

WYOMING ESTATES SUBDIVISION FILING NO. 2

(A REPLAT OF A PORTION OF WYOMING ESTATES FILING NO. 1)

FINAL DRAINAGE REPORT



PREPARED BY

Mike Bartusek RESPEC 102 S Tejon St., Suite 1110 Colorado Springs, CO 80903 719-640-8057

PREPARED FOR

Home Run Restorations, Inc. 5090 Wiley Road Peyton, CO 80904 719-649-7241

JUNE 2023

Project Number W0562.23001

SP237 and SF2322

PCD File No. MS ---





ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Michael A. Bartusel	k, P.E. #23329	

DEVELOPER'S STATEMENT:

I the Developer have read and will comply with all of the requirements specified in this

,	eport and plan.	the requirements specified in this	
Ву:	Shawn Shafer		
Title: Own Address:	er Home Run Restorations, Inc. 5090 Wiley Road Peyton, CO 80904		
Filed in acc Volumes 1	cordance with the El Paso County Land De and 2, and the Engineering Criteria Manua	velopment Code, Drainage Criteria II, as amended.	Manual
El Paso Cou	unty Engineer/ECM Administrator	Date	
Conditions	:	·	

Revise report to change "proposed" items to "existing" if infrastructure are already in place.

FINAL DRAINAGE REPORT WYOMING ESTATES SUBDIVISION FILING No. 2

PROJECT DESCRIPTION

This drainage report is for the development of the Wyoming Estates Subdivision Filing No. 2 which is a replat of a portion of Wyoming Estates Subdivision Filing No. 1. Wyoming Estates Subdivision Filing No. 2 encompasses 25.34 of the total 40.01 acres site. The project is located west of Curtis Road approximately 2.5 miles north of SH 94. Of the 40.01 acres, 3.53 acres have been dedicated to El Paso County for future Curtis Road expansion. It is further described as the southern portion of Section 33, Township 13 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado.

All of this lot is located in the Curtis Ranch and Livestock Company drainage basin. Flows from the site drain into the west ditch of Curtis Road and flow north to the West Fork of Squirrel Creek.

SOILS

The soil on the site can be described as having a rapid permeability, medium-surface runoff, and moderate to high hazard of erosion. The soils within the site are:

• 8

Blakeland Loamy Sand

Α

• 95

Truckton Sandy Loams

В

FLOODPLAIN STATEMENT

No portion of the developed site is located within a designated FEMA 100-year floodplain according to the information published in the Federal Emergency Management Agency Flood Plain Map No. 08041C0785G, dated December 7, 2018.

METHOD OF COMPUTATION

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual, Volumes 1*, dated May 2014. The Rational Method for computation of runoff was used for determining Sub-Basin flows.

Q = cia

Where

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration

required for the runoff to become established

a = drainage basin size in acres

HISTORIC DRAINAGE CONDITIONS

The original site was undeveloped except for a gravel road located along the north property line located within a 60 ft. Access Easement. Approximately 90% of the parcel is covered with rangeland grasses with slopes varying from 2% to 8%. The parcel generally slopes to the northeast except for the southwest corner which drains to the southwest. Also, a large 2.5' deep sump area exists in the southcentral portion of the site. The overflow swale for this sump area directs the flows to the northeast.

Sub-Basin Aex contains 3.66 acres and drains the southwest corner of the site. It produces flows of 0.9 cfs for the 5-year storm and 7.1 cfs for the 100-year storm. These flows travel off the site to the south.

Sub-Basin B1ex contains 19.80 acres and drains the southcentral area of the site. This area drains to the east and northeast and is tributary Sub-Basin OS1 which contains the west ditch along Curtis Road. This sub-basin produces flows of 4.5 cfs for the 5-year storm and 34.0 cfs for the 100-year storm.

Sub-basin OS1 contains 3.53 acres and is located east of the site and contains the Curtis Road ROW. Sub-basin will produce flows of 1.9 cfs and 8.4 cfs respectively. The combined flows from Sub-Basin B1ex and OS1 at DP1 will be 6.0 cfs for the 5-year storm and 41.1 cfs for the 100-year storm.

Sub-basin OS2 contains 6.86 acres and is located in the northwest area of the site. This undeveloped area sheet flows onto the site and produces flows of 3.32 cfs for the 5-year storm and 13.1 cfs for the 100-year storm. These flows sheet flow into Sub-Basin B2ex.

Sub-Basin B2ex contains 13.02 acres and drains the northeast portion of the site. This area drains to the east and southeast toward the existing ditch along the existing gravel access road which serves the properties to the west. This sub-basin produces flows of 3.0 cfs for the 5-year storm and 18.6 cfs for the 100-year storm. These flows will combine with the flows from Subbasin OS2 at DP2 to produce flows of 5.9 cfs for the 5-year storm and 30.3 cfs for the 100-year storm.

The flows from DP1 and DP2 will combine at DP3 to produce flows of 10.8 cfs for the 5-year storm and 63.5 cfs for the 100-year storm. These flows will continue within the west Curtis Road ditch to the West Fork of Squirrel Creek.

DEVELOPED DRAINAGE CONDITIONS

The proposed replatted portion of the subdivision will consist of four (4) lots with Lot 1 containing 5.13 acres, Lot 2 containing 5.41 acres, Lot 3 containing 8.44 acres and Lot 4 containing 6.36 acres. The remaining portion of Wyoming Estates Subdivision Filing No. 1 will consist of two (2) lots with Lot 2 containing 5.08 acres and Lot 3 containing 5.06 acres. It also contains an existing asphalt cul-de-sac located across from Patton Drive with an existing private gravel road extending from the cul-de-sac and connecting to the existing access road to the west. These new lots are assumed to be developed with 3000 sf homes and 12 ft gravel drives. No overlot grading will take place within the proposed subdivision. No revisions to the Subbasin boundaries delineated in the approved Final Drainage Report for the Wyoming Estates Subdivision Filing No. 1 are required.

Sub-Basin A contains 3.66 acres and will continue to drain to the southwest corner of the site. It produces flows of 0.9 cfs for the 5-year storm and 7.1 cfs for the 100-year storm. These flows travel off the site to the south.

Sub-Basin B1 contains 4.75 acres and will contain one (1) home and drains the eastern area of the site adjacent to Curtis Road. This area drains to the east and northeast and is tributary Sub-Basin OS1 which contains the west ditch along Curtis Road. This sub-basin produces flows of 1.6 cfs for the 5-year storm and 10.1 cfs for the 100-year storm.

Sub-basin OS1A contains 2.62 acres and is located east of the site and contains the Curtis Road ROW. This Sub-basin will produce flows of 1.5 cfs and 6.6 cfs respectively. The combined flows

from Sub-Basins B1 and OS1A at DP1 will be 3.0 cfs for the 5-year storm and 16.4 cfs for the 100-year storm.

Sub-basin B2A1 contains 0.20 acres and is located in the area northcentral area of the site, along the south side of the gravel road. This roadway area sheet flows into the ditch in Sub-basin B2B1 and produces flows of 0.4 cfs for the 5-year storm and 1.0 cfs for the 100-year storm.

Sub-Basin B2B1 contains 1.20 acres and drains the northcentral portion of the site and contains a small portion of Lot 1. This area drains to the northeast toward the proposed ditch along Teleo Point. This sub-basin produces flows of 0.8 cfs for the 5-year storm and 3.1 cfs for the 100-year storm. These flows will combine with the flows from Sub-basin B2A1at DP2 to produce flows of 1.1 cfs for the 5-year storm and 3.8 cfs for the 100-year storm. These flows continue east into Sub-Basin B2B2.

Sub-basin OS2A contains 1.26 acres and is located northwest of the site. This undeveloped area sheet flows onto the site and produces flows of 0.3 cfs for the 5-year storm and 1.9 cfs for the 100-year storm. These flows sheet flow into Sub-Basin B2.

Sub-Basin B2B2 contains 16.31 acres and will contain three (3) homes and drains the northcentral portion of the site. It contains a large portion of Lots 2, 3 and 4 and a small portion of Wyoming Estates Subdivision Filing No. 1 Lot 3. This area drains to the northeast toward the proposed ditch along Teleo Point. This Sub-basin produces revised flows of 4.0 cfs for the 5-year storm and 28.1 cfs for the 100-year storm. These flows will combine with the flows from Sub-basin OS2A at DP3 to produce flows of 3.9 cfs for the 5-year storm and 27.6 cfs for the 100-year storm. These flows will combine with the flows from DP2 at DP4 to produce flows of 5.2 cfs for the 5-year storm and 31.4 cfs for the 100-year storm. These ditch flows continue east toward the Curtis Road ditch. They will then combine with the flows from DP1 at the proposed public 30"x19" RCEP culvert under the Teleo Point cul-de-sac. The combined flows of DP1 and DP4 at DP5 will be 7.4 cfs for the 5-year storm and 43.5 cfs for the 100-year storm. These flows continue north into Sub-Basin OS1B.

Sub-basin B3A1 contains 0.165 acres and is located in the northwest area of the site, along the south side of the gravel road. This roadway area sheet flows into the ditch in Sub-basin B3B and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-basin B3A2 contains 0.165 acres and is located in the northwest area of the site approximately 275 ft from the west property line along the south side of the gravel road. This roadway area sheet flows into the ditch in Sub-basin B3B and produces flows of 0.4 cfs for the 5-year storm and 0.9 cfs for the 100-year storm.

Sub-basin OS2B contains 5.60 acres and is located in the northwest area of the site. This undeveloped area sheet flows onto the site and produces flows of 1.1 cfs for the 5-year storm and 8.2 cfs for the 100-year storm. These flows sheet flow into Sub-Basin B3.

Sub-Basin B3B contains 4.11 acres and will contain one (1) home and drains the northwestern portion of the site and contains a large portion of Lot 1. This area drains to the east toward the proposed ditch and sump along the new gravel access road. This sub-basin produces flows of 1.1 cfs for the 5-year storm and 8.0 cfs for the 100-year storm. The flows from Sub-basin B3B will combine with the flows from Sub-basin OS2B at DP8 to produce flows of 1.9 cfs for the 5-year storm and 13.7 cfs for the 100-year storm. These flows will combine with the flows from

Sub-basins B3A1 and B3A2 at DP9 to produce flows of 2.2 cfs for the 5-year storm and 14.6 cfs for the 100-year storm. These flows travel into Sub-Basin B4A2 through a private 30" cmp.

Sub-basin B4A1 contains 0.44 acres and is located in the northwest area of the site, along the north side of the gravel road. This roadway area sheet flows south along the roadway and into Sub-basin B4A2 and produces flows of 0.7 cfs for the 5-year storm and 2.1 cfs for the 100-year storm. These flows will combine with the flows from DP9 at DP10 to produce flows of 2.5 cfs for the 5-year storm and 15.4 cfs for the 100-year storm.

Sub-Basin B4A2 contains 4.40 acres and drains the northeastern portion of the site and contains Lot 2. This area drains to the east toward the existing ditch along the west property line which will be enlarged and stabilized. This sub-basin produces flows of 1.3 cfs for the 5-year storm and 9.0 cfs for the 100-year storm. These flows will combine with the flows from DP10 at DP11 to produce flows of 3.1 cfs for the 5-year storm and 19.2 cfs for the 100-year storm. These flows will then flow into the ditch along Curtis Road.

Sub-Basin B4B1 contains 0.38 acres and drains the northern portion of the Teleo Point gravel road. This area drains to the east toward Curtis Road. This sub-basin produces flows of 0.5 cfs for the 5-year storm and 1.6 cfs for the 100-year storm. These flows will then flow into Sub-basin B4B2.

Sub-Basin B4B2 contains 0.56 acres and drains the northern portion of the Teleo Point asphalt road. This area drains to the east toward Curtis Road. This sub-basin produces flows of 1.4 cfs for the 5-year storm and 3.3 cfs for the 100-year storm. These flows will combine with the flows from DP5 at DP6 to produce flows of 8.2 cfs for the 5-year storm and 45.5 cfs for the 100-year storm. These flows will then flow into the ditch along Curtis Road.

Sub-basin OS1B contains 0.91 acres and is located east of the site and north of Teleo Point culde-sac and contains the Curtis Road ROW. Sub-basin will produce flows of 0.6 cfs and 2.6 cfs respectively. These flows will combine with the flows from DP6 at DP7 to produce flows of 8.2 cfs for the 5-year storm and 44.8 cfs for the 100-year storm.

The combined flows of OS1B, DP7 and DP11 at DP12 will be 10.1 cfs for the 5-year storm and 58.1 cfs for the 100-year storm. These flows will continue within the west Curtis Road ditch to the West Fork of Squirrel Creek.

WATER QUALITY AND DETENTION

Water quality basins are not required for subdivisions containing lots greater than 5.0 acres per the Engineering Criteria Manual Section 1.7.1.B.5. Runoff Reduction calculations have been provided to eliminate the need for water quality basins.

Based on the large lots and longer Time of Concentration distances, the estimated Developed flows are less than the Existing Conditions flows so no detention facilities are warranted.

PRIVATE DRAINAGE FACILITIES

The proposed drainage improvements have been constructed. The private culvert and ditch improvements construction and maintenance will be the responsibility of Wyoming Estates Subdivision HOA.

Explain how fees were paid and accounted for in filing 1. ECM appendix L criteria states fees are due whenever lots are further subdivided. Refer to appendix L and prove that no additional fees are due.

DRAINAGE BASIN FEES

The proposed development is located within the Curtis Ranch and Livestock Company drainage basin. The Livestock Company drainage basin encompasses 3.66 acres of the site and has fees associated with it. The Curtis Ranch drainage basin encompasses the remainder of the area and has no fees associated with it. These fees were paid at the time of the Wyoming Estates Subdivision Filing No. 1 plat approval. Therefore no fees are required at this time.

2021 Livestock Company Drainage Fees

Impervious Coverage = 3.6% Area Subject to Fees = 0.036 x 3.66 = 0.13 Acres Livestock Company Fee = \$18,273/Acre Drainage Basin Fee = \$18,273 x 0.13 = \$2,375

2021 Livestock Company Bridge Fees

Impervious Coverage = 3.6%Area Subject to Fees = $0.036 \times 3.66 = 0.13$ Acres Livestock Company Fee = 217/Acre Drainage Basin Fee = $217 \times 0.13 = 286$

CONCLUSION

The proposed development and subsequent lot developments follow the "Four Step Process" as mandated by the EPA as follows:

Step 1: Employ runoff reduction practices

Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

- Impervious areas have been directed to the existing earth swales and ditches to encourage infiltration.
- A gravel roadway has been used for the upper portion of the project to reduce the impervious of the areas.

Step 2: Stabilize drainageways

All drainageways, ditches and channels have been stabilized by the following methods:

- Tributaries have been left in their relatively natural state where possible.
- New ditches have been stabilized with either riprap or erosion control fabric depending on the erosion potential.

Step 3: Provide water quality capture volume (WQCV)

Based on the Runoff Reduction calculations performed for the proposed development, the 2.2 acres for the asphalt and gravel roadway construction does not require any water quality basins, however a temporary sedimentation basin will be constructed.

Step 4: Consider need for industrial and commercial BMP's.

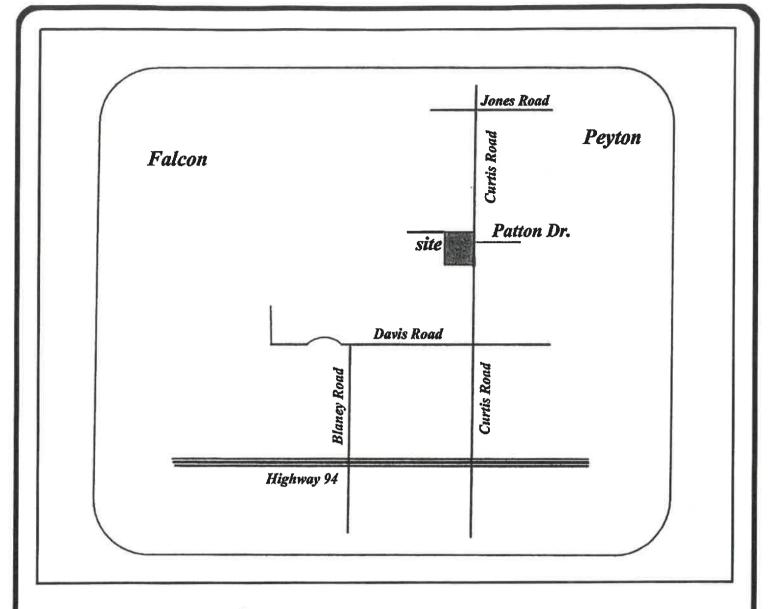
No industrial and commercial development is proposed for the site.

Based on longer times of concentration and minimal development, the proposed development flows of 58.1 cfs for the 100-year storm are below the historic levels of 63.5 cfs for the 100-year storm. Therefore, the proposed development will not adversely affect downstream or surrounding properties.

REFERENCES

- 1. City of Colorado Springs and El Paso County (2014). *Drainage Criteria Manual Volume* 1 (DCM).
- 2. City of Colorado Springs and El Paso County (2014)
- 3. Drainage Criteria Manual Volume II (DCM) as amended.
- 4. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
- 5. El Paso County (January 2016) Engineering Criteria Manual.
- 6. Urban Drainage and Flood Control District (June 2017). *Urban Storm Drainage Criteria Manual, Volume 1-3*.
- 7. Final Drainage Report Wyoming Estates Subdivision, prepared by Respec, Nov. 2020.

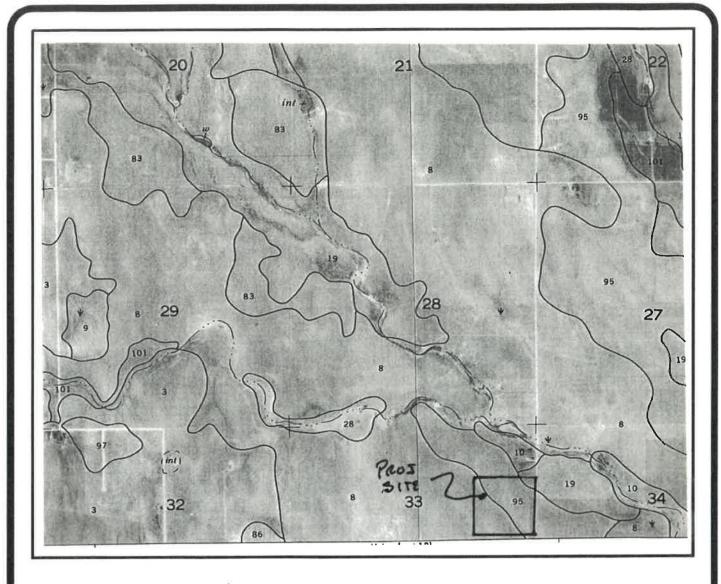
APPENDIX A MAPS







121 S Tejon St., Suite 1110 Colorado Springs, CO 80903 Phone: (719) 283-7671

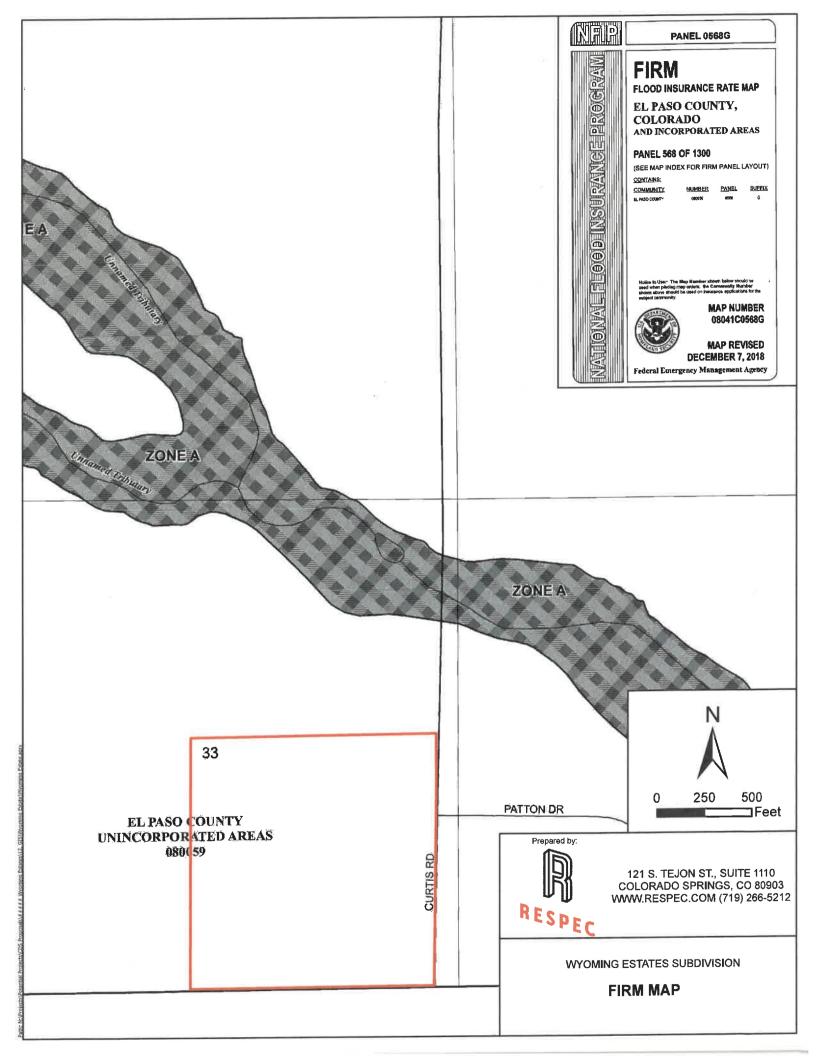




$\frac{\text{SOILS MAP}}{\text{\tiny N.T.S.}}$



121 S Tejon St., Suite 1110 Colorado Springs, CO 80903 Phone: (719) 283-7671



APPENDIX B DESIGN CALCULATIONS

The spreadsheet isn't calculating the results properly. I believe it is because you need to choose "none" for Downstream BMP Type. Please adjust. the WQCV Reduction % (highlighted in orange below) should be greater than or equal to 60% in order to achieve WQ runoff reduction.

			Desk	n Procedu			uction					Shoot 4 of 4
Designer:	Mike Bartusel	k		UD-BMP (Ve	rsion 3.07, Ma	rch 2018)						Sheet 1 of 1
Decigno.	Respec		-									
	June 19, 2023		/									
3	Wyoming Esta		n 2									
	3050 Curtis R		0. 2									
Location:	3030 Curus K	oad										
		$-\!\!\!/-$										
SITE INFORMATION (Use		ue Cells) ainfall Depth	0.60	inches								
Depth of Average Run	off Producing	Storm, d ₆ =	0.43	inches (for W	atersheds O	utside of the	Denver Regio	n, Figure 3-1	in USDCM V	ol. 3)		
Area Type	UA:RPA	SPA	UIA:RPA	SPA	UIA:RPA	UIA:RPA	SPA	UIA:RPA	UIA:RPA	UIA:RPA	SPA	
Area ID	B2A1	B2B1	B2A2	B2B2+OS2A	B3A1	B3A2	B3B+OS28	B4A1	B4B1	B4B2	B4A2	
wnstream Design Point ID	2	2	4	4	9	9	9	10	6	6	11	
Downstream BMP Type												
		-								_		
DCIA (ft²)	5,230		8,275	-	4,575	4,575		9,150	5,230	9,150		
UIA (ft²)			6,970		3,485	3,485	-	10,020	22,770	12,200		
RPA (ft²)	3,500	5,225	0,570	76,500	-		42,300	-			191,600	
SPA (ft²)		0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	
HSG A (%)	0% 100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	
HSG B (%)		0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	
HSG C/D (%)	0%	0%	0.250		0.250	0.250	- U/B	0.250	0.250	0.250		
verage Slope of RPA (ft/ft)	0.250		480.00	-	275.00	275.00	-	550.00	300.00	480.00		
A:RPA Interface Width (ft)	300.00		460.00		213.00	270.00		500.00	555.55	100.00		
CALCULATED RUNOFF		5054	DD40	Inono.ocasi	B3A1	B3A2	B3B+OS28	B4A1	B4B1	B4B2	B4A2	
Area ID	B2A1	B2B1	B2A2	B2B2+OS2A		8,060	D3D*U320	19,170	28,000	21,350		
UIA:RPA Area (ft²)	8,730		15,245	-	8,060			0.06	0.31	0.09	-	
L / W Ratio	0.10		0.07	-	0.11	0.11	-	0.4773	0.1868	0.4286		
UIA / Area	0.5991		0.5428		0.5676	0.5676	0.00	0.00	0.00	0.00	0.00	
Runoff (in)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0	0	0.00	
Runoff (ft ³)	0	0	0	0 3825	191	191	2115	381	218	381	9580	
Runoff Reduction (ft ³)	218	261	345	3023	131	101	2110	501	2.10			
CALCULATED WQCV RE	SULTS					Ľ						
Area ID	B2A1	B2B1	B2A2	B2B2+OS2A	B3A1	B3A2	B3B+OS28	B4A1	B4B1	B4B2	B4A2	
WQCV (ft ³)												
WQCV Reduction (ft3)												
WQCV Reduction (%)												
Untreated WQCV (ft ³)												
CALCULATED DESIGN F	OINT DECI	TS /eume *	equite from	all columns w	ith the sam	e Downstres	m Desian Po	int ID)				
wnstream Design Point ID	2	2	4	4	9	9	9	10	6	6	11	
	0	0	0	0	0	0	0	0	0	0	0	
DCIA (ft²)	5,230	5,230	8,275	8,275	9,150	9,150	9,150	9,150	14,380	14,380	0	
UIA (ft²)		3,500	6,970	6,970	6,970	6,970	6,970	10,020	34,970	34,970	0	
RPA (ft²)	3,500	5,225	76,500	76,500	42,300	42,300	42,300	0	0	0	191,600	
SPA (ft²)	5,225	13,955	91,745	91,745	58,420	58,420	58,420	19,170	49,350	49,350	191,600	
Total Area (ft²)	13,955			8,275	9,150	9,150	9,150	9,150	14,380	14,380	0	
Total Impervious Area (ft²)	5,230	5,230	8,275 0	0,275	9,150	0	0	0	0	0	0	
WQCV (ft ³)	0	0	0	0	0	0	0	0	0	0	0	
WQCV Reduction (ft3)	0		0%	0%	0%	0%	0%	0%	0%	0%	0%	
WQCV Reduction (%)	0%	0%	0%	0%	0	0	0	0	0	0	0	
Untreated WQCV (ft ³)	0	0		1 0 1	- 0							
CALCULATED SITE RES	ULTS (sums	results fron	all column	s in workshee	et)							
Total Area (ft²)	696,130											
Total Impervious Area (ft²)	92,370											
WQCV (ft ³)	0											
WQCV Reduction (ft ³)	0											
WQCV Reduction (%)												
MAGO A MAGGGGGG (30)												
Untrooted MOCV (A3)	l n											
Untreated WQCV (ft ³)	0											

WYOMING ESTATES SUBD C FACTOR CALCULATION							
C FACTOR CALCULATION	SHEET						
EXISTING CONDITIONS							
RUNOFF COEFICIENT							
TYPE A/B SOILS							
LAND USE		Imperv %	5 YR	100 YR			
UNDEV		0	0.08	0.35			
GRAVEL ROAD		80	0.59				
ASPHALT ROAD		100	0.9	0.96			
ROOFS		90	0.73	0.81			
						041 0111 4	TED 0
	TOTAL	SURFACE CO			DOOFO	CALCULA	
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100 VD
DESIG.	(acre)		ROAD	ROAD		YR	YR
Aex	3.66	3.66	0.00	0.00	0.00	0.08	0.35
B1ex	19.80	19.80		0.00	0.00	0.08	0.35
B2ex	13.02	12.47		0.00	0.00	0.10	0.36
OS1	3.53			0.36	0.00	0.16	0.41
OS2	6.20	6.20		0.00	0.00	0.08	0.35
002	0.20	0.20	0.00				
Aex+B1ex+B2ex	36.48	35.93	0.55	0.36	0.00		8
, 13	0.8	0.00	0.44	0.36	0.00		
	Imperviou	sness = (0.44)/	37.29 = 2.29	6			
DEVELOPED CONDITION RUNOFF COEFICIENT	NS						
TYPE A/B SOILS							
LAND USE		Imperv %	5 YR	100 YR			
UNDEV		0	0.08	0.35			
GRAVEL ROAD		80	0.59				
ASPHALT ROAD		100					
ROOFS		90	0.73	0.81			

Developed Conditions							
	TOTAL	SURFACE CO	NDITION A	REAS		CALCULA	TED C
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100
DESIG.	(acre)		ROAD	ROAD		YR	YR
A	3.66	3.66	0.00	0.00	0.00	0.08	0.35
B1	4.75			0.00	0.07	0.10	0.36
B2A1	0.20		0.12	0.00	0.00	0.39	0.56
B2A2	0.35	0.16	0.00	0.19	0.00	0.53	0.68
B2B1	1.20	0.95	0.25	0.00	0.00	0.19	0.42
B2B2	16.31	15.89	0.21	0.00	0.21	0.09	0.36
B3A	0.17	0.04	0.13	0.00	0.00	0.47	0.62
B3A	0.17	0.04	0.13	0.00	0.00	0.47	0.62
B3B	4.11	4.04	0.00	0.00	0.07	0.09	0.36
B4A1	0.44	0.23	0.21	0.00	0.00	0.32	0.52
B4A2	4.40	4.33	0.00	0.00	0.07	0.09	0.36
B4B1	0.38	0.26	0.12	0.00	0.00	0.24	0.46
B4B2	0.56	0.28	0.00	0.21	0.07	0.47	0.64
OS1A	2.62	2.35	0.00	0.27	0.00	0.16	0.41
OS1B	0.91	0.82	0.00	0.09	0.00	0.16	0.41
OS2A	1.26			0.00	0.00	0.08	0.35
OS2B	5.60			0.00	0.00	0.08	0.35
Avg House = 3000 sf w/ a	vg 250'x12' gr	avel driveway					

Proposed of the proposed of th	RAINAGE CALCULATIC	1																				
Mark Mark CS CS CS CS CS CS CS C	And the second	N SHEET																		Ī		
No.	1/23/20																					
Continue	4	, and a	5	1 2	> 2	2000		Initial Tci	3		Travel T	ime	ř	Ç		Н		. 11	ngth	vel.		A D C A
No. Colorido No.	ESIG.	(acre)		(100 yr)	ξ ()	× 000	L (ft)	(%)	(min)	L (ft)	edois (%)	(fps)	(min)		=			cfs)	(feet)	(fps)		DESIG
Sign	XISTING CONDITIONS																					
SSH-BERN 1958 0.00 0.00 0.45 0.45 0.40 0.45 0.40 0.20 0.45 0.40 0.20 0.40 0.40 0.40 0.40 0.40 0.40	Xe	3.66	0.08	0.35		1.28	100	3.00	13.27	440	4,50	2.00	-	16.94	Ш	5.55	0.93	7.11				Aex
SHERING SISS	1ex	19.80	0.08	0.35		6.93	100	3.50		1270		2.40	-	21.43	-	4.90	-	33.98				B1ex
Signature Color	151	3.53	0.16	0.41		1.45	100	7.00	-	1230	L	3.20	+	15.66	1	5.77	L	8.35	450	3.40	7	081
6.66 G. 10.1 G. 10.4 G. 1.2 G. 2.6 G. 20.0 C. 2.6 G. 2. G.	1P1(OS1+B1ex)	23.33			2.15						Ш		1	21.43	Ш	4.90	Ш	41.08				DP1(0
1312 1312 1314 1315 1315	182	98.9	0.19	0.43				2.00	ш	200		1.50		25.67		4.43		13.08				OS2
Philippe	12ex	13.02	0.10	0.36				3.00	-	1130		2.20	_	31.10		3.96		18.58				В2ех
Particle	0P2(OS@+B2ex)	19.88			2.61									31.10	_		4	30.27				DP2(0
Participa Part					2									2	i			2				5
350	EVELOPED CONDITIO		000	0				000		140		000	-	7007		i	000					
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		3.66	0.08	0.35			4	3.00	+	440	4	2.00	-	16.94	1	5,55	0.93	LL./				∢
SAHEBEH SAHE	7	4.75	0.10	0.36			100	3.50	_	450	1	2.80	+-	15.05		5.88	1.60	10.06				B1
1.0 1.0	JS1A	2.62	0.16	0.41				7.00		890		3.20	-	13.88		6.11	1.47	6.57				OS1A
244 25 0.20 0.53 0.56 11 26 11 26 440 320 6.50 6.10 6.10 1.00 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.20)P1(OS1A+B1)	7.37			0.89									15.05	3.37	5.88	3.01	16.38				DP1(0
120 0.14 0.42 0.23 0.50 100 7.00 8.96 8.90 4.40 3.20 4.64 13.69 3.44 1.06 3.80 3.41 1.06 3.80 3.00 3.246 2.74 4.78 3.93 2.762 3.26	12A1	0.20	0.39	0.56			26	10.00		0	1	3.20	00.0	5.00	5.19	9.06	0.40	1.02				B2A1
140 140	12B1	1.20	0.19	0.42				7.00		890	L	3.20	4.64	13.59		6.18	0.81	3.11				B2B1
1.25 0.06 0.35 0.35 0.41 0.04 300 2.00 26.28 0.20 0.35 2.20 3.20 2.40 2.60 3.20 3.20 2.40 3.20	JP2(B2A1+B2B1)	1.40												13.59		6.18	1.08	3.80				DP2(B
1. 1. 1. 1. 1. 1. 1. 1.)S2A	1.26	0.08	0.35			4	2.00	- 1	0	4	1.80	0.00	26.28	2.50	4.38	0.25	1.93				OS2A
NSCA-MERRY 1.57	32B2	16.31	0.09	0.36				3.00	_	1230	_	2.20	9.32	22.46	2.74	4.78	4	58.06				8282
PREADPHEAZA 0.35 0.68 0.19 0.04 2.04 2.04 4.04 3.20 4.64 7.18 4.61 6.05 1.39 4.04 3.20 4.64 7.18 4.61 6.05 1.39 1.00 2.04 0.00 0.00 5.00 6.00 2.00 6.00 5.00 6.00	DP3(OS2A+B2B2)	17.57							ľ		Н			26.28	2.50	4.38	Ш	27.62				DP3(C
Part Part Part Part Part Part Part Part	32A2	0.35	0.53	0.68				10.00	2,	890	4	3.20	4.64	7.18	4.61	8.05	0.85	1.91	Ī			B2A2
0.38 0.24 0.46 0.09 0.17 26 10.00 2.30 0.00 5.09 5.19 9.06 0.47 1.58 475 2.30 3.44 9.66 0.47 0.66 0.26 0.40 5.00	7F4(DF2+DF3+D2A2)	26.69			2.95									26.28	2.50	4.38	7.40	43.54	100	2.00	0.33	DP50
0.56 0.47 0.64 0.26 0.36 0.281 0.60 2.30 0.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 2.00 <t< td=""><td>34B1</td><td>0.38</td><td>0.24</td><td>0.46</td><td></td><td></td><td></td><td>10.00</td><td>Ш</td><td>0</td><td>L</td><td>2.30</td><td>0.00</td><td>2.00</td><td>5.19</td><td>9.06</td><td>0.47</td><td>1.58</td><td>475</td><td>2.30</td><td>3.44</td><td>B4B1</td></t<>	34B1	0.38	0.24	0.46				10.00	Ш	0	L	2.30	0.00	2.00	5.19	9.06	0.47	1.58	475	2.30	3.44	B4B1
4B1+B4B2) 0.94	34B2	0.56	0.47	0.64				10.00		0		2.30	0.00	2.00	5.19	90.6	1.37	3.25				B4B2
PSCAPPEADELIA 0.16 0.41 0.15 0.37 80 6.00 8.70 2.00 2.10 1.96 1.069 3.94 6.88 0.57 2.57 90 PSCAPPEADELIA PSCAPPEADELIA 0.15 0.44 0.10 2.00 2.00 2.00 1.50 2.22 28.50 2.39 4.17 1.07 8.18 45.0 2.21 SSCABLESIB 0.00 0.036 0.37 1.48 100 4.00 1.50 2.22 28.50 2.39 4.17 1.07 8.18 4.50 2.21 SSCABLESIB 9.71 0.03 0.01 2.60 1.00 2.81 0.00 4.40 3.20 0.00 5.00 5.00 8.01 2.21 4.75 3.71 2.29 3.99 1.87 4.75 9.00 0.00 9.00 0.00 2.81 0.00 6.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00	JP6(B4B1+B4B2)	0.94												26.62	2.49	4.34	0.88	2.32	300	2.00	2.50	DP6(B
P6+DP6+OBIB) 28.54 3.45 10.86 A.10	JS1B	0.91	0.16	0.41				9.00	4	250	-	2.10	1.98	10.69	3.94	6.88	0.57	2.57	İ			OS1B
5.60 0.08 0.35 0.45 1.96 3.00 2.00 2.00 1.50 2.22 28.50 2.39 4.17 1.07 8.18 4.50 3.40 2.21 4.11 0.09 0.36 0.37 1.48 100 4.00 1.96 6.50 3.40 1.90 5.70 17.65 3.11 5.43 1.15 8.04 9.06 9.04 1.374 9.06 9.04 9.03 9.04 9.04 9.05 9.04 9.03 9.04 9.03 9.04 9.03 9.04 9.03 9.04 9.03 9.04 9.03 9.04 9.03	OP7(DP5+DP6+OB1B)	28.54			3.45									29.12	2.36	4.12	8.15	44.76				DP7(C
4.11 0.09 0.36 0.37 1.48 100 4.00 1.95 650 3.40 1.90 5.70 17.65 3.11 5.43 1.15 8.04 9.04 9.71 2.29 3.99 1.87 13.74 9.06 9.04 0.93 9.04 9.05 9.04 0.93 9.04 9.05 9.06 0.40 0.93 9.06 0.40 0.93 9.06 0.40 0.93 9.06 0.40 0.93 9.06 0.93 9.06 0.93 9.06 0.93 9.06 0.93 9.06 0.93 9.06 0.93 9.06 0.93 9.06 0.73 2.07 9.03 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 2.07 9.06 0.73 0.74 2.27 3.07 2.23 <th< td=""><td>)S2B</td><td>5.60</td><td>0.08</td><td>0.35</td><td></td><td></td><td></td><td>2.00</td><td>-</td><td>200</td><td></td><td>1.50</td><td>2.22</td><td>28.50</td><td>2.39</td><td>4.17</td><td>1.07</td><td>8.18</td><td>450</td><td>3.40</td><td>2.21</td><td>OS2B</td></th<>)S2B	5.60	0.08	0.35				2.00	-	200		1.50	2.22	28.50	2.39	4.17	1.07	8.18	450	3.40	2.21	OS2B
DSSB+B3B 9.71 0.42 3.97 1.87 13.74 0.62 1.87 13.74 0.62 1.87 13.74 0.62 1.87 13.74 0.62 1.87 13.74 0.62 1.87 13.74 0.62 1.87 13.74 0.62 1.87 1.87 13.74 0.62 1.87 1.87 1.87 13.74 0.63 0.63 0.61 0.61 0.60 <td>33B</td> <td>4.11</td> <td>0.00</td> <td>0.36</td> <td></td> <td></td> <td>4</td> <td>4.00</td> <td></td> <td>920</td> <td>_</td> <td>1.90</td> <td>5.70</td> <td>17.65</td> <td>3.11</td> <td>5.43</td> <td>1.15</td> <td>8.04</td> <td></td> <td></td> <td></td> <td>B3B</td>	33B	4.11	0.00	0.36			4	4.00		920	_	1.90	5.70	17.65	3.11	5.43	1.15	8.04				B3B
0.17 0.62 0.08 0.10 2.6 10.00 2.81 0.0 5.00	DP8(OS2B+B3B)	9.71												30.71	2.29	3.99	1.87	13.74				DP8(C
DP9+B3A1+B3A2) 10.44 0.32 0.52 0.44 0.32 0.50 0.00 0.36 0.00 0.36 0.00 0.36 0.00 0.36 0.00 0.36 0.36	33A1	0.17	0.47	0.62						ی د	4	3.20	0.00	2.00	5.19	9.06	0.40	0.93				B3A1
DP9+B4A1) 10.48 0.32 0.52 0.14 0.32 0.52 0.14 0.23 26 10.00 3.48 0 6.00 2.30 0.00 5.00 5.19 9.06 0.73 2.07 2.09 0.00 5.00 0.00 0.00 0.00 0.00 0.00 0	3P9(DP8+R3A1+R3A2)	10.07	ř.	20.0	L	1			L		L	0.40	30.0	30.71	2 20	3 90	222	14.56	100	00 5	0.33	DP9/L
DP9+B4A1) 10.48 1.11 3.87 1.11 3.87 1.11 3.87 2.53 15.37 2.53 15.37 800 2.30 5.80 DP10+B4A2) 4.19 0.09 0.36 1.51 100 7.00 9.94 890 4.40 3.20 4.64 14.57 3.42 5.97 1.29 9.01	34A1	0.44	0.32	0.52				10.00	-	٥		2.30	00.00	2.00	5.19	9.06	0.73	2.07	3	3	3	B4A1
4.19 0.09 0.36 0.36 0.38 1.51 100 7.00 9.94 890 4.40 3.20 4.64 14.57 3.42 5.97 1.29 9.01 DP7+DP11) 43.21 4.95 16.24 16.24 16.24 16.24 10.12 36.84 2.05 3.58 10.12 58.06	JP10(DP9+B4A1)	10.48												31.04	2.27	3.97	2.53	15.37	800	2.30	5.80	DP10(
14.67 1.49 5.38 8.38 2.05 3.58 3.05 19.24 43.21 4.95 16.24 9.05 3.684 2.05 3.58 10.12 58.06	34A2	4.19	0.09	0.36				7.00	6	986	Ш	3.20	4.64	14.57	3.42	2.97	1.29	9.01				B4A2
43.21 4.95 16.24 10.12 58.06	DP11(DP10+B4A2)	14.67			1.49									36.84	2.05	3.58	3.05	19.24				DP11
	DP12(DP7+DP11)	43.21			4.95									36.84	2.05	3.58	10.12	28.06				DP12

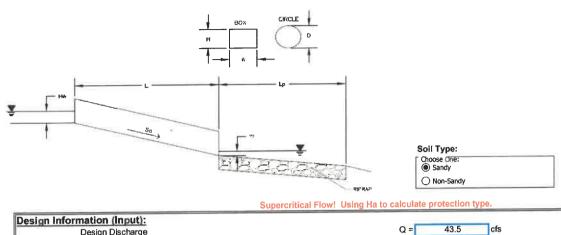
Location Q5 cfs Q100 cfs S % B ft Z D ft d100 ft V fps Froude # Size A1 (DP9) 2.2 14.6 4.5 0.0 4:1,3:1 1.5 0.9 5.2 1.35 ECM A2 (DP2) 1.1 3.1 6.4 0.0 4:1,3:1 2.0 0.5 4.0 1.45 ECM A3 (B4B1) 0.5 1.6 0.0 4:1,3:1 2.0 0.5 4.0 1.45 ECM A3 (B4B1) 0.5 1.6 0.0 4:1,3:1 1.5 0.4 3.4 1.39 ECM A3 (B4B1) 0.5 1.6 0.4 3.4 1.36 ECM 0.34 Use Type D50=12" Riprap B (DP10) 2.5 1.5 0.6 7.1 1.06 Type D50=12" Riprap C (DP11) 3.1 1.6 4.1,3:1 2.0 1.1 7.7 1.86 ECM D (DP4) 4.8 3.0 8.0 0.0 4:1,3:1 2.0 0.71 1.58 ECM E (DP1)	DITCH CAPACITY CALCULATION SHEET	ATION SE	EET				Ī				
Q5 cfs Q100 cfs S % B ft Z D ft d100 ft V fps Froude# 2.2 14.6 4.5 0.0 4:1,3:1 1.5 0.9 5.2 1.35 E 1.1 3.1 6.4 0.0 4:1,3:1 2.0 0.5 4.0 1.45 E 2.5 1.6 6.4 0.0 4:1,3:1 1.5 0.4 3.4 1.39 E 3.1 1.92 10.0 2.0 4:1,3:1 1.5 0.6 5.5 1.55 1.0 4.8 3.0 8.0 0.0 4:1,3:1 2.0 0.7 7.1 1.86 1.0 2.0 4:1,3:1 2.0 0.7 5.2 1.35 E 1.0 2.3 8.0 0.0 4:1,3:1 2.0 0.7 5.2 1.58 E 1.0 2.3 8.0 0.0 4:1,3:1 2.0 4.1,5:1 2.0 4.1,5:1 2.0 4.1,5:1	The material is in a second material and a s									Riprap	
2.2 14.6 4.5 0.0 4:1,3:1 1.5 0.9 5.2 1.35 E 1.1 3.1 6.4 0.0 4:1,3:1 2.0 0.5 4.0 1.45 E 0.5 1.6 6.4 0.0 4:1,3:1 2.0 0.5 4.0 1.45 E 2.5 15.4 6.0 2.0 4:1,3:1 1.5 0.6 5.5 1.55 1.55 3.1 19.2 10.0 2.0 4:1 1.5 0.6 7.1 2.0 4.8 30.6 8.0 0.0 4:1,3:1 2.0 1.7 1.36 E 9.0 2.3 8.0 0.0 4:1,3:1 2.0 1.5 0.5 4.0 1.58 E 9.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 8.2 44.8 1.0 2.0 4:1,3:1 2.0 4:1,3:1 2.0 4:1,3:1 2.0 4:1,3:1 <td< th=""><th>Location</th><th>Q5 cfs</th><th>Q100 cfs</th><th>%</th><th>8#</th><th>7</th><th>D#</th><th>d100 ft</th><th>V fps</th><th>Froude # Size</th><th></th></td<>	Location	Q5 cfs	Q100 cfs	%	8#	7	D#	d100 ft	V fps	Froude # Size	
1.1 3.1 6.4 0.0 4:1,3:1 2.0 0.5 4.0 1.45 E 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	(DP9)	2.2	14.6	4.5	0.0	4:1,3:1	1.5	0.9	5.2	1.35 ECM	
0.5 1.6 6.4 0.0 4:1,3:1 1.5 0.4 3.4 1.39 E 2.5 15.4 6.0 2.0 4:1 1.5 0.6 5.5 1.55 3.1 19.2 10.0 2.0 4:1 1.5 0.6 7.1 2.0 4.8 30.6 8.0 0.0 4:1,3:1 2.0 0.1 7.7 1.36 E 9.9 2.3 8.0 0.0 4:1,3:1 2.0 0.5 5.2 1.35 E 9.9 2.3 8.0 0.0 4:1,3:1 1.6 3.9 0.72 E 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 E 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 E 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 E	A2 (DP2)	1.1	3.1	6.4	0.0	4:1,3:1	2.0	0.5	4.0	1.45 ECM	
2.5 15.4 6.0 2.0 4.1 1.5 0.6 5.5 1.55 1.55 1.55 1.55 1.55 1.55 1.5	A3 (B4B1)	0.5	1.6	6.4	0.0	4:1,3:1	1.5	0.4	3.4	1.39 ECM	
3.1 19.2 10.0 2.0 4.1 1.5 0.6 7.1 2.00 4.8 30.6 8.0 0.0 4.1,3:1 2.0 1.1 7.7 1.86 3.0 16.4 4.4 2.0 4.1,3:1 2.0 0.7 5.2 1.35 E 0.9 2.3 8.0 0.0 4.1,3:1 2.0 1.6 3.9 0.72 8.2 44.8 1.0 2.0 4.1,3:1 2.0 1.6 3.9 0.72 Riprap Size D50=((VS^0.17)/4.5(2)	B (DP10)	2.5	15.4	0.9	2.0	4:1	1.5	9.0	5.5		
4.8 30.6 8.0 0.0 4.1,3:1 2.0 1.1 7.7 1.86 3.0 16.4 4.4 2.0 4.1,3:1 2.0 0.7 5.2 1.35 E 0.9 2.3 8.0 0.0 4:1,3:1 1.5 0.5 4.0 1.58 E 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 Rioran Size D50=((VSY0.17)/4.5(2)	C (DP11)	3.1	19.2	10.0	2.0	4:1	1 .	9.0	7.1		
3.0 16.4 4.4 2.0 4:1,3:1 2.0 0.7 5.2 1.35 E 0.9 0.9 2.3 8.0 0.0 4:1,3:1 1.5 0.5 4.0 1.58 E 0.9 8.2 44.8 1.0 2.0 4:1,3:1 2.0 1.6 3.9 0.72 Riorap Size D50=((VSY0.17)/4.5(2	D2 (DP4)	4.8	30.6	8.0	0.0	4:1,3:1	2.0	1.1	7.7		
0.9 2.3 8.0 0.0 4:1,3:1 1.5 8.2 44.8 1.0 2.0 4:1,3:1 2.0 Riprap	E (DP1)	3.0	16.4	4.4	2.0	4:1,3:1	2.0	0.7	5.2	1.35 Existing Curtis Rd Ditch	
8.2 44.8 1.0 2.0 4:1,3:1 2.0 Riprap	F2 (DP6)	6.0	2.3	8.0	0.0	4:1,3:1	1.5	0.5	4.0	1.58 ECM	
Riprap	G (D7)	8.2	44.8	1.0	2.0	4:1,3:1	2.0	1.6	3.9	0.72	
							ž		V))=050	S^0.17)/4.5(2.5-1)^0.66))^2	

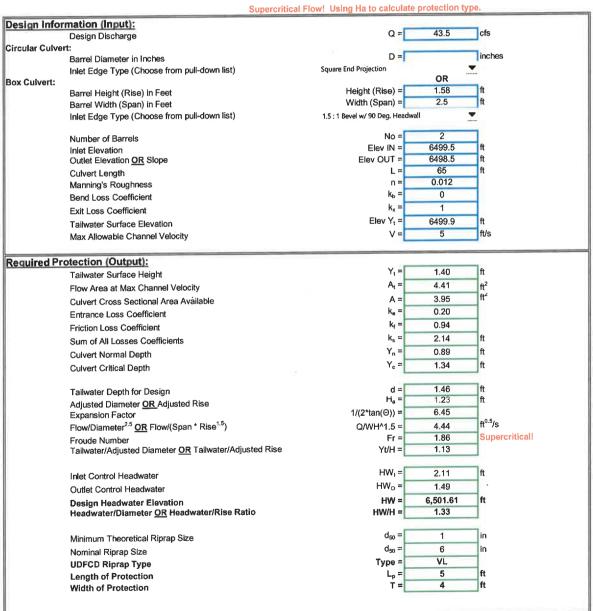
DESIGN FORM	M. M. 1 6/19/23	(11)		=	** 7[LEL. 446.5 (m)	\vdash	-	OUTL VELO	7	S S EXIST PRIME			22			BARREL SELECTED :		7	
1	DESIGNER / DATE : REVIEWER / DATE	ROADWAY ELEVATION : 6502.79		 		- FALL/L.	W.	TAW	E PO	99.7 99.7	101.35 101.35		(6) h. TW or (4c+D/2)(WHICHEVER IS GREATER)	20			CULVERT	SHAPE	MATERIAL:	ENTRANCE
CULVERT	DESIGN	ELEVAT		Ξ 	Z. CHUNAL STREAM BED	S-S-FALL S- 0.014			±Θ	0.1	1.30		HICHEVER	(7) He [+ hg+ (29n2 L) / RL33 V 2/29	!					1
		AD WAY				81 R - 1		OUTLET CONTROL	, i	2.0/	6		D/2)(W	2 L) /R ^{L3}	ء					
		R 0			H		ATIONS	OUTLET	0 S	-	17 1.55	_	or (de	164 (29 n	(6) ELho" ELo+H+ho					
7	ŀ		-	4	ZFALL		CALCULATIONS		de det D	D.7 1.14	1.35 1.47	1	F	<u>ٿ</u>	ELho.					
0+3	-0F	L (1)	4	H			HEADWATER		(S)	0.75	1.5.5		9	E	3					
1					EL 6499.570 (m)		HEAL	H	Et hi	0 42.06	12.001		jo L	(NOI	REAM	N Th				
STATION :	SHEET	ELhd:			ELIE			CONTROL	FALL E	ç Q	0.1		(4) ELN" HW;+ ELI(INVERT OF	LET CONTROL SECTION)	(5) TW BASED ON DOWN STREAM	CHANNEL.				
en .	w							INLET C	HWi	41.0	12.2		HWj+ E1	T CONTR	ASED ON	NOL OR FINEL.	DISCUSSION			
N					1			<u>=</u>	HW //D	24.0	04.1		4) ELN*	INCE	(5) TW B.	CHAN		•		
Suc File			-			15 12	FLOW	BARREL		3.7	22 .50		 _				COMMENTS			l
		«	STREAM SLOPE:		WATER	TW(fi)	TOTAL	F10	0.5	7.4	43.5				CHARTS		8			
PROJECT: WYOMINE BSTATSS		WETHON KON OLD ATA	DRAINAGE AREA: 26.57	HAPE: TO AP	DESIGN FLO	8.1. (YEARS) FLOW(cfs) 5 7.4	CULVERT DESCRIPTION:	MATERIAL - SHAPE - SIZE - ENTRANCE		ENS 2-RCEP-30"XI9" W/FES	*0		TECHNICAL FOOTNOTES:	(I) USE Q/NB FOR BOX CULVERTS	(2) HW, /D . HW /D OR HW, /D FROM DESIGN CHARTS	(3) FALL * HW - (EL _{hd} - EL _{pf}) ; FALL IS ZERO FOR QAVERTS ON GRADE	SUBSCRIPT DEFINITIONS: e. APPROXIMATE f. CULVERT FACE	NA, DESIGN MEADWATER NI. HEADWATER IN INLET CONTROL NO. HEADWATER IN OUTLET CONTROL	1. MILET CONTROL SECTION 0. OUTLET 1. STREAMBED AT CALVERT FACE 1. TAIL MATER	TOTAL TOTAL PER

Determination of Culvert Headwater and Outlet Protection

Project: Wyoming Subdivision

Basin ID: DP7



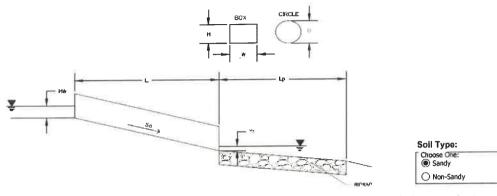


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											٦	REVIE	REVIEWER / DATE	ATE		
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WETHOD: DASTONAL											8	200000				
OBAINAGE AREA: 10 . 16	STREAM SLOPE: 10	E: 10?					7	-	4						H	
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. HOttorgrand Abus III 4	TOTAL	PLOW				Ī	HEADWATER		CALCULATIONS	SNO				N DI	A.I	
COLVERI DESCRIPTION:	204	5		INLET	CONTROL	8			8	OUTLET CONTROL	ONTRO			Air	117 [100	COMMENTS
MATERIAL - SHAPE-SIZE-ENTRANCE	o.	4 -	16	H W.	FALL	1 -	23	۳	9	4		z į	EL ho	ELEV HEAD	00TC	
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AT CHAP WITES	3	A j	4		ال	+	_	_	0						_	5'x 13' A.P.MP 02
	. X	** *	٦	2:2	2:0	43.2	9	0,40	1.70	-10	9	٥	0.74	3	- 1	
					_											
TECHNICAL FOOTHOTES:			(a) EL	(4) EL _N * HW _I * EL _I (INVERT OF	EL;(W)	ERT OF		(6) h.	2	3	W){2/(HICHEV	(6) No. TW or (4c+0/2)(WHICHEVER IS GREATER)	ATTER!		
(1) USE Q/NB FOR BOX CULVERTS			Ĭ	INLET CONTROL SECTIONS	TROL S	ECTION)		E	ن ب	(2342	L3 / R ^L	(7) H. [1. L. (25, (25, 2) / R(35)] V 2/29	62/			
(2) HW, /D . HW /D OR HW /D FROM DESIGN CHARTS	HARTS		(5) T ¥	BASED C	N DOWN	(5) TW BASED ON DOWN STREAM	-	(B) EL	(6) EL _{ho} · EL _e ·H·h _o	# · H · ·						
13) FALL + HW - EL hd - EL tt); FALL IS ZERO			35	CHANNEL.												
SUBSCRIPT DEFINITIONS :	8	COMMENTS		DISCUSSION	NOIS								CULVERT	- 1	BARREL	SELECTED:
S. APPROXIMATE													S12E:			
NA DESIGN NEADMATTR													SHAPE			
No HEADMAIRE IN CUILET CONTINUE. 1 INLET CONTINUE SECTION													MATE	MATERIAL:		
of STREAMED AT CALVERY PACE												7	ENTR	ENTRANCE"		

Determination of Culvert Headwater and Outlet Protection

Project: Wyoming Subdivision

Basin ID: DP9 (** / (5 T)



Supercritical Flow! Using Da to calculate protection type. Design Information (Input): 14.6 cfs Q= Design Discharge Circular Culvert: D = 24 inches Barrel Diameter in Inches Inlet Edge Type (Choose from pull-down list) Grooved End Projection OR Box Culvert: Barrel Height (Rise) in Feet Height (Rise) = Width (Span) = ft Barrel Width (Span) in Feet Inlet Edge Type (Choose from pull-down list) No= Number of Barrels Elev IN = 6543 Inlet Elevation 6541 Outlet Elevation OR Slope Elev OUT = ft Culvert Length L= 65 ft Manning's Roughness n= 0.024 k_b = 0 Bend Loss Coefficient k_x = Exit Loss Coefficient Elev Yt = 6541.7 Tailwater Surface Elevation 5 ft/s Max Allowable Channel Velocity Required Protection (Output): 0.70 Tailwater Surface Height 2.92 ft² ft² Flow Area at Max Channel Velocity 3.14 Culvert Cross Sectional Area Available k. 0.20 Entrance Loss Coefficient k_r : 2.74 Friction Loss Coefficient k_ε = 3.94 Sum of All Losses Coefficients Yn = 1.21 ft Culvert Normal Depth Y_c = ft Culvert Critical Depth 1.38 1.69 d = Tailwater Depth for Design D, = 1.60 ft Adjusted Diameter OR Adjusted Rise $1/(2*tan(\Theta)) =$ 5.50 Expansion Factor ft^{0.5}/s Flow/Diameter^{2.5} OR Flow/(Span * Rise^{1.5}) Q/D^2.5 = 2.58 1.29 Supercritical! Fr = Froude Number Tailwater/Adjusted Diameter OR Tailwater/Adjusted Rise 0.44 Yt/D =HW_i = 2.04 Inlet Control Headwater HWo = 1.01 Outlet Control Headwater HW= 6,545.04 Design Headwater Elevation Headwater/Diameter OR Headwater/Rise Ratio HW/D = 1.02 Minimum Theoretical Riprap Size d₅₀ = 5 $d_{50} =$ 6 in Nominal Riprap Size VL **UDFCD Riprap Type** Type = Length of Protection 12 ft ft Width of Protection

APPENDIX C DESIGN CHARTS

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

	Daniel						Runoff Co	effidents				,	
and Use or Surface haracteristics	Percent Impervious	2-γ	ear	5-γ	631,	10-	read	25-1	ear	50-1	ear	100-	year
		HSG A&B	HSG CAD	HSG ALB	HSECED	HIGAES	HSG CAD	HIGARE	HSG CAD	HSG A&B	HSG C&D	HSG AEB	HSG CAD
usiness													
Commercial Areas	9\$	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0,49	0.53	0,53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8Acre or less	65	0.41	0.45	0.45	0,49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0,46	0.41	0.51	0.46	0.56
1Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0,40	0.50	0.44	0.55
[edustrial													
Ught Areas	80	0.57	0.60	0.59	0.68	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0,71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0,80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0,34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0,48	0.41	0.54
Ratiroad Yard Areas	40	0.23	0.28	0.30	0.35	Q.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Mistoric Flow Analysis Graenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture /Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0,50
Exposed Rock	100	0,89	0.89	0.90	0.90	0.92	0.92	0,94	0,94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	032	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.55
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95		
Gravel	80	0.57	0.60	0.59	0.63	0.53	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Orive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94			_	
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78				The latest designation of the latest designa	
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.5

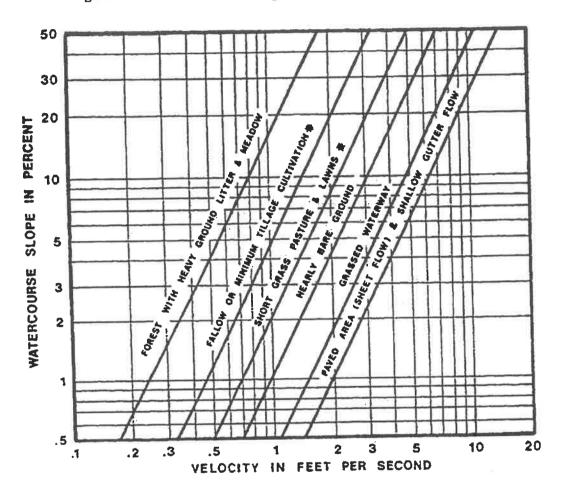


Figure 6-25. Estimate of Average Concentrated Shallow Flow

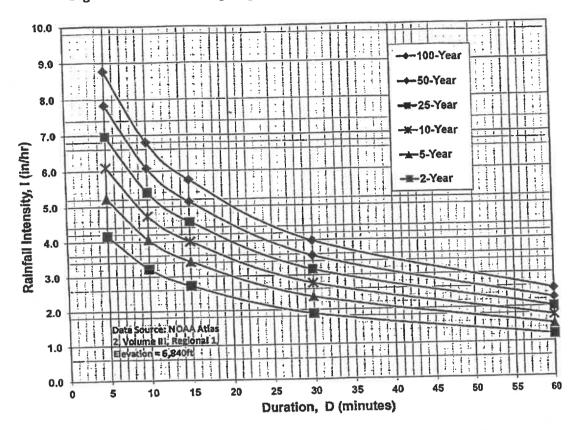


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \text{ ln}(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

