

# FINAL DRAINAGE REPORT FOR Northern Delivery System Booster Pump Station

PREPARED BY Richard Gallegos, P.E. RESPEC 121 S. Tejon St., Suite 1110 Colorado Springs, CO 80903

PREPARED FOR Triview Metropolitan District 16055 Old Forest Point STE 300 Monument, CO 80132

November 2022

Project 224.29

Add PCD File No. PPR-2262





#### **ENGINEER'S STATEMENT**

This report and plan for the drainage design of Northern Delivery System Booster Pump Station, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I understand that El Paso County does not, and will not, assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Richard Gallegos, P.E. Date Registered Professional Engineer State of Colorado No. 36247

#### **DEVELOPER'S STATEMENT**

The Triview Metropolitan District hereby certifies that the drainage facilities for the Northern Delivery System Booster Pump Station shall be constructed according to the design presented in this report. I understand that El Paso County does not, and will not, assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to El Paso County; and cannot, on behalf of the Northern Delivery System Booster Pump Station guarantee that final drainage design review will absolve the Triview Metropolitan District and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

Authorized Signature

Date

Printed Name

Address:

Title

### **EL PASO COUNTY STATEMENT**

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.



Replace with the following: "Joshua Palmer, P.E. Date

County Engineer / ECM Administrator Conditions: " Date



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#### **1.0 PURPOSE**

This drainage report is for the design of the Northern Delivery System Booster Pump Station. The site is located along Highway 83, Colorado Springs, Colorado in central El Paso County. See Vicinity Map in the Appendix below for reference. It is further described as the Southwest One-Quarter of the Northwest One-Quarter of Section 3, Township 12 South, Range 66 West of the 6<sup>th</sup> P.M. This 9.75-acre site is located within the Black Squirrel Creek – FOMO3600 basin.

One Drainage Basin Planning Study for Black Squirrel Creek was found within the County's files that included the project site:

• Black Squirrel Creek Drainage Basin Planning Study Final Report, City of Colorado Springs and El Paso County, January of 1989

The site is bound on the west by Highway 83 and on the south by Roller Coaster Drive. Work will include the construction of a 1500 square foot (sf) pump station and asphalt driveway. With an area of disturbance less than 1 acre, detention will not be required for the site per El Paso County Engineering Criteria Manual (ECM) Appendix I.7, 1.B. No portion of the site is located within a FEMA designated 100-year floodplain per Map No. 08041C0295G that was effective on December 7<sup>th</sup>, 2018.

### **2.0 SOIL CONDITIONS**

Remove inaccurate statement. Criteria does not imply detention will not be required for disturbance that is less than 1 acre.

According to the El Paso County Area Soil Survey, the soil on the site is classified as follows:

SOIL #	SOIL TYPE	HYDROLOGIC CLASSIFICATION	PERCENT OF SITE
41	Kettle Gravelly Loamy Sand, 8 to 40 Percent Slopes	В	10.8%
69	Peyton-Pring Complex, 8 to 15 Percent Slopes	В	0.0%
71	Pring Coarse Sandy Loam, 3 to 8 Percent Slopes	В	89.2%

The Kettle Gravelly soil can be described as having a high permeability, low surface runoff, and slight hazard of erosion. The Pring Coarse Sandy soils is described, similarly, as having high permeability and low surface runoff. The hydrologic soil classification used for this study is 'B'. See Soils Map in the Appendix for reference.

#### **3.0 HYDROLOGIC CRITERIA**

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual*. All references from the *El Paso County Drainage Criteria Manual* can be found in Appendix C. The Rational Method for computation of runoff was used.



FYI minor flows are 5 year per our criteria. You may change the 10 year analysis to the 5 year if you like. If change in analysis is done please change throughout report.

RESPEC

Where

Q = cia

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration required for the runoff to become established

a = drainage basin size in acres

The storm recurrence intervals, used to determine swale capacity, for this study were the  $10^{-1}$ -year storm and the 100-year storm. ManningSolver Version 1.019 was used in this analysis to calculate the Manning's normal depth.

#### **4.0 EXISTING DRAINAGE CONDITIONS**

The overall site consists of 9.75 acres. The site includes an existing 15940 sf water storage tank and gravel driveway. The areas of the site not covered by the potable water tank or gravel driveway are covered with scrub oak, grass, willows and pine trees. These undeveloped areas include slopes that range from 4.9% to 34.1%. The overall existing site is 3.5% impervious. See Existing Drainage Map in the Back Pocket for reference.

Flows from Sub-basin OS1, Sub-basin OS2, and Sub-basin Aex through Sub-basin Gex are tributary to the Black Squirrel Creek – FOMO3600 drainage basin.

Sub-basin OS1 contains 3.85 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 3.5 cfs for the 10-year storm and 9.2 cfs for the 100-year storm. These flows sheetflow to the southeast over nearly bare ground.

Sub-basin OS2 consists of 3.69 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 2.8 cfs for the 10-year storm and 8.5 cfs for the 100-year storm. These flows sheetflow to the southeast. Flows from Sub-basin OS2 combine with flows from Sub-basin Eex, Sub-basin Fex, and Sub-basin Gex to produce total flows of 7.5 cfs for the 10-year storm and 20.8 cfs for the 100-year storm at Design Point 1 (DP1). These flows proceed into the stream tributary to Black Squirrel Creek that is located southeast of the site.

Sub-basin Aex contains 3.89 acres and drains south towards a private access road. This sub-basin produces existing flows of 2.4 cfs for the 10-year storm and 7.8 cfs for the 100-year storm. These flows sheetflow to the south.

Sub-basin Bex consists of 2.37 acres and drains south along a private access road. This sub-basin produces existing flows of 2.1 cfs for the 10-year storm and 5.9 cfs for the 100-year storm. These flows sheetflow in the southerly direction.

Sub-basin Cex contains 7.96 acres and drains south towards a private access road. This sub-basin produces existing flows of 5.4 cfs for the 10-year storm and 17.4 cfs for the 100-year storm. These flows sheetflow to the south.

Page 2



Sub-basin Dex consists of 3.98 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. It produces flows of 2.7 cfs for the 10-year storm and 9.2 cfs for the 100-year storm. These flows sheetflow to the southeast, ultimately ending up in the stream noted on the Existing Drainage Plan in the Back Pocket. Flows from Sub-basin Dex combine with flows from Sub-basin Cex, Sub-basin OS1, and Design Point 1 (DP1) to produce total flows of 15.8 cfs for the 10-year storm and 46.9 cfs for the 100-year storm at Design Point 2 (DP2). These flows continue along the stream towards Black Squirrel Creek.

Sub-basin Eex contains 2.79 acres and drains east towards Sub-basin OS2. It produces flows of 3.3 cfs for the 10-year storm and 8.3 cfs for the 100-year storm. These flows sheetflow to the east, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin Fex contains 1.15 acres and drains southeast towards Sub-basin OS2. It produces flows of 1.4 cfs for the 10-year storm and 3.4 cfs for the 100-year storm. These flows sheetflow to the southeast, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin Gex consists of 0.96 acres and drains southeast towards Sub-basin OS1. It produces flows of 0.7 cfs for the 10-year storm and 2.5 cfs for the 100-year storm. These flows sheetflow to the southeast into the stream that is tributary to Black Squirrel Creek.

The estimated runoff amounts produced for the project under Existing Conditions are shown in Table 1 below.

TABI	LE 1 – EXISTING CONDITIONS	
Sub-basin	<b>Q</b> <sub>10</sub> (CFS)	Q <sub>100</sub> (CFS)
0S1	3.5	9.2
0S2	2.8	8.5
Aex	2.4	7.8
Bex	2.1	5.9
Cex	5.4	17.4
Dex	2.7	9.2
Eex	3.3	8.3
Fex	1.4	3.4
Gex	0.7	2.5
DP1 (Eex + Fex + Gex + OS2)	7.5	20.8
DP2 (DP1 + Cex + Dex + OS1)	15.8	46.9

#### **5.0 DEVELOPED DRAINAGE CONDITIONS**

The overall site consists of 9.75 acres, of which 0.88 acres will be disturbed as part of this project. A 1496 sf booster pump station building and 850 linear feet -15' wide asphalt access road is proposed on the east side of the site. A secondary gate access road is also proposed on the south end of the site along





that connects the site to the existing private asphalt driveway . Proposed Conditions Map is located below in the Back Pocket for reference.

Proposed site imperviousness is 5.4%, versus 3.5% in the existing conditions. Proposed flows are tributary to the Black Squirrel Creek – FOMO3600 drainage basin.

Sub-basin OS1 contains 3.85 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 3.5 cfs for the 10-year storm and 9.2 cfs for the 100-year storm. These flows sheetflow to the southeast over nearly bare ground.

Sub-basin OS2 contains 3.69 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. This sub-basin produces existing flows of 2.8 cfs for the 10-year storm and 8.5 cfs for the 100-year storm. These flows sheetflow to the southeast. Flows from Sub-basin OS2 combine with flows from Sub-basin E, Sub-basin F, and Sub-basin G to produce total flows of 8.3 cfs for the 10-year storm and 22.1 cfs for the 100-year storm at Design Point 1 (DP1). These flows proceed into the stream tributary to Black Squirrel Creek that is located southeast of the site.

Sub-basin A consists of 3.89 acres and drains south towards a private access road. This sub-basin produces existing flows of 2.4 cfs for the 10-year storm and 7.8 cfs for the 100-year storm. These flows sheetflow to the south.

Sub-basin B contains 2.37 acres and drains south along a private access road. This sub-basin produces existing flows of 2.3 cfs for the 10-year storm and 6.1 cfs for the 100-year storm. These flows sheetflow in the southerly direction.

Sub-basin C consists of 7.96 acres and drains south towards a private access road. This sub-basin produces existing flows of 5.4 cfs for the 10-year storm and 17.4 cfs for the 100-year storm. These flows sheetflow to the south over all roads (existing and proposed).

Sub-basin D contains 3.98 acres and drains southeast towards a stream that is tributary to Black Squirrel Creek. It produces flows of 3.1 cfs for the 10-year storm and 9.8 cfs for the 100-year storm. These flows sheetflow to the southeast over the proposed access road, ultimately ending up in the stream noted on the Existing Drainage Plan in the Back Pocket. Flows from Sub-basin D combine with flows from Sub-basin C, Sub-basin OS1, and Design Point 1 (DP1) to produce total flows of 16.8 cfs for the 10-year storm and 48.3 cfs for the 100-year storm at Design Point 2 (DP2). These flows continue along the stream towards Black Squirrel Creek.

Sub-basin E contains 2.79 acres and drains east towards the proposed pump station. It produces flows of 3.8 cfs for the 10-year storm and 9.1 cfs for the 100-year storm. Two 1.25' deep triangular swales with 4:1 side slopes route these flows around the proposed pump station. These flows sheetflow to the east, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

Sub-basin F consists of 1.15 acres and drains southeast towards Sub-basin OS2. It produces flows of 1.4 cfs for the 10-year storm and 3.4 cfs for the 100-year storm. These flows sheetflow to the southeast, ultimately ending up in the stream that is tributary to Black Squirrel Creek.

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Sub-basin G contains 0.96 acres and drains southeast towards Sub-basin OS1. It produces flows of 1.1 cfs for the 10-year storm and 3.0 cfs for the 100-year storm. These flows sheetflow to the southeast over the proposed access road and into the stream that is tributary to Black Squirrel Creek.

The estimated runoff amounts produced for the project under Proposed Conditions are shown in Table 2 below.

Please explain what the plans are for the new tank that was shown in the letter of intent. When is that expected to be built? Is only a tank expected to be built?

	TABLE 2 – PROPOSED CONDITIONS	
Sub-basin	Q <sub>10</sub> (CFS)	Q <sub>100</sub> (CFS)
0S1	3.5	9.2
0S2	2.8	8.5
A	2.4	7.8
В	2.3	6.1
С	5.4	17.4
D	3.1	9.8
E	3.8	9.1
F	1.4	3.4
G	1.1	3.0
DP1 (E + F + G + OS2)	8.3	22.1
DP2 (DP1 + C + D +OS1)	16.8	48.3

#### **6.0 WATER QUALITY**

The total disturbance for this development will be 0.88 acres. According to the El Paso County Engineering Criteria Manual (ECM), "The following types of sites and associated land disturbances are excluded from the requirements of this Section 1.7". Furthermore, in El Paso County ECM Appendix I.7, 1.B, a "County Growth Areas" are excluded from the requirements defined in Section 1.7. Since this site will be considered a "Commercial or industrial development site or larger common plans of development for which associated construction activities results in a land disturbance of less than or equal to 10 acres, the site can be excluded from water quality control measure requirements.

### 7.0 EROSION CONTROL PLAN

The site construction consists of constructing a new pump station and an asphalt access road, disturbing 0.88 acres of area. This does not require an Erosion and Stormwater Quality Control Permit. However, a Grading and Erosion Control Plan will be submitted in separate Construction Plans.

#### 8.0 FLOODPLAIN STATEMENT

Page 5

The site is not

considered a

located in what is

"County Growth Area". The

exclusion will not

apply to the site. Revise paragraph

to remove

statements.

No portion of the developed site is located within a designated FEMA 100-year floodplain according to the information published in the Federal Emergency Management Agency Flood Plain Map No.



08041C0295G dated December 7<sup>th</sup>, 2018. No portion of the site lies within the Zone 'A' of Black Squirrel Creek as noted on Map No. 08041C0295G.

#### 9.0 DRAINAGE BASIN FEES

The proposed development is located within the Black Squirrel Drainage Basin.

#### 2022 Black Squirrel Creek Drainage Fees

Impervious Coverage = 5.4% Area Subject to Fees = 0.054 x 9.75 = 0.53 Acres Black Squirrel Creek Fee = \$8,968/Acre Drainage Basin Fee = \$8,968 x 0.53 = \$4,753.04 Drainage fees will not apply to this development. Please remove the calculations and statement to say fees will not apply since there is no platting action.

2022 Black Squirrel Creek Bridge Fees Impervious Coverage = 5.4% Area Subject to Fees = 0.054 x 9.75 = 0.53 Acres Black Squirrel Creek Fee = \$565/Acre Bridge Fee = \$565 x 0.53 = \$299.45

#### **10.0 CONSTRUCTION COST OPINION**

The are no drainage facility costs associated with the proposed Northern Delivery System Booster Pump Station.

#### **11.0 CONCLUSIONS**

For this 9.75-acre site, work will include constructing a 1496 sf booster pump station and asphalt access road. Additionally, a secondary gate access road will be constructed that will allow access from the site from the private driveway south of the propoerty.-The total anticipated disturbance of the site will be 0.88 acres. The development increases total routed flows exiting the site at Design Point 2 (DP2) from 15.8 cfs to 16.8 cfs for the 10-year storm, while the 100-year storm flow increases from 46.9 cfs to 48.3 cfs. These increases do not warrant the need for detention. All developed flows will continue to flow along existing drainage patterns.

Disturbed areas shall be permanently stabilized as soon as construction activities are completed. Areas to be re-vegetated shall be treated with soil amendments to provide an adequate growth medium to sustain vegetation and shall match the pre-existing, pre-disturbed vegetation cover. Erosion control measures will be installed during construction of the proposed site per the approved Grading and Erosion Control Plan to be submitted separately for review and approval. Site runoff, storm drains, and





appurtenances associated with the development of the Triview Metropolitan District Northern Delivery System Booster Pump Station will not adversely affect the downstream and surrounding developments.

#### **12.0 REFERENCES**

*Black Squirrel Creek Drainage Basin Planning Study Final Report,* City of Colorado Springs and El Paso County, January of 1989

*Flood Insurance Rate Map Number 08041C0295G*, Federal Emergency Management Agency Floodplain Data, revised December 7, 2018

Municipal Code Corporation (2018). Drainage Criteria Manual of El Paso County, Colorado (DPM)

Urban Drainage and Flood Control District (June 2017). Urban Storm Drainage Criteria Manual, Volume 1-3.

USDA, NRCS. Soil Survey of El Paso County Area, Colorado.

Show the "Four-Step Process" for selecting structural BMPs (ECM Section I.7.2 BMP Selection). Under each step, summarize how the step was considered or implemented. (Employ runoff reduction practices, stabilize drainageways, provide WQCV, and other specialized BMPs)



## APPENDIX A MAPS



A-1





Map Unit Symbol	Map Unit Name	Rating	Percent of Site, %
41	Kettle gravelly loamy sand, 8 to 40 perent slopes	в	10.8
69	Peyton-Pring complex, 8 to 15 percent slopes	в	0.0
71	Pring coarse sandly loam, 3 to 8 percent slopes	В	89.2

Ν 100 200 0 ⊐Feet Prepared by: 121 S. TEJON ST., SUITE 1110 COLORADO SPRINGS, CO 80903 WWW.RESPEC.COM (719) 266-5212 RESPEC NORTHERN DELIVERY SERVICE BOOSTER PUMP STATION

SOILS MAP

Maxar, Microsoft, Esri Community Maps Contributors, © OpenStreetMap, Microsoft, Esri, HERE, Garmin, SafeGrapi GeoTechnologies, Inc, METI/NASA, USGS, EPA, NPS, US Census Bureau, USDA

ath:





## **APPENDIX B** CALCULATIONS



A-2

Northern Deli	very Service Bo	ooster Pump	Station							
PROJ.224.29										
C FACTOR C	ALCULATION S	HEET								
EXISTING CO	G CONDITIONS									
RUNOFF COE	FICIENT									
TYPE A/B SO	ILS									
LAND USE		Imperv %	10 YR	100 YR						
UNDEV		0	0.15	0.35						
GRAVEL ROA	ND	80	0.63	0.7						
ASPHALT RO	AD	100	0.92	0.96						
ROOFS		90	0.75	0.81						
			E	XISTING CO	NDITIONS					
	TOTAL	SURFAC	E CONDITIO	N AREAS		CALCUL	ATED C			
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	10	100	% IMPE	RVIOUS	
DESIG.	(acre)		ROAD	ROAD		YR	YR			
OS1	3.85	3.27	0.58	0.00	0.00	0.22	0.40		12.05	
OS2	3.68	3.54	0.14	0.00	0.00	0.17	0.36		3.04	
Aex	3.89	3.79	0.10	0.00	0.00	0.16	0.36		2.06	
Bex	2.37	2.15	0.22	0.00	0.00	0.19	0.38		7.43	
Cex	7.96	7.75	0.21	0.00	0.00	0.16	0.36		2.11	
Dex	3.98	3.98	0.00	0.00	0.00	0.15	0.35		0.00	
Eex	2.79	2.52	0.02	0.00	0.25	0.22	0.39		8.64	
Fex	1.15	0.99	0.03	0.00	0.13	0.25	0.41		12.26	
Gex	0.96	0.96	0.00	0.00	0.00	0.15	0.35		0.00	
Site Percent Ir	mpervious %	3 /0								

PROPOSED C	CONDITIONS								
RUNOFF COE	FICIENT								
TYPE A/B SO	ILS								
LAND USE		Imperv %	10 YR	100 YR					
UNDEV		0	0.15	0.35					
<b>GRAVEL ROA</b>	Ŋ.	80	0.63	0.7					
ASPHALT RO	AD	100	0.92	0.96					
ROOFS		90	0.75	0.81					
			PR	OPOSED CC	NDITIONS				
	TOTAL	SURFAC	E CONDITIO	N AREAS		CALCUL	ATED C		
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	10	100	% IMPEI	RVIOUS
DESIG.	(acre)						VD		
	(acre)		ROAD	RUAD		ĨŔ	лт		
OS1	(acre) 3.85	3.27	RUAD 0.58	RUAD 0.00	0.00	0.22	0.40		12.05
OS1 OS2	3.85 3.72	3.27 3.58	ROAD 0.58 0.14	0.00 0.00	0.00	0.22 0.17	0.40 0.36		12.05 3.01
OS1 OS2 A	3.85 3.72 3.89	3.27 3.58 3.79	ROAD 0.58 0.14 0.10	ROAD 0.00 0.00 0.00	0.00 0.00 0.00	0.22 0.17 0.16	0.40 0.36 0.36		12.05 3.01 2.06
OS1 OS2 A B	3.85 3.72 3.89 2.37	3.27 3.58 3.79 2.12	ROAD 0.58 0.14 0.10 0.21	ROAD 0.00 0.00 0.00 0.04	0.00 0.00 0.00 0.00	0.22 0.17 0.16 0.21	0.40 0.36 0.36 0.39		12.05 3.01 2.06 8.78
OS1 OS2 A B C	3.85 3.72 3.89 2.37 7.96	3.27 3.58 3.79 2.12 7.72	ROAD 0.58 0.14 0.10 0.21 0.21	ROAD 0.00 0.00 0.00 0.04 0.03	0.00 0.00 0.00 0.00 0.00	0.22 0.17 0.16 0.21 0.16	0.40 0.36 0.36 0.39 0.36		12.05 3.01 2.06 8.78 2.49
OS1 OS2 A B C D	3.85 3.72 3.89 2.37 7.96 3.98	3.27 3.58 3.79 2.12 7.72 3.83	ROAD 0.58 0.14 0.10 0.21 0.21 0.00	ROAD 0.00 0.00 0.04 0.03 0.15	0.00 0.00 0.00 0.00 0.00 0.00	0.22 0.17 0.16 0.21 0.16 0.17	0.40 0.36 0.36 0.39 0.36 0.37		12.05 3.01 2.06 8.78 2.49 3.77
OS1 OS2 A B C D E	3.85 3.72 3.89 2.37 7.96 3.98 2.83	3.27 3.58 3.79 2.12 7.72 3.83 2.45	ROAD 0.58 0.14 0.10 0.21 0.21 0.00 0.00	ROAD   0.00   0.00   0.00   0.00   0.01   0.03   0.15   0.10	0.00 0.00 0.00 0.00 0.00 0.00 0.28	0.22 0.17 0.16 0.21 0.16 0.17 0.25	0.40 0.36 0.39 0.39 0.36 0.37 0.42		12.05 3.01 2.06 8.78 2.49 3.77 12.44
OS1 OS2 A B C D E F	3.85 3.72 3.89 2.37 7.96 3.98 2.83 1.15	3.27 3.58 3.79 2.12 7.72 3.83 2.45 0.99	ROAD 0.58 0.14 0.10 0.21 0.21 0.00 0.00 0.00	ROAD   0.00   0.00   0.00   0.00   0.01   0.03   0.15   0.00   0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.28 0.13	0.22 0.17 0.16 0.21 0.16 0.17 0.25 0.25	0.40 0.36 0.39 0.39 0.37 0.42 0.41		12.05 3.01 2.06 8.78 2.49 3.77 12.44 12.26
OS1 OS2 A B C D E F G	3.85 3.72 3.89 2.37 7.96 3.98 2.83 1.15 0.96	3.27 3.58 3.79 2.12 7.72 3.83 2.45 0.99 0.85	ROAD 0.58 0.14 0.10 0.21 0.21 0.00 0.00 0.03 0.00	ROAD 0.00 0.00 0.04 0.03 0.15 0.10 0.00 0.11	0.00 0.00 0.00 0.00 0.00 0.00 0.28 0.13 0.00	0.22 0.17 0.16 0.21 0.16 0.17 0.25 0.25 0.22	0.40 0.36 0.39 0.36 0.37 0.42 0.41 0.42		12.05 3.01 2.06 8.78 2.49 3.77 12.44 12.26 11.46
OS1 OS2 A B C D E F G	3.85 3.72 3.89 2.37 7.96 3.98 2.83 1.15 0.96	3.27 3.58 3.79 2.12 7.72 3.83 2.45 0.99 0.85	ROAD 0.58 0.14 0.10 0.21 0.21 0.00 0.00 0.03 0.00	ROAD   0.00   0.00   0.00   0.01   0.03   0.15   0.10   0.00   0.11	0.00 0.00 0.00 0.00 0.00 0.28 0.13 0.00	0.22 0.17 0.16 0.21 0.16 0.17 0.25 0.25 0.25	0.40 0.36 0.36 0.39 0.36 0.37 0.42 0.41 0.42		12.05 3.01 2.06 8.78 2.49 3.77 12.44 12.26 11.46

Northern Delivery Service	e Booster	Pump Station																
PROJ.224.29																		
DRAINAGE CALCULAT	ION SHEE	ĒT																
file:North Delivery Servio	ce Booster	<sup>r</sup> Pump Station	.xlsx															
OCTOBER 2022																		
							Initial Tci			Travel T	ime							
AREA	AREA	C10	C100	C10 X A	C100 X A		Slope	ti		Slope	V	Tt	TC	I10	1100	Q10	Q100	AREA
DESIG.	(acre)	(10 yr)	(100 yr)			L (ft)	(%)	(min)	L (ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)	DESIG.
	· · · · ·									, , , , , , , , , , , , , , , , ,		/		· · · /		· · · · ·		
EXISTING																		
CONDITIONS																		
	3.85	0.22	0.40	0.85	1 54	100	5 50	9 38	780	6 10	2 40	5 4 2	14 79	4 13	5 95	3.5	92	0.51
082	3.69	0.22	0.40	0.63	1 33	100	7.40	8.98	495	6.60	2.50	3 30	12 28	4.10	6.00	2.8	8.5	052
Δογ	3.80	0.17	0.30	0.00	1.00	100	7.40	9.50	1125	5.00	2.00	7.81	16.98	3.80	5.60	2.0	7.8	
Bey	2 37	0.10	0.30	0.02	0.90	80	11.40	6.82	635	5.70	2.40	/ 81	11.63	1 55	6.55	2.4	5.9	Bey
	7.96	0.15	0.30	1.97	2.87	100	10.60	8.07	1000	8.60	2.20	5.05	1/ 02	4.00	6.08	5.1	17 /	
	7.90	0.10	0.30	0.60	1 30	100	10.00	8.26	580	0.00	2.00	3.35	14.02	4.23	6.61	2.4	0.2	
Eov	2.90	0.13	0.35	0.00	1.39	70	24.20	0.20	535	9.70	2.10	2.12	7.60	4.09	7.62	2.1	9.2	
	2.19	0.22	0.39	0.01	0.47	10 55	24.20	4.01 2 02	120	11.20	3.20	2.19	1.00	5.50	7.02	J.J 1 /	0.3	Eex
	1.10	0.20	0.41	0.29	0.47	100	3.20	0.00	100	14.40	3.30	0.91	0.94	5.01	7 20	0.7	5.4 2.5	Fex Cov
DP1 (Fex + Fex + Gex)	0.90	0.15	0.35	0.14	0.34	100	12.00	1.02	100	12.90	J.20	0.01	0.03	0.00	1.30	0.7	2.0	
	8.59	0.19	0.38	1.67	3.22	100	12.00	7.46	750	7.90	2.70	4.63	12.09	4.49	6.46	7.5	20.8	
+ 0.02)																		$\frac{\text{Gex} + \text{OS2}}{\text{DP2}(\text{DP1} + \text{Cex} + \text{OS2})}$
	24.38	0.18	0.37	4.39	9.02	100	10.60	7.89	1880	7.30	2.60	12.05	19.94	3.61	5.19	15.8	46.9	
+ 051)																		Dex + 051)
DDODOSED																		
PROPOSED																		
CONDITIONS	0.05	0.00	0.40	0.05	4.54	100	5 50	0.00	700	0.40	0.40	5.40	44.70	4.40	5.05	0.5	0.0	001
OS1	3.85	0.22	0.40	0.85	1.54	100	5.50	9.38	780	6.10	2.40	5.42	14.79	4.13	5.95	3.5	9.2	051
OS2	3.68	0.17	0.36	0.63	1.32	100	7.40	8.98	495	6.60	2.50	3.30	12.28	4.46	6.41	2.8	8.5	052
A	3.89	0.16	0.36	0.62	1.40	100	7.20	9.16	1125	5.90	2.40	7.81	16.98	3.89	5.60	2.4	7.8	A
В	2.37	0.21	0.39	0.50	0.92	80	11.40	0.07	635	5.70	2.20	4.81	11.48	4.58	6.58	2.3	6.1	В
	7.96	0.16	0.36	1.27	2.87	100	10.60	8.07	1000	8.60	2.80	5.95	14.02	4.23	0.08	5.4	17.4	
D	3.98	0.17	0.37	0.68	1.47	100	10.20	8.08	580	9.70	3.10	3.12	11.20	4.62	6.65	3.1	9.8	<u>D</u>
	2.83	0.25	0.42	0.71	1.19	70	24.20	4.65	535	10.20	3.20	2.79	7.43	5.34	7.68	3.8	9.1	<u>E</u>
F	1.15	0.25	0.41	0.29	0.47	55	3.20	8.03	180	14.40	3.30	0.91	8.94	5.01	7.21	1.4	3.4	F
G	0.96	0.22	0.42	0.21	0.40	100	12.00	7.25	155	12.90	3.20	0.81	8.05	5.20	7.48	1.1	3.0	
	8.62	0.21	0.39	1.82	3.39	100	12.00	7.32	750	7.90	2.70	4.63	11.95	4.51	6.48	8.2	22.0	DP1(E+F+G+
DP1 (E + F + G + OS2)																		
	24.41	0.19	0.38	4.62	9.27	100	10.60	7.81	1880	7.30	2.60	12.05	19.87	3.62	5.20	16.7	48.2	
051)		••			•.=.									0.01	0.20			031)

Critical Slope

<u>Irregu</u> Input	<u>ılar Se</u>	<u>ction</u>											
	Flow Slope			3.8 c 0.08	3.8 cfs 0.085 ft/ft								
	<b>Sta</b> 0	<b>Elev</b> 1.25	<b>n</b> 0.05	<b>Sta</b> 5	<b>Elev</b> 0	<b>n</b> 0.05	<b>Sta</b> 10	<b>Elev</b> 1.25	<b>n</b> 0.05	Sta	Elev	n	
Outpu	ıt												
•	u <b>tput</b> WSElev				3 ft		Base	d on these	swale ve	locities, pl	ease adjus	t the see	d mix
	Flow A	Area		1.09	sf		in act			voi. 1 1ac		unemen	
	Veloci	ity		3.47	fps								
	Veloci	ity Hea	d	0.18	7 ft								
	Тор М	/idth		4.18	ft								
	Froud	e Num	ber	1.20									
	Critica	al WSE	lev	0.56	2 ft								



ft/ft

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<u>Irregu</u> Input	lar Se	<u>ction</u>				Based on these swale velocities, please adjust the seed mix in accordance with DCM Vol. 1 Table 10-4 requirements.						
	Flow Slope			9.1 cfs 0.085 ft/ft								
	<b>Sta</b> 0	<b>Elev</b> 1.25	<b>n</b> 0.05	<b>Sta</b> 5	<b>Elev</b> 0	<b>n</b> 0.05	<b>Sta</b> 10	<b>Elev</b> 1.25	<b>n</b> 0.05	Sta	Elev	n
Outpu	ıt											
-	WSE	ev		0.726 ft								
	Flow A	Area		2.11 s	f							
	Veloci	ty		4.32 f	ps							
	Veloci	ty Hea	d	0.290	ft							
	Top W	/idth		5.81 ft	t							
	Froud	e Num	ber	1.26								
	Critica	al WSE	lev	0.797	ft							
	Critica	al Slope	е	ft/ft								



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## **APPENDIX C** Design charts





#### 3.1. - Rational Method Runoff Coefficient (C)

The runoff coefficient represents the integrated effects of infiltration, detention storage, evaporation, retention, flow routing, and interception, all of which affect the time distribution and peak rate of runoff. Runoff coefficients are based on the imperviousness of a particular land use and the hydrologic soil type of the area and are to be selected in accordance with Table 6-6.

The procedure for determining the runoff coefficient includes these steps:

- 1. Categorize the site area into one or more similar land uses, each with a representative imperviousness, according to the information in Table 6-6.
- 2. Based on the dominant hydrologic soil type in the area, use Table 6-6 to estimate the runoff coefficient for the particular land use category for the design storms of interest.
- 3. Calculate an area-weighted average runoff coefficient for the site based on the runoff coefficients from individual land use areas of the site.

When analyzing an area for design purposes, urbanization of the full watershed, including both on-site and off-site areas, shall be assumed.

Gravel parking areas, storage areas, and access drives proposed on Site Improvement Plans shall be analyzed based on an imperviousness of 80%. This is due to the potential for gravel areas being paved over time by property owners and the resulting adverse impacts on the stormwater management facilities and adjacent properties.

There are some circumstances where the selection of impervious percentage values may require additional investigation due to unique land characteristics (e.g., recent burn areas). When these circumstances arise, it is the designer's responsibility to verify that the correct land use assumptions are made.

When multiple sub-basins are delineated, the composite C value calculation is:

$$C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + ... C_{i}A_{i})/A_{t}$$
 (Eq. 6-6)

Where:

C c = composite runoff coefficient for total area

- C <sub>i</sub> = runoff coefficient for subarea corresponding to surface type or land use
- A <sub>i</sub> = area of surface type corresponding to Ci (units must be the same as those used for total area)
- A t = total area of all subareas for which composite runoff coefficient applies

i = number of surface types in the drainage area

#### Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or	Percent	Runoff Coefficients									
Surface	Impervious	_	_								
Characteristics		2-year	5-year	10-year	25-year	50-year	100-year				

		HSG A&B	HSG C&D										
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
<sup>1</sup> ∕₄ Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
¼ Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
⅓ Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
½ Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													

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Г

Historic Flow	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Analysis—													
Greenbelts,													
Agriculture													
	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Pasture/Meadow													
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Analysis (when													
landuse is													
undefined)													
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50



Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations  $I_{100} = -2.52 \ln(D) + 12.735$   $I_{50} = -2.25 \ln(D) + 11.375$   $I_{25} = -2.00 \ln(D) + 10.111$   $I_{10} = -1.75 \ln(D) + 8.847$   $I_{5} = -1.50 \ln(D) + 7.583$   $I_{2} = -1.19 \ln(D) + 6.035$ Note: Values calculated by equations may not precisely duplicate values read from figure.



Figure 6-25. Estimate of Average Concentrated Shallow Flow



# **BACK POCKET**







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11/21 9:31 AM By: Coleton Deitz



