

**PRELIMINARY DRAINAGE REPORT
FOR
HONOR CHARTER SCHOOL
LOCATED AT
8250 BENT GRASS MEADOWS DRIVE
PEYTON, EL PASO COUNTY, CO 80831**

Prepared for:

**Highmark School Development
10808 S. River Front Parkway Suite 3126B
South Jordan, Utah 84095**

Prepared by:



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April 2026

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name
By: _____
Title: _____
Address: _____

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Brian Campbell, P.E. #40196
Date _____

EL PASO COUNTY

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer, P.E.
County Engineer / ECM Administrator
Date _____

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1. GENERAL SITE LOCATION AND DESCRIPTION

A. LOCATION

The Site is located 8250 Bent Grass Meadows Drive located near Falcon in El Paso County, Colorado. The Site is bounded to the north by Woodmen Hills Filing No. 3, to the east by residential, to the south by Bent Grass Meadows Drive, and to the west by Falcon Meadows at Bent Grass Residential Filing No. 2.

B. DESCRIPTION OF PROPERTY

The Site consists of approximately 8.98 acres of existing, undeveloped land that is currently housing a local sediment pond for drainage from surrounding developments. To the north, the ground surface is covered with native grass and weeds, with some small trees in the vicinity. The existing topography is generally sloping to the southeast across the Site although there is a roughly defined swale along the west side of the site that captures existing off-site flows from the north and west and conveys them to the existing on-site sediment pond. The existing sediment pond is allowing 63.5 cfs to discharge in the 100-year event. The flows through this site outfall over the curb to Bent Grass Meadows Drive and are generally then conveyed to the east to the roadside drainage swale along the west side of Meridian Road. A portion of flows are assumed to be bypassing through the neighborhood to the south via curb and gutter and ultimately discharging through Bent Grass Pond 1. Per descriptions in the MDDP, the existing conditions currently allow 33.2 cfs of the 100-yr storm flow to be conveyed in the Bent Grass Meadows Roadway. The remainder of flows (30.3 cfs) are assumed to outfall through Bent Grass Residential Filing No.1 through Bent Grass Pond 1. These flows were not described in the Bent Grass Residential Filing No. 1 drainage report but were documented in the MDDP. This site is not in the 100 or 500 yr floodplain and it is in FEMA Zone x per the Firmette in Appendix C.

According to the Natural Resources Conversation Service (NRCS) Web Soil Survey, the native soils in this area are primarily Columbine gravelly sandy loam, 0 to 3 percent slopes (Map Unit Symbol #19), which is a Type A soil from 0 to 14 inches, and Type C from 14 to 60 inches.

Please refer to the NRCS soils information in the Appendix G.

Existing drainage facilities downstream of the site include existing culverts at the intersection of Bent Grass Meadows Drive and Meridian road to the east of the site.

2. DRAINAGE BASINS AND SUB-BASINS

A. MAJOR BASIN DESCRIPTION

The subject site is located within the Falcon Drainage Basin Planning Study, Please refer to the Appendix F for excerpts from the Falcon Drainage Basin Planning Study. The historic 100-year runoff for the subject site is 12.67 cfs of

on-site flow. Additionally, there is 72.5 cfs and 1.6 cfs of off-site flows from the north and the west respectively that flow through the site. The runoff from the site will be discharged to the north side of the intersection of Meridian and Bent Grass Meadows into roadside drainage swale on the west side of Meridian.

The drainage basin has been divided into sub-basins and analyzed for individual sub-basin characteristics such as runoff coefficients and peak runoff flows. For existing conditions, the on-site area has been divided into 3 onsite sub-basins EX1, EX2, and EX3. For post-development conditions, the basin has been divided into 7 onsite sub-basins: A1, A2, A3, A4, A5, A6, and A7. The runoff from these sub-basins is captured by proposed storm drain systems and conveyed to the detention pond located in the southeast corner of the site.

Drainage will generally be conveyed via sheet flow, grass swales, and curb and gutters to strategically placed inlets and will be routed southeast to the onsite detention pond in Basin A3. The discharge rates from the detention pond will not be allowed to exceed historical flow rate of 12.67 cfs as shown in the MHFD Detention Spreadsheet in Appendix E.

Hydrologic and hydraulic calculations have been provided with this drainage report. See Appendix D and E for calculation spreadsheets.

EXISTING SUB-BASIN DESCRIPTION

Basin EX1

Basin EX1 consists of the western half of the site area. This basin consists of 4.96 acres of native grasses and weeds and has been analyzed with an impervious of 20%. Runoff surface flows to the southern portion of the basin where it collects in an existing sediment pond. Overflow from the sediment pond overtops a riprap overflow and then continues south.

Basin EX2

Basin EX2 consists of the Northeast portion of the site. This basin consists of 2.05 acres of native grasses and weeds and has been analyzed with an impervious of 20%. Runoff surface flows to the southern portion of the basin where it collects in an existing depression. When flows overtop the depression, they flow to the southeast.

Basin EX3

Basin EX3 consists of the southeastern portion of the site. This basin consists of 1.97 acres of native grasses and weeds and has been analyzed with an impervious of 20%. Runoff surface flows to the south and east where it flows offsite into existing ROW.

PROPOSED SUB-BASIN DESCRIPTION

Basin A1

Basin A1 (1.03 acres) is located to the northwest of the building including a portion of the building roof. It consists of proposed drive aisles, landscaping, sidewalk, and roof and has an impervious percentage of 52.7%. Runoff will generally overland flow southeast via landscape and gutters into Type R inlet S1 and through a Storm pipe also known as Design Point 2 ultimately discharging to the detention pond. The 10-yr and 100-yr flow produced from this basin are 1.56 cfs and 2.96 cfs respectively.

Basin A2

Basin A2 (2.19 acres) is located to the northeast of the building including a portion of the building roof. It consists of proposed drive aisles, landscaping, sidewalk, and roof and has an impervious percentage of 46.0%. Runoff will generally flow southeast via landscape swales and gutters into Type R inlet S2 and through a Storm pipe also known as Design Point 2 ultimately discharging to the detention pond. The 10-yr and 100-yr flow produced from this basin are 2.60 cfs and 5.23 cfs respectively.

Basin A3

Basin A3 (2.07 acres) is located to the southeast of the building including a portion of the building roof. It consists of proposed drive aisles, landscaping, sidewalk, detention pond, playground area, and roof and has an impervious percentage of 30.5%. Runoff will generally flow southeast via a landscape swale from the north and via curb and gutter from the east, into the detention pond and through the outlet structure (S3) via a storm pipe also known as Design Point 3. Flow will then ultimately discharge to the off-site storm system flowing east along Bent Grass Meadows drive. The 10-yr and 100-yr flow produced from this basin are 1.78 cfs and 4.41 cfs respectively.

Basin A4

Basin A4 (1.52 acres) is located to the southwest of the building, including a portion of the building roof and the western side of the proposed parking lot. It consists of proposed drive aisles, parking, landscaping, sidewalk, trash enclosure, and roof and has an impervious percentage of 65.3%. Runoff will generally flow southwest into Type R curb inlets (S4 and S7) and discharge to the east via a storm pipe also known as Design Point 4 ultimately discharging to the detention pond. The 10-yr and 100-yr flow produced from this basin are 3.94 cfs and 6.79 cfs respectively.

Basin A5

Basin A5 (0.62 acres) is the eastern portion of the proposed parking lot and includes a portion of the building roof. It consists of proposed drive aisles, parking, landscaping, sidewalk, and roof and has an impervious percent of 85.3%. Runoff will generally flow southeast into Type R curb inlets (S5 and S8) and

discharge to the east via a storm pipe also known as Design Point 5 ultimately discharging to the detention pond. The 10-yr and 100-yr flow produced from this basin are 2.64 cfs and 4.10 cfs respectively.

Basin A6

Basin A6 (1.28 acres) is located along the north and eastern property lines of the site. It consists of native vegetation and has an impervious percent of 20%. Runoff will generally be conveyed via Grass channel to the east and then to the south, where it is collected and conveyed via the off-site Storm Pipe also known as Design Point 6 ultimately discharging to the into the regional channel along west side of Meridian Road. The 10-yr and 100-yr flow produced from this basin are 0.61 cfs and 1.93 cfs respectively.

Basin A7

Basin A7 (0.26 acres) is located along the south property line of the site. It consists of proposed drive entrances, parking, landscaping, and sidewalk and has an impervious percent of 45.6%. Runoff will generally sheetflow to the south, where it is collected in the curb and gutter along the north side of Bent Grass Meadows Drive. The 10-yr and 100-yr flow produced from this basin are 0.51 cfs and 1.03 cfs respectively.

While runoff from Basins A6 and A7 are not able to be captured/conveyed to the detention pond, the detention pond is still sized to store the necessary runoff for those basins.

Refer to Appendix D for and E for calculations.

3. DRAINAGE DESIGN CRITERIA

A. REGULATIONS

This report has been prepared in general accordance with the Mile High Flood District/Urban Storm Drainage Criteria Manual (USDCM), City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.

B. HYDROLOGIC CRITERIA

The subject site consists of approximately 8.98 acres. The site is currently undeveloped and the proposed project will consist of a proposed school building, parking lots, drive lanes, landscape areas, and detention pond.

The subject site is located within the Falcon Drainage Basin Planning Study, as shown in the Bent Grass Development MDDP and DBPS Amendment, January 2021, prepared by Galloway. All onsite and offsite flow is directed east via curb and gutter and 30 inch off-site storm drain pipe to the roadside drainage swale

along the west side of Meridian road, which is in compliance with the Bent Grass Development MDDP.

Runoff from impervious and pervious surfaces as a result of the proposed development will be routed through the proposed onsite detention pond. The controlled discharge from the detention pond will be released from the southeast corner of the subject site to a proposed 30 inch pipe to carry it to the roadside drainage swale along the west side of Meridian road.

C. HYDRAULIC CRITERIA

This report has been prepared in general accordance with the Mile High Flood District/Urban Storm Drainage Criteria Manual (USDCM), City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.

The design storms for this project are the 10-year and the 100-year recurrence intervals. Runoff is calculated using the Rational Method since the total project and all basins are smaller than 160 acres. The Rational calculations are estimates based on site areas and assumed uses within the proposed basins. Refer to Appendix E for Hydraulic computations.

4. DRAINAGE FACILITY DESIGN

A. GENERAL CONCEPT AND DESIGN

On-site Conveyance and Storage

The overall development has been analyzed for water quality treatment and the impacts of the 10-year minor storm event and the 100-year major storm event as well as adherence to the Bent Grass Development MDDP and DBPS Amendment. The contributing areas to be controlled by the detention pond outlet structure is 7.44 acres but the detention is sized to detain the entire site area of 8.98 acres. The contributing area will be conveyed to the proposed detention pond via underground storm drain system and overland flow for detention and treatment. The water quality treatment volume and storage for the 100-year event will be provided by the full spectrum extended detention which includes forebays within the pond and a micro pond at the outlet structure for sediment removal. An outlet at the southeast corner of the detention pond will allow discharge at a 100-year peak flow rate of 6.8 cfs into the proposed 30 inch offsite drainage system being developed with this project.

Off-site Run-on Conveyance

For conveying the 100-year off-site runoff through the site, the full 72.5 cfs from the north will be captured in a drainage channel along the north and flow to the northeast corner and then south to the proposed off-site pipe system. For the 100-year condition, approximately 33.2 cfs will overtop the curb and be conveyed via the Bent Grass Meadows roadway following existing conditions. The remainder

of the 72.5 cfs that is being bypassed will be captured and conveyed in the proposed 30 inch storm pipe that will run along the north side of Bent Grass Meadows drive. The 1.6 cfs from basin 5-1 (See sections of the MDDP) to the west will be captured via vegetated swales and conveyed through the on-site storm infrastructure to be conveyed through the pond. The proposed off-site storm drain will flow approximately 2000 ft to the east and outlet to the north of the intersection of Bent Grass Meadows Drive and Meridian Road to the Roadside Drainage Swale.

The drainage improvements designed for this proposed development will provide detention and water quality treatment for the project site 100-year event for on-site flows and conveyance of the 100-year storm event for off-site flows.

B. DETENTION

The proposed drainage patterns will follow existing drainage patterns, with all of the site ultimately discharging to the southeast through proposed storm drain system, including an off-site 30 inch pipe which runs approximately 2000 ft to the east and outlet to the north of the intersection of Bent Grass Meadows Drive and Meridian Road to the Roadside Drainage Swale.

The onsite detention pond shall be a full spectrum pond, which includes water quality (WQ), excess urban runoff volume (EURV) and 100-year volume. Stage 1 will be WQ; Stage 2 will be EURV and Stage 3 will be the 100-year volume.

The required WQ volume is 0.122 ac-ft and the provided volume is 0.122 ac-ft with a release rate of 0.1 cfs. The WQ surface elevation is 6955.08 ft. The required EURV volume is 0.194 ac-ft (including WQ) and the provided volume is 0.317 ac-ft at a release rate of 0.2 cfs. The EURV water surface elevation is 6955.66 ft. The required 100-year volume is 0.564 ac-ft and the provided volume is 0.580 ac-ft at a release rate of 4.6 cfs. The 100-year water surface elevation is 6956.33 ft.

The pond will have an emergency overflow spillway for a plugged outlet condition or for a storm event greater than the 100-year event. The emergency overflow spillway has been designed to be 20' long and have a water depth of +/- 5.6 inches. The runoff through the spillway was calculated by assuming a plugged outlet and summing post development peak flows across the site for the most extreme case. The spillway crest elevation is 6956.83 and the top of the proposed detention pond will be 6957.33 feet.

The detention pond will release via an 18 inch RCP into a proposed 96 inch storm manhole as part of the off-site system within Bent Grass Meadows. Runoff is then conveyed in the proposed 30 inch RCP along Bent Grass Meadows ultimately discharging on the north side of Bent Grass Meadows into the roadside drainage swale along the west side of Meridian Road.

The 100-year overflow spillway for the off-site flows to overtop the channel into Bent Grass Meadows drive and spills over the proposed sidewalk. The sidewalk is graded to provide a depth of 0.34 feet of flow to convey the 33.2 cfs to the roadway following existing drainage patterns per the MDDP.

C. STORMWATER QUALITY

Water quality for the subject development will be provided with the proposed extended detention pond. The outlet structure for the pond contains an orifice plate to limit the release and provide water quality for the development site.

The required water quality capture volume is 0.12 ac-ft and the water quality capture volume provided is 0.12 ac-ft at an elevation of 6955.08 ft. The water quality volume drains within 42 hours. The 100-year event volume drains within 60 hours.

The detention pond and outlet structure shall be regularly inspected and maintained by the property owner (at least 1 time every six months and 2 times per year). The inspections should include a log for the date, items inspected, maintenance actions and any updates to the drainage system. Maintenance access is an all-weather path on the south side of the structure. Maintenance shall follow Chapter 6: BMP Maintenance of the MHFD, Volume III.

Stormwater quality and erosion control measures will be addressed by applying Best Management Practices in general accordance with Urban Drainage Volume 3. A SWMP will be prepared for the site and will provide more detail on BMPs during construction and post-construction BMPs.

5. Four Step Process

- A. Runoff Reduction Proposed: Storm runoff sheet flows over pervious areas wherever possible to slow runoff and increase time of concentration to storm water system. Runoff is collected in a pervious detention basin to allow infiltration and slow water impact on County stormwater infrastructure.
- B. Stabilization of drainage ways: All drainage ways are stabilized with pervious landscaping where possible.
- C. Proposed Stormwater Quality Capture Volume (WQCV) proposed: Proposed on-site runoff is collected and diverted to the proposed extended detention pond, which releases at a pre-determined rate to ensure WQCV standards are met.
- D. Identify Best Management Practices (BMP's) to be used to control industrial and commercial pollutants: Refer to prepared SWMP and GEC plans for proposed BMP's as well as maintenance and care thereof.

6. SEDIMENT/EROSION CONTROL

The following practices/methods shall be implemented as a part of the overall sediment/erosion control for the proposed site:

- Silt Fence
- Inlet Protection
- Materials Handling and Spill Prevention (Concrete Washout Area)
- Stabilized Staging Area for Material/Equipment Storage
- Vehicle Tracking Control Pad
- Sanitary Facilities
- Curb Socks
- Seeding & Mulching
- Riprap

7. CONCLUSION

A. COMPLIANCE WITH STANDARDS

This project is in general compliance with the City of Colorado Springs/El Paso County Drainage Criteria Manual and the Mile High Flood District for storm water design. *Urban Storm Drainage Criteria Manuals Volume I and III* have been utilized in the placement of best management practices and design of the stormwater system regarding imperviousness and runoff coefficients. Adequate storm water treatment has been provided, and the peak flows have been reduced to below pre-development conditions for 10-year and 100-year rates.

B. DRAINAGE COMPLIANCE

The purpose of this report is to define and analyze existing and developed runoff quantities and conveyance methods for the Honor Charter School development. The design of the site was based on the 10-year and 100-year storm events. The streets and drainage conveyance facilities were designed to meet these events. The design of the release points from the site shows reduction in peak flows. No foreseeable negative impacts on the surrounding properties and drainage infrastructure are anticipated. The drainage is in accordance with requirements and criteria established by El Paso County and the Bent Grass Development MDDP and DBPS Amendment.

8. REFERENCES

Drainage Criteria Manual, Volumes 1-3. Urban Storm Drainage Criteria Manual. Updated March 2024.

City of Colorado Springs/El Paso County Drainage Criteria Manual

Bent Grass Development MDDP and DBPS Amendment

9. APPENDICES

- A. VICINITY MAP
- B. EXISTING AND PROPOSED DEVELOPMENT EXHIBITS
- C. FEMA FIRM MAP
- D. HYDROLOGIC COMPUTATIONS
- E. HYDRAULIC COMPUTATIONS
- F. SECTIONS FROM BENT GRASS MDDP/DBPS AMENDMENT & FALCON DRAINAGE BASIN STUDY
- G. SOILS REPORT
- H. GRADING AND STORM DRAINAGE PLANS

APPENDIX A
VICINITY MAP



VICINITY MAP

(NOT TO SCALE)

APPENDIX B

**EXISTING AND PROPOSED DEVELOPMENT
EXHIBITS**

Apr 29, 2026 - 3:28pm by tschneider_x\ENGINEERING\CO\1517\70 - Honor Charter School - Paycom_CO\GIS\Hydrology\CO1517_Hydro.dwg

GRADING PLAN



Know what's below
Call before you dig.

UNAUTHORIZED CHANGES & USES

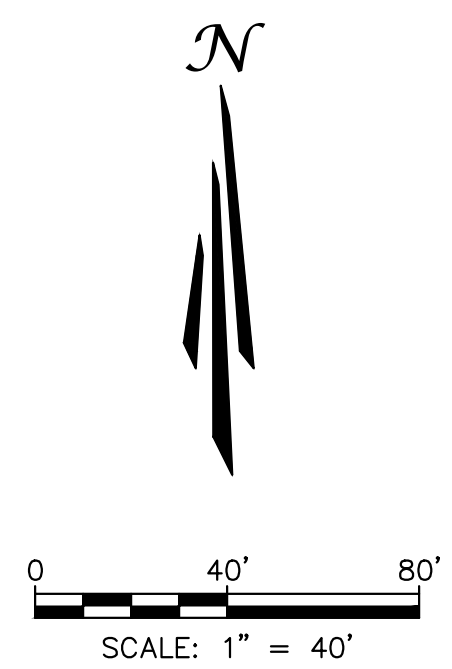
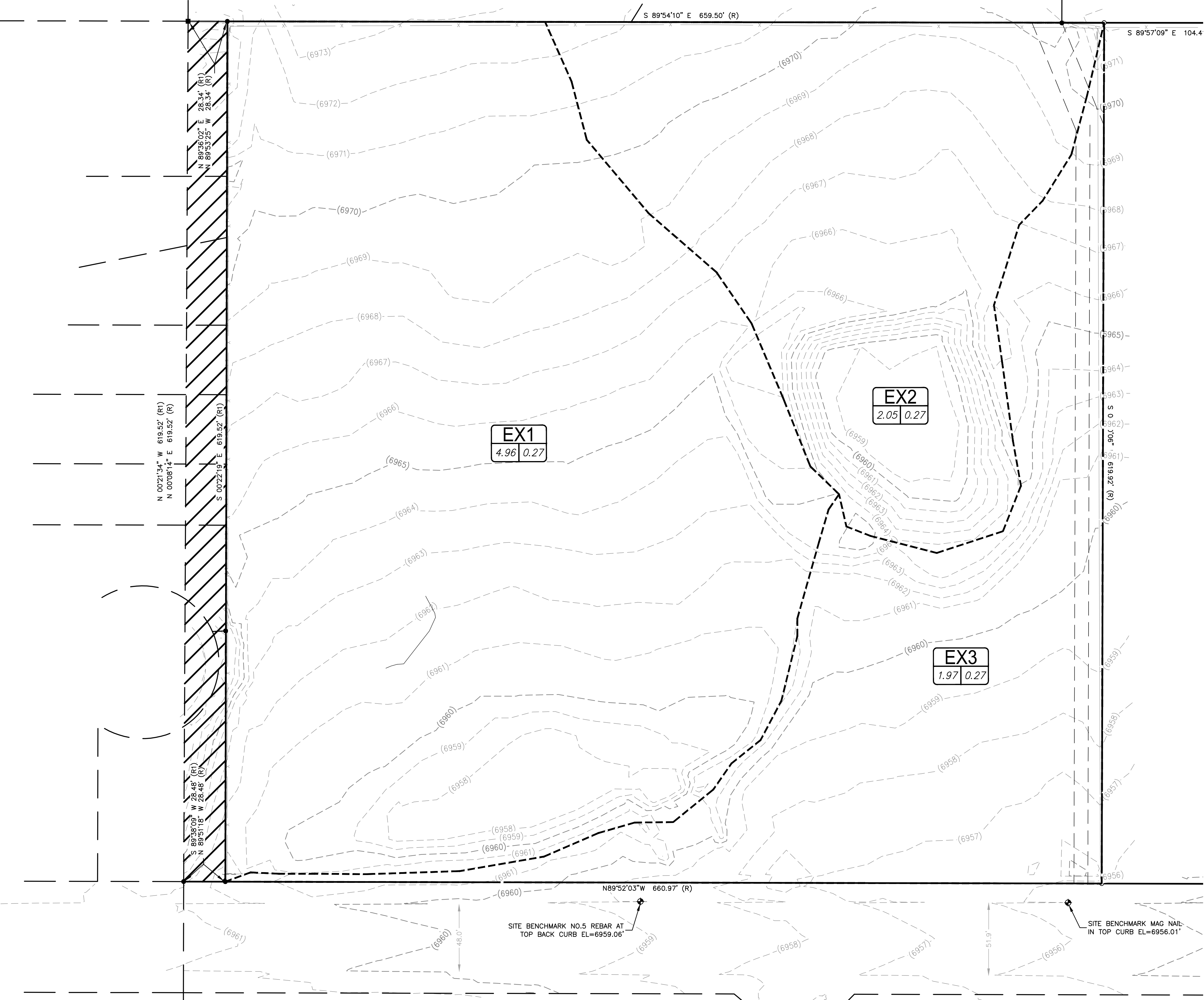
THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR, OR LIABLE FOR, UNAUTHORIZED CHANGES TO OR USES OF THESE PLANS. ALL CHANGES OF THESE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS PRIOR TO CONSTRUCTION. CONSTRUCTION CONTRACTOR AGREES THAT IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, CONSTRUCTION CONTRACTOR WILL BE REQUIRED TO ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION OF THE PROJECT, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY, THAT THIS REQUIREMENT SHALL BE MADE TO APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS, AND CONSTRUCTION CONTRACTOR FURTHER AGREES TO DEFEND, INDEMNIFY AND HOLD DESIGN PROFESSIONAL HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT, EXCEPTING LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF DESIGN PROFESSIONAL.

NOTE TO CONTRACTOR

THE EXISTENCE AND LOCATION OF ANY UNDERGROUND UTILITIES, PIPES, AND/OR STRUCTURES SHOWN ON THESE PLANS WERE OBTAINED BY A SEARCH OF AVAILABLE RECORDS. THERE MAY BE EXISTING UTILITIES NOT SHOWN ON THESE PLANS. THE CONTRACTOR SHALL ASCERTAIN THE TRUE VERTICAL AND HORIZONTAL LOCATION OF THOSE UNDERGROUND UTILITIES TO BE USED PRIOR TO CONSTRUCTION AND SHALL BE RESPONSIBLE FOR ANY DAMAGE TO ANY PUBLIC OR PRIVATE UTILITIES, SHOWN OR NOT SHOWN HEREON.

BASIS OF BEARINGS:
BEARINGS ARE BASED ON THE WESTERLY BOUNDARY OF THE SUBJECT PARCEL COINCIDENT WITH THE EASTERLY BOUNDARY OF THE BENT GRASS RESIDENTIAL FILING NO.2, MONUMENTED ON THE NORTH END WITH A NO.5 REBAR & 1-3/8" RED PLASTIC CAP MARKED "ALC PLS 38087", FOUND FLUSH WITH GRADE, AND ON THE SOUTH END WITH A NO. 4 REBAR & 1" ORANGE PLASTIC CAP MARKED "PLS 38141", RECOVERED 0.6 BELOW GRADE, AND IS ASSUMED TO BEAR N 00°08'14" E A MEASURED DISTANCE OF 619.52 FEET.

BENCHMARK:
ELEVATIONS ARE BASED ON THE PROJECT BENCHMARK IDENTIFIED AS JK0239 ELEVATION=6902.3'(NAVD88), PER DATA PUBLISHED BY THE NATIONAL GEODETIC SURVEY.



SYMBOLS LEGEND	
	PROPERTY LINE
	ADJACENT PROPERTY/ ROW LINE
	BUILDING SETBACK LINE
	PROPOSED EASEMENT
	LIMIT OF DISTURBANCE
	EXISTING WATER LINE
	EXISTING SEWER LINE
	PROPOSED TELEPHONE SERVICE LINE
	PROPOSED ELECTRIC SERVICE LINE
	PROPOSED WATER SERVICE LINE
	PROPOSED SS SERVICE LINE
	PROPOSED STORM DRAIN
	PROPOSED RIDGELINE
	PROPOSED GRADE BREAK
	PROPOSED TOP OF POND
	PROPOSED BOTTOM OF POND
	GRADING DETAIL BOUNDARY
	PROPOSED SS CLEANOUT
	PROPOSED BACKFLOW PREVENTOR
	EXISTING FIRE HYDRANT
	PROPOSED FIRE HYDRANT
	PROPOSED STREET LIGHT
	EXISTING ELEVATION
	PROPOSED ELEVATION
	EXISTING CONTOUR
	PROPOSED CONTOUR
	EXISTING SLOPE
	PROPOSED SLOPE
	EXISTING INLET
	PROPOSED INLET
	PROPOSED STORM INFRASTRUCTURE
	PROPOSED STORM MANHOLE
	PROPOSED TEE / THRUST BLOCK
	PROPOSED FLARED-END SECTION
	EXISTING SANITARY SEWER MANHOLE

DRAINAGE LEGEND:

	PROPOSED SLOPE	2.0%
	EXISTING SLOPE	1.0%
	BASIN LIMITS	
	IMPERVIOUS AREA	

A
B
C

A = BASIN DESIGNATION
B = AREA IN ACRES
C = 100-YR RUNOFF COEFFICIENT

NOTE:

ELEVATIONS ARE TRUNCATED BY 6900.00'.

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NOT FOR CONSTRUCTION

PREPARED UNDER THE SUPERVISION OF
TAIT & ASSOCIATES, INC.

DRAWING CW
DATE: 11/11/2024
CHECKED:
DATE:
REVISION #:
DATE:
JOB NO. CO1517

8
OF
48

BRIAN CAMPBELL
COLORADO P.E. #40196

GRADING PLAN

HONOR CHARTER SCHOOL
HIGHMARK SCHOOL DEVELOPMENT
8250 BENT GRASS MEADOWS DR.

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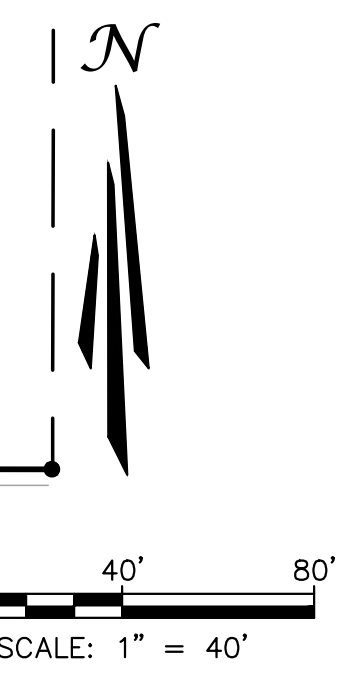
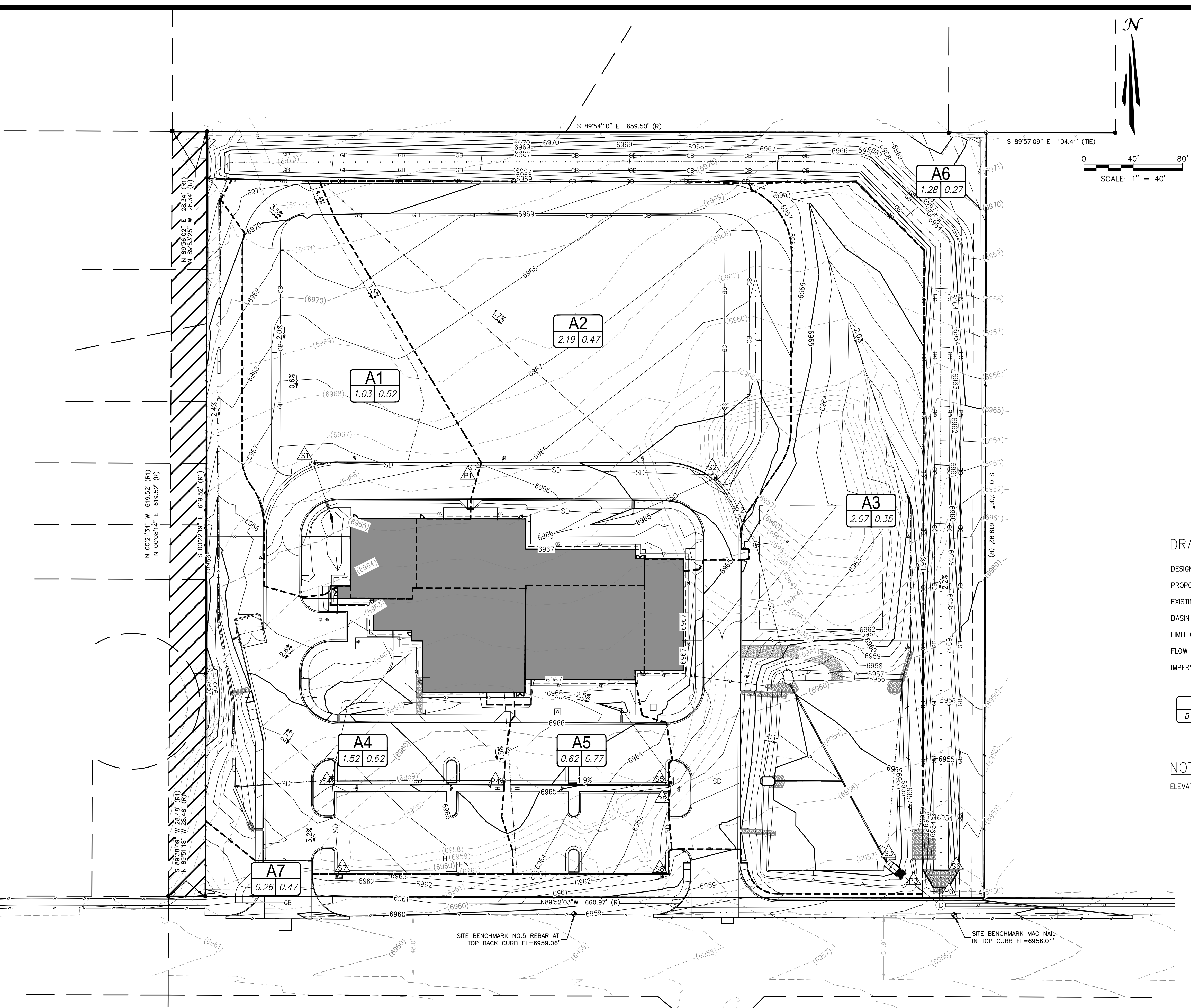
Since 1964

NO.	DESCRIPTION	BY	DATE
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2/6/2024 Internal Review #1

Apr 30, 2026 - 3:10pm by tschneider X:\ENGINEERING\CO\CO1517D - Honor Charter School - Payson, CO\ENR\Hydrology\CO1517D_HGRB.dwg



SYMBOLS LEGEND

- PROPERTY LINE
- ADJACENT PROPERTY/ ROW LINE
- BUILDING SETBACK LINE
- - - PROPOSED EASEMENT
- LIMIT OF DISTURBANCE
- W — EXISTING WATER LINE
- SS — EXISTING SEWER LINE
- T — PROPOSED TELEPHONE SERVICE LINE
- — PROPOSED ELECTRIC SERVICE LINE
- W — PROPOSED WATER SERVICE LINE
- SS — PROPOSED SS SERVICE LINE
- SD — PROPOSED STORM DRAIN
- R — PROPOSED RIDGELINE
- GB — PROPOSED GRADE BREAK
- — PROPOSED TOP OF POND
- — PROPOSED BOTTOM OF POND
- GRADING DETAIL BOUNDARY
- PROPOSED SS CLEANOUT
- PROPOSED BACKFLOW PREVENTOR
- EXISTING FIRE HYDRANT
- PROPOSED FIRE HYDRANT
- PROPOSED STREET LIGHT
- (40.00)ES — EXISTING ELEVATION
- 40.00FS — PROPOSED ELEVATION
- (2940) — EXISTING CONTOUR
- 2940 — PROPOSED CONTOUR
- (5.2%) — EXISTING SLOPE
- 5.4% — PROPOSED SLOPE
- — EXISTING INLET
- — PROPOSED INLET
- — PROPOSED STORM INFRASTRUCTURE
- — PROPOSED STORM MANHOLE
- — PROPOSED TEE / THRUST BLOCK
- — PROPOSED FLARED-END SECTION
- — EXISTING SANITARY SEWER MANHOLE
- — LONGEST FLOW PATH

DRAINAGE LEGEND:

- DESIGN POINT
 - PROPOSED SLOPE
 - EXISTING SLOPE
 - BASIN LIMITS
 - LIMIT OF DISTURBANCE
 - FLOW PATH
 - IMPERVIOUS AREA
- A = BASIN DESIGNATION
B = AREA IN ACRES
C = 100-YR RUNOFF COEFFICIENT

NOTE:

ELEVATIONS ARE TRUNCATED BY 6900.00'

GRADING PLAN



UNAUTHORIZED CHANGES & USES

THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR, OR LIABLE FOR, UNAUTHORIZED CHANGES TO OR USES OF THESE PLANS. ALL CHANGES OF THESE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS PRIOR TO CONSTRUCTION. CONSTRUCTION CONTRACTOR AGREES THAT IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, CONSTRUCTION CONTRACTOR WILL BE REQUIRED TO ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION OF THE PROJECT, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY, THAT THIS REQUIREMENT SHALL BE MADE TO APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS, AND CONSTRUCTION CONTRACTOR FURTHER AGREES TO DEFEND, INDEMNIFY AND HOLD DESIGN PROFESSIONAL HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT, EXCEPTING LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF DESIGN PROFESSIONAL.

NOTE TO CONTRACTOR

THE EXISTENCE AND LOCATION OF ANY UNDERGROUND UTILITIES, PIPES, AND/OR STRUCTURES SHOWN ON THESE PLANS WERE OBTAINED BY A SEARCH OF AVAILABLE RECORDS. THERE MAY BE EXISTING UTILITIES NOT SHOWN ON THESE PLANS. THE CONTRACTOR SHALL ASCERTAIN THE TRUE VERTICAL AND HORIZONTAL LOCATION OF THOSE UNDERGROUND UTILITIES TO BE USED PRIOR TO CONSTRUCTION AND SHALL BE RESPONSIBLE FOR ANY DAMAGE TO ANY PUBLIC OR PRIVATE UTILITIES, SHOWN OR NOT SHOWN HEREON.

BASIS OF BEARINGS:
BEARINGS ARE BASED ON THE WESTERLY BOUNDARY OF THE SUBJECT PARCEL COINCIDENT WITH THE EASTERLY BOUNDARY OF THE BENT GRASS RESIDENTIAL FILING NO.2, MONUMENTED ON THE NORTH END WITH A NO.5 REBAR & 1-3/8" RED PLASTIC CAP MARKED "ALC PLS 38087", FOUND FLUSH WITH GRADE, AND ON THE SOUTH END WITH A NO. 4 REBAR & 1" ORANGE PLASTIC CAP MARKED "PLS 38141", RECOVERED 0.6 BELOW GRADE, AND IS ASSUMED TO BEAR N 00°08'14" E A MEASURED DISTANCE OF 619.52 FEET.

BENCHMARK:
ELEVATIONS ARE BASED ON THE PROJECT BENCHMARK IDENTIFIED AS JK0239 ELEVATION=6902.3'(NAVD88), PER DATA PUBLISHED BY THE NATIONAL GEODETIC SURVEY.

FOR REVIEW ONLY
NOT FOR CONSTRUCTION

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GRADING PLAN
HONOR CHARTER SCHOOL
HIGHMARK SCHOOL DEVELOPMENT
8250 BENT GRASS MEADOWS DR.

DRAWING CW
DATE: 11/11/2024
CHECKED:
DATE:
REVISION #:
DATE:
JOB NO. CO1517

8 OF 48

BRIAN CAMPBELL
COLORADO P.E. #40196

2/6/2024 Internal Review #1

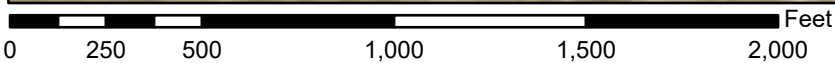
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APPENDIX C
FEMA FIRM MAP

National Flood Hazard Layer FIRMette



104°37'14"W 38°57'20"N



1:6,000

104°36'37"W 38°56'52"N

Basemap Imagery Source: USGS National Map 2023

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
GENERAL STRUCTURES		Area of Undetermined Flood Hazard Zone D
		Channel, Culvert, or Storm Sewer
OTHER FEATURES		Levee, Dike, or Floodwall
		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
MAP PANELS		17.5 Coastal Transect
		Base Flood Elevation Line (BFE)
MAP PANELS		Limit of Study
		Jurisdiction Boundary
MAP PANELS		Coastal Transect Baseline
		Profile Baseline
MAP PANELS		Hydrographic Feature
		Digital Data Available
MAP PANELS		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

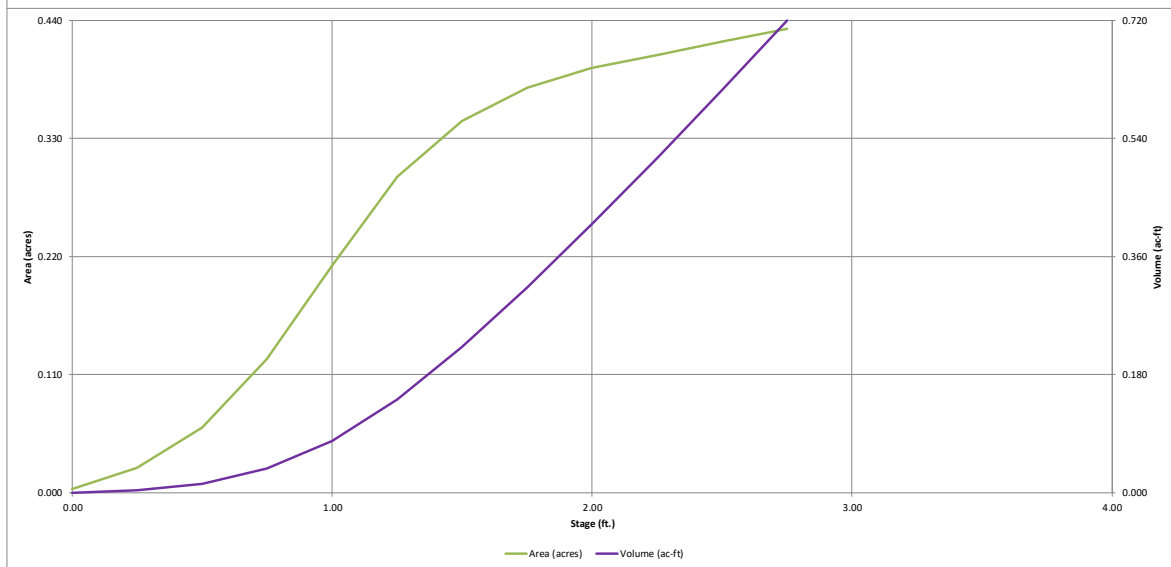
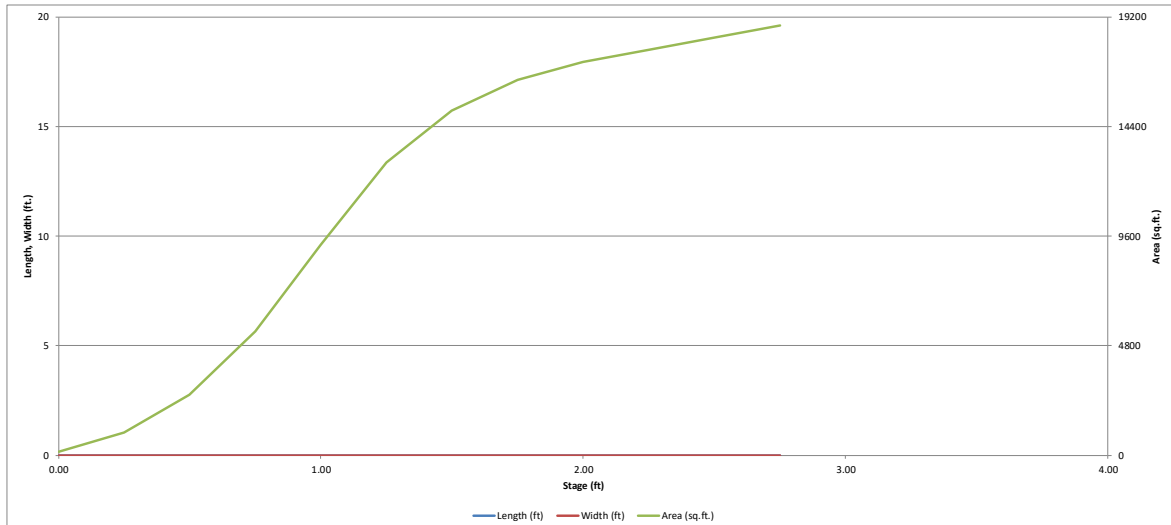
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **12/12/2025 at 4:34 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

APPENDIX D
HYDROLOGIC COMPUTATIONS

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.07 (June 2025)

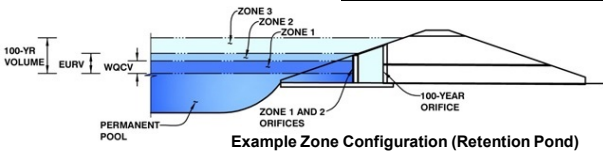


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.07 (June 2025)

Project: Honor Charter Academy

Basin ID: School Pond



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.18	0.122	Orifice Plate
Zone 2 (EURV)	1.76	0.194	Orifice Plate
Zone 3 (100-year)	2.39	0.248	Weir&Pipe (Circular)
Total (all zones)		0.564	

Example Zone Configuration (Retention Pond)

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration SCM)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation SCM)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	1.76	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.59	1.17					
Orifice Area (sq. inches)	0.75	1.25	6.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft ²
Vertical Orifice Centroid =	N/A	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	2.20	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	6.00	N/A	feet
Overflow Grate Type =	Close Mesh Grate	N/A	
Debris Clogging % =	50%	N/A	%

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H _t =	2.20	N/A	feet
Overflow Weir Slope Length =	6.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	16.11	N/A	
Overflow Grate Open Area w/o Debris =	28.48	N/A	ft ²
Overflow Grate Open Area w/ Debris =	14.24	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Circular	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	18.00	N/A	inches

	Zone 3 Circular	Not Selected	
Outlet Orifice Area =	1.77	N/A	ft ²
Outlet Orifice Centroid =	0.75	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	N/A	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =		ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =		feet
Spillway End Slopes =		H:V
Freeboard above Max Water Surface =		feet

Spillway Design Flow Depth =		feet
Stage at Top of Freeboard =		feet
Basin Area at Top of Freeboard =		acres
Basin Volume at Top of Freeboard =		acre-ft

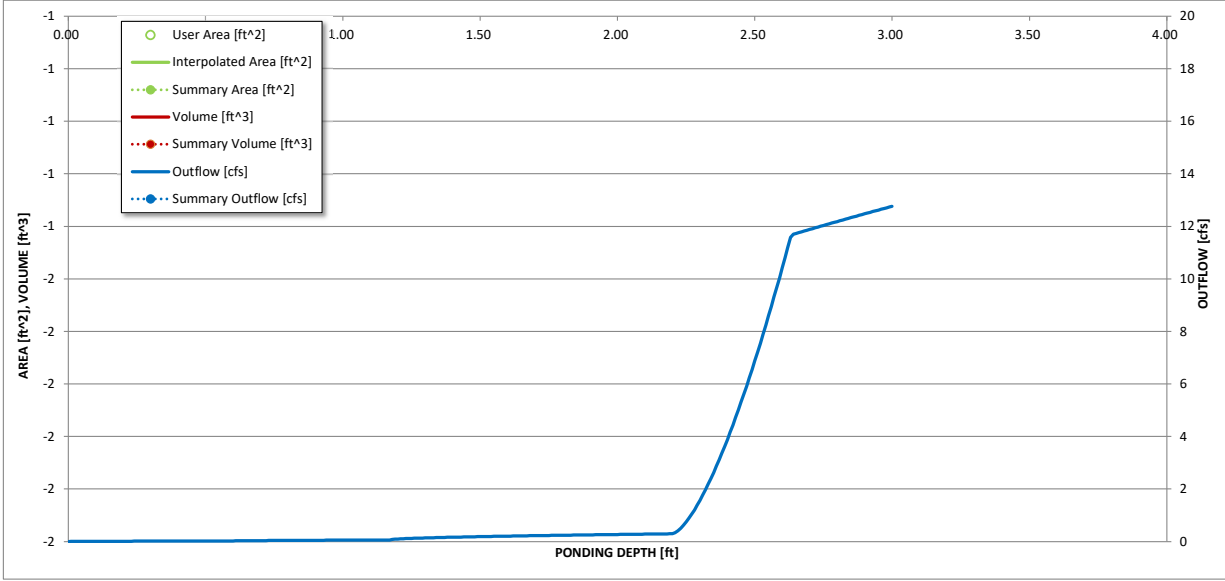
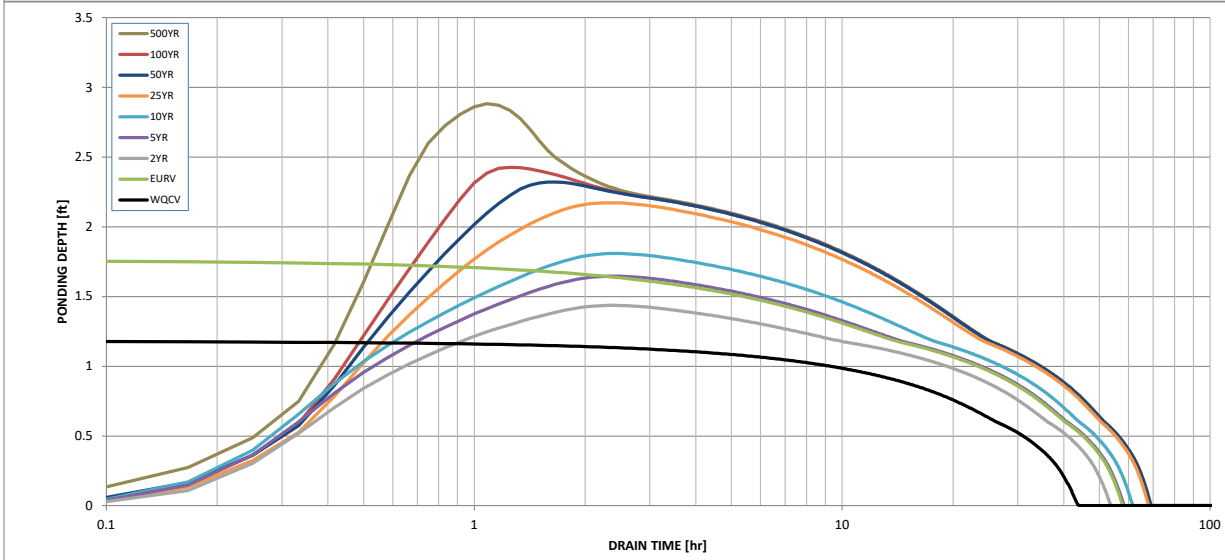
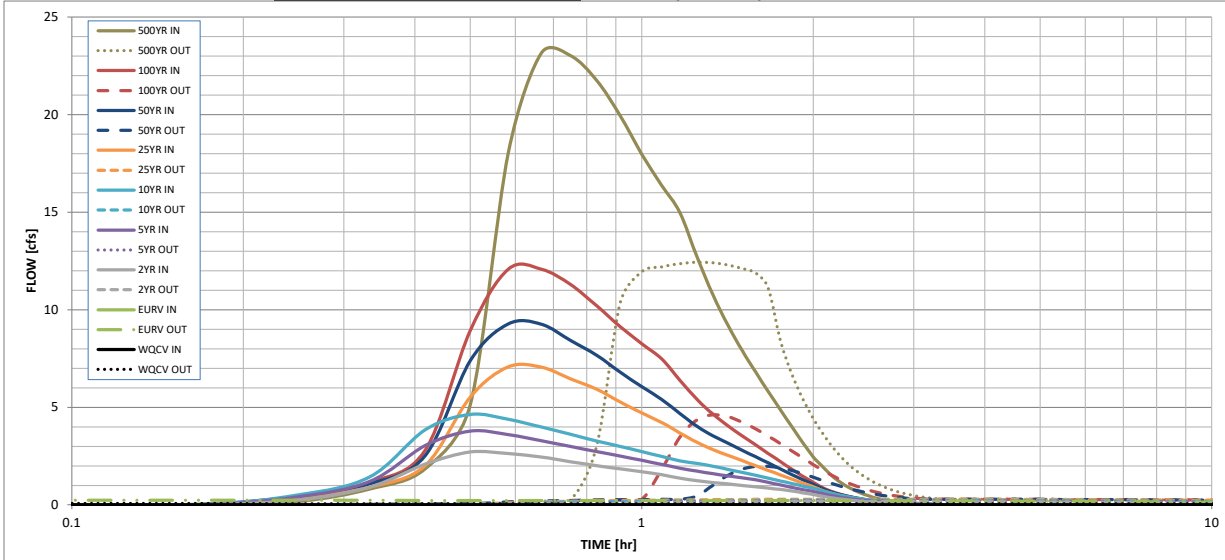
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.68
CUHP Runoff Volume (acre-ft) =	0.122	0.316	0.225	0.307	0.373	0.524	0.665	0.853	1.643
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.225	0.307	0.373	0.524	0.665	0.853	1.643
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.2	0.3	0.5	2.0	3.7	5.9	14.4
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						12.7	
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.02	0.04	0.05	0.23	0.42	1.41	1.60
Peak Inflow Q (cfs) =	N/A	N/A	2.7	3.8	4.6	7.1	9.3	12.1	23.1
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.2	0.2	0.3	2.0	4.6	12.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.6	0.5	0.1	0.5	0.4	0.9
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Outlet Plate
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	0.1	0.2	0.4
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	48	46	49	51	54	52	50	42
Time to Drain 99% of Inflow Volume (hours) =	42	54	50	54	57	62	62	60	55
Maximum Ponding Depth (ft) =	1.18	1.76	1.44	1.65	1.81	2.17	2.32	2.43	2.88
Area at Maximum Ponding Depth (acres) =	0.27	0.38	0.33	0.36	0.38	0.40	0.41	0.42	0.00
Maximum Volume Stored (acre-ft) =	0.122	0.317	0.199	0.272	0.332	0.477	0.539	0.580	#VALUE!

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.07 (June 2025)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

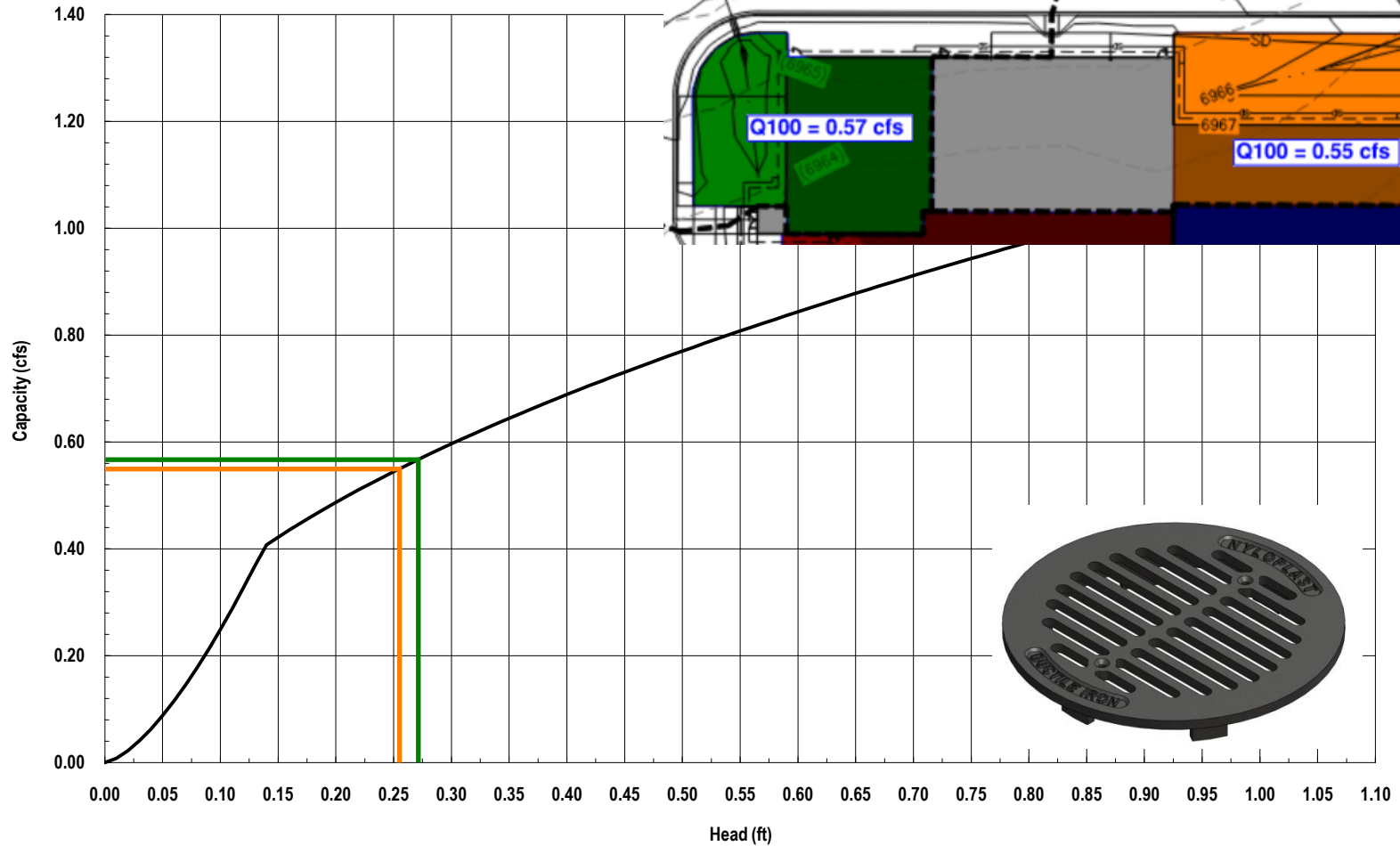
Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0	0.00	0.00	0.00	0.00	0.00	0.03	0.00	0.18
	0:15:00	0	0.00	0.25	0.41	0.51	0.35	0.44	0.43	0.81
	0:20:00	0	0.00	0.91	1.20	1.43	0.91	1.07	1.15	1.85
	0:25:00	0	0.00	2.08	3.04	3.84	2.01	2.51	2.79	5.13
	0:30:00	0	0.00	2.71	3.78	4.64	5.53	7.38	8.94	18.05
	0:35:00	0	0.00	2.63	3.60	4.38	7.07	9.27	12.08	23.15
	0:40:00	0	0.00	2.45	3.29	3.98	7.05	9.26	12.08	23.02
	0:45:00	0	0.00	2.21	2.99	3.61	6.46	8.42	11.29	21.76
	0:50:00	0	0.00	2.01	2.73	3.27	5.93	7.67	10.20	19.94
	0:55:00	0	0.00	1.84	2.50	3.00	5.27	6.79	9.13	17.97
	1:00:00	0	0.00	1.69	2.28	2.73	4.71	6.05	8.26	16.38
	1:05:00	0	0.00	1.54	2.07	2.48	4.22	5.41	7.48	14.97
	1:10:00	0	0.00	1.37	1.88	2.25	3.69	4.68	6.39	12.71
	1:15:00	0	0.00	1.24	1.72	2.12	3.20	4.02	5.41	10.75
	1:20:00	0	0.00	1.15	1.60	1.98	2.83	3.54	4.64	9.19
	1:25:00	0	0.00	1.07	1.49	1.82	2.54	3.16	4.05	7.91
	1:30:00	0	0.00	1.00	1.38	1.66	2.26	2.80	3.54	6.81
	1:35:00	0	0.00	0.93	1.29	1.51	2.01	2.47	3.08	5.81
	1:40:00	0	0.00	0.86	1.15	1.37	1.77	2.15	2.64	4.88
	1:45:00	0	0.00	0.79	1.02	1.23	1.54	1.85	2.22	4.00
	1:50:00	0	0.00	0.72	0.90	1.10	1.32	1.56	1.82	3.19
	1:55:00	0	0.00	0.61	0.78	0.97	1.11	1.29	1.46	2.46
	2:00:00	0	0.00	0.53	0.69	0.85	0.93	1.05	1.15	1.91
	2:05:00	0	0.00	0.43	0.56	0.70	0.72	0.81	0.86	1.44
	2:10:00	0	0.00	0.35	0.46	0.57	0.56	0.63	0.66	1.08
	2:15:00	0	0.00	0.29	0.38	0.47	0.45	0.50	0.51	0.82
	2:20:00	0	0.00	0.23	0.31	0.38	0.36	0.40	0.40	0.62
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	2:35:00	0	0.00	0.12	0.16	0.20	0.18	0.20	0.18	0.26
	2:40:00	0	0.00	0.10	0.13	0.15	0.14	0.15	0.14	0.20
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	3:10:00	0	0.00	0.02	0.02	0.03	0.02	0.03	0.02	0.03
	3:15:00	0	0.00	0.01	0.01	0.02	0.02	0.02	0.01	0.02
	3:20:00	0	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:25:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	3:50:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:00:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6:00:00	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	

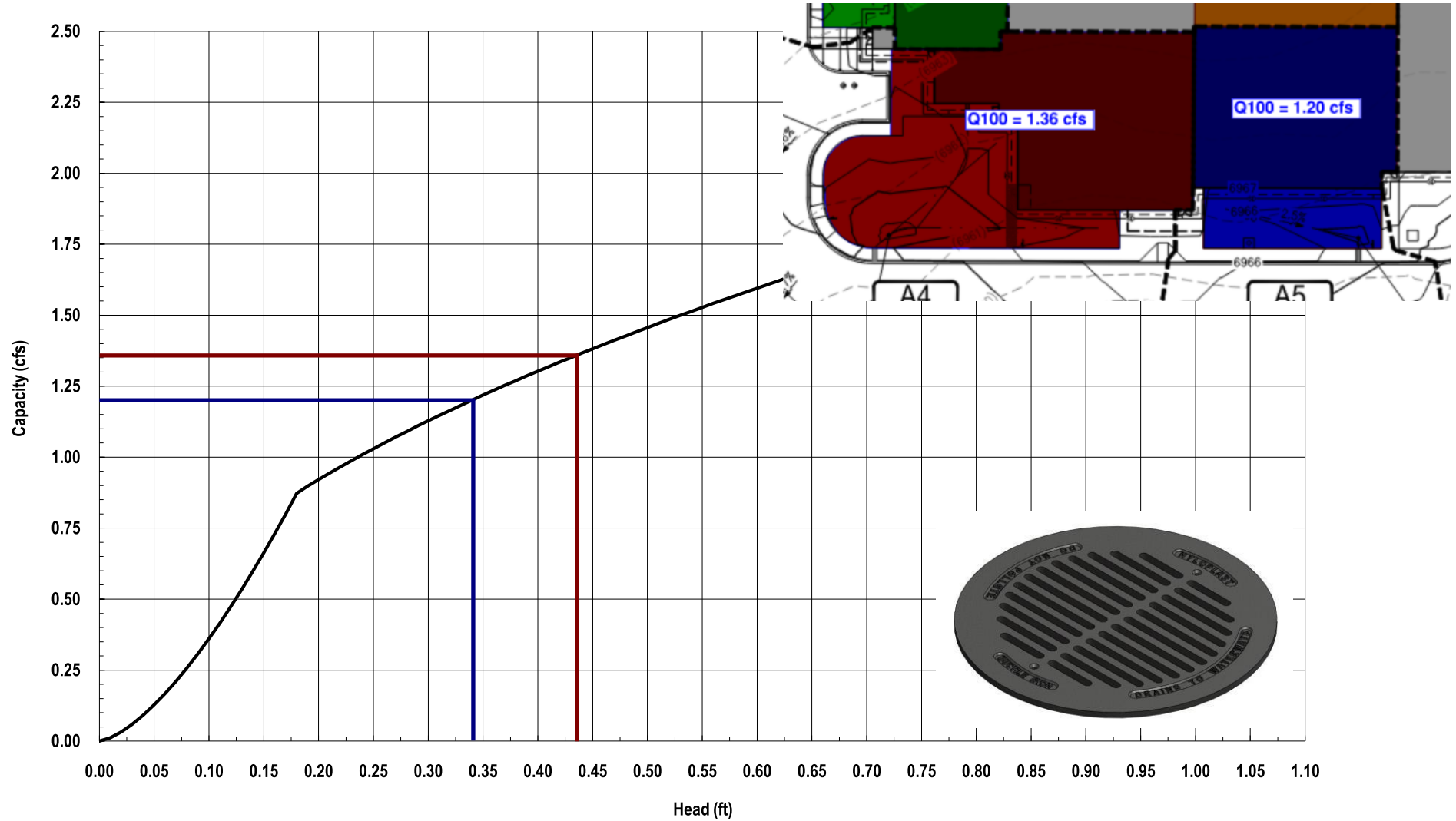
APPENDIX E
HYDRAULIC COMPUTATIONS

Nyloplast 10" Drop In Grate Inlet Capacity Chart



NW INLET
Qreq = 0.57 CFS --> 0.275 FT
NE INLET
Qreq = 0.55 CFS --> 0.26 FT

Nyloplast 15" Drop In Grate Inlet Capacity Chart



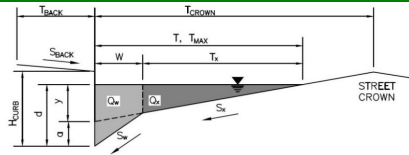
SW INLET
Qreq = 1.36 CFS --> 0.44 FT
SE INLET
Qreq = 1.20 CFS --> 0.34 FT



3130 Verona Avenue • Buford, GA 30518
 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

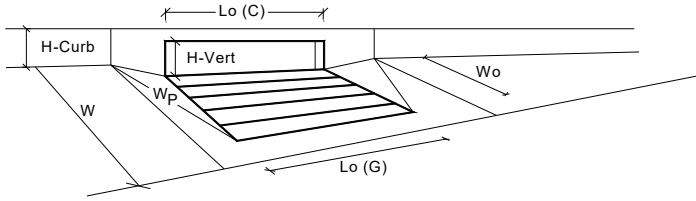
Project: **Honor Charter School**
 Inlet ID: **Inlet S1**



Gutter Geometry:	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 5.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} =$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 30.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_X = 0.046$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.000$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 30.0 & 30.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 6.0 & 6.0 \end{matrix}$ inches
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>
MINOR STORM Allowable Capacity is not applicable to Sump Condition	
MAJOR STORM Allowable Capacity is not applicable to Sump Condition	
$Q_{allow} =$	$\begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ \text{SUMP} & \text{SUMP} \end{matrix}$ cfs

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 6.00 (August 2025)



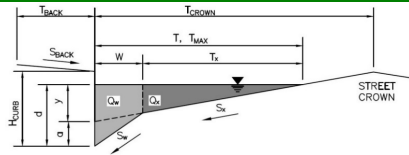
Design Information (Input)	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
Grate Information	MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	5.4	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	1.3	2.4	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Honor Charter School

Inlet ID: Inlet S2



Gutter Geometry:

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

T_{BACK} = 5.0 ft
 S_{BACK} = ft/ft
 n_{BACK} = 0.012

Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

H_{CURB} = 6.00 inches
 T_{CROWN} = 30.0 ft
 W = 2.00 ft
 S_X = 0.041 ft/ft
 S_W = 0.083 ft/ft
 S_0 = 0.000 ft/ft
 n_{STREET} = 0.016

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
T_{MAX} =	30.0	30.0	ft
d_{MAX} =	6.0	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

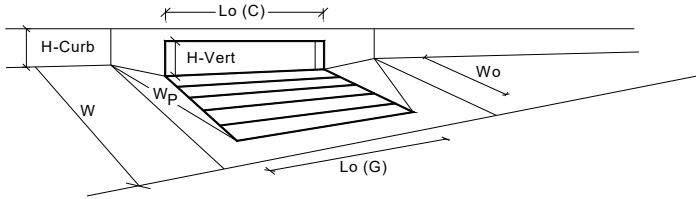
MINOR STORM Allowable Capacity is not applicable to Sump Condition
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

Q_{allow} =

Minor Storm	Major Storm	
SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

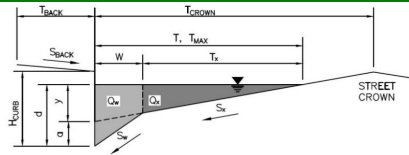
MHFD-Inlet, Version 6.00 (August 2025)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
Grate Information	MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	5.4	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	2.2	4.5	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

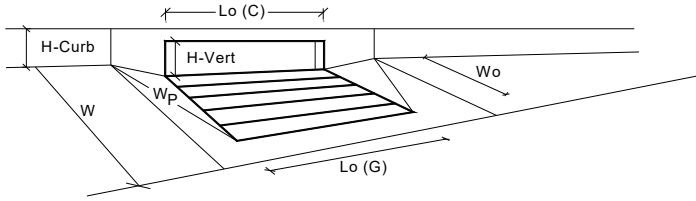
Project: **Honor Charter School**
 Inlet ID: **Inlet S4**



Gutter Geometry:	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 5.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} =$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.012$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 30.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_X = 0.020$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.000$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 30.0 & 30.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 6.0 & 6.0 \end{matrix}$ inches
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>
MINOR STORM Allowable Capacity is not applicable to Sump Condition	
MAJOR STORM Allowable Capacity is not applicable to Sump Condition	
$Q_{allow} =$	$\begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ \text{SUMP} & \text{SUMP} \end{matrix}$ cfs

INLET IN A SUMP OR SAG LOCATION

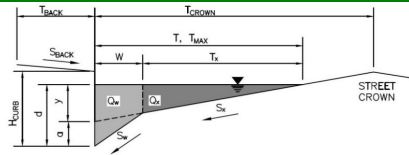
MHFD-Inlet, Version 6.00 (August 2025)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	Type = CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
Grate Information	MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	MINOR	MAJOR	
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	5.4	5.4	cfs
Q PEAK REQUIRED	1.0	1.5	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

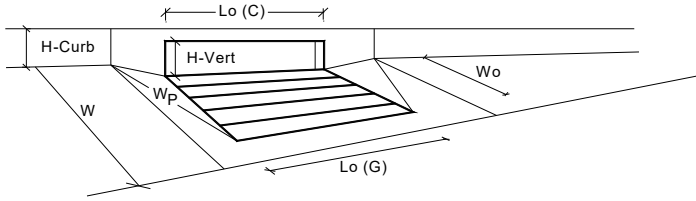
Project: **Honor Charter School**
 Inlet ID: **Inlet S5**



Gutter Geometry:	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 5.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} =$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.012$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 30.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_X = 0.036$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.000$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 30.0 & 30.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 6.0 & 6.0 \end{matrix}$ inches
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>
MINOR STORM Allowable Capacity is not applicable to Sump Condition	
MAJOR STORM Allowable Capacity is not applicable to Sump Condition	
$Q_{allow} =$	$\begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ \text{SUMP} & \text{SUMP} \end{matrix}$ cfs

INLET IN A SUMP OR SAG LOCATION

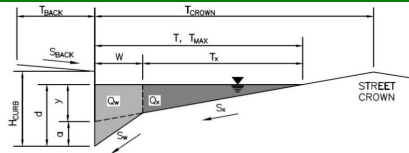
MHFD-Inlet, Version 6.00 (August 2025)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
Grate Information	MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	MINOR	MAJOR	
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	5.4	5.4	cfs
Q PEAK REQUIRED =	2.0	3.1	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

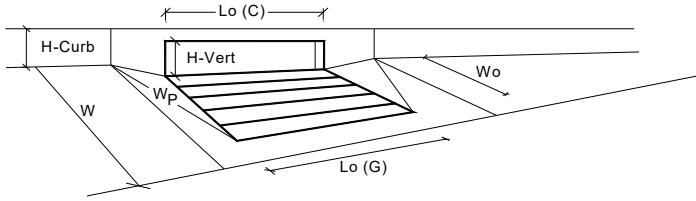
Project: **Honor Charter School**
 Inlet ID: **Inlet S7**



Gutter Geometry:					
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 5.0$ ft				
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} =$ ft/ft				
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.012$				
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches				
Distance from Curb Face to Street Crown	$T_{CROWN} = 30.0$ ft				
Gutter Width	$W = 2.00$ ft				
Street Transverse Slope	$S_X = 0.020$ ft/ft				
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft				
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.000$ ft/ft				
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$				
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} =$ <table border="1"><tr><th>Minor Storm</th><th>Major Storm</th></tr><tr><td>30.0</td><td>30.0</td></tr></table> ft	Minor Storm	Major Storm	30.0	30.0
Minor Storm	Major Storm				
30.0	30.0				
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} =$ <table border="1"><tr><th>Minor Storm</th><th>Major Storm</th></tr><tr><td>6.0</td><td>6.0</td></tr></table> inches	Minor Storm	Major Storm	6.0	6.0
Minor Storm	Major Storm				
6.0	6.0				
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>				
MINOR STORM Allowable Capacity is not applicable to Sump Condition					
MAJOR STORM Allowable Capacity is not applicable to Sump Condition					
$Q_{allow} =$	<table border="1"><tr><th>Minor Storm</th><th>Major Storm</th></tr><tr><td>SUMP</td><td>SUMP</td></tr></table> cfs	Minor Storm	Major Storm	SUMP	SUMP
Minor Storm	Major Storm				
SUMP	SUMP				

INLET IN A SUMP OR SAG LOCATION

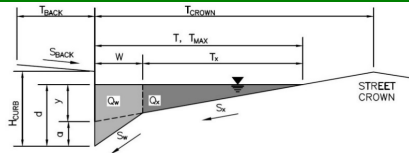
MHFD-Inlet, Version 6.00 (August 2025)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
Grate Information	MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	5.4	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	1.0	1.5	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

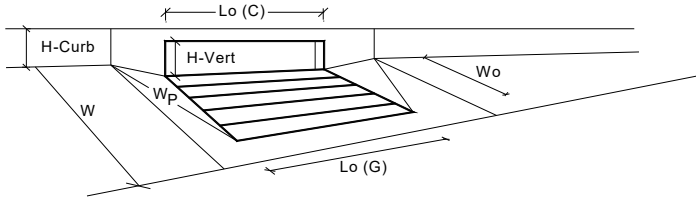
Project: **Honor Charter School**
 Inlet ID: **Inlet S8**



Gutter Geometry:	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 5.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} =$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.012$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 30.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_X = 0.030$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.000$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 30.0 & 30.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 6.0 & 6.0 \end{matrix}$ inches
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>
MINOR STORM Allowable Capacity is not applicable to Sump Condition	
MAJOR STORM Allowable Capacity is not applicable to Sump Condition	
$Q_{allow} =$	$\begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ \text{SUMP} & \text{SUMP} \end{matrix}$ cfs

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 6.00 (August 2025)



Design Information (Input)	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	6.0	inches
Grate Information	MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	MINOR	MAJOR	
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	5.4	5.4	cfs
Q PEAK REQUIRED =	1.0	1.5	cfs

Channel Report

A1-01

Circular

Diameter (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Known Q

Known Q (cfs) = 2.96

Highlighted

Depth (ft) = 0.49

Q (cfs) = 2.960

Area (sqft) = 0.60

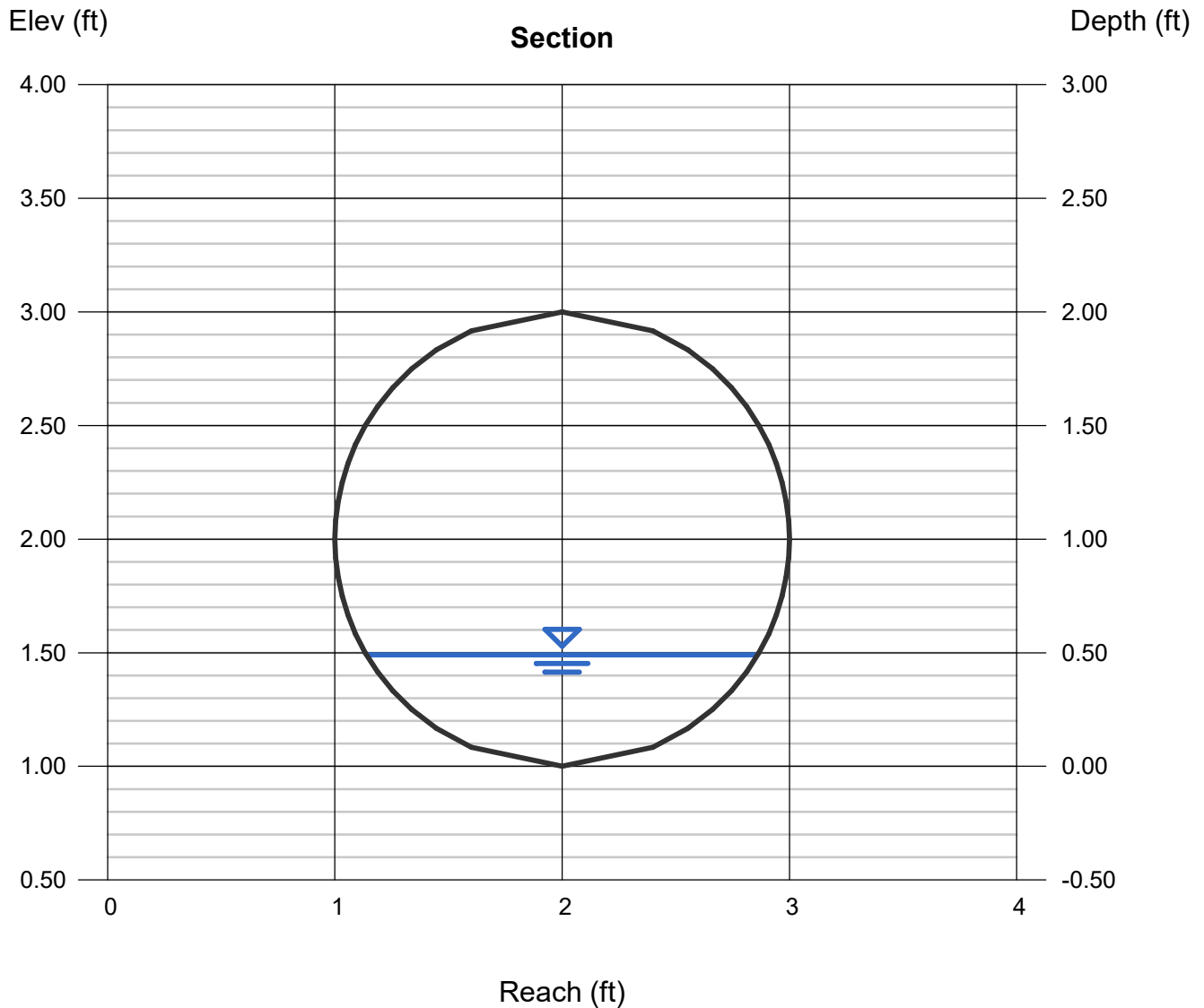
Velocity (ft/s) = 4.91

Wetted Perim (ft) = 2.08

Crit Depth, Y_c (ft) = 0.60

Top Width (ft) = 1.72

EGL (ft) = 0.86



Channel Report

A2-01

Circular

Diameter (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Known Q

Known Q (cfs) = 8.19

Highlighted

Depth (ft) = 0.84

Q (cfs) = 8.190

Area (sqft) = 1.26

Velocity (ft/s) = 6.49

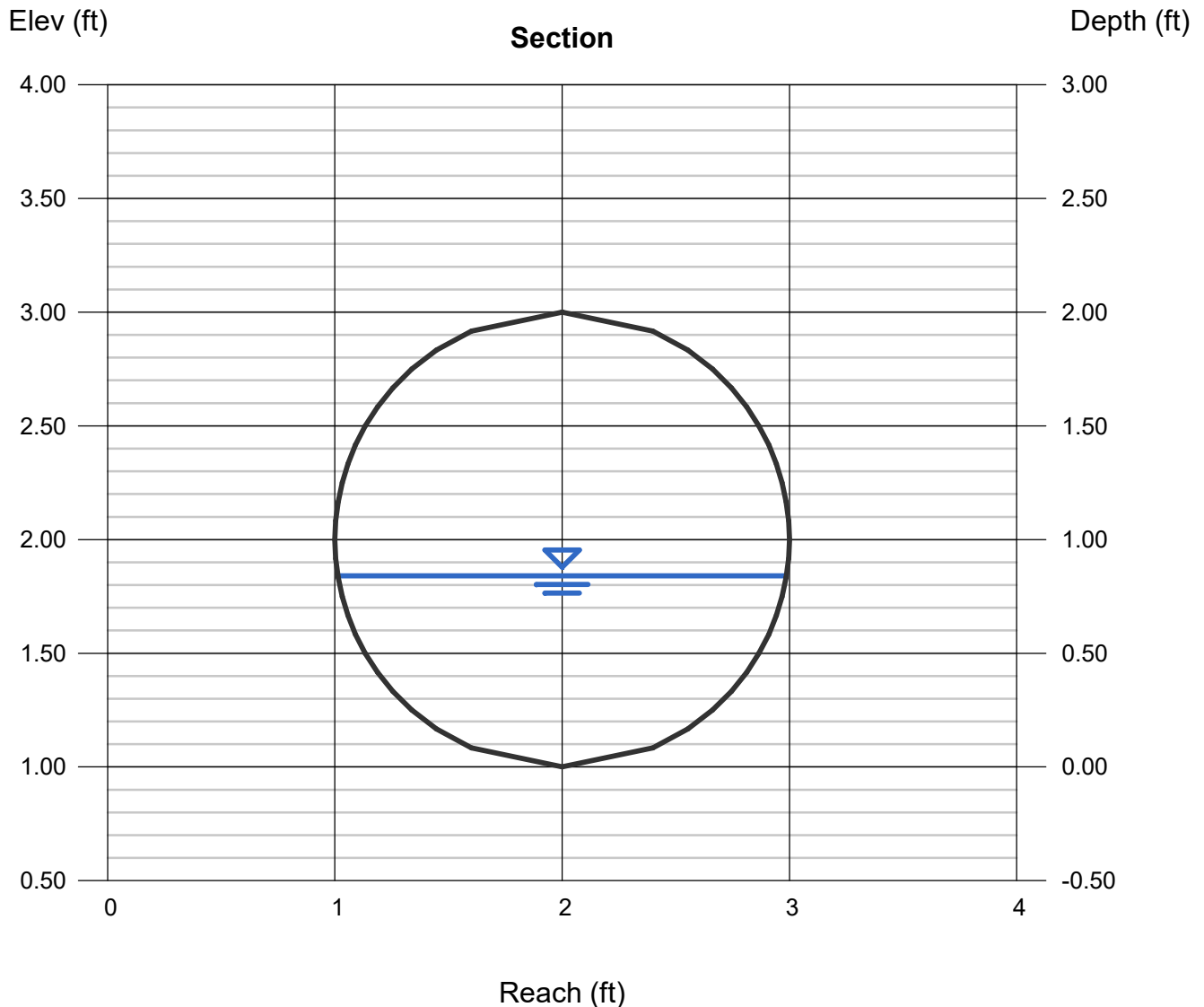
Wetted Perim (ft) = 2.83

Crit Depth, Yc (ft) = 1.02

Top Width (ft) = 1.98

EGL (ft) = 1.50

Basin A1 (2.96) +
Basin A2 (5.23)



Channel Report

A4-01

Circular

Diameter (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Known Q

Known Q (cfs) = 6.79

Highlighted

Depth (ft) = 0.75

Q (cfs) = 6.790

Area (sqft) = 1.08

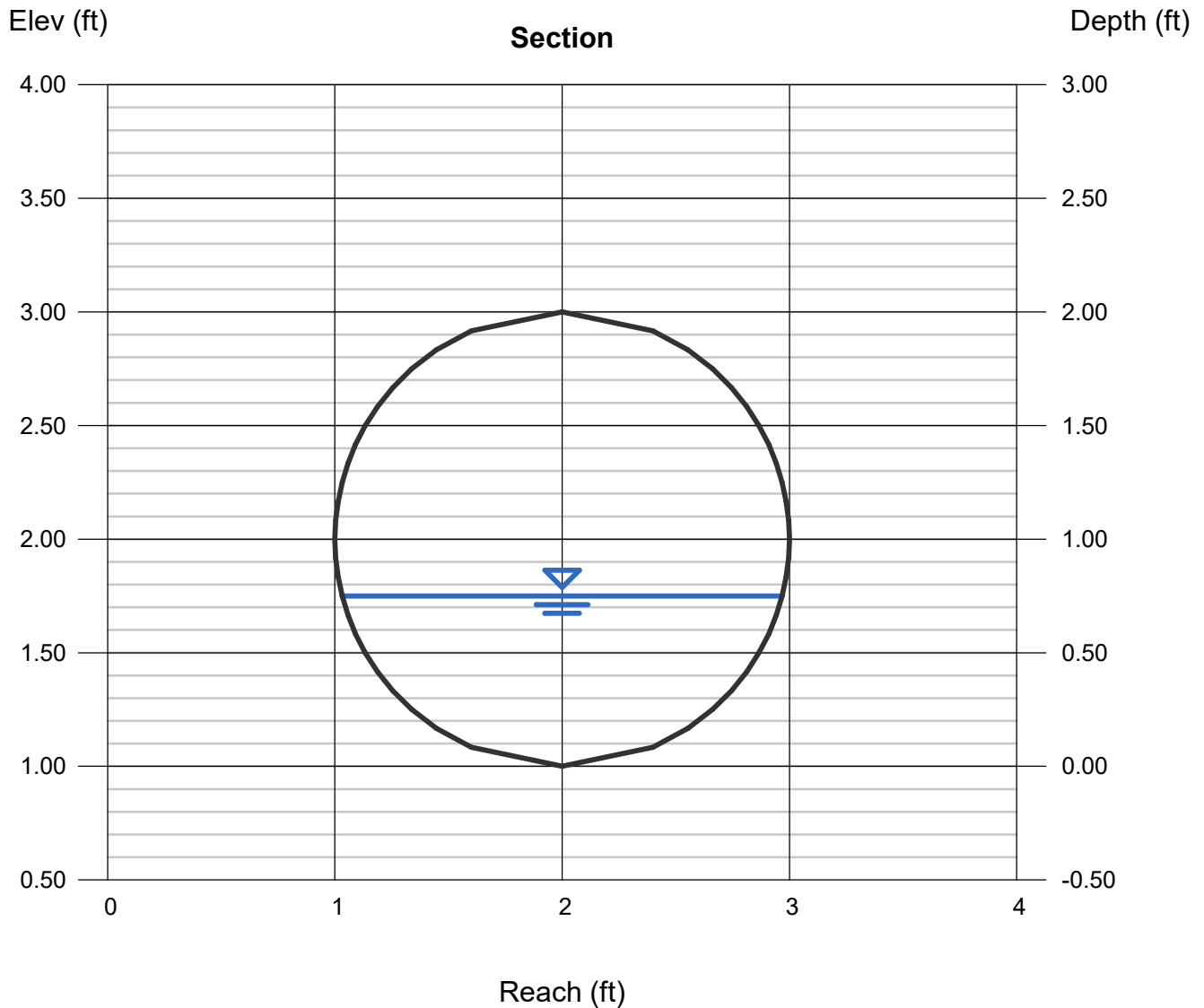
Velocity (ft/s) = 6.29

Wetted Perim (ft) = 2.64

Crit Depth, Y_c (ft) = 0.92

Top Width (ft) = 1.94

EGL (ft) = 1.37



Channel Report

A5-01

Circular

Diameter (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Known Q

Known Q (cfs) = 10.89

Highlighted

Depth (ft) = 0.98

Q (cfs) = 10.89

Area (sqft) = 1.54

Velocity (ft/s) = 7.08

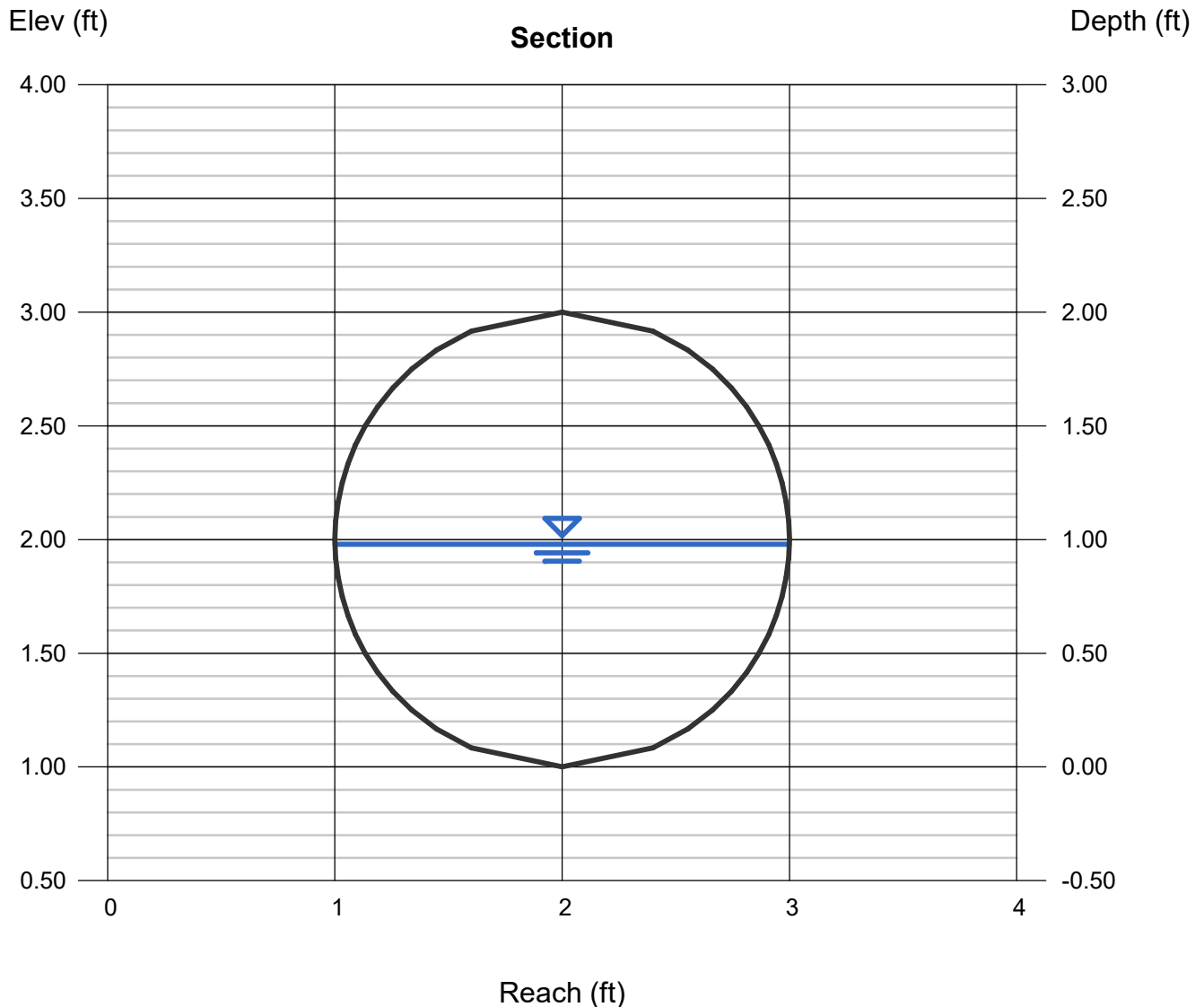
Wetted Perim (ft) = 3.11

Crit Depth, Yc (ft) = 1.19

Top Width (ft) = 2.00

EGL (ft) = 1.76

Basin A4 (6.79) +
Basin A5 (4.10)



Channel Report

A6-01

Circular

Diameter (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 1.00

N-Value = 0.013

Calculations

Compute by: Known Q

Known Q (cfs) = 1.93

Highlighted

Depth (ft) = 0.40

Q (cfs) = 1.930

Area (sqft) = 0.45

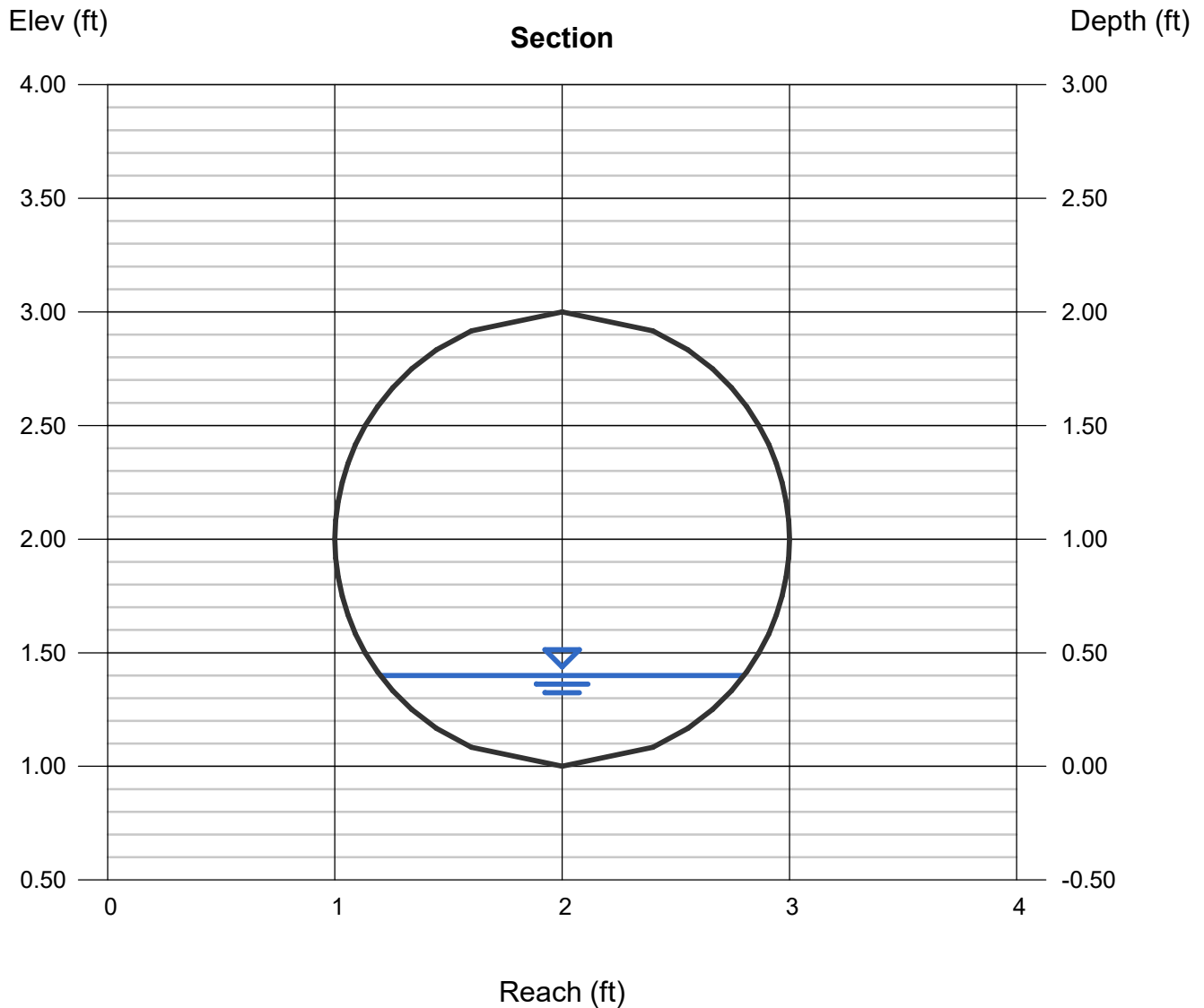
Velocity (ft/s) = 4.28

Wetted Perim (ft) = 1.86

Crit Depth, Y_c (ft) = 0.49

Top Width (ft) = 1.60

EGL (ft) = 0.69



Channel Report

Outflow Pipe 100 Year Flow

Circular

Diameter (ft) = 1.50

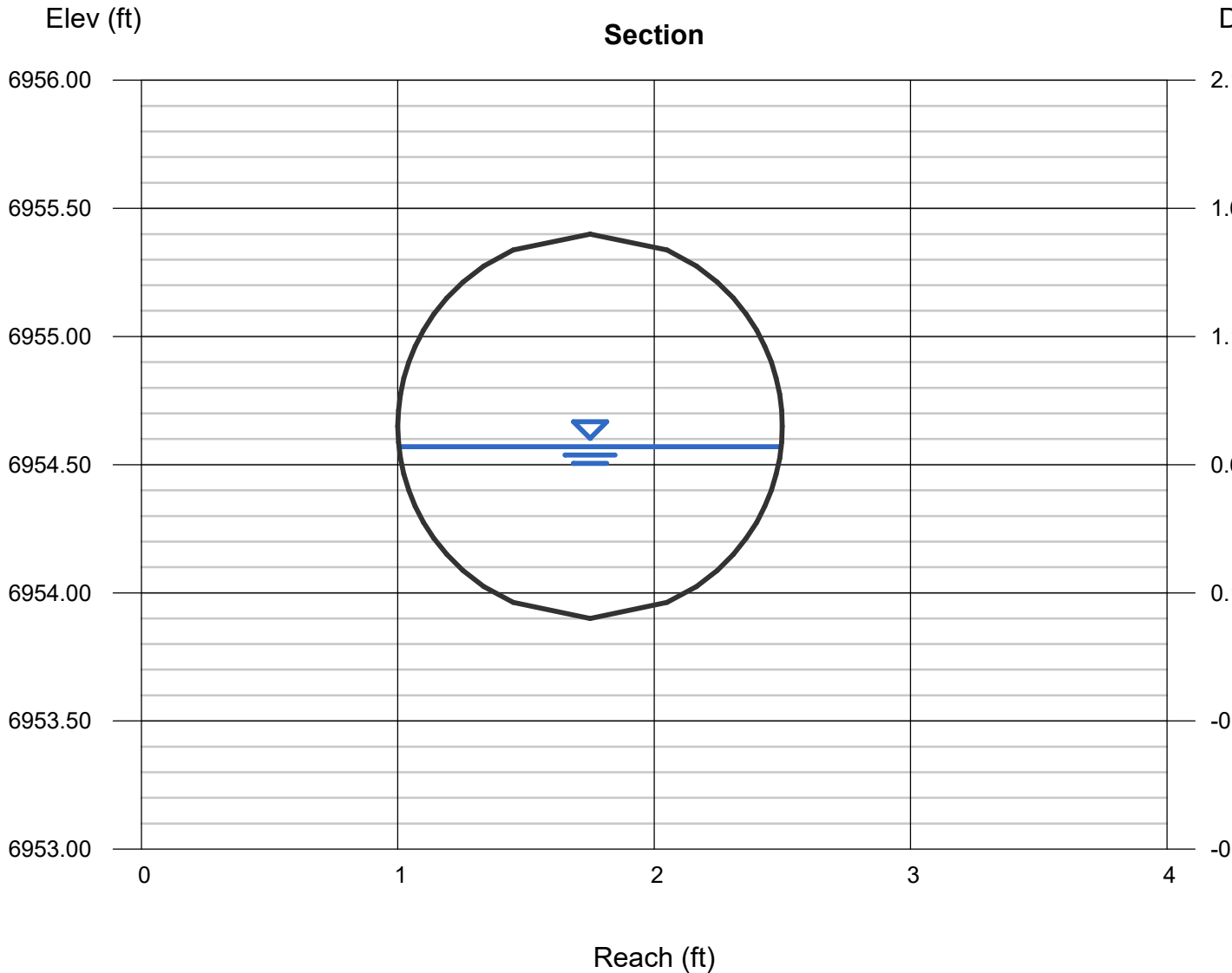
Invert Elev (ft) = 6953.90
Slope (%) = 1.00
N-Value = 0.012

Highlighted

Depth (ft) = 0.67
Q (cfs) = 4.600
Area (sqft) = 0.76
Velocity (ft/s) = 6.01
Wetted Perim (ft) = 2.20
Crit Depth, Yc (ft) = 0.83
Top Width (ft) = 1.49
EGL (ft) = 1.23

Calculations

Compute by: Known Q
Known Q (cfs) = 4.60



Weir Report

100-year Emergency Overflow Detention Pond

Trapezoidal Weir

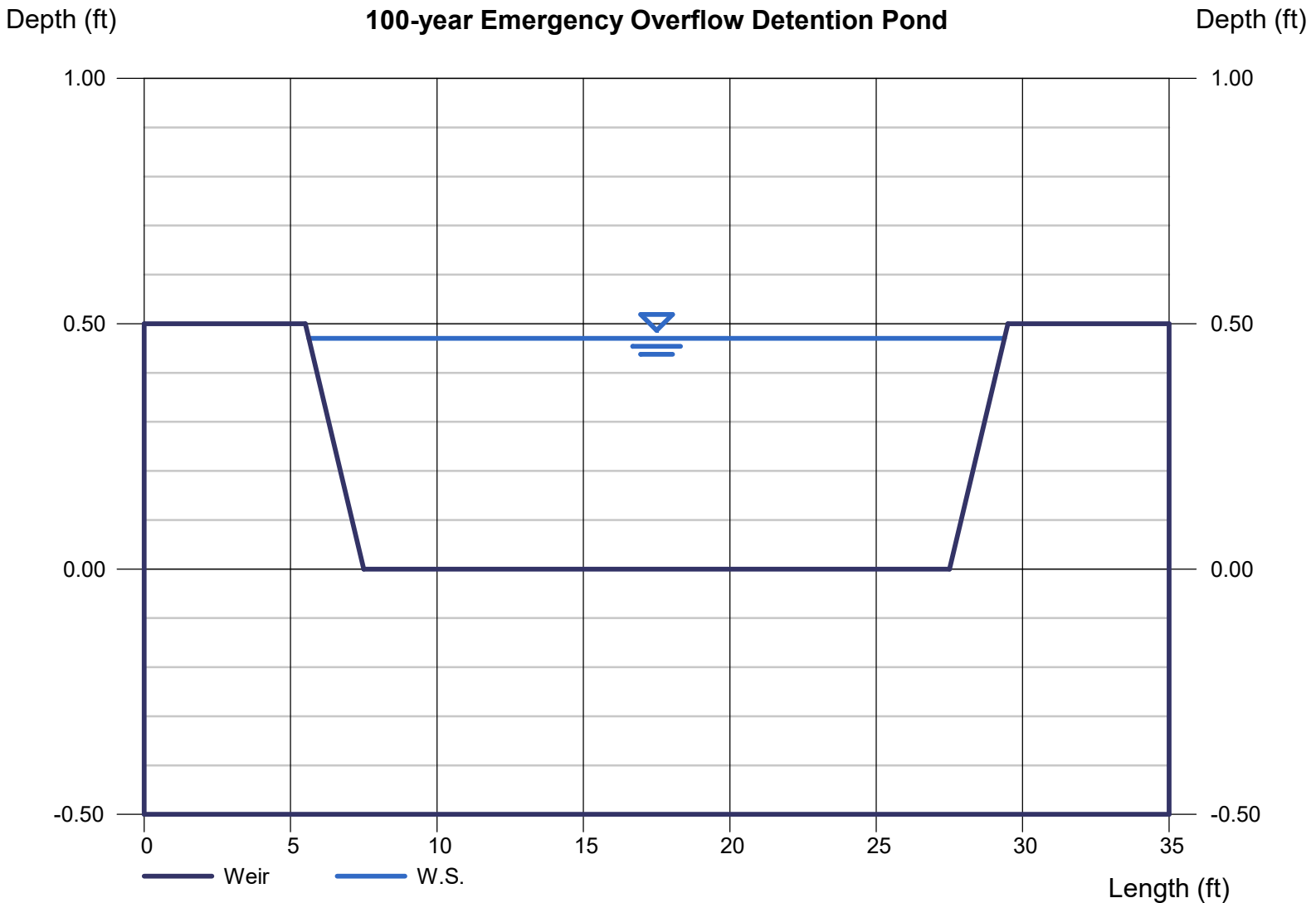
Crest = Sharp
Bottom Length (ft) = 20.00
Total Depth (ft) = 0.50
Side Slope (z:1) = 4.00

Highlighted

Depth (ft) = 0.47
Q (cfs) = 21.11
Area (sqft) = 10.28
Velocity (ft/s) = 2.05
Top Width (ft) = 23.76

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 21.11



Channel Report

Channel 100 Year Flow

Trapezoidal

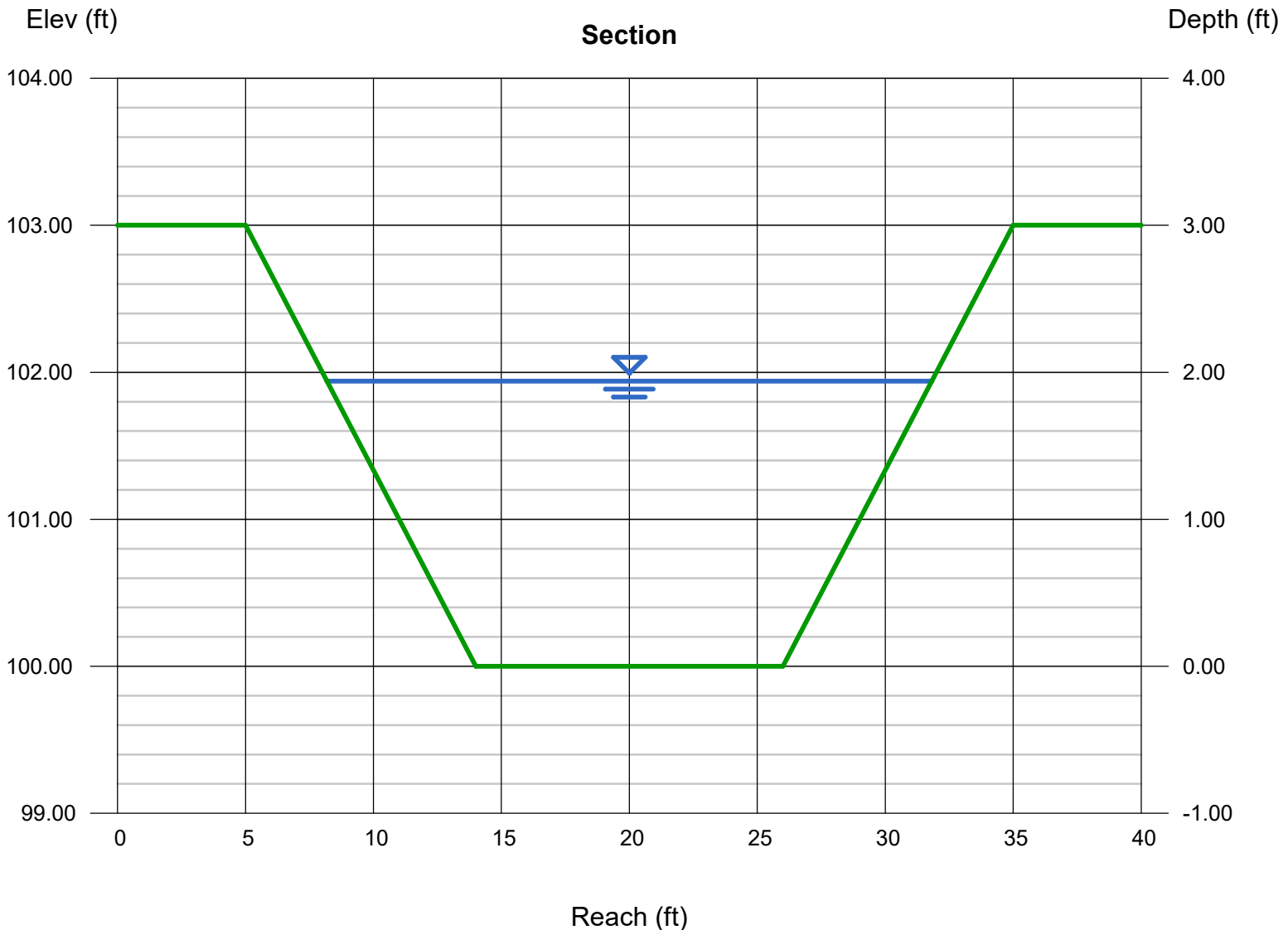
Bottom Width (ft) = 12.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 3.00
Invert Elev (ft) = 100.00
Slope (%) = 0.80
N-Value = 0.080

Highlighted

Depth (ft) = 1.94
Q (cfs) = 72.50
Area (sqft) = 34.57
Velocity (ft/s) = 2.10
Wetted Perim (ft) = 24.27
Crit Depth, Yc (ft) = 0.96
Top Width (ft) = 23.64
EGL (ft) = 2.01

Calculations

Compute by: Known Q
Known Q (cfs) = 72.50



Channel Report

100 Year Offsite Emergency Overflow

User-defined

Invert Elev (ft) = 55.62
Slope (%) = 1.50
N-Value = 0.012

Calculations

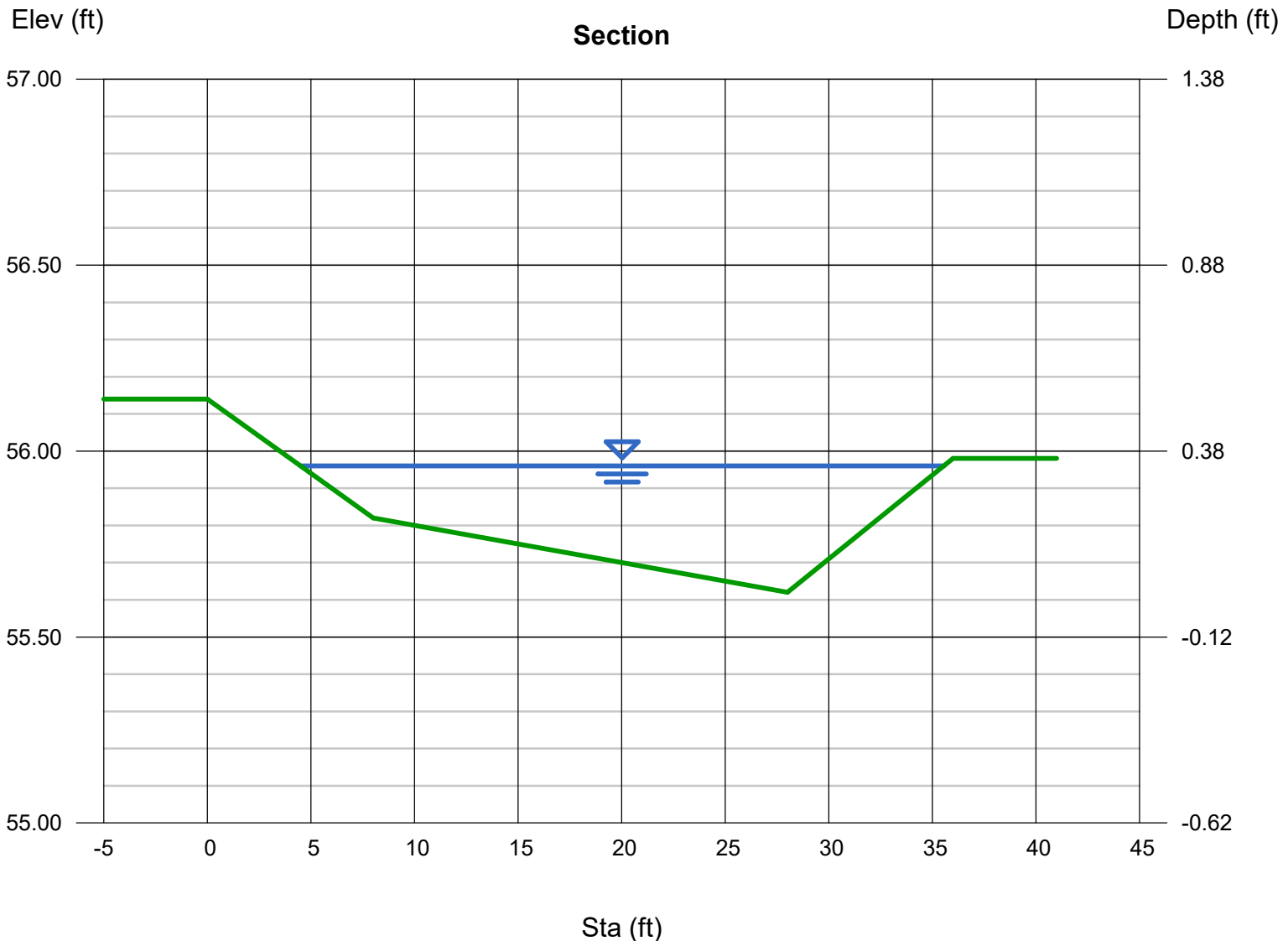
Compute by: Known Q
Known Q (cfs) = 33.20

Highlighted

Depth (ft) = 0.34
Q (cfs) = 33.20
Area (sqft) = 6.33
Velocity (ft/s) = 5.25
Wetted Perim (ft) = 31.07
Crit Depth, Yc (ft) = 0.47
Top Width (ft) = 31.06
EGL (ft) = 0.77

(Sta, El, n)-(Sta, El, n)...

(0.00, 56.14)-(8.00, 55.82, 0.012)-(28.00, 55.62, 0.012)-(36.00, 55.98, 0.012)



Channel Report

Off-site 30 inch Pipes 100-year at 1 percent

Circular

Diameter (ft) = 2.50

Invert Elev (ft) = 100.00

Slope (%) = 1.00

N-Value = 0.012

Calculations

Compute by:

Known Q (cfs)

Known Q

= 45.50

Highlighted

Depth (ft) = 2.11

Q (cfs) = 45.50

Area (sqft) = 4.42

Velocity (ft/s) = 10.29

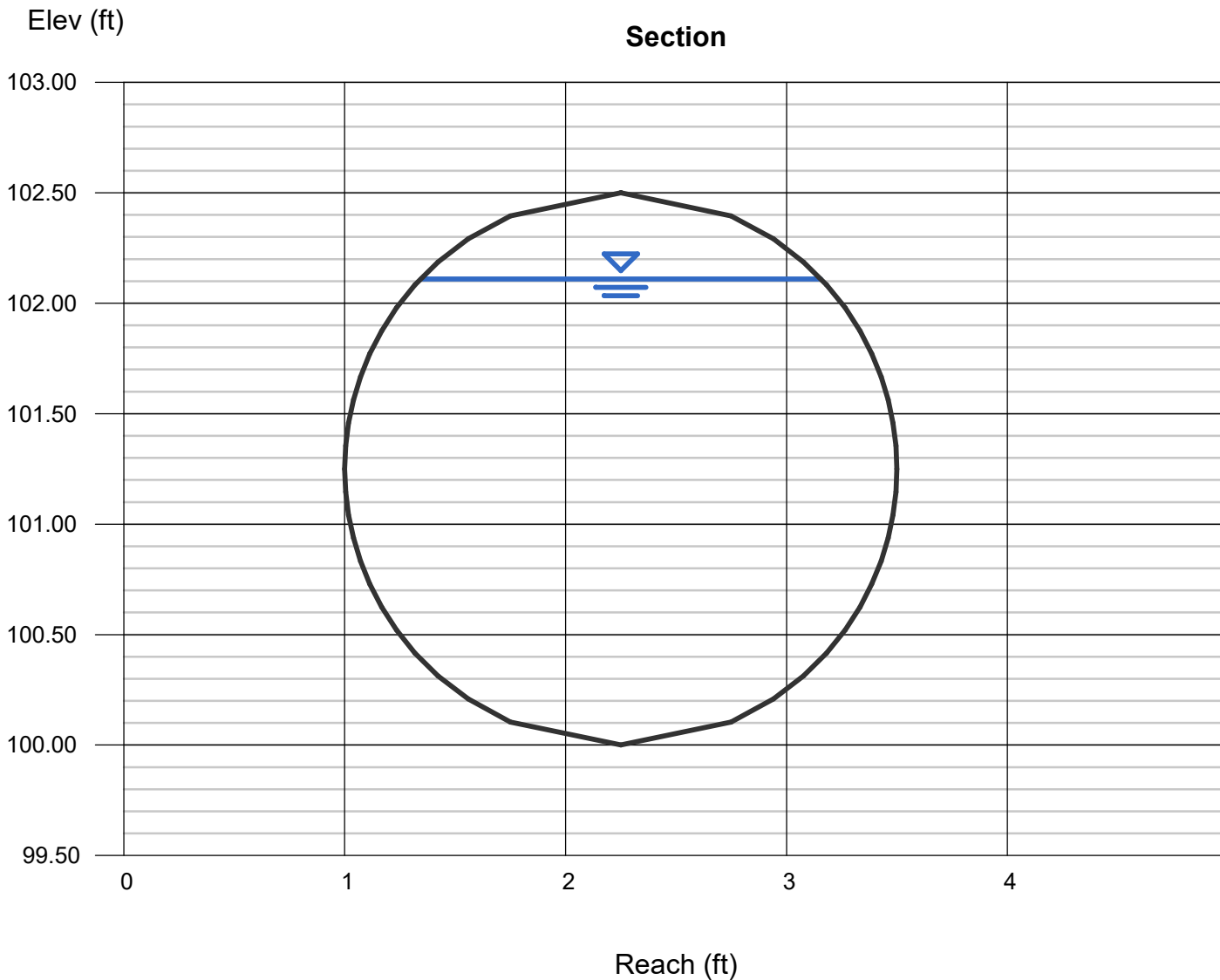
Wetted Perim (ft) = 5.83

Crit Depth, Yc (ft) = 2.24

Top Width (ft) = 1.81

EGL (ft) = 3.76

+72.5 cfs (Off-site North)
+1.6 cfs (Off-site West)
+4.6 cfs (On-site Discharge)
-33.2 cfs (Off-site Discharge to Bent Grass Meadows Roadway)
= 45.5 cfs (Discharge through Proposed Storm Pipe.)



Channel Report

Off-site Pipes 100-year at 0.5 percent

Circular

Diameter (ft) = 3.00

Invert Elev (ft) = 100.00

Slope (%) = 0.50

N-Value = 0.012

Calculations

Compute by:

Known Q (cfs)

Known Q

= 45.50

Highlighted

Depth (ft) = 2.21

Q (cfs) = 45.50

Area (sqft) = 5.59

Velocity (ft/s) = 8.15

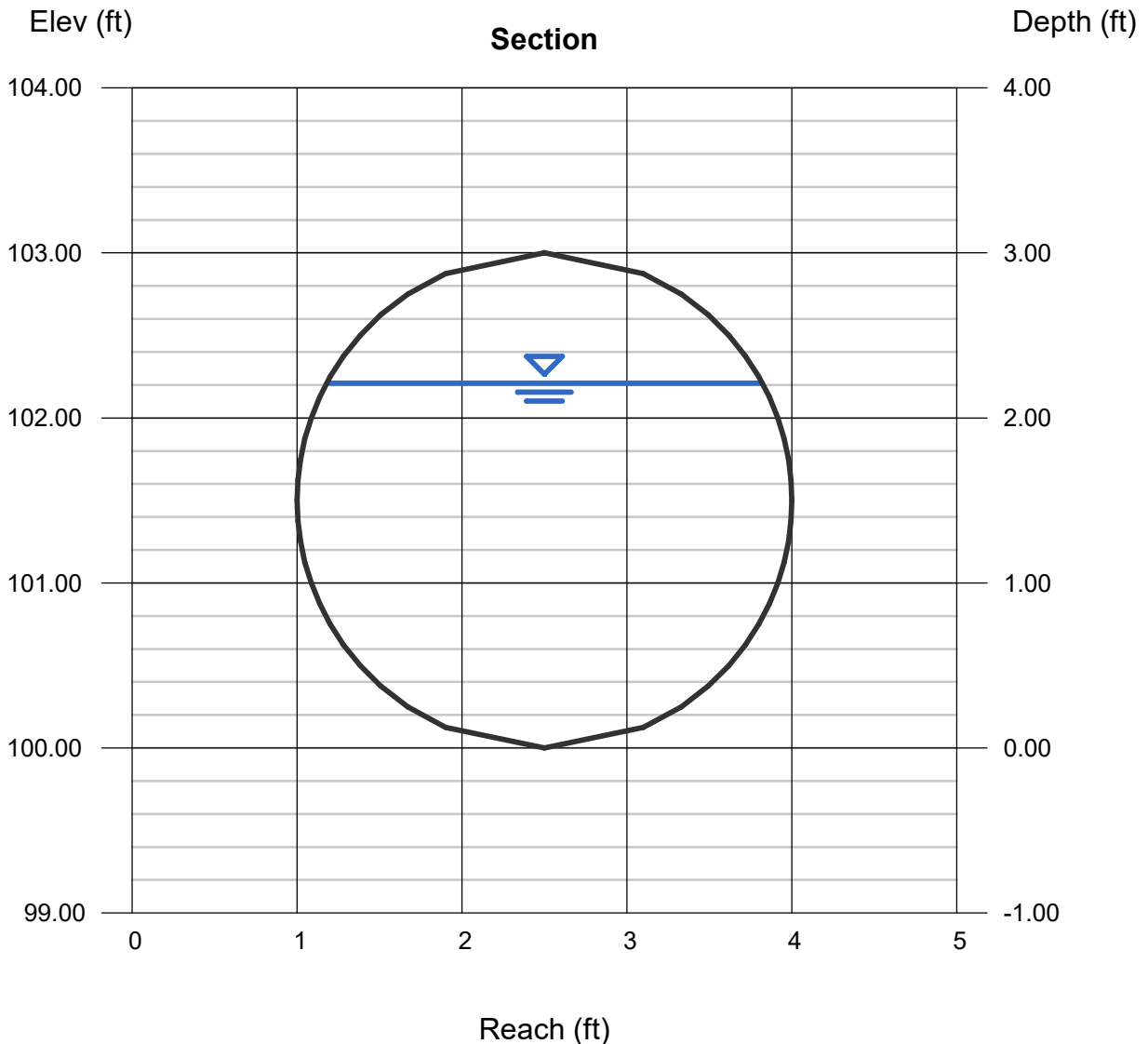
Wetted Perim (ft) = 6.20

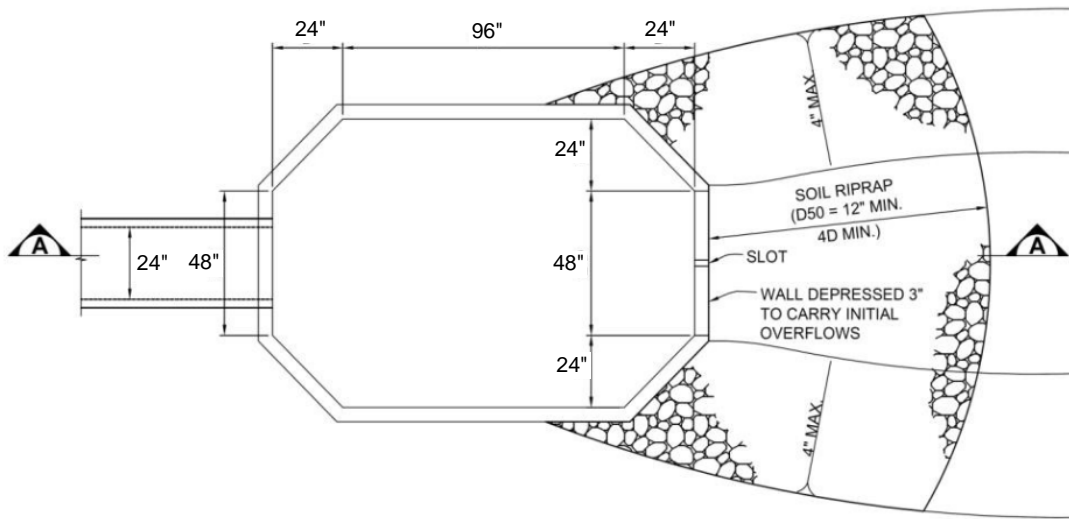
Crit Depth, Yc (ft) = 2.20

Top Width (ft) = 2.64

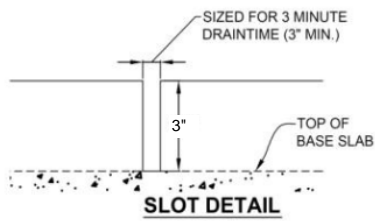
EGL (ft) = 3.24

+72.5 cfs (Off-site North)
+1.6 cfs (Off-site West)
+4.6 cfs (On-site Discharge)
-33.2 cfs (Off-site Discharge to Bent Grass Meadows Roadway)
= 45.5 cfs (Discharge through Proposed Storm Pipe.)



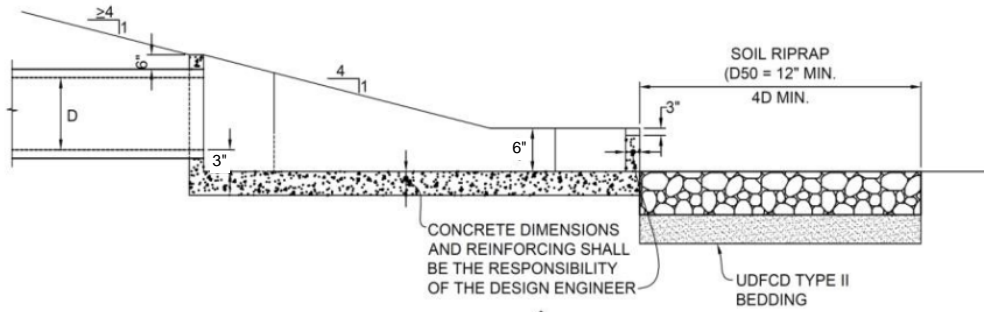


PLAN



NOTES:

1. DIMENSIONS SHOWN ARE MINIMUMS AND APPLY TO FOREBAYS WITHIN MODIFIED EXTENDED DETENTION BASINS. FOREBAYS IN STANDARD EXTENDED DETENTION BASINS SHALL BE SIZED BASED ON UDFCD CRITERIA.
2. FOR DEPTH \geq 2.5- FEET, FOREBAY REQUIRES RAMP INTO BOTTOM AND ACCESS ROAD LEADING TO STREET.



SECTION A

Basin A1 and A2 Forebay sizing

5. Forebay

A) Minimum Forebay Volume
($V_{\text{FMIN}} = \underline{\quad 1\% \quad}$ of the WQCV)

B) Actual Forebay Volume

C) Forebay Depth
($D_F = \underline{\quad 12 \quad}$ inch maximum)

D) Forebay Discharge

i) Undetained 100-year Peak Discharge

ii) Forebay Discharge Design Flow
($Q_F = 0.02 * Q_{100}$)

E) Forebay Discharge Design

F) Discharge Pipe Size (minimum 8-inches)

G) Rectangular Notch Width

$V_{\text{FMIN}} = \underline{\quad 0.00 \quad}$ ac-ft

$V_F = \underline{\quad 0.0010 \quad}$ ac-ft

$D_F = \underline{\quad 6.0 \quad}$ in

$Q_{100} = \underline{\quad 6.62 \quad}$ cfs

$Q_F = \underline{\quad 0.13 \quad}$ cfs

Choose One

- Berm With Pipe
 Wall with Rect. Notch
 Wall with V-Notch Weir

Flow too small for berm w/ pipe

Calculated $D_P = \underline{\quad \quad}$ in

Calculated $W_N = \underline{\quad 2.5 \quad}$ in

Basin A4 and A5 Forebay sizing

5. Forebay

A) Minimum Forebay Volume
($V_{\text{FMIN}} = \underline{\quad 1\% \quad}$ of the WQCV)

B) Actual Forebay Volume

C) Forebay Depth
($D_F = \underline{\quad 12 \quad}$ inch maximum)

D) Forebay Discharge

i) Undetained 100-year Peak Discharge

ii) Forebay Discharge Design Flow
($Q_F = 0.02 * Q_{100}$)

E) Forebay Discharge Design

F) Discharge Pipe Size (minimum 8-inches)

G) Rectangular Notch Width

$V_{\text{FMIN}} = \underline{\quad 0.00 \quad}$ ac-ft

$V_F = \underline{\quad 0.0010 \quad}$ ac-ft

$D_F = \underline{\quad 6.0 \quad}$ in

$Q_{100} = \underline{\quad 8.23 \quad}$ cfs

$Q_F = \underline{\quad 0.16 \quad}$ cfs

Choose One

- Berm With Pipe
 Wall with Rect. Notch
 Wall with V-Notch Weir

Flow too small for berm w/ pipe

Calculated $D_P = \underline{\quad \quad}$ in

Calculated $W_N = \underline{\quad 2.9 \quad}$ in

APPENDIX F

SECTIONS FROM BENT GRASS MDDP/DBPS
AMENDMENT & THE FALCON DRAINAGE
BASIN STUDY

**FOLLOWING PAGES FROM
MDDP/DBPS AMENDMENT**



**MDDP &
DBPS AMENDMENT**

BENT GRASS DEVELOPMENT

El Paso County, Colorado

PREPARED FOR:
Challenger Communities, LLC
8605 Explorer Dr., Suite 250
Colorado Springs, CO 80920

PREPARED BY:
Galloway & Company, Inc.
1155 Kelly Johnson Blvd., Suite 305
Colorado Springs, CO 80920

DATE:
January 2021
Revised: March 2021
Revised: April 2021
Revised: June 2021
Revised: August 2021
Revised: September 2021

PUDSP-20-005



A Current Conditions drainage basin map has also been provided. This scenario includes the development of Bent Grass residential Filing No. 2. Hydrology Calculations for this scenario have been provided in Appendix B. This was also provided as the existing conditions map and calculations in the Bent Grass West PDR.

Individual basin descriptions have not been included here, as they have been addressed in previously stated reports. General overall descriptions of the drainage patterns have been provided.

The Bent Grass development will impact the West Tributary and the Middle Tributary of the Falcon Basin. All development from the west of side of Bent Grass Residential Filing No. 1 and west will be contained within the West Tributary. Everything east of that property line, including the Bent Grass Meadows/Meridian Road intersection, will impact the Middle Tributary.

MIDDLE TRIBUTARY

The Middle Tributary drainage begins at Design Point 30.

Design Point 30 (225.0 AC, $Q_5 = 2.1$ cfs, $Q_{100} = 63.5$ cfs): is the release rate of the existing Meadows Pond #3, located in Meadows Filing No. 3, just north of Woodmen Hills Drive. The flows are based on the revised HEC-HMS (Current and Future Models), which is located in Appendix B. Flows will cross under Woodmen Hills Drive via an existing culvert, then sheet flow to the southeast, passing through Basin OS-25 to DP 31. The DBPS by Matrix had 160 cfs at this location under the “Do Nothing Analysis” and 99 cfs under the “Regional” and “Sub-Regional” design alternatives. Minor flows were not provided in the report. The flows are lower in the current HEC-HMS report, as more accurate design data and as-built information for the existing Meadows Pond 2 was utilized in the pond stage/storage and storage/discharge tables.

Design Point 30 will combine with offsite basins OS-25 & OS-26, until they reach an existing sedimentation pond at DP-32, located north of Bent Grass Meadows Drive, on what’s referred to as the “school” site. The current configuration of the pond has release rates of 2.1 and 63.5 cfs for the 5 and 100-year storm events, under the Current HEC HMS model. These flows will continue south to Bent Grass Meadows Drive. Curb and gutter in the roadway is able to handle 7.4 and 33.2 cfs in the minor and major storms. It is assumed that the max gutter flow will continue to the east and any remaining flow, of 30.3 cfs, will be directed to the south through the Bent Grass Filing No. 1 development. Flow will travel through curb and gutter and existing storm systems within Bent Grass Filing No. 1, ultimately out falling to Bent Grass Pond 1. Based on the local street section and slopes, flows were routed through the development based on overtopping and flows splitting at intersections. The routing of the storm flow can be found in Appendix B, under Surface Routing.

The existing detention pond, Pond 1 Bent Grass Filing No. 1, was analyzed with the additional flow and contributing area. From the FDR for Bent Grass Residential, Pond 1 had a 5-year release rate of 0.4 cfs and a 100-year release rate of 6.8 cfs. The 100-year water surface elevation was 6937.61. With the additional flow being re-routed to Pond 1, the current release rates for Pond 1 are 0.5 cfs for the 5-year event and 22.0 cfs for the 100-year event. The pond will have a 100-year water surface elevation of 6938.08. The spillway elevation for the pond is 6939.61.

Flows in Bent Grass Meadows will continue east, on the north side of the roadway, where they will combine with offsite flows from BG 50 (5-year flow is 280 cfs, 100-year flow=850 cfs), which is the flow obtained from the Falcon DBPS. There are 3 existing 45” x 29” elliptical rcp’s. For the current condition, the approved FDR for Meridian Road is allowing 2 additional elliptical rcp’s, which will handle the flow

from Bent Grass Meadows at Design Point 15n (5-year flow = 13.4 cfs, 100-year flow=62.2 cfs). Design Point 20 (5-year flow=304.8, 100-year flow=961.8 cfs) combines the roadside flow from offsite with the flow from Bent Grass Meadows Drive. Flows will then continue south in a roadside ditch along Meridian Road, on the west side. The Meridian Road ditch also captures flows from the Bent Grass East Commercial developments. Existing water quality facilities intercept the runoff and treat it, prior to being released into the ditch. Flows will eventually be intercepted by a set of existing twin 36" cmp's at Owl Place, at Design Point BG 25 (Q100=837.4, Q5=256.3 cfs). From the Meridian Road/Bent Grass Meadows FDR, it is shown that the existing culverts at Bent Grass Meadows Drive and Owl Place and the channel connecting the culverts are undersized and will need to be improved in the future to properly convey the flows outlined in the DBPS. Flow will continue through an existing channel and release into Pond SR-4.

The "school site" and areas north of it (Rational Basins OS-25 & OS-26), are now referred to as Basin MT060a in the HEC HMS model. MT060a is 19.8 acres and generates 8.3 cfs for the 5-year event and 28.3 cfs for the 100-year event. These flows are directed to an existing "sediment pond" which is referred to as the "School Pond". This area is a localized low area which holds flows and releases them through an existing spillway. This "pond" has been included in the "Current HEC_HMS model". Basin MT060-N is the area east of MT060a and north of Bent Grass Meadows Drive. MT060-N is 28.2 acres and flows towards the east to Meridian Road. MT060-N generates 17.6 cfs for the 5-year storm and 59.6 cfs for the 100-year storm. MT060-S is 70.9 acres and is south of Bent Grass Meadows Drive, It encompasses the remainder of the original DBPS MT060 basin and flows through an existing channel to the south. MT060-S generates 37.8 cfs for the 5-year storm and 125.7 cfs for the 100-year storm. These flows are released directly into Pond SR-4.

WEST TRIBUTARY

For the West Tributary of Falcon Basin, the hydrology analysis has the Bent Grass Residential Filing No. 2 as being constructed, as it is currently under construction. The basins for this development are part of the hydrology calculations which are provided in Appendix B, but a complete description of each of these basins has not been provided, as they can be referenced in the approved FDR for Bent Grass Residential Filing No. 2. With this development, there were 2 water quality ponds built, which release into the West Tributary channel. The offsite basins have also been discussed in the Bent Grass Filing No. 2 FDR.

The currently undeveloped portion of the Bent Grass site, referred to as Bent Grass West, is comprised of 8 undeveloped basins. Below is a brief description of them.

Basin EX-1 (1.19 AC, $Q_5 = 0.4$ cfs, $Q_{100} = 2.5$ cfs): is associated with the northeastern portion of the Bent Grass West site east of the existing channel. The basin is currently undeveloped. Runoff from the basin generally flows to the southwest, into Basin EX-2 at **DP 10**.

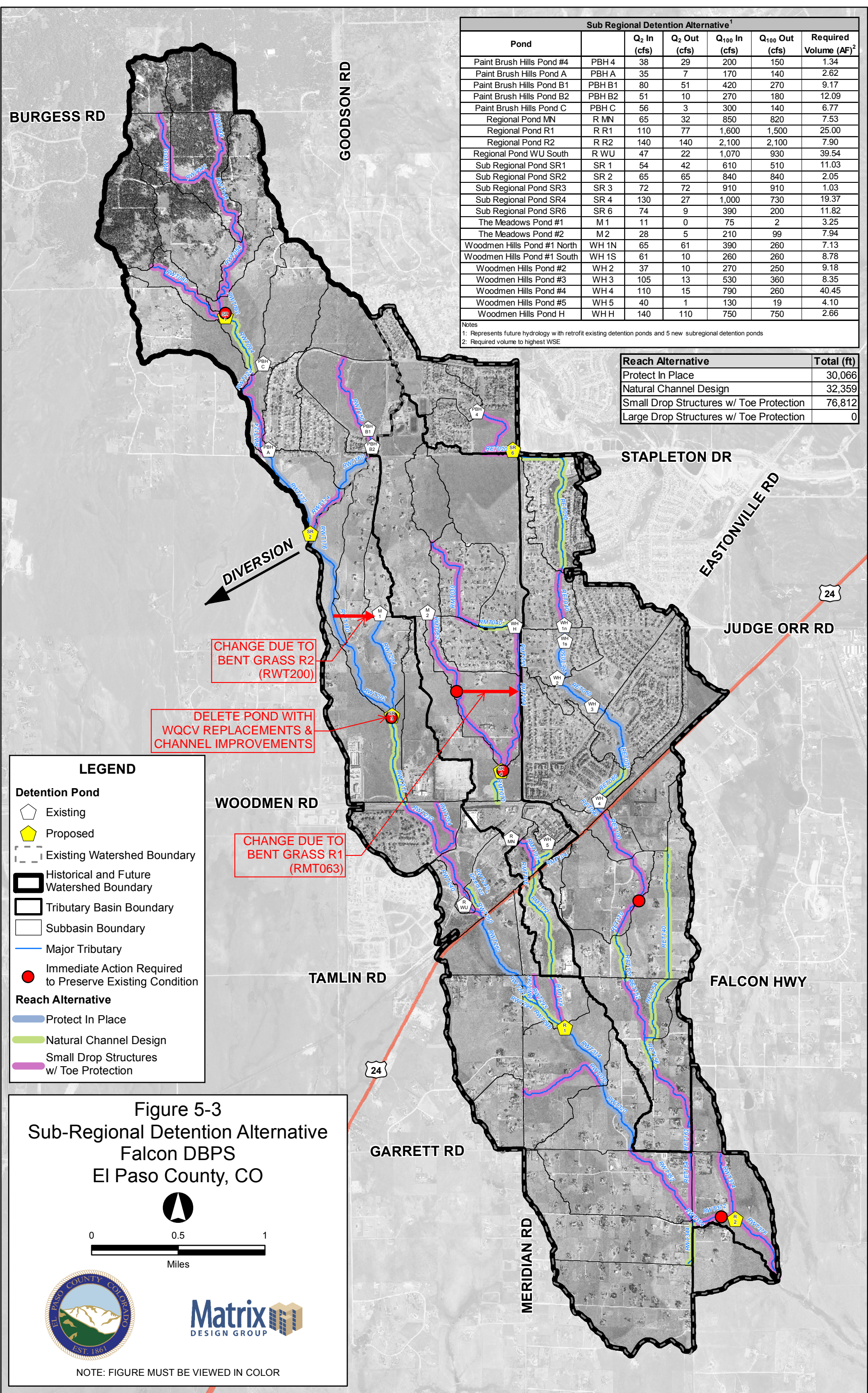
Basin EX-2 (1.56 AC, $Q_5 = 0.5$ cfs, $Q_{100} = 3.7$ cfs): is along the eastern boundary portion of the proposed site and is south of Basin EX-1, east of the existing channel. The basin is currently undeveloped and receives flows from Basins OS-4 & OS-5. Runoff from the basin generally flows to the southeast into Basin EX-3 at **DP 14** combined with flows from **DP 11 & 12**.

Basin EX-3 (0.62 AC, $Q_5 = 0.2$ cfs, $Q_{100} = 1.5$ cfs): is along the eastern boundary of the proposed site south of Basin EX-2 and east of the existing channel. The basin currently contains an existing WQCV pond created as part of Bent Grass Residential Filing No. 2. This basin receives flows from **DP 14** and **DP 8**.

Sub Regional Detention Alternative ¹						
Pond		Q ₂ In (cfs)	Q ₂ Out (cfs)	Q ₁₀₀ In (cfs)	Q ₁₀₀ Out (cfs)	Required Volume (AF) ²
Paint Brush Hills Pond #4	PBH 4	38	29	200	150	1.34
Paint Brush Hills Pond A	PBH A	35	7	170	140	2.62
Paint Brush Hills Pond B1	PBH B1	80	51	420	270	9.17
Paint Brush Hills Pond B2	PBH B2	51	10	270	180	12.09
Paint Brush Hills Pond C	PBH C	56	3	300	140	6.77
Regional Pond MN	R MN	65	32	850	820	7.53
Regional Pond R1	R R1	110	77	1,600	1,500	25.00
Regional Pond R2	R R2	140	140	2,100	2,100	7.90
Regional Pond WU South	R WU	47	22	1,070	930	39.54
Sub Regional Pond SR1	SR 1	54	42	610	510	11.03
Sub Regional Pond SR2	SR 2	65	65	840	840	2.05
Sub Regional Pond SR3	SR 3	72	72	910	910	1.03
Sub Regional Pond SR4	SR 4	130	27	1,000	730	19.37
Sub Regional Pond SR6	SR 6	74	9	390	200	11.82
The Meadows Pond #1	M 1	11	0	75	2	3.25
The Meadows Pond #2	M 2	28	5	210	99	7.94
Woodmen Hills Pond #1 North	WH 1N	65	61	390	260	7.13
Woodmen Hills Pond #1 South	WH 1S	61	10	260	260	8.78
Woodmen Hills Pond #2	WH 2	37	10	270	250	9.18
Woodmen Hills Pond #3	WH 3	105	13	530	360	8.35
Woodmen Hills Pond #4	WH 4	110	15	790	260	40.45
Woodmen Hills Pond #5	WH 5	40	1	130	19	4.10
Woodmen Hills Pond H	WH H	140	110	750	750	2.66

Notes
1: Represents future hydrology with retrofit existing detention ponds and 5 new subregional detention ponds
2: Required volume to highest WSE

Reach Alternative	Total (ft)
Protect In Place	30,066
Natural Channel Design	32,359
Small Drop Structures w/ Toe Protection	76,812
Large Drop Structures w/ Toe Protection	0



LEGEND

Detention Pond

- Existing (White pentagon)
- Proposed (Yellow pentagon)

Watershed Boundary

- Existing Watershed Boundary (Dashed line)
- Historical and Future Watershed Boundary (Thick black line)
- Tributary Basin Boundary (Thin black line)
- Subbasin Boundary (Thin grey line)

Major Tributary

- Major Tributary (Blue line)

Immediate Action Required to Preserve Existing Condition

- Immediate Action Required to Preserve Existing Condition (Red circle)

Reach Alternative

- Protect In Place (Blue line)
- Natural Channel Design (Green line)
- Small Drop Structures w/ Toe Protection (Purple line)

Figure 5-3
Sub-Regional Detention Alternative
Falcon DBPS
El Paso County, CO

0 0.5 1
Miles

NOTE: FIGURE MUST BE VIEWED IN COLOR

FILE: G:\gis_projects\Falcon_Creek_DBPStative\apps\20111215_alternatives\subregional_detention_alt.mxd, 12/19/2011, ron_ramold

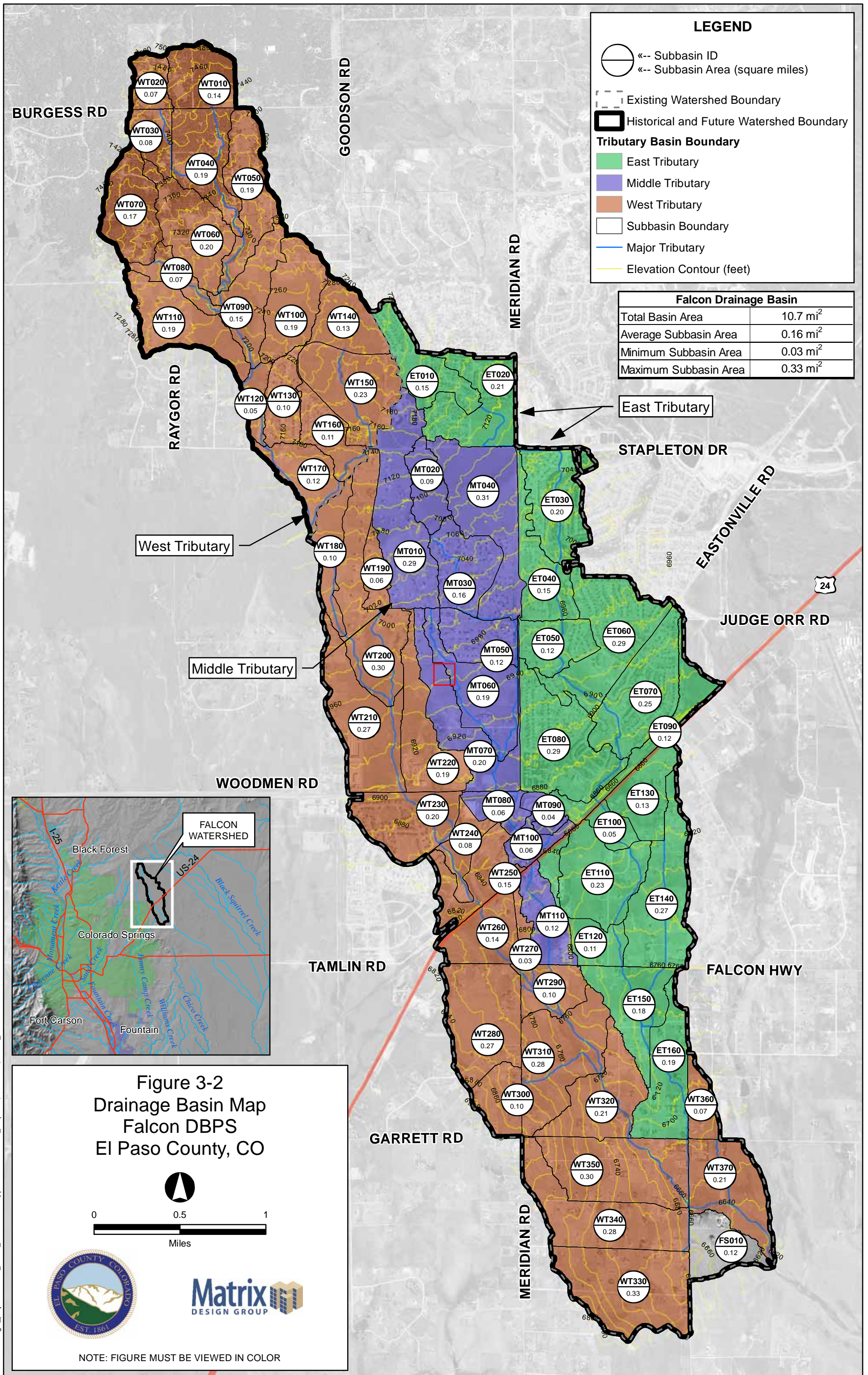
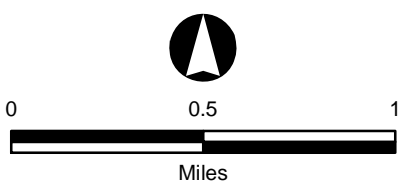


Figure 3-2
Drainage Basin Map
Falcon DBPS
El Paso County, CO



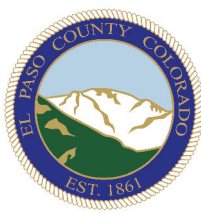
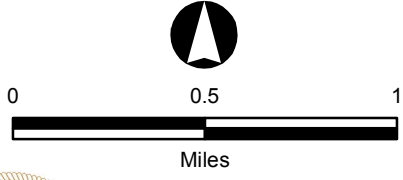
NOTE: FIGURE MUST BE VIEWED IN COLOR

LEGEND

- Subbasin ID
- 2-yr & 100-yr Flows (cfs)
- Detention Pond
- Junctions
- Existing Watershed Boundary
- Historical and Future Watershed Boundary
- Tributary Basin Boundary
- Subbasin Boundary
- Major Tributary

Hydrologic Element	Area (sq mi)	Future Peak Flows (cfs)		Hydrologic Element	Area (sq mi)	Future Peak Flows (cfs)	
		2-year	100-year			2-year	100-year
ET030	0.15	38	200	RET050	0.71	27	570
ET038	0.21	73	360	RET060	0.83	11	530
ET040	0.20	45	240	RET070	1.11	13	420
ET042	0.15	28	170	RET080	1.36	65	420
ET050	0.12	37	200	RET090	1.66	15	350
ET060	0.29	110	530	RET100	1.78	26	390
ET070	0.25	94	460	RET110	1.83	27	390
ET080	0.29	110	520	RET120	2.05	39	430
ET090	0.12	26	130	RET140	0.13	11	85
ET100	0.05	11	72	RET152	2.16	49	450
ET110	0.23	24	200	RET154	0.40	26	200
ET120	0.11	11	89	RET156	2.57	50	650
ET130	0.13	11	85	RET162	2.74	59	680
ET140	0.27	16	120	RET164	2.93	66	710
ET150	0.18	17	140	RMT030	0.09	25	140
ET160	0.19	19	140	RMT040	0.25	49	290
FS010	0.12	6	75	RMT050	0.56	110	750
JET010	0.15	29	150	RMT062	0.29	1	160
JET020	0.36	74	390	RMT064	0.67	120	850
JET030	0.56	97	580	RMT070	1.16	130	1,000
JET040	0.71	27	570	RMT080	1.36	150	1,200
JET050	0.83	11	520	RMT090	0.04	9	32
JET060	1.11	13	430	RMT102	1.42	86	1,200
JET070	1.36	94	480	RMT104	0.04	9	32
JET080	1.66	15	350	RMT106	1.46	91	1,200
JET090	1.78	26	390	RMT112	1.52	92	1,200
JET100	1.83	27	390	RMT114	1.64	94	1,200
JET110	2.05	40	460	RMT030	0.07	4	42
JET120	2.16	49	450	RMT042	0.14	9	85
JET130	0.13	11	85	RMT044	0.14	9	89
JET140	0.40	26	200	RMT046	0.28	15	170
JET152	2.57	51	650	RMT054	0.46	24	260
JET154	2.74	62	680	RMT080	0.17	14	130
JET160	2.93	66	710	RMT092	0.85	43	480
JFS010	0.12	6	75	RMT094	1.09	54	610
JMT010	0.29	1	160	RMT122	1.43	68	730
JMT020	0.09	26	140	RMT124	1.63	77	840
JMT030	0.25	50	290	RMT150	0.13	32	180
JMT040	0.56	110	750	RMT160	0.36	15	170
JMT050	0.67	120	850	RMT172	1.77	85	920
JMT060	1.16	130	1,000	RMT174	0.47	8	180
JMT070	1.36	150	1,200	RMT176	2.24	98	960
JMT080	1.42	86	1,200	RMT180	2.36	100	990
JMT090	0.04	9	32	RMT202	2.46	100	1,000
JMT102	1.46	91	1,200	RMT204	0.06	4	43
JMT104	0.04	9	32	RMT210	2.82	110	1,200
JMT106	1.52	92	1,200	RMT232	3.09	120	1,300
JMT110	1.64	94	1,200	RMT234	0.19	47	250
JMT120	0.14	9	89	RMT236	3.28	120	1,400
JMT130	0.07	4	42	RMT240	3.47	130	1,400
JMT140	0.14	9	85	RMT240	0.00	30	39
JMT150	0.28	15	170	Diversion	0.00	30	39
JMT160	0.46	24	260	RWT020	3.55	83	1,100
JMT170	0.85	43	480	RWT260	3.70	85	1,100
JMT180	0.17	14	130	RWT291	3.84	86	1,100
JMT190	1.09	54	610	RWT292	0.03	11	57
JMT200	1.43	68	730	RWT294	0.27	33	250
JMT210	1.63	77	840	RWT295	3.87	86	1,100
JMT220	1.77	85	920	RWT296	4.13	84	1,100
JMT230	0.13	32	180	RWT312	0.10	12	91
JMT240	0.36	15	170	RWT314	5.88	160	1,700
JMT250	0.47	35	190	RWT320	6.25	160	1,700
JMT260	2.24	99	960	RWT344	0.33	32	250
JMT270	2.36	100	990	RWT352	6.46	160	1,700
JMT280	2.46	100	1,000	RWT354	9.69	210	2,400
JMT290	0.06	4	43	RWT372	10.30	230	2,500
JMT300	2.82	110	1,200	RWT374	0.07	7	55
JMT310	3.09	120	1,300	RWT376	10.36	230	2,500
JMT320	0.19	47	250	M1	0.06	4	43
JMT330	3.28	120	1,400	M2	0.29	1	160
JMT340	3.47	130	1,400	WH1 North	0.71	28	570
JMT350	3.55	83	1,100	WH1 South	0.71	27	520
JMT360	3.70	85	1,100	WH2	0.83	11	530
JMT370	3.84	86	1,100	WH3	1.11	13	430
JMT380	0.03	11	57	WH4	1.66	15	350
JMT390	0.27	33	250	WH5	0.04	9	32
JMT400	3.87	86	1,100	WH6	0.56	110	750
JMT410	4.13	86	1,100	WT010	0.14	9	89
JMT420	5.88	160	1,700	WT020	0.07	4	42
JMT430	0.10	12	92	WT030	0.08	9	75
JMT440	6.25	160	1,700	WT040	0.19	9	93
JMT450	6.46	160	1,700	WT050	0.19	17	140
JMT460	0.33	32	250	WT060	0.20	14	120
JMT470	9.69	210	2,400	WT070	0.17	14	130
JMT480	10.30	230	2,500	WT080	0.07	9	67
JMT490	0.07	7	55	WT090	0.15	22	160
JMT500	10.36	230	2,500	WT100	0.19	56	300
JMT510	0.19	47	250	WT110	0.19	22	170
JMT520	10.58	230	2,500	WT120	0.05	8	55
OUTLET	0.29	28	210	WT130	0.10	35	170
MT020	0.09	26	140	WT140	0.13	32	180
MT030	0.16	39	230	WT150	0.23	49	250
MT040	0.31	95	460	WT160	0.11	35	180
MT050	0.12	17	110	WT170	0.12	21	140
MT060	0.19	30	200	WT180	0.10	8	66
MT070	0.20	25	170	WT190	0.06	11	75
MT080	0.06	62	190	WT200	0.30	25	190
MT090	0.04	40	130	WT210	0.27	32	190
MT100	0.06	17	88	WT220	0.19	47	250
MT110	0.12	19	120	WT230	0.20	71	350
PBH4	0.15	29	150	WT240	0.08	36	160
PBH1	0.10	10	130	WT250	0.15	63	290
PBH2	0.36	51	270	WT260	0.14	10	78
PBH3	0.36	51	270	WT270	0.03	11	57
PBHC	0.19	11	160	WT280	0.27	33	250
RMN	1.42	86	1,200	WT290	0.10	15	110
RWU				WT300	0.10	12	92
Diversion	3.55	83	1,100	WT310	0.28	31	250
RWU North	3.55	110	1,400	WT320	0.21	27	200
RWU South	3.55	55	1,000	WT330	0.33	32	250
RET020	0.15	29	150	WT340	0.28	19	150
RET030	0.36	71	380	WT350	0.30	38	280
RET040	0.56	95	580	WT360	0.07	7	55
				WT370	0.21	7	120

Figure 3-13
Future Hydrology
Falcon DBPS
El Paso County, CO

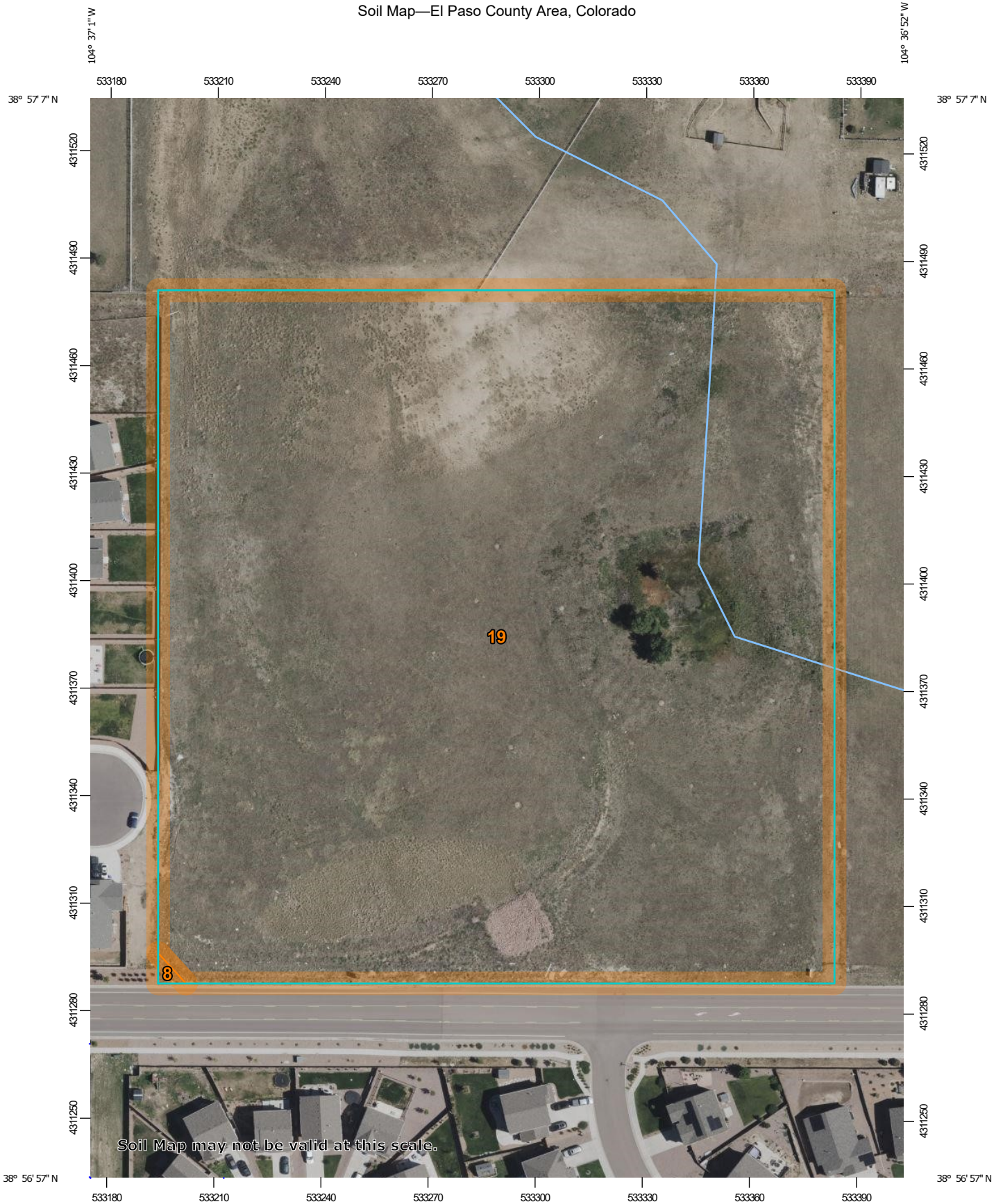


NOTE: FIGURE MUST BE VIEWED IN COLOR

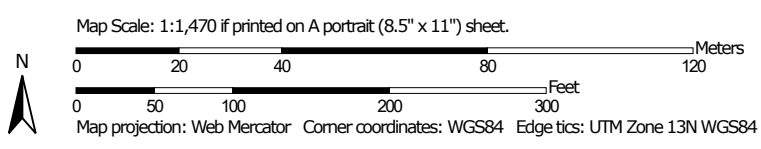
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APPENDIX G
SOILS REPORT

Soil Map—El Paso County Area, Colorado




Soil Map may not be valid at this scale.



MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 23, Aug 29, 2025

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 23, 2024—Aug 4, 2024

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	0.0	0.1%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	9.1	99.9%
Totals for Area of Interest		9.1	100.0%

El Paso County Area, Colorado

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p
Elevation: 6,500 to 7,300 feet
Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 50 degrees F
Frost-free period: 125 to 145 days
Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 97 percent
Minor components: 3 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Columbine

Setting

Landform: Fans, Fan terraces, Flood plains
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam
C - 14 to 60 inches: very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Ecological site: R049XY214CO - Gravelly Foothill
Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: 1 percent

Landform: Swales
Hydric soil rating: Yes

Other soils

Percent of map unit: 1 percent
Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent
Landform: Depressions
Hydric soil rating: Yes

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 23, Aug 29, 2025

APPENDIX H

GRADING AND STORM DRAINAGE PLANS