

Master Development Drainage Plan and Preliminary Drainage Report

Peerless Farms 16975 Falcon Hwy Peyton, CO 80831

Prepared for (Owner):

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Prepared: November 13th, 2023





Master Development Drainage Plan and Preliminary Drainage Report

Peerless Farms – El Paso County, Colorado

CERTIFICATION

ENGINEERS STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

SIGNATURE (Affix Seal): Mitchell Hess, Colorado F DEVELOPER'S STATEMENT	P.E. No. 53916 53916 7.E. No. 53916
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I, the owner/developer have read and will comply widrainage report and plan. Robert williams	th all of the requirements specified in this
Name of Developer Robert Williams 1/4/24 AF42CBD1A97948D	
Authorized Signature Date	•
Robert Williams	
	<u>-</u>
Printed Name	
Owner	
Title	
16975 Falcon Hwy	
Peyton, CO 80831	
Address:	•
EL PASO COUNTY	
Filed in accordance with the requirements of the Dra Paso County Engineering Criteria Manual and Land	
Joshua Palmer, P.E.	Date
County Engineer / ECM Administrator	Date
County Engineer / Low Administrator	
Conditions:	



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INTRODUCTION

PURPOSE AND SCOPE OF STUDY

The purpose of this final drainage report is to outline the drainage facilities for 16975 Falcon Hwy Peyton, CO (the "Property"), El Paso County, Colorado (the "County"). This final drainage report identifies drainage patterns and infrastructure for the Site and proposes to safely route storm water to adequate outfalls. The Property is 40 acres in size.

The Property is loca Squirrel Creek. The S dated May 2009 and KHA Response: Revised to one single family home and associated accessory structure.

inage basin and is tributary to Black
Basin Drainage Basin Planning Study,

Verify with LOI, as it states in one section that it is one house and an accessory building.

GENERAL PROJECT DESCRIPTION

The project improvements consist of the construction of a single public road (60' ROW), two private driveways, and private utilities (the "Project") within the Property (the "Site"). The Project will be processed through El Paso County.

The Project is located in a portion of the northwest quarter of Section 13, Township 13 south, Range 64 west of the 6th P.M., County of El Paso, State of Colorado (see Vicinity Map in Appendix A). More specifically, the site is located at 16975 Falcon Hwy Peyton, CO 80831. The Property is bound by Falcon Hwy to the north, privately owned pastures to the west and south, and Sagecreek South Filing No. 1 to the east. The Property is mostly vacant but contains two single family houses, one large barn and some small chicken coops and sheds. The Site is to be replatted as 7 individual lots approximately 5-6 acres each with two private driveways connected to a public access road branching from Falcon Hwy. Stormwater will ultimately outfall to Black Squirrel Creek after initially discharging into an unnamed vegetated creek along the western portion of the Property.

A field survey was completed by Centennial Surveying, dated January 2021, and is the basis for design for the drainage improvements.

PROJECT CHARACTERISTICS

The Project Site is 40 acres in size. The Project involves the construction of a public road with two private driveways, roadside ditches, and culverts. The Site will be subdivided into large-lot residential lots for future single-family residences. The proposed impervious area consists of 0.66 acres for the public/paved roadway in addition to any future single-family residences constructed as part of the development.

The existing Project Site generally slopes from east to west as well as from the southeast to the north at grades of approximately 1.5 - 3.5%. The historical drainage patterns will be generally maintained. The Site consists of two single-family homes, a large barn and some small chicken coops and sheds. The Site does not have any existing stormwater infrastructure with the exception of a 24" culvert beneath Falcon Highway that allows the unnamed drainageway to drain from the north side of Falcon Highway to the Site.

Provide a culvert analysis of existing culvert to show what happens/overtops during major storm.

KHA Response: An excerpt from the regional DBPS has done this analysis and states that in the major storm, overtopping is expected with the full basin buildout. This excerpt is included in the Appendix.



DRAINAGE BASIN PLANNING STUDY INFRASTRUCTURE AND ANALYSIS

The Project Site is contained within the Haegler Ranch Basin and is discussed within the DBPS. Haegler Ranch Drainage Basin consists of 16.6 square miles in unincorporated EI Paso County. The basin mostly consists of residential lots greater than 2-acres in size and large agricultural parcels. According to the DBPS, "...the subregional detention alternative is preferred and recommended for implementation" as the drainage basin continues to develop and more dense zoning uses are developed. The DBPS does not recommend that a subregional detention basin be constructed on the subject Site. The DBPS recommends that the existing storm drain culvert that is beneath Falcon Highway which discharges stormwater onto the property be upsized to a 66" RCP Culvert. As no improvements are proposed for Falcon Highway, this culvert will not be upsized as part of this Project. KHA Response: A soils table has been added to

SOILS CONDITIONS

NRCS soil data is available for this Site and it has been noted that onsite soils are primarily USCS Type A. The NRSC Soils map has been provided in Appendix B.

State what soil types are present.

this report.

DRAINAGE DESIGN CRITERIA

REGULATIONS

The proposed development does not propose any deviations from The City of Colorado Springs/El Paso County Drainage Criteria Manual, dated October 12, 1994 or any subsequent revisions.

DEVELOPMENT DESIGN CRITERIA REFERENCE AND CONSTRAINTS

The custom Flood Insurance Rate Map (FIRM) map listed in Appendix B shows the western portion of the Site to be located inside the 100-year flood plain. The proposed private storm facilities follow The City of Colorado Springs/El Paso County Drainage Criteria Manual (the "CRITERIA"), El Paso County Engineering Criteria Manual (the "ECM), and the Urban Storm Drainage Criteria Manual (the "MANUAL"). Site drainage is not significantly impacted by constraints such as utilities or existing development. Further detail regarding onsite drainage patterns has been provided in the Proposed Drainage Conditions Section.

HYDROLOGIC CRITERIA

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per Chapter 6 of the CRITERIA. Table 6-2 of the CRITERIA is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the CRITERIA and MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the CRITERIA by calculating weighted impervious values for each specific site sub-basin.

HYDRAULIC CRITERIA

The proposed drainage facilities are designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using a custom FIRMette map by FEMA and information provided in the CRITERIA. Results of hydraulic calculations are summarized in Appendix D.



VARIANCES FROM CRITERIA

Due to existing grades and to match the historical flows presented at the Site, some drainage will be directed back to the county ROW. This is an existing condition. Besides this condition, no variances from the CRITERIA have been proposed for this development.

EXISTING DRAINAGE CONDITIONS

EXISTING DRAINAGE BASIN

Sub-Basin EX1

Sub-basin EX1 is 35.36 acres with a basin impervious value of 2% and consists of agricultural fields, gravel driveways, single-family residences and multiple agricultural barns and sheds. The existing runoff within this sub-basin drains directly to the unnamed drainageway. Runoff during the 5-year and 100-year storm events is anticipated to be 5.99 and 38.94 cfs respectively. The total 100-year storm event direct runoff value (5-year values are unknown for T3-02 and T4), inclusive of the upstream Sub-Basins EX3, EX3B, EX2, T3-02 and T4 is 1,097.15 cfs. Refer to the Existing Drainage Map for the location of the design points associated with the upstream sub-basins.

Sub-Basin EX2

Sub-basin EX2 is 4.64 acres with a basin impervious value of 4% and consists of agricultural fields, gravel driveways and a portion of an agricultural barn. The existing runoff within this sub-basin drains to an existing roadside ditch within Sub-Basin EX3 before flowing into the unnamed drainageway. Runoff during the 5-year and 100-year storm events is anticipated to be 1.03 and 6.07 cfs respectively.

Sub-Basin EX3

Sub-Basin EX3 consists of a portion of the northern property frontage within the ROW that drains to the property. Sub-Basin EX3 is 2.63 acres with a basin impervious value of 27% and 5-year and 100-year storm event direct runoff values of 2.18 and 7.47 cfs respectively. Total 5-year and 100-year storm event direct runoff values, inclusive of the upstream Sub-Basins EX2 and EX3B (Design Point EX2 and EX3B flows), are 5.35 and 28.21 cfs respectively.

Sub-Basin EX3B

Sub-Basin EX3B is an offsite sub-basin which consists of the south half of Falcon Highway and the west half of Peerless Farms Road adjacent to Lot 1 of Sagecreek South Filing No. 1 as well as all of Lot 1. Stormwater runoff within Sub-Basin EX3B flows into the Falcon Highway ROW before flowing west to Sub-Basin EX3. Sub-Basin EX3B is 5.97 acres with a basin impervious value of 9% and 5-year and 100-year storm event direct runoff values of 2.14 and 14.67 cfs respectively.

Sub-Basin T3-02

Sub-Basin T3-02 consists of a named tributary discussed in the DBPS and is made up of Sub-Basins HR0290 and HR0300. Sub-Basin T3-02 is 289 acres in size and consists of agricultural/vacant land and large-lot single-family residential properties. A sub-basin impervious value was not identified in the DBPS for this area, but the 100-year storm event direct runoff was



found to be 460 cfs. Stormwater runoff within Sub-Basin T3-02 will continue to follow its historical path.

Sub-Basin T4

Sub-Basin T4 consists of a named tributary discussed in the DBPS and is made up of Sub-Basins HR0260, HR0270 and HR0280. Sub-Basin T4 is 350 acres in size and consists of agricultural/vacant land and large-lot single-family residential properties. A sub-basin impervious value was not identified in the DBPS for this area, but the 100-year storm event direct runoff was found to be 570 cfs. Stormwater runoff within Sub-Basin T4 will continue to follow its historical path.

Sagecreek South Drainage

As part of the Project drainage design, the Sagecreek South Drainage Final Drainage Report was reviewed and an onsite field visit was conducted. To the best of our knowledge, it appears that when the Sagecreek South Subdivision was constructed, grading at the western fence line/property line was done such that stormwater is not anticipated to drain directly from the Sagecreek South residential lots directly onto the Peerless Farms Property. Instead, stormwater runoff is anticipated to flow north to the Falcon Highway roadside ditch. A portion of these flows will enter Sub-Basin EX3 and eventually will flow onto the Peerless Farms Property. This Sagecreek South Subdivision related sub-Basin has been identified as Sub-Basin EX3B. The remaining flows from Sagecreek South Subdivision flow east or south, away from the Site. This drainage condition will remain the same in the proposed drainage condition, except a proposed stormwater culvert will be installed as part of the proposed extension of Sagecreek Road in order for flows to continue to follow their historic path.

PROPOSED DRAINAGE CONDITIONS

The developed runoff from the Project will generally be collected by means of roadside ditches located adjacent to the proposed public road and private gravel driveways. The runoff collected in the roadside ditches will be conveyed to the unnamed drainageway, following historical runoff patterns. The Property has been divided into 8 on-site sub-basins, Sub-Basins 1 - 8 and 3 off-site sub-basins, Sub-Basin EX3, Sub-Basin T3-02 and Sub-Basin T4. The proposed conditions map is provided in Appendix H.

KHA Response: Revised.

Sub-Basin 1

Sub-basin 1 is 19.97 acres with a basin impervious value of 10% and consists of the unnamed drainageway as well as future single-family residential lots. The runoff developed within this sub-basin drains directly to the unnamed drainageway. Developed runoff during the 5-year and 100-year storm events will be 6.21 and 27.04 cfs respectively. Stormwater runoff within Sub-Basin 1 will continue to generally follow its historical path. The total 100-year storm event direct runoff value (5-year values are unknown for T3-02 and T4), inclusive of the upstream Sub-Basins 2 – 8, EX3, EX3B, T3-02 and T4 is 1,115.63 cfs. Refer to the Proposed Drainage Map for the location of the design points associated with the upstream sub-basins.

Sub-Basin 2

Sub-basin 2 is 1.78 acres with a basin impervious value of 17% and consists primarily of a portion of a gravel driveway and driveway drainage ditch. Sub-Basin 2 also includes a small portion of the proposed public road. The runoff developed within this sub-basin will be collected within a proposed driveway ditch before flowing into the unnamed drainageway. Developed runoff during the 5-year and 100-year storm events will be 0.87 and 3.24 cfs respectively. Stormwater runoff within Sub-Basin 2 will continue to generally follow its historical path. Total 5-year and 100-year



→4 off-site basins, EX3B,

storm event direct runoff values, inclusive of the upstream Sub-Basin 3 (Design Point 3 flows), are 1.73 and 5.72 cfs respectively.

Sub-Basin 3

Sub-basin 3 is 0.78 acres with a basin impervious value of 31% and consists primarily of a portion of a gravel driveway and driveway drainage ditch. Sub-Basin 3 also includes a small portion of the proposed public road. The runoff developed within this sub-basin will be collected within a proposed driveway ditch before flowing into a drainage ditch within Sub-Basin 2 and being routed to the unnamed drainageway. Developed runoff during the 5-year and 100-year storm events will be 0.86 and 2.48 cfs respectively. Stormwater runoff within Sub-Basin 3 will continue to generally follow its historical path. Include discussion of culvert

4 with location

KHA Response: Flow through Culvert described added to sub-basin description.

Sub-Basin 4

Sub-basin 4 is 0.42 acres with a basin impervious value of 57% and consists of a portion of the proposed public road. The runoff developed within this sub-basin will be collected within a proposed roadside ditch before flowing into a driveway ditch within Sub-Basin 6 and being routed to the unnamed drainageway. Developed runoff during the 5-year and 100-year storm events will be 1.03 and 2.21 cfs respectively. Stormwater runoff within Sub-Basin 4 will continue to generally follow its historical path. Include discussion of culvert

1 and 3 with locations

KHA Response: Flow through Culvert described added to sub-basin description.

Sub-Basin 5

Sub-basin 5 is 0.85 acres with a basin impervious value of 40% and consists of a portion of the proposed public road, a portion of a gravel driveway and a driveway ditch. The runoff developed within this sub-basin will be collected within proposed roadside and driveway ditches before flowing into a drainage ditch within Sub-Basin 6 and being routed to the unnamed drainageway. Developed runoff during the 5-year and 100-year storm events will be 1.12 and 2.84 cfs respectively. Stormwater runoff within Sub-Basin 5 will continue to generally follow its historical path. Include discussion of culvert

2 and 3 with locations

KHA Response: Flow through Culvert described added to sub-basin description.

an existing roadside ditch, but rather a low spot. Clarify, will any

increase inflows at the idischarge point cause flooding?

Sub-Basin 6

Sub-basin 6 is 5.55 acres with a basin impervious value of 13% and consists of a portion of a gravel driveway, a driveway ditch and future single-family lots. The runoff developed within this sub-basin will be collected within proposed roadside and driveway ditches before flowing into the unnamed drainageway. Developed runoff during the 5-year and 100-year storm events will be 2.32 and 9.26 cfs respectively. Stormwater runoff within Sub-Basin 6 will continue to generally follow its historical path. Total 5-year and 100-year storm event direct runoff values, inclusive of the upstream Sub-Basins 4 and 5 (Design Point 4 and 5 flows), are 4.47 and 14.31 cfs respectively. Include discussion of culvert

3 with location

KHA Response: Flow through Culvert described added to sub-basin description.

Sub-Basin 7

Sub-basin 7 is 1.57 acres with a basin impervious value of 6% and consists of a portion of the proposed public road, roadside ditches and a future single-family lot. The runoff developed within this sub-basin will be collected within an existing roadside ditch within Sub-Basin EX3 before flowing into the unnamed drain ageway. Developed runoff during the 5-year and 100-year storm events will be 0.54 and 2.77 cfs respectively. Stormwater runoff within Sub-Basin 7 will continue to follow its historical path.

Based on the contours on the CDs, there does not appear to be

Sub-Basin 8

Sub-basin 8 is 9.09 acres with a basin impervious value of 10% and consists of future single-family residential lots. The runoff developed within this sub-basin drains directly to the unnamed

KHA Response: The contours as displayed by the surveyed surface do not accurately reflect the condition of the roadside ditch. The ditch's ability to transmit flows has been confirmed by a site visit, and photos showing the subject area of the roadside ditch have been added to Appendix F as figures 9 & 10.

Kimley»Horn

drainageway. Developed runoff during the 5-year and 100-year storm events will be 3.14 and 13.65 cfs respectively. Stormwater runoff within Sub-Basin 8 will continue to generally follow its historical path.

Sub-Basin EX3

Sub-Basin EX3 consists of a portion of the northern property frontage within the ROW that drains to the property. Sub-Basin EX3 is 2.63 acres with a basin impervious value of 27% and 5-year and 100-year storm event direct runoff values of 2.18 and 7.47 cfs respectively. Stormwater runoff within Sub-Basin EX3 will continue to follow its historical path. Total 5-year and 100-year storm event direct runoff values, inclusive of the upstream Sub-Basin 7 and EX3B (Design Point 7 and EX3B flows), are 4.86 and 24.91 cfs respectively. Total flows within Sub-Basin EX3 will decline in the proposed condition due to less of the onsite flows flowing directly to Sub-Basin EX3.

Sub-Basin EX3B

Sub-Basin EX3B is an offsite sub-basin which consists of the south half of Falcon Highway and the west half of Peerless Farms Road adjacent to Lot 1 of Sagecreek South Filing No. 1 as well as all of Lot 1. Stormwater runoff within Sub-Basin EX3B flows into the Falcon Highway ROW before flowing west to Sub-Basin EX3. Sub-Basin EX3B is 5.97 acres with a basin impervious value of 9% and 5-year and 100-year storm event direct runoff values of 2.14 and 14.67 cfs respectively. Include discussion of culvert

5 with location

Sub-Basin 13-02

KHA Response: Flow through Culvert described added to sub-basin description.

Sub-Basin T3-02 consists of a named tributary discussed in the DBPS and is made up of Sub-Basins HR0290 and HR0300. Sub-Basin T3-02 is 289 acres in size and consists of agricultural/vacant land and large-lot single-family residential properties. A sub-basin impervious value was not identified in the DBPS for this area, but the 100-year storm event direct runoff was found to be 460 cfs. Stormwater runoff within Sub-Basin T3-02 will continue to follow its historical path.

Sub-Basin T4

Sub-Basin T4 consists of a named tributary discussed in the DBPS and is made up of Sub-Basins HR0260, HR0270 and HR0280. Sub-Basin T4 is 350 acres in size and consists of agricultural/vacant land and large-lot single-family residential properties. A sub-basin impervious value was not identified in the DBPS for this area, but the 100-year storm event direct runoff was found to be 570 cfs. Stormwater runoff within Sub-Basin T4 will continue to follow its historical path. KHA Response: Additional hydraulic

calculations and modeling based on

Sagecreek South Drainage minimum and maximum conditions has been added to the appendix. As part of the Project drainage Final Drainage Report was

site field visit was conducted. To the best of our knowledge, it appears that alculations are only shown for ek South Subdivision was constructed, final gradin KHA Response: These requirements do 2.5% slopes. Should use a min and max slope for each ditch to the Sagecreek South Subdivision lots to the Peerle determine velocity and depth.

not apply to roadside ditches, per the EPC ECM, which states:

PUBLIC ROADWAY AND PRIVATE DRIVEWAY DITCHES

Ditches have been proposed adjacent to the proposed public roadway gravel driveways. Ditches will be constructed to meet the require Standard Detail SD_2-11. Ditches are considered roadside ditches a ECM, are not considered drainage ditches and therefore are not requ standards. Ditch calculations for each applicable Sub-Basin/have bee Based on ditch slopes between 0.5% and 5% as well as mean ditch

3.3.4. **Drainage Ditches**

A.Application of Standards. A ditch located within a development, not including roadside ditches, that conveys less than 15 cubic feet per second of public drainage is considered a drainage ditch.

Kimley » Horn Per EOM section 3.3.4.B.2, ditch should have

freeboard of 0.5'

Per ECM section 3.3.4.B. minimum ditch slope is

2.87 and 4.48 ft/s, ditches will be seeded/lined with either Bermudagrass, Reed Canary Grass or Tall Fescue Grass.

PUBLIC ROADWAY AND PRIVATE DRIVEWAY CULVERTS

Reinforced Concrete Pipes (RCP) and Concrete Flared-End Sections (FES) have been proposed as necessary where proposed public roadway or private gravel driveways intersect with roadside ditches. Culvert calculations have been included in Appendix D. Culverts range in size from 18-inches to 24-inches depending on the proposed stormwater runoff that will pass through the culvert in the 100-year storm event. Riprap will be provided at both ends of culverts. Riprap has been sized for the culvert with the highest flows and this size and type of riprap will be used on both ends of each culvert (18" thick Type L Riprap D50 = 9"). Riprap calculations have been included in Appendix D and a standard culvert detail for the riprap has been included on the Grading and Erosion Control Plans.

CONFORMANCE WITH THE DBPS

The proposed Project includes single-family lots which are all greater than 5-acres in size. The proposed Site imperviousness for the Project, inclusive of the proposed public road) is 12%. Individual lots will be limited to up to 10% imperviousness. The 5-year and 100-year storm event direct runoff for the site will be 16.08 and 63.49 cfs respectively. The proposed development is in general conformance with the DBPS and will not negatively affect downstream drainage.

EMERGENCY OVERFLOW ROUTING

All overflow routing will be directed to the existing unnamed drainageway that is located on the western side of the site. This flow path matches the historical stormwater runoff path.

HYDRAULIC ANALYSIS METHODOLOGY

The proposed drainage facilities were designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using a custom FIRMette map by FEMA and information provided in the CRITERIA. Apart from road culverts, no underground storm drain pipes as proposed for the development. Culvert sizing calculations were computed using Flow master and are included in Appendix D. There are no proposed variances from the City of Colorado Springs/El Paso County Criteria for the proposed development.

No inlets have been proposed as part of the Project. Stormwater runoff will be routed above ground through roadside ditches and culverts beneath the public roadway and private driveways.

Four-Step Process

The Site was designed in accordance with the four-step process to minimize adverse impacts of urbanization, as outlined in Section I.7.2 BMP Selection of the CRITERIA. The four-step process per the CRITERIA provides guidance and requirements for the selection of siting of structural Best Management Practices (BMPs) for new development and significant redevelopment.

Step 1: Employ Runoff Reduction Practices

Currently the site is mostly vacant land. Development of the site will increase current runoff conditions due to increased imperviousness values. The increase in impervious area is minimal though due to the Site size of 40-acres and the proposed large residential lot sizes.

As discussed in Section I.7.1B of Appendix I of the ECM, water-quality facilities are not required for the Project as the development consists of 5-acre residential lots. Water quality treatment will be provided for the Proposed Public ROW though through means of runoff



reduction. Stormwater within the Public ROW will drain to vegetated roadside ditches which will promote stormwater infiltration. A 94% WQVC reduction will be achieved to accomplish the requirements of the 60% Runoff Reduction Standard as outlined by the County's MS4. Calculations showing the runoff reduction amounts have been included in Appendix C.

The Site was designed to conserve as much of the existing vegetation as possible and to minimize the extent of paved areas. Additionally, the Site was designed to eliminate underground storm drains and storm drain culverts will only be used to route water beneath the public road and private driveways, allowing more opportunities for stormwater to infiltrate into the ground.

Step 2: Stabilize Drainageways

An existing unnamed drainageway flows through the western portion of the Site. During a Site visit, it was found that the drainageway is currently well-stabilized and extremely vegetated. Site visit photos of the drainageway have been included in Appendix F. As the drainageway is currently stable and the development of the large-lot subdivision will only minimally increase the stormwater runoff it has been determined that leaving the unnamed drainageway as-is. currently stabilized and vegetated, will allow the channel to remain stabilized. As discussed in the DBPS, "The disturbance of the native vegetation and failure to properly revegetate areas impacted by site development, utility, roadway and landscape construction activities have in some cases negatively affected downstream areas." Furthermore, as noted in Chapter 1, Section 1.4 of the CRITERIA, "Natural channel systems, primarily the designated Major Drainageways and Primary outfalls, serve to store flood waters, enhance water quality, provide for ground water recharge and preserve riparian corridors. The use of historical channels to convey storm water runoff from developed and developing areas is acceptable. However, if historical storm water flows are increased, or if historical channels are unstable in their natural conditions, these channels must be adequately stabilized to prevent excessive erosion." Additionally, Chapter 2, Section 2.2 of the CRITERIA states, "A stable natural channel reaches 'equilibrium' over many years. Therefore, channel modifications should be minimal." Because the existing drainageway is properly stabilized, it is felt that attempts to change the natural channel may lead to destabilization of the drainageway and therefore, no changes to the unnamed drainageway, with the exception of stabilization at the location of the proposed ditches, are recommended.

The proposed Project involves construction of roadside ditches which will discharge into the unnamed drainageway. To reduce the opportunity for erosion where the ditches outfall, riprap will be added to dissipate energy from stormwater runoff.

Step 3: Provide Water Quality Capture Volume (WQCV)

The proposed Project development includes large-lot single-family lots which include minimal impervious areas. The single-family lots will be restricted to a maximum impervious value of 10% per lot. Lots 2, 6 and 7 include private/shared gravel driveways which will count towards the 10% maximum impervious allotment of those lots. As all of the lots are built out with future impervious coverings such as houses, out-buildings, driveways, sidewalks and patios, impervious values for each lot will be considered up to a maximum of 10% for each lot. As discussed above in Step 1, the residential lots are exempt from WQCV requirements and the Public ROW will meet County MS4 requirements by using runoff reduction methods which will meet the 60% runoff reduction standard.

Step 4: Consider Need for Industrial and Commercial BMPs

The proposed Project consists of a single-family subdivision. No industrial and commercial uses or developments are anticipated as part of the proposed development.



WATER QUALITY AND DETENTION REQUIREMENTS

The proposed Project development includes large-lot single-family lots which include minimal impervious areas. As discussed above in Step 1 of the Four-Step Process, the residential lots are exempt from WQCV requirements and the Public ROW will meet County MS4 requirements by using runoff reduction methods which will meet the 60% runoff reduction standard.

The Project does not include a proposed detention pond for this development. Large-Lot Residential Developments, especially those in excess of 5-acre lots, do not increase post-development stormwater flows as substantially as smaller-lot residential and non-residential developments. Stormwater flows collected from this development will drain to the existing unnamed drainageway. As documented in the DBPS, the unnamed drainageway is made up of the combination of the T3-02 and T4 Tributaries which both cross Falcon Highway using corrugated metal pipes known as Facility Numbers 609 and 610. The proposed 100-year flows for these tributaries at these locations are 460 cfs and 570 cfs respectively. Therefore, the unnamed drainageway is expected to have proposed 100-year storm event flows of 1,030 cfs.

The Project currently contributes 7.02 cfs and 45.01 cfs to the unnamed drainageway during the 5-year and 100-year storm events respectively, and it is proposed that 16.08 cfs and 63.49 cfs will discharge to the unnamed drainageway in the redeveloped condition and during the 5-year and 100-year storm events respectively. During a 100-year storm event, the existing stormwater flows for the Site account for 4.37% of the total flows in the unnamed drainageway (45.01 cfs of 1,030 cfs). During a 100-year storm event, the proposed stormwater flows for the Site will account for 6.16% of the total flows in the unnamed drainageway (63.49 cfs of 1,030 cfs) which results in an increase of only 1.79%. All flows do not flow directly through the site some

Because the unnamed drainageway flows directly through the Site, it is advantageous to allow stormwater from the Project to flow directly and undetained into the unnamed drainage as the flows/suitable

KHA Response: The contours as displayed by the surveyed surface do not accurately reflect the condition of the roadside ditch. The ditch's ability to transmit flows has been confirmed by a site visit, and photos showing the subject area of the roadside ditch have been added to Appendix F as figures 9 & 10.

geway and flow downstream before outfall for arrive at this area of the drainage that basin because it lower numbered sub-basins located these sub-basins are 11, 23, 42, 17 different

and 31 minutes respectively. The three proposed sub-basins for the Project which contribute the largest peak flows are also the three sub-basins with the longest time of concentrations. Each of location. these sub-basins, 1, 6 and 8 also drain directly into the unnamed drainageway. Their time of concentrations are 39.28, 29.41 and 33.25 minutes respectively. Based on these time of concentrations being leach that the largest that the largest location in the largest peak flows and percentage increase relative to the largest which contribute the discharge largest peak flows are also the three sub-basins with the longest time of concentrations. Each of location.

and the fact that the leftows and percentage increase relative stormwater to arrive at what is planned for in the DBPS is all representations of the project will allow the paragraphs ing stormwater flows on

nt for channel flow times for the detaining stormwater flows for this stormwater flows from the overall e in a private extended detention of the released at a later time which

basin, would negatively impact the channel as peak flows would be released at a later time which could coincide with the peak flows in the channel, allowing higher volumes and velocities in the unnamed drainageway.

State what the increase in flows is

and percentage increase.

Due to the minimal increase of stormwater flows caused by the redevelopment, the large 5-acre and larger residential lot configuration, the recommendations of the DBPS for regional detention ponds as opposed to private onsite detention, the negligible impact to the the site outfall. However, this will not be in flows in the unnamed drainageway, no stormwater detention has been place accurately model the conditions, for seven

Provide a channel calculation showing increased flows in major channel, does not have any adverse effects. A full model is not needed, just a simple single channel analysis showing what depth, velocities, etc will be.

The full build-out of the proposed sub-bas addition of our sites increase in flows did relative to full buildout). However, upstrea Falcon Highway, and details of downstrea channel. Additionally, exact hydrologic co report, and is not in the full buildout condi

section of the public road does not flow directly to the finamed drainageway but rather flow to a low spot along Falcon Highway. Discuss any increase in flows/suitable outfall for that basin because it

KHA Response: GEC & CSWMP submitted Master Develo

ment Drainage Plan and Preliminary Drainage Report

Peerless Farms El Paso County, Colorado GEC plans & SWMP need to be

provided

EROSION CONTROL PLAN

Erosion Control Plans will be submitted separately as a standalone construction document. During construction temporary control measures will be installed to reduce erosion onsite. The temporary controls are anticipated to consist, at a minimum, of silt fencing, vehicle tracking control, ditches, check dams, culvert protection, erosion control blankets, seeding and mulching and temporary sediment basins.

As part of the construction associated with this subdivision, two temporary sediment basins will be constructed to meet County MS4 and State requirements. Although the sediment basins will be temporary erosion controls, permanent ditches will be constructed which will route stormwater to the temporary sediment basins during construction and to the unnamed drainageway post-construction. The temporary sediment basins will be sized according to El Paso County Standard Detail 900-TSB-2. This standard detail has been included in Appendix E. Final sizing for the temporary sediment basins will be included in the Grading and Erosion Control Plans and Stormwater Management Plant.

FLOODPLAIN STATEMENT

The western portion of the Site is within Area AE, special flood hazard areas with base flood elevations and Zone X, 0.2% annual chance flood hazard, areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

The remaining portion of the Site is located outside of the 100-year floodplain as determined by the custom FIRMette map created on April 20, 2021 and contained with Appendix B.

FEES DEVELOPMENT

APPLICABLE FEES

Drainage and Bridge Fees are required to be paid at the time of Final Plat recording for the Project. The Site is within the Haeger Drainage Basin. Drainage Fees are based on the number of impervious acres for the development. The 2023 Drainage and Bridge Fees are \$12,985 and \$1,916, respective, per impervious acre.

Total Acreage (40-acres) x Total Development (inclusive of Prop. Public ROW) Impervious Value (12%) = Impervious Acres (4.8)

Update to 2024 Drainage and Bridge fees

Drainage Basins Fees = 4.8-acres x (\$12,985 + \$1,916) = \$71,524.80

KHA Response: Fees updated to 2024 and broken out to better display Basin and Bridge Fees and calculation.

,643.60

Include total bridge fees.

CONSTRUCTION COST OPINION

An opinion of probable construction cost for the construction of the private drainage facilities for the Project has been included in Appendix E. There are no public drainage ponds or permanent control measures proposed as part of the Project.

MAINTENANCE AND OPERATIONS

No detention has been proposed as part of this Project. The public roadside ditches and culverts within the proposed Public ROW which provide water quality treatment will be maintained by El



Paso County, upon acceptance. Other proposed ditches, swales and culverts located outside of the proposed Public ROW will be maintained by property owners of the development. Easements will be provided over the shared driveways and ditches to allow all property owners the ability to access and maintain ditches and culverts as needed.

GROUNDWATER CONSIDERATIONS

A Geotechnical Evaluation by RMG and dated 4/14/2021 was performed for the Site. According to the Geotechnical Evaluation, "Groundwater was encountered in all three test borings at depths ranging from between 11.0 feet to 18.0 feet below the existing ground surface at the time of boring. When checked five days subsequent to drilling, groundwater was encountered at depths ranging between 4.0 feet to 18.6 feet. Groundwater levels are anticipated to have sufficient separation from the bottom of proposed crawlspace and basement foundation components on Lots 2, 4, 6 and 7. Due to the shallow groundwater conditions encountered near the unnamed intermittent creek, the use of basements on Lots 1 and 5 may be limited. Groundwater conditions should be considered in the site-specific soils investigations and OWTS designs."

SUMMARY

COMPLIANCE WITH STANDARDS

The drainage design presented within this report for the Peerless Farms Large-Lot Single-Family Development conforms to the City of Colorado Springs/El Paso County Storm Drainage Criteria and the Urban Drainage and Flood Control District Manual. Additionally, the Site runoff and private storm sewer facilities will not adversely affect the downstream and surrounding developments or waterways. This report and its findings are consistent with the drainage requirements documented in the DBPS. During construction at the Site, erosion control measures will be implemented as briefly discussed in the Erosion Control Plan Section above and as further detailed in the Grading and Erosion Control Plans and Stormwater Management Plan. The total anticipated project disturbance area for this Project as part of the proposed public road and site infrastructure is 7.3 acres.



REFERENCES

- 1. The City of Colorado Springs Drainage Criteria Manual, May 2014
- 2. El Paso County Drainage Criteria Manual, Vol. 1 and 2, October 1994
- 3. Urban Drainage and Flood Control District Drainage Criteria Manual (UDFCDCM), Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
- 4. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0553G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).
- 5. Haegler Ranch Basin Drainage Basin Planning Study. Prepared by URS, May 2009.
- 6. Geotechnical Evaluation prepared by RMG. April 14, 2021.



APPENDIX



APPENDIX A - VICINITY MAP





APPENDIX B - SOILS MAP AND FEMA FIRM PANEL





NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for El Paso County Area, Colorado



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

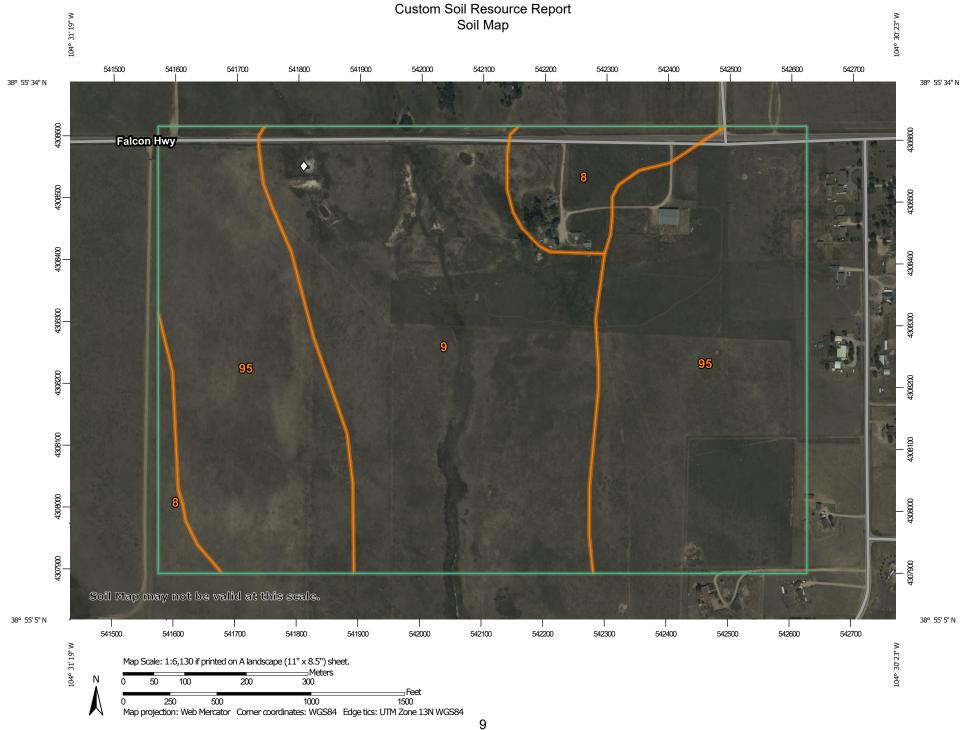
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) Spoil Area 1:24.000. Area of Interest (AOI) å Stony Spot Soils Very Stony Spot Warning: Soil Map may not be valid at this scale. Soil Map Unit Polygons Ŷ Wet Spot Soil Map Unit Lines Enlargement of maps beyond the scale of mapping can cause Other Δ misunderstanding of the detail of mapping and accuracy of soil Soil Map Unit Points line placement. The maps do not show the small areas of Special Line Features Special Point Features contrasting soils that could have been shown at a more detailed **Water Features** Blowout scale. ဖ Streams and Canals Borrow Pit Transportation Please rely on the bar scale on each map sheet for map Clay Spot measurements. Rails ---**Closed Depression** Interstate Highways Source of Map: Natural Resources Conservation Service Gravel Pit **US Routes** Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Gravelly Spot Major Roads Landfill Local Roads Maps from the Web Soil Survey are based on the Web Mercator 00 projection, which preserves direction and shape but distorts Lava Flow Background distance and area. A projection that preserves area, such as the Marsh or swamp Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. Mine or Quarry Miscellaneous Water This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Perennial Water Rock Outcrop Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 18, Jun 5, 2020 Saline Spot Sandy Spot Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Severely Eroded Spot Sinkhole Date(s) aerial images were photographed: Sep 11, 2018—Oct 20. 2018 Slide or Slip Sodic Spot The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	13.9	7.4%
9	Blakeland-Fluvaquentic Haplaquolls	75.0	39.7%
95	Truckton loamy sand, 1 to 9 percent slopes	99.9	52.9%
Totals for Area of Interest		188.9	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet

Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent

Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats

Landform position (three-dimensional): Side slope, talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Alluvium derived from sedimentary rock and/or eolian deposits

derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand

C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95

to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent Available water capacity: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R049XB210CO - Sandy Foothill

Hydric soil rating: No

Minor Components

Pleasant

Percent of map unit: 1 percent

Landform: Depressions Hydric soil rating: Yes

Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

9—Blakeland-Fluvaquentic Haplaquolls

Map Unit Setting

National map unit symbol: 36b6 Elevation: 3,500 to 5,800 feet

Mean annual precipitation: 13 to 17 inches Mean annual air temperature: 46 to 55 degrees F

Frost-free period: 110 to 165 days

Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 60 percent

Fluvaquentic haplaquolls and similar soils: 38 percent

Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats

Landform position (three-dimensional): Side slope, talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose and/or eolian deposits

derived from arkose

Typical profile

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand

C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95

to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent Available water capacity: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R049XB210CO - Sandy Foothill

Hydric soil rating: No

Description of Fluvaquentic Haplaquolls

Setting

Landform: Swales

Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

Typical profile

H1 - 0 to 12 inches: variable

Properties and qualities

Slope: 1 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.20 to 6.00 in/hr)

Depth to water table: About 0 to 24 inches

Frequency of flooding: Occasional Frequency of ponding: None

Maximum salinity: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)

Interpretive groups

Land capability classification (irrigated): 6w
Land capability classification (nonirrigated): 6w

Hydrologic Soil Group: D Hydric soil rating: Yes

Minor Components

Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent

Landform: Depressions Hydric soil rating: Yes

95—Truckton loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 36bd Elevation: 6,000 to 7,000 feet

Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 50 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Truckton and similar soils: 95 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Truckton

Setting

Landform: Hills, flats

Landform position (three-dimensional): Side slope, talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Arkosic alluvium derived from sedimentary rock and/or arkosic

residuum weathered from sedimentary rock

Typical profile

A - 0 to 8 inches: loamy sand Bt - 8 to 24 inches: sandy loam

C - 24 to 60 inches: coarse sandy loam

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.4 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R049XB210CO - Sandy Foothill

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 4 percent Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

Soil Information for All Uses

Soil Properties and Qualities

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Erosion Factors

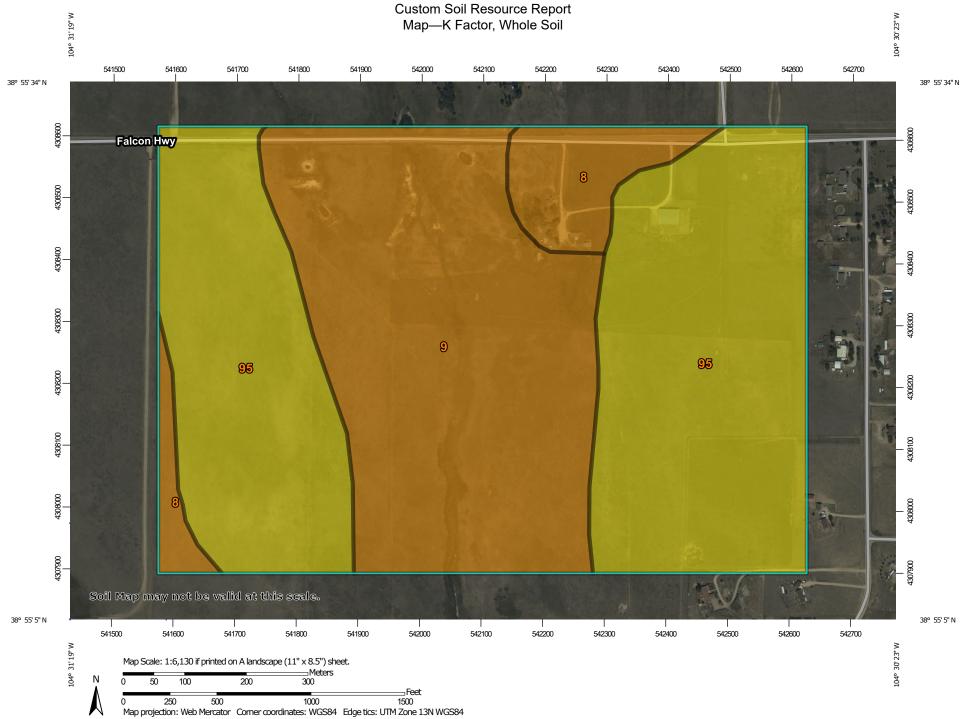
Soil Erosion Factors are soil properties and interpretations used in evaluating the soil for potential erosion. Example soil erosion factors can include K factor for the whole soil or on a rock free basis, T factor, wind erodibility group and wind erodibility index.

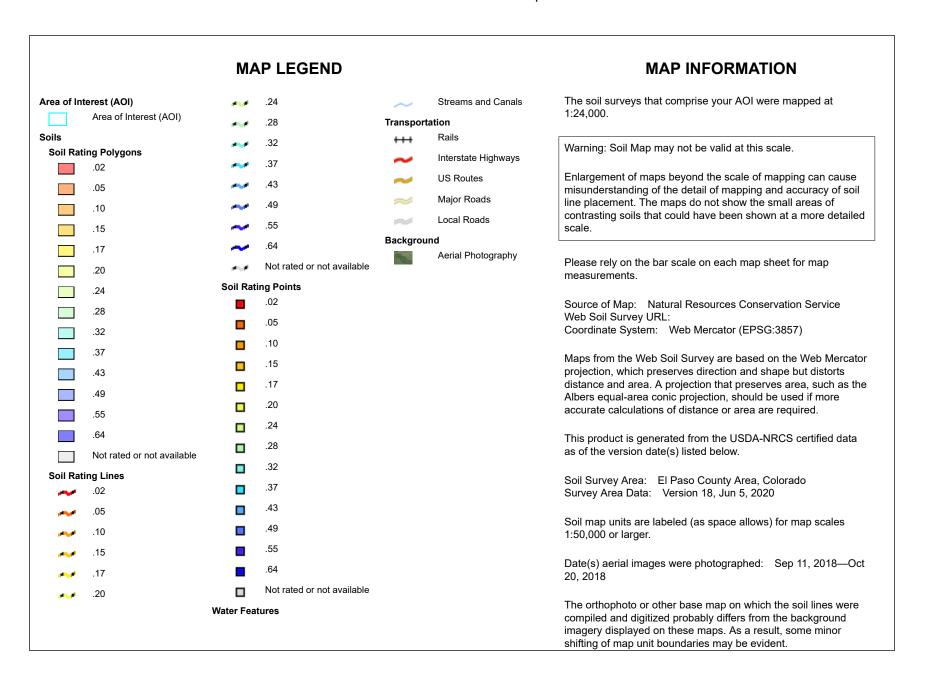
K Factor, Whole Soil

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Factor K does not apply to organic horizons and is not reported for those layers.





Table—K Factor, Whole Soil

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	.10	13.9	7.4%
9	Blakeland-Fluvaquentic Haplaquolls	.10	75.0	39.7%
95	Truckton loamy sand, 1 to 9 percent slopes	.17	99.9	52.9%
Totals for Area of Interes	st		188.9	100.0%

Rating Options—K Factor, Whole Soil

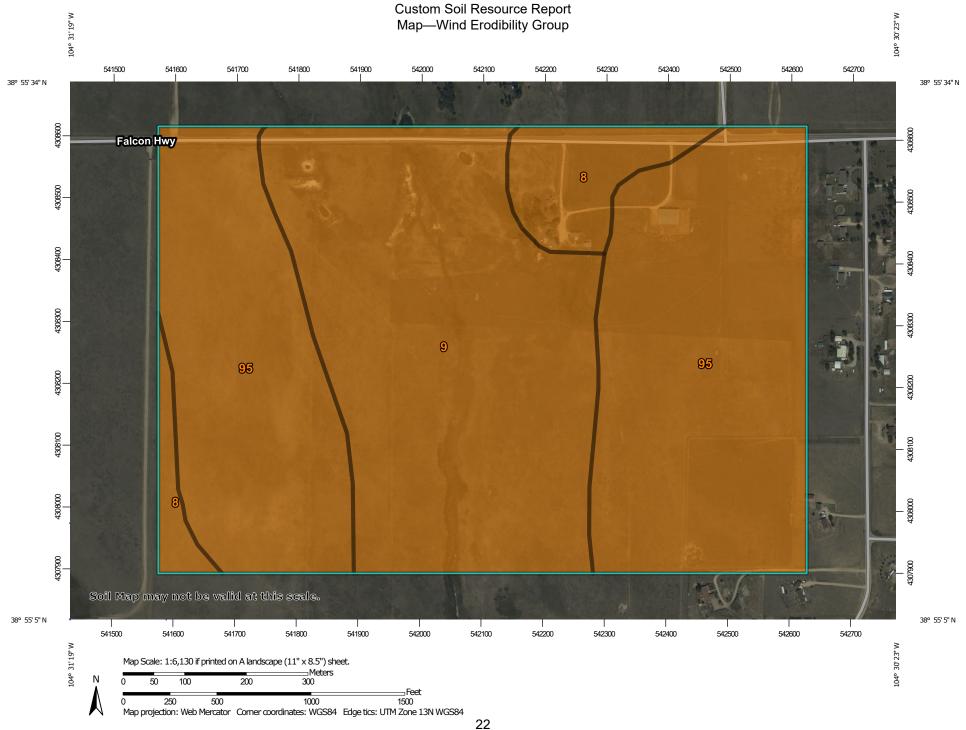
Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

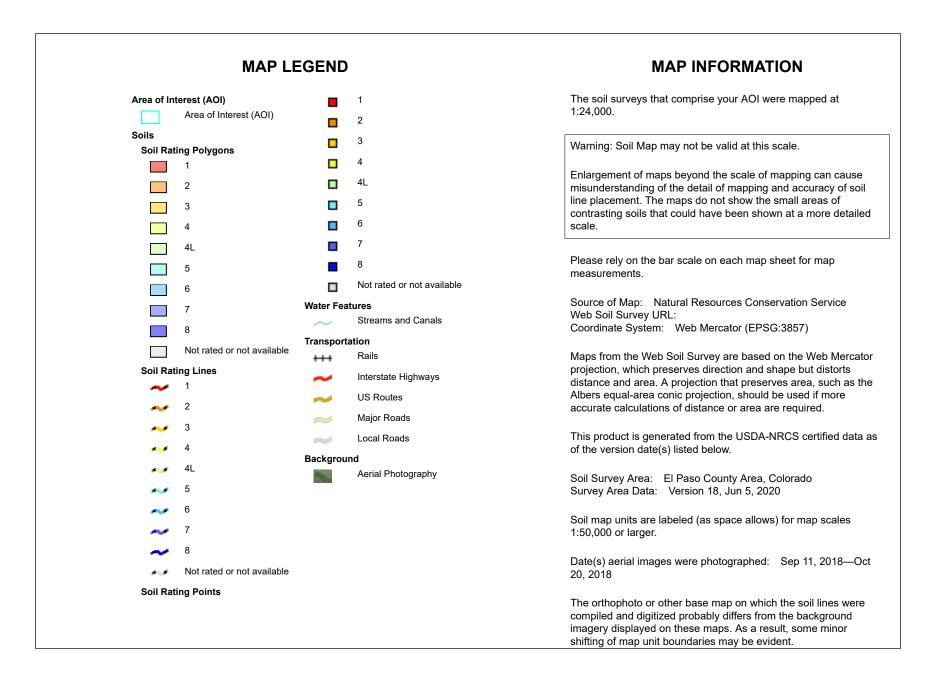
Tie-break Rule: Higher

Layer Options (Horizon Aggregation Method): Surface Layer (Not applicable)

Wind Erodibility Group

A wind erodibility group (WEG) consists of soils that have similar properties affecting their susceptibility to wind erosion in cultivated areas. The soils assigned to group 1 are the most susceptible to wind erosion, and those assigned to group 8 are the least susceptible.





Table—Wind Erodibility Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	2	13.9	7.4%
9	Blakeland-Fluvaquentic Haplaquolls	2	75.0	39.7%
95	Truckton loamy sand, 1 to 9 percent slopes	2	99.9	52.9%
Totals for Area of Interes	st		188.9	100.0%

Rating Options—Wind Erodibility Group

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Lower

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

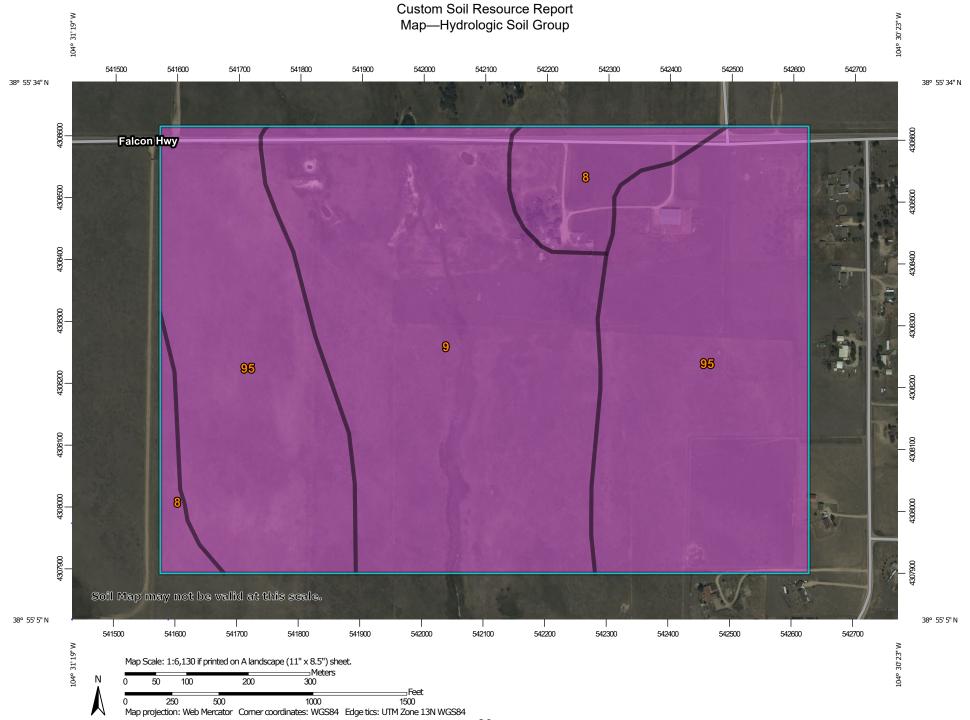
Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained

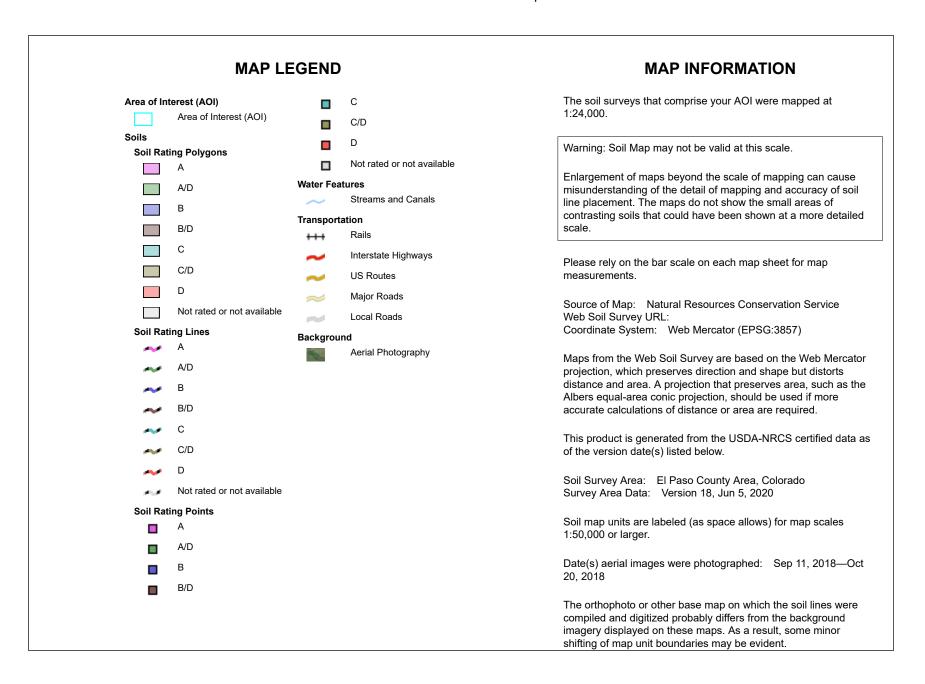
soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.





Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	А	13.9	7.4%
9	Blakeland-Fluvaquentic Haplaquolls	A	75.0	39.7%
95	Truckton loamy sand, 1 to 9 percent slopes	А	99.9	52.9%
Totals for Area of Interes	st	1	188.9	100.0%

Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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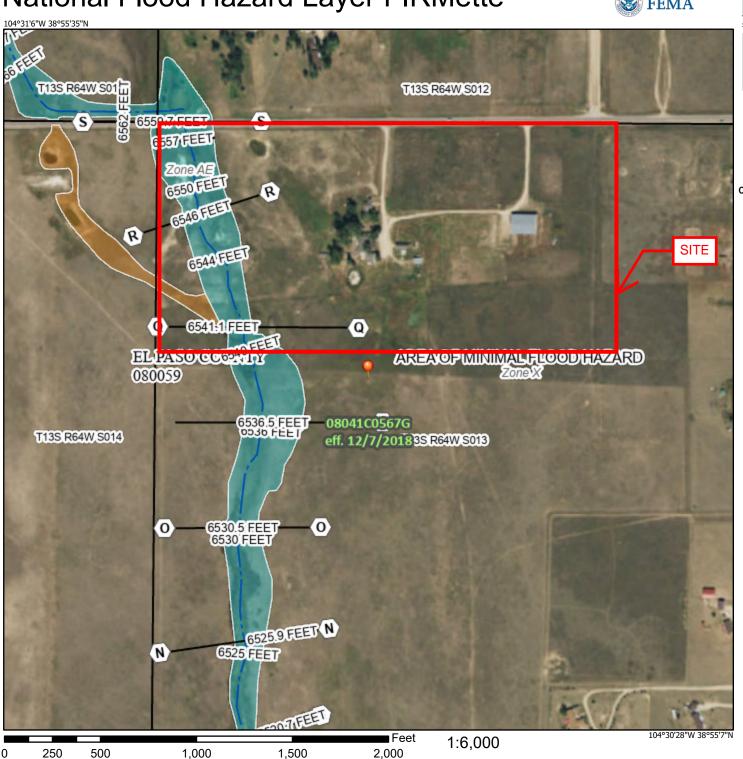
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National Flood Hazard Layer FIRMette

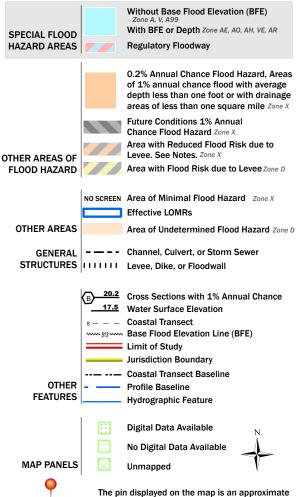


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/20/2021 at 4:13 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

Master Development Drainage Plan and Preliminary Drainage Report Peerless Farms – El Paso County, Colorado

APPENDIX C - HYDROLOGIC CALCULATIONS



Kimley » Horn

EXISTING RUNOFF COEFFICIENTS - IMPERVIOUS CALCULATION

PROJECT NAME: Peerless Farms DATE: 11/13/2023

PROJECT NUMBER: 196114000 CALCULATED BY: MOH CHECKED BY: MOH

CHECKED BY:	МОН										
SOIL:											
		Roof	Landscape	Pavement	Gravel						
	LAND USE:	<u>AREA</u>	<u>AREA</u>	<u>AREA</u>	<u>AREA</u>	-					
	2-YEAR COEFF.	0.71	0.02	0.89	0.57						
	5-YEAR COEFF.	0.73	0.08	0.90	0.59						
	10-YEAR COEFF.	0.75	0.15	0.92	0.63						
	100-YEAR COEFF.	0.81	0.35	0.96	0.70						
	IMPERVIOUS %	90%	0%	100%	80%						
		Roof	Landscape	Pavement	Gravel	TOTAL					
DESIGN	DESIGN	AREA	AREA	AREA	AREA	AREA					i
BASIN	POINT	(AC)	(AC)	(AC)	(AC)	(AC)	C(2)	C(5)	C(10)	C(100)	Imp %
On-Site Basins											
EX1	EX1	0.26	34.58	0.06	0.46	35.36	0.03	0.09	0.16	0.36	2%
EX2	EX2	0.09	4.45	0.00	0.10	4.64	0.05	0.10	0.17	0.37	4%
		0.35	39.03	0.06	0.56	40.00	0.04	0.09	0.16	0.36	2%
BASIN SUBTOTAL		1%	98%	0%	1%	100%					
Off-Site Basins											
EX3	EX3	0.00	1.93	0.70	0.00	2.63	0.25	0.30	0.35	0.51	27%
EX3B	EX3B	0.13	5.40	0.44	0.00	5.97	0.10	0.15	0.22	0.40	9%
T3-02	T3	-	-	-	-	289	-	-	-	-	-
T/4	T/4					250					

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

Kimley » Horn

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$

EXISTING Time of Concentration

PROJECT NAME: Peerless Farms
PROJECT NUMBER: 196114000
CALCULATED BY: MOH

DATE: 11/13/2023

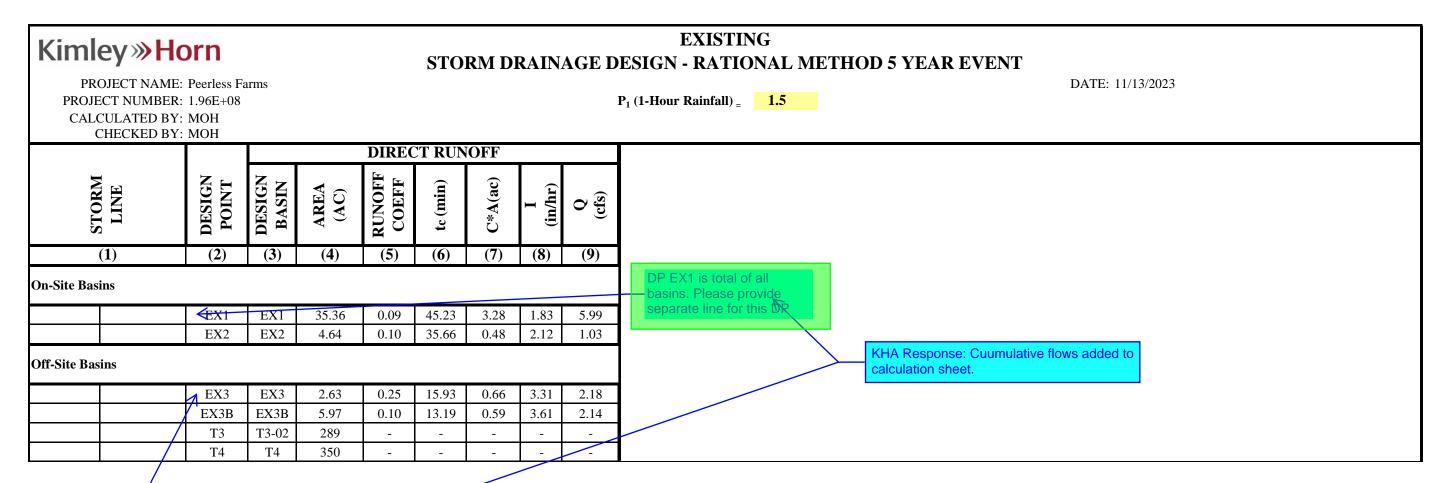
CHE	CKED BY:	МОН														
SUB-B DA				NITIAL IME (T _i)			$\begin{array}{c c} & TRAVEL\ TIME \\ & (T_t) \\ \hline \textbf{LENGTH} & SLOPE & C_v & VEL & T_t \\ \end{array}$					(UF	Te CHEC RBANIZED			FINAL Tc
DESIGN BASIN (1)	AREA Ac (2)	C5 (3)	LENGTH Ft (4)	SLOPE % (5)	T _i Min. (6)	ENGTH Ft. (7)	% (8)	C _v (9)	VEL fps (11)	T _t Min. (12)	tc (13)	TOTAL LENGTH (14)	TOTAL SLOPE (15)	TOTAL IMP. (16)	Tc Min. (17)	Min.
On-Site Basin	ıs															
EX1	35.36	0.093	300	1.6%	27.3	1,618	3.4%	2.5	0.5	58.5	85.8	1918	3.1%	2%	45.2	45.2
EX2	5	0.104	300	2.8%	22.4	569	1.9%	2.5	0.3	27.5	50.0	869	2.2%	4%	35.7	35.7
Off-Site Basin	ıs															
EX3	2.63	0.30	40	2.5%	6.9	1,500	1.9%	20.0	2.8	9.1	15.9	1540	1.9%	27%	36.1	15.9
EX3B	5.97	0.15	20	2.0%	6.2	1,034	1.5%	20.0	2.4	7.0	13.2	1054	1.5%	9%	38.3	13.2
T3-02	289	-	<i>7</i> \-	-	-	-	-	-	-	-	-	-	-	-	-	-
T4	350	-		-	-	-	-	-	-	-	-	-	_	-	-	-
			1													

*Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

For size of basin, this length seems short.

KHA Response: Initial Time is solely across Peerless Farms Rd. where flows runoff to roadside ditch, then flows travel through the ditch as 'channelized flow' the rest of the way through the basin.

 $t_{t} = \frac{L_{t}}{60K\sqrt{S_{o}}} = \frac{L_{t}}{60V_{t}} \qquad t_{c} = (26-17i) + \frac{L_{t}}{60(14i+9)\sqrt{S_{t}}}$



^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

DP EX3 is combined flows of Basins EX3, EX3B & EX2. Please provide separate line for DP

EXISTING Kimley » Horn STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT PROJECT NAME: Peerless Farms DATE: 11/13/2023 2.52 PROJECT NUMBER: 1.96E+08 P₁ (1-Hour Rainfall) = CALCULATED BY: MOH CHECKED BY: MOH **DIRECT RUNOFF** RUNOFF COEFF **DESIGN POINT** STORM LINE DESIGN BASIN C*A(ac) tc (min) AREA (AC) $\mathbf{Q}_{\mathbf{(cfs)}}$ **(1) (2)** (3) (4) (5) **(6) (7)** (8) (9) **On-Site Basins** 35.36 12.69 0.36 45.23 3.07 38.94 EX1 EX1 EX2 EX2 4.64 0.37 35.66 1.70 3.56 6.07 Off-Site Basins EX3 EX3 2.63 0.51 15.93 1.34 5.56 7.47 EX3B 5.97 0.40 13.19 2.42 6.07 EX3B 14.67 T3 T3-02 289 460

T4

T4

350

See comments on previous page

KHA Response: See response on previous page

570

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

Kimley»Horn

PROJECT NAME: Peerless Farms DATE: 11/13/2023

PROJECT NUMBER: 196114000 CALCULATED BY: MOH CHECKED BY: MOH

CHECKED B1: MOH											
	EXISTING	3 RATIONAL CALC	CULATIONS SUMMAR	RY							
DESIGN POINT	TRIBUTARY	TRIBUTARY AREA	IMPERVIOUSNESS	PEAK FLC	WS (CFS)						
DESIGN FOINT	BASINS	(AC)	%	Q5	Q100						
On-Site Basins											
EX1	EX1	35.36	2%	5.99	38.94						
EX2	EX2	4.64	4%	1.03	6.07						
TOTAL		40.00	2%	7.02	45.01						
Off-Site Basins											
EX3	EX3	2.63	27%	2.18	7.47						
EX3B	EX3B	5.97	9%	2.14	14.67						
T3-02	T3-02	289.00	-	-	460						
T4	T4	350.00	-	-	570						
TOTAL		647.60	-	-	1052.14						

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

Kimley»Horn PROPOSED														
•	RUNOFF COEFFICIENTS - IMPERVIOUS CALCULATION													
PROJECT NAME PROJECT NUMBER									DATE:	11/13/2023				
CALCULATED BY: CHECKED BY:														
SOIL:														
	LAND USE:	Roof <u>AREA</u>	Landscape <u>AREA</u>	Pavement <u>AREA</u>	Gravel <u>AREA</u>	_								
	2-YEAR COEFF.	0.71	0.02	0.89	0.57									
	5-YEAR COEFF.	0.73	0.08	0.90	0.59									
	10-YEAR COEFF.	0.75	0.15	0.92	0.63									
	100-YEAR COEFF.	0.81	0.35	0.96	0.70									
	IMPERVIOUS %	90%	0%	100%	80%									
		Roof	Landscape	Pavement	Gravel	TOTAL								
DESIGN BASIN	DESIGN	AREA	AREA	AREA	AREA	AREA	G(2)	G(5)	G(10)	G(100)	T 0/			
BASIN	POINT	(AC)	(AC)	(AC)	(AC)	(AC)	C(2)	C(5)	C(10)	C(100)	Imp %			
On-Site Basins														
1	1	2.30	17.64	0.00	0.03	19.97	0.10	0.16	0.22	0.40	10%			
2	2	0.00	1.43	0.09	0.26	1.78	0.14	0.20	0.26	0.43	17%			
3	3	0.00	0.49	0.04	0.26	0.78	0.24	0.29	0.35	0.50	31%			
4	4	0.00	0.18	0.24	0.00	0.42	0.51	0.55	0.59	0.70	57%			
5	5	0.00	0.47	0.16	0.22	0.85	0.33	0.37	0.42	0.56	40%			
6	6	0.56	4.70	0.06	0.23	5.55	0.12	0.18	0.24	0.42	13%			
7	7	0.00	1.48	0.09	0.00	1.57	0.07	0.13	0.19	0.38	6%			
8	8	1.00	8.03	0.03	0.03	9.09	0.10	0.16	0.22	0.40	10%			
		3.86	34.42	0.71	1.02	40.00	0.12	0.17	0.23	0.41	12%			
BASIN SUBTOTAL		10%	86%	2%	3%	100%								
Off-Site Basins														
EX3	EX3	0.00	1.93	0.70	0.00	2.63	0.25	0.30	0.35	0.51	27%			
EX3B	EX3B	0.13	5.40	0.44	0.00	5.97	0.10	0.15	0.22	0.40	9%			
T3-02	T3	-	-	-	-	289	-	-	-	-	-			
T4	T4	-	-	-	-	350	-	-	-	-	-			

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

Kimley » Horn

PROPOSEDTime of Concentration

PROJECT NAME: Peerless Farms
PROJECT NUMBER: 196114000
CALCULATED BY: MOH

DATE: 11/13/2023

SUB-B DA'				NITIAL IME (T _i)			TR	AVEL TIM (T _t)	Œ			(UF	Te CHEC RBANIZED			FINAL Tc
DESIGN BASIN (1)	AREA Ac (2)	C5 (3)	LENGTH Ft (4)	% (5)	T _i Min. (6)	LENGTH Ft. (7)	% (8)	C _v (9)	VEL fps (11)	T _t Min. (12)	tc (13)	TOTAL LENGTH (14)	TOTAL SLOPE (15)	TOTAL IMP. (16)	Tc Min. (17)	Min.
On-Site Basin	ıs															
1	19.97	0.16	300	6.0%	16.5	1,090	1.1%	5.0	0.5	34.6	51.1	1390	2.2%	10%	39.3	39.3
2	1.78	0.20	<mark>3</mark> 00	2.5%	21.1	1,243	3.2%	20.0	3.6	5.8	26.9	1543	3.1%	17%	36.1	26.9
3	0.78	0.29	61	5.0%	6.8	981	2.9%	20.0	3.4	4.8	11.6	1042	3.0%	31%	28.2	11.6
4	0.42	0.55	61	5.0%	4.6	477	1.7%	20.0	2.6	3.0	7.7	538	2.1%	57%	20.0	7.7
5	0.85	0.37	61	5.0%	6.1	1,056	1.5%	20.0	2.4	7.2	13.3	1117	1.7%	40%	29.1	13.3
6	5.55	0.18	300	2.0%	23.3	1,036	2.0%	20.0	2.8	6.1	29.4	1336	2.0%	13%	38.2	29.4
7	1.57	0.13	260	2.0%	22.9	5	3.0%	5.0	0.9	0.1	23.0	265	2.0%	6%	28.2	23.0
8	9.09	0.16	300	4.6%	18.0	958	4.4%	5.0	1.0	15.2	33.3	1258	4.4%	10%	33.7	33.3
Off-Site Basin	ıs		1													
EX3	2.63	0.30	40	2.5%	6.9	1,500	1.9%	20.0	2.8	9.1	15.9	1540	1.9%	27%	36.1	15.9
EX3B	5.97	0.15	2 0	2.0%	6.2	1,034	1.5%	20.0	2.4	7.0	13.2	1054	1.5%	9%	38.3	13.2
T3-02	289	-	<i>7</i> \-	-		-	-	-	-	-	-	-	-	-	-	-
T4	350	-		-		-	-	-	-	-	-	-	-	-	-	-
$t_i = \frac{0.1}{2}$	$\frac{395(1.1-C_{\odot})}{S_{o}^{0.33}}$	$\sqrt{L_i}$		$t_t = \frac{1}{60}$	$\frac{L_i}{K\sqrt{S_i}}$	$=\frac{L_t}{60V_t}$		$t_c = (26 -$	$17i) + {60}$	$\frac{L_i}{(14i+9)}$	$\sqrt{S_i}$					

^{*}Acreages and Q100 values for T3-02 and 74 were taken from the DBPS. Other values are not available.

See comment on existing hydrology spreadsheet

Highlighted lengths seem long when have smaller basins and flows reach culverts, ditches quicker. Show flow paths on drainage map

KHA Response: Flows generally do not take a direct route path to the outfall, and the roundabout routing makes for longer concentration paths. It is the responsibility of the design engineer to select and model the longest path for calculating time of concentration.

KHA Response: See response on previous page

PROPOSED STORM DRAINAGE DESIGN - RATIONAL METHOD 5 YEAR EVENT

DATE: 11/13/2023

PROJECT NAME: Peerless Farms

PROJECT NUMBER: 1.96E+08P₁ (1-Hour Rainfall) = 1.5

CALCULATED BY: MOH CHECKED BY: MOH

Kimley » Horn

CHECK	LD D1.	WIOII							
					DIREC	CT RUN	OFF		
STORM		DESIGN POINT	DESIGN BASIN	AREA (AC)	RUNOFF COEFF	tc (min)	C*A(ac)	I (in/hr)	Q (cfs)
(1)		(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
		\sim	\						
ne total of all basins	S	→ 1 -	1	19.97	0.16	39.28	3.11	2.00	6.21
asins 2 & 3 combine	ed		2	1.78	0.20	26.92	0.35	2.51	0.87
		3	3	0.78	0.29	11.60	0.23	3.82	0.86
		4	4	0.42	0.55	7.69	0.23	4.47	1.03
		5	5	0.85	0.37	13.32	0.31	3.60	1.12
			6	5.55	0.18	29.41	0.97	2.38	2.32
d		7	7	1.57	0.13	22.96	0.20	2.74	0.54
		8	8	9.09	0.16	33.25	1.42	2.21	3.14
Off-Site Basins		-							
		→EX3	EX3	2.63	0.25	15.93	0.66	3.31	2.18
		ЕХЗВ	EX3B	5.97	0.10	13.19	0.59	3.61	2.14
m		JIS T	T3-02	289	-	-	-	-	-
		T4	T4	350	-	-	=	-	-
	(1) On-Site Basins he total of all basins asins 2 & 3 combine asins 4, 5 & 6	(1) On-Site Basins he total of all basins asins 2 & 3 combined asins 4, 5 & 6 d Off-Site Basins s basins EX3, 7 &	(1) (2) On-Site Basins he total of all basins asins 2 & 3 combined 3 4 asins 4, 5 & 6 7 8 Off-Site Basins s basins EX3, 7 & ombined EX3B	## A STANDARD STANDAR	(1) (2) (3) (4) On-Site Basins he total of all basins he total of all basins 3	Composite Basins Composite B	Column C	Composite Basins Composite B	Composite Basins Composite B

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

Please provide individual design point calculation for each of those listed which combine flows from multiple basins.

KHA Response: Cuumulative flows added to calculation sheet.

Kimley » Horn

PROPOSED STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT

PROJECT NAME: Peerless Farms PROJECT NUMBER: 1.96E+08

CALCULATED BY: MOH

 P_1 (1-Hour Rainfall) = 2.52

DATE: 11/13/2023

CHECKED BY:	MOH							
				DIRF	ECT RU	JNOFI	₹	
STORM	DESIGN POINT	DESIGN BASIN	AREA (AC)	RUNOFF COEFF	tc (min)	C*A(ac)	I (in/hr)	Q (cfs)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
On-Site Basins								

	1	1	19.97	0.40	39.28	8.06	3.36	27.04
	2	2	1.78	0.43	26.92	0.77	4.21	3.24
	3	3	0.78	0.50	11.60	0.39	6.42	2.48
	4	4	0.42	0.70	7.69	0.29	7.51	2.21
	5	5	0.85	0.56	13.32	0.47	6.04	2.84
	6	6	5.55	0.42	29.41	2.32	4.00	9.26
	7	7	1.57	0.38	22.96	0.60	4.60	2.77
	8	8	9.09	0.40	33.25	3.67	3.72	13.65
	•			•	•		•	

Off-Site Basins

OII-DIC Das	IIIS								
		EX3	EX3	2.63	0.51	15.93	1.34	5.56	7.47
		EX3B	EX3B	5.97	0.40	13.19	2.42	6.07	14.67
		T3	T3-02	289	ı	1	ı	ı	460
		T4	T4	350	ı	ı	-	-	570

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

See comments on previous sheet

KHA Response: See response on previous page

Kimley»Horn

PROJECT NAME: Peerless Farms DATE: 11/13/2023

PROJECT NUMBER: 196114000 CALCULATED BY: MOH CHECKED BY: MOH

PROPOSED RATIONAL CALCULATIONS SUMMARY									
DEGIGNI BOINT	TRIBUTARY TRIBUTARY AREA IMPERVIOUSNESS PEAK FLOWS (CFS)								
DESIGN POINT	BASINS	(AC)	%	Q5	Q100				
On-Site Basins									
1	1	19.97	10%	6.21	27.04				
2	2	1.78	17%	0.87	3.24				
3	3	0.78	31%	0.86	2.48				
4	4	0.42	57%	1.03	2.21				
5	5	0.85	40%	1.12	2.84				
6	6	5.55	13%	2.32	9.26				
7	7	1.57	6%	0.54	2.77				
8	8	9.09	10%	3.14	13.65				
TOTAL		30.9	12%	16.08	63.49				
Off-Site Basins	Off-Site Basins								
EX3	EX3	2.63	27%	2.18	7.47				
EX3B	EX3B	5.97	9%	2.14	14.67				
T3-02	T3-02	289	-	-	460				
T4	T4	350	-	-	570				
TOTAL		647.60	-	-	1052.14				

^{*}Acreages and Q100 values for T3-02 and T4 were taken from the DBPS. Other values are not available.

If basins 1-8 are all on-site basins, total area should be 40 acres.

KHA Response: Revised

Design Procedure Form: Runoff Reduction UD-BMP (Version 3.07, March 2018) Sheet 1 of 1 Mitchell Hess Designer: Kimley-Horn Company Date: October 7, 2023 Peerless Farms Project: Location: Proposed Public ROW SITE INFORMATION (User Input in Blue Cells) WQCV Rainfall Depth 0.60 inches Depth of Average Runoff Producing Storm, d₆ = 0.43 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3) UIA:RPA UIA:RPA UIA:RPA UIA:RPA UIA:RPA UIA:RPA UIA:RPA Area Type Area ID В C1 D Е G Н C2 Downstream Design Point ID D Е C2 Α В C1 G Н Downstream BMP Type None None None None None None None None None DCIA (ft² 1,903 1,903 8,495 2,144 6,606 3,553 999 1,940 UIA (ft²) RPA (ft² 1,189 1,190 3,770 1,093 3,013 538 122 1,212 5,523 SPA (ft2 100% 100% 100% 100% 100% 100% 100% 100% HSG A (%) 100% HSG B (%) 0% 0% 0% 0% 0% 0% 0% 0% 0% HSG C/D (%) 0% 0% 0% 0% 0% 0% 0% 0% 0% Average Slope of RPA (ft/ft) 0.330 0.330 0.330 0.330 0.330 0.330 0.330 0.330 UIA:RPA Interface Width (ft) 119.00 119.00 424.00 118.00 314.00 125.00 19.00 121.00 CALCULATED RUNOFF RESULTS Area ID В C1 D Е G C2 UIA:RPA Area (ft2) 3,092 3,093 12,265 3,237 9,619 4,091 1,121 3,152 L/W Ratio 0.22 0.07 0.26 3.11 0.22 0.22 0.23 0.10 UIA / Area 0.6155 0.6153 0.6926 0.6623 0.6868 0.8685 0.8912 0.6155 Runoff (in 0.00 0.00 0.00 0.00 0.00 0.15 0.20 0.00 0.00 0 0 0 0 0 52 18 0 0 Runoff (ft3) 79 89 96 81 Runoff Reduction (ft3) 354 275 23 **CALCULATED WQCV RESULTS** В C1 D C2 Area ID F F G Н WQCV (ft3 79 79 354 89 275 148 42 0 81 WQCV Reduction (ft3) 79 354 89 275 96 23 81 WQCV Reduction (%) 100% 100% 100% 100% 100% 65% 56% 0% 100% 52 0 Untreated WQCV (ft3) 0 0 0 0 CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID) Downstream Design Point ID В C1 D C2 0 0 DCIA (ft2 1,903 1,903 8,495 2,144 6,606 3,553 999 1,940 LIIA (ft2 0 1.189 1.190 3,770 1.093 3.013 538 122 0 1.212 RPA (ft² SPA (ft² 0 0 0 0 0 0 0 5.523 0 Total Area (ft² 3,092 3,093 12,265 3,237 9,619 4,091 1,121 5,523 3,152 1,903 1,903 8,495 2,144 6,606 3,553 999 0 1,940 Total Impervious Area (ft2 42 79 79 354 89 275 148 0 81 WQCV (ft3 WQCV Reduction (ft³ 79 79 354 89 275 96 23 0 81 100% 100% 100% 65% 56% 0% WQCV Reduction (%) 100% 100% 100% Untreated WQCV (ft3) 0 0 0 52 18 0 0 CALCULATED SITE RESULTS (sums results from all columns in worksheet) Total Area (ft²) 45,193 27.543 Total Impervious Area (ft2) WQCV (ft3) 1.148 WQCV Reduction (ft3) 1.077 WQCV Reduction (%) 94% Untreated WQCV (ft3) 71

Master Development Drainage Plan and Preliminary Drainage Report Peerless Farms – El Paso County, Colorado

APPENDIX D - HYDRAULIC CALCULATIONS



Worksheet for Culvert 1

Project Description		
Friction Method	Manning	
Solve For	Formula Normal Depth	
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Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	18.0 in	
Discharge	2.21 cfs	
Results		
Normal Depth	6.7 in	
Flow Area	0.6 ft ²	
Wetted Perimeter	2.0 ft	
Hydraulic Radius	3.7 in	
Top Width	1.45 ft	
Critical Depth	6.7 in	
Percent Full	37.4 %	
Critical Slope	0.005 ft/ft	
Velocity	3.67 ft/s	
Velocity Head	0.21 ft	
Specific Energy	0.77 ft	
Froude Number	1.003	
Maximum Discharge	7.99 cfs	
Discharge Full	7.43 cfs	
Slope Full	0.000 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0.0 11	
·	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	37.4 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	6.7 in	
Critical Depth	6.7 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

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Notes:

Flows from Sub-Basin 4.

Worksheet for Culvert 2

Project Description		
Friction Method	Manning	
Solve For	Formula Normal Depth	
SOIVE FUI	поппат рерит	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	18.0 in	
Discharge	2.84 cfs	
Results		
Normal Depth	7.7 in	
Flow Area	0.7 ft ²	
Wetted Perimeter	2.1 ft	
Hydraulic Radius	4.1 in	
Top Width	1.48 ft	
Critical Depth	7.7 in	
Percent Full	42.9 %	
Critical Slope	0.005 ft/ft	
Velocity	3.92 ft/s	
Velocity Head	0.24 ft	
Specific Energy	0.88 ft	
Froude Number	0.991	
Maximum Discharge	7.99 cfs	
Discharge Full	7.43 cfs	
Slope Full	0.001 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	55.2 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	7.7 in	
Critical Depth	7.7 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

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Notes:

Flows from Sub-Basin 5.

Worksheet for Culvert 3

Friction Method Manning Formula
Formula
Solve For Normal Depth
Solve For Montal Depth
Input Data
Roughness Coefficient 0.013
Channel Slope 0.005 ft/ft
Diameter 24.0 in
Discharge 14.31 cfs
Results
Normal Depth 17.7 in
Flow Area 2.5 ft ²
Wetted Perimeter 4.1 ft
Hydraulic Radius 7.2 in
Top Width 1.76 ft
Critical Depth 16.4 in
Percent Full 73.8 %
Critical Slope 0.006 ft/ft
Velocity 5.76 ft/s
Velocity Head 0.52 ft
Specific Energy 1.99 ft
Froude Number 0.854
Maximum Discharge 17.21 cfs
Discharge Full 16.00 cfs
Slope Full 0.004 ft/ft
Flow Type Subcritical
GVF Input Data
Downstream Depth 0.0 in
Length 0.0 ft
Number Of Steps 0
GVF Output Data
Upstream Depth 0.0 in
Profile Description N/A
Profile Headloss 0.00 ft
Average End Depth Over Rise 0.0 %
Normal Depth Over Rise 55.2 %
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 17.7 in
Critical Depth 16.4 in
Channel Slope 0.005 ft/ft
Critical Slope 0.006 ft/ft

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Notes:

Flows from Sub-Basin 4, 5, and 6.

Worksheet for Culvert 4

Project Description		
Friction Method	Manning Formula	
Solve For	Formula Normal Depth	
JOING I UI	поппаг Берит	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	18.0 in	
Discharge	2.48 cfs	
Results		
Normal Depth	7.2 in	
Flow Area	0.7 ft ²	
Wetted Perimeter	2.0 ft	
Hydraulic Radius	3.8 in	
Top Width	1.47 ft	
Critical Depth	7.2 in	
Percent Full	39.8 %	
Critical Slope	0.005 ft/ft	
Velocity	3.78 ft/s	
Velocity Head	0.22 ft	
Specific Energy	0.82 ft	
Froude Number	0.998	
Maximum Discharge	7.99 cfs	
Discharge Full	7.43 cfs	
Slope Full	0.001 ft/ft	
Flow Type	Subcritical	
-		
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	55.2 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	7.2 in	
Critical Depth	7.2 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

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Notes:

Flows from Sub-Basin 3

Worksheet for Culvert 5

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	14.67 cfs	
Results		
Normal Depth	 18.1 in	
Flow Area	2.5 ft ²	
Wetted Perimeter	4.2 ft	
Hydraulic Radius	7.2 in	
Top Width	1.72 ft	
Critical Depth	16.6 in	
Percent Full	75.4 %	
Critical Slope	0.006 ft/ft	
Velocity	5.78 ft/s	
Velocity Head	0.52 ft	
Specific Energy	2.03 ft	
Froude Number	0.839	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.004 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
	0.0 in	
Downstream Depth	0.0 in 0.0 ft	
Length		
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	55.2 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	18.1 in	
Critical Depth	16.6 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

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Notes:

Flows from Sub-Basin EX3B

Worksheet for Sub-Basin 2 - Ditch

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.030	Provide analysis for
Channel Slope	0.025 ft/ft	steepest and flattest
Left Side Slope	4.000 H:V	section of ditch
Right Side Slope	4.000 H:V	
Discharge	5.72 cfs	
Results		
Normal Depth	7.6 in	
Flow Area	1.6 ft ²	KHA Response: Dual analysis added for each
Wetted Perimeter	5.2 ft	ditch section as requested.
Hydraulic Radius	3.7 in	anon occion de requestos.
Top Width	5.07 ft	
Critical Depth	7.9 in	
Critical Slope	0.020 ft/ft	
Velocity	3.57 ft/s	
Velocity Head	0.20 ft	
Specific Energy	0.83 ft	
Froude Number	1.117	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	7.6 in	
Critical Depth	7.9 in	
Channel Slope	0.025 ft/ft	
Critical Slope	0.020 ft/ft	

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Notes:

Flows from Sub-Basin 2 and 3.

Worksheet for Sub-Basin 3 - Ditch

Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Innut Data	'	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.025 ft/ft	Provide analysis for
Left Side Slope	4.000 H:V	steepest and flattest
Right Side Slope	4.000 H:V	section of ditch
Discharge	2.48 cfs	
Results		
Normal Depth	5.6 in	
Flow Area	0.9 ft ²	\
Wetted Perimeter	3.8 ft	KHA Response: Dual analysis added for each
Hydraulic Radius	2.7 in	ditch section as requested.
Top Width	3.70 ft	
Critical Depth	5.7 in	
Critical Slope	0.022 ft/ft	
Velocity	2.89 ft/s	
Velocity Head	0.13 ft	
Specific Energy	0.59 ft	
Froude Number	1.060	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.6 in	
Critical Depth	5.7 in	
Channel Slope	0.025 ft/ft	
Critical Slope	0.022 ft/ft	

Worksheet for Sub-Basin 3 - Ditch

Notes:

Flows from Sub-Basin 3.

Worksheet for Sub-Basin 4 - Ditch

Desired Desired		
Project Description		
Friction Method	Manning	
Calva Fair	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.030	Provide analysis for
Channel Slope	0.025 ft/ft	steepest and flattest
Left Side Slope	4.000 H:V	section of ditch
Right Side Slope	3.260 H:V	Scotled of alteri
Discharge	2.21 cfs	
Results		
Normal Depth	5.5 in	
Flow Area	0.8 ft ²	KHA Response: Dual analysis added for each
Wetted Perimeter	3.5 ft	ditch section as requested.
Hydraulic Radius	2.7 in	diterraction as requested.
Top Width	3.34 ft	
Critical Depth	5.6 in	
Critical Slope	0.022 ft/ft	
Velocity	2.87 ft/s	
Velocity Head	0.13 ft	
Specific Energy	0.59 ft	
Froude Number	1.055	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0.0 10	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	0.0 III N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.5 in	
Critical Depth	5.6 in	
Channel Slope	0.025 ft/ft	
Critical Slope	0.023 ft/ft 0.022 ft/ft	
описат эторе	U.UZZ 11/11	

Worksheet for Sub-Basin 4 - Ditch

Notes:

Flows from Sub-Basin 4.

Worksheet for Sub-Basin 5 - Ditch

Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.030	Provide analysis for
Channel Slope	0.025 ft/ft	steepest and flattest
Left Side Slope	4.000 H:V	section of ditch
Right Side Slope	4.000 H:V	Scotlan of diteri
Discharge	2.84 cfs	
Results		
Normal Depth	5.8 in	
Flow Area	0.9 ft ²	KHA Response: Dual analysis added for each
Wetted Perimeter	4.0 ft	ditch section as requested.
Hydraulic Radius	2.8 in	
Top Width	3.90 ft	
Critical Depth	6.0 in	
Critical Slope	0.022 ft/ft	
Velocity	2.99 ft/s	
Velocity Head	0.14 ft	
Specific Energy	0.63 ft	
Froude Number	1.069	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.8 in	
Critical Depth	6.0 in	
Channel Slope	0.025 ft/ft	
Critical Slope	0.022 ft/ft	

V	Vorksheet	for	Sub.	.Rasin	5 -	Ditch
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Notes:

Flows from Sub-Basin 5.

Worksheet for Sub-Basin 6 - Ditch

Project Description		
Friction Method Solve For	Manning Formula Normal Depth	
Input Data		
Roughness Coefficient Channel Slope Left Side Slope Right Side Slope Discharge	0.030 0.025 ft/ft 4.000 H:V 4.000 H:V 14.31 cfs	Provide analysis for steepest and flattest section of ditch
Results		
Normal Depth Flow Area Wetted Perimeter	10.7 in 3.2 ft ² 7.4 ft	KHA Response: Dual analysis added for each ditch section as requested.
Hydraulic Radius Top Width Critical Depth Critical Slope	5.2 in 7.15 ft 11.5 in 0.017 ft/ft	
Velocity Velocity Head Specific Energy	4.48 ft/s 0.31 ft 1.21 ft	
Froude Number Flow Type	1.182 Supercritical	
GVF Input Data		
Downstream Depth Length Number Of Steps	0.0 in 0.0 ft 0	
GVF Output Data		
Upstream Depth Profile Description Profile Headloss	0.0 in N/A 0.00 ft	
Downstream Velocity Upstream Velocity Normal Depth	Infinity ft/s Infinity ft/s 10.7 in	
Critical Depth Channel Slope Critical Slope	11.5 in 0.025 ft/ft 0.017 ft/ft	

Worksheet for Sub-Basin 6 - Ditch

Notes:

Flows from Sub-Basin 4, 5 and 6.

Worksheet for Sub-Basin 7 - Ditch

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.025 ft/ft	
Left Side Slope	4.000 H:V	
Right Side Slope	4.000 H:V	
Discharge	2.77 cfs	
Results		
Normal Depth	5.8 in	
Flow Area	0.9 ft ²	
Wetted Perimeter	4.0 ft	
Hydraulic Radius	2.8 in	
Top Width	3.86 ft	
Critical Depth	5.9 in	
Critical Slope	0.022 ft/ft	
Velocity	2.97 ft/s	
Velocity Head	0.14 ft	
Specific Energy	0.62 ft	
Froude Number	1.068	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.8 in	
Critical Depth	5.9 in	
Channel Slope	0.025 ft/ft	
Critical Slope	0.022 ft/ft	

Worksheet for Sub-Basin 7 - Ditch

Notes:

Flows from Sub-Basin 7.

Rip-Rap Calculation

Culvert 100-Year Outflow

Riprap Apron N4.1

Applicable	Equations

$L_p = (1/2 tan\Theta)(A_t/Y_t-D)$	Equation 9-11 per USCDM
$A_t = Q/V$	Equation 9-12 per USDCM
$\Theta = \tan^{-1}(1/(2*ExpansionFactor))$	Equation 9-13 per USDCM
$W = 2(L_p tan\Theta) + D$	Equation 9-14 per USDCM
$T = 2D_{50}$	Equation 9-15 per USDCM

Assumptions

Input parameters:

Description		Variable	Input	Unit
Width of the conduit (use diameter for circular conduits),		D:	2.00	ft
HGL Elevation			6567.93	ft
Invert Elevation			6566.45	ft
Tailwater depth (ft),		Y _t :	0.89	ft
Expansion angle of the culvert flow		Θ:	0.09	radians
Design discharge (cfs)*		Q:	14.31	cfs
Froude Number		F _r	0.85	Subcritical
Unitless Variables for Tables:				
	For Figure 9-35	Q/D ^{2.5}	2.53	
	For Figure 9-35	Y _t /D	0.45	
	For Figure 9-38	Q/D ^{1.5}	5.06	
	For Figure 9-38	Y _t /D	0.45	
Allowable non-eroding velocity in the downstream channel	el (ft/sec)	V:	7	ft/sec
Expansion Factor (Figure 9-35), $1/(2\tan(\theta))$			5.85	

Solve for:

Description	Variable	Output Unit
1. Required area of flow at allowable velocity (ft²)	A_t :	2.04 ft ²
2. Length of Protection	L _p :	1.71 ft
	$L_p < 3D$?	Yes
	$L_p > 10D$?	No
	$L_p > 10D \& F_r > 6$?	No
	L _{pmin} :	6.00 ft
Width of downstream riprap protection	W:	3.00 ft
4. Rip Rap Type (Figure 9-38)	-	L
5. Rip Rap Size (Figure 8-34)	D ₅₀ :	9 inches

Rin Ran Summary

Tup Tup Guillinary		
Length	Lp	6.00 ft
Width	W_{min}	3.00 ft
Size	D ₅₀	9 inches
Туре	-	L -
Thickness	T	18 inches

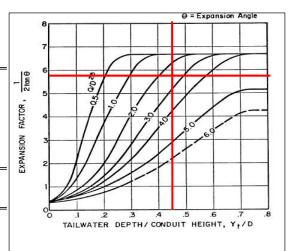
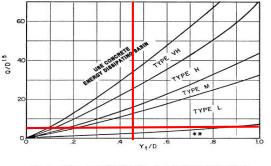


Figure 9-35. Expansion factor for circular conduits



Use D_a instead of D whenever flow is supercritical in the barrel. *** Use Type L for a distance of 3D downstream .

Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for $Q/D_{2.5} \le 6.0$)

PRAP DESIGNATION	% SMALLER THAN GIVEN SIZE BY WEIGHT	INTERMEDIATE ROCK DIMENSION (INCHES)	D ₅₀ * (INCHES)
TYPE VL	70 - 100 50 - 70 35 - 50 2 - 10	12 9 6 2	6
TYPE L	70 - 100 50 - 70 35 - 50 2 - 10	15 12 9 3	9
TYPE M	70 - 100 50 - 70 35 - 50 2 - 10	21 18 12 4	12
TYPE H	70 - 100 50 - 70 35 - 50 2 - 10	30 24 18 6	18

Figure 8-34. Riprap and soil riprap placement and gradation (part 1 of 3)

Master Development Drainage Plan and Preliminary Drainage Report Peerless Farms – El Paso County, Colorado

APPENDIX E - EOPCC AND TEMPORARY SEDIMENT BASIN STANDARD DETAIL





Kimley-Horn & Associates, Inc.

Opinion of Probable Construction Cost

Client:	Robert S. Williams	Date:	10/9/2023
Project:	Peerless Farms, El Paso County, CO	Prepared By:	MH
KHA No.:	196114000	Checked By:	

Sheet: 1 of 1

This OPC is not intended for basing financial decisions, or securing funding. Review all notes and assumptions. Since Kimley-Horn & Associates, Inc. has no control over the cost of labor, materials, equipment, or services furnished by others, or over methods of determining price, or over competitive bidding or market conditions, any and all opinions as to the cost herein, including but not limited to opinions as to the costs of construction materials, shall be made on the basis of experience and best available data. Kimley-Horn & Associates, Inc. cannot and does not guarantee that proposals, bids, or actual costs will not vary from the opinions on costs shown herein. The total costs and other numbers in this Opinion of Probable Cost have been rounded.

Item No.	Item Description	Quantity	Unit	Unit Price	Item Cost
	Private Storm Sewer (Non-Reimbursible)				
1	18" RCP Storm Pipe	90	LF	\$76.00	\$6,840
2	24" RCP Storm Pipe	65	LF	\$91.00	\$5,915
3	18" FES	6	EA	\$456.00	\$2,736
4	24" FES	4	EA	\$546.00	\$2,184
5	Riprap, d50 9"	16	Ton	\$97.00	\$1,552
		Subtotal:	•		\$19,227
		Contingency	(%,+/-)	10%	\$1,923
		Project Tota	al:		\$21,150

Basis for Cost Projection:

■ No Design Completed

☐ Preliminary Design

✓ Final Design

Design Engineer:

Mitchell O. Hess

Registered Professional Engineer, State of Colorado No. 53916

TEMPORARY SEDIMENT BASIN TSB



1.0 DESCRIPTION

 Temporary sediment basins are small impoundments of water with a small outlet structure built on a construction site.

2.0 PURPOSE

• Used to capture and slowly release runoff prior to discharge from a construction site to allow sediment to settle out.

3.0 IMPLEMENTATION

- Temporary sediment basins for drainage areas larger than 15 acres must be individually designed by engineer.
- Erosion and other sediment controls should be implemented upstream of temporary sediment basins.

4.0 TIMING

- Install prior to upstream land disturbance.
- Remove temporary sediment basin after upstream area has been stabilized. Permanently stabilize area after basin has been removed.

5.0 MAINTENANCE

- Remove sediment from basin as needed to maintain the effectiveness of the temporary sediment basin.
 This is typically when sediment depth reaches one foot.
- Inspect sediment basin embankments for stability and seepage.
- Inspect the inlet and outlet of the basin, repair damage, and remove debris.

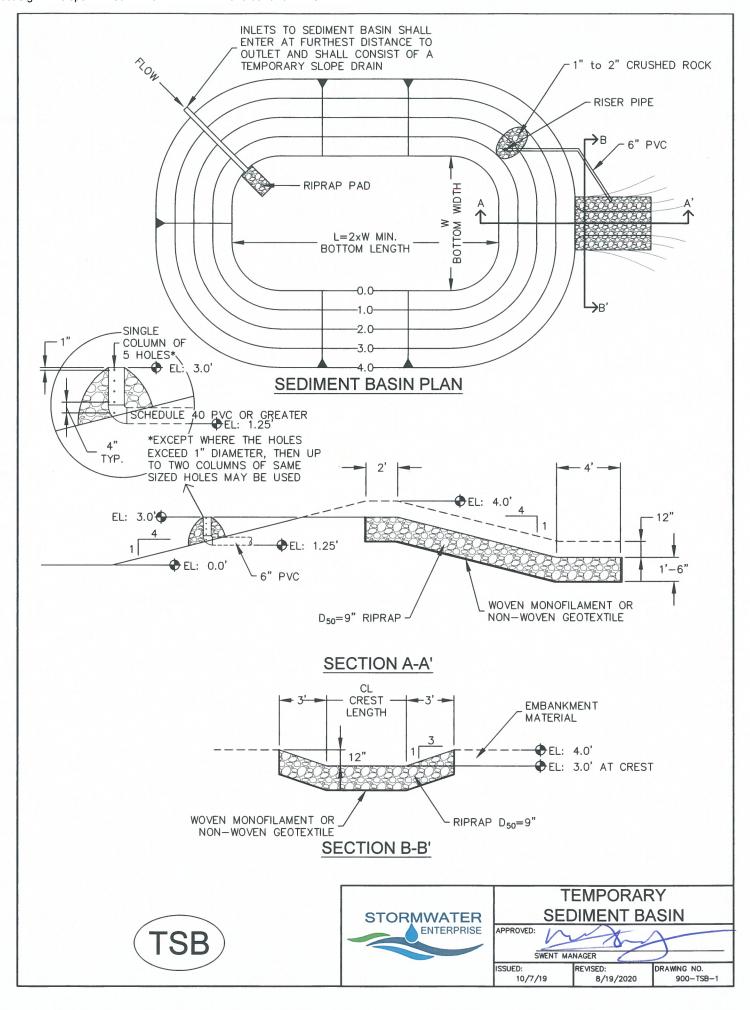


TABLE SB-1, SIZING INFORMATION FOR STANDARD SEDIMENT BASIN						
UPSTREAM DRAINAGE AREA (ROUNDED TO NEAREST ACRE), (AC) BASIN BOTTOM WIDTH SPILLWAY CREST LENGTH (CL), (FT) HOL DIAME (HD),						
1 2 3 4 5 6 7 8 9 10 11 12 13 14	12½" 21 28 33½ 38½ 43 47¼ 51 55 58¼ 61 64 67½ 70½ 73¼	2 3 5 6 8 9 11 12 13 15 16 18 19 21 22	932 1366 142 946 2132 2132 2532 2732 78 1546 3132 1 146 1 186 1 346			

INSTALLATION NOTES

- FOR STANDARD BASIN, BOTTOM DIMENSION MAY BE MODIFIED AS LONG AS BOTTOM AREA IS NOT REDUCED.
- EMBANKMENT MATERIAL SHALL CONSIST OF SOIL FREE OF DEBRIS, ORGANIC MATERIAL, AND ROCKS OR CONCRETE GREATER THAN 3 INCHES. AND SHALL HAVE A MINIMUM OF 15 PERCENT BY WEIGHT PASSING THE No. 200 SIEVE
- EMBANKMENT MATERIAL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DENSITY IN ACCORDANCE WITH ASTM D-698.
- PIPE SCHEDULE 40 OR GREATER SHALL BE USED.
- THE DETAILS SHOWN ON THESE SHEETS PERTAIN TO STANDARD SEDIMENT BASIN(S) FOR DRAINAGE AREAS LESS THAN 15 ACRES. SEE CONSTRUCTION DRAWINGS FOR EMBANKMENT, STORAGE VOLUME, SPILLWAY, OUTLET, AND OUTLET PROTECTION DETAILS FOR ANY SEDIMENT BASIN(S) THAT HAVE BEEN INDIVIDUALLY DESIGNED FOR DRAINAGE AREAS LARGER THAN 15 ACRES. DESIGN CALCULATIONS MUST BE APPROVED PRIOR TO IMPLEMENTATION.

MAINTENANCE NOTES

- FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN CONTROL MEASURES IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
- SEDIMENT ACCUMULATED IN BASIN SHALL BE REMOVED AS NEEDED TO MAINTAIN CONTROL MEASURE EFFECTIVENESS, TYPICALLY WHEN SEDIMENT DEPTH REACHES ONE FOOT (I.E. TWO FEET BELOW SPILLWAY CREST).
- 3. SEDIMENT BASINS ARE TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS PERMANENTLY STABILIZED.
- 4. PERMANENTLY STABILIZE AREA AFTER SEDIMENT BASIN REMOVAL.





TEMPORARY SEDIMENT BASIN APPROVED:

> SWENT MANAGER REVISED: 8/19/2020

10/7/19

DRAWING NO. 900-TSB-2 Master Development Drainage Plan and Preliminary Drainage Report Peerless Farms – El Paso County, Colorado

APPENDIX F - UNNAMED DRAINAGEWAY PHOTOGRAPHS





Figure 1: Storm Drain Culver Beneath Falcon Highway



Figure 2: Looking East Towards the Unnamed Drainageway



Figure 3: Looking East Towards the Unnamed Drainageway



Figure 4: Looking North Towards Falcon Highway



Figure 5: Looking Southeast at the Unnamed Drainageway



Figure 6: Unnamed Drainageway



Figure 7: Looking North at the Unnamed Drainageway



Figure 8: Looking East at the Unnamed Drainageway at the South End of the Site

Master Development Drainage Plan and Preliminary Drainage Report Peerless Farms – El Paso County, Colorado

APPENDIX G - EXCERPTS FROM DBPS



Table 6-5 Regional Detention Pond Summary

Pond Volume (AF)		Peak-In	flow (cfs)	Peak Outflow (cfs)	
1 Onu	, voidine (Atr)	2-yr	100-yr	2-yr	100-yr
RG-01	9.02	100	320	11	63
RG-02	170	600	4800	150	2200
RG-03	0.04	3	70	2	9
RG-04	1.07	19	140	1	. 55
RG-05	0.03	12	120	11	3

For the 100-year peak flow, flood impacts downstream from the regional detention pond will not increase.

6.3.1.1. Channels

Channels upstream of the regional detention ponds need to be sized for the future undetained 100-year peak flow rates from development, while culverts and channels downstream of regional ponds are sized for the existing 100-year peak flow rates. Proposed channel improvements along the corresponding reaches are summarized in Table 6-6.

Table 6-6 Channel Designs for Regional Detention Alternative

Table 6-6 Channel Designs for Regional Detention Alternative							
Channel	Existing 100-yr Flow (cfs)	Proposed 100-yr Flow (cfs)	Design Flow (cfs)	Channel Length (ft)	Material		
Main Stem (MS-04)	1700	3400	3500	7140	Riprap		
Main Stem (MS-05)	1500	3000	3000	11100	Grass		
Main Stem (MS-06)	. 590	890	900	7330 -	Grass		
Main Stem (MS-06)	660	930	1000	3170	Grass		
Main Stem (MS-06)	720	1500	1500	4450	Grass		
Main Stem (MS-06)	750	1600	2000	3330	Grass		
Tributary 3 (T3-01)	720	1500	1500	10710	Grass		
Tributary 4 (T4)	200	570	600	1840	Grass		
Tributary 5 (T5)	150	240	300	930	Grass		
Tributary 5 (T5)	270	410	500	7770	Grass		
Tributary 6 (T6)	200	440	500	4270	Grass		
Tributary 6 (T6)	240	570	600	3940	Grass		

6.3.1.2. Culverts

As with the channels, culverts upstream of a regional detention pond need to be sized for the future undetained 100-year peak flow rates, while culverts and channels downstream are sized for the existing 100-year peak flow rates. Proposed culvert improvements along the corresponding reaches are summarized in Table 6-7 for the Regional Detention Alternative.

Table 6-7 Culvert Designs for Regional Detention

Facility	Road	Channel	Existing	Proposed 100-yr Flow	Deficiency	Necessary Facility for Proposed
Number	Crossing		Size	(cfs)		100-year Flow
405	Murr Road	Main Stem (MS-04)	66" RCP	3,400	Overtops	6-10'X6' RCBs
507	Peerless Farms Road	Tributary 3 (T3-01)	60" CMP	1200	Overtops	2-10'X6' RCBs
609	Falcon Highway	Tributary 3 (T3-02)	18" CMP	460	Overtops	2-66" RCPs
610	Falcon Highway	Tributary 4 (T4)	24" CMP	570	Overtops	2-72" RCPs
612	Falcon Highway	Tributary 5 (T5)	24" CMP	240	Overtops	72" RCP
628	Falcon Highway	Main Stem (MS-05)	2-60" CMPs	2,200	Overtops	4-10'X6' RCBs
702	Curtis Road	Tributary 6 (T6)	36" CMP	140	Overtops	60" RCP
703	Curtis Road	Main Stem (MS-06)	24" CMP	890	Overtops	2-8'X6' RCBs
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	830	Overtops	2-8'X6' RCBs
1001	Future Pastura Street	Main Stem (MS-06)	N/A	930	Future Road	2-8'X6' RCBs
1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	N/A	930	Future Road	2-8'X6' RCBs
1003	Future Arroyo Hondo Blvd. S.	Main Stem (MS-06)	N/A	1500	Future Road	3-8'X6' RCBs
1004	Future Pastura Street	Tributary 6 (T6)	N/A	440	Future Road	2-66" RCPs
1005	Future El Vado Road	Tributary 6 (T6)	N/A	440	Future Road	2-66" RCPs
1006	Future Socorro Trail	Tributary 6 (T6)	N/A	440	Future Road	2-66" RCPs

Note: Changes recommended to other culverts under existing conditions still apply

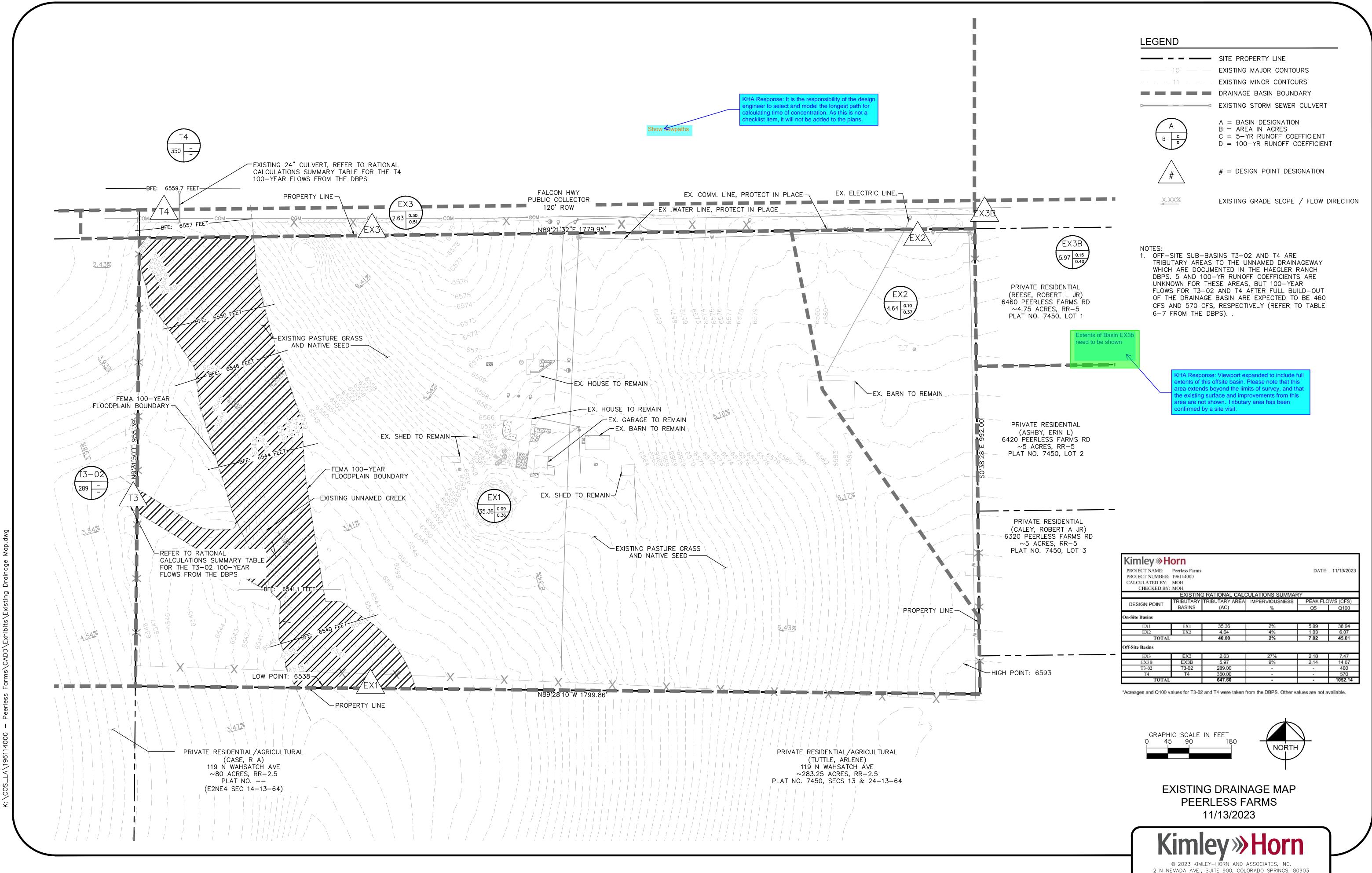
6.3.2. Subregional Detention

For this alternative, subregional detention ponds are located and sized to address development as it will occur. Locations of proposed subregional detention ponds are shown in Figure 6-2 and are summarized in Table 6-8. A connectivity diagram for the sub-regional HEC-HMS model is shown in Figure 6-3.

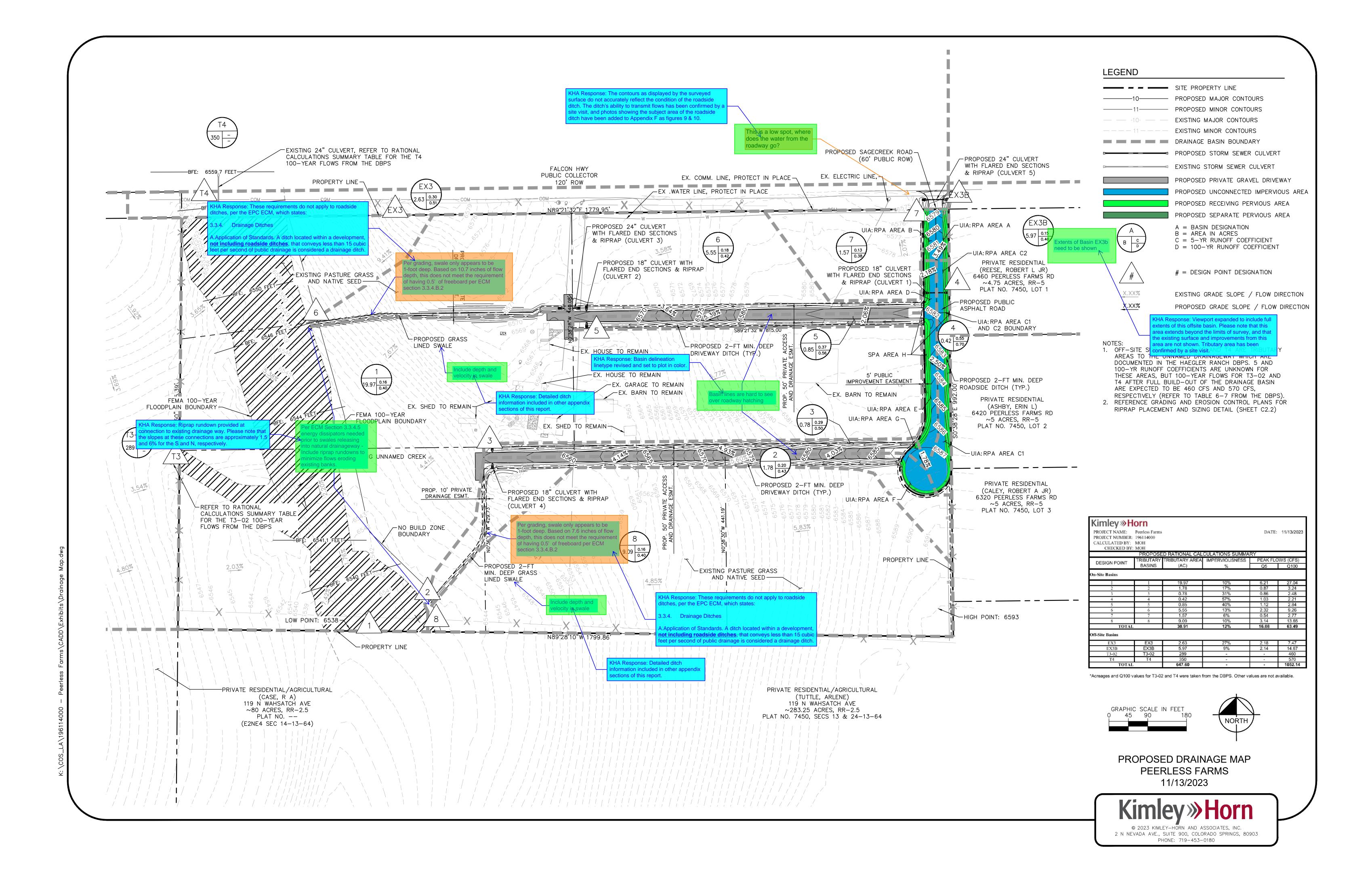
Master Development Drainage Plan and Preliminary Drainage Report Peerless Farms – El Paso County, Colorado

APPENDIX H - DRAINAGE EXHIBITS





PHONE: 719-453-0180



V1_Drainage Report - Final.pdf Markup Summary

Callout (25)



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 2:32:43 PM

Status: Color: Layer: Space: Revise to Final Drainage Report



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 2:35:25 PM

Status: Color: Layer: Space: Verify with LOI, as it states in one section that it is one house and an accessory building.

el driveways. The runoff collected ageway, following historical runoff ins, Sub-Basins 1 - 8 and 3 off-site T4. The proposed conditions map

0% and consists of the unnamed a runoff developed within this sub-

Subject: Callout Page Label:

Author: CDurham

Date: 3/25/2024 4:20:10 PM

Status: Color: Layer: Space: 4 off-site basins, EX3B,

ungain and parts becaused in an expension IVEP - John Mitted ableved not account for channel flow times is been concluded that not detailing stormwater flows is been concluded that not detailing stormwater flows in the flows from the ng stormwater flows on-site in a private extended of harmel as pass flows on-site in a private extended of harmel as pass flows over old to fericate at a later time in the channel, allowing higher volumes and velocities of the control of

Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:36:02 PM

Status: Color: Layer: Space: State what the increase in flows is and percentage increase.

100 Enter

Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:46:12 PM

Status: Color: Layer: Space: For size of basin, this length seems short.



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:52:40 PM

Status: Color: Layer: Space: DP1 is the total of all basins

Page Label:

Subject: Callout

Author: CDurham

Date: 3/25/2024 5:52:14 PM

Status: Color: Layer: Space:



Subject: Callout Page Label:

Author: CDurham

Date: 3/25/2024 5:52:37 PM

Status: Color: Layer: Space:



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:54:02 PM

Status: Color: Layer: Space:



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:56:59 PM

Status: Color: Layer: Space:

Highlighted lengths seem long when have smaller basins and flows reach culverts, ditches quicker.

DPEX3 is basins EX3, 7 & EX3B combined

Show flow paths on drainage map

DP6 is Basins 4, 5 & 6 combined

DP2 is Basins 2 & 3 combined



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:57:21 PM

Status: Color: Layer: Space:

See comment on existing hydrology spreadsheet



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 5:58:17 PM

Status: Color: Layer: Space:

If basins 1-8 are all on-site basins, total area

should be 40 acres.



Subject: Callout

Page Label: Author: CDurham

Date: 3/25/2024 6:28:24 PM

Status: Color: Layer: Space: Include depth and velocity in swale



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:28:34 PM

Status: Color: Layer: Space: Include depth and velocity in swale



Subject: Callout Page Label: Author: CDurham

Date: 3/26/2024 9:28:11 AM

Status: Color: Layer: Space: Per ECM Section 3.3.4.5 energy dissipators needed prior to swales releasing into natural drainageway - Include riprap rundowns to minimize flows are disconsisting banks.

flows eroding existing banks.



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:31:23 PM

Status: Color: Layer: Space: Basin lines are hard to see over roadway hatching



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:36:11 PM

Status: Color: Layer: Space: Calculations are only shown for 2.5% slopes. Should use a min and max slope for each ditch to

determine velocity and depth.



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:35:51 PM

Status: Color: Layer: Space: Per ECM section 3.3.4.B.2, ditch should have

freeboard of 0.5'



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:36:15 PM

Status: Color: Layer: Space: Per ECM section 3.3.4.B.1 minimum ditch slope is 2.0%.



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:44:33 PM

Status: Color: Layer: Space: Per grading, swale only appears to be 1-foot deep. Based on 10.7 inches of flow depth, this does not meet the requirement of having 0.5' of freeboard per ECM section 3.3.4.B.2



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:44:53 PM

Status: Color: Layer: Space: Per grading, swale only appears to be 1-foot deep. Based on 7.6 inches of flow depth, this does not meet the requirement of having 0.5' of freeboard

per ECM section 3.3.4.B.2



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:46:17 PM

Status: Color: Layer: Space: DP EX3 is combined flows of Basins EX3, EX3B & EX2. Please provide separate line for DP



Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:46:43 PM

Status: Color: Layer: Space: DP EX1 is total of all basins. Please provide separate line for this DP

ops and sheds. The Site does not ception of a 24" culvert beneath Falcon m the north side of Falcon Highway to

Subject: Callout Page Label: Author: CDurham

Date: 3/25/2024 6:48:59 PM

Status: Color: Layer: Space: Provide a culvert analysis of existing culvert to show what happens/overtops during major storm. that measurement and the control of the control of

Subject: Callout

Page Label:
Author: CDurham

Date: 3/25/2024 6:54:49 PM

Status: Color: Layer: Space: GEC plans & SWMP need to be provided.

Cloud+ (1)



Subject: Cloud+ Page Label: Author: CDurham

Date: 3/25/2024 5:54:22 PM

Status: Color: Layer: Space: Please provide individual design point calculation for each of those listed which combine flows from multiple basins.

Engineer (8)

the baryard or the time of Fourl Pink according to the various Black Coloning Pinks on based on the custies about Coloning Pinks on based on the custies in the 2012 Discharge of Black Pinks and Fourlish States of the 2012 Discharge of Black Pinks and Fourlish States of Pinks and Pinks

Subject: Engineer Page Label:

Author: Bret

Date: 3/22/2024 11:00:34 AM

Status: Color: Layer: Space: Update to 2024 Drainage and Bridge fees

No. SP-21-7

Page Label: Author: Bret

Subject: Engineer

Date: 3/22/2024 11:13:24 AM

Status: Color: Layer: Space: SP-21-7

11400 SF242

3P-21-7

Subject: Engineer Page Label:

Author: Bret

Date: 3/22/2024 11:13:46 AM

Status: Color: Layer: Space: SF242

2 acres with a basin impervious value of 57 bad. The runoff developed within this sub ditch before flowing into a driveway ditch will ainageway. Developed runoff during the 5-ye respectively. Stormwater runoff within Subpath. Include discussion of culvert 1 and 3 with locations

5 acres with a basin impervious value of 40° ad, a portion of a gravel driveway and a driv sin will be collected within proposed roads age ditch within Sub-Basin 6 and being rout Subject: Engineer Page Label: Author: Bret

Date: 3/22/2024 4:07:25 PM

Status: Color: Layer: Space: Include discussion of culvert 1 and 3 with locations

proposed public road, a portion of a gravel c within this sub-basin will be collected with flowing into a drainage ditch within Sub-Bas Developed runoff during the 5-year and respectively. Stormwater runoff within Sub-I path. Include discussion of culvert

2 and 3 with locations Sub-Basin 6

gravel driveway, a driveway ditch and futur sub-basin will be collected within proposed unnamed drainageway. Developed runoff Subject: Engineer Page Label:

Author: Bret

Date: 3/22/2024 4:07:38 PM

Status: Color: Layer: Space:

in will be collected within proposed roadside d drainageway. Developed runoff during th d 9.26 cfs respectively. Stormwater runoff s historical path. Total 5-year and 100-year tream Sub-Basins 4 and 5 (Design Poin leet). Include discussion of culvert 3 with location

sin 7 is 1.57 acres with a basin impervious of public road, roadside ditches and a future >-basin will be collected within an existing into the unnamed drainaneura. Payalona

Subject: Engineer Page Label: Author: Bret

Date: 3/22/2024 4:07:57 PM

Status: Color: Layer: Space:

ay and driveway drainage ditch. Sub-Basin: ic road. The runoff developed within this su ditch before flowing into a drainage ditch will sinageway. Developed runoff during the 5-ye Is respectively. Stormwater runoff within Sub path. Include discussion of culvert 4 with location

2 acres with a basin impervious value of 57 oad. The runoff developed within this subditch before flowing into a driveway ditch with alternative and provided the 5-weeks. Subject: Engineer Page Label: Author: Bret

Date: 3/22/2024 4:08:13 PM

Status: Color: Layer: Space:

sin EX3B is an offsite sub-basin which cons t half of Peerless Farms Road adjacent to L Lot 1. Stormwater runoff within Sub-Basin lowing west to Sub-Basin EX3. Sub-Basin I 19% and 5-year and 100-year storm event weby. Include discussion of culvert

asin T3-02 sin T3-02 consists of a named tributary dis HR0290 and HR0300. Sub-Basin T3-0 ural/vacant land and large-lot single-family Subject: Engineer Page Label: Author: Bret

Date: 3/22/2024 4:09:01 PM

Status: Color: Layer: Space: Include discussion of culvert 5 with location

Include discussion of culvert 2 and 3 with locations

Include discussion of culvert 3 with location

Include discussion of culvert 4 with location

Highlight (9)

Late Control Accordance (Late Control Accordan

Subject: Highlight Page Label: Author: CDurham

Date: 3/25/2024 2:33:01 PM

Status: Color: Layer: Space: Master Development Drainage Plan and Preliminary Drainage Report

Spa

Subject: Highlight Page Label: Author: CDurham

Date: 3/25/2024 2:33:46 PM

Status: Color: Layer: Space: wo single family houses,

Subject: Highlight two single-family homes, merally slopes from east to west as v nately 1.5 – 3.5%. The historical dra sts of two single-family homes, a larg ite does not have any existing store and Falcon Highway that allows the n Highway to the Site. Page Label: Author: CDurham Date: 3/25/2024 2:35:20 PM Status: Color: Layer: Space: Subject: Highlight Haeger are required to Page Label: he Haeger Dra Author: CDurham Date: 3/25/2024 5:36:48 PM development. Status: ranvious acra Color: Layer: Space: Subject: Highlight 300 3 Page Label: 300 Author: CDurham Date: 3/25/2024 5:55:43 PM Status: Color: Layer: Space: Subject: Highlight 300 Page Label: 300 Author: CDurham Date: 3/25/2024 5:55:47 PM 300 Status: Color: Layer: Space: Subject: Highlight 61 300 Page Label: 300 Author: CDurham Date: 3/25/2024 5:55:53 PM 260 Status: Color: Layer: Space: Subject: Highlight 300 260 Page Label: Author: CDurham 260 Date: 3/25/2024 5:55:55 PM 300 Status: Color: Layer: Space:

260 300

Subject: Highlight Page Label: Author: CDurham

Date: 3/25/2024 5:55:56 PM

Status: Color: Layer: Space: 300

Stamp - Stormwater Comment Legend (1)



Subject: Stamp - Stormwater Comment Legend

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 9:24:14 AM

Status: Color: Layer: Space:

SW - Highlight (3)



Subject: SW - Highlight

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 7:10:58 AM

Status: Color: Layer: Space: at 16.08 cfs and 63.49 cfs

will discharge to the unnamed drainageway in the redeveloped condition and during the 5-year and 100-year storm events respectively.

Figure 1 and 1 and

Subject: SW - Highlight

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 7:13:24 AM

Status: Color: Layer: Space: Because the unnamed drainageway flows directly

through the Site,



Subject: SW - Highlight

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 12:49:50 PM

Status: Color: Layer: Space: he runoff developed within

this sub-basin will be collected within an existing

roadside ditch

SW - Textbox (1)



Subject: SW - Textbox

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 12:51:23 PM

Status: Color: ■ Layer: Space: The last section of the public road does not flow directly to the unnamed drainageway but rather flow to a low spot along Falcon Highway. Discuss any increase in flows/suitable outfall for that basin because it has a different discharge location.

SW - Textbox with Arrow (3)



Subject: SW - Textbox with Arrow

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 9:13:39 AM

Status: Color: ■ Layer: Space: All flows do not flow directly through the site, some flow directly to the low spot along Falcon Highway.



Subject: SW - Textbox with Arrow

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 9:08:40 AM

Status: Color: ■ Layer: Space: This is a low spot, where does the water from the roadway go?



Subject: SW - Textbox with Arrow

Page Label:

Author: Mikayla Hartford Date: 3/25/2024 12:50:41 PM

Status: Color: ■ Layer: Space: Based on the contours on the CDs, there does not appear to be an existing roadside ditch, but rather a low spot. Clarify, will any increase inflows at the idischarge point cause flooding?

Text Box (13)

,985 + \$1,916) = \$71,524.80

60 Include total bridge fees.

or the construction of the private di κ E. There are no public drainage μ

Subject: Text Box Page Label: Author: CDurham

Date: 3/25/2024 5:41:42 PM

Status: Color: Layer: Space: Include total bridge fees.

points as opposed to private onsite deterunamed drainageway and the ability of 1 flows in the unnamed drainageway, no si Provide a channel calculation showing increased flows in major channel, does not have any adverte effects. A lift model is not needed, just a simple single channel analysis showing what objet, velocines, etc. will be. Subject: Text Box Page Label: Author: CDurham

Date: 3/25/2024 5:41:25 PM

Status: Color: Layer: Space: Provide a channel calculation showing increased flows in major channel, does not have any adverse effects. A full model is not needed, just a simple single channel analysis showing what

depth, velocities, etc will be.

nat onsite soils are primarily USCS

B. State what soil types are present.

Subject: Text Box Page Label: Author: CDurham

Date: 3/25/2024 5:43:01 PM

Status: Color: Layer: Space: State what soil types are present.

Subject: Text Box See comments on previous sheet Page Label: Author: CDurham Date: 3/25/2024 5:57:39 PM Status: Color: Layer: Space: Subject: Text Box Provide analysis for steepest and flattest section of Page Label: Author: CDurham Date: 3/25/2024 6:06:31 PM Status: Color: Layer: Space: Subject: Text Box Provide analysis for steepest and flattest section of Page Label: Author: CDurham Date: 3/25/2024 6:11:34 PM Status: Color: Layer: Space: Subject: Text Box Provide analysis for steepest and flattest section of Page Label: ditch Author: CDurham Date: 3/25/2024 6:12:19 PM Status: Color: Layer: Space: Subject: Text Box Provide analysis for steepest and flattest section of Page Label: ditch Author: CDurham Date: 3/25/2024 6:12:47 PM Status: Color: Layer: Space: Subject: Text Box Provide analysis for steepest and flattest section of Page Label: ditch Author: CDurham Date: 3/25/2024 6:13:13 PM Status: Color: Layer: Space:

Subject: Text Box Show flowpaths Page Label: Author: CDurham Show flowpaths Date: 3/25/2024 6:19:30 PM Status: Color: Layer: Space: Subject: Text Box Extents of Basin EX3b need to be shown Page Label: Author: CDurham Date: 3/25/2024 6:27:00 PM Status: Color: Layer: Space: Subject: Text Box Extents of Basin EX3b need to be shown Page Label: Author: CDurham Date: 3/25/2024 6:30:39 PM Status: ?) Color: Layer: Space: Subject: Text Box See comments on previous page Page Label: Author: CDurham Date: 3/25/2024 6:46:58 PM Status: Color: Layer: Space: