

Final Drainage Report

Misfit Crew Estates

Project No. 61160

May 21, 2024

PCD File No. SF2417

Final Drainage Report

for

Misfit Crew Estates

Project No. 61160

May 21, 2024

prepared for

Mark McDonald

5775 Mountain Shadow View Colorado Springs, CO 80908

prepared by

MVE, Inc.

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Statements and Acknowledgments

Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

David R. Gorman, P.E. Colorado No. 31672 For and on Behalf of MVE, Inc.

Conditions:

Developer's Statement	
l, the owner/developer have read and will comply with drainage report and plan.	all of the requirements specified in this
Mark McDonald Owner	Date
5775 Mountain Shadow View Colorado Springs, CO 80908	
El Paso County	
Filed in accordance with the requirements of the Draina Paso County Engineering Criteria Manual and Land Deve	
Joshua Palmer County Engineer XECM Administrator	Date

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Final Drainage Report

The purpose of this Final Drainage Report is to identify drainage patterns and quantities within and affecting the proposed Misfit Crew Estates site. The development project is a residential subdivision with 5.0± acre lots. The report will identify specific solutions to drainage concerns on-site and off-site resulting from the proposed project. The report and included maps present results of hydrologic and drainage facilities analyses. The report will discuss the recommended drainage improvements to the site and identify drainage requirements relative to the proposed project. This report has been prepared and submitted in accordance with the requirements of the El Paso County development approval process. An Appendix is included with this report with pertinent calculations and graphs used in the drainage analyses and design.

1 General Location and Description

1.1 Location

The proposed Misfit Crew Estates site is located within the east half of Section 24, Township 11 South, Range 66 West of the 6th principal meridian in El Paso County, Colorado. The 36.05± acre site is situated on the north side of Hodgen Road, at the end of Mountain Shadow View, a private gravel drive, ending at the east edge of the site. The parcel (Zone RR-5) contains a single family residence and out buildings. The El Paso County Assessor's Schedule Number for the site is 6124000013. A **Vicinity Map** is included in the **Appendix**. The site is located in El Paso County's East Cheery Creek Drainage Basin.

1.2 Description of Property

The Misfit Crew Estates site 36.05± acres and is zoned RR-5 (Residential Rural (5 Acres)). The property contains a single-family residence with an existing gravel driveway and sever out buildings. The proposed Misfit Crew Estates includes 3 rural residential lots.

The ground cover, which is in fair condition, consists of native grasses. The tree coverage is sporadic and located only around the residence.

The existing site topography slopes to the southeast with grades that range from 2% to 10%.

There are two major drainage ways in the Misfit Crew Estates site. For the north 4± acres, all storm runoff flows drain east off of the site. For the central 21± acres, all storm runoff flows drain southeast through a livestock pond and then southeast off of the site. For the south 11± acres, all storm runoff flows drain southeast off of the site. There is no storm drain system in the surrounding area. The site is located in El Paso County's East Cherry Creek Drainage Basin. The flows from the site flow southeast and eventually enter a tributary of East Cherry Creek.

According to the National Resource Conservation Service, there are two (2) soil types in the Misfit Crew Estates site. Peyton sandy loam (map unit 67) makes up about 78% of the soil on the site. The soil is deep and well drained. Permeability is moderate, surface runoff is medium, and the hazard of erosion is moderate. Peyton sandy loam is classified as being part of Hydrologic Soil Group B.

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The other soil type located on the site is Cruckton sandy loam (map unit 21) which makes up the remaining 22% of the soil on the site. The soil is deep and well drained. Permeability is moderately rapid, surface runoff is slow to medium, and the hazard of erosion is moderate. Cruckton sandy loam is classified as being part of Hydrologic Soil Group B.

A portion of the Soil Map and data tables from the National Cooperative Soil Survey and relevant Official Soil Series Descriptions (OSD) are included in the **Appendix**.¹

2 Drainage Basins and Sub-Basins

Please include relevant pages of this report in the Appendix.

2.1 Major Basin Descriptions

The Misfit Crew Estates site is located in the East Cherry Creek Drainage Basin (CYCY0200).

The current Flood Insurance Study of the region includes Flood Insurance Rate Maps (FIRM), effective on December 7, 2018.³ The proposed subdivision is included in the Community Panel Numbered 08041C0305 G of the Flood Insurance Rate Maps for the El Paso County. No part of the site is shown to be included in a 100-year flood hazard area as determined by FEMA. A portion of the current FEMA Flood Insurance Rate Maps with the site delineated is included in the **Appendix**.

2.2 Sub-Basin Description

The existing and developed drainage patterns of the Misfit Crew Estates project are described by two (3) on-site drainage basins and one (1) offsite basin along with two (2) points of off-site flows as detailed in the Final Drainage Report for Longview Estates. All of these basins are previously undisturbed or developed to a degree as described below. All existing basin delineations and data are depicted on the attached **Drainage Map**.

2.2.1 Existing / Developed Drainage Patterns (Off-Site)

Existing off-site Design Point DP8 is located west of the site at the north edge, being the pond outfall from an adjacent detention pond in Longview Estates, the outfall drains east onto the site. This flow enters the onsite sub-basin A1 and continues through the site.

Existing off-site sub-basin OS-B1 represents the off-site that combine with sub-basin B2 to travel southeast through the site to an existing livestock pond, then continues southeast off the site.

Existing off-site Design Point DP10 is located west of the site at the south edge, being the pond outfall from an adjacent detention pond in Longview Estates, the outfall drains east onto the site. This flow enters the onsite sub-basin C1 and continues through the site to a depression along the north side of Hodgen Road where it enters an existing 40" RCP and goes under Hodgen Road.

3 Drainage Design Criteria

42"

3.1 Development Criteria Reference

This Final Drainage Report for Misfit Crew Estates has been prepared according to the report guidelines presented in the latest edition of *El Paso County Drainage Criteria Manual* (DCM)⁴. The County has also adopted portions of the City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2, especially concerning the calculation of rainfall runoff flow rates.⁵ ⁶ The hydrologic analysis is based on a collection of data from the DCM, the NRCS Web Soil Survey⁷, and existing topographic data by Polaris.

¹ WSS

² OSD

FIRIVI
 DCM Section 4.3 and Section 4.4

⁵ CS DCM Vol 1

⁶ CS DCM Vol 2

⁷ WSS

Not included in the appendix.

3.2 Previous Drainage Studies

Longview Estates to the west was studied and the Final Drainage Report for Longview Estates by M.V.E., Inc, dated October 30, 2002 was used in the preparation of this report. Developed drainage basins from Longview Estates drain directly onto this site and the flows stated in the drainage report were used as off-site flows. A copy of this reports Drainage Map is included in the **Appendix**.

The existing 42" RCP under Hodgen Road, that is the nearest downstream facility to this site, was designed in the Final Drainage Report for Hodgen Road (State Highway 83 to Black Forest Road) by URS, dated December 8, 2009. Excerpts from this report and the culvert construction drawings are included in the **Appendix**.

3.3 Hydrologic Criteria

For this Final Drainage Report, the Rational Method as described in the Drainage Criteria Manual has been used for all Storm Runoff calculations, as the development and all sub-basins are less than 130 acres in area. "Colorado Springs Rainfall Intensity Duration Frequency" curves, Figure 6-5 in the DCM, was used to obtain the design rainfall values; a copy is included in the **Appendix**. The "Overland (Initial) Flow Equation" (Eq. 6-8) in the DCM, and Manning's equation with estimated depths were used in time of concentration calculations. "Runoff Coefficients for Rational Method", Table 6-6 in the DCM, was utilized as a guide in estimating runoff coefficient and Percent Impervious values; a copy is included in the **Appendix**. Peak runoff discharges were calculated for each drainage sub-basin for both the 5-year storm event and the 100-year storm event with the Rational Method formula, (Eq. 6-5) in the DCM.⁸

Please provide justification for this

statement.

4 Drainage Facility Design

4.1 General Concept

The intent of the drainage concept presented in this Final Drainage Report is to allow for the development of the three lots while maintaining the existing drainage patterns on the site. The site will be in compliance with the County's Stormwater Management regulations without the need for permanent water quality treatment facilities. Major and minor storm flows will continue to be safely conveyed through the site and downstream.

The existing and proposed drainage hydrologic conditions are described in more detail below. Input data and results for all calculations are included in the **Appendix**. A Drainage map for the hydrology are also included in the **Appendix**.

4.2 Existing / Developed Hydrologic Conditions

The Misfit Crew Estates site includes four (4) sub-basins, three (3) on site and one (1) off site as well as two (2) design points taken from the Final Drainage Report for Longview Estates. The site generally drains southeast. The sub-basins are described in more detail below.

Sub-basin A1, located at the very north end of the site, is $3.89\pm$ acres in area and accepts the flows from off-site Design Point DP8. Sub-basin A1 contains meadow/pasture and a portion of the roof of a barn, and is expected to remain as is. Peak storm runoff rates are $Q_5 = 1.0$ cfs and $Q_{100} = 7.0$ cfs (existing flows) with no change to the developed which drain east to DP1. These flows continue to drain east to the adjacent properties. The combined peak storm Indicate what happens to $Q_5 = 7.3$ cfs and $Q_{100} = 21.7$ cfs (existing / developed flows) which flc flows at DP1 when they exit There is no change to this sub-basin from existing to developed.

Existing offsite sub-basin OS-B1, located on the central west side of the site, is $1.22\pm$ acres in area. Sub-basin OS-B1 contains a meadow/pasture area of an existing developed residential lot in Longview Estates. Peak storm runoff rates are $Q_5 = 0.3$ cfs and $Q_{100} = 2.3$ cfs (existing / developed flows) which drain on-site to the southeast. These flows continue southeast through sub-basin B2.

State how much the culvert overtops (depth)

Sub-basin B2 located in approximately the middle half of the site, is $20.92\pm$ acres in area. Sub-basin B2 contains a single family residence, gravel drive, several out buildings and a livestock pond. This sub-basin is expected to remain as is. Peak storm runoff rates are $Q_5 = 4.8$ cfs and $Q_{100} = 33.4$ cfs (existing / developed flows) which drain southeast into the livestock pond where it collects and infiltrates. No clearly defined spillway or outlet exist for this structure. The State Dam Safety Engineer has directed that any future grading or improvements to this structure shall include the construction of an adequate spillway and outlet. The combined peak storm runoff rates from OS-B1 and sub-basin B2 flowing to DP2 are $Q_5 = 5.0$ cfs and $Q_{100} = 34.9$ cfs (existin Indicate what happens to which flow southeast to the edge of the property where a new driveway will be flows at DP2 when they exit 18" CMP culvert under the drive. The culvert is sized to accept the 5 year flow site. Swale, sheetflow, etc??? flows will overtop the driveway.

Sub-basin C1, located at south end of the site, is $11.01\pm$ acres in area and accepts the flows from off-site Design Point DP8. Sub-basin C1 currently contains meadow/pasture and is the proposed are of two new residential lets. Sub-basin C1's peak storm runoff rates are $Q_5 = 2.6$ cfs and $Q_{100} = \frac{1}{100}$ Provide calculations for cfs (existing flows) and $Q_5 = 3.3$ cfs and $Q_{100} = 20.8$ cfs (developed flows). The developed flows wale in the appendix assume a land use of 5 Acre lots with a percent imperviousness of 7.0%. A no-build / drainage easement is proposed for the existing swale through sub-basin C1. The swale is well vegetated and shows no signs of erosion. Calculations to determine the depth of flows and velocity of this swale are included in the **Appendix**. These flows, combined with those from off-site DP10 drain southeast to DP3. The combined peak storm runoff rates flowing to DP3 are $Q_5 = 24.7$ cfs and $Q_{100} = 72.3$ cfs (existing flows) and $Q_5 = 25.4$ cfs and $Q_{100} = 74.1$ cfs (developed flows). This is an increased of $Q_5 = 1.7$ cfs and $Q_{100} = 1.8$ cfs which flows southeast through adjacent property to a localized depression containing an existing 42° RCP that flows under Hodgen Road.

Also include the % increase that this is.

Indicate if outlet protection is provided for the culvert and if it's still in good condition.

The existing 42" RCP lying approximately 250 feet downstream of DP3 was designed using 100 year discharge of 100.9 cfs. This culvert was recalculated using 102.7 cfs (the increase in flows from existing to developed) and found to be capable of handling the minor increase in flows from this development. The culvert appears to be in stable condition with no signs of erosion at the downstream end. Excerpts from the URS drainage report showing the culvert calculations along with updated calculations for this culvert are included in the **Appendix**.

4.3 Erosion Control

There is no public infrastructure construction or overlot grading associated with this subdivision. Any required control measures (CM's) for the individual lot home construction will be handled on the BESQCP for each lot at time of building permit.

4.4 Four Step Process

The El Paso County Engineering Criteria Manual (Appendix I, Section I.7.2) requires the consideration of a "Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long term source controls". The Four Step Process is incorporated in this project and the elements are discussed below.

The entire site consists of 5-acre single family residential lots which are excluded from Post Construction Stormwater Management requirements by ECM 1.7.1.B.5 due to the low development density as 5-acre lots. There is no public roadway being dedicated or constructed as part of this project. The site is not subject to Post Construction Stormwater Treatment requirements.

- 1) Runoff Reduction Practices are employed in this project. Impervious surfaces have been reduced as much as practically possible. There is only minimal concrete or other hard surfaces proposed. Minimized Directly Connected Impervious Areas (MDCIA) is employed on the project because runoff passes through an open space meadow area before leaving the site.
- 2) There are no drainage paths on the site that are required to be stabilized as they are well vegetated with no visual erosion.

Please discuss permanent erosion control measures for the swale. The soils and geology report states that anything over 7 ft/s velocity might need channel stabilization.

ROW dedication is needed and shown on Plat drawing.

- 3) The project contains no potentially hazardous uses. The site is exempted from the use of WQCV CMs by ECM 1.7.1.B.5 by virtue of the large lot rural residential nature of the site having percent imperiousness of less than 10%.
- 4) The rural residential lot is not anticipated to contain storage of potentially harmful substances or use of potentially harmful substances. No site specific or other source control CMs are required.

5 Drainage and Bridge Fees

The southern portion of the site is located within the East Cherry Creek Drainage Basin, El Paso Basin Number CYCY0200, which which has no DBPS. There are no fees associated with this basin.

6 Conclusion

This Final Drainage Report presents existing and proposed drainage conditions for the proposed Misfit Crew Estates project. The development will have negligible and inconsequential effects on the existing site drainage and drainage conditions downstream. The site is exempted from the use of WQCV CMs by ECM 1.7.1.B.5 by virtue of the large lot rural residential nature of the site having percent imperviousness of less than 10%. The entire site is consists of 5-acre single family residential lots which are excluded from Post Construction Stormwater Management requirements due to the low development density as 5-acre lots. The site is not subject to Post Construction Stormwater Treatment requirements. With such a negligible increase in stormwater flows from the site, detention will not be necessary for the proposed development and will not be provided. The proposed project will not, with respect to stormwater runoff, negatively impact the adjacent properties and downstream properties.

References

NRCS Web Soil Survey. United States Department of Agriculture, Natural Resources Conservation Service ("http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx", accessed March, 2018).

NRCS Official Soil Series Descriptions. United States Department of Agriculture, Natural Resources Conservation Service

("http://soils.usda.gov/technical/classification/osd/index.html", accessed March, 2018).

Flood Insurance Rate Map. Federal Emergency Management Agency, National Flood Insurance Program (Washingon D.C.: FEMA, December 7, 2018).

NCSS Web Soil Survey. United States Department of Agriculture, Natural Resources Conservation Service ("http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx", accessed May, 2017).

Drainage Criteria Manual Volume 2, Stormwater Quality Policies, Procedures and Best Management Practices (BMPs). City of Colorado Spring Engineering Division (Colorado Springs: , May 2014).

City of Colorado Springs Drainage Criterial Manual, Volume 1. City of Colorado Springs Engineering Division Staff, Matrix Desgin Group/Wright Water Engineers (Colorado Springs: , May 2014).

City of Colorado Springs/El Paso County Drainage Criteria Manual. City of Colorado Springs, Department of Public Works, Engineering Division; HDR Infrastructure, Inc.; El Paso County, Department of Public Works, Engineering Division (Colorado Springs: City of Colorado Springs, Revised November 1991).

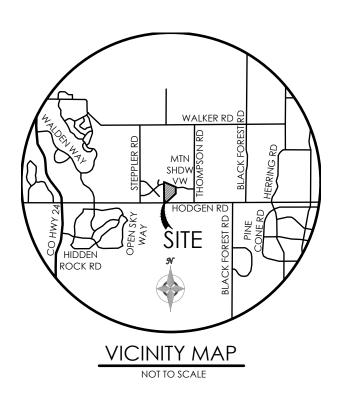
City of Colorado Springs Drainage Criteria Manual Volume 1. City of Colorado Springs Engineering Division with Matrix Design Group and Wright Water Engineers (Colorado Springs, Colorado: , May 2014).

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Appendices

1 General Maps and Supporting Data

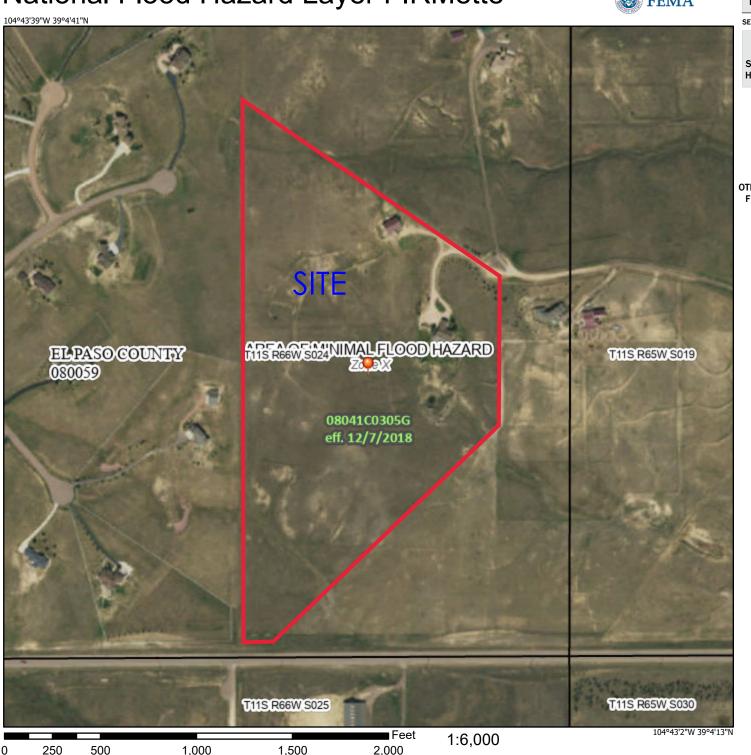
Vicinity Map
Portions of Flood Insurance Rate Map
NRCS Soil Map and Tables
SCS Soil Type Descriptions
Hydrologic Soil Group Map and Tables
Livestock Watertank Application



National Flood Hazard Layer FIRMette

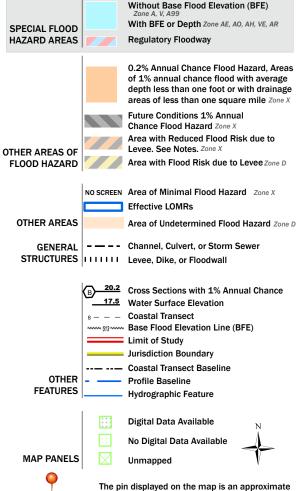


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/25/2021 at 5:59 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Natural Passuress

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for El Paso County Area, Colorado



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

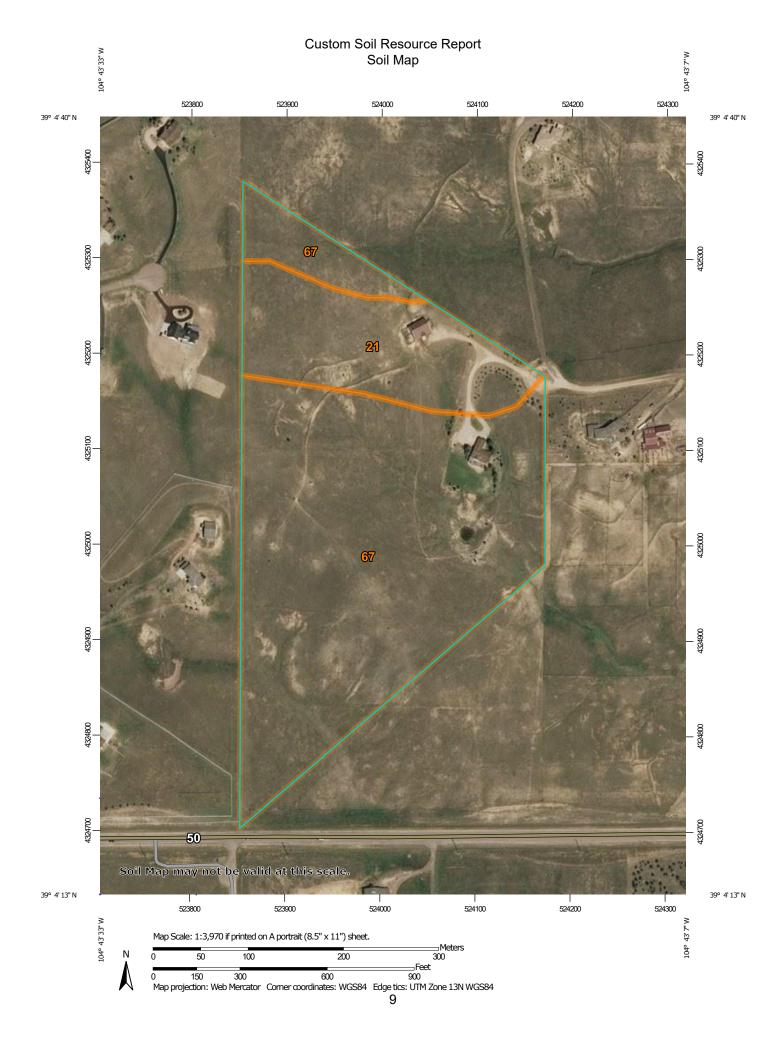
After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

(o)

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

 \Diamond

Closed Depression

Š

Gravel Pit

.

Gravelly Spot

Ø

Landfill Lava Flow

٨

Marsh or swamp

2

Mine or Quarry

0

Perennial Water

Miscellaneous Water

0

Rock Outcrop

+

Saline Spot

Sandy Spot

Severely Eroded Spot

A 5

Sinkhole

Ø

Sodic Spot

Slide or Slip

8

Spoil Area



Stony Spot Very Stony Spot



Wet Spot



Other

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Special Line Features

Water Features

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Streams and Canals

Transportation

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Rails

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Interstate Highways

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US Routes

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Major Roads

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Local Roads

Background

The same

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Sep 8, 2018—May 26, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
21	Cruckton sandy loam, 1 to 9 percent slopes	7.6	21.9%
67	Peyton sandy loam, 5 to 9 percent slopes	27.1	78.1%
Totals for Area of Interest		34.7	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

Custom Soil Resource Report

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

21—Cruckton sandy loam, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 367s Elevation: 7,200 to 7,600 feet

Mean annual precipitation: 16 to 18 inches
Mean annual air temperature: 42 to 46 degrees F

Frost-free period: 110 to 120 days

Farmland classification: Not prime farmland

Map Unit Composition

Cruckton and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Cruckton

Setting

Landform: Flats, hills

Landform position (three-dimensional): Side slope, talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Alluvium derived from arkose

Typical profile

A - 0 to 11 inches: sandy loam
Bt - 11 to 28 inches: sandy loam
C - 28 to 60 inches: loamy coarse sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: R049XB216CO - Sandy Divide

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

67—Peyton sandy loam, 5 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369d Elevation: 6,800 to 7,600 feet

Mean annual air temperature: 43 to 45 degrees F

Frost-free period: 115 to 125 days

Farmland classification: Not prime farmland

Map Unit Composition

Peyton and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Peyton

Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Arkosic alluvium derived from sedimentary rock and/or arkosic

residuum weathered from sedimentary rock

Typical profile

A - 0 to 12 inches: sandy loam

Bt - 12 to 25 inches: sandy clay loam

BC - 25 to 35 inches: sandy loam

C - 35 to 60 inches: sandy loam

Properties and qualities

Slope: 5 to 9 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: R049XB216CO - Sandy Divide

Hydric soil rating: No

Custom Soil Resource Report

Minor Components

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

Other soils

Percent of map unit: Hydric soil rating: No

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The main limitations of this complex for urban development are high frost action potential, moderate shrinkswell potential, the presence of stones and rock outcrop, and steep slopes. This complex requires special site or building designs because of the shrink-swell potential. Special designs are also needed when building on the steeper slopes. The roads and streets must have adequate cut-slope grade and be provided with drains to control surface runoff and keep soil losses to a minimum. Frost action is also a potential problem for the design of roads and streets. Capability subclass VIIe.

21—Cruckton sandy loam, 1 to 9 percent slopes. This deep, well drained soil formed in arkosic sandy loam deposits on uplands. Elevation ranges from 7,200 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 115 days.

Typically, the surface layer is dark grayish brown sandy loam about 4 inches thick. The subsoil is grayish brown sandy loam about 24 inches thick. The substratum is pale brown loamy coarse sand.

Included with this soil in mapping are small areas of Peyton sandy loam, 1 to 5 percent slopes, Peyton sandy loam, 5 to 9 percent slopes, and Pring coarse sandy loam, 3 to 8 percent slopes.

Permeability of this Cruckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate to high. Surface runoff is slow to medium, and the hazard of erosion is moderate. In places runoff from snowmelt in spring causes rills and small gullies to form in cultivated fields.

Most of this soil is in native grass that is used for grazing livestock. A small acreage on some of the more gentle slopes is used for small grain and corn for silage.

Native vegetation is mainly mountain muhly, bluestem, mountain brome, needleandthread, and blue grama. The soil is subject to invasion by Kentucky bluegrass and Gambel oak. Noticeable forbs are hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat.

Proper location of livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to protect the plant cover.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as komesites. Special design of roads and streets is needed because of frost action. Installation of drains helps to control surface runoff and keeps soil losses to a minimum. Capability subclass VIe.

22—Cushman loam, 1 to 5 percent slopes. This moderately deep, well drained soil formed in calcareous loamy material derived from weakly consolidated beds of sandstone and shale on uplands. Elevation ranges from 6,000 to 6,500 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown loam about 5 inches thick. The subsoil is brown sandy clay loam about 18 inches thick. The substratum is grayish brown fine sandy loam about 7 inches thick. Interbedded sandstone and shale are at a depth of 30 inches.

Included with this soil in mapping are small areas of Bresser sandy loam, 0 to 3 percent slopes; Kutch clay loam, 3 to 5 percent slopes; and Louviers silty clay loam, 3 to 18 percent slopes.

Permeability of this Cushman soil is moderate. Effective rooting depth is 20 to 40 inches. Available water capacity is low to moderate. Surface runoff is medium, and the hazard of erosion is moderate.

This soil is suitable for cultivation and is generally used for this purpose. Winter wheat is the main crop, and this is followed by a year of summer fallow because of limited precipitation. Feed grains such as millet and sorghum may be substituted for wheat in some years. Crop residue management and minimum tillage are the practices needed to protect this soil. The soil has a high producing potential, but production is reduced by low precipitation.

This soil is well suited to the production of native vegetation suitable for grazing. Native vegetation consists of western wheatgrass, needlegrasses, big bluestem, sideoats grama, blue grama, and native bluegrasses.

If the range has deteriorated, blue grama, junegrass, and native bluegrasses increase. Sleepygrass and annuals replace these grasses if the range is seriously deteriorated. Proper range management and proper location of livestock watering facilities are essential to help maintain the more desirable plants on this soil. Seeding is a good practice if the range is in poor condition. Seeding of the native vegetation is desirable, but the range can also be seeded with tame species of grasses such as Nordan crested wheatgrass, Russian wildrye, pubescent wheatgrass, or intermediate wheatgrass.

Windbreaks and environmental plantings are generally not suited to this soil. Onsite investigation is needed to determine if plantings are feasible.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, the provision of undisturbed nesting cover is

44 SOIL SURVEY

support a load and potential frost action on roads and streets. Roads and buildings can be designed to overcome these limitations. Capability subclass IVe.

67—Peyton sandy loam, 5 to 9 percent slopes. This deep, noncalcareous, well drained soil formed in alluvium and residuum derived from weathered arkosic sedimentary rock on uplands. Elevation ranges from 6,800 to 7,600 feet.

Typically, the surface layer is grayish brown sandy loam about 12 inches thick. The subsoil, about 23 inches thick, is pale brown sandy clay loam in the upper 13 inches and pale brown sandy loam in the lower 10 inches. The substratum is pale brown sandy loam to a depth of 60 inches.

Included with this soil in mapping are small areas of Holderness loam, 5 to 8 percent slopes; Pring coarse sandy loam, 3 to 8 percent slopes; and Tomah-Crowfoot loamy sands, 3 to 8 percent slopes.

Permeability of this soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is high. Surface runoff is medium, and the hazard of erosion is moderate. Gullies and rills are common.

Most of the acreage of this Peyton soil is used as rangeland. Some areas are used for wheat and oats. Stubble mulching or other crop residue management practices are needed to control water erosion. Wildlife habitat is also an important use.

This soil is well suited to the production of native vegetation suitable for grazing. The native vegetation is mainly mountain muhly, bluestem, mountain brome, needleandthread, and blue grama. This soil is subject to invasion by Kentucky bluegrass and Gambel oak. Minor amounts of forbs such as hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat are in the stand.

Proper location of livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to protect the plant cover.

Windbreaks and environmental plantings generally are suited to this soil. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be necessary when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to habitat for openland and rangeland wildlife. Rangeland wildife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for homesites. The main limitation is the limited ability to support a load and potential frost action. Buildings and roads can be designed to overcome these limitations. Capability subclass IVe.

68—Peyton-Pring complex, 3 to 8 percent slopes. These gently sloping to moderately sloping soils are on valley side slopes and on uplands. Elevation ranges from 6,800 to 7,600 feet. The average annual precipitation is about 17 inches, the average annual air temperature is about 43 degrees F, and the average frost-free period is about 120 days.

The Peyton soil makes up about 40 percent of the complex, the Pring soil about 30 percent, and other soils about 30 percent.

Included with these soils in mapping are areas of Holderness loam, 1 to 5 percent slopes; Holderness loam, 5 to 8 percent slopes; and Tomah-Crowfoot loamy sands, 3 to 8 percent slopes. In some places arkosic beds of sandstone and shale are at a depth of 0 to 40 inches.

The Peyton soil is commonly on the less sloping part of the landscape. It is deep, noncalcareous, and well drained. It formed in alluvium and residuum derived from weathered arkosic sedimentary rock. Typically, the surface layer is grayish brown sandy loam about 12 inches thick. The subsoil, about 23 inches thick, is pale brown sandy clay loam in the upper 13 inches and pale brown sandy loam in the lower 10 inches. The substratum is pale brown sandy loam to a depth of 60 inches or more.

Permeability of the Peyton soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is high. Surface runoff is medium, and the hazard of erosion is moderate.

The Pring soil is deep, noncalcareous, and well drained. It formed in sandy sediment derived from weathered arkosic sedimentary rock. Typically, the surface layer is dark grayish brown coarse sandy loam about 4 inches thick. The substratum is dark grayish brown coarse sandy loam about 10 inches thick over pale brown gravelly sandy loam that extends to a depth of 60 inches or more.

Permeability of the Pring soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is medium, and the hazard of erosion is moderate.

These soils are used as rangeland, for wildlife habitat, and for homesites.

These soils are well suited to the production of native vegetation suitable for grazing. The dominant native species are mountain muhly, bluestem, needleandthread, and blue grama. These soils are subject to invasion of Kentucky bluegrass and Gambel oak. Common forbs are hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat.

Properly locating livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to protect the plant cover.

Windbreaks and environmental plantings generally are suited to these soils. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good

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STATE OF COLORADO



DEPARTMENT OF WATER RESOURCES

Office of State Engineer

Standard Plans, Drawings

and

SPECIFICATIONS

Including

RULES AND REGULATIONS

Pertaining to

THE FILING OF APPLICATIONS

for eline or with behaving ad or noviese, and a

THE APPROVAL

of

LIVESTOCK WATER TANKS

PURSUANT TO H.B. No. 750 SESSION LAWS OF 1941 DENVER, COLORADO, MAY 1, 1941



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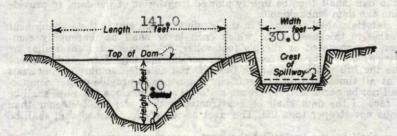
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APPLICATION FOR APPROVAL OF LIVESTOCK WATER TANK

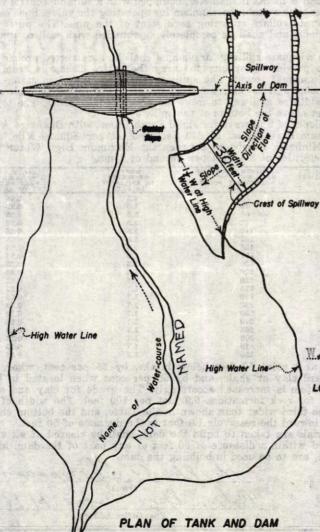
This application and Statement is made in conformity with provisions of the Livestock Water Tank Act of Colorado.
This application must be accompanied by a filing fee of one dollar, payable to the State
Engineer of Colorado. Wilbur Thompson Name of Owner Location of Tank SW-SE-Section 24, Township 11 So, Range 66 W-6 th PM Name of water course on which tank is located None Is water course normally dry Yes
Nature of vegetative cover over drainage basin above tank Grassland
Character of topography of drainage basin (steep, medium or flat) Medium
Character of surface formation of drainage basin (rock, rocky soil, or soil) Soil
Approximate elevation of drainage basin above sea level 7800 feet.
Is water course subject to floods at times Yes
Height of top of dam above bottom of water course 10.0 feet.
Height of bottom of spillway above bottom of water course 7.0 feet.
Approximate capacity of tank 1.0 0/6 acre feet.
Location of spillway with respect to dam Around end
Dallar mildth of chillway at narrowest point 30:0 feet
Bottom width of spillway at narrowest point 30.0 feet. Distance of lower end of spillway below dam 50.0 feet. Kind of formations in which spillway is located (rock, shale, clay, earth or mixture of soil and rock)
Width of top of dam \$.0 feet. Length of top of dam \$1.0 feet. Slope of upstream face of dam \$3:1 slope of downstream face of dam \$2:1. Nature of riprap or other protection to be placed over water face of dam To be seeded to grass
Is the reservoir to be provided with an outlet pipe
Give location by section, township and range, and size of every other stock tank now constructed in drainage basin in which this tank will be located No other dams in this drainage area
NOTE—Remainder of statements to be furnished by State Engineer's office.
NOTE—Remainder of statements to be furnished by State Engineer's office. Date of receipt of application by State Engineer Date of notice from applicant of completion of tank Oct. 25, , 19 46.
Tank or site inspected by
Recommendation of Inspector Date of return of plans and specifications to applicant for correction or revision
Reasons therefor
622 082.8 97.7 77.7 78.7 78.7 78.7 78.7 78.7 78
Filing Fee Paid NOV 2 9 1946 , 19 . Application approved this 28 m day of AUGUST , 1947 . Number assigned this stock tank is .
By G. State Engineer Lelef
Rv O. O. Parnalkales
Deputy

MAXIMUM CROSS-SECTION OF DAM



CROSS-SECTION OF DAM SITE AND SPILLWAY

Show length and height of dam and width of spillway on drawing



STATEMENT BY OWNER

Know all men by these presents: That the undersigned Wilbur. Thompson..... whose postoffice address is MeRt 5 GoloeSpes. has caused to be located this Stock Water Tank, the essential features of which are shown by this map and plans, which together with the accompanying application and statements are hereby filed with the State Engineer pursuant to the provisions of law.

First Objeth of dam above bottom of water-course is to deet.

Third: Total capacity of said Stock Water Tank is acre feet.

rifth: Filing of this map and accompanying statements with the State Engineer was made on the 29th day of NONE TODGE, 1947.

Will Chongs

MAP AND PLANS

FOR

W. Thompson STOCK WATER TANK AND DAM

LOCATED IN SECTION 24 TWP 11 STANGE 66 WOF 6them.

El Baso county

DRAINAGE AREA ABOVE DAM 60 ACRES

Approved this 28th day of AUGUST . 1947

BO Stafe Engineer Lell

DEPARTMENT OF WATER RESOURCES

OFFICE OF STATE ENGINEER

SPECIFICATIONS TO GOVERN THE CONSTRUCTION OF A LIVESTOCK WATER TANK IN COLORADO CONSTRUCTED AFTER APRIL 17, 1941

The following specifications and attached	d general plans shall be fo	ollowed in the construction of stock
water tank No. 1 , located in Sec. 24	, Township 11	, Range 66
for which the undersigned on	NOV 2 9 1946	filed an application with
the State Engineer, as required by law.		

Preparation of Foundation for Dam—All vegetable matter of every description, including roots to a depth of two feet, shall be removed from the entire area upon which the dam will rest, following which the top sixinch layer of soil, together with boggy or unstable materials shall be removed and deposited outside the toes of the dam. The banks of the stream channel shall be dressed to a slope of about 1½:1. A bonding trench, with sloping sides and a bottom width of not less than 5 feet and depth of 4 feet, shall then be excavated beneath the center line of the dam the full length thereof, which trench shall be refilled with the most impervious materials available. The foundation of the dam shall then be lightly plowed lengthwise of the dam, to provide proper contact between the foundation and the dam embankment.

Placing of Dam Embankment—The materials shall be placed in the bonding trench and in the embankment of the dam in layers not exceeding 6 inches in thickness, after which each layer shall be thoroughly compacted by a heavily loaded disc cultivator, a corrugated or sheep's foot roller, the treads of a caterpillar or trucks, or by livestock used in the construction. During the construction period, the top of the embankment shall be maintained as a horizontal plane the full width and length thereof, and no side dumping of materials shall be permitted. The materials shall at all times contain just sufficient moisture to provide proper compaction. Puddling of material with water shall not be permitted. No frozen material or large clods or stones shall be incorporated in the dam. The upstream face of the dam shall be constructed with a slope not steeper than 2½:1, and the downstream face on a slope not steeper than 2:1. The crest or top of the finished dam shall be not less than 8 feet in width.

The upstream two-thirds of the dam shall be constructed of the most impervious materials, such as clay loam, or a mixture of clay and sand, and the downstream one third of more pervious material, such as sand or gravel. The upstream face of the dam shall be adequately protected against wave action by stone riprap, or other suitable materials.

Outlet—Should the state engineer so require, there shall be located beneath the dam a galvanized, corrugated steel pipe of No. 14 gauge and not less than 8 inches in diameter, equipped with a suitable control valve attached to the upstream end of the pipe, together with suitable mechanism for operating the valve. Such outlet pipe, when required, shall be provided with concrete collars enclosing each joint of the pipe. The pipe shall be placed in a trench bottomed in stable formations, and shall be completely surrounded with well compacted impervious materials.

Spillway—For the protection of the dam, an adequate spillway or channel shall be constructed around one or both ends of the dam, of sufficient width to provide a capacity to carry the entire discharge from the drainage basin above the dam during periods of unusual runoff. The spillway shall be located in stable formations not easily eroded, and shall extend to a point well downstream from the dam. The following table shall be used to determine the necessary depth and width of spillway to meet the above requirements. The top of the dam at all points shall be not less than 4 feet above the bottom of the spillway.

the dam at all points shall be not less than 4 feet above the bottom of the spillway.

Table Showing Required Freeboard, Widths and slopes of Spillways for small Earth Dams, with Drainage Areas above the Same as Shown, Based upon a maximum Peak Runoff of 640 Second Feet per Square Mile, or 1 Second Foot per Acre, with an Allowance of a Minimum Freeboard between the Maximum High Water Line and Top of Dam, of 2.3 Feet, and Maximum Velocities of 3.5 Feet per Second of Time.

AREA OF DRAINAGE BASIN ABOVE DAM IN ACRES	PEAK RUNOFF IN CU. FT. PER SECOND	ASSUMED VELOCITY THROUGH SPILLWAY IN FEET PER SECOND	REQUIRED WIDTH OF SPILLWAY "W" AT NARROWEST POINT IN FEET	DEPTH OF WATER IN SPILLWAY IN FEET	SLOPE OF SPILLWAY IN FEET PER 100 FEET OF LENGTH
100	100	-3.0	22	1.5	0.25
200	200	3.0	44	1.5	0.25
300	300	3.0	66	1.5	0.25
400	400	8.0	88	1.5	0.25
500	500	3.0	110	1.5	0.25
600	600	3.0	133	1.5	0.25
700	700	8.0	155	1.5	0.25
800	800	3.0	177	1.5	0.25
900	900	3.0	200	1.5	0.25
1000	1000	3.0	220	1.5	0.25
1100	1100	8.0	210	1.6	0.25
1200	1200	8.2	214	1.7	0.25
1300	1800	3.3	220	1.7	0.25
1400	1400	8.4	240	1.7	0.25
1500	1500	8.4	260	1.7	0.25
1600	1600	3.5	270	1.7	0.25
1700	1700	3.5	285	1.7	0.25
1800	1800	3.5	800	1.7	0.25
1900	1900	3.5	315	1.7	0.25
2000	2000	8.5	330	1.7	0.25

The above spillway widths may be reduced at a point 50 feet below intake, by 25 per cent, where the spillway is located the full length thereof in hard clay or shale, and by 50 per cent when located in hard rock formations, if the slope or grade of the bottom is increased accordingly. The grade for clay and shale formations should be 0.30 foot per 100 feet, and for rock formations 0.9 foot per 100 feet. The width of the entrance to the spillway must in all cases be one-third wider than shown in the Table, and the bottom should slope from the lower end of the funnel section, toward the reservoir 1.0 foot in the distance of 50 feet.

slope from the lower end of the funnel section, toward the reservoir 1.0 foot in the distance of 50 feet.

Borrow Pits—Borrow pits, from which materials are taken to build the dam, shall be cleared of all vegetable matter, and no material shall be borrowed within a distance of 50 feet of any part of the dam. Materials excavated from the spillway, when suitable, are to be used in building the dam.

Date 1 Mov. 25 1946 NOV 29 1946

Colo. Space Colo- MR #3

2965

2 Hydrologic Calculations

Runoff Coefficients and Percent Imperviousness Table 6-6
Colorado Springs Rainfall Intensity Duration Frequency Table 6-5
Hydrologic Calculations Summary Form SF-1 for Existing & Developed Conditions
Hydrologic Calculations Summary 5-yr Form SF-2 for Existing & Developed Conditions
Hydrologic Calculations Summary 100-yr Form SF-2 for Existing & Developed Conditions

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent	Runoff Coefficients											
Characteristics	Impervious	2-y	ear	5-y	ear	10-1	year	25-1	year	50-1	year	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business						1				L. T			
Commercial Areas	95	_0.79	0.80	0,81	0.82	0,83	0,84	0.85	0.87	0.87	0.88	0.88	0,89
Neighborhood Areas	70	0.45	0.49	0.49	0,53	0,53	0.57	0,58	0,62	0.60	0.65	0.62	0.68
Residential	1						 -						
1/8 Acre or less	65	0.41	0,45	0.45	0.49	0,49	0.54	0.54	0,59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0,35	0.36	0.42	0,42	0.50	0.46	0.54	0.50	0,58
1/3 Acre	30	0.18	0.22	0.25	0,30	0.32	0.38	0.39	0,47	0.43	0.52	0.47	0.57
1/2 Acre	2,5	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0,46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0,20	0.26	0.27	0.34	0,35	0.44	0.40	0,50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0,63	0.66	0.66	0.70	0,68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	`0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0,07	0,13	0,16	0.23	0,24	0.31	0,32	0.42	0,37	0.48	0.41	0.54
Railroad Yard Areas	40	0,23	0.28	0,30	0,35	0,36	0.42	0.42	0.50	0,46	0.54	0,50	0.58
Undeveloped Areas	 											-	_
Historic Flow Analysis	!							<u>- </u>					
•	2]	0.03	0.05	0.09	0.15	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Greenbelts, Agriculture Pasture/Meadow	0	0.03	0.03	0.09	0.15	0.17	0.25	0.25	0.37	0.30	0.43	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.23	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when		- 60,00	-0.05	-0.50	-0.50	- 0.52	0.02	0.57	0,24	0,00	0.00	0.50	0.20
landuse is undefined)	45	0.26	0.31	0.32	0,37	0.38	0.44	0.44	0.51	0,48	0,55	0.51	0.59
Streets							ļ						
Paved	100	0,89	0.89	0.90	0,90	0.92	0.92	0,94	0.94	0.95	0.95	0.96	0,96
Gravel	80	0.57	0,60	0.59	0.63	0,63	0,66	0.66	0.70	0,68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0,90	0,90	0.92	0.92	0,94	0.94_	0.95	0.95	0.96	0,96
Roofs	90	0.71	0.73_	0.73	0.75	0.75	0.77	0,78	0.80	0.80	0.82	0.81	0,83
Lawns	0	0,02	0.04	80.0	0,15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

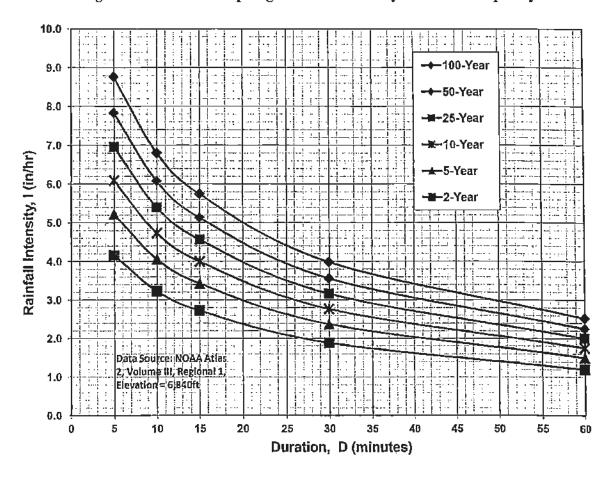


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_s = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Job No.:	61160
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Project: Misfit Crew Estates

(20% Probability)

Design Storm:
Jurisdiction:

5-Year Storm DCM Date: 5/31/2024 11:37
Calcs By: TJW
Checked By:

Sub-Basin and Combined Flows (Modified from Standard Form SF-2)

					Direct F	Runoff			Combine	ed Runoff		9	Streetflo	v		P	ine Flow			т,	ravel Tim	ne .
	Sub-	Area		t _c			Q5	t _c			Q5	Slope	Length	Q	Q	Slope	Mnngs	Length	D _{Pine}			t _t
DP			C5												(cfs)		l					(min)
DP1 DP2 EX-DP3 PP-DP3	PP-C1	flo	0.08 0.08 0.08 0.08 0.08 0.08 0.10 0.10	18.8 26.1 22.1 21.8	Direct CA (Acres) 0.32 0.10 1.78 0.88 1.10	Runoff 15 (in/hr) 3.06 3.19 2.69 2.94 2.96	Q5 (cfs) 0.99 0.31 4.77 2.59 3.26	20.4 #NAME? 22.1	0.32 1.87 0.88	#NAME? 2.94	#NAME? 2.6	Slope (%)	Etreetflov Length (ft)	Q (cfs)	(cfs)	Slope (%)	g data	Length (ft)	D _{Pipe} (in)	Ti Length (ft)	ravel Tim V _{Osc} (ft/s)	

DCM: I = C1 * In (tc) + C2

C1: 1.5 C1: 7.583

Job No.:	61160	
Project:	Miefit Crow Estates	

Project: Mistit Crew Estates

Design Storm: 100-Year Storm (1% Probability)

Jurisdiction: DCM

Date:		5/31/2024 11:37
Calcs By:	TJW	
Checked By:		

Sub-Basin and Combined Flows (Modified from Standard Form SF-2)

					Direct I	Runoff				d Runoff		ı	Streetflov			Р	ipe Flow			Tr	ravel Tim	16
	Sub-	Area		t _c	CA	1100	Q100	t _c	CA	1100	Q100		Length		Q	Slope	Mnnas	Length	D _{Pipe}	Length		t,
DP	Basin	(Acres)	C100	(min)	(Acres)	(in/hr)	(cfs)	(min)	(Acres)	(in/hr)	(cfs)	(%)	(ft)	(cfs)	(cfs)	(%)	n		(in)	(ft)		(min)
				` '	, ,		, ,				` '		, ,					` ′			` '	
	A1	3.89	0.35	20.4	1.37	5.13	7.03															
DP1		3.89	0.35					20.4	1.37	5.13	7.0											
	OS-B1	1.22	0.35	18.8	0.43		2.28															
	B2	20.92	0.35		7.40	4.51	33.36															
DP2		22.14	0.35					#NAME?	7.82	#NAME?	#NAME?											
	EX-C1	11.01	0.35	22.1	3.86	4.94	19.04															
EX-DP3		11.01	0.35					22.1	3.86	4.94	19.0											
	PP-C1	11.01	0.38	21.8	4.19	4.97	20.82															
PP-DP3	PP-C1	11.01	0.38		4.19	4.97	20.02	21.8	4.19	4.97	20.8											
FF-DF3		11.01	0.36					21.0	4.19	4.91	20.0											
		1 04 * 1						l							I.							

DCM: I = C1 * In (tc) + C2

C1: 2.52 C1: 12.735

Sub-Basin Ex-A1 Runoff Calculations

Job No.: 61160 Date: 5/31/2024 11:37 Project: **Misfit Crew Estates** Calcs by: TJW Checked by: В Jurisdiction DCM Soil Type Runoff Coefficient **Surface Type** Urbanization Non-Urban

Basin Land Use Characteristics

	Area			%					
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Pasture/Meadow	168,736	3.87	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved			0.89	0.9	0.92	0.94	0.95	0.96	100%
Roofs	789	0.02	0.71	0.73	0.75	0.78	8.0	0.81	90%
Combined	169,525	3.89	0.02	0.08	0.15	0.25	0.30	0.35	0.4%

169525

Basin Travel Time

Sha	allow Channel Gro	ound Cover	Short Past	ure/Lawns			
	$L_{\text{max,Overland}}$	300	ft		C_v	7	
	L (ft)	ΔZ_0 (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)	
Total	500	26	-	-	-	-	
Initial Time	300	16	0.053	-	18.3	N/A DCM Eq. 6-	-8
Shallow Channel	200	10	0.050	1.6	2.1	- DCM Eq. 6-	-9
Channelized			0.000	0.0	0.0	- V-Ditch	
				t _c	20.4 n	nin.	

Rainfall Intensity & Runoff

/11						
	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.44	3.06	3.57	4.08	4.59	5.13
Runoff (cfs)	0.2	1.0	2.1	4.0	5.4	7.0
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.2	1.0	2.1	4.0	5.4	7.0
DCM:	I = C1 * In	(tc) + C2				

C1 1.19 1.5 1.75 2 2.25 2.52 C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations - DP1

Includes Basins A1

Job No.: 61160 Date: 5/31/2024 11:37

Checked by:

Project: Misfit Crew Estates Calcs by: TJW

Jurisdiction DCM Soil Type

Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

	Area	Area			Runoff Coefficient							
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.			
Pasture/Meadow	168,736	3.87	0.02	0.08	0.15	0.25	0.3	0.35	0%			
Paved	-	0.00	0.89	0.9	0.92	0.94	0.95	0.96	100%			
Roofs	789	0.02	0.71	0.73	0.75	0.78	8.0	0.81	90%			
Combined	169.525	3.89	0.02	0.08	0.15	0.25	0.30	0.35	0.4%			

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q _i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach Channelized-1 Channelized-2 Channelized-3	A1	-	500	26	-	-	_	-	20.4
Total			500	26					

t_c 20.4 (min)

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas Off-Site DP8

 ${
m Q}_{
m Minor}$ 6.3 (cfs) - 5-year Storm ${
m Q}_{
m Major}$ 14.7 (cfs) - 100-year Storm

Rainfall Intensity & Runoff

11						
	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.44	3.06	3.57	4.08	4.59	5.13
Site Runoff (cfs)	0.22	0.99	2.12	4.01	5.40	7.03
OffSite Runoff (cfs)	-	6.30	-	-	-	14.70
Release Rates (cfs/ac) Allowed Release (cfs)		7.3	7	-		21.7
DCM: 1 C1	l = C1 * In (1.19	(tc) + C2 1.5	1.75	2	2.25	2.52

7.583

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concent These should be the flows

C2

6.035

shown in the summary table for DP1

10.111

11.375

12.735

8.847

Sub-Basin OS-B1 Runoff Calculations

Job No.: 61160 Date: 5/31/2024 11:37 Project: **Misfit Crew Estates** Calcs by: TJW Checked by: DCM В Jurisdiction Soil Type Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

	Area			Runc	off Coeffici	ent			%
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Pasture/Meadow	53,170	1.22	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved			0.89	0.9	0.92	0.94	0.95	0.96	100%
Roofs			0.71	0.73	0.75	0.78	8.0	0.81	90%
Combined	53,170	1.22	0.02	0.08	0.15	0.25	0.30	0.35	0.0%
	53170								

Basin Travel Time

Sha	allow Channel Gro	ound Cover	Short Pastu	ıre/Lawns		
	$L_{max,Overland}$	300	ft		C_{v}	7
	L (ft)	ΔZ_0 (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)
Total	300	15	-	-	-	-
Initial Time	300	15	0.050	-	18.8	N/A DCM Eq. 6-8
Shallow Channel			0.000	0.0	0.0	- DCM Eq. 6-9
Channelized			0.000	0.0	0.0	- V-Ditch
				t _c	18.8 ı	min.

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.55	3.19	3.72	4.25	4.78	5.35
Runoff (cfs)	0.1	0.3	0.7	1.3	1.8	2.3
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.1	0.3	0.7	1.3	1.8	2.3
DCM:	I = C1 * In	(tc) + C2				
C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

Sub-Basin B2 Runoff Calculations

Job No.: 61160 Date: 5/31/2024 11:37 Project: **Misfit Crew Estates** Calcs by: TJW Checked by: Jurisdiction DCM Soil Type Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

	Area			Runc	off Coeffici	ent			%
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Pasture/Meadow	904,717	20.77	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved	1,000	0.02	0.89	0.9	0.92	0.94	0.95	0.96	100%
Roofs	5,621	0.13	0.71	0.73	0.75	0.78	0.8	0.81	90%
Combined	911,338	20.92	0.03	0.08	0.15	0.25	0.30	0.35	0.7%

911338

Basin Travel Time

Sha	allow Channel Gro	ound Cover	Short Past	ure/Lawns			
	$L_{max,Overland}$	300	ft		C_v	7	
	L (ft)	ΔZ_0 (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)	
Total	1,200	78	-	-	-	-	
Initial Time	300	17	0.057	-	17.9	N/A DCM	<i>I</i> Eq. 6-8
Shallow Channel	900	61	0.068	1.8	8.2	- DCM	/I Eq. 6-9
Channelized			0.000	0.0	0.0	- V-Di	tch
				t _c	26.1	min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.15	2.69	3.14	3.58	4.03	4.51
Runoff (cfs)	1.1	4.8	10.1	19.0	25.6	33.4
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.1	4.8	10.1	19.0	25.6	33.4
DCM: I:	= C1 * In (tc) + C2				

DCM: I = C1 * In (tc) + C2 C1 1.19 1.5 1.75 2 2.25 2.52 C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations - DP2

Includes Basins OS-B1 B2

Job No.: 61160 Date: 5/31/2024 11:37

Checked by:

Misfit Crew Estates Project: Calcs by: TJW

Jurisdiction DCM Soil Type

Runoff Coefficient Non-Urban **Surface Type** Urbanization

Basin Land Use Characteristics

	Area			Runc	off Coeffici	ent			%
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Pasture/Meadow	957,887	21.99	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved	1,000	0.02	0.89	0.9	0.92	0.94	0.95	0.96	100%
Roofs	5,621	0.13	0.71	0.73	0.75	0.78	0.8	0.81	90%
Combined	964,508	22.14	0.02	0.08	0.15	0.25	0.30	0.35	0.6%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q _i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-B1	-	300	15	-	-	-	-	18.8
Channelized-1 Channelized-2 Channelized-3	Trap Ditch	2	1,200	78	2	2	2	#NAME?	#NAME?
Total			1,500	93					

2 = Natural, Winding, minimal vegetation/shallow grass

t_c #NAME?

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

 $\mathsf{Q}_{\mathsf{Minor}}$ (cfs) - 5-year Storm $\mathsf{Q}_{\mathsf{Major}}$ (cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	#NAME?	#NAME?	#NAME?	#NAME?	#NAME?	#NAME?
Site Runoff (cfs)	#NAME?	#NAME?	#NAME?	#NAME?	#NAME?	#NAME?
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	-	-	-	-	-

DCM: I = C1 * In (tc) + C2 1.19 1.5 1.75 2.25 2.52 7.583 6.035 8.847 C2 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

Sub-Basin EX-C1 Runoff Calculations

Job No.: 61160 Date: 5/31/2024 11:37 Project: **Misfit Crew Estates** Calcs by: TJW Checked by: В Jurisdiction DCM Soil Type Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

	Area			Runo	off Coeffici	ent			%
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Pasture/Meadow	479,797	11.01	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved			0.89	0.9	0.92	0.94	0.95	0.96	100%
Roofs			0.71	0.73	0.75	0.78	8.0	0.81	90%
	470.707	44.04	2.00	2.22	0.45			2.25	0.00/
Combined	479,797	11.01	0.02	0.08	0.15	0.25	0.30	0.35	0.0%

479797

Basin Travel Time

-						
Sha	allow Channel Gro	und Cover	Short Pasti	ure/Lawns		
	$L_{max,Overland}$	300	ft		C_v	7
	L (ft)	ΔZ_0 (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)
Total	1,110	54	-	-	-	-
Initial Time	300	26	0.087	-	15.6	N/A DCM Eq. 6-8
Shallow Channel	410	18	0.044	1.5	4.7	- DCM Eq. 6-9
Channelized	400	10	0.025	3.8	1.8	- Trap Ditch
				t _c	22.1 ו	min.

Rainfall Intensity & Runoff

•						
	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.35	2.94	3.43	3.92	4.41	4.94
Runoff (cfs)	0.5	2.6	5.7	10.8	14.6	19.0
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.5	2.6	5.7	10.8	14.6	19.0
DCM:	I = C1 * In	(tc) + C2				
				_		

Notes

Sub-Basin PP-C1 Runoff Calculations

Job No.: 61160 Date: 5/31/2024 11:37 Project: **Misfit Crew Estates** Calcs by: TJW Checked by: DCM В Jurisdiction Soil Type Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

Area			Runo	ff Coeffici	ent			%
(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
		0.02	0.08	0.15	0.25	0.3	0.35	0%
		0.89	0.9	0.92	0.94	0.95	0.96	100%
		0.71	0.73	0.75	0.78	0.8	0.81	90%
479,797	11.01	0.06	0.1	0.2	0.29	0.34	0.38	7%
479 797	11 01	0.06	0.10	0.20	0.29	0.34	0.38	7.0%
	(SF)	(SF) (Acres) 479,797 11.01	(SF) (Acres) C2 0.02 0.89 0.71 479,797 11.01 0.06	(SF) (Acres) C2 C5 0.02 0.08 0.89 0.9 0.71 0.73 0.06 0.1	(SF) (Acres) C2 C5 C10 0.02 0.08 0.15 0.89 0.9 0.92 0.71 0.73 0.75 0.06 0.1 0.2	(SF) (Acres) C2 C5 C10 C25 0.02 0.08 0.15 0.25 0.89 0.9 0.92 0.94 0.71 0.73 0.75 0.78 0.06 0.1 0.2 0.29	(SF) (Acres) C2 C5 C10 C25 C50 0.02 0.08 0.15 0.25 0.3 0.89 0.9 0.92 0.94 0.95 0.71 0.73 0.75 0.78 0.8 479,797 11.01 0.06 0.1 0.2 0.29 0.34	(SF) (Acres) C2 C5 C10 C25 C50 C100 0.02 0.08 0.15 0.25 0.3 0.35 0.89 0.9 0.92 0.94 0.95 0.96 0.71 0.73 0.75 0.78 0.8 0.81 0.06 0.1 0.2 0.29 0.34 0.38

479797

Basin Travel Time

Shr	allow Channel Gro	und Cover	Short Dact	uro/Lowns			
Sile	allow Charline Git			uic/Lawiis	_		
	L _{max,Overland}	300	ft		C_v	7	
	L (ft)	ΔZ_0 (ft)	S ₀ (ft/ft)	v (ft/s)	t (min)	t _{Alt} (min)	
Total	1,110	54	-	-	-	-	
Initial Time	300	26	0.087	-	15.3	N/A DCM Eq. 6-	8
Shallow Channel	410	18	0.044	1.5	4.7	- DCM Eq. 6-	.9
Channelized	400	10	0.025	3.8	1.8	- Trap Ditch	
				t _c	21.8	min.	

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.37	2.96	3.46	3.95	4.45	4.97
Runoff (cfs)	1.6	3.3	7.6	12.6	16.6	20.8
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.6	3.3	7.6	12.6	16.6	20.8
DCM:	I = C1 * In	(tc) + C2				

C1 1.19 1.5 1.75 2 2.25 2.52 C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Combined Sub-Basin Runoff Calculations - EX-DP3

Includes Basins EX-C1

Job No.: 61160 Date: 5/31/2024 11:37

Checked by:

Project: Misfit Crew Estates Calcs by: TJW

Jurisdiction DCM Soil Type B

Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

	Area	Area		Runoff Coefficient					%	
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.	
Pasture/Meadow	479,797	11.01	0.02	0.08	0.15	0.25	0.3	0.35	0%	
Paved	-	0.00	0.89	0.9	0.92	0.94	0.95	0.96	100%	
Roofs	-	0.00	0.71	0.73	0.75	0.78	8.0	0.81	90%	
5 Acre	-	0.00	0.06	0.1	0.2	0.29	0.34	0.38	7%	
Combined	479,797	11.01	0.02	0.08	0.15	0.25	0.30	0.35	0.0%	

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q _i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach Channelized-1 Channelized-2 Channelized-3	EX-C1	-	1,110	54	-	-	-	-	22.1
Total			1,110	54					

t_c 22.1 (min)

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas Off-Site DP10

 Q_{Minor} 22.1 (cfs) - 5-year Storm Q_{Major} 53.3 (cfs) - 100-year Storm

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.35	2.94	3.43	3.92	4.41	4.94
Site Runoff (cfs)	0.52	2.59	5.67	10.80	14.59	19.04
OffSite Runoff (cfs)	-	22.10	-	-	-	53.30
Release Rates (cfs/ac)	-		-	-	-	
Allowed Release (cfs)	-	24.7	-	-	-	72.3
DCM: I	= C1 * In ((tc) + C2				71

C1 1.19 1.5 1.75 2 2.25 2.52 C2 6.035 7.583 8.847 10.111 11.375 12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

These are the flows to show in the summary table for DP3

Combined Sub-Basin Runoff Calculations - PP-DP3

Includes Basins PP-C1

Job No.: 61160 Date: 5/31/2024 11:37

Project: Misfit Crew Estates Calcs by: TJW

Jurisdiction DCM Checked by:

Soil Type

Runoff Coefficient Surface Type Urbanization Non-Urban

Basin Land Use Characteristics

Area					%				
Surface	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Pasture/Meadow	-	0.00	0.02	0.08	0.15	0.25	0.3	0.35	0%
Paved	-	0.00	0.89	0.9	0.92	0.94	0.95	0.96	100%
Roofs	-	0.00	0.71	0.73	0.75	0.78	8.0	0.81	90%
5 Acre	479,797	11.01	0.06	0.1	0.2	0.29	0.34	0.38	7%
Combined	479,797	11.01	0.06	0.10	0.20	0.29	0.34	0.38	7.0%

Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. ΔZ_0 (ft)	Q _i (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach Channelized-1 Channelized-2 Channelized-3	PP-C1	-	1,110	54	-	-	-	-	21.8
Total			1,110	54					

t_c 21.8 (min)

Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas Off-Site DP10

 $\begin{array}{cc} Q_{\text{Minor}} & 22.1 \text{ (cfs) - 5-year Storm} \\ Q_{\text{Major}} & 53.3 \text{ (cfs) - 100-year Storm} \end{array}$

Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	2.37	2.96	3.46	3.95	4.45	4.97
Site Runoff (cfs)	1.57	3.26	7.62	12.62	16.65	20.82
OffSite Runoff (cfs)	-	22.10	-	-	-	53.30
Release Rates (cfs/ac)	-		-	-	-	
Allowed Release (cfs)	-	2 <mark>5.4</mark>	-	-	-	74.1
DCM: I	= C1 * In (1	tc) + C2				7
C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

These are the flows to show in the summary table for DP3

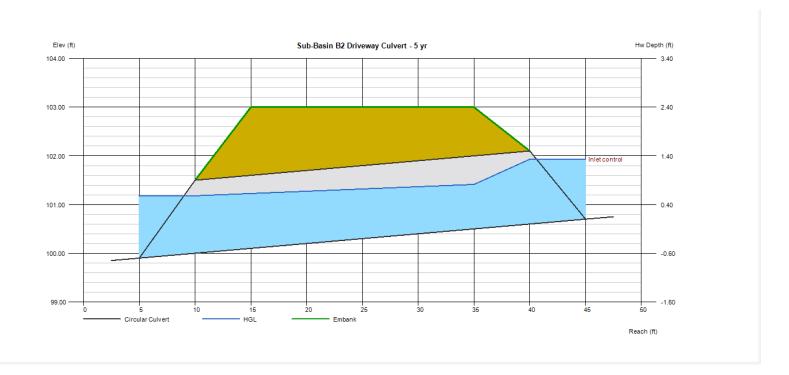
3 Hydraulic Calculations

Excerpts from URS Drainage Report Culvert Calculations

Wednesday, May 8 2024

Sub-Basin B2 Driveway Culvert - 5 yr

Invert Elev Dn (ft)	= 100.00	Calculations	
Pipe Length (ft)	= 30.00	Qmin (cfs)	= 5.00
Slope (%)	= 2.00	Qmax (cfs)	= 5.00
Invert Elev Up (ft)	= 100.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0	, ,	, ,
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 5.00
No. Barrels	= 1	Qpipe (cfs)	= 5.00
n-Value	= 0.023	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 3.35
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 4.77
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 101.18
		HGL Up (ft)	= 101.46
Embankment		Hw Elev (ft)	= 101.93
Top Elevation (ft)	= 103.00	Hw/D (ft)	= 0.89
Top Width (ft)	= 20.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 70.00	-	



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, May 8 2024

Looks like Q100

should be 35.6 cfs? Verify DP2

flows

Sub-Basin B2 Driveway Culvert - 100 yr

Invert Elev Dn (ft) = 100.00Pipe Length (ft) = 30.00Slope (%) = 2.00Invert Elev Up (ft) = 100.60Rise (in) = 18.0= Circular Shape Span (in) = 18.0= 1 No. Barrels n-Value = 0.023

Culvert Type = Circular Corrugate Metal Pipe

Culvert Entrance = Mitered to slope (C)

Coeff. K,M,c,Y,k = 0.021, 1.33, 0.0463, 0.75, 0.7

Embankment

Top Elevation (ft) = 103.00Top Width (ft) = 20.00Crest Width (ft) = 70.00

Calculations

Qmin (cfs) = 34.90 Qmax (cfs) = 34.90 Tailwater Elev (ft) = (dc+D)/2

Highlighted

 Qtotal (cfs)
 = 34.90

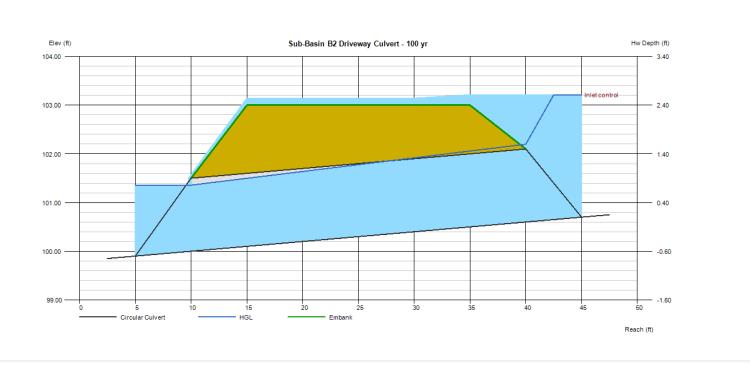
 Qpipe (cfs)
 = 9.94

 Qovertop (cfs)
 = 24.96

Veloc Dn (ft/s)= 5.91Provide outletVeloc Up (ft/s)= 5.63HGL Dn (ft)= 101.50

HGL Up (ft) = 102.20 Hw Elev (ft) = 103.21 Hw/D (ft) = 1.74

Flow Regime = Inlet Control



FINAL DRAINAGE REPORT Hodgen Road State Highway 83 to Black Forest Road

December 8, 2009

Submitted to





El Paso County Public Services Department – Transportation Division &
Pikes Peak Rural Transportation Authority
Prepared by



URS Corporation 9960 Federal Drive, Suite 300 Colorado Springs, CO 80921

URS Project No. 21711554

Culvert Analysis Report P Cu 121+51

Analysis Com	ponent						
Storm Event		Design		Discharge		100.90	cfs
Peak Dischar	ge Method: User-Specified						
Design Disch	arge	100.90	cfs	Check Discharge		49.60	cfs
ii							
Tailwater prop	perties: Trapezoidal Chann	el					
	perties: Trapezoidal Chann ditions for Design Storm.	el					
		100.90	cfs	Bottom Elevation		7,519.00	ft
Tailwater con				Bottom Elevation Velocity		7,519.00 4.11	
Tailwater cond		100.90		Velocity	Velocity	•	
Tailwater conditions of the Discharge Depth	ditions for Design Storm.	100.90	ft	Velocity e HW Elev.	Velocity 15.62 ft/s	•	

Culvert Analysis Report P Cu 121+51

Component:Culvert-1

Culvert Summary					
Computed Headwater Elevation	7,528.27	ft	Discharge	100.90	cfs
Inlet Control HW Elev.	7,528.27	ft	Tailwater Elevation	7,519.45	ft
Outlet Control HW Elev.	7,528.17	ft	Control Type	Infet Control	
Headwater Depth/Height	1.58				
Grades		***************************************			
Upstream Invert	7,522.73	ft	Downstream Invert	7,519.24	ft
Length	164.00		Constructed Slope	0.021280	
Hydraulic Profile					
Profile	S2		Depth, Downstream	2.23	ft
Slope Type	Steep		Normal Depth	2.13	
Flow Regime	Supercritical		Critical Depth	3.08	
Velocity Downstream	15.62	ft/s	Critical Slope	0.009054	ft/ft
Section					
Section Shape	Circular		Mannings Coefficient	0.013	
Section Material	Concrete		Span	3.50	ft
Section Size	42 inch		Rise	3.50	ft
Number Sections	1				
Outlet Control Properties			,		
Outlet Control HW Elev.	7,528.17	ft	Upstream Velocity Head	1.97	ft
Ke	0.20		Entrance Loss	0.39	ft
Inlet Control Properties					
Inlet Control HW Elev.	7,528,27	ft	Flow Control	Submerged	
	ng, 33.7° bevels		Area Full	9.6	ft²
K	0.00180		HDS 5 Chart	3	•
M	2.50000		HDS 5 Scale	В	
С	0.02430		Equation Form	1	
Υ	0.83000		•		

Oversight / NHS

FHWA REGION VIII OVERSIGHT?

■NO □YES

NATIONAL HIGHWAY SYSTEM?

■NO □YES

EL PASO COUNTY PUBLIC SERVICES DEPARTMENT TRANSPORTATION DIVISION

PLAN OF PROPOSED

HODGEN ROAD CORRIDOR IMPROVEMENTS PHASE 1 - SH 83 TO BLACK FOREST ROAD

CONSTRUCTION BID PLANS SEPTEMBER 1, 2010



Related Projects:

R.O.W. Projects: R.O.W. Project Description

P. E. UNDER PROJECT: PROJECT NUMBER: PROJECT CODE:

PPRTA PROJECT #06-00005

END PROJECT HODGEN ROAD STA 210+50.00

TABULATION OF LENGTH

EL PASO COUNTY PROJECT #75173

BEGIN PROJECT STA 10+32.56

END PROJECT 20,017.44 FT STA 210+50.00 (3.79 MI)

DESIGN DATA

DESIGN SPEED	60 MPH
MINIMUM RADIUS	1505'
MAXIMUM SUPERELEVATION RATE	4%
MAXIMUM GRADE	8%

HODGEN RD MURPHY RD

LOCATION MAP

INDEX OF SHEETS

1 TITLE SHEET

2 STANDARD PLANS LIST

3 GENERAL NOTES

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13 KEY MAP & LEGEND

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to 22 GEOMETRIC LAYOUT to 27 SURVEY CONTROL DIAGRAM

28 SURVEY TABULATION

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N.T.S.

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to 105 DRAINAGE AND EROSION CONTROL PLAN

to 112 DRAINAGE PROFILES AND DETAILS

to 116 CONSTRUCTION PHASING

to 131 SIGNING AND STRIPING PLAN

to 133 RETAINING WALL

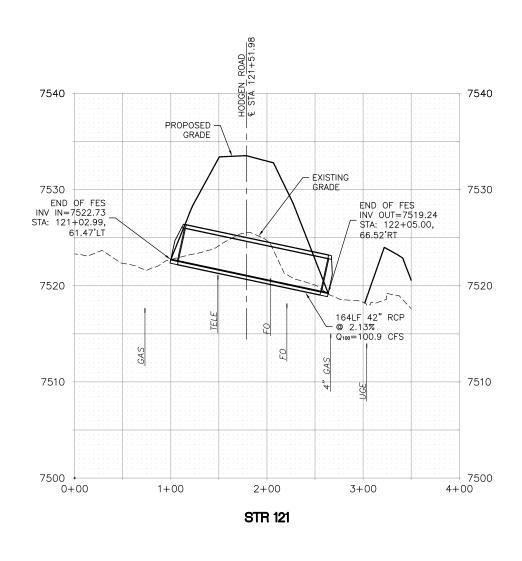
to 137 EXPLORATORY BORINGS

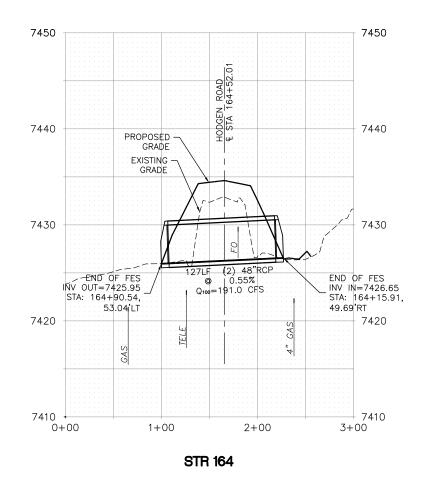
As-Constructed

BEGIN PROJECT HODGEN ROAD STA 10+32.56

9960 FEDERAL DRIVE, SUITE 300 COLORADO SPRINGS, CO. 80921 PHONE (719) 531-0001 FAX (719) 531-0007

Sheet Number





NOTE:

1. PIPES LENGTHS LISTED INCLUDE LENGTH OF FLARED END SECTIONS.

Computer File Information		ndex of	Revisions	
URS File Location: s031w2kfile1\projects\21711554	R-			
Last Modification Date: 31—Aug—10 Operator: MPR	R-			
Mapped Path:p:\hydraulics\sheets	R-			
Drawing File Name: drpr-culverts.dwg	R-			
Acad. Ver.2006 11x17 Scale:1"=100H, 10'V Units: Feet	R-			





URS	
9960 FEDERAL DRIVE SUITE 300 COLORADO SPRINGS, CO (719) 531-0001	80921

HODGEN ROAD CORRIDOR IMPROVEMENTS	JN: 21711554
DRAINAGE PROFILES	Drain. Profiles: 4 of 6

Sheet Number 109

STA. 121+00 TO STA. 165+00

Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Please label storm vear

Existing 42in RCP Under Hodgen Road

Invert Elev Dn (ft) = 7519.24 Pipe Length (ft) = 164.00Slope (%) = 2.13Invert Elev Up (ft) = 7522.73Rise (in) = 42.0Shape = Circular Span (in) = 42.0= 1 No. Barrels n-Value = 0.013

Culvert Type = Circular Concrete

Culvert Entrance = Groove end projecting (C) Coeff. K.M.c.Y.k = 0.0045, 2, 0.0317, 0.69, 0.2

Embankment

Top Elevation (ft) = 7533.50Top Width (ft) = 55.00Crest Width (ft) = 0.00

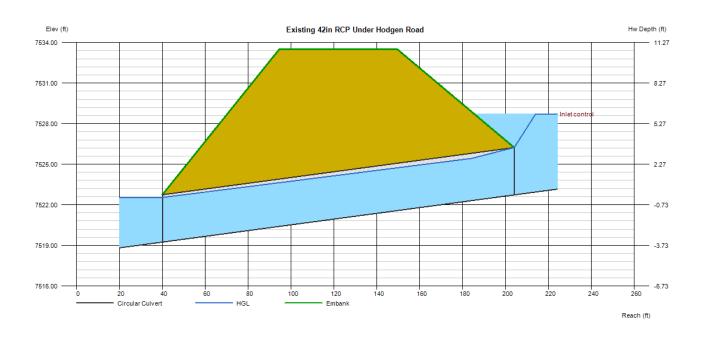
Calculations

Qmin (cfs) = 102.70 Qmax (cfs) = 102.70 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 102.70Qpipe (cfs) = 102.70Qovertop (cfs) = 0.00Veloc Dn (ft/s) = 10.93Veloc Up (ft/s) = 11.41HGL Dn (ft) = 7522.54HGL Up (ft) = 7525.83 Hw Elev (ft) = 7528.72Hw/D (ft) = 1.71

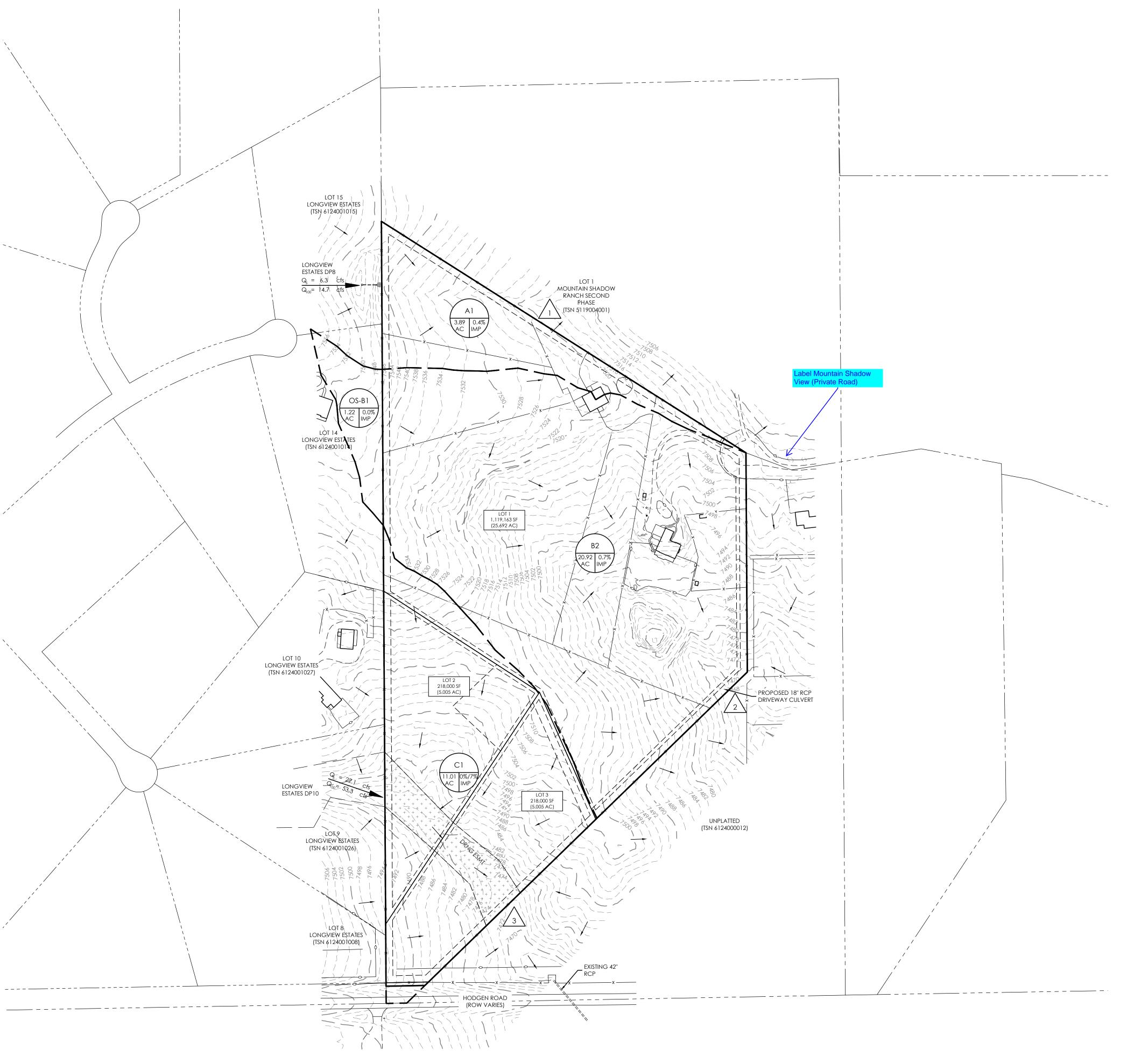
Flow Regime = Inlet Control

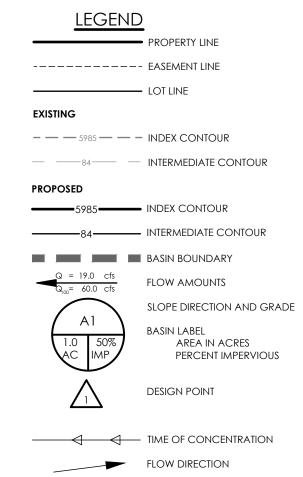


Friday, May 3 2024

4 Report Maps

Existing Condition Hydraulic Analysis Map (Map Pocket) Provide Existing Condition map Proposed Condition Hydraulic Analysis Map (Map Pocket)



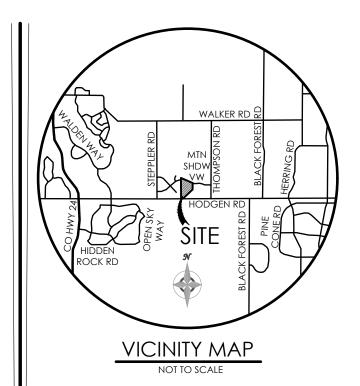


FLOODPLAIN STATEMENT

ACCORDING TO FEMA FLOOD INSURANCE RATE MAP COMMUNITY PANEL NO. 08041CO285 G, DATED DECEMBER 7, 2018, THE PROPERTY IS LOCATED IN ZONE "X", (AREAS DETERMINED TO BE OUTSIDE THE 500-YEAR FLOODPLAIN).

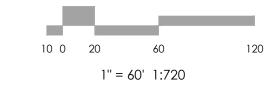
DEVELOPED DRAINAGE SUMMARY TABLE							
DESIGN POINTS	INCLUDED BASINS	AREA (AC)	Tc (MIN.)	RUNOFF Q5 Q100 METHOD (CFS) (CFS)			
	OS-A	0.75	17.0	0.2	1.5	RATIONAL	
	Α	5.67	23.2	1.7	10.0	RATIONAL	
DP-A	OS-A, A	6.42	28.8	1.7	10.0	RATIONAL	
	В	4.69	21.7	1.7	8.9	RATIONAL	
	OS-C	1.87	11.9	1.0	4.7	RATIONAL	
DP-C	B, OS-C	6.57	21.7	2.5	12.5	RATIONAL	

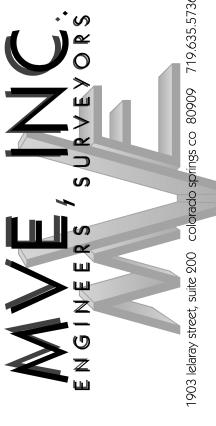
Table does not appear to have been updated. Please revise to match information on map and in hydrology spreadsheets.



BENCHMARK







REVISIONS

DESIGNED BY
DRAWN BY
CHECKED BY _____ ___
AS-BUILTS BY
CHECKED BY _____

MIISFIT CREW
ESTATES

DRAINAGE REPORT

DRAINAGE MAP

MVE PROJECT 61160
MVE DRAWING DRAIN-PP

MAY 21, 2024 SHEET 1 OF 1