April 14, 2023

SR Land, LLC 20 Boulder Crescent, 1st Floor, Suite 100 Colorado Springs, Colorado 80903

Attn: Chaz Collins

Re: Pavement Recommendations Homestead North at Sterling Ranch – Filing No. 1 El Paso County, Colorado Entech Job No. 222146

Dear Mr. Collins:

As requested, Entech Engineering, Inc. has obtained samples of the pavement subgrade soils from the roads in the Homestead North at Sterling Ranch Filing No. 1 Subdivision. This letter presents the results of the laboratory testing and pavement recommendations for the roadway sections within the filing.

Project Description

The roadways for this project consist of sections of Wheatland Drive, Nat Love Drive, Texas Jack Drive, along with Tom Ketchum Drive including the cul-de-sac, Jack Helm Drive, Harvey Logan Drive, and Jane Kirkham Drive located northeast of Colorado Springs, in the northern portion of El Paso County, Colorado. Subsurface Soil Investigation and laboratory testing were performed in order to determine the pavement support characteristics of the soils. The approximate locations of the test borings are presented on the Test Boring Location Plan, Figure No 1.

Subgrade Conditions

Eighteen test borings were drilled along the roadways to depths of approximately 5 and 10 feet below the existing subgrade surface at he required intervals. The soils in the test borings consisted of clayey sand fill and slightly silty to silty sand fill (Soil Type 1), native silty to clayey sand (Soil Type 2), native sandy clay (Soil Type 3) silty to slightly silty to clayey sandstone (Soil Type 4), and very sandy to sandy claystone to very clayey sandstone (Soil Type 5).

The pavement designs will be based on 2 soil types, Soil Type A and Soil Type B. The type 1, 2, and 4 soils will be grouped together as Soil Type A and the type 3 and 5 soils will be grouped together as Soil Type B due to similar characteristics. The Test Boring Logs are presented in Appendix A. Sieve Analyses and Atterberg Limit testing were performed on the subgrade soil samples obtained from the test borings for the purpose of classification. The percent passing the No. 200 sieve for the Type A soils is approximately 9 to 36 percent. The Type A subgrade soils generally classify as A-1-b, A-2-4, A-2-6 and A-4 soils. The Type B soils generally classify as A-4 to A-6 soils which typically provide poorer pavement support characteristics using the AASHTO classification system. Mitigation of the Type B soils will be required. Groundwater was not encountered in the test borings. Water soluble sulfate tests results indicated that the soils exhibit a negligible potential for sulfate attack.

EPC PROJECT No. SF-2213





505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238



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Atterberg Limits Testing on samples of all types of the soils taken from the test borings resulted in Liquid Limits of No-Value to 37 percent and Plastic Indexes of Non-Plastic to 19 percent. Swell/Consolidation Testing on random samples from all soil types resulted in volume changes from 0.2 to 1.6 percent and consolidations of 0.2 to 0.5 percent. These results indicate a low consolation potential and a low to moderate expansion potential. Test results indicate that mitigation due to expansive soils is not required on this site. Laboratory test results are presented in Appendix B and are summarized in Table 1.

California Bearing Ratio (CBR) testing was performed on representative samples of Soil Type 1 and Soil Type 2 to determine the support characteristics of the subgrade soils for the roadway sections. The results of the CBR testing, are presented in Appendix B and summarized as follows:

Soil Type A – Clayey Sand Fill	<u>Soil Type B – Very Clayey</u>
	Sandstone
R @ 90% = 60.0	R @ 90% = 1
R @ 95% = 74.0	R @ 95% = 14
Use $R = 50.0$ for design	Use $R = 14.0$ for design
-	

Cla	assificati	on Testing	
Soil Type A		Soil Type B	
Liquid Limit	28	Liquid Limit	29
Plasticity Index	13	Plasticity Index	11
Percent Passing 200	25.8	Percent Passing 200	39.2
AASHTO Classification	A-2-6	AASHTO Classification	A-6
Group Index	0	Group Index	1
Unified Soils Classification	SC	Unified Soils Classification	SC

Pavement Design

CBR testing was used to determine pavement sections for the roadways. Pavement sections were determined utilizing the El Paso County Pavement Design Criteria Manual. The cul-de-sac section on Tom Ketchum Drive classifies as an urban local (low volume) roadway, which will use an 18k ESAL value of 36,500 for design. The remaining roadways classify as urban local roads, which will use an 18k ESAL value of 292,000 for design purposes. Alternative pavement sections were determined for asphalt supported by aggregate basecourse, and asphalt supported by recycled concrete. County approval is required if recycled concrete is to be utilized. Additional laboratory testing for the recycled concrete is in process.

SR Land, LLC Pavement Recommendations Homestead North at Sterling Ranch – Filing No. 1 El Paso County, Colorado Entech Job No. 222146 Page 3

Design parameters used in the pavement analysis for the roadways are as follows:

Serviceability Index 2.0 2.0%	
Standard Deviation 0.44	
"R" Value Subgrade	
Soil Type A 50.0	
Soil Type B* 14.0*	
Resilient Modulus	
Soil Type A 13,168 p	si
Soil Type B* 4,060 p	si
Δpsi 2.0	
Structural Coefficients	
Hot Bituminous Pavement 0.44	
Aggregate Basecourse 0.11	
Recycled Concrete 0.11	

*The Type B soils, where encountered will require removal up to 18 inches of the Type B Soils and replacement with on-site Type A Soils.

The pavement design calculations are presented in Appendix C. Pavement section alternatives for the roadway sections are presented below. Any additional grading may result in subgrade soils with different support characteristics. The following pavement sections should be re-evaluated if additional grading is performed.

Soil Type A Pavement Sections ESAL = 36,500 – Urban Local (Low Volume)

Alternative	<u>Asphalt (in)</u>	Basecourse (in)	Recycled Concrete (in)
1. Asphalt Over Basecourse	3.0*	6.0*	-
2. Asphalt Over Recycled Concrete	3.0*	-	6.0*
	<u>Type A Paveme</u> L = 292,000 – L		
Alternative	<u>Asphalt (in</u>)	Basecourse (in)	Recycled Concrete (in)
1. Asphalt Over Basecourse	3.0*	8.0*	-
2. Asphalt Over Recycled Concrete	3.0*	-	8.0*

*Minimum sections required per El Paso County Pavement Design Criteria Manual. -Full Depth Asphalt is not aboved in unincorporated El Paso County.

Mitigation

El Paso County requires mitigation of expansive soils that have a swell of 2 percent or greater with a 150 pound per square foot surcharge. Based on the swell testing, the soils at subgrade depth do not require mitigation for expansion potential.

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The Type B soils consisted of expansive clays, which would require thicker asphalt sections. In the areas with Type B soils, it is recommended that 18 inches of the Type B soils be removed and replaced with Type A soils. The thinner Soil Type A sections can then be used. The approximate extents of the Type B soils are shown in Figure No. 1. The approximate locations for mitigation will be field determined.

Roadway Construction – Asphalt on Aggregate Basecourse or Recycled Concrete Alternatives

Prior to placement of the asphalt, the subgrade should be mitigated as required and compacted to a minimum of 95 percent of the soils maximum Modified Proctor Dry Density, ASTM D-1557 at ± 2 percent of optimum moisture content or to 95% of the soils maximum Standard Proctor Dry Density ASTM D-698 at 0 to 4 percent over optimum moisture content, and proofrolled. Any loose areas should be removed and replaced with suitable materials. Basecourse materials should be compacted to a minimum of 95 percent of its maximum Modified Proctor Dry Density, at ± 2 percent of optimum moisture content. Special attention should be given to areas adjacent to manholes, inlet structures and valves.

Based on the soils encountered, subgrade soil problem areas, if any, will be identified at proof roll. We do not anticipate issues with the subgrade in regards to shallow water, frost susceptible soils, groundwater or drainage conditions, soluble sulfates, or cold weather construction.

In addition to the above guidance, the asphalt, basecourse, recycled concrete, subgrade conditions, compaction of materials and roadway construction methods shall meet El Paso County pavement design specifications.

We trust that this report contains the information you require. If you have questions or need additional information, please contact us.

Respectfully Submitted,

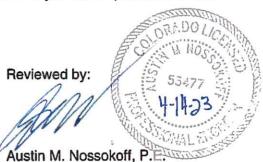
ENTECH ENGINEERING, INC.

Daniel P. Stegman

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Encl.

Entech Job No. 222146 AAprojects/2022/222146 pr



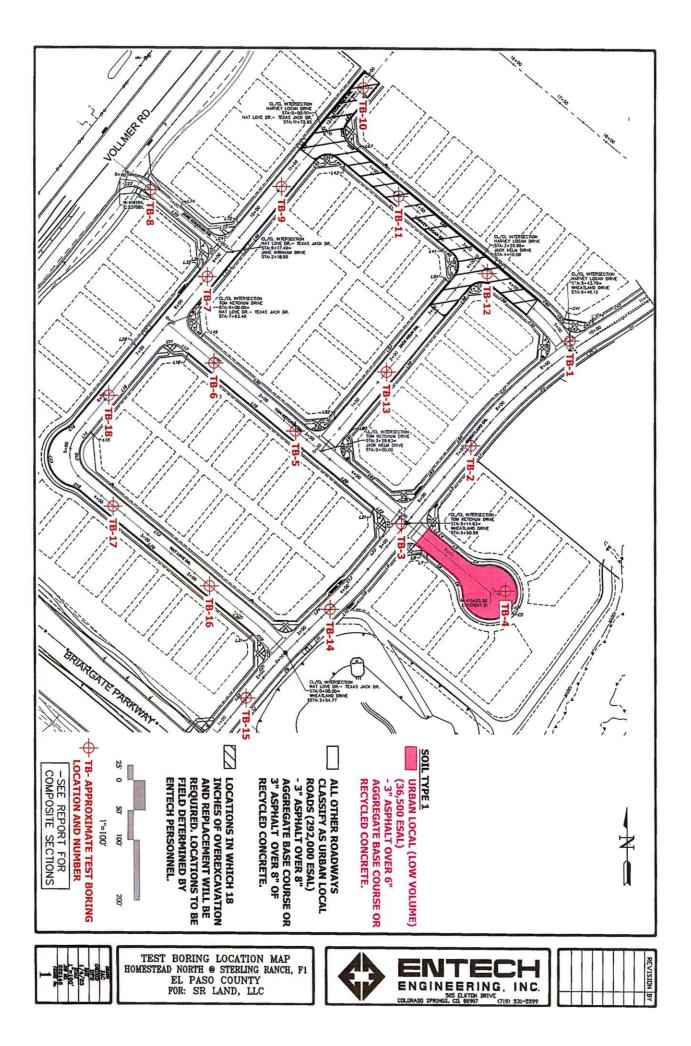
EPC PROJECT No. SF-2213

TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

<u>CLIENT</u> SR LAND, LLC <u>PROJECT</u> STERLING RANCH, F-1 JOB NO. 222146

	T	r-	_		-	<u> </u>	_	1	_	_	_	-	_	1	-	-	_		_	-	-		_	_		1		-		.	<u> </u>	
SOIL DESCRIPTION	FILL, SAND, CLAVEY	FILL, SAND, CLAYEY	FILL, SAND, CLAYEY	FILL, SAND, CLAYEY	FILL, SAND, CLAYEY	FILL, SAND, SILTY	FILL, SAND, SIL'TY	FILL, SAND, SILTY	FILL, SAND, SLIGHTLY SILTY	FILL, SAND, CLAYEY	FILL, SAND, CLAYEY	FILL, SAND, SILTY	SAND, SILTY	SAND, SILTY	SAND, SILTY	SAND, CLAYEY	SAND, SILTY	SAND, SILTY	CLAY, SANDY	SANDSTONE, CLAYEY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, SLIGHTLY SILTY	SANDSTONE, CLAYEY	SANDSTONE, SILTY	SANDSTONE, SILTY	SANDSTONE, VERY CLAYEY	CLAYSTONE, VERY SANDY	SANDSTONE, VERY CLAYEY	CLAYSTONE, SANDY	SANDSTONE, VERY CLAYEY
UNIFIED CLASSIFICATION	sc	ပ္ပ	ပ္တ	sc	sc	SM	SM	SM	SM-S-WS	SC	sc	SM	SM	SM	SM	SC	SM	SM	ซ	SC	SC	SM	SM	SM-SW	SC	SM	SM	sc	ซ	SC	ы	SC
(%) CONSOL SWELL	0.5	0.2	0.3							0 .2	0.2					-0.5			1.6	0.3					0.7					0.3	1.1	6.0
AASHTO CLASS.	A-2-6	A-2-6	A-2-6	A-4	A-4	A-2-4	A-2-4	A-1-b	A-1-b	A-2-6	A-2-6		A-2-4	A-2-4	A-1-b	A-2-4			A-6	A-2-6	A-2-4	A-1-b	A-1-b	A-1-b	A-6	A-1-b		A-6	A-4	A-6	A-6	A-6
SULFATE (WT %)		<0.01			0.00	<0.01										<0.01							0.0									
PLASTIC INDEX (%)	13	15	12	10	10	NP	NP	NP	NP	11	18		NP	NP	NP	6			19	11	10	đ	đ	ď	12	٩N		11	9	13	13	13
LIQUID LIMIT %)	28	35	8	32	29	Ň	Ŵ	Š	ş	27	34		N	N	N	29			37	58	29	Š	Š	≩	ß	Ş		88	26	g	31	31
PASSING NO. 200 SIEVE (%)	25.8	25.4	34.8	33.7	30.0	18.6	19.4	18.8	9.1	15.0	34.2	21.2	16.0	15.3	16.8	29.2	21.7	28.8	64.4	28.2	21.4	13.3	12.4	11.3	35.5	12.3	18.5	39.2	51.2	46.9	73.0	43.3
DRY DENSITY (PCF)	112.7	113.1	113.3							119.1	117.0					103.4			111.2	116.7					117.6					119.5	109.3	111.5
WATER (%)	13.1	11.1	12.5							9.9	10.3					7.0			13.3	9.8					10.1				i	9.5	15.4	14.0
DEPTH (FT)	z	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	1-2	0-3	1-2	1-2	1-2	5	ş	53	1-2	1-2	1-2	1-2	2	₽	10	ß	13	?	1-2	10	9	5
TEST BORING NO.	6	1	2	3	4	7	8	14	15	16	17	15	5	8	8	8	9	6	10	11	13	18	5	6	15	16	18	12	12	8	9	10
SOIL	1, CBR	-	-	1	+	1		, 1	1	+	+	1	8	2	2	2	2	2	0	4	4	4	4	4	4	4	4	5, CBR #2	5	5	ß	5



APPENDIX A: Test Boring Logs

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TEST BORING NO. 1 DATE DRILLED 11/16/202 Job # 222146	22				TEST BORING NO. DATE DRILLED CLIENT LOCATION	2 11/16/20 SR LANI STERLIN	22), LL(C ANCH	<u>1, F</u>	-1		
REMARKS DRY TO 5', 11/16/22 FILL 0-5', SAND, CLAYEY, FINE TO MEDIUM GRAINED, BROWN, MEDIUM DENSE, MOIST			11.8 Watercontent %	1	REMARKS	EY, FINE), BROWN,	(t) the dec		Samples	G Blows per foot	1.2 Natercontent %	1 1 Soil Type
ENTECH ENGINEERING, 505 ELKTON DRIVE COLORADO SPRINGS, COL	INC. Orado 6	10907	DRAW	ſN:		DRING LO		TE: -23-2	22)	22	BNO.: 2146 INO.: A- 1

DATE DRILLED 11/16/20 Job # 222146							TEST BORING NO. DATE DRILLED CLIENT LOCATION	4 11/16/202 SR LAND STERLIN	22), LLC		1, F-	·1		
REMARKS DRY TO 10', 11/16/22	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type	REMARKS DRY TO 5', 11/16/22		Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
FILL 0-4', SAND, CLAYEY, FINE TO MEDIUM GRAINED, BROWN, MEDIUM DENSE, MOIST SANDSTONE, VERY CLAYEY, FINE TO MEDIUM GRAINED, GRAY BROWN, VERY DENSE, MOIST	5 10 15 20			35	11.2		FILL 0-5', SAND, CLAY TO MEDIUM GRAINED DENSE TO MEDIUM DI	, BROWN, ENSE, DRY				29	2.2	

TEST BORING NO. 5 DATE DRILLED 11/16/20 Job # 222146	22		i		1	1	LOCATION STER	6 2022 ND, LL _ING R		- <u>1, F</u>	-1		
REMARKS DRY TO 5', 11/16/22	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type	REMARKS DRY TO 10', 11/16/22	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
SAND, SILTY, FINE TO COARSE GRAINED, TAN, DENSE, MOIST SANDSTONE, SILTY, FINE TO COARSE GRAINED, TAN, VERY DENSE, MOIST	5			45 <u>50</u> 7"	4.1 10.7		SAND, SILTY, FINE TO COARS GRAINED, TAN, MEDIUM DEN DRY TO MOIST CLAYSTONE, SANDY, GRAY				24	2.5 14.4	2
	10 - - - 15 -						BROWN, HARD, MOIST	10 15			<u>50</u> 7"	14.8	5
	13 - - 20 -							20					
	- •		- •						-	-	- •		

TEST BORING NO. 7 DATE DRILLED 11/16/202 Job # 222146 REMARKS	22	-	[1	TEST BORING NO. DATE DRILLED CLIENT LOCATION REMARKS	8 11/16/20 SR LAND STERLIN	22), LL(<u>I, F</u>	-1		
DRY TO 5', 11/16/22	Depth (ft) Symbol	Samples	Blows per foot	Watercontent %	Soil Type	DRY TO 5', 11/16/22		Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
FILL 0-5', SAND, SILTY FINE TO MEDIUM COARSE, TAN, MEDIUM DENSE TO DENSE, DRY TO MOIST			24	2.2	1	FILL 0-3', SAND, SILTY, COARSE GRAINED, TA DENSE, DRY SAND, CLAYEY, FINE MEDIUM GRAINED, GR DENSE, MOIST	IN, MEDIUM TO IAY BROW				29	1.9 18.2	1
	<u> </u>					TEST BO	RING LOG				$\overline{)}$	22	08 NO. 2146 16 NO.

TEST BORING NO. 9 DATE DRILLED 11/17/20 Job # 222146	22		TEST BORING NO. DATE DRILLED CLIENT LOCATION	10 11/17/2022 SR LAND, LI STERLING 8	LC RANCH, F-1	
REMARKS DRY TO 10', 11/17/22 SAND, SILTY, FINE TO COARSE GRAINED, TAN, DENSE, DRY SANDSTONE, SLIGHTLY SILTY, FINE TO COARSE GRAINED, TAN, VERY DENSE, MOIST	(1) 10 10 10 10 10 10 10 10 10 10	9 1.6 2 0 9.8 4	LOCATION REMARKS DRY TO 5', 11/17/22 CLAY, SANDY, TAN, V MOIST SANDSTONE, VERY FINE GRAINED, BROW DENSE, MOIST	ERY STIFF, CLAYEY,	6 55 Blows per foot	2 15.2 3 2 10.5 5
ENTECH ENGINEERING, 505 ELKTON DRIVE COLORADO SPRINGS, COL		DRAWN:		DRING LOG	DATE: 7-23-22-	JOB NO.: 222146 FIG NO.: A-

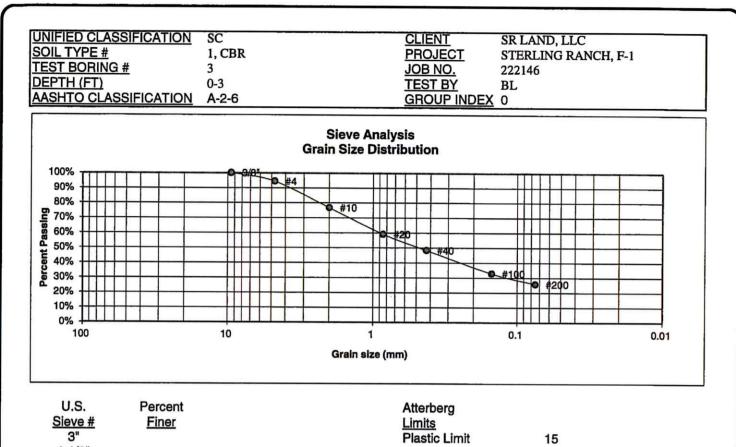
TEST BORING NO. 11 DATE DRILLED 11/17/202 Job # 222146 REMARKS	22	T	TEST BORING NO. DATE DRILLED CLIENT LOCATION	12 11/17/2022 SR LAND, LLC STERLING RANC	<u>Ж, F-1</u>
DRY TO 5', 11/17/22 SAND, SILTY, TAN SANDSTONE, CLAYEY, FINE TO MEDIUM GRAINED, BROWN, VERY DENSE, MOIST	(t) http://www.second	50 9.2 10"	REMARKS		Samples Samples 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6
ENTECH ENGINEERING, I 505 ELKTON DRIVE COLORADO SPRINGS, COL		DRAWN:			-25

REMARKS	r 1	T	LOCATION	STERLING	LC RANCH	l, F-1	r	
DRY TO 5', 11/17/22 SAND, SILTY, TAN SANDSTONE, CLAYEY, FINI MEDIUM GRAINED, BROWN, VERY DENSE, MOIST	2. 100 Blows per foot 2. 2. Watercontent %	2	REMARKS DRY TO 5', 11/17/22 FILL 0-5', SAND, SILTY TO MEDIUM COARSE, MEDIUM DENSE, MOIS	TAN,		12 Blows per foot	% Matercontent % 3.6	L L Soil Type
			TEST BO	DRING LOG				¹²¹ 46 ^{⊨1} 8 [№] 1

TEST BORING NO. 15 DATE DRILLED 11/17/202 Job # 222146 REMARKS 1	22			TEST BORING NO. DATE DRILLED CLIENT LOCATION REMARKS	16 11/17/202 SR LAND STERLIN	22), LLC	<u>), F</u>	-1 [1		
DRY TO 10', 11/17/22	Depth (ft) Symbol Samples	Blows per foot	Watercontent % Soil Type	DRY TO 5', 11/17/22		Depth (ft) Symbol	Samples	Blows per foot	Watercontent %	Soli Type
FILL 0-9', SAND, SILTY, FINE TO COARSE GRAINED, TAN, MEDIUM DENSE, MOIST TO DRY				FILL 0-3', SAND, CLAY TO MEDIUM GRAINED MEDIUM DENSE, MOIS SANDSTONE, SILTY,	, TAN, ST				5.9	1
	5	29 7	.4 1	COARSE GRAINED, TA DENSE, MOIST		5		<u>50</u> 6"	8.6	4
SANDSTONE, CLAYEY, FINE TO MEDIUM GRAINED, TAN, VERY DENSE, MOIST	10 <u>: : : :</u>	<u>50</u> 13 11"	3.7 4			10				
	15					- 15 -				
	20_					20				
I	1 1 1	1	I	I	1	I	1	ı t	I	
				TEST BC	RING LO	3				ов NO.: 2146
ENTECH ENGINEERING, IN										

TEST BORING NO. 17 DATE DRILLED 11/17/20 Job # 222146 REMARKS 11/17/20	22		TEST BORING NO. DATE DRILLED CLIENT LOCATION REMARKS	18 11/17/2022 SR LAND, LI STERLING F		
DRY TO 5', 11/17/22 FILL 0-5', SAND, CLAYEY, FINE TO MEDIUM GRAINED, BROWN, MEDIUM DENSE, MOIST	20 10 10 10 10 10 10 10 10 10 1	8.1 1	DRY TO 5', 11/17/22 SAND, SILTY, TAN SANDSTONE, SILTY, COARSE GRAINED, BF VERY DENSE, MOIST		11. 50 11. 51. 51. 61 61	2 7.2 4
ENTECH ENGINEERING, I 505 ELKTON DRIVE COLORADO SPRINGS, COL	INC.	DRAWN:	TEST BO	RING LOG	DATE:	JOB NO.: 222146 FIG NO.:

APPENDIX B: Laboratory Test Results

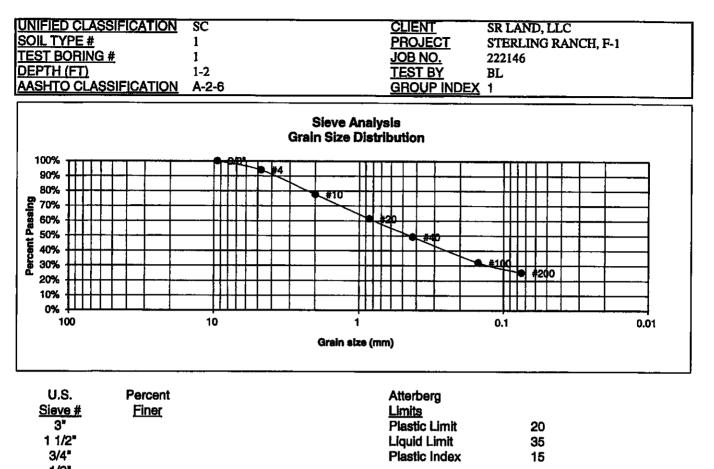


1 1/2"		Liquid Limit 28
3/4"		Plastic Index 13
1/2"		
3/8"	100.0%	
4	94.5%	Swell
10	76.7%	Moisture at start
20	59.1%	Moisture at finish
40	48.3%	Moisture increase
100	32.8%	Initial dry density (pcf)
200	25.8%	Swell (psf)

\mathbf{O}	ENTECH ENGINEERING, INC.		LABOR	ATORY TEST
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED:

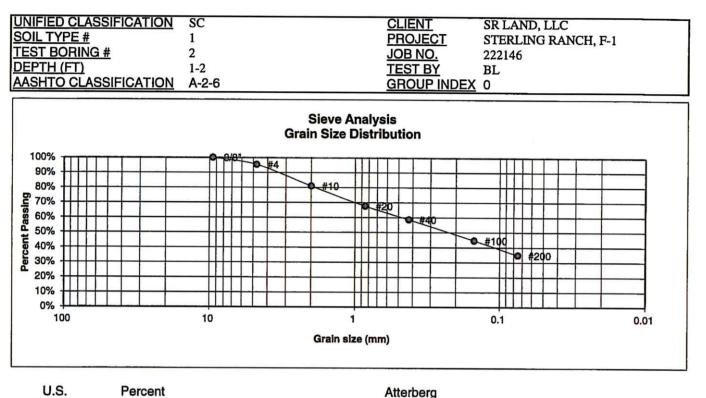
JOB NO.: 222146 FIG NO.: B-1

12-23-22



1/2"		
3/8"	100.0%	
4	94.0%	<u>Swell</u>
10	77.7%	Moisture at start
20	61.3%	Moisture at finish
40	49.3%	Moisture increase
100	32.0%	Initial dry density (pcf)
200	25.4%	Swell (psf)

6	ENTECH ENGINEERING, INC.		LABOF RESUL	ATORY TEST		JOB NO.: 222146 FIG NO.:
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED:	12-23-22	B-2



U.S.	Percent	Atterberg	
Sieve #	<u>Finer</u>	Limits	
3"		Plastic Limit 20	
1 1/2"		Liquid Limit 32	
3/4"		Plastic Index 12	
1/2"			
3/8"	100.0%		
4	95.4%	Swell	
10	81.0%	Moisture at start	
20	67.5%	Moisture at finish	
40	58.7%	Moisture increase	
100	44.6%	Initial dry density (pcf)	
200	34.8%	Swell (psf)	

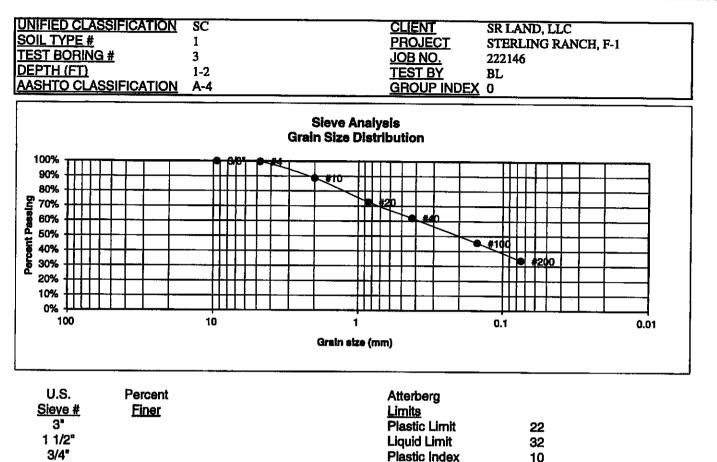
DRAWN:

	ENTECH
27	ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

LABOF RESUL	ATORY TEST	
DATE:		12-23-22

JOB NO.: 222146

FIG NO.:

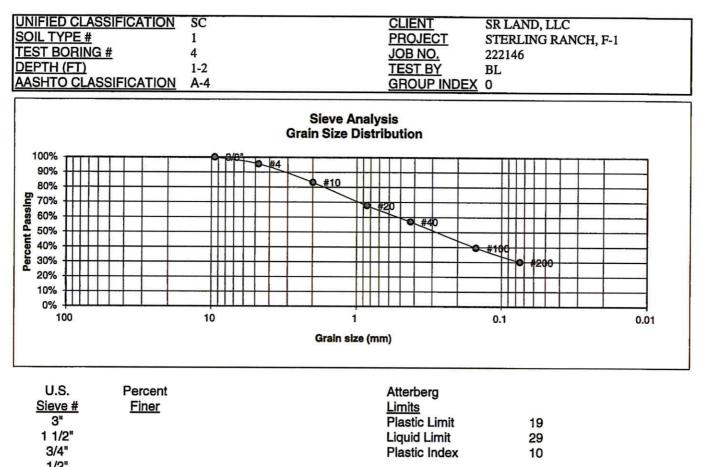


1/2"		
3/8"	100.0%	
4	99.6%	Swell
10	88.7%	Moisture at start
20	72.6%	Moisture at finish
40	62.0%	Molsture increase
100	45.4%	initial dry density (pcf)
200	33.7%	Swell (psf)

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\diamond	ENTECH ENGINEERING, INC. 505 ELKTON DRIVE
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, ,) (JOB NO.:			
	RESUL	TS			222146 FIG NO.:
DRAWN:	DATE:	CHECKED:	12-23-22		B-4

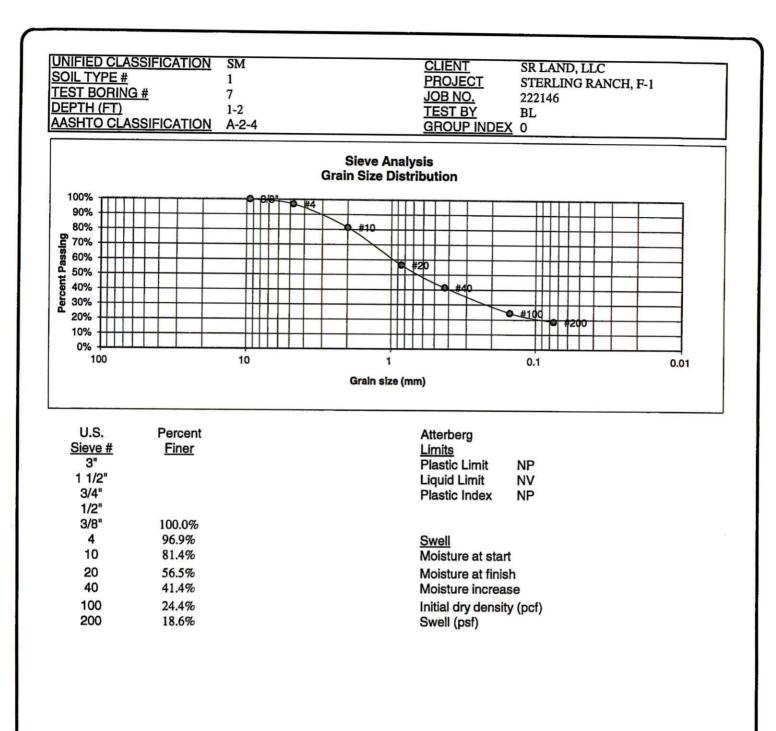


1/2"		
3/8"	100.0%	
4	95.5%	Swell
10	83.2%	Moisture at start
20	67.6%	Moisture at finish
40	57.0%	Moisture increase
100	39.5%	Initial dry density (pcf)
200	30.0%	Swell (psf)

	ENTECH
27	ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

		LABORATORY TEST RESULTS			
J	DRAWN:	DATE:	CHECKED: SW	12-23-22	

JOB NO .:
222146
FIG NO .:
10-5



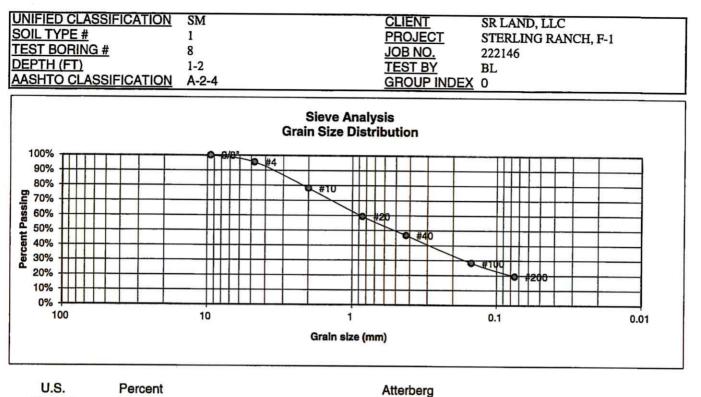
	ENTECH
27	ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

LABOF RESUL	ATORY TEST	
DATE:	CHECKED: SW	DATE: 12-23-22

DRAWN:

JOB NO .:

222146 FIG NO.: B-C



Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
100.0%	
95.4%	Swell
78.1%	Moisture at start
59.3%	Moisture at finish
46.8%	Moisture increase
28.3%	Initial dry density (pcf)
19.4%	Swell (psf)
	Finer 100.0% 95.4% 78.1% 59.3% 46.8% 28.3%

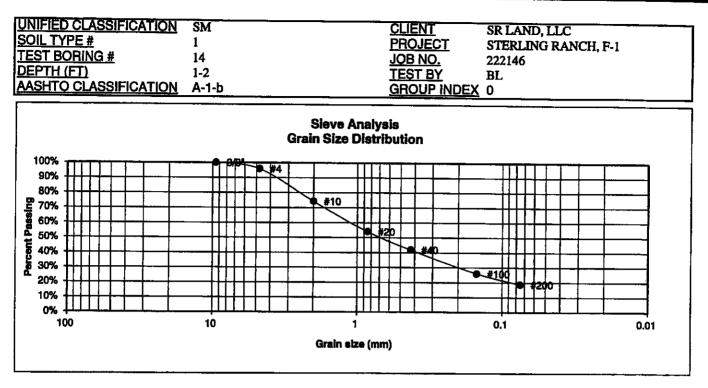
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ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

4

	JOB NO .:			
	222146			
DRAWN:	DATE:	CHECKED:	12-23-22	B-7

7



U.S. <u>Sieve #</u> 3"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP	
1 1/2" 3/4" 1/2"		Liquid Limit NV Plastic Index NP	
3/8"	100.0%		
4	95.9%	<u>Swell</u>	
10	74.2%	Moisture at start	
20	54.0%	Moisture at finish	
40	41.9%	Moisture increase	
100	25.9%	Initial dry density (pcf)	
200	18.8%	Swell (psf)	

ENTECH ENGINEERING, INC.
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

LABOF RESUL	ATORY TEST	
DATE:	CHECKED:	D

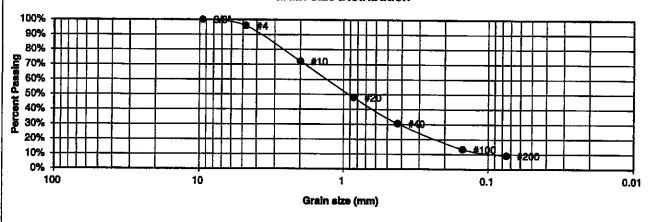
JOB	NO,
222	146

FIGNO .: D-8

DRAWN:

HECKED: SW L2-23-22

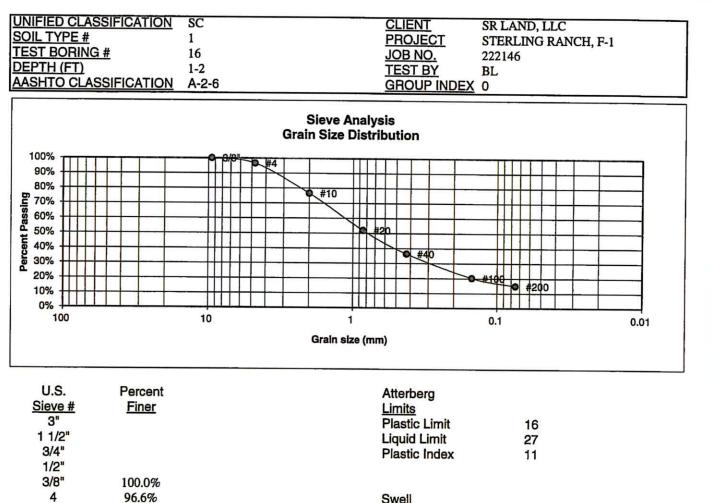
SOIL TYPE # TEST BORING # DEPTH (FT) AASHTO CLASSIEICATION	1 15 1-2	PROJECT JOB NO. TEST BY	STERLING RANCH, F-1 222146 BL		
AASHTO CLASSIFICATION A-1-b GROUP INDEX 0 Sieve Analysis Grain Size Distribution					



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	95.9%	Swell
10	72.1%	Moisture at start
20	47.9%	Moisture at finish
40	30.6%	Moisture increase
100	13.4%	Initial dry density (pcf)
200	9.1%	Swell (psf)

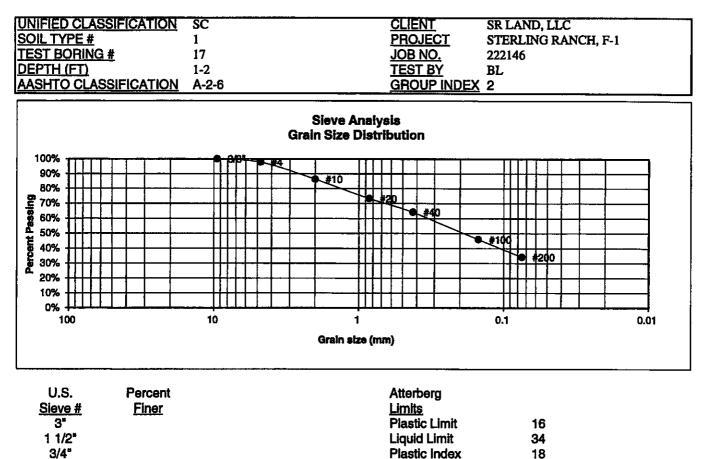
$\mathbf{\Theta}$	ENTECH ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

(JOB NO.:			
	RESUL	_TS		222146 FIG.NO.;
DRAWN:	DATE:	HECKED: SW	12-23-22	6-9



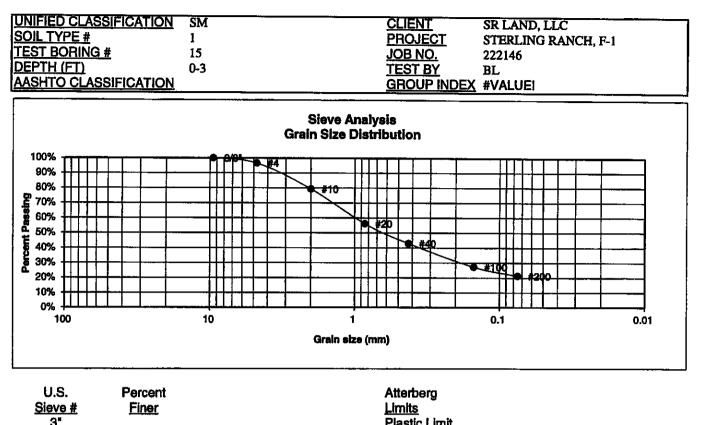
4	96.6%	Swell
10	76.6%	Moisture at start
20	52.0%	Moisture at finish
40	36.4%	Moisture increase
100	20.2%	Initial dry density (pcf)
200	15.0%	Swell (psf)

ENTECH ENGINEERING, INC.	LABORATORY TEST RESULTS			JOB NO.: 222146 FIG NO :	
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED: SW	12-23-22	A-10



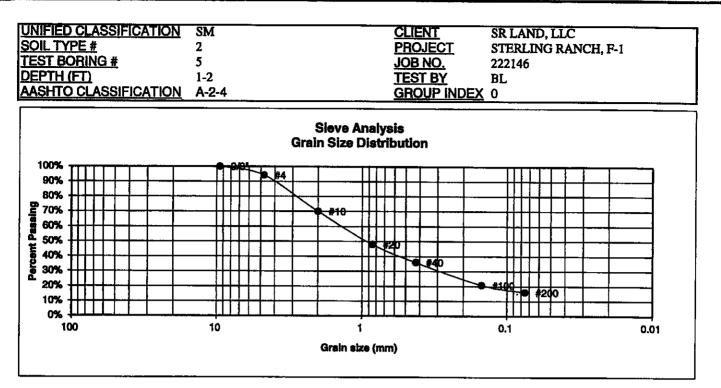
3/4"		Plastic Index
1/2*		
3/8*	100.0%	
4	97.8%	<u>Swell</u>
10	86.3%	Moisture at start
20	73.3%	Moisture at finish
40	64.2%	Moisture increase
100	46.0%	Initial dry density (pcf)
200	34.2%	Swell (psf)

>	ENTECH ENGINEERING, INC.	LABORATORY TEST RESULTS			JOB NO.: 222146 Fig No.:	
505 ELKT	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 50907	DRAWN:	DATE:		12-22-22	B-11



3"		Plastic Limit
1 1/2"		Liquid Limit
3/4"		Plastic Index
1/2"		
3/8"	100.0%	
4	96.6%	<u>Swell</u>
10	79.3%	Moisture at start
20	56.1%	Moisture at finish
40	43.0%	Moisture increase
100	27.3%	Initial dry density (pcf)
200	21.2%	Swell (psf)

\Diamond	ENTECH ENGINEERING, INC.	LABORATORY TEST RESULTS				JOB NO.: 222146 FIG NO.:
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED: SW	12-23-22	B-12



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	94.2 %	Swell
10	70.0%	Moisture at start
20	47.9%	Moisture at finish
40	36.0%	Moisture increase
100	20.7%	Initial dry density (pcf)
200	16. 0%	Swell (psf)

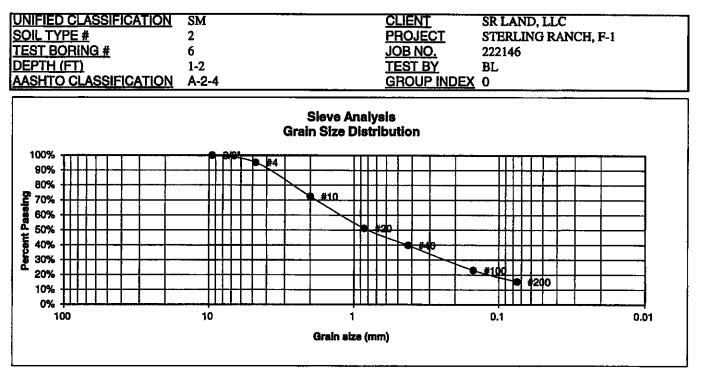
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ENTECH

ENGINEERING, INC.

505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

		JOB NO.:		
	RESU	LTS		222146 FIG NO.:
DRAWN:	DATE:		12-23-22	B-13

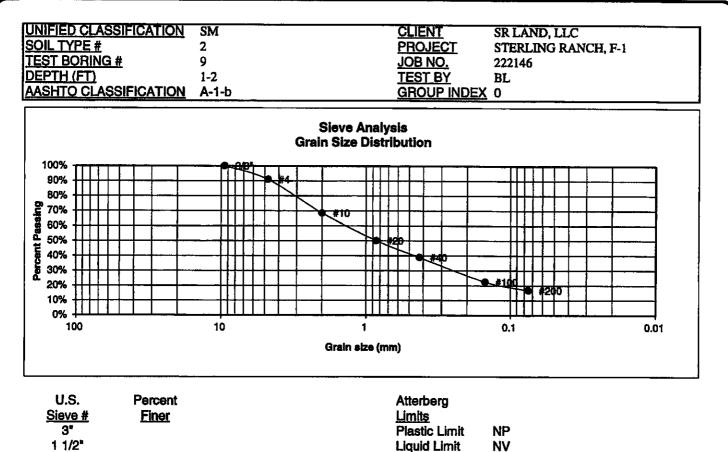


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	95.2%	<u>Swell</u>
10	72.5%	Moisture at start
20	51.2%	Moisture at finish
40	39.9%	Moisture increase
100	23.0%	Initial dry density (pcf)
200	15.3%	Swell (psf)

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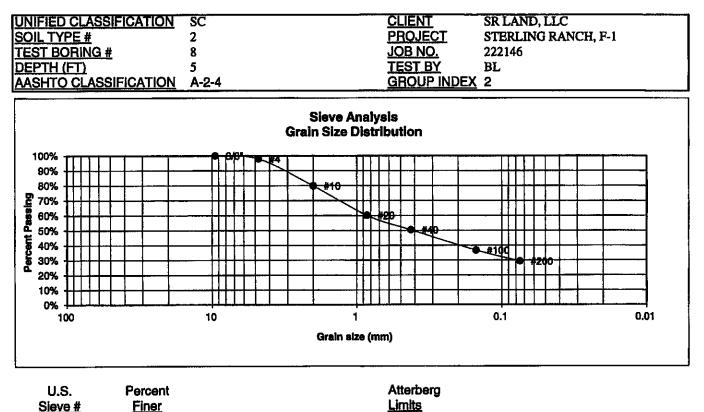
ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 60907

ſ	LABORATORY TEST RESULTS				
DRAWN:	DATE:	CHECKED: SW	12-23-22	FIG NO.: B-14	



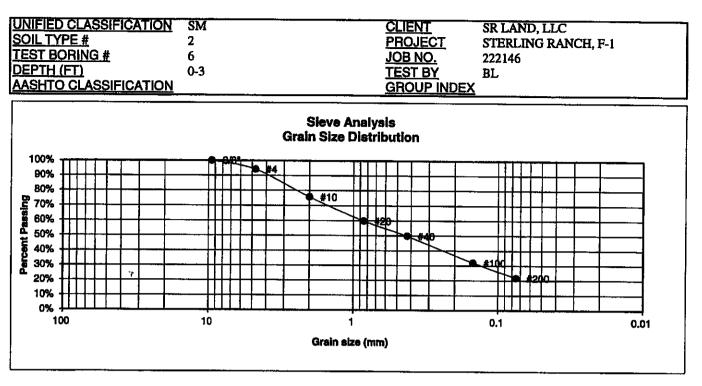
3/4"		Plastic Index NP		
1/2"				
3/8*	100.0%			
4	91.0%	Swell		
10	68. 5%	Moisture at start		
20	50.1%	Moisture at finish		
40	38.9%	Moisture increase		
100	22.5%	Initial dry density (pcf)		
200	16.8%	Swell (psf)		

\diamondsuit	ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80807	LABORATORY TEST RESULTS				JOB NO.: 222146 FIG NO.;
		DRAWN:	DATE:	CHECKED: W	12-23-22	FIG NO.: B-15



		· ·······
<u>Sieve #</u>	<u>Finer</u>	Limits
3*		Plastic Limit 20
1 1/2"		Liquid Limit 29
3/4"		Plastic Index 9
1/2"		
3/8*	100.0%	
4	98.0%	<u>Swell</u>
10	79.9%	Moisture at start
20	60.1%	Moisture at finish
40	50.4%	Moisture increase
100	36.6%	Initial dry density (pcf)
200	29.2%	Swell (psf)

ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	$\overline{}$	LABORATORY TEST RESULTS			JOB NO.: 222146 FIG NO.;
	DRAWN:	DATE:		12-23-22	B-16

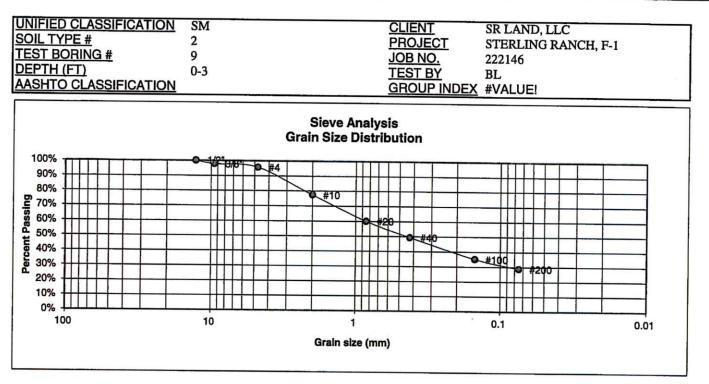


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
3/8"	100.0%	
4	94.2%	<u>Sweli</u>
10	75.7%	Moisture at start
20	59.7%	Moisture at finish
40	49.7%	Moisture increase
100	31.9%	Initial dry density (pcf)
200	21.7%	Swell (psf)

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ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

LABORATORY TEST RESULTS					JOB NO.: 222146 FIG NO.;
DRAWN:	DATE:		12-23-22	j (B-17

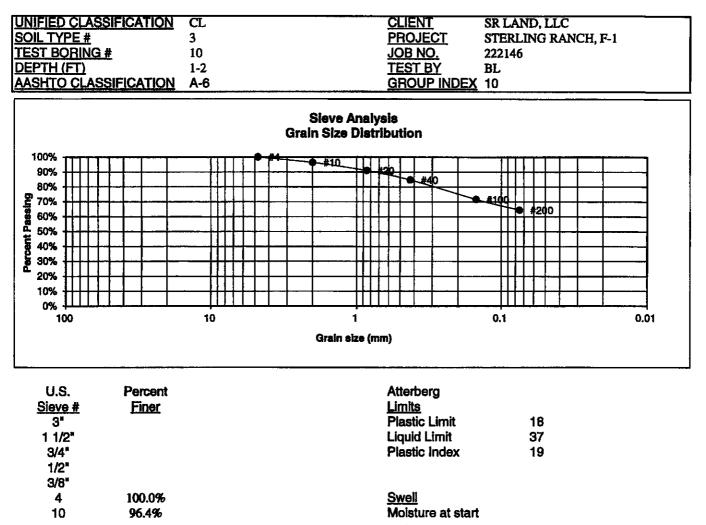


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index
1/2" 3/8" 4 10	100.0% 97.8% 95.7% 77.3%	<u>Swell</u> Moisture at start
20 40 100 200	60.1% 49.4% 35.1% 28.8%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



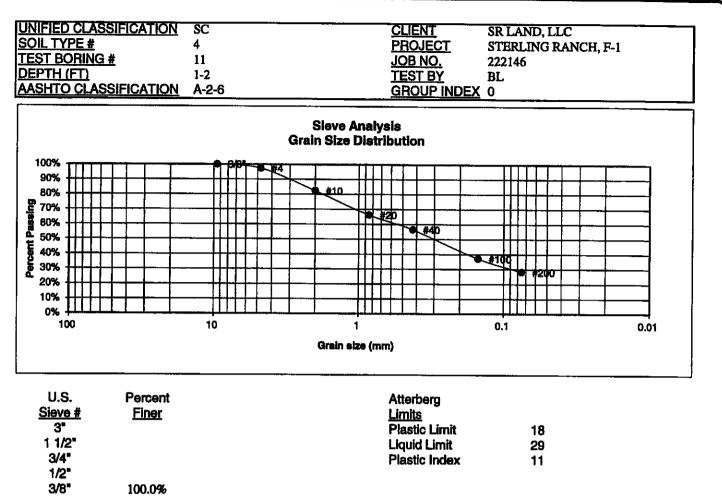
LABORATORY TEST			JOL	
RESULTS				222
DRAWN:	DATE:	CHECKED: SW	12-23-22	B

JOB NO.: 222146 FIG NO.: B 18



4	100.070	<u>Owen</u>
10	96.4%	Moisture at start
20	91.0%	Moisture at finish
40	84.7%	Moisture increase
100	71.6%	Initial dry density (pcf)
200	64.4%	Swell (psf)

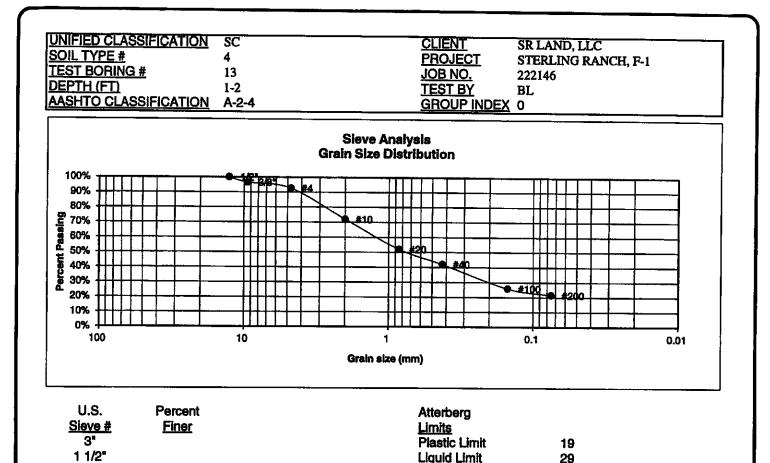
ENTECH ENGINEERING, INC.		LABORATORY TEST RESULTS				JOB NO.: 222146 Fig NO.;
 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED: SW	DATE 12-23-22)	B-19



4	97.3%	Swell
10	82.3%	Moisture at start
20	66.1%	Moisture at finish
40	56.5%	Moisture increase
100	37.1%	Initial dry density (pcf)
200	28.2%	Swell (psf)

\mathbf{O}	ENTECH ENGINEERING, INC.		LABOF RESUL	ATORY TEST	
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED: SW	12-23-22

JOB NO.: 222146 FIG NO.: **B ~ 20**



Plastic Index

Moisture at start

Moisture at finish

Moisture increase

Swell (psf)

Initial dry density (pcf)

<u>Sweli</u>

10

3/4"

1/2"

3/8*

4

10

20

40

100

200

100.0%

96.6%

92.6%

71.9%

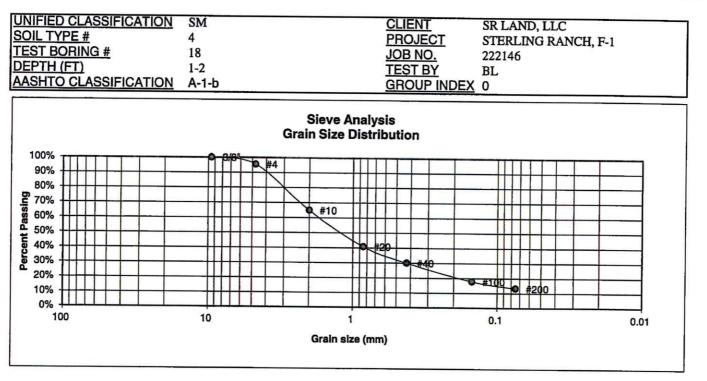
52.1%

42.0%

25.9%

21.4%

ENTECH ENGINEERING, INC.	\square	JOB NO.: 222146 FIG NO.:			
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 50907	DRAWN:	DATE:	DATE 12-23-22	8-21

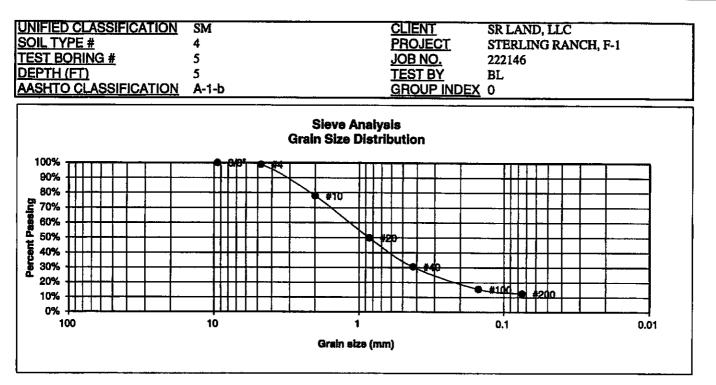


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	95.6%	Swell
10	64.8%	Moisture at start
20	40.8%	Moisture at finish
40	30.0%	Moisture increase
100	17.8%	Initial dry density (pcf)
200	13.3%	Swell (psf)



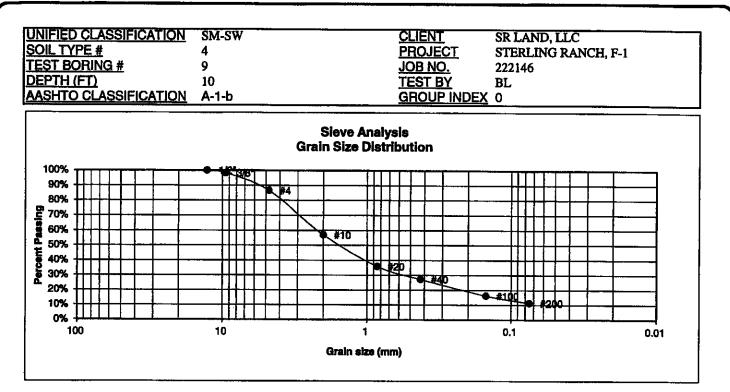
		ATORY TEST		JOB NO .:
	RESUL	.TS		222146 FIG NO.:
DRAWN:	DATE:	CHECKED:	12-23-22	B-2

6 22



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
3/8"	100.0%	
4	98.8%	Swell
10	77.9%	Moisture at start
20	49.9%	Moisture at finish
40	30.5%	Moisture increase
100	15.4%	Initial dry density (pcf)
200	12.4%	Swell (psf)

ENTECH ENGINEERING, INC.		LABORATORY TEST RESULTS			
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 60907	DRAWN:	DATE	CHECKED:	12-23-22	B-23



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
1/2" 3/8" 4 10	100.0% 98.3% 86.6% 57.0%	<u>Swell</u> Moisture at start
20 40 100 200	35.9% 27.2% 16.2% 11.3%	Moisture at finish Moisture increase Initial dry density (pcf) Swell (psf)



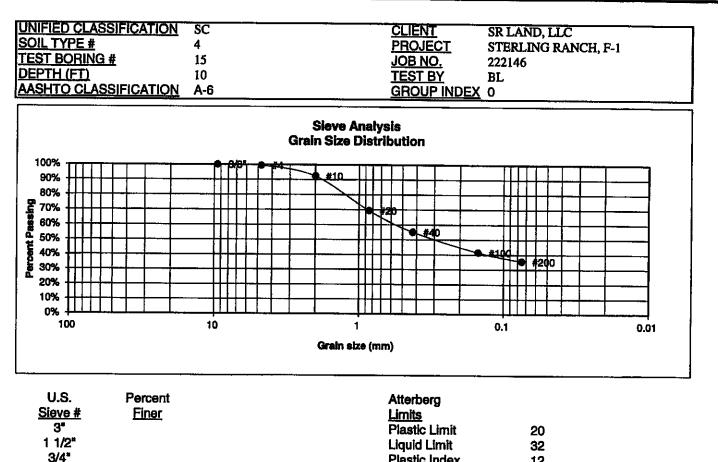
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ENGINEERING, INC.

505 ELICTON DRIVE COLORADO SPRINGS, COLORADO 80907

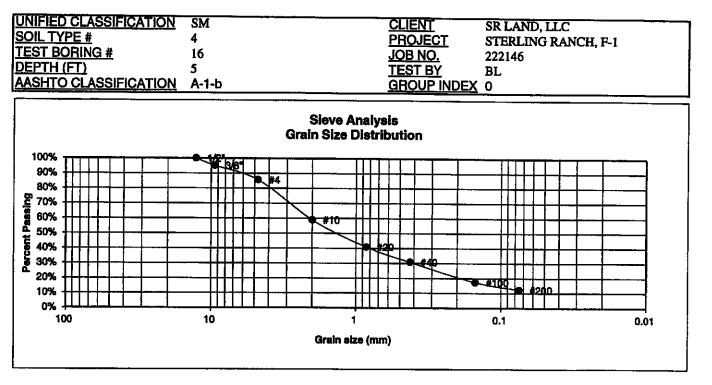
[JOB NO.: 222146 FIG NO.:			
DRAWN:	DATE:	CHECKED:	12-23-22	B-24

6 4



3/4-		Plastic Index 12	
1/2"		•••••••••••••••••••••••••••••••••••••••	
3/8"	100.0%		
4	99.4%	Swell	
10	92.3%	Moisture at start	
20	69.3%	Moisture at finish	
40	55.1%	Moisture increase	
100	41.4%	Initial dry density (pcf)	
200	35.5%	Swell (psf)	

\diamond	ENTECH ENGINEERING, INC.		LABOF RESUL	ATORY TES	г	JOB NO.: 222146 FIG NO.:
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED	12-23-22	8-25

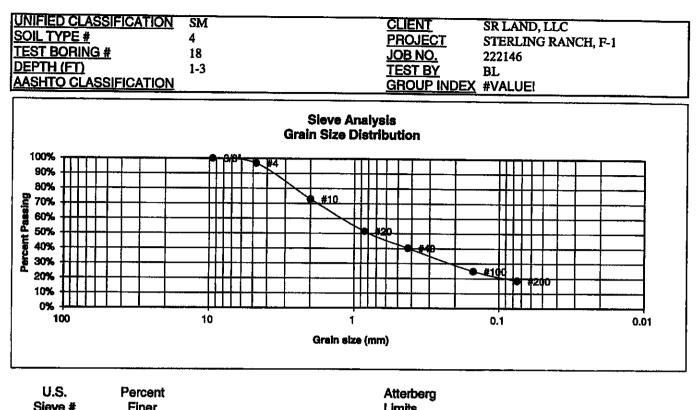


U.S.	Percent	Atterberg
<u>Sieve #</u>	<u>Finer</u>	<u>Limits</u>
3"		Plastic Limit NP
1 1/2"		Liquid Limit NV
3/4"		Plastic Index NP
1/2*	100.0%	
3/8"	95.1%	
4	85.7%	<u>Swell</u>
10	58.9%	Moisture at start
20	40.9%	Moisture at finish
40	30.8%	Moisture increase
100	17.3%	Initial dry density (pcf)
200	12.3%	Swell (psf)
20 40 100	40.9% 30.8% 17.3%	Moisture at finish Moisture increase Initial dry density (pcf)



		JOB NO.:		
_	RESUL	.TS		222146 Fig NO.:
DRAWN:	DATE:	CHECKED:	12-23-22	B-2

222146
FIG NO.:
B-26
D"# (A



<u>Sieve #</u>	<u>Finer</u>	Limits
3"		Plastic Limit
1 1/2"		Liquid Limit
3/4"		Plastic Index
1/2"		
3/8"	100.0%	
4	96.8%	<u>Swell</u>
10	72.9%	Moisture at start
20	51.5%	Moisture at finish
40	40.3%	Moisture increase
100	24.8%	Initial dry density (pcf)
200	18.5%	Swell (psf)



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	LABOF RESUL	ATORY TEST	·	JOB NO.: 222146
DRAWN:	DATE:	CHECKED:	DATE 12-23-22	FIGNO.:

INIFIEI OIL TY EST B EPTH ASHT(YF SO	2 <u>E</u> 81	# N(<u>3</u> (ŧ				-	S(5, 12 1- A	, Cl 2 -3	BR	.#.	2									E JU T	DB ES	NC NC	<u>Ст</u> <u>).</u>			ST 22 BL	EF 214	L		, LI G R			H, 1	F-1		
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100% 90%	I	T						Τ				Π			Ľ	Ľ	F		. #	0		Π	Τ	Ţ			Τ			Π	Π	Τ	T	1	Т				
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1	100)									10										1								0	1								0.0	

Grain size (mm)

U.S. <u>Sieve #</u> 3* 1 1/2* 3/4* 1/2*	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 18 Liquid Limit 29 Plastic Index 11
3/8"	100.0%	
4	99.4%	Swell
10	91.7%	Moisture at start
20	80.8%	Moisture at finish
40	72.6%	Moisture increase
100	51.6%	Initial dry density (pcf)
200	39.2%	Swell (psf)



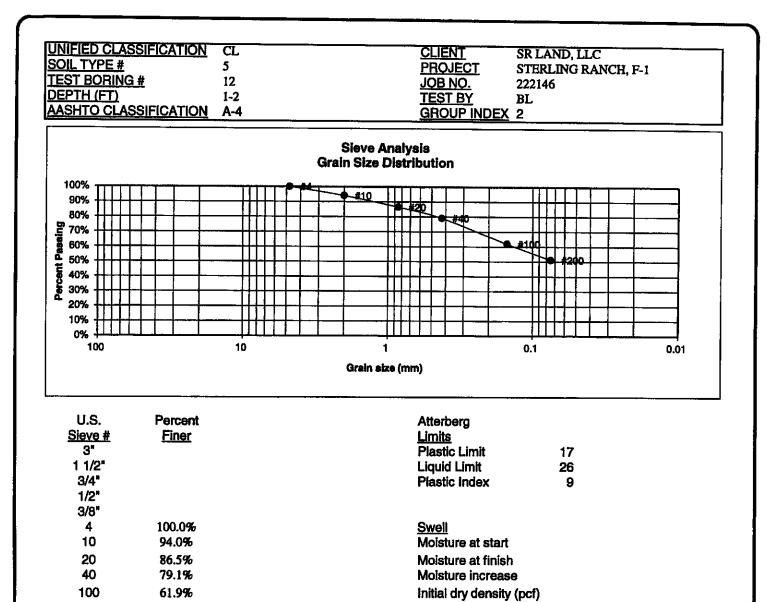
ENTECH

	LABOF RESUL	RATORY TEST		JOB NO 222146 FIG NO
DRAWN:	DATE:	CHECKED:	12-23-22	B-2

0.1

JOB NO.:
222146
FIG NO .:
R-29

0.01



Swell (psf)

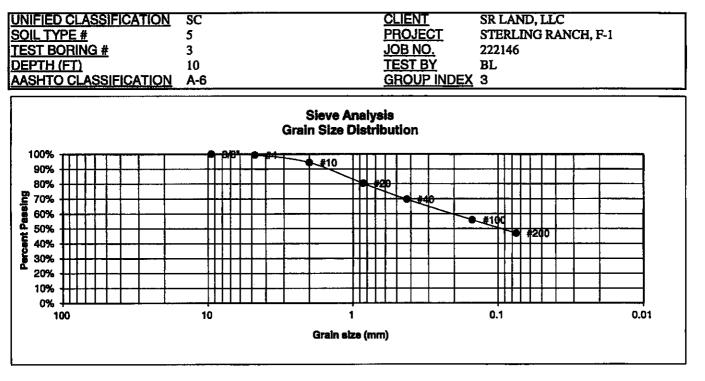
$\mathbf{\mathbf{O}}$	ENTECH ENGINEERING, INC.		LABOF RESUL	RATORY TEST		JOB N 22214
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKED: 5W	12-23-22	B-

200

51.2%

Ю.:

16 29

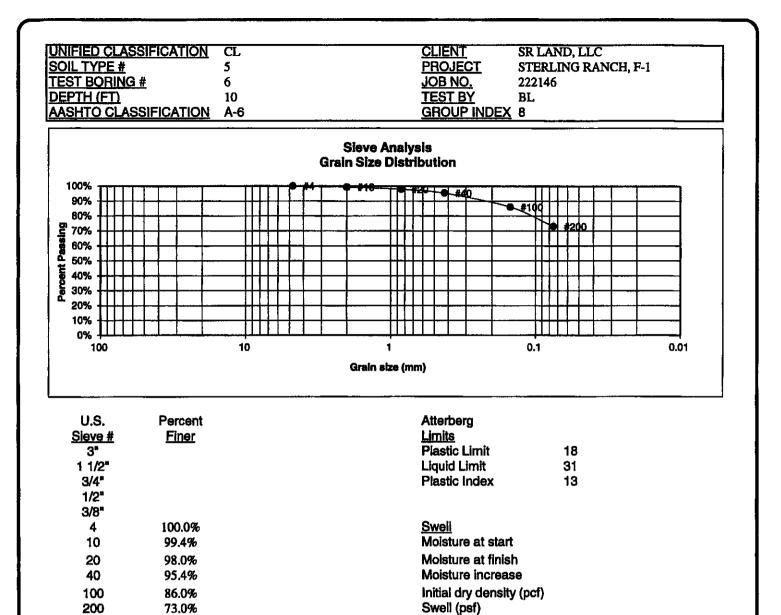


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 20 Liquid Limit 33 Plastic Index 13
3/8"	100.0%	
4	99.4%	Swell
10	94.3%	Moisture at start
20	80.3%	Moisture at finish
40	69.6%	Moisture increase
100	55.8%	Initial dry density (pcf)
200	46.9%	Swell (psf)

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ENTECH ENGINEERING, INC. 505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 50907

		ATORY TEST	r)	JOB NO.: 222146
	RESUL	.15		FIG NO.:
DRAWN:	DATE:	CHECKED W	12-23-22	B-30



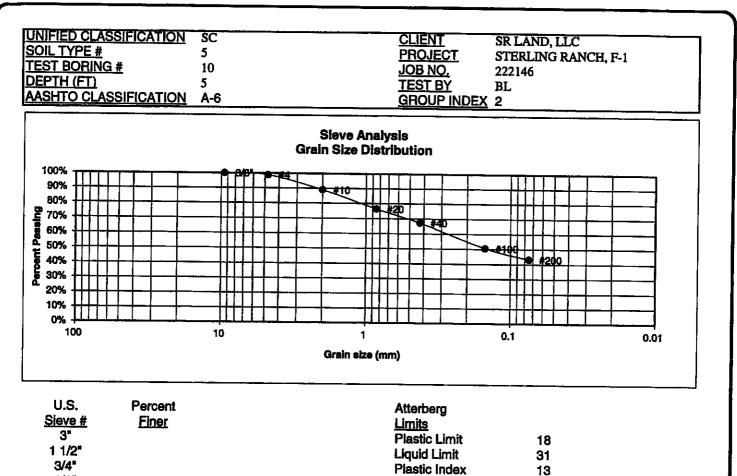
ENGINEERING, INC.		ENTECH
	Z. 7	ENGINEERING, INC.

LABOF RESUL	RATORY TES .TS	Т	
DATE:	CHECKED:	DATE:	

(JOB NO.:		
	222146 FIG NO.:	1	
L	<u></u>	1	

...

DRAWN:



1/2"		
3/8"	100.0%	
4	98.8%	Swell
10	88.9%	Moisture at start
20	76.4%	Moisture at finish
40	67.2%	Moisture increase
100	50.5%	Initial dry density (pcf)
200	43.3%	Swell (psf)

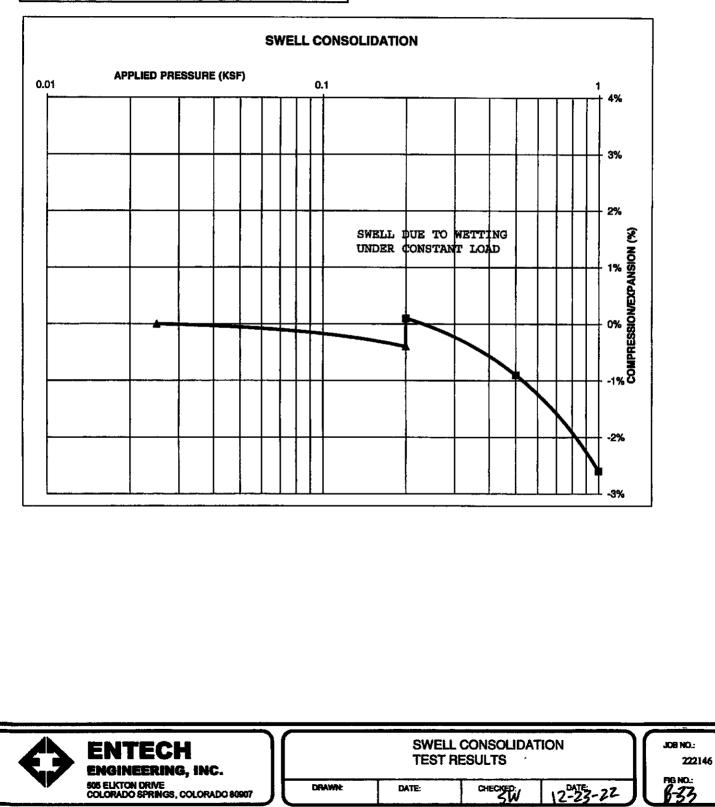


LABORATORY TEST RESULTS				
DRAWN:	DATE:	HECKED: SW	DATE: 12-23-22	

JOB NO.: 222146 FIG NO.:

B-32

TEST BORING #	3	DEPTH(ft)	0-3
DESCRIPTION	SC	SOIL TYPE	1, CBR
NATURAL UNIT DRY	Y WEIGH	IT (PCF)	113
NATURAL MOISTUP			13.1%
SWELL/CONSOLID/			0.5%



	TEST BORING #	1	DEPTH(ft)	1-2
	DESCRIPTION	SC	SOIL TYPE	1
1	NATURAL UNIT DRY	'WEIGH	IT (PCF)	113
	NATURAL MOISTUR			11.1%
	SWELL/CONSOLIDA			0.2%

JOB NO. 222146 CLIENT SR LAND, LLC PROJECT STERLING RANCH, F-1

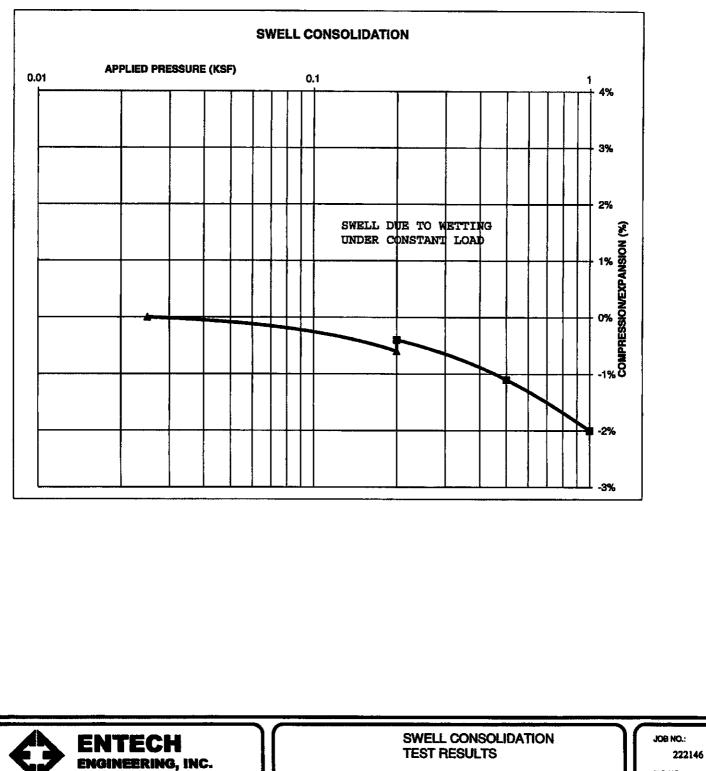


FIG NO .: B-34 12-23-22

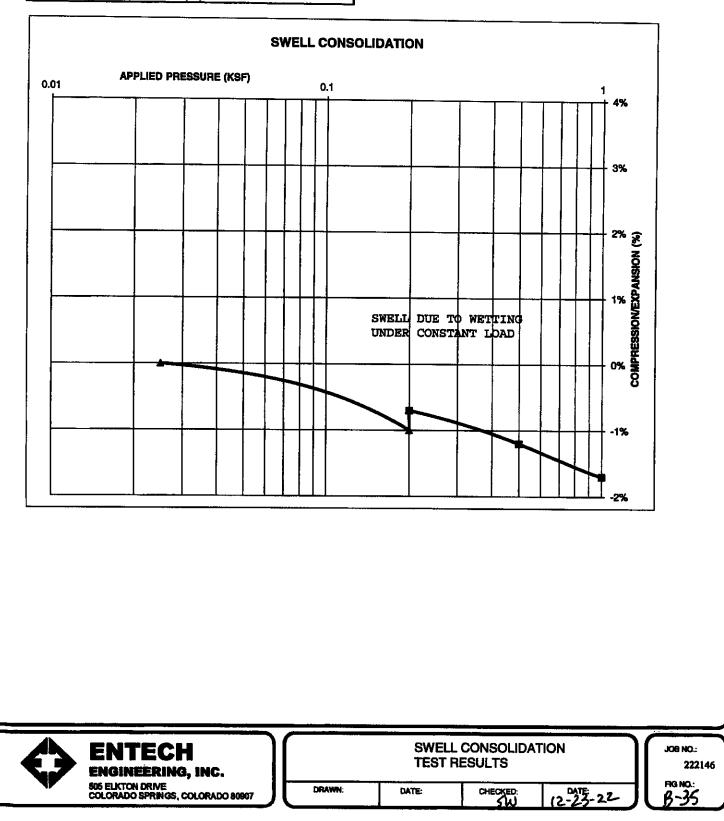
CHECKED:

505 ELICTON DRIVE COLORADO SPRINGS, COLORADO 80907

DRAWN:

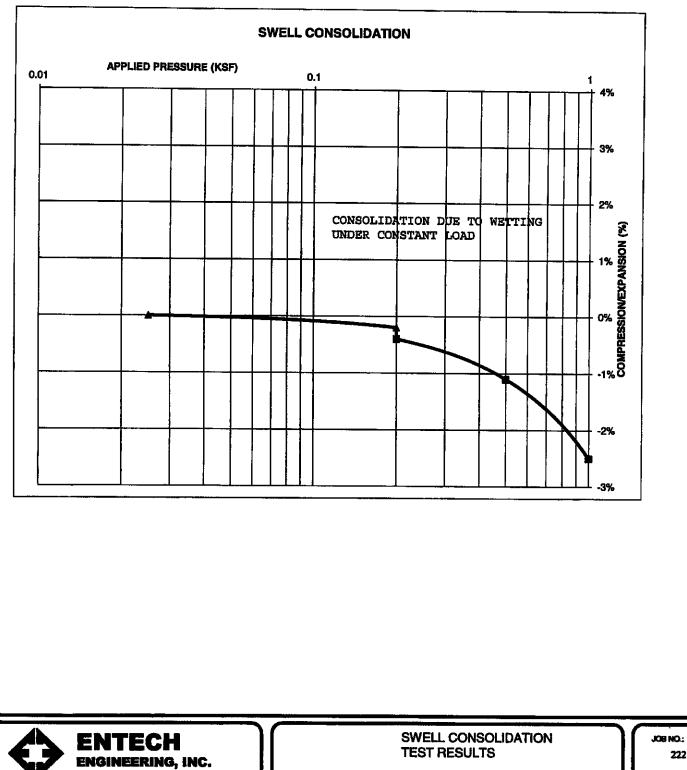
DATE:

TEST BORING #	2	DEPTH(ft)	1-2
DESCRIPTION	SC	SOIL TYPE	1
NATURAL UNIT DR	Y WEIGH	IT (PCF)	113
NATURAL MOISTUF		ENT	12.5%
SWELL/CONSOLID/	ATION (9	6)	0.3%



TEST BORING #	16	DEPTH(ft)	1-2
DESCRIPTION	SC	SOIL TYPE	
NATURAL UNIT DRY	' WEIGH	T (PCF)	119
NATURAL MOISTUR	E CONT	FENT	9.9%
SWELL/CONSOLIDA			-0.2%

JOB NO. 222146 CLIENT SR LAND, LLC PROJECT STERLING RANCH, F-1

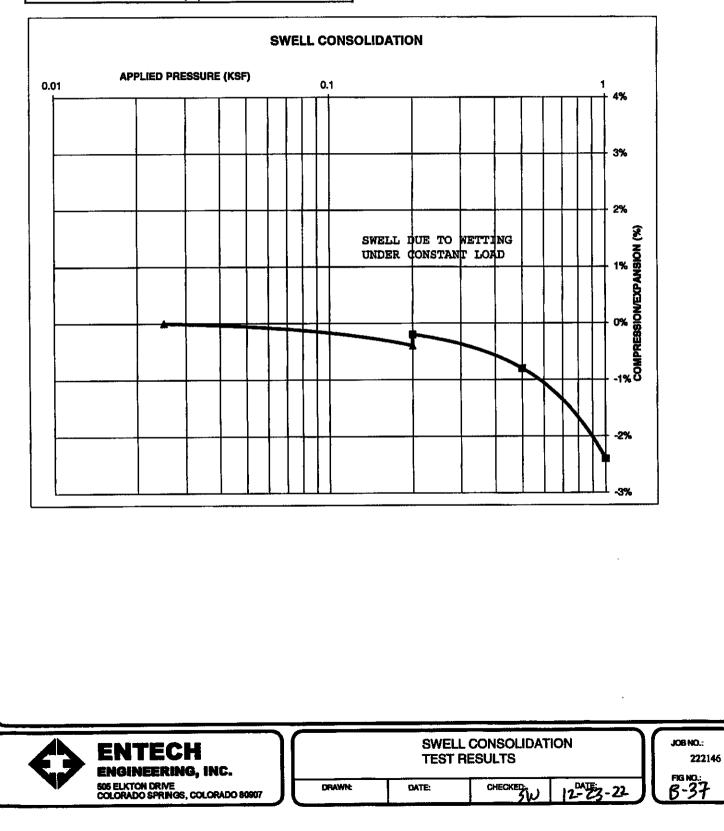


222146
FIG NO.: 8-36

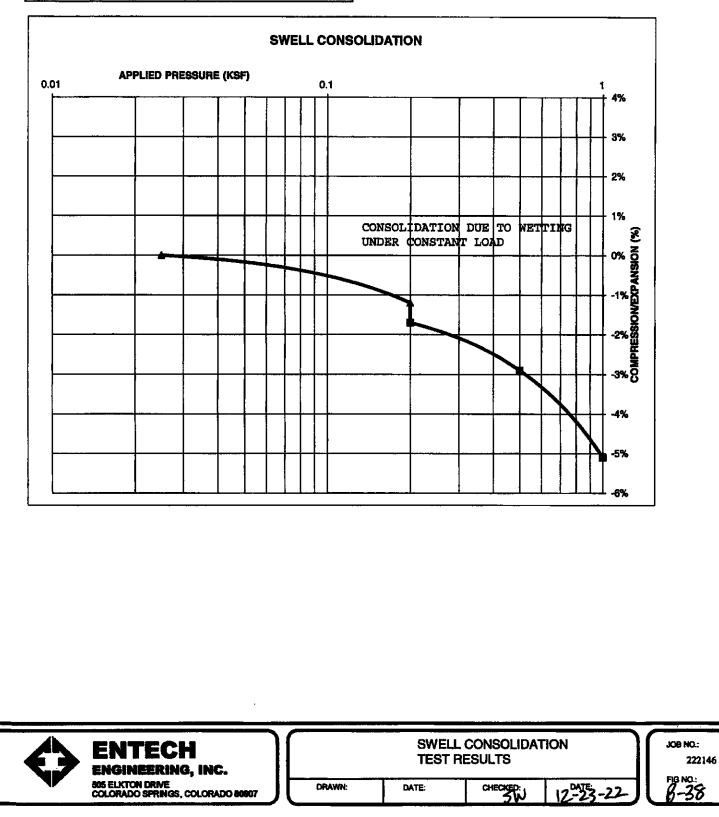
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

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TEST BORING #	17	DEPTH(ft)	1.2	
	17			
DESCRIPTION	SC	SOIL TYPE	1	
NATURAL UNIT DRY	' WEIGH	IT (PCF)	117	
NATURAL MOISTUR	E CON	ENT	10.3%	
SWELL/CONSOLIDA	TION (9	6)	0.2%	



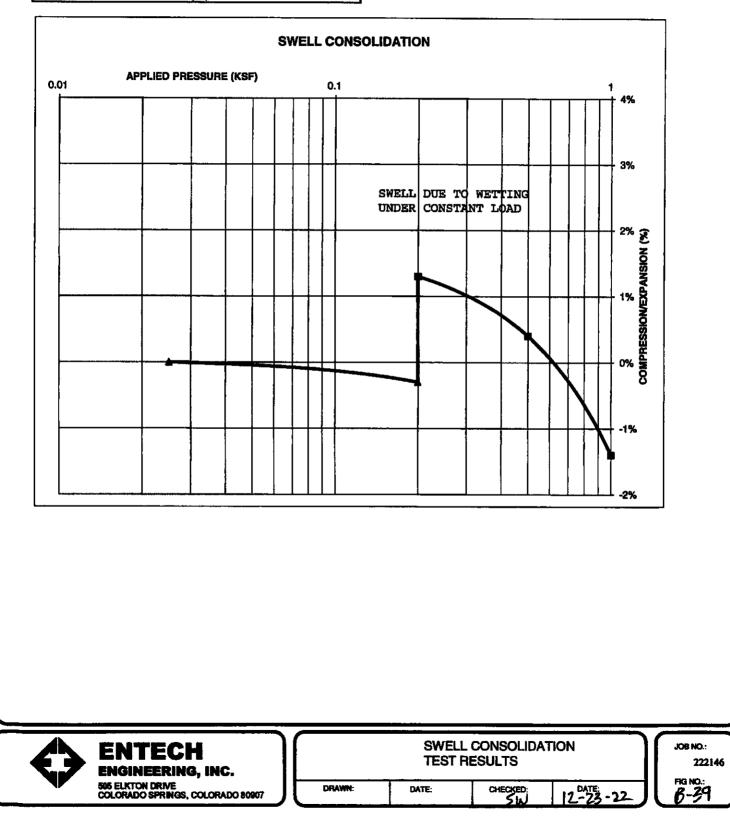
	TEST BORING #	8	DEDTUM	E
		0	DEPTH(ft)	2
	DESCRIPTION	SC	SOIL TYPE	2
	NATURAL UNIT DRY	WEIGH	IT (PCF)	103
ļ	NATURAL MOISTUR	E CONT	TENT	7.0%
	SWELL/CONSOLIDA	TION (9	6)	-0.5%



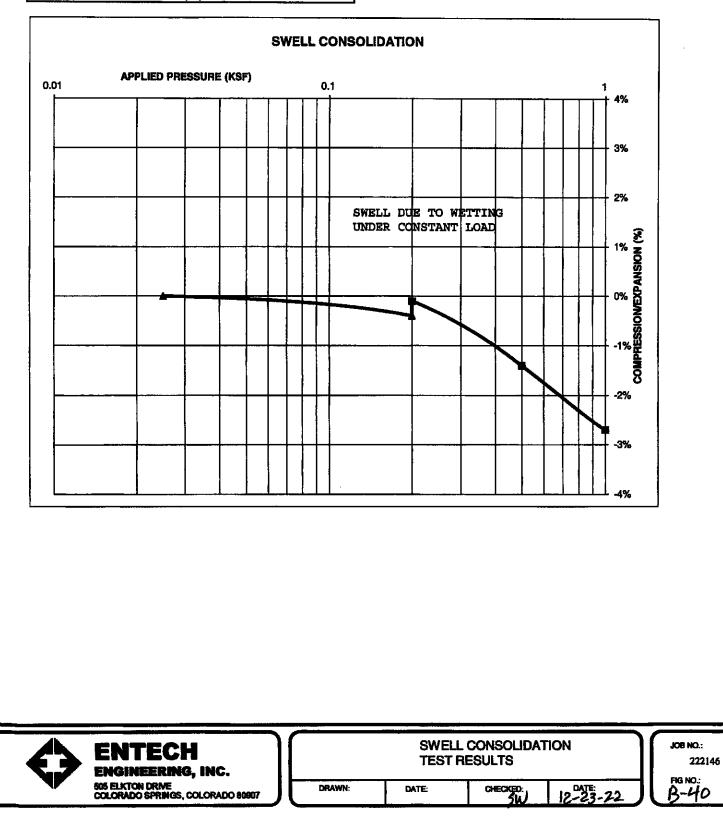
TEST BORING #	10	DEPTH(ft)	1-2
DESCRIPTION	CL	SOIL TYPE	3
NATURAL UNIT DRY	WEIG	HT (PCF)	111
NATURAL MOISTUR	E CON	FENT	13.3%
SWELL/CONSOLIDA	TION (9	%)	1.6%

JOB NO. 222146 CLIENT SR LAND, LLC PROJECT STERLING RANCH, F-1

.



TEST BORING #	11	DEPTH(ft)	1-2
DESCRIPTION	SC	SOIL TYPE	4
NATURAL UNIT DRY	WEIGH	IT (PCF)	117
NATURAL MOISTUR			9.8%
SWELL/CONSOLIDA			0.3%



TEST BORING #	15	DEPTH(ft)	10
DESCRIPTION	SC	SOIL TYPE	4
NATURAL UNIT DRY	WEIGH	HT (PCF)	118
NATURAL MOISTUR	E CON	FENT	10.1%
SWELL/CONSOLIDA			0.7%

JOB NO. 222146 CLIENT SR LAND, LLC PROJECT STERLING RANCH, F-1

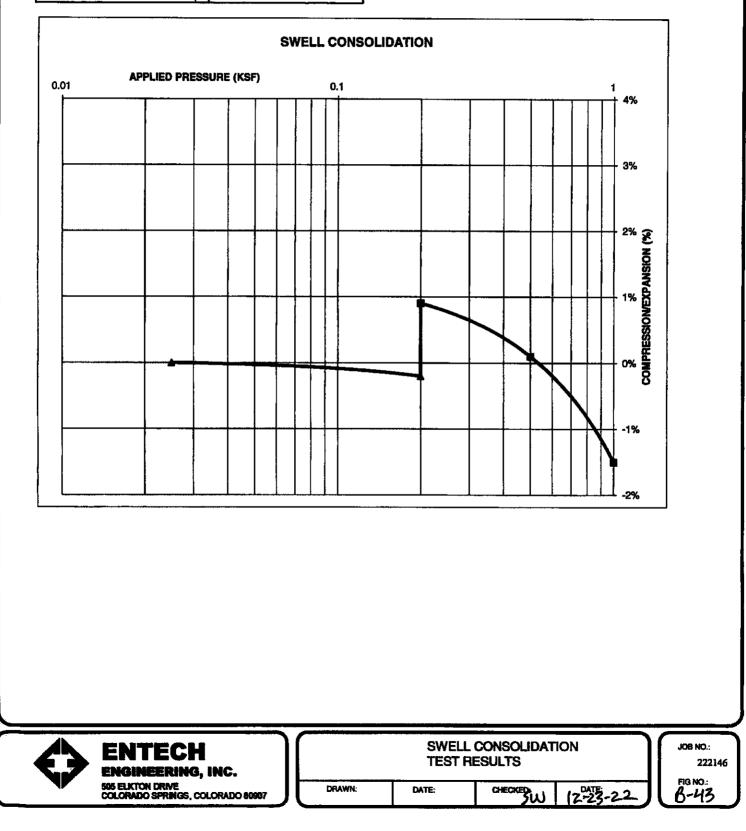
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	SW	/ELL C	CONSOLID	ATION			
APPLIED PRESSURE (KSF)			0.1				1 -+ 4%
		+					3%
				l due to Ir constan			
							- 2% §
							NEXPA
		╡┽					%; %; % COMPRESSION/EXPANSION (%)
							1%00
						\mathbb{N}	
 			<u></u>			++	-2%
 ,							⊥ .3%
 	_			······································			
ENTECH ENGINEERING, INC.					L CONSOLID. RESULTS	ATION	
505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 8090		 	RAWN:	DATE:	CHECKED:	DATE:	-22

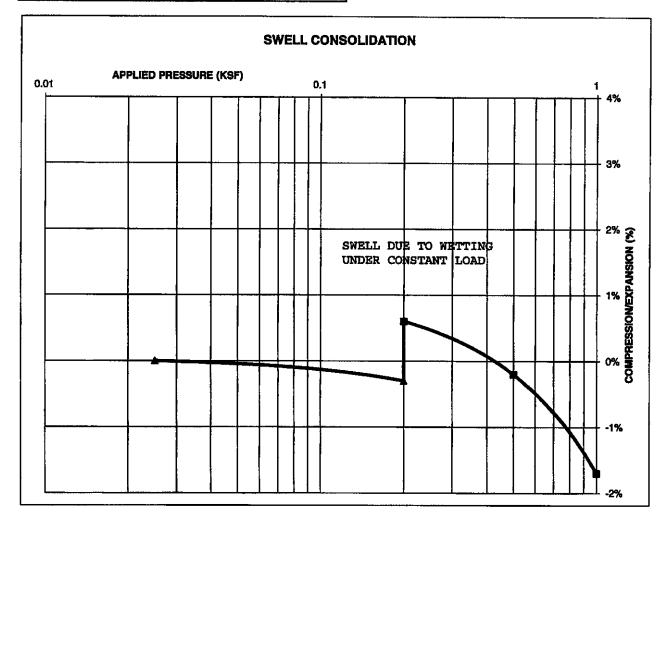
TEST BORING #	3	DEPTH(ft)	10
DESCRIPTION	SC	SOIL TYPE	5
NATURAL UNIT DRY	WEIGI	HT (PCF)	120
NATURAL MOISTURI	e con	TENT	9.5%
SWELL/CONSOLIDA			0.3%

			SWE	ELL C	CONSOLI	DATIO	N					
	PRESSURE	: (KSF)			D.1			r	·	1 1	- 1 - 1 - •	1 + 4%
												3%
							DUE TO CONSTA					+ 2%
 												1% NOISN
 				╈┽	 							ONEXPA
 												COMPRESSIONEXPANSION (%)
 												-2%
 												-3%

TEST BORING #	6	DEPTH(ft)	10
DESCRIPTION	CL	SOIL TYPE	5
NATURAL UNIT DRY	WEIGH	IT (PCF)	109
NATURAL MOISTUR			15.4%
SWELL/CONSOLIDA			1.1%



TEST BORING #	10	DEPTH(ft)	5
DESCRIPTION	SC	SOIL TYPE	5
NATURAL UNIT DRY	WEIGH	IT (PCF)	111
NATURAL MOISTUF			14.0%
SWELL/CONSOLID/			0.9%

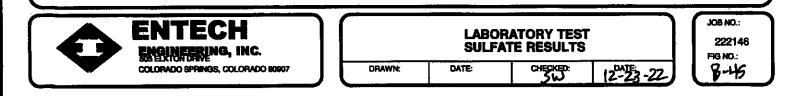


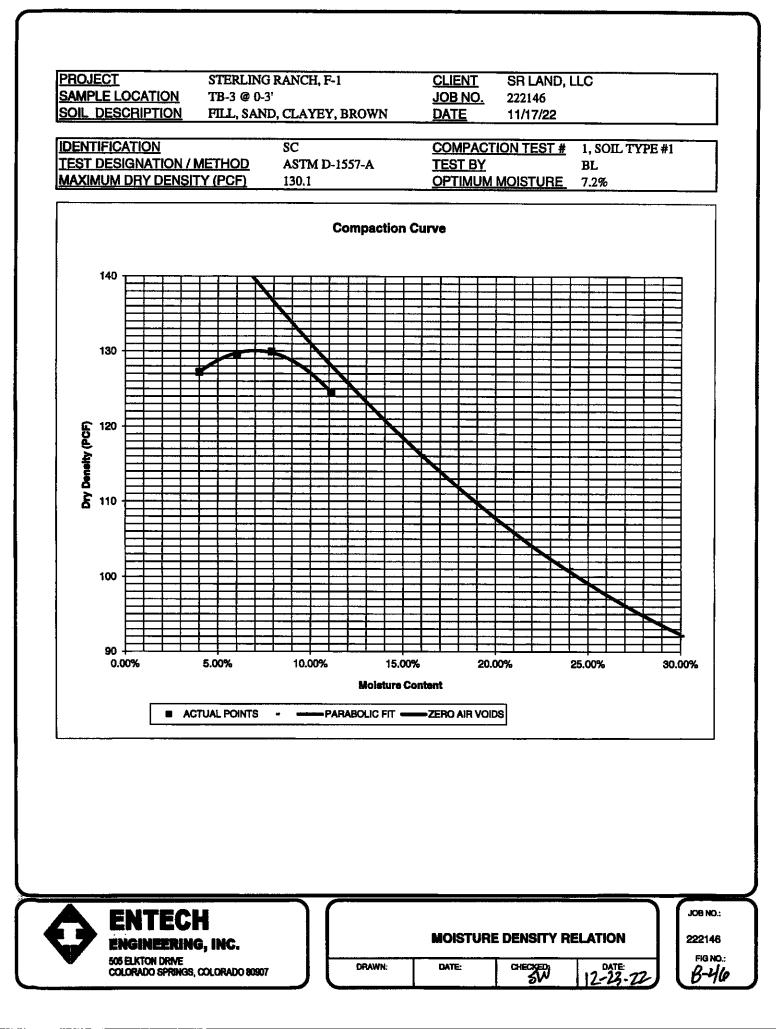
\mathbf{O}	ENTECH ENGINEERING, INC.			L CONSOLIDA RESULTS	TION	JOB NO.: 222146
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907	DRAWN:	DATE:	CHECKGED:	12-23-22	FIG NO.: B-44

CLIENT	SR LAND, LLC	JOB NO.	222146
PROJECT	STERLING RANCH, F-1	DATE	12/20/2022
LOCATION	STERLING RANCH, F-1	TEST BY	BL

BORING NUMBER	DEPTH, (ft)	Soil type Number	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (w1%)
TB-1	1-2	1	SC	<0.01
TB-4	1-2	1	sc	0.00
TB-7	1-2	1	SM	<0.01
TB-5	5	4	SM	0.00
TB-8	5	2	sc	<0.01
		<u></u>		
				· - · · · ·

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CBR TEST LOAD DATA

			CLIENT:	SR LAND, LI	LC	
PISTON	PISTON		PROJECT:	STERLING F	RANCH, F-1	
DIAMETER (cm)	AREA (in ²)		SOIL TYPE:	1, CBR #1		
4.958	2.993					
	10 BLOWS		25 BLOWS		56 BLOWS	
PENETRATION	MOLD #	1	MOLD #	2	MOLD #	3
DEPTH	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS
(INCHES)	(LBS)	(PSI)	(LBS)	(PSI)	(LBS)	(PSI)
0.000	0	0.00	0	0.00	0	0.00
0.025	200	66.83	214	71.51	585	195.49
0.050	258	86.22	489	163.41	800	267.33
0.075	294	98.25	675	225.56	969	323.81
0.100	336	112.28	954	318.80	1276	426.40
0.125	369	123.31	1110	370.93	1989	664.66
0.150	457	152.71	1295	432.75	2415	807.02
0.175	480	160.40	1461	488.22	2923	976.77
0.200	519	173.43	1605	536.34	3229	1079.03
0.300	593	198.16	2120	708.44	4454	1488.38
0.400	716	239.26	2546	850.79	5463	1825.56
0.500	808	270.01	2609	871.84	6000	2005.01

JOB NO:

222146

FINAL MOISTURE CONTENT

	MOLD #	1	MOLD #	2	MOLD #	3
CAN #		346		351		354
WT. CAN		6.92		7.04		6.92
WT. CAN+WET		139.28		120.99		109.19
WT. CAN+DRY		120.53		107.18		98.65
<u>WT. H20</u>		18.75		13.81		10.54
WT. DRY SOIL		113.61		100.14		91.73
MOISTURE CONTENT		16.50%		13.79%		11.49%
WET DENSITY (PCF)		122.9		131.7		137.9
DRY DENSITY (PCF)		114.7		122.8		128.7
BEARING RATIO		11 .23		31.88		42.64
90% OF DRY DENSITY	117.1					
95% OF DRY DENSITY	123.6					
BEARING RATIO AT 90% OF MAX		17.36	~ R VALUE	60		
BEARING RATIO AT 95% OF MAX		33.32	~ R VALUE	74		

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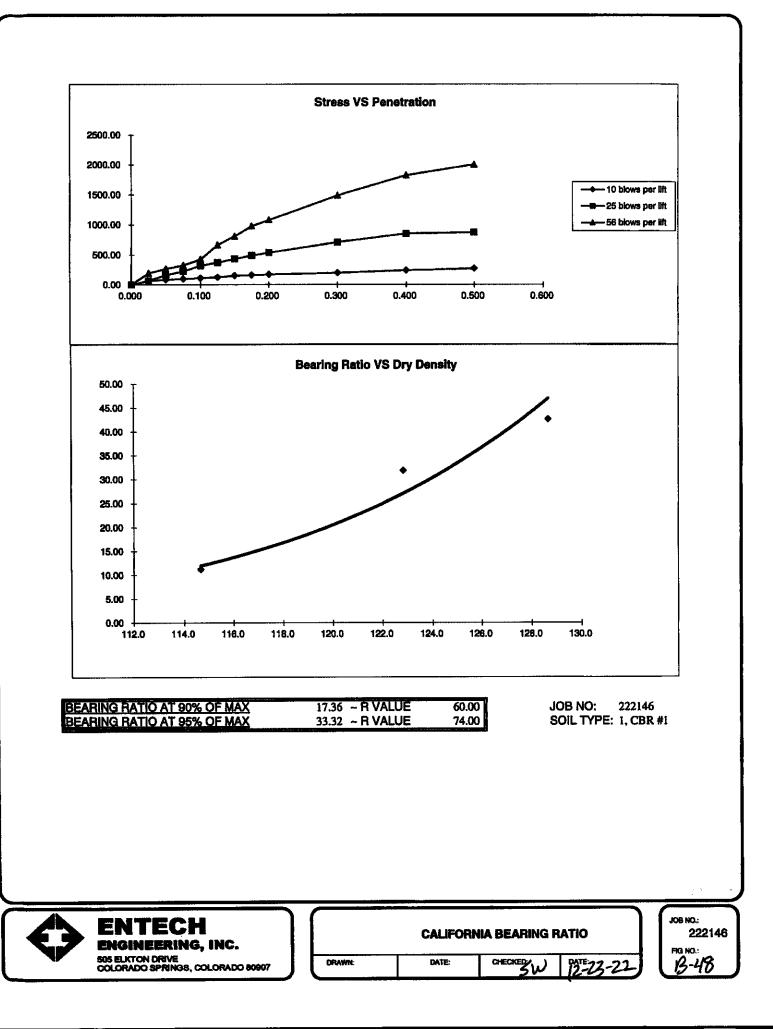


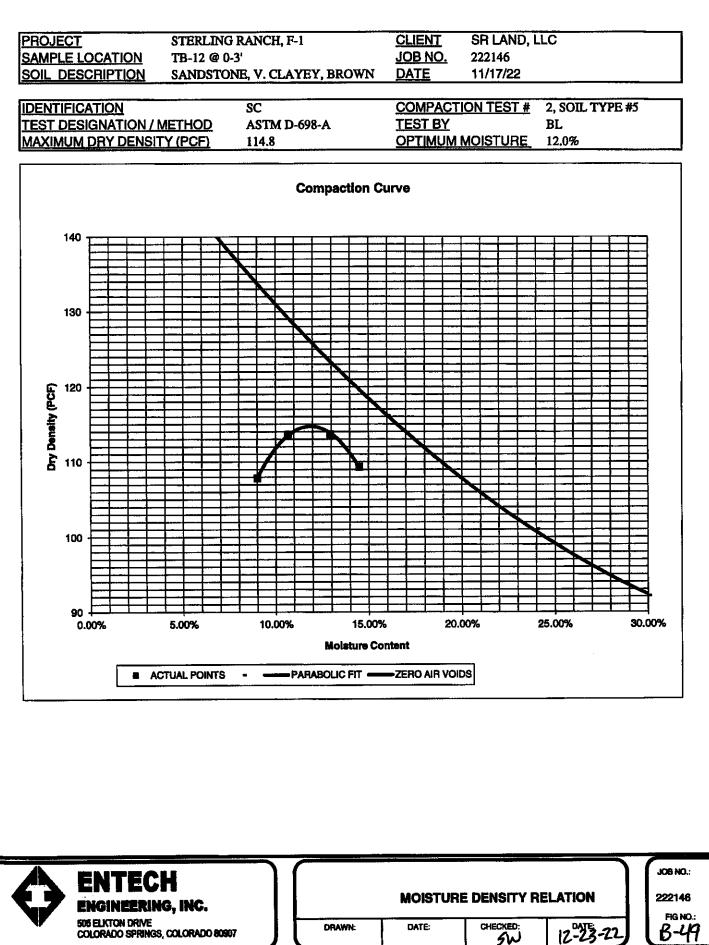
ENTECH	
ENGINEERING, INC.	
505 ELICTON DRIVE COLORADO SPRINGS, COLORADO 80907]

CBR TEST DATA				
	DATE:		12-23-22-	

JOB NO.: 222146 FIG NO.: B-47

.





CBR TEST LOAD DATA

CLIENT: SR LAND, LLC PROJECT: STERLING RANCH, F-1 PISTON PISTON SOIL TYPE: 5, CBR #1 DIAMETER (cm) AREA (in²) 4.958 2.993 10 BLOWS 25 BLOWS 56 BLOWS MOLD # 3 MOLD # 2 PENETRATION MOLD # 1 STRESS LOAD(LBS) STRESS LOAD(LBS) STRESS DEPTH LOAD(LBS) (PSI) (LBS) (PSI) (LBS) (PSI) (LBS) (INCHES) 0 0.00 0.00 0 0.00 0 0.000 25.06 96 32.08 151 50.46 0.025 75 93 31.08 134 44.78 213 71.18 0.050 160 53.47 241 80.53 103 34.42 0.075 274 91.56 191 63.83 0.100 115 38.43 108.94 125 41.77 233 77.86 326 0.125 268 89.56 382 127.65 131 43.78 0.150 140.02 419 294 98.25 0.175 139 46.45 156.06 467 0.200 148 49.46 341 113.95 420 140.35 613 204.84 53.80 0.300 161 238.26 160.73 713 481 0.400 175 58.48 272.01 814 525 175.44 0.500 189 63.16

JOB NO:

222146

FINAL MOISTURE CONTENT

	MOLD #	1	MOLD #	2	MOLD #	3
CAN #		350		352		348
WT. CAN		6.57		6.71		6.85
WT. CAN+WET		154.45	1	168.07		105.13
WT. CAN+DRY		132.49		142.71	ļ	92.85
WT. H20		21.96		25.36		12.28
WT. DRY SOIL		125.92		136		86
MOISTURE CONTENT		17.44%		18.65%		14.28%
WET DENSITY (PCF)		119.0		122.0		131.1
DRY DENSITY (PCF)		106.2		108.9		117.1
BEARING RATIO		3.84		6.38		9.16
<u>DEATHING FRATES</u>						
90% OF DRY DENSITY	103.3					
95% OF DRY DENSITY	109.1					
gere et antentert						
BEARING RATIO AT 90% OF MAX	·····	1.04	- R VALUE	1		
BEARING RATIO AT 95% OF MAX			- R VALUE	14		

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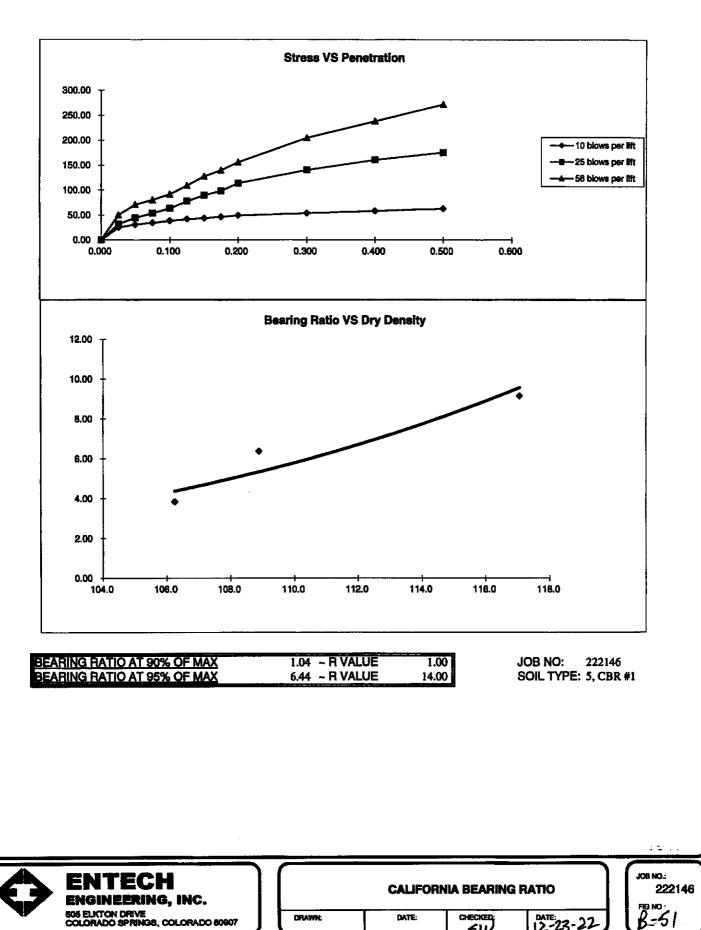


ENTECH

ENGINEERING, INC. 525 ELITON DRIVE COLORADO SPRINGS, COLORADO 80907

CBR TEST DATA				
WN:	DATE:	CHECKED W DATE SW 12-23-22	JL	P

јов но.: 222146 гна но.: B-50



CHECKED DATE:

APPENDIX C: Pavement Design Calculations

FLEXIBLE PAVEMENT DESIGN

DESIGN DATA	SR LAND, LLC				
	HOMESTEAD NORTH AT STERI			1	
Travit 1 1 1 1	URBAN LOCAL LOW VOLUME		-		
•	8 kip) Single Axle Load Applications (ESAL): ES	$SAL(W_{18}) =$	36,500	
	ometer (R Value) Results:		R =	50	
Standard Dev			S _o =	0.45	
Loss in Servi	ceability	_	∆psi =	2.0	
Reliability]	Reliability =	80	
Reliability (z-	-		Z _R =	-0.84	
Soil Resilient	Modulus		$M_R =$	13168	
Weighted Str	uctural Number (WSN):			WSN =	1.46
DESIGN TABLES A	ND EQUATIONS				
·		Reliability (4	%) Z a (7-9	statistic)	
$S_1 = [(R - 5) / 11.2]$	-	80).84	
$M_R = 10^{I(S_1 + 18.72)/6}$	5 24]	85		.04	
		90		.28	
k = M _R /19.4		93		.48	
		94			
Where:		95		.65	
M _R = resilient mod	lulus (psi)	96		.75	
S_1 = the soil suppo	ort value	97		.88	
R = R-value obtair	ned from the Hveem stabilometer	98		.05	
CBR = California I		99		.33	
		99.9	-3	.09	
		99.99	-3	.75	
log ₁₀ ₩ ₁₈ = Z _R * S _O +	- 9.36*log ₁₆ (SN+1) - 0.20 +	$\log_{10} \left[\begin{array}{c} \Delta \ Ps \\ 4.2 \\ 1094 \end{array} \right]$	1.5 •	2.32*юg,,,	1 _R - 8.07

 $0.40 + \frac{1094}{(SN+1)^{5.19}}$

)7 10¹⁴¹R

Left	Right	Difference
4.56	4.56	0.0

DESIGN CALCULATIONS

DESIGN DATA SR LAND, LLC HOMESTEAD NORTH AT STERLING RANCH FILING NO. 1 URBAN LOCAL LOW VOLUME - SOIL TYPE A

Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL =	36,500
Hveem Stabilometer (R Value) Results:	R =	50
Weighted Structural Number (WSN):	WSN =	1.46

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.11$ Strength Coefficient - Aggregate Basecourse

D₁ = Depth of Asphalt (inches) D₂ = Depth of Basecourse (inches)

FOR FULL DEPTH ASPHALT SECTION (currently not allowed)

 $D_i = (WSN)/C_i = 3.3$ inches of Full Depth Asphalt Use 5.0 inches Full Depth

FOR ASPHALT + AGGREGATE BASECOURSE SECTION

Asphalt Thickness (t) = 3 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 1.3$ inches of Aggregate Basecourse, use 6.0 inches USE 6 INCHES MINIMUM.

RECOMMENDED ALTERNATIVES

- 1. 3.0 inches of Asphalt + 6.0 inches of Aggregate Basecourse, or
- 2. 5.0 inches of Asphalt

DESIGN CALCULATIONS

RECYCLED CONCRETE SECTIONS

DESIGN DATA SR LAND, LLC HOMESTEAD NORTH AT STERLING RANCH URBAN LOCAL LOW VOLUME - SOI TYPE A

Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL =	36,500
Hveem Stabilometer (R Value) Results:	R =	50
Weighted Structural Number (WSN):	WSN =	1.46

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.11$ Strength Coefficient - Recycled Concrete

 $D_1 = Depth of Asphalt (inches)$

 $D_2 = Depth of Recycled Concrete (inches)$

FOR ASPHALT + CEMENT STABILIZED SUBGRADE SECTION

Asphalt Thickness (t) = 3 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 1.3$ inches of Recycled Concrete Recycled Concrete, Use 6.0 inches minimum

RECOMMENDED ALTERNATIVES

1. 3.0 inches of Asphalt + 6.0 inches of Recycled Concrete

FLEXIBLE PAVEMENT DESIGN

DESIGN DATA SR LAND, LLC HOMESTEAD NORTH AT STERLING RANCH FILING NO. 1 **URBAN LOCAL - SOIL TYPE A** Equivalent (18 kip) Single Axle Load Applications (ESAL): $ESAL(W_{18}) =$ 292,000 Hveem Stabilometer (R Value) Results: 50 R = Standard Deviation $S_{o} =$ 0.45 Loss in Serviceability ∆psi = 2.0 Reliability Reliability = 80 Reliability (z-statistic) $Z_R =$ -0.84 Soil Resilient Modulus $M_R =$ 13168 Weighted Structural Number (WSN): WSN = 2.10 **DESIGN TABLES AND EQUATIONS** Reliability (%) Z_R (z-statistic) $S_1 = [(R - 5) / 11.29] + 3$ 80 -0.84 $M_R = 10^{[(S_1 + 18.72)/6.24]}$ 85 -1.04 90 -1.28 $k = M_R / 19.4$ 93 -1.48 94 -1.56 Where: 95 -1.65 M_R = resilient modulus (psi) 96 -1.75 S₁ = the soil support value 97 -1.88 98 -2.05 R = R-value obtained from the Hyeem stabilometer 99 -2.33 CBR = California Bearing Ratio **99.9** -3.09 99.99 -3.75

$$\log_{10}W_{16} = Z_{R}^{*}S_{O}^{+} 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\frac{4.2 - 1.5}{4.2 - 1.5}\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R}^{-} 8.07$$

Left	Right	Difference
5.47	5.47	0.0

DESIGN CALCULATIONS

DESIGN DATA SR LAND, LLC HOMESTEAD NORTH AT STERLING RANCH FILING NO. 1 URBAN LOCAL - SOIL TYPE A

Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL =	292,000
Hveem Stabilometer (R Value) Results:	R =	50
Weighted Structural Number (WSN):	WSN =	2.10

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.11$ Strength Coefficient - Aggregate Basecourse

 D_1 = Depth of Asphalt (inches) D_2 = Depth of Basecourse (inches)

FOR FULL DEPTH ASPHALT SECTION (currently not allowed)

 $D_1 = (WSN)/C_1 = 4.8$ inches of Full Depth Asphalt Use 5.0 inches Full Depth

FOR ASPHALT + AGGREGATE BASECOURSE SECTION

Asphalt Thickness (t) = $\boxed{3}$ inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 7.1$ inches of Aggregate Basecourse, use 8.0 inches USE 8 INCHES MINIMUM.

RECOMMENDED ALTERNATIVES

- 1. 3.0 inches of Asphalt + 8.0 inches of Aggregate Basecourse, or
- 2. 5.0 inches of Asphalt

DESIGN CALCULATIONS

RECYCLED CONCRETE SECTIONS

DESIGN DATA SR LAND, LLC HOMESTEAD NORTH AT STERLING RANCH URBAN LOCAL - SOI TYPE A

Equivalent (18 kip) Single Axle Load Applications (ESAL):	ESAL =	292,000
Hveem Stabilometer (R Value) Results:	R =	50
Weighted Structural Number (WSN):	WSN =	2.10

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.11$ Strength Coefficient - Recycled Concrete

D₁ = Depth of Asphalt (inches) D₂ = Depth of Recycled Concrete (inches)

FOR ASPHALT + CEMENT STABILIZED SUBGRADE SECTION

Asphalt Thickness (t) = 3 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 3.8$ inches of Recycled Concrete Recycled Concrete, Use 8 inches minimum

RECOMMENDED ALTERNATIVES

1. 3.0 inches of Asphalt + 8.0 inches of Recycled Concrete