

FALCON RANCHETTES FILING NO. 1A MERIDIAN STORAGE

El Paso County, Colorado

PCD File No. VR239 & PPR2336

PREPARED FOR:

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DATE:

May 6, 2024



Signature Page Falcon Ranchettes Filing No. 1a (Meridian Storage)

Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

| responsibility for arry hability eadsed by arry hegilgent dots, errors or | omissions on my part in proparing this report. |
|--|---|
| Brady Shyrock, PE # 38164 For and on behalf of Galloway & Company, Inc. | 05/21/2024 Date |
| Developer's Certification | |
| I, the developer, have read and will comply with all of the requirement | nts specified in this drainage report and plan. |
| By: Mike Texer | 05/15/2024 |
| Address: Mike D. Texer 11750 Owl Place Petyon, CO 80831 | Date |
| El Paso County Certification | |
| Filed in accordance with the requirements of the Drainage Criteria M Criteria Manual and Land Development Code as amended. | lanual, Volumes 1 and 2, El Paso County Engineering |
| Joshua Palmer, P.E. County Engineer/ECM Administrator | Date |
| Conditions: | |

TABLE OF CONTENTS

| I. Introduction | 4 |
|--|----|
| II. Drainage Design Criteria | 5 |
| Development Criteria Reference | 5 |
| Hydrologic Criteria | 5 |
| Hydraulic Criteria | 7 |
| Four Step Process | 8 |
| III. Existing Drainage Patterns and Features | 9 |
| Existing Drainage Patterns | 9 |
| Sub-Basin Descriptions | 9 |
| IV. Proposed Drainage Patterns and Features | 10 |
| Proposed Drainage Plan | 10 |
| Sub-Basin Descriptions | 11 |
| Proposed Pond #1 Full Spectrum Extended Detention Basin | 14 |
| Sub-Regional Detention Pond (SR4) Outfall | 15 |
| Drainage Channel Improvements – UTBSC East Branch (RMT064) | 15 |
| Existing 36" Twin Culverts | 19 |
| V. Ownership & Maintenance | 19 |
| VI. Fee Development | 19 |
| Drainage & Bridge Fees | 19 |
| Improvements and Reimbursable Costs | 20 |
| VII. Conclusion | 22 |
| VIII. References | 22 |

Appendices:

- A. Exhibits and Figures
- B. Existing Drainage Reports
- C. Hydrologic Computations
- D. Hydraulic Computations
- E. Pond Calculations
- F. Drainage Maps

I. Introduction

This document is the Final Drainage Report for Falcon Ranchettes Filing No. 1a (Meridian Storage). The project consists of two lots and public right-of-way that make up 9.604 acres. This project proposes storage units, an office building, roadway and utility infrastructure, RV parking, a water quality treatment pond, and drainage channel improvements to the existing east branch of Unnamed Tributary to Black Squirrel Creek (UTBSC East Branch).

Purpose

The purpose of this report is to identify on and offsite drainage patterns and confirm that the new development has no significant changes to existing drainage patterns.

Previous Drainage Studies

- Falcon Drainage Basin Planning Study, dated September 2015 Referred to as Falcon DBPS hereon.
- Bent Grass MDDP Amendment & DBPS Amendment, dated September 2021 Referred to as **Bent Grass MDDP** hereon.
- Request for Conditional Letter of Map Revision, Unnamed Tributary to Black Squirrel Creek,
 Falcon Owl Place, dated October 25, 2022 Referred to as Falcon Owl Place CLOMR hereon.
- Request for Letter of Map Revision, Unnamed Tributary to Black Squirrel Creek, Falcon Marketplace, dated March 15, 2021 – Referred to as Falcon Marketplace LOMR hereon.
- Final Drainage Report for Falcon Marketplace, dated November 4, 2019 Referred to as **Falcon Marketplace FDR** hereon.

Relevant excerpts from existing drainage reports are provided in **Appendix B** for reference.

Location

Falcon Ranchettes Filing No. 1a is located in the Southeast Quarter of Section 1, Township 13 South, Range 65 West of the 6th Principal Meridian, County of El Paso, State of Colorado.

The project site is located at the northwest corner of Owl Place and Meridian Road, bounded to the North by Lot 2A Bent Grass East Commercial Fil No 2a and Tract A Bent Grass East Commercial Fil No 2, to the south by Lots 14 & 15 of Falcon Ranchettes, to the East by Meridian Road right-of-way, to the West by Lot 3 of Falcon Ranchettes. A Vicinity Map is provided in **Appendix A**.

Description of Property

The existing parcel is currently developed with two residential properties (*Lot 1 & 2 of Falcon Ranchettes*). Two single-family homes occupy the site, but the majority of the existing parcels are covered by native prairie grass land. An existing drainage-way flows north to south along the eastern property line adjacent to Meridian Road right-of-way, named "Unnamed Tributary to Black Squirrel Creek - East Branch".

Soils

According to the U.S. Department of Agriculture Natural Resources Conservation Service Soil Survey of El Paso County, Colorado (See **Appendix A**) the primary soil found is Columbine gravelly sandy loam, classified as Soil Conservation Service (SCS) hydrologic soil group "A".

Climate

This area of El Paso County is located at the foothills of the Southern Rocky Mountains. Classified as an alpine desert, Falcon, CO averages 300 days of sunshine with low humidity. Annual precipitation ranges between 10-16 inches, occurring mostly in spring and summer months.

Geotechnical Recommendations

Positive drainage away from the structures should be provided during construction and maintained throughout the life of the structures. Any downspouts, roof drains or scuppers should discharge into splash blocks or extensions and away from the structures. Backfill against footings, exterior walls and in utility trenches should be properly compacted and free of all construction debris to reduce the possibility of moisture infiltration. Refer to the Geotechnical Exploration Report prepared by Universal Engineering Sciences for more detailed information.

Flood Insurance Rate Map

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) #08041C0553G, effective date December 7, 2018. The project site is located in Zone X (Areas determined to be outside of the 0.2% annual chance floodplain). A copy of the FIRM map is provided in **Appendix A** for reference.

Major Drainage Basin

Falcon Ranchettes Filing No. 1a is located within the MT060 drainage basin as described in the **Falcon DBPS**. The Falcon Watershed is located in the north central portion of El Paso County and flows southeasterly from the southern slope of the Black Forest. The Falcon watershed contains three perennial streams and has a contributing drainage area of approximately 10.6 square miles at its confluence with Black Squirrel Creek.

Detailed recommendations from the **Falcon DBPS** are included below under "*IV. Proposed Drainage Patterns and Features*".

II. Drainage Design Criteria

Development Criteria Reference

The analysis and design of the drainage concept and stormwater management system for this project was prepared in accordance with the criteria set forth in the Mile High Flood District (MHFD) Urban Storm Drainage Criteria Manual (USDCM) dated January 2016 and the adopted chapters 6 & 13 from the City of Colorado Springs Drainage Criteria Manual (DCM) Vol. 1, last revised January 2021

Hydrologic Criteria

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres. An analysis of the hydrology using the rational method can be found in **Appendix C** - Hydrologic Calculations. The rational method has proved to be accurate for basins of this size and is based on the following formula:

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|---------------------|---|--------------|----|
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Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff intensity (inches/hour)

A = Drainage area (acres)

The rainfall intensity calculations are based on the DCM Figure 6-5 and IDF equations. The one hour point rainfall data for the design are listed in Table 1 below.

Table 1 - Precipitation Data (Table 6.2 in DCM Vol. 1)

| Return Period | One Hour Depth (in). | Intensity (in/hr) |
|---------------|----------------------|-------------------|
| 5-year | 1.50 | 5.17 |
| 100-year | 2.52 | 8.68 |

Time of concentrations have been adapted from equation 6-7 of The City of Colorado Springs Drainage Criteria Manual, Volume 1 which are as follows:

Where:

 T_c = time of concentration (min)

 T_i = overland (initial) flow time (min)

 T_t = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

Overland (Initial) Flow Time: from equations 6-8 from the City of Colorado Springs Drainage Criteria Manual, Volume 1.

$$t_t = \frac{0.395(1.1-C_5)\sqrt{L}}{S^{0.33}}$$

Where:

T_i = overland (initial) flow (min)

 C_5 = runoff coefficient for 5-year frequency

L = length of overland flow (ft) (300 ft maximum for non-urban land uses, 100 ft maximum for urban land uses)

S = average basin slope (ft/ft)

Travel Time

$$V = C_v * S_w 0.5$$

Where:

V = Velocity (ft/s)

 C_v = conveyance coefficient

S_w = watercourse slope (ft/ft)

The runoff coefficients are calculated based on land use, percent imperviousness, and design storm for each basin, as shown in the DCM, (Table 6-6).

Hydraulic Criteria

Storm Pipe

Hydraulic design and analysis for this report were performed through the usage of StormCAD. A tabular summary from analysis performed by StormCAD can be found in **Appendix D** - Hydraulic Calculations. Additionally, the table below shows the parameters used for StormCAD Standard Method Coefficients taken from *DCM Vol 1 Chapter 9 Table 9-4*.

| BEND LOSS | | | |
|---------------------------|-----------------|------------|--|
| BEND ANGLE | K COEFFICIENT | | |
| 0° | 0.05 | | |
| 22.5° | 0.10 | | |
| 45° | 0.40 | | |
| 60° | 0.64 | | |
| 90° | 1.32 | | |
| LATERAL LOSS | | | |
| ONE LATERAL K COEF | FICIENT | | |
| BEND ANGLE | NON -SURCHARGED | SURCHARGES | |
| 45° | 0.27 | 0.47 | |
| 60° | 0.52 | 0.90 | |
| 90° | 1.02 | 1.77 | |
| TWO LATERAL K COEFFICIENT | | | |
| 45° | 0.96 | | |
| 60° | 1.16 | | |
| 90° | 1.52 | | |

Storm Inlets

CDOT-Type R Storm Curb Inlets and CDOT Type C Area Inlets are sized using the UD-Inlet_v5.02 spreadsheet from Mile High Flood District. Additionally, CDOT Type 13 area inlets are sized using a depth to capacity line graph. These calculations are provided in **Appendix D**.

Detention Pond

As shown in Part IV: Onsite PWQ Requirements, Documentation and Considerations of the PBMP Applicability Form, this project is required to provide treatment for the Water Quality Capture Volume (WQCV) Standard.

Proposed *Pond #1* was designed using the Mile High Flood District (MHFD) software spreadsheets; It is the recommended design software because it provides tabulated results of the WQCV, EURV, 2-, 5-, 10-, 25-, 50-, 100- and 500-year storm events routed through the pond. The detention criteria provided by the MHFD's design spreadsheets *MHFD-Detention_v4.06* was used to determine the adequate storage

capacity of the detention pond, and the associated elements of the outlet structure. The UDFCD Manual provides approximate, empirical equations that are utilized in the spreadsheet provided by MHFD. These equations and methods are further described in the USDCM Vol. 2, Ch. 12. The required volume calculations as well as the outlet structure design calculations are provided in **Appendix E** – Pond Calculations of this report.

Detailed water surface elevations and pond design information are included below under "IV. Proposed Drainage Patterns and Features".

Drainage Channel

Proposed improvements to UTBSC East Branch was analyzed using Bentley software *FlowMaster* to properly size a trapezoidal channel to safely convey stormwater while providing 1.0-ft minimum of freeboard. Additionally, the 3 proposed grouted stepped boulder drop structures were designed using criteria set forth in USDCM from Mile High Flood District. FlowMaster calculations can be found in **Appendix D.**

Detailed steps of the Simplified Design Procedure as shown in the USDCM are included below under "IV. Proposed Drainage Patterns and Features".

Four Step Process

The Four Step Process is used to minimize the adverse impacts of urbanization and is a vital component of developing a balanced, sustainable project. Below identifies the approach to the four-step process:

1. Employ Runoff Reduction Practices

This step uses low impact development (LID) practices to reduce runoff at the source. Generally, rather than creating point discharges that are directly connected to impervious areas runoff is routed through pervious areas to promote infiltration. The Impervious Reduction Factor (IRF) method was used and calculations can be found in Appendix E.

2. Implement BMP's That Provide a Water Quality Capture Volume with Slow Release This step utilizes formalized water quality capture volume to slow the release of runoff from the site, while the WQCV will release in no less than 40 hours. Proposed Pond #1 will provide water quality treatment for all developed areas prior to the runoff being released into existing subregional detention pond SR-4.

3. Stabilize Drainageways

This step implements stabilization to channels to accommodate developed flows while protecting infrastructure and controlling sediment loading from erosion in the drainageways. Drainage channel improvements are proposed to the existing UTBSC East Branch (RMT064), including widening the existing channel with 3 proposed grouted stepped boulder drop structures.

4. Implement Site Specific and Other Source Control BMPs

The biggest source control BMP is public education which can be found on the City of Colorado Springs website and discuss topics such as: pet waste, car washing, private maintenance landscaping, fall leaves, and snow melt and deicer. A no vehicle maintenance policy will be enforced to avoid the potential contaminations caused from vehicle fluid replacement, and

equipment replacement and repair. In addition, the landscaping and snow removal is handled completely by the property management to ensure proper lawn mowing and grass clipping disposal, lawn aeration, and fertilizer application is being followed. Snow removal will also be handled by the property manager to ensure proper consideration of snow pile placement and use of deicing chemicals.

III. Existing Drainage Patterns and Features

Existing Drainage Patterns

On-Site:

The existing drainage pattern sheet flows from north to south. Basin MT060 represents all flows from the existing roadside ditch entering the project site, including the 24" pond outfall from Bent Grass. Flows from basin EX-1 sheet flow into the existing roadside ditch (RMT064) and then conveyed to DP1 where existing 36" twin CMP culverts pipe conveys flows under Owl Place. The culverts are severely undersized and partially filled with sediment, a detailed analysis of these culverts is provided in the Owl Place CLOMR. Basins EX-2 and EX-3 flow south and pool along the north edge Owl Place near DP2 and DP3. Flows eventually overtop the gravel road and continue south.

Off-Site:

Basins **EX-4**, **OS-1**, **OS-2** and **OS-3** flow south and pool at **DP4**. These flows eventually overtop the gravel road and continue south.

Sub-Basin Descriptions

Note: an existing drainage map is provided in **Appendix F** and should be referenced when reading the basin descriptions below.

Basin MT060 (Q5 = 304.6 cfs, Q100 = 915.3 cfs): a basin that encompasses all flows from the existing roadside ditch (RMT064) entering the project site at the northeast corner, including the 24" pond outfall from Bent Grass. Flows are conveyed south to **DP1** where existing 36" twin CMP culverts pipe flows under Owl Place. Existing drainage channel (RMT064) conveys flows south to sub-regional detention pond SR4.

Basin EX-1 (4.97 acres, Q5 = 1.6 cfs, Q100 = 7.7 cfs): a basin that encompasses the northeast portion of the project site. Runoff sheet flows from north to south and eventually spills into the existing Meridian Road roadside ditch, RMT064. Flows continue south to **DP1** where existing 36" twin CMP culverts pipe flows under Owl Place. Existing drainage channel (RMT064) conveys flows south to sub-regional detention pond SR4.

Basin EX-2 (2.32 acres, Q5 = 0.6 cfs, Q100 = 3.2 cfs): a basin that encompasses a portion of the center of the site. Flows drain from north to south to **DP2** where flows pool along the north edge of Owl Place until eventually overtopping the gravel road and continuing south, ultimately to sub-regional detention pond SR4.

Basin EX-3 (2.85 acres, Q5 = 0.3 cfs, Q100 = 3.0 cfs): a basin that encompasses the west portion of the site. Flows drain from north to south to **DP3** where flows pool along the north edge of Owl Place until

eventually overtopping the gravel road and continuing south, ultimately to sub-regional detention pond SR4.

Basin EX-4 (1.08 acres, Q5 = 0.0 cfs, Q100 = 0.9 cfs): a basin that encompasses the far west portion of the site. Flows drain from north to south to **DP4** where flows pool along the north edge of Owl Place until eventually overtopping the gravel road and continuing south, ultimately to sub-regional detention pond SR4.

Basin OS-1 (3.89 acres, Q5 = 0.7 cfs, Q100 = 4.5 cfs): a basin that is associated with Lot 3 and 4 Falcon Ranchettes, and portions of the rear of lots 24, 25 and 26 of Bent Grass Residential Filing No. 1. Runoff sheet flows into a shallow swale and then conveyed from north to south to **DP4** where flows pool along the north edge of Owl Place until eventually overtopping the gravel road and continuing south, ultimately to sub-regional detention pond SR4.

Basin OS-2 (2.35 acres, Q5 = 0.6 cfs, Q100 = 3.0 cfs): a basin that is associated with Lot 3 and 4 Falcon Ranchettes, and portions of the rear of lots 26 and 27 of Bent Grass Residential Filing No. 1. Runoff sheet from north to south to **DP4** where flows pool along the north edge of Owl Place until eventually overtopping the gravel road and continuing south, ultimately to sub-regional detention pond SR4.

Basin OS-3 (0.24 acres, Q5 = 0.0 cfs, Q100 = 0.2 cfs): a basin that is associated with Lot 3 Falcon Ranchettes, a parcel immediately west of the project site. Flows drain from north to south to **DP4** where flows pool along the north edge of Owl Place until eventually overtopping the gravel road and continuing south, ultimately to sub-regional detention pond SR4.

Basin OS-4E (0.05 acres, Q5 = 0.2 cfs, Q100 = 0.4 cfs): a basin that encompasses the existing cul-desac in Meridian Park Drive ROW. This basin represents the limits of disturbance for roadway improvements and should be compared to proposed basin **OS-4P** located below in "*IV. Proposed Drainage Patterns and Features*". Runoff sheet flows north onto Type A curb and gutter and conveyed to an existing 6' CDOT Type 'R' Sump Inlet (Public), **DP14**.

IV. Proposed Drainage Patterns and Features

Proposed Drainage Plan

On-Site:

Proposed Lot 1a consists of 1 office building and 9 self-storage. Access is provided from Meridian Park Drive near the center of the site, with an emergency access drive to the north for emergency services only. An inverted crowned roadway with concrete valley gutter are used for all internal drive aisles to route runoff to proposed storm drain infrastructure. Flows are then piped to Pond #1 providing detention and treatment for the WQCV, EURV, and 100-Year. The pond outfall conveys flows south, directly outfalling into existing sub-regional pond (SR-4).

Proposed Lot 2a consists of RV Parking, Pond #1 is located at the southern end of the lot. RV Parking will likely be a temporary condition until Lot 2a is eventually redeveloped into additional self-storage units. Pond #1 is designed to accommodate the future self-storage imperviousness.

The proposed public roadway improvements convey runoff using curb and gutter and routing flows to proposed storm drain infrastructure and then piped to Pond #1 to provide detention and treatment for the WQCV. The pond outfall conveys flows south directly to an existing sub-regional pond (SR-4).

Drainage channel improvements to the existing RMT064 is discussed below under "*IV. Proposed Drainage Patterns and Features*", including the existing culvert crossing at Owl Place.

Off-Site:

The existing drainage pattern of OS-1, OS-2 and OS-3 remains unchanged. However, to avoid the stormwater pooling and overtopping at Owl Place, a CDOT Type C Area Inlet (Private) is proposed to capture flows and route the runoff safely to Pond SR-4.

Sub-Basin Descriptions

Note: a proposed drainage map is provided in **Appendix F** and should be referenced when reading the basin descriptions below.

Basin MT060 (Q5 = 304.6 cfs, Q100 = 915.3 cfs): a basin that encompasses all flows from the existing roadside ditch (RMT064) entering the project site at the northeast corner, including the 24" pond outfall from Bent Grass. Flows are conveyed south to **DP1** where existing 36" twin CMP culverts pipe flows under Owl Place. Existing drainage channel (RMT064) conveys flows south to sub-regional detention pond SR4.

Basin A-1 (1.82 AC, $Q_5 = 2.0$ cfs, $Q_{100} = 5.4$ cfs): a basin that encompasses the far east side of the site, this basin consists of the proposed drainage channel, and a portion of Meridian Road. Runoff from this basin will sheet flow into the drainage channel and then be conveyed south to **DP1** where existing 36" twin culverts pipes flows under Owl Place. Existing drainage channel (RMT064) conveys flows south to sub-regional detention pond SR4. Total flows at DP1 were slightly increased in the 5-year event and reduced in the 100-year event. The change to flows at DP1 is due to the change in tributary area. *The majority of Basin A-1 is eligible for WQ treatment exclusion as defined in Permit Part I E.4.a.i.(H). Refer to Appendix F for Water Quality Drainage Map, DR-4.*

Basin B-1 (1.46 AC, $Q_5 = 6.0$ cfs, $Q_{100} = 10.8$ cfs): a basin that encompasses the north half of the storage unit buildings and drive aisles. Runoff from this basin collects into a roof drain system and outfalls onto the proposed drive aisles. Then, an inverted crowned roadway with concrete valley gutter will convey flows south to a proposed CDOT Type 13 Area Inlet-Triple (Private), **DP3**. Lastly, flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4.

Basin B-2 (1.18 AC, $Q_5 = 5.1$ cfs, $Q_{100} = 9.0$ cfs): a basin that encompasses the south half of the storage unit buildings and drive aisles. Runoff from this basin collects into a roof drain system and outfalls onto the proposed drive aisles. Then, an inverted crowned roadway with concrete valley gutter will convey flows south to a proposed CDOT Type 13 Area Inlet-Triple (Private), **DP4**. Lastly, flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4.

Basin B-3 (0.95 AC, $Q_5 = 2.1$ cfs, $Q_{100} = 4.4$ cfs): a basin that encompasses the east half of Meridian Park Drive, landscaping and buildings A and E. Runoff from this basin will sheet flow onto Type A curb

and gutter and conveyed south to a 10' CDOT Type 'R' On-Grade Curb Inlet (Public), **DP5**. Captured flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4. Any bypass flow will continue south to a riprap pad, DP12. Flows are ultimately conveyed to sub-regional detention pond SR4 via existing RMT064.

Basin B-4 (0.52 AC, $Q_5 = 1.6$ cfs, $Q_{100} = 3.1$ cfs): a basin that encompasses the east half of Meridian Park Drive. Runoff from this basin will sheet flow onto Type A curb and gutter and conveyed south to a 10' CDOT Type 'R' On-Grade Curb Inlet (Public), **DP6**. Captured flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4. Any bypass flow will continue south to a riprap pad, DP13 (No bypass flows are anticipated in the minor and major storms). Flows are ultimately conveyed to sub-regional detention pond SR4 via existing RMT064.

Basin B-5 (0.13 AC, $Q_5 = 0.5$ cfs, $Q_{100} = 0.9$ cfs): a basin that encompasses the south half of Owl Place improvements. Runoff from this basin will sheet flow onto Type A curb and gutter and conveyed east to a 5' CDOT Type 'R' On-Grade Curb Inlet (Public), **DP7**. Captured flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4. Any bypass flow will continue east to a riprap pad, DP13 (No bypass flows are anticipated in the minor and major storms). Flows are ultimately conveyed to sub-regional detention pond SR4 via existing RMT064.

Basin B-6 (0.16 AC, $Q_5 = 0.4$ cfs, $Q_{100} = 0.9$ cfs): a basin that encompasses the south half of Owl Place improvements. Runoff from this basin will sheet flow onto Type A curb and gutter and conveyed east to a 5' CDOT Type 'R' On-Grade Curb Inlet (Public), **DP8**. Captured flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4. Any bypass flow will continue east to a riprap pad, DP13. Flows are ultimately conveyed to sub-regional detention pond SR4 via existing RMT064.

Basin B-7 (0.56 AC, $Q_5 = 0.2$ cfs, $Q_{100} = 1.1$ cfs): a basin that encompasses Pond #1 (Private) Full Spectrum Extended Detention Basin. Runoff from this basin sheet flows onto a concrete trick channel and conveyed to the outlet structure, **DP9**. After treatment, flows are conveyed via storm pipe to sub-regional detention pond SR4.

Basin C-1 (0.29 AC, $Q_5 = 0.3$ cfs, $Q_{100} = 0.8$ cfs): a basin that encompasses a portion of RV Storage and landscaping. Runoff from this basin will sheet flow onto Type A curb and gutter and conveyed south to a 10' CDOT Type 'R' On-Grade Curb Inlet (Public), **DP6**. Captured flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4. Any bypass flow will continue south to a riprap pad, DP13. Flows are ultimately conveyed to sub-regional detention pond SR4 via existing RMT064.

Basin C-2 (3.12 AC, $Q_5 = 5.2$ cfs, $Q_{100} = 11.3$ cfs): a basin that encompasses most of Lot 2a and RV Storage. Runoff from this basin sheet flows south and directly enters Pond #1. Runoff is collected by a concrete trick channel and conveyed to the outlet structure, **DP9**. After treatment, flows are conveyed via storm pipe to sub-regional detention pond SR4.

Basin C-3 (0.29 AC, $Q_5 = 0.4$ cfs, $Q_{100} = 1.0$ cfs): a basin that encompasses the southwest corner of RV Storage. Runoff from this basin will sheet flow onto Type A curb and gutter and conveyed east to a 5' CDOT Type 'R' On-Grade Curb Inlet (Public), **DP8**. Captured flows are conveyed to Pond #1 via storm pipe, then routed south after treatment to sub-regional detention pond SR4. Any bypass flow will continue

east to a riprap pad, DP13. Flows are ultimately conveyed to sub-regional detention pond SR4 via existing RMT064.

Basin C-4 (0.09 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.1$ cfs): a basin that is associated with the proposed drainage swale, located at the southwest corner of proposed Lot 2a. Flows are conveyed south via a drainage swale to a proposed CDOT Type C Area Inlet-Sump (Private), **DP10**. Flows are conveyed via storm pipe and directly outfall into proposed Forebay B at sub-regional detention pond SR4. Basin C-4 is eligible for WQ treatment exclusion as defined in Permit Part I E.4.a.i.(C). Refer to Appendix F for Water Quality Drainage Map, DR-4.

Basin D-1 (0.08 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.1$ cfs): a basin that encompasses the north half of Owl Place containing tie-back grading and landscaping. Flows sheet flow south until overtopping proposed curb and gutter (by others) and continue south through Meridian Park Drive. Flows are ultimately routed to subregional detention pond SR4 via proposed storm infrastructure. Refer to the Final Drainage Report for Owl Marketplace Filing No. 1 prepared by Drexel, Barrel & Co., for more details. *A portion of Basin D-1 is eligible for WQ treatment exclusion as defined in Permit Part I E.4.a.i.(G). Refer to Appendix F for Water Quality Drainage Map, DR-4.*

Basin D-2 (0.05 AC, $Q_5 = 0.1$ cfs, $Q_{100} = 0.3$ cfs): a basin that encompasses the northeast corner of Meridian Park Drive & Owl Place intersection. Flows collect at **DP12** and continue south through Meridian Park Drive via curb and gutter (by others). Flows are ultimately routed to sub-regional detention pond SR4 via proposed storm infrastructure. Refer to the Final Drainage Report for Owl Marketplace Filing No. 1 prepared by Drexel, Barrel & Co., for more details. *A portion of Basin D-2 is eligible for WQ treatment exclusion as defined in Permit Part I E.4.a.i.(C). Refer to Appendix F for Water Quality Drainage Map, DR-4.*

Basin D-3 (0.33 AC, $Q_5 = 1.0$ cfs, $Q_{100} = 2.0$ cfs): a basin that encompasses the west side of Meridian Park Drive & Owl Place intersection. Flows collect in a proposed cross pan that conveys flows south to **DP13**. Flows are ultimately routed to sub-regional detention pond SR4 via proposed storm infrastructure. Refer to the Final Drainage Report for Owl Marketplace Filing No. 1 prepared by Drexel, Barrel & Co., for more details. *A portion of Basin D-2 is eligible for WQ treatment exclusion as defined in Permit Part I E.4.a.i.(C). Refer to Appendix F for Water Quality Drainage Map, DR-4.*

Basin OS-1 (3.89 acres, Q5 = 0.7 cfs, Q100 = 4.5 cfs): a basin that is associated with Lot 3 and 4 Falcon Ranchettes, and portions of the rear of lots 24, 25 and 26 of Bent Grass Residential Filing No. 1. Runoff sheet flows into a shallow swale and conveyed from north to south to a proposed CDOT Type C Area Inlet-Sump (Private), **DP10**. Flows are conveyed via storm pipe and directly outfall into proposed Forebay B at sub-regional detention pond SR4.

Basin OS-2 (2.35 acres, Q5 = 0.6 cfs, Q100 = 3.0 cfs): a basin that is associated with Lot 3 and 4 Falcon Ranchettes, and portions of the rear of lots 26 and 27 of Bent Grass Residential Filing No. 1. Runoff sheet from north to south to a proposed CDOT Type C Area Inlet-Sump (Private), **DP10**. Flows are conveyed via storm pipe and directly outfall into proposed Forebay B at sub-regional detention pond SR4.

Basin OS-3 (0.24 acres, Q5 = 0.0 cfs, Q100 = 0.2 cfs): a basin that is associated with Lot 3 Falcon Ranchettes, a parcel immediately west of the project site. Flows drain from north to south to a proposed

CDOT Type C Area Inlet-Sump (Private), **DP10**. Flows are conveyed via storm pipe and directly outfall into proposed Forebay B at sub-regional detention pond SR4.

Basin OS-4P (0.07 acres, Q5 = 0.3 cfs, Q100 = 0.5 cfs): a basin that is associated with the improvements to the existing cul-de-sac in Meridian Park Drive ROW. This basin represents increased tributary area and runoff and should be compared to existing basin **OS-4E** located above in "*III. Existing Drainage Patterns and Features*". Runoff sheet flows north onto Type A curb and gutter and conveyed to an existing 6' CDOT Type 'R' Sump Inlet (Public), **DP14**. The total flow to DP14 increased by 0.1 cfs in the 5-year and 100-year storm event. The increase in flow is considered nominal, and therefore, no analysis is provided for the downstream infrastructure.

Basin OS-5 (0.19 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.2$ cfs): a basin that is associated with Tract A, Bent Grass East Commercial Filing No. 2, located just north of proposed Lot 2a, Falcon Ranchettes Filing No. 1a. This basin consists of the outside berm of the existing detention pond. Runoff from this basin sheet flows south and directly enters Pond #1. Runoff is collected by a concrete trick channel and conveyed to the outlet structure, **DP9**. After treatment, flows are conveyed via storm pipe to sub-regional detention pond SR4.

Basin OS-6 (0.08 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.1$ cfs): a basin that is associated with Lot 2a, Bent Grass East Commercial Filing No. 2, located just north of proposed Lot 1a, Falcon Ranchettes Filing No. 1a. Flows are conveyed east by a drainage swale created from tie-back grading. Flows enter improved RMT064 and conveyed south to **DP1** where existing 36" twin culverts pipes flows under Owl Place. Existing drainage channel (RMT064) conveys flows south to sub-regional detention pond SR4. Total flows at DP1 we're increased in the 5-year event and remain the same in the 100-year event. The change to flows at DP1 is due to the decreased tributary area and slight increase in imperviousness from Building D.

Proposed Pond #1 Full Spectrum Extended Detention Basin

Pond #1 consists of 2 forebays, trickle channel, micropool, outlet structure (with trash rack, orifice plate, and overflow weir), and emergency spillway. Pond #1 provides treatment for the WQCV, EURV, and 100-Year.

| Zone | Max Volume Stored |
|-------------------------------------|-------------------|
| Water Quality Capture Volume (WQCV) | 0.265 (ac-ft) |
| Excess Urban Runoff Volume (EURV) | 0.739 (ac-ft) |
| 100-Year | 0.303 (ac-ft) |
| Total | 1.307 (ac-ft) |

Pond #1 is oversized in excess above the 100-year water surface elevation due to the hydraulic design of the storm sewer system. In order to keep 100-Year HGL's greater than 1 foot below finish grade, the pond footprint and depth was increased to lower the tailwater elevation (100-Year water surface elevation of Pond #1).

All drainage basins adjacent to Pond #1 are included in determining the tributary drainage area and imperviousness for Pond #1. It is anticipated that all C-Group basins will soon develop into additional

storage units or similar commercial use. Therefore, the C-Group drainage basins imperviousness are "overridden" to 100% imperviousness to accommodate for future development.

Refer to **Appendix E** for Pond #1 calculations.

Sub-Regional Detention Pond (SR4) Outfall

The outfall pipe for Pond #1 is routed south, directly into pond SR4. The calculated 100-Year storm event will result in a peak outflow of 1.6 cfs in the 5-year storm and 12.1 cfs in the 100-year storm. A concrete forebay is provided to adequately dissipate the proposed flows into pond SR4. A concrete trickle channel is proposed to directly connect to the existing trickle channel.

Sub-Regional Detention Pond (SR4) was designed to receive flows from Lot 1a and 2a (formerly Lot 1 and 2, Falcon Ranchettes). As shown in Figure 3-2 Drainage Basin Map, all lots located within the Falcon Ranchettes subdivision are routed to pond SR4. However, the assumed imperviousness was for 5 Acre Rural Residential land use, as shown in Figure 3-6 Future Land Use Buildout Condition. Therefore, detention and water quality are required to treat the difference in flows from 5 Acre Rural Residential to Commercial land uses.

As shown in the <u>existing</u> drainage map (refer to **Appendix F**) the total flow leaving the project site (Design Points 2, 3 and 4) totals 2.1 cfs in the minor storm, and 11.3 cfs in the major storm. The <u>proposed</u> peak outflow of 1.6 cfs in the minor storm and 12.1 cfs in the major storm shows a decrease of 0.5 cfs in the minor storm and an increase of 0.8 cfs in the major storm. The increase in the major storm can be attributed to the reroute of basin EX-1 to the southwest corner of the project, instead of the adjacent drainage channel. Therefore, sub-regional pond SR4 is adequate to receive the proposed flows from this project.

Drainage Channel Improvements – UTBSC East Branch (RMT064)

Falcon DBPS Analysis:

El Paso County completed hydrologic and hydraulic analyses summarized in the **Falcon DBPS**. The **Falcon DBPS** watershed encompasses three major basins, including the "Middle Tributary" which includes the subject property. The unnamed tributary to Black Squirrel Creek (UTBSC) in the Middle Tributary consists of an "East Branch" and "West Branch" that converges at the Falcon Marketplace site. The UTBSC East Branch is located along the eastern edge of the project site adjacent to Meridian Road, the West Branch does not cross the subject property.

The Falcon DBPS provides junctions north and south of the project site, named JMT050 and JMT060. These junctions are summarized below, also see **Appendix B** for Falcon DBPS excerpts showing the physical location of each junction.

| Future Peak Discharges from Falcon DBPS | | | | |
|---|-----------------------|-------------|-------------------------------|-----|
| Falcon DBPS Model Location Physical Location Branch Proximity to Project Site Q100 (cfs) | | | | |
| JMT050 | Bent Grass Meadows | East Branch | Upstream from Project Site | 850 |

| | Drive & Meridian Road | | | |
|--------|--|------------------------------|------------------------------------|-------|
| JMT060 | Eastonville Road & Meridian Road | East and West Convergence | Downstream from Project Site | 1,000 |

The **Falcon DBPS** specifies reach improvements between junctions JMT050 and JMT060, the reach between these two junctions is named "RMT064". This is visually shown in the **Falcon DBPS**, *Figure 6-1. Selected Plan*, located in **Appendix B**. These improvements include small drop structures w/ toe protection.

Bent Grass MDDP Analysis:

A drainage diversion took place as part of the Bent Grass Residential Filing No. 1 development. The UTBSC West Branch was rerouted to the East towards the intersection of Meridian Road and Bent Grass Meadows Drive. This diversion is discussed extensively in the **Bent Grass MDDP**.

Because of the diversion, a new junction was created in the Middle Tributary named JMT060a. This junction is primarily known as "Design Point 20" in the text and drainage maps in **Bent Grass MDDP**. This new junction is located just south of JMT050 from the **Falcon DBPS** and summarized in the table below.

| Future Peak Discharges from Bent Grass MDDP | | | | | |
|--|---|-------------|-------------------------------|-------|--|
| Bent Grass MDDP Model Location Physical Location Branch Proximity to Project Site Q100 (cfs) | | | | | |
| JMT060a | Bent Grass Meadows Drive & Meridian Road | East Branch | Upstream from Project Site | 909.3 | |

The **Bent Grass MDDP** specifies a 15' wide bottom channel with 4:1 side slopes, 6.5' deep and a longitudinal slope of 0.30% for RMT064 of the UTBSC East Branch. An excerpt of these calculations is provided in **Appendix B**.

Owl Place CLOMR Analysis:

The Falcon Owl Place development (located south of the project site across Owl Place) includes regrading and rerouting a portion of the UTBSC East Branch. The improvements intercept the existing creek immediately north of Owl Place and conveys it via a 10'x6' box culvert to the subregional detention pond (SR4). The box culvert is designed to convey the full 100-year discharge.

The **Falcon DBPS** did not include a junction on the East Branch immediately upstream of the convergence (Pond SR4). Therefore, the **Owl Place CLOMR** modified the HMS model to create a new junction located at the southern boundary of the Falcon Owl Place development, immediately upstream of Pond SR4. This junction is summarized in the table below.

| Peak Discharges from Owl Place CLOMR | | | | |
|--------------------------------------|----------------------|--------|------------------------------|---------------------------|
| Owl Place CLOMR Model Location | Physical Location | Branch | Proximity to Project Site | Future Flow Q100 (cfs) |

| JMT051 | Immediately Upstream of | East Branch | Downstream from Project | 920 |
|--------|----------------------------|-------------|-------------------------|-----|
| | Pond SR4 | | Site | |

Previous Reports Conclusions:

Per **Falcon DBPS**, channel improvements are required to stabilize the adjacent RMT064 of UTBSC East Branch. A design flow of 925 cfs was used as the design flow for these improvements, as specified in the **Bent Grass MDDP**. The table below compares the proposed design flow against previous reports.

| Proposed Design Flow Comparison | | | | | |
|---------------------------------|---|----------------|---------------------------------|------------------------------|--|
| Model Location | del Location Physical Location | | Proximity to Project Site | Future Flow Q100 (cfs) | |
| RMT064 | North of Owl Place, South of Bent Grass Meadows Drive | East Branch | - | 925 | |
| JMT050 (Falcon DBPS) | Bent Grass Meadows Drive & Meridian Road | East Branch | Upstream from Project Site | 850 | |
| JMT060a (Bent Grass MDDP) | Bent Grass Meadows Drive & Meridian Road | East Branch | Upstream from Project Site | 909.3 | |
| JMT051 (Owl Place CLOMR) | Immediately Upstream of Pond SR4 | East Branch | Downstream from Project Site | 920 | |

Because of added junctions (JMT060a & JMT051) from **Bent Grass MDDP** and **Owl Place CLOMR**, no revisions to existing HMS models are needed for identifying the proposed design flow for RMT064. As shown above, the design flow of 925 cfs exceeds all projected HMS models for junctions north and south of RMT064.

Due to the design slope of 0.30%, 3 drop structures are required. The USDCM provides guidance for a "Simplified Design Procedure" for drop structure design that requires no hydraulic analysis. This method was used to design the grade control structures for RMT064.

Urban Storm Drainage Criteria Manual (USDCM) Design Guidance:

The USDCM Vol. 2, Chapter 9, Section 2 includes guidance and design procedures for Grade Control Structures.

The simplified design procedure can be used for grade control structures meeting design criteria provided in the table below and where all of the following criteria are met:

- Maximum unit discharge for the design event (typically the 100-year) over any portion of the drop structure is 35 cfs/ft or less,
- Net drop height (upstream channel invert less downstream channel invert exclusive of stilling basin depth) is 5 feet or less,

- Drop structure is constructed of GSB or SC,
- Drop structure is located within a tangent section and at least twice the distance of the width of the drop at the crest both upstream and downstream from a point of curvature,
- Drop structure is located in a reach that has been evaluated per the design requirements of the Open Channel chapter.

The table below summarizes the specific design and geometric parameters used for RMT064.

Note: Channel construction drawings were prepared for the RMT064 improvements and should be referenced when reading this table.

| Design Parameter | Requirement to Use Simplified Design Procedure (As shown in USDCM) | Proposed Design | Meets or Exceeds Criteria? |
|---|--|------------------------------|----------------------------------|
| Maximum Net Drop Height (Hd) | 5 feet | 3 feet | Yes |
| Maximum Unit Discharge over any Portion of Drop Width | 35 cfs per foot of drop width | 25.9 cfs* | Yes |
| Maximum Longitudinal Slope (Steepest Face Slope) | 4(H):1(V) | 4:1 | Yes |
| Minimum Stilling Basin Depression (Db) | 1 foot | N/A** | Yes |
| Minimum Length of Approach Riprap | 8 feet | 10 feet | Yes |
| Minimum Stilling Basin Length (Lb) | Determine using Figure 9-1 | N/A** | Yes |
| Minimum Stilling Basin Width (B) | Same as crest width | N/A** | Yes |
| Minimum Cutoff Wall Depth | 6 feet | 6 feet | Yes |
| Minimum Length of Riprap Downstream of Stilling Basin | 10 feet | N/A** | Yes |
| Minimum D50 for Approach and Downstream Riprap | 12 inches | 12 inches (Type M Riprap) | Yes |
| Minimum Boulder Size for Drop Structure | Per Figure 9-1 | 24" Boulder Size | Yes |

Existing 36" Twin Culverts

The two 36" CMP culverts located at the southeast end of the project site, crossing Owl Place are severely undersized and partially filled with sediment. As stated in the **Owl Place CLOMR**, the culverts only convey 86-95 cfs, depending on tailwater depth. The remaining flow (approximately 825-834 cfs) in the 100-year event overtops Owl Place.

The Falcon Owl Place development (located south of the project site across Owl Place) includes regrading and rerouting a portion of the UTBSC East Branch. The improvements intercept the existing creek immediately north of Owl Place and conveys it via a 10'x6' box culvert to the subregional detention pond (SR4). The proposed box culvert begins just north of Owl Place and will replace the undersized culverts. Per discussions with the adjacent developer, construction is expected to run concurrently with the Meridian Storage project. If the proposed culvert replacements are not completed prior to the completion of Meridian Storage, flows will continue to overtop Owl Place.

Construction plans for the culvert replacement and associated improvements are located in Appendix B.

V. Ownership & Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated all public drainage facilities are to be owned and maintained by El Paso County. All private drainage facilities are to be owned and maintained my Meridian Storage, LLC. The table below provides a summary of each facilities' ownership & maintenance responsibilities.

| Drainage Facility | Ownership and Maintenance Entity | |
|--|--|--|
| Drainage Channel (UTBSC East Branch) – RMT064 | El Paso County & Meridian Storage, LLC | |
| Dialilage Charmer (OTBSC East Branch) - Rivi1004 | (Refer to O&M Manual for more details) | |
| Pond #1 | Meridian Storage, LLC | |
| Public Storm Drain Infrastructure (See Construction | | |
| Drawings, and "VI. Fee Development" below for | El Paso County | |
| breakdown) | | |
| Private Storm Drain Infrastructure (See Construction | | |
| Drawings, and "VI. Fee Development" below for | Meridian Storage, LLC | |
| breakdown) | | |

VI. Fee Development

Drainage & Bridge Fees

The project is located within the Falcon drainage basin. The property is already platted, however, due to requirements in the ECM Appendix L 3.13a, if a replat results in an increase in the impervious acreage,

^{*}Results from FlowMaster were used to calculate the approximate unit discharge per foot of drop width

^{**}Due to the sandy soils on site and within the channel, future degradation is expected. Therefore, the stilling basins were removed and replaced with a sloping face extending five feet below the downstream toe invert of each drop structure.

drainage basin fees shall be assessed on the additional impervious acreage. The two lots proposed for vacation and replat were previously platted as 5-acre residential lots. The Falcon DBPS was used to approximate the existing impervious acres by multiplying the total parcel area by 3%.

Note: a proposed impervious exhibit is provided in **Appendix A** and should be referenced when reading the table below.

| | Existing Impervious | Proposed | Impervious Acres Eligible |
|---------------------|----------------------------|------------------|---------------------------|
| | Acres | Impervious Acres | for Fee Calculation |
| Lot 1a | $3\% \times 5.00 = 0.150$ | 2.832 | 2.832 - 0.150 = 2.682 |
| Lot 2a | 3% x 4.61 = 0.138 | 3.598 | 3.598 - 0.138 = 3.460 |
| Tract A | $3\% \times 0.732 = 0.022$ | 0.125 | 0.125 - 0.022 = 0.103 |
| Meridian Park Drive | 3% x 0.879 = 0.026 | 0.748 | 0.748 - 0.026 = 0.722 |
| Meridian Road | 3% x 0.507 = 0.015 | 0.067 | 0.067 - 0.015 = 0.052 |
| | | Total = | 7.019 |

Drainage Fee (2024)

 $40,088 \times 7.019$ Impervious Acres = 281,377

Bridge Fee (2024)

 $5,507 \times 7.019$ Impervious Acres = 38,653

<u>Improvements and Reimbursable Costs</u>

The Falcon Drainage Basin Planning Study – Fee Development, categorizes improvements into Developer Costs, County Costs, and Metro District Costs. Items identified as Developer Costs (those incurred by the Developer) are eligible for reimbursement. County Costs and Metro District Costs are not eligible for reimbursement. The applicable reach is classified in the DBPS as follows:

| Reach/Feature | Reach Length (ft) | Improvement | Cost Category | Eligible for Reimbursement | Cost As Shown in Falcon DBPS |
|---------------|----------------------|---|------------------|-------------------------------|------------------------------------|
| RMT064 | 3,358 | Small Drop Structures w/ Toe Protection | County | No | \$1,231,110 (\$366/LF) |

The developer intends to amend the Falcon DBPS to allow for the costs of ~700 LF of RMT064 (starting at Owl Place and measuring north) to become reimbursable by the process outlined below:

- 1. Drainage Reimbursement request application with PCD.
- 2. Prepare an amendment to the DBPS outlining the request for a portion of RMT064 changed from a County Cost to Developer Cost
 - a. Amendment request hearing to the Drainage Board and Board of County Commissioners (BOCC).
- 3. Once construction of the reimbursable facilities is completed, procedures for Drainage Improvement Credits and Reimbursement outlined in Chapter 3 of the Drainage Criteria Manual will be utilized.

An Engineering Opinion of Probable Cost (OPC) for all drainage improvements is provided below:

| Non-Reimbursable Public Facilities Estimate Total (Anticipated to be eligible for reimbursement pending DBPS Amendment) | | | | | |
|---|-----|----|-----------|--------------|--|
| Item Quantity Unit Unit Cost Cost | | | | | |
| Drainage Channel Improvements | | | | | |
| Drainage Channel Construction | 700 | LF | \$ 200.00 | \$ 50,000.00 | |
| Type M Riprap | 180 | CY | \$ 135.00 | \$ 24,300.00 | |
| Grouted Boulders (24") | 514 | SY | \$ 225.00 | \$115,650.00 | |
| 6' Concrete Cutoff Wall | 106 | CY | \$ 631.00 | \$ 66,886.00 | |
| Reimbursable Public Facilities Estimate Total | | | | \$256,836.00 | |

| Non-Reimbursable Public Facilities Estimate Total | | | | | |
|---|--|------|-------------|--------------|--|
| Item | Quantity | Unit | Unit Cost | Cost | |
| Sub-Regional Detention Pond (SR4) Improvem | Sub-Regional Detention Pond (SR4) Improvements | | | | |
| Grouted Sloped Boulder Removal | 20 | SF | \$ 250.00 | \$ 5,000.00 | |
| Concrete Forebay | 1 | EA | \$10,000.00 | \$ 10,000.00 | |
| Guard Rail Fence (Forebay) | 35 | LF | \$ 6.00 | \$ 210.00 | |
| Type M Riprap (Forebay Apron) | 5 | CY | \$ 125.00 | \$ 625.00 | |
| Trickle Channel | 60 | LF | \$ 35.00 | \$ 2,100.00 | |
| | | | | | |
| Subtotal | | | | \$ 17,935.00 | |
| Storm Drain Improvements | | | | | |
| 15" Reinforced Concrete Pipe | 43 | LF | \$ 70.00 | \$ 3,010.00 | |
| 36" Reinforced Concrete Pipe | 42 | LF | \$ 151.00 | \$ 6,342.00 | |
| 5' CDOT Type R Curb Inlet | 2 | EA | \$ 9,377.00 | \$ 18,754.00 | |
| 10' CDOT Type R Curb Inlet | 2 | EA | \$10,230.00 | \$ 20,460.00 | |
| 5' Storm Drain Manhole, Slab Base | 1 | EA | \$ 8,322.00 | \$ 8,322.00 | |
| | | | | | |
| Subtotal | | | | \$ 56,888.00 | |
| Non-Reimbursable Public Facilities Estimate Total | | | | \$ 74,823.00 | |

| Private Facilities Estimate Total | | | | | |
|---|------|----|-------------|--------------|--|
| Item Quantity Unit Unit Cost Cost | | | | | |
| Pond #1 | | | | | |
| Earthwork | 5000 | CY | \$ 10.00 | \$ 50,000.00 | |
| Forebay | 2 | EA | \$ 5,000.00 | \$ 10,000.00 | |
| Guard Rail Fence (Forebays & Micropool) | 165 | LF | \$ 6.00 | \$ 990.00 | |

| Type M Riprap (Forebay Aprons) | 10 | CY | \$ 125.00 | \$ 1,250.00 |
|---|------|----|-------------|--------------|
| Type L Riprap (Emergency Spillway) | 60 | CY | \$ 100.00 | \$ 6,000.00 |
| Trickle Channel | 130 | LF | \$ 15.00 | \$ 1,950.00 |
| Outlet Structure w/ Concrete Micropool | 1 | EA | \$15,000.00 | \$ 15,000.00 |
| Pond Access Road (CDOT Class 6 Gravel) | 95 | CY | \$ 45.00 | \$ 4,275.00 |
| | | | | |
| Subtotal | | | | \$ 89,465.00 |
| Storm Drain Improvements | | | | |
| 15" Reinforced Concrete Pipe | 40 | LF | \$ 70.00 | \$ 2,800.00 |
| 18" Reinforced Concrete Pipe | 1150 | LF | \$ 82.00 | \$ 94,300.00 |
| 24" Reinforced Concrete Pipe | 126 | LF | \$ 98.00 | \$ 12,348.00 |
| 36" Reinforced Concrete Pipe | 46 | LF | \$ 151.00 | \$ 6,946.00 |
| 4' Storm Drain Manhole, Box Base | 1 | EA | \$ 8,322.00 | \$ 8,322.00 |
| CDOT Type C Area Inlet | 1 | EA | \$ 6,037.00 | \$ 6,037.00 |
| CDOT Typ 13 Area Inlet (Triple) | 2 | EA | \$15,130.00 | \$ 30,260.00 |
| | | | | |
| Subtotal | | | | \$161,013.00 |
| Non-Reimbursable Public Facilities Estimate Total | | | | \$250,478.00 |

VII. Conclusion

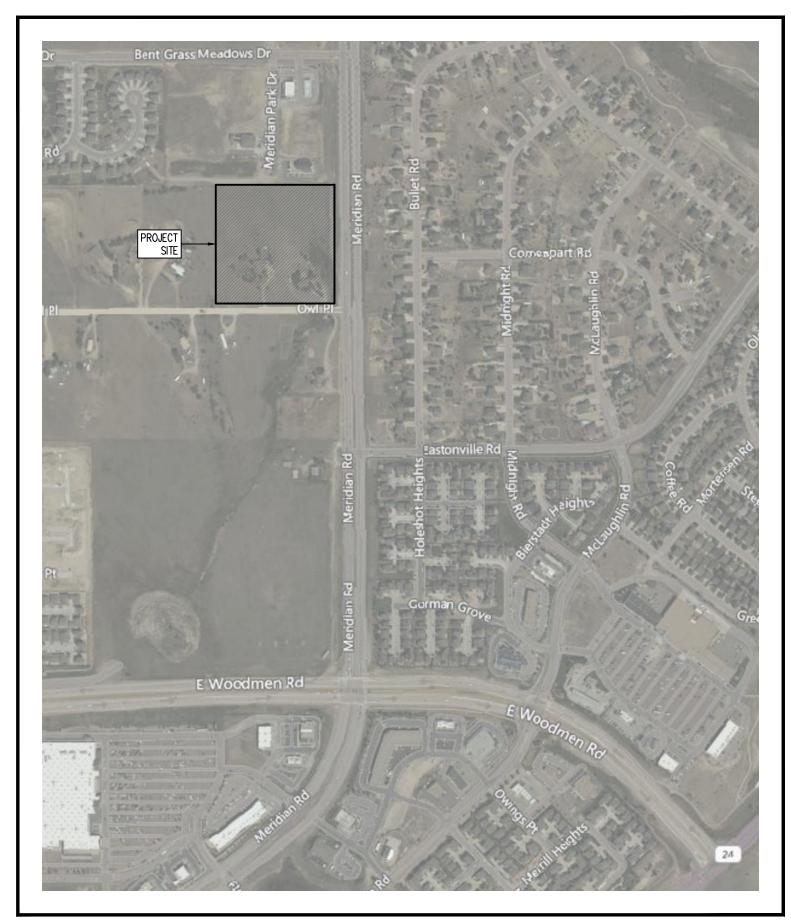
This Final Drainage Report for Falcon Ranchettes Filing No. 1a was prepared using the criteria and methods as described in the Mile High Flood District (MHFD) Urban Storm Drainage Criteria Manual (USDCM) and the adopted chapters 6 & 13 from the City of Colorado Springs Drainage Criteria Manual (DCM) Vol. 1. The downstream facilities are adequate to protect the runoff proposed from the site. The site runoff will not adversely affect the downstream and surrounding developments. This report is in general conformance with all previously prepared reports that included this site.

VIII. References

- 1. Drainage Criteria Manual Volume 1, City of Colorado Springs, May 2014, revised January 2021.
- 2. Drainage Criteria Manual Volume 2, City of Colorado Springs, May 2014, revised December 2020.
- 3. El Paso County Board Resolution No. 15-042: El Paso County adoption of Chapter and Section 3.2.1, Chapter 14 of the City of Colorado Springs Drainage Criteria Manual Volume 1, May 2014
- 4. Urban Storm Drainage Criteria Manuals, Mile High Flood District, latest revisions.
- 5. Flood Insurance Rate Map, El Paso County Area, Colorado and Incorporated Areas, Map Number 08041C0553G, Effective Date December 7, 2018
- 6. Soil Map, El Paso County Area, Colorado as available through the Natural Resources Conservation Service National Cooperative Soil Survey website via Web Soil Survey 2.0

- 7. Geotechnical Exploration Report for 11690 and 11750 Owl Place, Prepared by Universal Engineering Sciences, April 18, 2023
- 8. Falcon Drainage Basin Planning Study, Prepared by Matrix Design Group, September 2015
- 9. Bent Grass MDDP Amendment & DBPS Amendment, Prepared by Galloway & Company, Inc., September 2021
- 10. Request for Conditional Letter of Map Revision, Unnamed Tributary to Black Squirrel Creek, Falcon Owl Place, Prepared by Drexel, Barrel & Co., October 25, 2022
- 11. Request for Letter of Map Revision, Unnamed Tributary to Black Squirrel Creek, Falcon Marketplace, Prepared by Drexel, Barrel & Co., March 15, 2021
- 12. Final Drainage Report for Falcon Marketplace, Prepared by Drexel, Barrel & Co., November 4, 2019

APPENDIX A

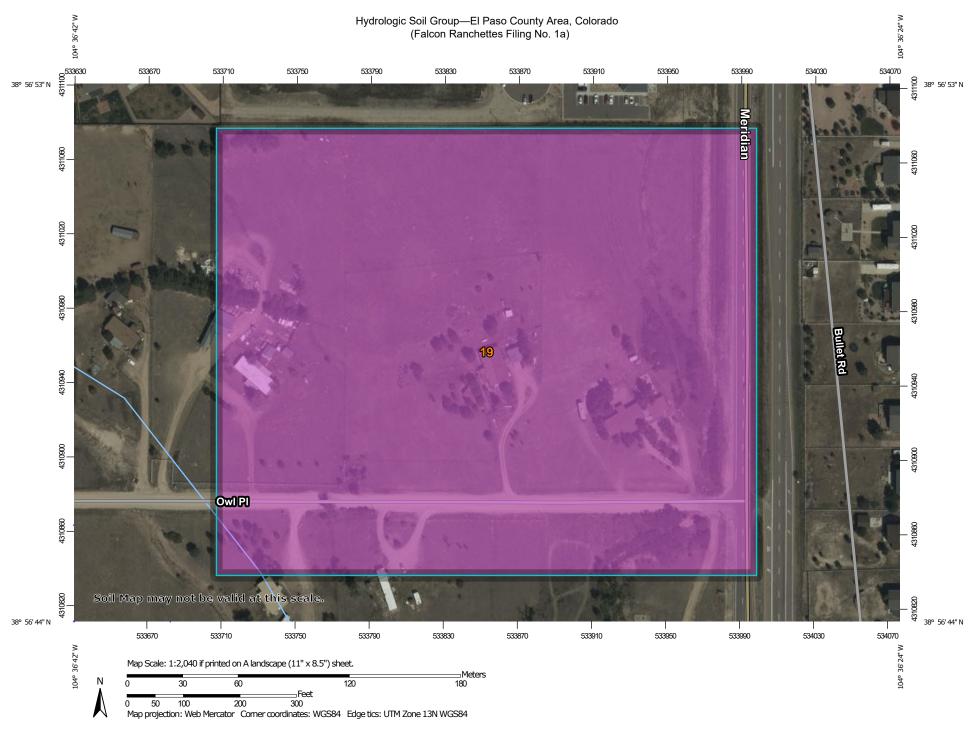


MERIDIAN STORAGE FALCON RANCHETTES FILING NO. 1A

| Project No: | MRS01 |
|-------------|------------|
| Drawn By: | CMWJ |
| Checked By: | RGD |
| Date: | 09/08/2023 |



1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920 719.900.7220 • GallowayUS.com



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Sep 11, 2018—Oct 20. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|-----------------------------|--|--------|--------------|----------------|
| 19 | Columbine gravelly sandy loam, 0 to 3 percent slopes | A | 17.4 | 100.0% |
| Totals for Area of Interest | | 17.4 | 100.0% | |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

nis map is for use in administering the National Flood Insurance Program. It doe to necessarily identify all areas subject to flooding, particularly from local drainag purces of small size. The community map repository should be consulted for sssible updated or additional flood hazard information.

obtain more detailed information in areas where Base Flood Elevations (BFE o obtain more detailed information in areas where Base Flood Elevations (BFEs ind/or floodways) have been determined, users are encouraged to consult the Floo rofiles and Floodway Data and/or Summary of Stillwater Elevations tables containe inthin the Flood Insurance Study (FlS) report that accompanies this FIRM. User bould be aware that BFEs shown on the FIRM represent rounded whole-focevations. These BFEs are intended for flood insurance rating purposes only an hould not be used as the sole source of flood elevation information. Accordingly ood elevation and presented in the FIS report should be utilized in conjunction wite FIRM for purposes of construction and/or floodplain management.

revauors table in the Flood insurance Study report for this jurisdiction. Elevationown in the Summary of Stillwater Elevations table should be used for construction floodplain management purposes when they are higher than the elevationown on this FIRM.

oundaries of the **floodways** were computed at cross sections and interpolate tetween cross sections. The floodways were based on hydraulic considerations wit agard to requirements of the National Flood Insurance Program. Floodway with nd other pertinent floodway data are provided in the Flood Insurance Study repo

The projection used in the preparation of this map was Universal Transvers Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spherio Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight position differences in map features across jurisdiction boundaries. These differences do na affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure an argound elevations referenced to the same verifical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey websited antiplication of the National Geodetic Survey websited antiplication of the National Geodetic Survey websited antiplication of the National Geodetic Survey was the following contents.

lver Spring, MD 20910-3282

Base Map information shown on this FIRM was provided in digital format by EI Pa ase Map information shown on this FIRM was provided in digital format by EI Pas ounty, Colorado Springs Utilities, City of Fountain, Bureau of Land Managemen ational Oceanic and Atmospheric Administration, United States Geological Surve nd Anderson Consulting Engineers, Inc. These data are current as of 2006.

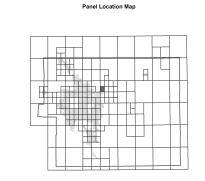
map reflects more detailed and up-to-date **stream channel configurations an** plain **delineations** than those shown on the previous FIRM for this jurisdiction loodplains and floodways that were transferred from the previous FIRM ma The floodplains and floodways that were transferred from the previous FIRM make been adjusted to conform to these new stream channel configurations. As result, the Flood Profiles and Floodway Data tables in the Flood Insurance Stud Report (which contains authoritative hydraulic data) may reflect stream channe distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profile and Floodway Data Tables if applicable, in the FIS report. As a result, the profil baselines may deviate significantly from the new base map channel representation. d may appear outside of the floodplain

Please refer to the separately printed **Map Index** for an overview map of the count showing the layout of map panels; community map repository addresses; and sisting of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

ontact FEMA Map Service Center (MSC) via the FEMA Map Information eXchar

f you have **questions about this map** or questions concerning the National Flo nsurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) risit the FEMA website at http://www.fema.gov/business/nfip.

Flooding Source REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSUFOR STREAM BY STREAM VERTICAL DATUM CONVERSION II



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management



available from local communities and the Colora Water Conservation Board.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or oxceeded in any given year. The Special Flood Hazard Area is the area subject in flooding by the 1% annual chance flood. Areas of Special Flood Hazard India Chazard In

No Base Flood Elevations determined.
Base Flood Elevations determined.
Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. ZONE VE

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

____ Floodway boundary

Zone D Boundary CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

Base Flood Elevation line and value; elevation in feet (EL 987) Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

A Cross section line

M1.5

(23)-----(23)

97° 07' 30.00" 32° 22' 30.00" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

DX5510

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Co Map History Table located in the Flood Insurance Study report for this jurisdiction

MAP SCALE 1" = 500' 250 0 500 1000 HHH FEET

METERS

FIRM

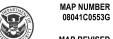
FLOOD INSURANCE RATE MAP EL PASO COUNTY,

PANEL 0553G

COLORADO AND INCORPORATED AREAS

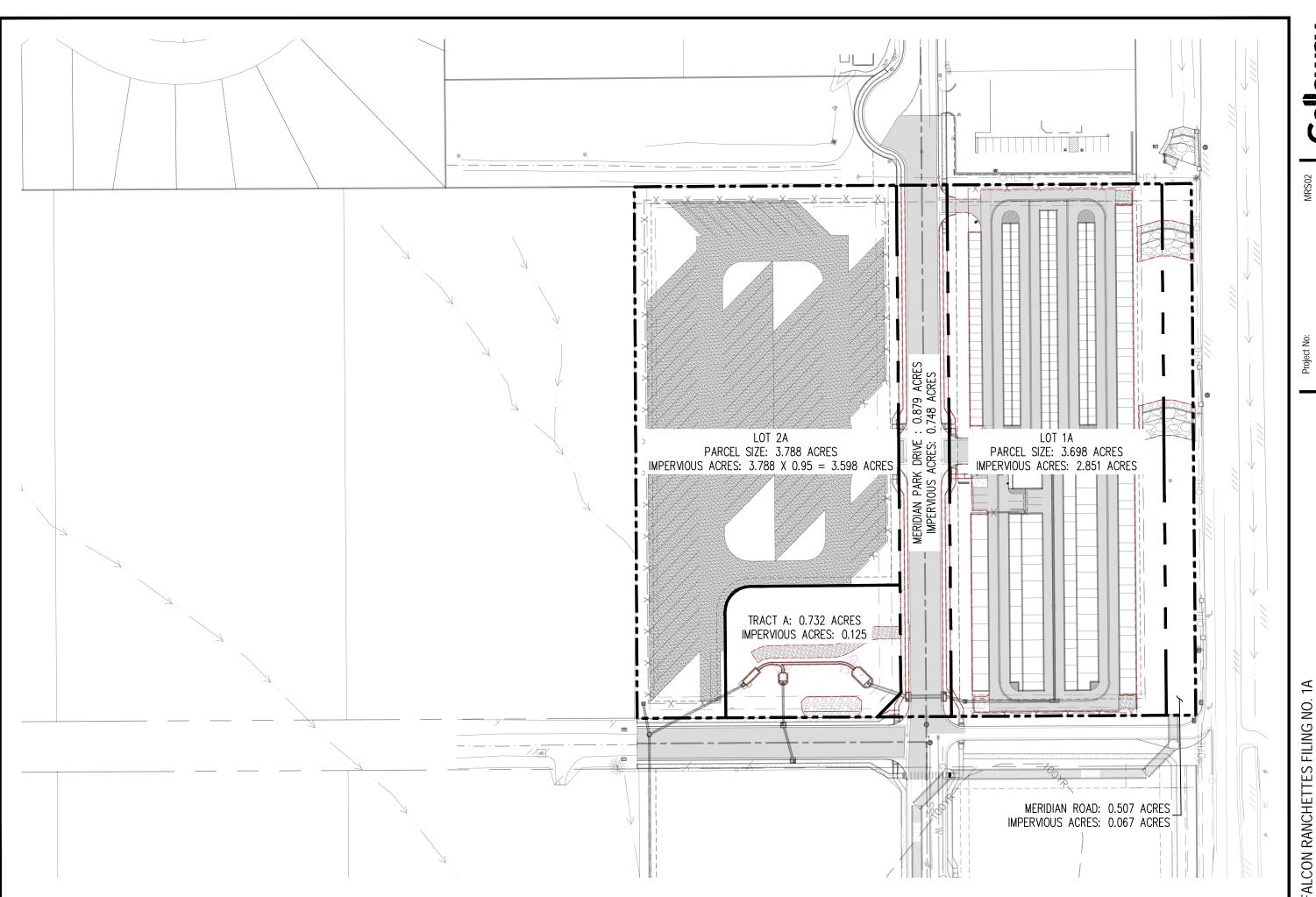
PANEL 553 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: COMMUNITY



MAP REVISED

DECEMBER 7, 2018 Federal Emergency Management Agency



Galloway

1155 Kely Johnson Blvd., Sulte 305

Colorado Springs, CO 80920

CMWJ BAS 04/26/2024

Drawn By:
Checked By:
Date:

FALCON RANCHETTES FILING NO. 1A MERIDIAN STORAGE

% IMPERVIOUS EXHIBIT

APPENDIX B

FALCON DRAINAGE BASIN PLANNING STUDY SELECTED PLAN REPORT FINAL - SEPTEMBER 2015

Prepared for:



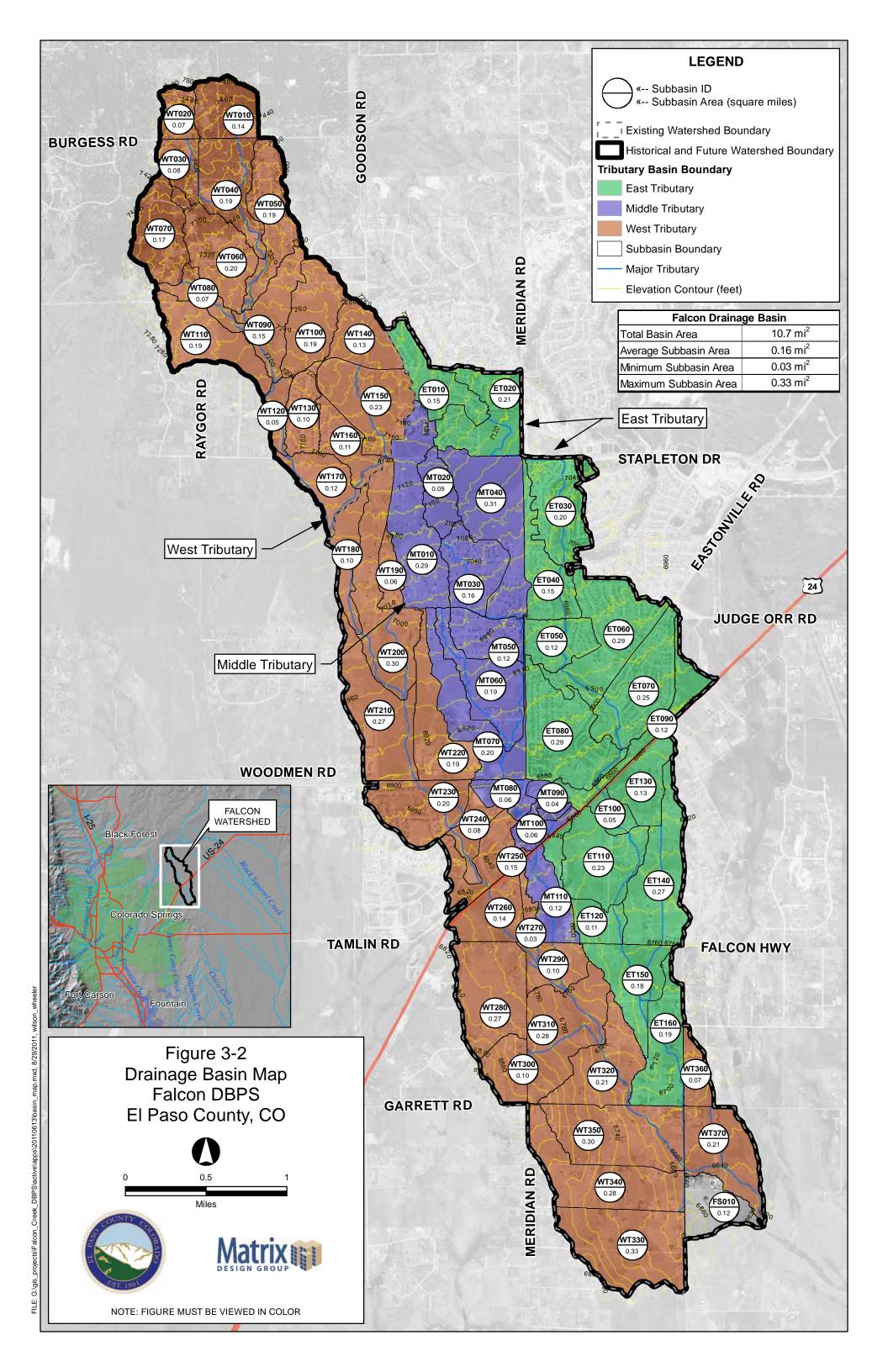
El Paso County Public Services Department 3275 Akers Drive Colorado Springs, CO 80922

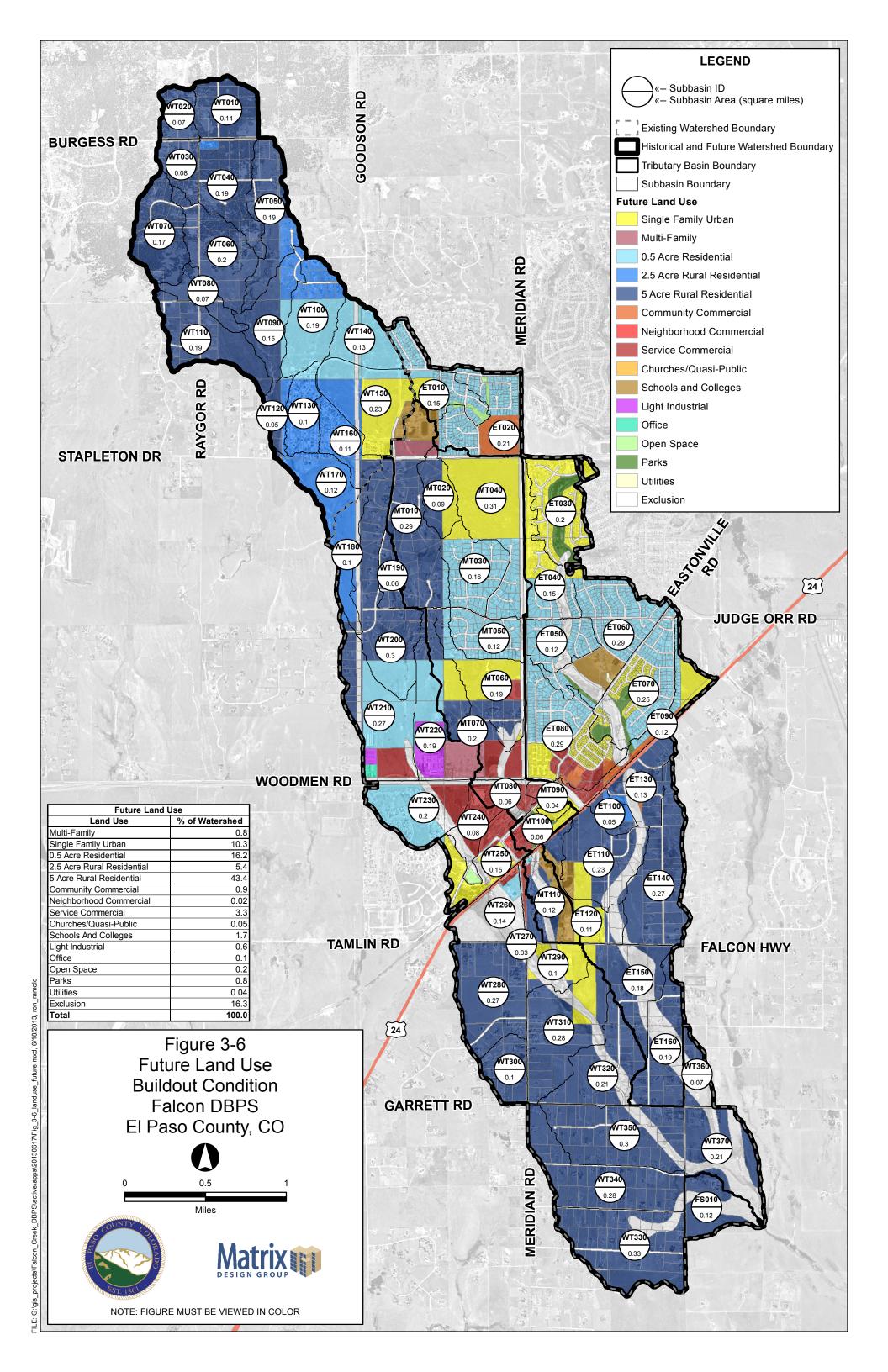
Prepared By:

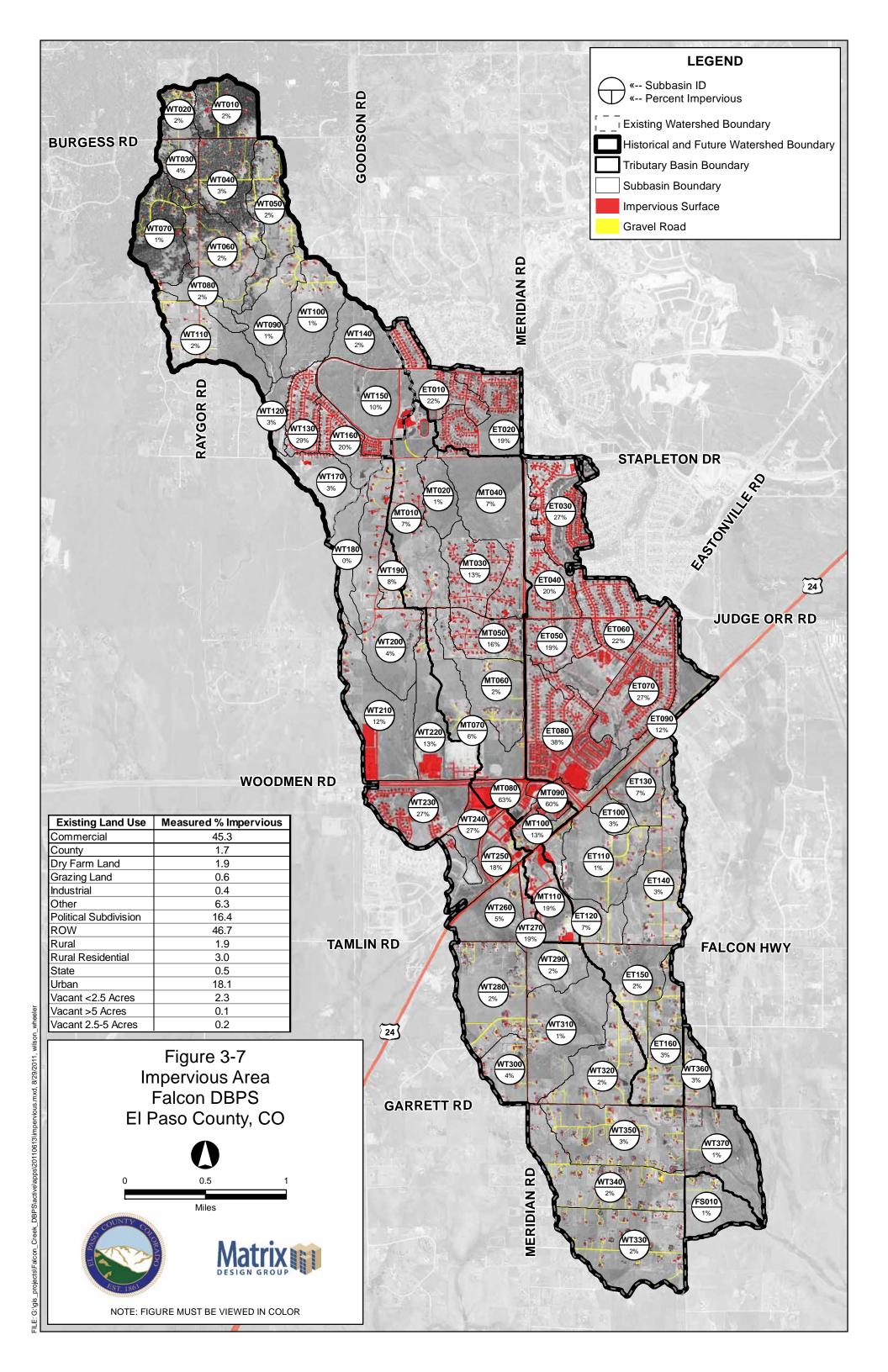


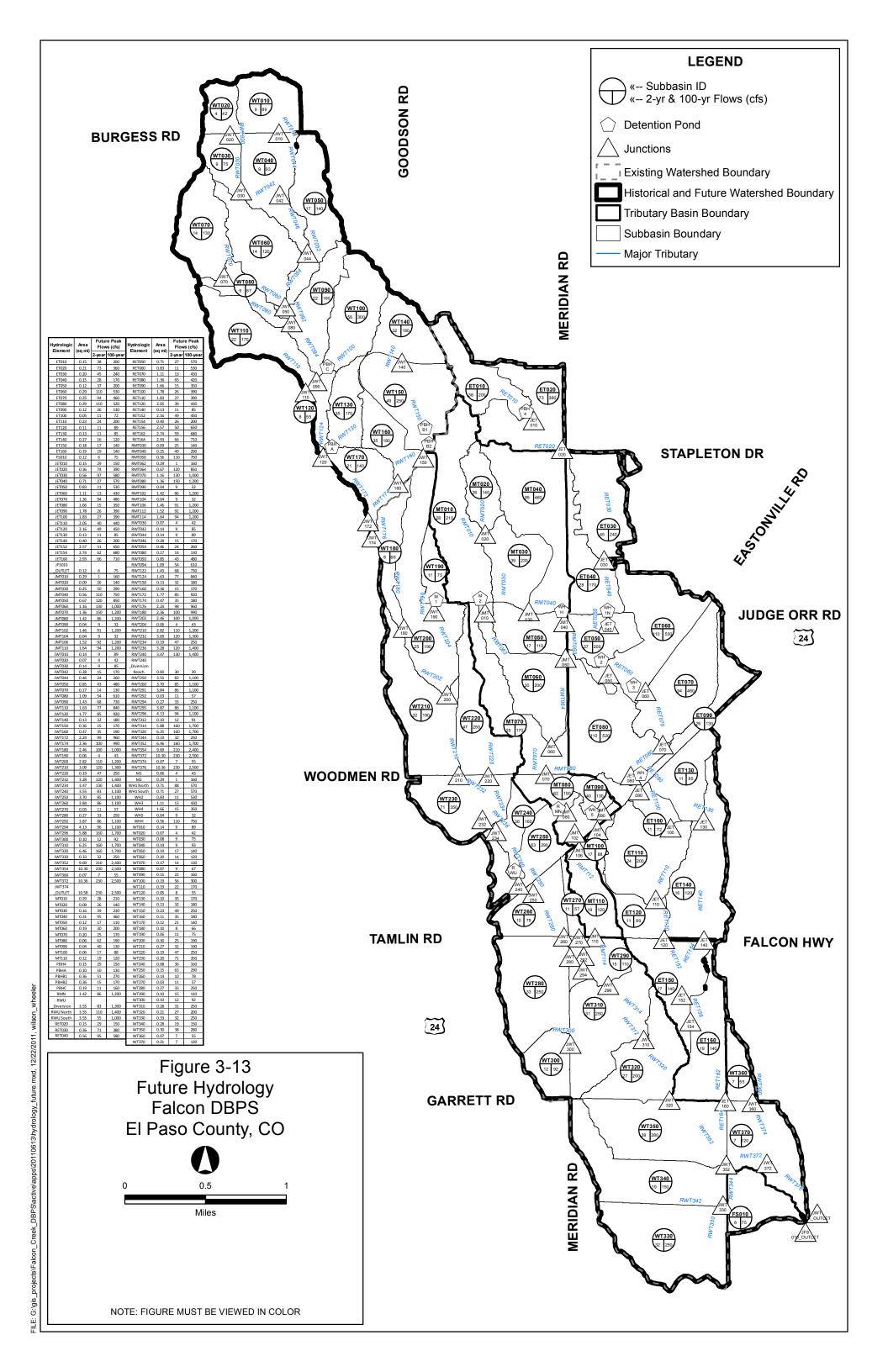
Matrix Design Group 2435 Research Parkway, Suite 300 Colorado Springs, CO 80920

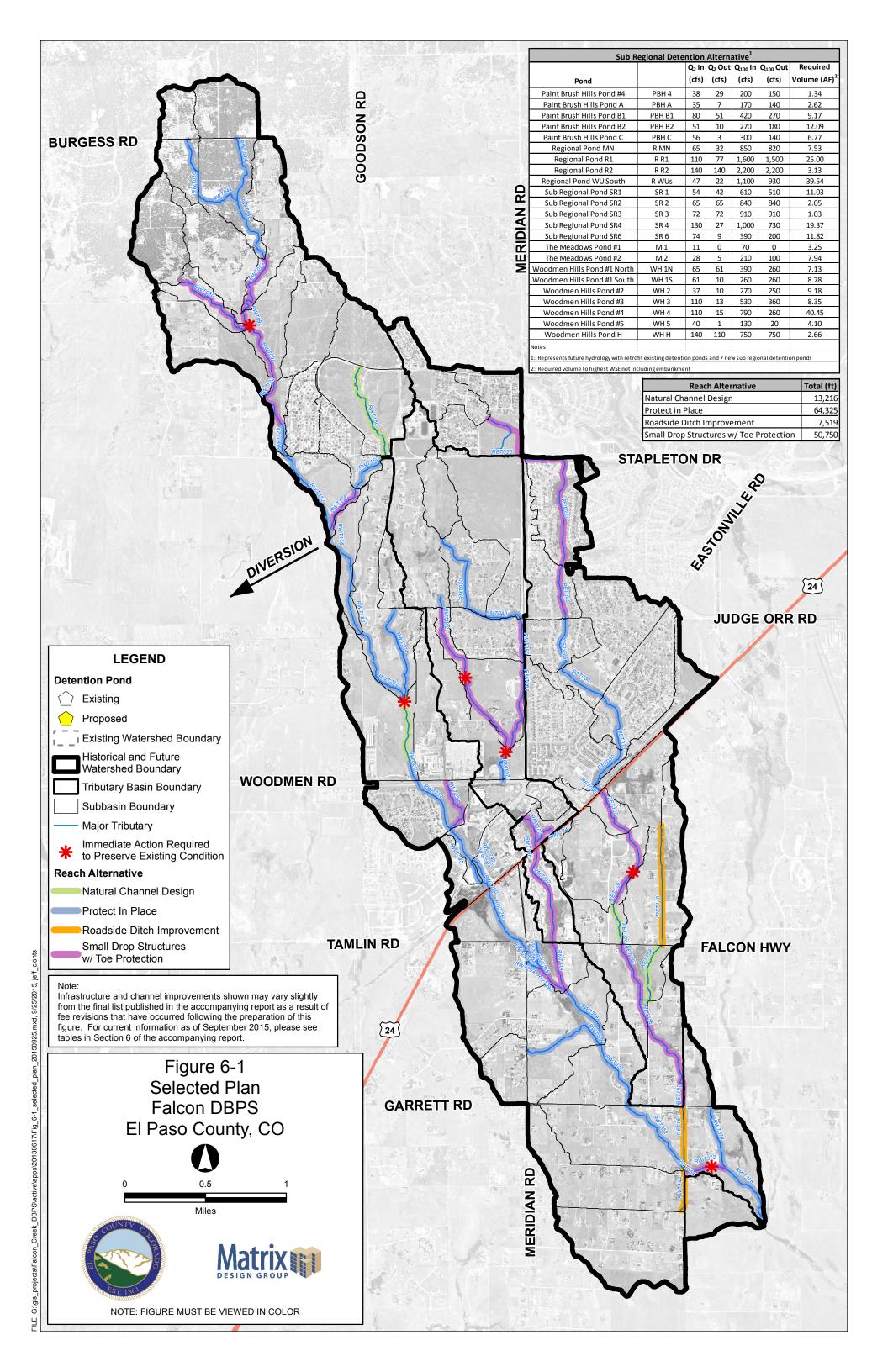
Matrix Project No. 10.122.003

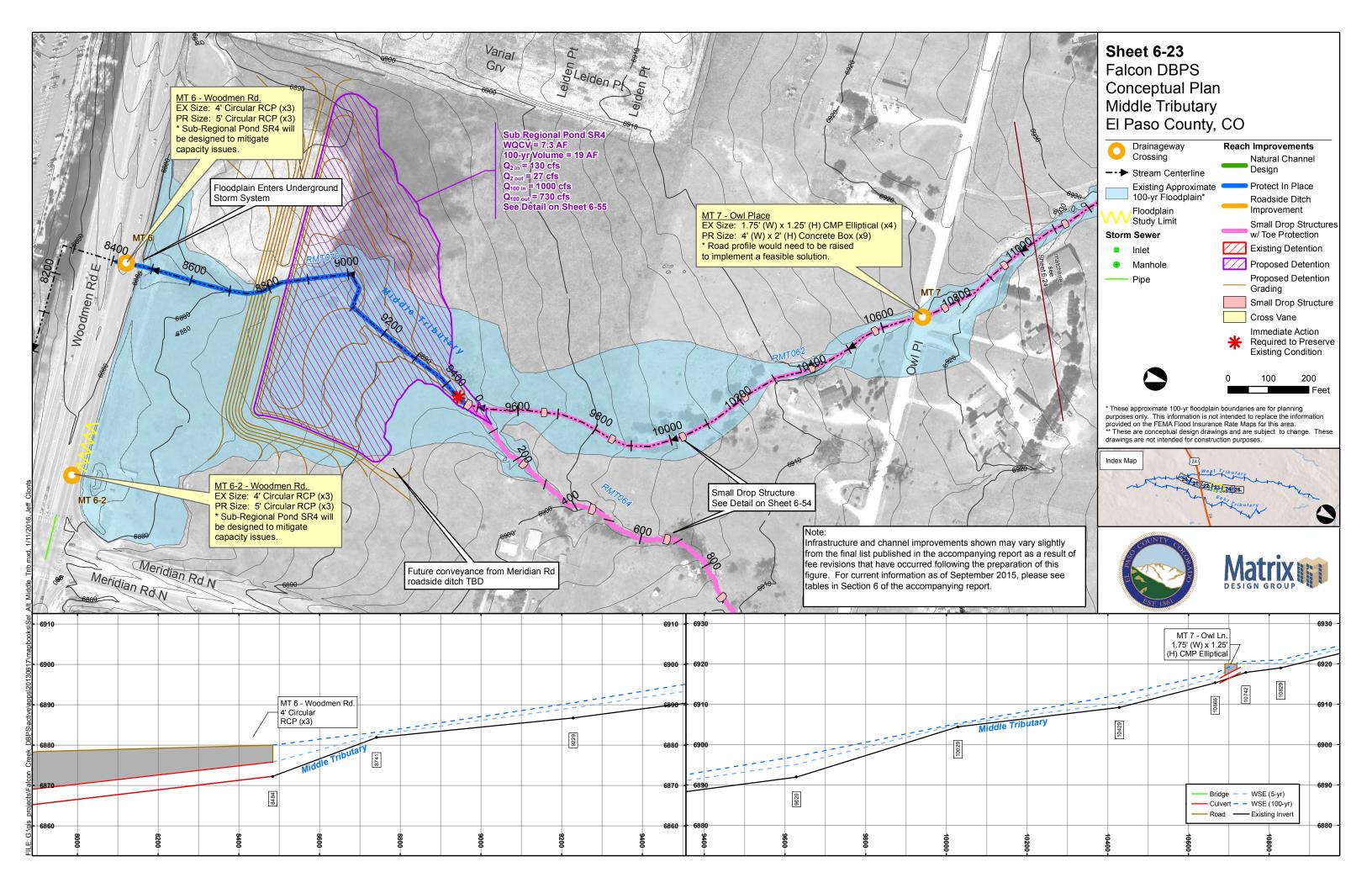


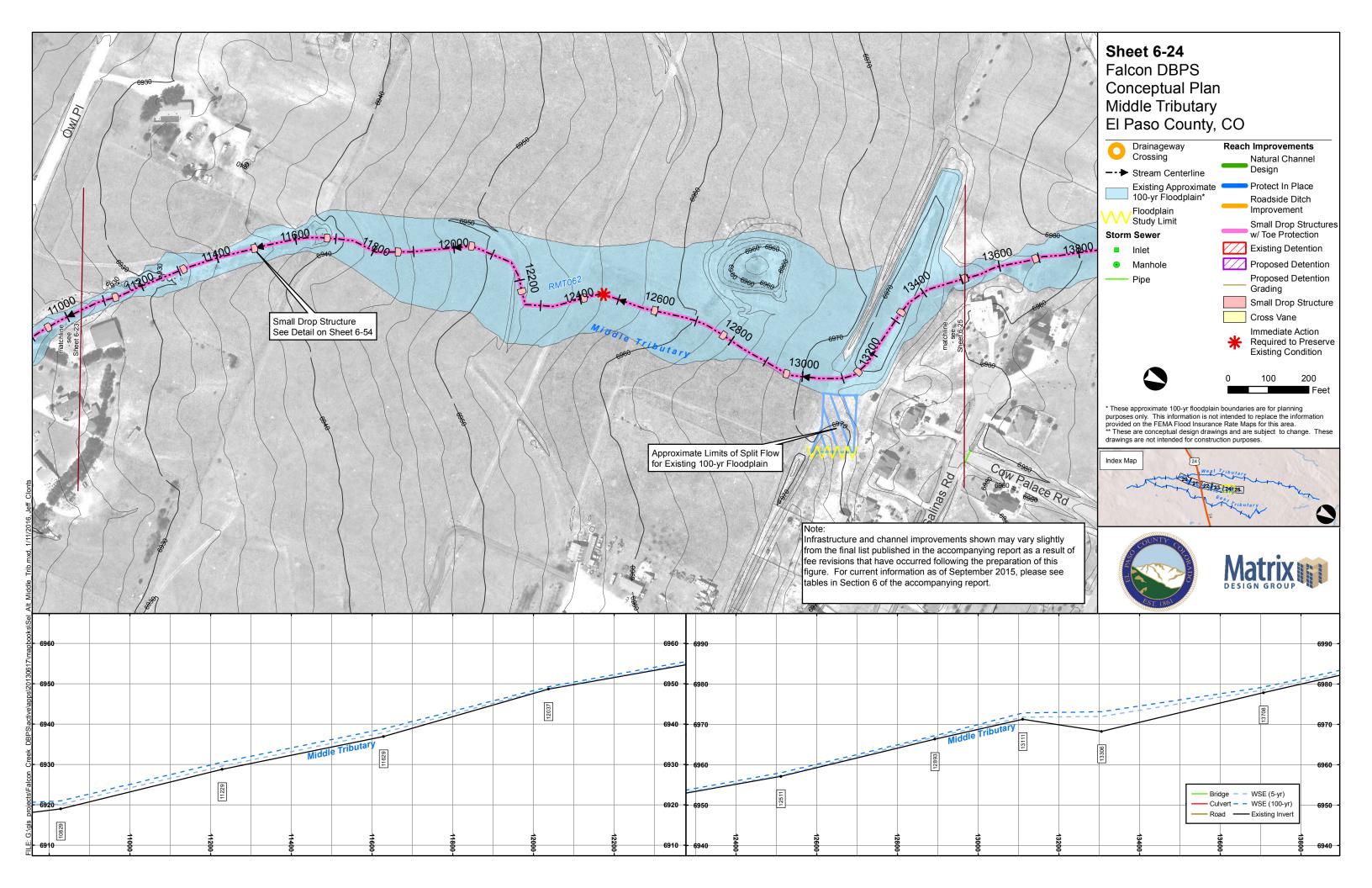












7.0 FEE DEVELOPMENT

7.1. Introduction

The objective of the fee development exercise was to determine the equitable share of drainage improvement costs that a developer is responsible for paying to El Paso County if they wish to plat a property. This fee is a function of the total cost for the selected plan outlined in Section 6 and will be used by the County to pay for drainage improvements that are necessary as a result of development. The product of this calculation is a unit fee (cost/impervious acre) that is a one-time charge to the developer based on the number of impervious acres within the platted property.

7.2. Developable Land

The Falcon Watershed has a total area of 6,847 acres. The entirety of the watershed is within the County with 1,969 acres unplatted, according to the GIS dataset received from the County. This dataset also includes unplatted areas that can't be developed because of specific land use designations. Table 7-1 provides a summary of land classifications in the Falcon Watershed. A complete summary of unplatted area land use is provided in Appendix E.

| Tuble / 1: Lana Classification | | |
|--------------------------------|--------------|--|
| Classification | Area (acres) | |
| Platted | 3,670 | |
| Unplatted | 1,969 | |
| Other | 1,208 | |
| Total | 6,847 | |

Table 7-1. Land Classification

The projected impervious acreage within unplatted areas totals 645.58 acres. A summary of land classification within the Falcon Watershed is provided in Figure 7-3.

7.3. Fee Calculation & County Cost

The total cost for the Selected Plan was separated into a Development Fee, County Cost, Metropolitan District Cost, and Drainage and Bridge Funds. A description of how the aforementioned were defined is as follows:

- **County Cost** Drainage improvement costs that are the responsibility of the County as shown in Figure 7-1.
- **Metropolitan District Cost** Drainage improvement costs that are the responsibility of a metropolitan district as shown in Figure 7-2.
- **Development Fee** All drainage improvement costs that are directly associated with new development.
- **Drainage and Bridge Funds** The balance of drainage and bridge funds as of August 2015 was \$584,134 and \$510,777, respectively, with a liability of \$300,000 cost for this DBPS (an additional contract amendment increased the cost of this DBPS to \$339,088).

The anticipated reimbursements due for work completed in the Falcon Watershed are approximately equivalent to the available drainage and bridge funds. As a result, reimbursements were not included in

the fee calculation. Drainage improvements that are required as a result of new development are listed in Appendix E.

The costs apportioned to County and metropolitan district drainage improvements are provided in Table 7-2 and Table 7-3. The bridge improvement fees shown in Table 7-2 and Table 7-3 were determined by classification of the crossing as either a bridge or a culvert. This classification was based on the DCM criteria.

Table 7-2. County Cost

| Drainage Improvements | \$ 24,051,349 |
|-----------------------|---------------|
| Bridge Improvements | \$ 2,887,437 |
| Total Cost | \$ 26,938,786 |

Table 7-3. Metropolitan District Cost

| Drainage Improvements | \$ 3,972,407 |
|-----------------------|--------------|
| Bridge Improvements | \$ 1,855,620 |
| Total Cost | \$ 5,828,027 |

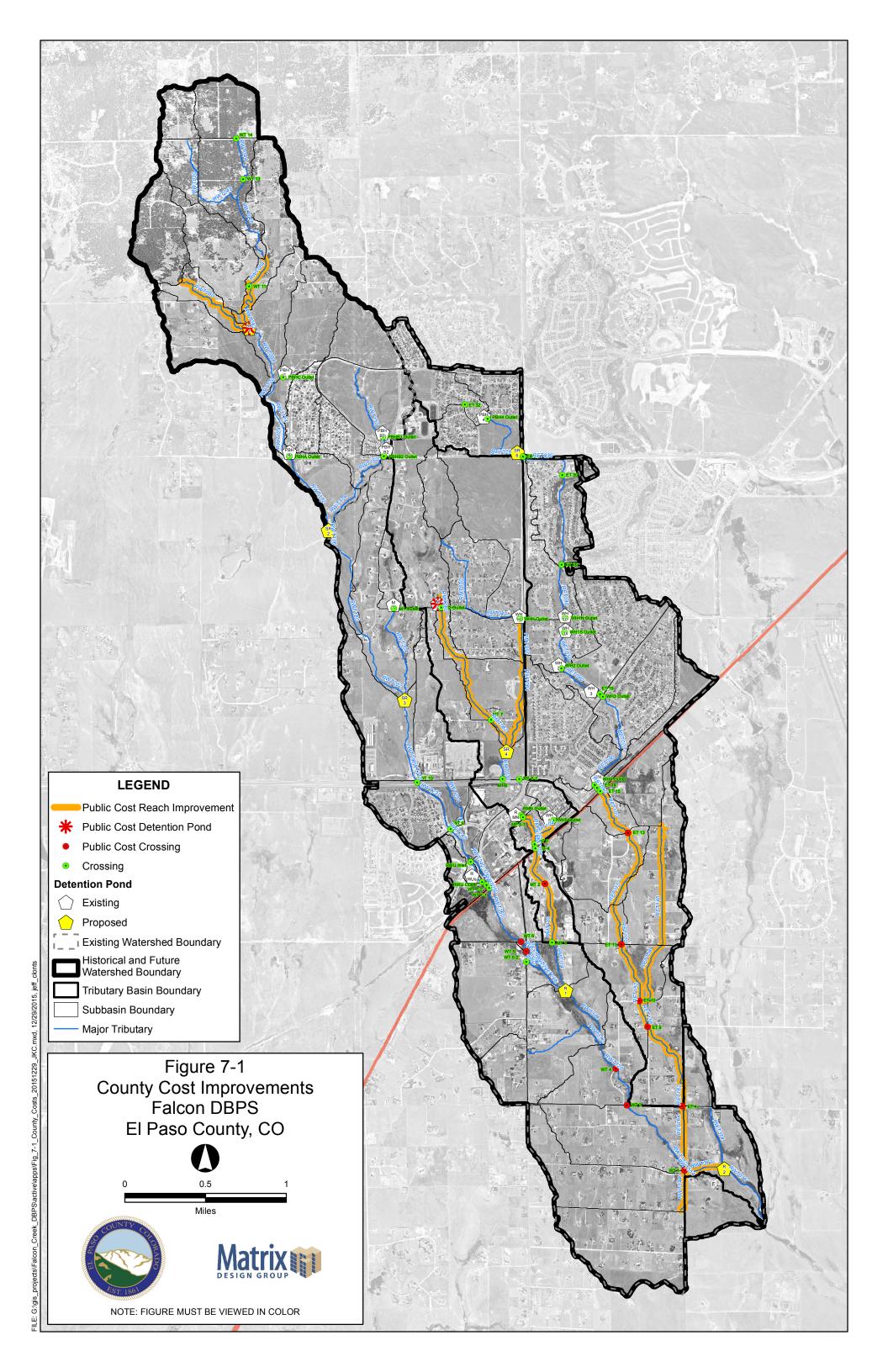
The development cost and corresponding fee calculations based on impervious acreage are provided in Table 7-4 and 7-5.

Table 7-4. Development Drainage Cost and Fee

| Drainage Improvements | \$ 14,649,163 |
|-----------------------------|---------------|
| DBPS Cost | \$ 339,088 |
| Total Cost | \$ 14,988,251 |
| Drainage Fee (per imp. ac.) | \$ 23,217 |

Table 7-5. Development Bridge Cost and Fee

| Bridge Improvements | \$ 2,058,474 |
|---------------------------|--------------|
| Total Cost | \$ 2,058,474 |
| Bridge Fee (per imp. ac.) | \$ 3,189 |



Falcon DBPS
County Costs

| | | CO | unty | Costs |
|-----------------------|----------------------|--|------|-----------|
| | | Drainage Fees | | |
| Reach/Pond | Reach Length (ft) | Improvement | | Cost |
| RWT344 | 1,379 | Roadside Ditch Improvement | \$ | 167,006 |
| RET140 | 4,052 | Roadside Ditch Improvement | \$ | 295,914 |
| RET164 | 2,072 | Roadside Ditch Improvement | \$ | 132,703 |
| RET100 | 1,791 | Small Drop Structures w/Toe Protection | \$ | 1,342,120 |
| RET110 | 2,751 | Small Drop Structures w/Toe Protection | \$ | 1,055,51 |
| RET152 | 2,030 | Small Drop Structures w/Toe Protection | \$ | 1,081,390 |
| RET120 | 1,379 | Natural Channel Design | \$ | 72,798 |
| RET162 | 3,256 | Small Drop Structures w/Toe Protection | \$ | 656,460 |
| RMT050 | 1,568 | Small Drop Structures w/Toe Protection | \$ | 814,189 |
| RMT062 | 5,688 | Small Drop Structures w/Toe Protection | \$ | 2,381,12 |
| RMT064 | 3,358 | Small Drop Structures w/Toe Protection | \$ | 1,231,11 |
| RMT112 | 3,372 | Small Drop Structures w/Toe Protection | \$ | 1,276,14 |
| RWT054 | 2,497 | Small Drop Structures w/Toe Protection | \$ | 1,414,53 |
| RWT080 | 3,494 | Small Drop Structures w/Toe Protection | \$ | 2,345,15 |
| RWT092 | 626 | Small Drop Structures w/Toe Protection | \$ | 414,43 |
| RWT372 | 1,377 | Small Drop Structures w/Toe Protection | \$ | 947,22 |
| RMT102 | 1,021 | Small Drop Structures w/Toe Protection | \$ | 636,08 |
| RMT104 | 874 | Small Drop Structures w/Toe Protection | \$ | 186,34 |
| RET154 | 2,357 | Natural Channel Design | \$ | 468,92 |
| RET156 | 942 | Natural Channel Design | \$ | 73,72 |
| WT 5 | 43 | Crossing - Culvert | \$ | 8,65 |
| ET 13 | 50 | Crossing - Culvert | \$ | 113,99 |
| ET 11 | 40 | Crossing - Culvert | \$ | 84,34 |
| ET 9 | 40 | Crossing - Culvert | \$ | 84,10 |
| ET 4 | 61 | Crossing - Culvert | \$ | 106,06 |
| Sub Regional Pond SR1 | | Detention Pond | \$ | 405,76 |
| he Meadows Pond #2 | | Detention Pond | \$ | 20,00 |
| | | Subtotal | \$ | 17,815,81 |
| | | Engineering/Construction Admin (15%) | | 2,672,37 |
| | | Contingency (20%) | | 3,563,16 |
| | | Total | \$ | 24,051,34 |

County Costs Appendix E 1/1

| Bridge Fees | | | | |
|--------------------------------------|-------------------|-------------------|----------|-----------|
| Reach/Pond | Reach Length (ft) | Improvement | | Cost |
| | <u> </u> | - - | ! | |
| WT 6 | 43 | Crossing - Bridge | \$ | 249,775 |
| WT 4 | 48 | Crossing - Bridge | \$ | 528,324 |
| WT 3 | 46 | Crossing - Bridge | \$ | 218,292 |
| WT 1 | 40 | Crossing - Bridge | \$ | 636,648 |
| MT 2 | 83 | Crossing - Bridge | \$ | 343,147 |
| ET 10 | 44 | Crossing - Bridge | \$ | 162,656 |
| Subtotal | | | \$ | 2,138,842 |
| Engineering/Construction Admin (15%) | | | \$ | 320,826 |
| Contingency (20%) | | | \$ | 427,768 |
| | | Total | \$ | 2,887,437 |



MDDP & DBPS AMENDMENT

BENT GRASS DEVELOPMENT

El Paso County, Colorado

PREPARED FOR:

Challenger Communities, LLC 8605 Explorer Dr., Suite 250 Colorado Springs, CO 80920

PREPARED BY:

Galloway & Company, Inc. 1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920

DATE:

January 2021

Revised: March 2021 Revised: April 2021 Revised: June 2021 Revised: August 2021 Revised: September 2021

PUDSP-20-005



recommendations from the Falcon DBPS, when additional land is obtained to expand the ROW along the southbound portion of Meridian Road.

In the interim condition, it has been proposed to add a temporary lining to the existing channel to handle the excess velocities and depth associated with the DBPS flows and Bent Grass development re-routed flows. This analysis has been included in the Appendix.

The West Tributary Channel will be natural, vegetated facility, helping to ensure that the overall velocities will be reduced, flow depth will not exceed 5' and minimize any potential for scour. If needed, grade control structures may be designed as proposed in the DBPS to ensure these criteria are met.

3. Implement BMPs That Provide a Water Quality Capture Volume with Slow Release This step utilizes formalized water quality capture volume to slow the release of runoff from the site. The WQCV will release in no less than 40 hours. On-site water quality control volume detention ponds will provide water quality treatment prior to the runoff being released into the channel. WQCV facilities will be designed as Extended Detention Basins.

The Falcon Meadows at Bent Grass development, west of Bent Grass Residential, Filing No. 1 and No. 2, will include several water quality ponds throughout the site to ensure flows will be treated prior to being released into the West Tributary Channel, running through the site. Only a small area, less than 1.0 acres will not be treated prior to releasing into the channel.

Currently, the existing Meridian Road roadside ditch, ultimately conveys runoff to the existing detention and water quality pond MN, as shown and discussed in the Falcon DBPS. The Falcon DBPS also shows a future detention and water quality pond SR-4 that is to receive flows from basin MT060 and discharge into basin MT070, ultimately routing to existing Pond MN. Flows from Bent Grass Meadows Drive are listed in basin MT060 but are being routed to the existing roadside ditch along Meridian Road, which is in basin MT070. The flows from the "School Site" and upstream basins will release into the east side of Pond SR-4 (west of Falcon Market Place). Pond SR-4 is currently under construction. The proposed improvements impact on the existing drainage basin and both Pond MN and Pond SR-4 are discussed later in the report.

4. Consider Need for Industrial and Commercial BMPs

Source control BMPs for homeowners include the use of garages as the primary area where pollutants can be stored. The single-family detached homes provide garages which can act as storage areas. The proposed development does not include outdoor storage or the potential for introduction of contaminants to the Counties' MS4, thus no targeted source control BMPs are necessary. The biggest source control BMP is public education and discuss topics such as: pet waste, car washing, lawn care, fall leaves, and snow melt and deicer.

Bent Grass East Commercial Filing No. 1 contains commercial development. This area will need to consider the need for Industrial & Commercial BMPs. No industrial uses or outside storage is proposed for this area. Drainage will be routed through water quality ponds prior to leaving the site to minimize contaminants into the public system.

VII. Future Drainage Conditions

MIDDLE TRIBUTARY

Design Point 30 and Basins OS-25 and OS-26 are as described under Existing Drainage Conditions. However, Basins OS-25 and OS-26 now route through proposed "future" detention pond, on what's been previously referred to as the "School Site", north of Bent Grass Meadows Drive and just west of Bent Grass Filing No. 2. This "future" pond will replace the current sedimentation pond on the "School Site". Upon any additional development within the Middle Tributary area of the Bent Grass Development and north of Bent Grass Meadows Drive, this pond will need to be constructed to accommodate the re-routed flows from the Meadows Pond #2 at DP 30.

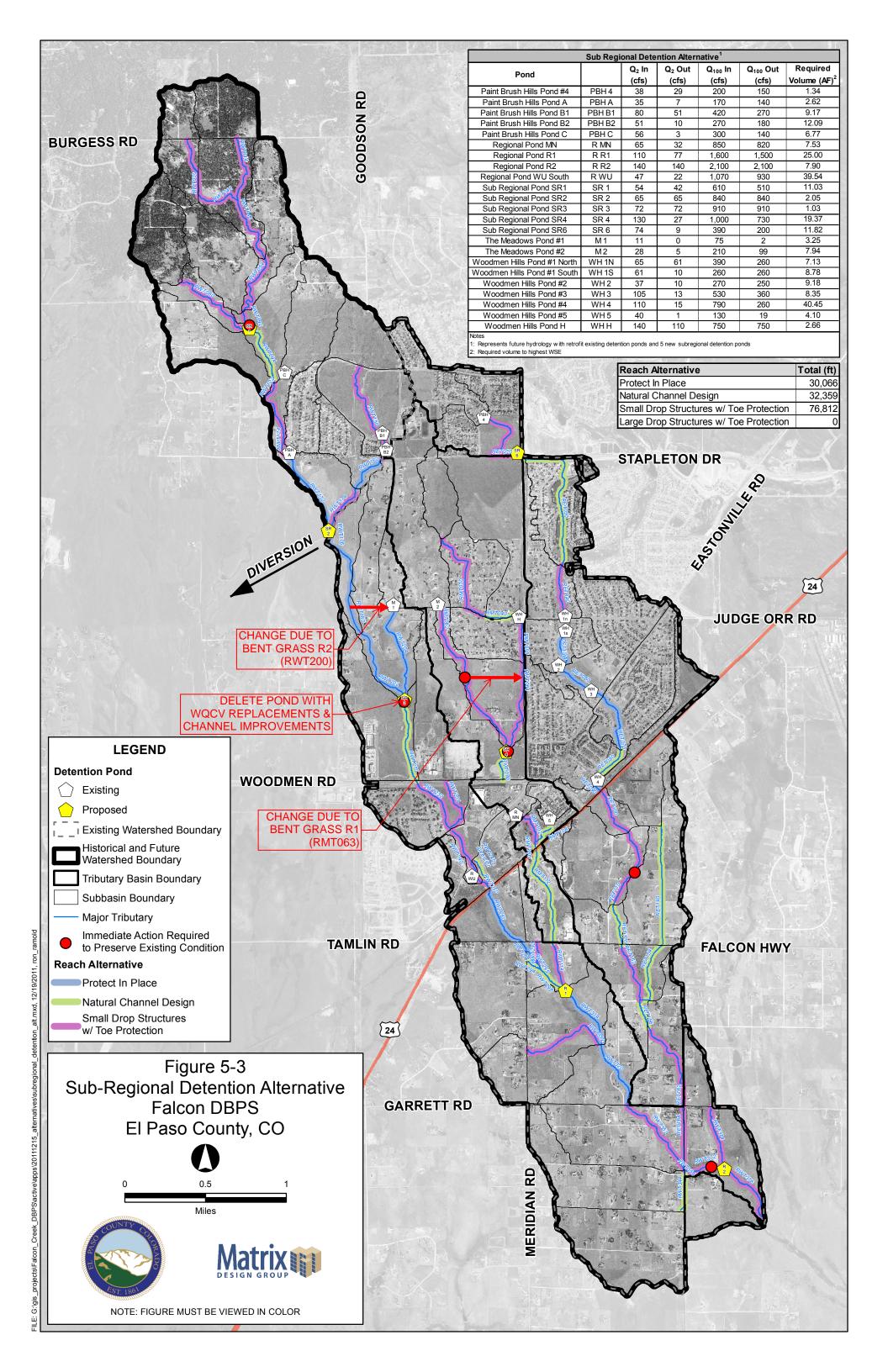
This future facility will need to provide 2.76 ac-ft of water quality, 6.26 ac-ft for EURV and 11.98 ac-ft for 100-year storage volume. Preliminary release rates for the 5 and 100-year storms are 3.8 cfs and 32.2 cfs. These flows were then routed to Bent Grass Meadows to the south. With the decrease in flows, flows will not overtop Bent Grass Meadows Drive and continue east to the future box culvert under Bent Grass Meadows Drive at DP BG20 (5-year flow=292.5 cfs, 100-year flow=909.3 cfs). Flows were still checked against street capacity on the north and south side of Bent Grass Meadows Drive, as it continues to the east. With the construction of the future pond, Bent Grass Meadows Drive will be able to adequately handle the flows and no additional storm infrastructure would need to be built to carry these future developed flows. Any area north of Bent Grass Meadows Drive that will develop in the future will need to provide its own on-site detention. Should future development not be able to release flows into Bent Grass Meadows Drive, a 42" RCP would be able to convey the flows of DP BG 15n (Q100=40.9 cfs, Q5=8.8 cfs) to the northwest corner of the Bent Grass Meadows Drive and Meridian Road intersection. Analysis for this culvert sizing has been included in the appendix.

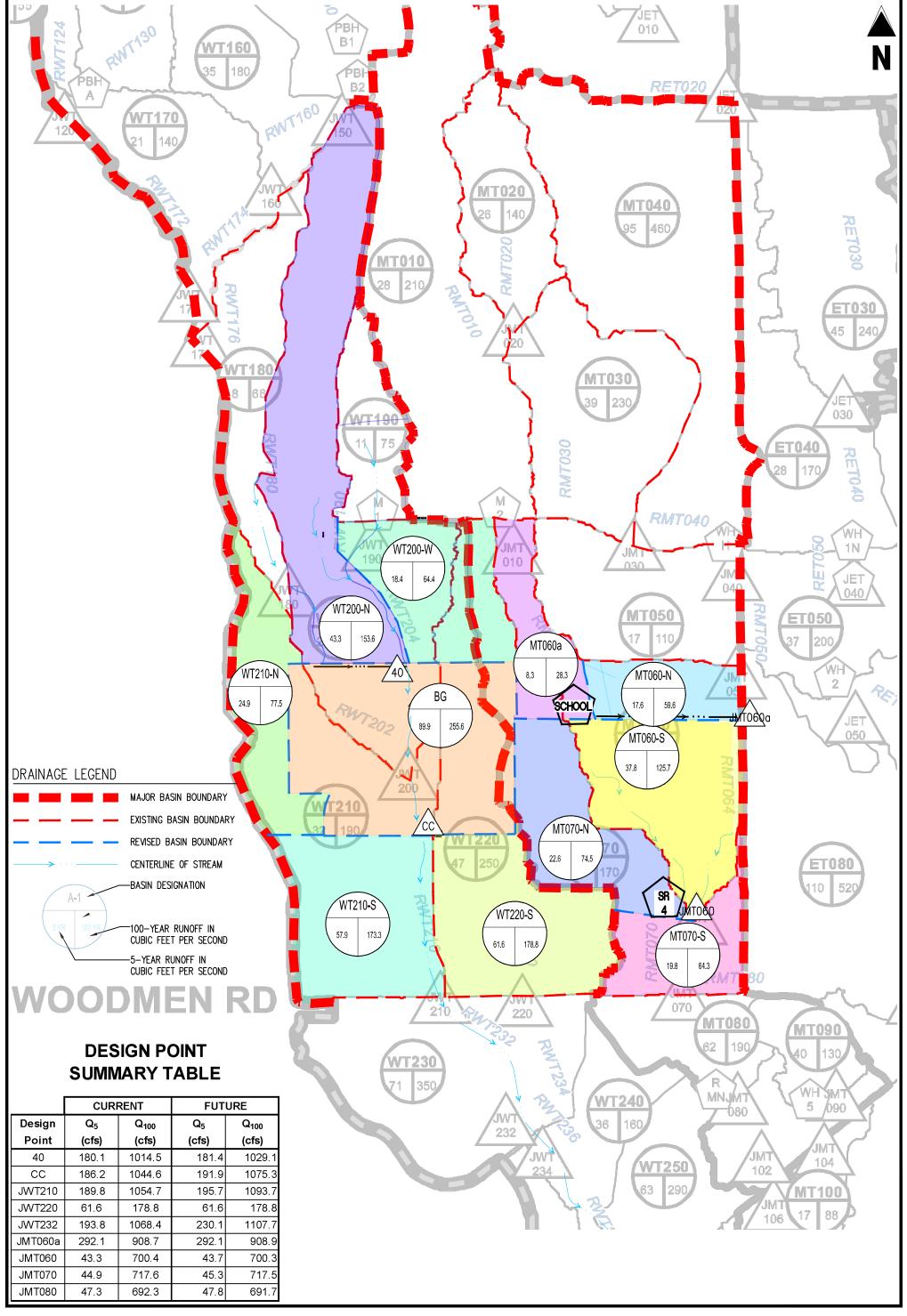
At the Bent Grass Meadows Drive/Meridian Road intersection, the elliptical rcp's will need to be replaced with a double 16' x 4' rcbc. The future roadside ditch will have a 15' wide bottom channel with 4:1 side slope, 6.5' deep and a longitudinal slope of 0.30%. This will result is a flow depth of 5.15' and velocity of 5.04 fps. This channel will direct flows to Owl Place where the existing twin cmp's will be replaced with a 20' x 4' rcbc or equivalent. This structure will need to be built when any development west of Meridian Road at the intersection of Owl Place happens. With future development, it is anticipated that the existing channel conveying flows to the south will be removed to accommodate the new development. The new channel will need to be a 35' wide bottom channel with 4:1 sides, 5' deep and a longitudinal slope of 0.30%. This will produce a flow depth of 3.7' and a velocity of 4.6 fps. If the channel option is not viable, twin 78" rcp's at a minimum 0.50% slope would be able to handle this future flow. Analysis for this design option has been included in the appendix.

Calculations are provided in Appendix C for the future culverts and roadside channel.

WEST TRIBUTARY

Offsite flows entering the west tributary location of Bent Grass have not changed from what was discussed under Current Conditions. Reach RWT202 at the northwest corner of the development has a 100-year flow of 1000 cfs and Reach RWT204 has a flow of 43 cfs. These were obtained from the DBPS by Matrix. The Flood Insurance Study (FIS) by FEMA does not have flows evaluated this far north. The have a flow of 1482 cfs beginning at RWT210. The 8 undeveloped on-site basins for Bent Grass West have been replaced with 17 developed basins. These basins are found in the Falcon Meadows for Bent Grass PDR. A summary of these basins is provided below and are part of the hydrology analysis provided in Appendix B.

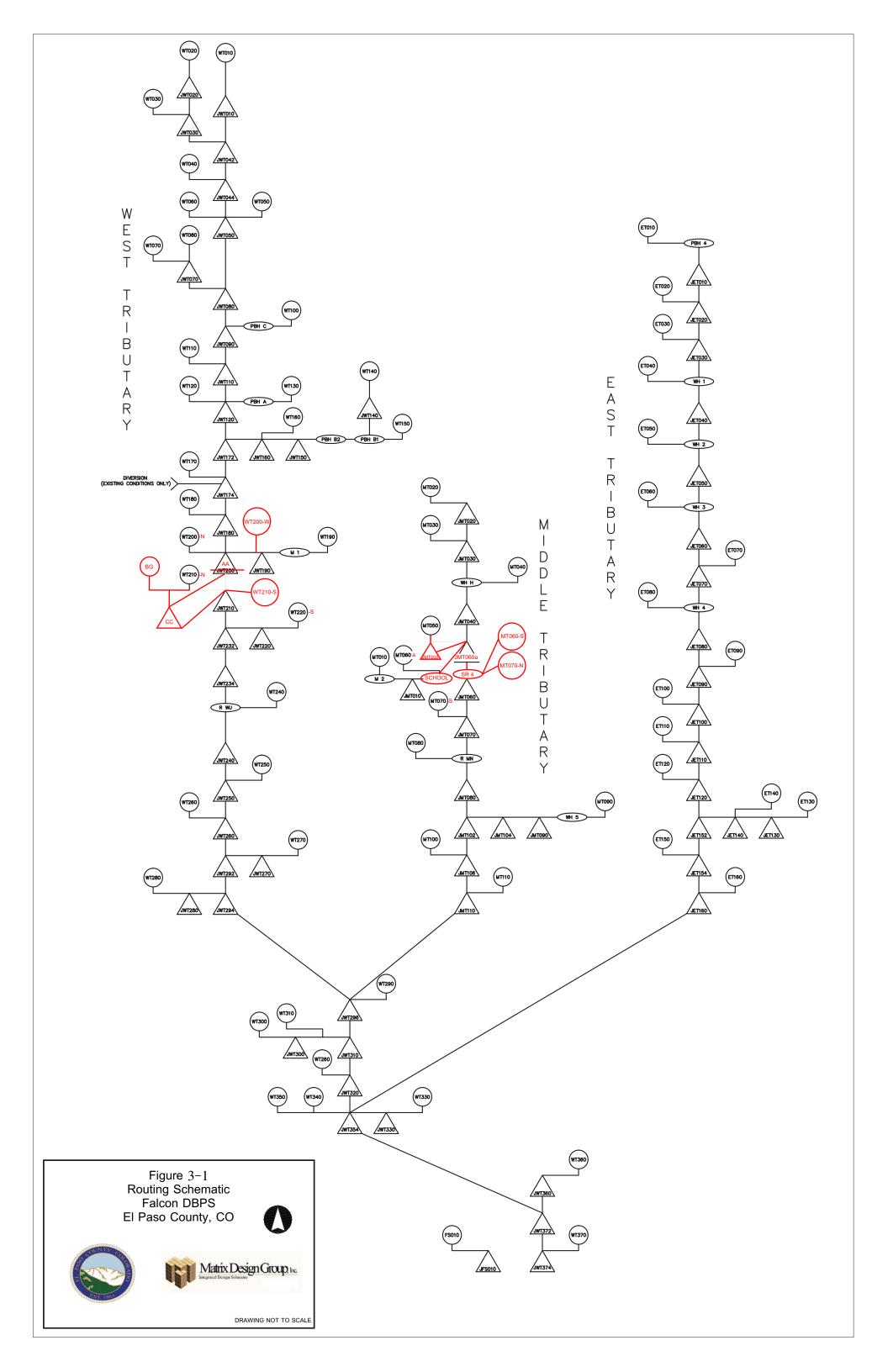




FALCON MEADOWS AT BENT GRASS MDDP

| Project No: | CLH0017 |
|-------------|----------|
| Drawn By: | CMD |
| Checked By: | GD |
| Date: | 06/16/21 |

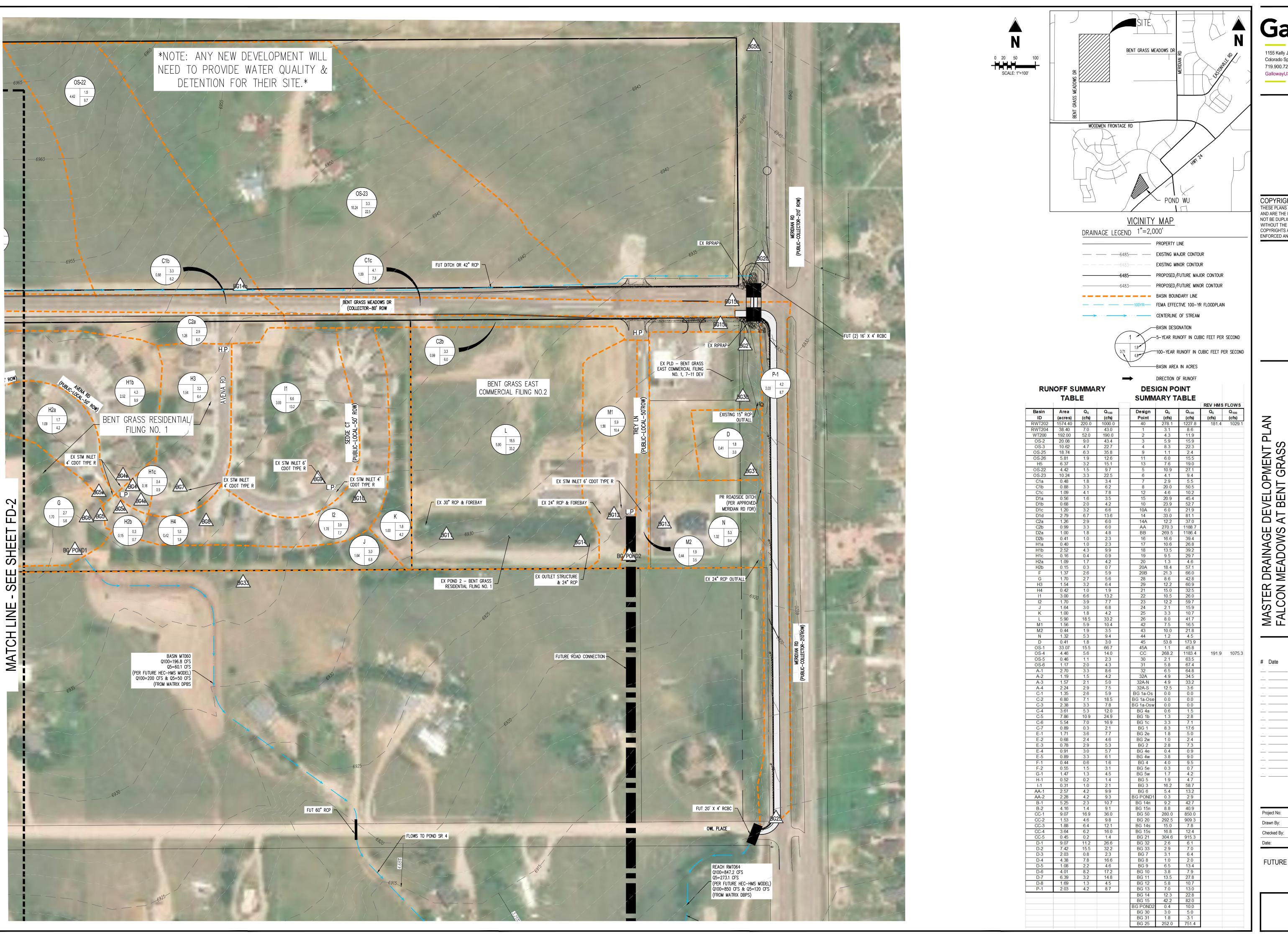




MERIDIAN ROAD

Worksheet for Fut Channel - Pr 100 Yr Flow-MR

| Desired Description | | | |
|---|-----------------|----------|-------------|
| Project Description | | | |
| Friction Method | Manning Formula | | |
| Solve For | Normal Depth | | |
| Input Data | | | |
| Roughness Coefficient | | 0.035 | |
| Channel Slope | | 0.30 | % |
| Left Side Slope | | 4.00 | ft/ft (H:V) |
| Right Side Slope | | 4.00 | ft/ft (H:V) |
| Bottom Width | | 15.00 | ft |
| Discharge | | 925.00 | ft³/s |
| Results | | | |
| Normal Depth | | 5.15 | ft |
| Flow Area | | 183.50 | ft² |
| Wetted Perimeter | | 57.49 | ft |
| Hydraulic Radius | | 3.19 | ft |
| Top Width | | 56.22 | ft |
| Critical Depth | | 3.58 | ft |
| Critical Slope | | 0.01368 | ft/ft |
| Velocity | | 5.04 | ft/s |
| Velocity Head | | 0.39 | ft |
| Specific Energy | | 5.55 | ft |
| Froude Number | | 0.49 | |
| Flow Type | Subcritical | | |
| GVF Input Data | | | |
| Downstream Depth | | 0.00 | ft |
| Length | | 0.00 | ft |
| Number Of Steps | | 0 | |
| GVF Output Data | | | |
| Upstream Depth | | 0.00 | ft |
| Profile Description | | | |
| Profile Headloss | | 0.00 | ft |
| Downstream Velocity | | Infinity | ft/s |
| Upstream Velocity | | Infinity | ft/s |
| Normal Depth | | 5.15 | ft |
| Critical Depth | | 3.58 | ft |
| - · · · · · · · · · · · · · · · · · · · | | | |



Galloway

1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920 719.900.7220 GallowayUS.com

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MASTER DRAINAGE D FALCON MEADOWS A FOR CHALLENGER COMMI

FUTURE CONDITIONS DRAINAGE MAP

REQUEST FOR CONDITIONAL LETTER OF MAP REVISION

UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK, FALCON OWL PLACE

Falcon, Colorado October 25, 2022

Prepared by:

Drexel, Barrell & Co. 1376 Miners Drive, Suite 107 Lafayette, Colorado 80026 (303) 442-4338

Contact: Michelle Iblings, P.E., CFM

Prepared for:

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DBC Project No. 21611-00BLWR

TABLE OF CONTENTS

REPORT

| 1.0 | INTE | RODUCTION | 1 |
|---------|-------|--|---|
| | 1.1 | Background | 1 |
| | 1.2 | General Location and Project Description | 1 |
| | | Regulatory Floodplain | |
| 2.0 | PRE | VIOUS STUDIES | 2 |
| 3.0 | HYD | ROLOGIC ANALYSIS | 3 |
| | 3.1 | Falcon DBPS | 3 |
| | 3.2 | Falcon Owl Place | 3 |
| 4.0 | HYD | RAULIC ANALYSIS | 4 |
| | 4.1 | General | 4 |
| | 4.2 | Vertical Datum | 4 |
| | 4.3 | Horizontal Datum | 5 |
| | 4.4 | Box Culvert Hydraulic Analysis | 5 |
| | 4.5 | Existing Owl Place Culverts | 5 |
| 5.0 | NFIP | REGULATION COMPLIANCE | 7 |
| | 5.1 | Floodplain Work Map and Annotated FIRM | 7 |
| | 5.2 | Forms and Notifications | |
| | 5.3 | Compliance with Section 65.12 | 7 |
| | | Endangered Species Act (ESA) | |
| 6.0 | CON | CLUSIONS | 7 |
| 7.0 | REFI | ERENCES | 8 |
| | | | |
| LIST (| OF FI | GURES | |
| Figure | 1 V | icinity Map | 2 |
| LIST (| OF TA | ABLES | |
| | | | |
| | | uture Land Use Conditions Peak Discharges, Falcon DBPS | |
| Table 3 | 3-2 P | roposed Peak Discharges at Falcon Owl Place | 3 |
| APPE | NDIC | ES | |
| Appen | div 1 | Construction Drawings | |
| Appen | | FEMA Comment Responses | |
| Appen | | Falcon DBPS | |
| Appen | | HEC-HMS Modeling | |
| Appen | | Hydraulic Modeling | |
| Appen | | FEMA MT-2 Forms | |
| Appen | | FPWM & Annotated FIRM | |
| Appen | | Endangered Species Act | |
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REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK FALCON OWL PLACE

1.0 INTRODUCTION

1.1 Background

The following report and supporting documentation are being submitted to FEMA for the purpose of requesting a Conditional Letter of Map Revision (CLOMR) for a portion of the Unnamed Tributary to Black Squirrel Creek (UTBSC) in El Paso County, Colorado.

The Falcon Owl Place consists of approximately 4.6 acres at the southwest corner of Owl Place and Meridian Road as shown in **Figure 1**. The property currently has an address of 11745 Owl Place, and is currently known as Lot 15 of the Falcon Ranchettes. The East Branch of the UTBSC flows southwest across the property and is proposed to be contained within a 10'x6' box culvert that will discharge into the Subregional Pond SR4 recently constructed on the Falcon Marketplace property. A general site layout of the Falcon Owl Place development is shown in the construction drawings included in **Appendix 1**.

The improvements associated with Falcon Owl Place are in general conformance with the Falcon Basin, Drainage Basin Planning Study (Falcon DBPS), prepared by El Paso County in 2015. The hydrologic analysis completed for the Falcon DBPS was used as the basis for the current CLOMR.

The Effective FEMA Flood Insurance Rate Map (FIRM) Number 08041C0553G in **Appendix 7** shows the East Branch of the UTBSC 100-year Zone A floodplain across the western portion of the Owl Place site. This report presents hydrologic and hydraulic study results showing that the proposed 100-year floodplain will be confined within a piped storm drain system (10'x 6' box culvert).

It is the Owner/Developer's intent to comply with all floodplain regulations.

1.2 General Location and Project Description

This CLOMR is limited to the 4.6-acre parcel located at the southwest corner of Owl Place and Meridian Road, SE 1/4 of the SE 1/4 of Section 1, Township 13 S, Range 65 W of the 6th P.M., El Paso County, Colorado. The subject property will be developed with a multipad shopping center (Falcon Owl Place).

The Falcon Owl Place development includes regrading the site and rerouting the East Branch of the UTBSC across the site. Approximately 1022 feet of the creek will be impacted by the development, which intercepts the existing creek north of Owl Place and conveys it via a 10'x6' box culvert to an off-site subregional detention pond (SR4). The box culvert is designed to convey the full 100-year discharge.

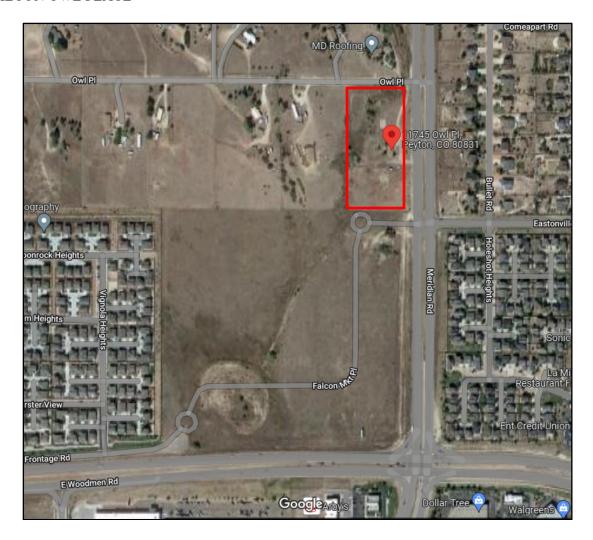


Figure 1 – Vicinity Map

1.3 Regulatory Floodplain

The Effective Zone A limits for the East Branch of the UTBSC on the Falcon Owl Place site are defined on Map Number 8041C0553G dated December 7, 2018. No flow rates, floodway data or flood profiles were defined for this section of UTBSC in the effective FIS for El Paso County, Colorado, Revised December 7, 2018.

2.0 PREVIOUS STUDIES

El Paso County completed hydrologic and hydraulic analyses summarized in a report titled Falcon Basin, Drainage Basin Planning Study, Selected Plan Report, Final, September 2015 (Falcon DBPS). The Falcon DBPS encompasses three unnamed tributaries to Black Squirrel Creek, including the "Middle Tributary" which flows across the subject property. Select output from the Falcon DBPS is included in **Appendix 3**.

3.0 HYDROLOGIC ANALYSIS

3.1 Falcon DBPS

The Falcon DBPS completed hydrologic analysis for the Falcon Basin Watershed, using HEC-HMS v3.5 software, for historical, existing, and future land use conditions by applying a 24-hour storm event with 2-, 5-, 10-, 25-, 50-, and 100-year recurrence intervals and current drainage infrastructure. Chapter 3 and Appendix A of the Falcon DBPS include a detailed discussion of the hydrologic analysis. An electronic copy of the HEC-HMS model (File: Aug15_Working_Falcon_DBPS_S.hms) is also provided.

The Falcon DBPS identified Subregional Pond SR4 to be installed on the Falcon Marketplace property. Pond SR4 was constructed in early 2021 and the property floodplain mapping was updated in LOMR Case Number 21-08-0534P.

El Paso County requires regional drainage infrastructure to be sized for future land use conditions. Therefore, peak discharges with existing drainage infrastructure and future land use conditions near Owl Place are summarized in Table 3-1.

Table 3-1. Future Land Use Conditions Peak Discharges near Falcon Owl Place on the Middle Tributary, Falcon DBPS

| Model Location | Physical Location | Branch | Proximity to Owl Place | Q100 (cfs) |
|-------------------|--|-----------------------------------|------------------------|------------|
| JMT050 | Bent Grass Meadows Drive | Only East Branch | Upstream of Site | 850 |
| JMT060 | Eastonville Road (Pond SR4 inflow) | Both East and West Branches | Downstream of Site | 1,000 |

3.2 Falcon Owl Place

The Falcon DBPS HEC-HMS model with existing drainage infrastructure and future land use (Existing Conditions) was used as the basis for the Falcon Owl Place hydrologic analysis. The Existing Conditions model was replicated in HEC-HMS version 4.7.1, due to instabilities and runtime issues with the prior, outdated model version (3.5). The Existing model produced 100-year peak flows of 859 and 1,023 cfs upstream (JMT050) and downstream (JMT060) of the site, which are comparable to and more conservative than the 850 and 1,000 cfs in the DBPS. It should be noted that in Existing Conditions, JMT050 is on the East Branch of the Middle Tributary, whereas JMT060 includes flows from both the West and East Branches, immediately upstream of Pond SR4.

The Falcon watershed did not include a design point on the East Branch immediately upstream of Pond SR4. Therefore, it was necessary to modify the HMS model to obtain a design flow for Owl Place. In the Proposed Conditions basin model, the junction JMT051 was created on the East Branch of the UTBSC at the southern boundary of the Falcon Owl Place property, immediately upstream of Pond SR4.

The lag time and drainage area for Basin MT060 were reduced to 0.077 square miles and 17 minutes, respectively. The length and slope of Routing RMT060 were also updated. The NRCS soils for the proposed basin are Columbine gravelly sandy loam with a Hydrologic Soil Group (HSG) A. The basin is zoned for a combination of 5-acre residential, commercial, and planned unit development (PUD). The nearby PUD (Bent Grass Meadows) is residential with an average lot size of 0.22 acres. Based on TR-55 Table 2-2a, areas with 0.22-acre lots and HSG A have a Curve Number (CN) of 65. However, it is unknown how and when this area will develop in the future. For example, the Owl Place site is currently being rezoned from RR-5 to CS, which would increase the CN from 46 to 89. The future conditions CN of 66 used in the Falcon DBPS is a reasonable representation of the future development potential in the basin and was used in the proposed conditions model.

The hydrologic parameter calculations, base mapping, and select output from the HEC-HMS model is included in **Appendix 4**, and the model files (HEC-HMS file: Falcon_OwlCLOMR.hms) are provided. Proposed peak discharges used for the Falcon Owl Place development are summarized in Table 3-2.

Table 3-2. Proposed Peak Discharges at Falcon Owl Place (East Branch of the UTBSC)

| Recurrence Interval | Q100 (cfs) |
|------------------------|------------|
| 100-year | 920 |
| 5-year | 288.5 |

4.0 HYDRAULIC ANALYSIS

4.1 General

The effective FIRM identifies an approximate Zone A floodplain across the Falcon Owl Place property with no flood profiles, discharges, or BFE's defined. The Falcon Owl Place development includes filling and regrading the site and rerouting the East Branch of the UTBSC through a box culvert across the site.

4.2 Vertical Datum

The effective FIRM is on the North American Vertical Datum of 1988 (NAVD88). The ALTA survey completed for the site (Olsson, 2021) and the design and construction

drawings are on the National Geodetic Vertical Datum of 1929 (NGVD29). The Falcon DBPS and the hydraulic analysis for this CLOMR were both completed on the NGVD29. The difference between the NGVD29 and NAVD88 is 3.8 feet on the Falcon Owl Place.

4.3 Horizontal Datum

The field survey, design, construction drawings and hydraulic modeling for the Falcon Owl Place project were completed on the North American Datum of 1983 (NAD83), Colorado State Plane coordinate system, Central Zone.

4.4 Box Culvert Hydraulic Analysis

Under existing and proposed conditions, the East Branch of the UTBSC leaving the Falcon Owl Place site discharges to Pond SR4 on the Falcon Marketplace. The pond was designed for a 100-year discharge of 1,016 cfs, which includes both West and East branches of the UTBSC. The 100-year water surface elevation upstream of the pond as shown in the LOMR is 6902.5 (NAVD88), or 6898.7 (NGVD29). The starting HGL for the box culvert analysis was conservatively placed at the top of pipe elevation of 6895.84 feet (NGVD29) for analyzing flows to the East branch only. However, an additional analysis was performed with a starting HGL of 6898.7, to evaluate the backwater effects from the pond.

StormCAD was used to evaluate the hydraulic performance of the 10'x6' box culvert. The profile and output for the 100-year storm event is included in **Appendix 5**, and the model files are provided.

4.5 Existing and Proposed Owl Place Culverts

The East Branch of the UTBSC is currently conveyed under Owl Place via two 36" CMP near the northeast corner of the site. The HY-8 software was used to analyze the existing culverts for the 100-year storm event.

The 2-36" CMP culverts are severely undersized and partially filled with sediment as shown in the photo below. The culverts only convey 86-95 cfs, depending on tailwater depth. The remaining flow (approximately 825-834 cfs) in the 100-year event overtops Owl Place. The proposed box culvert will convey the entire 100-year event (920 cfs) with an HGL of 6911.31 at the proposed headwall upstream of Owl Place, which is more than one foot below Owl Place and contained within the existing and proposed channel upstream. Channel grading will be required for approximately 30 feet to tie into the existing creek profile upstream. The channel side slopes will be reduced from approximately 5.5H:1V to 1.8H:1V and protected with riprap.

The HY-8 output is included in **Appendix 5** and the model file (Owl Place.hy8) is provided.



Existing 2-36" CMP under Owl Place (Upstream Inlets)

5.0 NFIP REGULATION COMPLIANCE

5.1 Floodplain Work Map and Annotated FIRM

The effective Zone AE 100-year floodplain delineation for the UTBSC terminates at the boundary between the Falcon Marketplace and Falcon Owl Place properties and represents flows from both West and East branches. No changes are proposed to the Zone AE floodplain. The 100-year flood discharge for the East Branch is contained in the proposed culvert. Therefore, the Zone A floodplain for this branch has been removed, and the split between the Zone A floodplains for the West and East branches is denoted in the Annotated FIRM. The effective and proposed UTBSC floodplains are delineated on the Floodplain Work Map and Annotated FIRM in **Appendix 7**.

5.2 Forms and Notifications

The appropriate FEMA forms are located in **Appendix 6**. Modifications to 100-year floodplain elevations and delineations are limited to the Falcon Owl Place development. Furthermore, there are no proposed increases to the BFE's or floodplain extents. Therefore, individual legal notices are not required for this CLOMR submittal.

5.3 Compliance with Section 65.12

Although there are no increases to BFE's due to the proposed project, an alternatives evaluation was performed to evaluate options for closed conduit and open channel conveyance of the East Branch of the UTBSC. The alternatives evaluation can be provided upon request.

Furthermore, no structures are located in areas that would be impacted by the floodplain modifications proposed by this CLOMR.

5.4 Endangered Species Act (ESA)

ESA Compliance information is provided in **Appendix 8**.

6.0 CONCLUSIONS

The Falcon Owl Place development will relocate a portion of the East Branch of an Unnamed Tributary of Black Squirrel Creek (Middle Tributary). This report and supporting documentation are being submitted to FEMA for the purpose of requesting a CLOMR to conditionally change the floodplain in accordance with NFIP regulations.

REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK, FALCON OWL PLACE

7.0 REFERENCES

City of Colorado Springs/El Paso County, Drainage Criteria Manual, Revised January 2021.

FEMA, FIRM Number 08041C0553G, El Paso County, Colorado and Incorporated Areas, Revised December 7, 2018.

FEMA, FIS Number 08041CV001A, El Paso County, Colorado and Incorporated Areas, Revised December 7, 2018.

Hydraflow Storm Sewers Extension for Autodesk Civil 3D, Version 12.

Matrix Design Group, Falcon Drainage Basin Planning Study, Selected Plan Report, Final, September 2015.

Olsson, ALTA Survey for Lot 15, Falcon Ranchettes, September 30, 2021.

USACE, Hydraulic Modeling System (HEC-HMS), Version 4.7.1, Build 11161, January 14, 2021.

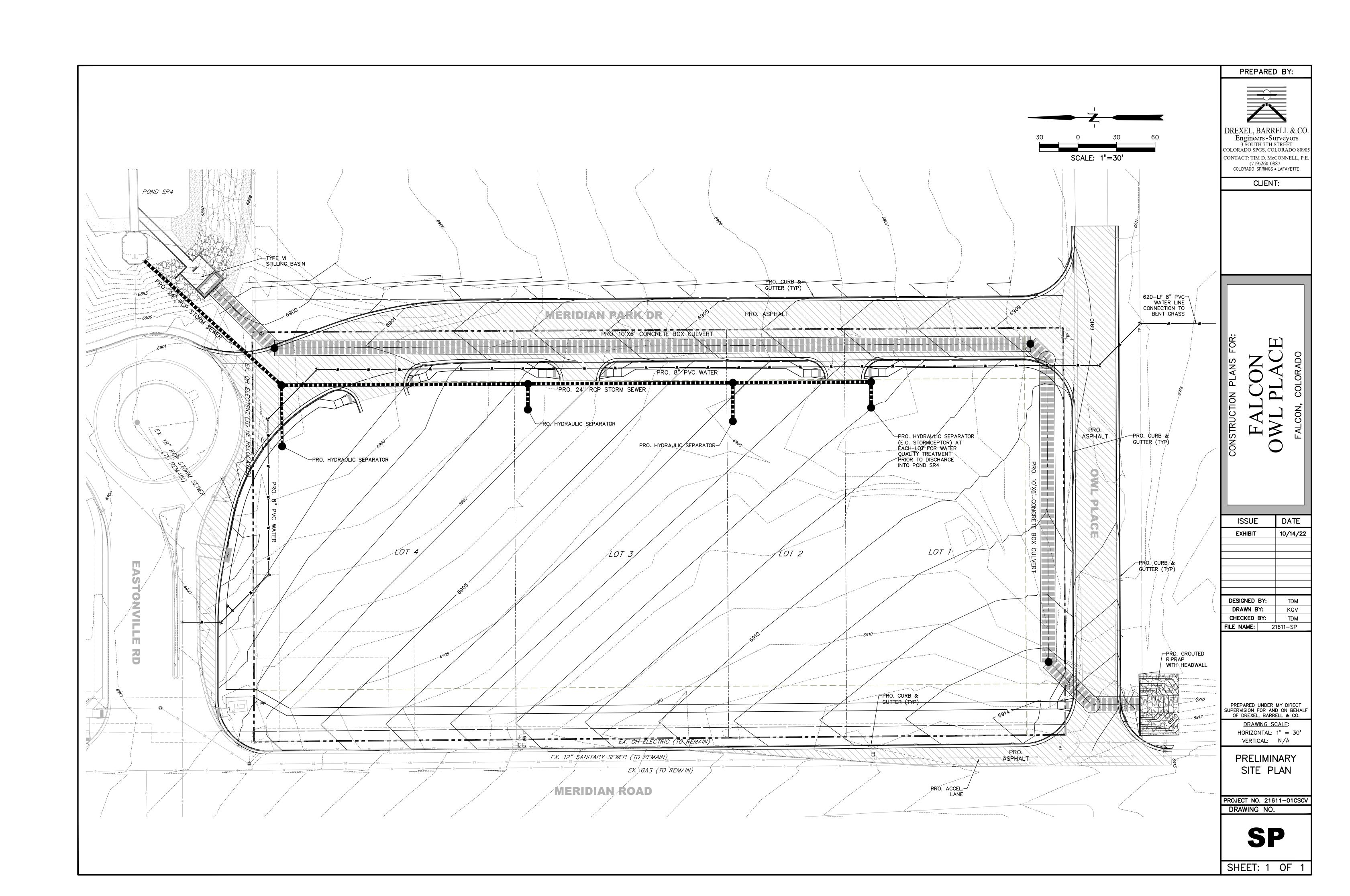
REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK Falcon Owl Place

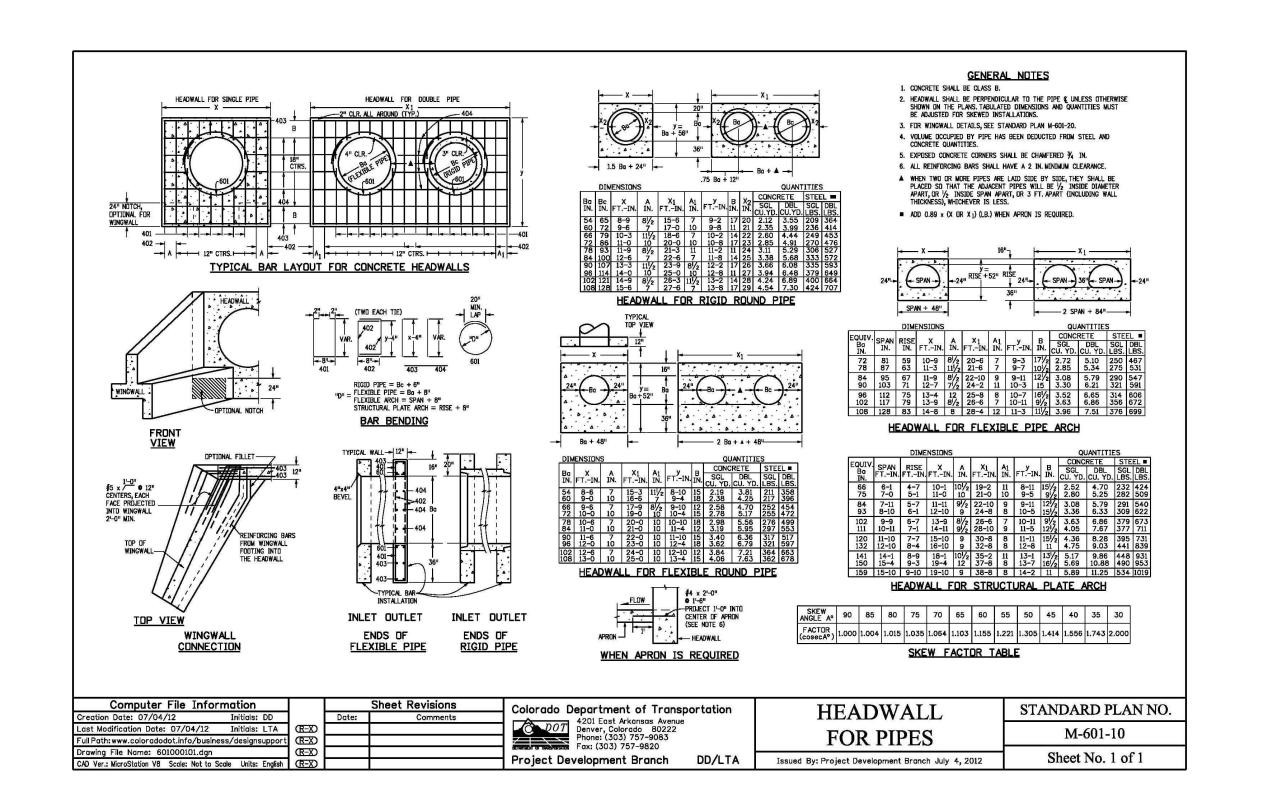
APPENDICES

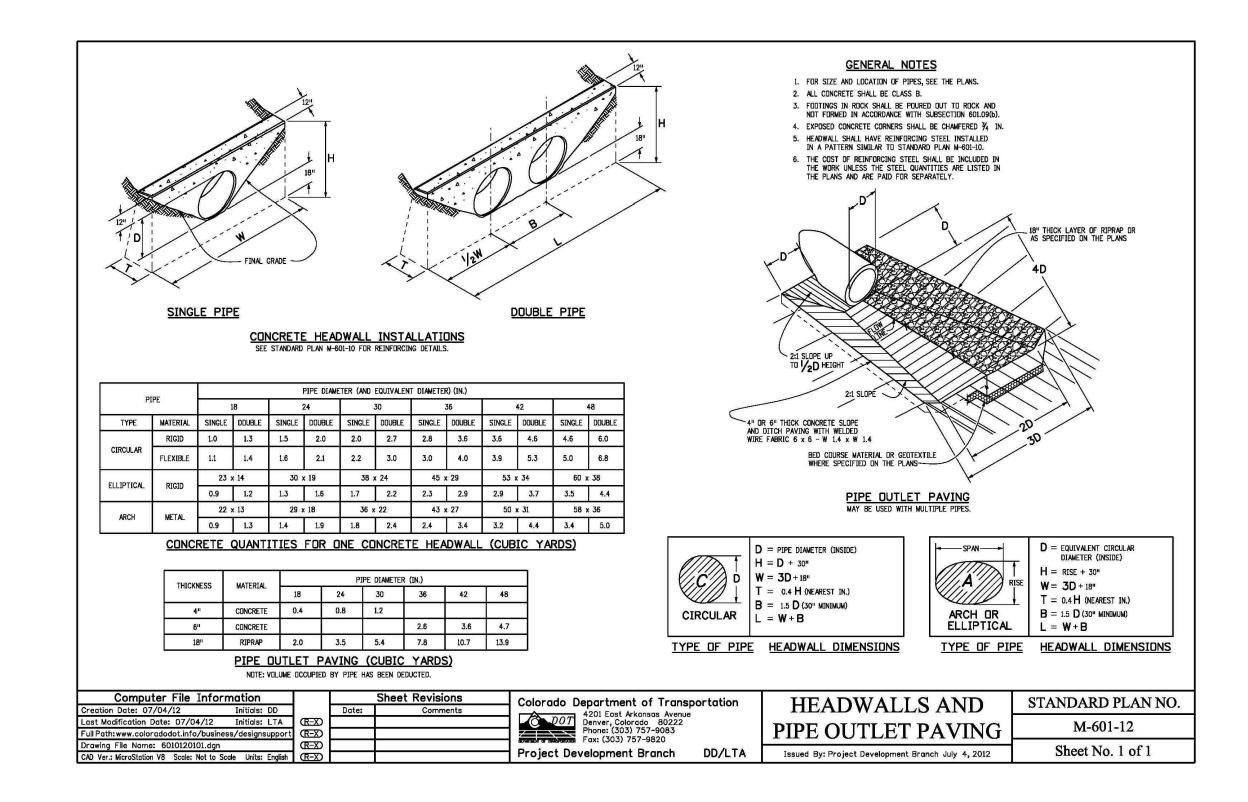
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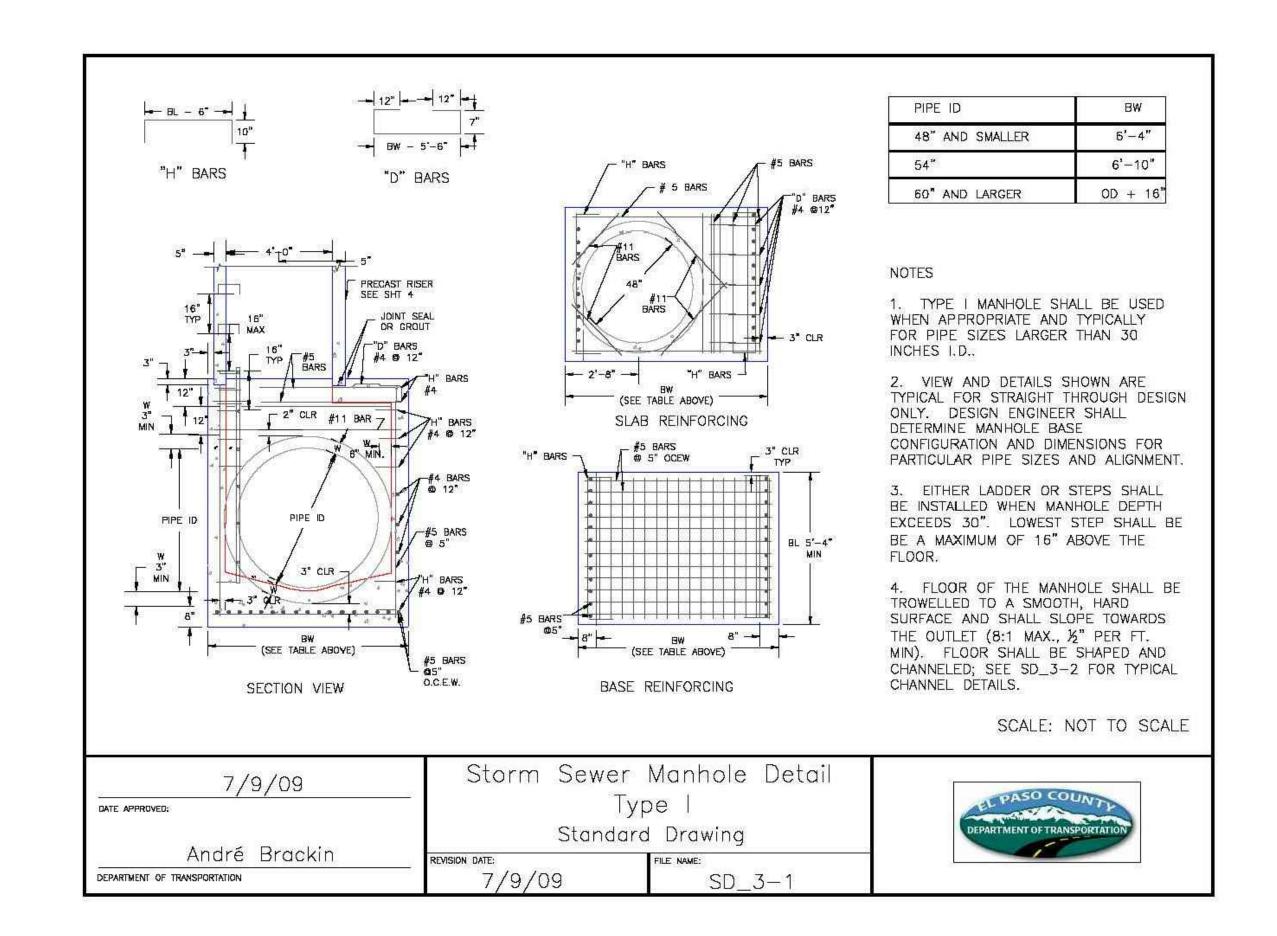
APPENDIX 1 CONSTRUCTION DRAWINGS

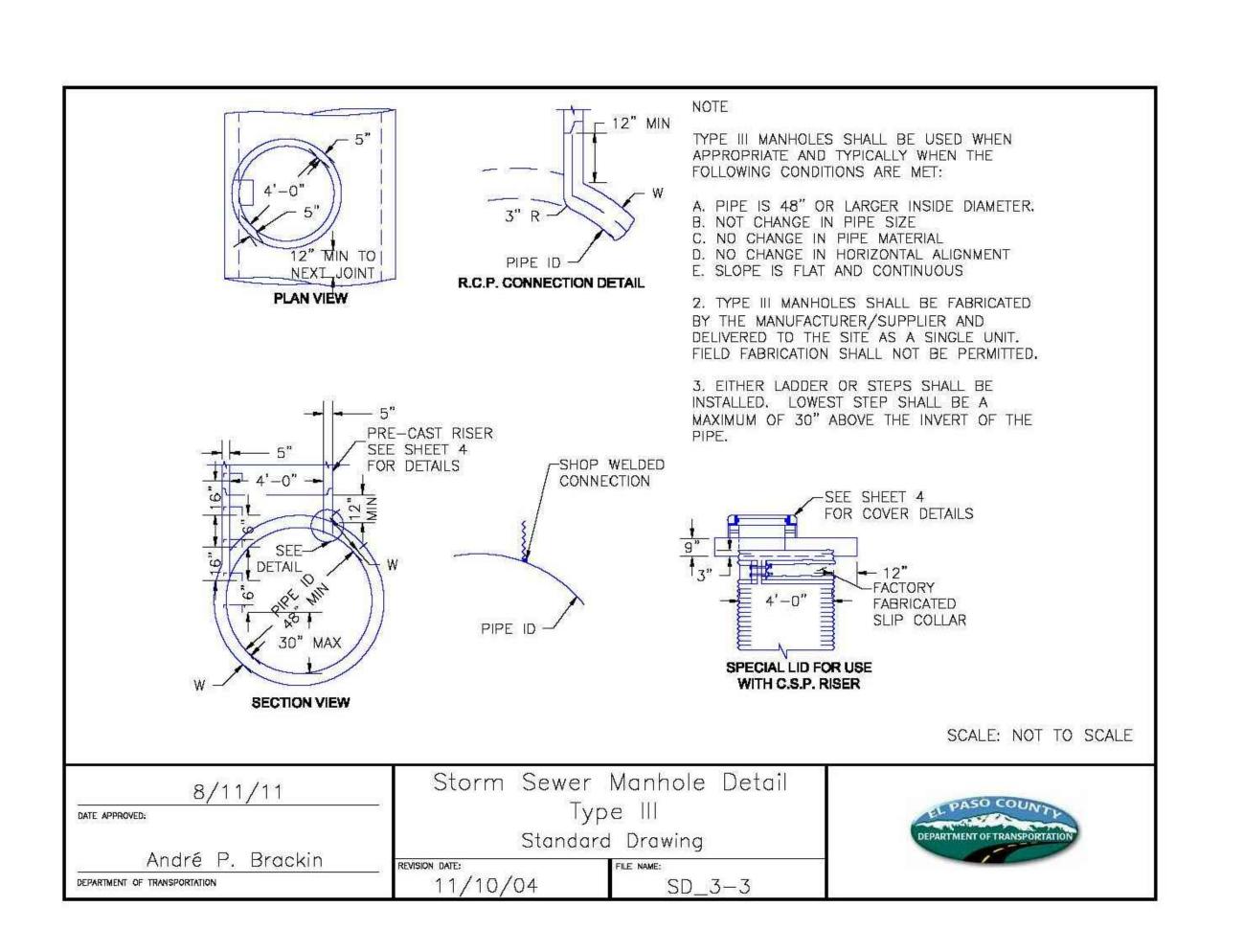
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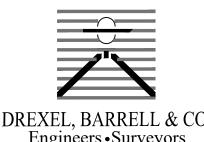








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CONTACT: TIM D. McCONNELL, P.E
(719)260-0887
COLORADO SPRINGS • LAFAYETTE

CLIENT:

FALCON OWL PLACE

| ISSUE | DATE | | | |
|------------|------------|-----|--|--|
| EXHIBIT | 10/14/22 | | | |
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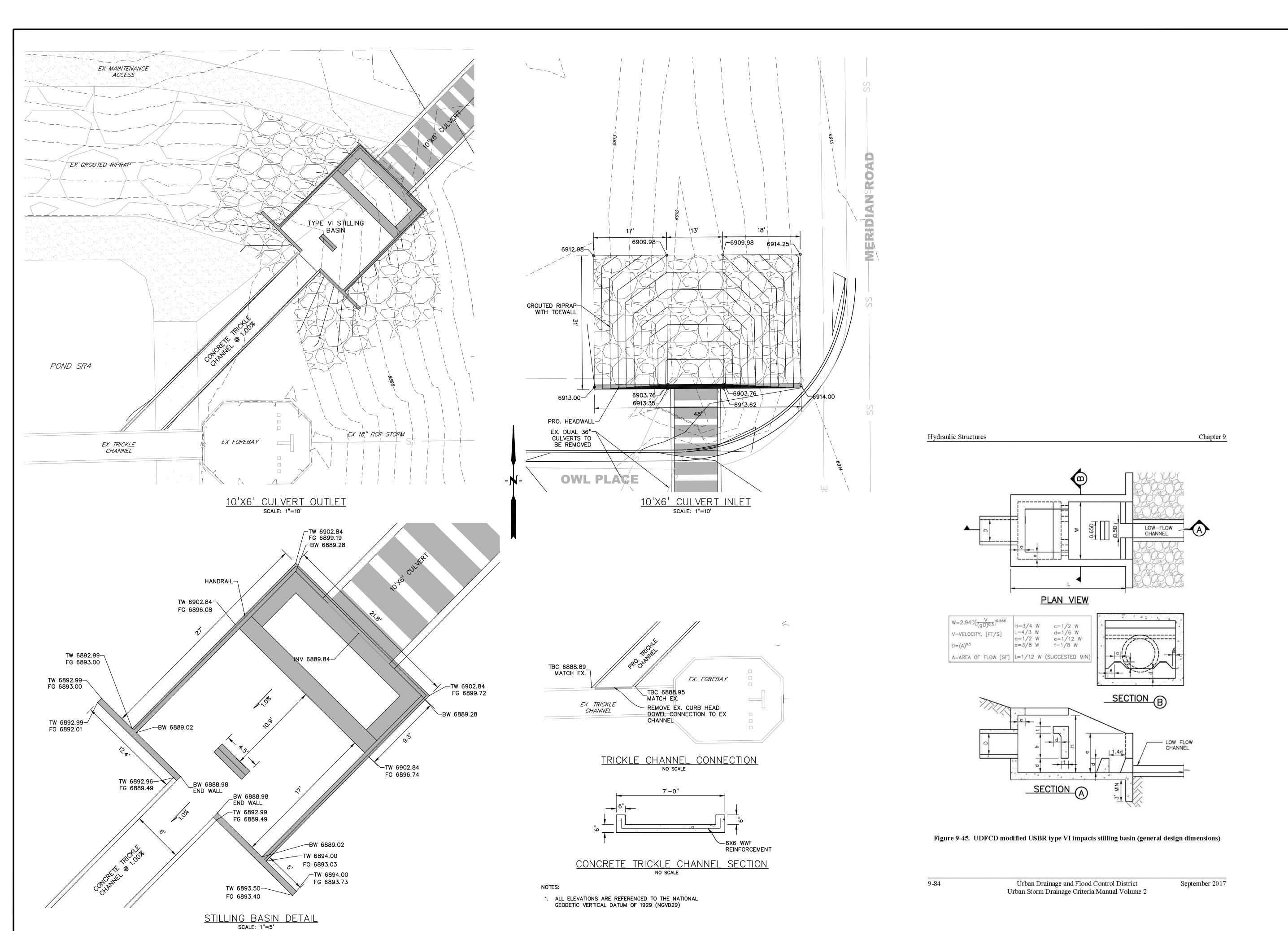
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HORIZONTAL: 1" = 10'
VERTICAL: N/A

PRELIMINARY STORM CULVERT DETAILS

PROJECT NO. 21611-01CSCV DRAWING NO.



SHEET: 1 OF 2



DDEYEL BADDELL & C

PREPARED BY:

DREXEL, BARRELL & CO.
Engineers • Surveyors
3 SOUTH 7TH STREET
COLORADO SPGS, COLORADO 80903
CONTACT: TIM D. McCONNELL, P.E
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COLORADO SPRINGS • LAFAYETTE

CLIENT:

FALCON OWL PLACE

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| EXHIBIT | 10/14/22 |
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DRAWN BY: KGV
CHECKED BY: TDM
FILE NAME: 21611—STDT

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF DREXEL, BARRELL & CO.

DRAWING SCALE:
HORIZONTAL: 1" = 10'
VERTICAL: N/A

PRELIMINARY STORM CULVERT DETAILS

PROJECT NO. 21611-01CSCV DRAWING NO.

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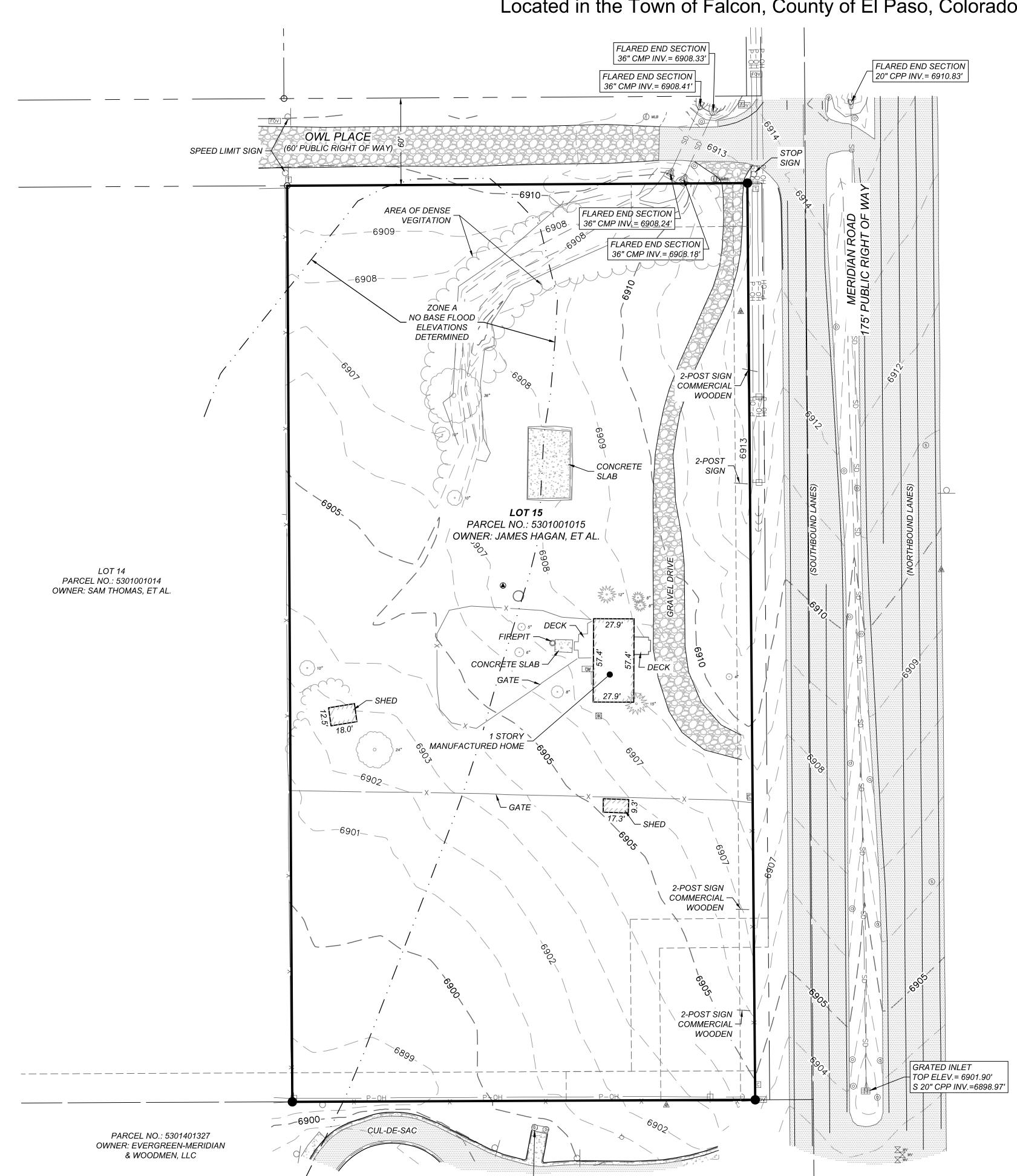
SHEET: 2 OF 2

ALTA / NSPS Survey

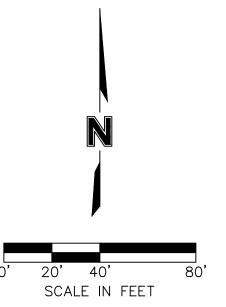
LOT 15, FALCON RANCHETTES

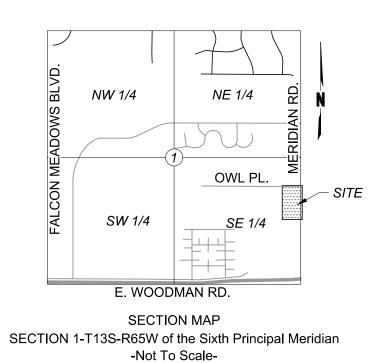
Part of the Southeast Quarter of Section 1, Township 13 South, Range 65 West of the 6th Principal Meridian

Located in the Town of Falcon, County of El Paso, Colorado



STORM MANHOLE RIM ELEV.=6899.55'





LEGEND ▲ Control Point (As-Described) O Found Monument Section Corner Bollard Electric Meter ▲ Electric Transformer Fov Fiber-Optic Vault Fiber-Optic Valve ← Guy Wire Sanitary Manhole Storm Manhole Single Support Sign Telephone Pedestal Water Manhole ⋈ Water Valve Storm Drain Pipe (As-Described) ----- Right-of-Way Line —— Parcel Line Easement Line - Underground Gas Overhead Power Barbed-Wire Fence Chain Link Fence Wrought Iron Fence



RESPONSIBILITY FOR EXISTING UTILITY LOCATIONS (HORIZONT OR VERTICAL). THE EXISTING UTILITIES SHOWN ON THIS DRAWING HAVE BEEN PLOTTE FROM THE BEST AVAILABLE INFORMATION. IT IS HOWEVER THE RESPONSIBILITY OF THE THE LOCATION OF ALL UTILITIES PRIOR TO THE COMMENCEMENT OF ANY CONSTRUCTION $\overline{\mathbf{m}}$

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ALTA / NSPS LAND TITLE SU JB Partners CS, LLC

checked by:
 QA/QC by:
 EJD

 project no.:
 021-06643

 drawing no.:
 V XALT 02106643

 date:
 09.29.2021

SHEET 3 of 3

REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK Falcon Owl Place

APPENDIX 4 HEC-HMS MODELING

LEGEND
EX. CONTOUR

PR. STORM SEWER

EFFECTIVE 100-YR
FLOODPLAIN

EX. BASIN MT060

PR. BASIN MT060

PR. SHALIOW FLOW

PR. CHANNEL FLOW

PR. RMT064

EX. FALCON OWL PLACE
PROPERTY BOUNDARY

FLOW DIRECTION

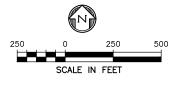
<u>NOTES</u>

- SPATIAL PROJECTION IS NAD83 COLORADO STATE PLANE, CENTRAL ZONE (FEET).
- 2. VERTICAL DATUM IS NGVD29.

The existing basin delineation is approximated from the Falcon DBPS, which was developed in 2015.

The existing conditions contours are from Lidar, and may not reflect roadway and drainage infrastructure that is shown on the aerial image.

The proposed basin delineation is based on a combination of Lidar contours, drainage and roadway infrastructure, aerial mapping, and site survey.



JMT051 (proposed)

> JMT060 (existing)

PREPARED BY:

DBC

Drexel, Barrell & Co.

Tractions Services, figure for Striction

Drexel, Barrell & Co.
Engineers •Surveyors
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CONTACT: MICHELLE IBLINGS, P.E.
(303) 442-4338
BOULDER
COLORADO SPRINGS
GREELEY

OWNER/CLIENT:

EXHIBIT FOR:
FALCON
OWL PLACE

| ISSUE | DATE |
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| EXHIBIT | 06/07/22 |
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HORIZONTAL: SEE PLAN
VERTICAL: N/A

HYDROLOGIC BASE MAP

PROJECT:21611-00BLWR DRAWING NO.

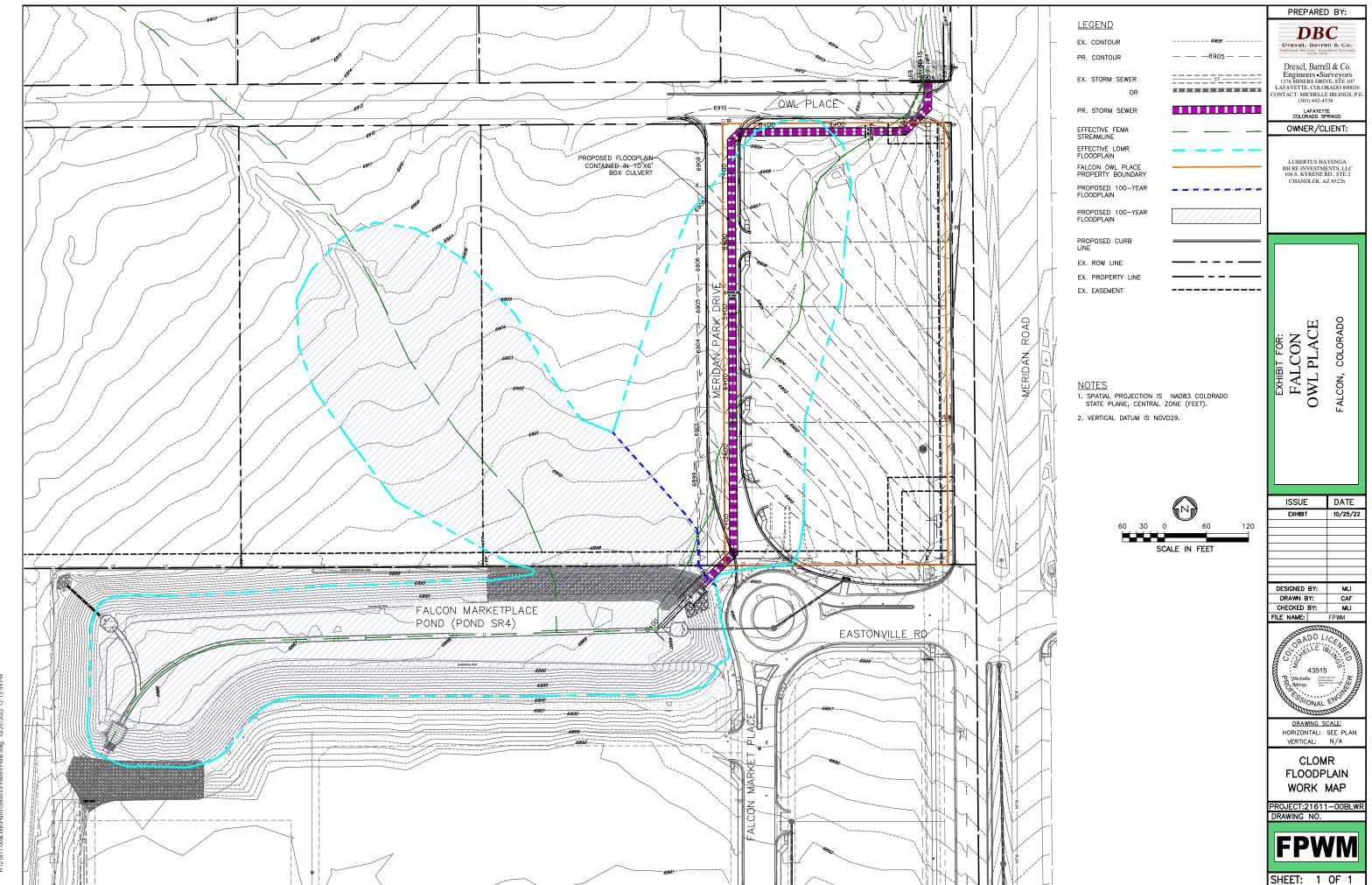


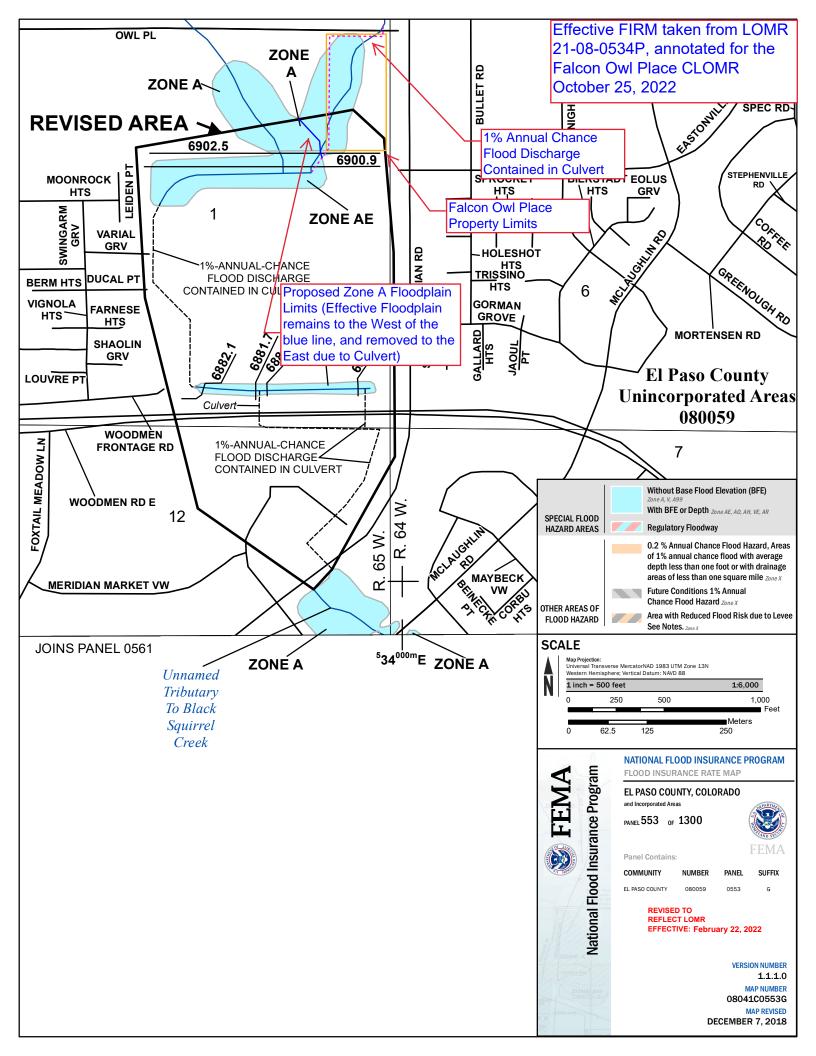
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REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK Falcon Owl Place

APPENDIX 7

FPWM & ANNOTATED FIRM





U.S. Fish and Wildlife Service

National Wetlands Inventory

Falcon Owl Place NWI



May 27, 2022

Wetlands

Estuarine and Marine Deepwater

Estuarine and Marine Wetland

Freshwater Emergent Wetland

Freshwater Pond

Freshwater Forested/Shrub Wetland

Lake

Other

Riverine

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.

FINAL DRAINAGE REPORT for FALCON MARKETPLACE

El Paso County, Colorado

November 4, 2019

SF-19-001

Prepared for:

LG HI Falcon, LLC. 3953 Maple Ave, #290 Dallas, TX 75219 Contact: Ben Hummel (214) 416-9820

Prepared by:

Drexel, Barrell & Co. 3 South 7th Street Colorado Springs, CO 80905 Contact: Tim McConnell, P.E. (719) 260-0887

TABLE OF CONTENTS

| 1.0 | CERTIFICATION STATEMENTS | 1 |
|------|--|----|
| 2.0 | PURPOSE | 2 |
| 3.0 | GENERAL SITE DESCRIPTION | 2 |
| 4.0 | DBPS ANALYSIS | 3 |
| 5.0 | UPSTREAM DRAINAGE DIVERSIONS | 7 |
| 6.0 | EXISTING CONDITION HYDROLOGY SUMMARY | 7 |
| 7.0 | PROPOSED HYDROLOGY (RATIONAL METHOD) & HYDRAULIC SUMMARY | 9 |
| 8.0 | PROPOSED DETENTION/WATER QUALITY FACILITIES | 15 |
| 9.0 | EXISTING CULVERTS AT E. WOODMEN ROAD | 16 |
| 10.0 | FOUR-STEP PROCESS | 17 |
| | GEOTECHNICAL HAZARDS | |
| 12.0 | EXISTING ONSITE UTILITY INFRASTRUCTURE | 18 |
| 13.0 | CONDITIONAL LETTER OF MAP REVISION (CLOMR) | 18 |
| 14.0 | DRAINAGE/BRIDGE FEES | 19 |
| 15.0 | CONSTRUCTION COST ESTIMATE | 20 |
| 16.0 | CONCLUSIONS | 21 |
| 17.0 | REFERENCES | 21 |

APPENDICES

VICINITY MAP
SOILS MAP
FLOODPLAIN MAP
HYDROLOGY CALCULATIONS
HYDRAULIC CALCULATIONS
DBPS EXCERPTS
CLOMR EXCERPTS
CLOMR APPROVAL
DRAINAGE MAPS

FINAL DRAINAGE REPORT

for

FALCON MARKETPLACE

Falcon, Colorado

1.0 CERTIFICATION STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E.

Colorado P.E. License No. 33797

For and on Behalf of Drexel, Barrell & Co.

DEVELOPER'S STATEMENT

i, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name:

LG HI Falcon, LLC.

By:

Ben Hummel

Date

12-18-19

Title:

Owner

Address:

3953 Maple Ave, #290

Dallas, TX 75219

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

For the County Engineer CONDITIONS:

By: Elizabeth Nijkamp

Date: 12/19/2019

El Paso County Planning & Community Development

Peak Discharges for the Future Developed Conditions at Points of Interest in vicinity of Falcon Marketplace Development (DBPS) without Pond SR4

| | | | Conditions, | | _ | _ | | ture | |
|--|----------------|-----------------|------------------------|----------|---------|-------|-----------|-------|--------|
| Location | HEC- | (5 | ource: Falco Basin/ | n basın, | рвгэ, п | | low (cfs) |) | |
| | HMS Element | Area (sq mi) | Design Point | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| West Branch at North Property Line of Falcon Marketplace | RMT062 | 0.29 | 1 | 1 | 11 | 25 | 62 | 110 | 160 |
| East Branch at North Property Line of Falcon Marketplace | RMT064 | 0.67 | 2 | 120 | 270 | 370 | 590 | 710 | 850 |
| Local Basin | MT060 | 0.19 | MT060 | 30 | 59 | 83 | 140 | 170 | 200 |
| Downstream of Proposed Falcon Marketplace Pond SR4 | JMT060 | 1.16 | 3 | 130 | 310 | 430 | 690 | 840 | 1000 |
| Local Basin | MT070 | 0.2 | MT070 | 25 | 50 | 69 | 110 | 140 | 170 |
| E. Woodmen Road, South Property Line of Falcon Marketplace | JMT070 | 1.36 | 4 | 150 | 350 | 490 | 800 | 980 | 1200 |

Peak Discharges for the Future Developed Conditions at Points of Interest in vicinity of Falcon Marketplace Development (DBPS) with Pond SR4

| | Future Co | | with existing ource: Falco | - | _ | | | nd SR4 (F | Pond #1) |
|--|-----------|---------|----------------------------|------------|----------------|-------|-----------|-----------|----------|
| Location | HEC- | (3 | Basin/ | ii basiii, | ББРЗ, П | | low (cfs) |) | |
| | HMS | Area | Design | | | | | | |
| | Element | (sq mi) | Point | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| West Branch at North | | | | | | | | | |
| Property Line of Falcon | RMT062 | 0.29 | 1 | 5 | 21 | 34 | 64 | 81 | 99 |
| Marketplace | | | | | | | | | |
| East Branch at North | | | | | | | | | |
| Property Line of Falcon | RMT064 | 0.67 | 2 | 121 | 273 | 373 | 591 | 712 | 847 |
| Marketplace | | | | | | | | | |
| Local Basin | MT060 | 0.19 | MT060 | 30 | 59 | 83 | 137 | 167 | 199 |
| Sub Regional Pond SR4 (Pond #1) Inflow | | 1.16 | | 133 | 310 | 431 | 697 | 847 | 1016 |
| Sub Regional Pond SR4 (Pond #1) Outflow | JMT060 | 1.16 | 3 | 27 | 142 | 246 | 467 | 595 | 727 |
| Local Basin | MT070 | 0.2 | MT070 | 25 | 50 | 69 | 114 | 139 | 165 |
| E. Woodmen Road, | | | | | | | | | |
| South Property Line of | JMT070 | 1.36 | 4 | 31 | 162 | 281 | 535 | 685 | 844 |
| Falcon Marketplace | | | | | | | | | |

As shown by the above tables, the existing 100-year discharge to E. Woodmen Road at the south property line (JMT070) is 760-cfs. Future developed conditions with no drainage improvements result in a 100-year discharge at JMT070 of 1200-cfs, hence the need for drainage improvements recommended by the DBPS.

The DBPS went on to study the placement of a sub-regional detention facility (Pond SR4) on the Falcon Marketplace property, resulting in a 100-year discharge of 844-cfs at JMT070. To be in conformance with the DBPS recommendations and current drainage criteria, the allowable 100-year discharge from the Falcon Marketplace development can be no greater than **760-cfs**. The following describes the further refining of the Pond SR4 design, and other improvements required in order for the release in conformance.

<u>Proposed Development & CLOMR Study</u>

On October 17, 2016 a CLOMR, prepared by Drexel, Barrell & Co., was submitted to FEMA. The CLOMR specifically details how the Falcon Marketplace development proposes filling the site and rerouting the UTBSC. This will be accomplished by intercepting the existing creek at the north property line and conveying it via a rundown into a subregional detention pond (SR4 - Pond #1), as recommended by the DBPS.

Pond #1 Inflow/Outflow/Stage/Storage Parameters

| Recurrence Interval | Pond Inflow (cfs) | Pond Outflow (cfs) | Water Surface Elevation (ft) | Storage Volume (ac-ft) |
|------------------------|-------------------|--------------------|---------------------------------|---------------------------|
| 100-year | 1,016 | 644 | 6897.0 | 26.6 |
| 50-year | 847 | 481 | 6896.4 | 24.5 |
| 25-year | 697 | 338 | 6895.8 | 22.5 |
| 10-year | 431 | 106 | 6894.6 | 18.3 |
| 5-year | 310 | 52 | 6894.2 | 17.0 |
| 2-year | 133 | 12 | 6891.8 | 10.0 |

Peak discharges resulting from proposed Pond #1 are summarized above.

Pond #1 will discharge to a new 96" RCP storm drainage system which will flow from south to east across the property and discharge to a section of grass-lined channel that parallels the south perimeter of the property.

Onsite runoff generated from the site, represented as a portion of MT070 in the HEC-HMS model, will be conveyed via curb and gutter, and storm sewer to proposed water quality basins at the south end of the site. The water quality basins will discharge into the open grass-lined channel along the south perimeter of the site.

Specific developed runoff quantities for the site were determined using the Rational Method and are discussed further in section 5.0 of this report.

The open grass-lined channel will then discharge into two sets of existing triple 48" culverts under E. Woodmen Road. Detention pond #1, 96" pipe and open channel are all designed to convey the full 100-year discharge.

No changes to the existing culverts under E. Woodmen Road are proposed. HY-8 software was used to quantify a 765-cfs total capacity of the existing culverts with the culvert headwater at the elevation of the north edge of the roadway pavement.

Specific developed runoff quantities for the site were determined using the Rational Method and are discussed further in section 5.0 of this report.

Peak Discharges at Points of Interest of Falcon Marketplace

| | Future Cor Marketplace De | | | _ | _ | | | |
|--|------------------------------|---------|------|------|--------|-----------|-------|--------|
| Location | HEC-HMS | Area | | | Peak F | low (cfs) | | |
| | Element | (sq mi) | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| West branch at North Property Line of Falcon Marketplace | RMT062 | 0.29 | 5 | 21 | 34 | 64 | 81 | 99 |
| East branch at North Property Line of Falcon Marketplace | RMT064 | 0.67 | 121 | 273 | 373 | 591 | 712 | 847 |
| Local Basin | MT060 | 0.19 | 30 | 59 | 83 | 137 | 167 | 199 |
| Sub Regional Pond SR4 Inflow | - | 1.16 | 133 | 310 | 431 | 697 | 847 | 1016 |
| Sub Regional Pond SR4 Outflow | JMT060 | 1.16 | 12 | 52 | 106 | 338 | 481 | 644 |
| Local Basin (Falcon Marketplace) | MT070 | 0.20 | 30 | 57 | 79 | 129 | 157 | 186 |
| E. Woodmen Road, South Property Line of Falcon Marketplace | JMT070 | 1.36 | 32 | 62 | 119 | 398 | 562 | 757 |

Per the above table, the 100-year discharge at the south property line is 757-cfs, which is less than the capacity of the existing culverts (765-cfs), and also less than the maximum allowable 100-year discharge (760-cfs) identified by the DBPS.

5.0 UPSTREAM DRAINAGE DIVERSIONS

During the drainage analysis for this Falcon Marketplace project, it came to light that upstream drainage diversions had taken place as part of the Bent Grass subdivision to the north. These diversions were not studied as part of this report, but will need to be addressed with any further development upstream.

6.0 EXISTING CONDITION HYDROLOGY SUMMARY

In addition to the DBPS, in order to confirm the "local basin (Falcon Marketplace)" flows listed above, a site specific analysis of the existing conditions was completed.

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| 5 |

| | ا. | | | | | | | | | | |
|-----------------|----------|------------------------------|------------------------|--------------|-----------|-------|-------|---------|---|--------------------|-----------------|
| Total Runoff | Vel | Vel | Vel Vel Hd Dn Hd Up | Vel Hd Up | vel Up | Cover | Cover | Storage | | | |
| (cfs) | (ft/s) | (ft/s) | (£ | £) | (tt/s) | (£ | (£ | (cft) | | | |
| 00.00 | 9. 9. | 5.90 | 45.0 | 0.24 | 3.92 | 500 | 1.92 | 559.85 | | | |
| Project F | File: P3 | Project File: P3-OUT-STM.stm | d.stm | | | | | | | Number of lines: 1 | Date: 7/18/2019 |
| NOTES: | * Critic | NOTES: ** Critical depth | | | | | | | 1 | | |
| | | | | | | | | | | | |

Storm Sewers

Inlet Summary (see figures 8-7, 8-10 & 8-11)

| | | | F | low | Сар | acity |
|-------|------------|----------|----------|------------|----------|------------|
| Inlet | Туре | | Q5 (cfs) | Q100 (cfs) | Q5 (cfs) | Q100 (cfs) |
| IA1 | 10' Type R | sump | 3.4 | 7.7 | | |
| IB1 | 10' Type R | at-grade | 2.8 | 5.1 | 8.0 | 14.0 |
| IB2 | 10' Type R | at-grade | 2.0 | 3.7 | 8.0 | 14.0 |
| IB3 | 10' Type R | at-grade | 1.4 | 2.5 | 8.0 | 14.0 |
| IB4 | 10' Type R | at-grade | 0.8 | 1.4 | 8.0 | 14.0 |
| IB5 | 10' Type R | sump | 0.8 | 1.5 | 10.5 | 10.5 |
| IB6 | 10' Type R | sump | 0.9 | 1.6 | 10.5 | 10.5 |
| IB7 | 5' Type R | at-grade | 1.6 | 2.9 | 4.0 | 6.5 |
| IB8 | 10' Type R | sump | 1.6 | 2.9 | 10.5 | 10.5 |
| IB9 | 10' Type R | sump | 1.5 | 2.7 | 10.5 | 10.5 |
| IC1 | 5' Type R | sump | 1.3 | 2.6 | 6.5 | 6.5 |
| IC3 | 5' Type R | sump | 0.8 | 1.5 | 6.5 | 6.5 |

Inlets Chapter 8

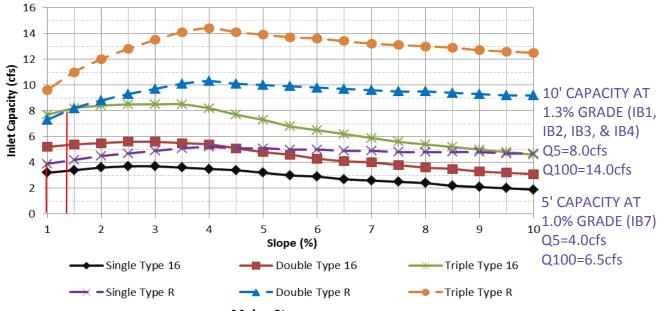
Figure 8-7. Inlet Capacity Chart Continuous Grade Conditions, Residential (Local) (Attached and Detached Sidewalk)

Street Section Data: Street Width Flowline to Flowline = 34'

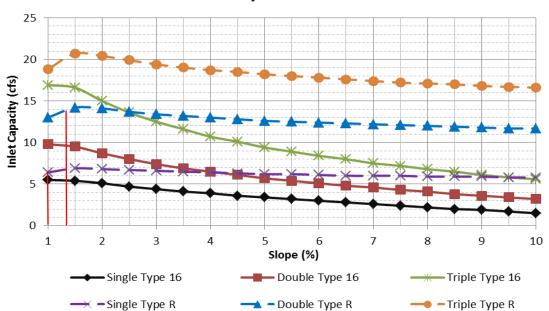
Type of Curb and Gutter: D-10-R = 8" vertical

Type 16 = 6" vertical

Minor Storm

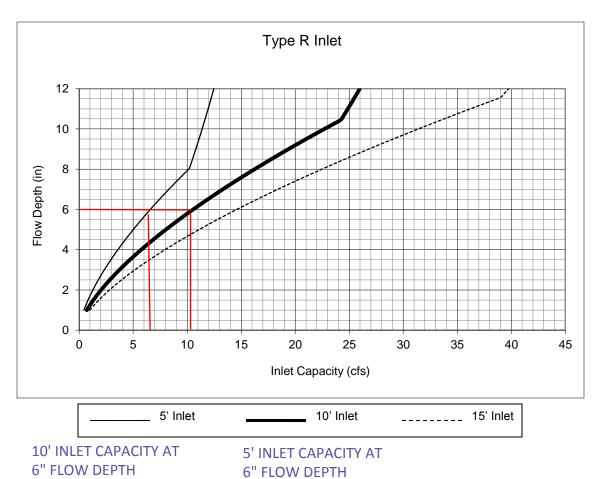


Major Storm



The standard street section parameters as defined in Chapter 7 must apply to use these charts. For non-standard sections, the inlet capacity shall be calculated using the UDFCD spreadsheets. The maximum spread width is limited by the curb height based on no curb overtopping during a minor storm and flow being contained within the public right-of-way during the major storm. Calculations were done using UD-Inlet 3.00.xls, Mar., 2011 with the default clogging factors.

Inlets Chapter 8



(IC1 & IC3)

Q=6.5cfs

Figure 8-11. Inlet Capacity Chart Sump Conditions , Curb Opening (Type R) Inlet

Notes:

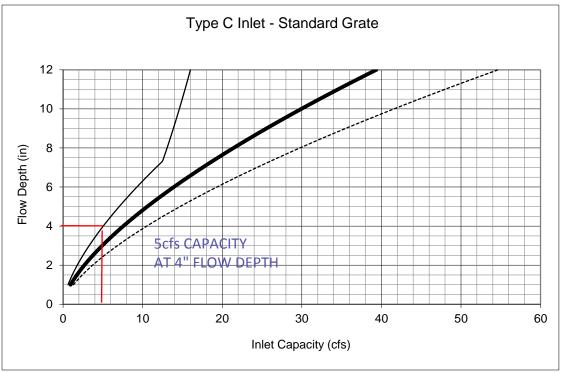
1. The standard inlet parameters must apply to use this chart.

(IB5, IB6, IB8 & IB9)

Q=10.5cfs

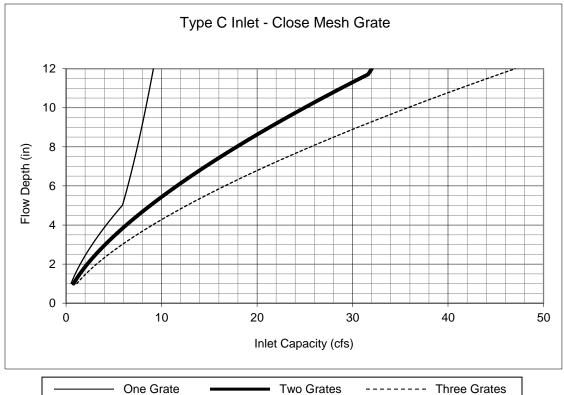
Chapter 8 Inlets

Figure 8-10. Inlet Capacity Chart Sump Conditions, Area (Type C) Inlet



INLET IA2 Q5=0.0cfs Q100= 0.2cfs

INLET IC2 Q5=0.0cfs Q100=0.3cfs



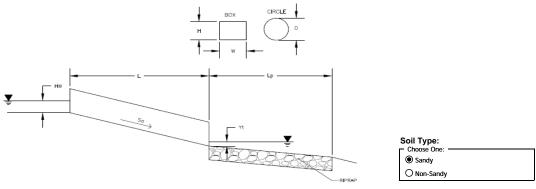
Notes:

1. The standard inlet parameters must apply to use these charts.

Determination of Culvert Headwater and Outlet Protection

Project: Falcon Marketplace

Basin ID: DP27

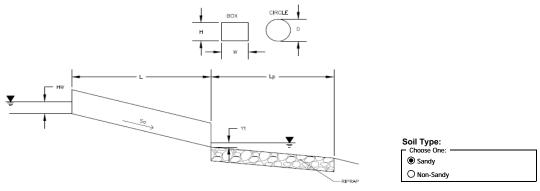


Supercritical Flow! Using Da to calculate protection type Design Information (Input): Q = 1.9 cfs Design Discharge Circular Culvert: Barrel Diameter in Inches D= inches Inlet Edge Type (Choose from pull-down list) Square End with Headwall Box Culvert: OR Barrel Height (Rise) in Feet Height (Rise) = Barrel Width (Span) in Feet Width (Span) = Inlet Edge Type (Choose from pull-down list) Number of Barrels No = Inlet Elevation Elev IN : Outlet Elevation ${\color{red} {\bf OR}}$ Slope Elev OUT = 6885 Culvert Length 24 L= Manning's Roughness n: 0.012 Bend Loss Coefficient 0 k_b = k_x = Exit Loss Coefficient 1 Elev Y, = Tailwater Surface Elevation Max Allowable Channel Velocity ft/s Required Protection (Output): Tailwater Surface Height 0.60 Flow Area at Max Channel Velocity A, 0.38 ft² Culvert Cross Sectional Area Available 1 77 Entrance Loss Coefficient k_e 0.50 Friction Loss Coefficient 0.37 Sum of All Losses Coefficients 1.87 **Culvert Normal Depth** $Y_{n} \\$ 0.34 **Culvert Critical Depth** Y_c : 0.52 Tailwater Depth for Design d = 1.01 D_a 0.92 Adjusted Diameter OR Adjusted Rise Expansion Factor 1/(2*tan(Θ)) 6.70 ft^{0.5}/s $\label{eq:flow_decomposition} Flow/Diameter^{2.5}\,\underline{\textbf{OR}}\;Flow/(Span\;\star\;Rise^{1.5})$ Q/D^2.5 = 0.69 Froude Number Fr 2.22 Supercritical! Tailwater/Adjusted Diameter OR Tailwater/Adjusted Rise 0.65 Yt/D = Inlet Control Headwater HW_I : 0.71 HW_{O} 0.54 Outlet Control Headwater **Design Headwater Elevation** HW 6,886.21 Headwater/Diameter OR Headwater/Rise Ratio HW/D 0.47 d₅₀ Minimum Theoretical Riprap Size Nominal Riprap Size $d_{50} \\$ **UDFCD Riprap Type** Type ٧L Length of Protection 5 Width of Protection

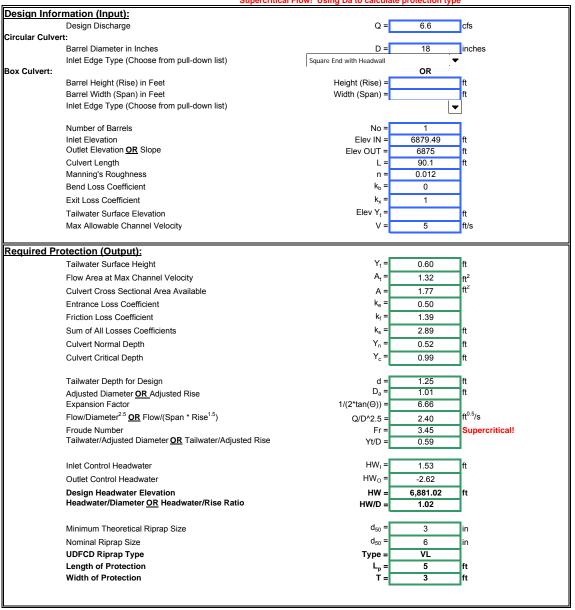
Determination of Culvert Headwater and Outlet Protection

Project: Falcon Marketplace

Basin ID: DP30



Supercritical Flow! Using Da to calculate protection type



DETENTION VOLUME BY THE FULL SPECTRUM METHOD

| Project: | |
|-----------|--|
| Basin ID: | |

| _ | | |
|---|--------------------|--------------|
| Area of Watershed (acres) | 740.00 | |
| Subwatershed Imperviousness | 15.0% | |
| Level of Minimizing Directly Connected Impervious Area (MDCIA) | 0 | 0 |
| Effective Imperviousness ¹ | 15.0% | |
| Hydrologic Soil Type | Percentage of Area | Area (acres) |
| Type A | 100.0% | 740.0 |
| Type B | | 0.0 |

Type C or D

| Recommended | Horton's Equation Paran | neters for CUHP |
|-----------------------|-------------------------|-----------------|
| Infiltration (inc | ches per hour) | Decay |
| Initialf _i | Finalfo | Coefficientα |
| 5 | 1.0 | 0.0007 |

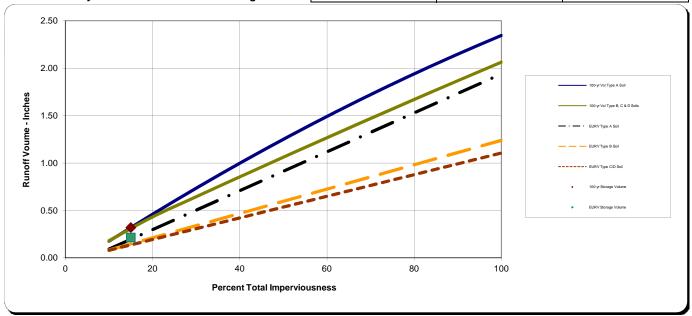
0.0

* User input data shown in blue.

| Detention \ | /olumes ^{2,5} | |
|--------------------|------------------------|--|
| (watershed inches) | (acre-feet) | Maximum Allowable Release Rate, cfs ³ |
| 0.22 | 13.30 | Design Oulet to Empty EURV in 72 Hours |
| 0.32 | 19.72 | 370.00 |

Excess Urban Runoff Volume⁴

100-year Detention Volume Including WQCV 5

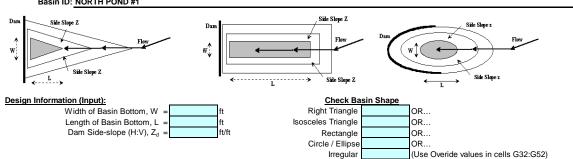


Notes:

- 1) Effective imperviousness is based on Figure ND-1 of the Urban Storm Drainage Criteria Manual (USDCM).
- 2) Results shown reflect runoff reduction from Level 1 or 2 MDCIA and are plotted at the watershed's total imperviousness value; the impact of MDCIA is reflected by the results being below the curves.
- 3) Maximum allowable release rates for 100-year event are based on Table SO-1. Outlet for the Excess Urban Runoff Volume (EURV) to be designed to empty out the EURV in 72 hours. Outlet design is similar to one for the WQCV outlet of an extended detention basin (i.e., perforated plate with a micro-pool) and extends to top of EURV water surface elevation.
- 4) EURV approximates the difference between developed and pre-developed runoff volume.
- 5) 100-yr detention volume includes EURV. No need to add more volume for WQCV or EURV

STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: FALCON MARKETPLACE Basin ID: NORTH POND #1



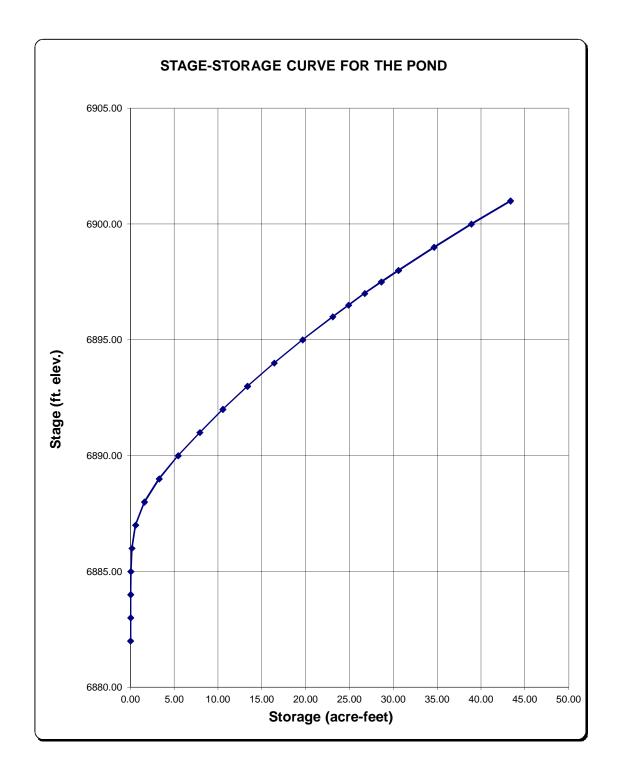
Stage-Storage Relationship:

| | MINACK | MAJOK | |
|---|--------|-------|----------|
| Storage Requirement from Sheet 'Modified FAA': | | | acre-ft. |
| Storage Requirement from Sheet 'Hydrograph': | | | acre-ft. |
| Storage Requirement from Sheet 'Full-Spectrum': | 13.30 | 19.72 | acre-ft. |

| Labels | Water | Side | Basin | Basin | Surface | Surface | Volume | Surface | Volume | Target Volumes |
|------------------|-----------|-----------|----------|-----------|-----------------|----------------------|-----------------|----------|----------|------------------|
| for WQCV, Minor, | Surface | Slope | Width at | Length at | Area at | Area at | Below | Area at | Below | for WQCV, Minor, |
| & Major Storage | Elevation | (H:V) | Stage | Stage | Stage | Stage | Stage | Stage | Stage | & Major Storage |
| Stages | ft | ft/ft | ft | ft | ft ² | ft ² User | ft ³ | acres | acre-ft | Volumes |
| (input) | (input) | Below El. | (output) | (output) | (output) | Overide | (output) | (output) | (output) | (for goal seek) |
| | 6882.00 | (input) | | | | 531 | | 0.012 | 0.000 | |
| | 6883.00 | | 0.00 | 0.00 | | 531 | 531 | 0.012 | 0.012 | |
| | 6884.00 | | 0.00 | 0.00 | | 531 | 1,062 | 0.012 | 0.024 | |
| | 6885.00 | | 0.00 | 0.00 | | 886 | 1,771 | 0.020 | 0.041 | |
| | 6886.00 | | 0.00 | 0.00 | | 9,189 | 6,808 | 0.211 | 0.156 | |
| | 6887.00 | | 0.00 | 0.00 | | 27,880 | 25,343 | 0.640 | 0.582 | |
| | 6888.00 | | 0.00 | 0.00 | | 60,263 | 69,414 | 1.383 | 1.594 | |
| | 6889.00 | | 0.00 | 0.00 | | 85,329 | 142,210 | 1.959 | 3.265 | |
| | 6890.00 | | 0.00 | 0.00 | | 103,874 | 236,812 | 2.385 | 5.436 | |
| | 6891.00 | | 0.00 | 0.00 | | 111,922 | 344,710 | 2.569 | 7.913 | |
| | 6892.00 | | 0.00 | 0.00 | | 116,616 | 458,979 | 2.677 | 10.537 | |
| WQCV | 6893.00 | | 0.00 | 0.00 | | 128,472 | 581,523 | 2.949 | 13.350 | |
| | 6894.00 | | 0.00 | 0.00 | | 136,926 | 714,222 | 3.143 | 16.396 | |
| | 6895.00 | | 0.00 | 0.00 | | 145,498 | 855,434 | 3.340 | 19.638 | |
| | 6896.00 | | 0.00 | 0.00 | | 154,188 | 1,005,277 | 3.540 | 23.078 | |
| | 6896.50 | | 0.00 | 0.00 | | 158,590 | 1,083,471 | 3.641 | 24.873 | |
| 100-YR | 6897.00 | | 0.00 | 0.00 | | 162,992 | 1,163,867 | 3.742 | 26.719 | |
| | 6897.50 | | 0.00 | 0.00 | | 167,639 | 1,246,524 | 3.848 | 28.616 | |
| | 6898.00 | | 0.00 | 0.00 | | 172,286 | 1,331,506 | 3.955 | 30.567 | |
| | 6899.00 | | 0.00 | 0.00 | | 181,155 | 1,508,226 | 4.159 | 34.624 | |
| | 6900.00 | | 0.00 | 0.00 | | 190,124 | 1,693,866 | 4.365 | 38.886 | |
| | 6901.00 | | 0.00 | 0.00 | | 199,194 | 1,888,525 | 4.573 | 43.355 | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |
| | | | | | | | #N/A | | #N/A | |

STAGE-STORAGE SIZING FOR DETENTION BASINS

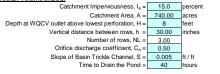
Project:
Basin ID:

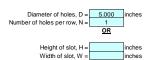


STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Project: FALCON MARKETPLACE Basin ID: NORTH POND #1

WQCV Design Volume (Input):





Watershed Design Information (Input):

Percent Soil Type A = 100 %
Percent Soil Type B = %
Percent Soil Type C/D = %



Perforated Plate Examples

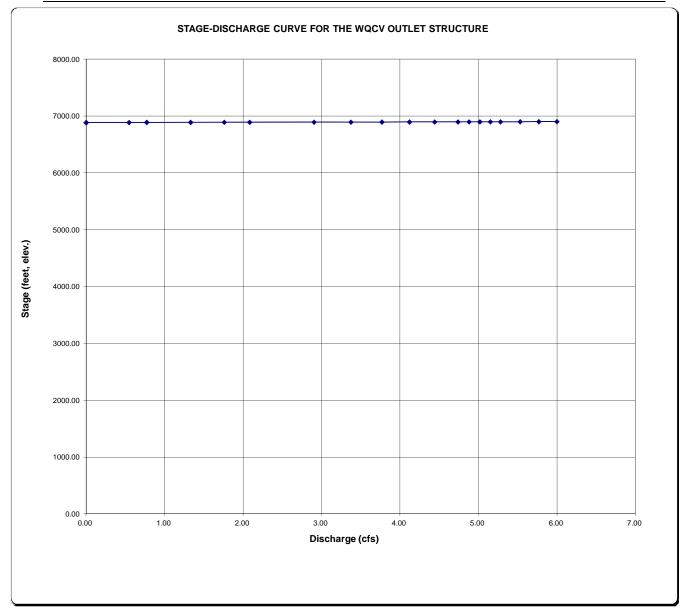
Outlet Design Information (Output):

| Excess Urban Runoff Volume (From 'Full-Spectrum Sheet') | 0.216 | watershed inch |
|---|--------|----------------|
| | N/A | |
| xcess Urban Runoff Volume (From 'Full-Spectrum Sheet') | 13.300 | acre-feet |
| Outlet area per row, Ao = _ | 69.21 | square inches |
| otal opening area at each row based on user-input above, Ao = | 19.63 | square inches |
| otal opening area at each row based on user-input above. Ao = | 0.136 | square feet |

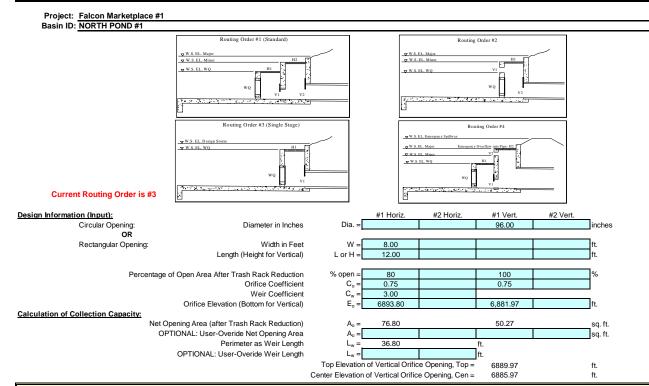
| | | | | | | | | | | | Central E | levations of | Rows of Ho | les in feet | | | | | | | | | | |] |
|----|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--------------|--------------|------------|---------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----|
| | Row 1 | Row 2 | Row 3 | Row 4 | Row 5 | Row 6 | Row 7 | Row 8 | Row 9 | Row 10 | Row 11 | Row 12 | Row 13 | Row 14 | Row 15 | Row 16 | Row 17 | Row 18 | Row 19 | Row 20 | Row 21 | Row 22 | Row 23 | Row 23 | |
| | 6885.00 | 6887.50 | 6890.00 | | | | | | | | <u> </u> | | | l | | | | | | | | | | | ı |
| | | | | | | | | | | | Collection C | apacity for | Each Row o | f Holes in cf | s | | | | | | | | | | |
| | 0.0000 | 0.0000 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | - 1 |
| | 0.0000 | 0.0000 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | - |
| | 0.0000 | 0.0000 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | 1 |
| | 0.0000 | 0.0000 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | |
| | 0.5457 | 0.0000 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | |
| | 0.7717 | 0.0000 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | |
| | 0.9452 | 0.3859 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.0914 | 0.6683 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.2202 | 0.8628 | 0.0000 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.3367 | 1.0209 | 0.5457 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.4438 | 1.1576 | 0.7717 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.5435 | 1.2798 | 0.9452 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.6371 | 1.3913 | 1.0914 | | | | | | | | | | | | | | | | | | | | | | |
| | 1.7256 | 1.4945 | 1.2202 | | | | | | | | | | | | | | | | | | | | | | |
| 00 | 1.8099 | 1.5910 | 1.3367 | | | | | | | | | | | | | | | | | | | | | | |
| 50 | 1.8505 | 1.6371 | 1.3913 | | | | | | | | | | | | | | | | | | | | | | |
| 00 | 1.8904 | 1.6820 | 1.4438 | | | | | | | | | | | | | | | | | | | | | | |
| 0 | 1.9293 | 1.7256 | 1.4945 | | | | | | | | | | | | | | | | | | | | | | |
| 0 | 1.9675 | 1.7683 | 1.5435 | | | | | | | | | | | | | | | | | | | | | | |
| 00 | 2.0418 | 1.8505 | 1.6371 | | | | | | | | | | | | | | | | | | | | | | |
| 00 | 2.1135 | 1.9293 | 1.7256 | | | | | | | | | | | | | | | | | | | | | | |
| 00 | 2.1828 | 2.0050 | 1.8099 | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | - |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | 1 | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | 1 | | | | | | | | | | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | 1 | | | | | | | | |
| | #N/A | #N/A | #N/A | | | | | | | | | | | | | | | | | | | | | | |
| | Override | Override | Override | Override | Override | Override | Override | Override | Override | Override | Override | Override | Override | Override | |
| | Area | Area | Area | Area | Area | Area | Area | Area | Area | Area | Area | Area | Area | Area | 1 |
| | Row 1 | Row 2 | Row 3 | Row 4 | Row 5 | Row 6 | Row 7 | Row 8 | Row 9 | Row 10 | Row 11 | Row 12 | Row 13 | Row 14 | Row 15 | Row 16 | Row 17 | Row 18 | Row 19 | Row 20 | Row 21 | Row 22 | Row 23 | Row 24 | 1 |
| | 0.44 | 0.14 | 0.14 | 11011 | | | | | | | | 71011 12 | | / | | | 110001 | | | | | | | | |

FM Pond #1rev (w6897.0) -KV.xls, WQCV

Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1



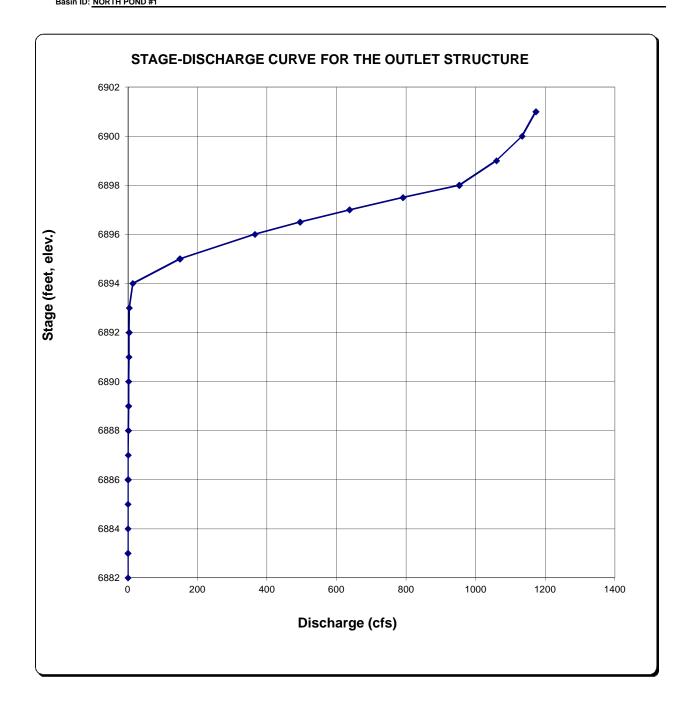
STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)



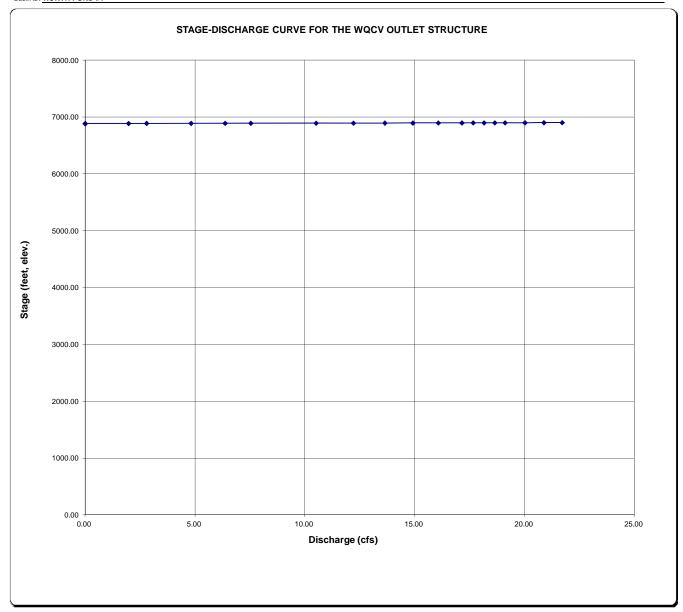
Routing 3: Single Stage - Water flows through WQCV plate and #1 horizontal opening into #1 vertical opening. This flow will be applied to culvert sheet (#2 vertical & horizontal openings is not used).

| | | | Horizontal Orifi | ces | | | Vertical Orifices | 5 | | |
|------------------|-----------|---------------|------------------|--------------|--------------|--------------|-------------------|------------|--------------|----------------------|
| Labels | Water | WQCV | #1 Horiz. | #1 Horiz. | #2 Horiz. | #2 Horiz. | #1 Vert. | #2 Vert. | Total | Target Volumes |
| for WQCV, Minor, | Surface | Plate/Riser | Weir | Orifice | Weir | Orifice | Collection | Collection | Collection | for WQCV, Minor, |
| & Major Storage | Elevation | Flow | Flow | Flow | Flow | Flow | Capacity | Capacity | Capacity | & Major Storage |
| W.S. Elevations | ft | cfs | cfs | cfs | cfs | cfs | cfs | cfs | cfs | Volumes |
| (input) | (linked) | (User-linked) | (output) | (output) | (output) | (output) | (output) | (output) | (output) | (link for goal seek) |
| (,) | 6882.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | 0.00 | 0.00 | (|
| | 6883.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 27.95 | 0.00 | 0.00 | |
| | 6884.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 77.34 | 0.00 | 0.00 | |
| | 6885.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 141.04 | 0.00 | 0.00 | |
| | 6886.00 | 0.55 | 0.00 | | | 0.00 | 216.33 | 0.00 | 0.55 | |
| | | 0.55 | 0.00 | 0.00 | 0.00 | | 1 | | 0.55 | |
| | 6887.00 | | | 0.00 | | 0.00 | 301.66 | 0.00 | | |
| | 6888.00 | 1.33 | 0.00 | 0.00 | 0.00 | 0.00 | 395.95 | 0.00 | 1.33 | |
| | 6889.00 | 1.76 | 0.00 | 0.00 | 0.00 | 0.00 | 498.43 | 0.00 | 1.76 | |
| | 6890.00 | 2.08 | 0.00 | 0.00 | 0.00 | 0.00 | 607.33 | 0.00 | 2.08 | |
| | 6891.00 | 2.90 | 0.00 | 0.00 | 0.00 | 0.00 | 678.51 | 0.00 | 2.90 | |
| | 6892.00 | 3.37 | 0.00 | 0.00 | 0.00 | 0.00 | 742.90 | 0.00 | 3.37 | |
| WQCV | 6893.00 | 3.77 | 0.00 | 0.00 | 0.00 | 0.00 | 802.14 | 0.00 | 3.77 | |
| | 6894.00 | 4.12 | 9.87 | 206.72 | 0.00 | 0.00 | 857.30 | 0.00 | 13.99 | |
| | 6895.00 | 4.44 | 145.12 | 506.36 | 0.00 | 0.00 | 909.11 | 0.00 | 149.56 | |
| | 6896.00 | 4.74 | 360.25 | 685.61 | 0.00 | 0.00 | 958.13 | 0.00 | 364.99 | |
| | 6896.50 | 4.88 | 489.80 | 759.53 | 0.00 | 0.00 | 981.72 | 0.00 | 494.67 | |
| 100-YR | 6897.00 | 5.02 | 631.97 | 826.88 | 0.00 | 0.00 | 1004.76 | 0.00 | 636.98 | |
| | 6897.50 | 5.15 | 785.73 | 889.13 | 0.00 | 0.00 | 1027.28 | 0.00 | 790.88 | |
| | 6898.00 | 5.28 | 950.26 | 947.31 | 0.00 | 0.00 | 1049.32 | 0.00 | 952.58 | |
| | 6899.00 | 5.53 | 1309.10 | 1054.06 | 0.00 | 0.00 | 1092.06 | 0.00 | 1059.59 | |
| | 6900.00 | 5.77 | 1704.34 | 1150.96 | 0.00 | 0.00 | 1133.19 | 0.00 | 1133.19 | |
| | 6901.00 | 6.00 | 2132.89 | 1240.31 | 0.00 | 0.00 | 1172.88 | 0.00 | 1172.88 | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A #N/A | #N/A #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | 0.00 | #N/A #N/A | |
| | | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A | 0.00 | #N/A #N/A | |
| | | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A | 0.00 | #N/A #N/A | |
| | | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A #N/A | #N/A | 0.00 | #N/A #N/A | + |
| | | #N/A | #N/A #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | - |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |
| | | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A | 0.00 | #N/A | |

Project: Falcon Marketplace #1
Basin ID: NORTH POND #1



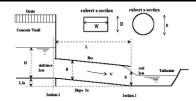
Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1



STAGE-DISCHARGE SIZING OF THE OUTLET CULVERT (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1

Status: Culvert Data is valid!



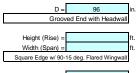
Design Information (Input):

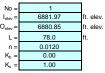
Circular Culvert: Barrel Diameter in Inches
Circular Culvert: Inlet Edge Type (choose from pull-down list)

OR:

Box Culvert: Barrel Height (Rise) in Feet
Box Culvert: Barrel Width (Span) in Feet
Box Culvert: Inlet Edge Type (choose from pull-down list)

Number of Barrels Inlet Elevation at Culvert Invert Outlet Elevation at Culvert Invert Culvert Length in Feet Manning's Roughness Bend Loss Coefficient Exit Loss Coefficient





Design Information (calculated):

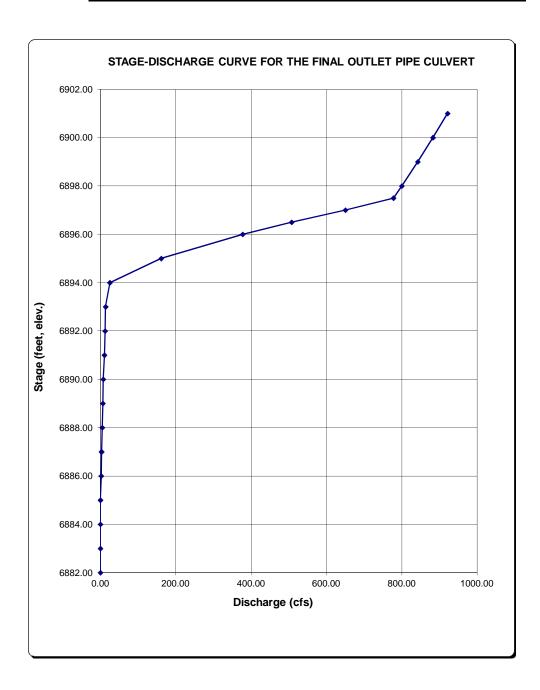
Entrance Loss Coefficient Friction Loss Coefficient Sum of All Loss Coefficients Orifice Inlet Condition Coefficient Minimum Energy Condition Coefficient

| K _e = | 0.20 |
|---------------------|-------|
| $K_f =$ | 0.13 |
| K _s = | 1.33 |
| C _d = | 0.99 |
| KE _{low} = | -0.04 |

Calculations of Culvert Capacity (output):

| Water Surface | Tailwater | Culvert | Culvert | Flowrate | Controlling | Inlet |
|---------------|------------------|---------------|----------------|---------------|-------------|----------------------|
| Elevation | Surface | Inlet-Control | Outlet-Control | Into Culvert | Culvert | Equation |
| From Sheet | Elevation | Flowrate | Flowrate | From Sheet | Flowrate | Used |
| "Basin" | ft | cfs | cfs | "Outlet" | cfs | |
| (ft., linked) | (input if known) | (output) | (output) | (cfs, linked) | (output) | (output) |
| 6882.00 | 0.00 | 0.10 | 73.88 | 0.00 | 0.00 | Min. Energy. Eqn. |
| 6883.00 | 0.00 | 8.20 | 127.58 | 0.00 | 0.00 | Min. Energy. Eqn. |
| 6884.00 | 0.00 | 38.80 | 179.44 | 0.00 | 0.00 | Min. Energy. Eqn. |
| 6885.00 | 0.00 | 83.70 | 227.39 | 0.00 | 0.00 | Min. Energy. Egn. |
| 6886.00 | 0.00 | 142.70 | 253.50 | 1.98 | 1.98 | Regression Eqn. |
| 6887.00 | 0.00 | 207.40 | 260.30 | 2.79 | 2.79 | Regression Eqn. |
| 6888.00 | 0.00 | 284.50 | 274.34 | 4.82 | 4.82 | Regression Eqn. |
| 6889.00 | 0.00 | 370.40 | 296.59 | 6.37 | 6.37 | Regression Eqn. |
| 6890.00 | 0.00 | 456.70 | 327.85 | 7.54 | 7.54 | Regression Eqn. |
| 6891.00 | 0.00 | 537.00 | 401.74 | 10.51 | 10.51 | Regression Eqn. |
| 6892.00 | 0.00 | 609.70 | 475.03 | 12.21 | 12.21 | Regression Eqn. |
| 6893.00 | 0.00 | 675.30 | 541.57 | 13.64 | 13.64 | Regression Eqn. |
| 6894.00 | 0.00 | 735.40 | 601.48 | 24.79 | 24.79 | Regression Eqn. |
| 6895.00 | 0.00 | 790.90 | 656.53 | 161.20 | 161.20 | Regression Eqn. |
| 6896.00 | 0.00 | 843.00 | 707.57 | 377.40 | 377.40 | Regression Eqn. |
| 6896.50 | 0.00 | 867.90 | 731.66 | 507.45 | 507.45 | Regression Eqn. |
| 6897.00 | 0.00 | 892.20 | 755.10 | 650.12 | 650.12 | Regression Eqn. |
| 6897.50 | 0.00 | 915.90 | 777.72 | 804.36 | 777.72 | Regression Eqn. |
| 6898.00 | 0.00 | 939.10 | 799.86 | 966.41 | 799.86 | Regression Eqn. |
| 6899.00 | 0.00 | 984.10 | 842.42 | 1074.08 | 842.42 | Regression Eqn. |
| 6900.00 | 0.00 | 1027.50 | 882.74 | 1133.19 | 882.74 | Regression Eqn. |
| 6901.00 | 0.00 | 1069.50 | 921.46 | 1172.88 | 921.46 | Regression Eqn. |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |
| 0.00 | 0.00 | 0.00 | 0.00 | #N/A | #N/A | No Flow (WS < inlet) |

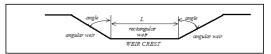
Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1



FM Pond #1rev (w6897.0) -KV.xls, Culvert 5/1/2017, 11:25 AM

STAGE-DISCHARGE SIZING OF THE SPILLWAY

Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1



Design Information (input):

Bottom Length of Weir Angle of Side Slope Weir Elev. for Weir Crest Coef. for Rectangular Weir Coef. for Trapezoidal Weir

160.00 feet L= Angle = 75.96 degrees EL. Crest = 6,898.00 feet $C_w =$ $C_t =$ 3.50

Calculation of Spillway Capacity (output):

| Г | Water | Rect. | Triangle | Total | Total |
|---|-----------|----------|----------|----------|----------|
| | Surface | Weir | Weir | Spillway | Pond |
| | Elevation | Flowrate | Flowrate | Release | Release |
| | ft. | cfs | cfs | cfs | cfs |
| | (linked) | (output) | (output) | (output) | (output) |
| | 6882.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 6883.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 6884.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 6885.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 6886.00 | 0.00 | 0.00 | 0.00 | 1.98 |
| | 6887.00 | 0.00 | 0.00 | 0.00 | 2.79 |
| | 6888.00 | 0.00 | 0.00 | 0.00 | 4.82 |
| | 6889.00 | 0.00 | 0.00 | 0.00 | 6.37 |
| | 6890.00 | 0.00 | 0.00 | 0.00 | 7.54 |
| | 6891.00 | 0.00 | 0.00 | 0.00 | 10.51 |
| | 6892.00 | 0.00 | 0.00 | 0.00 | 12.21 |
| | 6893.00 | 0.00 | 0.00 | 0.00 | 13.64 |
| | 6894.00 | 0.00 | 0.00 | 0.00 | 24.79 |
| | 6895.00 | 0.00 | 0.00 | 0.00 | 161.20 |
| | 6896.00 | 0.00 | 0.00 | 0.00 | 377.40 |
| | 6896.50 | 0.00 | 0.00 | 0.00 | 507.45 |
| | 6897.00 | 0.00 | 0.00 | 0.00 | 650.12 |
| | 6897.50 | 0.00 | 0.00 | 0.00 | 777.72 |
| | 6898.00 | 0.00 | 0.00 | 0.00 | 799.86 |
| | 6899.00 | 0.00 | 14.00 | 14.00 | 856.42 |
| | 6900.00 | 0.00 | 79.17 | 79.17 | 961.91 |
| | 6901.00 | 0.00 | 218.18 | 218.18 | 1,139.63 |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |
| L | #N/A | #N/A | #N/A | #N/A | #N/A |

PROJECT INFORMATION

PROJECT: Falcon Marketplace PROJECT NO: 20988-00CSCV

DESIGN BY: KGV REV. BY: TDM

AGENCY: EI Paso County REPORT TYPE: Preliminary DATE: 6/19/2017



 $Q=CL(H^{(2/3)})$

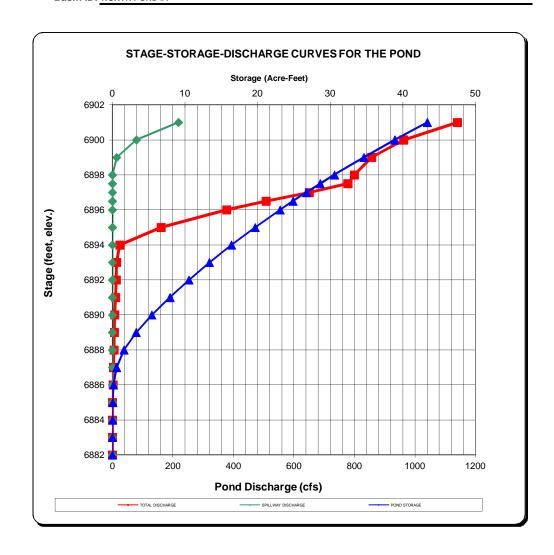
Weir coefficient C: 3.5
Depth H, ft: 1.5
Flowrate Q. cfs: 1016

Required L, ft: 158.01



STAGE-DISCHARGE SIZING OF THE SPILLWAY

Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1



Aluminum Bar Grating

TRASH RACK GRATE AT FRONT OF BOX

RECTANGULAR BAR SWAGE-LOCKED 1-3/16" C/C Bearing Bars

PRESS-LOCKED 1-3/16" C/C Bearing Bars









Cross Rods 4" C/C

Cross Rods 2" C/C

Cross Bars 4" C/C

Cross Bars 2" C/C

NON-SERRATED & SERRATED

LOAD & DEFLECTION TABLE

| Bar | Symbol | Approx. Weight | Sec. Mod Per R. | | SPAN | (Direc | tion of | | ng Bai | r) | | | | J = sate C = sate |
|--|-----------|-------------------|--|---|-------|--------------|---------------------|-------|--------------|--------------|--------------|-------|-------|----------------------|
| Size | | psi | O! Width | | 24" | District Co. | STATE OF THE PARTY. | 42" | | | | | D |) = defle |
| | 19-SR-4 | 1.4 | | U | 237 | 152 | 105 | 77 | | | | | E | = mod |
| 3/4" x 1/8" | 19-SR-2 | 1.6 | 0.118 | D | 0.192 | 0,300 | 0.432 | 0.588 | | | | | | = fiber |
| 3/4 X 1/0 | 19-AP-4 | 1,5 | 471 | C | 237 | 189 | 158 | 135 | | | | | | |
| market and a second of the sec | 19-AP-2 | 1.6 | and the second | D | 0.154 | 0.240 | 0.346 | 0.470 | | | | | | /laterial: |
| The state of | 19-SR-4 | 1.9 | The state of the | Ü | 355 | 227 | 158 | 116 | | | | | | ellectio |
| 3/4" x 3/16" | 19-SR-2 | 2.1 | 0.178 | D | 0.192 | 0.300 | 0.432 | 0.588 | | | | | | he bold l |
| OID VOLID | 19-AP-4 | 2.2 | News P | C | 355 | 284 | 237 | 203 | 48" | | | | | orm load |
| | 19-AP-2 | 2.7 | 7.5 | D | 0.154 | 0.240 | 0.346 | 0.470 | 100 | () | | | | edestria |
| | 19-\$A-4 | 1.7 | | ū | 421 | 269 | 187 | 137 | 105 | | | | | or other |
| 1" x 1/8" | 19-\$A-2 | 1.9 | 0.211 | D | 0.144 | 0.225 | 0.324 | 0.441 | 0.576 | | | | a | ipproval. |
| 1 X 1/0 | 19-AP-4 | 1.8 | | C | 421 | 337 | 281 | 241 | 211 | 54" | | | S | Serraled |
| Commence of the Commence of th | 19-AP-2 | 2.2 | ercla theory | D | 0.115 | 0.180 | 0.259 | 0.353 | 0.461 | 125 | | | 0 | of grating |
| A PART OF THE PART | 19-SR-4 | 2.5 | ASOMES! | Ū | 632 | 404 | 281 | 206 | 158 | | | | ď | leeper th |
| 1" x 3/16" | 19-SR-2 | 2.7 | 0.316 | D | 0.144 | 0.225 | 0.324 | 0.441 | 0.576 | 0.729 | | | | ieneral: |
| 1 A 0/10 | 19-AP-4 | 2.8 | | C | 632 | 505 | 421 | 361 | 316 | 281 0.583 | | | | al and b |
| | 19-AP-2 | 3.3 | | D | 0.115 | | 0.259 | 0.353 | 0.461 | | | | | Finish: A |
| | 19-SR-4 | 2.1 | | U | 658 | 421 | 292 | 215 | 164 | 130 | | | • | inisn: w |
| 1-1/4" x 1/8" | 19-SR-2 | 2.3 | 0.329 | D | 0.115 | 0.180 | 0.259 | 0.353 | 0.461 | 0.583 | | | | |
| 1-1/4 × 1/0 | 19-AP-4 | 2.4 | | Ç | 658 | 526 | 439 | 376 | 329 | 292 | 60" | | LA | 100 |
| | 19-AP-2 | 2.8 | THE PARTY OF THE P | D | 0.092 | 0.144 | 0.207 | 0.282 | 0.369 | 0.467 | 158 | | 1.0 | 1.CO |
| | (19-SR-4) | 3.1 | 10/20/00/0 | Ü | 987 | 632 | 439 | 322 | 247 0.461 | 0.583 | 0.720 | | 14 | |
| 1-1/4" x 3/16" | 19-SR-2 | 3.3 | 0.493 | D | 0.115 | 0.180 | 0.259 | 0.353 | | 439 | 395 | | 15 | 7-F7 |
| 1-1/4 X 0/10 | 19-AP-4 | 3.5 | 615867 | Ç | 987 | 789 | 658 | 564 | 493 | 0.467 | 0.576 | | 1 - | , , , , |
| THE RESTRICTED | 19-AP-2 | 4.2 | | D | 0.092 | 0.144 | 0.207 | 0.282 | 0.369 | 187 | 152 | | | |
| | 19-SR-4 | 2.5 | | U | 947 | 606 | 421 | 309 | 237 | | | | | |
| 1-1/2" x 1/8" | 19-SR-2 | 2.7 | 0.474 | D | 0.096 | 0.150 | 0.216 | 0.294 | 0.384 | 0.486 | 0.600 379 | | | |
| 1-1/E X 1/0 | 19-AP-4 | 2.8 | | C | 947 | 758 | 632 | 541 | 474 | 421 0.389 | | 66" | | |
| | 19-AP-2 | 3.2 | omet robin | D | 0.077 | 0.120 | 0.173 | 0.235 | 0.307 | | 0.480 | 188 | | |
| | 19-SR-4 | 3.7 | | Ŋ | 1421 | 909 | 632 | 464 | 355 | 281 | 0.600 | 0.726 | | |
| 1-1/2" x 3/16" | 19-SR-2 | 3.9 | 0.711 | D | 0.096 | 0.150 | 0.216 | 0.294 | 0.384 | 0.486 632 | 568 | 517 | | |
| 1-1/2 X 0/10 | 19-AP-4 | 4,1 | E CHANGE | Ç | 1421 | 1137 | 947 | 812 | 711 0.307 | 0.389 | 0.480 | 0.581 | 72" | 78" |
| | 19-AP-2 | 4.8 | 100 | 0 | 0.077 | 0.120 | 0.173 | 0.235 | | 382 | 309 | 256 | 215 | 183 |
| | 19-SR-4 | 4.2 | | Ū | 1934 | 1238 | 860 | 632 | 484 | | | 0.622 | 0.741 | 0.869 |
| 1-3/4" x 3/16" | 19-\$R-2 | 4.4 | 0.967 | D | 0.082 | 0.129 | 0.185 | 0.252 | 0.329 | 0.417. | 0.514 | 703 | 645 | 595 |
| 1-0/4 X 0/10 | 19-AP-4 | 4.7 | | C | 1934 | 1547 | 1289 | 1105 | 967 | 860 | 774 | | 0.592 | 0.695 |
| | 19-AP-2 | 5.3 | | D | 0.066 | 0.103 | 0.148 | 0.202 | 0.263 | | 0.411 | 0.498 | 281 | 239 |
| | 19-SR-4 | 4.8 | | U | 2526 | 1617 | 1123 | 825 | 632 | 499 | 404 | | 0.648 | 0.761 |
| 2" x 3/16" | 19-SR-2 | 5.0 | 1.263 | D | 0.072 | 0.113 | 0.162 | 0,221 | 0.288 | 0.365 | 0.450 | 0.545 | 842 | 777 |
| Z X 0/10 | 19-AP-4 | 5.3 | 035134 | C | 2526 | 2021 | 1684 | 1444 | 1263 | 1123 | 1011 | 919 | | 0.608 |
| | 19-AP-2 | 5.9 | STANCES. | D | 0.050 | 0.090 | 0.130 | 0.176 | 0.230 | 0.292 | 0.360 | 0.436 | 0.518 | 303 |
| 12 | 19-SR-4 | 5.4 | | Ū | 3197 | 2046 | 1421 | 1044 | 799 | 632 | 512 | 423 | 355 | |
| 2-1/4" x 3/16" | 19-SR-2 | 5.6 | 1.599 | D | 0.064 | 0.100 | 0.144 | 0.196 | 0.256 | | 0.400 | 0.484 | | 0.676 |
| 4-1/4 X 0/10 | 19-AP-4 | 5.8 | | C | 3197 | 2558 | 2132 | 1827 | 1599 | 1421 | 1279 | 1163 | 1066 | 984 |

U = sałe uniform load, psf (page 93)

C = sale concentrated load, psf (page 93)

D = deflection, inches

E = modulus of elasticity, 10,000,000 psi

F = fiber stress, 12,000 psi

206 0.882 722 0.706

261 0.784

914

322

0.627

1128

0.461 0.541

374

1215

0.608 0.706

439

1316

200

799

195

1.166

1.024

0.819

247 0.922

987

Material: ASTM B-221, 6063 or 6061

Deflection: Spans and loads to the right of the bold line exceed 1/4" deflection for uniform load of 100 psf which provides safe pedestrian comfort. These can be exceeded for other types of loads with engineer's approval.

Serrated Bars: For serrated grating, the depth of grating required for a specified load is 1/4" deeper than that shown in the table."

General: Loads and deflections are theoretical and based on static loading.

Finish: Mill finish unless otherwise specified.

FALCON MARKETPLACE
15-FT Head x 62-4 = 936 psf

| SR/AP-19 PA | MEL W | intu / | nahaa) | | | | | 1 | | | | | extended o | | |
|-------------|--------------------|--------|---------|---------|--------|--------------------|--------|---------|----------|-----------------|-----------|------------|------------------|---------------------|--------|
| No. of Bars | NEL W | 3 a | nches) | 5 | 6 | 7 | В | 9 | 10 | ed (SR) a 11 | nd extend | ed cross b | ars on pre 14 | ss-locked 15 | (AP). |
| 1/8" Bar | 19/16 | 23/4 | 315/16 | 51/6 | 65/16 | 71/2 | 811/16 | 97/8 | 111/16 | 121/4 | 137/16 | | 1513/16 | 17 | 183/16 |
| 3/16" Bar | 15/e | 213/16 | 4 | 53/16 | 63/8 | 79/16 | 83/4 | 915/16 | 111/8 | 125/16 | 131/2 | 1411/16 | 157/a | 17 ¹ /16 | 181/4 |
| No. of Bars | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 26 | 29 | 30 | 31 |
| 1/8" Bar | 19 ³ /e | 209/16 | 213/4 | 2215/16 | 241/8 | 255/16 | 261/2 | 2711/16 | $28^7/e$ | 301/16 | 311/4 | 327/16 | 335/8 | 3413/16 | 36 |
| 3/16" Bar | 197/16 | 205/6 | 2113/16 | 23 | 243/16 | 25 ³ /a | 269/16 | 273/4 | 2815/16 | 301/s | 315/16 | 321/2 | 3311/16 | 347/6 | 361/16 |

0.080

2526

0.090

3158

0.051

3947

0.058

0.115

0.130

2632

0.157

1289

0.176

2256

0.205

987

0.230

1974

0.259

0.292

1754

780

0.320

632

1579

0.072 0.104 0.141 0.184 0.233 0.288 0.348 0.415 0.487 0.564 0.737 0.933

0.387

522

0.360 0.436 0.518

1435

Ď

DOC

1,974

19-AP-2

19-SR-4

2-1/2" x 3/16"

6.5

5.9 6.1

6.4

Flow depths entering Pond SR4

CLOMR

Min Ch El 6895.98
WS Elev 6898.75
Max flow depth (north) **2.8** ft

NORTHWEST SWALE

Assuming trapezoidal channelized flow at riprap entry

| Q100 | 30.2 | cfs |
|-------------|-------|-----|
| Width | 8 | ft |
| Side Slopes | 5 | :1 |
| Slope | 1.6 | % |
| n | 0.020 | |

Calculated flow depth 0.5 ft

Project: Falcon Marketplace

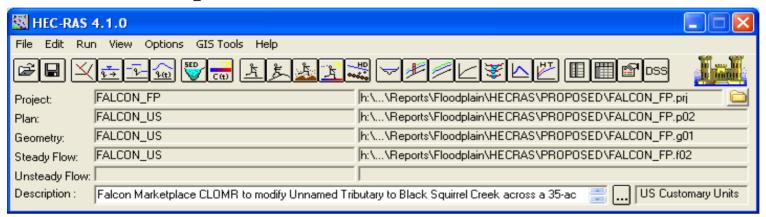
Project No.: 20988-00

HEC-RAS Data Output

Proposed Conditions Model, North (Drexel Barrell Model)

File: H:\20988-00CSCV\Reports\Floodplain\HECRAS\PROPOSED\FALCON_FP.prj

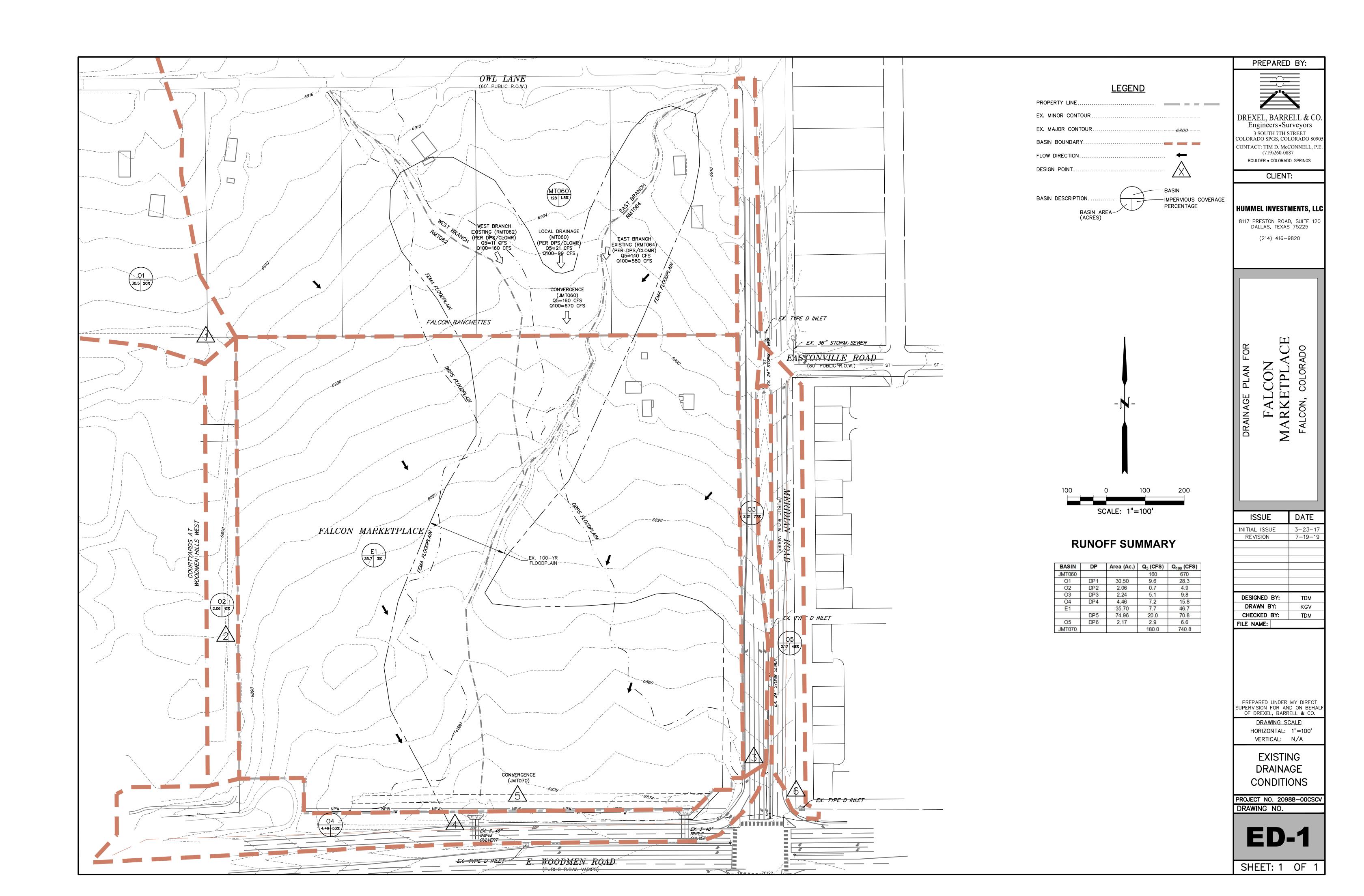
Plan: FALCON_US

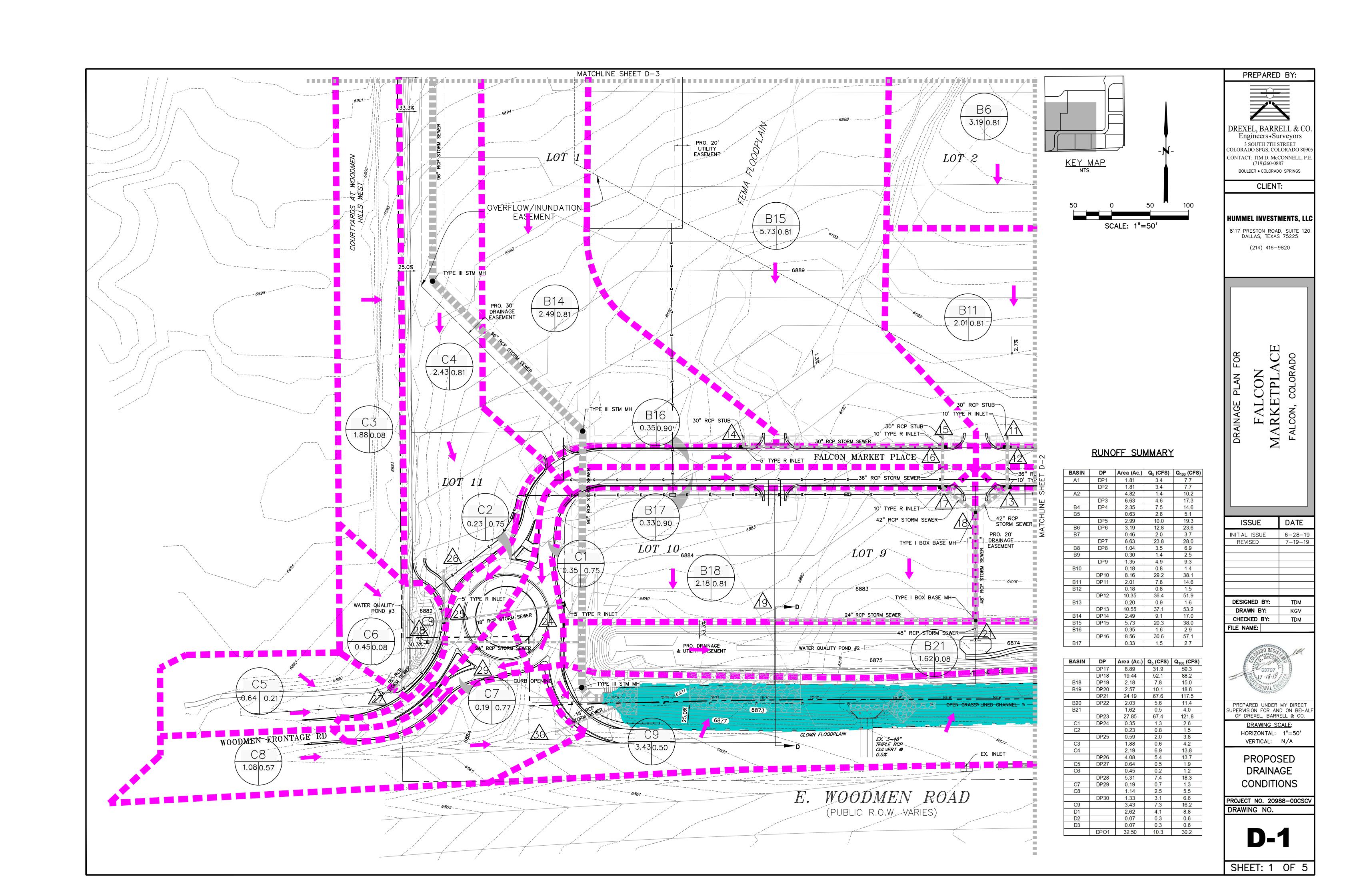


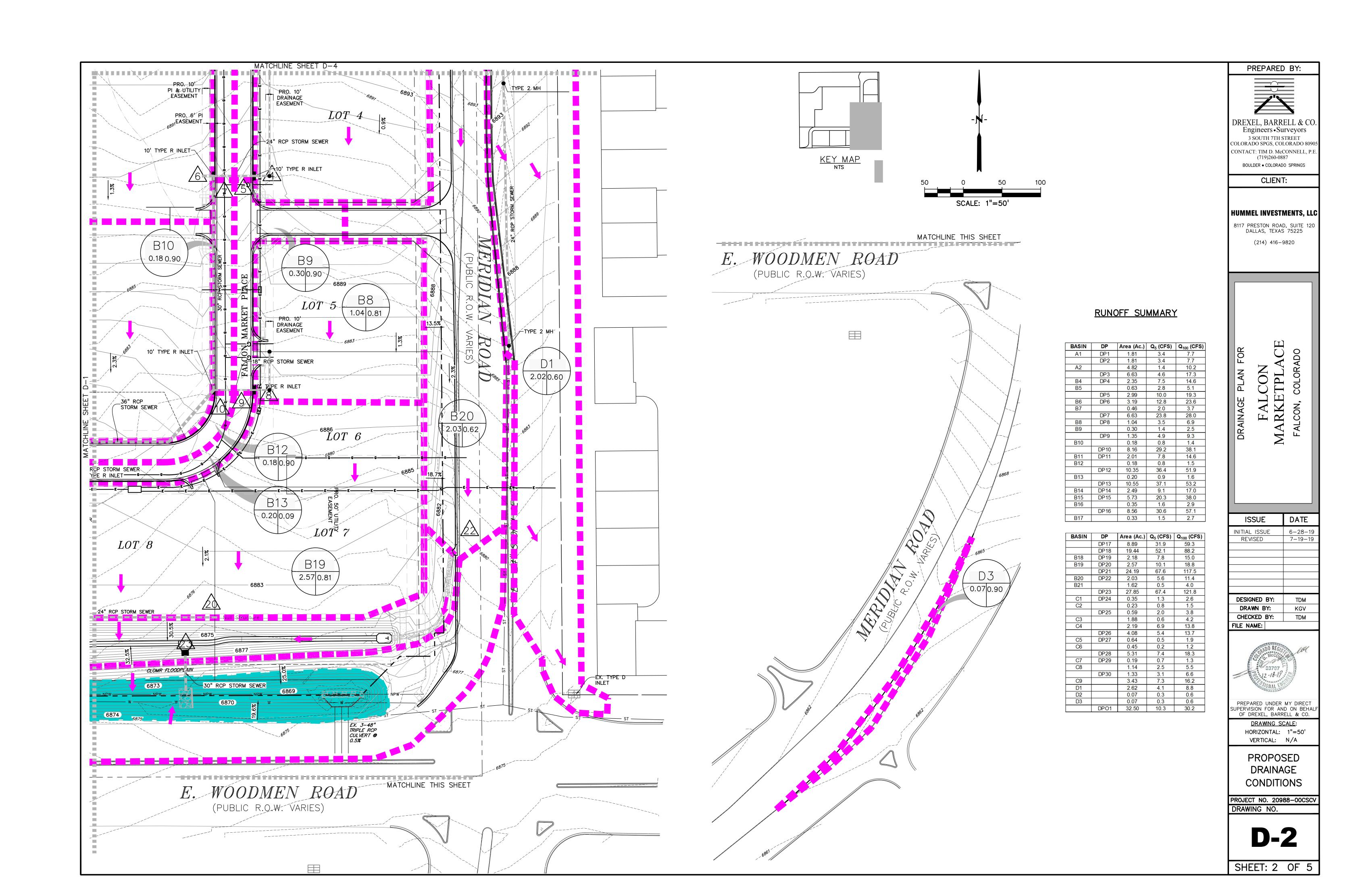
Date: 10/17/16 100-year Output, Standard Tabel 1 Cross Sections: 2926-2842

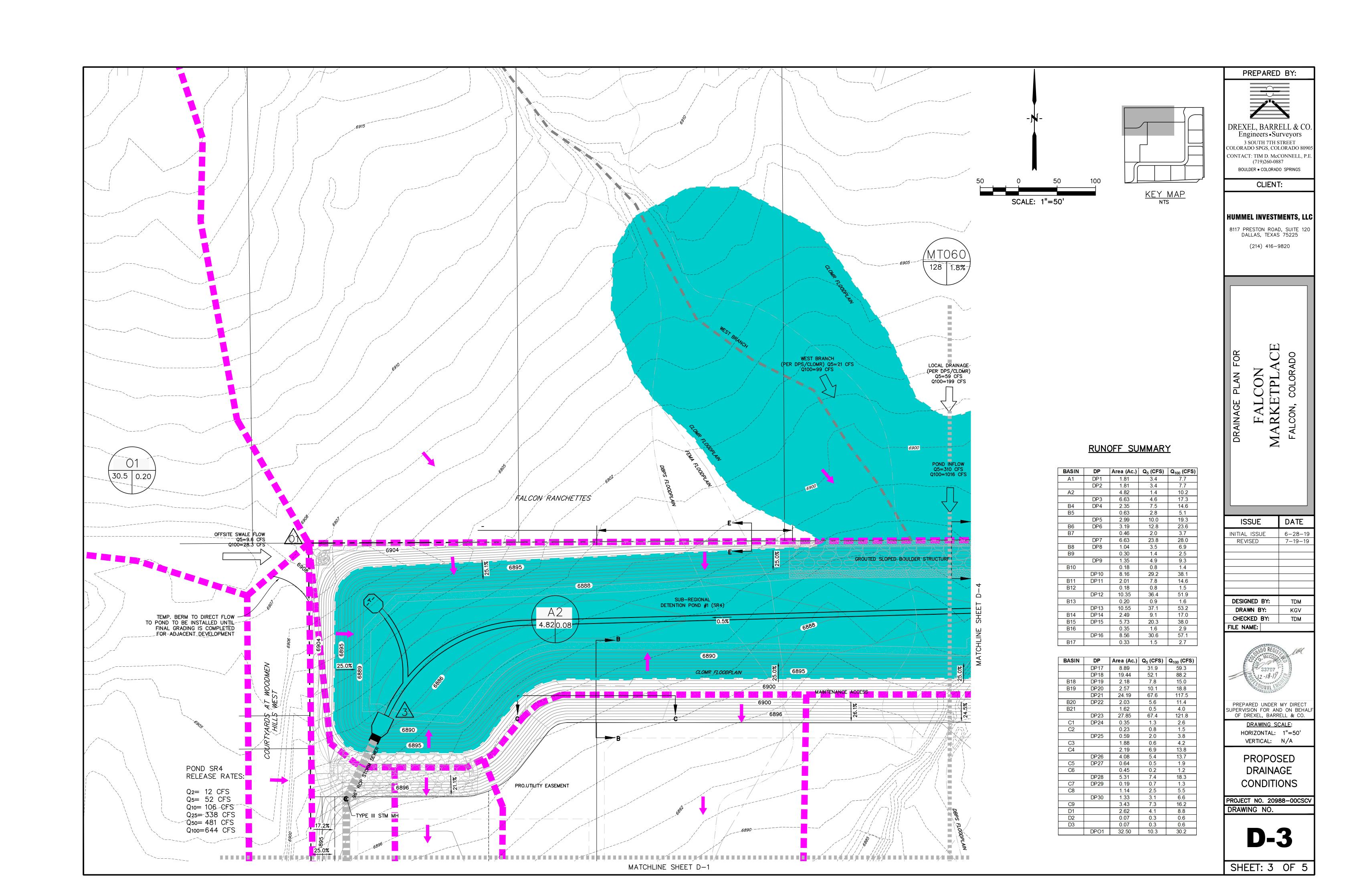
| | | | | | | | | | | | | Froude # |
|-----------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|----------|
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Chl |
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| FALCON_US | 2926 | 100-YR | 1016 | 6895.98 | 6898.75 | 6898.75 | 6899.12 | 0.025538 | 6.71 | 306.22 | 403.31 | 0.91 |
| FALCON US | 2842 | 100-YR | 1016 | 6888.58 | 6897 | 6889.37 | 6897 | 0.000001 | 0.15 | 6775.42 | 897.89 | 0.01 |

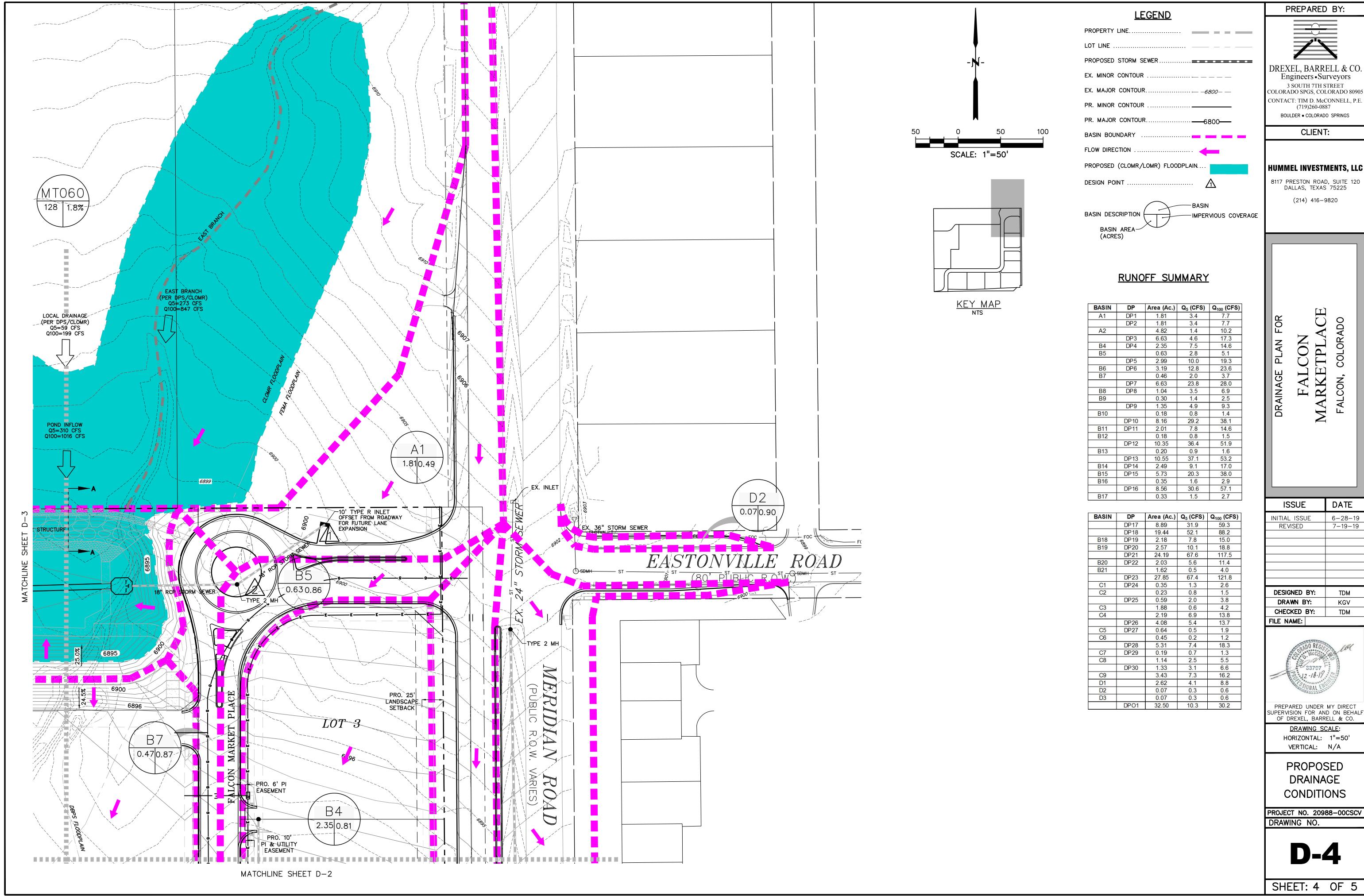












PREPARED BY:

DREXEL, BARRELL & CO. Engineers • Surveyors 3 SOUTH 7TH STREET COLORADO SPGS, COLORADO 80905 CONTACT: TIM D. McCONNELL, P.I

(719)260-0887 BOULDER • COLORADO SPRINGS

CLIENT:

8117 PRESTON ROAD, SUITE 120 DALLAS, TEXAS 75225

(214) 416-9820

FALCON 1ARKETPLACE COLORADO

DATE ISSUE INITIAL ISSUE 6-28-19 REVISED 7-19-19

DESIGNED BY: DRAWN BY: CHECKED BY: FILE NAME:



PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHAL OF DREXEL, BARRELL & CO.

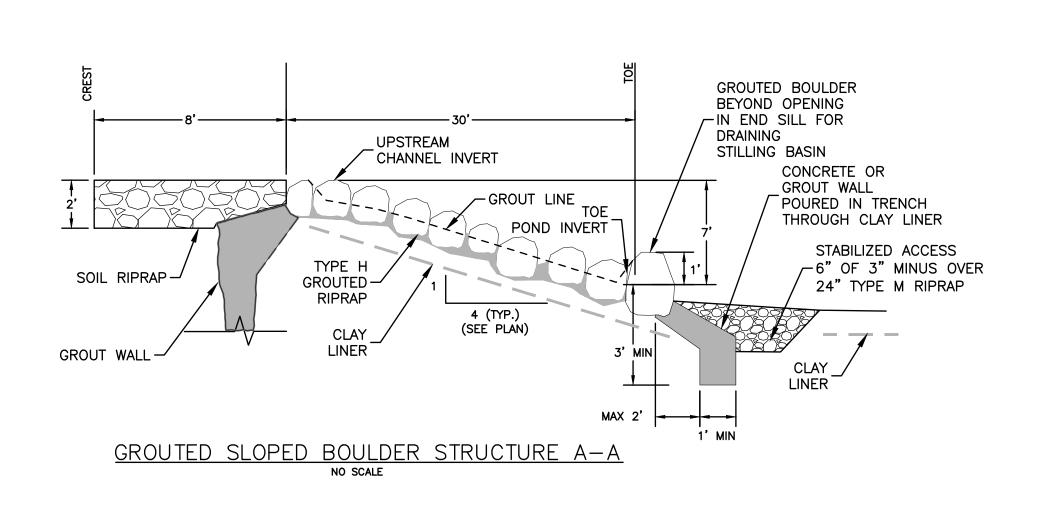
DRAWING SCALE: HORIZONTAL: 1"=50' VERTICAL: N/A

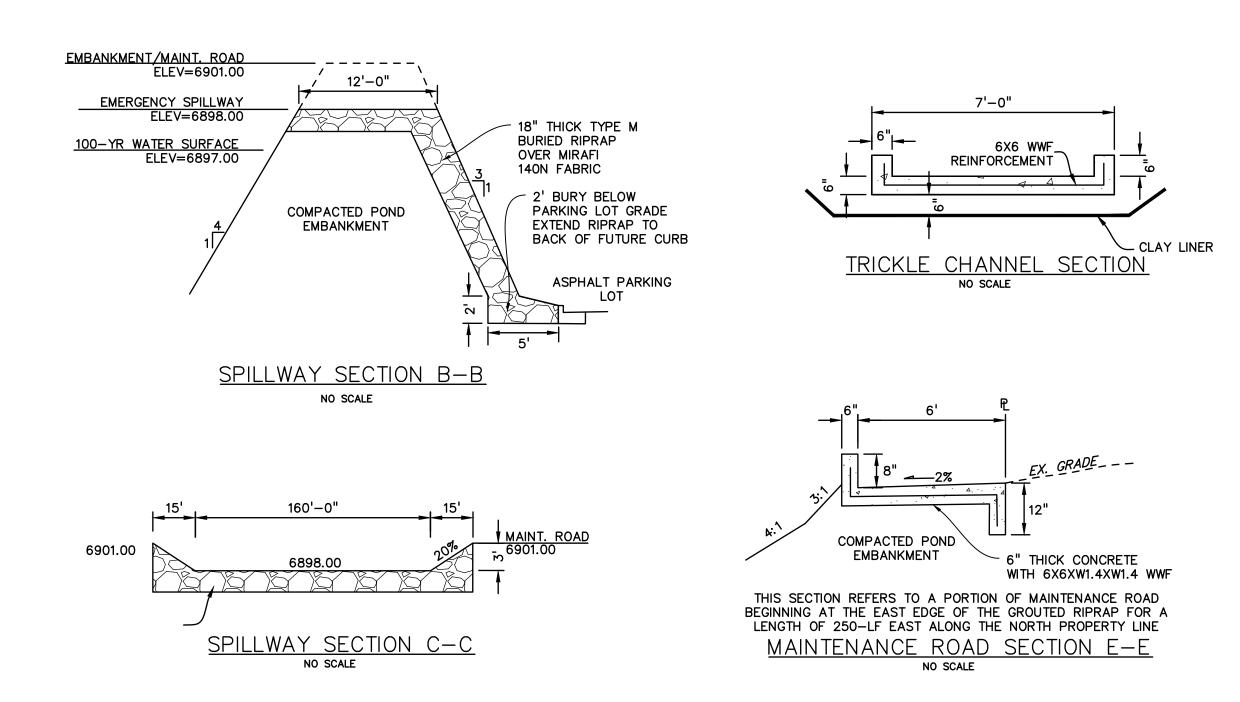
PROPOSED DRAINAGE CONDITIONS

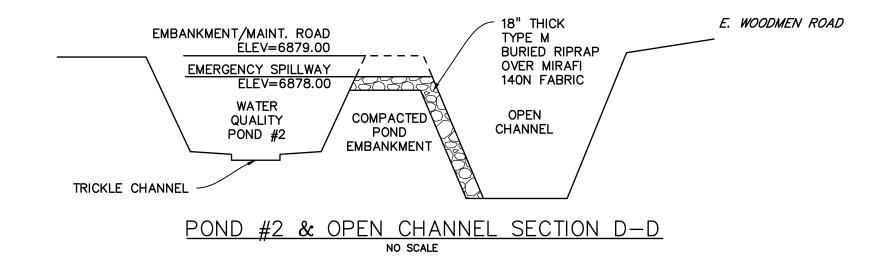
PROJECT NO. 20988-00CSCV DRAWING NO.

D-4

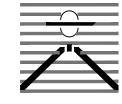
SHEET: 4 OF 5







PREPARED BY:



DREXEL, BARRELL & CO. Engineers • Surveyors 3 SOUTH 7TH STREET COLORADO SPGS, COLORADO 80905 CONTACT: TIM D. McCONNELL, P.E. (719)260-0887

BOULDER • COLORADO SPRINGS

CLIENT:

.....

HUMMEL INVESTMENTS, LLC

8117 PRESTON ROAD, SUITE 120 DALLAS, TEXAS 75225 (214) 416-9820

> FALCON MARKETPLACE

| ISSUE | DATE |
|---------------|---------|
| INITIAL ISSUE | 6-28-19 |
| REVISED | 7-19-19 |
| | |
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| | |
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| | |
| | |
| | |

| DESIGNED BY: | TDM |
|--------------|-----|
| DRAWN BY: | KGV |
| CHECKED BY: | TDM |
| FILE NAME: | |
| | |



PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALI OF DREXEL, BARRELL & CO.

DRAWING SCALE:
HORIZONTAL: N/A
VERTICAL: N/A

PROPOSED DRAINAGE DETAILS

PROJECT NO. 20988-00CSCV DRAWING NO.

D-5

SHEET: 5 OF 5

APPENDIX C

COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: Falcon Ranchettes Filing No. 1A

Location: CO, Colorado Springs

Project Name: Meridian Storage

Project No.: MRS01
Calculated By: CMWJ

Checked By: BAS

Date: 4/26/24

| | | | Roads | | | Lawns | | | Roofs | | Danis a Takal |
|----------|-----------------|--------|-----------|--------------------|--------|-----------|-----------------|--------|-----------|--------------------|---------------------------------|
| Basin ID | Total Area (ac) | % Imp. | Area (ac) | Weighted % Imp. | % Imp. | Area (ac) | Weighted % Imp. | % Imp. | Area (ac) | Weighted % Imp. | Basins Total Weighted % Imp. |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| EX-1 | 4.97 | 100 | 0.68 | 13.7 | 2 | 4.27 | 1.7 | 100 | 0.02 | 0.40 | 15.8 |
| EX-2 | 2.32 | 80 | 0.26 | 9.0 | 2 | 1.99 | 1.7 | 100 | 0.07 | 3.00 | 13.7 |
| EX-3 | 2.85 | 80 | 0.12 | 3.4 | 2 | 2.67 | 1.9 | 100 | 0.06 | 2.10 | 7.4 |
| EX-4 | 1.08 | 80 | 0.01 | 0.7 | 2 | 1.07 | 2.0 | 100 | 0.00 | 0.00 | 2.7 |
| OS-1 | 3.89 | 80 | 0.38 | 7.8 | 2 | 3.46 | 1.8 | 100 | 0.05 | 1.30 | 10.9 |
| OS-2 | 2.35 | 80 | 0.30 | 10.2 | 2 | 2.00 | 1.7 | 100 | 0.05 | 2.10 | 14.0 |
| OS-3 | 0.24 | 100 | 0.00 | 0.0 | 2 | 0.24 | 2.0 | 100 | 0.00 | 0.00 | 2.0 |
| OS-4E | 0.05 | 100 | 0.05 | 100.0 | 2 | 0.00 | 0.0 | 100 | 0.00 | 0.00 | 100.0 |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| A-1 | 1.82 | 100 | 0.68 | 37.4 | 2 | 1.14 | 1.3 | 100 | 0.00 | 0.00 | 38.7 |
| B-1 | 1.46 | 100 | 0.89 | 61.0 | 2 | 0.08 | 0.1 | 100 | 0.49 | 33.60 | 94.7 |
| B-2 | 1.18 | 100 | 0.59 | 50.0 | 2 | 0.02 | 0.0 | 100 | 0.57 | 48.30 | 98.3 |
| B-3 | 0.95 | 100 | 0.41 | 43.2 | 2 | 0.37 | 0.8 | 100 | 0.17 | 17.90 | 61.9 |
| B-4 | 0.52 | 100 | 0.41 | 78.9 | 2 | 0.11 | 0.4 | 100 | 0.00 | 0.00 | 79.3 |
| B-5 | 0.13 | 100 | 0.11 | 84.6 | 2 | 0.02 | 0.3 | 100 | 0.00 | 0.00 | 84.9 |
| B-6 | 0.16 | 100 | 0.11 | 68.8 | 2 | 0.05 | 0.6 | 100 | 0.00 | 0.00 | 69.4 |
| B-7 | 0.56 | 100 | 0.07 | 12.5 | 2 | 0.49 | 1.8 | 100 | 0.00 | 0.00 | 14.3 |
| C-1 | 0.29 | 80 | 0.15 | 41.4 | 2 | 0.14 | 1.0 | 100 | 0.00 | 0.00 | 42.4 |
| C-2 | 3.12 | 80 | 2.25 | 57.7 | 2 | 0.87 | 0.6 | 100 | 0.00 | 0.00 | 58.3 |
| C-3 | 0.29 | 80 | 0.19 | 52.4 | 2 | 0.10 | 0.7 | 100 | 0.00 | 0.00 | 53.1 |
| C-4 | 0.09 | 100 | 0.00 | 0.0 | 2 | 0.09 | 2.0 | 100 | 0.00 | 0.00 | 2.0 |
| D-1 | 0.08 | 100 | 0.00 | 0.0 | 2 | 0.08 | 2.0 | 100 | 0.00 | 0.00 | 2.0 |
| D-2 | 0.05 | 100 | 0.03 | 60.0 | 2 | 0.02 | 0.8 | 100 | 0.00 | 0.00 | 60.8 |
| D-3 | 0.33 | 100 | 0.25 | 75.8 | 2 | 0.08 | 0.5 | 100 | 0.00 | 0.00 | 76.3 |
| OS-4P | 0.07 | 100 | 0.06 | 85.7 | 2 | 0.01 | 0.3 | 100 | 0.00 | 0.00 | 86.0 |
| OS-5 | 0.19 | 100 | 0.00 | 0.0 | 2 | 0.19 | 2.0 | 100 | 0.00 | 0.00 | 2.0 |
| OS-6 | 0.08 | 100 | 0.00 | 0.0 | 2 | 0.08 | 2.0 | 100 | 0.00 | 0.00 | 2.0 |
| | 0.00 | 100 | 0.00 | 0.0 | | 0.00 | 2.0 | 100 | 0.00 | 0.00 | |

^{*}Impervious values are taken directly from "Table 6-6 Runoff Coefficients for Rational Method"



STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Falcon Ranchettes Filing No. 1A

Location: CO, Colorado Springs

Project Name: Meridian Storage
Project No.: MRS01
Calculated By: CMWJ
Checked By: BAS
Date: 4/26/24

| | | SUB-BA | ASIN | | | INIT | AL/OVERL | AND | | TR | AVEL TIM | E | | | Tc CHECK | | |
|-------|------|-------------|------------|------------------|----------------|------|-------------------|----------------|------|-----|-------------------|-------|----------------|----------------------|----------------|--------------------------|----------------|
| | | DAT | Α | | | | (T _i) | | | | (T _t) | | | | (URBANIZED BAS | SINS) | FINAL |
| BASIN | D.A. | Hydrologic | Impervious | C ₁₀₀ | C ₅ | L | S | T _i | L | S | Cv | VEL. | T _t | COMP. T _c | TOTAL | Urbanized T _c | T _c |
| ID | (AC) | Soils Group | (%) | | | (FT) | (%) | (MIN) | (FT) | (%) | | (FPS) | (MIN) | (MIN) | LENGTH (FT) | (MIN) | (MIN) |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| EX-1 | 4.97 | Α | 15.8 | 0.23 | 0.08 | 25 | 15.0 | 3.8 | 830 | 1.8 | 15.0 | 2.0 | 6.9 | 10.7 | 855.0 | 14.8 | 10.7 |
| EX-2 | 2.32 | Α | 13.7 | 0.22 | 0.07 | 15 | 1.0 | 7.3 | 540 | 1.9 | 5.0 | 0.7 | 13.1 | 20.4 | 555.0 | 13.1 | 13.1 |
| EX-3 | 2.85 | Α | 7.4 | 0.17 | 0.03 | 25 | 15.0 | 4.0 | 650 | 2.2 | 5.0 | 0.7 | 14.6 | 18.6 | 675.0 | 13.8 | 13.8 |
| EX-4 | 1.08 | Α | 2.7 | 0.13 | 0.01 | 25 | 1.0 | 10.0 | 620 | 2.3 | 5.0 | 0.8 | 13.6 | 23.6 | 645.0 | 13.6 | 13.6 |
| OS-1 | 3.89 | Α | 10.9 | 0.19 | 0.05 | 100 | 5.3 | 11.1 | 600 | 2.1 | 10.0 | 1.4 | 6.9 | 18.0 | 700.0 | 13.9 | 13.9 |
| OS-2 | 2.35 | Α | 14.0 | 0.22 | 0.07 | 100 | 5.3 | 10.8 | 900 | 1.9 | 7.0 | 1.0 | 15.5 | 26.4 | 1000.0 | 15.6 | 15.6 |
| OS-3 | 0.24 | Α | 2.0 | 0.13 | 0.01 | 25 | 10.0 | 4.6 | 325 | 2.4 | 7.0 | 1.1 | 5.0 | 9.6 | 350.0 | 11.9 | 9.6 |
| OS-4E | 0.05 | Α | 100.0 | 0.89 | 0.86 | 10 | 1.0 | 1.4 | 80 | 1.0 | 15.0 | 1.5 | 0.9 | 2.3 | 90.0 | 10.5 | 5.0 |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| A-1 | 1.82 | Α | 38.7 | 0.41 | 0.26 | 25 | 25.0 | 2.6 | 620 | 1.3 | 15.0 | 1.7 | 6.2 | 8.8 | 645.0 | 13.6 | 8.8 |
| B-1 | 1.46 | Α | 94.7 | 0.85 | 0.80 | 60 | 7.0 | 2.2 | 350 | 2.0 | 20.0 | 2.8 | 2.1 | 4.3 | 410.0 | 12.3 | 5.0 |
| B-2 | 1.18 | Α | 98.3 | 0.88 | 0.84 | 12.5 | 2.0 | 1.3 | 335 | 1.2 | 20.0 | 2.2 | 2.5 | 3.9 | 347.5 | 11.9 | 5.0 |
| B-3 | 0.95 | Α | 61.9 | 0.59 | 0.47 | 20 | 2.0 | 4.1 | 640 | 3.2 | 20.0 | 3.6 | 3.0 | 7.1 | 660.0 | 13.7 | 7.1 |
| B-4 | 0.52 | Α | 79.3 | 0.73 | 0.64 | 20 | 2.0 | 3.0 | 640 | 3.2 | 20.0 | 3.6 | 3.0 | 6.0 | 660.0 | 13.7 | 6.0 |
| B-5 | 0.13 | Α | 84.9 | 0.77 | 0.70 | 30 | 2.2 | 3.1 | 148 | 0.8 | 20.0 | 1.8 | 1.4 | 4.5 | 178.0 | 11.0 | 5.0 |
| B-6 | 0.16 | Α | 69.4 | 0.65 | 0.54 | 30 | 2.2 | 4.3 | 154 | 0.8 | 20.0 | 1.8 | 1.4 | 5.8 | 184.0 | 11.0 | 5.8 |
| B-7 | 0.56 | Α | 14.3 | 0.22 | 0.07 | 25 | 25.0 | 3.2 | 125 | 3.0 | 7.0 | 1.2 | 1.7 | 4.9 | 150.0 | 10.8 | 5.0 |
| C-1 | 0.29 | Α | 42.4 | 0.44 | 0.29 | 100 | 2.8 | 10.5 | 190 | 2.8 | 20.0 | 3.3 | 0.9 | 11.5 | 290.0 | 11.6 | 11.5 |
| C-2 | 3.12 | Α | 58.3 | 0.56 | 0.43 | 100 | 2.2 | 9.4 | 450 | 2.2 | 20.0 | 3.0 | 2.5 | 12.0 | 550.0 | 13.1 | 12.0 |
| C-3 | 0.29 | А | 53.1 | 0.52 | 0.38 | 100 | 2.3 | 10.0 | 200 | 2.3 | 20.0 | 3.0 | 1.1 | 11.1 | 300.0 | 11.7 | 11.1 |
| C-4 | 0.09 | А | 2.0 | 0.13 | 0.01 | 5 | 25.0 | 1.5 | 250 | 2.0 | 15.0 | 2.1 | 2.0 | 3.5 | 255.0 | 11.4 | 5.0 |
| D-1 | 0.08 | А | 2.0 | 0.13 | 0.01 | 25 | 25.0 | 3.4 | 1 | 1.0 | 20.0 | 2.0 | 0.0 | 3.4 | 26.0 | 10.1 | 5.0 |
| D-2 | 0.05 | Α | 60.8 | 0.58 | 0.46 | 35 | 15.0 | 2.8 | 35 | 1.5 | 20.0 | 2.4 | 0.2 | 3.1 | 70.0 | 10.4 | 5.0 |
| D-3 | 0.33 | Α | 76.3 | 0.70 | 0.61 | 30 | 2.0 | 3.9 | 166 | 1.0 | 20.0 | 2.0 | 1.4 | 5.3 | 196.0 | 11.1 | 5.3 |
| OS-4P | 0.07 | А | 86.0 | 0.78 | 0.71 | 20 | 2.0 | 2.5 | 46 | 1.0 | 20.0 | 2.0 | 0.4 | 2.9 | 66.0 | 10.4 | 5.0 |
| OS-5 | 0.19 | А | 2.0 | 0.13 | 0.01 | 25 | 15.0 | 4.0 | 1 | 1.0 | 5.0 | 0.5 | 0.0 | 4.1 | 26.0 | 10.1 | 5.0 |
| OS-6 | 0.08 | А | 2.0 | 0.13 | 0.01 | 25 | 15.0 | 4.0 | 160 | 1.0 | 5.0 | 0.5 | 5.3 | 9.4 | 185.0 | 11.0 | 9.4 |
| | | | | | | | | | | | | | | | | | |

NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$, S in ft/ft

T_t=L/60V (Velocity From Fig. 501)

Velocity V=Cv*S^0.5, S in ft/ft

Tc Check = 10+L/180

For Urbanized basins a minimum T_{c} of 5.0 minutes is required.

For non-urbanized basins a minimum T_c of 10.0 minutes is required



STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Ranchettes Filing No. 1A

Location: CO, Colorado Springs

Design Storm: 5-Year

 Project Name:
 Meridian Storage

 Project No.:
 MRS01

 Calculated By:
 CMWJ

 Checked By:
 BAS

 Date:
 4/26/24

| | 1 | | | | DIRECT R | LINOEE | | | | TOTAL | DIINOE | | СТЕ | EET | | PIPE | 7/20/2 | | AVEL TI | NAE | |
|--|--------------|----------|-----------|---------------|----------|----------|-----------|---------|----------|----------|-----------|---------|-----------|-------------------|-------------------|-----------|--------------------|-------------|----------------|----------|---|
| STREET | Design Point | Basin ID | Area (Ac) | Runoff Coeff. | Tc (min) | C*A (Ac) | I (in/hr) | Q (cfs) | Tc (min) | C*A (Ac) | ı (in/hr) | Q (cfs) | Slope (%) | Street Flow (cfs) | Design Flow (cfs) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | Tt (min) | REMARKS |
| | | | | | | | | | | | | | | | | | | | | | |
| | 1 | MT060 | | | | | | 304.6 | | | | | | | | | | | | | Flows from upstream offsite basin = 304.6 cfs |
| | 1 | EX-1 | 4.97 | 0.08 | 10.7 | 0.40 | 4.03 | 1.6 | | | | | | | | | | | | | Flows from project site at DP1 = 1.6 cfs |
| | 1 | EV-1 | 4.37 | 0.08 | 10.7 | 0.40 | 4.03 | 1.0 | | | | 306.2 | | | | | | | | | Total flow at DP1 = 306.2 cfs |
| | | EV 2 | 2.22 | 0.07 | 12.1 | 0.46 | 2.72 | 0.5 | | | | 300.2 | | | | | | | | | |
| | 2 | EX-2 | 2.32 | | 13.1 | | | 0.6 | | | | | | | | | | | | | Total flow at DP2 = 0.6 cfs |
| | 3 | EX-3 | 2.85 | | 13.8 | | | 0.3 | | | | | | | | | | | | | Total flow at DP3 = 0.3 cfs |
| | 4 | EX-4 | 1.08 | | 13.6 | | | 0.0 | | | | | | | | | | | | | Flows from basin at DP4 = 0 cfs |
| | 4 | OS-1 | 3.89 | | 13.9 | | | 0.7 | | | | | | | | | | | | | Flows from basin at DP4 = 0.7 cfs |
| | 4 | OS-2 | 2.35 | | 15.6 | | | 0.6 | | | | | | | | | | | | | Flows from basin at DP4 = 0.6 cfs |
| | 4 | OS-3 | 0.24 | 0.01 | 9.6 | 0.00 | 4.19 | 0.0 | | | | | | | | | | | | | Flows from basin at DP4 = 0 cfs |
| | 4 | | | | | | | | 15.6 | 0.36 | 3.47 | 1.2 | | | | | | | | | Total flow at DP4 = 1.2 cfs |
| See basin comparison OS-4E / OS-4P | 14 | OS-4E | 0.05 | 0.86 | 5.0 | 0.04 | 5.17 | 0.2 | | | | | | | | | | | | | Existing condition of contributing flow to DP14 = 0.2 cfs |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | 1 | MT060 | | | | | | 304.6 | | | | | | | | | | | | | Flows from upstream offsite basin = 304.6 cfs |
| | 1 | OS-6 | 0.08 | 0.01 | 9.4 | 0.00 | 4.22 | 0.0 | | | | | | | | | | | | | Flows from basin = 0 cfs |
| | 1 | A-1 | 1.82 | 0.26 | 8.8 | 0.47 | 4.32 | 2.0 | | | | | | | | | | | | | Flows from basin = 2 cfs |
| | 1 | | | | | | | | 9.4 | 0.47 | 4.22 | 306.6 | | | | | | | | | Total flow at DP1 = 306.6 cfs |
| | | D-1 | 0.08 | 0.01 | 5.0 | 0.00 | 5.17 | 0.0 | | | | | | | | | | | | | Total flow = 0 cfs |
| | 3 | B-1 | 1.46 | 0.80 | 5.0 | 1.17 | 5.17 | 6.0 | | | | | | | 6.0 | 1.3 | | 290 | 2.2 | 2.2 | Total flow captured by inlet, DP3 = 6 cfs |
| | 4 | B-2 | 1.18 | 0.84 | 5.0 | 0.99 | 5.17 | 5.1 | | | | | | | | | | | | | Total flow captured by inlet, DP4 = 5.1 cfs |
| | 4 | | | | | | | | 7.2 | 2.16 | 4.63 | 10.0 | | | 10.0 | 1.0 | | 128 | | | Total flow in storm system, DP4 = 10 cfs |
| Proposed on-grade 10' CDOT Type R | 5 | B-3 | 0.95 | 0.47 | 7.1 | 0.45 | 4.65 | 2.1 | | | | | 1.5 | 0.0 | 2.1 | | | 95 | 2.4 | | Qcap = 2.1 cfs, Qbyp = 0 cfs; Qbyp to DP12 |
| | 5 | | | | | | | | 8.2 | 2.61 | 4.42 | 11.5 | | | 11.5 | 0.5 | | 41 | 1.4 | 0.5 | Total flow in storm system, DP5 = 11.5 cfs |
| | 6 | B-4 | 0.52 | 0.64 | 6.0 | 0.33 | 4.90 | 1.6 | | | | | | | | | | | | | Flows from basin = 1.6 cfs |
| | 6 | C-1 | 0.29 | 0.29 | 11.5 | 0.08 | 3.92 | 0.3 | | | | | 2.15 | 0.3 | | | | 210 | 2.9 | 1.2 | Flows from basin to DP6 = 0.3 cfs |
| Proposed on-grade 10' CDOT Type R | 6 | | | | | | | | 12.7 | 0.41 | 3.77 | 1.5 | 1.5 | 0.0 | 1.5 | | | 95 | 2.4 | 0.6 | Qcap = 1.5 cfs, Qbyp = 0 cfs; Qbyp to DP13 |
| | 6 | | | | | | | | 12.7 | 3.01 | 3.77 | 11.3 | | | 11.3 | 1.0 | | 29 | 2.0 | 0.2 | Total flow in storm system, DP6 = 11.3 cfs; piped to Forebay A |
| Proposed on-grade 5' CDOT Type R | 7 | B-5 | 0.13 | 0.70 | 5.0 | 0.09 | 5.17 | 0.5 | | | | | 0.8 | 0.0 | 0.5 | 1.0 | | 150 42 | 1.8 2.0 | 1.4 | Qcap = 0.5 cfs, Qbyp = 0 cfs; Qbyp to DP13 |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 8 | C-3 | 0.29 | | 11.1 | 0.11 | 3.97 | 0.4 | | | | | 0.5 | 0.4 | | | | 75 | 1.4 | 0.9 | Flows from basin to DP8 = 0.4 cfs |
| | 8 | B-6 | 0.16 | | 5.8 | | | 0.4 | | | | | | | | | | | | | Flows from basin = 0.4 cfs |
| Proposed on-grade 5' CDOT Type R | 8 | 50 | 0.10 | 0.54 | 5.0 | 0.03 | 4.50 | 0.4 | 12.0 | 0.20 | 3.86 | 0.8 | 1.5 | 0.0 | 0.8 | | | 95 | 2.4 | 0.6 | Qcap = 0.8 cfs, Qbyp = 0 cfs; Qbyp to DP13 |
| rioposed oingiade 3. CDOT Type N | 8 | | | | | | | | | | | | | | 0.8 | | | | | | |
| | | 05.0 | | | 0.5 | | | | 12.9 | 0.30 | 3./3 | 1.1 | | | | | | | | | Total flow in storm system, DP8 = 1.1 cfs; piped to Forebay D |
| | 9 | OS-3 | 0.24 | | 9.6 | | | 0.0 | | | | | | | | | | | | | Flows from basin = 0 cfs |
| | 9 | OS-5 | 0.19 | | 5.0 | | | 0.0 | | | | | | | | | | | | | Flows from basin = 0 cfs |
| | 9 | C-2 | 3.12 | | 12.0 | | 3.86 | 5.2 | | | | | | | | | | | | | Flows from basin = 5.2 cfs |
| | 9 | B-7 | 0.56 | 0.07 | 5.0 | 0.04 | 5.17 | 0.2 | | | | | | | | | | | | | Flows from basin = 0.2 cfs |
| Flow taken from UD-Detention Worksheet | 9 | | 1 | | | | | | | | | 16.5 | | | | | | | | | Total Flow entering Pond #1 = 16.5 cfs |
| Flow taken from UD-Detention Worksheet | 9 | | | | | | | | | | | 0.4 | | | 0.4 | 1.0 | | 140 | 2.0 | 1.2 | Peak Outflow from Pond #1 = 0.4 cfs |
| | 10 | OS-1 | 3.89 | 0.05 | 13.9 | 0.19 | 3.64 | 0.7 | | | | | | | | | - | | | | Flows from basin at DP10 = 0.7 cfs |
| | 10 | OS-2 | 2.35 | 0.07 | 15.6 | 0.16 | 3.47 | 0.6 | | | | | | | | | | | | | Flows from basin at DP10 = 0.6 cfs |
| | 10 | C-4 | 0.09 | 0.01 | 5.0 | 0.00 | 5.17 | 0.0 | | | | | | | | | _ | | | | Flows from basin at DP10 = 0 cfs |
| | 10 | | | | | - | | | 15.6 | 0.35 | 3.47 | 1.2 | | | 1.2 | 10.0 | - | 40 | 6.3 | 0.1 | Total flow captured by inlet, DP10 = 1.2 cfs |
| | 11 | | - | | | | | | 15.7 | 0.35 | 3.46 | 1.6 | | | | | | | | | Total flow at manhole, DP11 = 1.6 cfs; conveyed to Subregional Pond SR4 |
| | 12 | D-2 | 0.05 | 0.46 | 5.0 | 0.02 | 5.17 | 0.1 | | | | | | | | | _ | | | | Flows from basin = 0.1 cfs Add bypass flows from DP5 |
| | 12 | | | | | | | | 5.0 | 0.02 | 5.17 | 0.1 | | | | | _ | | | | Total flow at DP12 = 0.1 cfs |
| | 13 | D-3 | 0.33 | 0.61 | 5.3 | 0.20 | 5.09 | 1.0 | | | | | | | | | | | | | Flows from basin = 1 cfs Add bypass flows from DP6, DP7, DP8 |
| | 13 | | <u> </u> | | | | | | 5.3 | 0.20 | 5.09 | 1.0 | | | | | <u> </u> | | | | Add bypass flows from DP6, DP7, DP8 Total flow at DP13 = 1 cfs |
| See basin comparison OS-4P / OS-4E | 14 | OS-4P | 0.07 | 0.71 | 5.0 | 0.05 | 5.17 | 0.3 | | | | | | | | | | | | | Proposed condition of contributing flow to DP14 = 0.3 cfs |
| | | | | | | | | | | | | | | | | | | | | | |

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Ranchettes Filing No. 1A
Location: CO, Colorado Springs
Design Storm: 100-Year

 Project Name:
 Meridian Storage

 Project No.:
 MRS01

 Calculated By:
 CMWJ

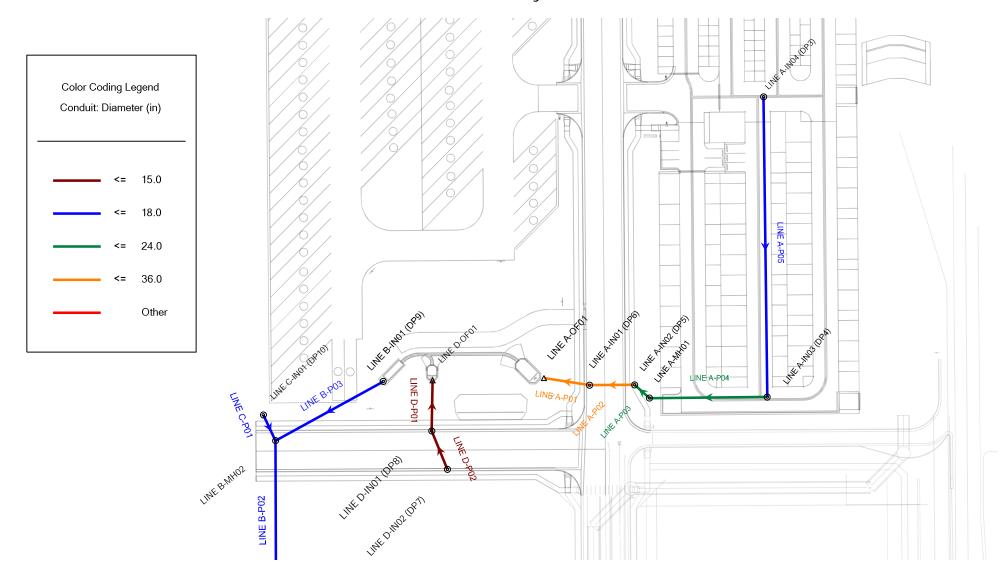
 Checked By:
 BAS

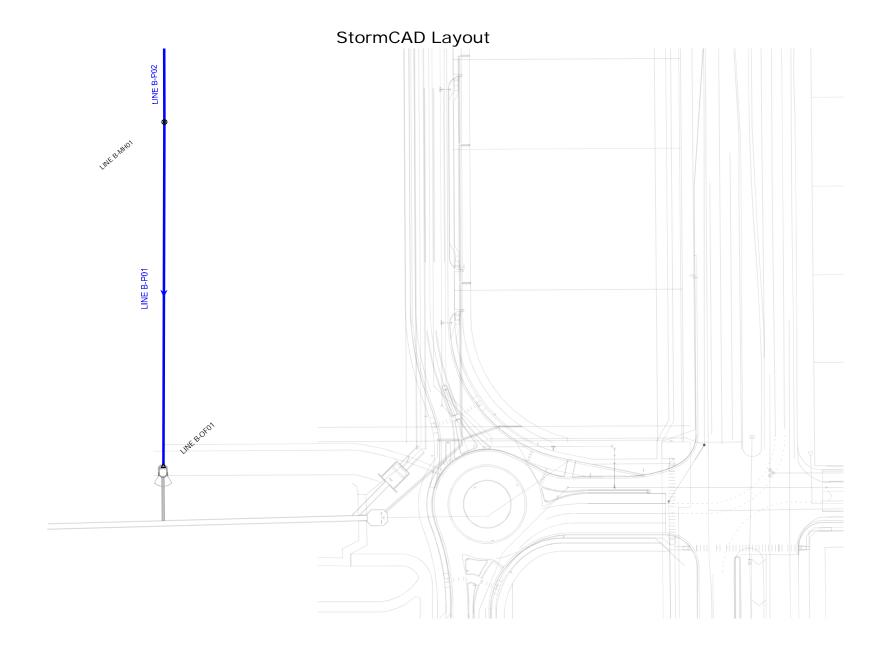
 Date:
 4/26/24

| | | | | | | | | | | | | | | | | | 4/26/2 | | | | | |
|--|--------------|----------|-----------|---------------|----------|----------|-----------|---------|----------|----------|---------------------|---------|---------------|-------------------|-------------------|-----------|--------------------|-----------|----------------|------------|--|--|
| STREET | Design Point | Basin ID | Area (Ac) | Runoff Coeff. | Tc (min) | C*A (Ac) | I (in/hr) | Q (cfs) | Tc (min) | C*A (Ac) | RUNOFF I (in/hr) | Q (cfs) | STR (%) adolS | Street Flow (cfs) | Design Flow (cfs) | Slope (%) | Pipe Size (inches) | TR/ | Velocity (fps) | Tt (min) | REMARKS | |
| | | | | | | | | | | | | | | | | | | | | | | |
| | 1 | MT060 | | | | | | 915.3 | | | | | | | | | | | | | Flows from upstream offsite basin = 915.3 cfs | |
| | 1 | EX-1 | 4.97 | 0.23 | 10.7 | 1.14 | 6.77 | 7.7 | | | | | | | | | | | | | Flows from project site at DP1 = 7.7 cfs | |
| | 1 | LX-1 | 4.37 | 0.23 | 10.7 | 1.14 | 0.77 | 7.7 | | | | 923.0 | | | | | | | | | Total flow at DP1 = 923 cfs | |
| | 2 | EV 3 | 2 22 | 0.22 | 12.1 | 0.51 | 6.26 | 2.2 | | | | 923.0 | | | | | | | | | Total flow at DP2 = 3.2 cfs | |
| | 3 | EX-2 | 2.32 | | 13.1 | | 6.26 | 2.9 | | | | | | | | | | | | | Total flow at DP3 = 2.9 cfs | |
| | 4 | EX-4 | 1.08 | | 13.6 | | 6.16 | 0.9 | | | | | | | | | | | | | Flows from basin at DP4 = 0.9 cfs | |
| | 4 | OS-1 | 3.89 | | 13.9 | | 6.10 | 4.5 | | | | | | | | | | | | | | |
| | 4 | OS-2 | 2.35 | | 15.6 | | 5.82 | 3.0 | | | | | | | | | | | | | Flows from basin at DP4 = 4.5 cfs Flows from basin at DP4 = 3 cfs | |
| | 4 | OS-3 | 0.24 | | 9.6 | | 7.03 | 0.2 | | | | | | | | | | | | | Flows from basin at DP4 = 0.2 cfs | |
| | 4 | 05-5 | 0.24 | 0.13 | 9.0 | 0.03 | 7.03 | 0.2 | 15.6 | 4.42 | F 02 | 0.3 | | | | | | | | | | |
| See heady assuranteen OS AF / OS AD | | 05.45 | 0.05 | 0.00 | | 0.04 | 0.50 | 0.3 | 15.6 | 1.43 | 5.82 | 8.3 | | | | | | | | | Total flow at DP4 = 8.3 cfs | |
| See basin comparison OS-4E / OS-4P | 14 | OS-4E | 0.05 | 0.89 | 5.0 | 0.04 | 8.68 | 0.3 | | | | | | | | | | | | | Existing condition of contributing flow to DP14 = 0.3 cfs | |
| | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | |
| | 1 | MT060 | | | | | | 915.3 | | | | | | | | | | | | | Flows from upstream offsite basin = 915.3 cfs | |
| | 1 | OS-6 | 0.08 | | 9.4 | | 7.09 | 0.1 | | | | | | | | | | | | | Flows from basin = 0.1 cfs | |
| | 1 | A-1 | 1.82 | 0.41 | 8.8 | 0.75 | 7.26 | 5.4 | | | | | | | | | | | | | Flows from basin = 5.4 cfs | |
| | 1 | | | | | | | | 9.4 | 0.76 | 7.09 | 920.7 | | | | | | | | | Total flow at DP1 = 920.7 cfs Total flow = 0.1 cfs | |
| | | D-1 | 0.08 | 0.13 | 5.0 | 0.01 | 8.68 | 0.1 | | | | | | | | | | | | | Total flow = 0.1 cfs | |
| | 3 | B-1 | 1.46 | 0.85 | 5.0 | 1.24 | 8.68 | 10.8 | | | | | | | 10.8 | 1.3 | 3 | 290 | 2.2 | 2.2 | Total flow captured by inlet, DP3 = 10.8 cfs | |
| | 4 | B-2 | 1.18 | 0.88 | 5.0 | 1.04 | 8.68 | 9.0 | | | | | | | | | | | | | Total flow captured by inlet, DP4 = 9 cfs | |
| | 4 | | | | | | | | 7.2 | 2.28 | 7.77 | 17.7 | 1.5 | 0.2 | 17.7 | 1.0 |) | 128 95 | 2.0 | 1.1 0.6 | Total flow in storm system, DP4 = 17.7 cfs | |
| Proposed on-grade 10' CDOT Type R | 5 | B-3 | 0.95 | 0.59 | 7.1 | 0.56 | 7.80 | 4.4 | | | | | | | 4.2 | | | | | | Qcap = 4.2 cfs, Qbyp = 0.2 cfs; Qbyp to DP12 | |
| | 5 | | | | | | | | 8.2 | 2.82 | 7.42 | 20.9 | | | 20.9 | 0.5 | 5 | 41 | 1.4 | 0.5 | Total flow in storm system, DP5 = 20.9 cfs | |
| | 6 | B-4 | 0.52 | 0.73 | 6.0 | 0.38 | 8.23 | 3.1 | | | | | 2.15 | 0.9 | | | | 210 | 2.9 | 1.2 | Flows from basin = 3.1 cfs Flows from basin to DP6 = 0.9 cfs | |
| | 6 | C-1 | 0.29 | 0.44 | 11.5 | 0.13 | 6.59 | 0.9 | | | | | 1.5 | | | | | 95 | | 0.6 | | |
| Proposed on-grade 10' CDOT Type R | 6 | | | | | | | | 12.7 | 0.51 | 6.34 | 3.2 | 1.5 | 0.0 | 3.2 | | | 33 | 2 | 0.0 | Qcap = 3.2 cfs, Qbyp = 0 cfs; Qbyp to DP13 | |
| | 6 | | | | | | | | 12.7 | 3.32 | 6.34 | 21.1 | 0.8 | 0.0 | 21.1 | 1.0 |) | 29 150 | 2.0 | 0.2 | Total flow in storm system, DP6 = 21.1 cfs; piped to Forebay A | |
| Proposed on-grade 5' CDOT Type R | 7 | B-5 | 0.13 | 0.77 | 5.0 | 0.10 | 8.68 | 0.9 | | | | | 0.5 | 1.0 | 0.9 | 1.0 |) | 42 75 | 2.0 | 0.4 | Qcap = 0.9 cfs, Qbyp = 0 cfs; Qbyp to DP13 Flows from basin to DP8 = 1 cfs | |
| | 8 | C-3 | 0.29 | 0.52 | 11.1 | 0.15 | 6.67 | 1.0 | | | | | 0.5 | 1.0 | | | | /3 | 1.4 | 0.9 | Flows Hulli Dasiii to Dro - 1 cis | |
| | 8 | B-6 | 0.16 | 0.65 | 5.8 | 0.10 | 8.33 | 0.8 | | | | | 4.5 | 0.4 | | | | 05 | 2.4 | 0.6 | Flows from basin = 0.8 cfs | |
| Proposed on-grade 5' CDOT Type R | 8 | | | | | | | | 12.0 | 0.25 | 6.48 | 1.6 | 1.5 | 0.1 | 1.5 | | | 95 | 2.4 | 0.6 | Qcap = 1.5 cfs, Qbyp = 0.1 cfs; Qbyp to DP13 | |
| | 8 | | | | | | | | 12.9 | 0.34 | 6.29 | 2.1 | | | | | | | | | Total flow in storm system, DP8 = 2.1 cfs; piped to Forebay D | |
| | 9 | OS-3 | 0.24 | 0.13 | 9.6 | 0.03 | 7.03 | 0.2 | | | | | | | | | | | | | Flows from basin = 0.2 cfs | |
| | 9 | OS-5 | 0.19 | 0.13 | 5.0 | 0.02 | 8.68 | 0.2 | | | | | | | | | | | | | Flows from basin = 0.2 cfs | |
| | 9 | C-2 | 3.12 | 0.56 | 12.0 | 1.75 | 6.48 | 11.3 | | | | | | | | | | | | | Flows from basin = 11.3 cfs | |
| | 9 | B-7 | 0.56 | 0.22 | 5.0 | 0.12 | 8.68 | 1.0 | | | | | | | | | | | | | Flows from basin = 1 cfs | |
| Flow taken from UD-Detention Worksheet | 9 | | | | | | | | | | | 31.2 | | | | | | | | | Total Flow entering Pond #1 = 31.2 cfs | |
| Flow taken from UD-Detention Worksheet | 9 | | | | | | | | | | | 4.7 | | | 4.7 | 1.0 |) | 140 | 2.0 | 1.2 | Peak Outflow from Pond #1 = 4.7 cfs | |
| | 10 | OS-1 | 3.89 | 0.19 | 13.9 | 0.74 | 6.10 | 4.5 | | | | | | | | | | | | | Flows from basin at DP10 = 4.5 cfs | |
| | 10 | OS-2 | 2.35 | 0.22 | 15.6 | 0.52 | 5.82 | 3.0 | | | | | | | | | | | | | Flows from basin at DP10 = 3 cfs | |
| | 10 | C-4 | 0.09 | 0.13 | 5.0 | 0.01 | 8.68 | 0.1 | | | | | | | L | | | L | | | Flows from basin at DP10 = 0.1 cfs | |
| | 10 | | | | | | | | 15.6 | 1.27 | 5.82 | 7.4 | | | 7.4 | 10.0 |) | 40 | 6.3 | 0.1 | Total flow captured by inlet, DP10 = 7.4 cfs | |
| | 11 | | | | | | | | 15.7 | 1.27 | 5.80 | 12.1 | | | | | | | | | Total flow at manhole, DP11 = 12.1 cfs; conveyed to Subregional Pond SR4 | |
| | 12 | D-2 | 0.05 | 0.58 | 5.0 | 0.03 | 8.68 | 0.3 | | | | | | | | | | | | | Flows from basin = 0.3 cfs | |
| | 12 | | | | | | | | 5.0 | 0.05 | 8.68 | 0.4 | | | | | | | | | Add bypass flows from DP5 Total flow at DP12 = 0.4 cfs | |
| | 13 | D-3 | 0.33 | 0.70 | 5.3 | 0.23 | 8.54 | 2.0 | | | | 2.1 | | | | | Ì | | | | Flows from basin = 2 cfs | |
| | 13 | | 3.55 | | 3.3 | | 3.5 T | 2.0 | 5.3 | 0.25 | 8.54 | 2.1 | | | | | | | | | Add bypass flows from DP6, DP7, DP8 Total flow at DP13 = 2.1 cfs | |
| See basin comparison OS-4P / OS-4E | 14 | OS-4P | 0.07 | 0.78 | 5.0 | 0.05 | 8.68 | 0.4 | J.3 | J.23 | 0.34 | 2.1 | | | | | 1 | | | | Proposed condition of contributing flow to DP14 = 0.4 cfs | |
| See Sasin comparison OS-4r/ / OS-4E | 14 | 03-4F | 0.07 | 0.78 | 3.0 | 0.03 | 0.08 | 0.4 | | | | | | | | | | | | | reposed continuous of continuous now to br 14 - 0.4 tis | |

APPENDIX D

StormCAD Layout





FlexTable: Conduit Table Active Scenario: 5-Year

| Label | Start Node | Stop Node | Invert (Start) (ft) | Invert (Stop) (ft) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Section Type | Diameter (in) | Manning's n | Flow (cfs) | Velocit y (ft/s) | Capacity (Full Flow) (cfs) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) |
|----------------|-----------------------|----------------------|---------------------------|--------------------------|-------------------------------------|----------------------------------|-----------------|------------------|----------------|---------------|------------------------|-------------------------------------|---|---|--------------------------------------|--|
| LINE A- P04 | LINE A-IN03 (DP4) | LINE A-MH01 | 6,907.71 | 6,906.44 | 101.6 | 0.013 | Circle | 24.0 | 0.013 | 10.00 | 7.58 | 25.29 | 6,908.84 | 6,907.31 | 6,909.30 | 6,908.21 |
| LINE B- P03 | LINE B-IN01 (DP9) | LINE B-MH02 | 6,901.92 | 6,900.67 | 125.1 | 0.010 | Circle | 18.0 | 0.013 | 0.40 | 2.86 | 10.50 | 6,902.15 | 6,901.02 | 6,902.23 | 6,901.05 |
| LINE C- P01 | LINE C-IN01 (DP10) | LINE B-MH02 | 6,906.50 | 6,901.37 | 36.0 | 0.143 | Circle | 18.0 | 0.013 | 1.20 | 10.06 | 39.67 | 6,906.91 | 6,901.55 | 6,907.06 | 6,903.12 |
| LINE A- P03 | LINE A-MH01 | LINE A-IN02 (DP5) | 6,906.34 | 6,906.05 | 23.3 | 0.012 | Circle | 24.0 | 0.013 | 10.00 | 7.56 | 25.22 | 6,907.47 | 6,907.41 | 6,907.93 | 6,907.71 |
| LINE A- P02 | LINE A-IN02 (DP5) | LINE A-IN01 (DP6) | 6,905.05 | 6,904.64 | 41.3 | 0.010 | Circle | 36.0 | 0.013 | 11.50 | 7.04 | 66.43 | 6,907.40 | 6,907.41 | 6,907.46 | 6,907.45 |
| LINE A- P01 | LINE A-IN01 (DP6) | LINE A-OF01 | 6,904.54 | 6,904.08 | 45.4 | 0.010 | Circle | 36.0 | 0.013 | 11.30 | 7.06 | 67.16 | 6,907.40 | 6,907.39 | 6,907.44 | 6,907.43 |
| LINE A- P05 | LINE A-IN04 (DP3) | LINE A-IN03 (DP4) | 6,911.91 | 6,908.21 | 295.9 | 0.013 | Circle | 18.0 | 0.013 | 6.00 | 6.68 | 11.75 | 6,912.86 | 6,909.45 | 6,913.26 | 6,909.68 |
| LINE D- P02 | LINE D-IN02 (DP7) | LINE D-IN01 (DP8) | 6,906.75 | 6,906.32 | 42.8 | 0.010 | Circle | 15.0 | 0.013 | 0.40 | 2.93 | 6.47 | 6,907.40 | 6,907.40 | 6,907.41 | 6,907.40 |
| LINE D- P01 | LINE D-IN01 (DP8) | LINE D-OF01 | 6,906.22 | 6,903.94 | 45.9 | 0.050 | Circle | 15.0 | 0.013 | 1.10 | 6.94 | 14.40 | 6,907.40 | 6,907.39 | 6,907.41 | 6,907.40 |
| LINE B- P02 | LINE B-MH02 | LINE B-MH01 | 6,900.37 | 6,897.69 | 268.3 | 0.010 | Circle | 18.0 | 0.013 | 1.60 | 4.29 | 10.50 | 6,900.85 | 6,898.09 | 6,901.02 | 6,898.37 |
| LINE B- P01 | LINE B-MH01 | LINE B-OF01 | 6,897.59 | 6,889.40 | 425.0 | 0.019 | Circle | 18.0 | 0.013 | 1.60 | 5.42 | 14.58 | 6,898.06 | 6,894.20 | 6,898.24 | 6,894.21 |

FlexTable: Manhole Table Active Scenario: 5-Year

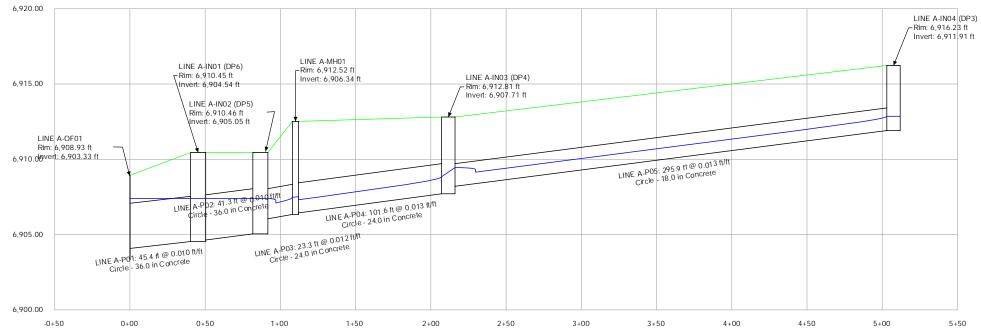
| Label | Elevation (Rim) (ft) | Flow (Total Out) (cfs) | Headloss Method | Headloss Coefficient (Standard) | Headloss (ft) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) |
|--------------------|----------------------------|------------------------------|--------------------|---------------------------------------|------------------|--------------------------------------|---------------------------------------|-----------------------------------|------------------------------------|
| | | ` ' | | , , | | | | | |
| LINE A-IN03 (DP4) | 6,912.81 | 10.00 | Standard | 1.320 | 0.61 | 6,909.45 | 6,908.84 | 6,909.68 | 6,909.30 |
| LINE B-MH02 | 6,911.39 | 1.60 | Standard | 1.020 | 0.18 | 6,901.02 | 6,900.85 | 6,901.05 | 6,901.02 |
| LINE C-IN01 (DP10) | 6,909.45 | 1.20 | Standard | 0.000 | 0.00 | 6,906.91 | 6,906.91 | 6,907.06 | 6,907.06 |
| LINE A-MH01 | 6,912.52 | 10.00 | Standard | 0.100 | 0.05 | 6,907.52 | 6,907.47 | 6,908.41 | 6,907.93 |
| LINE A-IN02 (DP5) | 6,910.46 | 11.50 | Standard | 0.100 | 0.01 | 6,907.41 | 6,907.40 | 6,907.71 | 6,907.46 |
| LINE A-IN01 (DP6) | 6,910.45 | 11.30 | Standard | 0.100 | 0.00 | 6,907.41 | 6,907.40 | 6,907.45 | 6,907.44 |
| LINE B-IN01 (DP9) | 6,907.92 | 0.40 | Standard | 0.000 | 0.00 | 6,902.15 | 6,902.15 | 6,902.23 | 6,902.23 |
| LINE A-INO4 (DP3) | 6,916.23 | 6.00 | Standard | 0.000 | 0.00 | 6,912.86 | 6,912.86 | 6,913.26 | 6,913.26 |
| LINE D-IN01 (DP8) | 6,910.66 | 1.10 | Standard | 0.100 | 0.00 | 6,907.40 | 6,907.40 | 6,907.40 | 6,907.41 |
| LINE D-IN02 (DP7) | 6,910.30 | 0.40 | Standard | 0.000 | 0.00 | 6,907.40 | 6,907.40 | 6,907.41 | 6,907.41 |
| LINE B-MH01 | 6,905.18 | 1.60 | Standard | 0.100 | 0.02 | 6,898.08 | 6,898.06 | 6,898.37 | 6,898.24 |

FlexTable: Outfall Table

Active Scenario: 5-Year

| Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Boundary Condition Type | Elevation (User Defined Tailwater) (ft) | Flow (Total Out) (cfs) | Hydraulic Grade (ft) | Energy Grade Line (ft) |
|-------------|-------------------------------|-------------------------------|-------------------------|--|---------------------------|-------------------------|------------------------------|
| LINE B-OF01 | 6,898.00 | 6,888.65 | User Defined Tailwater | 6,894.20 | 1.60 | 6,894.20 | 6,894.20 |
| LINE A-OF01 | 6,908.93 | 6,903.33 | User Defined Tailwater | 6,907.39 | 11.30 | 6,907.39 | 6,907.39 |
| LINE D-OF01 | 6,906.80 | 6,903.19 | User Defined Tailwater | 6,907.39 | 1.10 | 6,907.39 | 6,907.39 |

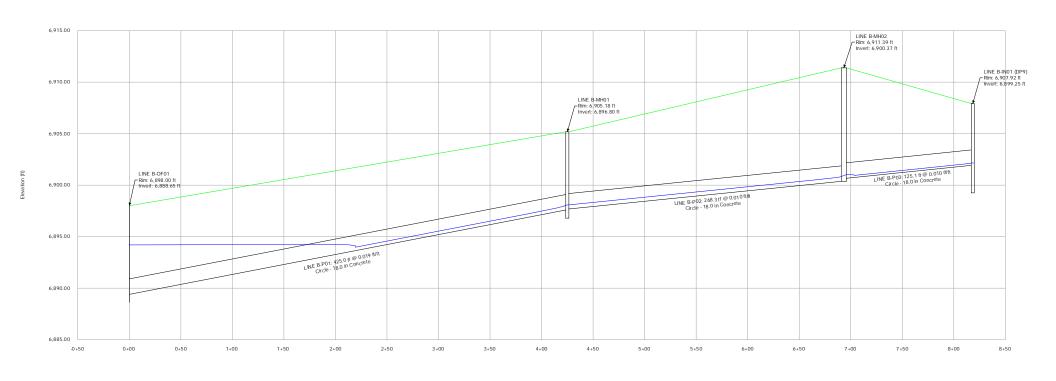




Station (ft)

Profile Report Engineering Profile - LINE B (MRS01_StormCAD.stsw)

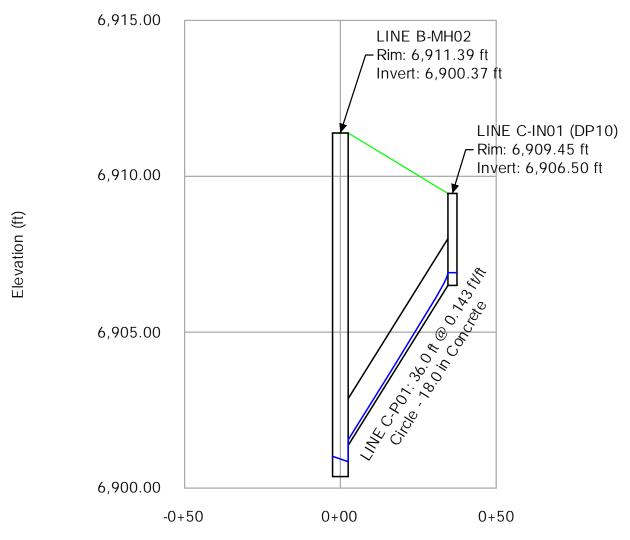
Active Scenario: 5-Year



Station (ft)

Profile Report
Engineering Profile - LINE C (MRS01_StormCAD.stsw)

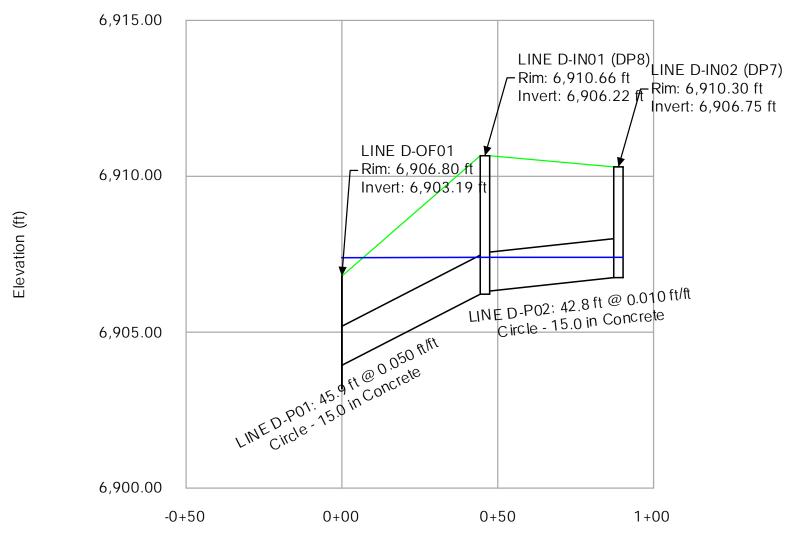
Active Scenario: 5-Year



Station (ft)

Profile Report Engineering Profile - LINE D (MRS01_StormCAD.stsw)

Active Scenario: 5-Year



Station (ft)

FlexTable: Conduit Table Active Scenario: 100-Year

| Label | Start Node | Cton Nodo | Laurant | Louisent | Longeth | Clana | Cootion | Diameter | Manainala | Пан | Valasit | Canaaitu | I lyalmayılla | Lludeaulia | Гионан | Гюски |
|----------------|-----------------------|----------------------|-------------------|------------------|-----------------|-----------------------|-----------------|------------------|----------------|---------------|-------------|-------------------|--------------------|--------------------|-----------------|-----------------|
| Label | Start Noue | Stop Node | Invert (Start) | Invert (Stop) | Length (User | Slope (Calculated) | Section Type | Diameter (in) | Manning's n | Flow (cfs) | Velocit | Capacity (Full | Hydraulic Grade | Hydraulic Grade | Energy Grade | Energy Grade |
| | | | (ft) | (5t0p) (ft) | Defined) | (ft/ft) | Туре | (111) | " | (013) | y (ft/s) | Flow) | Line (In) | Line | Line (In) | Line |
| | | | (11) | (11) | (ft) | (17/17) | | | | | (11/3) | (cfs) | (ft) | (Out) | (ft) | (Out) |
| | | | | | () | | | | | | | (0.0) | () | (ft) | (, | (ft) |
| LINE A- | LINE A-IN03 | | | | | | | | | | | | | , , | | |
| PO4 | (DP4) | LINE A-MH01 | 6,907.71 | 6,906.44 | 101.6 | 0.013 | Circle | 24.0 | 0.013 | 17.70 | 8.71 | 25.29 | 6,909.58 | 6,909.00 | 6,910.10 | 6,909.49 |
| LINE B- | LINE B-IN01 | LINE B-MH02 | 6,901.92 | 6,900.67 | 125.1 | 0.010 | Circle | 18.0 | 0.013 | 4.70 | 2.66 | 10.50 | 6,907.27 | 6,907.02 | 6.907.38 | 6,907.13 |
| P03 | (DP9) | 22 502 | 0,701.72 | 0,700.07 | .20 | 0.0.0 | 00.0 | | 0.0.0 | | 2.00 | | 0,707.127 | 0,707.102 | 0,707.00 | 3,707113 |
| LINE C- P01 | LINE C-IN01 (DP10) | LINE B-MH02 | 6,906.50 | 6,901.37 | 36.0 | 0.143 | Circle | 18.0 | 0.013 | 7.40 | 17.18 | 39.67 | 6,907.55 | 6,907.02 | 6,908.04 | 6,907.29 |
| LINE A- P03 | LINE A-MH01 | LINE A-IN02 (DP5) | 6,906.34 | 6,906.05 | 23.3 | 0.012 | Circle | 24.0 | 0.013 | 17.70 | 5.63 | 25.22 | 6,908.95 | 6,908.80 | 6,909.44 | 6,909.30 |
| LINE A- P02 | LINE A-IN02 (DP5) | LINE A-IN01 (DP6) | 6,905.05 | 6,904.64 | 41.3 | 0.010 | Circle | 36.0 | 0.013 | 20.90 | 2.96 | 66.43 | 6,908.79 | 6,908.75 | 6,908.93 | 6,908.89 |
| LINE A- P01 | LINE A-IN01 (DP6) | LINE A-OF01 | 6,904.54 | 6,904.08 | 45.4 | 0.010 | Circle | 36.0 | 0.013 | 21.10 | 2.99 | 67.16 | 6,908.74 | 6,908.69 | 6,908.87 | 6,908.83 |
| LINE A- P05 | LINE A-IN04 (DP3) | LINE A-IN03 (DP4) | 6,911.91 | 6,908.21 | 295.9 | 0.013 | Circle | 18.0 | 0.013 | 10.80 | 7.54 | 11.75 | 6,913.39 | 6,910.27 | 6,913.98 | 6,910.85 |
| LINE D- P02 | LINE D-IN02 (DP7) | LINE D-IN01 (DP8) | 6,906.75 | 6,906.32 | 42.8 | 0.010 | Circle | 15.0 | 0.013 | 0.80 | 0.65 | 6.47 | 6,908.75 | 6,908.74 | 6,908.76 | 6,908.75 |
| LINE D- P01 | LINE D-IN01 (DP8) | LINE D-OF01 | 6,906.22 | 6,903.94 | 45.9 | 0.050 | Circle | 15.0 | 0.013 | 2.10 | 1.71 | 14.40 | 6,908.74 | 6,908.69 | 6,908.78 | 6,908.74 |
| LINE B- P02 | LINE B-MH02 | LINE B-MH01 | 6,900.37 | 6,897.69 | 268.3 | 0.010 | Circle | 18.0 | 0.013 | 12.10 | 6.85 | 10.50 | 6,906.27 | 6,902.71 | 6,907.00 | 6,903.44 |
| LINE B- P01 | LINE B-MH01 | LINE B-OF01 | 6,897.59 | 6,889.40 | 425.0 | 0.019 | Circle | 18.0 | 0.013 | 12.10 | 6.85 | 14.58 | 6,902.64 | 6,897.00 | 6,903.37 | 6,897.73 |

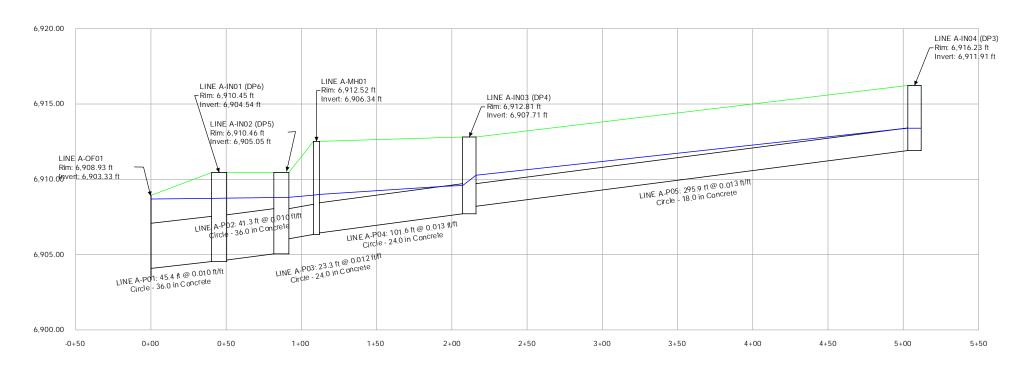
FlexTable: Manhole Table Active Scenario: 100-Year

| Label | Elevation (Rim) | Flow (Total Out) | Headloss Method | Headloss Coefficient | Headloss (ft) | Hydraulic Grade Line (In) | Hydraulic Grade Line (Out) | Energy Grade Line (In) | Energy Grade Line (Out) |
|--------------------|--------------------|---------------------|--------------------|-------------------------|------------------|------------------------------|-------------------------------|---------------------------|----------------------------|
| | (ft) | (cfs) | | (Standard) | | (ft) | (ft) | (ft) | (ft) |
| LINE A-IN03 (DP4) | 6,912.81 | 17.70 | Standard | 1.320 | 0.69 | 6,910.27 | 6,909.58 | 6,910.85 | 6,910.10 |
| LINE B-MH02 | 6,911.39 | 12.10 | Standard | 1.020 | 0.74 | 6,907.02 | 6,906.27 | 6,907.29 | 6,907.00 |
| LINE C-IN01 (DP10) | 6,909.45 | 7.40 | Standard | 0.000 | 0.00 | 6,907.55 | 6,907.55 | 6,908.04 | 6,908.04 |
| LINE A-MH01 | 6,912.52 | 17.70 | Standard | 0.100 | 0.05 | 6,909.00 | 6,908.95 | 6,909.49 | 6,909.44 |
| LINE A-IN02 (DP5) | 6,910.46 | 20.90 | Standard | 0.100 | 0.01 | 6,908.80 | 6,908.79 | 6,909.30 | 6,908.93 |
| LINE A-IN01 (DP6) | 6,910.45 | 21.10 | Standard | 0.100 | 0.01 | 6,908.75 | 6,908.74 | 6,908.88 | 6,908.87 |
| LINE B-IN01 (DP9) | 6,907.92 | 4.70 | Standard | 0.000 | 0.00 | 6,907.27 | 6,907.27 | 6,907.38 | 6,907.38 |
| LINE A-INO4 (DP3) | 6,916.23 | 10.80 | Standard | 0.000 | 0.00 | 6,913.39 | 6,913.39 | 6,913.98 | 6,913.98 |
| LINE D-IN01 (DP8) | 6,910.66 | 2.10 | Standard | 0.100 | 0.00 | 6,908.74 | 6,908.74 | 6,908.75 | 6,908.78 |
| LINE D-IN02 (DP7) | 6,910.30 | 0.80 | Standard | 0.000 | 0.00 | 6,908.75 | 6,908.75 | 6,908.76 | 6,908.76 |
| LINE B-MH01 | 6,905.18 | 12.10 | Standard | 0.100 | 0.07 | 6,902.71 | 6,902.64 | 6,903.44 | 6,903.37 |

FlexTable: Outfall Table

Active Scenario: 100-Year

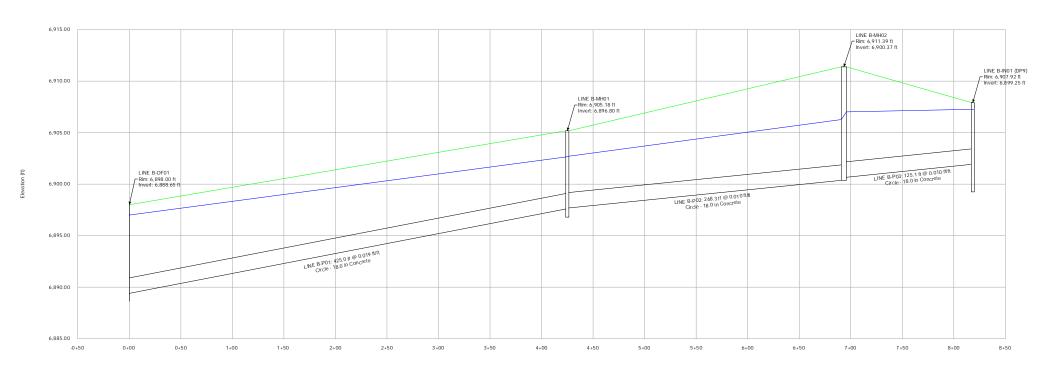
| Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Boundary Condition Type | Elevation (User Defined Tailwater) (ft) | Flow (Total Out) (cfs) | Hydraulic Grade (ft) | Energy Grade Line (ft) |
|-------------|-------------------------------|-------------------------------|-------------------------|--|---------------------------|-------------------------|------------------------------|
| LINE B-OF01 | 6,898.00 | 6,888.65 | User Defined Tailwater | 6,897.00 | 12.10 | 6,897.00 | 6,897.00 |
| LINE A-OF01 | 6,908.93 | 6,903.33 | User Defined Tailwater | 6,908.69 | 21.10 | 6,908.69 | 6,908.69 |
| LINE D-OF01 | 6,906.80 | 6,903.19 | User Defined Tailwater | 6,908.69 | 2.10 | 6,908.69 | 6,908.69 |



Station (ft)

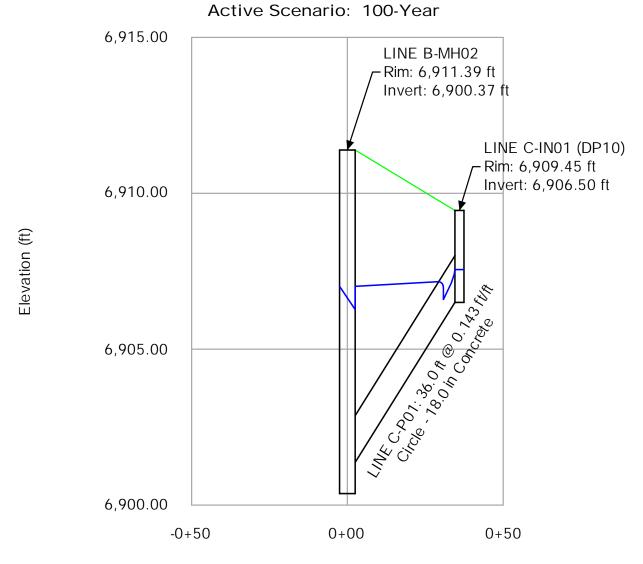
Profile Report Engineering Profile - LINE B (MRS01_StormCAD.stsw)

Active Scenario: 100-Year



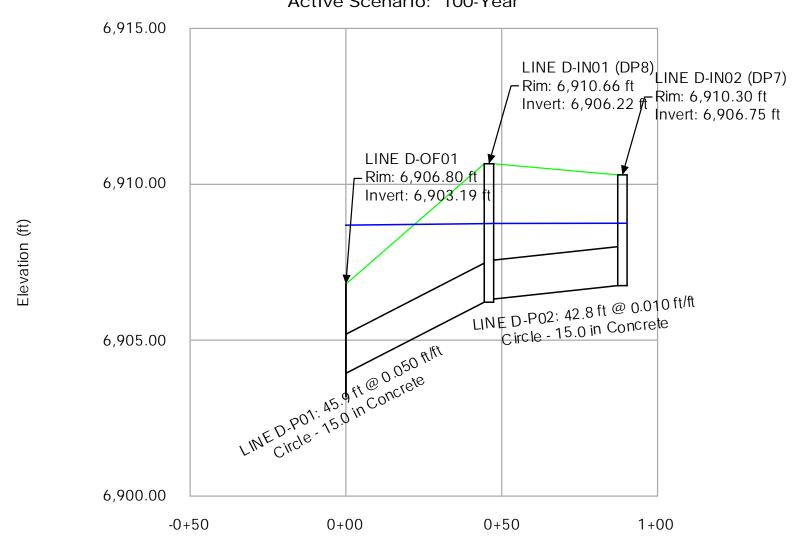
Station (ft)

Profile Report
Engineering Profile - LINE C (MRS01_StormCAD.stsw)



Station (ft)

Profile Report
Engineering Profile - LINE D (MRS01_StormCAD.stsw)
Active Scenario: 100-Year



Station (ft)

Type 13 Inlet Capacity Chart

Subdivision: Falcon Ranchettes Filing No. 1a
Location: El Paso County, CO

Project Name: Meridian Storage

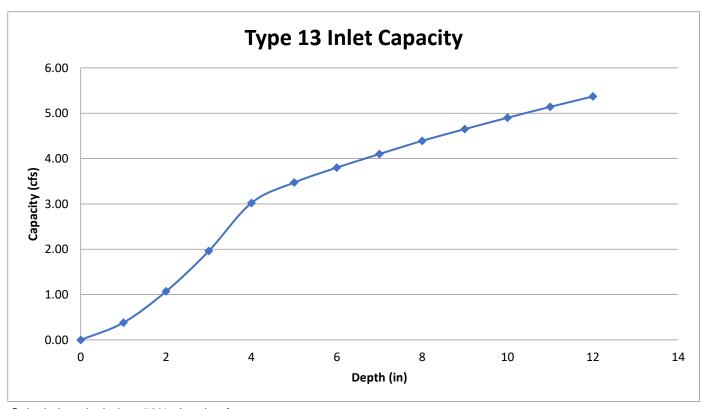
Project No.: MRS01
Calculated By: CMWJ

Checked By: BAS

Date: 9/8/23

Type 13 Inlet Capacity

| Type to mot dapacity | | | | | | |
|----------------------|----------------|----------------|----------------|--|--|--|
| Depth (in) | Single | Double | Triple | | | |
| Deptii (iii) | Capacity (cfs) | Capacity (cfs) | Capacity (cfs) | | | |
| 0 | 0.00 | 0.00 | 0.00 | | | |
| 1 | 0.38 | 0.76 | 1.14 | | | |
| 2 | 1.07 | 2.14 | 3.21 | | | |
| 3 | 1.96 | 3.92 | 5.88 | | | |
| 4 | 3.02 | 6.04 | 9.06 | | | |
| 5 | 3.47 | 6.94 | 10.41 | | | |
| 6 | 3.80 | 7.60 | 11.40 | | | |
| 7 | 4.10 | 8.20 | 12.30 | | | |
| 8 | 4.39 | 8.78 | 13.17 | | | |
| 9 | 4.65 | 9.30 | 13.95 | | | |
| 10 | 4.90 | 9.80 | 14.70 | | | |
| 11 | 5.14 | 10.28 | 15.42 | | | |
| 12 | 5.37 | 10.74 | 16.11 | | | |

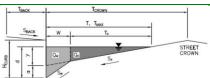


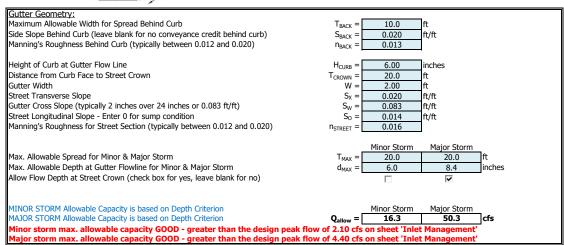
Calculations include a 50% clogging factor.

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

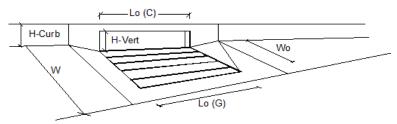
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Falcon Ranchettes Filing No. 1a (Meridian Storage)
Inlet ID: DP5





INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)



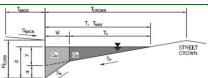
| Design Information (Input) | 1 | MINOR | MAJOR | _ |
|--|------------|-------------|--------------|--------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a') a _{LOCAL} | | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) No = | | 1 | 1 | |
| Length of a Single Unit Inlet (Grate or Curb Opening) | | 10.00 | 10.00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | | N/A | N/A | ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | $C_f(G) =$ | N/A | N/A | |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | $C_f(C) =$ | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Allowable Street Capacity' | | MINOR | Major | _ |
| Total Inlet Interception Capacity | | 2.1 | 4.2 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) Q _b | | 0.0 | 0.2 | cfs |
| Capture Percentage = Q_a/Q_0 C% | | 100 | 96 | % |

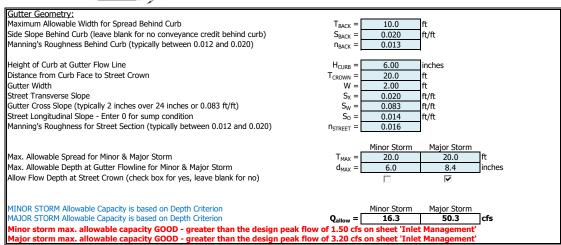
MRS01_MHFD-Inlet_v5.02.xlsm, DP5 9/10/2023, 10:04 PM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

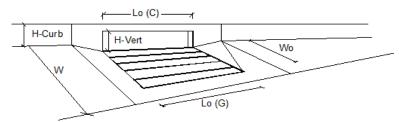
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Falcon Ranchettes Filing No. 1a (Meridian Storage)
Inlet ID: DP6





INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)



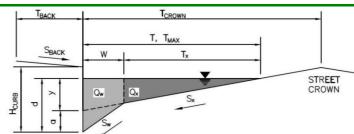
| Design Information (Input) Type of Inlet CDOT Type R Curb Opening | Type = | MINOR CDOT Type R | MAJOR Curb Opening | 1 |
|---|----------------------|----------------------|-----------------------|--------|
| Local Depression (additional to continuous gutter depression 'a') | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) No = | | 1 | 1 | |
| Length of a Single Unit Inlet (Grate or Curb Opening) Lo = | | | 10.00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) $W_0 =$ | | N/A | N/A | ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | $C_f(G) =$ | N/A | N/A | |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | $C_f(C) =$ | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Allowable Street Capacity' | | MINOR | MAJOR | |
| Total Inlet Interception Capacity | Q = | 1.5 | 3.2 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) $Q_b =$ | | 0.0 | 0.0 | cfs |
| Capture Percentage = Q_a/Q_o | C% = | 100 | 100 | % |

MRS01_MHFD-Inlet_v5.02.xlsm, DP6 9/10/2023, 10:05 PM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

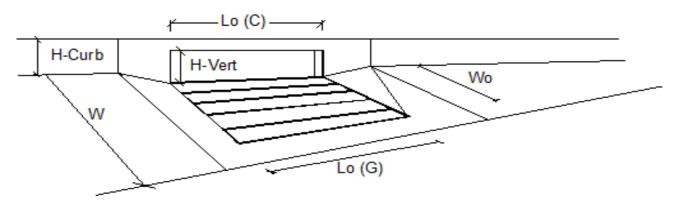
Project: Falcon Ranchettes Filing No. 1a (Meridian Storage)
Inlet ID: DP7



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb $T_{BACK} =$ 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{BACK} =$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 $n_{BACK} =$ $H_{CURB} =$ Height of Curb at Gutter Flow Line 6.00 inches Distance from Curb Face to Street Crown $T_{CROWN} =$ 20.0 Gutter Width W =2.00 Street Transverse Slope $S_X =$ 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition $S_0 =$ 0.008 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.016 n_{STREET} = Major Storm Minor Storm Max. Allowable Spread for Minor & Major Storm $T_{MAX} =$ 20.0 20.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm $d_{MAX} =$ inches 6.0 8.4 Allow Flow Depth at Street Crown (check box for yes, leave blank for no) MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 12.3 38.0 cfs Minor storm max. allowable capacity GOOD - greater than the design peak flow of 0.50 cfs on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design peak flow of 0.90 cfs on sheet 'Inlet Management'

MRS01_MHFD-Inlet_v5.02.xlsm, DP7

INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)



| Design Information (Input) | | MINOR | MAJOR | |
|---|------------|-------------|--------------|--------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a') | | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) | | 1 | 1 | |
| Length of a Single Unit Inlet (Grate or Curb Opening) | | 5.00 | 5.00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | | N/A | N/A | ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | $C_f(G) =$ | N/A | N/A | |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | $C_f(C) =$ | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Allowable Street Capacity' | | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity Q = | | 0.5 | 0.9 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) $Q_b =$ | | 0.0 | 0.0 | cfs |
| Capture Percentage = Q_a/Q_o C% = | | 100 | 100 | % |

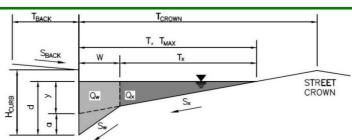
MRS01_MHFD-Inlet_v5.02.xlsm, DP7 10/19/2023, 5:10 PM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Falcon Ranchettes Filing No. 1a (Meridian Storage)

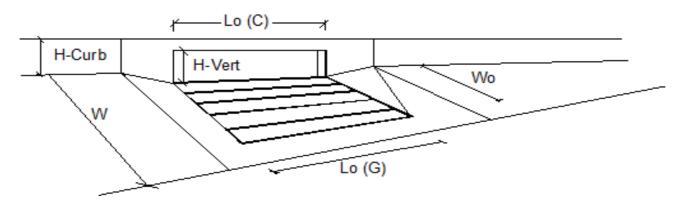
Inlet ID: DP8



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb $T_{BACK} =$ 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{BACK} =$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.013 $n_{BACK} =$ $H_{CURB} =$ Height of Curb at Gutter Flow Line 6.00 inches Distance from Curb Face to Street Crown $T_{CROWN} =$ 20.0 Gutter Width W =2.00 Street Transverse Slope $S_X =$ 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition $S_0 =$ 0.005 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.016 n_{STREET} = Major Storm Minor Storm Max. Allowable Spread for Minor & Major Storm $T_{MAX} =$ 20.0 20.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm $d_{MAX} =$ inches 6.0 8.4 Allow Flow Depth at Street Crown (check box for yes, leave blank for no) MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 9.7 30.1 cfs

Minor storm max. allowable capacity GOOD - greater than the design peak flow of 0.80 cfs on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design peak flow of 1.60 cfs on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)

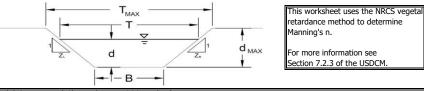


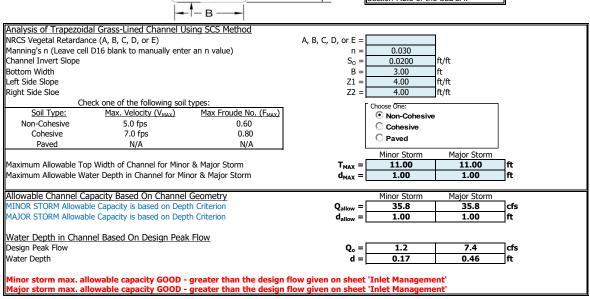
| Design Information (Input) | _ | MINOR | MAJOR | |
|---|--------|-------------|--------------|--------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a') a _{LOCAL} = | | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) | | 1 | 1 | |
| Length of a Single Unit Inlet (Grate or Curb Opening) | | 5.00 | 5.00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | | N/A | N/A | ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | | N/A | N/A | |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) $C_f(C) =$ | | | 0.10 | |
| Street Hydraulics: OK - Q < Allowable Street Capacity' | _ | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity | | 0.8 | 1.5 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) $Q_b =$ | | 0.0 | 0.1 | cfs |
| Capture Percentage = Q_a/Q_o | C% = | 100 | 93 | % |

MRS01_MHFD-Inlet_v5.02.xlsm, DP8 10/19/2023, 5:09 PM

MHFD-Inlet, Version 5.02 (August 2022) AREA INLET IN A SWALE

Falcon Ranchettes Filing No. 1a (Meridian Storage)





MRS01_MHFD-Inlet_v5.02.xlsm, DP10

MHFD-Inlet, Version 5.02 (August 2022) AREA INLET IN A SWALE

Falcon Ranchettes Filing No. 1a (Meridian Storage)

Inlet Design Information (Input) Type of Inlet CDOT Type C (Depressed) Inlet Type = CDOT Type C (Depressed) Angle of Inclined Grate (must be <= 30 degrees) Width of Grate 10.00 degrees W = 3.00 Length of Grate L= 3.00 Open Area Ratio A_{RATIO} = 0.70 $H_B = C_f =$. Height of Inclined Grate 0.52 Clogging Factor 0.50 $C_d = C_0 = 0$ Grate Discharge Coefficient 0.57 Orifice Coefficient Weir Coefficient 0.38 1.23 MINOR MAJOR Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) Total Inlet Interception Capacity (assumes clogged condition) d 1.17 **11.4** 1.46 **16.4** Qa = cfs cfs Bypassed Flow $Q_b =$ 0.0 0.0 Capture Percentage = Qa/Qo C% = % 100 100

Warning 04: Froude No. exceeds USDCM Volume I recommendation.

PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Falcon Ranchettes Filing No. 1A

Location: CO, Colorado Springs

Project Name: Meridian Storage

Project No.: MRS01
Calculated By: CMWJ

Checked By: BAS
Date: 4/26/24

| | STC | ORM DRAIN SYSTEM | |
|-------------------------|---------|------------------|--|
| | DP-12 | DP-13 | |
| Q100 (cfs) | 0.4 | 2.1 | Flows are the greater of proposed vs. future |
| D or H (in) | 6 | 6 | vs. ratare |
| W (ft) | 2 | 2 | |
| Slope (%) | 1.40 | 1.40 | |
| Yn (in) | 6.00 | 6.00 | |
| Yt (ft) | Unknown | Unknown | If "unknown" Yt/D=0.4 |
| Yt/D, Yt/H | 0.40 | 0.40 | Per section 11-3 |
| Supercritical | Yes | Yes | |
| Q/D^2.5, Q/WH^1.5 | 0.63 | 3.02 | |
| Q/D^1.5, Q/WH^0.5 | | | |
| Da, Ha (in) * | 6.00 | 6.00 | Da=0.5(D+Yn), Ha=0.5(H+Yn) |
| Q/Da^1.5, Q/WHa^0.5 * | 0.32 | 1.51 | |
| d50 (in), Required | 0.13 | 0.63 | |
| Required Riprap Size | L | L | Fig. 8-34 |
| Use Riprap Size | L | L | |
| d50 (in) | 9 | 9 | Fig. 8-34 |
| 1/(2 tan q) | 4.75 | 2.90 | Fig. 9-35 OR Fig 9-36 |
| Erosive Soils | Yes | Yes | |
| At | 0.08 | 0.39 | At=Q/5.5 |
| L | -7.6 | -0.2 | L=(1/(2 tan q))(At/Yt - D) |
| Min L | 1.5 | 1.5 | Min L=3D or 3H |
| Max L | 5.0 | 5.0 | Max L=10D or 10H |
| Length (ft) | 1.5 | 1.5 | |
| Bottom Width (ft) | 6.0 | 6.0 | Width=3D (Minimum) |
| Riprap Depth (in) | 18 | 18 | Depth=2(d50) |
| Type II Base Depth (in) | 6 | 6 | Table 8-34 fine grained soils) |
| Cutoff Wall | No | No | |
| Cutoff Wall Depth (ft) | | | Depth of Riprap and Base |
| Cutoff Wall Width (ft) | | | |

Note: No Type II Base to be used if Soil Riprap is specified within the plans

CEDP--CONCRETE ENERGY DISIPATING BASIN



^{*} For use when the flow in the culvert is supercritical (and less than full).

Unnamed Tributary to Black Squirrel Creek - East Branch (RMT064) Project Description Friction Method Manning Formula Solve For Normal Depth Input Data 0.035 Roughness Coefficient 0.00300 ft/ft Channel Slope Left Side Slope 4.00 ft/ft (H:V) Right Side Slope 4.00 ft/ft (H:V) 15.00 Bottom Width ft 925.00 Discharge Results Normal Depth 5.15 Flow Area 183.50 ft² Wetted Perimeter 57.49 ft Hydraulic Radius 3.19 ft Top Width 56.22 ft Critical Depth 3.58 ft Critical Slope 0.01368 ft/ft Velocity 5.04 ft/s Velocity Head 0.39 ft Specific Energy 5.55 ft Froude Number 0.49 Flow Type Subcritical

| G۷ | 'F | In | but | Data |
|----|----|----|-----|------|
| | | | | |

| Downstream Depth | 0.00 | ft |
|------------------|------|----|
| Length | 0.00 | ft |
| Number Of Steps | 0 | |

GVF Output Data

Upstream Depth

| · | | |
|---------------------|----------|-------|
| Profile Description | | |
| Profile Headloss | 0.00 | ft |
| Downstream Velocity | Infinity | ft/s |
| Upstream Velocity | Infinity | ft/s |
| Normal Depth | 5.15 | ft |
| Critical Depth | 3.58 | ft |
| Channel Slope | 0.00300 | ft/ft |
| Critical Slope | 0.01368 | ft/ft |
| | | |

0.00 ft

APPENDIX E

DETENTION POND TRIBUTARY AREAS

Subdivision: Falcon Ranchettes Filing No. 1A

Location: CO, Colorado Springs

Project Name: Meridian Storage

Project No.: MRS01

Calculated By: CMWJ

Checked By: BAS

Date: 4/26/24

Detention Pond #1

| Basin | Area | % lmp |
|-------|------|-------|
| B-1 | 1.46 | 94.7 |
| B-2 | 1.18 | 98.3 |
| B-3 | 0.95 | 61.9 |
| B-4 | 0.52 | 79.3 |
| B-5 | 0.13 | 84.9 |
| B-6 | 0.16 | 69.4 |
| B-7 | 0.56 | 14.3 |
| * C-1 | 0.29 | 100.0 |
| * C-2 | 3.12 | 100.0 |
| * C-3 | 0.29 | 100.0 |
| OS-3 | 0.24 | 2.0 |
| OS-5 | 0.19 | 2.0 |
| | | |
| Total | 9.09 | 83.1 |

*All "C" group basins' imperviousness changed to 100%. This will accomdate the future build out of the associated lot and provide full spectrum detention and avoid construction of an additional pond.



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Falcon Ranchettes Filing No. 1a (Meridian Storage)

1.19

1.50

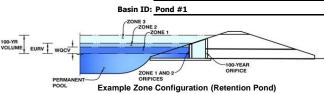
1.75

2.00

2.25

2.52

3.68



| Watershed | Information |
|-----------|-------------|

| Selected BMP Type = | EDB | | | | |
|--|--------|---------|--|--|--|
| Watershed Area = | 9.09 | acres | | | |
| Watershed Length = | 1,055 | ft | | | |
| Watershed Length to Centroid = | 300 | ft | | | |
| Watershed Slope = | 0.018 | ft/ft | | | |
| Watershed Imperviousness = | 83.10% | percent | | | |
| Percentage Hydrologic Soil Group A = | 100.0% | percent | | | |
| Percentage Hydrologic Soil Group B = | 0.0% | percent | | | |
| Percentage Hydrologic Soil Groups C/D = | 0.0% | percent | | | |
| Target WQCV Drain Time = | 40.0 | hours | | | |
| Location for 1-hr Rainfall Depths = User Input | | | | | |

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

| the embedded Colorado Urban Hydro | | |
|--|-------|-----------|
| Water Quality Capture Volume (WQCV) = | 0.264 | acre-feet |
| Excess Urban Runoff Volume (EURV) = | 1.004 | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) = | 0.691 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) = | 0.893 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) = | 1.057 | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) = | 1.243 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) = | 1.426 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 1.635 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.68 in.) = | 2.513 | acre-feet |
| Approximate 2-yr Detention Volume = | 0.660 | acre-feet |
| Approximate 5-yr Detention Volume = | 0.858 | acre-feet |
| Approximate 10-yr Detention Volume = | 1.022 | acre-feet |
| Approximate 25-yr Detention Volume = | 1.211 | acre-feet |
| Approximate 50-yr Detention Volume = | 1.321 | acre-feet |
| Approximate 100-yr Detention Volume = | 1.421 | acre-feet |

Define Zones and Basin Geometry

| 91 | ine Zones and Basin Geometry | | |
|----|---|-------|-----------------|
| | Zone 1 Volume (WQCV) = | 0.264 | acre-feet |
| | Zone 2 Volume (EURV - Zone 1) = | 0.740 | acre-feet |
| | Zone 3 Volume (100-year - Zones 1 & 2) = | 0.417 | acre-feet |
| | Total Detention Basin Volume = | 1.421 | acre-feet |
| | Initial Surcharge Volume (ISV) = | user | ft³ |
| | Initial Surcharge Depth (ISD) = | user | ft |
| | Total Available Detention Depth $(H_{total}) =$ | user | ft |
| | Depth of Trickle Channel $(H_{TC}) =$ | user | ft |
| | Slope of Trickle Channel (S_{TC}) = | user | ft/ft |
| | Slopes of Main Basin Sides (S _{main}) = | user | H:V |
| | Basin Length-to-Width Ratio ($R_{L/W}$) = | user | |
| | | | - - |
| | Initial Surcharge Area $(A_{ISV}) =$ | user | ft ² |
| | Surcharge Volume Length $(L_{ISV}) =$ | user | ft |
| | Surcharge Volume Width $(W_{ISV}) =$ | user | ft |
| | Depth of Basin Floor $(H_{FLOOR}) =$ | user | ft |
| | Length of Basin Floor $(L_{FLOOR}) =$ | user | ft |
| | Width of Basin Floor (W_{FLOOR}) = | user | ft |
| | Area of Basin Floor $(A_{FLOOR}) =$ | user | ft ² |
| | Volume of Basin Floor $(V_{FLOOR}) =$ | user | ft ³ |
| | Depth of Main Basin $(H_{MAIN}) =$ | user | ft |
| | Length of Main Basin $(L_{MAIN}) =$ | user | ft |
| | Width of Main Basin (W_{MAIN}) = | user | ft |
| | | | |

Area of Main Basin (A_{MAIN})

Volume of Main Basin (V_{MAIN}) Calculated Total Basin Volume (V_{total}) = user

user

| 2021 | | | _ | | | | | |
|-------------------------|--------------------------------|---------------|------------------------------------|----------------|---------------|----------------------------|---|----------------|
| AR DE | Depth Increment = | | ft | | | | | |
| on Pond) | Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft ²) | Optional Override Area (ft ²) | Area (acre) |
| 6902.167 | Top of Micropool | | 0.00 | | | | 129 | 0.003 |
| 6902.50 | Trickle Chan. Inv. | | 0.33 | | | | 129 | 0.003 |
| | 6903 | | 0.83 | | | | 318 | 0.007 |
| | 6904 | | 1.83 | | | | 3,600 | 0.083 |
| | 6905 | | 2.83 | | | | 8,014 | 0.184 |
| | 6906 | | 3.83 | | | | 11,924 | 0.274 |
| | 6907 | | 4.83 | | | | 13,843 | 0.318 |
| | 6908 | | 5.83 | | | | 15,900 | 0.365 |
| | 6909 | | 6.83 | | | | 18,058 | 0.415 |
| | 6910 | | 7.83 | | | | 20,359 | 0.467 |
| 6910.50 | Spillway Invert | | 8.33 | | | | 21,511 | 0.494 |
| | 6911 | | 8.83 | | | | 22,752 | 0.522 |
| | 6912 | | 9.83 | | | | 25,223 | 0.579 |
| | | | | | | | | |
| Optional User Overrides | | | | | | | | |
| acre-feet | | | | | | | | |
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Volume

(ft 3)

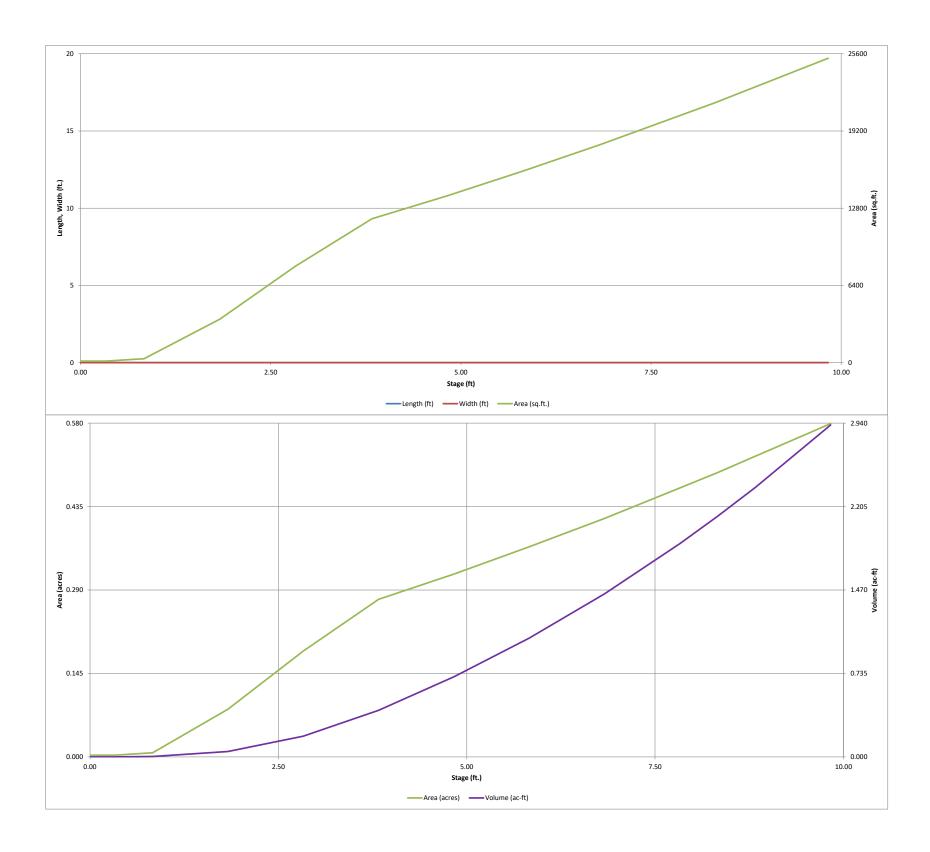
43

Volume (ac-ft)

0.001

| | | Trickle Chan. Inv. | 0.33 | | | 129 | 0.003 | 43 | 0.001 |
|---|-----------|--------------------|----------|------|---|--------|---------|--|--|
| | | 6903 | 0.83 | | | 318 | 0.007 | 154 | 0.004 |
| | | | | | | | | | |
| | | 6904 | 1.83 | | | 3,600 | 0.083 | 2,108 | 0.048 |
| | | 6905 | 2.83 | | | 8,014 | 0.184 | 7,915 | 0.182 |
| | | 6906 | 3.83 | | - | 11,924 | 0.274 | 17,884 | 0.411 |
| | | 6907 | 4.83 | | | 13,843 | 0.318 | 30,768 | 0.706 |
| | | | | | | | | | |
| | | 6908 | 5.83 | | | 15,900 | 0.365 | 45,639 | 1.048 |
| | | 6909 | 6.83 | | | 18,058 | 0.415 | 62,618 | 1.438 |
| | | 6910 | 7.83 | | | 20,359 | 0.467 | 81,827 | 1.878 |
| | 6010 50 | | | | - | | | | |
| | 6910.50 | | 8.33 | | | 21,511 | 0.494 | 92,294 | 2.119 |
| | | 6911 | 8.83 | | | 22,752 | 0.522 | 103,360 | 2.373 |
| | | 6912 | 9.83 | | - | 25,223 | 0.579 | 127,347 | 2.923 |
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| r | Overrides | | | | | | | | |
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MRS01_MHFD-Detention_v4-06.xlsm, Basin

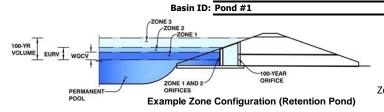


MRS01_MHFD-Detention_v4-06.xlsm, Basin 5/6/2024, 2:26 PM

ON BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: Falcon Ranchettes Filing No. 1a (Meridian Storage)



| | Estimated | Estimated | |
|-------------------|-------------------|----------------|----------------------|
| _ | Stage (ft) | Volume (ac-ft) | Outlet Type |
| Zone 1 (WQCV) | 3.24 | 0.264 | Orifice Plate |
| Zone 2 (EURV) | 5.71 | 0.740 | Orifice Plate |
| Zone 3 (100-year) | 6.80 | 0.417 | Weir&Pipe (Restrict) |
| • | Total (all zones) | 1.421 | |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface) Underdrain Orifice Diameter = N/A inches

Underdrain Orifice Area N/A Underdrain Orifice Centroid = N/A

Calculated Parameters for Underdrain ft² feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

| Centroid of Lowest Orifice = | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
|--|------|---|
| Depth at top of Zone using Orifice Plate = | 5.71 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing = | N/A | inches |

Orifice Plate: Orifice Area per Row = sq. inches

Calculated Parameters for Plate WQ Orifice Area per Row = ft² N/A Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area : N/A ft²

<u>User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)</u>

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 1.67 | 3.50 | | | | | |
| Orifice Area (sq. inches) | 0.99 | 1.22 | 5.94 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A Depth at top of Zone using Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = N/A N/A feet Vertical Orifice Diameter = N/A N/A

| User Input: Overflow Weir (Dropbox with Flat or | Sloped Grate and (| Outlet Pipe OR Rec | tangular/Trapezoidal Weir and No Outlet Pipe) | Calculated Paramet | ters for Overflow W | eir |
|---|--------------------|--------------------|--|--------------------|---------------------|-----------------|
| | Zone 3 Weir | Not Selected | | Zone 3 Weir | Not Selected | ĺ |
| Overflow Weir Front Edge Height, Ho = | 5.75 | N/A | ft (relative to basin bottom at Stage = 0 ft) $$ Height of Grate Upper Edge, $H_t =$ | 6.48 | N/A | feet |
| Overflow Weir Front Edge Length = | 2.92 | N/A | feet Overflow Weir Slope Length = | 3.01 | N/A | feet |
| Overflow Weir Grate Slope = | 4.00 | N/A | H:V Grate Open Area / 100-yr Orifice Area = | 13.18 | N/A | 1 |
| Horiz. Length of Weir Sides = | 2.92 | N/A | feet Overflow Grate Open Area w/o Debris = | 6.95 | N/A | ft ² |
| Overflow Grate Type = | Close Mesh Grate | N/A | Overflow Grate Open Area w/ Debris = | 3.48 | N/A | ft ² |
| Debris Clogging % = | 50% | N/A | % | | - | |

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)</u> Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

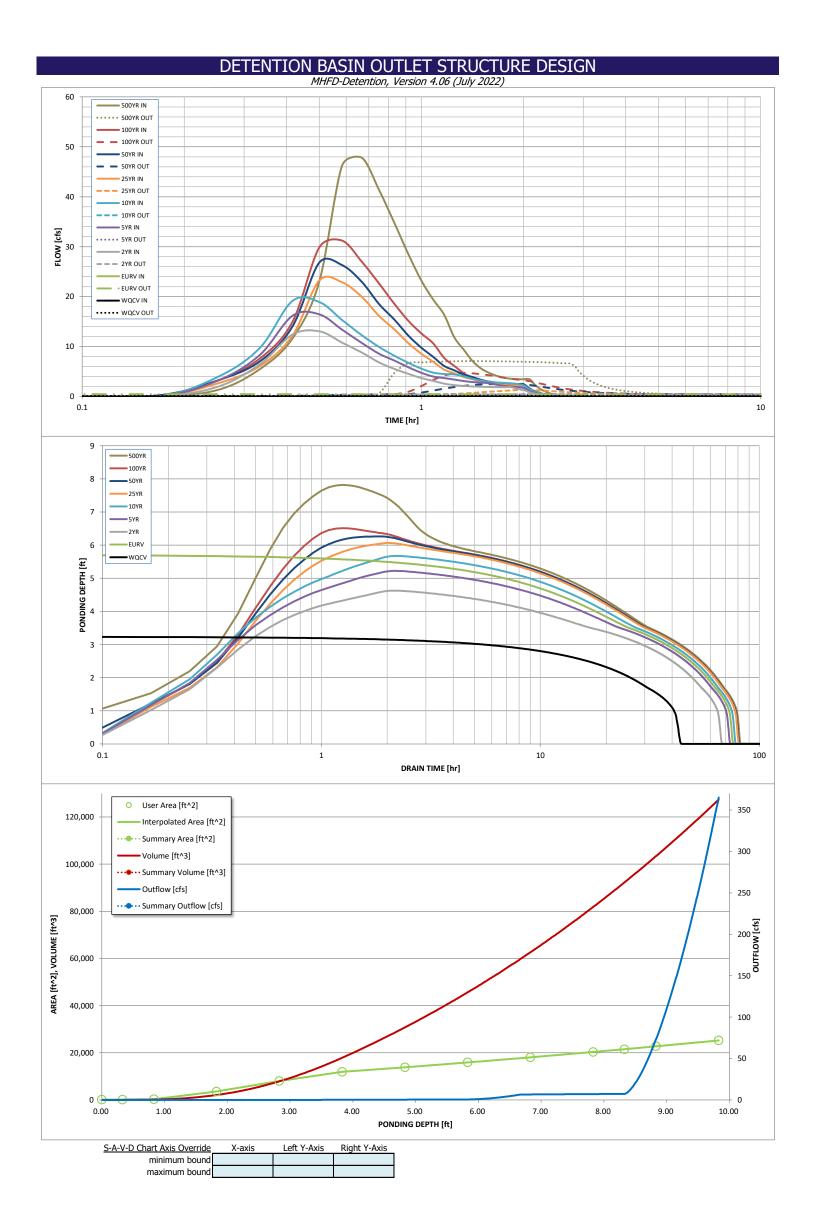
| | Zone 3 Restrictor | Not Selected | | | Zone 3 Restrictor | Not Selected | |
|---|-------------------|--------------|--|------------------------------|-------------------|--------------|-----------------|
| Depth to Invert of Outlet Pipe = | 0.25 | N/A | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area = | 0.53 | N/A | ft ² |
| Outlet Pipe Diameter = | 18.00 | N/A | inches | Outlet Orifice Centroid = | 0.30 | N/A | feet |
| Restrictor Plate Height Above Pipe Invert = | 6.10 | • | inches Half-Central Angle o | f Restrictor Plate on Pipe = | 1.24 | N/A | radians |

Calculated Parameters for Spillway User Input: Emergency Spillway (Rectangular or Trapezoidal) ft (relative to basin bottom at Stage = 0 ft) Spillway Invert Stage= Spillway Design Flow Depth= 0.32 feet

| Spilivay Invert Stage | 0.55 | re (relative to basin bottom at stage – o re) | Spilittay Design Flow Depart | 0.52 | ICCC |
|-------------------------------------|-------|---|------------------------------------|------|---------|
| Spillway Crest Length = | 60.00 | feet | Stage at Top of Freeboard = | 9.83 | feet |
| Spillway End Slopes = | 4.00 | H:V | Basin Area at Top of Freeboard = | 0.58 | acres |
| Freeboard above Max Water Surface = | 1.18 | feet | Basin Volume at Top of Freeboard = | 2.92 | acre-ft |
| , | | | | | • |

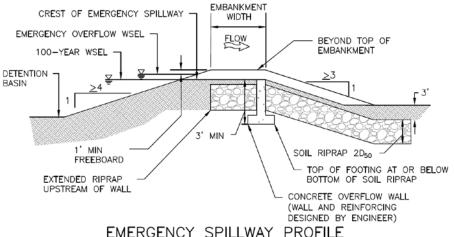
| Routed Hydrograph Results | The user can over | ride the default CUF | HP hydrographs and | d runoff volumes by | entering new value | es in the Inflow Hya | rographs table (Col | umns W through A | F). |
|---|-------------------|----------------------|--------------------|---------------------|--------------------|----------------------|---------------------|------------------|----------------|
| Design Storm Return Period = | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
| One-Hour Rainfall Depth (in) = | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.68 |
| CUHP Runoff Volume (acre-ft) = | 0.264 | 1.004 | 0.691 | 0.893 | 1.057 | 1.243 | 1.426 | 1.635 | 2.513 |
| Inflow Hydrograph Volume (acre-ft) = | N/A | N/A | 0.691 | 0.893 | 1.057 | 1.243 | 1.426 | 1.635 | 2.513 |
| CUHP Predevelopment Peak Q (cfs) = | N/A | N/A | 0.1 | 0.1 | 0.2 | 1.8 | 3.6 | 5.9 | 15.0 |
| OPTIONAL Override Predevelopment Peak Q (cfs) = | N/A | N/A | | | | | | | |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | N/A | N/A | 0.01 | 0.02 | 0.02 | 0.20 | 0.40 | 0.65 | 1.65 |
| Peak Inflow Q (cfs) = | N/A | N/A | 13.0 | 16.5 | 19.1 | 23.2 | 26.8 | 31.2 | 47.8 |
| Peak Outflow Q (cfs) = | 0.1 | 0.5 | 0.4 | 0.4 | 0.5 | 1.3 | 2.5 | 4.7 | 7.1 |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 2.8 | 2.3 | 0.7 | 0.7 | 0.8 | 0.5 |
| Structure Controlling Flow = | Plate | Plate | Plate | Plate | Plate | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | N/A | N/A | 0.1 | 0.3 | 0.6 | 0.9 |
| Max Velocity through Grate 2 (fps) = | | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 40 | 65 | 60 | 64 | 67 | 68 | 67 | 66 | 62 |
| Time to Drain 99% of Inflow Volume (hours) = | 42 | 72 | 64 | 70 | 73 | 75 | 75 | 75 | 73 |
| Maximum Ponding Depth (ft) = | 3.24 | 5.71 | 4.63 | 5.22 | 5.68 | 6.07 | 6.26 | 6.52 | 7.82 |
| Area at Maximum Ponding Depth (acres) = | 0.22 | 0.36 | 0.31 | 0.34 | 0.36 | 0.38 | 0.39 | 0.40 | 0.47 |
| Maximum Volume Stored (acre-ft) = | 0.265 | 1.004 | 0.641 | 0.834 | 0.990 | 1.133 | 1.209 | 1.307 | 1.874 |

MRS01_MHFD-Detention_v4-06.xlsm, Outlet Structure 5/6/2024, 2:26 PM

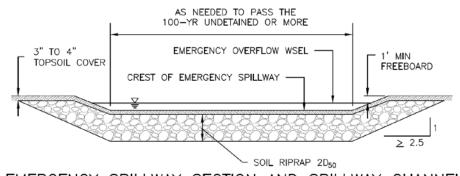


MRS01_MHFD-Detention_v4-06.xlsm, Outlet Structure 5/6/2024, 2:26 PM

Chapter 12 Storage



EMERGENCY SPILLWAY PROFILE



EMERGENCY SPILLWAY SECTION AND SPILLWAY

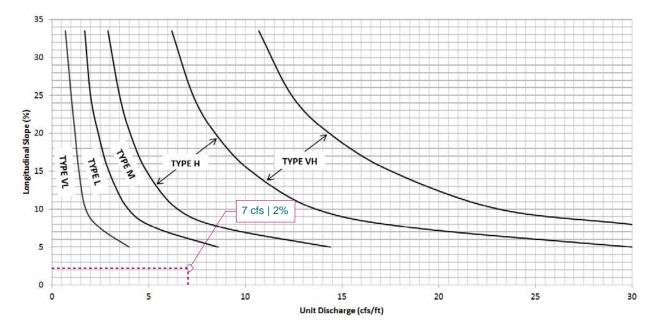


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

Micropool/ISV SIZING CALCULATIONS

 Subdivision:
 Falcon Ranchettes Filing No. 1a
 Project Name:
 Meridian Storage

 Location:
 CO, El Paso County
 Project No.:
 MRS01

 Calculated By:
 CMWJ

 Checked By:
 BAS

Date: 5/6/24

| | Pond #1 | | |
|---------------------------------------|---------|--|--|
| WQCV Volume (Ac-Ft) | 0.265 | | From MHFD-Detention Spreadsheet |
| Provided ISV Depth (in) | 4.00 | | 4" Min. per USDCM, Volume 3 |
| Provided Micropool/ISV Area (Sq. Ft.) | 129.00 | | |
| Provided ISV Volume (Cu. Ft.) | 43.00 | | |
| Micropool/ISV Deisgn Results | | | |
| Minimum Micropool Area (Sq. Ft.) | 104 | | Assuming ISV above - Min. 10 ft ² per USDCM, Volume 3 |
| Required ISV Volume (Cu. Ft.) | 35 | | 0.3% of WQCV, per USDCM, Volume 3 |
| Is Required Micropool Area Met? | YES | | |
| Is Required ISV Volume Met? | YES | | |



FOREBAY TRIBUTARY AREAS

Subdivision: Falcon Ranchettes Filing No. 1A **Project Name:** Meridian Storage

 Location:
 CO, Colorado Springs
 Project No.:
 MRS01

Calculated By: CMWJ
Checked By: BAS

Date: 4/26/24

Forebay A

| Basin | Area | % lmp |
|-------|------|-------|
| B-1 | 1.46 | 94.66 |
| B-2 | 1.18 | 98.3 |
| B-3 | 0.95 | 61.86 |
| B-4 | 0.52 | 79.25 |
| * C-1 | 0.29 | 100 |
| | | |
| Total | 4.4 | 87.1 |

*All "C" group basins' imperviousness changed to 100%. This will accomdate the future build out of the associated lot and provide sufficient area and imperviousness for future access drives.



FOREBAY TRIBUTARY AREAS

Subdivision: Falcon Ranchettes Filing No. 1A **Project Name:** Meridian Storage

 Location:
 CO, Colorado Springs
 Project No.:
 MRS01

Calculated By: CMWJ
Checked By: BAS

Date: 4/26/24

Forebay B

| Basin | Area | % lmp |
|-------|------|-------|
| OS-1 | 3.89 | 10.91 |
| OS-2 | 2.35 | 14.01 |
| OS-3 | 0.24 | 2 |
| C-4 | 0.09 | 2 |
| | | |
| Total | 6.57 | 11.6 |



FOREBAY TRIBUTARY AREAS

Subdivision: Falcon Ranchettes Filing No. 1A **Project Name:** Meridian Storage

Location:CO, Colorado SpringsProject No.:MRS01

Calculated By: CMWJ
Checked By: BAS

Checked by: BAS

Date: 4/26/24

Forebay D

| | Basin | Area | % lmp |
|---|-------|------|-------|
| | B-5 | 0.13 | 84.92 |
| | B-6 | 0.16 | 69.35 |
| * | C-3 | 0.29 | 100 |
| | | | |
| Ī | Total | 0.58 | 88.2 |

*All "C" group basins' imperviousness changed to 100%. This will accomdate the future build out of the associated lot and provide sufficient area and imperviousness for future access drives.



FOREBAY SIZING CALCULATIONS

Subdivision: Falcon Ranchettes Filing No. 1a **Project Name:** Meridian Storage

Location: CO, El Paso County Project No.: MRS01

Calculated By: CMWJ
Checked By: BAS

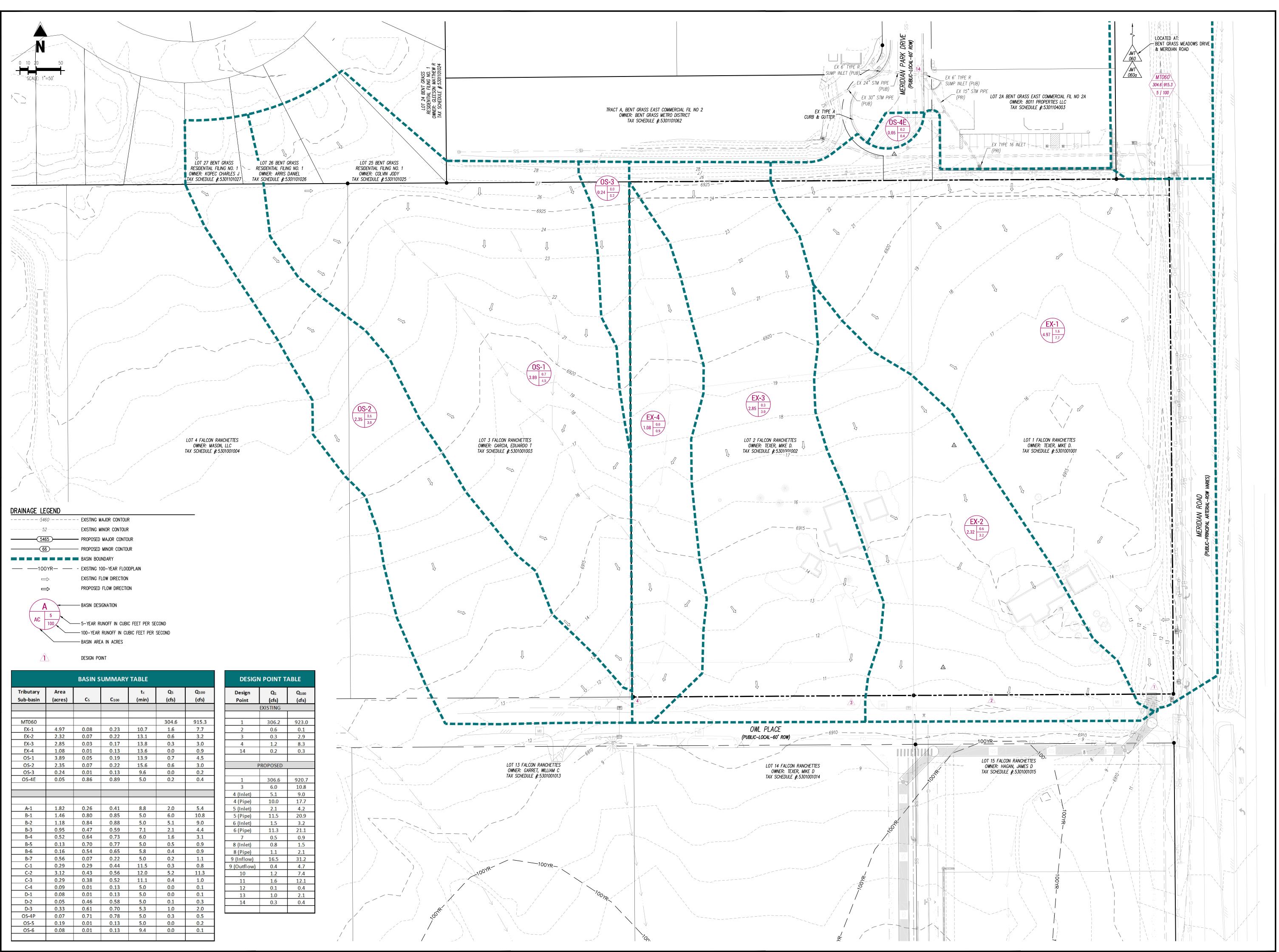
Date: 5/6/24

Pond #1

| | Forebay A | Forebay B | Forebay D | |
|--------------------------------|-----------|-----------|-----------|---|
| Impervious % (I) | 87.1% | 11.60% | 88.20% | Total impervious area of contributing upstream basins |
| WQCV Drain Time Coeff (a) | 1 | 1 | 1 | a = 1 for 40 Hr WQCV Drain Time |
| Tributary Area (Ac) | 4.40 | 6.57 | 0.58 | |
| Forebay Depth (Ft) | 1.50 | 1.50 | 1.50 | (see Table EDB-4 of the USDCM Volume 3 for depth requirement) |
| % of WQCV for Forebay Volume | 3.0% | 3.0% | 3.0% | (see Table EDB-4 of the USDCM Volume 3 for requirement) |
| 100-year Discharge (Q) | 21.1 | 12.10 | 2.10 | 100-Year Flow entering Forebay (undetained) |
| WQCV Depth (in) | 0.38 | 0.08 | 0.39 | WQCV Depth = a(0.91*I ³ - 1.19*I ² + 0.78*I) |
| WQCV Volume (Ac-Ft) | 0.14 | 0.04 | 0.02 | |
| Forebay Volume (Cu. Ft.) | 181 | 54 | 24 | |
| Forebay Discharge (Q) | 0.42 | 0.24 | 0.04 | (Release 2% of 100-year discharge via notch or berm/pipe configuration) |
| Forebay Notch Height (in) | 15.00 | 15.00 | 15.00 | (3" depression @ top of forebay assumed per COS DCM Volume 1, 13-30) |
| Forebay Deisgn Results | | | | |
| Minimum Forebay Area (Sq. Ft.) | 121 | 36 | 16 | |
| Forebay Notch width (in) | 3 | 3 | 3 | From $Q=C_w*W*H^{1.5}$ assuming $C_w=3.33$ for sharp-crested weir - If notch width <3", use 3" minimum. |



APPENDIX F



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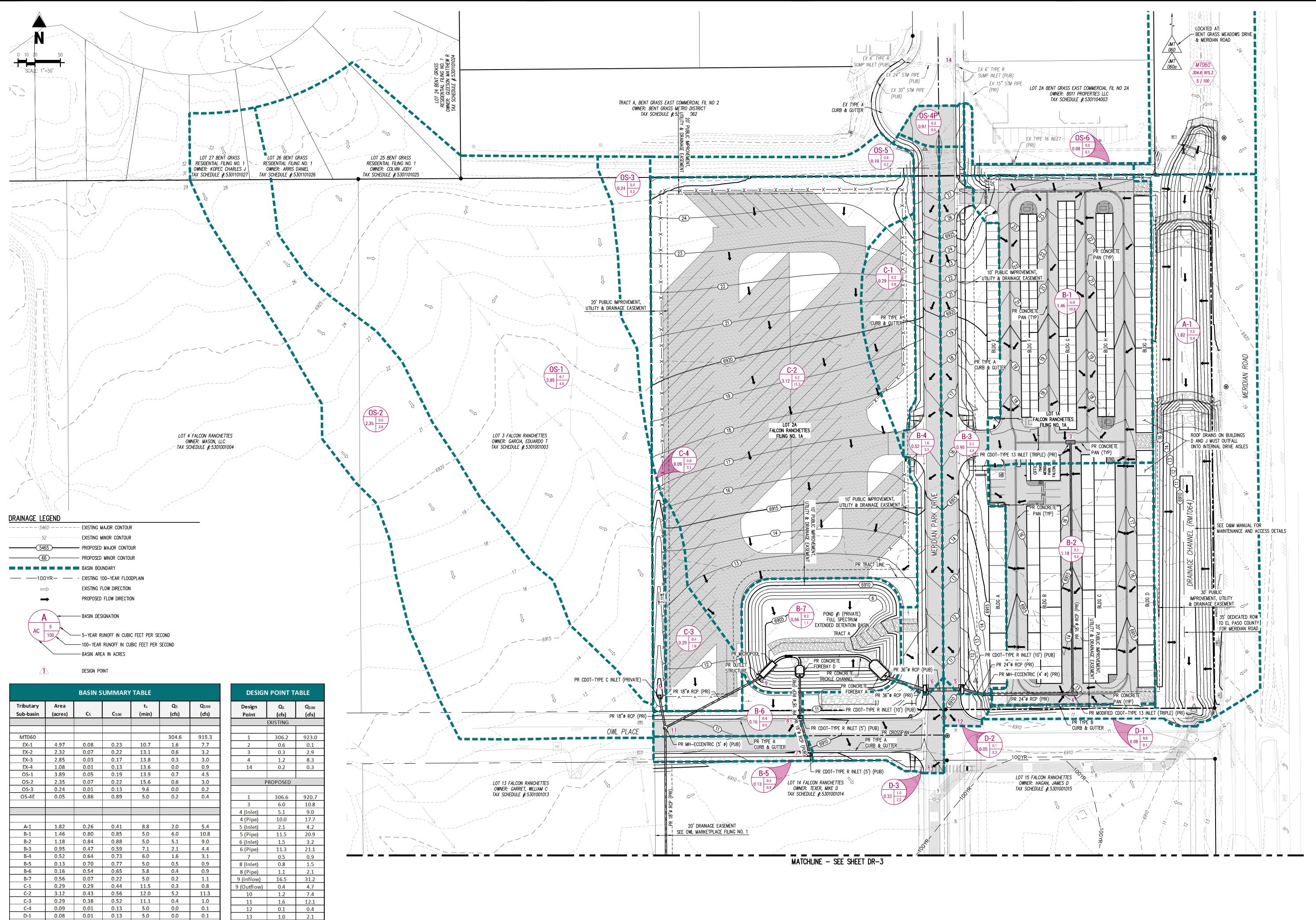
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SANCHETTES FILING NO. 1A STORAGE

Date Issue / Description Init.

roject No: MRS01
rawn By: BLB
hecked By: CMWJ
ate: 04/26/2024

EXISTING DRAINAGE MAP



0.05 0.46 0.58 5.0 0.1

0.19 0.01 0.13 5.0 0.0

0.08 0.01 0.13 9.4 0.0

OS-6

 0.33
 0.61
 0.70
 5.3
 1.0
 2.0

 0.07
 0.71
 0.78
 5.0
 0.3
 0.5

14 0.3 0.4

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ING NO. 1A

FALCON RANCHETTES F MERIDIAN STORAGE DRAINAGE MAP

Date Issue / Description Init.

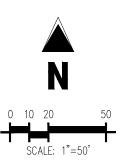
 Project No:
 MRS01

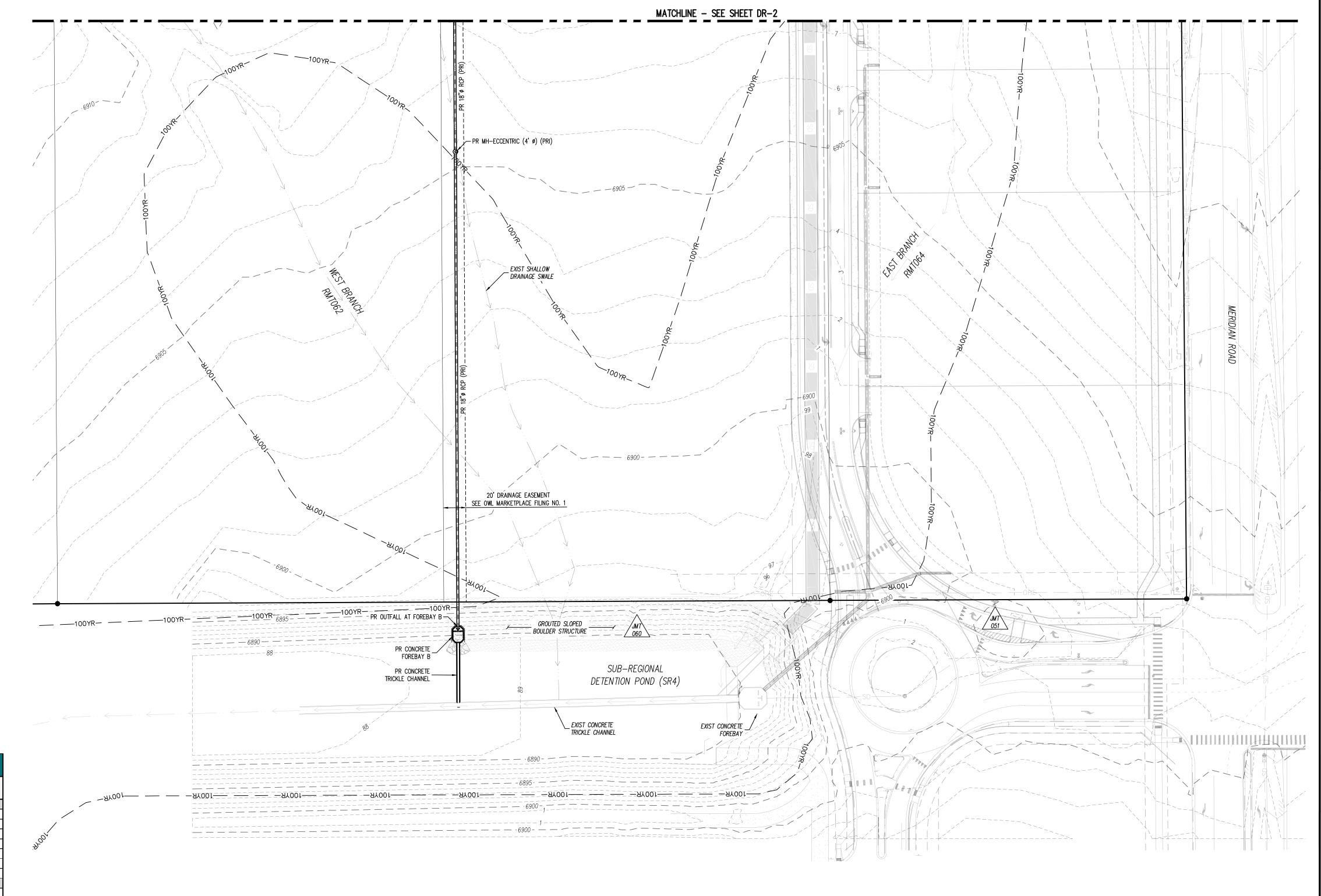
 Drawn By:
 BLB

 Checked By:
 CMWJ

 Date:
 04/26/2024

PROPOSED DRAINAGE MAP



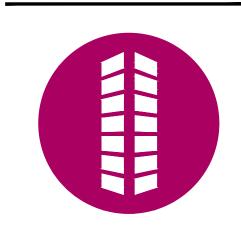


| Tributary Sub-basin | Area | C 5 | Cenn | t _c | Q ₅ (cfs) | Q ₁₀₀ |
|------------------------|---------|------------|------------------|----------------|-------------------------|------------------|
| Sub-basin | (acres) | C5 | C ₁₀₀ | (min) | (CTS) | (cfs) |
| | | | | | | |
| MT060 | | | | | 304.6 | 915.3 |
| EX-1 | 4.97 | 0.08 | 0.23 | 10.7 | 1.6 | 7.7 |
| EX-2 | 2.32 | 0.07 | 0.22 | 13.1 | 0.6 | 3.2 |
| EX-3 | 2.85 | 0.03 | 0.17 | 13.8 | 0.3 | 3.0 |
| EX-4 | 1.08 | 0.01 | 0.13 | 13.6 | 0.0 | 0.9 |
| OS-1 | 3.89 | 0.05 | 0.19 | 13.9 | 0.7 | 4.5 |
| OS-2 | 2.35 | 0.07 | 0.22 | 15.6 | 0.6 | 3.0 |
| OS-3 | 0.24 | 0.01 | 0.13 | 9.6 | 0.0 | 0.2 |
| OS-4E | 0.05 | 0.86 | 0.89 | 5.0 | 0.2 | 0.4 |
| | | | | | | |
| | | | | | | |
| A-1 | 1.82 | 0.26 | 0.41 | 8.8 | 2.0 | 5.4 |
| B-1 | 1.46 | 0.80 | 0.85 | 5.0 | 6.0 | 10.8 |
| B-2 | 1.18 | 0.84 | 0.88 | 5.0 | 5.1 | 9.0 |
| B-3 | 0.95 | 0.47 | 0.59 | 7.1 | 2.1 | 4.4 |
| B-4 | 0.52 | 0.64 | 0.73 | 6.0 | 1.6 | 3.1 |
| B-5 | 0.13 | 0.70 | 0.77 | 5.0 | 0.5 | 0.9 |
| B-6 | 0.16 | 0.54 | 0.65 | 5.8 | 0.4 | 0.9 |
| B-7 | 0.56 | 0.07 | 0.22 | 5.0 | 0.2 | 1.1 |
| C-1 | 0.29 | 0.29 | 0.44 | 11.5 | 0.3 | 0.8 |
| C-2 | 3.12 | 0.43 | 0.56 | 12.0 | 5.2 | 11.3 |
| C-3 | 0.29 | 0.38 | 0.52 | 11.1 | 0.4 | 1.0 |
| C-4 | 0.09 | 0.01 | 0.13 | 5.0 | 0.0 | 0.1 |
| D-1 | 0.08 | 0.01 | 0.13 | 5.0 | 0.0 | 0.1 |
| D-2 | 0.05 | 0.46 | 0.58 | 5.0 | 0.1 | 0.3 |
| D-3 | 0.33 | 0.61 | 0.70 | 5.3 | 1.0 | 2.0 |
| OS-4P | 0.07 | 0.71 | 0.78 | 5.0 | 0.3 | 0.5 |
| OS-5 | 0.19 | 0.01 | 0.13 | 5.0 | 0.0 | 0.2 |
| OS-6 | 0.08 | 0.01 | 0.13 | 9.4 | 0.0 | 0.1 |

| | DESIGN | DESIGN POINT TABLE | | |
|---------------------------|-----------------|-------------------------|---------------------------|--|
| Q ₁₀₀ (cfs) | Design Point | Q ₅ (cfs) | Q ₁₀₀ (cfs) | |
| | | EXISTING | | |
| | | | | |
| 15.3 | 1 | 306.2 | 923.0 | |
| 7.7 | 2 | 0.6 | 0.1 | |
| 3.2 | 3 | 0.3 | 2.9 | |
| 3.0 | 4 | 1.2 | 8.3 | |
| 0.9 | 14 | 0.2 | 0.3 | |
| 4.5 | | | | |
| 3.0 | P | PROPOSED | | |
| 0.2 | | | | |
| 0.4 | 1 | 306.6 | 920.7 | |
| | 3 | 6.0 | 10.8 | |
| | 4 (Inlet) | 5.1 | 9.0 | |
| | 4 (Pipe) | 10.0 | 17.7 | |
| 5.4 | 5 (Inlet) | 2.1 | 4.2 | |
| 10.8 | 5 (Pipe) | 11.5 | 20.9 | |
| 9.0 | 6 (Inlet) | 1.5 | 3.2 | |
| 4.4 | 6 (Pipe) | 11.3 | 21.1 | |
| 3.1 | 7 | 0.5 | 0.9 | |
| 0.9 | 8 (Inlet) | 0.8 | 1.5 | |
| 0.9 | 8 (Pipe) | 1.1 | 2.1 | |
| 1.1 | 9 (Inflow) | 16.5 | 31.2 | |
| 8.0 | 9 (Outflow) | 0.4 | 4.7 | |
| 11.3 | 10 | 1.2 | 7.4 | |
| 1.0 | 11 | 1.6 | 12.1 | |
| 0.1 | 12 | 0.1 | 0.4 | |
| 0.1 | 13 | 1.0 | 2.1 | |
| 0.3 | 14 | 0.3 | 0.4 | |
| 2.0 | | | | |
| 0.5 | | • | • | |

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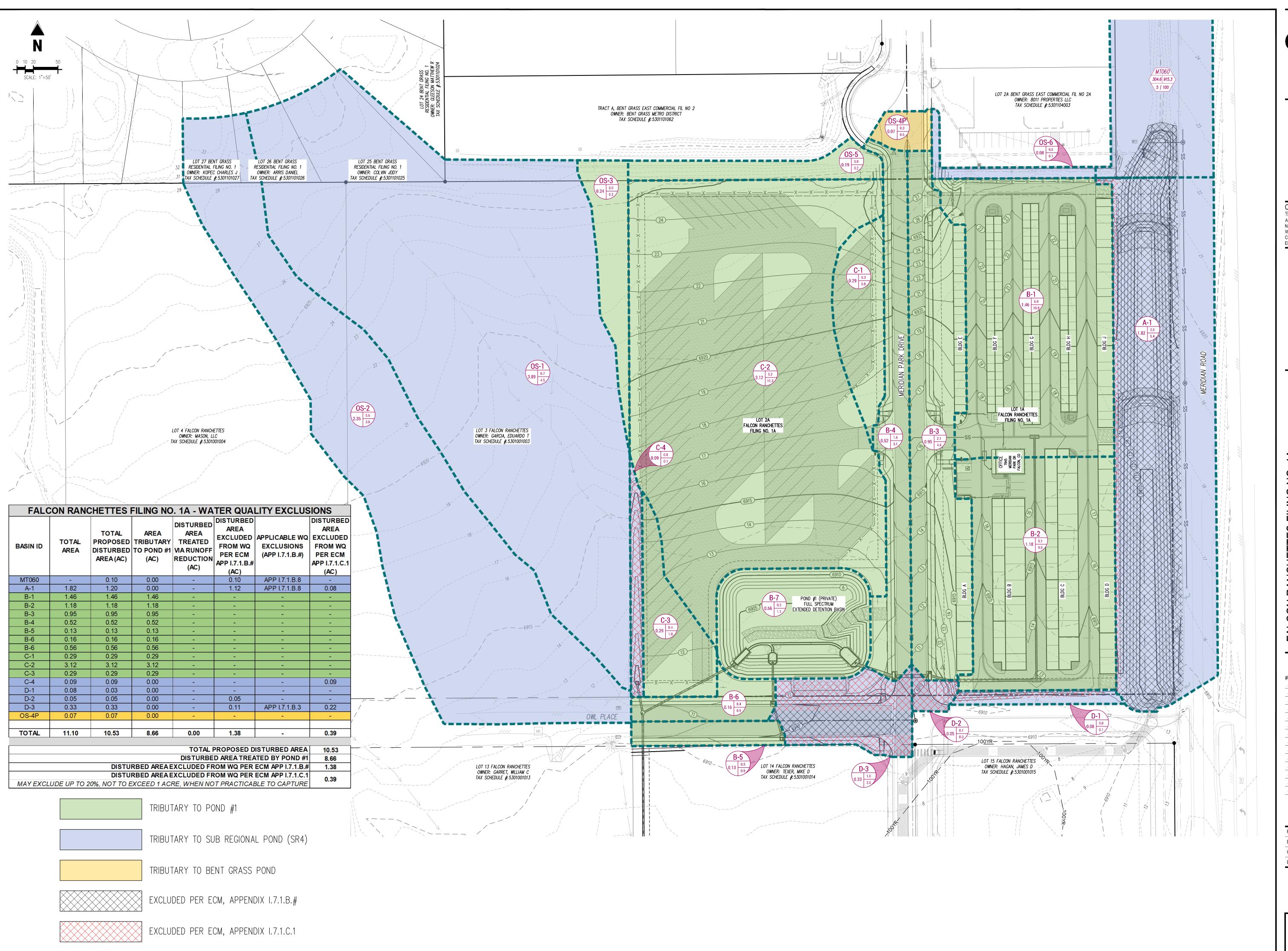


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ALCON RANCHETTES FILING NO. 1A ERIDIAN STORAGE RAINAGE MAP

roject No: MRS01
rawn By: BLB
necked By: CMWJ
ate: 04/26/2024

PROPOSED DRAINAGE MAP



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FALCON RANCHETTES FILING NO. 1A MERIDIAN STORAGE DRAINAGE MAP FOR M.D. ROOFING

| ate | Issue / Description | Ini |
|-----|---------------------|-----|
| | | |
| | | |

| Project No: | MRS01 |
|-------------|------------|
| Drawn By: | BLB |
| Checked By: | CMWJ |
| Date: | 04/26/2024 |
| | |

WATER QUALITY DRAINAGE MAP