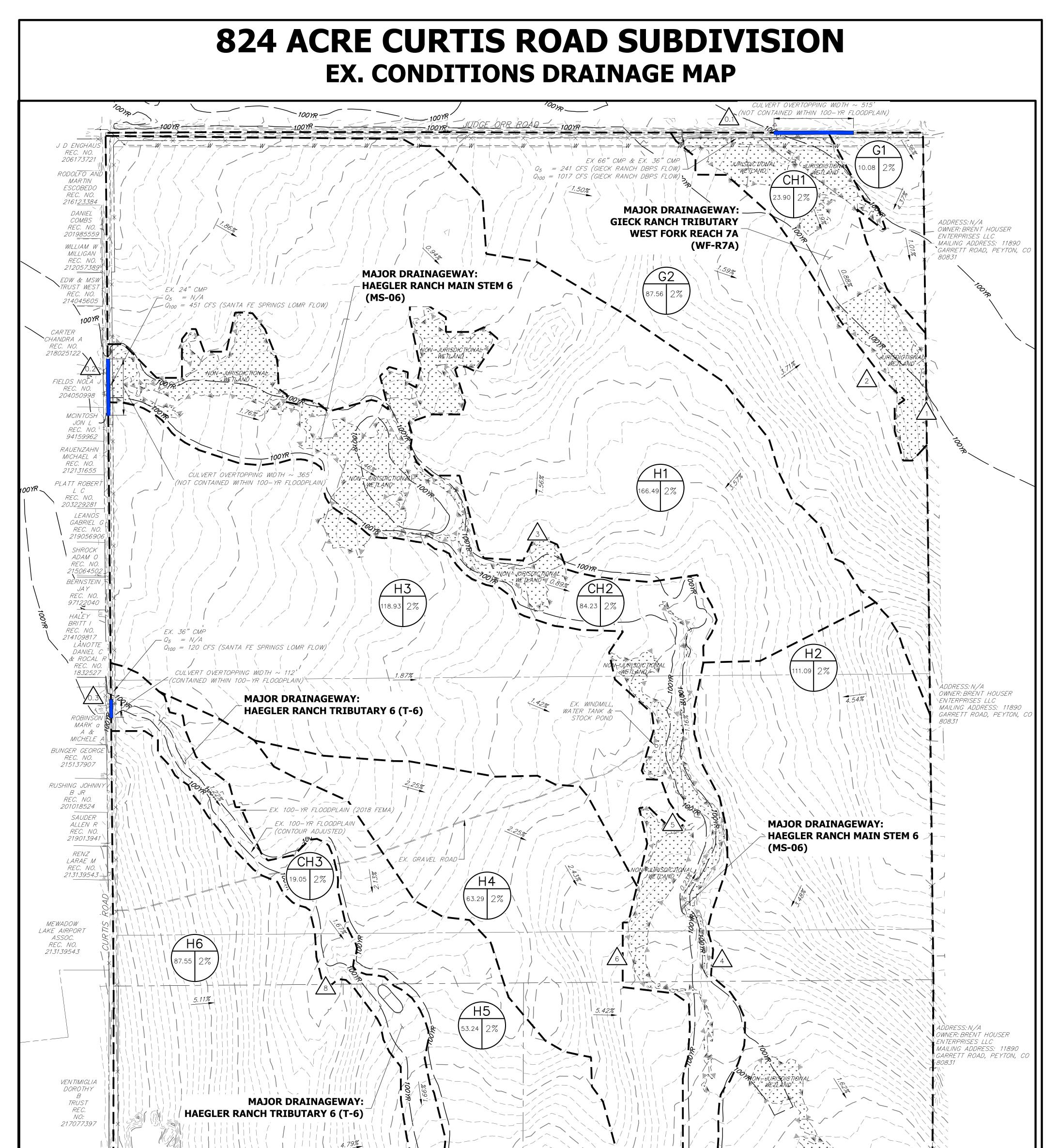
### WATER QUALITY AND DETENTION CALCULATIONS

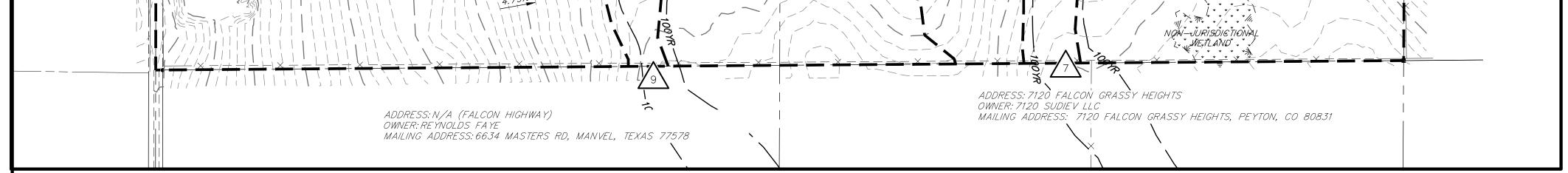
### APPENDIX E

### **REFERENCE MATERIALS**

### APPENDIX F

### **DRAINAGE MAPS**





### LEGEND



BASIN DESIGNATION

I.D.: BASIN IDENTIFIER A: BASIN AREA B: % IMPERVIOUS



DESIGN POINT

BASIN DELINEATION

- ---6100-- EXISTING INDEX CONTOURS
- ----- EXISTING INTERMEDIATE CONTOURS
- EXISTING FLOW DIRECTION

BASIN SUMMARY TABLE							
TributaryAreaPercentQ5 (cfs)Q100 (cfs)Sub-Basin(acres)ImperviousImperviousImpervious							
G1	10.1	2.0%	0.00	0.1			
G2	87.6	2.0%	1.5	76.4			
H1	166.5	2.0%	0.1	81.0			
H2	111.1	2.0%	0.2	91.1			
H3	118.9	2.0%	0.9	64.1			
H4	63.3	2.0%	1.4	73.2			
H5	53.2	2.0%	0.3	28.2			
H6	87.6	2.0%	0.2	110.1			
CH1	23.9	2.0%	5.4	21.0			
CH2	84.2	2.0%	2.6	33.7			
CH3	19.1	2.0%	0.1	6.5			
Total	825.4	N/A	12.7	585.4			

DES	DESIGN POINT					
SUM	MARY T	ABLE				
Tributary Sub-	Q₅ (cfs)	Q ₁₀₀ (cfs)				
0.1	241.00	1017.0				
0.2	-	451.0				
0.3	-	120.0				
1	<mark>6.9</mark>	1114.0				
2	1.5	76.4				
3	0.1	80.9				
4	0.1	91.1				
5	0.9	64.1				
6	1.4	73.2				
7	4.1	704.9				
8	0.2	110.1				
9	0.4	248.1				

EX. DRAINAGE MAP 824 CURTIS ROAD 25142.00 5/8/20 SHEET 1 OF 1

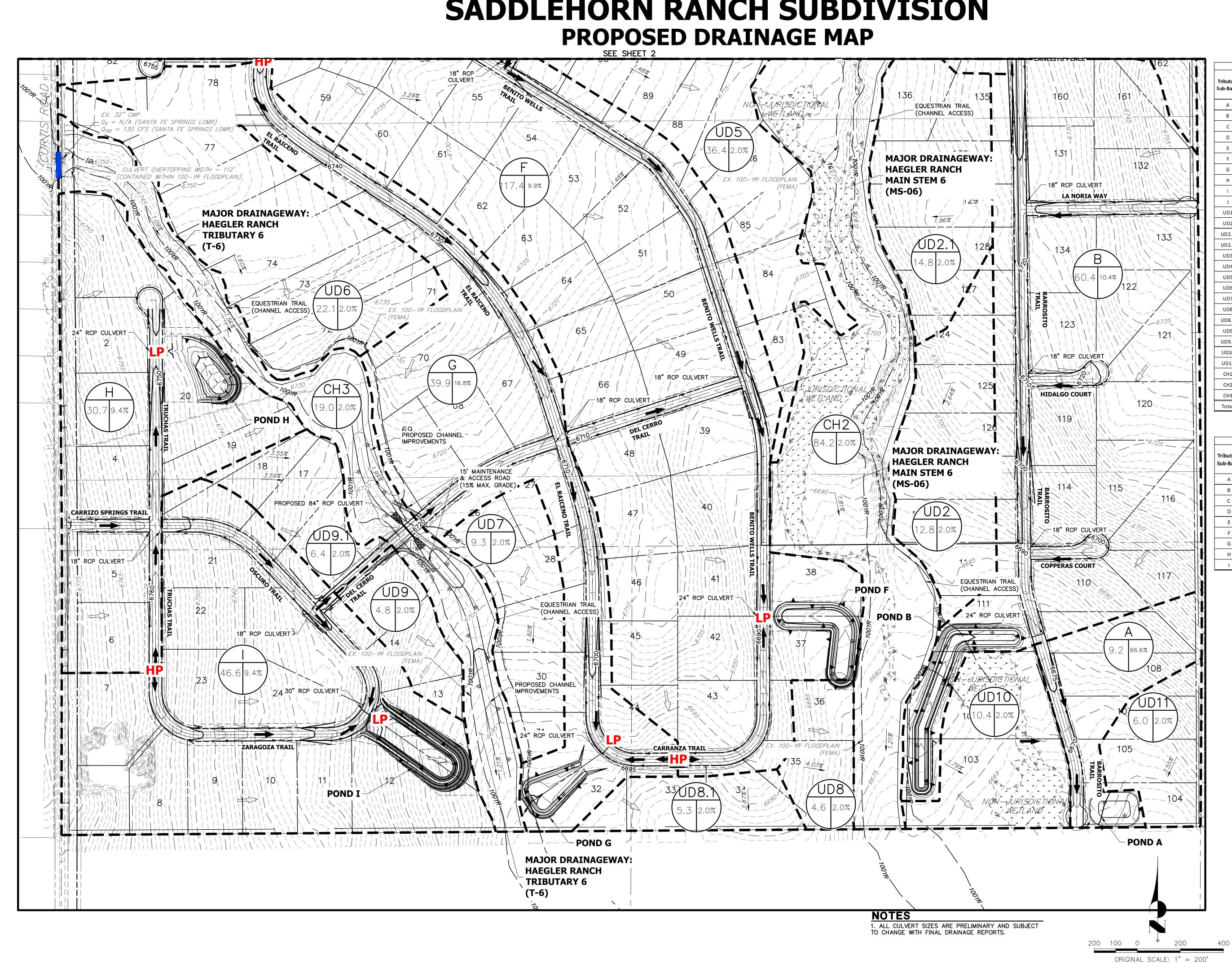
300

ORIGINAL SCALE: 1" = 300'

600

300 150 0



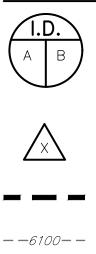


# **SADDLEHORN RANCH SUBDIVISION**

	BASIN	SUMMARY T	ABLE	
Tributary Sub-Basin	Area (acres)	Composite Percent Impervious	Q₅ (cfs)	Q ₁₀₀ (cfs)
Α	9.2	66.6%	9.5	20.7
В	60.4	10.4%	9.9	<mark>46.3</mark>
С	102.5	11.4%	15. <mark>8</mark>	69.4
D	99.2	10.8%	29.4	<mark>95.4</mark>
E	11.6	11.6%	2.0	9. <mark>9</mark>
F	117.4	9.9%	17.0	69.9
G	39.9	16.8%	6.1	25.3
Н	30.7	9.4%	3.7	17.9
I	46.6	9.4%	15.9	63.1
J	10.1	2.0%	3.0	10.5
UD1	12.4	2.0%	0.3	13.9
UD2	12.8	2.0%	0.1	7.7
UD2.1	14.8	2.0%	0.1	<b>14.7</b>
UD2.2	7.2	2.0%	0.1	5.5
UD3	13.4	2.0%	0.2	13.1
UD4	4.8	2.0%	<mark>0.03</mark>	3.4
UD5	<mark>36.4</mark>	2.0%	4.1	27.4
UD6	22.1	2.0%	0.1	12. <mark>4</mark>
UD7	9.3	2.0%	0.7	7.4
UD8	4.6	2.0%	0.03	3.3
UD8.1	5.3	2.0%	<mark>0.1</mark>	<mark>5.6</mark>
UD9	4.8	2.0%	0.1	4.2
UD9.1	6.4	2.0%	0.2	8.1
UD10	10.4	2.0%	0.1	6.7
UD11	6	2.0%	0.02	4.3
CH1	23.9	2.0%	5.4	21.0
CH2	84.2	2.0%	2.6	33.7
CH3	19.0	2.0%	0.1	6.5
Total	825.4	N/A	126.7	627.3

Tributary Sub-Basin	Pond Name	Tributary Acres	WQ Volume (ac-ft)	100-Year Volume (ac-ft)	Provided Volume (ac-ft)	100-Year Peak Discharge (cfs)	Ex. 100- Year Peak Discharge (cfs)
А	POND A	9.2	0.20	1.14	1.14	2.5	2.8
В	POND B	60.4	0.35	1.46	2.17	18.9	21.0
С	POND C	102.5	0.64	2.69	2.77	26.0	28.9
D	POND D	<mark>99.2</mark>	0.59	2.86	2.97	47.7	53.0
E	POND E	11.6	0.05	0.23	0.39	4.7	5.2
F	POND F	117.4	0.65	3.20	3.35	50.7	56.3
G	POND G	39.9	0.34	1.36	1.62	10.1	11.2
н	POND H	30.7	0.16	0.70	1.18	10.5	11.7
I	POND I	46.6	0.25	1.09	1.41	26.8	29.8

### LEGEND



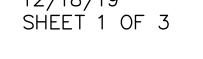
BASIN DESIGNATION I.D.:BASIN IDENTIFIER A:BASIN AREA B:COMP. % IMPERVIOUS

DESIGN POINT

BASIN DELINEATION

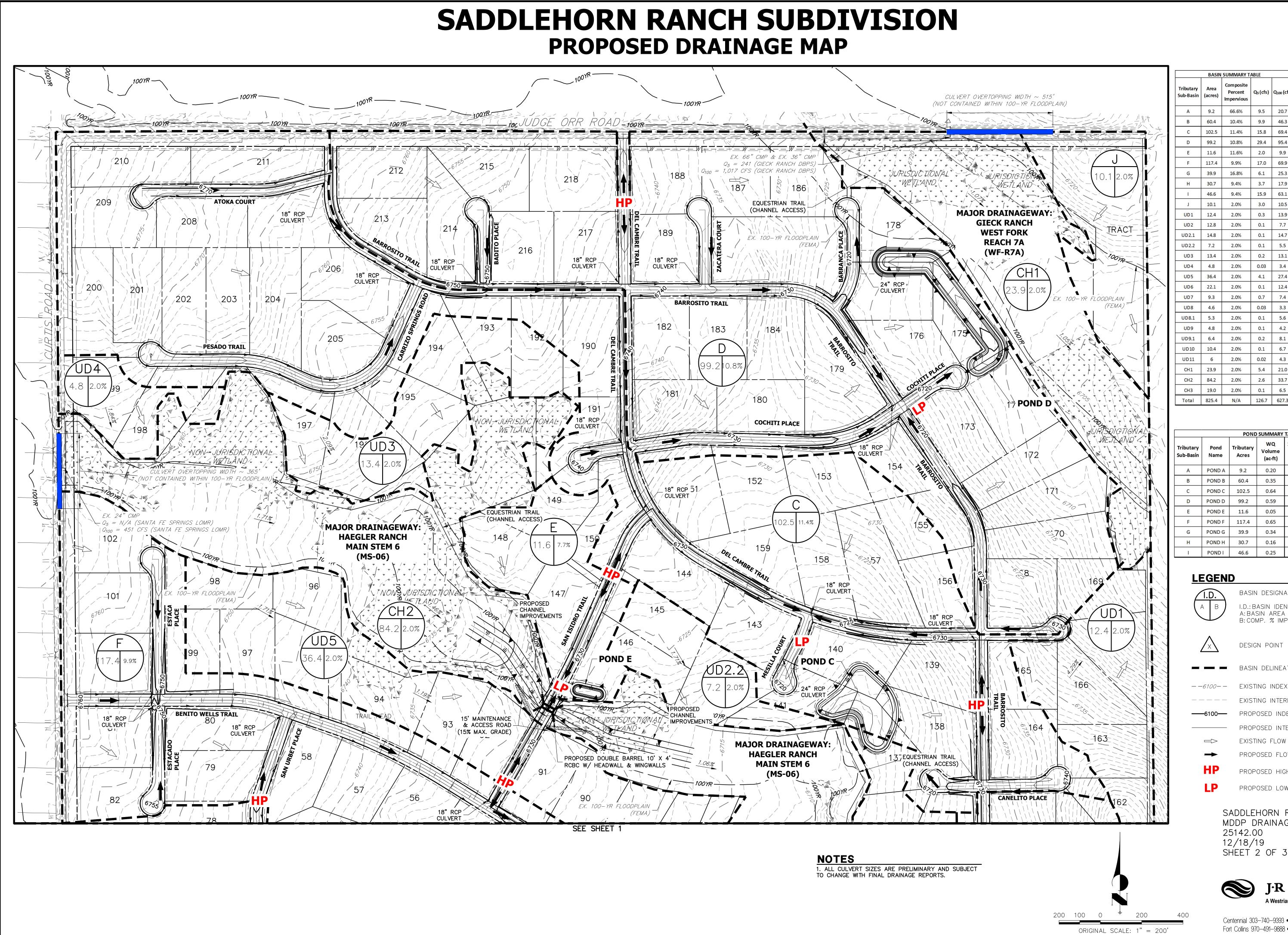
---6100-- EXISTING INDEX CONTOURS ----- EXISTING INTERMEDIATE CONTOURS

- PROPOSED INTERMEDIATE CONTOURS
- EXISTING FLOW DIRECTION  $\Rightarrow$ PROPOSED FLOW DIRECTION ╼
- HP PROPOSED HIGH POINT
- LP PROPOSED LOW POINT
- SADDLEHORN RANCH SUBDIVISION MDDP DRAINAGE MAP 25142.00 12/18/19





J·R ENGINEERING A Westrian Company



D	99.2	10.8%	29.4	95.	.4			
E	11.6	11.6%	2.0	9.	9			
F	117.4	9.9%	17.0	<mark>6</mark> 9.	.9			
G	<u>39.</u> 9	16.8%	<mark>6.1</mark>	25.	.3			
н	30.7	9.4%	3.7	17.	.9			
I	<u>46.6</u>	9.4%	15.9	63.	.1			
J	10.1	2.0%	3.0	10	.5			
UD1	12.4	2.0%	0.3	13.	.9			
UD2	12.8	2.0%	0.1	7.	7			
UD2.1	14.8	2.0%	0.1	14.	.7			
UD2.2	7.2	2.0%	<mark>0</mark> .1	5.	5			
UD3	13.4	2.0%	0.2	13.	.1			
UD4	4.8	2.0%	0.03	3.	4			
UD5	36.4	2.0%	4.1	27.	.4			
UD6	22.1	2.0%	0.1	12.	.4			
UD7	9.3	2.0%	0.7	7.	4			
UD8	<mark>4.</mark> 6	2.0%	0.03	3.	3			
UD8.1	5.3	2.0%	<mark>0.1</mark>	5.	6			
UD9	4.8	2.0%	0.1	4.	2			
UD9.1	6.4	2.0%	0.2	8.	1			
UD10	10.4	2.0%	0.1	6.	7			
UD11	6	2.0%	0.02	4.	3			
CH1	23.9	2.0%	5.4	21.	.0			
CH2	84.2	2.0%	2.6	33.	.7			
CH3	<u>19.0</u>	2.0%	<mark>0.1</mark>	6.	5			
Total	825.4	N/A	126.7	627	.3			
	·	PO		MARY	TABLE			
			W		100-Year	Provided	100-Year	Ex. 100-
Tributary Sub-Basin	Pond Name		Volu		Volume	Volume	Peak Discharge	Year Peak Discharge
			(ac	-ft)	(ac-ft)	(ac-ft)	(cfs)	(cfs)
А	POND	A 9.2	0.2	20	1.14	1.14	2.5	2.8
В	POND	B 60.4	0.3	35	1.46	2.17	18.9	21.0
С	POND	C 102.5	0.0	64	2.69	2.77	26.0	28.9
D	POND	D 99.2	0.5	59	2.86	2.97	47.7	53.0
E	POND	E 11.6	0.0	05	0.23	0.39	4.7	5.2

56.3

11.2

11.7

50.7

10.1

10.5

**BASIN SUMMARY TABL** 

Composite

Impervious

66.6%

10.4%

9.2

Percent Q5 (cfs) Q100 (cfs

9.5 20.7

9.9 46.3

	G	Ε	Ν	D
_	а			v.

POND G

POND I

BASIN DESIGNATION I.D.: BASIN IDENTIFIER A: BASIN AREA B: COMP. % IMPERVIOUS

DESIGN POINT

117.4 0.65

30.7 0.16

46.6 0.25

39.9

0.34

3.20

1.36

0.70

3.35

1.62

1.18

1.09 1.41 26.8 29.8

	BASIN DELINEATION
-6100— —	EXISTING INDEX CONTOURS
	EXISTING INTERMEDIATE CONTOURS
-6100	PROPOSED INDEX CONTOURS
	PROPOSED INTERMEDIATE CONTOURS
	EXISTING FLOW DIRECTION
→	PROPOSED FLOW DIRECTION
HP	PROPOSED HIGH POINT
LP	PROPOSED LOW POINT

SADDLEHORN RANCH MDDP DRAINAGE MAP 25142.00 12/18/19 SHEET 2 OF 3



J·R ENGINEERING A Westrian Company



January 5, 2022

Keith Curtis, PE, CFM Floodplain Administrator, PPRBD 2880 International Circle Colorado Springs, CO 80910

Re: Engineer's Certification of No Impact Case No. :

Dear Mr. Curtis,

This letter serves as Certification of No Impact to the Floodplain for the project entitled "Saddlehorn Ranch – Filing 3." The project is located in the unincorporated El Paso County and involves a proposed rural 2.5 acre lot subdivision.

The Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) shows the project area located on Panel No. 08041C0558G for El Paso County, Colorado dated December 7, 2018. The project area is located along Haegler Ranch MS-06 and is within a designated Zone AE Special Flood Hazard Area (SFHA).

JR Engineering has evaluated the effects of the proposed development on the Haegler Ranch floodplain using the effective modeling as a baseline. The HEC-RAS modeling was obtained in PDF format from the *"Santa Fe Springs – Haegler Ranch Drainage Basin Letter of Map Revision (LOMR)"* by Tri-Core Engineering, dated October 20, 2004, from the Federal Emergency Management Agency (FEMA). The effective model is the *"Santa Fe Springs – Haegler DB. – Letter of Map Revision"* prepared for FEMA by Tri-Core Engineering. The effective model was pared down to the stretch between Cross Sections 4 and 19 along Reach H8 (Haegler Ranch Tributary 3) for purposes of analysis within the context of this project.

JR Engineering utilized the calculated 100-year water surface from the aforementioned model to establish the existing 100-year floodplain. Proposed channel and culvert improvements were modeled utilizing the 100-year flow of 505 cfs established in the *"Santa Fe Springs – Haegler Ranch Drainage Basin Letter of Map Revision (LOMR)"*. Cross sections located between cross sections 4 and 19 were modeled using AutoCAD Hydraflow Express, Version 2020.4. Cross Section 13 aligns with the front of the project's proposed dual 12'x4' RCBC. Therefore, the Federal Highway Authority's HY-8, Version 7.60, was used for modeling the backwater effect to establish an accurate base flood elevation. The computed water surface elevation at each cross section was compared to the effective model to ensure a no rise scenario.

Select results of the analysis are presented in Table 1, on the following page:

	Base Flood Elevation (ft)			
Cross	Ex. 100-	Pr. 100-		
Section	Year	Year		
13	6723.61	6721.71		
14	6722.03	6720.43		
15	6720.65	6719.28		
16	6717.71	6717.59		
17	6714.03	1714.03		

Table 1: Base Flood Elevation Comparison

Based on the results of the proposed cross section modeling and the HY-8 culvert analysis, no increase to either the floodplain width or water surface elevation will result from the proposed site development.

Sincerely,

Bryan Law PE Colorado P.E. #25043

### No Rise Certification

I certify that I am a duly qualified registered Professional Engineer in the State of Colorado.

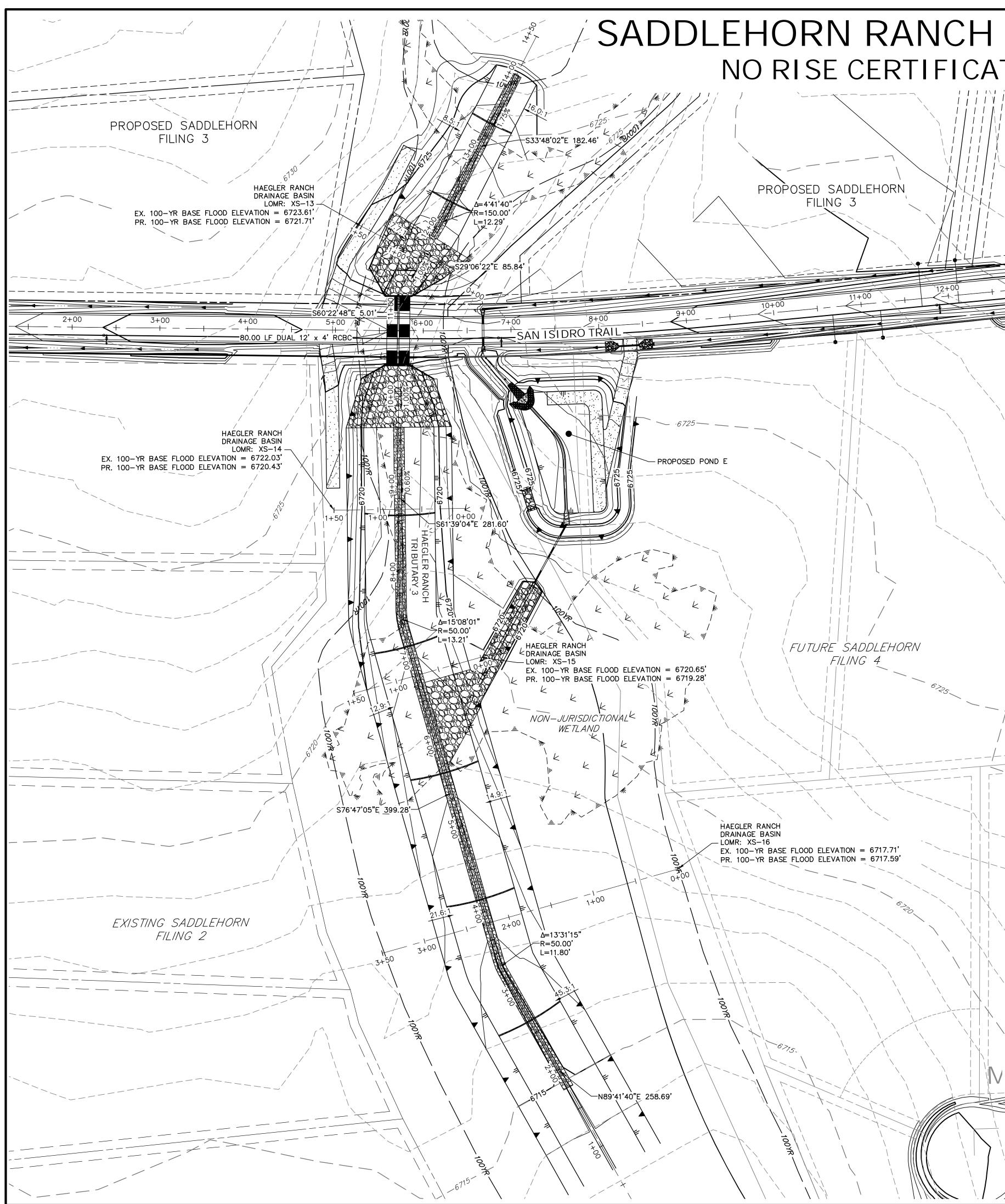
I certify the proposed project, Saddlehorn Ranch Filing No. 3, as detailed on the following sheets and calculations will result in zero rise in the FEMA designated 100 year flood heights, and no increase in the 100-year discharge and no increase in the 100-year floodplain width, at published and unpublished cross sections of the current FEMA floodplain of Haegler Ranch MS-06 as shown on FEMA map 08041C0558G. This certification is intended as proof of meeting the requirements set forth in the Pikes Peak Regional Building Code RBC313.20.1.

I further certify that the design conditions needed to meet the zero rise, box culvert and wing walls, are detailed in sufficient nature to allow for field confirmation and included among the supporting documentation.

I further certify that the structure in question will be securely anchored to prevent flotation, collapse or lateral movement in order to withstand the velocity of floodwaters as required by RCB313.18.1 and RBC313.21.2.

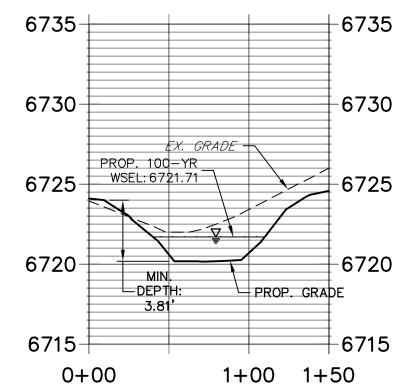
Bryan Law PE Colorado P.E. #25043



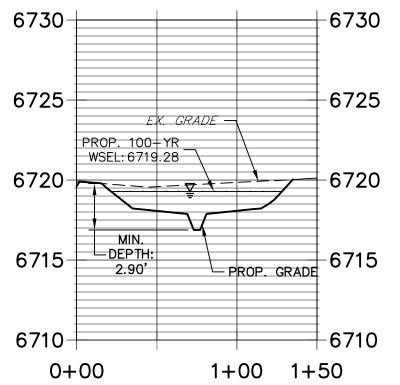


# SADDLEHORN RANCH - FILING 3 NO RISE CERTIFICATION

# CROSS SECTION 13 PROFILE STA 0+00.00 TO 1+50.00



# CROSS SECTION 15 PROFILE STA 0+00.00 TO 1+50.00



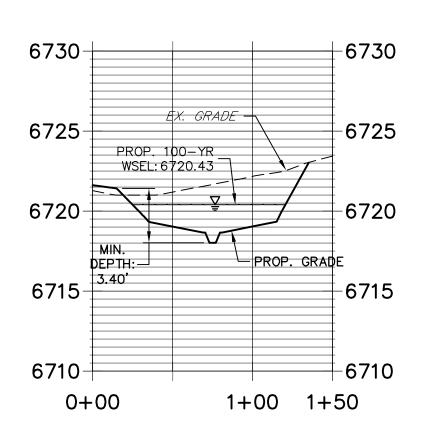
# CROSS SECTION 14 PROFILE STA 0+00.00 TO 1+50.00



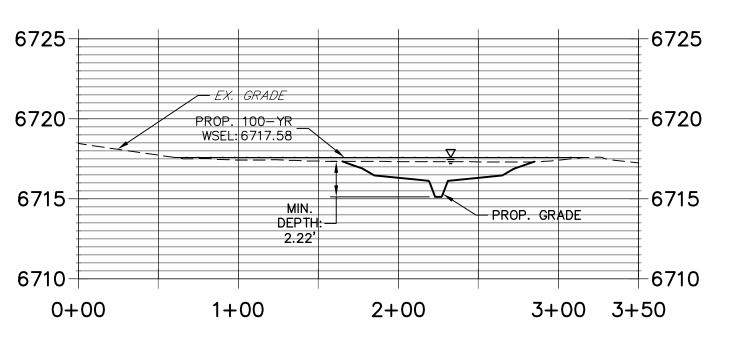
6725

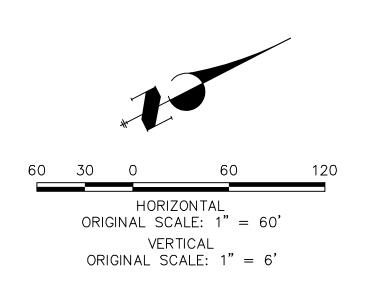
6720

+6710



CROSS SECTION 16 PROFILE STA 0+00.00 TO 3+50.00

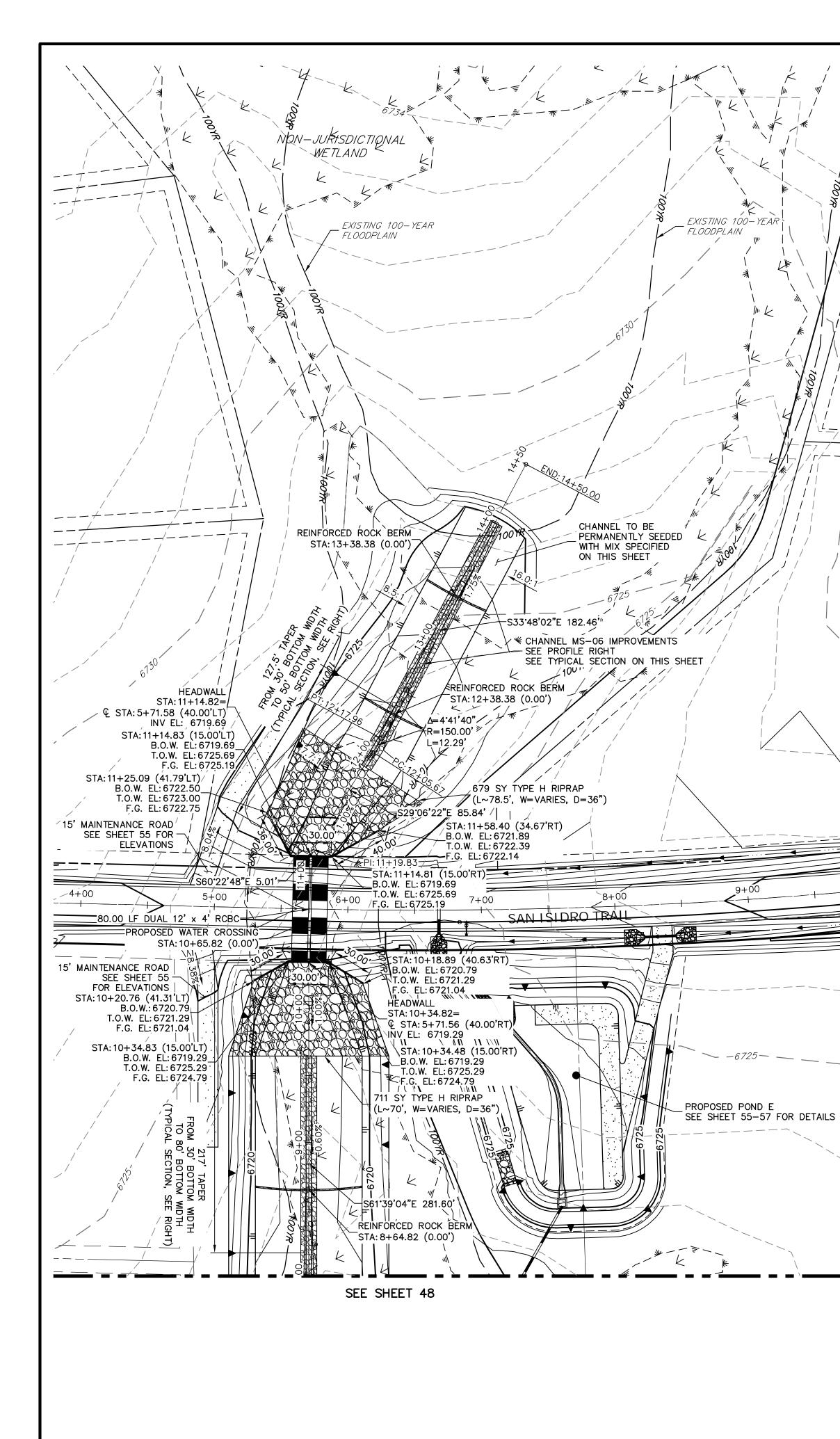


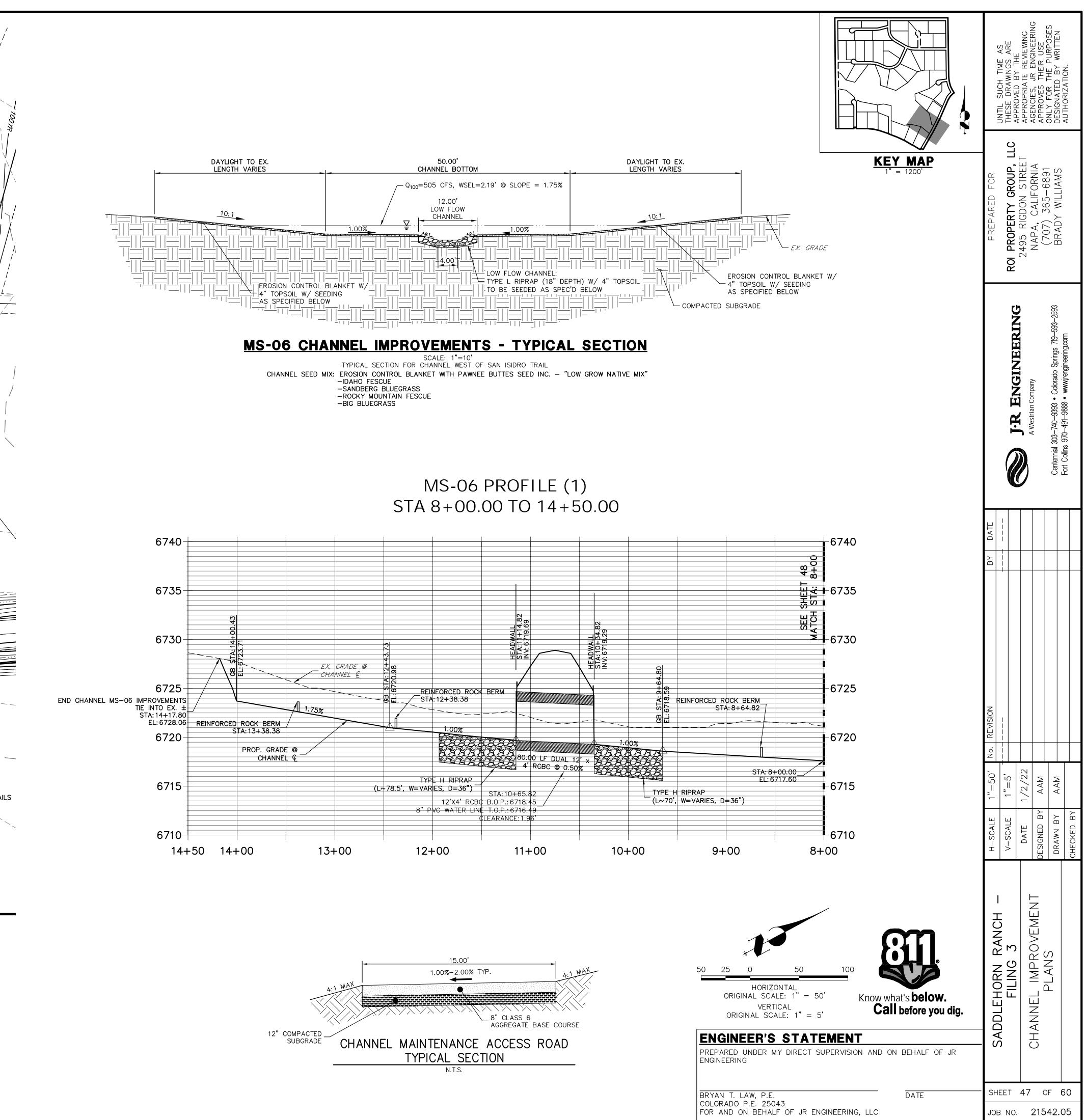


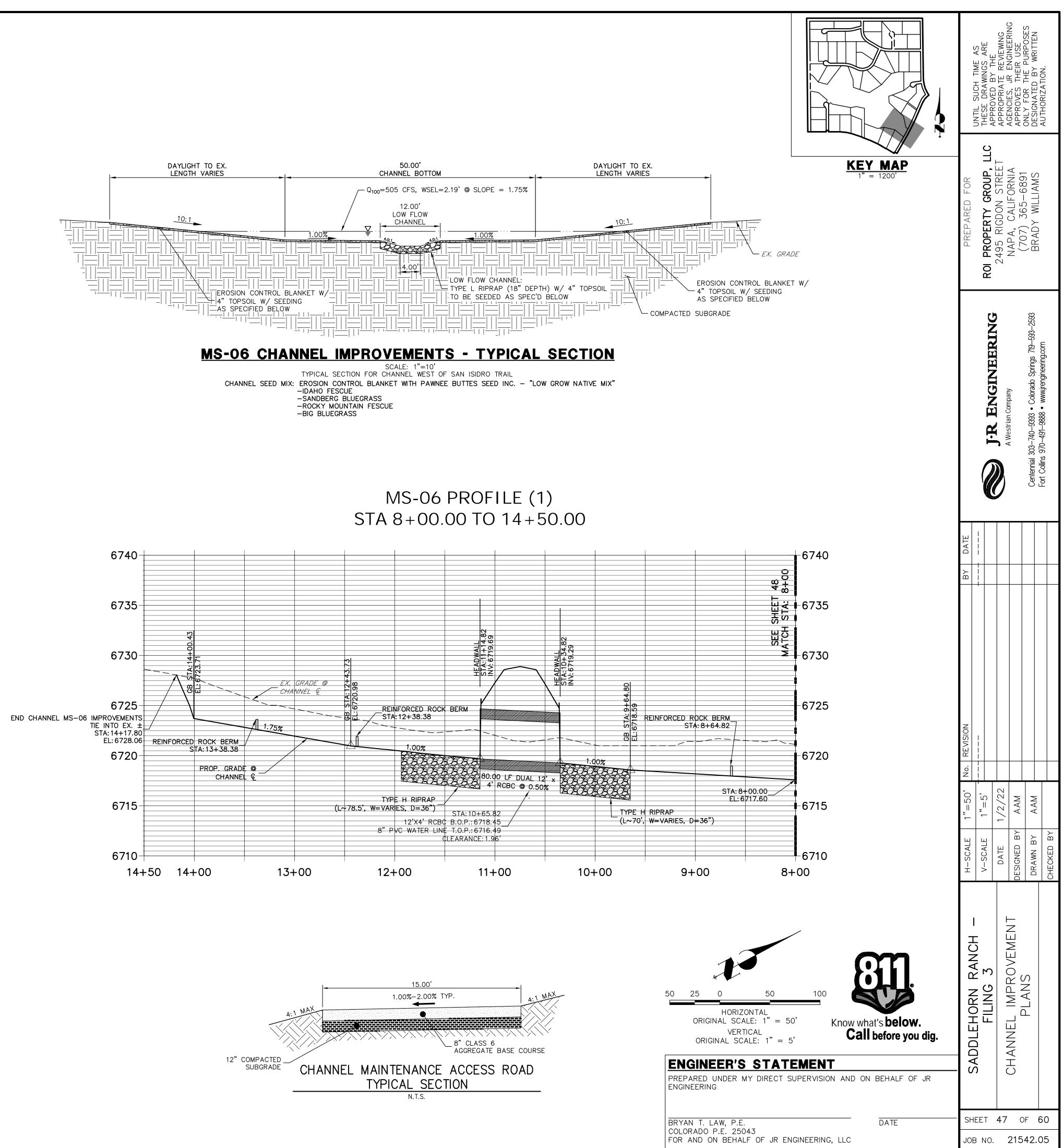
NO RISE CERTIFICATION SADDLEHORN RANCH - FILING 3 JOB NO. 25142.05 1/4/21 SHEET 1 OF 1

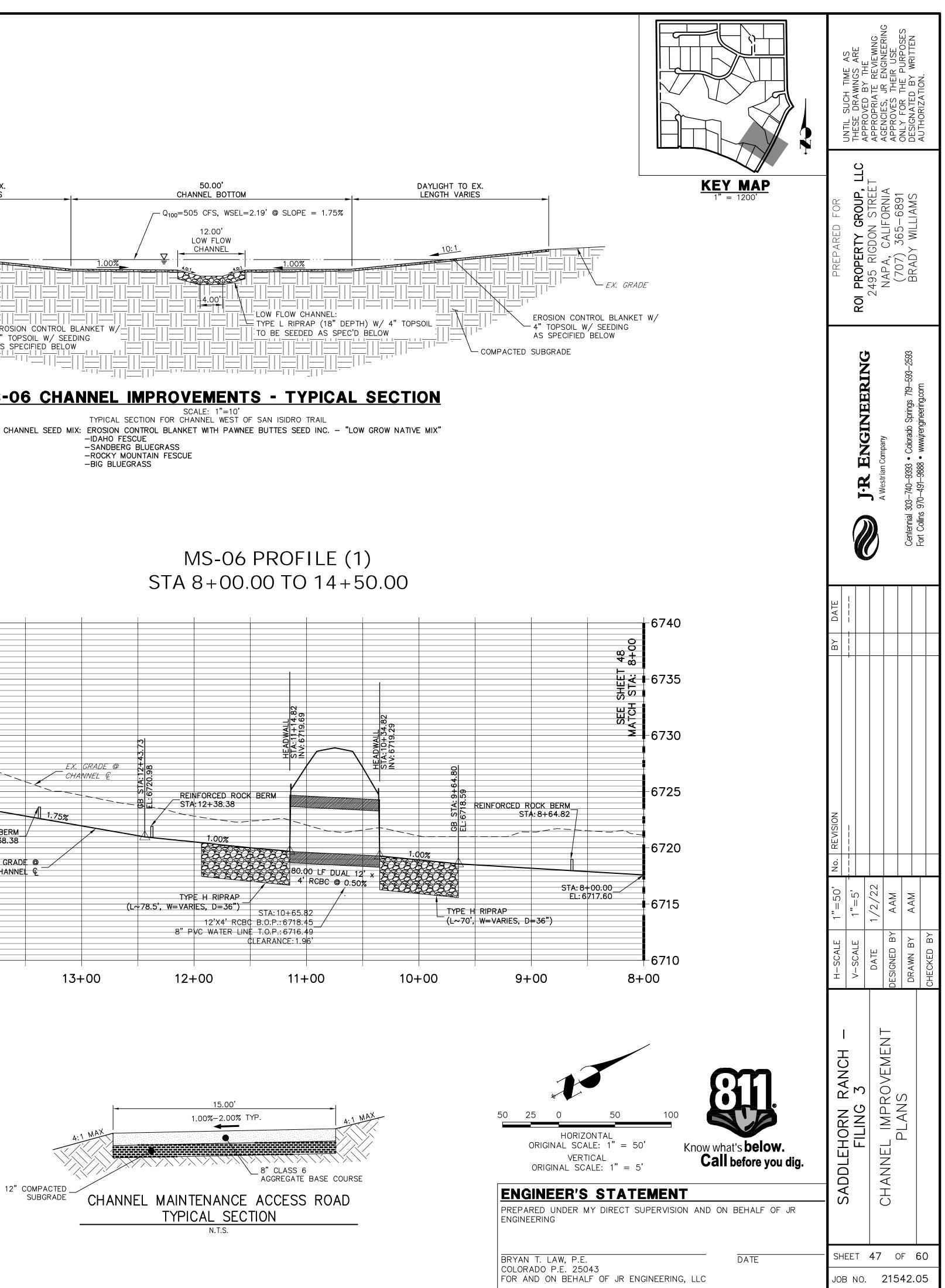


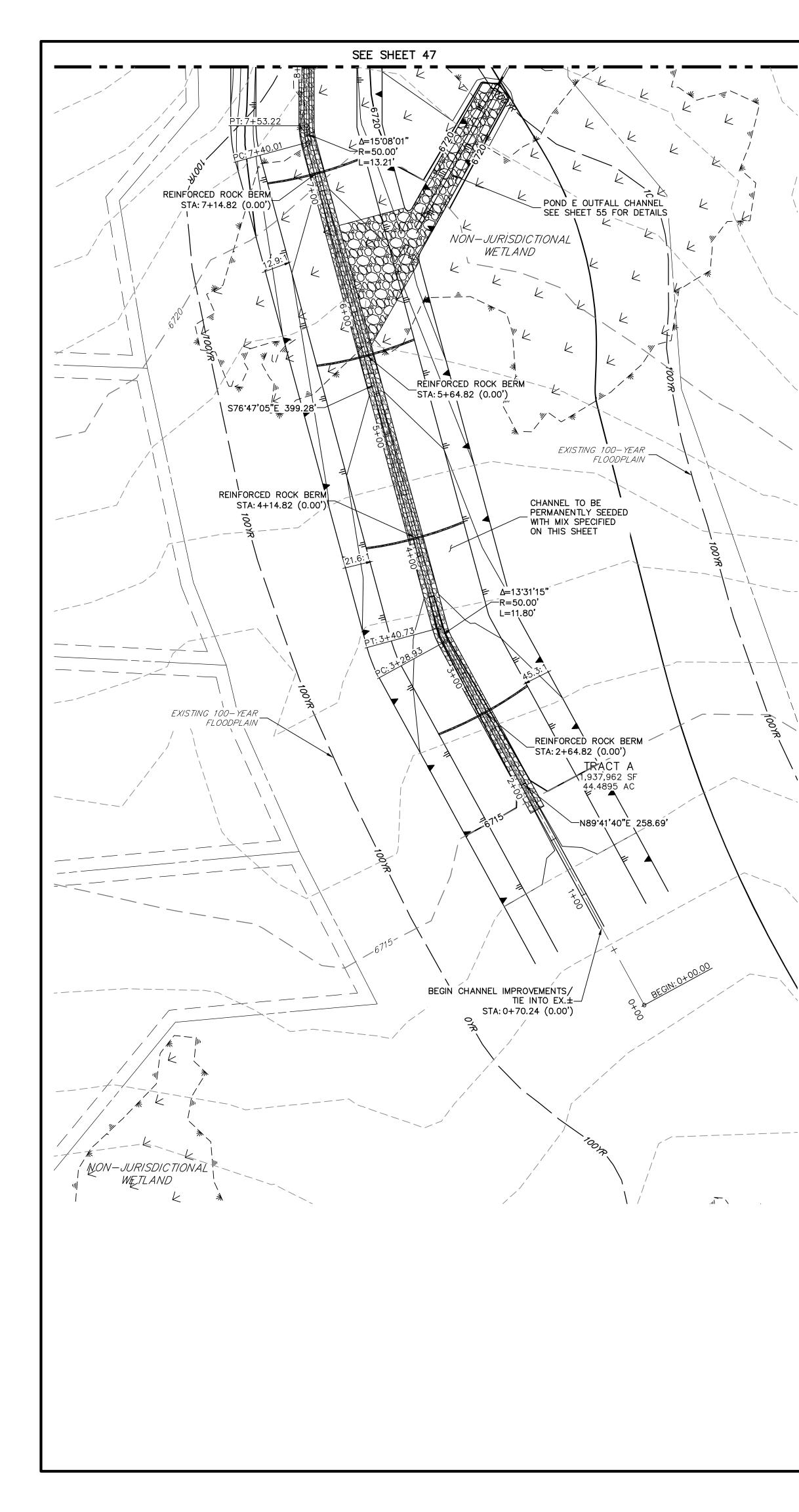
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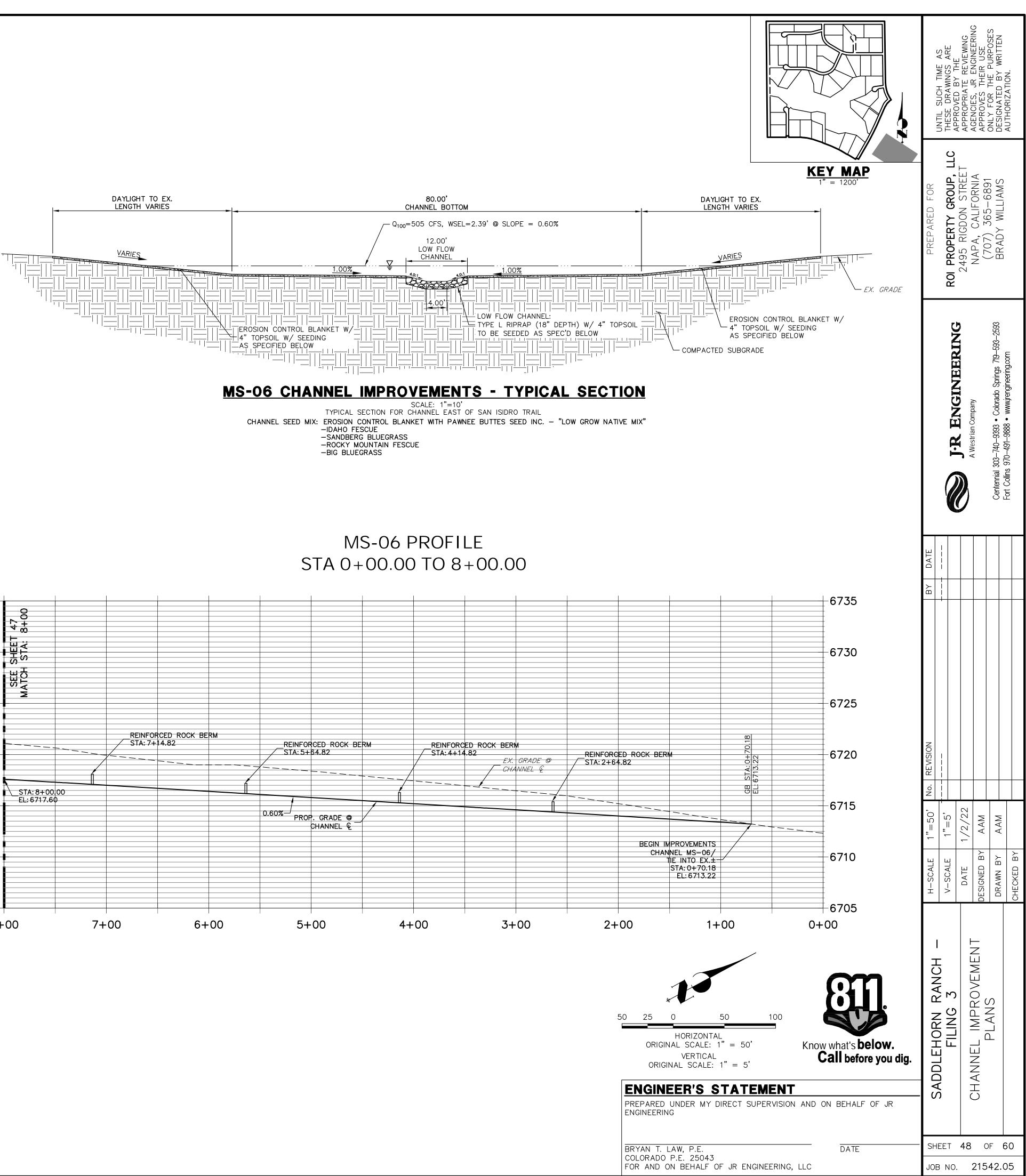


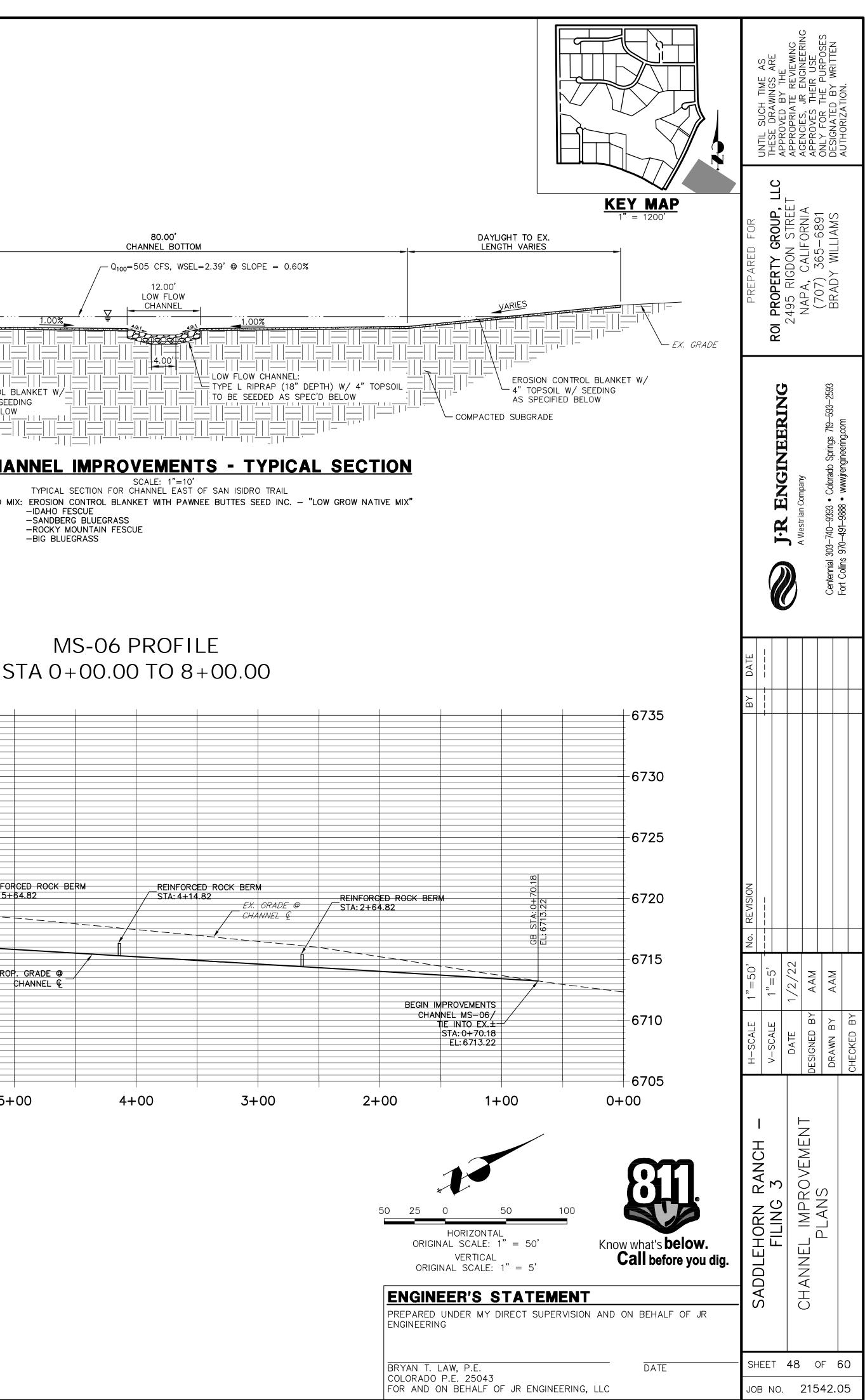


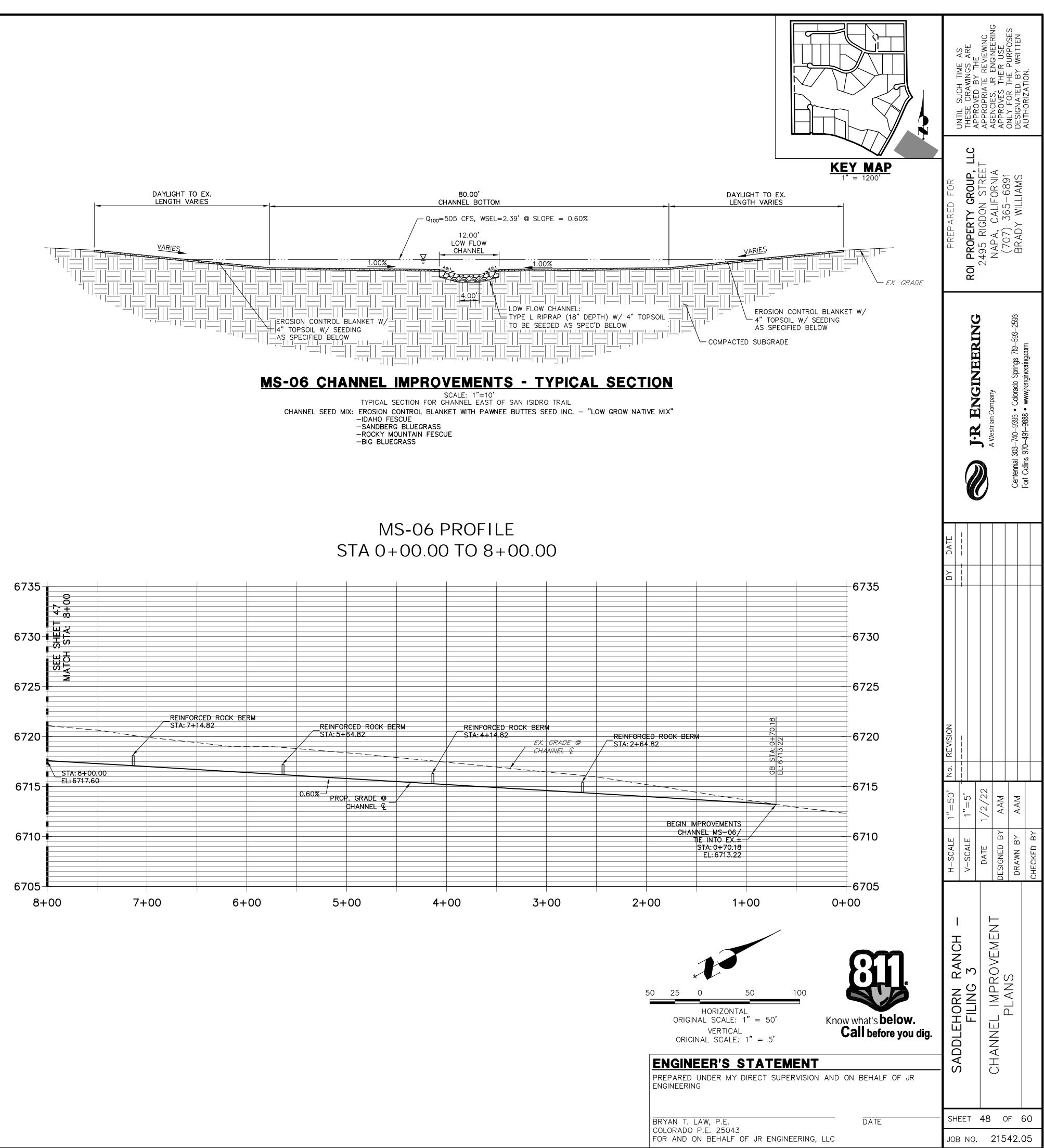












# **HY-8 Culvert Analysis Report**

### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

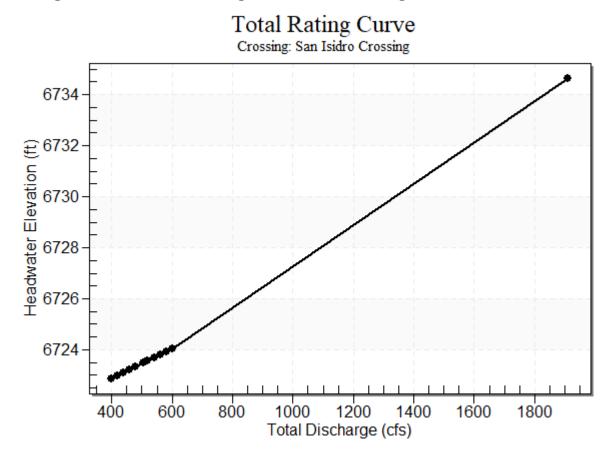
Minimum Flow: 400 cfs

Design Flow: 505 cfs

Maximum Flow: 600 cfs

	•	•		•
Headwater Elevation	Total Discharge (cfs)	San Isidro Crossing	Roadway Discharge	Iterations
(ft)		Discharge (cfs)	(cfs)	
6722.88	400.00	400.00	0.00	1
6722.99	420.00	420.00	0.00	1
6723.11	440.00	440.00	0.00	1
6723.22	460.00	460.00	0.00	1
6723.34	480.00	480.00	0.00	1
6723.48	505.00	505.00	0.00	1
6723.57	520.00	520.00	0.00	1
6723.68	540.00	540.00	0.00	1
6723.80	560.00	560.00	0.00	1
6723.91	580.00	580.00	0.00	1
6724.03	600.00	600.00	0.00	1
6728.59	1176.67	1176.67	0.00	Overtopping

### Table 1 - Summary of Culvert Flows at Crossing: San Isidro Crossing



### Rating Curve Plot for Crossing: San Isidro Crossing

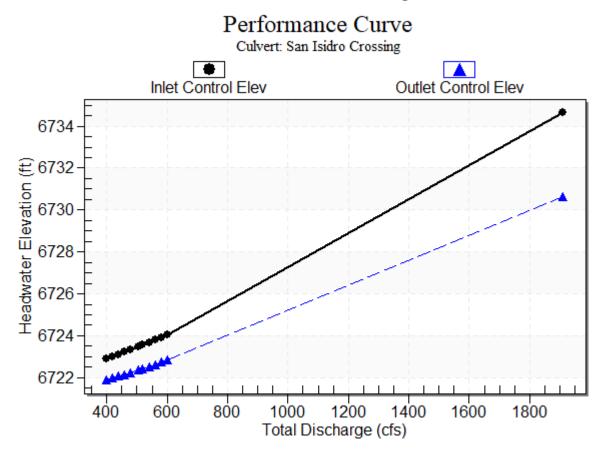
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
400.00	400.00	6722.88	3.460	2.468	1-S2n	1.613	2.051	1.708	2.429	9.757	4.329
420.00	420.00	6722.99	3.575	2.556	1-S2n	1.666	2.119	1.767	2.470	9.901	4.394
440.00	440.00	6723.11	3.689	2.646	1-S2n	1.718	2.185	1.826	2.510	10.041	4.457
460.00	460.00	6723.22	3.803	2.737	1-S2n	1.769	2.251	1.884	2.550	10.176	4.517
480.00	480.00	6723.34	3.917	2.829	1-S2n	1.819	2.316	1.941	2.588	10.305	4.576
505.00	505.00	6723.48	4.060	2.947	5-S2n	1.881	2.396	2.011	2.635	10.462	4.646
520.00	520.00	6723.57	4.146	3.019	5-S2n	1.918	2.443	2.053	2.663	10.553	4.687
540.00	540.00	6723.68	4.261	3.116	5-S2n	1.967	2.505	2.108	2.699	10.672	4.740
560.00	560.00	6723.80	4.377	3.214	5-S2n	2.015	2.567	2.163	2.735	10.787	4.792
580.00	580.00	6723.91	4.494	3.315	5-S2n	2.063	2.627	2.218	2.769	10.894	4.842
600.00	600.00	6724.03	4.612	3.417	5-S2n	2.110	2.687	2.273	2.804	11.000	4.891

 Table 2 - Culvert Summary Table: San Isidro Crossing

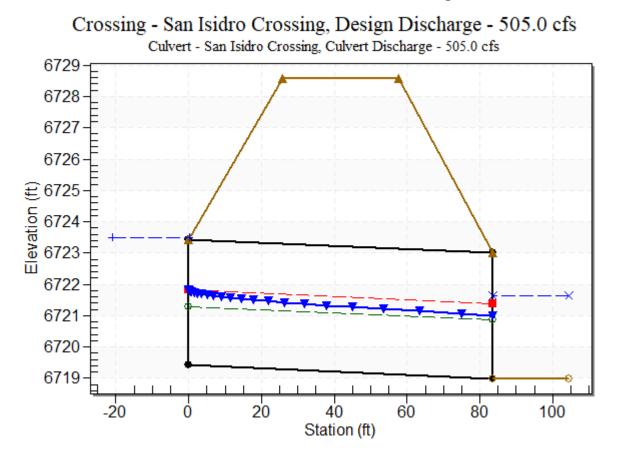
### 

Straight Culvert

Inlet Elevation (invert): 6719.42 ft, Outlet Elevation (invert): 6719.00 ft Culvert Length: 83.50 ft, Culvert Slope: 0.0050



### Culvert Performance Curve Plot: San Isidro Crossing



### Water Surface Profile Plot for Culvert: San Isidro Crossing

### Site Data - San Isidro Crossing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 6719.42 ft Outlet Station: 83.50 ft Outlet Elevation: 6719.00 ft Number of Barrels: 2

### Culvert Data Summary - San Isidro Crossing

Barrel Shape: Concrete Box Barrel Span: 12.00 ft Barrel Rise: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
400.00	6721.43	2.43	4.33	0.91	0.70
420.00	6721.47	2.47	4.39	0.92	0.70
440.00	6721.51	2.51	4.46	0.94	0.70
460.00	6721.55	2.55	4.52	0.95	0.70
480.00	6721.59	2.59	4.58	0.97	0.70
505.00	6721.64	2.64	4.65	0.99	0.71
520.00	6721.66	2.66	4.69	1.00	0.71
540.00	6721.70	2.70	4.74	1.01	0.71
560.00	6721.73	2.73	4.79	1.02	0.71
580.00	6721.77	2.77	4.84	1.04	0.71
600.00	6721.80	2.80	4.89	1.05	0.72

### Table 3 - Downstream Channel Rating Curve (Crossing: San Isidro Crossing)

### Tailwater Channel Data - San Isidro Crossing

Tailwater Channel Option: Irregular Channel

### Roadway Data for Crossing: San Isidro Crossing

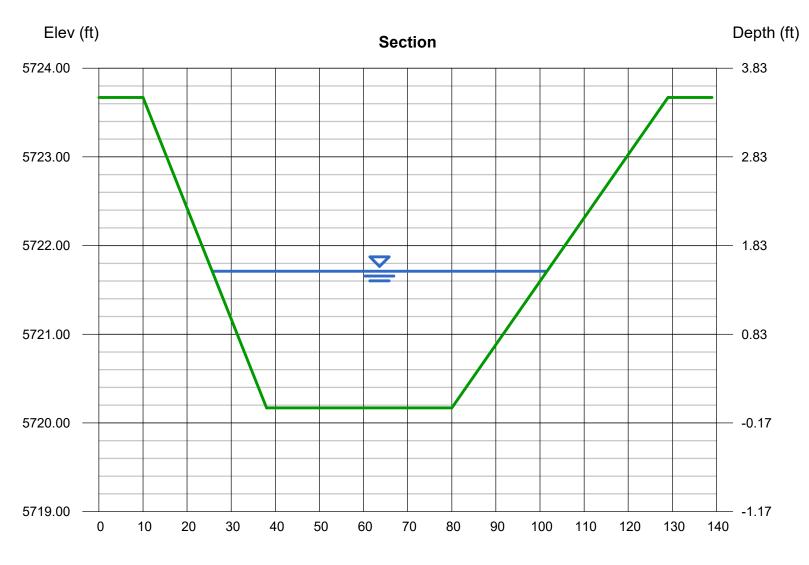
Roadway Profile Shape: Constant Roadway Elevation Crest Length: 6.00 ft Crest Elevation: 6728.59 ft Roadway Surface: Paved Roadway Top Width: 32.00 ft

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 21 2021

### Section 13

Trapezoidal		Highlighted	
Bottom Width (ft)	= 42.00	Depth (ft)	= 1.54
Side Slopes (z:1)	= 8.00, 14.00	Q (cfs)	= 505.00
Total Depth (ft)	= 3.50	Area (sqft)	= 90.77
Invert Elev (ft)	= 5720.17	Velocity (ft/s)	= 5.56
Slope (%)	= 1.00	Wetted Perim (ft)	= 76.03
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.45
		Top Width (ft)	= 75.88
Calculations		EGL (ft)	= 2.02
Compute by:	Known Q		
Known Q (cfs)	= 505.00		



Reach (ft)

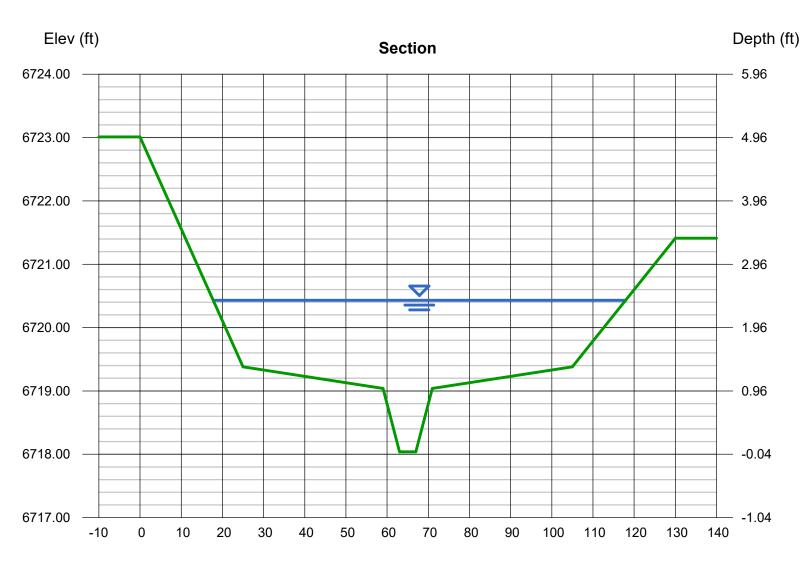
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 21 2021

### Section 14

User-defined		Highlighted	
Invert Elev (ft)	= 6718.04	Depth (ft)	= 2.39
Slope (%)	= 0.60	Q (cfs)	= 505.00
N-Value	= 0.030	Area (sqft)	= 118.25
		Velocity (ft/s)	= 4.27
Calculations		Wetted Perim (ft)	= 100.53
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.11
Known Q (cfs)	= 505.00	Top Width (ft)	= 100.17
		EGL (ft)	= 2.67

(Sta, El, n)-(Sta, El, n)... (0.00, 6723.01)-(25.00, 6719.38, 0.030)-(59.00, 6719.04, 0.030)-(63.00, 6718.04, 0.030)-(67.00, 6718.04, 0.030)-(71.00, 6719.04, 0.030)-(105.00, 6719.38, 0.030) -(130.00, 6721.41, 0.030)



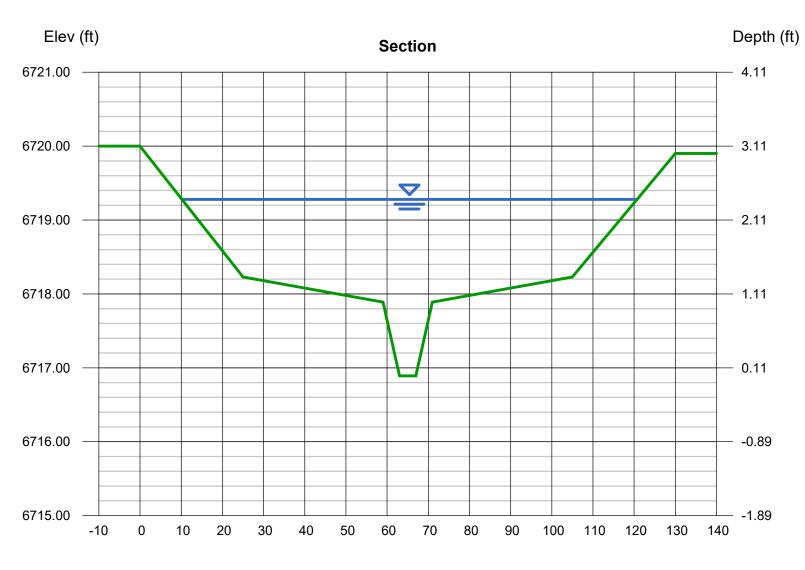
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 21 2021

### Section 15

User-defined		Highlighted	
Invert Elev (ft)	= 6716.89	Depth (ft)	= 2.39
Slope (%)	= 0.60	Q (cfs)	= 505.00
N-Value	= 0.030	Area (sqft)	= 123.70
		Velocity (ft/s)	= 4.08
Calculations		Wetted Perim (ft)	= 110.88
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.11
Known Q (cfs)	= 505.00	Top Width (ft)	= 110.56
		EGL (ft)	= 2.65

(Sta, El, n)-(Sta, El, n)... (0.00, 6720.00)-(25.00, 6718.23, 0.030)-(59.00, 6717.89, 0.030)-(63.00, 6716.89, 0.030)-(67.00, 6716.89, 0.030)-(71.00, 6717.89, 0.030)-(105.00, 6718.23, 0.030) -(130.00, 6719.90, 0.030)



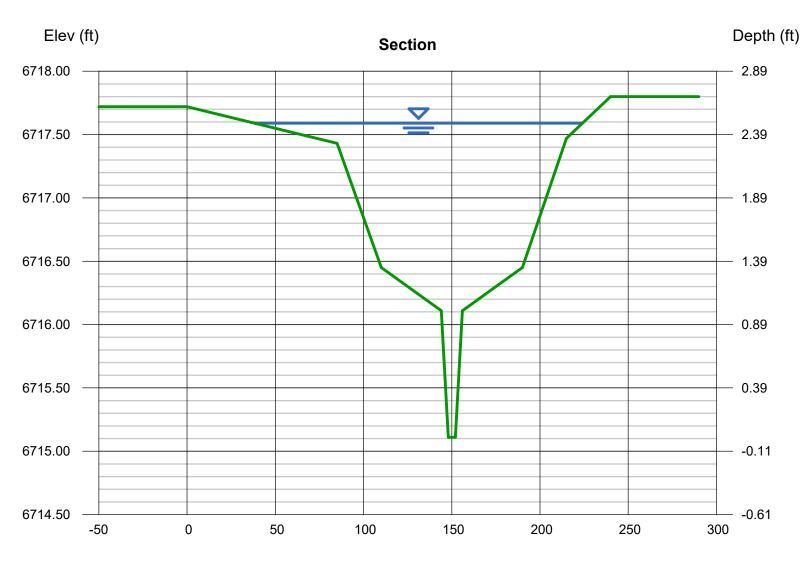
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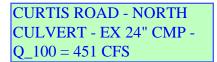
Tuesday, Dec 21 2021

### Section 16

User-defined		Highlighted	
Invert Elev (ft)	= 6715.11	Depth (ft)	= 2.48
Slope (%)	= 0.60	Q (cfs)	= 505.00
N-Value	= 0.030	Area (sqft)	= 151.09
		Velocity (ft/s)	= 3.34
Calculations		Wetted Perim (ft)	= 186.16
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.10
Known Q (cfs)	= 505.00	Top Width (ft)	= 185.87
		EGL (ft)	= 2.65

(Sta, El, n)-(Sta, El, n)... (0.00, 6717.72)-(85.00, 6717.43, 0.030)-(110.00, 6716.45, 0.030)-(144.00, 6716.11, 0.030)-(148.00, 6715.11, 0.030)-(152.00, 6715.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(1 -(190.00, 6716.45, 0.030)-(215.00, 6717.47, 0.030)-(240.00, 6717.80, 0.030)





### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 400 cfs

Design Flow: 451 cfs

Maximum Flow: 500 cfs

Headwater Elevation	Total Discharge (cfs)	Culvert 1 Discharge	Roadway Discharge	Iterations
(ft)		(cfs)	(cfs)	
				_
6766.93	400.00	20.40	379.08	7
6766.94	410.00	20.45	389.44	3
6766.95	420.00	20.49	398.64	2
6766.96	430.00	20.54	409.36	3
6766.97	440.00	20.58	418.71	2
6766.98	450.00	20.62	429.31	3
6766.98	451.00	20.62	430.26	2
6767.00	470.00	20.70	448.42	2
6767.01	480.00	20.74	458.27	2
6767.01	490.00	20.78	468.29	2
6767.02	500.00	20.81	478.44	2
6766.00	14.84	14.84	0.00	Overtopping

### Table 10 - Summary of Culvert Flows at Crossing: North Curtis Road

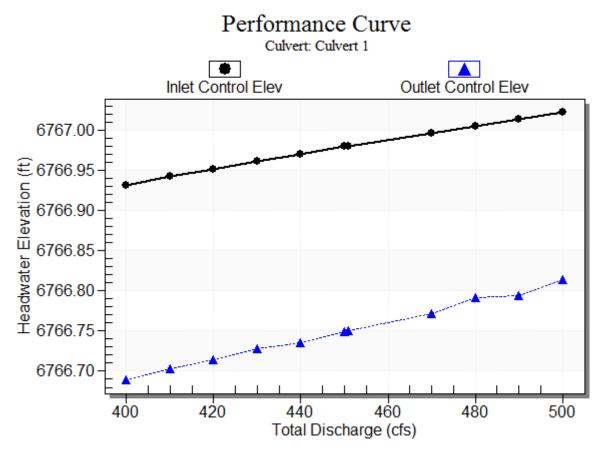
Total Rating Curve Crossing: North Curtis Road

Rating Curve Plot for Crossing: North Curtis Road

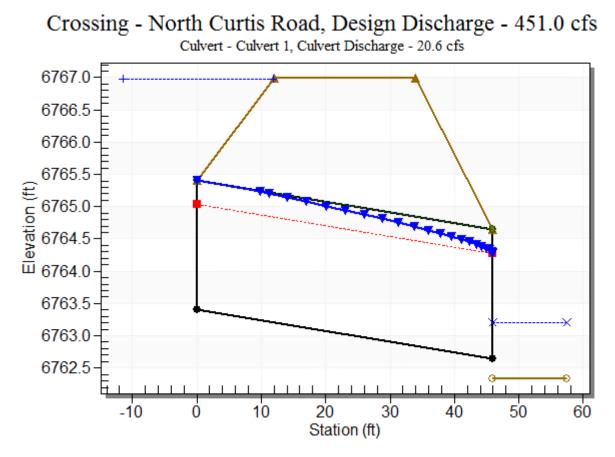
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
400.00	20.40	6766.93	3.521	3.279	7-M2c	2.000	1.619	1.619	0.818	7.488	2.820
410.00	20.45	6766.94	3.532	3.293	7-M2c	2.000	1.621	1.621	0.827	7.498	2.843
420.00	20.49	6766.95	3.540	3.305	7-M2c	2.000	1.622	1.622	0.836	7.507	2.866
430.00	20.54	6766.96	3.551	3.318	7-M2c	2.000	1.624	1.624	0.845	7.517	2.888
440.00	20.58	6766.97	3.559	3.326	7-M2c	2.000	1.625	1.625	0.853	7.525	2.910
450.00	20.62	6766.98	3.569	3.339	7-M2c	2.000	1.627	1.627	0.862	7.535	2.932
451.00	20.62	6766.98	3.570	3.340	7-M2c	2.000	1.627	1.627	0.863	7.536	2.934
470.00	20.70	6767.00	3.586	3.362	7-M2c	2.000	1.630	1.630	0.879	7.551	2.974
480.00	20.74	6767.01	3.595	3.382	7-M2c	2.000	1.631	1.631	0.887	7.560	2.995
490.00	20.78	6767.01	3.604	3.384	7-M2c	2.000	1.632	1.632	0.895	7.568	3.015
500.00	20.81	6767.02	3.612	3.404	7-M2c	2.000	1.634	1.634	0.904	7.576	3.035

Table 11 - Culvert Summary Table: Culvert 1

#### **Culvert Performance Curve Plot: Culvert 1**



#### Water Surface Profile Plot for Culvert: Culvert 1

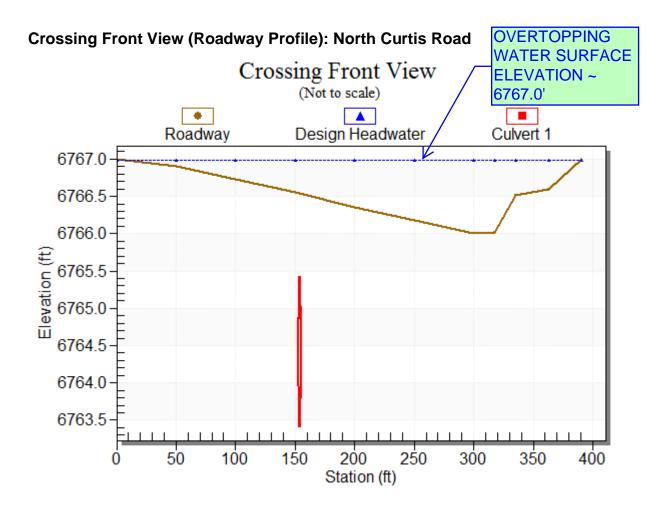


#### Site Data - Culvert 1

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 6763.41 ft Outlet Station: 46.00 ft Outlet Elevation: 6762.64 ft Number of Barrels: 1

#### **Culvert Data Summary - Culvert 1**

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Corrugated Steel Embedment: 0.00 in Barrel Manning's n: 0.0220 Culvert Type: Straight Inlet Configuration: Thin Edge Projecting Inlet Depression: None



## GIECK RANCH DRAINAGE BASIN PLANNING STUDY El Paso County, Colorado

Volume 1 – Final Report

October 1, 2007 Revised: February 10, 2010

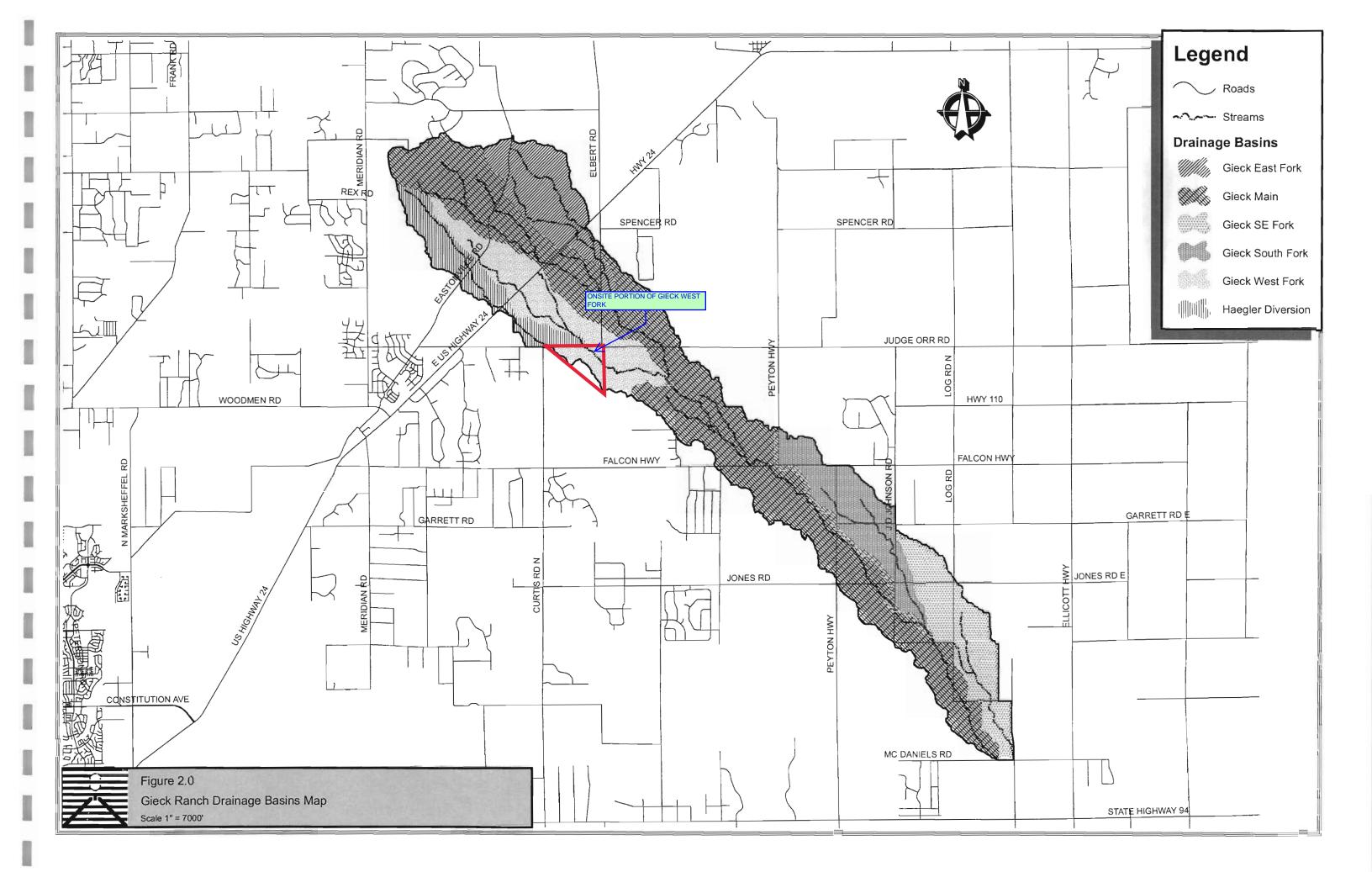
#### PREPARED FOR:

 $\widehat{\mu}_{i}^{(0)}$ 

975 Ford LP, LLP 118 North Tejon Street, Suite 213 Colorado Springs, CO 80903 (719) 491-4169 Contact: Neil McLeod

#### PREPARED BY:

Drexel, Barrell & Co. 3 S. 7th Street Colorado Springs, CO 80905 (719) 260-0887 Contact: James A. Brzostowicz , P.E. DBC Project Number: C-7706-2



			Accumulative	Existing	Future	%	Existing	Future	%
Design		Hydrologic	Accumulative	Peak Flow	Peak Flow	Difference	Volume	Volume	Difference
Point ID	Design Point Location	Element	$(mi^2)$	(cfs)	(cfs)	Peak Flow	(ac-ft)	(ac-ft)	Volume
1	Haegler Diversion at Eastonville Road	HD-J2	0.8	431	1060	146%	77	96	25%
2	West Fork at Eastonville Road	WF-J1	0.3	146	389	166%	29	39	33%
3	Main Channel at Eastonville Road	MS-J4	1.3	730	1233	69%	112	135	20%
4	Haegler Diversion at Highway 24	HD-J4	1.3	521	1223	135%	97	121	24%
5	West Fork at Highway 24	WF-J3	0.4	224	605	170%	49	62	26%
6	Main Channel at Highway 24 CONTRIBUTING ACREAGE TO WE	MS-J6	2.5	997	1896	90%	194	225	16%
7	East Fork at Highway 24	EF-J4	1.2	1054	1113	6%	124	126	1%
8	Main Channel at Elbert Road	MS-J7	3.0	1010	1896	88%	220	253	15%
9	Fast Fork at Filtert Road	EF-16	2.1	1120	1172	5%	183	187	2%
10	West Fork at Judge Orr Road	WF-J6	$\rightarrow$ 1.5	1017	2213	117%	244	291	19%
11	Confluence of East Fork and Main Channel	MS-J9	5.7	1817	3068	69%	429	467	9%
12	Main Channel at Judge Orr Road	MS-J11	6.7	1968	3383	72%	487	564	16%
13	Confluence of West Fork and Main Channel	MS-J12	11.2	2732	6104	123%	805	993	23%
14	Main Channel at Falcon Highway	MS-J16	13.4	3045	6784	_123%	936	1191	27%
15	Main Channel at Peyton Highway	MS-J19	15.1	3200	6946	117%	1012	1269	25%
16	Main Channel at Jones Road	MS-J20	15.6	3250	7056	117%	1040	1308	26%
17	South Fork at Jones Road	SF-J4	1.3	454	454	0%	133	133	0%
18	Confluence of South Fork and Main Channel	MS-J22	17.9	3650	7392	103%	1210	1489	23%
19	Southeast Fork at McDaniels Road	SE-J3	2.4	547	546	0%	210	210	0%
20	Main Channel at McDaniels Road	MS-J29	19.6	3791	7525	99%	1293	1597	23%
21	Total Combined Outfall	SE-J3 plus MS-J29	22.0	4326	7687	78%	1503	1807	20%

Table 6.4: Summary of Flows at Selected Design Points - 100-year Storm Event

The 100-year storm event future undetained peak flow is estimated to increase by 78% over the existing peak flow while the future volume of runoff is estimated to increase by 20%. During the hydrologic analysis it was observed that the Black Squirrel Creek lies very close to the eastern boundary of the Gieck Ranch Basin from Falcon Highway downstream to Log Road. It is possible that flow from Black Squirrel Creek could spill into the Gieck Ranch Basin during extreme storm events. The flows in Black Squirrel Creek in this area are expected to be more than 5,000 cfs for the 100-year event. If the Black Squirrel Creek were to overflow its' banks and flow into the Gieck Ranch Basin it could increase the flows shown in the above tables. Possible improvements to address this potential problem include channel improvements to increase the Black Squirrel Creek conveyance in this area or constructing berms on the east bank to prevent overflow.

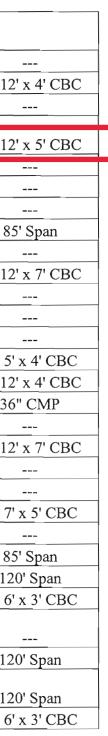
35	Elbert Road south of structure 34	24" CMP	Good	100%	Y	
36	Elbert Road at Main Channel	2 - 48" CMP	Good	19%	N	3 - 12
37	Elbert Road south of structure 36	24" CMP	Poor	55%	Y	
		67" - 05"				
38	Judge Orr Road at West Fork	CMP	Good	20%	<u>N</u>	4 - 12
39	Judge Orr Road east of structure 38	36" CMP	Good	100%	Y	
40	Judge Orr Road west of structure 41	24" CMP	Poor	90%	Y	
41	Judge Orr Road at Main Channel	Bridge	Good	100%	Y	
42	Falcon Hwy at Main Channel	Bridge	Good	57%	N	85
13	Peyton Road at headwaters of South Fork	24" CMP	Fair	75%	Y	
14	Peyton Road at Main Channel	4 - 24" RCP	Good	2%	N	5 - 12
45	Peyton Road south of structure 44	36" CMP	Poor	100%	Y	
46	Peyton Road south of structure 45	24" CMP	Good	100%	Y	
17	East Garrett Road west of structure 48	24" CMP	Poor	100%	Y	
48	East Garrett Road at South Fork	48" CMP	Good	14%	N	2 - 5'
19	J.D. Johnson Road at South Fork	4 - 42" RCP	Good	63%	N	2 - 12
50	J.D. Johnson Road south of structure 49	30" CMP	Fair	56%	N	36
51	J.D. Johnson Road south of structure 50	30" CMP	Fair	100%	Y	
52	Jones Road at Main Channel	60" CMP	Fair	4%	N	6 - 12
53	J.D. Johnson Road at Jones Road	30" CMP	Fair	55%	Y	
54	Jones Road east of J.D. Johnson Road	30" CMP	Good	73%	Y	
55	Jones Road at South Fork	36" CMP	Good	6%	N	2 - 7'
56	Jones Road east of structure 55	30" CMP	Fair	67%	Y	
57	J.D. Johnson Road at Main Channel US of structure 58	3 - 60" RCP	Good	14%	N	85
58	J.D. Johnson Road at Main Channel	30" CMP	Good	1%	N	120
59	J.D. Johnson Road and Log Road	24" CMP	Fair	23%	N	2 - 6'
		48" CMP				
50	Main Channel at private driveway	(est.)	Unknown	2%	<u>N.E.</u>	
51	Log Road at Main Channel	Bridge	Good	36%	N	12
		30" x 48"				
<u>5</u> 2	McDaniel Road at Main Channel	Oval CMP	Good	1%	<u>N</u>	120
53	Log Road and McDaniels Road	24" CMP	Good	2%	N	5 - 6'

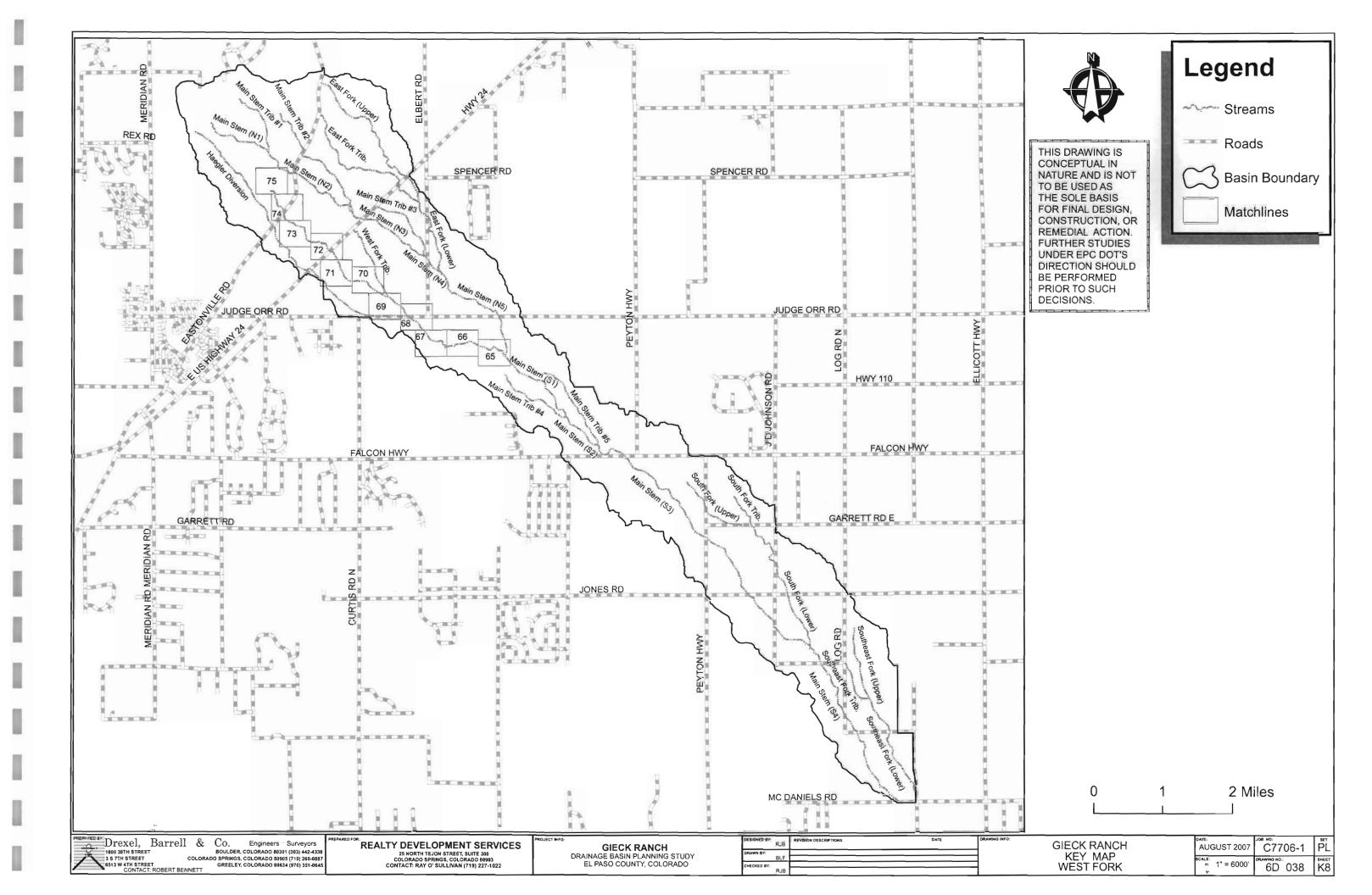
* Road over-topping not included

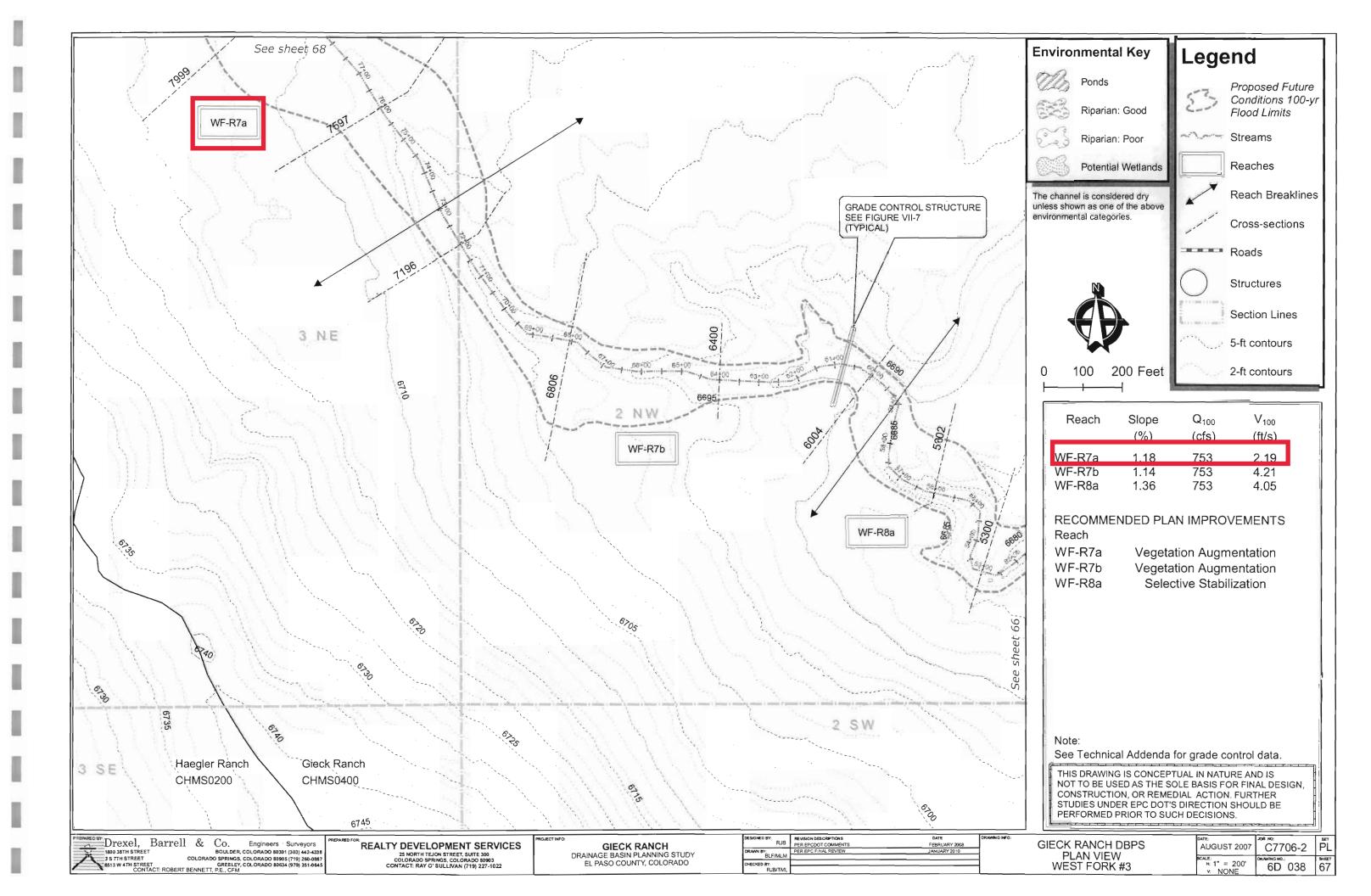
** Allowable road over-topping included in adequacy analysis

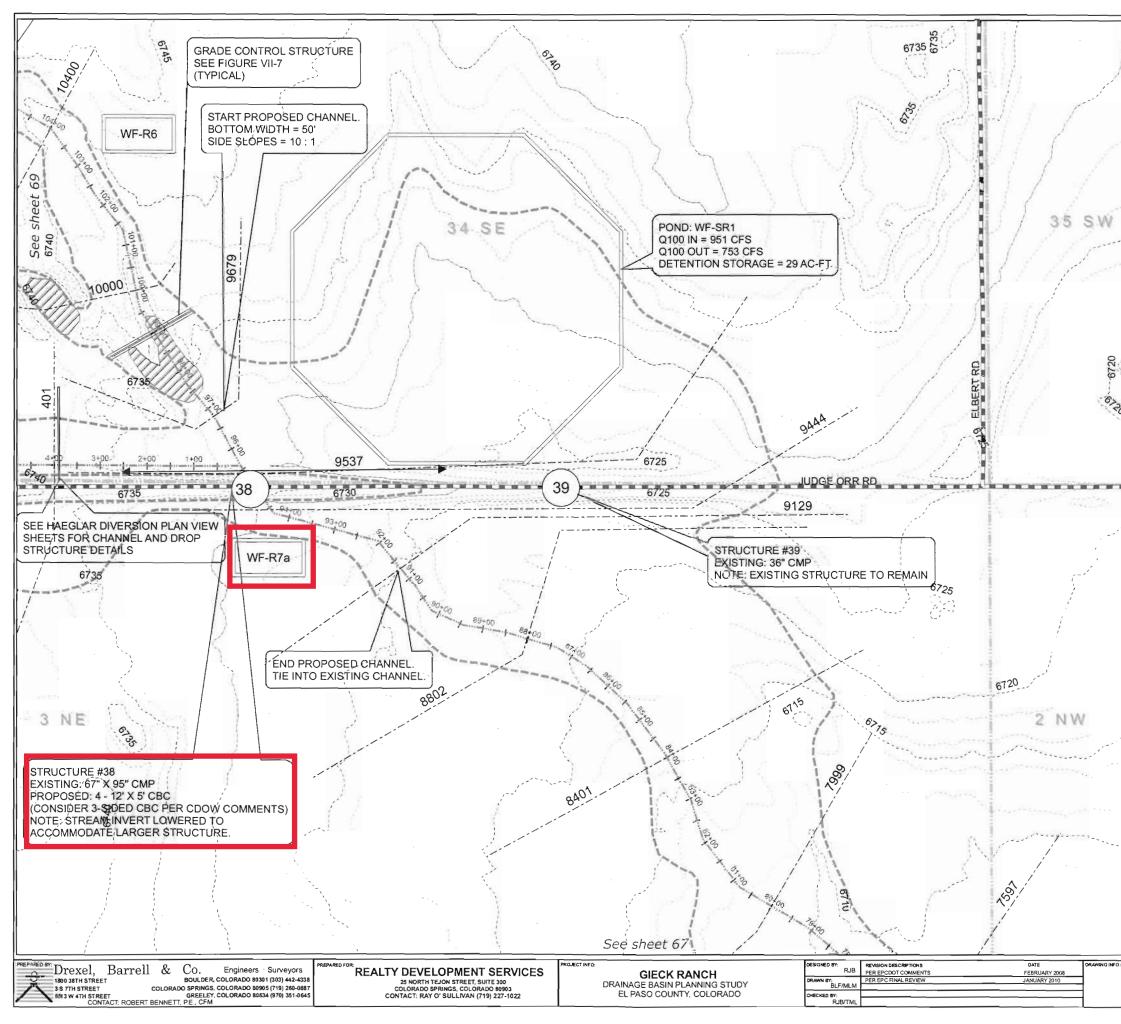
*** Based on proposed (with selected drainage basin plan) flows

N.E. Not Evaluated, not EPCDOT responsibility







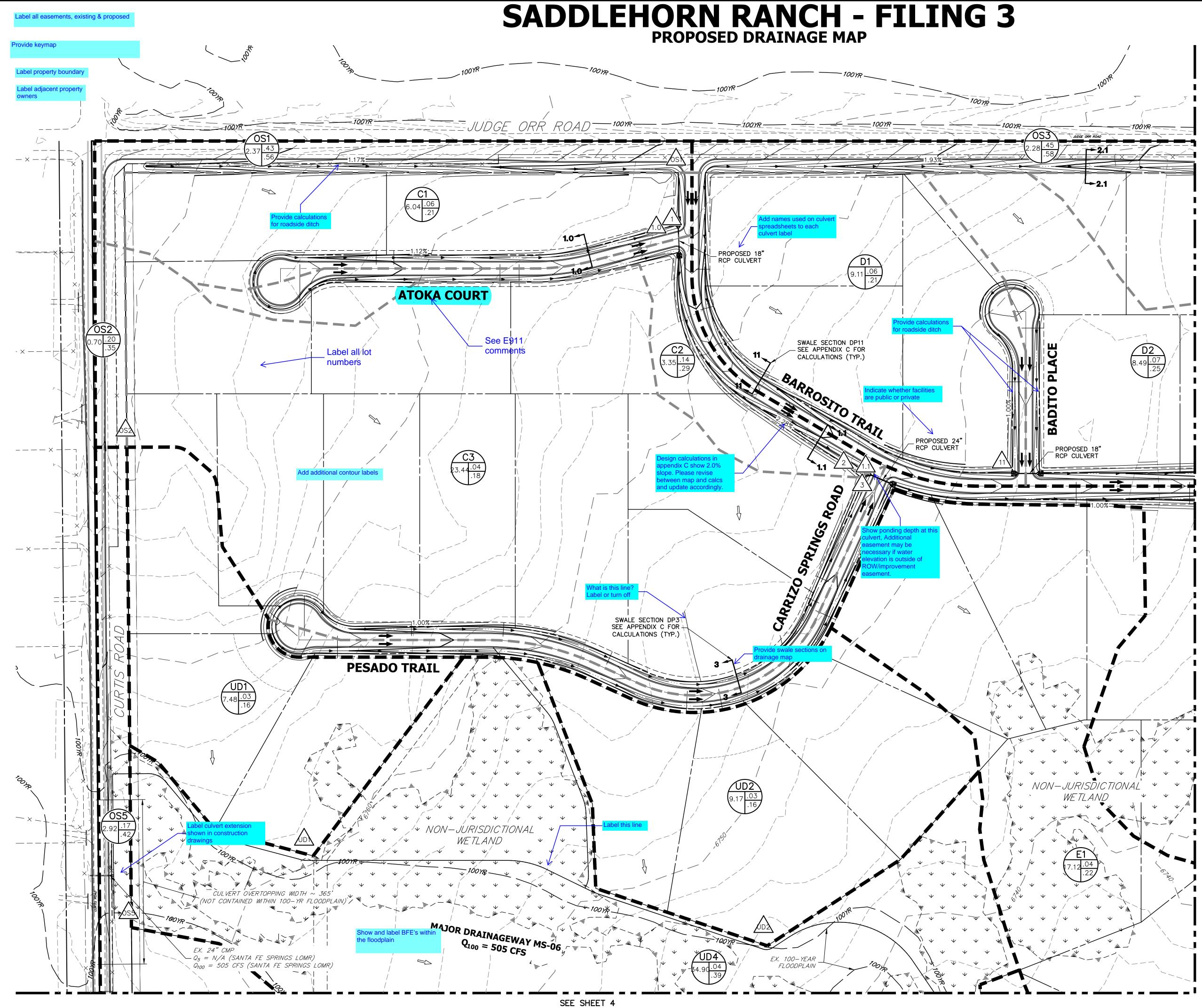


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/	En	viror	nmenta	l Key	Lege	end	
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ð	E	20	Riparian	: Poor	~~~~	Streams	
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			tal categor			Cross-sections	
				- 1	30000	Roads	
			N	- 1	$\bigcirc$	Structures	
		4				Section Lines	
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- 7					( - )		
-			De	(%) 1.04	(cfs)	(ft/s)	
		WF-		. ,	. ,	. ,	
		WF-	R7a	1.04 1.18	608 753	2.45	
		WF- REC Rea	R7a ℃OMME ch	1.04 1.18 NDED PLA	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a ℃OMME ch	1.04 1.18 NDED PLA Selec	608 753	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- REC Rea WF-	R7a COMME ch -R6	1.04 1.18 NDED PLA Selec	753 AN IMPRC	2.45 2.19 OVEMENTS	
		WF- Rea WF	R7a COMME ch -R6 -R7a	1.04 1.18 NDED PLA Selec Vegeta	753 AN IMPRC ctive Stab	2.45 2.19 OVEMENTS ilization nentation	
		WF- REC Rea WF- WF-	R7a COMME ch -R6 -R7a	1.04 1.18 NDED PLA Selec Vegeta G IS CONCEP ED AS THE SCONCEP SON, OR REME	TUAL IN NATI	2.45 2.19 OVEMENTS ilization nentation URE AND IS OR FINAL DESIGN, V. FURTHER	
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Final Drainage Report Filing 3 - Saddlehorn Ranch

#### APPENDIX F

### **DRAINAGE MAPS & PLANS**

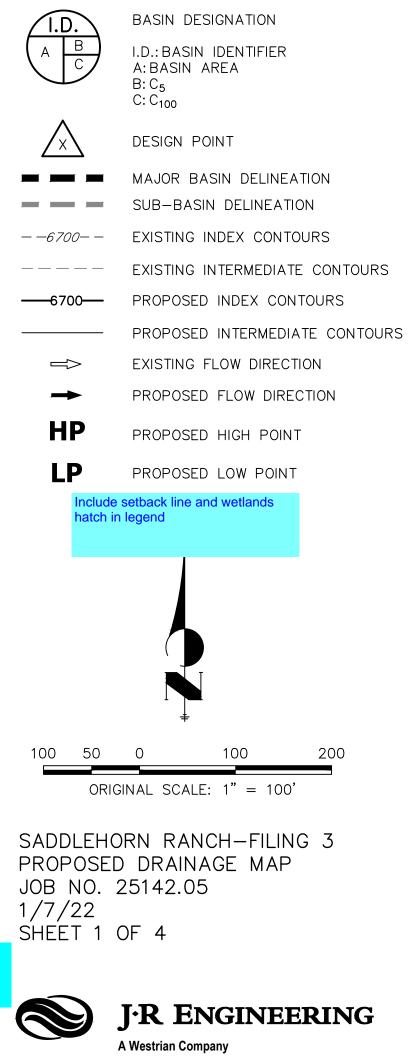


Tributary	Area	Percent			t _c	Q₅	<b>Q</b> ₁₀₀
Sub-basin	(acres)	Impervious	C₅	C ₁₀₀	(min)	(cfs)	(cfs)
C1	6.04	13%	0.06	0.21	35.8	0.9	4.8
C2	3.35	24%	0.14	0.29	31.5	1.1	4.0
C3	23.44	9%	0.04	0.18	41.2	1.8	14.1
C4	10.94	18%	0.14	0.42	40.3	3.2	15.5
C5	2.35	20%	0.11	0.26	23.8	0.7	2.9
C6	3.95	22%	0.12	0.28	26.6	1.3	5.0
C7	2.14	24%	0.17	0.38	13.9	1.3	4.9
C8	22.55	10%	0.05	0.19	33.7	2.4	16.4
C9	2.63	35%	0.23	0.39	29.6	1.5	4.3
C10	16.38	12%	0.05	0.20	27.6	2.3	14.3
D1	9.11	13%	0.06	0.21	27.8	1.5	8.3
D2	8.49	13%	0.07	0.25	34.7	1.4	8.2
D3	3.21	8%	0.04	0.18	21.1	0.4	2.8
D4	10.01	7%	0.07	0.40	39.8	1.5	13.9
D5	9.56	17%	0.14	0.43	37.6	3.0	14.9
D6	0.34	45%	0.36	0.57	<mark>8</mark> .3	0.5	1.4
D7	33.94	15%	0.10	0.31	38.3	6.9	37.3
E1	17.12	7%	0.04	0.22	46.6	1.3	11.8
E2	0.37	45%	0.31	0.46	7.8	0.5	1.3
E3	0.20	45%	0.32	0.48	5.2	0.3	0.8
E4	0.68	3%	0.01	0.14	14.6	0.04	0.6
UD1	7.48	6%	0.03	0.16	33.5	0.4	4.6
UD2	9.17	6%	0.03	0.16	30.4	0.6	6.0
UD3	2.23	6%	0.04	0.24	27.0	0.2	2.3
UD4	34.90	2%	0.04	0.39	54.3	2.2	36.5
UD5	20.49	6%	0.05	0.30	41.9	2.0	20.3
OS1	2.37	58%	0.43	0.56	20.3	3.1	6.8
OS2	0.70	31%	0.20	0.35	13.1	0.5	1.6
OS3	2.28	<mark>60%</mark>	0.45	0.58	19.5	3.2	6.9
OS4	1.08	<mark>55%</mark>	0.44	0.63	11.8	<u>1.9</u>	4.4
OS5	2.92	23%	0.17	0.42	17.8	1.7	6.7
F1	1.35	40%	0.27	0.43	12.7	1.4	3.6
F2	7.67	11%	0.05	0.20	35.0	0.9	5.7
F3	2.37	45%	0.32	0.49	29.8	<mark>1.</mark> 9	4.9
F4	2.93	45%	0.34	0.52	32.3	2.3	6.0

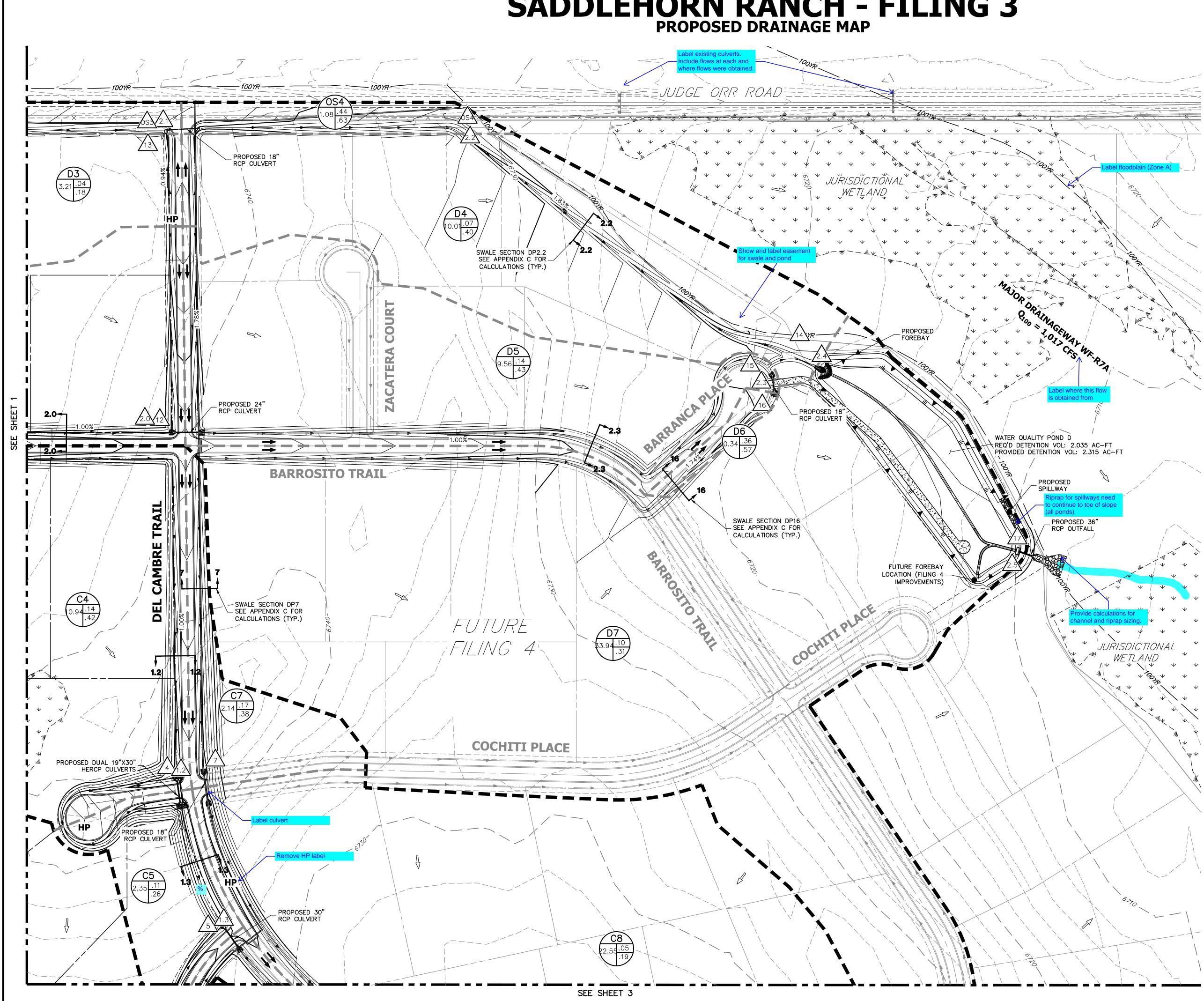
FILING 3 - DESIGN DOINT CLIMANAA DV

Q₅ (cfs) 0.9 1.1 1.8 3.2 0.7 1.3 1.3 2.4 1.5 2.3 1.5 1.4 0.4 1.5 1.4 0.4 1.5 3.0 0.5 6.9	Q ₁₀₀ (Cfs) 4.8 4.0 14.1 15.5 2.9 5.0 4.9 16.4 4.3 14.3 8.3 8.2 2.8 13.9 14.9 14.9 14.9
(cfs) 0.9 1.1 1.8 3.2 0.7 1.3 1.3 2.4 1.5 2.3 1.5 1.4 0.4 1.5 3.0 0.5	(Cfs) 4.8 4.0 14.1 15.5 2.9 5.0 4.9 16.4 4.3 14.3 8.3 8.3 8.2 2.8 13.9 14.9
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$ \begin{array}{c} 1.1\\ 1.8\\ 3.2\\ 0.7\\ 1.3\\ 1.3\\ 2.4\\ 1.5\\ 2.3\\ 1.5\\ 1.4\\ 0.4\\ 1.5\\ 3.0\\ 0.5\\ \end{array} $	4.0 14.1 15.5 2.9 5.0 4.9 16.4 4.3 14.3 8.3 8.3 8.2 2.8 13.9 14.9
1.8         3.2         0.7         1.3         1.3         2.4         1.5         2.3         1.5         1.4         0.4         1.5         3.0         0.5	14.1 15.5 2.9 5.0 4.9 16.4 4.3 14.3 8.3 8.3 8.2 2.8 13.9 14.9
3.2 0.7 1.3 1.3 2.4 1.5 2.3 1.5 1.4 0.4 1.5 3.0 0.5	15.5         2.9         5.0         4.9         16.4         4.3         14.3         8.3         8.2         2.8         13.9         14.9
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1.3 1.3 2.4 1.5 2.3 1.5 1.4 0.4 1.5 3.0 0.5	5.0 4.9 16.4 4.3 14.3 8.3 8.2 2.8 13.9 14.9
1.3         2.4         1.5         2.3         1.5         1.4         0.4         1.5         3.0         0.5	4.9 16.4 4.3 14.3 8.3 8.2 2.8 13.9 14.9
2.4 1.5 2.3 1.5 1.4 0.4 1.5 3.0 0.5	16.4 4.3 14.3 8.3 8.2 2.8 13.9 14.9
1.5 2.3 1.5 1.4 0.4 1.5 3.0 0.5	4.3 14.3 8.3 8.2 2.8 13.9 14.9
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	1 4
0.9	
1 2	37.3
	11.8
	1.3
	0.8
	0.6
	6.8
	1.6
	6.9
	4.4
	6.7
	4.6
	6.0
	2.3
	36.5
	20.3
3.1	9.7
5.6	26.2
6.8	32.2
6.8	32.2
7.6	35.0
3.2	19.6
10.5	50.0
11.1	58.1
2.7	15.4
3.4	9.5
4.3	11.3
4.8	30.1
7.6	38.6
12.2	75.8
1.6	12.6
1.5	12.6
Highlighted match hydro	ology
	6.9 1.3 0.5 0.3 0.04 3.1 0.5 3.2 1.9 1.7 0.4 0.6 0.2 2.2 2.0 3.1 5.6 6.8 6.8 7.6 3.2 10.5 11.1 2.7 3.4 4.3 4.3 4.8 7.6 12.2 1.6 1.5

## LEGEND



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# SADDLEHORN RANCH - FILING 3 PROPOSED DRAINAGE MAP

EILIN							
FILING 3 - DESIGN							
POINT SUMMARYDesignQ5Q100							
Point	(cfs)						
1	0.9	(Cfs) 4.8					
2	1.1	4.0					
3	1.8	14.1					
4	3.2	15.5					
5	0.7	2.9					
6	1.3	5.0					
7	1.3	4.9					
8	2.4	16.4					
9	1.5	4.3					
10	2.3	14.3					
11	1.5	8.3					
12	1.4	8.2					
13	0.4	2.8					
14	1.5	13.9					
15	3.0	14.9					
16	0.5	1.4					
17	6.9	37.3					
21	1.3	11.8					
22	0.5	1.3					
23	0.3	0.8					
24	0.04	0.6					
OS1	3.1	6.8					
OS2	0.5	1.6					
OS3	3.2	6.9					
OS4	1.9	4.4					
OS5	1.7	6.7					
UD1	0.4	4.6					
UD2	0.6	6.0					
UD3	0.2	2.3					
UD4	2.2	36.5					
UD5	2.0	20.3					
1.0	3.1	9.7					
1.1	5.6	26.2					
1.2	6.8	32.2					
1.3	6.8	32.2					
1.4	7.6	35.0					
1.4	3.2	19.6					
	10.5	50.0					
1.6 1.7							
	11.1	58.1					
2.0	2.7	15.4					
2.1	3.4	9.5					
2.2	4.3	11.3					
2.3	4.8	30.1					
2.4	7.6	38.6					
2.5	12.2	75.8					
3.0	1.6	12.6					
3.1	1.5	12.6					

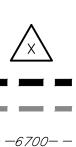
#### FILING 3 - SUB-BASIN SUMMARY TABLE

Tributary	Area	Percent			t _c	Q₅	<b>Q</b> ₁₀₀
Sub-basin	(acres)	Impervious	<b>C</b> ₅	<b>C</b> ₁₀₀	(min)	(cfs)	(cfs)
C1	6.04	13%	0.06	0.21	35.8	0.9	4.8
C2	3.35	24%	0.14	0.29	31.5	1.1	4.0
C3	23.44	9%	0.04	0.18	41.2	1.8	14.1
C4	10.94	18%	0.14	0.42	40.3	3.2	15.5
C5	2.35	20%	0.11	0.26	23.8	0.7	2.9
C6	3.95	22%	0.12	0.28	26.6	1.3	5.0
C7	2.14	24%	0.17	0.38	13.9	1.3	4.9
C8	22.55	10%	0.05	0.19	33.7	2.4	16.4
C9	2.63	35%	0.23	0.39	29.6	1.5	4.3
C10	16.38	12%	0.05	0.20	27.6	2.3	14.3
D1	9.11	13%	0.06	0.21	27.8	1.5	8.3
D2	8.49	13%	0.07	0.25	34.7	1.4	8.2
D3	3.21	8%	0.04	0.18	21.1	0.4	2.8
D4	10.01	7%	0.07	0.40	39.8	1.5	13.9
D5	9.56	17%	0.14	0.43	37.6	3.0	14.9
D6	0.34	45%	0.36	0.57	8.3	0.5	1.4
D7	33.94	15%	0.10	0.31	38.3	6.9	37.3
E1	17.12	7%	0.04	0.22	46.6	1.3	11.8
E2	0.37	45%	0.31	0.46	7.8	0.5	1.3
E3	0.20	45%	0.32	0.48	5.2	0.3	0.8
E4	0.68	3%	0.01	0.14	14.6	0.04	0.6
UD1	7.48	6%	0.03	0.16	33.5	0.4	4.6
UD2	9.17	6%	0.03	0.16	30.4	0.6	6.0
UD3	2.23	<mark>6%</mark>	0.04	0.24	27.0	0.2	2.3
UD4	34.90	2%	0.04	0.39	54.3	2.2	36.5
UD5	20.49	6%	0.05	0.30	41.9	2.0	20.3
OS1	2.37	58%	0.43	0.56	20.3	3.1	6.8
OS2	0.70	31%	0.20	0.35	13.1	0.5	1.6
OS3	2.28	60%	0.45	0.58	19.5	3.2	6.9
OS4	1.08	55%	0.44	0.63	11.8	1.9	4.4
OS5	2.92	23%	0.17	0.42	17.8	1.7	6.7
F1	1.35	40%	0.27	0.43	12.7	1.4	<b>3.6</b>
F2	7.67	11%	0.05	0.20	35.0	0.9	5.7
F3	2.37	45%	0.32	0.49	29.8	1.9	<mark>4.</mark> 9
F4	2.93	45%	0.34	0.52	32.3	2.3	<u>6.0</u>

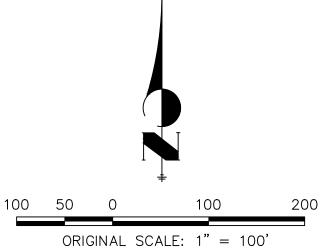
	NG 3 - DE: NT SUMM		$\left(\begin{array}{c} I.D. \\ A & B \end{array}\right)$
	Q₅	Q ₁₀₀	
	(cfs)	(Cfs)	
	0.9	4.8	
	1.1	4.0	$\wedge$
	1.8	14.1	
	3.2	15.5	
_	0.7	2.9	
	1.3	5.0	
	1.3	4.9	
	2.4	16.4	0700
	1.5	4.3	
	2.3	14.3	
	1.5	8.3	
	1.4	8.2	
	0.4	2.8	
	1.5	13.9	
	3.0	14.9	
	0.5	1.4	
	6.9	37.3	HP
	1.3	11.8	
	0.5	1.3	LP
	0.3	0.8	
	0.04	0.6	
	3.1	6.8	
	0.5	1.6	
	3.2	6.9	
	1.9	4.4	
	1.7	6.7	
	0.4	4.6	
	0.6	6.0	
	0.2	2.3	
	2.2	36.5	
	2.0	20.3	100 50
_	3.1 5.6	9.7	
	6.8	26.2 32.2	OR
	6.8	32.2	
	7.6	35.0	SADDLEH
	3.2	19.6	PROPOSE
	10.5	50.0	JOB NO.
	11.1	58.1	
	2.7	15.4	1/7/22
	3.4	9.5	SHEET 2
	4.3	11.3	
	4.8	30.1	
	7.6	38.6	
-			

## LEGEND

BASIN DESIGNATION I.D.: BASIN IDENTIFIER A: BASIN AREA B: C₅ C: C₁₀₀



DESIGN POINT MAJOR BASIN DELINEATION SUB-BASIN DELINEATION EXISTING INDEX CONTOURS EXISTING INTERMEDIATE CONTOURS PROPOSED INDEX CONTOURS PROPOSED INTERMEDIATE CONTOURS EXISTING FLOW DIRECTION PROPOSED FLOW DIRECTION PROPOSED HIGH POINT PROPOSED LOW POINT

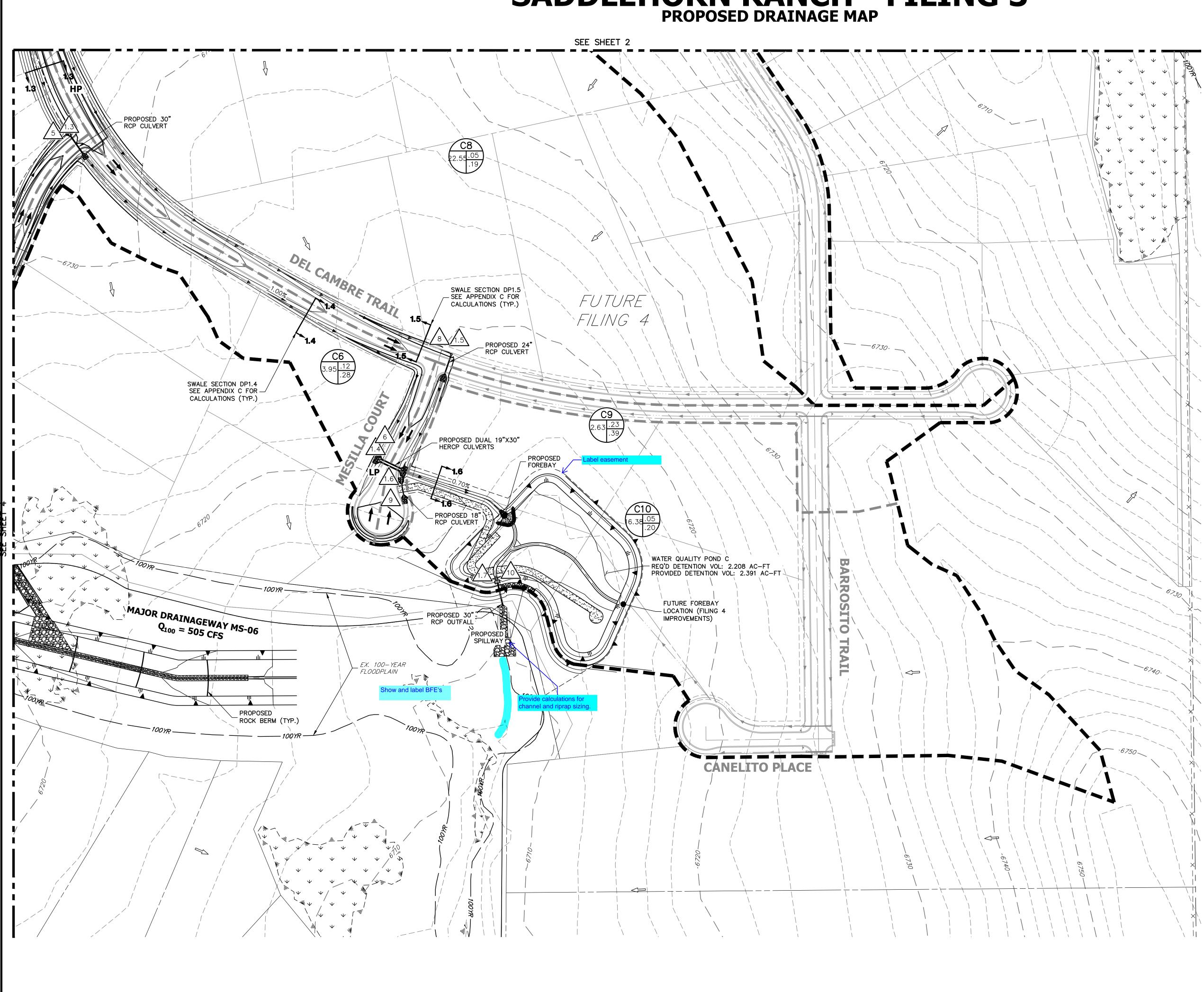


SADDLEHORN RANCH-FILING 3 PROPOSED DRAINAGE MAP JOB NO. 25142.05 1/7/22 SHEET 2 OF 4



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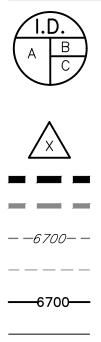
## SADDLEHORN RANCH - FILING 3 PROPOSED DRAINAGE MAP

	FILING 3 - SUB-BASIN SUMMARY TABLE							
Tributary	Area	Percent			t _c	Q₅	<b>Q</b> ₁₀₀	
Sub-basin	(acres)	Impervious	<b>C</b> ₅	<b>C</b> ₁₀₀	(min)	(cfs)	(cfs)	
C1	6.04	13%	0.06	0.21	35.8	0.9	4.8	
C2	3.35	24%	0.14	0.29	31.5	1.1	4.0	
C3	23.44	9%	0.04	0.18	41.2	1.8	14.1	
C4	10.94	18%	0.14	0.42	40.3	3.2	15.5	
C5	2.35	20%	0.11	0.26	23.8	0.7	2.9	
C6	3.95	22%	0.12	0.28	<mark>26.6</mark>	1.3	5.0	
C7	2.14	24%	0.17	0.38	13.9	1.3	4.9	
C8	22.55	10%	0.05	0.19	33.7	2.4	16.4	
C9	2.63	35%	0.23	0.39	29.6	1.5	<mark>4.</mark> 3	
C10	16.38	12%	0.05	0.20	27.6	2.3	14.3	
D1	9.11	13%	0.06	0.21	27.8	1.5	8.3	
D2	8.49	13%	0.07	0.25	34.7	1.4	8.2	
D3	3.21	8%	0.04	0.18	21.1	0.4	2.8	
D4	10.01	7%	0.07	0.40	39.8	1.5	13.9	
D5	9.56	17%	0.14	0.43	<mark>37.6</mark>	3.0	14.9	
D6	0.34	45%	0.36	0.57	<mark>8.3</mark>	0.5	1.4	
D7	33.94	15%	0.10	0.31	38.3	6.9	37.3	
E1	17.12	7%	0.04	0.22	46.6	1.3	11.8	
E2	0.37	45%	0.31	0.46	7.8	0.5	1.3	
E3	0.20	45%	0.32	0.48	5.2	0.3	0.8	
E4	0.68	3%	0.01	0.14	14.6	0.04	0.6	
UD1	7.48	6%	0.03	0.16	33.5	0.4	4.6	
UD2	9.17	6%	0.03	0.16	30.4	0.6	6.0	
UD3	2.23	6%	0.04	0.24	27.0	0.2	2.3	
UD4	34.90	2%	0.04	0.39	54.3	2.2	36.5	
UD5	20.49	<mark>6%</mark>	0.05	0.30	41.9	2.0	20.3	
OS1	2.37	58%	0.43	0.56	20.3	3.1	6.8	
OS2	0.70	31%	0.20	0.35	13.1	0.5	1.6	
OS3	2.28	60%	0.45	0.58	19.5	3.2	6.9	
OS4	1.08	55%	0.44	0.63	11.8	1.9	4.4	
OS5	2.92	23%	0.17	0.42	17.8	1.7	6.7	
F1	1.35	40%	0.27	0.43	12.7	1.4	3.6	
F2	7.67	11%	0.05	0.20	35.0	0.9	5.7	
F3	2.37	45%	0.32	0.49	29.8	1.9	4.9	
F4	2.93	45%	0.34	0.52	32.3	2.3	6.0	

### FILING 3 - DESIGN

POIN	<b>NT SUMN</b>	<b>IARY</b>
Design	Q₅	<b>Q</b> ₁₀₀
Point	(cfs)	(Cfs)
1	0.9	4.8
2	1.1	4.0
3	1.8	14.1
4	3.2	15.5
5	0.7	2.9
6	1.3	5.0
7	1.3	4.9
8	2.4	16.4
9	1.5	4.3
10	2.3	14.3
11	1.5	8.3
12	1.4	8.2
12	0.4	2.8
19	1.5	13.9
15	3.0	14.9
15	0.5	14.5
10	6.9	37.3
21	1.3	11.8
22	0.5	1.3
22	0.3	0.8
23	0.04	0.8
0S1	3.1	6.8
OS1 OS2	0.5	1.6
OS2 OS3	3.2	6.9
O33 OS4		4.4
034 0S5	1.9 1.7	6.7
UD1		4.6
	0.4	
UD2	0.6	6.0
UD3	0.2	2.3
UD4	2.2	36.5
UD5 1.0	2.0	20.3
	3.1	9.7
1.1	5.6	26.2
1.2	6.8	32.2
1.3	6.8	32.2
1.4	7.6	35.0
1.5	3.2	19.6
1.6	10.5	50.0
1.7	11.1	58.1
2.0	2.7	15.4
2.1	3.4	9.5
2.2	4.3	11.3
2.3	4.8	30.1
2.4	7.6	38.6
2.5	12.2	75.8
3.0	1.6	12.6
3.1	1.5	12.6

## LEGEND



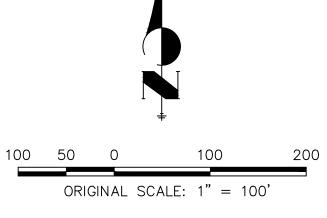
HP

LP

B: C₅ C: C₁₀₀ DESIGN POINT MAJOR BASIN DELINEATION SUB-BASIN DELINEATION EXISTING INDEX CONTOURS EXISTING INTERMEDIATE CONTOURS PROPOSED INDEX CONTOURS PROPOSED INTERMEDIATE CONTOURS EXISTING FLOW DIRECTION PROPOSED FLOW DIRECTION PROPOSED HIGH POINT PROPOSED LOW POINT

BASIN DESIGNATION

I.D.: BASIN IDENTIFIER A: BASIN AREA

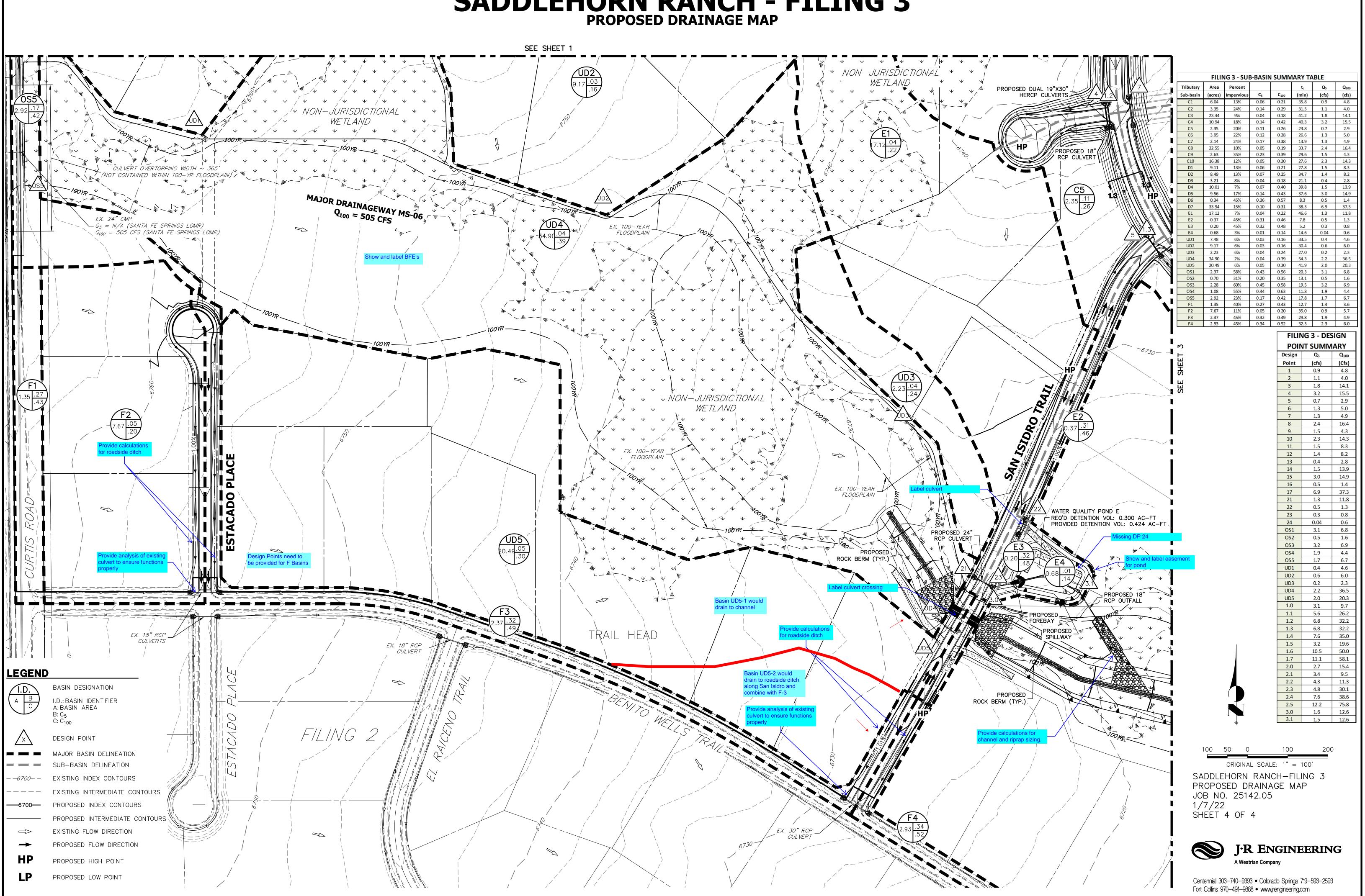


SADDLEHORN RANCH-FILING 3 PROPOSED DRAINAGE MAP JOB NO. 25142.05 1/7/22 SHEET 3 OF 4



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## SADDLEHORN RANCH - FILING 3 PROPOSED DRAINAGE MAP

