## **FINAL DRAINAGE REPORT**

# ORTON PIT 17710 CO115 El Paso County, Colorado 80926

Prepared For:

## **Castle Rock Construction Co. of Colorado LLC**

6374 South Racine Circle Centennial, Colorado 80111

Prepared By:

## **Baseline Engineering Corporation**

1046 Elkton Drive Colorado Springs, Colorado 80907

Steven Baggs, PE

Date: July 12, 2022

Revised: August 19, 2022

PCD File No.: CDR2211





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El Paso County
Planning and Community Development
2880 International Circle, Suite 110
Colorado Springs, Colorado 80910

August 19, 2022

Re:

Final Drainage Report For Orton Borrow Pit

Located on 17710 CO115 El Paso County, CO 80926

To Whom It May Concern:

Transmitted herewith is the Final Drainage Report for the Orton Borrow Pit, located on an unplatted parcel addressed 17710 CO115 Colorado Springs, El Paso County, Colorado 80926. The Orton Borrow Pit is approximately 10 acres and located on the property's southeastern corner. The site is currently zoned RR-5 with an existing residence, and a historic borrow pit. The purpose of the proposed borrow pit on the southern edge of El Paso County is to provide earthen fill for CDOT Project 22903 on SH115. The proposed pit would expand a historic pit from the original construction of SH115 and only be permitted/used for this one Project (less than 2 years). We would therefore like to submit for a special use permit through El Paso County in accordance with section 5.2.34(C) of the Counties land development code.

This drainage analysis was prepared in accordance with the most current El Paso County Drainage Criteria Manual. If there are any comments or questions regarding any part of this drainage analysis, please contact the undersigned.

Very truly yours,

BASELINE ENGINEERING CORP.

Sean P Callahan, E.I.

Reviewed by:

Steven G. Baggs, P.E.





#### **Certification Statements**

## **Engineer's Statement**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

| applicable master plan of the drainage basin. I accept responsibility for any liability caused by any  |
|--|
| negligent acts, errors or omissions on my part in preparing this report.  REGISTATION REGI |
| Name of Developer: Castle Rock Construction Company of Colorado, Wo Authorized Signature/Date: Brooks 8/18/22  Printed Name: Army Brooks  Title: COO  Address: 6374 S. Racine Circle Centennial, CO Bolli  |
| El Paso County Certification  Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.   |
| APPROVED  Engineering Department  09/15/2022 3:25:18 PM  dsdnijkamp  EPC Planning & Community Development Department   |





## 1) General Location and Description

#### a) Location

This Final Drainage Report has been prepared for Orton Borrow Pit, located on an unplatted parcel addressed 17710 CO115 Colorado Springs, El Paso County, Colorado 80926. The property is bound to the North by two rural residential properties (RR-5), the East by CO115 Right-of-Way, the South by vacant land, and the West by vacant land on the West limits of El Paso County.

The site is located within the NW  $\frac{1}{4}$  of the NW  $\frac{1}{4}$  of Section 18, Township 17 S, Range 67 West of the 6<sup>th</sup> Principal Meridian.

There is a historic borrow pit from the original construction of SH115 and an existing residential building on the property. There are no major drainageways adjacent to the site.

There are no existing platted developments adjacent to the site.

#### b) Description of Property

For the purposes of this report "the site" will refer to the Orton Borrow Pit site, which is approximately 10 acres of disturbed area. The entirety of the property which the Orton Borrow Pit site is located on encompasses 93.75 acres.

The proposed Orton Borrow Pit portion of the site consists of a historic borrow pit and undeveloped land covered by native grasses, trees, and weeds.

The existing site drains from the Northwest to the Southeast primarily at slopes between 0-3% into an existing depression on the Northeast side of CO-115.

The soil type at the site was identified as Satanta Loam, with slopes ranging from 0-3%, and a hydrologic soil grouping of "B". Soils associated with hydrologic soil group B have a moderate infiltration rate when thoroughly wet. These are moderately deep, well-draining soils with a moderate rate of water transmission.

There are no major drainageways adjacent to the site. There is a FEMA floodplain (Zone A) on the northeast portion of the parcel, northeast of the disturbed area for this project. The floodplain will not be disturbed with this project, refer to the appendix for the FIRM Map.

There are no known existing irrigation facilities located on the site.

There is an existing overhead transmission line on the eastern boundary of the site. The transmission line will not be disturbed with this project. There are no other known utilities or encumbrances on the borrow pit portion of the site.





## 2) Drainage Basins and Sub-Basins

#### a) Major Basin Descriptions

This project is within the Red Creek Drainage Basin. Stormwater from this site drains from the Northwest to the Southeast into an existing depression on the Northeast side of CO-115. The immediate receiving water for the site is Red Creek, with the ultimate receiving water being the Arkansas River (COARUA14d\_C).

According to the FEMA Flood Insurance Rate Map (FIRM) Panel No. 08041C1125G, effective 12/07/2018, the disturbed area of the site is located within an area of minimal flood hazard (Zone X). Refer to the appendix for FIRM Map.

The Red Creek Drainage Basin generally drains south, until its confluence with the Arkansas River approximately 14 miles south of the borrow pit site.

There are no known irrigation facilities or other obstructions which could influence or be influenced by the local drainage patterns.

#### b) Sub-basin Description

An Existing Conditions Drainage Plan has been included in the Appendix of this report. A description of the existing subbasins is as follows:

**Subbasin E1** (16.43 acres) consists of the entirety of the disturbed area for the borrow pit site and the historic borrow pit area. This subbasin drains from the Northwest to the Southeast generally at slopes between 0-4% into an existing depression from a historic borrow pit on the Northeast side of CO-115 at DP1. Stormwater infiltrates into soils at the existing depression in existing conditions. The determined existing runoff quantities from subbasin E1 draining to DP1 are  $Q_5$ =3.18 cfs and  $Q_{100}$ =21.37 cfs in the minor and major storms. The total accumulative flows from subbasins E1 & E2 draining to DP1 are  $Q_5$ =7.30 cfs and  $Q_{100}$ =48.97 cfs in the minor and major storms

**Subbasin E2** (26.40 acres) consists of an undeveloped offsite area tributary to the existing borrow pit. This subbasin drains from the Northwest to the Southeast generally at slopes between 3-4% into the west edge of basins E1/P1. Ultimately draining to the existing depression from a historic borrow pit on the Northeast side of CO-115 at DP1. Stormwater infiltrates into soils at the existing depression in existing conditions. The determined existing runoff quantities from subbasin E2 draining to DP2 are  $Q_5$ =4.11 cfs and  $Q_{100}$ =27.60 cfs in the minor and major storms.

A Proposed Conditions Drainage Plan has been included in the Appendix of this report. A description of the proposed subbasins is as follows:

**Subbasin P1** (16.43 acres) consists of the entirety of the disturbed area for the borrow pit site and the historic borrow pit area. This subbasin will maintain existing drainage patterns. The proposed subbasin drains from the Northwest to the Southeast generally at slopes between 0-3.7% into an existing depression from a historic borrow pit on the Northeast side of CO-115 at DP1. Stormwater infiltrates





into soils at the existing depression in existing conditions. The determined proposed runoff quantities from subbasin P1 draining to DP1 are  $Q_5$ =3.17 cfs and  $Q_{100}$ =21.26 cfs in the minor and major storms. The total accumulative flows from subbasins P1 & E2 draining to DP1 are  $Q_5$ =7.28 cfs and  $Q_{100}$ =48.85 cfs in the minor and major storms

Other than Subbasin E2, there are no known off-site drainage flow patterns that will impact this project.

## 3) Drainage Design Criteria

#### a) Development Criteria Reference

This drainage analysis has been prepared in accordance with the current El Paso County Drainage Criteria Manual Volumes 1 & 2, as well as applicable portions of the City of Colorado Springs Drainage Criteria Manual Volumes 1 & 2.

This site is located within the Red Creek Drainage Basin (BEBE0200). There are no previous drainage studies completed for this project site. There are no associated drainage fees for this basin.

#### b) Hydrologic Criteria

The design rainfall depths for the site were determined from the NOAA Atlas 14, Volume 8, Version 2. Design rainfall depths have been included in the appendix of this report.

The Rational Method was used to determine developed flow volumes for historic and developed conditions. The Rational Formula is Q = CiA, where Q, the maximum rate of runoff is equal to the runoff coefficient C, times the rainfall intensity (I), times the area (A).

The minor and major design storms were analyzed as the 5-yr and 100-yr storm events in this report. A summary of calculated direct runoff flows has been provided below, refer to the Appendix for additional rational calculations.

There were no detention discharge calculation methods required for this report. The existing historic borrow pit storage volume and tributary area runoff quantities were analyzed using the MHFD Detention Workbook v4.06

## 4) Drainage Facility Design

## a) General Concept

The proposed drainage patterns of the site will maintain the existing drainage patterns. The site drains from Northwest to the Southeast into a historic borrow pit from the original construction of SH115 at DP1. Stormwater infiltrates into soils at the existing depression in existing conditions and will continue to after operation of the proposed borrow pit is completed. This project will expand the historic pit from its original construction to provide earthen fill for CDOT Project 22903 on SH115 and only be





permitted/used for this one Project (less than 2 years). This project will not have a negative impact on downstream drainageways.

Subbasin E2 contributes off-site runoff to the proposed borrow pit disturbed area. The borrow pit will be expanded and runoff will continue to flow in its historic patterns. Runoff that currently enters the historic borrow pit will continue to flow to the exiting borrow pit depression as the pit is expanded. There will be no change to the amount of runoff captured at the existing borrow pit depression.

The existing borrow pit storage volume was analyzed, and it was determined that the 100-year storm volume will be contained within the historic borrow pit without overtopping into the CDOT roadside ditch adjacent to the site. The 100-year storm will pond to an elevation of 6379.99. The infiltration of storm events stored in the historic borrow pit was not analyzed. However, a permeability test was completed for soils on site and the permeation trial data has been provided in the appendix of this report.

<u>Four Step Process:</u> The four-step process for minimizing adverse impacts of urbanization must be applied to all new or redevelopment projects for which construction activities disturb greater than or equal to one acre, including projects less than one acre that are part of a larger common plan of development or sale. The four steps have been applied to this site as follows:

Step 1: Reduce runoff by disconnecting impervious area, eliminating "unnecessary" impervious area and encouraging infiltration into soils that are suitable.

The stormwater management for the Orton Borrow Pit does employ runoff reduction practices. No impervious area will be added during operations of the borrow pit. The UD-BMP IRF spreadsheet was prepared for this project and is included in the Hydrologic Calculations section of the Appendix.

#### Step 2: Treat and slowly release the WQCV.

This site is exempt from water quality treatment per the exclusion in ECM Appendix I.E.4.a.i.G. Also, per the post construction stormwater management applicability evaluation from, no permanent post construction stormwater management is required since the undeveloped land will remain undeveloped following the borrow pit activity.

#### Step 3: Stabilize stream channels.

All new and re-development projects are required to construct or participate in the funding of channel stabilization measures. There are no associated drainage fees for the Red Creek Drainage Basin. There are no major drainage ways that are adjacent to the site. Negative impacts on downstream drainageways will not occur as no impervious area will be added to the site and runoff is contained on-site. Runoff from the site is conveyed via sheet flow to a historic depression from the original construction of SH115. Stormwater infiltrates into soils at the existing depression.

Step 4: Implement source controls.





This development will implement a Stormwater Management Plan utilizing construction control measures, proper housekeeping practices, and spill containment procedures. There is no outdoor storage of contaminants or outside pollutant sources anticipated at this site.

#### b) Specific Details

Below is a summary of the existing and proposed direct runoff summaries for the disturbed area of the borrow pit. Rational calculations have been provided in the appendix of this report.

**Table 1. Subbasin Direct Runoff Summary** 

| DIRECT RU      | DIRECT RUNOFF SUMMARY |       |      |      |      |                |       |                    |       |       |  |  |  |
|----------------|-----------------------|-------|------|------|------|----------------|-------|--------------------|-------|-------|--|--|--|
| BASIN<br>LABEL | DESIGN<br>POINT       | AREA  | Imp. | C5   | C100 | LOCAL<br>(CFS) |       | ACCUMULATIVE (CFS) |       | Notes |  |  |  |
|                |                       |       |      |      |      | Q5             | Q100  | Q5                 | Q100  |       |  |  |  |
| E2             | 2                     | 26.40 | 2%   | 0.09 | 0.36 | 4.11           | 27.60 |                    |       |       |  |  |  |
| E1             | 1                     | 16.43 | 2%   | 0.09 | 0.36 | 3.18           | 21.37 | 7.30               | 48.97 |       |  |  |  |
| P1             | 1                     | 16.43 | 2%   | 0.09 | 0.36 | 3.17           | 21.26 | 7.28               | 48.85 |       |  |  |  |

There are no negative drainage impacts on downstream facilities as no impervious area will be added and runoff is contained on-site. Runoff from the site is conveyed via sheet flow to a historic depression from the original construction of SH115. Stormwater will continue to infiltrate into soils at the existing depression as in historic conditions.

The purpose of the proposed borrow pit is to provide earthen fill for CDOT Project 22903 on SH115. The proposed pit would expand a historic pit from the original construction of SH115 and only be permitted/used for this one Project (less than 2 years).

The existing borrow pit creates a depression on the east edge of the site and the west side of SH115. There is no known outfall for this low point and stormwater will infiltrate into soils on site.

There are no known environmental or drainage issues existing on site.

Maintenance for the site will be provided off of the proposed haul road for the operation of the borrow pit. The haul road will not be developed with an impervious surface material.

There is no permanent detention structure proposed with this project. Temporary erosion control CM's will be in place prior to final stabilization of the site. Grading and Erosion Control Plans for the site will be submitted separately.

There are no public or private drainage facilities proposed for this project. Applicable portions of the 2022 Financial Assurance Estimate From has been completed and provided to the County.

There are no associated drainage fees for the Red Creek Drainage Basin.





#### c) Other Government Agency Requirements

#### Federal Emergency Management Agency (FEMA)

According to the FEMA Flood Insurance Rate Map (FIRM) Panel No. 08041C1125G, effective 12/07/2018, this site is located within an area of minimal flood hazard (Zone X). A copy of a portion of the appropriate FIRM panel is included in the Appendix.

#### **Army Corps of Engineers (COE)**

N/A

#### **Colorado State Engineer**

Following conversation between Travis Bell with Castle Rock Construction Company (CRCC) and Dan Henrichs the Division 2, District 12 Water commissioner for the Colorado Division of Water Resources, it was confirmed that no water rights are required for the proposed borrow pit. Included in the appendix of this report is an email from Mr. Henrichs confirming this.

#### **Colorado Water Conservation Board (CWCB)**

N/A

#### **CDOT**

The existing borrow pit storage volume was analyzed, and it was determined that up to the 100-year storm volume will be contained within the historic borrow pit without overtopping into the CDOT roadside ditch adjacent to the site. The infiltration of the storm events stored in the historic borrow pit was not analyzed. A permeability test was completed for soils on site and the permeation trial data has been provided in the appendix of this report.





## **Drawings/Appendix**

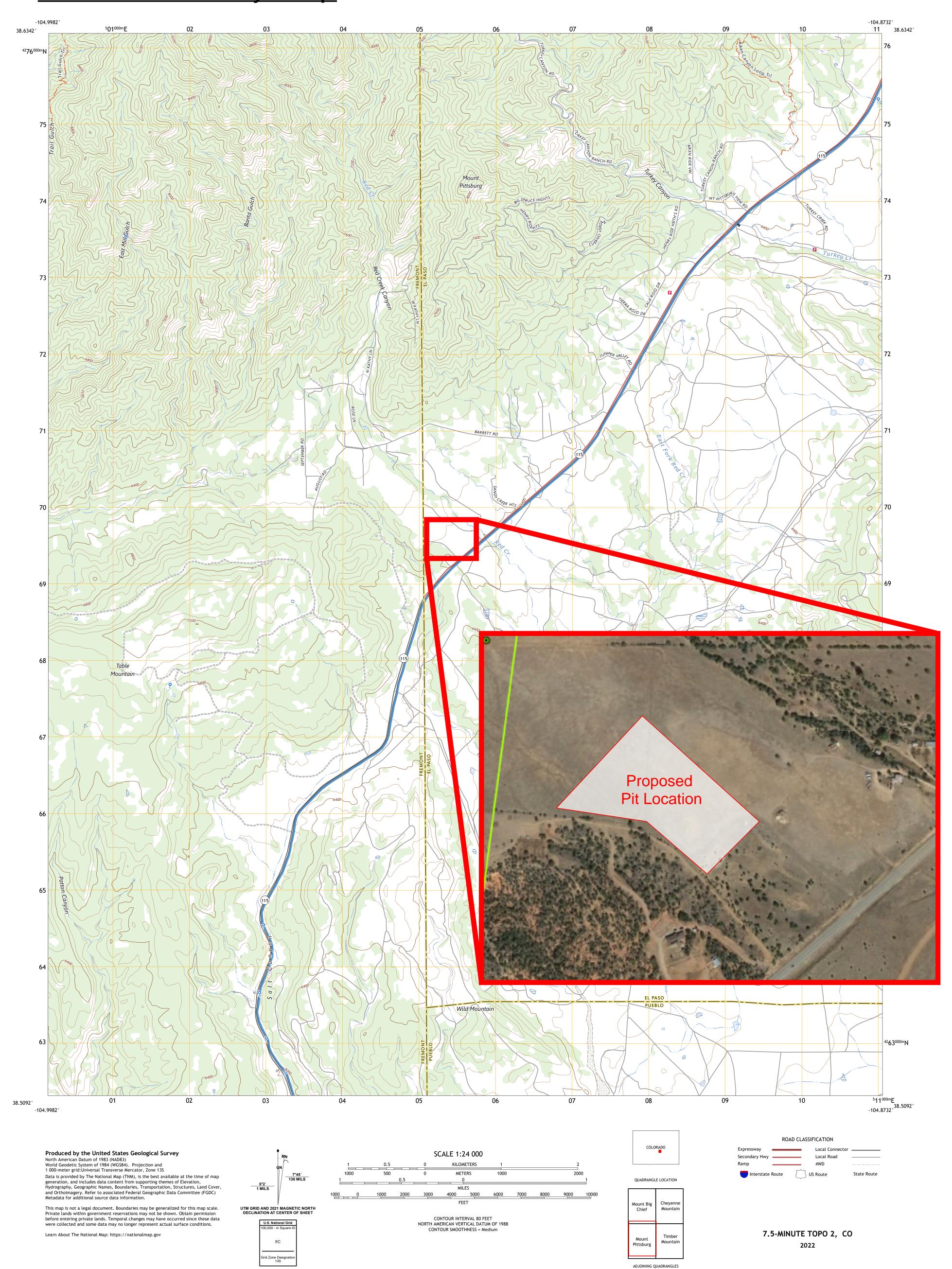
- A. General Location (Vicinity) Map
- **B.** Hydrologic Calculations
- **C.** Drainage Plans
- **D. Coordination Documents**



# APPENDIX A



# Orton Pit Vicinity Map



# APPENDIX B





NOAA Atlas 14, Volume 8, Version 2 Location name: Colorado, USA\* Latitude: 38.5744°, Longitude: -104.9385° Elevation: 6466.82 ft\*\*

7744°, Longitude: -104.9385°
vation: 6466.82 ft\*\*
'source: ESRI Maps
\*\* source: USGS

#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

| PDS      | PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup> |                               |                               |                               |                            |                            |                           |                              |                          |                          |  |  |  |  |
|----------|--|-------------------------------|-------------------------------|-------------------------------|----------------------------|----------------------------|---------------------------|------------------------------|--------------------------|--------------------------|--|--|--|--|
| Duration |  |                               |                               | Average                       | recurrence                 | interval (ye               | ars)                      |                              |                          |                          |  |  |  |  |
| Duration | 1  | 2                             | 5                             | 10                            | 25                         | 50                         | 100                       | 200                          | 500                      | 1000                     |  |  |  |  |
| 5-min    | <b>0.247</b><br>(0.195-0.313)  | <b>0.294</b><br>(0.232-0.373) | <b>0.380</b><br>(0.299-0.484) | <b>0.459</b><br>(0.359-0.588) | <b>0.579</b> (0.442-0.788) | <b>0.680</b> (0.504-0.939) | <b>0.789</b> (0.563-1.12) | <b>0.908</b><br>(0.619-1.34) | <b>1.08</b> (0.704-1.64) | <b>1.21</b> (0.768-1.87) |  |  |  |  |
| 10-min   | <b>0.361</b><br>(0.286-0.458)  | <b>0.431</b><br>(0.340-0.547) | <b>0.557</b><br>(0.438-0.709) | <b>0.672</b><br>(0.526-0.861) | <b>0.848</b> (0.647-1.15)  | <b>0.996</b> (0.738-1.38)  | <b>1.16</b> (0.825-1.65)  | <b>1.33</b> (0.907-1.96)     | <b>1.58</b> (1.03-2.40)  | <b>1.78</b> (1.13-2.74)  |  |  |  |  |
| 15-min   | <b>0.440</b><br>(0.348-0.558)  | <b>0.526</b> (0.415-0.667)    | <b>0.679</b><br>(0.534-0.865) | <b>0.820</b> (0.641-1.05)     | <b>1.03</b> (0.789-1.41)   | <b>1.22</b> (0.900-1.68)   | <b>1.41</b> (1.00-2.01)   | <b>1.62</b> (1.11-2.39)      | <b>1.92</b> (1.26-2.93)  | <b>2.17</b> (1.37-3.34)  |  |  |  |  |
| 30-min   | <b>0.632</b><br>(0.500-0.801)  | <b>0.756</b> (0.597-0.959)    | <b>0.979</b> (0.771-1.25)     | <b>1.18</b> (0.926-1.52)      | <b>1.49</b> (1.14-2.03)    | <b>1.76</b> (1.30-2.42)    | <b>2.04</b> (1.45-2.90)   | <b>2.34</b> (1.60-3.46)      | <b>2.78</b> (1.82-4.24)  | <b>3.14</b> (1.99-4.83)  |  |  |  |  |
| 60-min   | <b>0.801</b> (0.634-1.01)  | <b>0.945</b> (0.747-1.20)     | <b>1.22</b> (0.957-1.55)      | <b>1.47</b> (1.15-1.89)       | <b>1.88</b> (1.44-2.57)    | <b>2.23</b> (1.65-3.09)    | <b>2.61</b> (1.87-3.73)   | <b>3.03</b> (2.07-4.49)      | <b>3.64</b> (2.39-5.57)  | <b>4.15</b> (2.63-6.39)  |  |  |  |  |
| 2-hr     | <b>0.970</b> (0.773-1.22)  | <b>1.14</b> (0.903-1.43)      | <b>1.45</b> (1.15-1.83)       | <b>1.76</b> (1.39-2.24)       | <b>2.26</b> (1.75-3.08)    | <b>2.70</b> (2.02-3.72)    | <b>3.18</b> (2.30-4.52)   | <b>3.72</b> (2.57-5.47)      | <b>4.51</b> (2.99-6.84)  | <b>5.16</b> (3.30-7.88)  |  |  |  |  |
| 3-hr     | <b>1.06</b> (0.845-1.32)   | <b>1.22</b> (0.975-1.53)      | <b>1.55</b> (1.23-1.95)       | <b>1.88</b> (1.49-2.38)       | <b>2.43</b> (1.90-3.31)    | <b>2.92</b> (2.20-4.02)    | <b>3.46</b> (2.52-4.92)   | <b>4.08</b> (2.84-5.99)      | <b>5.00</b> (3.33-7.56)  | <b>5.76</b> (3.70-8.75)  |  |  |  |  |
| 6-hr     | <b>1.23</b> (0.990-1.52)   | <b>1.40</b> (1.12-1.73)       | <b>1.75</b> (1.40-2.18)       | <b>2.12</b> (1.69-2.65)       | <b>2.74</b> (2.16-3.72)    | <b>3.30</b> (2.52-4.53)    | <b>3.95</b> (2.90-5.57)   | <b>4.68</b> (3.29-6.81)      | <b>5.77</b> (3.89-8.66)  | <b>6.68</b> (4.35-10.1)  |  |  |  |  |
| 12-hr    | <b>1.44</b> (1.17-1.78)  | <b>1.63</b> (1.32-2.01)       | <b>2.03</b> (1.64-2.51)       | <b>2.44</b> (1.96-3.03)       | <b>3.13</b> (2.49-4.20)    | <b>3.75</b> (2.89-5.09)    | <b>4.46</b> (3.31-6.23)   | <b>5.27</b> (3.74-7.60)      | <b>6.47</b> (4.41-9.62)  | <b>7.47</b> (4.91-11.1)  |  |  |  |  |
| 24-hr    | <b>1.69</b> (1.38-2.06)  | <b>1.92</b> (1.56-2.34)       | <b>2.38</b> (1.94-2.91)       | <b>2.85</b> (2.30-3.51)       | <b>3.61</b> (2.89-4.79)    | <b>4.30</b> (3.33-5.76)    | <b>5.07</b> (3.79-7.00)   | <b>5.95</b> (4.26-8.47)      | <b>7.23</b> (4.97-10.6)  | <b>8.31</b> (5.52-12.3)  |  |  |  |  |
| 2-day    | <b>1.94</b> (1.60-2.34)  | <b>2.23</b> (1.84-2.70)       | <b>2.80</b> (2.29-3.39)       | <b>3.35</b> (2.73-4.09)       | <b>4.24</b> (3.41-5.55)    | <b>5.02</b> (3.92-6.65)    | <b>5.89</b> (4.44-8.03)   | <b>6.86</b> (4.96-9.66)      | <b>8.28</b> (5.75-12.0)  | <b>9.46</b> (6.35-13.8)  |  |  |  |  |
| 3-day    | <b>2.11</b> (1.75-2.53)  | <b>2.45</b> (2.02-2.95)       | <b>3.10</b> (2.55-3.74)       | <b>3.72</b> (3.05-4.52)       | <b>4.71</b> (3.80-6.12)    | <b>5.57</b> (4.37-7.32)    | <b>6.52</b> (4.94-8.83)   | <b>7.58</b> (5.50-10.6)      | <b>9.11</b> (6.36-13.2)  | <b>10.4</b> (7.01-15.1)  |  |  |  |  |
| 4-day    | <b>2.26</b> (1.88-2.71)  | <b>2.63</b> (2.18-3.15)       | <b>3.32</b> (2.75-4.00)       | <b>3.99</b> (3.28-4.83)       | <b>5.04</b> (4.08-6.52)    | <b>5.96</b> (4.68-7.80)    | <b>6.96</b> (5.29-9.39)   | <b>8.08</b> (5.89-11.3)      | <b>9.70</b> (6.80-13.9)  | <b>11.0</b> (7.48-16.0)  |  |  |  |  |
| 7-day    | <b>2.68</b> (2.24-3.19)  | <b>3.08</b> (2.57-3.67)       | <b>3.83</b> (3.19-4.58)       | <b>4.55</b> (3.76-5.46)       | <b>5.67</b> (4.62-7.27)    | <b>6.65</b> (5.26-8.63)    | <b>7.73</b> (5.91-10.3)   | <b>8.92</b> (6.55-12.3)      | <b>10.6</b> (7.52-15.2)  | <b>12.1</b> (8.26-17.3)  |  |  |  |  |
| 10-day   | <b>3.07</b> (2.58-3.64)  | <b>3.50</b> (2.94-4.15)       | <b>4.31</b> (3.60-5.12)       | <b>5.06</b> (4.21-6.06)       | <b>6.24</b> (5.09-7.93)    | <b>7.25</b> (5.76-9.34)    | <b>8.36</b> (6.42-11.1)   | <b>9.57</b> (7.06-13.1)      | <b>11.3</b> (8.05-16.1)  | <b>12.8</b> (8.79-18.3)  |  |  |  |  |
| 20-day   | <b>4.17</b> (3.52-4.89)  | <b>4.78</b> (4.04-5.61)       | <b>5.83</b> (4.91-6.88)       | <b>6.76</b> (5.67-8.02)       | <b>8.13</b> (6.63-10.1)    | <b>9.24</b> (7.37-11.7)    | <b>10.4</b> (8.03-13.6)   | <b>11.7</b> (8.65-15.7)      | <b>13.4</b> (9.57-18.7)  | <b>14.8</b> (10.3-20.9)  |  |  |  |  |
| 30-day   | <b>5.05</b> (4.29-5.90)  | <b>5.82</b> (4.94-6.80)       | <b>7.10</b> (6.00-8.32)       | <b>8.18</b> (6.88-9.64)       | <b>9.69</b> (7.92-11.9)    | <b>10.9</b> (8.70-13.6)    | <b>12.1</b> (9.37-15.6)   | <b>13.4</b> (9.95-17.8)      | <b>15.0</b> (10.8-20.8)  | <b>16.4</b> (11.5-23.0)  |  |  |  |  |
| 45-day   | <b>6.14</b> (5.24-7.14)  | <b>7.09</b> (6.05-8.24)       | <b>8.62</b> (7.33-10.1)       | <b>9.87</b> (8.35-11.6)       | <b>11.6</b> (9.46-14.1)    | <b>12.9</b> (10.3-15.9)    | <b>14.1</b> (11.0-18.0)   | <b>15.4</b> (11.5-20.4)      | <b>17.1</b> (12.3-23.3)  | <b>18.3</b> (12.9-25.6)  |  |  |  |  |
| 60-day   | <b>7.05</b> (6.04-8.16)  | <b>8.13</b> (6.96-9.42)       | <b>9.85</b> (8.40-11.5)       | <b>11.2</b> (9.53-13.1)       | <b>13.1</b> (10.7-15.8)    | <b>14.4</b> (11.6-17.8)    | <b>15.8</b> (12.3-20.0)   | <b>17.0</b> (12.8-22.4)      | <b>18.7</b> (13.5-25.4)  | <b>19.9</b> (14.1-27.7)  |  |  |  |  |

<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

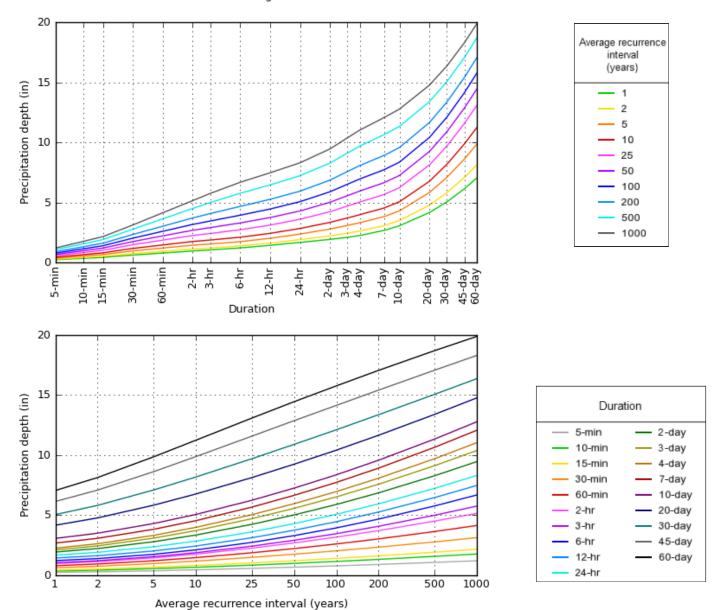
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical

#### PDS-based depth-duration-frequency (DDF) curves Latitude: 38.5744°, Longitude: -104.9385°



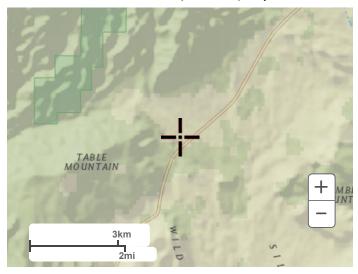
NOAA Atlas 14, Volume 8, Version 2

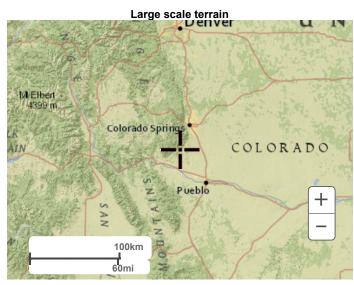
Created (GMT): Fri Jun 24 18:50:52 2022

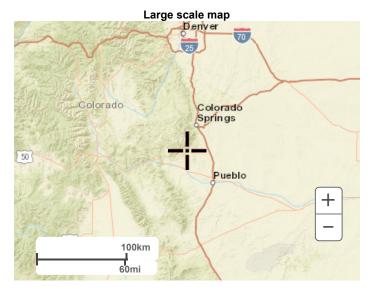
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#### Maps & aerials

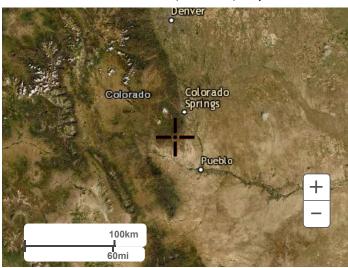
Small scale terrain







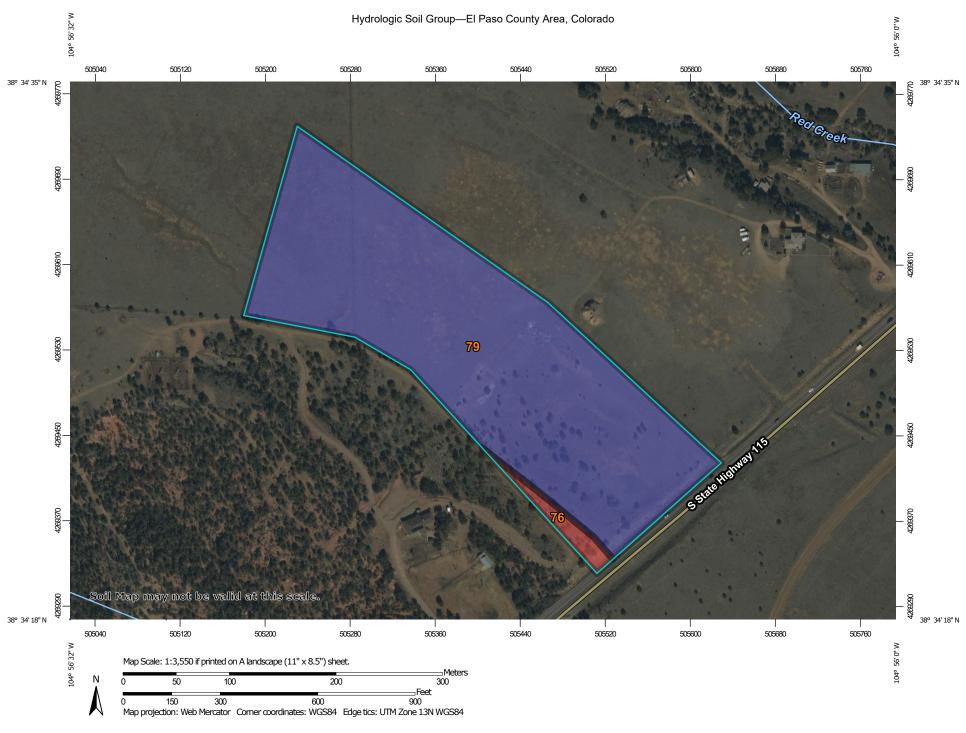
Large scale aerial



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US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

**Disclaimer** 



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Sep 11, 2018—Oct 20. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

## **Hydrologic Soil Group**

| Map unit symbol           | Map unit name                                     | Rating | Acres in AOI | Percent of AOI |  |  |  |  |  |  |  |  |
|---------------------------|---|--------|--------------|----------------|--|--|--|--|--|--|--|--|
| 76                        | Rizozo-Neville complex,<br>3 to 30 percent slopes | D      | 0.5          | 3.0%           |  |  |  |  |  |  |  |  |
| 79                        | Satanta loam, 0 to 3 percent slopes               | В      | 16.2         | 97.0%          |  |  |  |  |  |  |  |  |
| Totals for Area of Intere | st  | 16.7   | 100.0%       |                |  |  |  |  |  |  |  |  |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

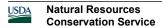
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition



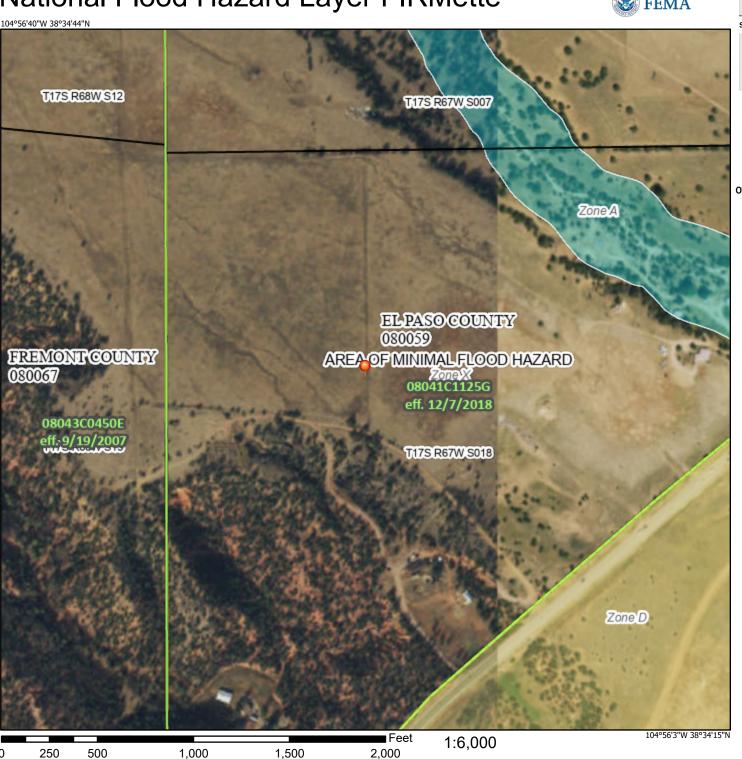
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

## National Flood Hazard Layer FIRMette

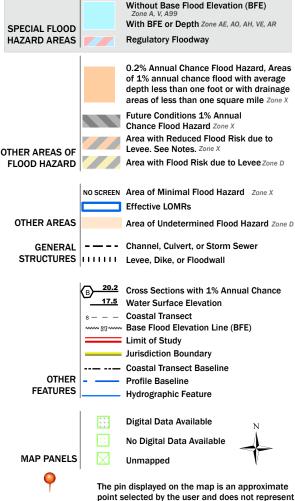


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

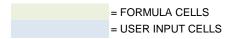
an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 6/20/2022 at 11:41 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



JOB NO.: 35059 CALC. BY: SPC DATE: 8/16/2022



| Project Location |  |
|------------------|--|
| User Input       |  |

#### **IDF Rainfall Data**

|         | P <sub>1</sub> : 1-hour Rainfall Depths (inches) |             |  |  |  |  |  |  |  |  |  |  |  |
|---------|--|-------------|--|--|--|--|--|--|--|--|--|--|--|
|         | Minor Storm                                      | Major Storm |  |  |  |  |  |  |  |  |  |  |  |
| D       | 5-Year ▼   | 100-Year ▼  |  |  |  |  |  |  |  |  |  |  |  |
| Minutes | 1.47   | 2.61        |  |  |  |  |  |  |  |  |  |  |  |
| 5       | 5.22   | 8.53        |  |  |  |  |  |  |  |  |  |  |  |
| 10      | 4.20   | 6.73        |  |  |  |  |  |  |  |  |  |  |  |
| 20      | 3.18   | 4.92        |  |  |  |  |  |  |  |  |  |  |  |
| 30      | 2.58   | 3.86        |  |  |  |  |  |  |  |  |  |  |  |
| 40      | 2.16   | 3.11        |  |  |  |  |  |  |  |  |  |  |  |
| 50      | 1.83   | 2.52        |  |  |  |  |  |  |  |  |  |  |  |
| 60      | 1.56   | 2.05        |  |  |  |  |  |  |  |  |  |  |  |

Figure 6-5  $I_5$ =-P<sub>1</sub> In(D) + 7.583;  $I_{100}$ = -P<sub>1</sub> In(D) + 12.735

I = rainfall intensity (inches per hour)

 $P_1$  = 1-hour point rainfall depth (inches)

D = storm duration (minutes)

#### Reference:

- 1) El Paso County Drainage Criteria Manual Volume I, Revised 1987
- 2) City of Colorado Springs Drainage Criteria Manual Volume I, May 2014
- 3) Rainfall depths determined via the NOAA Atlas 14, Volume 8, Version 2 (https://hdsc.nws.noaa.gov/hdsc/pfds/pfds map\_cont.html?bkmrk=co)

JOB NO.: 35059 CALC. BY: SPC DATE: 8/16/2022 = FORMULA CELLS = USER INPUT CELLS



## Runoff Coefficients & Impervious Values for Rational Method - per CS DCM Vol I, Table 6-6.

|               | Impervious<br>Percentage | C <sub>2</sub> | C <sub>5</sub> | C <sub>10</sub> | C <sub>25</sub> | C <sub>50</sub> | C <sub>100</sub> |
|---------------|--------------------------|----------------|----------------|-----------------|-----------------|-----------------|------------------|
| Flow Analysis | 2%                       | 0.03           | 0.09           | 0.17            | 0.26            | 0.31            | 0.36             |
| Land Use      | 0%                       | 0.00           | 0.00           | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use      | 0%                       | 0.00           | 0.00           | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use      | 0%                       | 0.00           | 0.00           | 0.00            | 0.00            | 0.00            | 0.00             |

|          | Impervious<br>Percentage | $C_2$ | <b>C</b> <sub>5</sub> | C <sub>10</sub> | C <sub>25</sub> | C <sub>50</sub> | C <sub>100</sub> |
|----------|--------------------------|-------|-----------------------|-----------------|-----------------|-----------------|------------------|
| Land Use | 0%                       | 0.00  | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use | 0%                       | 0.00  | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use | 0%                       | 0.00  | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use | 0%                       | 0.00  | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |

Hydrologic Soil Group

A or B

## PROPOSED COMPOSITE IMPERVIOUSNESS

|                 | Weighted Impervious and C Values |      |                |                |                 |                 |                 | Areas (ac)       |   |           |          |          |          |          |          |          |
|-----------------|----------------------------------|------|----------------|----------------|-----------------|-----------------|-----------------|------------------|---|-----------|----------|----------|----------|----------|----------|----------|
| Basin Area (ac) |                                  | lmp. | C <sub>2</sub> | C <sub>5</sub> | C <sub>10</sub> | C <sub>25</sub> | C <sub>50</sub> | C <sub>100</sub> | UA- Historic<br>Flow Analysis<br>Greenbelts,<br>Agriculture | Land Use  | Land Use | Land Use | Land Use | Land Use | Land Use | Land Use |
|                 |                                  |      |                |                |                 |                 |                 | Existi           | ng Conditions   | Subbasins |          |          |          |          |          |          |
| E1              | 16.43                            | 2%   | 0.03           | 0.09           | 0.17            | 0.26            | 0.31            | 0.36             | 16.43   |           |          |          |          |          |          |          |
| E2              | 26.40                            | 2%   | 0.03           | 0.09           | 0.17            | 0.26            | 0.31            | 0.36             | 26.40   |           |          |          |          |          |          |          |

JOB NO.: 35059 CALC. BY: SPC DATE: 8/16/2022 = FORMULA CELLS = USER INPUT CELLS



## Runoff Coefficients & Impervious Values for Rational Method - per CS DCM Vol I, Table 6-6.

|               | Impervious<br>Percentage | $C_2$ | C <sub>5</sub> | C <sub>10</sub> | C <sub>25</sub> | C <sub>50</sub> | C <sub>100</sub> |
|---------------|--------------------------|-------|----------------|-----------------|-----------------|-----------------|------------------|
| Flow Analysis | 2%                       | 0.03  | 0.09           | 0.17            | 0.26            | 0.31            | 0.36             |
| Land Use      | 0%                       | 0.00  | 0.00           | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use      | 0%                       | 0.00  | 0.00           | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use      | 0%                       | 0.00  | 0.00           | 0.00            | 0.00            | 0.00            | 0.00             |

|          | Impervious<br>Percentage | C <sub>2</sub> | <b>C</b> <sub>5</sub> | C <sub>10</sub> | C <sub>25</sub> | C <sub>50</sub> | C <sub>100</sub> |
|----------|--------------------------|----------------|-----------------------|-----------------|-----------------|-----------------|------------------|
| Land Use | 0%                       | 0.00           | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use | 0%                       | 0.00           | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use | 0%                       | 0.00           | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |
| Land Use | 0%                       | 0.00           | 0.00                  | 0.00            | 0.00            | 0.00            | 0.00             |

Hydrologic Soil Group

A or B

## PROPOSED COMPOSITE IMPERVIOUSNESS

|       | Weighted Impervious and C Values |      |                |                |                 |                 |                 |                  |   | Areas (ac) |          |          |          |          |          |          |  |  |  |
|-------|----------------------------------|------|----------------|----------------|-----------------|-----------------|-----------------|------------------|---|------------|----------|----------|----------|----------|----------|----------|--|--|--|
| Basin | Area (ac)                        | lmp. | C <sub>2</sub> | C <sub>5</sub> | C <sub>10</sub> | C <sub>25</sub> | C <sub>50</sub> | C <sub>100</sub> | UA- Historic<br>Flow Analysis<br>Greenbelts,<br>Agriculture | Land Use   | Land Use | Land Use | Land Use | Land Use | Land Use | Land Use |  |  |  |
|       |                                  |      |                |                |                 |                 |                 | Propos           | sed Conditions  | Subbasins  |          |          |          |          |          |          |  |  |  |
| P1    | 16.43                            | 2%   | 0.03           | 0.09           | 0.17            | 0.26            | 0.31            | 0.36             | 16.43   |            |          |          |          |          |          |          |  |  |  |



## **STANDARD FORM SF-1**

#### TIME OF CONCENTRATION SUMMARY

Calculated By: SPC
Date: 8/16/2022

Project: ORTON PIT SITE
Job No.: 35059
Checked By: SGB

| (     | SUB-BA                        | SIN   |       | INITIA | AL/OVERL   | AND            | TRAVEL TIME |      |            |         |                |                        | t <sub>c</sub> CHE | CK   | FINAL        | REMARKS |  |
|-------|-------------------------------|-------|-------|--------|--|----------------|-------------|------|------------|---------|----------------|------------------------|--------------------|------|--------------|---------|--|
|       | DATA                          | ı     |       |        | TIME (t <sub>i</sub> )   |                |             |      | $(t_t)$    |         |                | (URBANIZED BASINS)     |                    |      |              |         |  |
| Basin | i                             | $C_5$ | AREA  | LENGTH | SLOPE  | t <sub>i</sub> | LENGTH      |      | SLOPE      | VEL.    | t <sub>t</sub> | COMP.                  | TOT. LENGTH        | So   | tc (Equation | n 6-7)  |  |
|       |                               |       | Ac    | Ft     | %  | Min            | Ft          | Cv   | %          | FPS     | Min            | $t_c$                  | Ft                 | %    | Min          | Min     |  |
| (1)   | (2)                           | (3)   | (4)   | (5)    | (6)  | (7)            | (8)         |      | (9)        | (10)    | (11)           | (12)                   | (13)               | (14) | (15)         | (16)    |  |
|       |                               |       |       |        |  |                | Existing    | Cond | litions Su | bbasins |                |                        |                    |      |              |         |  |
| E1    | 0.02                          | 0.09  | 16.43 | 100    | 3.5  | 12.06          | 1,516       | 5    | 4.0        | 1.00    | 25.27          | 37.3                   | 1,616              | 3.97 | 40.2         | 37.33   |  |
| E2    | 0.02                          | 0.09  | 26.40 | 100    | 3.8  | 11.74          | 2,484       | 5    | 3.8        | 0.97    | 42.48          | 54.2                   | 2,584              | 3.80 | 49.5         | 49.47   |  |
|       | Proposed Conditions Subbasins |       |       |        |  |                |             |      |            |         |                |                        |                    |      |              |         |  |
| P1    | 0.02                          | 0.09  | 16.43 | 100    | 100         5.5         10.39         1,578         5         3.7         0.97         27.24 |                |             |      |            |         |                | 37.6 1,678 3.84 41.0 3 |                    |      |              |         |  |

 $t_{c} = t_i + t_t$ 

 $t_i=((0.395(1.1-C_5)SQRT(L))/(S_0^0.33))$ 

 $V = C_v * S_w^{0.5}$ 

| Table 6-7. Conveyance Co             | pefficient, C <sub>v</sub> |
|--------------------------------------|----------------------------|
| Heavy meadow                         | 2.5                        |
| Tillage/Field                        | 5                          |
| Riprap (not buried)*                 | 6.5                        |
| Short pasture and lawns              | 7                          |
| Nearly bare ground                   | 10                         |
| Grassed waterway                     | 15                         |
| Paved areas and shallow paved swales | 20                         |

<sup>\*</sup>For bured riprap, select C<sub>v</sub> value based on type of vegetative cover.

= FORMULA CELLS = USER INPUT CELLS Calculated By: SPC
Date: 8/16/2022
Checked By: SGB

5-Year

1-hour rainfall=

## **STANDARD FORM SF-2**

Project: ORTON PIT SITE
Job No.: 35059
Design Storm: 5-Year

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

= FORMULA CELLS = USER INPUT CELLS

|       |                               |                | DI           | RECT F       | SLINIOE | F          |              |            | Т                       | ΟΤΔΙ Ε            | RUNOF   | F          | STR       | FFT      |                      | PIPE      |                     |                |                   |                         | 0021(1111 01 02220 |
|-------|-------------------------------|----------------|--------------|--------------|---------|------------|--------------|------------|-------------------------|-------------------|---------|------------|-----------|----------|----------------------|-----------|---------------------|----------------|-------------------|-------------------------|--------------------|
| BASIN | DESIGN                        | AREA<br>DESIGN | AREA<br>(AC) | RUNOFF COEFF | (MIN)   | C * A (AC) | I<br>(IN/HR) | Q<br>(CFS) | t <sub>c</sub><br>(MIN) | S (C * A)<br>(CA) | (IN/HR) | Q<br>(CFS) | SLOPE (%) | STREET F | DESIGN<br>FLOW (CFS) | SLOPE (%) | PIPE DIAM.<br>(IN.) | LENGTH<br>(FT) | VELOCITY<br>(FPS) | t <sub>t</sub><br>(MIN) | REMARKS            |
|       | (2)                           | (3)            | (4)          | (5)          | (6)     | (7)        | (8)          | (9)        | (10)                    | (11)              | (12)    | (13)       | (14)      | (15)     | (16)                 | (17)      | (18)                | (19)           | (20)              | (21)                    | (22)               |
|       |                               |                |              |              |         |            |              |            |                         | Exi               | sting C | onditio    | ns Sul    | bbasin   | S                    |           |                     |                |                   |                         |                    |
| E1    | 1                             | DP1            | 16.43        | 0.09         | 37.3    | 1.48       | 2.15         | 3.18       |                         |                   |         |            |           |          |                      |           |                     |                |                   |                         |                    |
| E2    | 2                             | DP1            | 26.40        | 0.09         | 49.5    | 2.38       | 1.73         | 4.11       |                         |                   |         |            |           |          |                      |           |                     |                |                   |                         |                    |
|       | Proposed Conditions Subbasins |                |              |              |         |            |              |            |                         |                   |         |            |           |          |                      |           |                     |                |                   |                         |                    |
| P1    | 1                             | DP1            | 16.43        | 0.09         | 37.6    | 1.48       | 2.14         | 3.17       |                         |                   |         |            |           |          |                      |           |                     |                |                   |                         |                    |

Calculated By: SPC

Date: 8/16/2022 Checked By: SGB

100-Year 1-hour rainfall=

## **STANDARD FORM SF-2**

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project: ORTON PIT SITE

Job No.: 35059
Design Storm: 100-Year

= FORMULA CELLS = USER INPUT CELLS

|       |        |                |              |                 |                         |               |              |            |                         |                   |              |            |              |                |                      |              |                     |                |                   |                         | - 0021(1111 01 02220 |
|-------|--------|----------------|--------------|-----------------|-------------------------|---------------|--------------|------------|-------------------------|-------------------|--------------|------------|--------------|----------------|----------------------|--------------|---------------------|----------------|-------------------|-------------------------|----------------------|
|       |        |                | D            | IRECT           | RUNO                    | FF            |              |            | T                       | OTAL I            | RUNOF        | F          | STR          | EET            |                      | PIPE         |                     |                |                   |                         |                      |
| BASIN | DESIGN | AREA<br>DESIGN | AREA<br>(AC) | RUNOFF<br>COEFF | t <sub>c</sub><br>(MIN) | C * A<br>(AC) | I<br>(IN/HR) | Q<br>(CFS) | t <sub>c</sub><br>(MIN) | S (C * A)<br>(CA) | I<br>(IN/HR) | Q<br>(CFS) | SLOPE<br>(%) | STREET<br>FLOW | DESIGN<br>FLOW (CFS) | SLOPE<br>(%) | PIPE DIAM.<br>(IN.) | LENGTH<br>(FT) | VELOCITY<br>(FPS) | t <sub>t</sub><br>(MIN) | REMARKS              |
|       | (2)    | (3)            | (4)          | (5)             | (6)                     | (7)           | (8)          | (9)        | (10)                    | (11)              | (12)         | (13)       | (14)         | (15)           | (16)                 | (17)         | (18)                | (19)           | (20)              | (21)                    | (22)                 |
|       |        |                |              |                 |                         |               |              |            |                         | Ex                | isting (     | Condition  | ons Su       | bbasin         | S                    |              |                     |                |                   |                         |                      |
| E1    | 1      | DP1            | 16.43        | 0.36            | 37.3                    | 5.92          | 3.61         | 21.37      |                         |                   |              |            |              |                |                      |              |                     |                |                   |                         |                      |
| E2    | 2      | DP1            | 26.40        | 0.36            | 49.5                    | 9.50          | 2.90         | 27.60      |                         |                   |              |            |              |                |                      |              |                     |                |                   |                         |                      |
|       |        |                |              |                 |                         |               |              |            |                         | Pro               | posed        | Condit     | ions S       | ıbbasiı        | าร                   |              |                     |                |                   |                         |                      |
| P1    | 1      | DP1            | 16.43        | 0.36            | 37.6                    | 5.92          | 3.59         | 21.26      |                         |                   |              |            |              |                |                      |              |                     |                |                   |                         |                      |

JOB NO.: 35059 CALC. BY: SPC DATE: 8/16/2022



|                | DIRECT RUNOFF SUMMARY |              |        |      |          |          |            |      |                |       |
|----------------|-----------------------|--------------|--------|------|----------|----------|------------|------|----------------|-------|
| BASIN<br>LABEL | DESIGN<br>POINT       | AREA<br>[ac] | Imp. % | C5   | C100     |          | CAL<br>FS) |      | ULATIVE<br>FS) | Notes |
| LADEL          | 1 Ollvi               | [ac]         |        |      |          | Q5       | Q100       | Q5   | Q100           |       |
|                |                       |              |        |      | Existing | Subbasi  | ins        |      |                |       |
| E2             | 2                     | 26.40        | 2%     | 0.09 | 0.36     | 4.11     | 27.60      |      |                |       |
| E1             | 1                     | 16.43        | 2%     | 0.09 | 0.36     | 3.18     | 21.37      | 7.30 | 48.97          |       |
|                |                       |              |        |      | Proposed | d Subbas | sins       |      |                |       |
| P1             | 1                     | 16.43        | 2%     | 0.09 | 0.36     | 3.17     | 21.26      | 7.28 | 48.85          |       |

11 (5 (

# Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

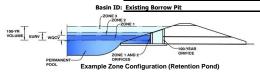
|  |                 | LID Credi     | _          |               |               |                |                | _             |              |               |            |  |            |  |
|--|-----------------|---------------|------------|---------------|---------------|----------------|----------------|---------------|--------------|---------------|------------|--|------------|--|
|  |                 |               | UD         | O-BMP (Versio | n 3.06, Noven | nber 2016)     |                |               |              |               |            |  |            |  |
| User Input   |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Calculated cells   |                 |               |            | Designer:     | SPC           |                |                |               |              |               |            |  |            |  |
| Carculated cens  |                 |               |            | Company:      |               | ine Enginee    | ring Corp      |               |              |               |            |  |            |  |
| ***Design Storm: 1-Hour Rain Depth WQCV Event  | 0.02            | inches        |            | Date:         |               | st 16, 2022    | <u>B</u> 60. P |               |              |               |            |  |            |  |
| ***Minor Storm: 1-Hour Rain Depth 5-Year Event   | 1.22            | inches        |            | Project:      |               |                |                |               |              |               |            |  |            |  |
| ***Major Storm: 1-Hour Rain Depth 100-Year Event   | 2.61            | inches        |            | Location:     |               | so County      |                |               |              |               |            |  |            |  |
| Optional User Defined Storm CUHP   |                 |               |            |               |               | <u>-</u>       |                |               |              |               |            |  |            |  |
| (CUHP) NOAA 1 Hour Rainfall Depth and Frequency  | 2.61            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| for User Defined Storm   |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Max Intensity for Optional User Defined Storm 2.60478  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| SITE INFORMATION (USER-INPUT)  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Sub-basin Identifier   | P1              |               |            |               |               | Т              |                | Т             | т —          |               | Т          |  |            |  |
| Sub-basin identifier   | PI              |               |            |               |               |                |                | -             |              |               |            |  |            |  |
| Receiving Pervious Area Soil Type  | Loam            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)   | 16.43           |               |            |               |               |                |                |               |              |               |            | <del>                                     </del> |            | $\overline{}$                                    |
| Directly Connected Impervious Area (DCIA, acres)   | 0.00            |               |            |               |               |                |                |               |              |               |            | $\overline{}$                                    |            | $\overline{}$                                    |
| Unconnected Impervious Area (UIA, acres)   | 0.00            |               |            |               |               |                |                |               |              |               |            | $\overline{}$                                    |            | $\overline{}$                                    |
| Receiving Pervious Area (RPA, acres)   | 0.00            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Separate Pervious Area (SPA, acres)  | 16.43           |               |            |               |               |                |                |               |              |               |            |  |            |  |
| RPA Treatment Type: Conveyance (C),  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Volume (V), or Permeable Pavement (PP)   | С               |               |            |               |               |                |                |               |              |               |            |  |            |  |
|  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
|  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| CALCULATED RESULTS (OUTPUT)  |                 |               |            |               |               | _              |                | _             | _            |               | _          |  |            |  |
| Total Calculated Area (ac, check against input)  | 16.430          |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Directly Connected Impervious Area (DCIA, %)   | 0.0%            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Unconnected Impervious Area (UIA, %)   | 0.0%            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| Receiving Pervious Area (RPA, %)   | 0.0%            |               |            |               |               |                |                |               |              |               |            | <u> </u>   |            |  |
| Separate Pervious Area (SPA, %)  | 100.0%          |               |            |               |               |                |                |               |              |               |            | <u> </u>   | <u> </u>   |  |
| A <sub>R</sub> (RPA / UIA)   | 0.000           |               |            |               |               |                |                |               |              |               |            |  |            |  |
| I <sub>a</sub> Check   | 1.000           |               |            |               |               |                |                |               |              |               |            |  |            |  |
| f / I for WQCV Event:  | 28.7            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| f / I for 5-Year Event:  | 0.4             |               |            |               |               | 1              |                |               | 1            |               | 1          |  |            |  |
| f / I for 100-Year Event:  | 0.2             |               |            |               |               | 1              |                |               | 1            |               | 1          |  |            |  |
| f / I for Optional User Defined Storm CUHP:  | 0.18            |               |            |               |               |                |                |               |              |               |            |  |            |  |
| IRF for WQCV Event:  | 1.00            |               |            |               |               | 1              |                |               | -            |               |            | <del> </del>                                     |            |  |
| IRF for 5-Year Event:  | 1.00            |               |            |               |               | 1              |                | 1             | 1            |               | 1          |  |            |  |
| IRF for 100-Year Event:  | 1.00            |               |            |               |               | 1              |                | 1             | 1            |               | 1          |  |            |  |
| IRF for Optional User Defined Storm CUHP:  | 1.00            |               |            |               |               | 1              |                | 1             | 1            |               | 1          |  |            |  |
| Total Site Imperviousness: I <sub>total</sub>  | 0.0%            |               |            |               |               | 1              |                | 1             | 1            |               | 1          | +  | +          | -  |
| Effective Imperviousness for WQCV Event:   | 0.0%            |               |            |               |               | 1              |                | 1             | 1            |               | 1          | +  | +          | -  |
| Effective Imperviousness for 5-Year Event:   | 0.0%            |               |            |               | -             | +              | -              | +             | +            |               | +          | +  | +          | +  |
| Effective Imperviousness for 100-Year Event:  Effective Imperviousness for Optional User Defined Storm CUHP: | 0.0%            |               |            |               |               | +              |                |               |              |               | +          | +  | +          | <del>                                     </del> |
| Effective imperviousness for Optional User Defined Storm COHP:   | U.U%            |               |            | ]             |               |                |                | 1             | 1            |               | 1          |  |            |  |
|  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| LID / EFFECTIVE IMPERVIOUSNESS CREDITS   |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |
| WQCV Event CREDIT: Reduce Detention By:  | N/A             | N/A           | N/A        | N/A           | N/A           | N/A            | N/A            | N/A           | N/A          | N/A           | N/A        | N/A  | N/A        | N/A  |
| This line only for 10-Year Event<br>100-Year Event CREDIT**: Reduce Detention By:                            | N/A<br>N/A      | N/A<br>N/A    | N/A<br>N/A | N/A<br>N/A    | N/A<br>N/A    | N/A<br>N/A     | N/A<br>N/A     | N/A<br>N/A    | N/A<br>N/A   | N/A<br>N/A    | N/A<br>N/A | N/A<br>N/A                                       | N/A<br>N/A | N/A<br>N/A                                       |
| User Defined CUHP CREDIT: Reduce Detention By:   | 0.0%            | IN/A          | IN/ A      | IV/A          | IN/A          | IN/A           | IN/ A          | IN/A          | IN/A         | IN/ A         | IN/A       | IN/A   | IN/A       | IN/A   |
|  |                 |               |            | ·             | •             | •              | •              | •             | •            | •             | •          | -  | -          |  |
|  | Total Site Imp  | perviousness: | 0.0%       |               | Notes:        |                |                |               |              |               |            |  |            |  |
| Total Site Effective Impe  | WOCV Fvent      | 0.0%          |            | * Hsp Groom   | ı-Ampt averag | e infiltration | rate values f  | rom Table 2-3 | ł            |               |            |  |            |  |
| Total Site Effective Impe  | 0.0%            | 1             |            |               |               |                |                |               | Storage Chan | ter of USDCM  | l.         |  |            |  |
| Total Site Effective Impervi   | 0.0%            | ]             |            |               |               |                |                |               |              | ation purpose |            |  |            |  |
| Total Site Effective Imperviousness for Optiona  | al User Defined | Storm CUHP:   | 0.0%       | J             |               |                |                |               |              |               |            |  |            |  |
|  |                 |               |            |               |               |                |                |               |              |               |            |  |            |  |

35059 - UD-BMP\_v3.06, IRF

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Orton Pit (THIS SHEET ONLY USED FOR VOLUME CALCULATIONS)



#### Watershed Information

| Selected BMP Type =                     | RP         |         |
|---|------------|---------|
| Watershed Area =                        | 42.83      | acres   |
| Watershed Length =                      | 4,005      | ft      |
| Watershed Length to Centroid =          | 1,825      | ft      |
| Watershed Slope =                       | 0.020      | ft/ft   |
| Watershed Imperviousness =              | 2.00%      | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                |            | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

L / W Ratio = 8.6

Note: L / W Ratio > 8

**Drain Time Too Short** 

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  | SP    |           |
|--|-------|-----------|
| Water Quality Capture Volume (WQCV) =  |       | acre-feet |
| Excess Urban Runoff Volume (EURV) =    |       | acre-feet |
| 2-yr Runoff Volume (P1 = 0.95 in.) =   | 0.039 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.22 in.) =   | 0.288 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.47 in.) =  | 0.787 | acre-feet |
| 25-yr Runoff Volume (P1 = 1.88 in.) =  | 2.485 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.23 in.) =  | 3.612 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.61 in.) = | 5.216 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.64 in.) = | 8.873 | acre-feet |
| Approximate 2-yr Detention Volume =    |       | acre-feet |
| Approximate 5-yr Detention Volume =    |       | acre-feet |
| Approximate 10-yr Detention Volume =   |       | acre-feet |
| Approximate 25-yr Detention Volume =   |       | acre-feet |
| Approximate 50-yr Detention Volume =   |       | acre-feet |
| Approximate 100-yr Detention Volume =  |       | acre-feet |
|  |       |           |

| 0 | pti | ona | ıΙU | Jsei | - 0 | ve | rrid | les |
|---|-----|-----|-----|------|-----|----|------|-----|
|   |     |     |     |      |     |    |      |     |

|      | acre-feet |
|------|-----------|
|      | acre-feet |
| 0.95 | inches    |
| 1.22 | inches    |
| 1.47 | inches    |
| 1.88 | inches    |
| 2.23 | inches    |
| 2.61 | inches    |
| 3.64 | inches    |
|      |           |

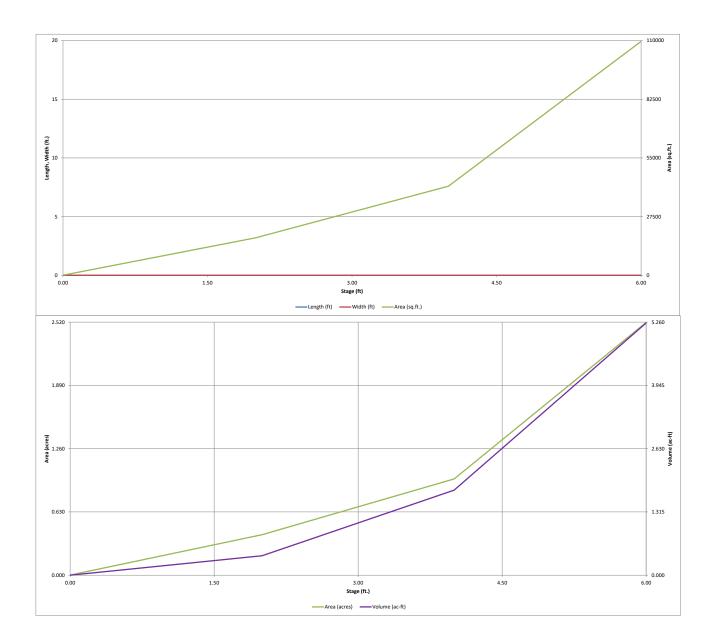
#### Define Zones and Basin Geometry

| Jenne Zones and Basin Geometry                          |      |                 |
|---|------|-----------------|
| Select Zone 1 Storage Volume (Required) =               |      | acre-fee        |
| Select Zone 2 Storage Volume (Optional) =               |      | acre-feet       |
| Select Zone 3 Storage Volume (Optional) =               |      | acre-fee        |
| Total Detention Basin Volume =                          |      | acre-fee        |
| Initial Surcharge Volume (ISV) =                        | N/A  | ft <sup>3</sup> |
| Initial Surcharge Depth (ISD) =                         | N/A  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | user | ft              |
| Depth of Trickle Channel $(H_{TC}) =$                   | N/A  | ft              |
| Slope of Trickle Channel ( $S_{TC}$ ) =                 | N/A  | ft/ft           |
| Slopes of Main Basin Sides (Smain) =                    | user | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | user |                 |
|   |      | •               |

| Initial Surcharge Area (A <sub>ISV</sub> ) =    | ft²             |
|---|-----------------|
| Surcharge Volume Length $(L_{ISV}) =$           | ft              |
| Surcharge Volume Width $(W_{ISV}) =$            | ft              |
| Depth of Basin Floor $(H_{FLOOR}) =$            | ft              |
| Length of Basin Floor $(L_{FLOOR})$ =           | ft              |
| Width of Basin Floor $(W_{FLOOR}) =$            | ft              |
| Area of Basin Floor $(A_{FLOOR}) =$             | ft 2            |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =   | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =      | ft              |
| Length of Main Basin $(L_{MAIN}) =$             | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =      | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =       | ft 2            |
| Volume of Main Basin (V <sub>MAIN</sub> ) =     | ft <sup>3</sup> |
| Calculated Total Basin Volume ( $V_{total}$ ) = | acre-fe         |
|   |                 |

| Depth Increment =              |               | ft                                 |                |               |                            |   |                |                              |                   |
|--------------------------------|---------------|------------------------------------|----------------|---------------|----------------------------|---|----------------|------------------------------|-------------------|
| Stage - Storage<br>Description | Stage<br>(ft) | Optional<br>Override<br>Stage (ft) | Length<br>(ft) | Width<br>(ft) | Area<br>(ft <sup>2</sup> ) | Optional<br>Override<br>Area (ft <sup>2</sup> ) | Area<br>(acre) | Volume<br>(ft <sup>3</sup> ) | Volume<br>(ac-ft) |
| Permanent Pool                 | -             | 0.00                               |                |               |                            | 54  | 0.001          |                              |                   |
|                                | -             | 2.00                               |                |               |                            | 17,574  | 0.403          | 17,628                       | 0.405             |
|                                | -             | 4.00                               |                |               |                            | 41,758  | 0.959          | 76,960                       | 1.767             |
|                                | -             | 6.00                               |                |               |                            | 109,623   | 2.517          | 228,341                      | 5.242             |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    | -              |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    | -              |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                | 1                            |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                | -                            |                   |
|                                | -             |                                    |                |               |                            |   |                | 1                            |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    | -              |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | _             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    | -              |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                | 1                            |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                | <del></del>                  |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               | <br><br>                   |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                | <del> </del>                 |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    | -              |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                | 1                            |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                | -             |                                    |                |               |                            |   |                |                              |                   |
|                                |               |                                    |                |               |                            |   |                |                              |                   |

35059 - Pit Calcs - MHFD-Detention\_v4-06, Basin



35059 - Pit Calcs - MHFD-Detention\_v4-06, Basin 8/16/2022, 3:20 PM



PROJECT NAME: ORTON PIT

PROJECT NUMBER: 385
CALCULATED BY: SPC
CHECKED BY: SGB

## **Existing Borrow Pit Storage Calculations**

#### **Existing Volume**

| Stage (ft) | Contour<br>Elevation (ft) | Area (ft <sup>2</sup> ) | Total Volume (ft <sup>3</sup> ) | Total Volume (ac-ft) |
|------------|---------------------------|-------------------------|---------------------------------|----------------------|
| 0          | 6374                      | 54                      | 0                               | 0.000                |
| 2          | 6376                      | 17,574                  | 17,628                          | 0.405                |
| 4          | 6378                      | 41,758                  | 76,960                          | 1.767                |
| 6          | 6380                      | 109,623                 | 228,341                         | 5.242                |

| Stormwater Runoff Quantities (from MHFD Detention Workbook v.4.06) |                |             |             |            |  |  |  |  |
|--|----------------|-------------|-------------|------------|--|--|--|--|
|  |                |             |             |            |  |  |  |  |
| _  | Volume (AC-FT) | Volume (CF) | <u>WSEL</u> | Depth (ft) |  |  |  |  |
| 5-YR   | 0.288          | 12,545      | 6375.42     | 1.42       |  |  |  |  |
| 100-YR   | 5.216          | 227,209     | 6379.99     | 5.99       |  |  |  |  |

<sup>\*</sup>This calculation assumes no additional infiltration within the exisitng borrow pit depression. Runoff quantities reaching the existing borrow pit depression will remain unchanged from historic to proposed conditions.



Client: Castle Rock Construction

Company, Inc.

 Project No.:
 22-1154

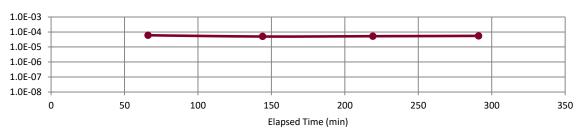
 Report Date:
 8/12/2022

Reviewed By: EK

#### **CRCC Laboratory Testing Services**

## Permeability - Flexible Wall (ASTM D5084)





| Method |                                    | Tested By | Prep.  | Specific Gravity | Water Density (pcf) |
|--------|------------------------------------|-----------|--------|------------------|---------------------|
|        | C - Falling Head, Rising Tailwater | JW        | Remold | 2.65 Estimated   | 62.24               |

| Specimen Data             |          |           |  |  |  |  |
|---------------------------|----------|-----------|--|--|--|--|
| Property                  | Pre-Test | Post-Test |  |  |  |  |
| Mass (gm)                 | 653.1    | 662.7     |  |  |  |  |
| Average Diameter (in)     | 2.790    | 2.788     |  |  |  |  |
| Diameter Variation (%)    | 0.1      | 0.1       |  |  |  |  |
| Average Length (in)       | 2.987    | 2.970     |  |  |  |  |
| Length Variation (%)      | 0.1      | 0.1       |  |  |  |  |
| Area (in²)                | 6.112    | 6.105     |  |  |  |  |
| Volume (in <sup>3</sup> ) | 18.255   | 18.133    |  |  |  |  |
| Wet Density (pcf)         | 136.3    | 139.2     |  |  |  |  |
| Moisture (%)              | 10.2     | 12.1      |  |  |  |  |
| Dry Density (pcf)         | 123.6    | 124.2     |  |  |  |  |
| Void Ratio                | 0.334    | 0.328     |  |  |  |  |
| Saturation (%)            | 81       | 98        |  |  |  |  |

| Back Pressure Saturation / Consolidation |      |        |  |  |  |  |
|--|------|--------|--|--|--|--|
| Permeant Deaired Tap W                   |      |        |  |  |  |  |
| Start Date                               |      | 8/9/22 |  |  |  |  |
| Cell Pressure (psi)                      | 45.0 |        |  |  |  |  |
| Back Pressure (psi)                      | 40.0 |        |  |  |  |  |
| Effective Consol. Stress (psi)           | 5.0  |        |  |  |  |  |
| B-Value                                  | 0.98 |        |  |  |  |  |

| Permeation Conditions      |      |  |  |  |  |
|----------------------------|------|--|--|--|--|
| Inflow Burette Area (cm²)  | 1.00 |  |  |  |  |
| Outflow Burette Area (cm²) | 1.00 |  |  |  |  |
| Cell Pressure (psi)        | 45.0 |  |  |  |  |
| Top Cap Pressure (psi)     | 40.0 |  |  |  |  |
| Base Cap Pressure (psi)    | 40.0 |  |  |  |  |

|      | Permeation Trial Data |          |            |          |                   |                   |          |         |             |         |
|------|-----------------------|----------|------------|----------|-------------------|-------------------|----------|---------|-------------|---------|
| Date | Time                  | Temp. ºC | Heads (cm) |          | Incrementa<br>(cr | al Volumes<br>n³) | Gradient | •       | onductivity |         |
|      |                       |          | Elev.      | Pressure | Total             | Outflow           | Inflow   |         | m/s         | cm/s    |
| 8/11 | 8:00                  | 23.0     | 15.0       | 0.0      | 15.0              | 0.00              | 0.00     | 2.0     | -           | -       |
| 8/11 | 9:06                  | 23.3     | 1.0        | 0.0      | 1.0               | 7.00              | 7.00     | 0.1     | 6.1E-07     | 6.1E-05 |
| 8/11 | 10:00                 | 23.3     | 15.0       | 0.0      | 15.0              | 0.00              | 0.00     | 2.0     | -           | -       |
| 8/11 | 11:18                 | 23.7     | 1.0        | 0.0      | 1.0               | 7.00              | 7.00     | 0.1     | 5.1E-07     | 5.1E-05 |
| 8/11 | 11:30                 | 23.7     | 15.0       | 0.0      | 15.0              | 0.00              | 0.00     | 2.0     | -           | -       |
| 8/11 | 12:45                 | 24.1     | 1.0        | 0.0      | 1.0               | 7.00              | 7.00     | 0.1     | 5.2E-07     | 5.2E-05 |
| 8/11 | 13:00                 | 24.1     | 15.0       | 0.0      | 15.0              | 0.00              | 0.00     | 2.0     | -           | -       |
| 8/11 | 14:12                 | 23.4     | 1.0        | 0.0      | 1.0               | 7.00              | 7.00     | 0.1     | 5.5E-07     | 5.5E-05 |
| -    | -                     | -        | -          | -        | 1                 | -                 | -        | -       | -           | -       |
| -    | -                     | -        | -          | -        | -                 | -                 | -        | -       | -           | -       |
| -    | -                     | -        | -          | -        | -                 | -                 | -        | -       | -           | -       |
| -    | -                     | -        | -          | -        | -                 | -                 | -        | -       | -           | -       |
| •    |                       | •        |            |          | •                 | •                 |          | Average | 5.5E-07     | 5.5E-05 |

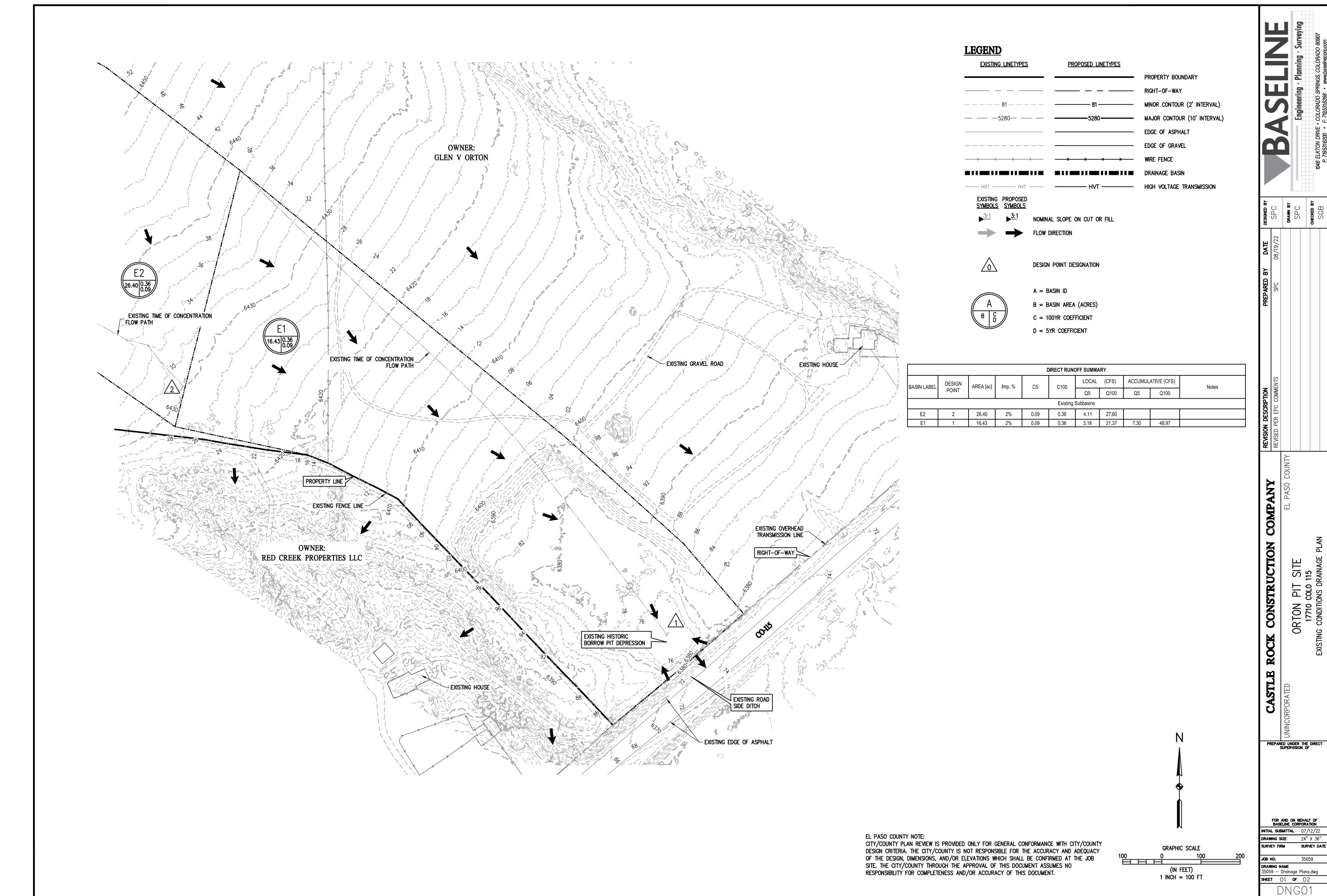
Sample: Client delivered Classification: - < No. 200 (%): 22.3

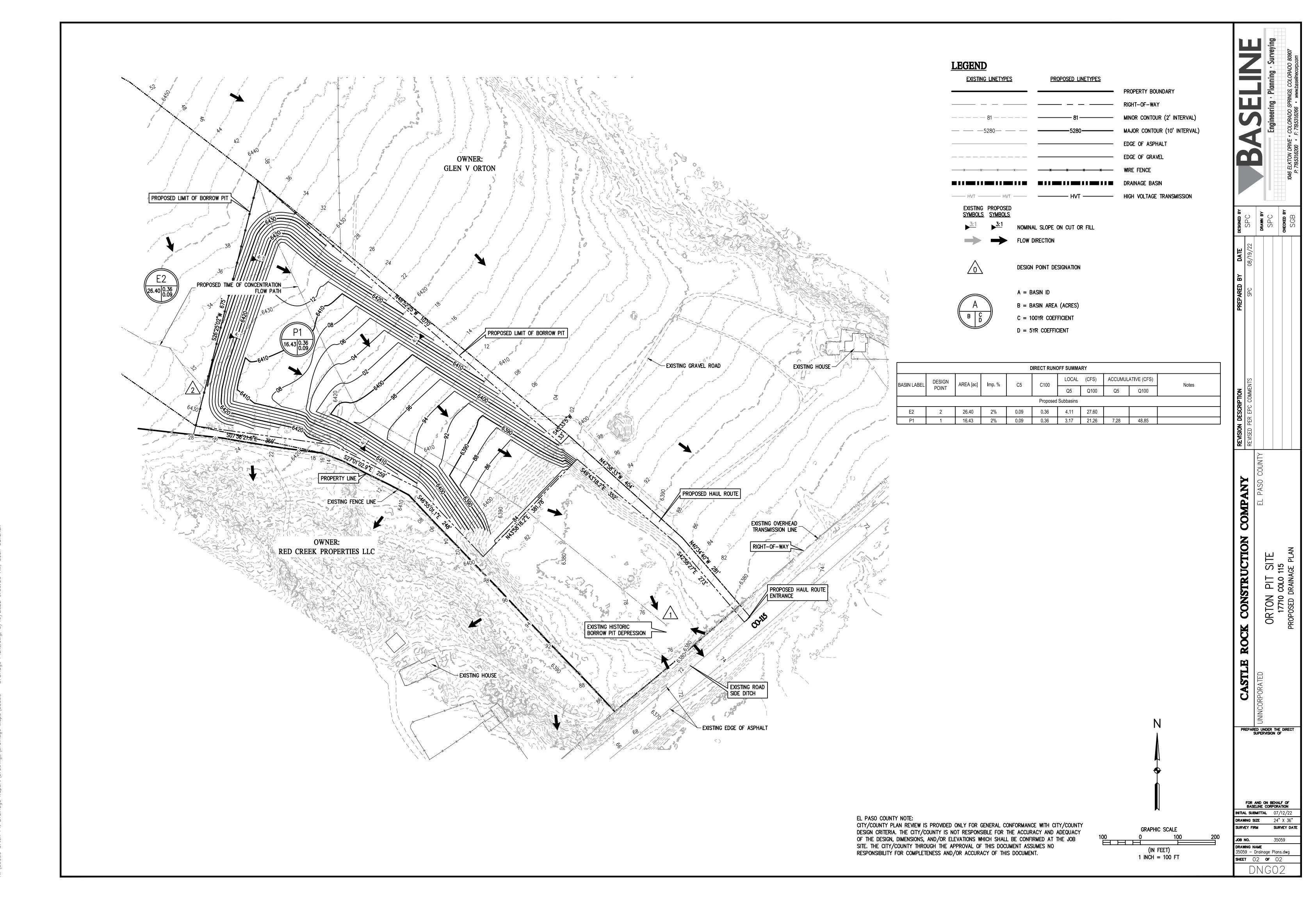
Description: Sand with silt and gravel Liquid Limit: 
Plasticity Index: -

Test Remarks: Only the material passing the 1/2 inch sieve was used for testing.

# APPENDIX C







2.\35059 Orton Pit Drainage Report\Drawings\Drainage Mans\35059 — Drainage Plans dwa -8/19/2022 9:56:20 AM Sean Callaban

# APPENDIX D





6374 S. Racine Circle

Centennial, Colorado 80111

www.castlerockconstructionco.com

August 17th, 2022

El Paso County Planning and Community Development Department 2880 International Circle, Suite 110 Colorado Springs, CO 80910

Re: Water Rights Documents for the Proposed Orton Pit

To Whom it Concerns,

Following the completion of the final drainage report it was confirmed by Baseline Engineering that the Orton Pit will not retain water following completion of the project, and will convey all storm drainage in the same pattern that the existing drainage follows. Due to this fact CRCC does not intend to acquire water rights, since they will not be legally required.

Following conversations with Dan Henrichs the Division 2, District 12 Water Commissioner for the Colorado Division of Water Resources, it was confirmed that no water rights are required for the proposed pit. Attached is an email from Mr. Henrichs confirming this.

Sincerely,

Travis Bell

General Superintendent

## **Travis Bell**

| From:<br>Sent:<br>To:<br>Cc:<br>Subject:   | Henrichs - DNR, Dan <dan.henrichs@state.co.us> Wednesday, August 17, 2022 12:06 PM Travis Bell Amy Brooks Re: Orton Borrow Pit</dan.henrichs@state.co.us>   |
|--|---|
| Follow Up Flag:<br>Flag Status:  | Follow up<br>Flagged  |
| Travis yes you are good with   | DWR   |
| On Tue, Aug 16, 2022 at 5:25   | 5 PM Travis Bell < tbell@crccllc.com > wrote:   |
| Dan-   |   |
|  |   |
| currently permitted through<br>to an existing depression an<br>Baseline Engineering perfor<br>same as the historic flows g<br>in this area. All dust suppres<br>with our mining permit, we | I just want to confirm that we are in the clear concerning the Orton Borrow pit which is a the Division of Mining Reclamation and Safety. This pit has been designed to freely drain and the newly excavated pit will not retain any water in accordance with our mining permit. It med a drainage report for us which confirmed that all the final flow patterns will remain the oing into the existing depression, thus we will not be affecting the historic drainage pattern assion water will be obtained through our SWSP in Penrose (WDID 1203393). In accordance will be leaving a minimum of two feet of cover above any ground water we encounter. If all lease confirm that we should be clear with regards to Division of Water Resources |
| Best Regards,  |   |
|  |   |
| Travis Bell  |   |
| General Superintendent   |   |
| Castle Rock Construction Co  | mpany of Colo. LLC  |
| (720) 273-6227   |   |
|  |   |



Dan Henrichs
District 12 Water commissioner



dan.henrichs@state.co.us

719-269-2800 cell P.O. Box 304 Florence CO 81226 water.state.co.us