# FINAL DRAINAGE REPORT FOR NORTHERN DELIVERY SYSTEM BOOSTER PUMP STATION

#### PREPARED BY

Richard Gallegos, P.E. RESPEC 121 S. Tejon St., Suite 1110 Colorado Springs, CO 80903

#### PREPARED FOR

Triview Metropolitan District 16055 Old Forest Point STE 300 Monument, CO 80132

April 2023

Project 224.29

El Paso County PD File No. PPR2262





# **ENGINEER'S STATEMENT**

For the County Engineer

This report and plan for the drainage design of Northern Delivery System Booster Pump Station, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I understand that El Paso County does not, and will not, assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.
Richard Gallegos, P.E.  Registered Professional Engineer State of Colorado No. 36247
DEVELOPER'S STATEMENT
The Triview Metropolitan District hereby certifies that the drainage facilities for the Northern Delivery System Booster Pump Station shall be constructed according to the design presented in this report. I understand that El Paso County does not, and will not, assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to El Paso County; and cannot, on behalf of the Northern Delivery System Booster Pump Station guarantee that final drainage design review will absolve the Triview Metropolitan District and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.
James M Trady 5-26-23
Printed Name  Date
Title Address: 16055 OLI FIRST POINT  SUITE 302  MONUMENT, CO 80132
EL PASO COUNTY STATEMENT
Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Date



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#### 1.0 PURPOSE

This drainage report is for the design of the Northern Delivery System Booster Pump Station. The site is located along Highway 83, Colorado Springs, Colorado in central El Paso County. See Vicinity Map in the Appendix below for reference. It is further described as the Southwest One-Quarter of the Northwest One-Quarter of Section 3, Township 12 South, Range 66 West of the 6<sup>th</sup> P.M. This 9.75-acre site is located within the Black Squirrel Creek – FOMO3600 basin.

One Drainage Basin Planning Study for Black Squirrel Creek was found within the County's files that included the project site:

 Black Squirrel Creek Drainage Basin Planning Study Final Report, City of Colorado Springs and El Paso County, January of 1989

The site is bounded to the west by Highway 83. Work will include the construction of a 1500 square foot (sf) pump station and asphalt driveway. No portion of the site is located within a FEMA designated 100-year floodplain per Map No. 08041C0295G that was effective on December 7<sup>th</sup>, 2018.

## 2.0 SOIL CONDITIONS

According to the El Paso County Area Soil Survey, the soil on the site is classified as follows:

SOIL#	SOIL TYPE	HYDROLOGIC CLASSIFICATION	PERCENT OF SITE
41	Kettle Gravelly Loamy Sand, 8 to 40 Percent Slopes	В	10.8%
69	Peyton-Pring Complex, 8 to 15 Percent Slopes	В	0.0%
71	Pring Coarse Sandy Loam, 3 to 8 Percent Slopes	В	89.2%

The Kettle Gravelly soil can be described as having a high permeability, low surface runoff, and slight hazard of erosion. The Pring Coarse Sandy soils is described, similarly, as having high permeability and low surface runoff. The hydrologic soil classification used for this study is 'B'. See Soils Map in the Appendix for reference.



### 3.0 HYDROLOGIC CRITERIA

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual*. All references from the *El Paso County Drainage Criteria Manual* can be found in Appendix C. The Rational Method for computation of runoff was used.

Q = cia Where

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration required for the runoff

to become established

a = drainage basin size in acres

The storm recurrence intervals, used to determine swale capacity, for this study were the 10-year storm and the 100-year storm. ManningSolver Version 1.019 was used in this analysis to calculate the Manning's normal depth.

## 4.0 EXISTING DRAINAGE CONDITIONS

The overall site consists of 9.75 acres. The site includes an existing water storage tank and gravel driveway. The areas of the site not covered by the potable water tank or gravel driveway are covered with scrub oak, grass, willows and pine trees. These undeveloped areas include slopes that range from 4.9% to 34.1%. The overall existing site is 3.5% impervious. See Existing Drainage Map in the Back Pocket for reference.

Flows from Sub-basin OS1, Sub-basin OS2, and Sub-basin Aex through Sub-basin Gex are tributary to the Black Squirrel Creek – FOMO3600 drainage basin.

Sub-basin OS1 contains 3.85 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 3.5 cfs for the 10-year storm and 9.2 cfs for the 100-year storm. These flows sheetflow to the southeast over nearly bare ground.

Sub-basin OS2 consists of 3.69 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 2.8 cfs for the 10-year storm and 8.5 cfs for the 100-year storm. These flows sheetflow to the southeast. Flows from Sub-basin OS2 combine with flows from Sub-basin Eex, Sub-basin Fex, and Sub-basin Gex to produce total flows of 7.5 cfs for the 10-year storm and 20.8 cfs for the 100-year storm at Design Point 1 (DP1). These flows proceed into the stream tributary to Black Squirrel Creek that is located southeast of the site.

Sub-basin Aex contains 3.89 acres and drains south towards a private access road. This sub-basin produces existing flows of 2.4 cfs for the 10-year storm and 7.8 cfs for the 100-year storm. These flows sheetflow to the south.



Sub-basin Bex consists of 2.37 acres and drains south along a private access road. This sub-basin produces existing flows of 2.1 cfs for the 10-year storm and 5.9 cfs for the 100-year storm. These flows sheetflow in the southerly direction.

Sub-basin Cex contains 7.96 acres and drains south towards a private access road. This sub-basin produces existing flows of 5.4 cfs for the 10-year storm and 17.4 cfs for the 100-year storm. These flows sheetflow to the south.

Sub-basin Dex consists of 3.98 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. It produces flows of 2.7 cfs for the 10-year storm and 9.2 cfs for the 100-year storm. These flows sheetflow to the southeast, ultimately ending up in the stream noted on the Existing Drainage Plan in the Back Pocket. Flows from Sub-basin Dex combine with flows from Sub-basin Cex, Sub-basin OS1, and Design Point 1 (DP1) to produce total flows of 15.8 cfs for the 10-year storm and 46.9 cfs for the 100-year storm at Design Point 2 (DP2). These flows continue along the stream towards Black Squirrel Creek.

Sub-basin Eex contains 2.79 acres and drains east towards Sub-basin OS2. It produces flows of 3.3 cfs for the 10-year storm and 8.3 cfs for the 100-year storm. These flows sheetflow to the east, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin Fex contains 1.15 acres and drains southeast towards Sub-basin OS2. It produces flows of 1.4 cfs for the 10-year storm and 3.4 cfs for the 100-year storm. These flows sheetflow to the southeast, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin Gex consists of 0.96 acres and drains southeast towards Sub-basin OS1. It produces flows of 0.7 cfs for the 10-year storm and 2.5 cfs for the 100-year storm. These flows sheetflow to the southeast into the stream that is tributary to Black Squirrel Creek.

The estimated runoff amounts produced for the project under Existing Conditions are shown in Table 1 below.

TABLE 1 – EXISTING CONDITIONS											
Sub-basin	Q <sub>10</sub> (CFS)	Q <sub>100</sub> (CFS)									
0\$1	3.5	9.2									
0\$2	2.8	8.5									
Aex	2.4	7.8									
Bex	2.1	5.9									
Cex	5.4	17.4									
Dex	2.7	9.2									
Eex	3.3	8.3									
Fex	1.4	3.4									
Gex	0.7	2.5									
DP1 (Eex + Fex + Gex + OS2)	7.5	20.8									
DP2 (DP1 + Cex + Dex + OS1)	15.8	46.9									



### **5.0 DEVELOPED DRAINAGE CONDITIONS**

The overall site consists of 9.75 acres, of which 0.9 acres will be disturbed for permanent improvements as part of this project. A booster pump station building and 15' wide asphalt access road is proposed on the east side of the site. A secondary gate access road is also proposed on the south end of the site along that connects the site to the existing private asphalt driveway. Proposed Conditions Map is located below in the Back Pocket for reference.

Proposed site imperviousness is 5.4%, versus 3.5% in the existing conditions. Proposed flows are tributary to the Black Squirrel Creek – FOMO3600 drainage basin.

Sub-basin OS1 contains 3.85 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 3.5 cfs for the 10-year storm and 9.2 cfs for the 100-year storm. These flows sheetflow to the southeast over nearly bare ground.

Sub-basin OS2 contains 3.68 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 2.8 cfs for the 10-year storm and 8.5 cfs for the 100-year storm. These flows sheetflow to the southeast. Flows from Sub-basin OS2 combine with flows from Sub-basin E, Sub-basin F, and Sub-basin G to produce total flows of 8.2 cfs for the 10-year storm and 22.0 cfs for the 100-year storm at Design Point 1 (DP1). These flows proceed into the stream tributary to Black Squirrel Creek that is located southeast of the site.

Sub-basin A consists of 3.89 acres and drains south towards a private access road. This sub-basin produces existing flows of 2.4 cfs for the 10-year storm and 7.8 cfs for the 100-year storm. These flows sheetflow to the south.

Sub-basin B contains 2.37 acres and drains south along a private access road. This sub-basin produces existing flows of 2.3 cfs for the 10-year storm and 6.1 cfs for the 100-year storm. These flows sheetflow in the southerly direction.

Sub-basin C consists of 7.96 acres and drains south towards a private access road. This sub-basin produces existing flows of 5.4 cfs for the 10-year storm and 17.4 cfs for the 100-year storm. These flows sheetflow to the south over all roads (existing and proposed).

Sub-basin D contains 3.98 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. It produces flows of 3.1 cfs for the 10-year storm and 9.8 cfs for the 100-year storm. These flows sheetflow to the southeast over the proposed access road, ultimately ending up in the stream noted on the Existing Drainage Plan in the Back Pocket. Flows from Sub-basin D combine with flows from Sub-basin C, Sub-basin OS1, and Design Point 1 (DP1) to produce total flows of 16.8 cfs for the 10-year storm and 48.3 cfs for the 100-year storm at Design Point 2 (DP2). These flows continue along the stream towards Black Squirrel Creek.

Sub-basin E contains 2.83 acres and drains east towards the proposed pump station. It produces flows of 3.8 cfs for the 10-year storm and 9.1 cfs for the 100-year storm. Two 1.25' deep triangular swales



with 4:1 side slopes route these flows around the proposed pump station. These flows sheetflow to the east, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin F consists of 1.15 acres and drains southeast towards Sub-basin OS2. It produces flows of 1.4 cfs for the 10-year storm and 3.4 cfs for the 100-year storm. These flows sheetflow to the southeast, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin G contains 0.96 acres and drains southeast towards Sub-basin OS1. It produces flows of 1.1 cfs for the 10-year storm and 3.0 cfs for the 100-year storm. These flows sheetflow to the southeast over the proposed access road and into the stream that is tributary to Black Squirrel Creek.

The estimated runoff amounts produced for the project under Proposed Conditions are shown in Table 2 below.

TAE	BLE 2 - PROPOSED CONDITIONS	
Sub-basin	Q <sub>10</sub> (CFS)	Q <sub>100</sub> (CFS)
0\$1	3.5	9.2
OS2	2.8	8.5
A	2.4	7.8
В	2.3	6.1
С	5.4	17.4
D	3.1	9.8
E	3.8	9.1
F	1.4	3.4
G	1.1	3.0
DP1 (E + F + G + OS2)	8.3	22.1
DP2 (DP1 + C + D +OS1)	16.8	48.3

# **6.0 WATER QUALITY**

The total disturbance for this development will be 0.98 acres. Due to the proximity of an environmentally sensitive area located west of the project site and as part of the El Paso County regulations, an Erosion and Stormwater Quality Control Permit (ESQCP) will be prepared and submitted separately from this Final Drainage Report. The site is also less than one-acre of disturbance area, and therefore does not require additional water quality features.



#### 7.0 FOUR STEP PROCESS

El Paso County utilizes a "Four Step Process" for receiving water protection, which focuses on reducing runoff volumes and implementing long-term source controls and is intended to help manage more frequently occurring storm events. A summary of the Four Step Process for this project is as follows.

- Step 1: Reduce runoff by disconnecting impervious area, eliminating "unnecessary impervious
  area and encouraging infiltration into soils that are suitable. For this project, the following
  elements will be implemented:
  - Use of gravel parking areas adjacent to the building rather than use of asphalt, allowing additional area of infiltration
  - Runoff from the pump station rooftop will discharge onto landscaped areas and reseeded areas adjacent to the building
  - The proposed asphalt road is sloped to the southeast to encourage sheet flow patterns across the driveway and onto areas with native grasses prior
  - Use of curb and gutter and a crowned section was avoided for the asphalt drive to avoid point discharges
- Step 2: Treat and slowly release the Water Quality Capture Volume
  - The site is less than one-acre in size and does not require formal Water Quality treatment
  - Where possible, sheet flow patterns are maintained to help enhance water quality
- Step 3: Stabilize stream channels
  - o There are no major drainageways within the project boundary
  - A tributary to Black Squirrel Creek exists to the east
  - An environmentally sensitive area exists to the east of the site. Proposed improvements have been offset as much as reasonably from the area to provide a buffer, including allowing sheet flow patterns to filter through native grasses.
  - Grass swales will direct flows around the proposed building, allowing for additional infiltration
- Step 4: Implement Source Controls
  - Erosion control measures will be installed during prior to, and during the initial construction activities at the site to provide source control of sediment
  - Landscaping will be placed within the proposed development and permanent seeding of all disturbed areas will be completed per the Grading and Erosion Control Plan requirements
  - No other potential pollutants are anticipated from the site, post construction

The development of this site will have no adverse impacts on downstream properties.



#### 8.0 EROSION CONTROL PLAN

The site construction consists of constructing a new pump station and an asphalt access road, disturbing 0.98 acres of area. This does not require an Erosion and Stormwater Quality Control Permit. However, a Grading and Erosion Control Plan will be submitted in separate Construction Plans.

# 9.0 FLOODPLAIN STATEMENT

No portion of the developed site is located within a designated FEMA 100-year floodplain according to the information published in the Federal Emergency Management Agency Flood Plain Map No. 08041C0295G dated December 7<sup>th</sup>, 2018. No portion of the site lies within the Zone 'A' of Black Squirrel Creek as noted on Map No. 08041C0295G.

#### **10.0 DRAINAGE BASIN FEES**

The proposed development is located within the Black Squirrel Drainage Basin, which assesses drainage and bridge fees at the time of platting. A plat is not proposed as part of this project, so do drainage or bridge fees are due.

# 10.0 CONSTRUCTION COST OPINION

Flows will either sheet flow or be directed to outfall points via ditch. No culverts, storm sewers, or other drainage structures are needed for this project, and no Construction Cost Opinion is required for this report.

#### 11.0 CONCLUSIONS

For this 9.75-acre site, work will include constructing a booster pump station and 15' wide asphalt access road. Additionally, a secondary gate access road will be constructed that will allow access from the site from the private driveway south of the property. The total anticipated disturbance of the site will be 0.9 acres. The development increases total routed flows exiting the site at Design Point 2 (DP2) from 15.9 cfs to 16.8 cfs for the 10-year storm, while the 100-year storm flow increases from 46.9 cfs to 48.4 cfs. These increases do not warrant the need for detention. All developed flows will continue to flow along existing drainage patterns.

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Disturbed areas shall be permanently stabilized as soon as construction activities are completed. Areas to be re-vegetated shall be treated with soil amendments to provide an adequate growth medium to sustain vegetation and shall match the pre-existing, pre-disturbed vegetation cover. Erosion control



measures will be installed during construction of the proposed site per the approved Grading and Erosion Control Plan to be submitted separately for review and approval. Site runoff, storm drains, and appurtenances associated with the development of the Triview Metropolitan District Northern Delivery System Booster Pump Station will not adversely affect the downstream and surrounding developments.

# 12.0 REFERENCES

Black Squirrel Creek Drainage Basin Planning Study Final Report, City of Colorado Springs and El Paso County, January of 1989

*Flood Insurance Rate Map Number 08041C0295G*, Federal Emergency Management Agency Floodplain Data, revised December 7, 2018

Municipal Code Corporation (2018). Drainage Criteria Manual of El Paso County, Colorado (DPM)

Urban Drainage and Flood Control District (June 2017). *Urban Storm Drainage Criteria Manual, Volume* 1-3.

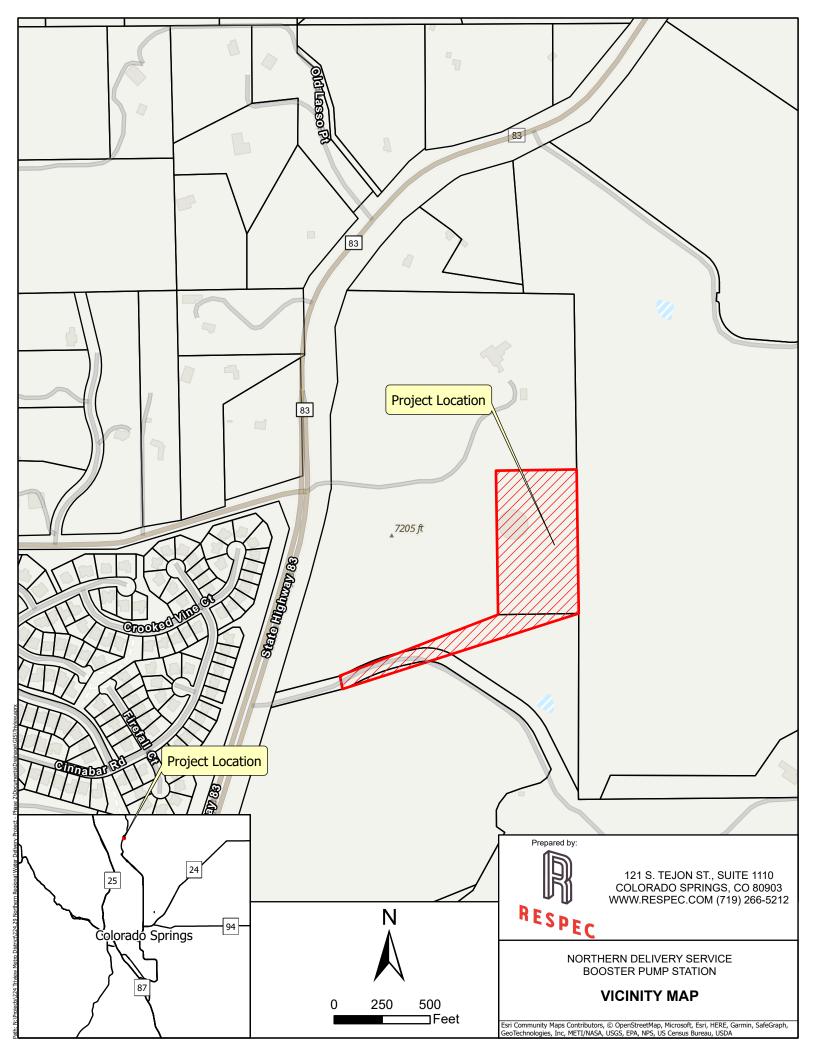
USDA, NRCS. Soil Survey of El Paso County Area, Colorado.

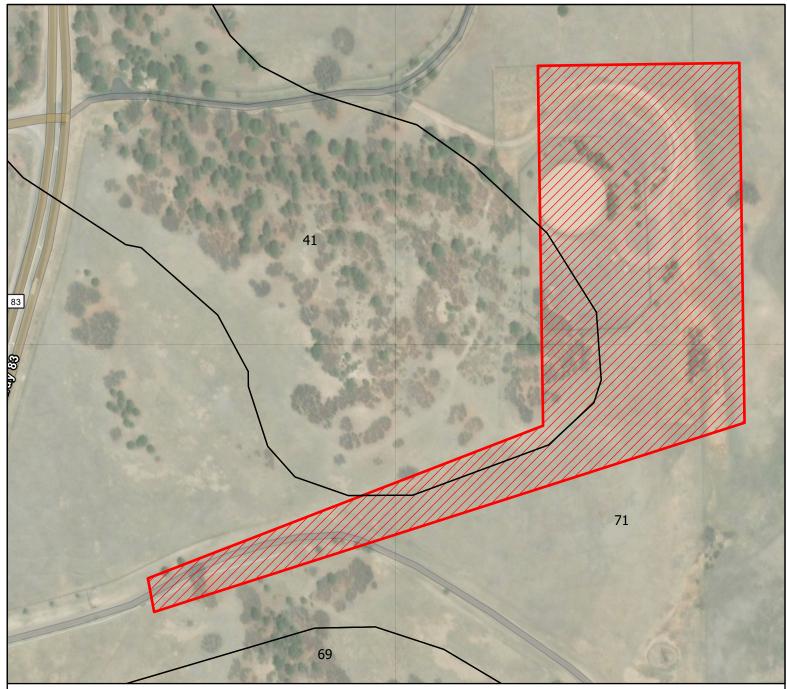


# **APPENDIX A**

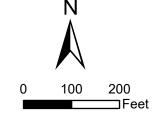
**MAPS** 







Map Unit Symbol	Map Unit Name	Rating	Percent of Site, %
41	Kettle gravelly loamy sand, 8 to 40 perent slopes	В	10.8
69	Peyton-Pring complex, 8 to 15 percent slopes	В	0.0
71	Pring coarse sandly loam, 3 to 8 percent slopes	В	89.2



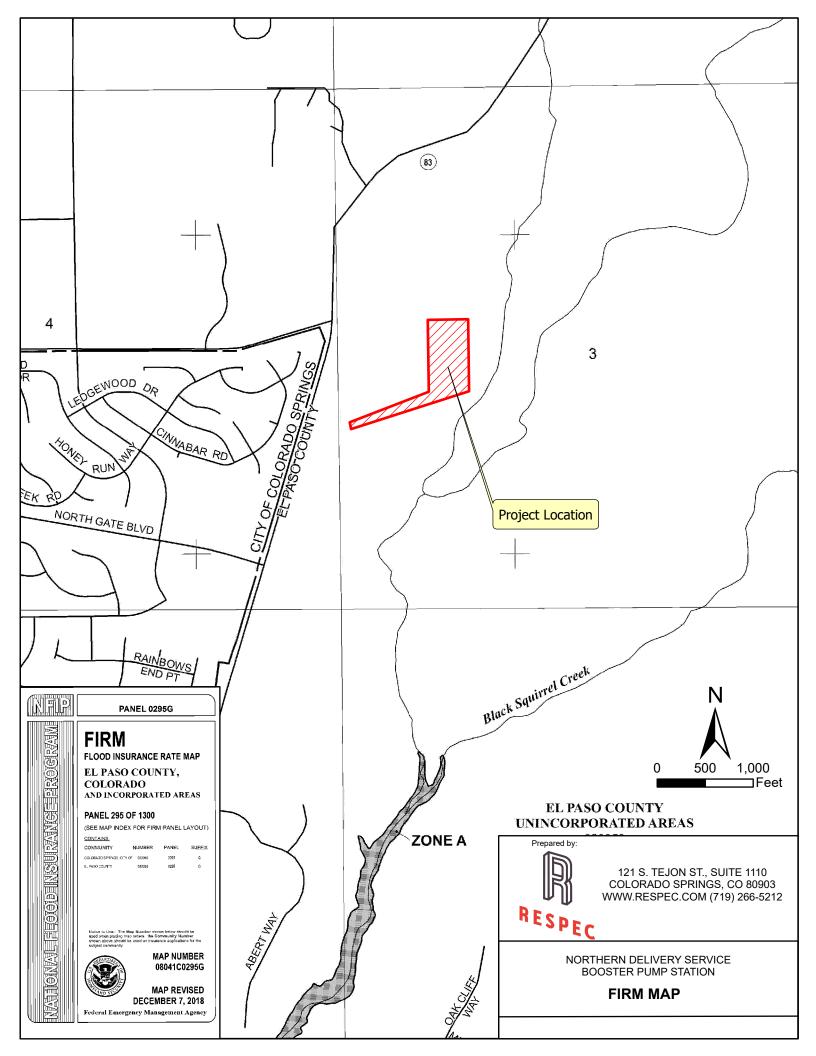


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NORTHERN DELIVERY SERVICE BOOSTER PUMP STATION

**SOILS MAP** 

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# **APPENDIX B**

**CALCULATIONS** 



Northern Deli	very Service Bo	ooster Pump	Station						
PROJ.224.29		_							
C FACTOR C	<b>ALCULATION S</b>	HEET							
<b>EXISTING CO</b>	NDITIONS								
<b>RUNOFF COE</b>	FICIENT								
TYPE A/B SO	ILS								
LAND USE		Imperv %	10 YR	100 YR					
UNDEV		0	0.15	0.35					
<b>GRAVEL ROA</b>		80	0.63						
ASPHALT RO	AD	100							
ROOFS		90	0.75	0.81					
			_						
				XISTING CO	NDITIONS				
	TOTAL		E CONDITIO			CALCULATED C			
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	10	100	% IMPE	RVIOUS
DESIG.	(acre)		ROAD	ROAD		YR	YR		10.05
OS1	3.85		0.58		0.00		0.40		12.05
OS2	3.68		0.14	0.00	0.00	0.17	0.36		3.04
Aex	3.89				0.00	0.16	0.36		2.06
Bex	2.37			0.00	0.00	0.19	0.38		7.43
Cex	7.96			0.00	0.00	0.16	0.36		2.11
Dex	3.98				0.00	0.15	0.35		0.00
Eex	2.79			0.00	0.25	0.22	0.39		8.64
Fex	1.15				0.13	0.25	0.41		12.26
Gex	0.96	0.96	0.00	0.00	0.00	0.15	0.35		0.00
0.1 D		0.40							
Site Percent Ir	npervious, %	3.49							

PROPOSED (	CONDITIONS													
RUNOFF COE	FICIENT													
TYPE A/B SO	ILS													
LAND USE		Imperv %	10 YR	100 YR										
UNDEV		0	0.15	0.35										
GRAVEL ROA	AD	80	0.63											
ASPHALT RO		100	0.92	0.96										
ROOFS		90	0.75											
	PROPOSED CONDITIONS													
	TOTAL	SURFAC	E CONDITIO	N AREAS		CALCUL	ATED C							
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	10	100	% IMPE	RVIOUS					
DESIG.	(acre)		ROAD	ROAD		YR	YR							
OS1	3.85				0.00	0.22	0.40		12.05					
OS2	3.72	3.58			0.00	0.17	0.36		3.01					
A	3.89	3.79			0.00	0.16	0.36		2.06					
В	2.37	2.12		0.04	0.00	0.21	0.39		8.78					
С	7.96			0.03	0.00	0.16	0.36		2.49					
D	3.98	3.83			0.00	0.17	0.37		3.77					
E	2.83	2.45			0.28	0.25	0.42		12.44					
F	1.15				0.13	0.25	0.41		12.26					
G	0.96	0.85	0.00	0.11	0.00	0.22	0.42		11.46					
Sita Dargant In	mportious 9/	5.35												
Site Percent Ir	ripervious, %	5.35												

Northern Delivery Service	ce Booster	Pump Station	n l															
PROJ.224.29	1																	
DRAINAGE CALCULAT	ION SHEE	ΪΤ																
file:North Delivery Service			n.xlsx															
OCTOBER 2022																		
							Initial Tci			Travel T	ime							
AREA	AREA	C10	C100	C10 X A	C100 X A		Slope	ti		Slope	V	Tt	TC	I10	I100	Q10	Q100	AREA
DESIG.	(acre)	(10 yr)	(100 yr)			L (ft)	(%)	(min)	L (ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)	DESIG.
		, ,					,											
EXISTING	1																	
CONDITIONS																		
OS1	3.85	0.22	0.40	0.85	1.54	100	5.50	9.38	780	6.10	2.40	5.42	14.79	4.13	5.95	3.5	9.2	OS1
OS2	3.69	0.17	0.36	0.63	1.33	100	7.40	8.98	495	6.60	2.50	3.30	12.28	4.46	6.41	2.8	8.5	OS2
Aex	3.89	0.16	0.36	0.62	1.40	100	7.20	9.16	1125	5.90	2.40	7.81	16.98	3.89	5.60	2.4	7.8	Aex
Bex	2.37	0.19	0.38	0.45	0.90	80	11.40	6.82	635	5.70	2.20	4.81	11.63	4.55	6.55	2.1	5.9	Bex
Cex	7.96	0.16	0.36	1.27	2.87	100	10.60	8.07	1000	8.60	2.80	5.95	14.02	4.23	6.08	5.4	17.4	Cex
Dex	3.98	0.15	0.35	0.60	1.39	100	10.20	8.26	580	9.70	3.10	3.12	11.37	4.59	6.61	2.7	9.2	Dex
Eex	2.79	0.22	0.39	0.61	1.09	70	24.20	4.81	535	10.20	3.20	2.79	7.60	5.30	7.62	3.3	8.3	Eex
Fex	1.15	0.25	0.41	0.29	0.47	55	3.20	8.03	180	14.40	3.30	0.91	8.94	5.01	7.21	1.4	3.4	Fex
Gex	0.96	0.15	0.35	0.14	0.34	100	12.00	7.82	155	12.90	3.20	0.81	8.63	5.08	7.30	0.7	2.5	Gex
DP1 (Eex + Fex + Gex	8.59	0.19	0.38	1.67	3.22	100	12.00	7.46	750	7.90	2.70	4.63	12.09	4.49	6.46	7.5	20.8	DP1 (Eex + Fex +
+ OS2)	0.00	0.13	0.50	1.07	0.22	100	12.00	7.40	730	7.50	2.70	4.00	12.00	7.70	0.40	7.5	20.0	Gex + OS2)
DP2 (DP1 + Cex + Dex	24.38	0.18	0.37	4.39	9.02	100	10.60	7.89	1880	7.30	2.60	12.05	19.94	3.61	5.19	15.8	46.9	DP2 (DP1 + Cex +
+ OS1)	21.00	0.10	0.07	1.00	0.02	100	10.00	1.00	1000	7.00	2.00	12.00	10.01	0.01	0.10	10.0	10.0	Dex + OS1)
PROPOSER																		
PROPOSED																		
CONDITIONS	0.05	0.00	0.40	0.05	4.54	400	5.50	0.00	700	0.40	0.40	5.40	44.70	1.10	5.05	0.5	0.0	004
OS1	3.85	0.22	0.40	0.85	1.54	100	5.50	9.38	780	6.10	2.40	5.42	14.79	4.13	5.95	3.5	9.2	OS1 OS2
OS2	3.68	0.17	0.36 0.36	0.63 0.62	1.32	100	7.40	8.98	495	6.60	2.50	3.30	12.28	4.46	6.41	2.8	8.5	052
A D	3.89 2.37	0.16 0.21	0.30	0.62	1.40 0.92	100 80	7.20 11.40	9.16 6.67	1125 635	5.90 5.70	2.40	7.81 4.81	16.98 11.48	3.89 4.58	5.60 6.58	2.4	7.8 6.1	B
<u>С</u>	7.96	0.21	0.36	1.27	2.87	100	10.60	8.07	1000	8.60	2.80	5.95	14.02	4.33	6.08	5.4	17.4	C
	3.98	0.10	0.37	0.68	1.47	100	10.20	8.08	580	9.70	3.10	3.12	11.20	4.62	6.65	3.1	9.8	D
F	2.83	0.25	0.42	0.71	1.19	70	24.20	4.65	535	10.20	3.20	2.79	7.43	5.34	7.68	3.8	9.1	뉘
F	1.15	0.25	0.41	0.29	0.47	55	3.20	8.03	180	14.40	3.30	0.91	8.94	5.01	7.21	1.4	3.4	<del>                                     </del>
G	0.96	0.22	0.42	0.21	0.40	100	12.00	7.25	155	12.90	3.20	0.81	8.05	5.20	7.48	1.1	3.0	G
DP1 (E + F + G + OS2)	9.60	0.21	0.39	1.82	3.39	100	12.00	7.32	750	7.90	2.70	4.63	11.95	4.51	6.48	8.2	22.0	DP1 (E + F + G +
DP2 (DP1 + C + D +					+					+					+			OS2) DP2 (DP1 + C + D +
OS1)	24.41	0.19	0.38	4.62	9.27	100	10.60	7.81	1880	7.30	2.60	12.05	19.87	3.62	5.20	16.7	48.2	OS1)
																		231)
										+					1			
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#### **Manning Formula:**

#### **Irregular Section**

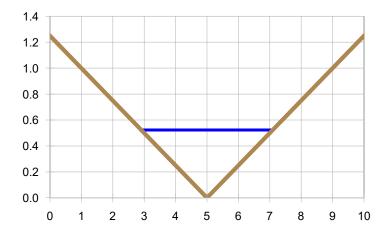
Input

Flow 3.8 cfs Slope 0.085 ft/ft

Sta Elev n Sta Elev Sta Elev n Sta Elev n 0.05 0.05 1.25 1.25 0.05 10

#### Output

**WSElev** 0.523 ft 1.09 sf Flow Area 3.47 fps Velocity Velocity Head 0.187 ft Top Width 4.18 ft Froude Number 1.20 Critical WSElev 0.562 ft Critical Slope ft/ft



#### **Irregular Section**

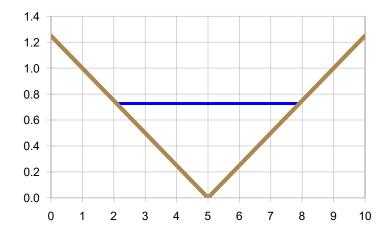
Input

Flow 9.1 cfs Slope 0.085 ft/ft

Sta Elev n Sta Elev Sta Elev n Sta Elev n 0.05 0.05 0.05 1.25 1.25 10

#### Output

WSElev 0.726 ft Flow Area 2.11 sf 4.32 fps Velocity Velocity Head 0.290 ft Top Width 5.81 ft Froude Number 1.26 Critical WSElev 0.797 ft Critical Slope ft/ft





# **APPENDIX C**

**DESIGN CHARTS** 

#### 3.1. - Rational Method Runoff Coefficient (C)

The runoff coefficient represents the integrated effects of infiltration, detention storage, evaporation, retention, flow routing, and interception, all of which affect the time distribution and peak rate of runoff. Runoff coefficients are based on the imperviousness of a particular land use and the hydrologic soil type of the area and are to be selected in accordance with Table 6-6.

The procedure for determining the runoff coefficient includes these steps:

- 1. Categorize the site area into one or more similar land uses, each with a representative imperviousness, according to the information in Table 6-6.
- 2. Based on the dominant hydrologic soil type in the area, use Table 6-6 to estimate the runoff coefficient for the particular land use category for the design storms of interest.
- 3. Calculate an area-weighted average runoff coefficient for the site based on the runoff coefficients from individual land use areas of the site.

When analyzing an area for design purposes, urbanization of the full watershed, including both on-site and off-site areas, shall be assumed.

Gravel parking areas, storage areas, and access drives proposed on Site Improvement Plans shall be analyzed based on an imperviousness of 80%. This is due to the potential for gravel areas being paved over time by property owners and the resulting adverse impacts on the stormwater management facilities and adjacent properties.

There are some circumstances where the selection of impervious percentage values may require additional investigation due to unique land characteristics (e.g., recent burn areas). When these circumstances arise, it is the designer's responsibility to verify that the correct land use assumptions are made.

When multiple sub-basins are delineated, the composite C value calculation is:

$$C_c = (C_1 A_1 + C_2 A_2 + C_3 A_3 + ... C_i A_i)/A_t$$
 (Eq. 6-6)

#### Where:

C<sub>c</sub> = composite runoff coefficient for total area

C<sub>i</sub> = runoff coefficient for subarea corresponding to surface type or land use

A i = area of surface type corresponding to Ci (units must be the same as those used for total area)

A t = total area of all subareas for which composite runoff coefficient applies

i = number of surface types in the drainage area

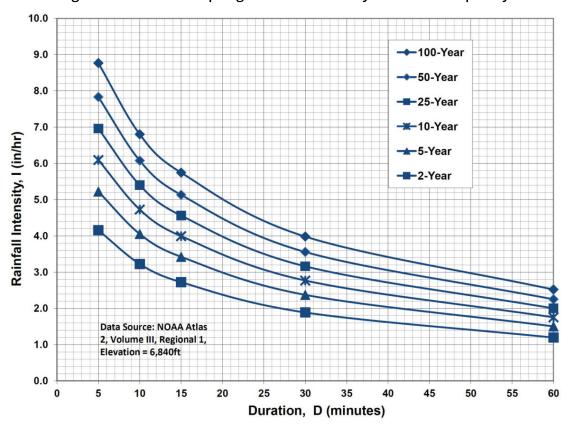
Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

Land Use or	Percent	Runoff Coef	Runoff Coefficients										
Surface Characteristics	Impervious	2-year	5-year	10-year	25-year	50-year	100-year						

		HSG A&B	HSG C&D										
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
⅓ Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
¼ Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
⅓ Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
½ Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													

Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



#### **IDF** Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

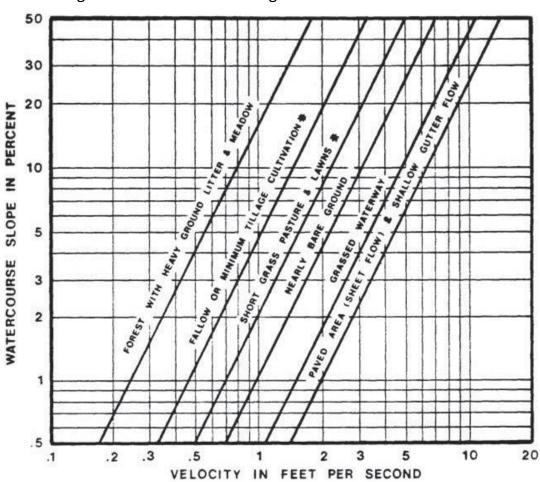
$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Figure 6-25. Estimate of Average Concentrated Shallow Flow





# **BACK POCKET**



