

MASTER DEVELOPMENT DRAINAGE PLAN

For

CORVALLIS PUD

Prepared for:
City of Fountain
116 S. Main Street
Fountain, CO 80817

On Behalf of:
HPR Properties, LLC
555 Middle Creek Parkway, Suite 380
Colorado Springs, CO 80921

Prepared by:



Matrix

2435 Research Parkway, Suite 300
Colorado Springs, CO 80920
(719) 575-0100
fax (719) 572-0208

January 2021

Project No. 20.1105.002

ENGINEER'S STATEMENT:

This report and plan for the drainage design of Corvallis PUD was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Fountain does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, error or omissions on my part in preparing this report.

Signature: _____

Date : _____

Nicole M. Schanel
Colorado Professional Engineer No. 52434

DEVELOPER'S STATEMENT:

HPHR Properties, LLC hereby certifies that the drainage facilities for Corvallis PUD shall be constructed according to the design presented in this report. I understand that the City of Fountain does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Fountain pursuant to the City Code; and cannot, on behalf of HPHR Properties, LLC, guarantee that final drainage design review will absolve HPHR Properties, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

Name of Developer: HPHR Properties, LLC

Authorized Signature: _____ **Date:** _____

Printed Name: Ed Houle

Title: *Director of Land Acquisition and Development*

Address: 14160 Gleneagle Drive
Colorado Springs, CO 80921

CITY OF FOUNTAIN STATEMENT:

Filed in accordance with the Code of the City of Fountain, 2009, as amended.

For the City Engineer

Date

Conditions:

TABLE OF CONTENTS

I.	INTRODUCTION.....	4
II.	PROJECT CHARACTERISTICS	6
III.	HYDROLOGIC ANALYSIS.....	8
IV.	HYDRAULIC ANALYSIS	21
V.	ENVIRONMENTAL EVALUATIONS.....	22
VI.	SELECTED PLAN.....	28
VII.	FEE DEVELOPMENT.....	29
VIII.	REFERENCES	31

APPENDIX

A. Hydrologic and Hydraulic Calculations

1. Existing and Proposed Rational Calculations
2. Storm Infrastructure Sizing
3. Storm System Capacity modeling
4. UDFCD Detention Basin Design Workbook

B. Standard Design Charts and Tables

1. 2019 Drainage Fee Schedule
2. Shallow Flow Velocities Figure 6-25
3. DCM Street Capacity Chart Figure 7-7
4. DCM Runoff Coefficients Table 6-6

C. Report References

1. Soils Map
2. FEMA FIRM Floodplain Maps
3. Report Maps

D. Maps

1. Existing Conditions Drainage Basin Map
2. Proposed Conditions Drainage Basin Map
3. National Wetlands Inventory Map
4. WFJCC DBPS Land Use Map

I. Introduction

A. PURPOSE AND SCOPE OF STUDY

The purpose of this report is intended to fulfill the City of Fountain requirements for a Master Development Drainage Plan (MDDP), submitted with the Overall Development Plan (ODP) for the proposed Corvallis project. The report will provide a summary of the site drainage issues impacting the proposed development, including identification and evaluation of the offsite and onsite drainage patterns associated with the project, analysis of upstream impacts from upstream drainage, and impacts to downstream facilities. This MDDP has been prepared based on the guidelines and criteria presented in the City of Colorado Springs Drainage Criteria Manual (DCM).

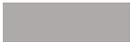
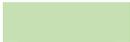
B. AGENCY JURISDICTIONS

This project is located within the City of Fountain and is subject to the design criteria set forth in the *City of Colorado Springs Drainage Criteria Manual, Volumes I and II, dated May 2014 (DCM)*.

C. GENERAL PROJECT DESCRIPTION

Corvallis is a 275-acre mixed-use parcel located at the southwest intersection of Marksheffel Road and Fontaine Boulevard. The Corvallis ODP prepared by Matrix Design Group, Inc dated September 5, 2020 (currently in review) includes single-family and multi-family residential units, commercial development, a school site, and dedicated open space. Figure 1 below displays in further detail the Land Use Summary.

Figure 1. Land Use Summary of proposed Corvallis site.

	Commercial (office/retail)	34.9 Acres
	Residential (single-family)	139.8 Acres
	Residential (multi-family)	17.3 Acres
	School Site	12 Acres
	Collector Roadways	25.4 Acres
	Open Space	45.6 Acres

More specifically, the site is located as follows:

1. General Location: Part of the Northeast $\frac{1}{4}$ of Section 21, and the Northwest $\frac{1}{4}$ and a Portion of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$ of Section 22, all in Township 15 South, Range 65 West of the 6th P.M. in the City of Fountain, County of El Paso, State of Colorado.

2. **Surrounding Streets:** Fontaine Boulevard directly borders the parcel to the north, and a portion of the eastern boundary is bordered directly by Marksheffel Road. Powers Boulevard (State Highway 21) is located approximately ½ mile to the west.
3. **Drainageway:** The proposed site lies entirely within the West Fork Jimmy Camp Creek Drainage Basin and is currently undeveloped land, mostly covered by natural vegetation. The Fountain Mutual Irrigation Company (FMIC) irrigation ditch also enters and exits the site multiple times.
4. **Surrounding Developments:** The site is bound by vacant land to the north, the Peaceful Valley Estates development to the West, The Glen at Widefield Subdivisions to the south, and Lorson Ranch to the east.

Refer to Appendix D for the Vicinity Map.

D. DATA SOURCES

Topographical information for the site was found using a combination of ***United States Geological Survey*** (USGS) mapping, GIS LIDAR, as well as field surveying. The ***Web Soil Survey***, created by the ***Natural Resources Conservation Service***, was utilized to investigate the existing general soil types within the site.

E. APPLICABLE CRITERIA AND STANDARDS

As required by the City of Fountain, Colorado, this report has been prepared in accordance to the criteria set forth in the ***City of Colorado Springs Drainage Criteria Manual Volume 1*** (Drainage Criteria Manual), dated May 2014 and ***Volume 2 Stormwater Quality Policies, Procedures, and BMP's***, dated May 2014.

In addition to the City Criteria Manual, the ***Urban Storm Drainage Criteria Manuals, Volumes 1-3*** (UDFCD), published by the Urban Drainage and Flood Control District, latest update, have been used to supplement the Drainage Criteria Manual for water quality capture volume (WQCV).

F. REFERENCED DRAINAGE REPORTS

West Fork Jimmy Camp Creek Drainage Basin Planning Study (WFJCC DBPS), by Kiowa Engineering Corp. October 2003.

Master Drainage Development Plan (MDDP) The Glen at Widefield, by Kiowa Engineering Corp. December 1999.

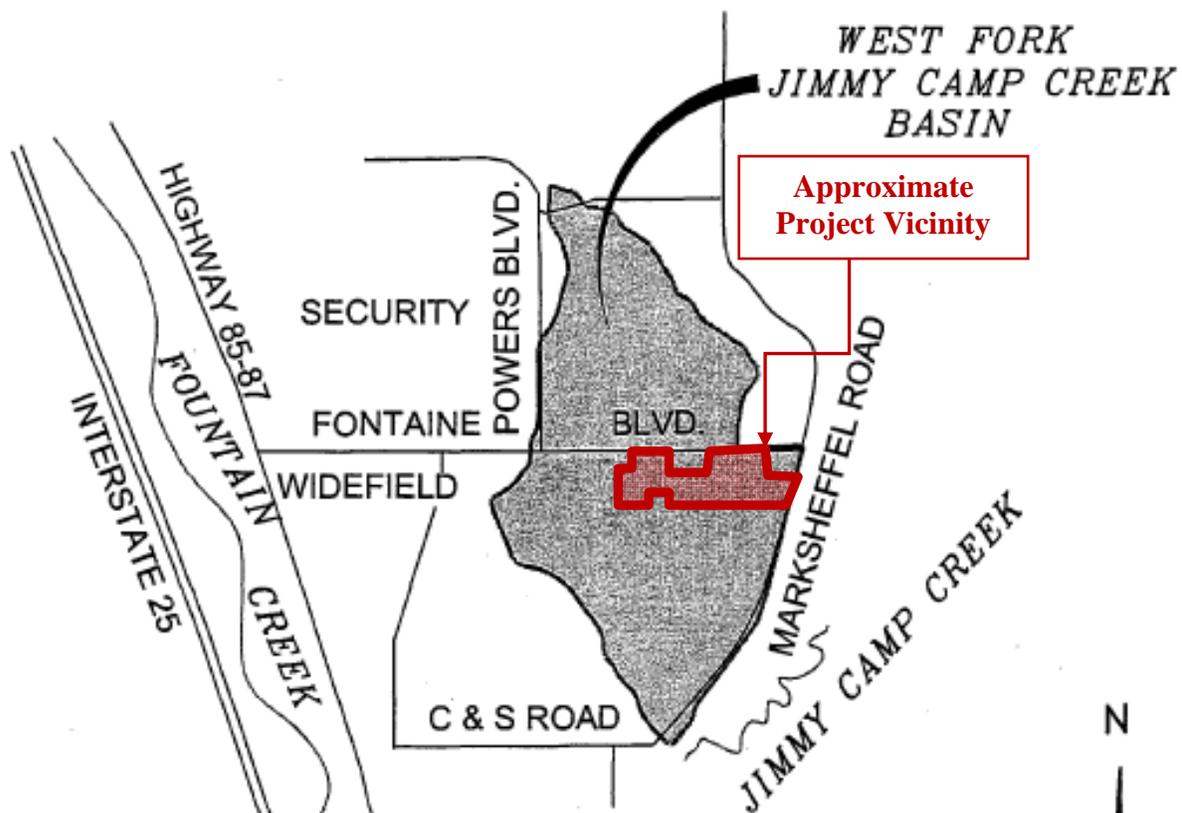
Final Drainage Report (FDR F9) The Glen at Widefield Filing No. 9, by Kiowa Engineering Corp. July 2018.

Final Drainage Report (FDR F11) The Glen at Widefield Filing No. 11, by Kiowa Engineering Corp. December 2019.

II. Project Characteristics

A. MAJOR BASIN

Corvallis lies entirely within the West Fork Jimmy Camp Creek (WFJCC) Drainage Basin. The project includes offsite and onsite drainage area with the major confluence of offsite drainage happening at an existing bridge crossing that conveys the WFJCC flows southerly across Fontaine Boulevard. These flows continue south through the Corvallis site until they enter the Glen at Widefield Subdivision Filing No. 9. Two more natural channels run through the site, draining north to south, and join with the WFJCC after they have left the Corvallis development. The West Fork of Jimmy Camp Creek covers a total of 4 square miles. The developed area for the site of 275-acres is approximately 10.7% of the total drainage area within the WFJCC.



B. COMPLIANCE WITH DBPS

This study complies with the latest DBPS study (*WFJCC DBPS*) of the West Fork Jimmy Camp Creek basin dated October 2003. All developed runoff from the site will be detained and released at pre-development peak rates, and the water quality volume will be treated. Both as determined by the UDFCD detention spreadsheet UD-Detention.

C. GEOLOGY

The majority of the site is currently undeveloped and consists of natural vegetative land cover, as well as multiple natural creeks.

Soils can be classified in four different hydrologic groups, A, B, C, or D to help predict storm water runoff rates. Hydrologic group “A” is characterized by deep, well-drained coarse-grained soils with a rapid infiltration rate when thoroughly wet and having a low runoff potential. Group “D” typically has a clay layer at or near to the surface, or a very shallow depth to impervious bedrock and has a very slow infiltration rate and a high runoff potential. See Soils Map; Appendix D. Table 1.1 on the following page indicates which soil types are present in the development area:

Table 1.1 – NRCS Soil Survey for El Paso County

Soil ID Number	Soil	Hydrologic Classification	Permeability	Percent on Site
30	Fort Collins Loam (0% - 3% slopes)	B	Moderately Rapid	3.9%
52	Manzanst Clay Loam (0% - 3% slopes)	C	Low Rapidity	1.8%
56	Nelson-Tassel Fine Sandy Loams (3% - 18% slopes)	B	Moderately Rapid	34.5%
59	Nunn Clay Loam (0% - 3% slopes)	C	Low Rapidity	16.2%
75	Razor-Midway Complex	D	Very Low Rapidity	0.9%
86	Stoneham Sandy Loam (3% - 8% slopes)	B	Moderately Rapid	35.6%
101	Ustic Torrfluvents, Loamy	B	Moderately Rapid	0.8%
108	Wiley Silt Loam (3% - 9% slopes)	B	Moderately Rapid	6.3%

D. GROUNDWATER

According to the GeoTech report for the site, groundwater levels vary. There is some seasonal and temporary raising of the water table along the FMIC and natural ditches. This fluctuation is likely due to irrigation water releases during the growing season; therefore, it is anticipated that the rerouting of the FMIC ditch via storm sewer, described in Section F below, will mitigate some of the water table fluctuations. Groundwater will be mitigated for in the construction plans as recommended in the Geotech report.

E. LAND USES

Presently, the site is unplatted and consists of undeveloped land. Corvallis is a proposed planned unit development (PUD) which includes both residential and commercial uses. Development of utilities and internal roadways are to be included in this parcel.

F. UTILITIES AND ENCUMBERANCES

- **Storm Sewer:** Existing storm sewer includes a 30-inch CMP culvert that crosses Fontaine Boulevard. In addition, WFJCC and associated proposed storm infrastructure will run through the site. Sizing is as described within this report and subject to change as site design progresses.

- **Sanitary Sewer:** An existing 24-inch sanitary sewer main lies within the intersection of Marksheffel Road and Lorson Boulevard near the site's southeast corner which will take flow east of the ridge internal to Corvallis Development. There is also an existing 12-inch sanitary sewer main which runs north-south through the site that will tie into the sanitary system at The Glen at Widefield development to the south of the site, and will take the site's internal sanitary flow west of the ridge.
- **Gas:** Gas service to the proposed development will be provided by Black Hills Energy through the extension of the existing gas main infrastructure that currently lies adjacent to the site. No encumbrance to the project is anticipated.
- **Water:** The following existing water mains surround the site: a 16-inch water main in Marksheffel Road, a 24-inch water main in Spring Glen, a 12-inch water stub at Dutch Loop, and an 8-inch water main at Fontaine Boulevard near Cottonwood Grove. A network of new 12-inch and 8-inch water mains will be constructed throughout the Corvallis site to provide looping and water services to the development.
- **Electric:** There is existing overhead electric power in Fontaine Boulevard along the north side of the property and along the site's western property line. Underground electric power is also located within the residential developments to the south and east of the site. Electric service will be provided to the Corvallis Development by extending underground electric throughout the subdivision for residential and commercial services. No encumbrance to the project is anticipated.
- **Communications:** Underground communication lines currently serve the residential neighborhoods adjacent to the project site which will be extended underground to serve Corvallis Development. No encumbrance to the project is anticipated.
- **Irrigation:** There is an existing FMIC irrigation ditch meandering through both the east and west portions of the site. Both sections of the FMIC ditch running through the Corvallis site will be rerouted via 60-inch storm pipes sized to convey the 60 cfs that FMIC has indicated as a peak irrigation flow. Due to the lack of grade in the existing ditch, both sections of pipe are very flat with the west section at 0.06% and the east section at 0.08% grade. Entry and exit locations to and from the site will remain unchanged.

Written acceptance of planned modifications to FMIC ditch must be acquired from FMIC prior to beginning construction of these improvements. Pursuit of this acceptance is in progress. Documentation will be added to the MDDP when it is available.

III. Hydrologic Analysis

A. GENERAL CONCEPT

The general concept for management of storm water for the proposed Corvallis development will be to provide clear conveyance through the property to the multiple onsite detention facilities to mitigate developed runoff flows from the site. Development of the site will require over-lot grading, roadway paving, residential and commercial construction which will increase the imperviousness of the property from existing conditions. The general drainage patterns will consist of positive drainage away from building sites, across lawns, parking lots, or open space, to curb and gutter within the internal roadways. Storm water within the roadways will be directed to inlet collection points, where it is captured and conveyed through a pipe network system to a full spectrum detention pond. Majority of offsite runoff will be either be diverted around the site or

collected and directed separately through the site before being discharged at historic drainage locations and discharge.

The Water Quality Capture Volume (WQCV) is comprised within the proposed Full Spectrum Extended Detention Basin (EDB), where the “initial flush” of storm water will be drained over a 40-hour time period. The onsite ponds have been evaluated to reduce the developed flows from the site to a maximum of the historic peak flows. The detention pond has been sized and evaluated based upon the 100-year storm events in accordance with City Criteria.

B. METHODOLOGY

a. Rational Method

i. Method of Analysis

Storm sewer sizing for this project uses the Rational Method as recommended by the Drainage Criteria Manual for the minor and major storms for drainage basins less than 100-acres in size (Inlets will also be sized using this method in the subsequent FDRs). The Rational Method uses the following equation:

$$Q=C*i*A$$

Where:

- Q = Maximum runoff rate in cubic feet per second (cfs)
- C = Runoff coefficient
- i = Average rainfall intensity (inches per hour)
- A = Area of drainage sub-basin (acres)

ii. Runoff Coefficient

Coefficients from Table 6-6 of the Drainage Criteria Manual for developed land were utilized in the Rational Method calculations. See Appendix B for more information.

iii. Time of Concentration

The time of concentration consists of the initial time of overland flow and the travel time in a channel to the inlet or point of interest. A minimum time of concentrations of 5 minutes is utilized for urban areas.

iv. Rainfall Intensity

The hypothetical rainfall depths for the 1-hour storm duration were taken from Table 6-2 of the Colorado Springs Drainage Criteria Manual. Table 3.1, below, lists the rainfall depth for the Major and Minor 1-hour storm events.

Table 3.1 – Project Area 1-Hour Rainfall Depth

Storm Recurrence Interval	Rainfall Depth (inches)
5-year	1.50
100-year	2.52

The rainfall intensity equation for the Rational Method was taken from Drainage Criteria Manual Volume 1 Figure 6-5.

C. BASIN HYDROLOGY

Existing Drainage Conditions

Under the existing conditions, the site flows in a general north to south pattern until reaching one of three low points. As such, the site has been divided into major basin delineations (west, central, east) which collect flow at these three discharge points, in conformance with the **WFJCC DBPS, MDDP, and FDRs** for the area.

West Basin:

Sub-basin OS-1 borders the site to the west and is comprised of large lot, single-family residential homes. Runoff from this site drains to the east until reaching the Corvallis boundary, represented at Design Point E1.

Sub-basin OS-2 borders the site to the northwest and consists of drainage on Fontaine Boulevard from the crown of the roadway to the south. These flows drain from the existing roadway high point to the east until reaching the existing low point at Design Point E2. In the existing conditions, this road corridor drainage connects with a 30-inch CMP that directs localized flows from the north underneath Fontaine Boulevard and discharging into the WFJCC.

Sub-basin EX-2 is an onsite, undeveloped basin that sheet flows in a general southwest to northeast pattern until it combines with Sub-basin OS-2 at Design Point E2. Runoff from this design point discharges directly into the WFJCC.

Sub-basin OS-3 is an offsite, undeveloped basin that drains to the southeast until reaching the WFJCC floodway at Design Point E3.

Sub-basin OS-4 is an offsite, undeveloped basin adjacent to the WFJCC which drains to the southeast until reaching Design Point E3.

In addition to the above listed sub-basin flows that reach Design Point E3, the approved **WFJCC DBPS** also specifies a Design Point 3020 which consists of the upstream flows, including the existing 30" CMP mentioned previously) collected in the WFJCC as it enters the Corvallis site. In a conservative effort, the approved existing **WFJCC DBPS** flows have been added to the previously described sub-basins to achieve the flows at Design Point E3.

Sub-basin EX-1 is comprised of the west quarter of the Corvallis site. Currently undeveloped, flows generated in this basin combine with offsite flows from Sub-basin OS-1 and drain in a general northwest to south east pattern until reaching the WFJCC at Design Point E4.

Sub-basin OS-8 is an offsite, agriculturally zoned parcel that sheet flows from west to east until reaching the WFJCC at Design Point E4.

Sub-basin OS-5 contains the southern half of Fontaine Boulevard as it drains from an existing roadway high point to the west until discharging and combining with onsite drainage.

Sub-basin EX-3 accepts the flows from Sub-basin OS-5 and continues to drain from the northeast to south west until reaching Design Point E5 at the site's southern border.

Flows from Design Points E4 and E5 combine at the West Basin’s final discharge point, Design Point E8. This is located at the flowline of the WFJCC drainageway as it leaves the Corvallis development and continues into the Glen at Widefield development located to the south. In both the approved **WFJCC DBPS** and **MDDP**, the flowrates at this point are $Q_5 = 601$ cfs and $Q_{100} = 2216$ cfs. As previously mentioned, rational calculations were performed for all onsite basins and added to the **WFJCC DBPS** Design Point 3020 existing condition flows ($Q_5 = 528$ cfs and $Q_{100} = 1857$ cfs) located at the WFJCC entrance into the site. This results in Design Point 8 flows of $Q_5 = 590.5$ cfs and $Q_{100} = 2178.5$ cfs. The previously approved **WFJCC DBPS** and **MDDP** will govern on the discharge flows at this point.

A summary of the existing basins and design points contributing to the West Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions Map.

West Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-1a	38.5	19.2	70.9
OS-1b	38.3	12.3	47.7
OS-2	1.0	3.9	7.1
OS-3	1.9	0.6	4.0
OS-4	18.3	3.3	21.8
OS-5	0.8	3.2	5.8
OS-8	22.1	4.2	28.1
EX-1	67.9	9.0	60.3
EX-2	10.3	2.5	17.0
EX-3	51.9	8.2	54.8

West Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E1: OS-1	19.2	70.9
E2: OS-2, EX-2	5.4	22.5
E3: E2, OS-3, OS-4	6.5	34.4
E4: E1, E3, EX-1, OS-8	52.4	264.0
E5: OS-5, EX-3	10.2	57.5
E8: E4, E5, +DPBS3020	590.5	2178.5

Central Basin

Sub-basin EX-4 is an onsite, undeveloped portion of land that drains from the northeast to the southwest until reaching Design Point E6, the final discharge point of the Central Basin.

This discharge point is centrally located on the southern border of the Corvallis development. An existing area inlet and corresponding 48-inch RCP collects the flows ($Q_5 = 7.2$ cfs and $Q_{100} = 48.1$ cfs) and conveys them directly to the WFJCC. Per the approved FDR for the Glen at Widefield Filing No. 9, this point collects 44.8 cfs in the 5-year storm and 163 cfs in the 100-year storm. As with Design Point E8, the allowable release of flows for this point are set by the approved **WFJCC DPBS** and **MDDP**.

A summary of the existing basins and design points contributing to the Central Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions Map.

Central Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
EX-4	58.6	7.2	48.1

Central Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E6: EX-4	7.2	48.1

East Basin

Sub-basin OS-6 contains the southern portion of Fontaine Boulevard, to the crown of the roadway, that borders the site to the northeast. These flows are collected in a roadside swale and discharge onsite.

Sub-basin OS-7 consists of a single-family residential development located on the east side of the site. The back half of the existing residential lots drain to the south and west until discharging onto the Corvallis site.

Sub-basin EX-5 is the easternmost onsite basin. Currently undeveloped, this basin collects the flows from Sub-basins OS-6 and OS-7 and slopes from the northwest to the southeast until reaching Design Point E7.

The final discharge point for the East Basin (Design Point E7, $Q_5 = 16.5$ cfs and $Q_{100} = 93.1$ cfs) is located at the southeast corner of the site. These flows will be conveyed to the south in the existing roadside swale that runs parallel to Marksheffel Road. Discharge at this design point was set in the **WFJCC DBPS** and **MDDP** as $Q_5 = 38$ cfs and $Q_{100} = 153$ cfs and will control the allowable discharge in developed conditions.

A summary of all existing basins and design points, offsite and onsite, as well as a summary of design points contributing to the East Basin are shown below. Calculations can be found in Appendix A. Please refer to Appendix D for the Existing Conditions drainage maps.

East Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-6	0.8	3.2	5.8
OS-7	2.9	2.5	9.4
EX-5	86.5	12.8	86.3

East Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E7: EX-5, OS-6, OS-7	16.5	93.1

As previously mentioned, the Fountain Mutual Irrigation Company (FMIC) ditch system enters and exits the site periodically. The ditch in this area is approximated to have flows of 60 cfs as it meanders through the Corvallis site. This MDDP follows the guidelines previously set in the **WFJCC DPBS** that states, “Existing and proposed runoff was assumed to be passed over or under the ditch in the hydrologic modeling of the basin. There was no diversion of runoff by the ditch assumed in compilation of the hydrologic model for this basin.” As such, no additional drainage from the site is anticipated to be conveyed by the FMIC and all flows released into the ditch are assumed to remain within the canal. There is a possibility of a bypass pipeline being constructed that will convey flows from Big Johnson Reservoir to the east side of Marksheffel Road, near Jimmy Camp Creek, however this has not been considered for this report.

Developed Drainage Conditions

As explained in the existing conditions, the developed site drainage will also discharge at three site low points and has been broken down into three drainage basins for clarity. These design points have been specified in the **WFJCC DBPS** and subsequent reports as the discharge points from the Corvallis development. Runoff from the developed site will conform to these specified flows.

Developed hydrology calculations for the basins and design points can be found in Appendix A. Preliminary hydraulic calculations have been completed for the anticipated trunk mains. Storm infrastructure internal to the sub-basins will be completed with each filing's Final Drainage Report.

West Basin:

Sub-basin OS-1 previously explained in the existing conditions will continue to drain easterly until reaching the Corvallis site boundary. At this point, the offsite flows will either be conveyed via swale or pipe to the north and east until reaching Design Point E1. Preliminary calculations have been completed for this swale (OS-1 Swale) or pipe (OS-1 Pipe) and can be found in Appendix A. Once entering the Corvallis site, these offsite flows will be conveyed via storm drain to the east and south until reaching DP1. This drainage will be kept separate from any untreated, developed runoff and will therefore not require any detention or water quality treatment.

Sub-basin 1B includes both commercial and multi-family development at the northwest corner of the site. The commercial and multi-family parcels will each have their own onsite water quality and detention facilities, DF-1 and DF-2, respectively. Discharge from these facilities will be released at prehistoric peak flow values as required per the City criteria. Treated flows leaving DF-1 will be conveyed to the south via an 18-inch storm drain until reaching DP1. Preliminary calculations for the ponds and storm drain have been calculated and can be found in Appendix A. Discharge from DF-2 will be conveyed to DP2 via a 24-inch storm drain.

Design Point DP1 combines Design Point E1 and Sub-basin 1B. At this point, treated flows combine with routed flows. In an effort to be conservative, the treated discharge has simply been added to the routed flow, resulting in 25.0 cfs and 107.0 cfs in the minor and major storms, respectively. These combined flows will be carried in a 36-inch storm drain to along Autumn Glen and Residential Collector A road corridors until reaching Design Point DP3.

Sub-basin 1A is comprised of 1/8 acre or less, single-family residential lots. Runoff generated from this basin will be conveyed via curb and gutter and storm drain to the north and east until reaching Design Point DP2.

Sub-basin 2 is planned for 1/8 acre (or less) single-family residential. Developed runoff will be directed to the south via curb, gutter, and proposed internal storm drains, crossing beneath Residential Collector A, until reaching Design Point DP2.

Sub-basin 3 will consist of undeveloped land and detention and water quality pond DF-3.

Detention facility DF-3 will collect developed runoff from Sub-basins 1A, 2, and 3 and will then release at historic rates via a 36-inch storm drain until reaching Design Point DP3.

Sub-basin OS-8 is unchanged from the existing conditions and will meet with the treated flows released from DF-3 at Design Point DP3, discharging directly into the WFJCC.

Sub-basin 8 is a proposed commercial development that will have its own onsite water quality and detention pond, DF-6. Once treated, the historic release will be directed to the west in an 18-inch storm drain, releasing onto Sub-basin 7.

Sub-basin 7 will remain undeveloped open space in the proposed conditions and, therefore, does not require any detention or water quality. This sub-basin will accept the treated flows from Sub-basin 8 and continue to drain to the south and west until reaching Sub-basin OS-4 and Design Point DP5.

Sub-basin OS-3 is unchanged from the existing conditions and will continue to drain to the south and east until reaching Design Point DP5.

Sub-basin OS-4 is unchanged from the existing conditions and will continue to drain to the south and west until reaching Design Point DP5.

As previously mentioned, flow at Design Point 5 (E3 in the existing conditions discussion) includes **WFJCC DBPS** Design Point 3020 existing flows. The approved **WFJCC DBPS** also recommends removal of the existing 30-inch CMP crossing Fontaine Boulevard and, instead, routing these flows to the east until reaching the WFJCC bridge crossing at the north side of Fontaine Boulevard. The DBPS includes calculations show that this crossing is adequately sized to handle the additional flows. As such, it has been assumed that the **WFJCC DBPS** Design Point 3020 flows include those from the 30-inch CMP and all converge north of Fontaine Boulevard. From here, Design Point DP5 flows continue south within the WFJCC floodway until reaching the West Basin discharge point at DP 7.

Sub-basin 5 will be a proposed single-family development with lot sizes equal or lesser than 1/8 of an acre. Developed runoff will be taken to the south and west by internal curb, gutter and storm drain. The collected stormwater will cross underneath Residential Collector A, until reaching Sub-basin 4.

Sub-basin 4 will be comprised of 1/8 acre, or less, single-family lots. This basin will accept flows from Sub-basin 6 and continue to direct them to the basin low point, located at the southwest corner, Design Point DP6. At this point, detention and water quality pond DF-4 will accept and treat the flows, then discharge into the WFJCC via a 24-inch storm drain.

The convergence of Design Points DP3, DP5, and DP6 results in the ultimate West Basin discharge point, DP7 ($Q_5 = 586.3$ cfs and $Q_{100} = 2127.7$ cfs). These flows are less than both the routed calculations completed for Design Point E8, as well as the previously approved and governing releases specified in the **WFJCC DBPS** and **MDDP**. Drainage from this point will continue to the south until reaching the Glen at Widefield developments.

A summary of the sub-basins and design points within the West Basin are summarized below:

West Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-1a	38.5	12.7	49.3
OS-1b	38.3	12.3	47.7
OS-2	1.0	3.9	7.1
OS-3	1.9	0.6	4.0
OS-4	18.3	3.3	21.9
OS-5	0.8	3.2	5.8
OS-8	22.1	4.2	28.1
1A	28.3	43.1	94.9
1B	13.9	45.7	88.2
2	28.6	43.0	94.8
3	7.5	2.7	13.6
4	17.2	25.7	53.6
6	10.0	15.5	34.1
7	19.3	2.6	17.8
8	5.1	22.5	40.8

West Basin		
Design Point	Peak Flows	
	5-Year	100-Year
E1	21.7	84.4
DP1	25.0	107.0
DP2	91.4	212.1
DP3	44.9	196.3
DP4	4.8	26.6
DP5	536.7	1909.4
DP6	22.4	47.3
DP7	586.3	2127.7

DP7 Summary							
Approved DBPS/MDDP		Glen at Widefield FDR 9		MDDP (Ex. Cond.)		MDDP (Pr. Cond.)	
5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
601.0	2216.0	601.0	2216.0	590.5	2178.5	586.3	2127.7

Central Basin:

Sub-basin OS-5 collects the runoff from required improvements to Fontaine Boulevard, adjacent to the Corvallis development which will have the required improvements at the time of development. Runoff from the roadway crown to the south will be collected in the proposed curb and gutter and directed to required inlets at the road low point. From here, flows will be conveyed to Sub-basin 9 via proposed storm drain.

Sub-basins 9 & 10 includes single-family development with lots equal to or less than 1/8 of an acre in size. Proposed curb, gutter, and storm drain will collect the developed runoff and direct it to the south, until reaching Residential Collector A. Flows will cross underneath this roadway and join with Sub-basin 10.

Sub-basin 11 is currently designated single-family residential. Runoff from this site will join with incoming Sub-basin 9 & 10 flows and continue to the south and west until crossing underneath the proposed Spring Glen Drive roadway, discharging into detention and water quality pond DF-5 at Design Point DP10. This basin is considered to be approximately 65 percent impervious per Table 6-3 of the USDCM.

Sub-basin 5 contains single-family residential units with maximum lot sizes of 1/8 acre. Developed runoff will be accumulated within the internal curb, gutter, and storm drain system until discharging into pond DF-5 at Design Point DP9.

Design Point DP11 is the ultimate discharge point for the Central Basin and consists of the historical release from proposed detention and water quality pond DF-5 ($Q_5 = 7.2$ cfs and $Q_{100} = 48.1$ cfs). This discharge point is comparative to Design Point E6 in the existing conditions. The prehistoric discharge is equal to the calculated routed flows in the existing conditions and well underneath the approved flows from the **WFJCC DBPS** and **MDDP**, as well as the anticipated flows per the Glen at Widefield Filing No. 9 FDR.

A summary of the sub-basins and design points within the Central Basin are summarized below:

Central Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
OS-5	0.8	3.2	5.8
5	5.9	19.5	38.6
9	20.2	38.5	84.7
10	17.7	31.0	68.2
11	13.1	20.7	45.5

Central Basin		
Design Point	Peak Flows	
	5-Year	100-Year
DP8	54.5	119.5
DP9	38.1	82.4
DP10	60.3	130.9
DP11	7.2	48.1

DP11 Summary							
Approved DBPS/MDDP		Glen at Widefield FDR 9		MDDP (Ex. Cond.)		MDDP (Pr. Cond.)	
5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
48.0	163.0	44.8	163.0	7.2	48.1	7.2	48.1

East Basin:

Sub-basin OS-6 consists of the southern half of Fontaine Boulevard, to include the proposed improvements that will be required adjacent to the Corvallis development. Inlets will need to be designed to capture this flow and route it south to Sub-basin 12 at time of Final Drainage Report for the adjacent filing.

Sub-basin 12 is a proposed multi-family development that will convey drainage via proposed curb, gutter, and storm drain to the south and east until reaching Design Point DP12 at detention facility DF-7. This parcel will have its own onsite water quality and detention to treat its runoff as well as the runoff from Sub-basin OS-6. Treated runoff will be released at historical peak discharge by a 30-inch storm drain. This storm drain will continue to the south and east, separated from any untreated flows, until reaching Design Point DP15.

Sub-basin OS-7 is a large acre, single-family subdivision located at the Corvallis site's northeastern corner. Stormwater from the backs of these lots will drain through side lot swales until discharging onto Sub-basin 16 and eventually being treated in detention and water quality pond DF-9.

Sub-basin 16 is a proposed commercial development. Developed runoff will drain to the southeast via internal curb, gutter, and storm drain until reaching the onsite water quality and detention facility, DF-9. This pond will release the treated flow via a 36-inch storm drain, combining with the above-mentioned East Basin flows at DP15.

Treated flows from Design Point DP15 will be conveyed in a 42-inch storm drain until reaching Design Point DP16.

Sub-basin 13 is to be comprised of single-family housing. The lots within this basin are expected to have a maximum size of 1/8 acre. Internal site curb, gutter, and storm drain will direct the flows to the south and east until reaching Sub-basin 14.

Sub-basin 14 will also be single-family residential with lot sizes equal or less than 1/8 of an acre. Runoff internal to this basin, as well as the accepted flows from Sub-basin 13, will be routed via curb, gutter, and storm drain to the south and east until entering Sub-basin 15.

Sub-basin 15 is a proposed single-family subdivision with 1/8 acre, or less, lot sizes. Developed runoff from this basin (as well as Sub-basins 13 and 14) will be collected in the onsite curb, gutter, and storm drain and directed to the basin low point at the southeastern corner. At this point, detention and water quality facility DF-8 will accept the flows at Design Point DP14.

Sub-basin 17 is currently designated as commercial. Runoff from this site will be collected in curb, gutter, and onsite storm drain and directed to the west to discharge into detention and water quality pond DF-8 at Design Point DP14.

Discharge from DF-8 will be equal to or lesser than the historical peak discharge as required by the City. From here, flows will be conveyed to the south via a 36-inch storm drain until reaching Design Point DP16.

Design Point DP16 is the ultimate discharge for the East Basin. The combined flows calculated for this design point result in 28.5 cfs in the minor storm event and 121.9 cfs in the major storm event. In the existing conditions, this discharge point was estimated to have 16.5 cfs in the minor storm and 93.1 cfs in the major storm. However, the previously approved **MDDP** and **WFJCC DBPS** for the area specify an allowable release of 38 cfs for the 5-year storm and 153 cfs in the 100-year storm.

The current report in review with the City of Fountain for the Glen at Widefield Filing No. 11, which receives the discharge from Corvallis DP16 has proposed two 36-inch culverts to convey the drainage from the Corvallis East Basin to the roadside swale being constructed as a part of the Marksheffel Road improvements. The capacity of these culverts is 87.06 cfs. Refer to Appendix C for the structures (CV177) referenced from the Final Drainage Report for the Glen at Widefield Filing No. 11.

As basins tributary to the East Basin are designed, additional analysis will be required in order to confirm the downstream capacity available.

A summary of the sub-basins and design points within the East Basin are summarized below:

East Basin			
Basin Name	Acreage	Peak Flows	
		5-Year	100-Year
<i>OS-6</i>	0.8	3.2	5.8
<i>OS-7</i>	2.9	2.5	9.4
<i>12</i>	18.0	29.5	65.1
<i>13</i>	5.6	11.4	25.1
<i>14</i>	11.4	18.9	41.6
<i>15</i>	16.9	29.0	63.8
<i>16</i>	34.1	101.6	193.7
<i>17</i>	2.5	10.9	19.9

Central Basin		
Design Point	Peak Flows	
	5-Year	100-Year
<i>DP12</i>	25.6	55.7
<i>DP13</i>	21.2	46.8
<i>DP14</i>	33.8	73.3
<i>DP15</i>	17.5	74.1
<i>DP16</i>	28.5	121.9

DP16 Summary							
Approved DBPS/MDDP		Glen at Widefield FDR 11		MDDP (Ex. Cond.)		MDDP (Pr. Cond.)	
5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year
38.0	153.0	N/A	87.1	16.5	93.1	28.5	121.9

Full Spectrum Detention Facilities

In accordance with the City of Fountain drainage criteria, the proposed Corvallis development will provide onsite full spectrum detention facilities to mitigate developed drainage impacts. Detained flows will release at historic rates and drainage patterns. At this time, ponds in series are not anticipated. This requires treated flows and offsite flows to be conveyed separately from untreated flows. Further design will need to be done if this design intent changes. A breakdown of the required storage volume and historic release rates for each of the water quality and detention facilities are summarized below:

PROPOSED WATER QUALITY AND DETENTION SUMMARY							
<i>Corvallis</i>							
<i>Detention/ WQ Pond</i>	<i>TOTAL AREA (AC)</i>	<i>CONTRIBUTING BASINS</i>	<i>% IMPERVIOUS</i>	<i>VOLUME REQUIRED (AC-FT)</i>	<i>Q(5) PRE- DEVELOPED (cfs)</i>	<i>Q(100) PRE- DEVELOPED (cfs)</i>	<i>DESCRIPTION:</i>
DF-1	5.65	1B-COMMERCIAL	95%	0.89	2.1	8.8	<i>Northwest Commercial</i>
DF-2	8.25	1B-MULTIFAMILY	70%	1.00	1.2	13.8	<i>Northwest Multi- Family</i>
DF-3*	61.51	1A, 2, 3, OS-2	65%	7.02	15.7	61.3	<i>West Single-Family</i>
DF-4*	23.14	4, 6	65%	2.64	4.8	22.0	<i>Southwest Single- Family</i>
DF-5*	57.67	5, 9, 10, 11, OS-5	70%	6.98	7.2	48.1	<i>South Single-Family & School Site</i>
DF-6	5.08	8	95%	0.80	2.2	8.8	<i>Northeast Commercial</i>
DF-7	18.75	12, OS-6	70%	2.27	6.2	26.1	<i>Northeast Multi- Family</i>
DF-8*	36.43	13, 14, 15, 17	70%	4.41	11.0	47.8	<i>Southeast Single- Family & Commercial</i>
DF-9*	34.13	16	80%	4.61	11.3	48.0	<i>Southeast Commercial Pond</i>

*Asterisk * denotes "Sub-Regional" Detention. The other ponds are considered "Onsite" Detention.*

IV. Hydraulic Analysis

A. OVERVIEW, METHODOLOGY & DESIGN

Developed sub-basins and proposed drainage improvements are depicted on the attached Developed Drainage Basin Map (DR02) in Appendix D. Preliminary hydraulic design calculations for sizing of onsite facilities are provided for in Appendix A. In general, the hydraulic criteria and intent are summarized as follows:

In accordance with City of Fountain drainage criteria, major drainage will be conveyed through the Corvallis development using a combination of open channels, underground storm sewer capacity and allowable street capacity. For local residential streets, the maximum allowable depth during the 100-year event is 8-inches or the extent of the street right-of-way such that buildings are not inundated at the ground line.

The interior roads will be graded with a minimum longitudinal slope of 1.0 percent. In accordance with the street spread calculations in the DCM, the allowable minor storm street capacity is 8 cfs per side for 6-inch ramp curb and 12 cfs per side for 6-inch vertical curb. The allowable major storm street capacity is approximately 36 cfs per side (72 cfs full width). Reference Appendix B for sizing chart.

Curb inlets (CDOT Type R or equivalent City approved 6-inch curb inlet type) will be specified where required for at-grade and sump collection point locations. Inlets will convey runoff to a storm sewer consisting of reinforced pipes (RCP) with a minimum pipe diameter of 18-inches. Preliminary storm sewer sizing has been provided based on full flow capacity at a minimum slope of 1.0 percent and can be referenced in Appendix A. Riprap stilling basins will be utilized at storm pipe outfalls. Detailed inlet, storm sewer and riprap sizing calculations will be provided with the Final Drainage Reports for each filing.

A preliminary hydraulic analysis been completed as part of this study to determine the required storm pipe sizing for the site trunk mains. Hydraulic grade lines (calculated in StormCAD and using head loss coefficients from Table 9-4 of the DCM) will be provided with either the FDR or along with construction drawings. Initial sizing of the onsite detention ponds was completed using UDFCD Detention Pond software for Extended Detention Basins. The pond has been evaluated to determine the peak release rates from the proposed detention pond and the storage required for the 100-year storm event. Most proposed storm pipes have been upsized to accommodate larger flows as a conservative design.

If further design of the site alters the design intent as discussed within this MDDP, an amendment will be required to show compliance with the City of Fountain criteria.

B. FLOODPLAINS

Per the *Flood Insurance Rate Map (FIRM) 08041C 0956 G and 08041C 0957 G*, effective date December 7, 2018, published by the Federal Emergency Management Agency (FEMA), a portion of Corvallis lies within the designated 100-year floodplain of Jimmy Camp Creek West Tributary. A FIRMette of the project area is included in Appendix D.

Per the approved **WFJCC DBPS**, as land is developed adjacent to the WFJCC, creek improvements will be required. **WFJCC DBPS** Map 4A (Appendix D) shows the existing 30-inch culvert to be removed north of Fontaine Boulevard and directed to the existing bridge crossing. The sections of the WFJCC that traverse through the Corvallis site are specified as 3030-2 and 3030-1. The **WFJCC DBPS** recommends channel improvements to include a rip-rap lined channel up to the 100-year water surface elevation as well as check dams at 150' intervals in both sections. Actual channel design will differ from the DBPS recommendations slightly and will follow more recent channel design criteria and likely act to preserve the existing wetlands (to be delineated in the future).

Creek improvements will be triggered when development within the sub-basins listed as a part of this MDDP's West Basin begins but will be partially reimbursable via the required drainage fees paid by the development. After this trigger occurs, further investigation into the true creek requirements based on actual field conditions will be required.

As development progresses in the Corvallis development, a Letter of Map Amendment (LOMA) and/or Letter of Map Revision (LOMR) will be required once channel improvements are triggered by the above indicated criteria in order to show the revised extent of the regulatory floodplain through the site. The channel and improvements will be located within a tract and will be owned and maintained by the metro district.

V. Environmental Evaluations

A. WETLAND IMPACTS

Per the U.S. Fish and Wildlife National Wetlands Inventory, there are freshwater emergent wetlands located onsite. *Wetland delineation will be required once channel improvements are triggered by future development.*

B. STORMWATER QUALITY

All onsite detention facilities shall be designed to accommodate water quality requirements. As the development of each parcel progresses, the detention guidelines outlined in this report are to be upheld.

Per the DCM Chapter 1, Section 4, the City of Fountain requires the UDFCD Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls.

Step 1: ***Reduce runoff by disconnecting impervious area, eliminating “unnecessary” impervious area and encouraging infiltration into soils that are suitable.***

Site specific landscaping will be done on each lot to decrease the connectivity of impervious areas. Grass lined swales will be used where possible to allow ground infiltration. The open space running along the existing gas right of way is a site-specific example of disconnection between impervious surfaces on this project.

Step 2: *Treat and slowly release the WQCV.*

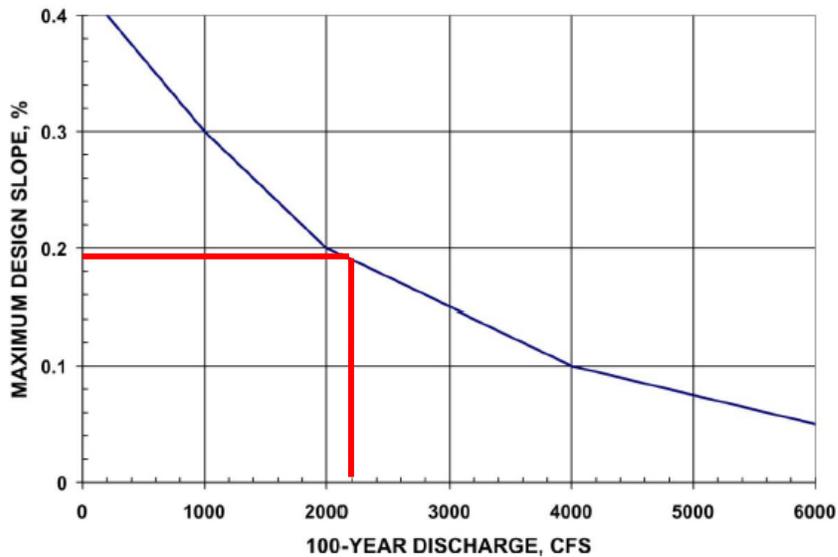
The proposed detention ponds meet or exceed the DCM standards for the release rates of Full Spectrum Detention Ponds for Water Quality Capture Volumes.

Step 3: *Stabilize stream channels.*

Drainage fees paid at the time of platting should be utilized in the construction of the future stream improvements for the West Fork Jimmy Camp Creek Drainage Fee Basin as it runs through the development.

Based on the available LIDAR contour data for the site, the existing channel has a slope of approximately 0.65%. Field investigations of the site appear to show a stable channel. There are four pond areas in the channel bottom providing stilling and energy dissipation. Per the DCM Figure 12-4 and the indicated DBPS Q100 of 2216 cfs the anticipated design slope for channel changes is 0.19%. Using these two slopes and a channel length through the Corvallis site of 2,652 feet, we anticipate approximately 12 feet of drop structures will be required. This will likely mean three 4' drop structures designed and placed to preserve the existing ponds. Depth of drop may vary slightly if the future channel improvements recommend changes to the sinuosity of the stream bed and thereby alter the length and slope of the channel through this development.

Figure 12-4. Maximum Low-flow Channel Design Slope for Sand-bed Channels



The other likely improvement will be rip rap slope protection along the outside banks on the bends of the channel meander to preserve the current stream path.

Field investigations of the channel show a series of three small elongated ponds and one smaller pond.



Figure 1-South Pond

Southernmost pond above. The southernmost, as shown above, and the northernmost two ponds have flat and stable banks. Other ponds, as shown below, have short sections with steeper banks.



Figure 2-North End of Middle Pond

Sloughing of banks is very minimal and only evident in a couple of instances. One instance is visible in the upper right bank in the photo above. Most of the bare soil along the channel is caused by cattle grazing the area. The south end of the same pond shown in Figure 2 shows stable banks



Figure 3-South end of Middle Pond



Figure 4-North Elongated Pond Looking South

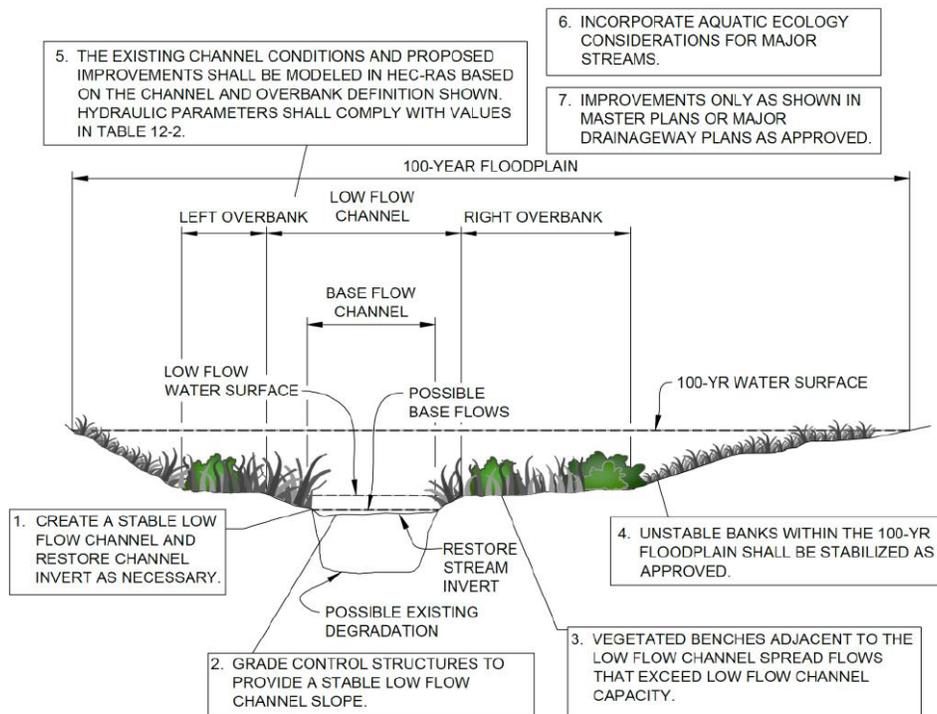
The northernmost of the elongated ponds is shown above. Note the shallow, steeper banks closer to the north end of the pond and the flatter banks towards the south end of the pond.



Figure 5-Northernmost Pond

Future improvements to the channel will likely involve laying back some of the steeper banks and providing a channel section more in line with the typical section indicated in the DCM.

Figure 12-3. Design Elements Associated With Major Natural Drainageways



The above section is already reflected in much of the channel. It is anticipated that future improvements will regrade the steeper banks of the channel to more closely match this section, add overbanks for lower probability flows where they are lacking and armor the outside banks of bends in the stream. Drop structures will likely be constructed between the existing pond areas in an attempt to preserve, and limit disturbance to, the wetlands, but some minor modifications of the middle pond location may be required to facilitate the proposed crossing of the stream by Residential Collector A.

Given the existing apparent stability of much of the channel, it may be more optimal to use some buried drop structures in some locations of the channel design to preserve the existing channel conditions, spot fix areas with bank issues and place normal drop structures as appropriate to preserve the channel flow line and ponded areas.

The future channel design report will consider the above factors as well as any potential changes to the design criteria which have arisen in the interim.



Figure 6 & 7-Jimmy Camp Creek-West Fork Looking North from South End of Property

Step 4: *Implement source controls.*

During construction, the contractor will have designated concrete washout areas and will implement sediment control logs and inlet protection in order to control pollutants at their

source. If long term stockpiling of materials is desired, further source controls must be designed to comply with the GEC and SWMP criteria.

C. PERMITTING REQUIREMENTS

A USACE 404 permit and PPRBD floodplain development permit are anticipated permits which will be required along with the future channel improvements.

VI. Selected Plan

A. PLAN HYDROLOGY

Land Use

In the approved ***WFJCC DBPS***, this area was specified as the “Crescent Heights Development” and was anticipated to have medium/high density residential as well as office and commercial. In compliance with the ***WFJCC DBPS***, Corvallis is anticipated to be a multi-use planned unit development. Anticipated developed uses include commercial, multi-family residential, and single-family residential (1/8 acre or less). Some portions of the site will remain as undeveloped open space. The land use map from the ***WFJCC DBPS*** is included in the Appendix D.

Runoff

The proposed 275-acre site is located entirely within the West Fork Jimmy Camp Creek. This tributary has a drainage area of 4 square miles according to ***WFJCC DBPS***. The developed area makes up less than 11% of the tributary’s drainage area.

As noted in Section II-C, 81 percent of the site is made up of Type B soils. Drainage coefficients for HSG A&B soil types used were per Table 6-6 in the DCM. Refer to Appendix A for specific runoff coefficient values.

Flows

According to ***WFJCC DBPS***, the Corvallis (Crescent Heights) development will discharge at 3 separate points. Per UD-Detention modeling of the proposed detention basin, detention from this project will either be equal to or reduce the Q100 (Major Storm) discharge from the property from the pre-development. As the proposed development is not projected to increase runoff from the site, no additional burden should be placed on downstream drainage and detention basins. Additionally, due to the large size of the offsite drainage areas, the peak discharge from the proposed detention ponds are significantly offset from the peak flows from the offsite basins.

The hydrology for the site, which has been provided above, shows that this development complies with the latest study (***WFJCC DBPS***).

B. SYSTEM PRIORITIES/PHASING

No phasing of the development has been provided at this time. Once development of any portion of the site begins, the owner will be responsible for providing detention and water quality in accordance with this ***MDDP*** and the ***WFJCC DBPS***, before releasing downstream.

C. GOVERNMENTAL AGENCY REQUIREMENTS

Other than the USACE 404 permit, there are no external governmental agency requirements for this development. A final Drainage Report for each future phase of development will be presented to the City of Fountain with the development of the construction documents.

D. MAINTENANCE REQUIREMENTS

All proposed road and drainage construction within the Corvallis development will be performed to City of Fountain standards. Proposed roads and drainage facilities within the public right of way will be maintained by the City of Fountain upon acceptance of these facilities after the warranty period. The proposed detention ponds will be privately owned and maintained by the metropolitan district. Maintenance requirements for all stormwater quality and erosion control procedures will be outlined in individual Erosion Control and Storm Water Management Plans.

E. RECOMMENDATION FOR IMPLEMENTATION

It is recommended that any development of the site initiates the implementation of the detention and water quality procedures that have been detailed in this report. In doing so, the developed conditions will produce runoff comparable to or lower than existing conditions, which allows continued adherence to **WFJCC DBPS** and protects downstream owners and facilities.

VII. Fee Development

A. Construction Cost Opinion

An engineer's estimate of probable construction costs will be provided with the Final Drainage Report for each phase of the development. The developer will pay all capital costs for the proposed roadway and drainage facilities.

Channel improvements are required as part of the DBPS. Costs for these improvements offset the drainage fees due to the City of Fountain from the site. When originally produced, the DBPS indicated that the City of Fountain did not collect drainage fees. The City has since instituted a drainage fee which, therefore, will apply towards the channel improvements.

B. Drainage Basin Fees

The parcel is located within the West Fork Jimmy Camp Creek Drainage Basin, which has a drainage fee requirement based on City of Fountain drainage policies. The City of Fountain Municipal Code in Ordinance 1705 established the Drainage Fees for Jimmy Camp Creek Drainage Basin Fees at a rate of \$10,892.03 per impervious acre after July 1, 2018. Per this ordinance a Jimmy Camp Drainage Basin Fee of \$1,513,992.17 is estimated for this project based on a calculated 139 acres of impervious area. A drainage fee will be collected by the governing Metro District to complete funding of the future channel improvements.

Within the 2003 WFJCC DBPS a unit cost for channel improvements along this section (3030-2) of channel of \$458.30 is estimated. Using 2% inflation and the channel length through the site of 2645 linear feet, (Note: there is more sinuosity in the natural channel than demonstrated in the DBPS, however, the DBPS indicates two other channel improvement areas through the proposed site which will be addressed via storm sewer.), an overall cost in today's dollars of \$1,697,378 is estimated using the DBPS numbers. The channel improvements below are within about 10% of this number.

a. Estimated Cost of Channel Improvements

Corvallis PUD West Fork - Jimmy Camp Creek Engineer's Opinion of Probable Cost					
BID ITEM NO.	DESCRIPTION OF BID ITEM	QUANTITY	PAY UNIT	UNIT PRICE	TOTAL COST OF BID ITEM
1	Mobilization	1	LS	\$100,000.00	\$100,000
2	Water Control & Dewatering	1	LS	\$60,000.00	\$60,000
3	Erosion & Sediment Control	1	LS	\$30,000.00	\$30,000
4	Clearing & Grubbing	1	LS	\$10,000.00	\$10,000
5	Drop Structures (4 ft)	4	EA	\$190,000.00	\$760,000
6	Seeding (Wetland, Riparian, Upland)	1	LS	\$20,000.00	\$20,000
7	Willow Stakes	1	LS	\$10,000.00	\$10,000
8	Erosion Control Blanket	500	SY	\$20.00	\$10,000
9	Earthwork (Onsite Cut & Fill)	1	LS	\$20,000.00	\$20,000
10	Soil Rip Rap (Outside Bends)	2,200	SY	\$100.00	\$220,000
11	CDOT Class II Road Base (Access Road)	765	CY	\$85.00	\$65,000
Subtotal					\$1,305,000
10% Contingency					\$130,500
Engineering					\$78,300
Estimated Total Cost					\$1,513,800
Developed Acres					275
Anticipated Cost / Developed AC.					\$5,505

Since the engineer has no control over the cost of labor, materials, equipment or services furnished by others, or over the contractor's method of determining prices, or over the competitive bidding or market conditions, the opinion of probable construction costs provided herein are made on the basis of the engineer's experience and qualifications and represents the best judgment as an experienced and qualified professional familiar with the construction industry. The engineer cannot, and does not guarantee that proposals, bid or actual construction costs will not vary from the opinion of probable costs.

Construction costs for channel improvements, outside of reimbursable expenses, will be paid for by the Metropolitan District. A combination of Drainage Fees and mill levees will reimburse the Metropolitan District.

VIII. Summary

As described above, this report demonstrates compliance with the governing DCM and DBPS and will comply with downstream drainage reports.

IX. References

1. *City of Colorado Springs Drainage Criteria Manual*, City of Colorado Springs, May 2014
2. *Web Soil Survey of El Paso County Area, Colorado. Unites States Department of Agriculture Soil Conservation Service*, November 2015.
3. *Flood Insurance Rate Maps for El Paso County, Colorado and Incorporated Areas, Panel 958 of 1300, Federal Emergency Management Agency*, Effective Date December 7, 2018.
4. *Urban Storm Drainage Criteria Manual, Vol. 1-3* by Urban Drainage and Flood Control District (UDFCD), January 2016
5. *West Fork Jimmy Camp Creek Drainage Basin Planning Study (WFJCC DBPS)*, by Kiowa Engineering Corp. October 2003.
6. *Master Drainage Development Plan (MDDP) The Glen at Widefield*, by Kiowa Engineering Corp. December 1999.
7. *Final Drainage Report (FDR F9) The Glen at Widefield Filing No. 9*, by Kiowa Engineering Corp. July 2018.
8. *Final Drainage Report (FDR F11) The Glen at Widefield Filing No. 11*, by Kiowa Engineering Corp. December 2019.

APPENDIX A

HYDROLOGIC AND HYDRAULIC CALCULATIONS

Project Name: Corvallis
 Project Location: Fourrain, CO
 Designer: NMS
 Notes: Existing Conditions



Channel Flow Type Key
 Heavy Meadow 2
 Tillage/Field 3
 Short Pasture and Lawns 4
 Nearly Bare Ground 5
 Grassed Waterway 6
 Paved Areas 7

Average Channel Velocity: 5 ft/s (If specific channel vel is used, this will be ignored)
 Average Slope for Initial Flow: 0.04 ft/B (If Elevations are used, this will be ignored)

Basin	Description	Area		Rational 'C' Values												Flow Lengths				Initial Flow			Channel Flow					Tc	Rainfall Intensity & Rational Flow Rate								% Imp					
		SF	Acres	Surface Type 1 (Single-Family 1 & 1/3 Ac. Lots)			Surface Type 2 (Greenbelts & Agriculture)			Surface Type 3 (Single-Family 1/8 Ac. Lots & Multi-Family)			Surface Type 4 (Impervious)			Weighted C-Factor		Initial	True Initial	Channel	True Channel	High Point	Low Point	Average	Initial	High Point	Low Point		Average	Channel Flow Type (See Key above)	Velocity	Channel	Total	i2	Q2	i5		Q5	i10	Q10	i100	Q100
				C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C5	C100	Area	C5	C100	ft	Length ft	ft	Length ft	Elevation	Elevation	Slope	Tc (min)	Elevation	Elevation		Slope	Ground Type	(ft/s)	Tc (min)	(min)	in/hr	cfs	in/hr		cfs	in/hr	cfs	in/hr	cfs
OS-1a	Single Family > 2.5 Acr Lots (12% Impervious (min.))	1,675,407	38.46	0.20	0.44		0.09	0.36	1474358	0.45	0.59		0.90	0.96	201049	0.19	0.44	300	300	2,290	2290	5,807	5,800	0.023	22.2	5800	5,725	3.28	4	1.3	30.5	52.7	1.4	10.1	1.7	12.7	2.0	14.8	2.9	49.3	13.8%	
OS-1b	Single Family > 2.5 Acr Lots (12% Impervious (min.))	1,668,351	38.30	0.20	0.44		0.09	0.36	1468149	0.45	0.59		0.90	0.96	200202	0.19	0.44	900	300	1,871	2471	5,894	5,820	0.082	14.6	5820	5,780	2.14	4	1.0	40.6	55.2	1.3	9.7	1.7	12.3	1.9	14.3	2.8	47.7	13.8%	
OS-2	Frontage Backward to crown of road	42809	0.98	0.20	0.44		0.09	0.36	42809	0.45	0.59		0.90	0.96	42809	0.90	0.96	25	25	1362	1362	5758	5757	0.040	1.2	5757	5719	2.79	7	3.3	6.9	8.1	3.5	3.1	4.4	3.9	5.2	4.6	7.4	7.1	100.0%	
OS-3	Offsite undeveloped parcel	80878	1.86	0.20	0.44		0.09	0.36	80878	0.45	0.59		0.90	0.96		0.09	0.36	170	170	275	275	5739	5718	0.124	10.7	5718	5703	5.45	3	1.2	3.9	14.6	2.8	0.5	3.5	0.6	4.1	0.7	5.9	4.0	2.0%	
OS-4	Offsite undeveloped parcel	797941	18.32	0.20	0.44		0.09	0.36	797941	0.45	0.59		0.90	0.96		0.09	0.36	301	300	1018	1019	5732	5719	0.045	20.1	5719	5696	2.26	3	0.7	22.9	43.0	1.6	2.6	2.0	3.3	2.3	3.8	3.3	21.8	2.0%	
OS-5	Frontage Backward to crown of road	32917	0.76	0.20	0.44		0.09	0.36	32917	0.45	0.59		0.90	0.96	32917	0.90	0.96	25	25	1100	1100	5771	5770	0.040	1.2	5770	5740	2.73	7	3.3	5.6	6.8	3.7	2.6	4.7	3.2	5.5	3.8	7.9	5.8	100.0%	
OS-6	Frontage Backward to crown of road	33529	0.77	0.20	0.44		0.09	0.36	33529	0.45	0.59		0.90	0.96	33529	0.90	0.96	25	25	1100	1100	5771	5770	0.040	1.2	5770	5743	2.45	7	3.1	5.9	7.1	3.7	2.6	4.6	3.2	5.4	3.8	7.8	5.8	100.0%	
OS-7	Single Family Residential to east	126529	2.90	0.20	0.44	126529	0.09	0.36		0.45	0.59		0.90	0.96		0.20	0.44	40	40	160	160	5708	5706	0.050	6.2	5706	5702	2.50	4	1.1	2.4	8.6	3.4	2.0	4.3	2.5	5.1	3.0	7.3	9.4	7.0%	
OS-8	Offsite undeveloped parcel	961463	22.07	0.20	0.44		0.09	0.36	961463	0.45	0.59		0.90	0.96		0.09	0.36	300	300	1055	1055	5731	5715	0.053	18.7	5715	5682	3.13	3	0.9	30.0	38.7	1.7	3.3	2.1	4.2	2.4	4.9	3.5	28.1	2.0%	
EX-1	West side of site	2959892	67.95	0.20	0.44		0.09	0.36	2959892	0.45	0.59		0.90	0.96		0.09	0.36	300	300	2266	2266	5753	5736	0.057	18.3	5736	5682	2.38	3	0.8	49.8	68.2	1.2	7.1	1.5	9.0	1.7	10.5	2.4	60.3	2.0%	
EX-2	Northwest corner	449242	10.31	0.20	0.44		0.09	0.36	449242	0.45	0.59		0.90	0.96		0.09	0.36	300	300	350	350	5752	5738	0.047	19.6	5738	5719	5.43	3	1.2	5.0	24.6	2.1	2.0	2.7	2.5	3.2	3.0	4.5	17.0	2.0%	
EX-3	Central-east	2262585	51.94	0.20	0.44		0.09	0.36	2262585	0.45	0.59		0.90	0.96		0.09	0.36	300	300	1530	1530	5740	5728	0.040	20.6	5728	5688	2.61	3	0.8	31.6	52.2	1.4	6.5	1.7	8.2	2.0	9.5	2.9	54.8	2.0%	
EX-4	Central-east	2551274	58.57	0.20	0.44		0.09	0.36	2551274	0.45	0.59		0.90	0.96		0.09	0.36	300	300	2710	2710	5768	5756	0.040	20.6	5756	5685	2.62	3	0.8	56.0	76.6	1.1	5.7	1.3	7.2	1.6	8.3	2.3	48.1	2.0%	
EX-5	East side of site	3769253	86.53	0.20	0.44		0.09	0.36	3769253	0.45	0.59		0.90	0.96		0.09	0.36	300	300	1830	1830	5770	5765	0.017	27.6	5765	5686	4.32	3	1.0	29.4	57.0	1.3	10.2	1.6	12.8	1.9	15.0	2.7	86.3	2.0%	

Note: Q2, Q5 & Q10 are based on C5; Q25, Q50 & Q100 are based on C100

RATIONAL METHOD - PROPOSED CONDITIONS

Project Name: Corvallis
 Project Location: Fountain, CO
 Designer: NMS
 Notes: Proposed Conditions



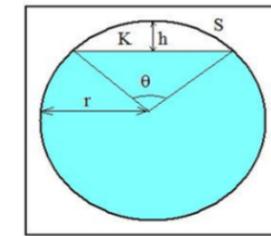
Channel Flow Type Key
 Heavy Meadow 2
 Tillage/Field 3
 Short Pasture and Lawns 4
 Nearly Bare Ground 5
 Grassed Waterway 6
 Paved Areas 7

Average Channel Velocity: 5 ft/s (If specific channel vel is used, this will be ignored)
 Average Slope for Initial Flow: 0.04 ft/ft (If Elevations are used, this will be ignored)

Basin	Description	Area		Rational 'C' Values												Flow Lengths				Initial Flow			Channel Flow					Tc (min)	Rainfall Intensity & Rational Flow Rate				% Imp	Impervious (Acres)				
		SF	Acres	Surface Type 1 (Single-Family 1 & 1/3 Ac. Lots)			Surface Type 2 (Greenbelts & Agriculture)			Surface Type 3 (Single-Family 1/8 Ac. Lots & Multi-Family)			Surface Type 4 (Impervious)			Weighted C-Factor	Initial ft	True Initial Length ft	Channel ft	True Channel Length ft	High Point Elevation	Low Point Elevation	Average Slope	Initial Tc (min)	High Point Elevation	Low Point Elevation	Average Slope		Channel Flow Type (See Key above)	Velocity (ft/s)	Channel Tc (min)	Total (min)			i5 in/hr	Q5 cfs	i100 in/hr	Q100 cfs
		C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C5	C100	Area																									
OS-1a	Single Family > 2.5 /Ac Lots (12% Impervious (min.))	1,675,407	38.46	0.20	0.44		0.09	0.36	1474358	0.45	0.59		0.90	0.96	201049	0.19	0.44	300	300	2,290	2,290	5,807	5,800	0.025	22.2	5800	5,725	3.28	4	1.3	30.5	52.7	1.7	12.7	2.9	49.3	13.8%	
OS-1b	Single Family > 2.5 /Ac Lots (12% Impervious (min.))	1,668,351	38.30	0.20	0.44		0.09	0.36	1468149	0.45	0.59		0.90	0.96	200202	0.19	0.44	900	300	1,871	2,471	5,894	5,820	0.082	14.6	5820	5,780	2.14	4	1.0	40.6	55.2	1.7	12.3	2.8	47.7	13.8%	
OS-2	Fountain BL3/D	42,809	0.98	0.20	0.44		0.09	0.36		0.45	0.59		0.90	0.96	42809	0.09	0.36	25	25	1,362	1,362	5,758	5,757	0.040	1.2	5757	5,719	2.79	7	3.3	6.9	8.1	4.4	3.9	7.4	7.1	100.0%	
OS-3	Agricultural Land	80,878	1.86	0.20	0.44		0.09	0.36	80878	0.45	0.59		0.90	0.96		0.09	0.36	170	170	275	275	5,739	5,718	0.124	10.7	5718	5,703	5.45	3	1.2	3.9	14.6	3.5	0.6	5.9	4.0	2.0%	
OS-4	Agricultural Land	797,941	18.32	0.20	0.44		0.09	0.36	797941	0.45	0.59		0.90	0.96		0.09	0.36	300	300	1,018	1,018	5,732	5,719	0.043	20.1	5719	5,696	2.26	3	0.7	22.9	42.9	2.0	3.3	3.3	21.9	2.0%	
OS-5	Fountain BL3/D	32,917	0.76	0.20	0.44		0.09	0.36		0.45	0.59		0.90	0.96	32917	0.09	0.36	25	25	1,100	1,100	5,771	5,770	0.040	1.2	5770	5,740	2.73	7	3.3	5.6	6.8	4.7	3.2	7.9	5.8	100.0%	
OS-6	Fountain BL3/D	33,529	0.77	0.20	0.44		0.09	0.36		0.45	0.59		0.90	0.96	33529	0.09	0.36	25	25	1,100	1,100	5,771	5,770	0.040	1.2	5770	5,743	2.45	7	3.1	5.9	7.1	4.6	3.2	7.8	5.8	100.0%	
OS-7	Back of Lots in Cottonwood Grove V1	126,529	2.90	0.20	0.44	126529	0.09	0.36		0.45	0.59		0.90	0.96		0.20	0.44	40	40	160	160	5,708	5,706	0.050	6.2	5706	5,702	2.50	4	1.1	2.4	8.6	4.3	2.5	7.3	9.4	30.0%	
OS-8	Singer's Subdivision Tract No. 1 - Offsite (Agricultural)	961,463	22.07	0.20	0.44		0.09	0.36	961463	0.45	0.59		0.90	0.96		0.09	0.36	300	300	1,055	1,055	5,731	5,715	0.053	18.7	5715	5,682	3.13	3	0.9	20.0	38.7	2.1	4.2	3.5	28.1	2.0%	
1A	Single Family Residential	1,231,685	28.28	0.20	0.44		0.09	0.36		0.45	0.59	1231685	0.90	0.96		0.45	0.59	50	50	2,025	2,025	5,775	5,772	0.070	4.5	5772	5,694	3.85	6	2.9	11.5	16.0	3.4	43.1	5.6	94.9	65.0%	18.38
1B	Commercial & Multi-Family Residential	606,159	13.92	0.20	0.44		0.09	0.36	120250	0.45	0.59	0	0.90	0.96	485909	0.74	0.85	50	50	940	940	5,745	5,744	0.020	3.8	5744	5,714	3.19	7	3.5	4.4	8.2	4.4	45.7	7.4	88.2	0.0%	0.00
2	Single Family Residential	1,245,687	28.60	0.20	0.44		0.09	0.36		0.45	0.59	1245687	0.90	0.96		0.45	0.59	50	50	1,916	1,916	5,758	5,746	0.240	3.0	5746	5,698	2.51	6	2.4	13.5	16.4	3.3	43.0	5.6	94.8	65.0%	18.59
3	Single Family Residential	1,245,623	28.59	0.20	0.44		0.09	0.36	294823	0.45	0.59	30800	0.90	0.96		0.13	0.39	50	50	875	875	5,714	5,712	0.040	8.1	5712	5,682	3.43	3	0.9	15.8	23.9	2.7	2.7	4.6	13.6	8.0%	0.59
4	Single Family Residential	1,501,305	34.22	0.20	0.44		0.09	0.36	92356	0.45	0.59	442453	0.90	0.96	215496	0.54	0.67	50	50	1,390	1,390	5,707	5,704	0.060	4.1	5704	5,695	0.65	6	1.2	19.9	24.0	2.7	25.7	4.6	53.6	67.3%	11.59
5	Single Family Residential	259,041	5.95	0.20	0.44		0.09	0.36	77712	0.45	0.59		0.90	0.96	181329	0.66	0.78	50	50	425	425	5,710	5,708	0.040	3.7	5708	5,686	5.18	6	3.4	2.1	5.8	4.9	19.5	8.3	38.6	70.6%	6.53
6	Single Family Residential	437,600	10.05	0.20	0.44		0.09	0.36		0.45	0.59	437600	0.90	0.96		0.45	0.59	50	50	1,039	1,039	5,717	5,716	0.020	6.8	5716	5,698	1.78	6	2.0	8.9	15.7	3.4	15.5	3.7	34.1	65.0%	6.53
7	Single Family Residential	840,080	19.29	0.20	0.44		0.09	0.36	840080	0.45	0.59		0.90	0.96		0.09	0.36	300	300	1,477	1,477	5,739	5,736	0.010	32.7	5736	5,700	2.44	3	0.8	31.8	64.5	1.5	2.6	2.5	17.8	2.0%	0.39
8	Single Family Residential	221,448	5.08	0.20	0.44		0.09	0.36	11072	0.45	0.59		0.90	0.96	210376	0.86	0.93	50	50	610	610	5,767	5,763	0.080	1.6	5763	5,749	2.30	7	3.0	3.4	8.0	5.1	22.5	8.6	40.8	95.1%	4.83
9	Single Family Residential	881,274	20.23	0.20	0.44		0.09	0.36		0.45	0.59	881274	0.90	0.96		0.45	0.59	50	50	827	827	5,767	5,764	0.060	4.7	5764	5,732	3.87	6	2.9	4.7	9.4	4.2	38.5	7.0	84.7	65.0%	13.15
10	Single Family Residential	769,918	17.67	0.20	0.44		0.09	0.36		0.45	0.59	769918	0.90	0.96		0.45	0.59	50	50	960	960	5,730	5,728	0.050	5.0	5728	5,702	2.66	6	2.4	6.6	11.6	3.9	31.0	6.5	68.2	65.0%	11.49
11	Single Family Residential	569,166	13.07	0.20	0.44		0.09	0.36		0.45	0.59	569166	0.90	0.96		0.45	0.59	50	50	1,241	1,241	5,725	5,724	0.020	6.8	5724	5,686	3.06	6	2.6	8.0	14.8	3.5	20.7	3.9	45.5	65.0%	8.49
12	Single Family Residential	783,308	17.98	0.20	0.44		0.09	0.36		0.45	0.59	783308	0.90	0.96		0.45	0.59	50	50	1,484	1,484	5,770	5,768	0.040	5.4	5768	5,733	2.36	7	3.0	8.2	13.6	3.6	29.5	6.1	65.1	65.0%	11.69
13	Single Family Residential	244,872	5.62	0.20	0.44		0.09	0.36		0.45	0.59	244872	0.90	0.96		0.45	0.59	50	50	484	484	5,756	5,754	0.040	5.4	5754	5,731	4.75	6	3.3	2.5	7.9	4.5	11.4	7.5	25.1	65.0%	3.65
14	Single Family Residential	497,323	11.42	0.20	0.44		0.09	0.36		0.45	0.59	497323	0.90	0.96		0.45	0.59	50	50	1,030	1,030	5,728	5,727	0.020	6.8	5727	5,695	3.11	6	2.6	6.5	13.3	3.7	18.9	6.1	41.6	65.0%	7.42
15	Single Family Residential	737,061	16.92	0.20	0.44		0.09	0.36		0.45	0.59	737061	0.90	0.96		0.45	0.59	50	50	1,095	1,095	5,725	5,723	0.040	5.4	5723	5,688	3.20	6	2.6	6.9	12.3	3.8	29.0	6.3	63.8	65.0%	11.00
16	Commercial and Park	1,486,601	34.13	0.20	0.44		0.09	0.36	307137	0.45	0.59		0.90	0.96	1179464	0.74	0.84	50	50	1,511	1,511	5,727	5,724	0.060	2.6	5724	5,687	2.45	7	3.1	8.1	10.7	4.0	101.6	6.7	193.7	79.8%	27.22
17	Commercial	107,558	2.47	0.20	0.44		0.09	0.36	5378	0.45	0.59		0.90	0.96	102180	0.86	0.93	50	50	175	175	5,688	5,687	0.020	2.5	5687	5,686	0.57	7	1.4	2.1	5.0	5.1	10.9	8.6	19.9	95.1%	2.35

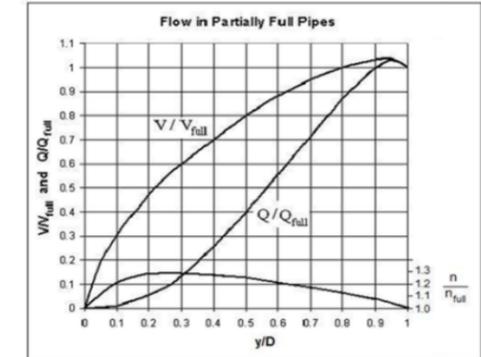
PROPOSED DESIGN POINT	Description	Area		Rational 'C' Values												Flow Lengths				Initial Flow			Channel Flow					Tc (min)	Rainfall Intensity & Rational Flow Rate				% Imp	Impervious (Acres)				
		SF	Acres	Surface Type 1 (Single-Family 1 & 1/3 Ac. Lots)			Surface Type 2 (Greenbelts & Agriculture)			Surface Type 3 (Single-Family 1/8 Ac. Lots & Multi-Family)			Surface Type 4 (Impervious)			Weighted C-Factor	Initial ft	True Initial Length ft	Channel ft	True Channel Length ft	High Point Elevation	Low Point Elevation	Average Slope	Initial Tc (min)	High Point Elevation	Low Point Elevation	Average Slope		Channel Flow Type (See Key above)	Velocity (ft/s)	Channel Tc (min)	Total (min)			i5 in/hr	Q5 cfs	i100 in/hr	Q100 cfs
		C5	C100	Area (SF)	C5	C100	Area (SF)	C5	C100	Area	C5	C100	Area																									
E1	OS-1a and OS-1b	3,343,757	76.76	0.20	0.44	0	0.09	0.36	2942507	0.45	0.59	0	0.90	0.96	401251	0.19	0.44	900	300	3,152	3,752	5,885	5,820	0.072	15.2	5820	5,725	3.01	4	1.2	51.6	66.8	1.5	21.7	2.5	84.4	13.8%	</

Design Point	Notes	Max Q (Q100) Proposed	Capacity Analysis	Storm Pipe		Percent of Pipe Capacity Used	n(full)	Slope (ft/ft)	n	Pipe Diameter (ft)	Width (ft) Box Culvert Only	Pipe Depth (inches)	Optimum Flow Depth (+/- 0.94 x D)	θ (Radians)	A (Sq. Ft.)	Wetted Perimeter (ft)	Velocity at Max Pipe Capacity
				Calculated Max Q for Pipe (CFS)	Storm Pipe												
E1	OS-1a and OS-1b	84.4	Adequate	105.4	80%	0.013	0.010	0.013	3.5			42	3.29	0.990	9.385	9.263	11.23
DP1	E1+DF-1 Release+DF-2 Release	107.0	Adequate	150.4	71%	0.013	0.010	0.013	4			48	3.76	0.990	12.259	10.587	12.27
1A	Sub-basin 1A	94.9	Adequate	105.4	90%	0.013	0.010	0.013	3.5			42	3.29	0.990	9.385	9.263	11.23
DP2	OS-2, 1A, 2, 3	212.1	Adequate	278.1	76%	0.013	0.010	0.013	5			60	4.7	0.990	19.154	13.233	14.52
DP3	DP1+DP2 Treated (DF-3 Release)+OS-8	196.3	Adequate	205.9	95%	0.013	0.010	0.013	4.5			54	4.23	0.990	15.515	11.910	13.27
DP4	7+8(DF-6 Release)	26.6	Adequate	43.0	62%	0.013	0.010	0.013	2.5			30	2.35	0.990	4.788	6.617	8.97
6	Sub-basin 6	34.1	Adequate	43.0	79%	0.013	0.010	0.013	2.5			30	2.35	0.990	4.788	6.617	8.97
DP6	4, 6	47.3	Adequate	52.6	90%	0.013	0.015	0.013	2.5			30	2.35	0.990	4.788	6.617	10.99
DP8	9, 10, OS-5	119.5	Adequate	129.0	93%	0.013	0.015	0.013	3.5			42	3.29	0.990	9.385	9.263	13.75
DP9	DP8, 5	82.4	Adequate	105.4	78%	0.013	0.010	0.013	3.5			42	3.29	0.990	9.385	9.263	11.23
DP11	DP10 Treated (DF-5 Release)	48.1	Adequate	69.8	69%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13
DP12	OS-6, 12	55.7	Adequate	69.8	80%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13
13	Sub-basin 13	25.1	Adequate	43.0	58%	0.013	0.010	0.013	2.5			30	2.35	0.990	4.788	6.617	8.97
DP13	13, 14	46.8	Adequate	69.8	67%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13
DP15	DP12 Treated (DF-7Release), 16 Treated (DF-9 Release)	74.1	Adequate	105.4	70%	0.013	0.010	0.013	3.5			42	3.29	0.990	9.385	9.263	11.23
DF-1	PRELIMINARY DETENTION POND OUTFALL PIPE	8.8	Adequate	11.0	80%	0.013	0.010	0.013	1.5			18	1.41	0.990	1.724	3.970	6.38
DF-2	PRELIMINARY DETENTION POND OUTFALL PIPE	13.8	Adequate	23.7	58%	0.013	0.010	0.013	2			24	1.88	0.990	3.065	5.293	7.73
DF-3	PRELIMINARY DETENTION POND OUTFALL PIPE	61.3	Adequate	69.8	88%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13
DF-4	PRELIMINARY DETENTION POND OUTFALL PIPE	22.0	Adequate	23.7	93%	0.013	0.010	0.013	2			24	1.88	0.990	3.065	5.293	7.73
DF-5	PRELIMINARY DETENTION POND OUTFALL PIPE	48.1	Adequate	69.8	69%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13
DF-6	PRELIMINARY DETENTION POND OUTFALL PIPE	8.8	Adequate	11.0	80%	0.013	0.010	0.013	1.5			18	1.41	0.990	1.724	3.970	6.38
DF-7	PRELIMINARY DETENTION POND OUTFALL PIPE	26.1	Adequate	43.0	61%	0.013	0.010	0.013	2.5			30	2.35	0.990	4.788	6.617	8.97
DF-8	PRELIMINARY DETENTION POND OUTFALL PIPE	47.8	Adequate	69.8	68%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13
DF-9	PRELIMINARY DETENTION POND OUTFALL PIPE	48.0	Adequate	69.8	69%	0.013	0.010	0.013	3			36	2.82	0.990	6.895	7.940	10.13



$r = D/2$
 $h = 2r - y$
 (hydraulic radius)
 $R = A/P$
 (Manning Equation)
 $Q = (1.49/n)(A)(R^{2/3})(S^{1/2})$
 $V = Q/A$
 $P = 2\pi r - r*\theta$
 $\theta = 2 \arccos \left(\frac{r-h}{r} \right)$
 $A = \pi r^2 - \frac{r^2(\theta - \sin \theta)}{2}$

Equation used for n/n_{full}: $n/n_{full} = 1.25 \cdot (y/D - 0.5)^{0.5}$ (for $0.5 \leq y/D \leq 1$)



Flow in Partially Full Pipes

PROPOSED WATER QUALITY AND DETENTION SUMMARY
Corvallis

<i>Detention/W Q Pond</i>	<i>TOTAL AREA (AC)</i>	<i>CONTRIBUTING BASINS</i>	<i>% IMPERVIOUS</i>	<i>VOLUME REQUIRED (AC-FT)</i>	<i>Q(5) PRE- DEVELOPED (cfs)</i>	<i>Q(100) PRE- DEVELOPED (cfs)</i>	<i>DESCRIPTION:</i>	<i>Discharge Pipe Size</i>
DF-1	5.65	1B-COMMERCIAL	95%	0.89	2.1	8.8	Northwest Commercial	18.0
DF-2	8.25	1B-MULTIFAMILY	70%	1.00	1.2	13.8	Northwest Multi-Family	24.0
DF-3*	61.51	1A, 2, 3, OS-2	65%	7.02	15.7	61.3	West Single-Family	36.0
DF-4*	23.14	4, 6	65%	2.64	4.8	22.0	Southwest Single-Family	24.0
DF-5*	57.67	5, 9,10, 11, OS-5	70%	6.98	7.2	48.1	South Single-Family & School Site	36.0
DF-6	5.08	8	95%	0.80	2.2	8.8	Northeast Commercial	18.0
DF-7	18.75	12, OS-6	70%	2.27	6.2	26.1	Northeast Multi-Family	30.0
DF-8*	36.43	13, 14, 15, 17	70%	4.41	11.0	47.8	Southeast Single-Family & Commercial	36.0
DF-9*	34.13	16	80%	4.61	11.3	48.0	Southeast Commercial Pond	36.0

Culvert Calculator Report

CV177

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	5,688.70 ft	Headwater Depth/Height	1.13
Computed Headwater Elevation	5,688.17 ft	Discharge	87.06 cfs
Inlet Control HW Elev.	5,688.06 ft	Tailwater Elevation	5,684.52 ft
Outlet Control HW Elev.	5,688.17 ft	Control Type	Outlet Control

Grades			
Upstream Invert	5,684.78 ft	Downstream Invert	5,684.52 ft
Length	77.00 ft	Constructed Slope	0.003377 ft/ft

Hydraulic Profile			
Profile	M2	Depth, Downstream	2.15 ft
Slope Type	Mild	Normal Depth	N/A ft
Flow Regime	Subcritical	Critical Depth	2.15 ft
Velocity Downstream	8.03 ft/s	Critical Slope	0.005723 ft/ft

Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	2		

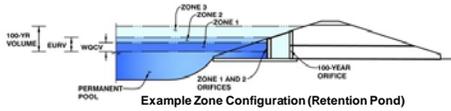
Outlet Control Properties			
Outlet Control HW Elev.	5,688.17 ft	Upstream Velocity Head	0.74 ft
Ke	0.20	Entrance Loss	0.15 ft

Inlet Control Properties			
Inlet Control HW Elev.	5,688.06 ft	Flow Control	Transition
Inlet Type	Beveled ring, 33.7° bevels	Area Full	14.1 ft ²
K	0.00180	HDS 5 Chart	3
M	2.50000	HDS 5 Scale	B
C	0.02430	Equation Form	1
Y	0.83000		

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Defention, Version 4.02 (February 2020)

Project: **Singer Ranch**
 Basin ID: **DF-1 (NW Commercial Pond)**



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB
Watershed Area =	5.66 acres
Watershed Length =	585 ft
Watershed Length to Centroid =	430 ft
Watershed Slope =	0.055 ft/ft
Watershed Imperviousness =	95.00% percent
Percentage Hydrologic Soil Group A =	0.0% percent
Percentage Hydrologic Soil Group B =	100.0% percent
Percentage Hydrologic Soil Groups C/D =	0.0% percent
Target WQC Drain Time =	40.0 hours
Location for 1-hr Rainfall Depths =	User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.211 acre-feet
Excess Urban Runoff Volume (EURV) =	0.605 acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.498 acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.643 acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.760 acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.880 acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.998 acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.127 acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) =	1.615 acre-feet
Approximate 2-yr Detention Volume =	0.488 acre-feet
Approximate 5-yr Detention Volume =	0.633 acre-feet
Approximate 10-yr Detention Volume =	0.771 acre-feet
Approximate 25-yr Detention Volume =	0.827 acre-feet
Approximate 50-yr Detention Volume =	0.858 acre-feet
Approximate 100-yr Detention Volume =	0.885 acre-feet

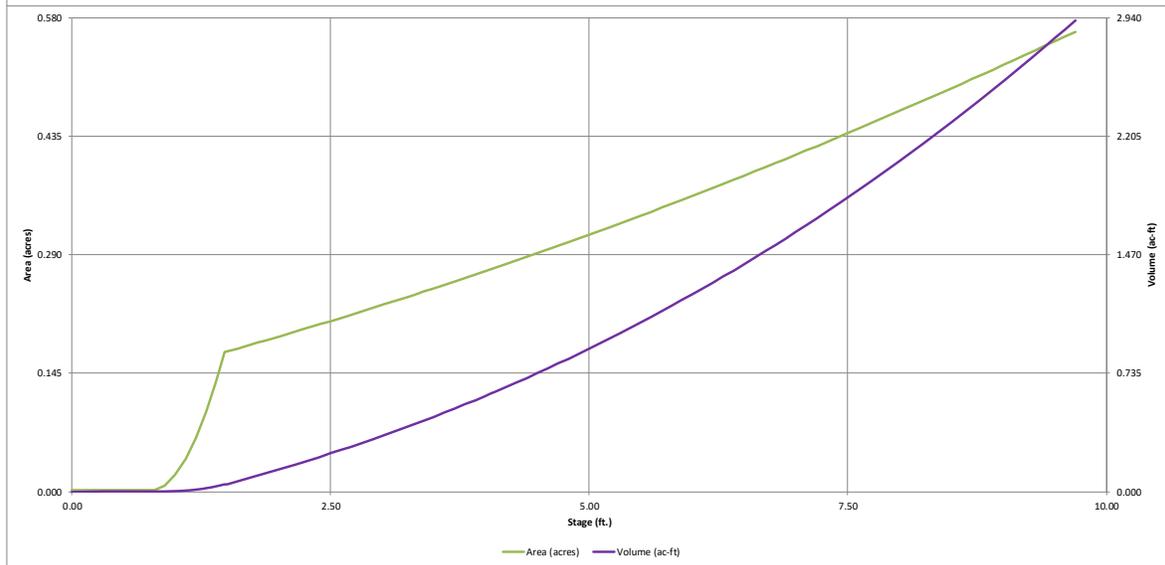
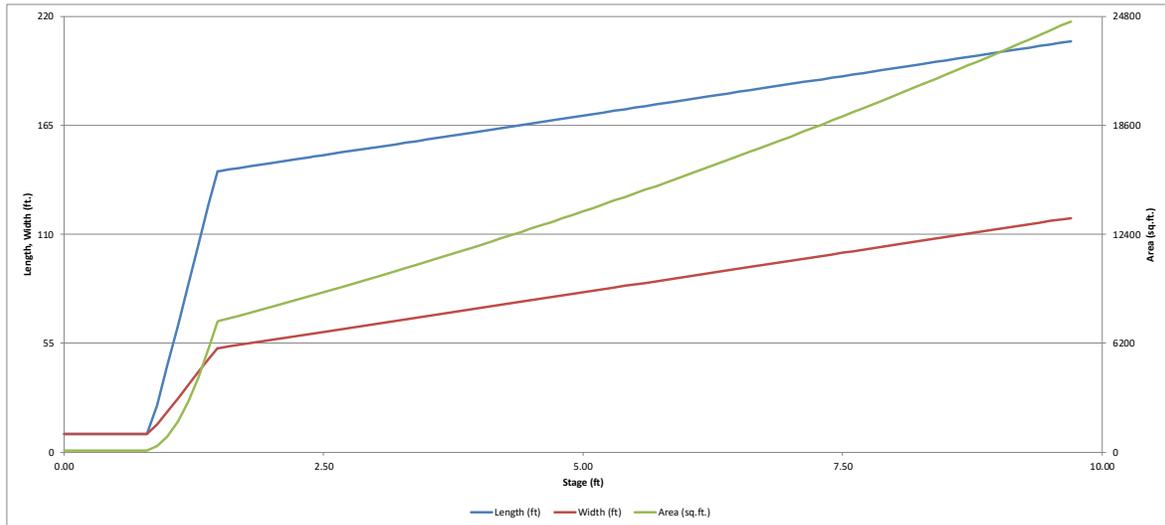
Optional User Overrides

acre-feet	
acre-feet	
1.19 inches	
1.50 inches	
1.75 inches	
2.00 inches	
2.25 inches	
2.52 inches	
3.55 inches	

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Top of Micropool	0.00		9.1	9.1	83		0.002		
ISV	0.33		9.1	9.1	83		0.002	28	0.001
	0.40		9.1	9.1	83		0.002	33	0.001
	0.50		9.1	9.1	83		0.002	42	0.001
	0.60		9.1	9.1	83		0.002	50	0.001
	0.70		9.1	9.1	83		0.002	58	0.001
	0.80		9.1	9.1	83		0.002	67	0.002
	0.90		23.4	13.8	323		0.007	83	0.002
	1.00		43.8	20.5	897		0.021	141	0.003
	1.10		64.2	27.1	1,743		0.040	271	0.006
	1.20		84.6	33.8	2,860		0.066	499	0.011
	1.30		105.0	40.5	4,250		0.098	852	0.020
	1.40		125.4	47.1	5,912		0.136	1,358	0.031
Floor	1.48		141.7	52.5	7,437		0.171	1,891	0.043
	1.50		141.9	52.6	7,468		0.171	2,040	0.047
	1.60		142.7	53.4	7,624		0.175	2,795	0.064
	1.70		143.5	54.2	7,782		0.179	3,565	0.082
	1.80		144.3	55.0	7,941		0.182	4,351	0.100
	1.90		145.1	55.8	8,101		0.186	5,153	0.118
	2.00		145.9	56.6	8,262		0.190	5,971	0.137
	2.10		146.7	57.4	8,425		0.193	6,805	0.156
	2.20		147.5	58.2	8,589		0.197	7,656	0.176
	2.30		148.3	59.0	8,754		0.201	8,523	0.196
Zone 1 (WQCV)	2.38		148.9	59.7	8,887		0.204	9,229	0.212
	2.40		149.1	59.8	8,920		0.205	9,407	0.216
	2.50		149.9	60.6	9,088		0.209	10,307	0.237
	2.60		150.7	61.4	9,257		0.213	11,225	0.258
	2.70		151.5	62.2	9,428		0.216	12,159	0.279
	2.80		152.3	63.0	9,599		0.220	13,110	0.301
	2.90		153.1	63.8	9,772		0.224	14,079	0.323
	3.00		153.9	64.6	9,946		0.228	15,065	0.346
	3.10		154.7	65.4	10,122		0.232	16,068	0.369
	3.20		155.5	66.2	10,299		0.236	17,089	0.392
	3.30		156.3	67.0	10,477		0.241	18,128	0.416
	3.40		157.1	67.8	10,656		0.245	19,184	0.440
	3.50		157.9	68.6	10,836		0.249	20,259	0.465
	3.60		158.7	69.4	11,018		0.253	21,352	0.490
	3.70		159.5	70.2	11,201		0.257	22,463	0.516
	3.80		160.3	71.0	11,386		0.261	23,592	0.542
	3.90		161.1	71.8	11,572		0.266	24,740	0.568
	4.00		161.9	72.6	11,759		0.270	25,906	0.595
Zone 2 (EURV)	4.04		162.2	72.9	11,834		0.272	26,378	0.606
	4.10		162.7	73.4	11,947		0.274	27,092	0.622
	4.20		163.5	74.2	12,136		0.279	28,296	0.650
	4.30		164.3	75.0	12,327		0.283	29,519	0.678
	4.40		165.1	75.8	12,519		0.287	30,761	0.706
	4.50		165.9	76.6	12,713		0.292	32,023	0.735
	4.60		166.7	77.4	12,907		0.296	33,304	0.765
	4.70		167.5	78.2	13,103		0.301	34,604	0.794
	4.80		168.3	79.0	13,300		0.305	35,925	0.825
	4.90		169.1	79.8	13,499		0.310	37,265	0.855
Zone 3 (100-year)	5.00		169.9	80.6	13,699		0.314	38,624	0.887
	5.10		170.7	81.4	13,900		0.319	40,004	0.918
	5.20		171.5	82.2	14,102		0.324	41,404	0.951
	5.30		172.3	83.0	14,306		0.328	42,825	0.983
	5.40		173.1	83.8	14,511		0.333	44,266	1.016
	5.50		173.9	84.6	14,717		0.338	45,727	1.050
	5.60		174.7	85.4	14,924		0.343	47,209	1.084
	5.70		175.5	86.2	15,133		0.347	48,712	1.118
	5.80		176.3	87.0	15,343		0.352	50,236	1.153
	5.90		177.1	87.8	15,554		0.357	51,781	1.189
	6.00		177.9	88.6	15,767		0.362	53,347	1.225
	6.10		178.7	89.4	15,981		0.367	54,934	1.261
	6.20		179.5	90.2	16,196		0.372	56,543	1.298
	6.30		180.3	91.0	16,412		0.377	58,173	1.335
	6.40		181.1	91.8	16,630		0.382	59,825	1.373
	6.50		181.9	92.6	16,849		0.387	61,499	1.412
	6.60		182.7	93.4	17,069		0.392	63,195	1.451
	6.70		183.5	94.2	17,291		0.397	64,913	1.490
	6.80		184.3	95.0	17,514		0.402	66,653	1.530
	6.90		185.1	95.8	17,738		0.407	68,416	1.571
	7.00		185.9	96.6	17,963		0.412	70,201	1.612
	7.10		186.7	97.4	18,190		0.418	72,009	1.653
	7.20		187.5	98.2	18,418		0.423	73,839	1.695
	7.30		188.3	99.0	18,647		0.428	75,692	1.738
	7.40		189.1	99.8	18,877		0.433	77,568	1.781
	7.50		189.9	100.6	19,109		0.439	79,468	1.824
	7.60		190.7	101.4	19,342		0.444	81,390	1.868
	7.70		191.5	102.2	19,577		0.449	83,336	1.913
	7.80		192.3	103.0	19,812		0.455	85,306	1.958
	7.90		193.1	103.8	20,049		0.460	87,299	2.004
	8.00		193.9	104.6	20,287		0.466	89,316	2.050
	8.10		194.7	105.4	20,527		0.471	91,356	2.097
	8.20		195.5	106.2	20,768		0.477	93,421	2.145
	8.30		196.3	107.0	21,010		0.482	95,510	2.193
	8.40		197.1	107.8	21,253		0.488	97,623	2.241
	8.50		197.9	108.6	21,497		0.494	99,760	2.290
	8.60		198.7	109.4	21,743		0.499	101,922	2.340
	8.70		199.5	110.2	21,990		0.505	104,109	2.390
	8.80		200.3	111.0	22,239		0.511	106,321	2.441
	8.90		201.1	111.8	22,489		0.516	108,557	2.492
	9.00		201.9	112.6	22,740		0.522	110,818	2.544
	9.10		202.7	113.4	22,992		0.528	113,105	2.597
	9.20		203.5	114.2	23,245		0.534	115,417	2.650
	9.30		204.3	115.0	23,500		0.539	117,754	2.703
	9.40		205.1	115.8	23,756		0.545	120,117	2.758
	9.50		205.9	116.6	24,014		0.551	122,505	2.812
	9.60		206.7	117.4	24,272		0.557	124,920	2.868
	9.70		207.5	118.2	24,532		0.563	127,360	2.924

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

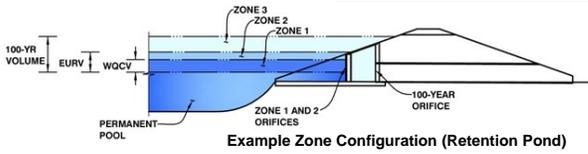
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-1 (NW Commercial Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.38	0.211	Orifice Plate
Zone 2 (EURV)	4.04	0.394	Circular Orifice
Zone 3 (100-year)	5.00	0.281	Weir&Pipe (Restrict)
Total (all zones)		0.885	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 15/16 inch)

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.79	1.59					
Orifice Area (sq. inches)	0.73	0.73	0.73					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.38	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.04	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	1.23	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.01	N/A	ft ²
Vertical Orifice Centroid =	0.05	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	4.04	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H _i =	4.04	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	22.14	N/A	
Overflow Gate Open Area w/o Debris =	16.80	N/A	ft ²
Overflow Gate Open Area w/ Debris =	8.40	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	8.00	N/A	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.76	N/A	ft ²
Outlet Orifice Centroid =	0.39	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.46	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	4.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	7.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.79	feet
Stage at Top of Freeboard =	6.29	feet
Basin Area at Top of Freeboard =	0.38	acres
Basin Volume at Top of Freeboard =	1.33	acre-ft

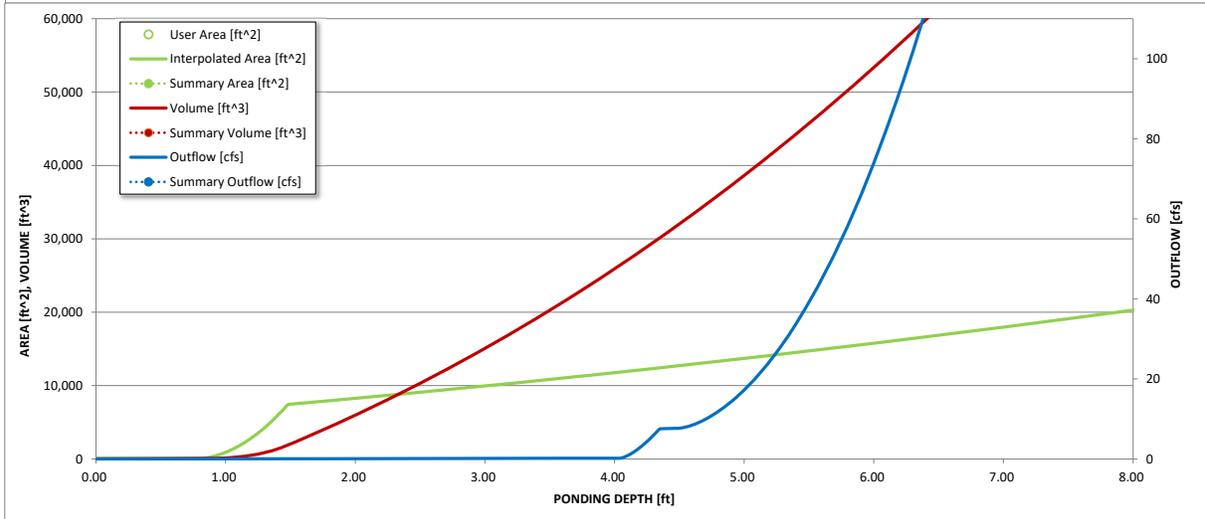
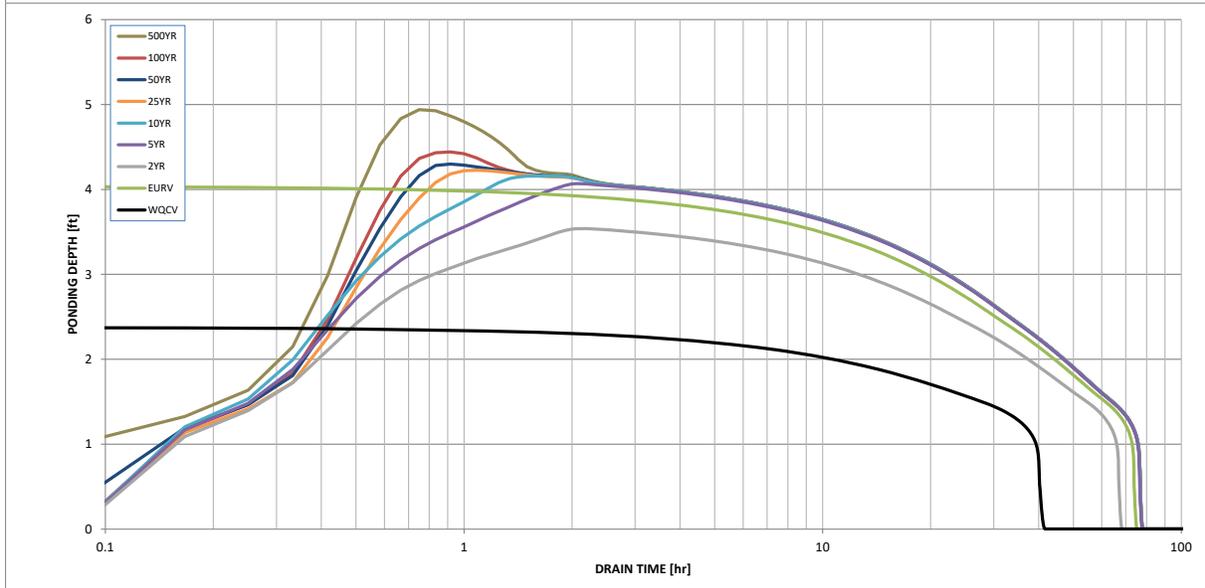
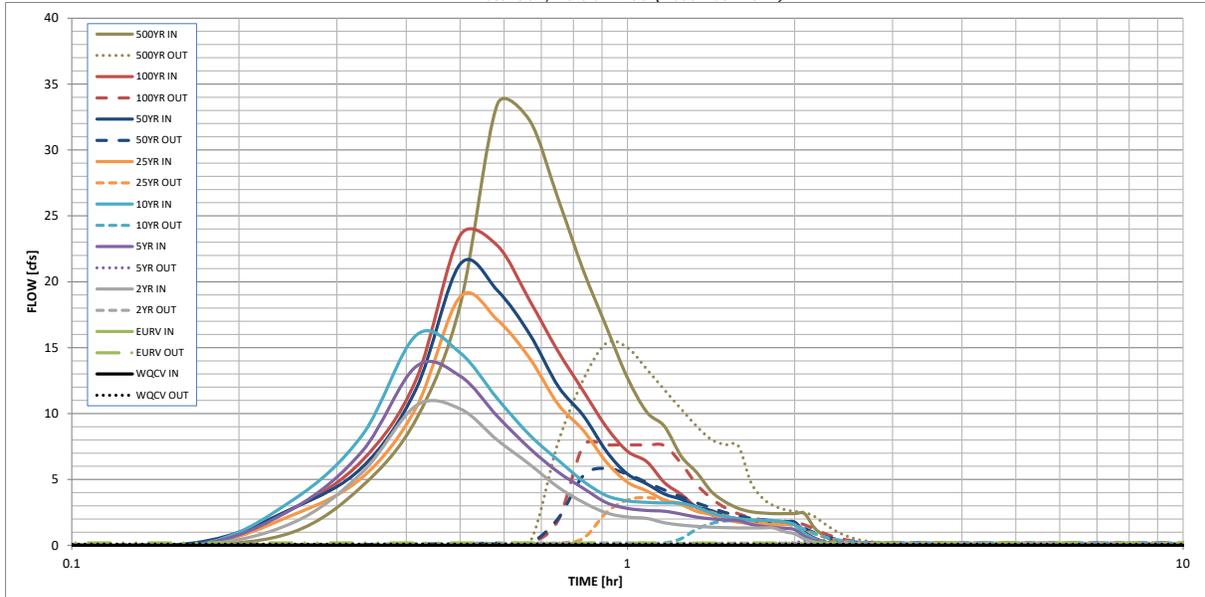
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.211	0.605	0.498	0.643	0.760	0.880	0.998	1.127	1.615
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.498	0.643	0.760	0.880	0.998	1.127	1.615
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.8	2.1	3.2	5.6	7.0	8.8	14.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.8	2.1	3.2	5.6	7.0	8.8	14.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.14	0.38	0.56	0.99	1.24	1.55	2.58
Peak Inflow Q (cfs) =	N/A	N/A	10.6	13.6	15.9	18.8	21.3	23.5	33.5
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.4	1.9	3.6	5.8	7.6	15.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.6	0.6	0.8	0.9	1.1
Structure Controlling Flow =	Vertical Orifice 1	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.1	0.2	0.3	0.4	0.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	69	63	71	70	69	68	68	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	66	75	75	74	74	73	72
Maximum Ponding Depth (ft) =	2.38	4.04	3.54	4.07	4.16	4.22	4.30	4.44	4.94
Area at Maximum Ponding Depth (acres) =	0.20	0.27	0.25	0.27	0.28	0.28	0.28	0.29	0.31
Maximum Volume Stored (acre-ft) =	0.212	0.606	0.473	0.611	0.636	0.655	0.675	0.718	0.865

DETENTION BASIN OUTLET STRUCTURE DESIGN

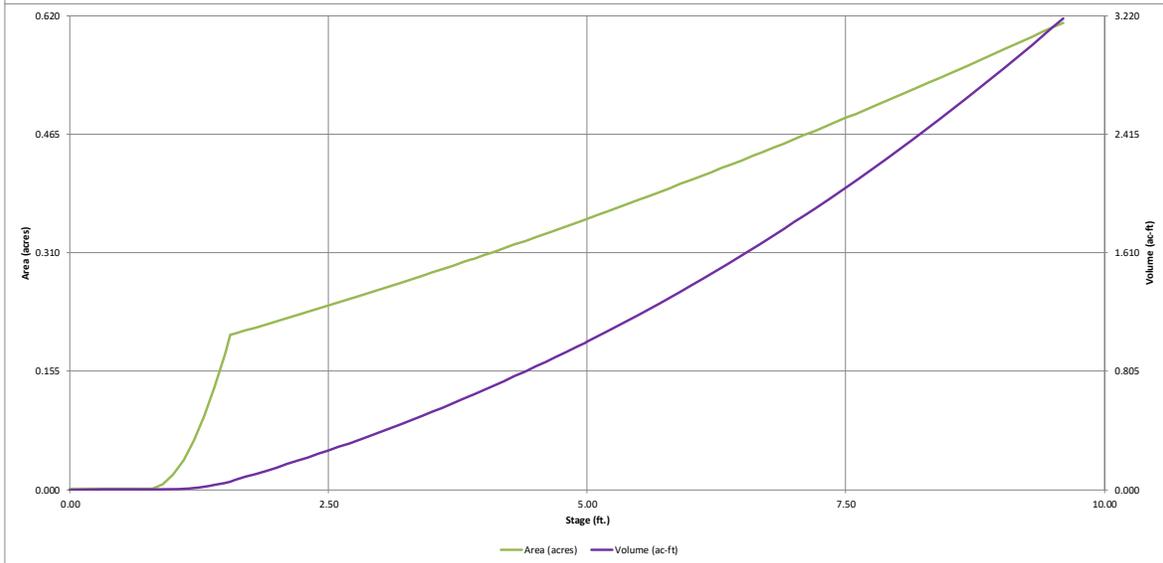
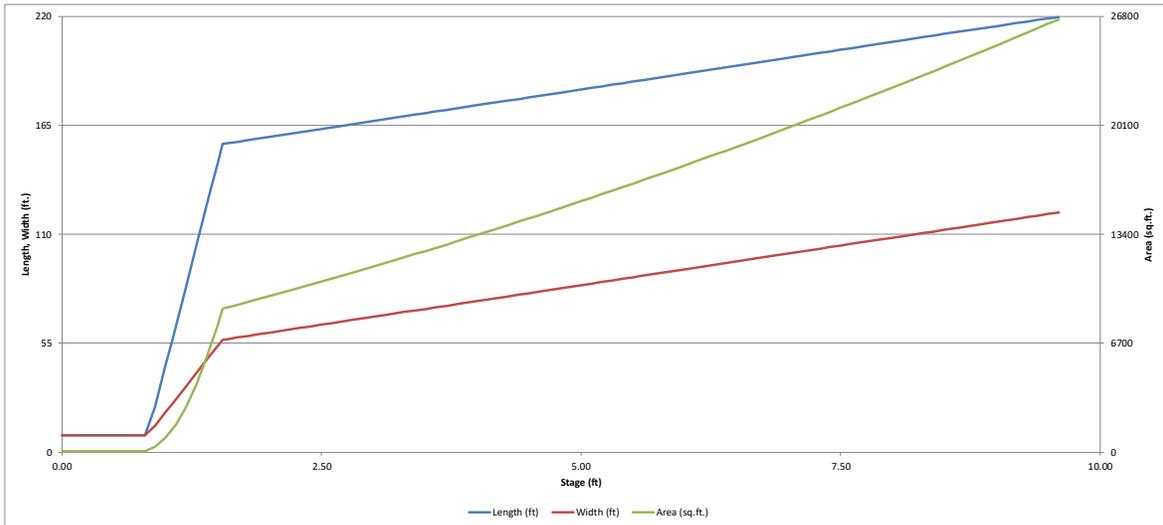
MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

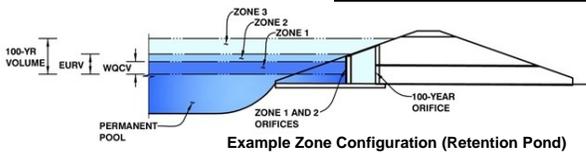
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: **Singer Ranch**
Basin ID: **DF-2 (NW Multi-Family Pond)**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.18	0.189	Orifice Plate
Zone 2 (EURV)	3.87	0.445	Circular Orifice
Zone 3 (100-year)	4.98	0.364	Weir&Pipe (Restrict)
Total (all zones)		0.998	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.18	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	8.70	inches
Orifice Plate: Orifice Area per Row =	0.64	sq. inches (diameter = 7/8 inch)

Calculated Parameters for Plate

WQ Orifice Area per Row =	4.444E-03	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.73	1.45					
Orifice Area (sq. inches)	0.64	0.64	0.64					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.18	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.87	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	1.89	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.02	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.87	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H ₁ =	3.87	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	12.03	N/A	
Overflow Gate Open Area w/o Debris =	16.80	N/A	ft ²
Overflow Gate Open Area w/ Debris =	8.40	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	10.95		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	1.40	N/A	ft ²
Outlet Orifice Centroid =	0.53	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.48	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	4.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	10.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.86	feet
Stage at Top of Freeboard =	6.66	feet
Basin Area at Top of Freeboard =	0.44	acres
Basin Volume at Top of Freeboard =	1.66	acre-ft

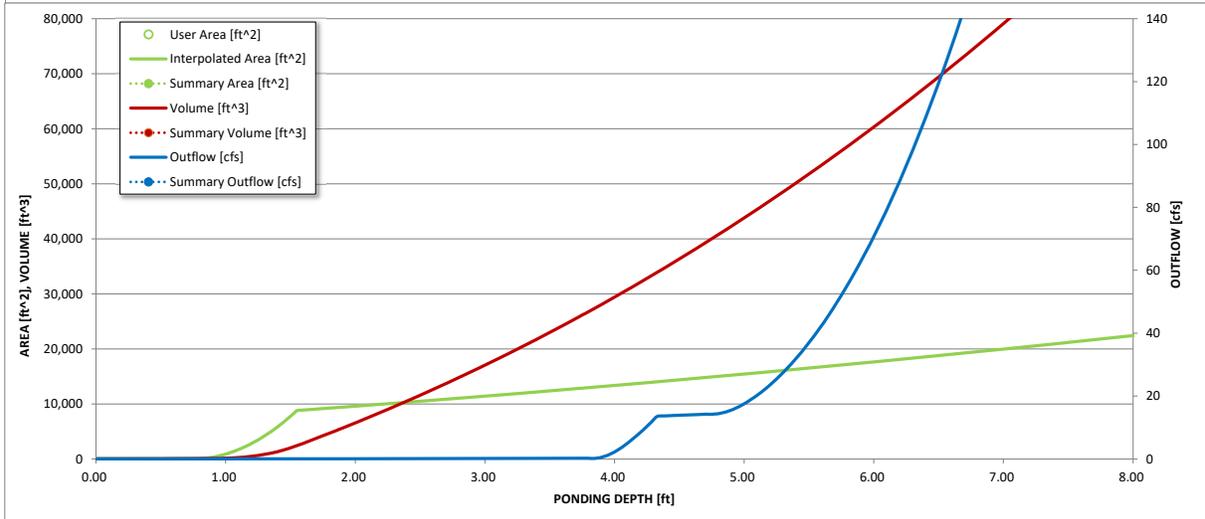
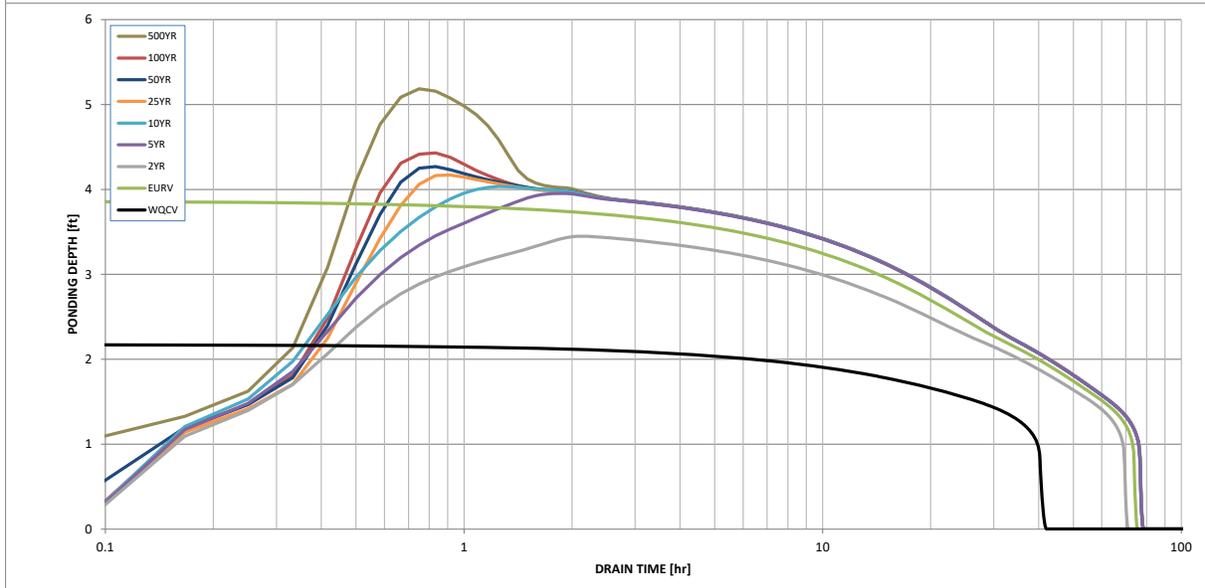
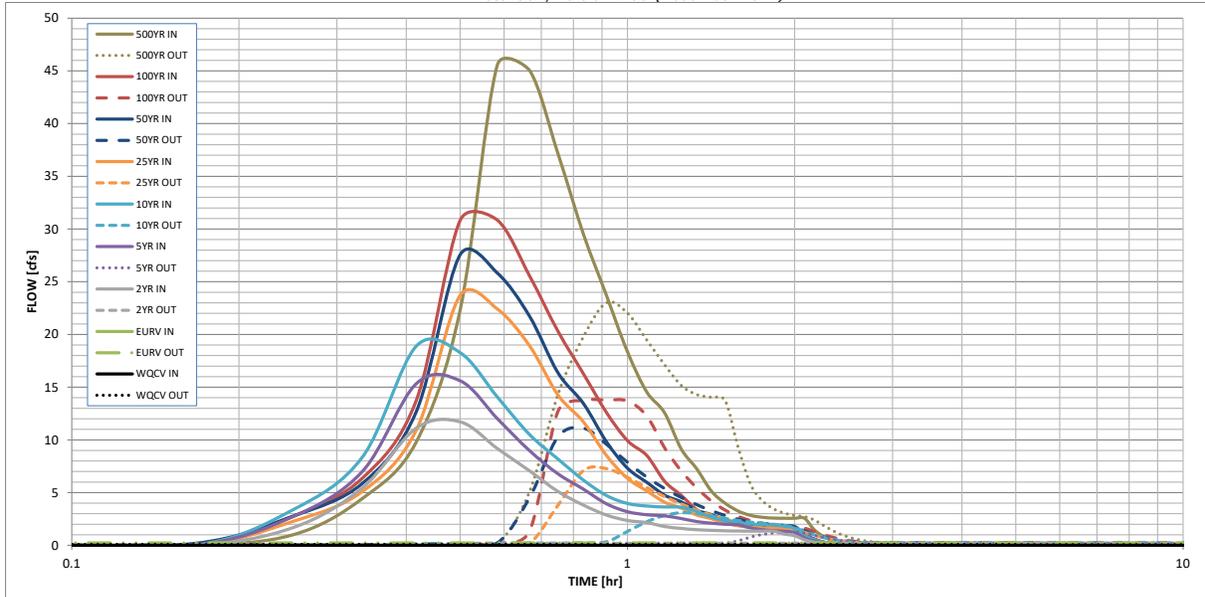
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.189	0.634	0.542	0.730	0.889	1.077	1.244	1.442	2.147
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.542	0.730	0.889	1.077	1.244	1.442	2.147
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.2	3.4	5.0	8.8	11.0	13.8	22.9
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.15	0.41	0.61	1.07	1.34	1.67	2.77
Peak Inflow Q (cfs) =	N/A	N/A	11.7	15.6	18.9	23.7	27.6	30.8	45.6
Peak Outflow Q (cfs) =	0.1	0.2	0.2	1.2	3.1	7.3	11.1	13.8	23.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.8	1.0	1.0	1.0
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.2	0.4	0.6	0.8	0.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	65	70	69	67	66	64	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	68	75	74	74	73	72	70
Maximum Ponding Depth (ft) =	2.18	3.87	3.45	3.95	4.03	4.17	4.27	4.43	5.18
Area at Maximum Ponding Depth (acres) =	0.23	0.30	0.28	0.30	0.31	0.31	0.32	0.33	0.36
Maximum Volume Stored (acre-ft) =	0.191	0.636	0.511	0.660	0.684	0.725	0.756	0.808	1.070

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)

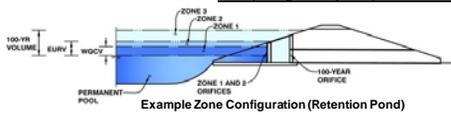


S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Defention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-3 (W Single Family Pond)



Example Zone Configuration (Retention Pond)

Watershed Information

Table with watershed parameters including Selected BMP Type (EDB), Watershed Area (61.51 acres), Watershed Length (2,720 ft), Watershed Slope (0.030 ft/ft), and various runoff and detention volumes.

Optional User Overrides

Table of optional user overrides for various parameters such as Initial Surcharge Volume (ISV) and Surcharge Volume Length (LSV).

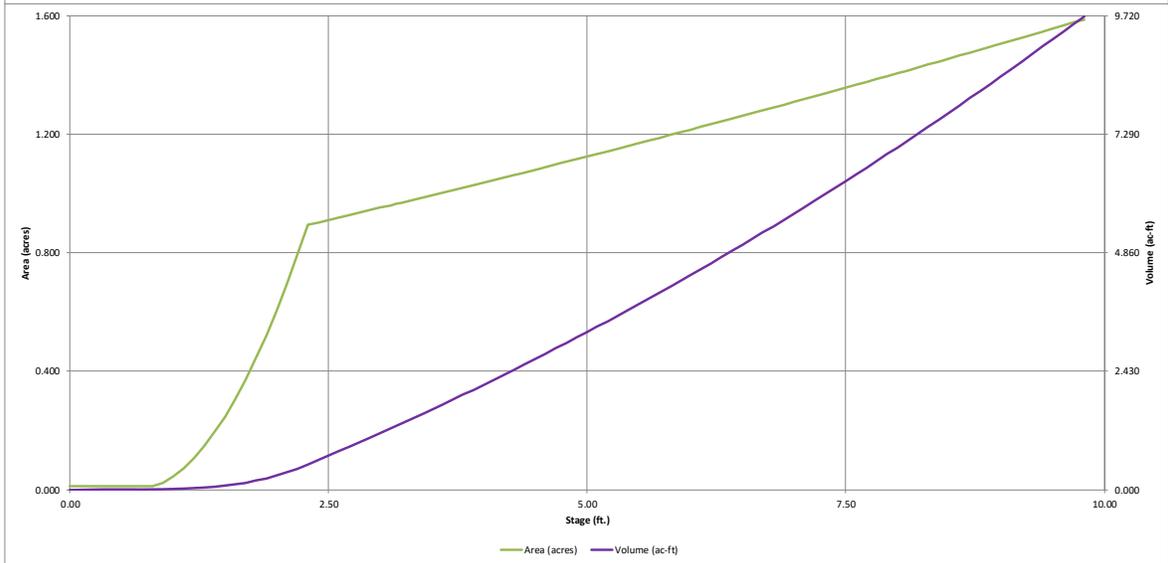
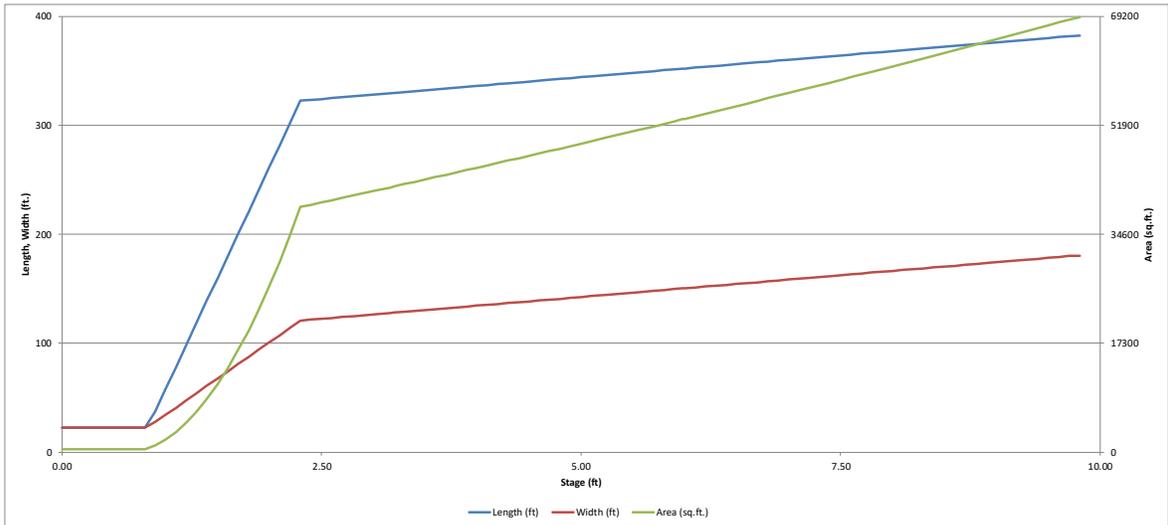
Define Zones and Basin Geometry

Table defining zone volumes (Zone 1, 2, 3), basin geometry (Initial Surcharge Area, Surcharge Volume Length, Depth of Basin Floor, etc.), and main basin geometry.

Main stage-storage table with columns: Depth Increment (ft), Stage (ft), Optional Override Stage (ft), Length (ft), Width (ft), Area (ft²), Optional Override Area (ft²), Area (acre), Volume (ft³), and Volume (ac-ft). Rows include Top of Micropool, ISV, and Zone 1, 2, and 3 data.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

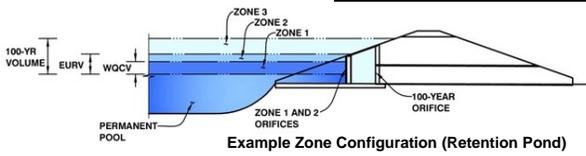
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: **Singer Ranch**
Basin ID: **DF-3 (W Single Family Pond)**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.16	1.303	Orifice Plate
Zone 2 (EURV)	5.98	3.062	Circular Orifice
Zone 3 (100-year)	8.00	2.650	Weir&Pipe (Restrict)
Total (all zones)		7.015	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	3.16	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	12.60	inches
Orifice Plate: Orifice Area per Row =	3.94	sq. inches (use rectangular openings)

Calculated Parameters for Plate

WQ Orifice Area per Row =	2.736E-02	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.05	2.11					
Orifice Area (sq. inches)	3.94	3.94	3.94					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	3.16	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.98	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	3.95	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.09	N/A	ft ²
Vertical Orifice Centroid =	0.16	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	6.10	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	7.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	7.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H _i =	6.10	N/A	feet
Overflow Weir Slope Length =	7.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	7.19	N/A	
Overflow Gate Open Area w/o Debris =	34.30	N/A	ft ²
Overflow Gate Open Area w/ Debris =	17.15	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	36.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	23.00	N/A	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	4.77	N/A	ft ²
Outlet Orifice Centroid =	1.08	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.85	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	9.15	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	58.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.96	feet
Stage at Top of Freeboard =	11.11	feet
Basin Area at Top of Freeboard =	1.73	acres
Basin Volume at Top of Freeboard =	11.88	acre-ft

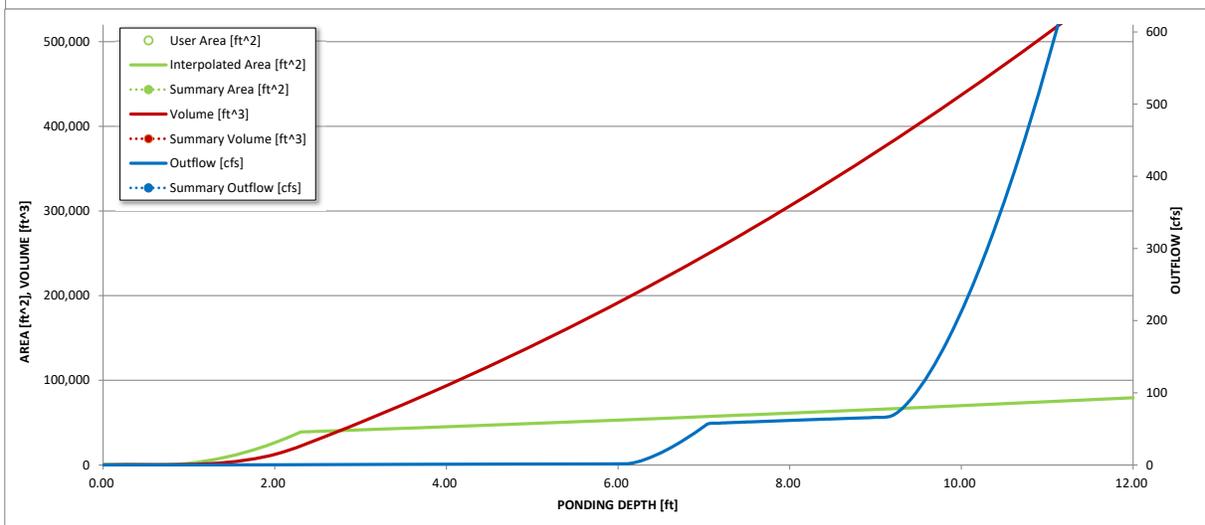
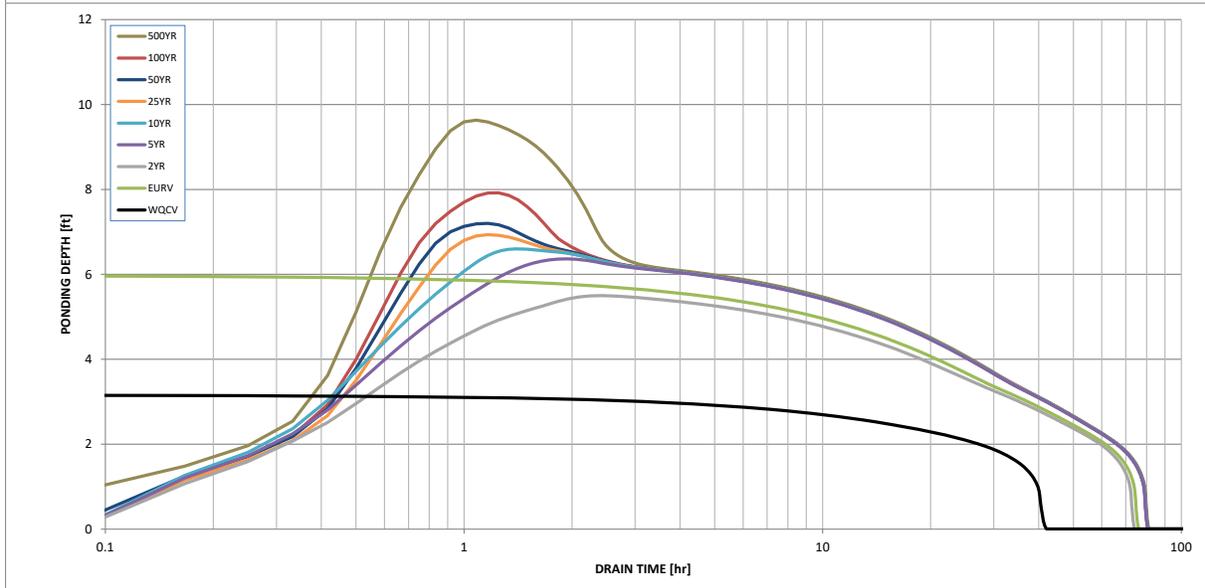
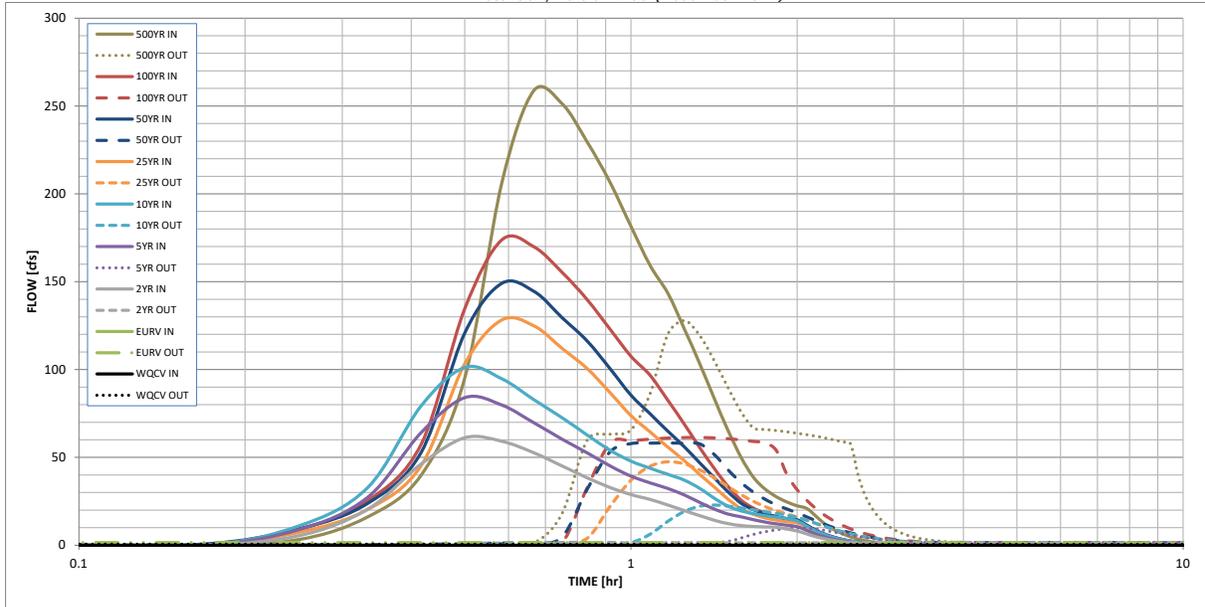
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	1.303	4.365	4.029	5.495	6.743	8.270	9.589	11.188	16.796
CUHP Runoff Volume (acre-ft) =	N/A	N/A	4.029	5.495	6.743	8.270	9.589	11.188	16.796
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	5.6	15.7	24.0	43.6	54.7	70.1	116.8
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	61.2	84.0	101.2	128.2	149.0	173.7	258.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.09	0.26	0.39	0.71	0.89	1.14	1.90
Peak Inflow Q (cfs) =	N/A	N/A	61.2	84.0	101.2	128.2	149.0	173.7	258.6
Peak Outflow Q (cfs) =	0.6	1.5	1.4	9.8	22.8	47.5	58.2	61.3	127.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.6	1.0	1.1	1.1	0.9	1.1
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.6	1.3	1.6	1.7	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	71	70	68	66	64	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	76	76	75	74	74	71
Maximum Ponding Depth (ft) =	3.16	5.98	5.50	6.36	6.60	6.93	7.20	7.92	9.63
Area at Maximum Ponding Depth (acres) =	0.97	1.21	1.17	1.25	1.27	1.30	1.33	1.40	1.57
Maximum Volume Stored (acre-ft) =	1.310	4.376	3.792	4.844	5.133	5.571	5.926	6.893	9.443

DETENTION BASIN OUTLET STRUCTURE DESIGN

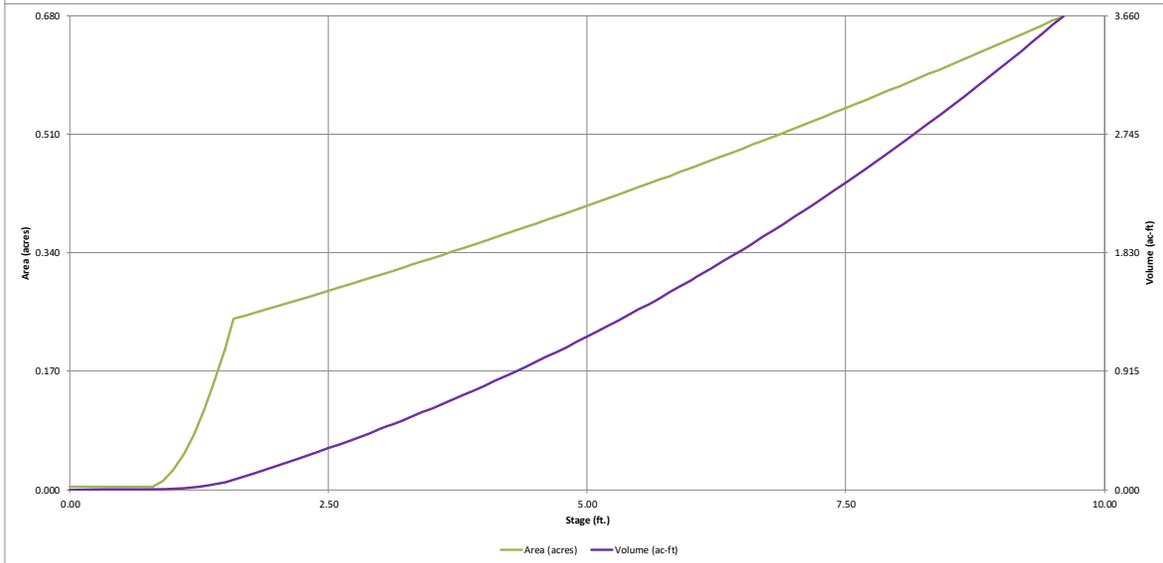
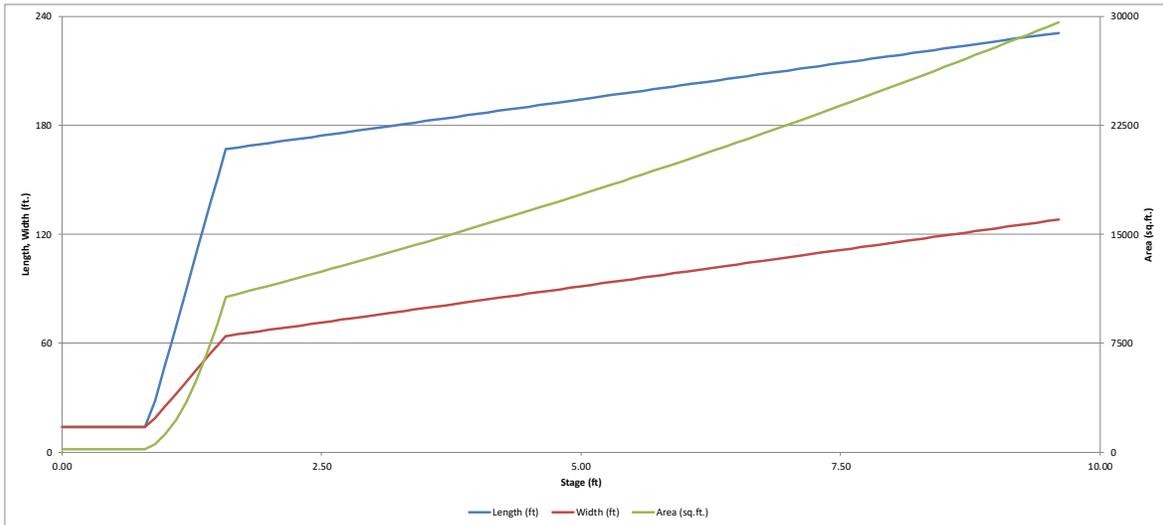
MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

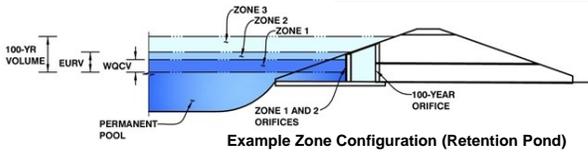
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-4 (SW Single Family Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.08	0.490	Orifice Plate
Zone 2 (EURV)	6.06	1.152	Circular Orifice
Zone 3 (100-year)	7.98	0.997	Weir&Pipe (Restrict)
Total (all zones)		2.639	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Calculated Parameters for Underdrain

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	1.139E-02	ft ²
Depth at top of Zone using Orifice Plate =	3.08	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	12.30	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	1.64	sq. inches (diameter = 1-7/16 inches)	Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.03	2.05					
Orifice Area (sq. inches)	1.64	1.64	1.64					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected		Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	3.08	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.02	ft ²
Depth at top of Zone using Vertical Orifice =	6.06	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.08	feet
Vertical Orifice Diameter =	1.97	N/A	inches			

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.25	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Gate Upper Edge, H ₁ =	6.25	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	Overflow Weir Slope Length =	4.00	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V	Gate Open Area / 100-yr Orifice Area =	10.16	N/A
Horiz. Length of Weir Sides =	4.00	N/A	feet	Overflow Gate Open Area w/o Debris =	16.80	ft ²
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area	Overflow Gate Open Area w/ Debris =	8.40	ft ²
Debris Clogging % =	50%	N/A	%			

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected		Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.65	ft ²
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.60	feet
Restrictor Plate Height Above Pipe Invert =	12.50		inches	Half-Central Angle of Restrictor Plate on Pipe =	1.61	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

Spillway Invert Stage =	7.80	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth =	0.89	feet
Spillway Crest Length =	19.00	feet	Stage at Top of Freeboard =	9.69	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.69	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	3.72	acre-ft

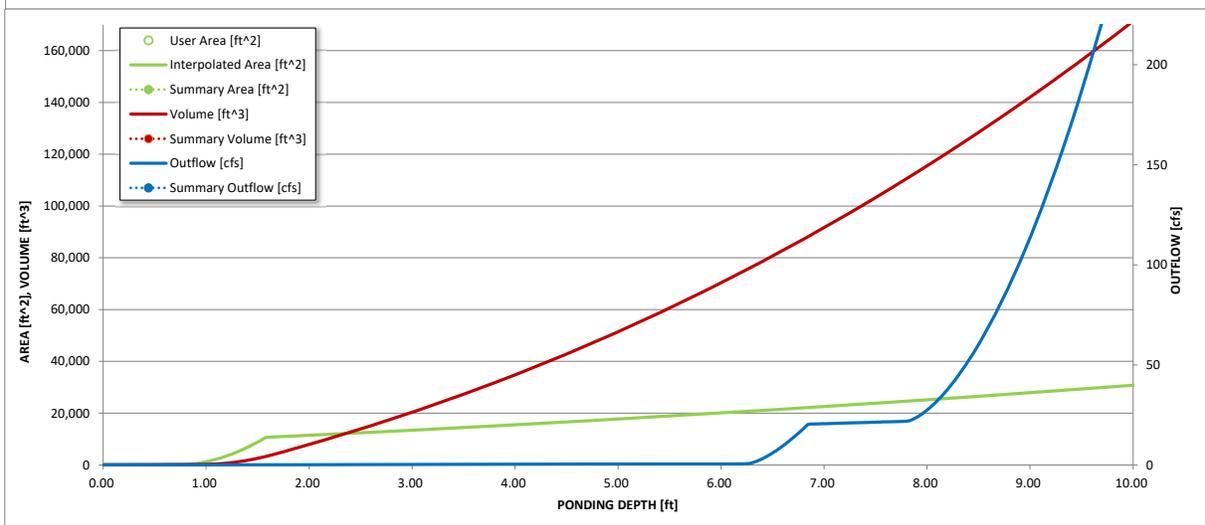
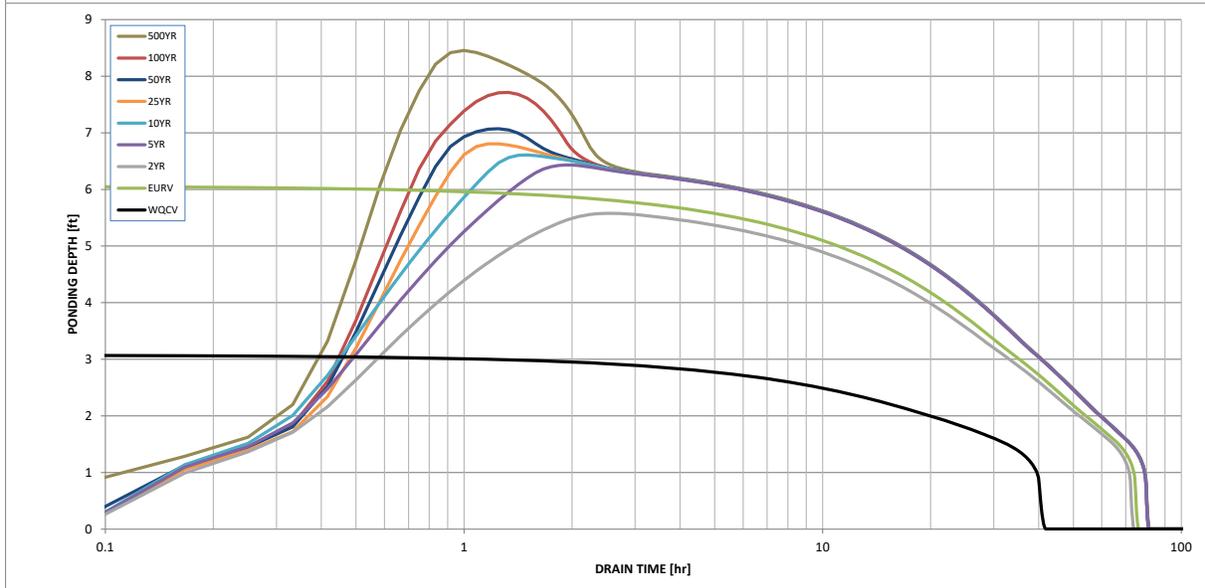
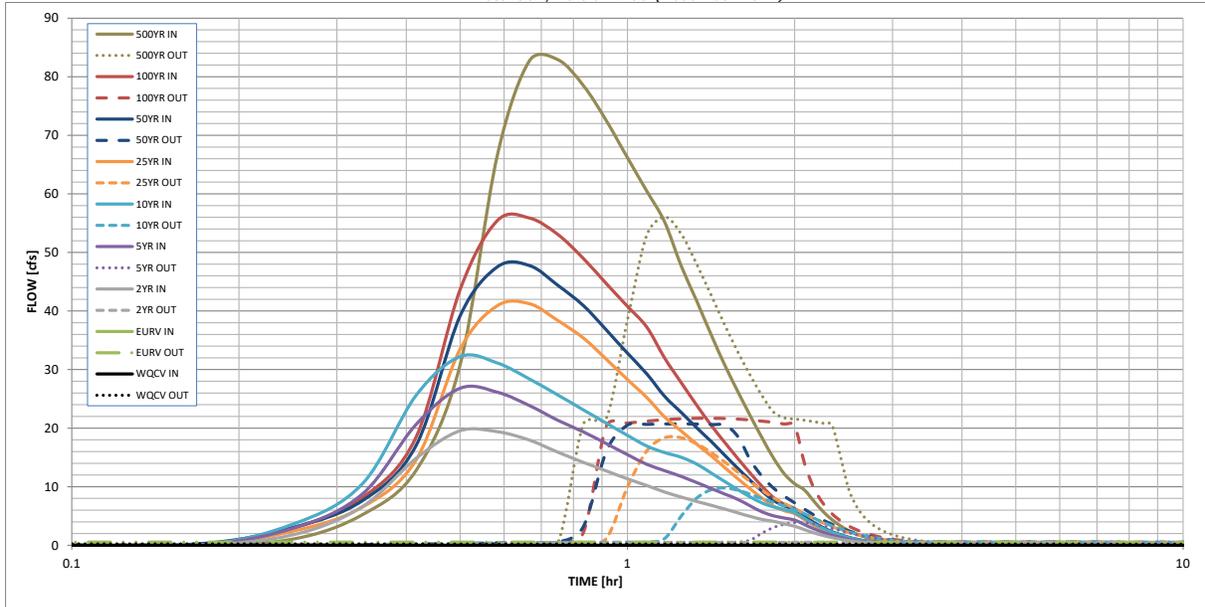
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.490	1.642	1.513	2.063	2.531	3.104	3.598	4.197	6.300
CUHP Runoff Volume (acre-ft) =	N/A	N/A	1.513	2.063	2.531	3.104	3.598	4.197	6.300
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.7	4.8	7.4	13.7	17.2	22.0	36.9
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.07	0.21	0.32	0.59	0.74	0.95	1.60
Peak Inflow Q (cfs) =	N/A	N/A	19.5	26.8	32.2	41.2	47.8	55.9	82.9
Peak Outflow Q (cfs) =	0.2	0.5	0.5	3.9	9.8	18.4	20.7	21.7	56.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.8	1.3	1.3	1.2	1.0	1.5
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.6	1.0	1.2	1.3	1.3
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	72	70	68	67	65	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	77	76	75	75	74	72
Maximum Ponding Depth (ft) =	3.08	6.06	5.58	6.43	6.61	6.80	7.07	7.71	8.45
Area at Maximum Ponding Depth (acres) =	0.31	0.46	0.44	0.49	0.49	0.51	0.52	0.56	0.61
Maximum Volume Stored (acre-ft) =	0.492	1.642	1.421	1.818	1.901	2.001	2.140	2.487	2.918

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)

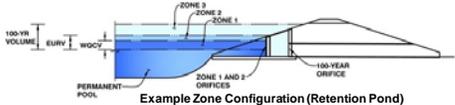


S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD- Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-5 (S Single Family & School Pond)



Example Zone Configuration (Retention Pond)

Watershed Information

- Selected BMP Type = EDB
Watershed Area = 57.67 acres
Watershed Length = 2.851 ft
Watershed Length to Centroid = 1.555 ft
Watershed Slope = 0.013 ft/ft
Watershed Imperviousness = 70.00% percent
Percentage Hydrologic Soil Group A = 0.0% percent
Percentage Hydrologic Soil Group B = 100.0% percent
Percentage Hydrologic Soil Groups C/D = 0.0% percent
Target WQC Drain Time = 40.0 hours
Location for 1-hr Rainfall Depths = User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Optional User Overrides

- Water Quality Capture Volume (WQC) = 1.322 acre-feet
Excess Urban Runoff Volume (EURV) = 4.433 acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) = 4.058 acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) = 5.472 acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) = 6.664 acre-feet
25-yr Runoff Volume (P1 = 2 in.) = 8.074 acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) = 9.321 acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) = 10.806 acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) = 16.089 acre-feet
Approximate 2-yr Detention Volume = 3.464 acre-feet
Approximate 5-yr Detention Volume = 4.616 acre-feet
Approximate 10-yr Detention Volume = 5.827 acre-feet
Approximate 25-yr Detention Volume = 6.261 acre-feet
Approximate 50-yr Detention Volume = 6.513 acre-feet
Approximate 100-yr Detention Volume = 6.977 acre-feet

Define Zones and Basin Geometry

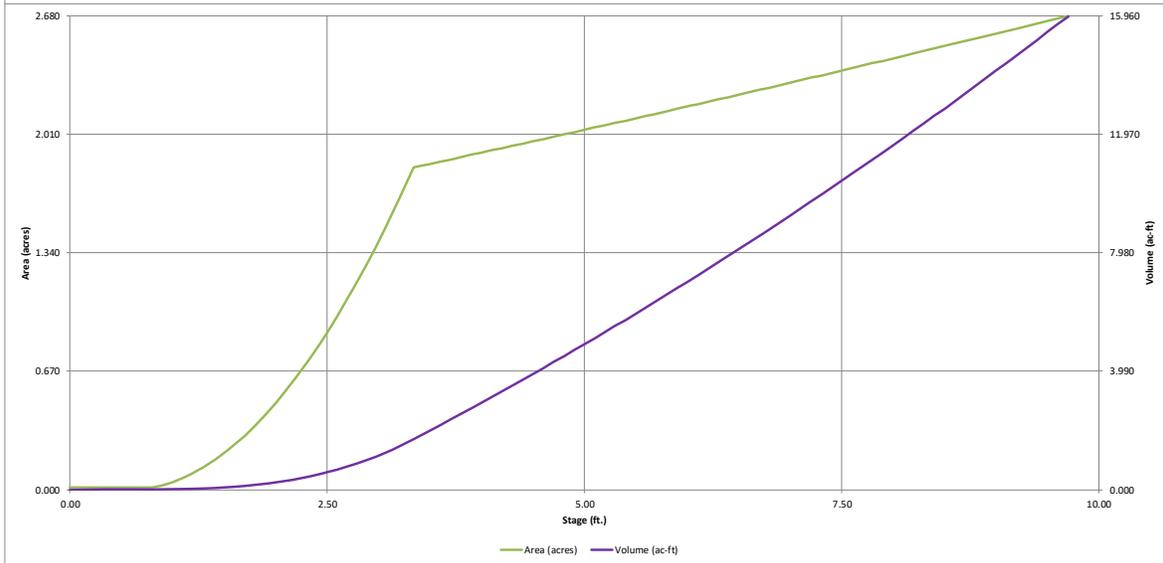
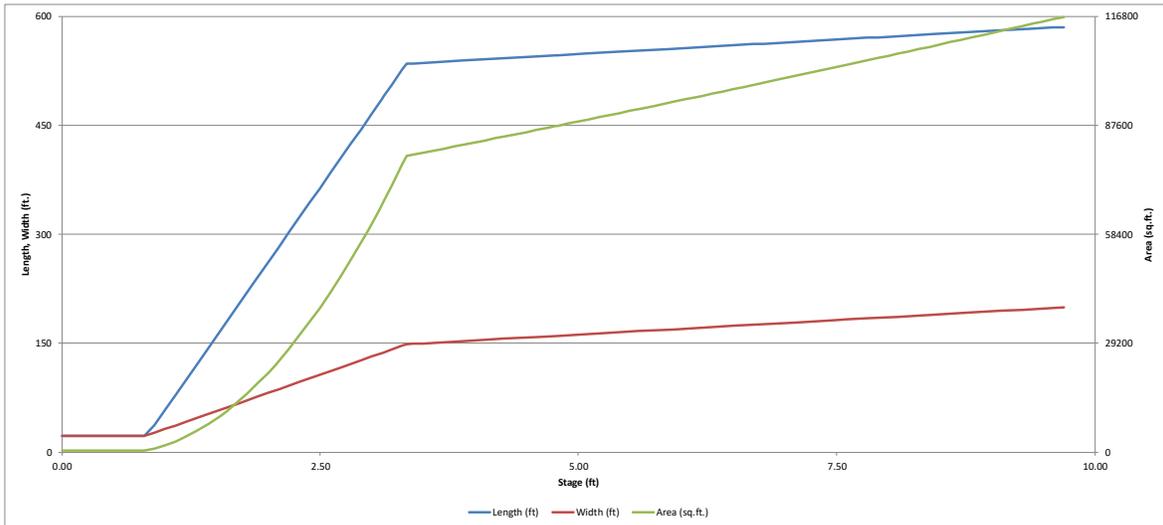
- Zone 1 Volume (WOCV) = 1.322 acre-feet
Zone 2 Volume (EURV - Zone 1) = 3.112 acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) = 2.544 acre-feet
Total Detention Basin Volume = 6.977 acre-feet
Initial Surcharge Volume (ISV) = 173 ft^3
Initial Surcharge Depth (ISD) = 0.33 ft
Total Available Detention Depth (Htotal) = 6.00 ft
Depth of Trickle Channel (Htr) = 0.50 ft
Slope of Trickle Channel (Str) = 0.005 ft/ft
Slopes of Main Basin Sides (Smain) = 4 ft:1
Basin Length-to-Width Ratio (RL/W) = 4

- Initial Surcharge Area (AISV) = 523 ft^2
Surcharge Volume Length (LISV) = 22.9 ft
Surcharge Volume Width (WISV) = 22.9 ft
Depth of Basin Floor (Hflood) = 2.51 ft
Length of Basin Floor (Lflood) = 534.9 ft
Width of Basin Floor (Wflood) = 148.4 ft
Area of Basin Floor (Aflood) = 79,370 ft^2
Volume of Basin Floor (Vflood) = 72,237 ft^3
Depth of Main Basin (Hmain) = 2.66 ft
Length of Main Basin (Lmain) = 556.2 ft
Width of Main Basin (Wmain) = 169.7 ft
Area of Main Basin (Amain) = 94,364 ft^2
Volume of Main Basin (Vmain) = 230,779 ft^3
Calculated Total Basin Volume (Vtotal) = 6.966 acre-feet

Table with 10 columns: Depth Increment, Stage - Storage Description, Stage (ft), Optional Override Stage (ft), Length (ft), Width (ft), Area (ft^2), Optional Override Area (ft^2), Area (acre), Volume (ft^3), Volume (ac-ft). Rows include Top of Micropool, ISV, Zone 1 (WOCV), Floor, Zone 2 (EURV), and Zone 3 (100-year).

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

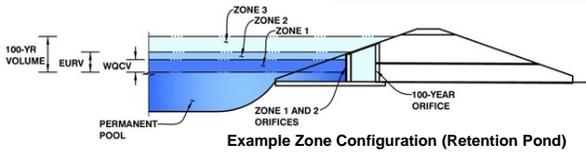
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-5 (S Single Family & School Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.12	1.322	Orifice Plate
Zone 2 (EURV)	4.78	3.112	Circular Orifice
Zone 3 (100-year)	6.00	2.544	Weir&Pipe (Restrict)
Total (all zones)		6.977	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Calculated Parameters for Underdrain

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	2.639E-02	ft ²
Depth at top of Zone using Orifice Plate =	3.12	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	12.50	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	3.80	sq. inches (use rectangular openings)	Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.04	2.08					
Orifice Area (sq. inches)	3.80	3.80	3.80					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected		Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	3.12	N/A	ft (relative to basin bottom at Stage = 0 ft)	0.18	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	4.78	N/A	ft (relative to basin bottom at Stage = 0 ft)	0.24	N/A	feet
Vertical Orifice Diameter =	5.72	N/A	inches			

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.79	N/A	ft (relative to basin bottom at Stage = 0 ft)	4.79	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V	5.84	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet	25.20	N/A	ft ²
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area	12.60	N/A	ft ²
Debris Clogging % =	50%	N/A	%			

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected		Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	4.32	N/A	ft ²
Outlet Pipe Diameter =	36.00	N/A	inches	1.00	N/A	feet
Restrictor Plate Height Above Pipe Invert =	21.15		inches	1.75	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

Spillway Invert Stage =	6.10	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth =	0.96	feet
Spillway Crest Length =	50.00	feet	Stage at Top of Freeboard =	8.06	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	2.45	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	11.72	acre-ft

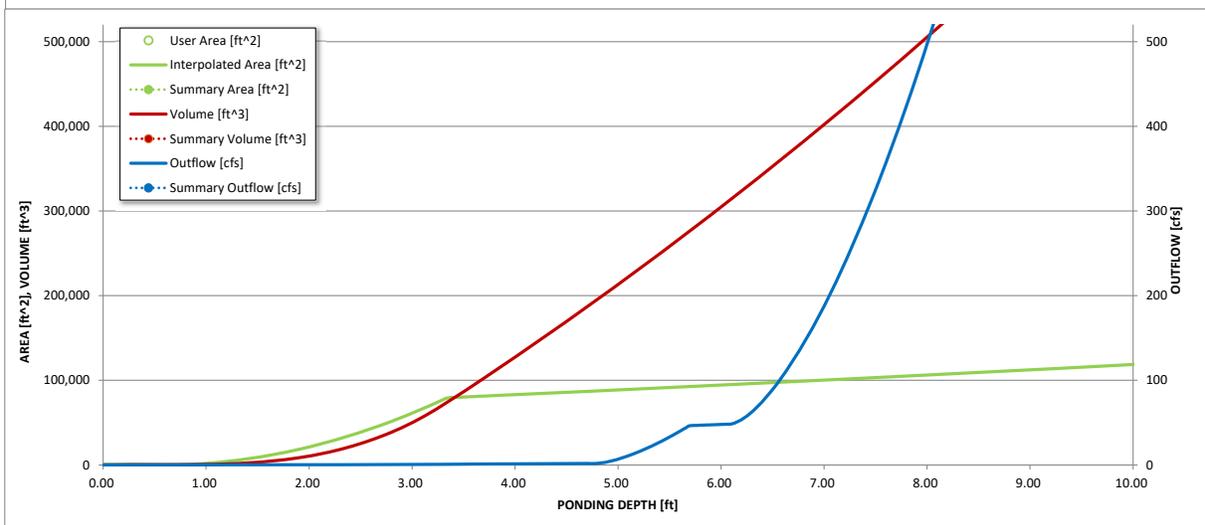
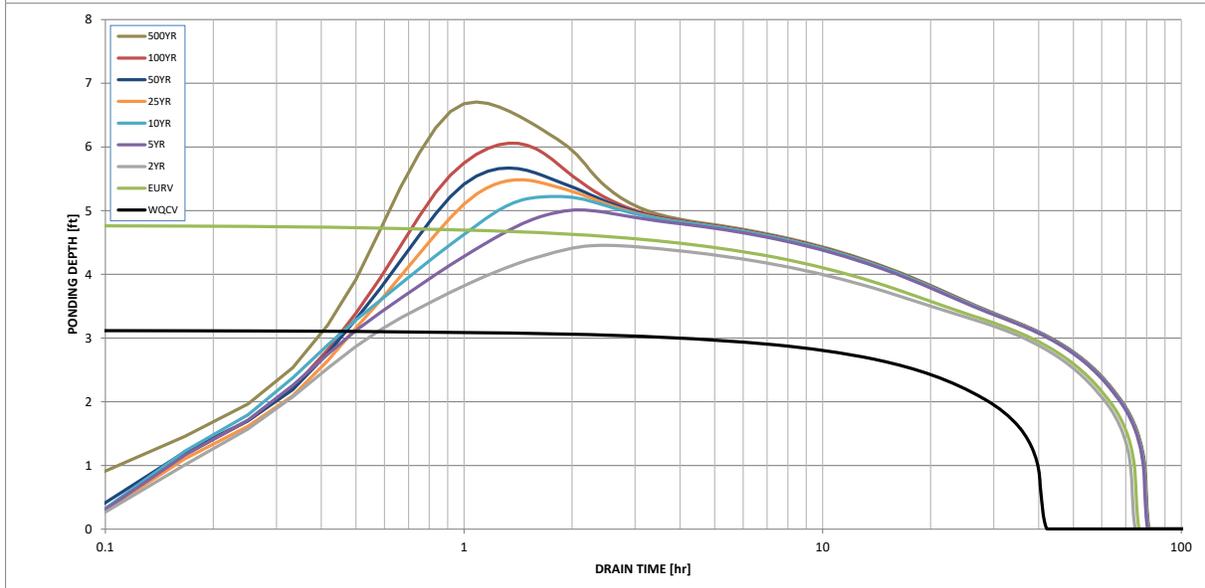
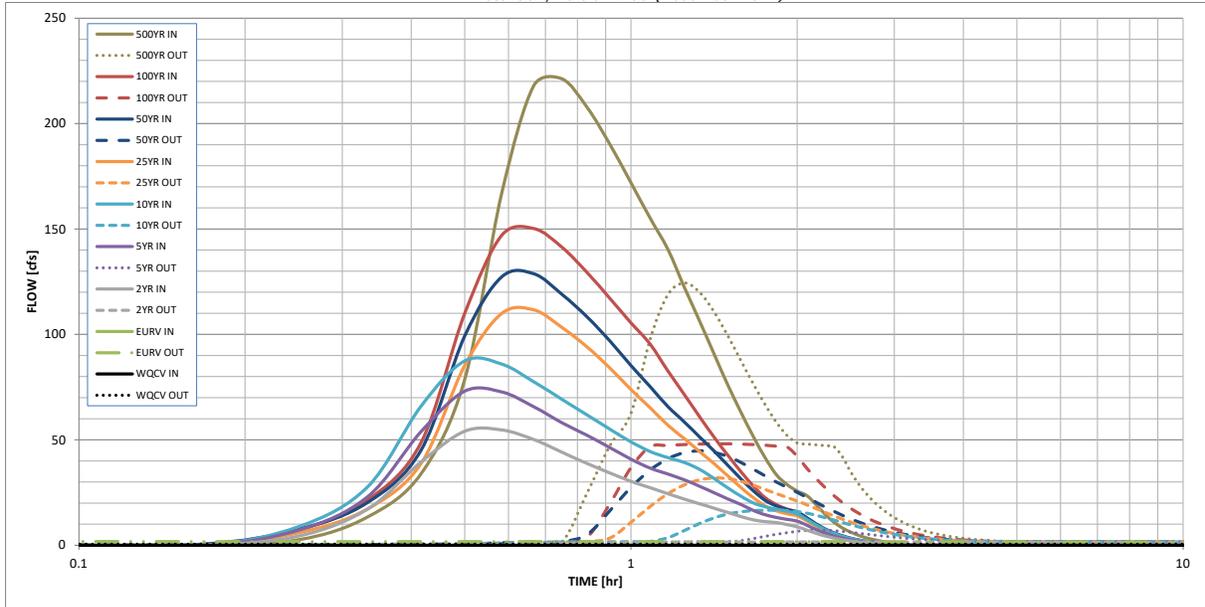
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	1.322	4.433	4.058	5.472	6.664	8.074	9.321	10.806	16.089
CUHP Runoff Volume (acre-ft) =	N/A	N/A	4.058	5.472	6.664	8.074	9.321	10.806	16.089
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	4.3	12.2	18.9	34.7	43.6	56.2	94.1
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.08	0.21	0.33	0.60	0.76	0.97	1.63
Peak Inflow Q (cfs) =	N/A	N/A	54.7	73.1	87.4	111.6	128.8	150.2	221.2
Peak Outflow Q (cfs) =	0.5	1.8	1.6	7.2	16.6	31.9	44.8	48.1	124.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.6	0.9	0.9	1.0	0.9	1.3
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.6	1.2	1.7	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	71	70	68	67	65	60
Time to Drain 99% of Inflow Volume (hours) =	40	72	71	76	76	75	74	74	72
Maximum Ponding Depth (ft) =	3.12	4.78	4.45	5.01	5.22	5.48	5.67	6.06	6.71
Area at Maximum Ponding Depth (acres) =	1.55	2.01	1.96	2.04	2.06	2.10	2.12	2.17	2.26
Maximum Volume Stored (acre-ft) =	1.325	4.450	3.795	4.915	5.345	5.886	6.266	7.103	8.544

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



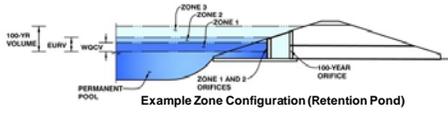
S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch

Basin ID: DF-6 (NE Commercial Pond)



Example Zone Configuration (Retention Pond)

Watershed Information

Table with watershed information: Selected BMP Type = EDB, Watershed Area = 5.08 acres, Watershed Length = 660 ft, Watershed Length to Centroid = 175 ft, Watershed Slope = 0.030 ft/ft, Watershed Imperviousness = 95.00% percent, Percentage Hydrologic Soil Group A = 0.0% percent, Percentage Hydrologic Soil Group B = 100.0% percent, Percentage Hydrologic Soil Groups C/D = 0.0% percent, Target WQC Drain Time = 40.0 hours, Location for 1-hr Rainfall Depths = User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Table with Optional User Overrides for WQC, EURV, and runoff volumes. Includes columns for Runoff Volume (P1), Runoff Volume (P2), Runoff Volume (P3), Runoff Volume (P4), Runoff Volume (P5), Runoff Volume (P6), Runoff Volume (P7), Runoff Volume (P8), Runoff Volume (P9), Runoff Volume (P10), Runoff Volume (P11), Runoff Volume (P12), Runoff Volume (P13), Runoff Volume (P14), Runoff Volume (P15), Runoff Volume (P16), Runoff Volume (P17), Runoff Volume (P18), Runoff Volume (P19), Runoff Volume (P20).

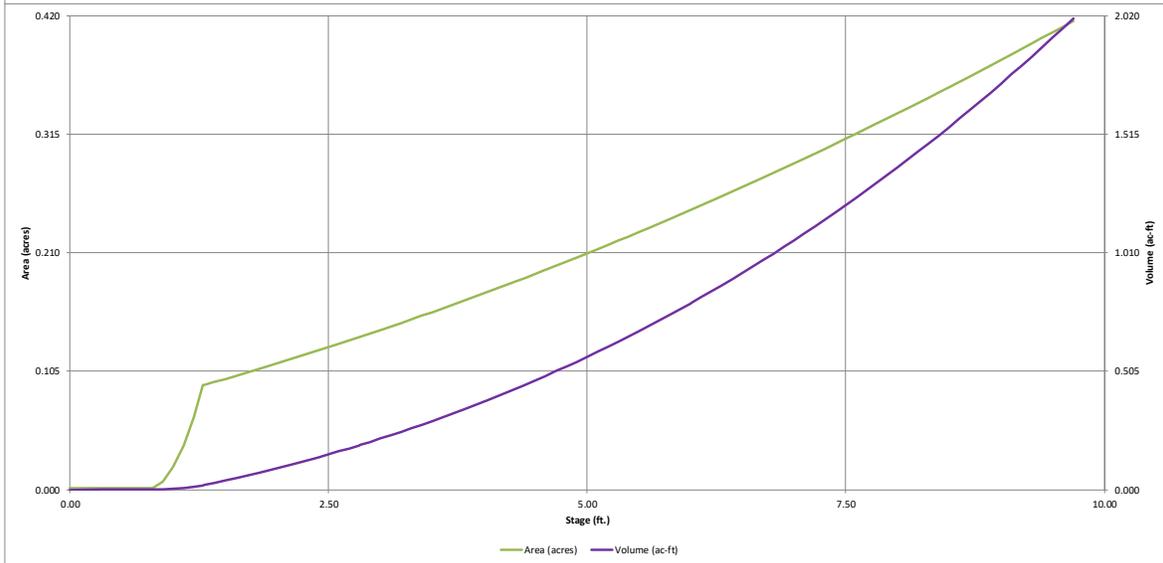
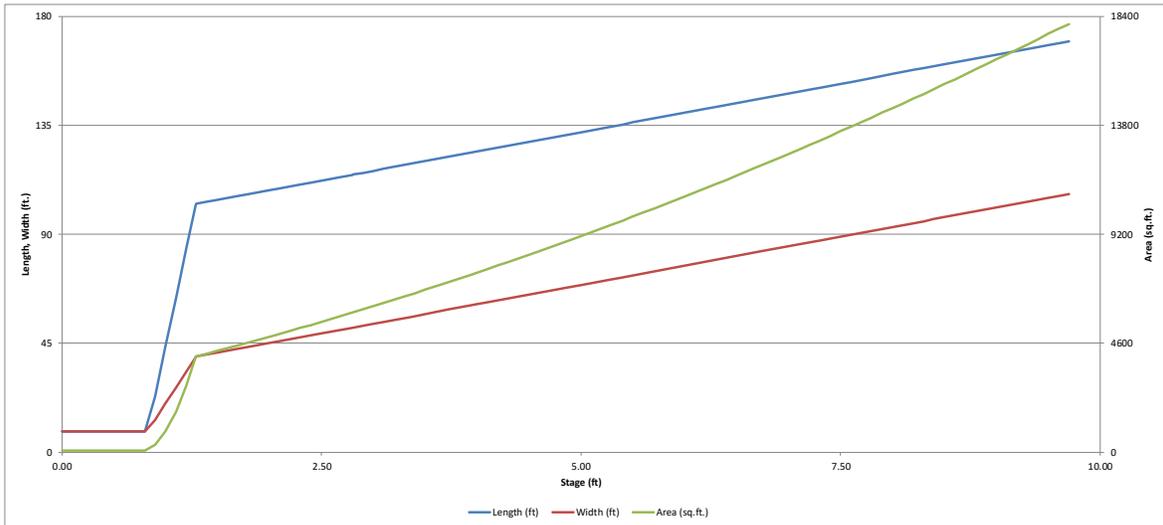
Define Zones and Basin Geometry

Table with basin geometry parameters: Zone 1 Volume (WQC), Zone 2 Volume (EURV - Zone 1), Zone 3 Volume (100-year - Zones 1 & 2), Total Detention Basin Volume, Initial Surge Volume (ISV), Initial Surge Depth (ISD), Total Available Detention Depth (Htotal), Depth of Trickle Channel (Htc), Slope of Trickle Channel (S1c), Slopes of Main Basin Sides (Smain), Basin Length-to-Width Ratio (RLW), Initial Surge Area (AISV), Surge Volume Length (LISV), Surge Volume Width (WISV), Depth of Basin Floor (Hflood), Length of Basin Floor (Lfllood), Width of Basin Floor (Wfllood), Area of Basin Floor (Afllood), Volume of Basin Floor (Vfllood), Depth of Main Basin (HMAN), Length of Main Basin (LMAN), Width of Main Basin (WMAN), Area of Main Basin (AMAN), Volume of Main Basin (VMAN), Calculated Total Basin Volume (Vtotal)

Main table with columns: Depth Increment = 0.10 ft, Stage - Storage Description, Stage (ft), Optional Override Stage (ft), Length (ft), Width (ft), Area (ft^2), Optional Override Area (ft^2), Area (acre), Volume (ft^3), Volume (ac-ft). Rows include Top of Micropool, ISV, Floor, Zone 1 (WQC), Zone 2 (EURV), Zone 3 (100-year).

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

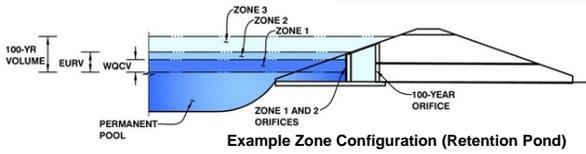
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: **Singer Ranch**
Basin ID: **DF-6 (NE Commercial Pond)**



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.81	0.189	Orifice Plate
Zone 2 (EURV)	4.90	0.354	Circular Orifice
Zone 3 (100-year)	6.01	0.252	Weir&Pipe (Restrict)
Total (all zones)		0.795	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.81	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	11.20	inches
Orifice Plate: Orifice Area per Row =	0.66	sq. inches (diameter = 7/8 inch)

Calculated Parameters for Plate

WQ Orifice Area per Row =	4.583E-03	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.94	1.87					
Orifice Area (sq. inches)	0.66	0.66	0.66					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.81	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.90	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	0.84	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.00	N/A	ft ²
Vertical Orifice Centroid =	0.04	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.90	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H ₁ =	4.90	N/A	feet
Overflow Weir Slope Length =	4.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	22.89	N/A	
Overflow Gate Open Area w/o Debris =	16.80	N/A	ft ²
Overflow Gate Open Area w/ Debris =	8.40	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	7.80		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.73	N/A	ft ²
Outlet Orifice Centroid =	0.38	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.44	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.30	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	8.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.79	feet
Stage at Top of Freeboard =	7.09	feet
Basin Area at Top of Freeboard =	0.29	acres
Basin Volume at Top of Freeboard =	1.09	acre-ft

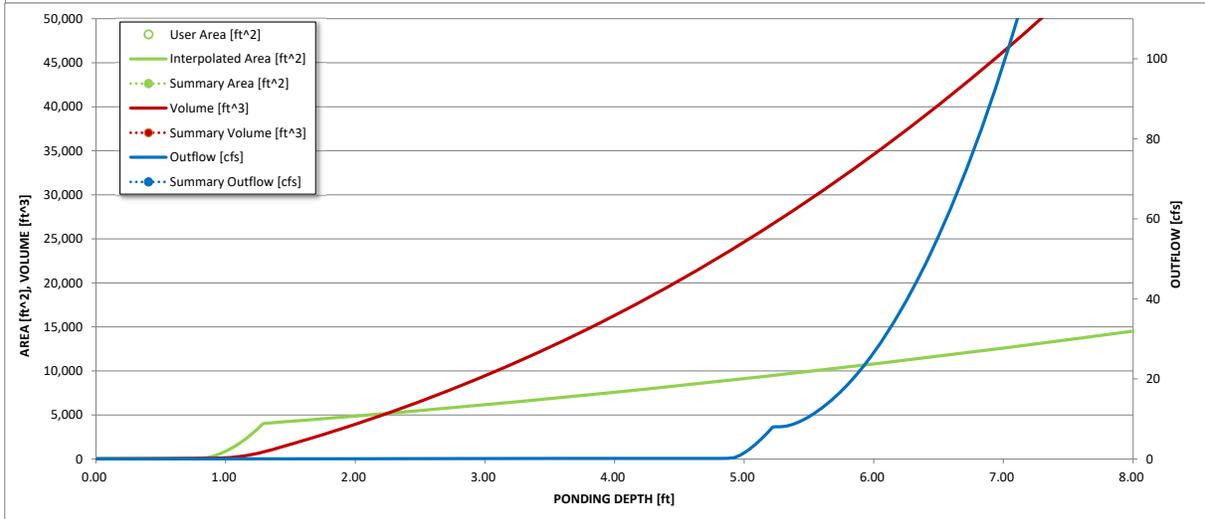
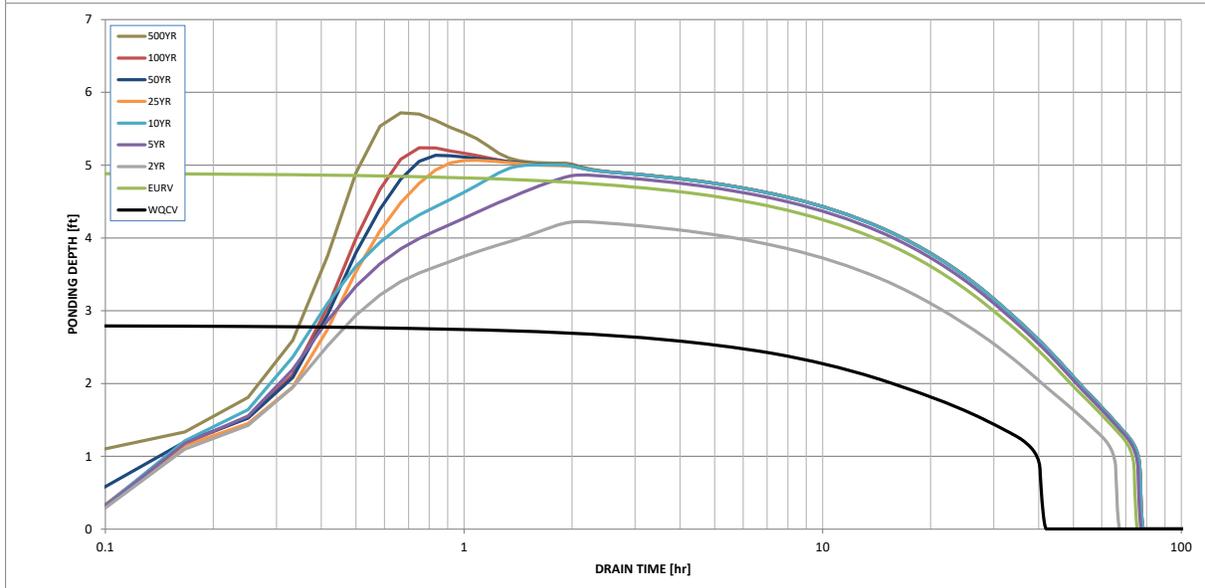
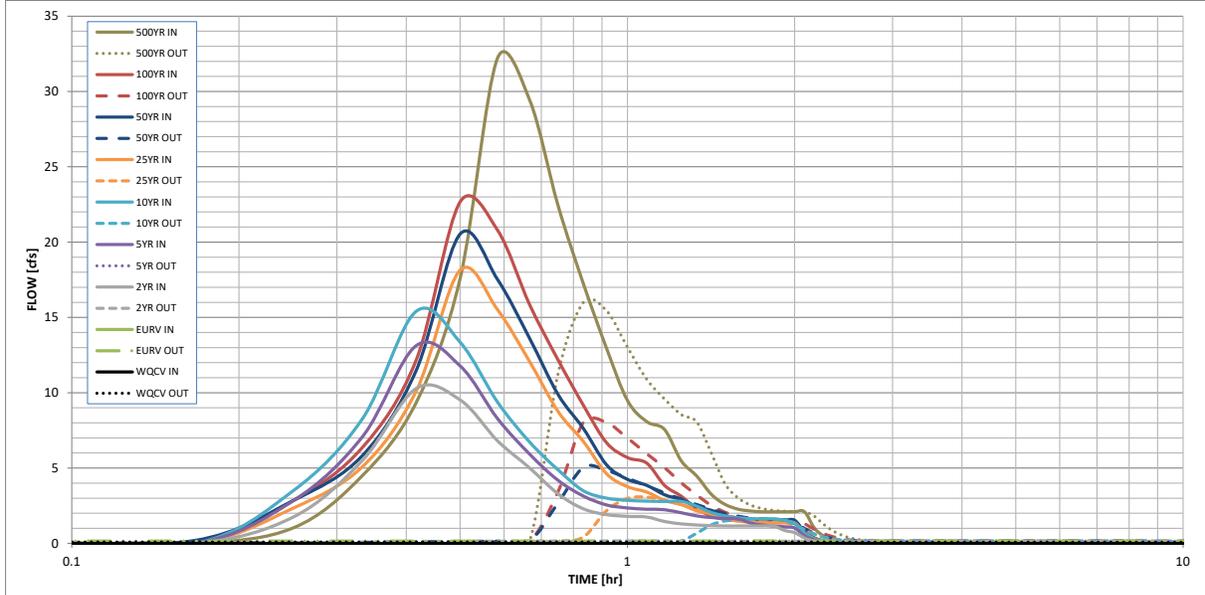
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.189	0.543	0.434	0.560	0.662	0.767	0.870	0.982	1.408
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.434	0.560	0.662	0.767	0.870	0.982	1.408
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.8	2.2	3.3	5.6	7.0	8.8	14.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.16	0.43	0.64	1.11	1.38	1.73	2.87
Peak Inflow Q (cfs) =	N/A	N/A	10.3	13.1	15.4	18.1	20.5	22.7	32.2
Peak Outflow Q (cfs) =	0.1	0.2	0.1	0.2	1.6	3.1	5.0	8.0	16.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.1	0.5	0.5	0.7	0.9	1.1
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.2	0.3	0.5	0.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	61	70	70	69	68	67	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	64	74	74	74	74	73	72
Maximum Ponding Depth (ft) =	2.80	4.90	4.22	4.86	5.00	5.07	5.13	5.24	5.72
Area at Maximum Ponding Depth (acres) =	0.14	0.21	0.18	0.20	0.21	0.21	0.21	0.22	0.24
Maximum Volume Stored (acre-ft) =	0.189	0.545	0.413	0.537	0.566	0.578	0.593	0.615	0.724

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



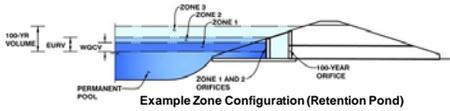
S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Defention, Version 4.02 (February 2020)

Project: Singer Ranch

Basin ID: DF-7 (NE Multi-Family Pond)



Example Zone Configuration (Retention Pond)

Watershed Information

- Selected BMP Type = EDB
Watershed Area = 18.75 acres
Watershed Length = 1,535 ft
Watershed Length to Centroid = 525 ft
Watershed Slope = 0.030 ft/ft
Watershed Imperviousness = 70.00% percent
Percentage Hydrologic Soil Group A = 0.0% percent
Percentage Hydrologic Soil Group B = 100.0% percent
Percentage Hydrologic Soil Groups C/D = 0.0% percent
Target WQC Drain Time = 40.0 hours
Location for 1-hr Rainfall Depths = User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

- Water Quality Capture Volume (WQCV) = 0.430 acre-feet
Excess Urban Runoff Volume (EURV) = 1.441 acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) = 1.274 acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) = 1.717 acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) = 2.091 acre-feet
25-yr Runoff Volume (P1 = 2 in.) = 2.534 acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) = 2.925 acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) = 3.392 acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) = 5.049 acre-feet
Approximate 2-yr Detention Volume = 1.126 acre-feet
Approximate 5-yr Detention Volume = 1.501 acre-feet
Approximate 10-yr Detention Volume = 1.894 acre-feet
Approximate 25-yr Detention Volume = 2.036 acre-feet
Approximate 50-yr Detention Volume = 2.118 acre-feet
Approximate 100-yr Detention Volume = 2.268 acre-feet

Optional User Overrides

- Optional User Overrides table with columns for description and value.

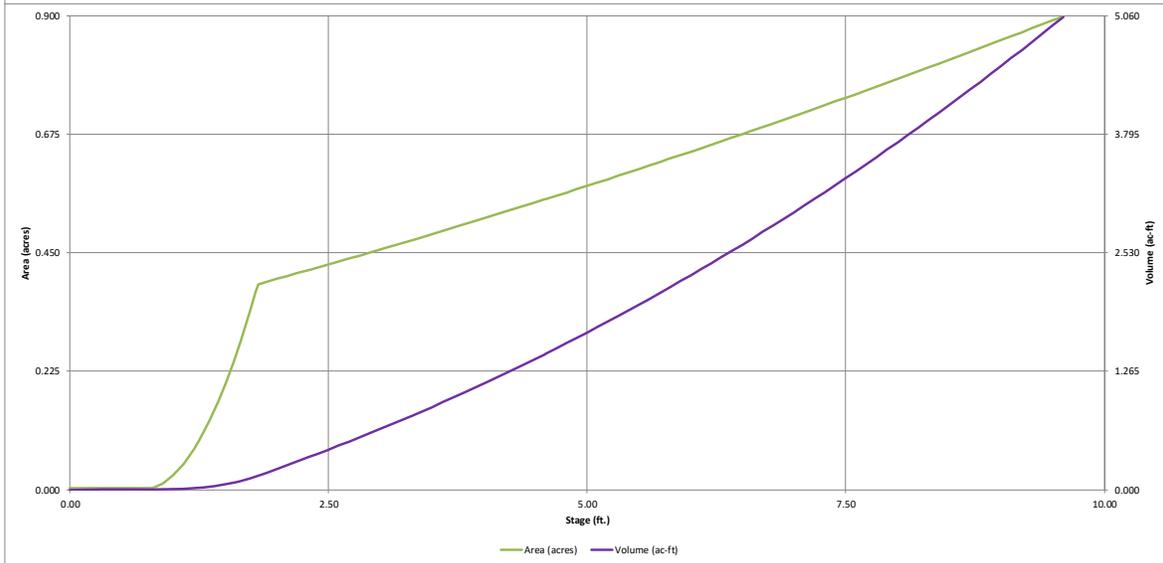
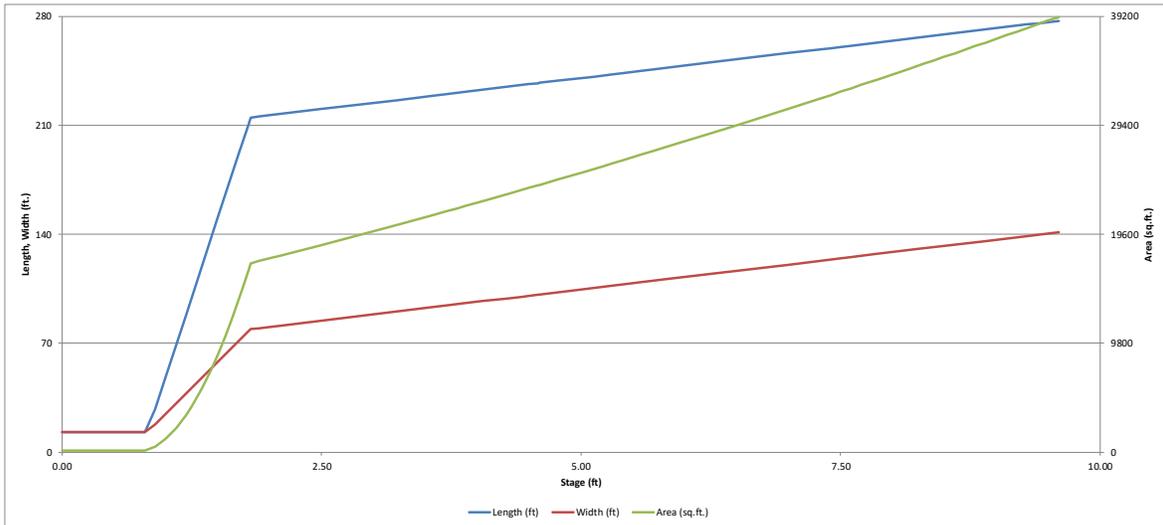
Define Zones and Basin Geometry

- Zone 1 Volume (WQCV) = 0.430 acre-feet
Zone 2 Volume (EURV - Zone 1) = 1.012 acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) = 0.827 acre-feet
Total Detention Basin Volume = 2.268 acre-feet
Initial Surcharge Volume (ISV) = 56 ft^3
Initial Surcharge Depth (ISD) = 0.33 ft
Total Available Detention Depth (Htotal) = 6.00 ft
Depth of Trickle Channel (Htc) = 0.50 ft
Slope of Trickle Channel (Strc) = 0.005 ft/ft
Slopes of Main Basin Sides (Smbasin) = 4 H:V
Basin Length-to-Width Ratio (RLNW) = 3
Initial Surcharge Area (AISV) = 170 ft^2
Surcharge Volume Length (LSV) = 13.0 ft
Surcharge Volume Width (WSV) = 13.0 ft
Depth of Basin Floor (HFLOOR) = 0.99 ft
Length of Basin Floor (LFLOOR) = 215.0 ft
Width of Basin Floor (WFLOOR) = 79.0 ft
Area of Basin Floor (AFLOOR) = 16,995 ft^2
Volume of Basin Floor (VFLOOR) = 6,226 ft^3
Depth of Main Basin (HMBASIN) = 4.18 ft
Length of Main Basin (LMBASIN) = 248.4 ft
Width of Main Basin (WMBASIN) = 112.5 ft
Area of Main Basin (AMBASIN) = 27,946 ft^2
Volume of Main Basin (VMBASIN) = 92,984 ft^3
Calculated Total Basin Volume (VTOTAL) = 2.281 acre-feet

Main data table with columns: Depth Increment (ft), Stage - Storage Description, Stage (ft), Optional Override Stage (ft), Length (ft), Width (ft), Area (ft^2), Optional Override Area (ft^2), Area (acre), Volume (ft^3), and Volume (ac-ft). The table lists stages from 0.00 to 9.60, including sections for Top of Micropool, ISV, Floor, Zone 1 (WQCV), Zone 2 (EURV), and Zone 3 (100-year).

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

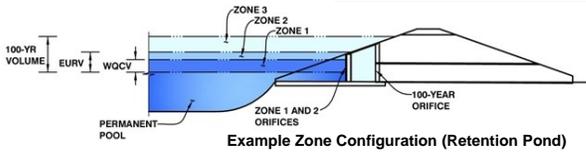
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-7 (NE Multi-Family Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.51	0.430	Orifice Plate
Zone 2 (EURV)	4.59	1.012	Circular Orifice
Zone 3 (100-year)	5.98	0.827	Weir&Pipe (Restrict)
Total (all zones)		2.268	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-5/16 inches)

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.84	1.67					
Orifice Area (sq. inches)	1.40	1.40	1.40					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.51	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.59	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	2.56	N/A	inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.59	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	5.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	5.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir
Height of Gate Upper Edge, H₁ = feet
Overflow Weir Slope Length = feet
Gate Open Area / 100-yr Orifice Area = N/A
Overflow Gate Open Area w/o Debris = ft²
Overflow Gate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	13.60		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.60	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	21.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres
Basin Volume at Top of Freeboard = acre-ft

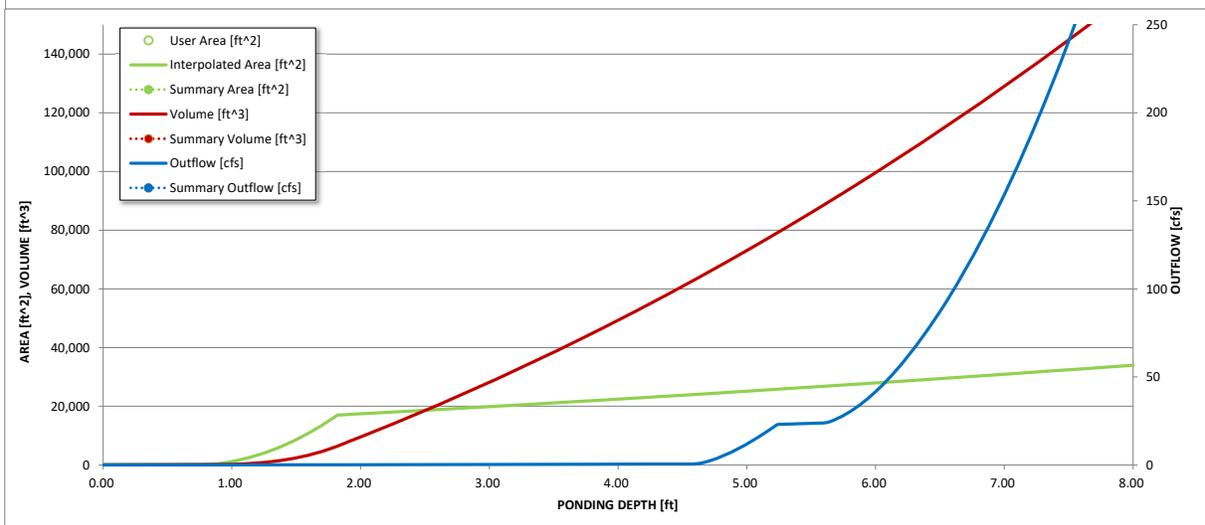
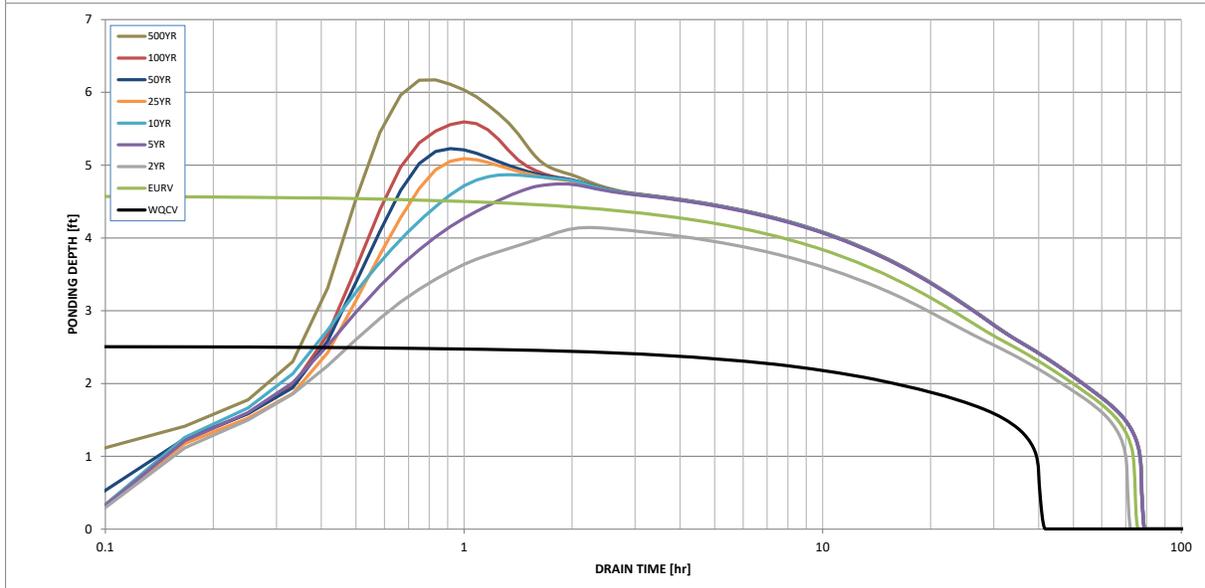
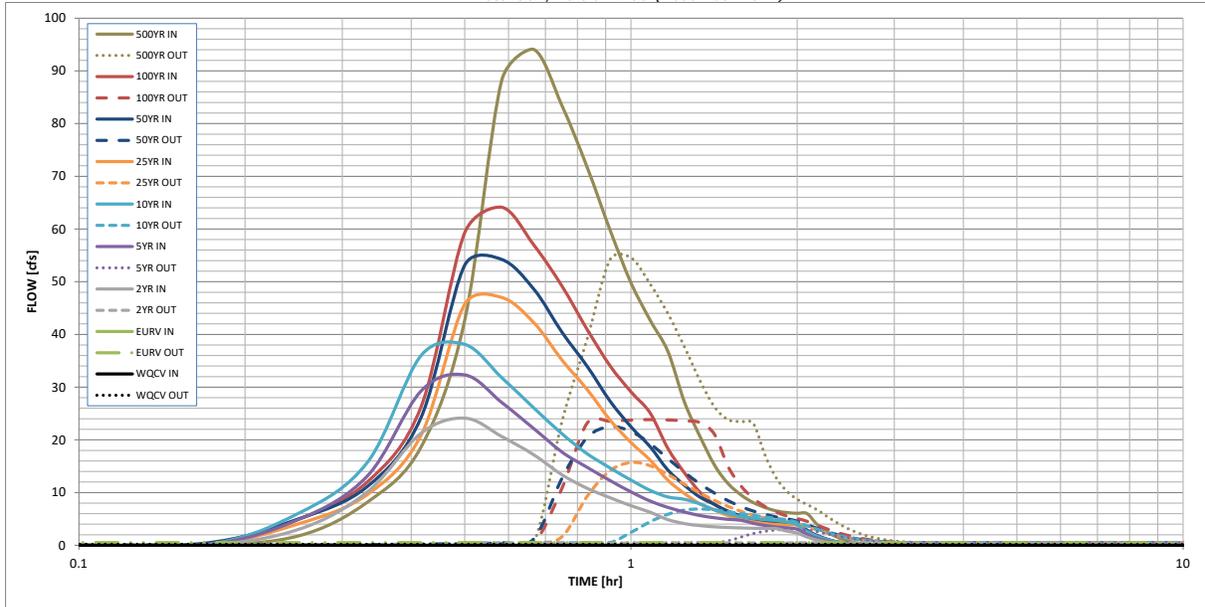
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.430	1.441	1.274	1.717	2.091	2.534	2.925	3.392	5.049
CUHP Runoff Volume (acre-ft) =	N/A	N/A	1.274	1.717	2.091	2.534	2.925	3.392	5.049
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.2	6.2	9.4	16.6	20.9	26.1	43.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.33	0.50	0.89	1.11	1.39	2.33
Peak Inflow Q (cfs) =	N/A	N/A	24.1	32.3	38.1	47.0	54.2	64.1	94.1
Peak Outflow Q (cfs) =	0.2	0.5	0.5	3.1	6.9	15.7	22.5	23.8	54.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.7	0.9	1.1	0.9	1.3
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.9	1.3	1.3	1.4
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	65	70	69	67	66	64	59
Time to Drain 99% of Inflow Volume (hours) =	40	72	69	75	74	74	73	73	70
Maximum Ponding Depth (ft) =	2.51	4.59	4.14	4.74	4.87	5.09	5.23	5.59	6.17
Area at Maximum Ponding Depth (acres) =	0.43	0.55	0.52	0.56	0.57	0.58	0.59	0.61	0.65
Maximum Volume Stored (acre-ft) =	0.430	1.446	1.204	1.529	1.597	1.724	1.806	2.029	2.390

DETENTION BASIN OUTLET STRUCTURE DESIGN

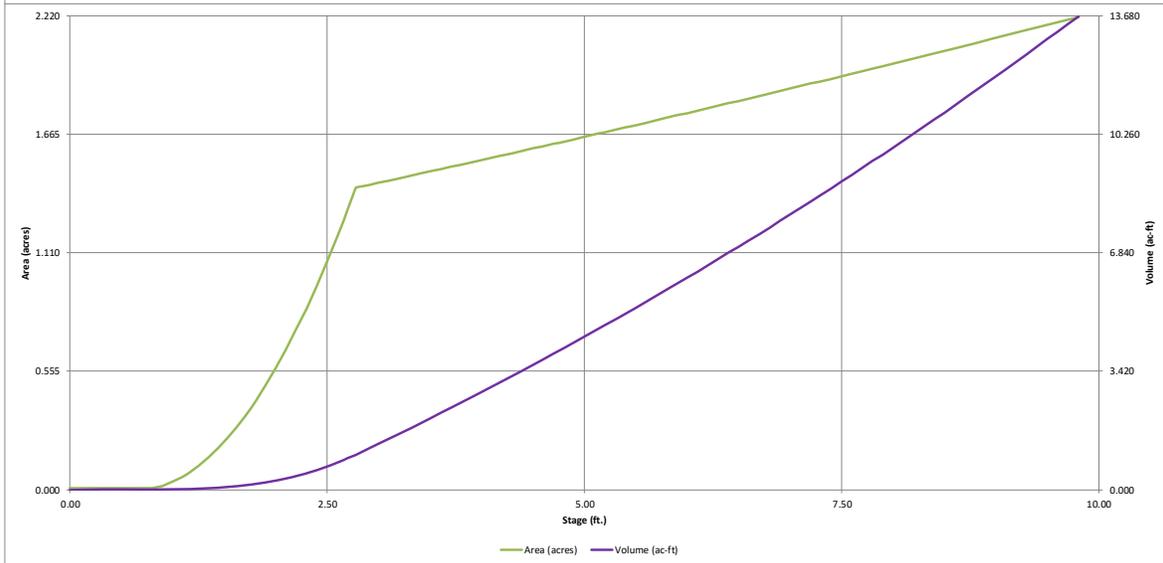
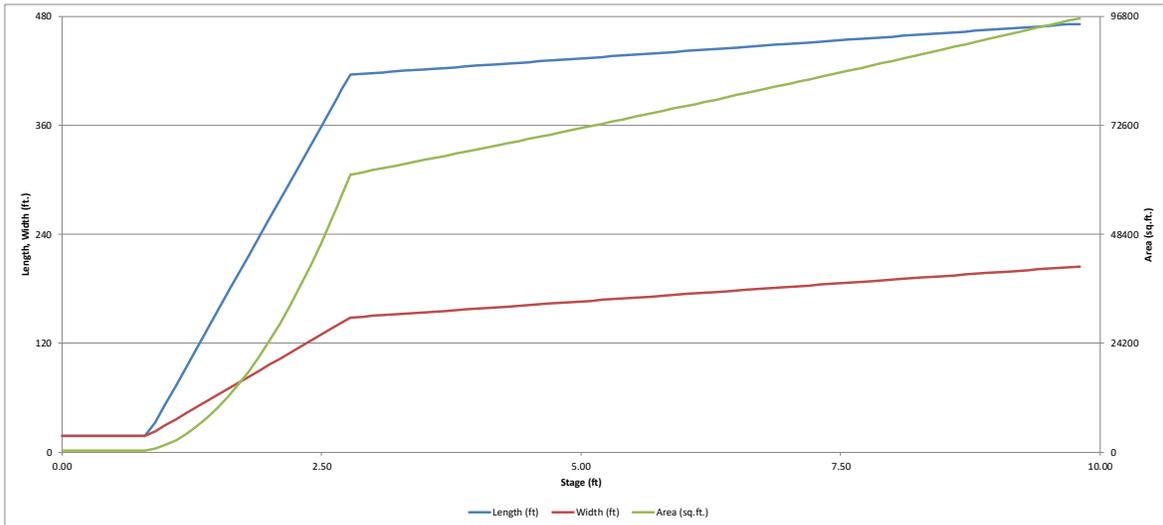
MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

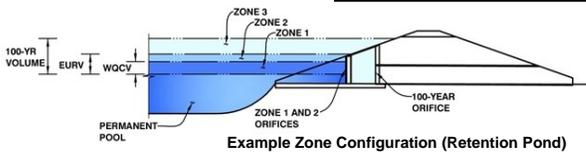
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-8 (SE Single-Family & Commercial Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.66	0.835	Orifice Plate
Zone 2 (EURV)	4.00	1.966	Circular Orifice
Zone 3 (100-year)	5.00	1.607	Weir&Pipe (Restrict)
Total (all zones)		4.407	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.66	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	10.60	inches
Orifice Plate: Orifice Area per Row =	2.51	sq. inches (diameter = 1-3/4 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row =	1.743E-02	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.89	1.77					
Orifice Area (sq. inches)	2.51	2.51	2.51					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.66	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	5.24	N/A	inches

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.15	N/A	ft ²
Vertical Orifice Centroid =	0.22	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	6.00	N/A	feet
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Gate Upper Edge, H _i =	4.00	N/A	feet
Overflow Weir Slope Length =	6.00	N/A	feet
Gate Open Area / 100-yr Orifice Area =	5.63	N/A	
Overflow Gate Open Area w/o Debris =	25.20	N/A	ft ²
Overflow Gate Open Area w/ Debris =	12.60	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	36.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	21.80	N/A	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	4.48	N/A	ft ²
Outlet Orifice Centroid =	1.03	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.78	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	40.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.95	feet
Stage at Top of Freeboard =	6.95	feet
Basin Area at Top of Freeboard =	1.87	acres
Basin Volume at Top of Freeboard =	7.84	acre-ft

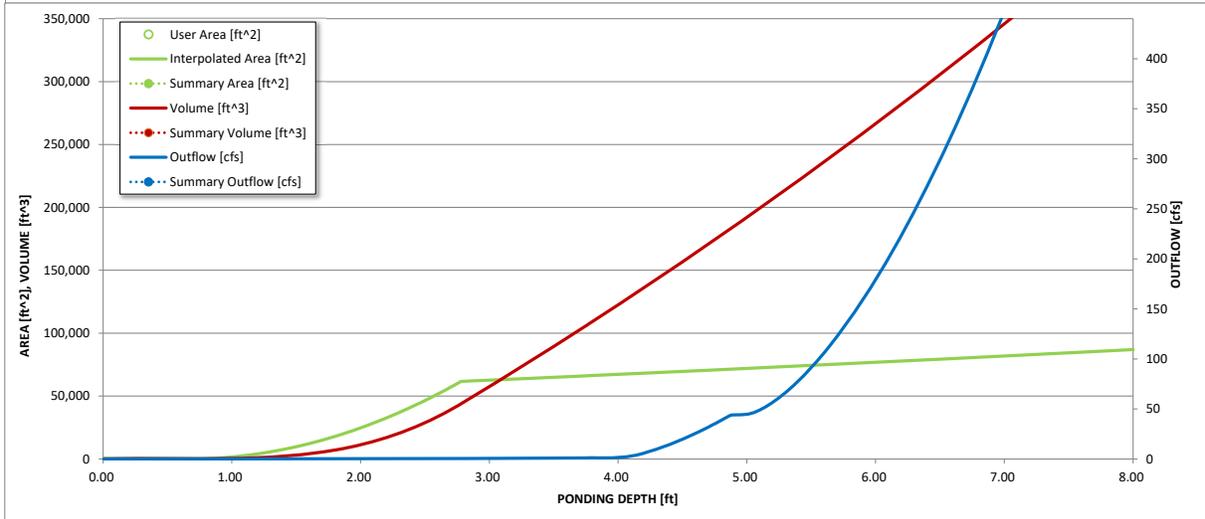
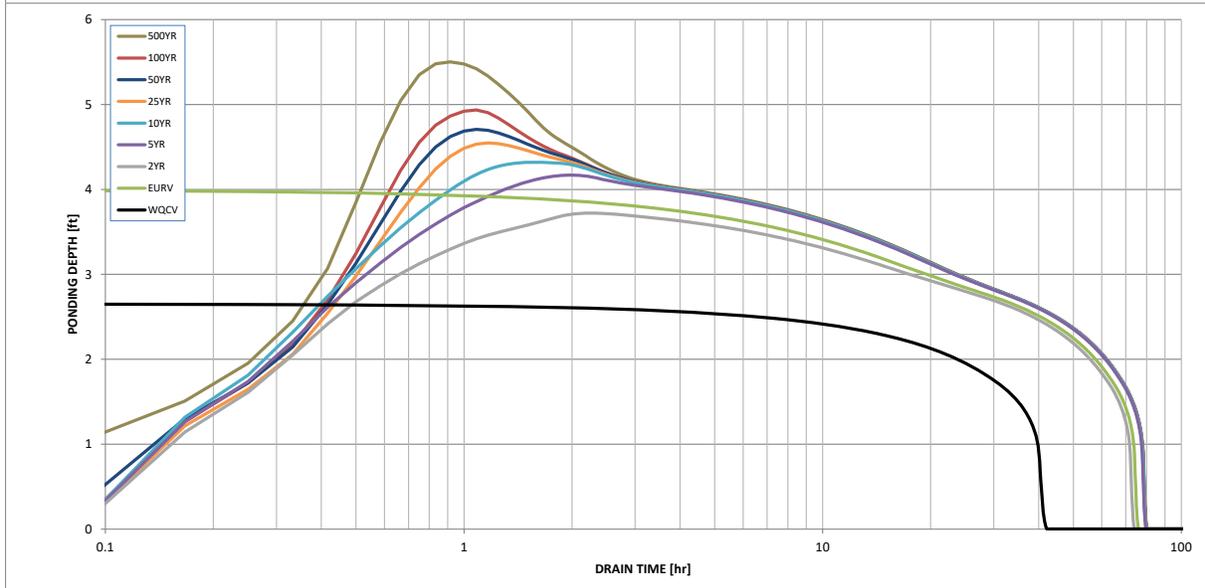
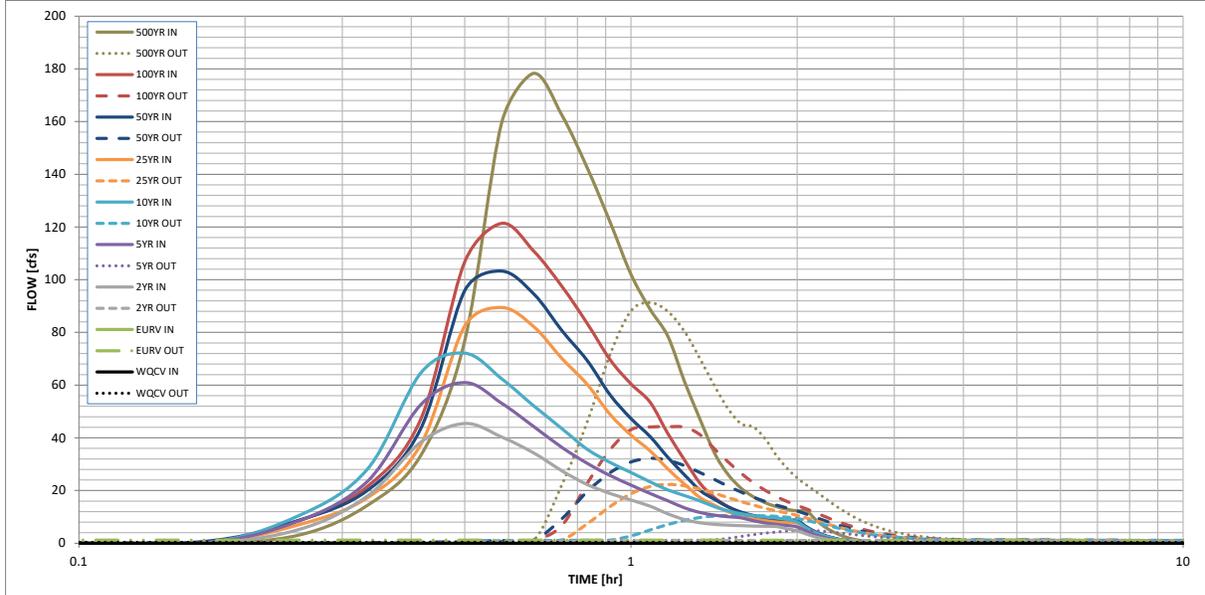
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.835	2.801	2.539	3.423	4.169	5.051	5.831	6.760	10.064
CUHP Runoff Volume (acre-ft) =	N/A	N/A	2.539	3.423	4.169	5.051	5.831	6.760	10.064
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	4.0	11.0	16.6	29.9	37.4	47.8	79.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.11	0.30	0.46	0.82	1.03	1.31	2.18
Peak Inflow Q (cfs) =	N/A	N/A	45.4	61.0	72.1	89.5	103.3	121.4	178.3
Peak Outflow Q (cfs) =	0.3	1.2	1.1	4.9	10.6	22.3	32.2	44.2	91.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.9	0.9	1.1
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.2	1.7	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	67	70	69	68	66	65	60
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	75	75	74	74	73	71
Maximum Ponding Depth (ft) =	2.66	4.00	3.72	4.17	4.32	4.55	4.71	4.93	5.50
Area at Maximum Ponding Depth (acres) =	1.26	1.54	1.51	1.56	1.58	1.60	1.62	1.64	1.71
Maximum Volume Stored (acre-ft) =	0.847	2.812	2.384	3.076	3.296	3.661	3.919	4.294	5.250

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)

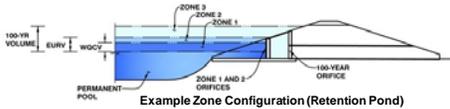


S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD- Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-9 (SE Commercial Pond)



Example Zone Configuration (Retention Pond)

Watershed Information

- Selected BMP Type = EDB
Watershed Area = 34.13 acres
Watershed Length = 1,960 ft
Watershed Length to Centroid = 730 ft
Watershed Slope = 0.030 ft/ft
Watershed Imperviousness = 80.00% percent
Percentage Hydrologic Soil Group A = 0.0% percent
Percentage Hydrologic Soil Group B = 100.0% percent
Percentage Hydrologic Soil Groups C/D = 0.0% percent
Target WQC Drain Time = 40.0 hours
Location for 1-hr Rainfall Depths = User Input

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

- Water Quality Capture Volume (WQCV) = 0.934 acre-feet
Excess Urban Runoff Volume (EURV) = 3.031 acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) = 2.670 acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) = 3.533 acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) = 4.247 acre-feet
25-yr Runoff Volume (P1 = 2 in.) = 5.038 acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) = 5.775 acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) = 6.618 acre-feet
500-yr Runoff Volume (P1 = 3.55 in.) = 9.700 acre-feet
Approximate 2-yr Detention Volume = 2.401 acre-feet
Approximate 5-yr Detention Volume = 3.164 acre-feet
Approximate 10-yr Detention Volume = 3.928 acre-feet
Approximate 25-yr Detention Volume = 4.210 acre-feet
Approximate 50-yr Detention Volume = 4.373 acre-feet
Approximate 100-yr Detention Volume = 4.608 acre-feet

Optional User Overrides

- acre-feet
acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches
2.25 inches
2.52 inches
3.55 inches

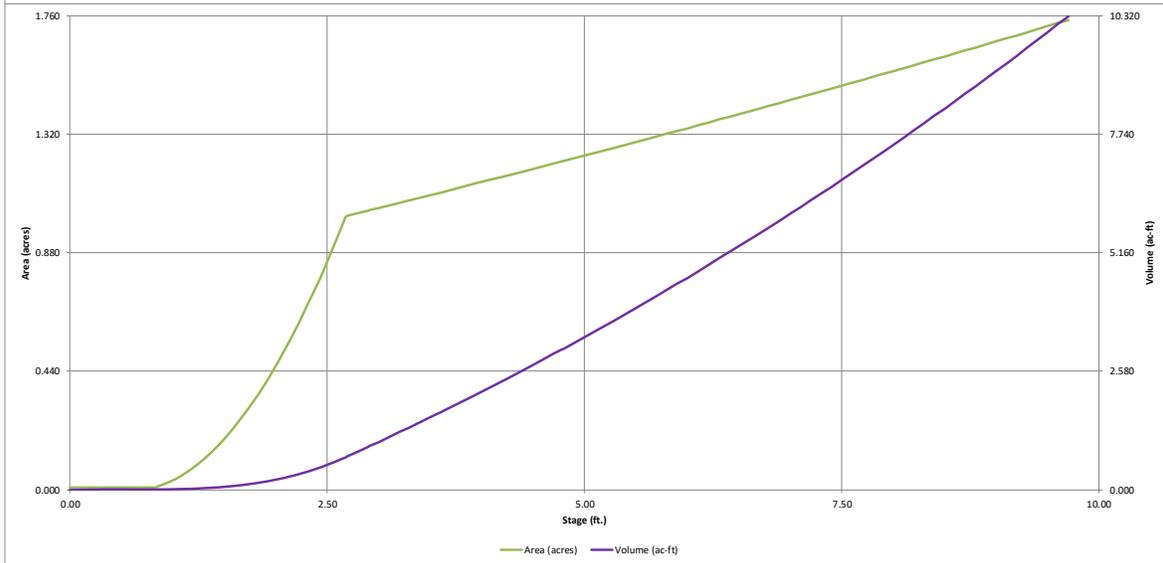
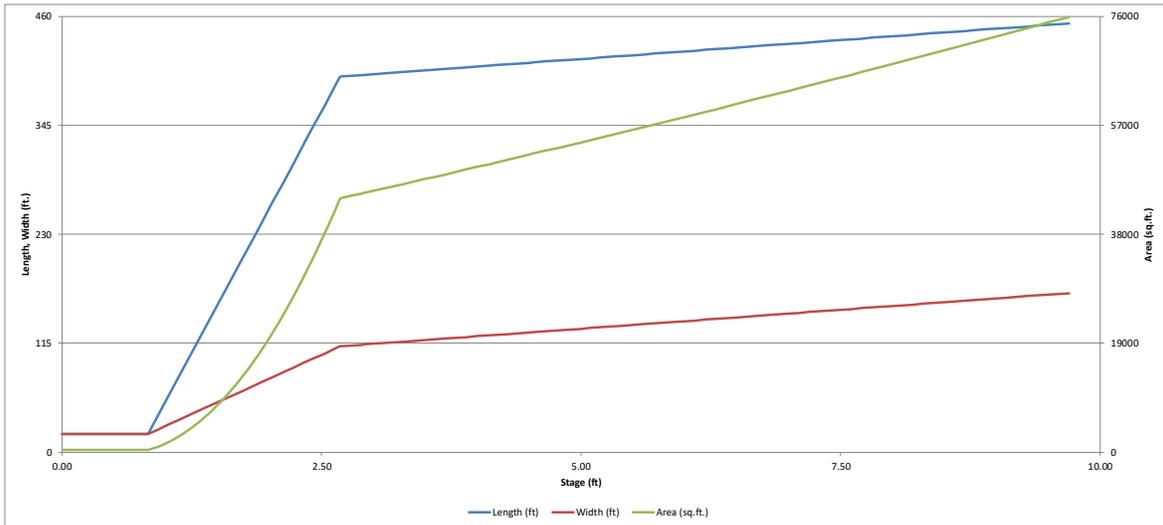
Define Zones and Basin Geometry

- Zone 1 Volume (WQCV) = 0.934 acre-feet
Zone 2 Volume (EURV - Zone 1) = 2.097 acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) = 1.577 acre-feet
Total Detention Basin Volume = 4.608 acre-feet
Initial Surcharge Volume (ISV) = 122 ft^3
Initial Surcharge Depth (ISD) = 0.33 ft
Total Available Detention Depth (Htotal) = 6.00 ft
Depth of Trickle Channel (Htr) = 0.50 ft
Slope of Trickle Channel (Str) = 0.005 ft/ft
Slopes of Main Basin Sides (Smain) = 4 ft:H:V
Basin Length-to-Width Ratio (RL/W) = 4
Initial Surcharge Area (AISV) = 366 ft^2
Surcharge Volume Length (LISV) = 19.1 ft
Surcharge Volume Width (WISV) = 19.1 ft
Depth of Basin Floor (HfLOOR) = 1.85 ft
Length of Basin Floor (LfLOOR) = 396.5 ft
Width of Basin Floor (WfLOOR) = 111.6 ft
Area of Basin Floor (AfLOOR) = 44,271 ft^2
Volume of Basin Floor (VfLOOR) = 30,010 ft^3
Depth of Main Basin (HMAIN) = 3.32 ft
Length of Main Basin (LMAIN) = 423.1 ft
Width of Main Basin (WMAIN) = 138.2 ft
Area of Main Basin (AMAIN) = 58,461 ft^2
Volume of Main Basin (VMAIN) = 169,836 ft^3
Calculated Total Basin Volume (Vtotal) = 4,595 acre-feet

Table with columns: Depth Increment, Stage - Storage Description, Stage (ft), Optional Override Stage (ft), Length (ft), Width (ft), Area (ft^2), Optional Override Area (ft^2), Area (acre), Volume (ft^3), Volume (ac-ft). Rows include Top of Micropool, Floor, Zone 1 (WQCV), Zone 2 (EURV), and Zone 3 (100-year).

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

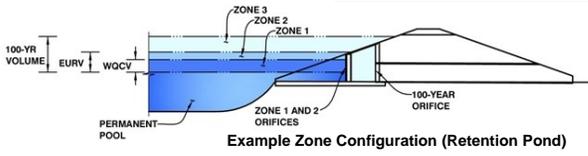
MHFD-Detention, Version 4.02 (February 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.02 (February 2020)

Project: Singer Ranch
Basin ID: DF-9 (SE Commercial Pond)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.91	0.934	Orifice Plate
Zone 2 (EURV)	4.77	2.097	Circular Orifice
Zone 3 (100-year)	6.00	1.577	Weir&Pipe (Restrict)
Total (all zones)		4.608	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Calculated Parameters for Underdrain

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	1.910E-02	ft ²
Depth at top of Zone using Orifice Plate =	2.91	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	11.60	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	2.75	sq. inches (diameter = 1-7/8 inches)	Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.97	1.94					
Orifice Area (sq. inches)	2.75	2.75	2.75					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

	Zone 2 Circular	Not Selected		Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.91	N/A	ft (relative to basin bottom at Stage = 0 ft)	0.09	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	4.77	N/A	ft (relative to basin bottom at Stage = 0 ft)	0.17	N/A	feet
Vertical Orifice Diameter =	4.13	N/A	inches			

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.77	N/A	ft (relative to basin bottom at Stage = 0 ft)	4.77	N/A	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	6.00	N/A	feet
Overflow Weir Gate Slope =	0.00	N/A	H:V	6.21	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet	25.20	N/A	ft ²
Overflow Gate Open Area % =	70%	N/A	%, gate open area/total area	12.60	N/A	ft ²
Debris Clogging % =	50%	N/A	%			

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected		Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.30	N/A	ft (distance below basin bottom at Stage = 0 ft)	4.06	N/A	ft ²
Outlet Pipe Diameter =	36.00	N/A	inches	0.96	N/A	feet
Restrictor Plate Height Above Pipe Invert =	20.10		inches	1.69	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

Spillway Invert Stage =	5.80	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth =	0.95	feet
Spillway Crest Length =	42.00	feet	Stage at Top of Freeboard =	7.75	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	1.53	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	7.12	acre-ft

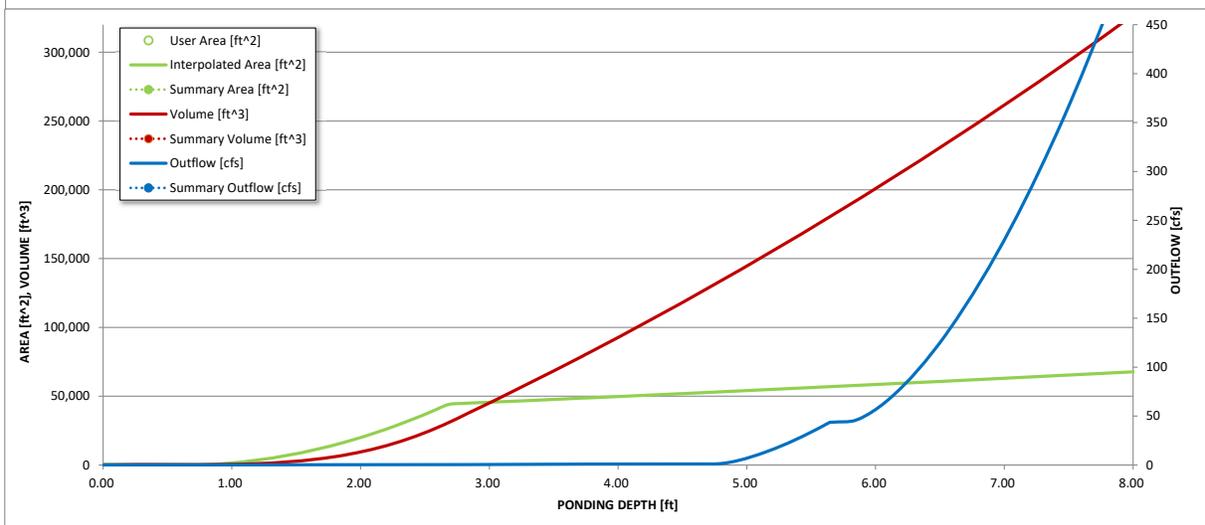
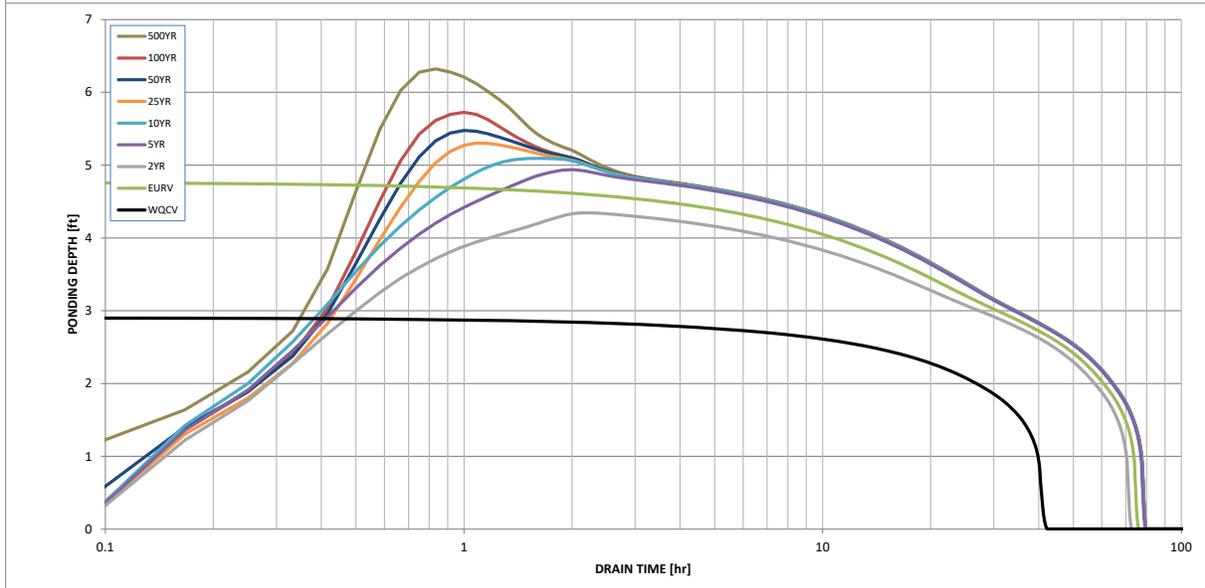
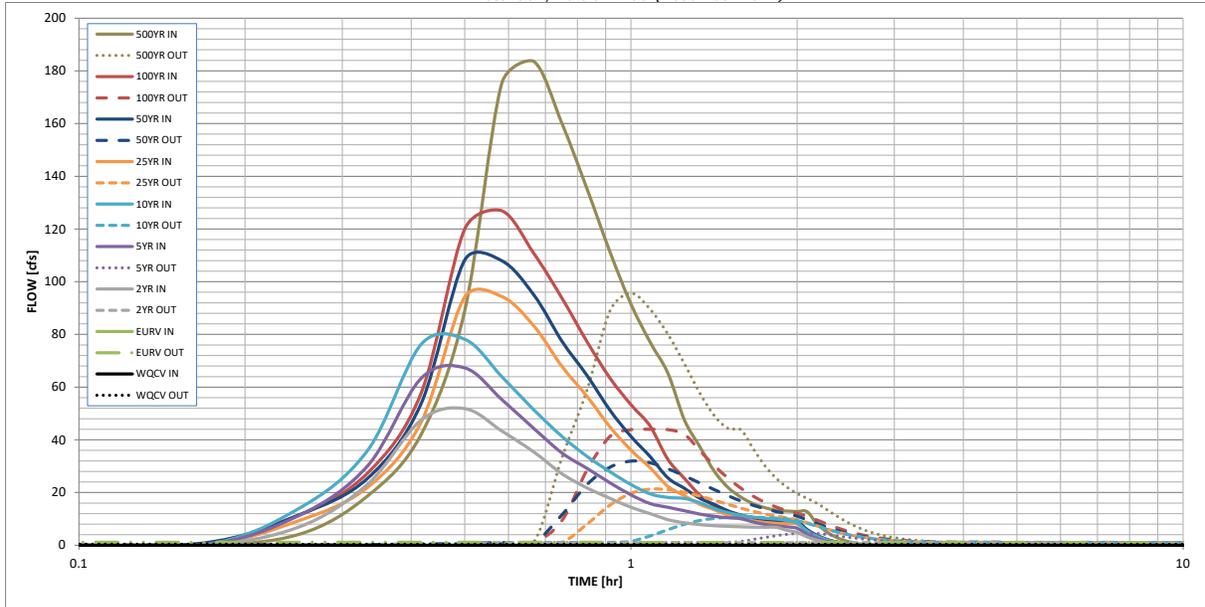
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.55
One-Hour Rainfall Depth (in) =	0.934	3.031	2.670	3.533	4.247	5.038	5.775	6.618	9.700
CUHP Runoff Volume (acre-ft) =	N/A	N/A	2.670	3.533	4.247	5.038	5.775	6.618	9.700
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	4.0	11.3	17.1	30.0	37.8	48.0	79.7
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.12	0.33	0.50	0.88	1.11	1.41	2.33
Peak Inflow Q (cfs) =	N/A	N/A	51.9	67.3	78.2	94.4	108.2	126.9	183.6
Peak Outflow Q (cfs) =	0.4	1.1	1.0	4.7	10.6	21.3	31.9	44.0	95.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.6	0.7	0.8	0.9	1.2
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	0.8	1.2	1.7	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	65	70	69	68	67	65	61
Time to Drain 99% of Inflow Volume (hours) =	40	72	69	75	75	74	74	73	71
Maximum Ponding Depth (ft) =	2.91	4.77	4.34	4.94	5.09	5.30	5.48	5.72	6.32
Area at Maximum Ponding Depth (acres) =	1.04	1.22	1.18	1.23	1.25	1.27	1.29	1.31	1.37
Maximum Volume Stored (acre-ft) =	0.941	3.037	2.522	3.233	3.431	3.696	3.913	4.238	5.031

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

APPENDIX B

STANDARD DESIGN CHARTS AND TABLES

**2019 DRAINAGE, BRIDGE AND POND FEES
CITY OF COLORADO SPRINGS**

Basin Name	DBPS Year	Drainage Fee/Acre	Bridge Fee/Acre	Pond Land Fee/Acre	Pond Facility Fee/Acre	Surcharge/Acre
19th Street	1964	\$4,030				
21st Street	1977	\$6,151				
Bear Creek	1980	\$3,959	\$373			
Big Johnson, Crews	1991	\$15,316	\$1,259	\$241		
Black Squirrel Creek	1989	\$14,302	\$1,603	\$789		
Camp Creek	1964	\$2,270				
Cottonwood Creek ^{1, 2}	2000	\$13,923	\$1,130			\$723
Douglas Creek	1981	\$12,728	\$285			
Dry Creek ³	1966	\$0.00				
Elkhorn Basin ⁴	n/a	\$0.00				
Fishers Canyon ⁵	1991	\$0.00				
Fountain Creek ⁶	n/a	VAR				
Jimmy Camp Creek	2015	\$7,975			\$2,599	
Kettle Creek ⁷ Old Ranch Trib.	2001	\$0.00				
Little Johnson	1988	\$13,367		\$1,227		
Mesa	1986	\$10,699				
Middle Tributary	1987	\$6,995		\$1,121		
Miscellaneous ⁸	n/a	\$11,905				
Monument Branch ¹²	1987	\$0.00				
North Rockrimmon	1973	\$6,152				
Park Vista (MDDP)	2004	\$17,135				
Peterson Field	1984	\$12,925	\$595			
Pine Creek ⁹	1988	\$0.00				
Pope's Bluff	1976	\$4,096	\$701			
Pulpit Rock	1968	\$6,784				
Sand Creek ¹⁰	1996	\$12,645	\$761	\$1,070	\$3,676	\$1,333
Shooks Run ¹¹	1994	\$0.00				
Smith Creek ¹²	2002	\$0.00				
South Rockrimmon	1976	\$4,810				
Southwest Area	1984	\$13,467				
Spring Creek	1968	\$10,609				
Templeton Gap	1977	\$6,997	\$77			
Windmill Gulch	1992	\$14,594	\$271	\$3,055		

All Drainage, Bridge and Detention Pond Facilities Fees adjusted by 6.7% over 2018 by City Council Resolution No. 159-18 on December 11, 2018 to be effective on January 1, 2019. Land Fees are based on the Park Land Dedication Fee which is currently \$76,602/acre (0% change for inflation in 2018).

¹ The 2018 Cottonwood Creek drainage fee consists of a capital improvement fee of \$10,853 per acre and land fee of \$3,069 per acre for a total of \$13,923 per acre. These fees are adjusted annually using different procedures but are combined for collection purposes. **The surcharge fee of \$723/ac is due in cash; credits for prior facility construction cannot be used to offset this fee**, which is deposited into a separate City fund known as the "Cottonwood Creek Surcharge" fund.

² The Wolf Ranch portion of the Cottonwood Creek Drainage Basin was approved as a "no fee" basin **as to Drainage Fees only** by City Council on August 28, 2018 by Resolution No. 96-18

³ Dry Creek is a closed basin per City Council Resolution No.118-08 on June 24, 2008

⁴ Elkhorn Basin is a closed basin per the Annexation Agreements for the area.

⁵ Fishers Canyon is a closed basin per City Council Resolution No. 74-08 on April 22, 2008.

⁶Pursuant to the recommendation of the Subdivision Storm Drainage Board adopted at its meeting of September 15, 1977, there are exempted and excluded from the provisions of this part construction of the main Fountain Creek Channel from the confluence of Fountain Creek with Monument Creek northwest to the City limits. Land developments taking place adjacent to Fountain Creek shall remain responsible for dedicating rights of way necessary for the channelization of Fountain Creek, and the developers shall continue to pay to the City as a condition of subdivision plat approval the applicable drainage fees. Drainage fees are required in accordance with the appropriate basin study.

⁷ Kettle Creek Old Ranch Tributary is a closed basin per City Council Resolution 139-02 on August 27, 2002.

⁸ Miscellaneous fee is assessed on unstudied areas and the Roswell and Westside Basins.

⁹ Pine Creek is a closed basin per City Council Resolution No.236-88 on December 13, 1988.

¹⁰Sand Creek Detention Pond #2 Surcharge (Ridgeview and Indigo Ranch) = \$1,333/ac. for 2019. Sand Creek Pond fees include two components, one for facility construction costs (\$3,676) and one for land dedication costs (\$1,070), the total Pond fee within Sand Creek is \$4,746/ac.

¹¹ Shooks Run is a closed basin pursuant to the recommendation of the Drainage Board, adopted at its meeting on October 15, 1963.

¹² Smith Creek is a closed basin per City Council Resolution 140-02 on August 27, 2002

¹² Monument Branch Basin is a closed basin per City Council Res. 177-10 on October 12, 2010

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis-- Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_t) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_t) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Figure 6-25. Estimate of Average Concentrated Shallow Flow

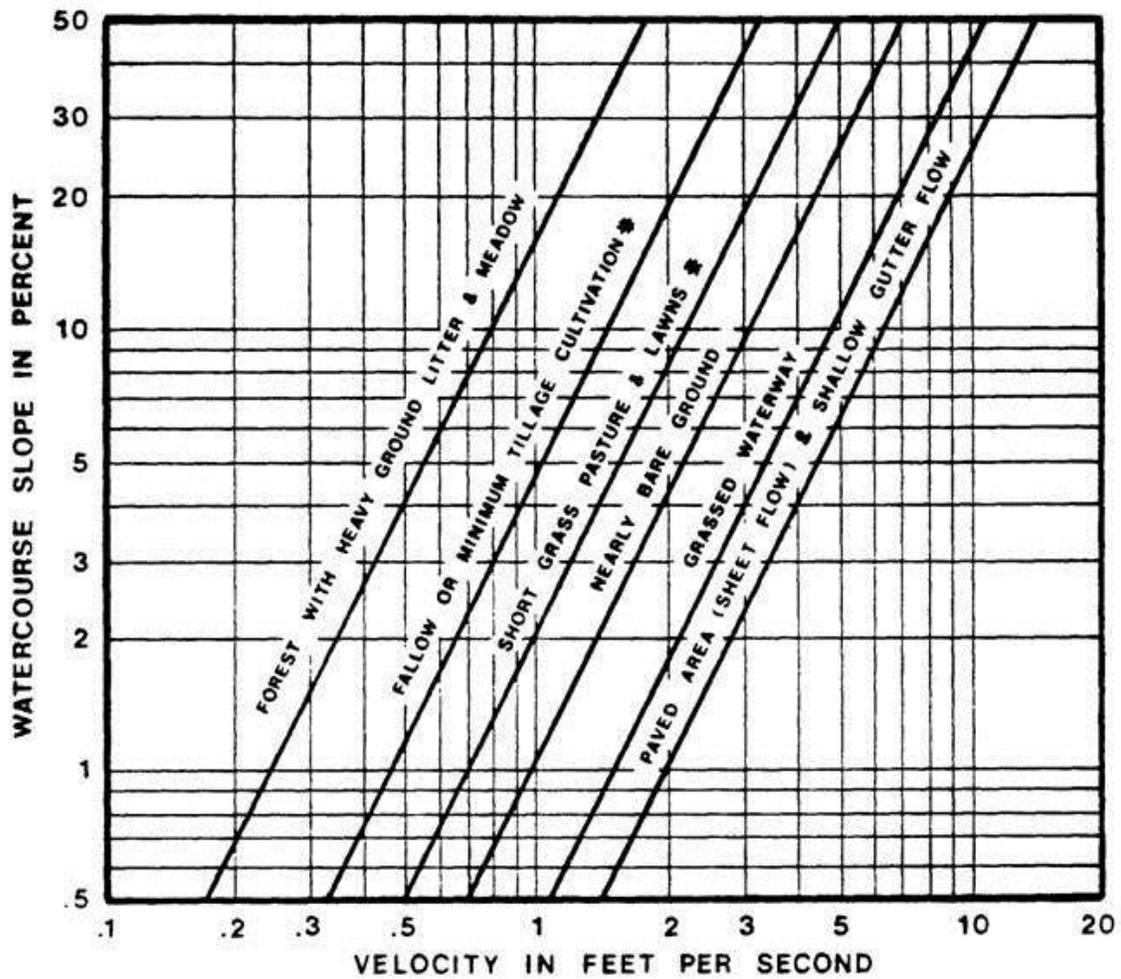
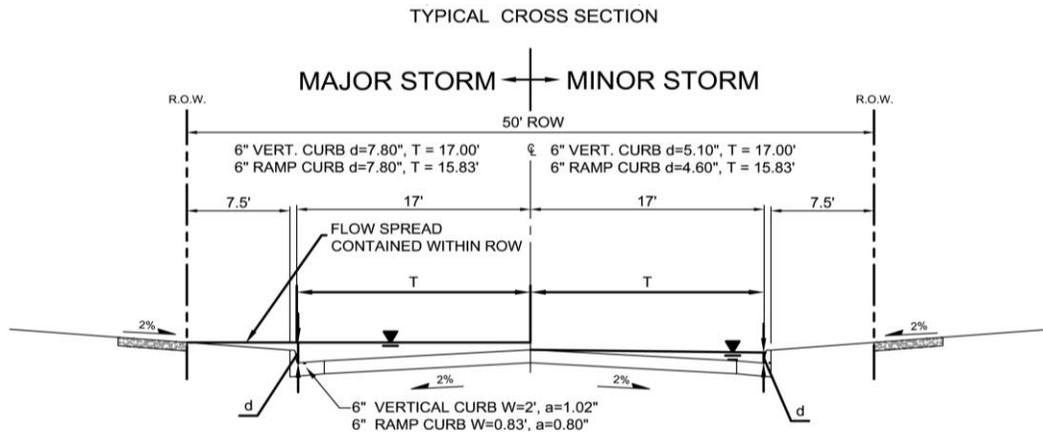
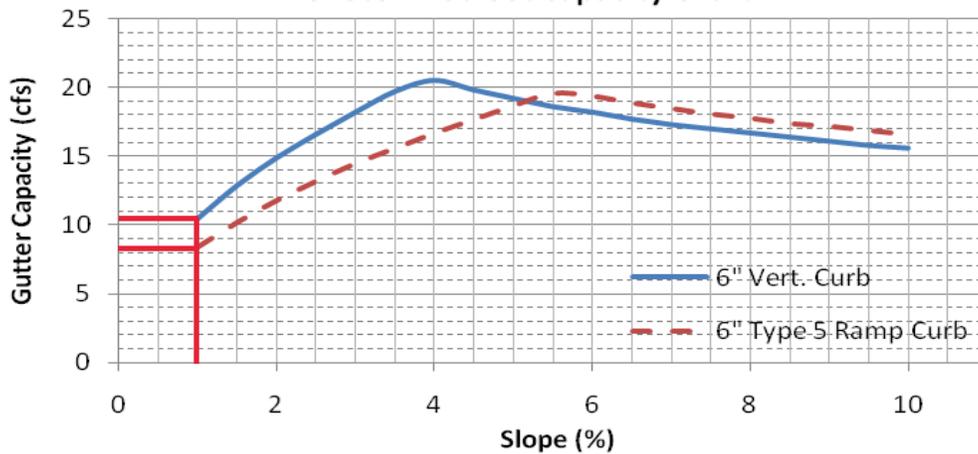


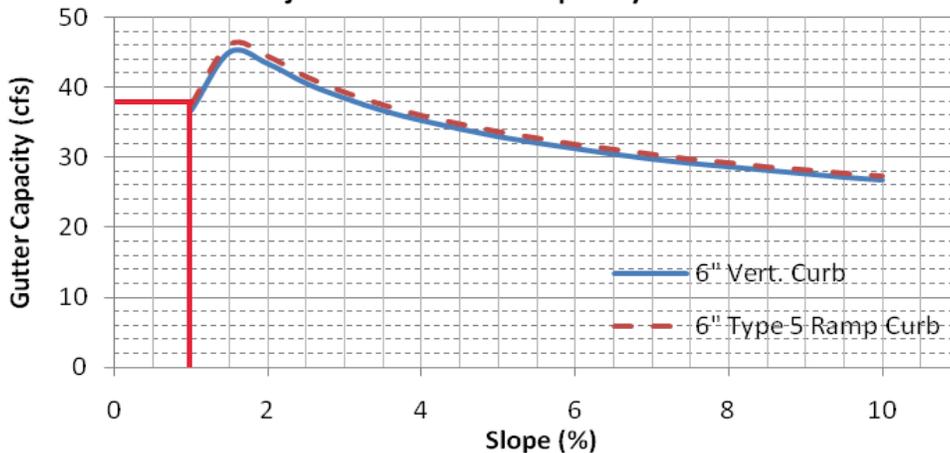
Figure 7-7. Street Capacity Charts Residential (Detached Sidewalk)



Minor Storm Street Capacity Chart



Major Storm Street Capacity Chart



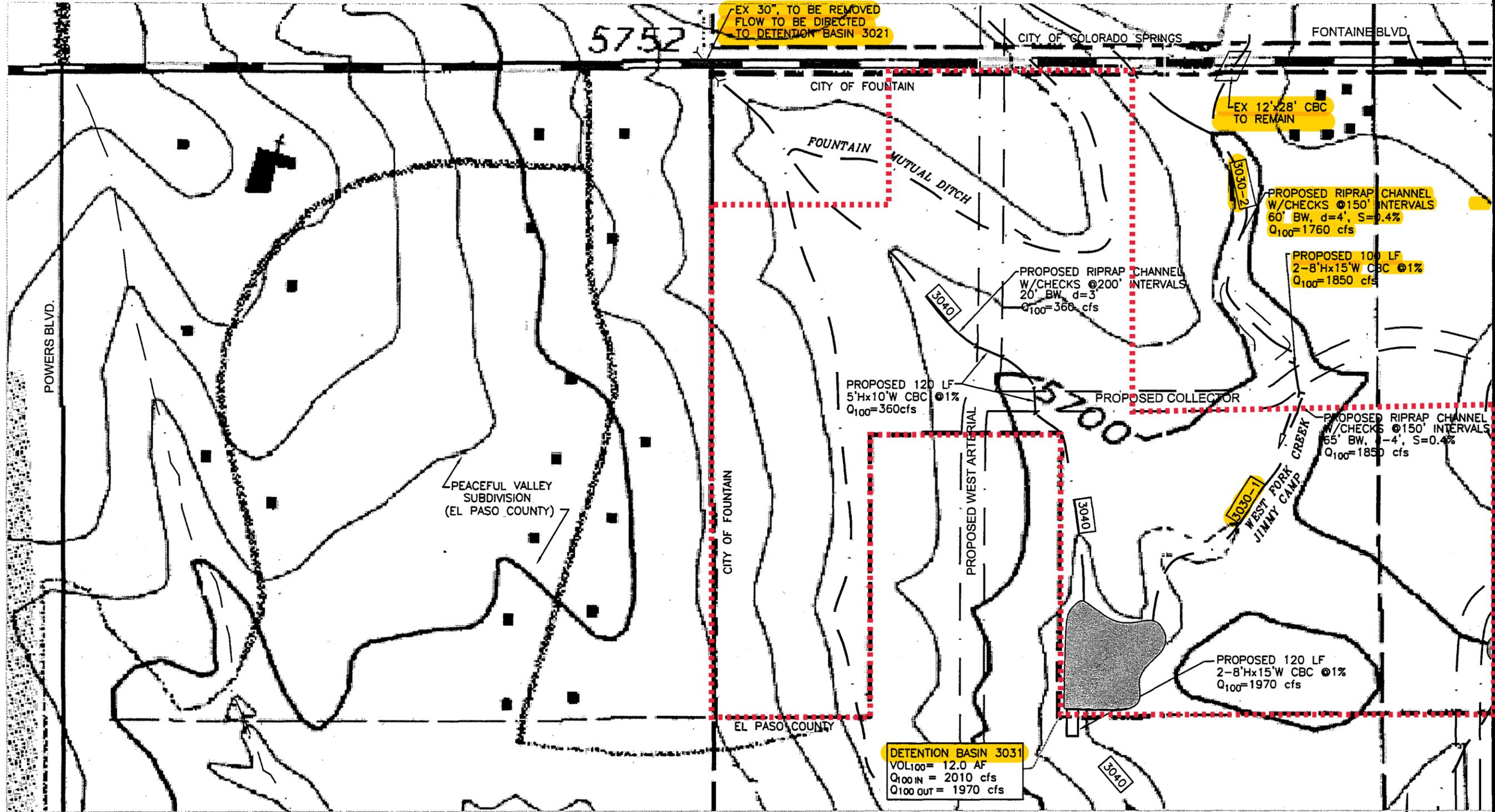
These charts shall only be used for the standard street sections as shown. The capacity shown is based on ½ the street section as calculated by the UD-Inlet spreadsheets. Minor storm capacities are based on no crown overtopping, curb height or maximum allowable spread widths. Major storm capacities are based on flow being contained within the public right-of-way, including conveyance capacity behind the curb. The UDFCD Safety Reduction Factor was applied. An 'n_{STREET}' of 0.016 and 'n_{BACK}' of 0.020 was used. Calculations were done using UD-Inlet 3.00.xls, March, 2011.

Table 6-3. Recommended percentage imperviousness values

Land Use or Surface Characteristics	Percentage Imperviousness (%)
Business:	
Downtown Areas	95
Suburban Areas	75
Residential lots (lot area only):	
Single-family	
2.5 acres or larger	12
0.75 – 2.5 acres	20
0.25 – 0.75 acres	30
0.25 acres or less	45
Apartments	75
Industrial:	
Light areas	80
Heavy areas	90
Parks, cemeteries	10
Playgrounds	25
Schools	55
Railroad yard areas	50
Undeveloped Areas:	
Historic flow analysis	2
Greenbelts, agricultural	2
Off-site flow analysis (when land use not defined)	45
Streets:	
Paved	100
Gravel (packed)	40
Drive and walks	90
Roofs	90
Lawns, sandy soil	2
Lawns, clayey soil	2

APPENDIX C

REPORT REFERENCES



EX 30", TO BE REMOVED
FLOW TO BE DIRECTED
TO DETENTION BASIN 3021

EX 12'x28' CBC
TO REMAIN

PROPOSED RIPRAP CHANNEL
W/CHECKS @150' INTERVALS
60' BW, d=4', S=0.4%
Q₁₀₀=1760 cfs

PROPOSED 100 LF
2-8'Hx15'W CBC @1%
Q₁₀₀=1850 cfs

PROPOSED RIPRAP CHANNEL
W/CHECKS @200' INTERVALS
20' BW, d=3'
Q₁₀₀=360 cfs

PROPOSED 120 LF
5'Hx10'W CBC @1%
Q₁₀₀=360 cfs

PROPOSED RIPRAP CHANNEL
W/CHECKS @150' INTERVALS
65' BW, d=4', S=0.4%
Q₁₀₀=1850 cfs

3030-1
WEST FORK
JIMMY CAMP

PROPOSED 120 LF
2-8'Hx15'W CBC @1%
Q₁₀₀=1970 cfs

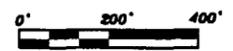
DETENTION BASIN 3031
VOL₁₀₀= 12.0 AF
Q_{100 IN} = 2010 cfs
Q_{100 OUT} = 1970 cfs

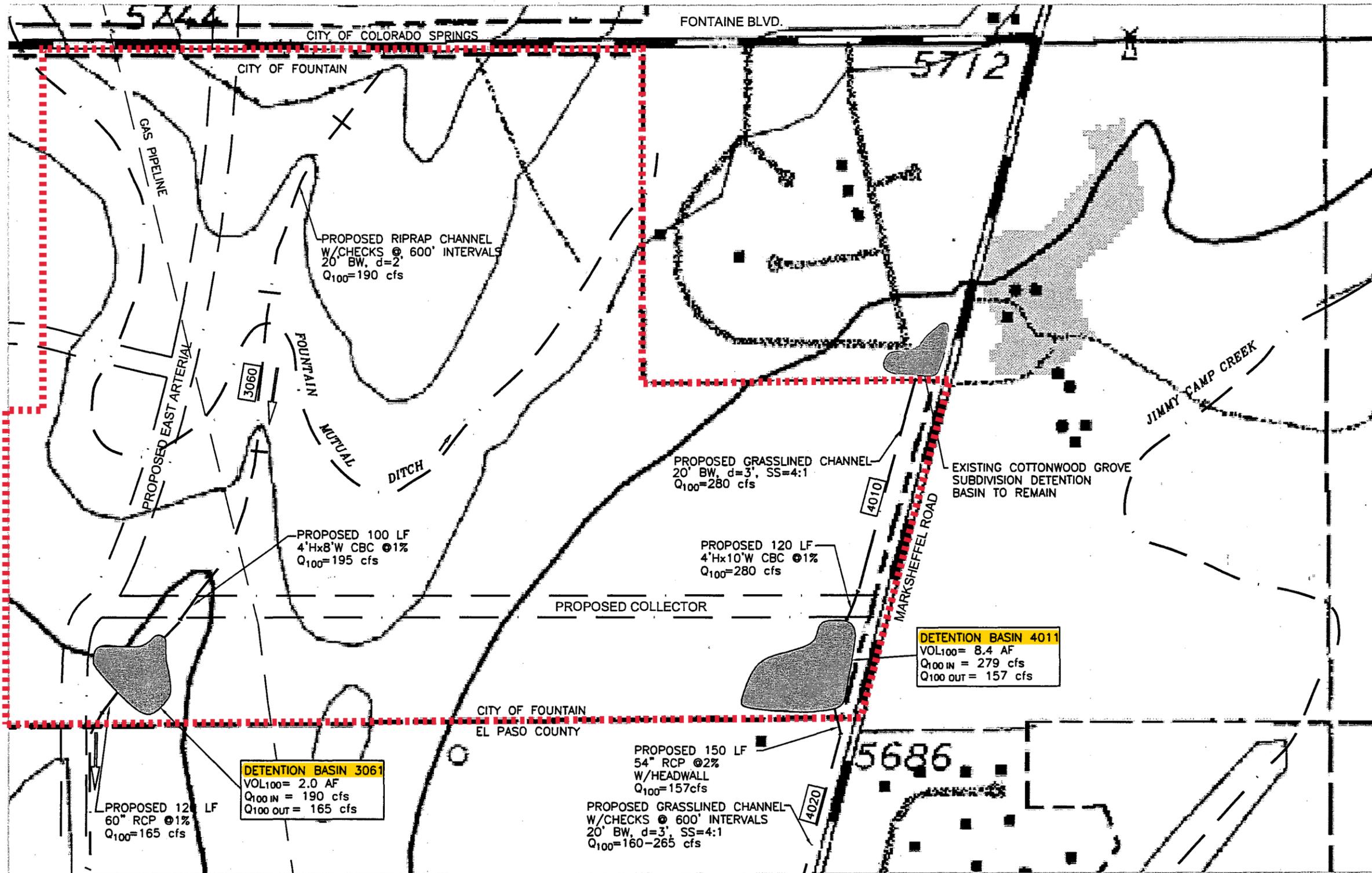
Kiowa Engineering Corporation
1604 South 21st Street
Colorado Springs, Colorado
80904
(719) 630-7342

WEST FORK JIMMY CAMP CREEK
DRAINAGE BASIN PLANNING STUDY
PRELIMINARY PLAN
EL PASO COUNTY, COLORADO

Project No.:	9893
Date:	7/00
Design:	RNW
Drawn:	CAD
Check:	RNW
Revisions:	

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.



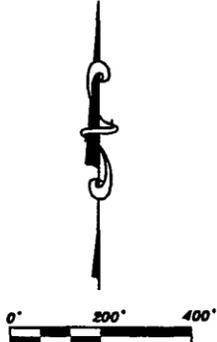


Kiowa Engineering Corporation
 1604 South 21st Street
 Colorado Springs, Colorado
 80904
 (719) 630-7342

**WEST FORK JIMMY CAMP CREEK
 DRAINAGE BASIN PLANNING STUDY**
 PRELIMINARY PLAN
 EL PASO COUNTY, COLORADO

Project No.:	9893
Date:	7/00
Design:	RNW
Drawn:	CAD
Check:	RNW
Revisions:	

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
 NOAA, NINGS12
 National Geodetic Survey
 SSMC-3, #9202
 1315 East-West Highway
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

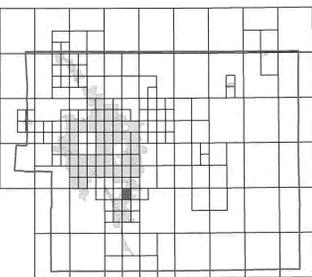
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FIMX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip>.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

LEGEND

- SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD
- The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equalled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.
- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decommissioned. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.
- FLOODWAY AREAS IN ZONE AE
- The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.
- OTHER FLOOD AREAS**
- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot, or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.
- OTHER AREAS**
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS
- OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation line and value; elevation in feet* (EL 987)

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

- Cross section line
- Transsect line
- Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 5000-foot grid ticks; Colorado State plane coordinate system, central zone (FIPSZONE 0902), Lambert Conformal Conic Projection
- Bench mark (see explanation in Notes to Users section of this FIRM panel)
- River Mile

MAP REPOSITORIES
 Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
 MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
 DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



PANEL 0956G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 956 OF 1300
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

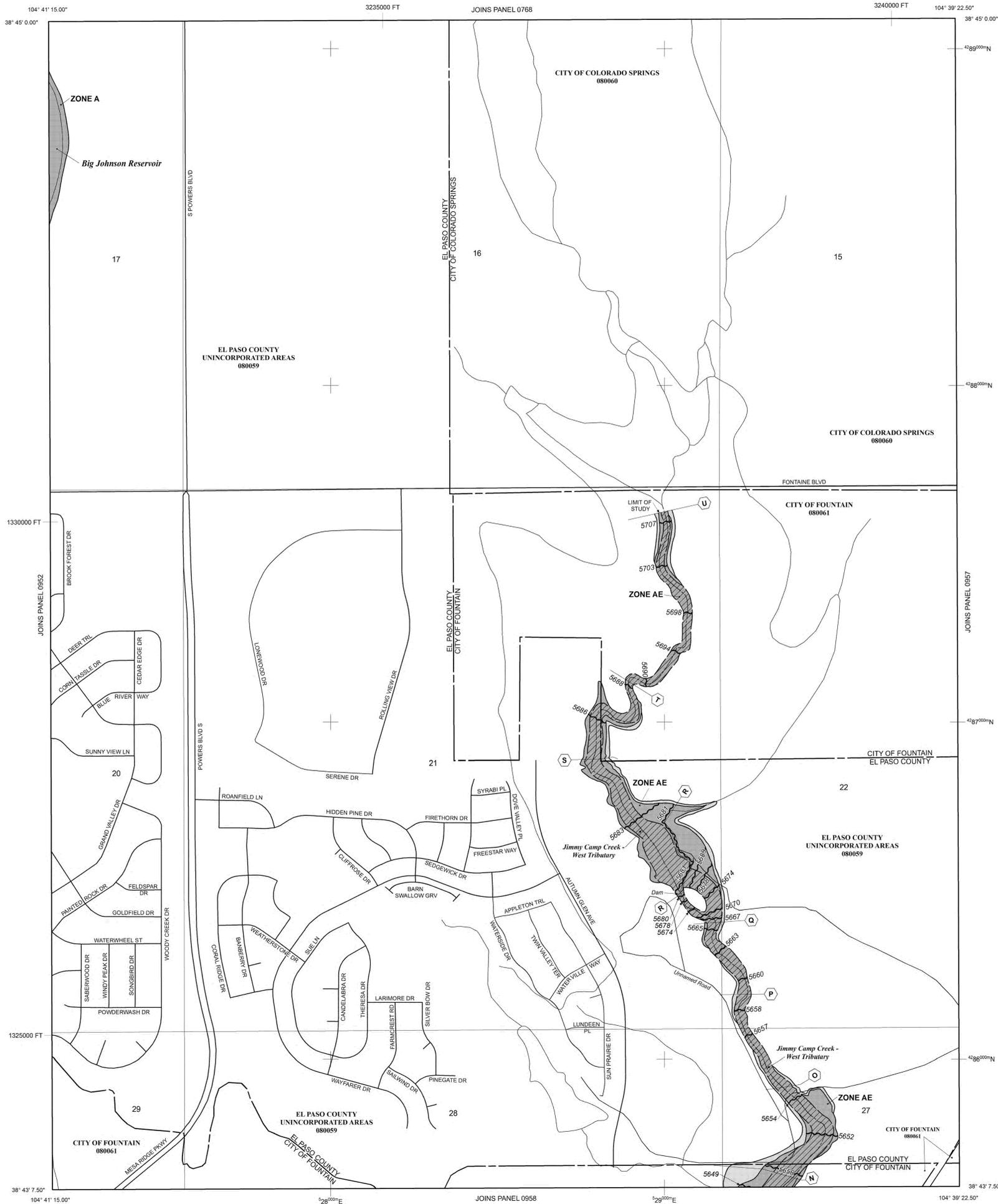
COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0956	G
EL PASO COUNTY	080259	0956	G
FOUNTAIN, CITY OF	080261	0956	G

Notice to User: The **Map Number** shown below should be used when placing map orders. The **Community Number** shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0956G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST.

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NIMS12
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FIMX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

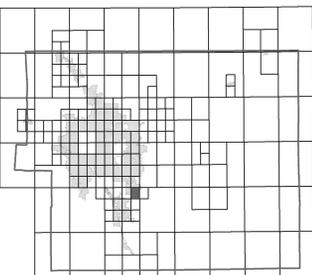
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP (1-877-336-2627)** or visit the FEMA website at <http://www.fema.gov/business/nfp>.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

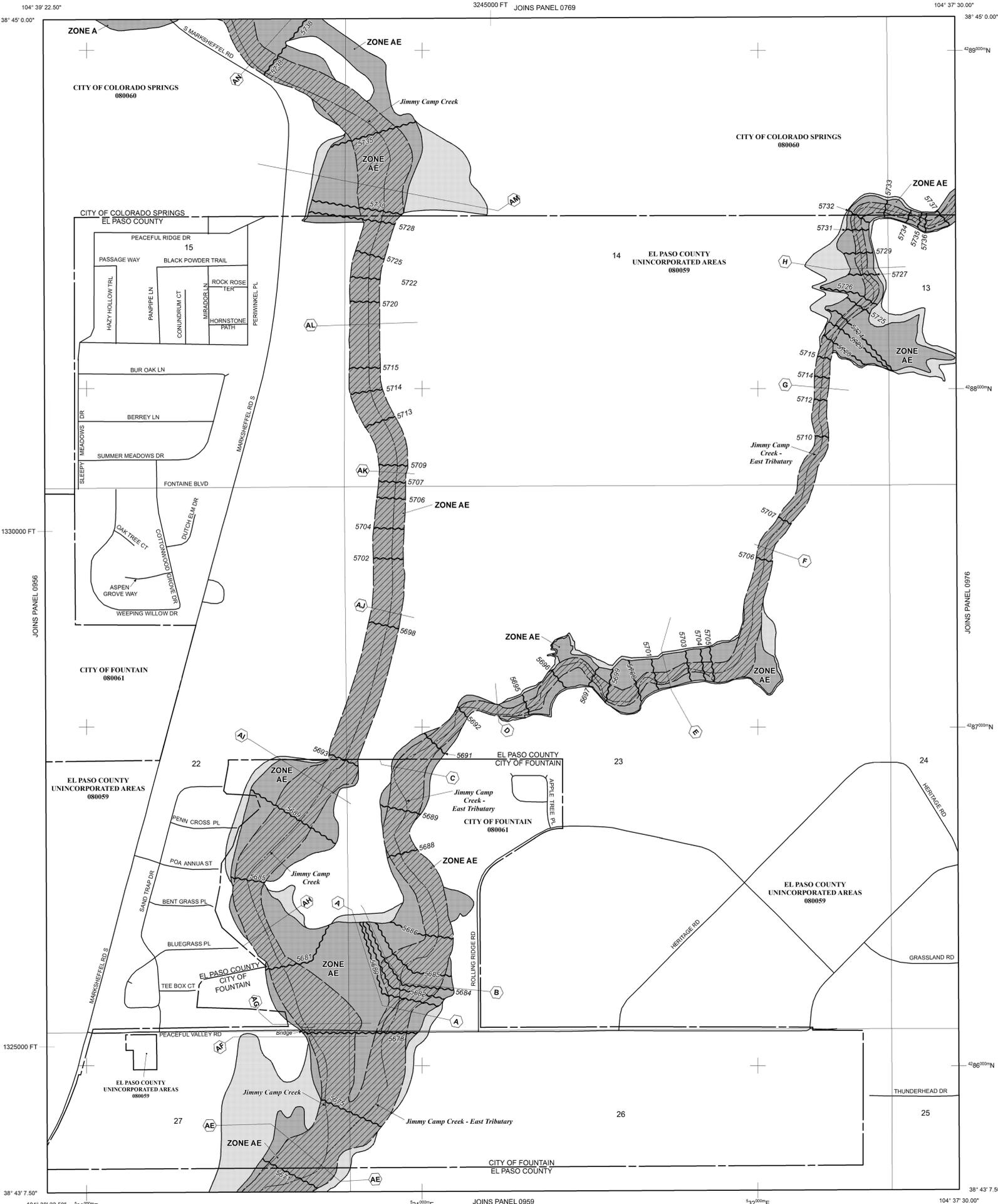
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST.

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equalled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE
The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS
ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot, or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

- OTHER AREAS**
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**
- OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D Boundary
- CBRS and OPA boundary

- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

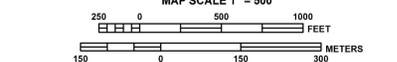
- Cross section line
- Transsect line
- Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection
- Bench mark (see explanation in Notes to Users section of this FIRM panel)
- River Mile

MAP REPOSITORIES
Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.
To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



NFIP **PANEL 0957G**

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 957 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	08060	0957	G
EL PASO COUNTY	08059	0957	G
FOUNTAIN, CITY OF	08061	0957	G

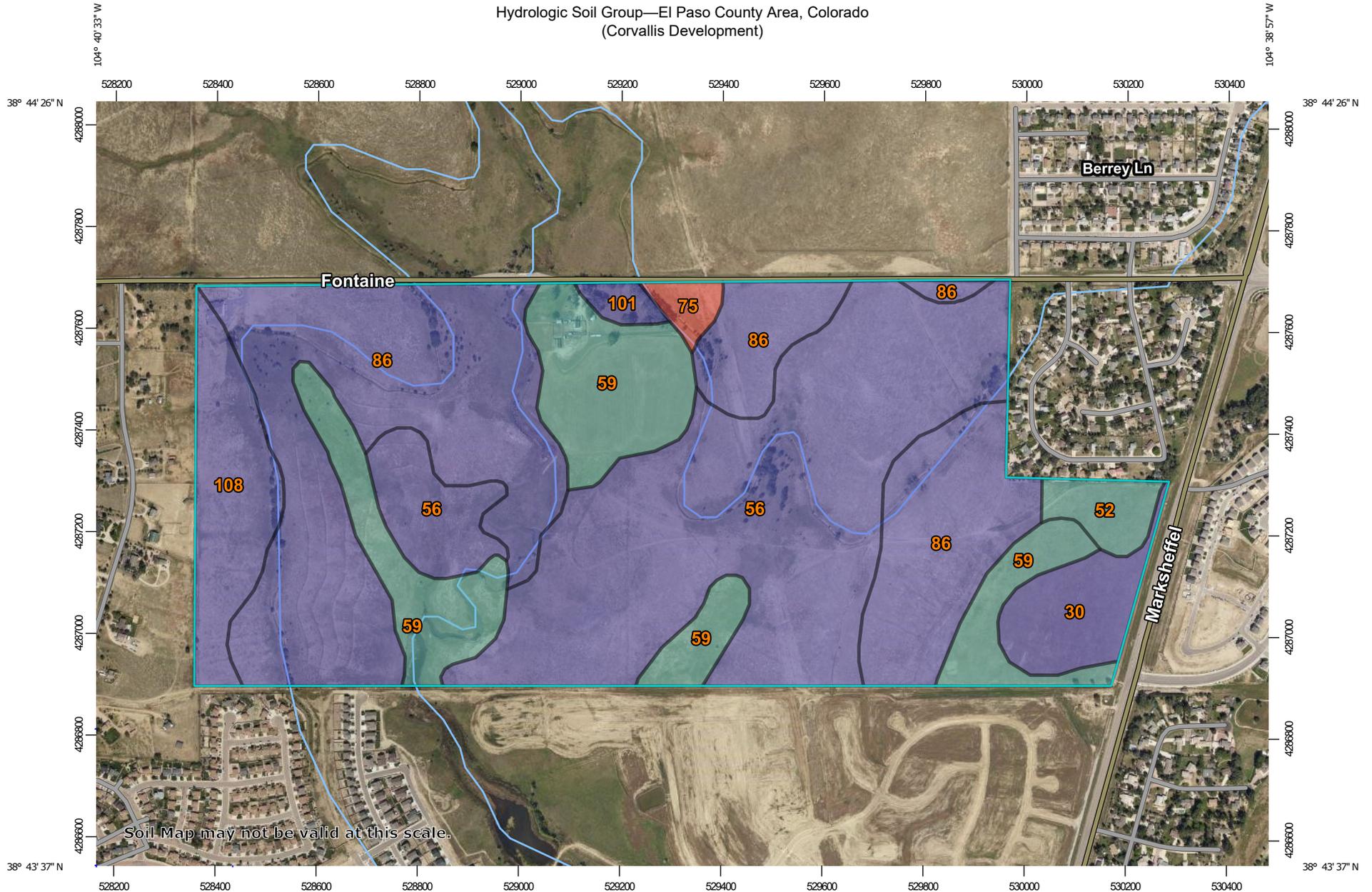
Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the Notice-to-User Letter that accompanied this correction for details.

Notice to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0957G

MAP REVISED
DECEMBER 7, 2018
Federal Emergency Management Agency

Hydrologic Soil Group—El Paso County Area, Colorado
(Corvallis Development)



Soil Map may not be valid at this scale.

Map Scale: 1:10,600 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84

Hydrologic Soil Group—El Paso County Area, Colorado
(Corvallis Development)

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

Soil Rating Polygons

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points

-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 17, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 14, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
30	Fort Collins loam, 0 to 3 percent slopes	B	13.3	3.9%
52	Manzanst clay loam, 0 to 3 percent slopes	C	6.3	1.8%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	B	118.2	34.5%
59	Nunn clay loam, 0 to 3 percent slopes	C	55.5	16.2%
75	Razor-Midway complex	D	3.1	0.9%
86	Stoneham sandy loam, 3 to 8 percent slopes	B	122.1	35.6%
101	Ustic Torrfluvents, loamy	B	2.6	0.8%
108	Wiley silt loam, 3 to 9 percent slopes	B	21.4	6.3%
Totals for Area of Interest			342.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

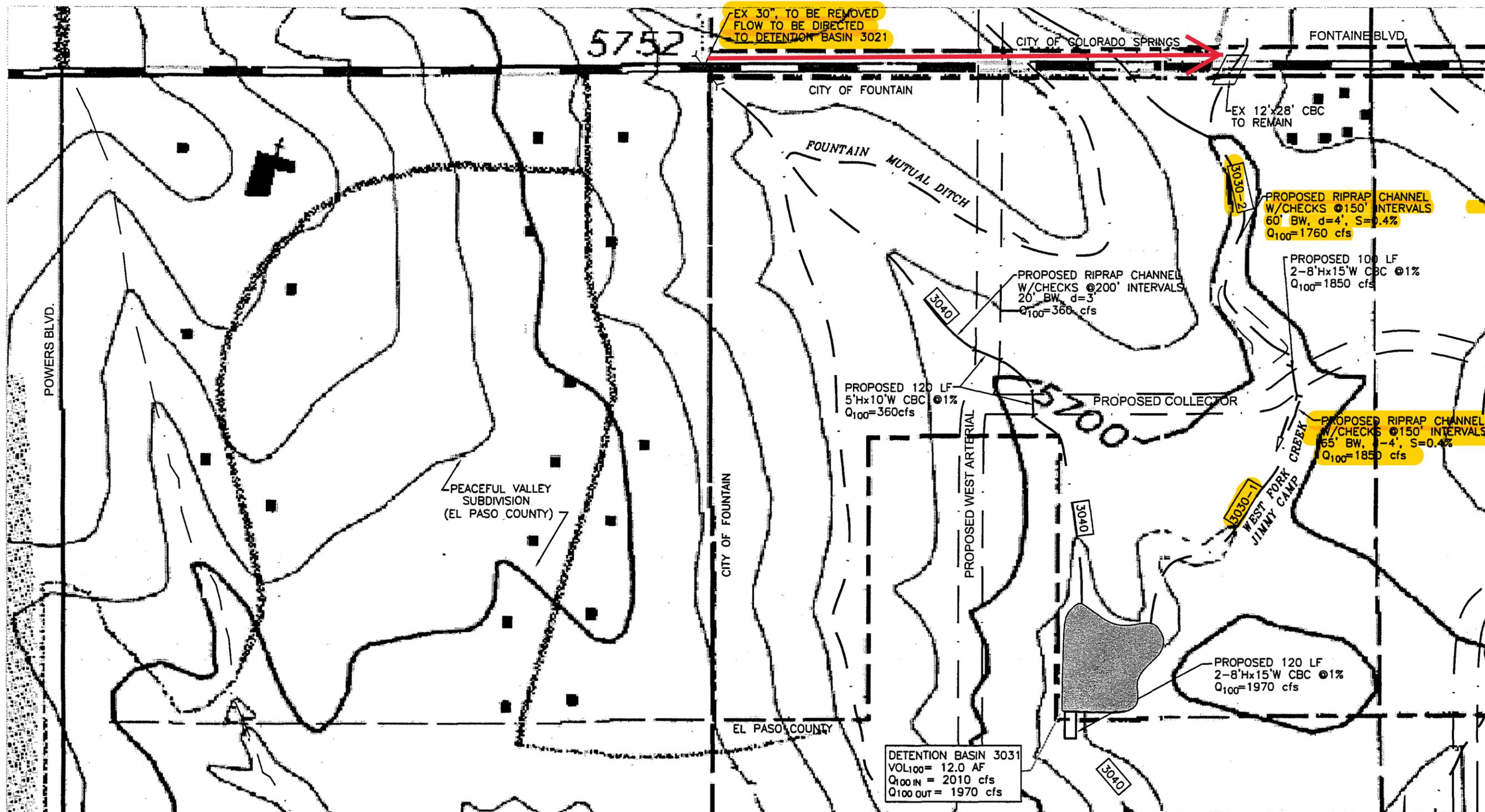
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



EX 30" TO BE REMOVED
FLOW TO BE DIRECTED
TO DETENTION BASIN 3021

DETENTION BASIN 3031
VOL₁₀₀ = 12.0 AF
Q_{100 IN} = 2010 cfs
Q_{100 OUT} = 1970 cfs

PROPOSED RIPRAP CHANNEL
W/CHECKS @150' INTERVALS
60' BW, d=4', S=0.4%
Q₁₀₀=1760 cfs

PROPOSED RIPRAP CHANNEL
W/CHECKS @200' INTERVALS
20' BW, d=3'
Q₁₀₀=360 cfs

PROPOSED 100 LF
2-8'Hx15'W CBC @1%
Q₁₀₀=1850 cfs

PROPOSED RIPRAP CHANNEL
W/CHECKS @150' INTERVALS
65' BW, d=4', S=0.4%
Q₁₀₀=1850 cfs

PROPOSED 120 LF
2-8'Hx15'W CBC @1%
Q₁₀₀=1970 cfs

Kiowa Engineering Corporation
1604 South 21st Street
Colorado Springs, Colorado
80904
(719) 630-7342

WEST FORK JIMMY CAMP CREEK
DRAINAGE BASIN PLANNING STUDY
PRELIMINARY PLAN
EL PASO COUNTY, COLORADO

Project No.:	9893
Date:	7/00
Design:	RNW
Drawn:	CAD
Check:	RNW
Revisions:	

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

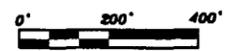


TABLE 2: SUMMARY OF SUB-BASIN DISCHARGES
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

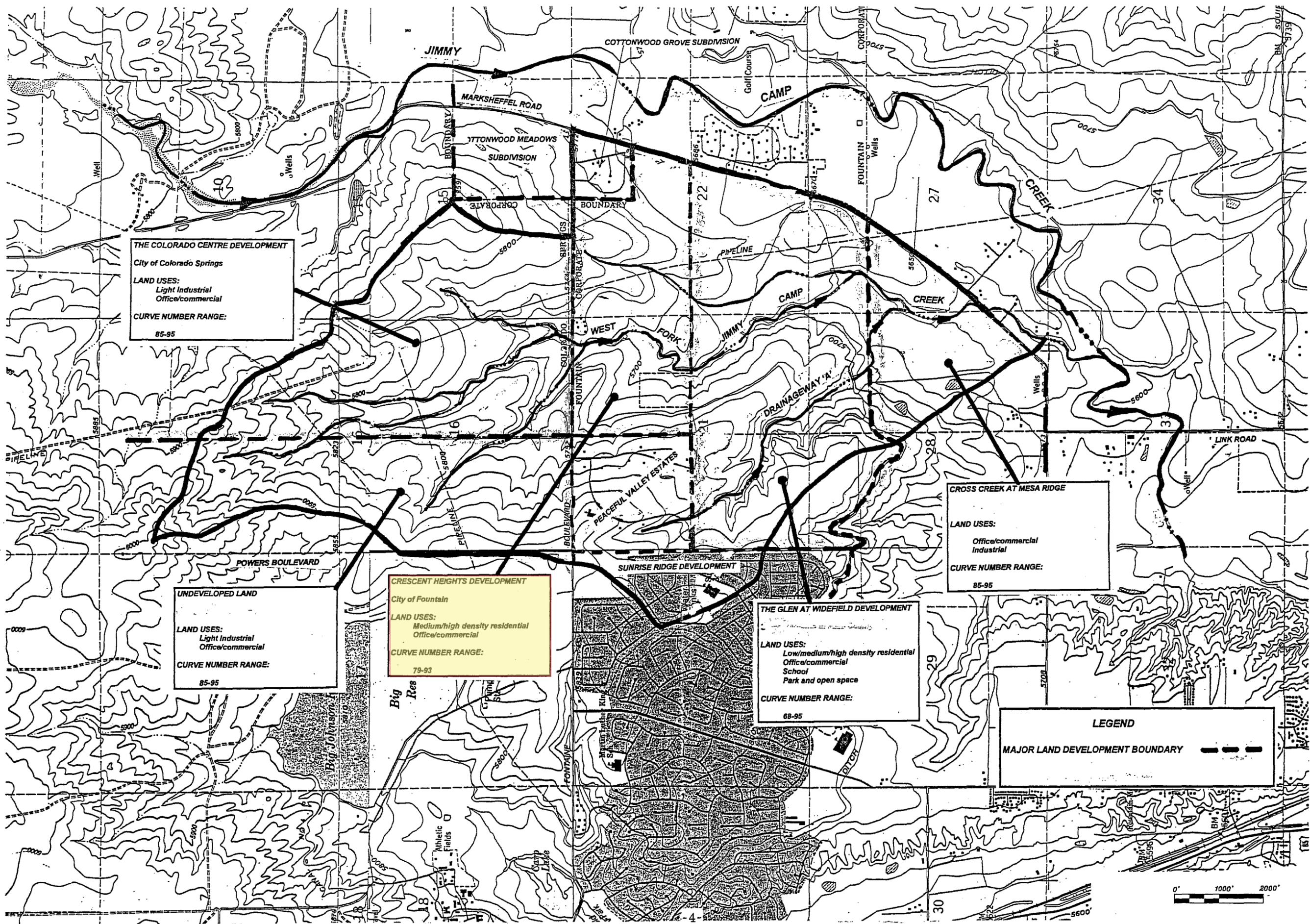
SUB-BASIN NUMBER	EX/FUT DRAINAGE AREA (sm)	EX/FUT DRAINAGE AREA (ac)	EXISTING CONDITION (cfs)		FUTURE CONDITION (cfs)	
			5 YR	100 YR	5 YR	100YR
2010	0.125	80.0	40	142	40	142
2020	0.062	39.7	9	47	19	68
2030	0.021	13.4	5	22	6	24
2040	0.026	16.6	5	26	7	29
2045	0.061	39.0	48	124	48	124
2050	0.020	12.8	4	17	4	19
2060	0.024	15.4	5	24	8	30
2070	0.068	43.5	8	44	17	65
2080	0.057	36.5	12	58	15	64
2090	0.019	12.2	3	14	5	19
2100	0.095	60.8	13	64	24	89
2110	0.034	21.8	6	29	8	33
2120	0.047	30.1	9	45	9	45
2130	0.010	6.4	2	11	2	11
2140	0.007	4.5	2	4	2	9
2150	0.015	9.6	6	20	6	21
2160	0.012	7.7	8	18	17	35
3000	0.420	268.8	140	474	190	568
3005	0.240	153.6	107	347	144	407
3010	0.220	140.8	81	288	138	383
3012	0.210	134.4	54	199	94	272
3015	0.110	70.4	55	181	75	212
3020	0.190	121.6	69	231	204	428
3025	0.260	166.4	82	324	347	712
3030	0.260	166.4	65	262	116	361
3035	0.160	102.4	63	234	106	306
3040	0.115	73.6	23	110	31	129
3050	0.049/074	31.4/47.4	18	61	56	136
3060	0.119	76.2	48	163	63	189
3070	0.077	49.3	23	78	27	87
3080	0.050	32.0	16	58	23	68
3090	0.082/05	52.5/32.0	27	93	21	67
3100	0.095	60.8	35	123	61	166
3110	0.018	11.5	5	17	14	31
4010	0.190	121.6	38	153	108	279
4020	0.135	86.4	26	90	39	114
4030	0.018	11.5	7	25	20	44
5010	0.156	99.8	35	133	101	246
5020	0.200	128.0	52	200	1514	362

TABLE 3: SUMMARY OF DESIGN POINT DISCHARGES
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

DESIGN POINT NUMBER	EX/FUT DRAINAGE AREA (sm)	EX/FUT DRAINAGE AREA (acres)	EXISTING CONDITION		FUTURE CONDITION	
			5 YR cfs	100 YR cfs	5 YR cfs	100YR cfs
2020	0.190	121.6	47	189	57	210
2040	0.300	192.0	97	335	109	362
2060	0.340	217.6	105	372	120	406
2080	0.130	83.2	17	88	28	113
2090	0.480	307.2	123	473	152	535
2100	0.610	390.4	140	558	181	651
2120	0.660	422.4	148	600	189	692
2130	0.670	428.8	145	594	186	687
2160	0.700	448.0	151	624	196	723
3000	0.660	422.4	147	233	317	935
3020	1.650	1056.0	528	1857	1059	2737
3030	2.070	1324.8	601	2216	1209	3267
3040	2.180	1395.2	618	2316	1239	3364
3050	2.26/2.23	1446/1427	627	2351	1275	3444
3070	0.200	128.0	67	235	86	270
3080	.25/.05	160/32	82	290	23	72
3090	.33/.11	211/70	106	373	44	138
3091	2.560	1638.4	732	2722	1380	3843
3100	2.660	1702.4	757	2828	1428	3990
3110	2.670	1708.8	761	2845	1442	4022
4020	0.320	204.8	63	238	145	383
5010	3.730	2387.2	943	3550	1722	4904

WFCC FLOWS @
SITE ENTRANCE

WFCC FLOWS @
SITE EXIT

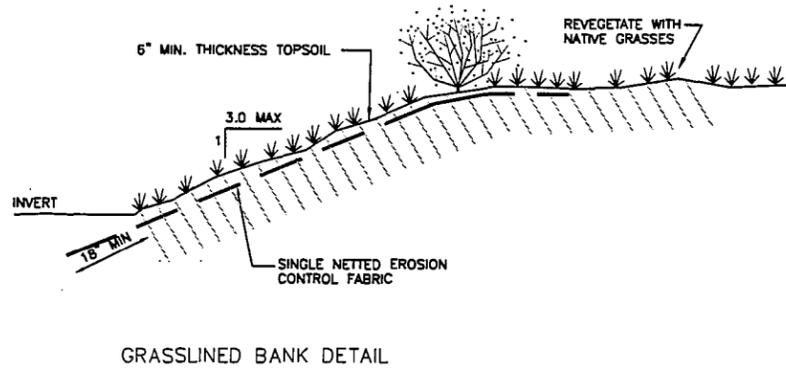


Kiowa Engineering Corporation
 1604 South 21st Street
 Colorado Springs, Colorado
 80904
 (719) 630-7342

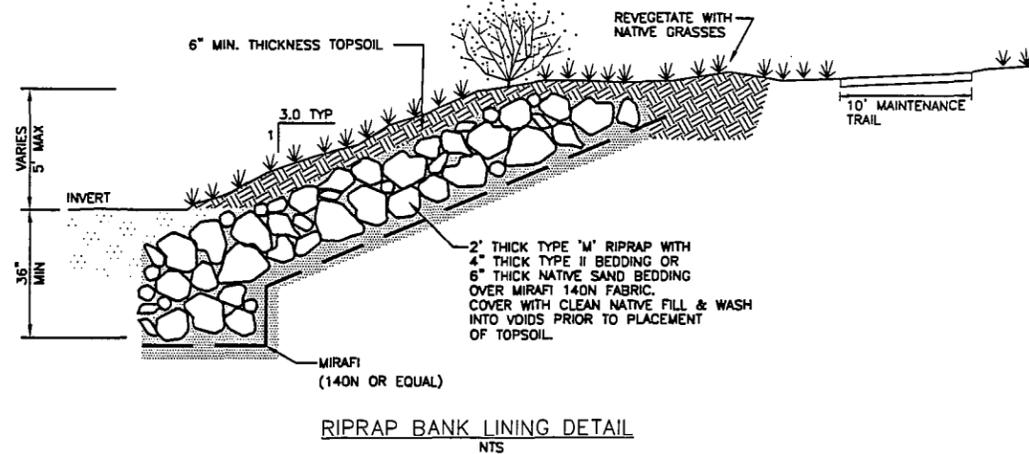
**West Fork Jimmy Camp Creek
 Drainage Basin Planning Study
 MAJOR DEVELOPMENT & LAND USE MAP**
 EL PASO COUNTY, COLORADO

Project No.: 9893
 Date: 6/99
 Design: RNW
 Drawn: CAD
 Check: RNW
 Revisions:

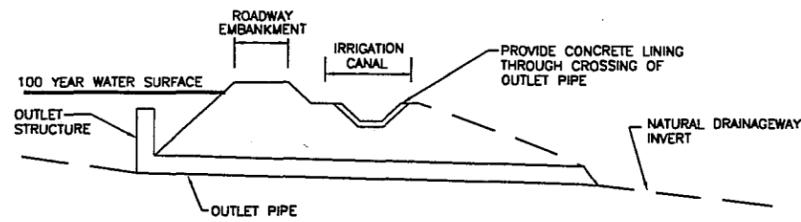
FIGURE 2



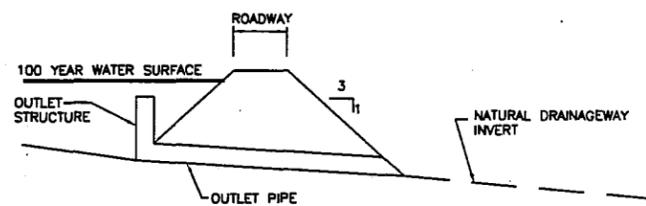
GRASSLINED BANK DETAIL



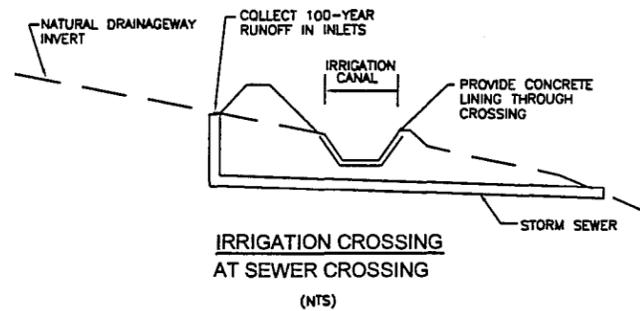
RIPRAP BANK LINING DETAIL
NTS



IRRIGATION CANAL CROSSING
AT DETENTION BASIN
(NTS)



IRRIGATION CROSSING WITH SIPHON
AT DETENTION BASIN
(NTS)



IRRIGATION CROSSING
AT SEWER CROSSING
(NTS)

RIPRAP GRADATIONS

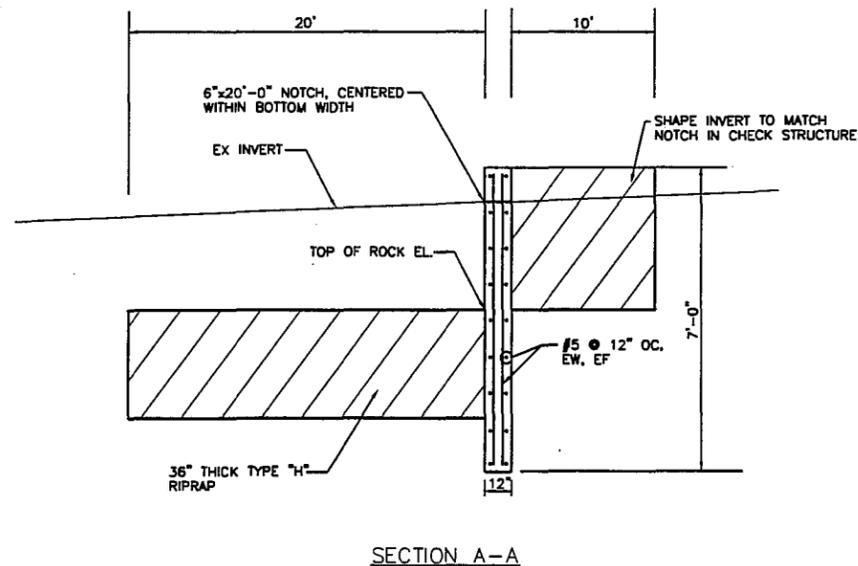
TYPE H RIPRAP INTERMEDIATE ROCK DIMENSION IN INCHES	% SMALLER THAN GIVEN SIZE BY WEIGHT	D ₅₀ INCHES
30	100	18
24	50-70	
18	35-50	
6	2-10	

TYPE M RIPRAP INTERMEDIATE ROCK DIMENSION IN INCHES	% SMALLER THAN GIVEN SIZE BY WEIGHT	D ₅₀ INCHES
21	100	12
18	50-70	
12	35-50	
4	2-10	

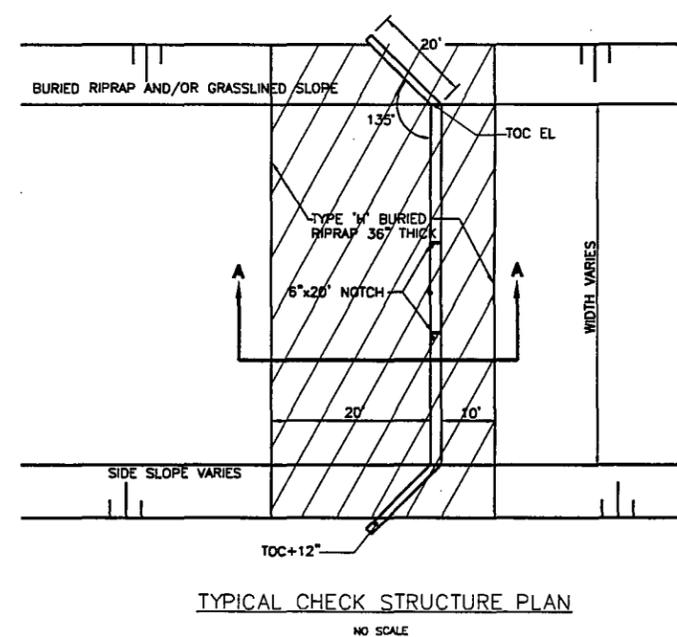
SEED MIX

AREAS DISTURBED BY THE EARTHWORK SHALL BE PERMANENTLY REVEGETATED WITH NATIVE GRASSES. NATIVE SEED MIX FOR THIS PROJECT SHALL BE AS FOLLOWS:

NATIVE SEED MIX		pls/acre
BLUE GRAMA	<i>Chondrosium hirsutum</i>	2.0
SIDEOATS GRAMA	<i>Bouteloua curtipendula</i>	3.0
SLENDER WHEATGRASS	<i>Agropyron trachycalum trachycalum</i>	2.0
WESTERN WHEATGRASS	<i>Agropyron smithii</i>	4.0
		11.0 lbs



SECTION A-A

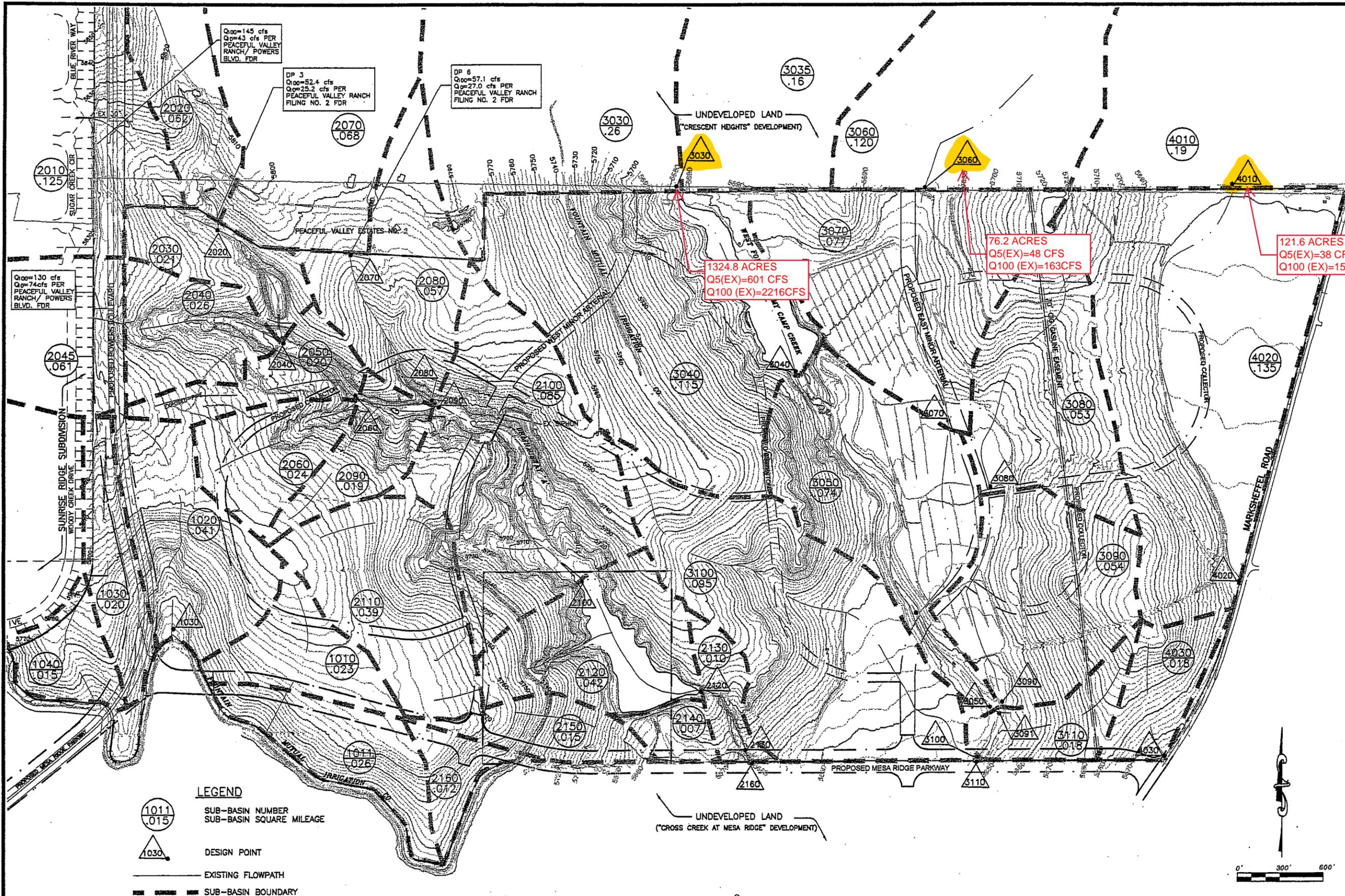


TYPICAL CHECK STRUCTURE PLAN
NO SCALE

Kiowa Engineering Corporation
1604 South 21st Street
Colorado Springs, Colorado
8004
(719) 630-7342

West Fork Jimmy Camp Creek
Drainage Basin Planning Study
TYPICAL DRAINAGEWAY DETAILS
EL PASO COUNTY, COLORADO

Project No.: 9893
Date: 7/00
Design: RNW
Drawn: CAD
Check: RNW
Revisions:



LEGEND

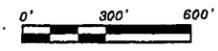
 SUB-BASIN NUMBER
 SUB-BASIN SQUARE MILEAGE

 DESIGN POINT

 EXISTING FLOWPATH

 SUB-BASIN BOUNDARY

UNDEVELOPED LAND
("CROSS CREEK AT MESA RIDGE" DEVELOPMENT)



Kiowa Engineering Corporation
 1604 S. 21st Street
 Colorado Springs, Colorado
 80904
 (719) 630-7342

**West Fork Jimmy Camp Creek
 Drainage Basin Planning Study
 HYDROLOGIC SUB-BASIN MAP
 EL PASO COUNTY, COLORADO**

Project No.:	9893
Date:	7/00
Design:	RNW
Drawn:	CAD
Check:	RNW
Revisions:	

FIG.3A



Figure 1-Existing 34" HDPE FMIC Pipe at Weeping Willow and Fontaine (Northeast of Corvallis)



Figure 2-Existing 56" x 38" CMAP FMIC Culvert across Fontaine



Figure 3-Existing 10' x 28' Concrete Box Culvert across Fontaine (Jimmy Camp Creek-West Fork)



Figure 4-Existing 69" x 46" CMAP FMIC Culvert across Fontaine



*Figure 5-Existing 29" x 19" CMAP Fontaine Road Ditch Across Rolling View Drive (Appears to be grouted in insert)
(NW of development)*



Figure 6-Existing 60" RCP FMIC Culvert in Glens at Widefield Filing No. 6 (South of Corvallis)



Figure 7-Existing 18" CMP and Embankment (Jimmy Camp Creek-West Fork) Located south of proposed Corvallis Development



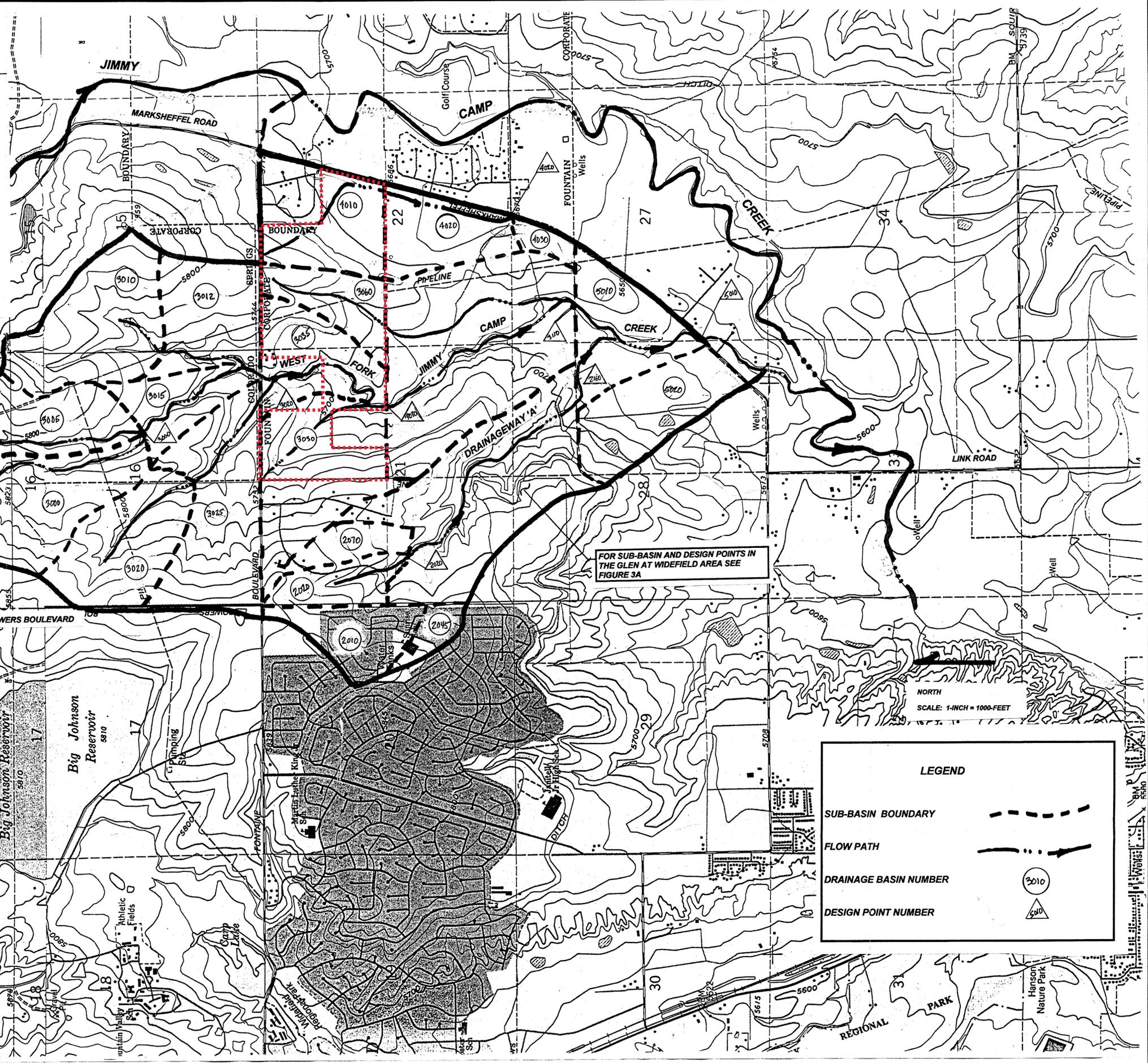
Figure 8-Existing 18" CMP and Embankment (Jimmy Camp Creek-West Fork) Located south of proposed Corvallis Development

TABLE 3: SUMMARY OF DESIGN POINT DISCHARGES
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

DESIGN POINT NUMBER	EX/FUT DRAINAGE AREA (sqm)	EX/FUT DRAINAGE AREA (acres)	EXISTING CONDITION		FUTURE CONDITION	
			5 YR cfs	100 YR cfs	5 YR cfs	100YR cfs
2020	0.190	121.6	47	189	57	210
2040	0.300	192.0	97	335	109	362
2060	0.340	217.6	105	372	120	406
2080	0.130	83.2	17	88	28	113
2090	0.480	307.2	123	473	152	535
2100	0.610	390.4	140	558	181	651
2120	0.660	422.4	148	600	189	692
2130	0.670	428.8	145	594	186	687
2160	0.700	448.0	151	624	196	723
3000	0.660	422.4	147	233	317	935
3020	1.650	1056.0	528	1857	1059	2737
3030	2.070	1324.8	601	2216	1209	3267
3040	2.180	1395.2	618	2316	1239	3364
3050	2.28/2.23	1446/1427	627	2351	1275	3444
3070	0.200	128.0	67	235	86	270
3080	25/05	160/32	82	290	23	72
3090	33/11	211/70	106	373	44	138
3091	2.560	1638.4	732	2722	1380	3843
3100	2.660	1702.4	757	2828	1428	3990
3110	2.670	1708.8	761	2845	1442	4022
4020	0.320	204.8	63	238	145	383
5010	3.530	2259.2	943	3550	1722	4904

TABLE 2: SUMMARY OF SUB-BASIN DISCHARGES
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

SUB-BASIN NUMBER	EX/FUT DRAINAGE AREA (sqm)	EX/FUT DRAINAGE AREA (ac)	EXISTING CONDITION (cfs)		FUTURE CONDITION (cfs)	
			5 YR	100 YR	5 YR	100YR
2010	0.125	80.0	40	142	40	142
2020	0.062	39.7	47	19	68	68
2030	0.021	13.4	5	22	6	24
2040	0.026	16.6	5	26	7	29
2045	0.061	39.0	48	124	48	124
2050	0.020	12.8	4	17	4	19
2060	0.024	15.4	5	24	6	30
2070	0.068	43.5	12	58	15	64
2080	0.057	36.5	3	14	5	19
2090	0.019	12.2	63	24	89	89
2100	0.056	36.8	6	29	8	33
2110	0.034	21.8	6	29	8	33
2120	0.047	30.1	2	11	2	11
2130	0.010	6.4	2	4	2	9
2140	0.007	4.5	6	20	6	21
2150	0.015	9.6	8	18	17	35
2160	0.012	7.7	8	18	17	35
3000	0.420	268.8	140	474	190	598
3005	0.240	153.6	107	347	144	407
3010	0.220	140.8	81	288	138	383
3012	0.210	134.4	54	199	94	272
3015	0.110	70.4	95	181	75	212
3020	0.190	121.6	89	231	204	428
3025	0.290	186.4	82	324	347	712
3030	0.290	186.4	85	262	116	391
3035	0.190	122.4	63	234	106	306
3040	0.190	122.4	23	110	31	129
3045	0.115	73.6	18	61	56	136
3050	0.049/074	31.447/4	48	163	63	189
3060	0.119	76.2	23	78	27	87
3070	0.077	49.3	16	58	23	68
3080	0.050	32.0	27	93	21	67
3090	0.062/05	52.532/0	63	123	61	166
3100	0.095	60.8	36	117	14	31
3110	0.018	11.5	5	17	14	31
4010	0.190	121.6	38	153	108	279
4020	0.135	86.4	26	90	39	114
4030	0.018	11.5	7	25	20	44
5010	0.156	99.8	35	133	101	248
5020	0.200	128.0	52	200	151/4	392



FOR SUB-BASIN AND DESIGN POINTS IN THE GLEN AT WIDEFIELD AREA SEE FIGURE 3A

LEGEND

- SUB-BASIN BOUNDARY: - - - - -
- FLOW PATH: - · - · -
- DRAINAGE BASIN NUMBER: (3010)
- DESIGN POINT NUMBER: (4010)

Kiowa Engineering Corporation
1604 South 21st Street
Colorado Springs, Colorado
80904
(719) 630-7342

**West Fork Jimmy Camp Creek
Drainage Basin Planning Study
HYDROLOGIC SUB-BASIN MAP**
EL PASO COUNTY, COLORADO

Project No.: 9893
Date: 6/99
Design: RNW
Drawn: CAD
Check: RNW
Revisions:

FIGURE 3

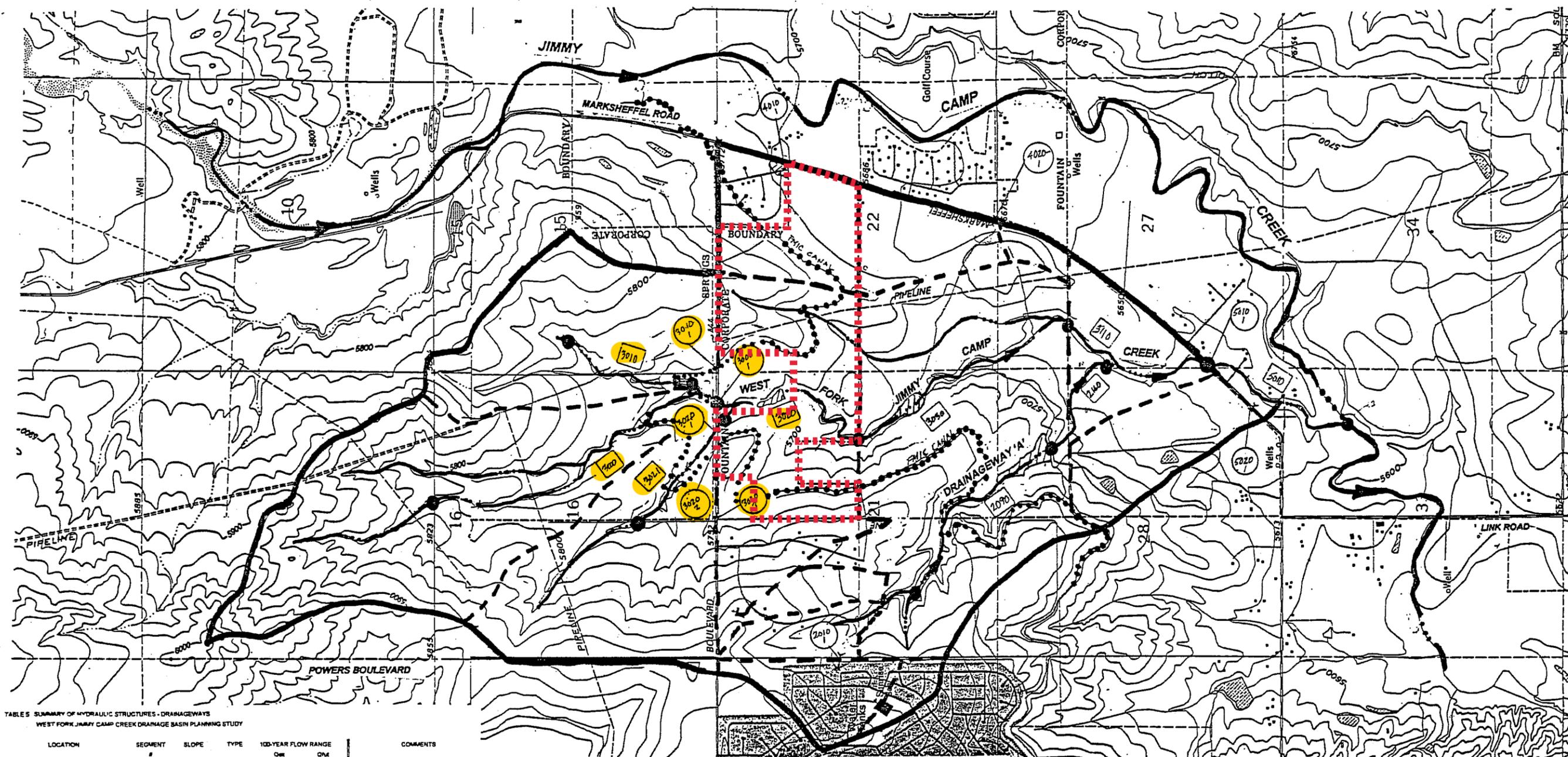


TABLE 3 SUMMARY OF HYDRAULIC STRUCTURES - DRAINAGEWAYS
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

LOCATION	SEGMENT #	SLOPE (Percent)	TYPE	100-YEAR FLOW RANGE		COMMENTS
				Old (cfs)	Old (cfs)	
WEST FORK JIMMY CAMP CREEK						
JIMMY CAMP CREEK TO MARKSHEFFEL ROAD	3010	0.2	UNIMPROVED	3,500	4,800	DRAINAGEWAY OUTFALLS TO JIMMY CAMP CREEK
MARKSHEFFEL ROAD TO MESA RIDGE PARKWAY	3110	0.6	UNIMPROVED	2,800-3,500	3,300-4,800	WIDE AND SHALLOW FLOODPLAIN
MESA RIDGE PARKWAY TO N PL OF THE GLEN	3000	0.7	UNIMPROVED	2,275-2,800	3,150-3,300	CHANNEL STABLE AND WELL VEGETATED WITH WETLAND AND NATIVE GRASSES
NORTH PL OF THE GLEN TO FONTAINE BOULEVARD	3000	0.8	UNIMPROVED	1,900-2,275	2,710-3,150	
FONTAINE BLVD TO STUDY LIMITS	3000	1.0	UNIMPROVED	800	1,050	CHANNEL LIES WITHIN COLORADO CENTRE DEVELOPMENT
FONTAINE BLVD TO STUDY LIMITS	3010	1.0	UNIMPROVED	400	640	CHANNEL LIES WITHIN COLORADO CENTRE DEVELOPMENT
FONTAINE BLVD TO STUDY LIMITS	3021	0.8	UNIMPROVED	600	1,100	CHANNEL LIES WITHIN COLORADO CENTRE DEVELOPMENT
DRAINAGEWAY A						
CONFLUENCE WITH WEST FORK JIMMY TO LAKE	2180	2.6	UNIMPROVED	600	700	
LAKE TO DESIGN POINT OF 2000	3300	1.8	UNIMPROVED	335-600	390-700	CHANNEL STABLE AND WELL VEGETATED WITH WETLAND AND NATIVE GRASSES

TABLE 4 SUMMARY OF HYDRAULIC STRUCTURES - CROSSINGS
WEST FORK JIMMY CAMP CREEK DRAINAGE BASIN PLANNING STUDY

LOCATION	CULVERT #	SIZE	TYPE	PROPOSED FLOW		CAPACITY EXISTING	CAPACITY FUTURE (I)	COMMENTS
				OS (cfs)	O100 (cfs)			
FONTAINE BLVD	3000-1	12'-0"	CBC	770	1,070	ADEQUATE	ADEQUATE	STRUCTURE HAS ADEQUATE CAPACITY TO PASS THE PROPOSED 100-YEAR FLOW
FONTAINE BLVD	3010-1	30'-5"	CMP ARCH	N/A	N/A	N/A	N/A	FONTAINE MUTUAL IRRIGATION DITCH ROADWAY CROSSING
FONTAINE BLVD	3020-1	30'	CMP	500	1,100	INADEQUATE	INADEQUATE	CULVERT CAN CONVEY ONLY LOCALIZED ROADWAY DRAINAGE WHICH REACHES IT
FONTAINE BLVD	3020-2	30'-5"	CMP ARCH	NA	NA	N/A	N/A	FONTAINE MUTUAL IRRIGATION DITCH ROADWAY CROSSING
FONTAINE BLVD	3020-3	30'	CMP	N/A	N/A	ADEQUATE	INADEQUATE	CULVERT CAN CONVEY ONLY LOCALIZED ROADWAY DRAINAGE WHICH REACHES IT
MARKSHEFFEL ROAD	3010-1	30'	CMP	1,700	4,800	INADEQUATE	INADEQUATE	PARTIALLY PLUGGED
MARKSHEFFEL ROAD	3020-1	30'	CMP	100	300	INADEQUATE	INADEQUATE	PARTIALLY PLUGGED
POWERS BOULEVARD	2010-1	30'	CMP	40	142	ADEQUATE	ADEQUATE	CULVERT TO BE REPLACED WITH CONSTRUCTION OF POWERS BOULEVARD
MARKSHEFFEL ROAD	4010-1	N/A	DETENTION BASIN	N/A	N/A	ADEQUATE	ADEQUATE	DETENTION BASIN SERVES THE COTTONWOOD GROVE SUBDIVISION
MARKSHEFFEL ROAD	4020-1	30' (wall)	CMP	145	383	INADEQUATE	INADEQUATE	PARTIALLY PLUGGED

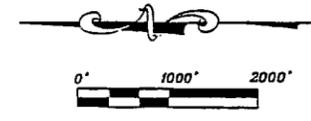
LEGEND

ROADWAY CROSSING DESIGNATION 

DRAINAGEWAY DESIGNATION 

FONTAINE MUTUAL IRRIGATION DITCH 

EXISTING IMPOUNDMENT 

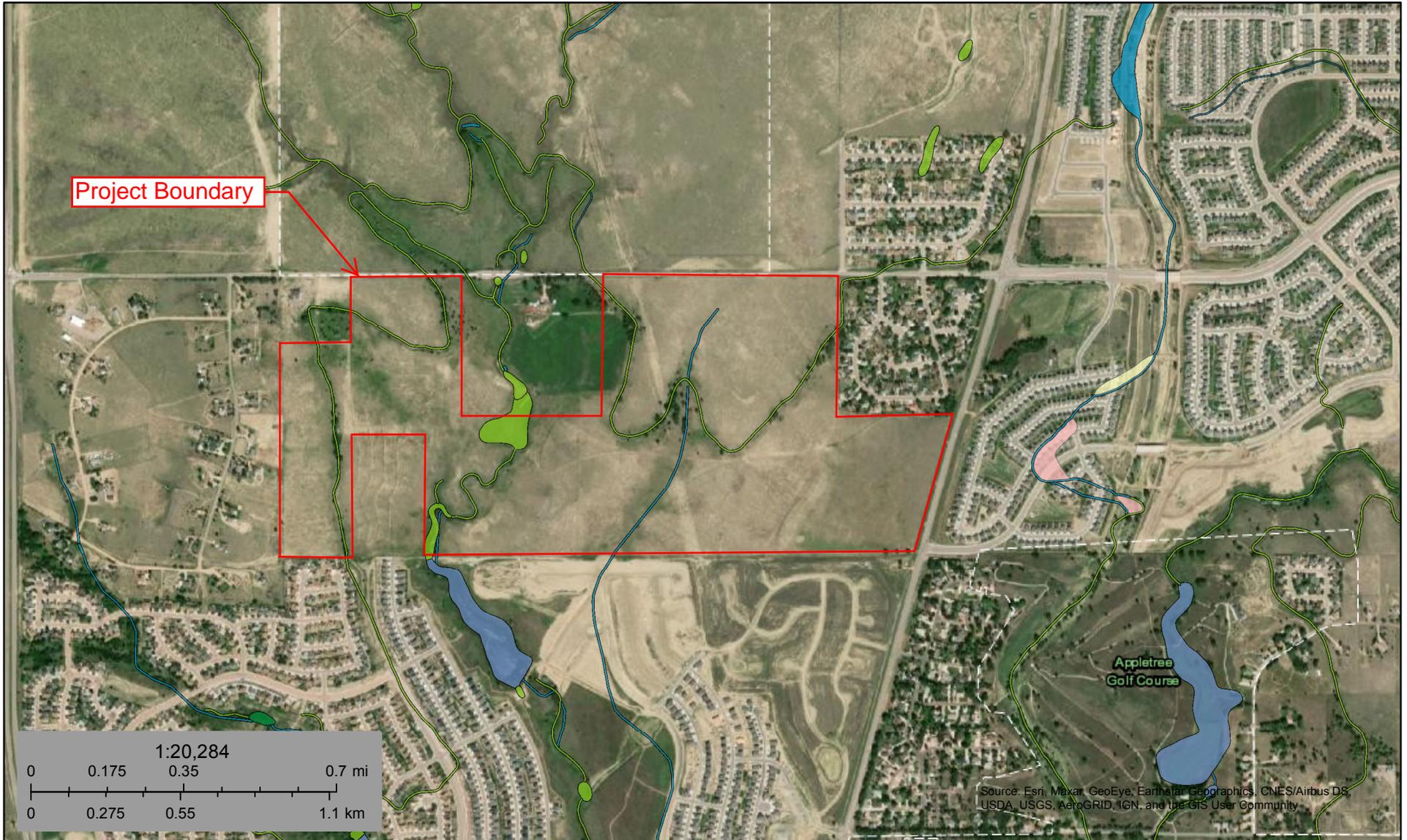


Kiowa Engineering Corporation
 1604 South 21st Street
 Colorado Springs, Colorado
 80904
 (719) 630-7342

**West Fork Jimmy Camp Creek
 Drainage Basin Planning Study
 INVENTORY OF EXISTING DRAINAGE STRUCTURES
 EL PASO COUNTY, COLORADO**

Project No.: 9893
 Date: 6/99
 Design: RNW
 Drawn: CAD
 Check: RNW
 Revision:

FIGURE 4



September 10, 2020

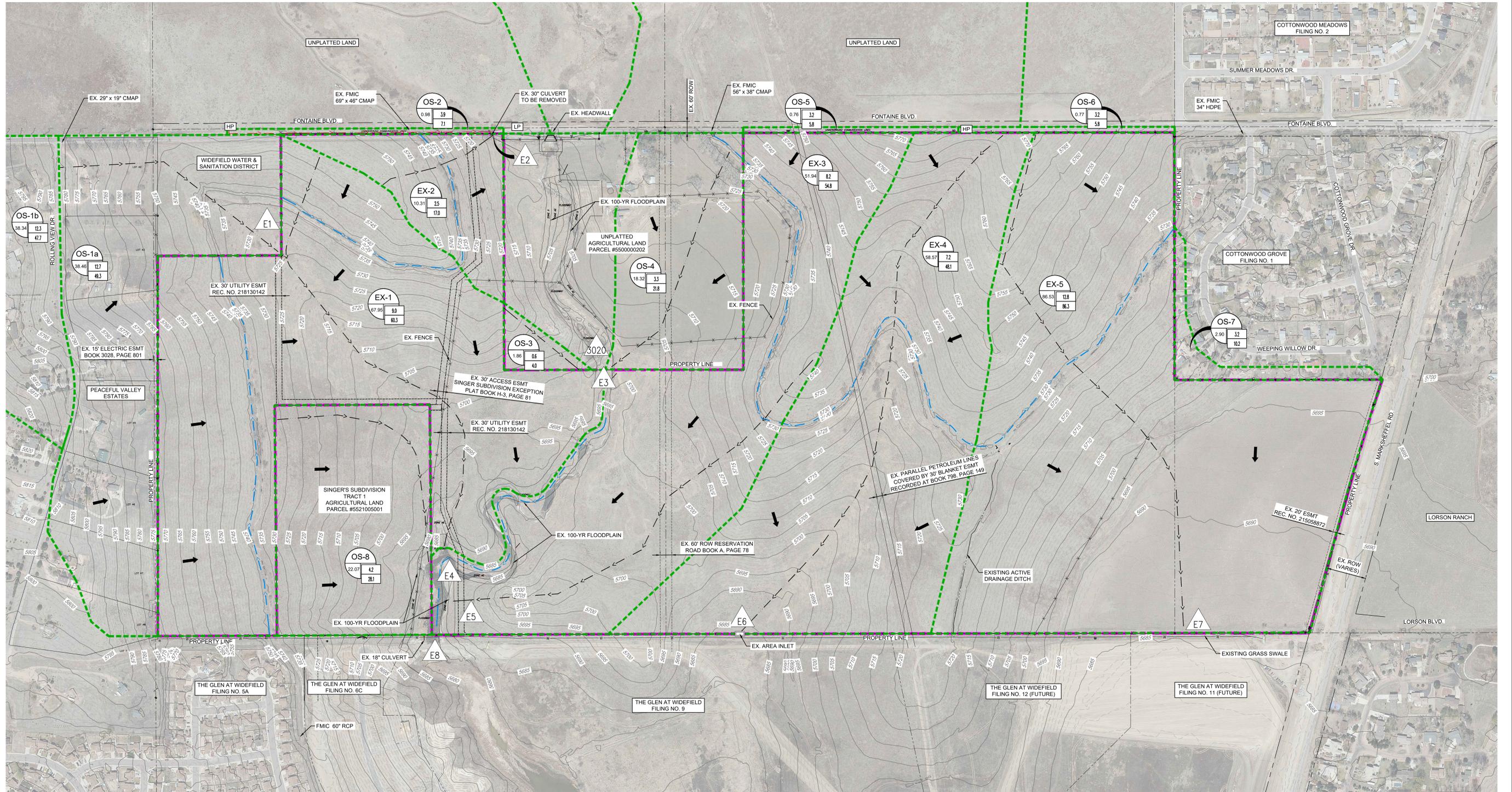
Wetlands

- | | | |
|--------------------------------|-----------------------------------|----------|
| Estuarine and Marine Deepwater | Freshwater Emergent Wetland | Lake |
| Estuarine and Marine Wetland | Freshwater Forested/Shrub Wetland | Other |
| | Freshwater Pond | Riverine |

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.

APPENDIX D

MAPS



Corvallis Existing Conditions Basin Summary Table

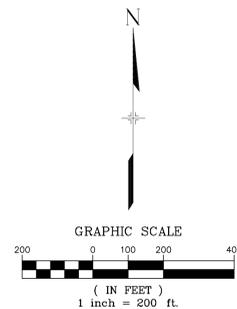
Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)
OS-1a	38.5	19.2	70.9
OS-1b	38.3	12.3	47.7
OS-2	1.0	3.9	7.1
OS-3	1.9	0.6	4.0
OS-4	18.3	3.3	21.8
OS-5	0.8	3.2	5.8
OS-6	0.8	3.2	5.8
OS-7	2.9	2.5	9.4
OS-8	22.1	4.2	28.1
EX-1	67.9	9.0	60.3
EX-2	10.3	2.5	17.0
EX-3	51.9	8.2	54.8
EX-4	58.6	7.2	48.1
EX-5	86.5	12.8	86.3

Corvallis Existing Conditions Design Point Summary Table

Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)
E1: OS-1	38.5	19.2	70.9
E2: OS-2, EX-2	11.3	5.4	22.5
E3: E2, OS-3, OS-4	31.5	6.5	34.4
E4: E1, E3, EX-1, OS-8	160.0	52.4	264.0
E5: OS-5, EX-3	52.7	10.2	57.5
E6: EX-4	58.6	7.2	48.1
E7: EX-5, OS-6, OS-7	90.2	16.5	93.1
E8: E4, E5, +DPBS020	212.7	590.5	2178.5

LEGEND

- EXISTING BASIN BOUNDARY
- EXISTING CONTOUR
- DRAINAGE CHANNEL
- PROPOSED PROPERTY LINE
- EXISTING FLOW DIRECTION
- EXISTING FLOW PATH
- DESIGN POINT
- SUB BASIN DESIGNATION
- 5-YEAR STORM EVENT PEAK FLOW (CFS)
- 100-YEAR STORM EVENT PEAK FLOW (CFS)
- SUB BASIN AREA (AC.)



PREPARED BY:



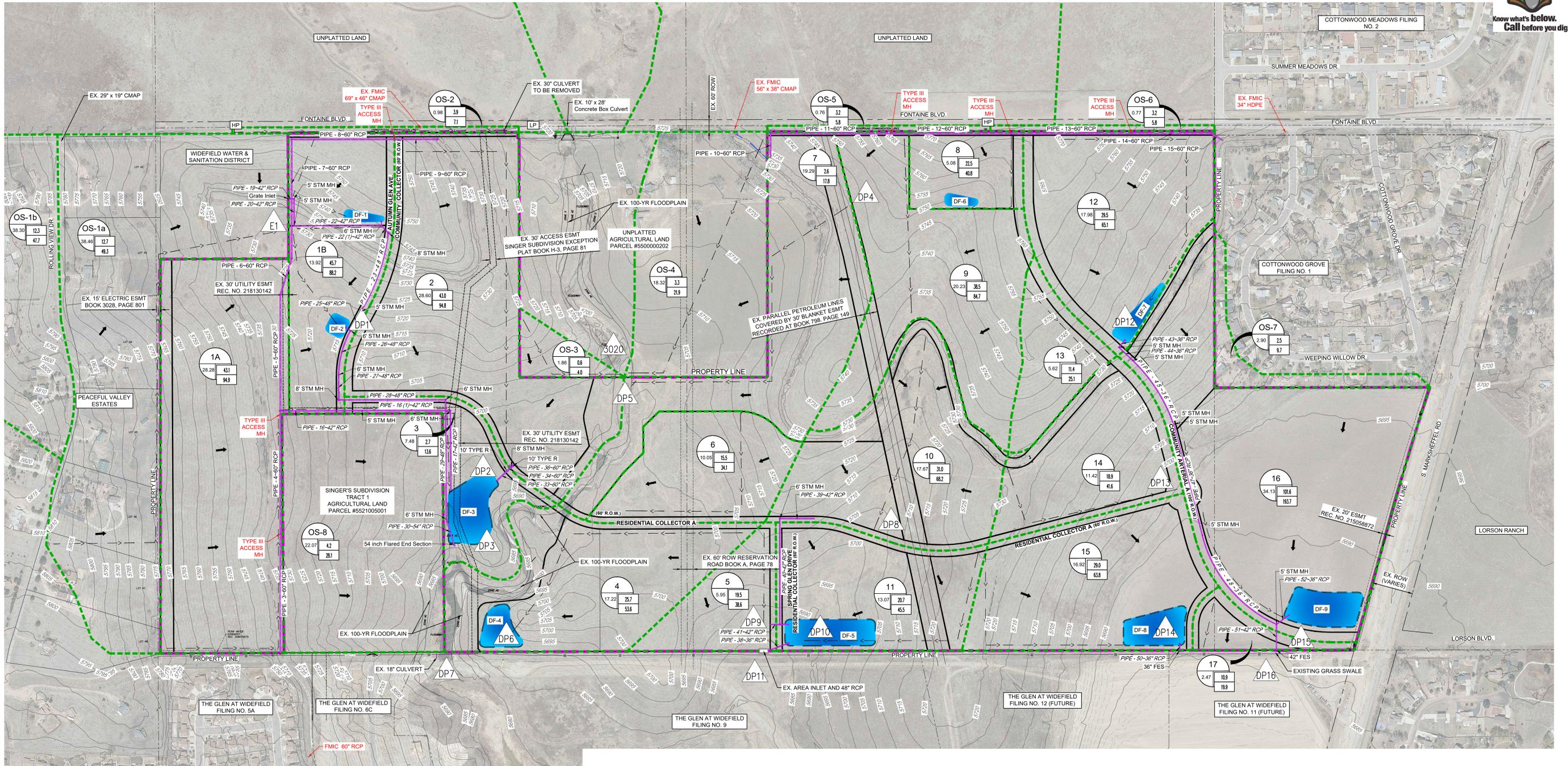
2435 Research Pkwy, Suite 300
Colorado Springs, CO 80920
Phone 719.575.0100

CORVALLIS

MASTER DRAINAGE DEVELOPMENT PLAN
FOUNTAIN, CO

EXISTING CONDITIONS

DESIGNED BY: NMS SCALE: DATE ISSUED: JANUARY 2021 DRAWING No: DR01
DRAWN BY: JTS HORIZ: 1" = 200' SHEET: 01 OF 04
CHECKED BY: NMS VERT: N/A

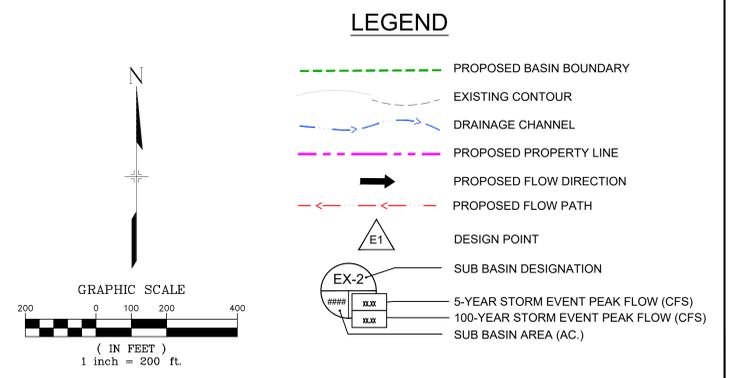


Corvallis Proposed Conditions Basin Summary Table

Area ID	Area (Acres)	Q5 (cfs)	Q100 (cfs)
OS-1a	38.46	12.7	49.3
OS-2	0.98	3.9	7.1
OS-3	1.86	0.6	4.0
OS-4	18.32	3.3	21.9
OS-5	0.76	3.2	5.8
OS-6	0.77	3.2	5.8
OS-7	2.90	2.5	9.4
OS-8	22.07	4.2	28.1
1A	28.28	43.1	94.9
1B	13.92	45.7	88.2
2	28.60	43.0	94.8
3	7.48	2.7	13.6
4	17.22	25.7	53.6
5	5.95	19.5	38.6
6	10.05	15.5	34.1
7	19.29	2.6	17.8
8	5.08	22.5	40.8
9	20.23	38.5	84.7
10	17.67	31.0	68.2
11	13.07	20.7	45.5
12	17.98	29.5	65.1
13	5.62	11.4	25.1
14	11.42	18.9	41.6
15	16.92	29.0	63.8
16	34.13	101.6	193.7
17	2.47	10.9	19.9

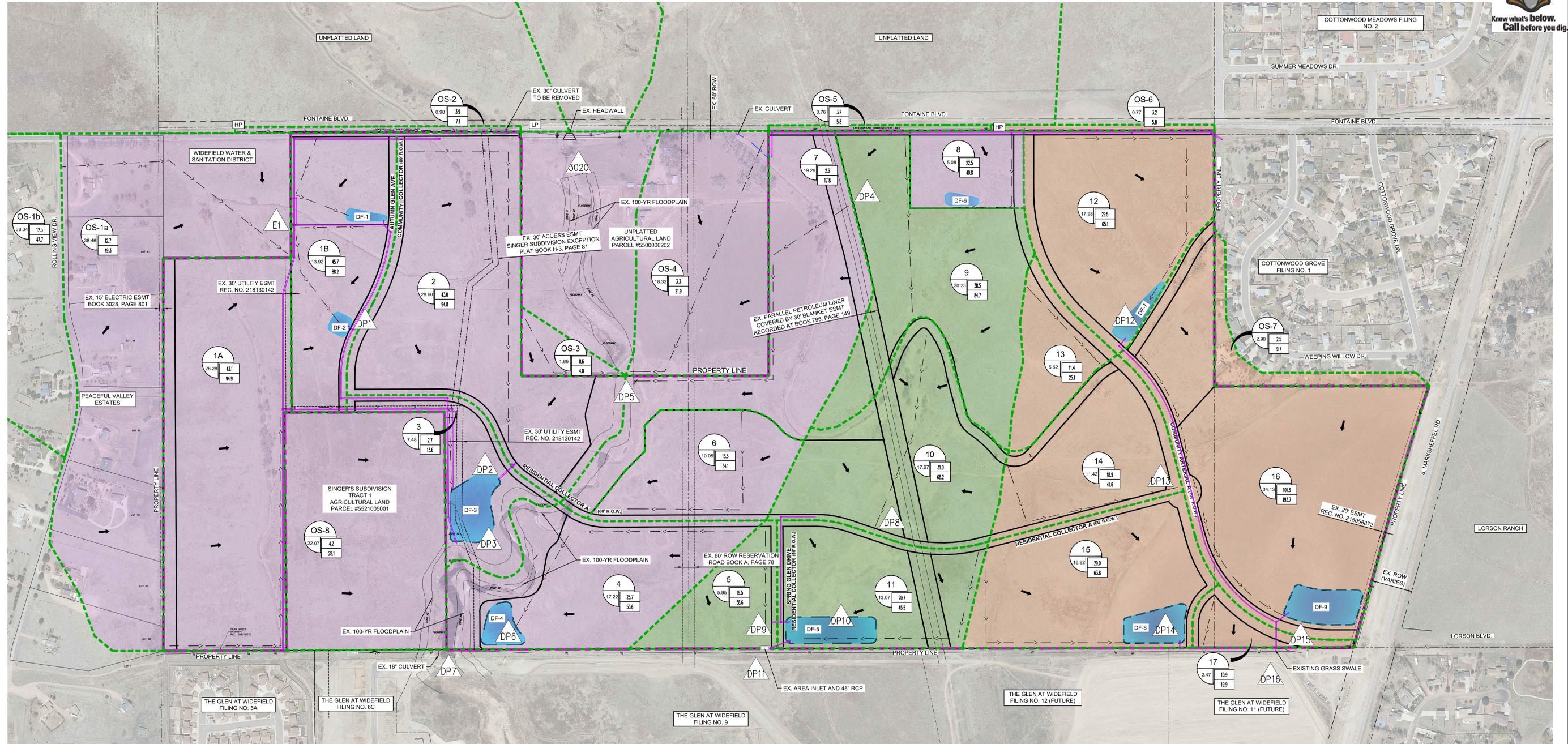
Corvallis Proposed Conditions Design Point Summary Table

Design Point	Description	Area (Acres)	Q5 (cfs)	Q100 (cfs)
E1	OS-1a and OS-1b	76.8	21.7	84.4
DP1	E1+DF-1 Release+DF-2 Release	105.0	25.0	107.0
DP2	OS-2, 1A, 2, 3	65.3	91.4	212.1
DP3	DP1+DP2 Treated (DF-3 Release)+OS-8	192.4	44.9	196.3
DP4	7+8+9+10+6 (Release)	24.4	4.8	26.6
DP5	OS-3, OS-4, DPBS 3020, DP4	75.0	536.7	1909.4
DP6	4, 6	27.3	22.4	47.3
DP7	DP5+DP6+DP6 Treated (DF-4 Release)	294.7	586.3	2127.7
DP8	9, 10, OS-5	38.7	54.5	119.5
DP9	DP8, 5	44.6	38.1	82.4
DP10	DP9, 11	57.7	60.3	130.9
DP11	DP10 Treated (DF-5 Release)	57.7	7.2	48.1
DP12	OS-6, 12	18.8	25.6	55.7
DP13	13, 14	17.0	21.2	46.8
DP14	DP13, 15, 17	36.4	33.8	73.3
DP15	DP12 Treated (DF-7 Release), 16 Treated (DF-9 Release)	52.9	17.5	74.1
DP16	DP14 Treated (DF-8 Release)+DP15	89.3	28.5	121.9



PREPARED BY:
Matrix
2435 Research Pkwy, Suite 300
Colorado Springs, CO 80920
Phone 719.575.0100

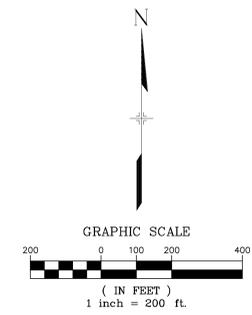
CORVALLIS			
MASTER DRAINAGE DEVELOPMENT PLAN FOUNTAIN, CO			
PROPOSED CONDITIONS			
DESIGNED BY: NMS	SCALE: HORIZ. 1" = 200'	DATE ISSUED: JANUARY 2021	DRAWING No. DR02
DRAWN BY: JTS	VERT. NA	SHEET 02 OF 04	
CHECKED BY: NMS			



LEGEND

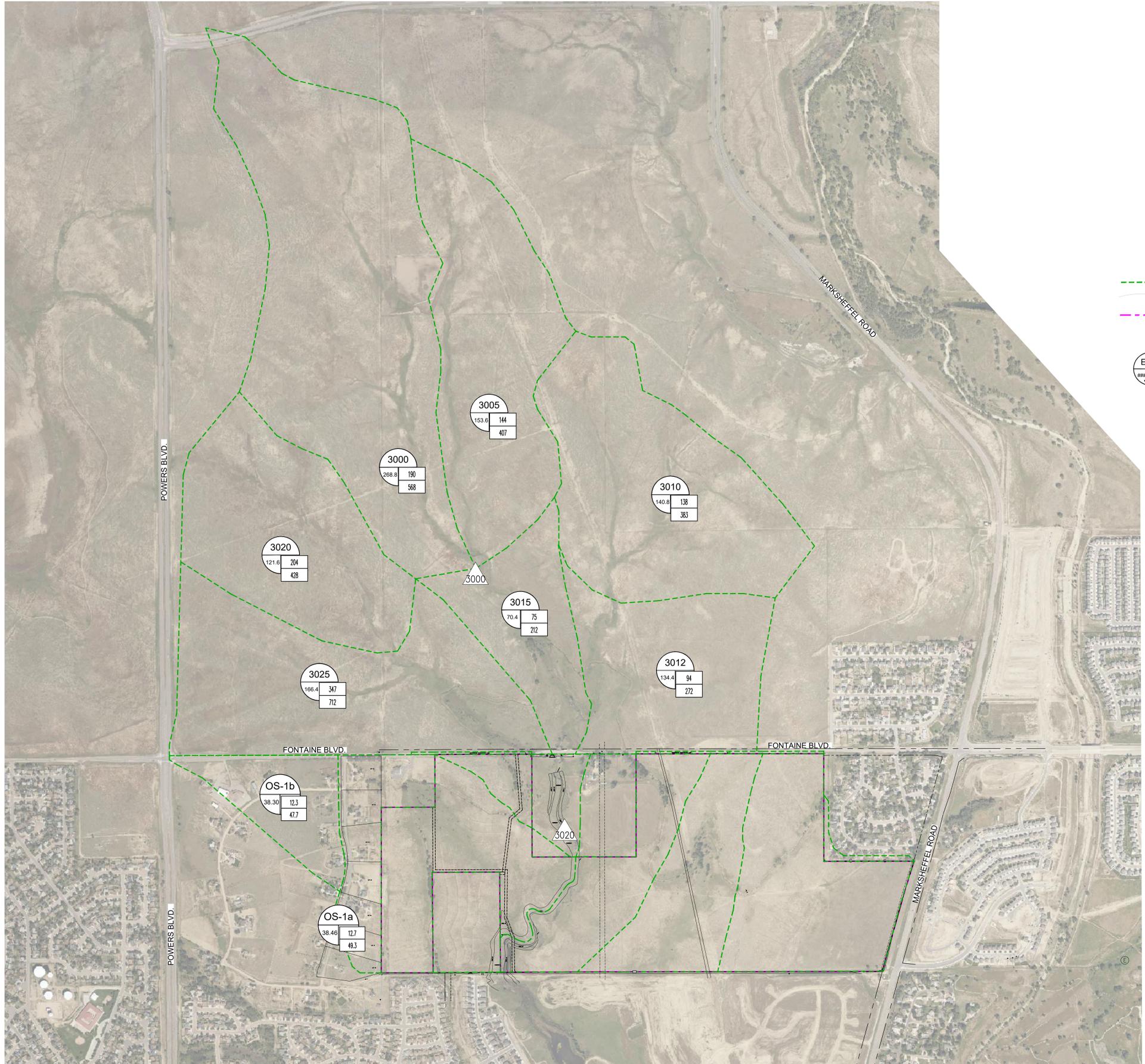
- PROPOSED BASIN BOUNDARY
 - EXISTING CONTOUR
 - DRAINAGE CHANNEL
 - PROPOSED PROPERTY LINE
 - PROPOSED FLOW DIRECTION
 - PROPOSED FLOW PATH
 - ▲ DESIGN POINT
 - ▲ SUB BASIN DESIGNATION
 - 5-YEAR STORM EVENT PEAK FLOW (CFS)
 - 100-YEAR STORM EVENT PEAK FLOW (CFS)
 - SUB BASIN AREA (AC.)
- WEST BASIN DESIGN FLOW
 - CENTRAL BASIN DESIGN FLOW
 - EAST BASIN DESIGN FLOW

SEE DR-02 FOR STORM SEWER LABELS



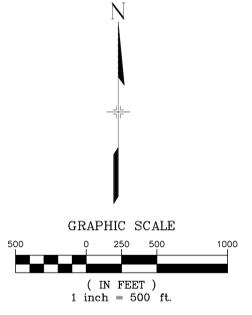
PREPARED BY:		CORVALLIS	
		MASTER DRAINAGE DEVELOPMENT PLAN FOUNTAIN, CO	
2435 Research Pkwy, Suite 300 Colorado Springs, CO 80920 Phone 719.575.0100		DRAINAGE BASIN EXHIBIT	
DESIGNED BY: AMS	SCALE: HORIZ: 1" = 200'	DATE ISSUED: JANUARY 2021	DRAWING No.
DRAWN BY: JTS	VERT: N/A	SHEET 03 OF 04	DR03
CHECKED BY: AMG			

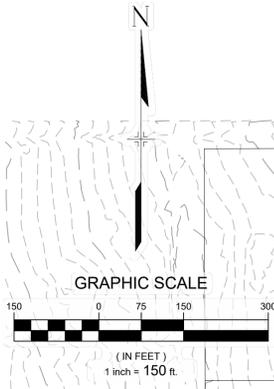
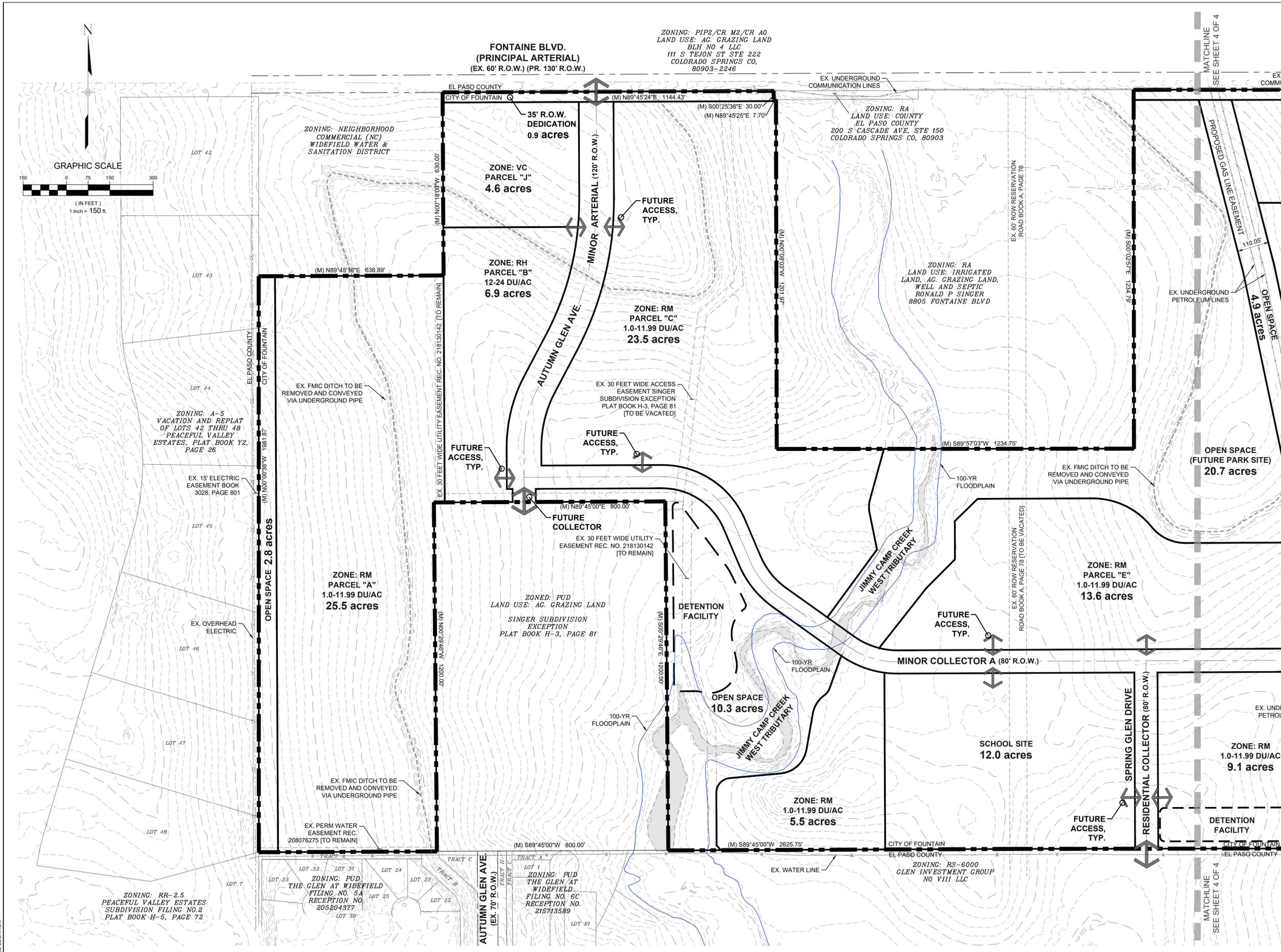
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.
January 7, 2021 10:31 AM
S:\20_1105_002_Singer_Ranch\200_Drainage\201_Drainage_Reports\MDP\DWG\DR03.dwg



LEGEND

- EXISTING BASIN BOUNDARY
- EXISTING CONTOUR
- PROPOSED PROPERTY LINE
- DESIGN POINT
- SUB BASIN DESIGNATION
- 5-YEAR STORM EVENT PEAK FLOW (CFS)
- 100-YEAR STORM EVENT PEAK FLOW (CFS)
- SUB BASIN AREA (AC.)





FONTAINE BLVD.
(PRINCIPAL ARTERIAL)
(EX. 60' R.O.W.) (PR. 130' R.O.W.)

ZONING: PIP2/CR M2/CR A0
LAND USE: AG, GRAZING LAND
BLH NO 4 LLC
111 S TEJON ST STE 222
COLORADO SPRINGS CO,
80903-2246

CONSULTANTS:
PLANNER/LANDSCAPE ARCHITECT/CIVIL ENGINEER:
Matrix
2435 RESEARCH PARKWAY,
SUITE 300
COLORADO SPRINGS, CO 80920
PHONE: (719) 575-0100
FAX: (719) 575-0208

OWNER/DEVELOPER:
HPCR PROPERTIES, LLC
14160 GLENEAGLE DRIVE
COLORADO SPRINGS, CO 80921

VICINITY MAP:

PROJECT:
CORVALLIS
CITY OF FOUNTAIN
OVERALL DEVELOPMENT PLAN

DATE: INITIAL SUBMITTAL: 09/15/2020

REVISION HISTORY:

NO.	DATE	DESCRIPTION	BY

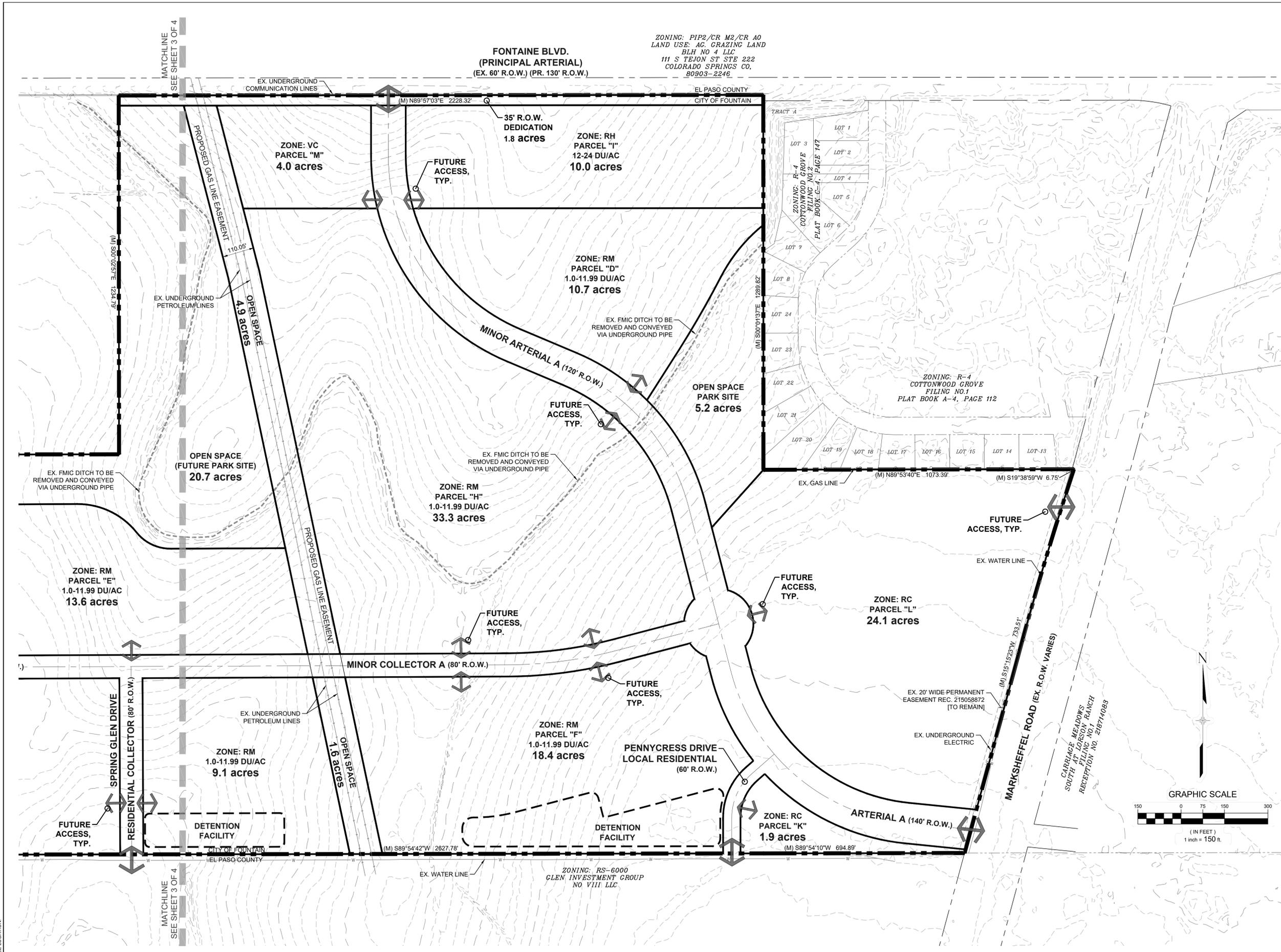
DRAWING INFORMATION:
PROJECT NO: 20.1105.002
DRAWN BY: RAF
CHECKED BY: JAA
APPROVED BY: JAA
SHEET TITLE:

OVERALL DEVELOPMENT PLAN (1)

ODP03

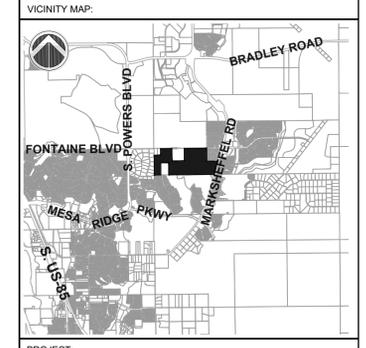
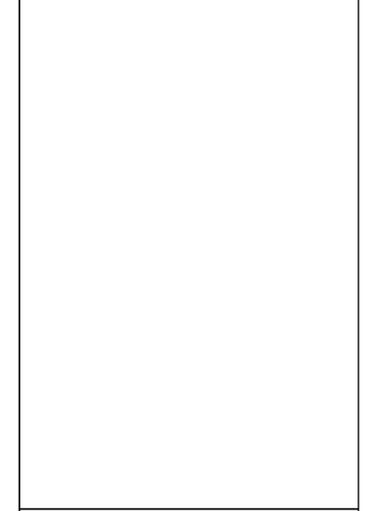
SHEET 03 OF 04

PCD FILE NO.:



CONSULTANTS:
PLANNER/ LANDSCAPE ARCHITECT/ CIVIL ENGINEER:
Matrix
2435 RESEARCH PARKWAY,
SUITE 300
COLORADO SPRINGS, CO 80920
PHONE: (719) 575-0100
FAX: (719) 575-0208

OWNER/DEVELOPER:
HPCR PROPERTIES, LLC
14160 GLENEAGLE DRIVE
COLORADO SPRINGS, CO 80921



CORVALLIS
CITY OF FOUNTAIN
OVERALL DEVELOPMENT PLAN

DATE: INITIAL SUBMITTAL: 09/15/2020

REVISION HISTORY:

NO.	DATE	DESCRIPTION	BY

DRAWING INFORMATION:
PROJECT NO: 20.1105.002
DRAWN BY: RAF
CHECKED BY: JAA
APPROVED BY: JAA

OVERALL DEVELOPMENT PLAN (2)

ODP04
SHEET 04 OF 04

PCD FILE NO.: