# FINAL DRAINAGE REPORT FOR TAMLIN ROAD RV & BOAT STORAGE

Prepared For: C&M Properties, LLC 12748 Barossa Valley Road Colorado Springs, CO 80921

> July 2020 Project No. 2513400

Prepared By: JR Engineering, LLC 5475 Tech Center Drive, Suite 235 Colorado Springs, CO 80919 719-593-2593

#### PCD FILE NO.: PPR1945



#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report. anna an

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Mike Bramlett, Colorado P.E. # 32314	Q14/26 28	Date	
For and On Behalf of JR Engineering, LLC	No.		
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#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

**C&M** Properties, LLC

By:

Title: Address:

the Cando Manager

12748 Barossa Valley Road Colorado Springs. CO 80921

Peter Carroll

Edward-McDonald

#### **EL PASO COUNTY**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended,

#### APPROVED Engineering Department

Jennifer Irvine, P.E. County Engineer/ ECM Administrator

09/09/2020 4:56:20 PM dsdnijkamp **EPC Planning & Community Development Department** 

Conditions:

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- Appendix D Hydraulic Calculations
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# PURPOSE

This document is the Final Drainage report for Tamlin Road Storage Yard. The purpose of this report is to:

- 1. Identify on-site and off-site drainage patterns.
- 2. Recommend storm water facilities to collect and convey storm runoff from the proposed development to appropriate discharge and/or detention locations.
- 3. Recommend water quality and detention facilities to control discharge release rates to below historic.
- 4. Demonstrate compliance with surrounding major drainage basin planning studies, master development drainage plans and flood insurance studies.

# **GENERAL SITE DESCRIPTION**

# LOCATION

Tamlin Road Storage Yard, known as 'the site' from herein, is currently vacant land located in a portion of Section 20, Township 13 South, Range 65 West of the Sixth Principal Meridian in unincorporated El Paso County, Colorado. The site is located northeast of the Tamlin Road and Marksheffel Road intersection. The site is bound by Tamlin Road to the west and north, vacant land owned by Norwood to the east and south. Stetson Hills Filing No. 3 and 4 is located adjacent to the site on the west side of Marksheffel Road. A vicinity map has been presented in Appendix A.

Sand Creek East Fork tributary is located approximately <sup>1</sup>/<sub>4</sub> mile east of the site. The ultimate outfall of this drainageway is Fountain Creek. However, there are no existing stormwater facilities located on site.

#### **DESCRIPTION OF PROPERTY**

The site is approximately 16.5 acres and is covered with sparse trees and native vegetation. There are no existing structures on the site. An existing dirt road proceeds southeast from Tamlin Road through the site to service an existing water tank, located south of the site. There is a ridge that divides the drainage on the site. Roughly 6.5 acres drains southwest with slopes between 3-10% while the remaining 10 acres drains east with slopes up to 8%. In the developed condition, the site will be asphalt drive aisles, parking stalls and a single trash enclosure.

The site is comprised solely of Truckton sandy loam, which is classified as a Type A soil by the NRCS. Group A soils exhibit a high infiltration rate when thoroughly wet and consist chiefly of deep, well drained to excessively drained gravelly sands. These soils have a high rate of water transmission. A NRCS soil survey map is presented in Appendix A.



There are no known irrigation facilities located on the project site. An existing water line (size unknown) runs north-south through the site in a 30' utility easement. Additionally, three gas mains (size unknown) cross the site. Two of the existing gas lines are parallel to the water main within two separate 50' easements. The third gas line runs parallel to Tamlin in a dedicated 50' easement. All existing utilities will remain and no grading will occur within the limits of the easements.

# **EXISTING DRAINAGE CONDITIONS**

# MAJOR BASIN DESCRIPTIONS

The site lies within the West Tributary Sand Creek regional sub basin within the Sand Creek Major Drainage Basin. The "*Sand Creek Drainage Basin Planning Study*" prepared by Kiowa Engineering revised in March 1996, evaluated the Sand Creek Major Drainage Basin, the existing facilities therein and provided recommendations for future development. A map of the Sand Creek regional sub basins is presented in Appendix B.

The Sand Creek Basin covers approximately 54 square miles in unincorporated El Paso County and Colorado Springs, CO. The undeveloped portions of the basin are typified by rolling range land with fair vegetative cover associated with semi-arid climates. The headwaters of the basin are in The Black Forest and general topography trends south to southwest towards its ultimate outfall into Fountain Creek. Per the *Sand Creek DBPS*, the Sand Creek East Fork Subtributary runs outside the western boundary of the site. This drainageway begins at the confluence with the mainstem of East Fork Sand Creek and runs north to Barnes Road.

Based on the FEMA FIRM Map number 08041C0543G and 08041C0545G, the site does not fall within a FEMA defined floodplain and is classified as Zone X, which are areas determined to be outside the 0.2% annual chance floodplain. FIRM maps of the site and surrounding areas have been presented in Appendix A.

# **EXISTING SUB-BASIN DRAINAGE**

Existing drainage patterns are split on the site by a ridge running north-south. The eastern portion of the site drains across undeveloped land to Sand Creek East Fork Subtributary. The western portion of the site drains across Tamlin Road and Marksheffel road into Eastview Estates Filing No. 3 storm sewer. An existing drainage analysis and map are presented in Appendix C and F, respectively.



# **PROPOSED DRAINAGE CONDITIONS**

# **PROPOSED SUB-BASIN DRAINAGE**

In general, runoff generated from the site will be collected and conveyed to a full spectrum water quality and detention pond, Pond A. All proposed parking and drive aisles will be constructed of crushed asphalt. However, there is a possibility of the owner paving the drive aisles and parking stalls with asphalt in the future. Therefore, all calculations (hydrologic and hydraulic) have been performed per the future asphalt condition. The west side of the parcel was not delineated as a basin since the land will not be developed and will continue to follow historic drainage patterns.

The proposed basin descriptions are as follows:

#### Basins Tributary to Proposed Full Spectrum Detention and Water Quality Pond A

Basin A1 consists of approximately 0.09 acres of existing Tamlin Road pavement and undeveloped areas paralleling Tamlin Road. Runoff from these areas will sheet flow southeast to Design Point (DP) #1. From here, Basin A1 flows ( $Q_5 = 0.2$  cfs and  $Q_{100} = 0.4$  cfs) to DP#2 prior to being captured and detained in Full Spectrum Detention and Water Quality Pond A. This is the only offsite flow that will be captured in the proposed pond.

Basin A2 consists of approximately 4.05 acres of crushed asphalt drives, crushed asphalt parking stalls and landscaped areas. Runoff from this basin ( $Q_5 = 13.5$  cfs and  $Q_{100} = 26.0$  cfs) sheet flows southeast to DP #2 before being captured and detained in Full Spectrum Detention and Water Quality Pond A.

Basin A3 consists of approximately 4.72 acres of crushed asphalt drives, crushed asphalt parking stalls and landscaped areas. Runoff from this basin ( $Q_5 = 16.0$  cfs and  $Q_{100} = 30.0$  cfs) sheet flows northeast to DP #2 before being captured in Full Spectrum Detention and Water Quality Pond A.

Basin A4 consists of approximately 0.70 acres and consists of Full Spectrum Detention and Water Quality Pond A. Runoff from this basin ( $Q_5 = 0.3$  cfs and  $Q_{100} = 1.9$  cfs) will be captured within the pond. Full Spectrum Detention and Water Quality Pond A will release at equal to or less than historic rates and is detailed later in this report.

# Basins Not Tributary to Proposed Full Spectrum Detention and Water Quality Pond A (Undetained Release Offsite)

Basin E is an existing offsite basin tributary to the site and is described by Park Engineering in the "Drainage Technical Memo – Trojan Storage 246-67" dated 7/5/16. Refer to the memo and corresponding plan in Appendix B. Basin E consists of approximately 5.55 acres of existing storage buildings and asphalt driveways. Runoff from this basin is routed to an existing water quality /



detention pond located on the northwest side of Tamlin Road. Refer to the drainage maps in Appendix F for the pond location in relation to the site. The discharge from this pond ( $Q_{100} = 5.6$  cfs (the memo does not give the 5-year flow)) enters the existing ditch on the northwest side of Tamlin Road at DP E1. The existing ditch is in a sump condition. Stormwater that overtops Tamlin Road will enter Basin A5 and will be bypassed around the site via proposed swales and a culvert to a proposed low-tailwater basin at DP#4 ( $Q_{100} = 11.0$  cfs). The low-tailwater basin will act as an energy dissipater and release these existing flows across gradually sloping undeveloped land as sheet flow towards the Sand Creek East Fork Subtributary approximately 1,000 feet east.

Basin A5 consists of approximately 1.84 acres of existing Tamlin Road asphalt and undeveloped land. Runoff from this basin ( $Q_5 = 1.2$  cfs and  $Q_{100} = 5.5$  cfs) will follow historic patterns and sheet flow southeast offsite along the property line or enter the proposed swale and discharge offsite at the proposed low-tailwater basin at DP#4. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A5 will not be detained in Full Spectrum Detention and Water Quality Pond A.

Basin A6 consists of approximately 0.22 acres of landscape area and undeveloped land. Runoff from this basin ( $Q_5 = 0.1$  cfs and  $Q_{100} = 0.7$  cfs) will follow historic patterns and sheet flow east offsite at DP#5. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A6 will not be detained in Full Spectrum Detention and Water Quality Pond A.

Basin A7 consists of approximately 0.39 acres of landscape area and undeveloped land. Runoff from this basin ( $Q_5 = 0.2$  cfs and  $Q_{100} = 1.2$  cfs) will follow historic patterns and sheet flow east offsite at DP#6. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A7 will not be detained in Full Spectrum Detention and Water Quality Pond A.

Basin A8 consists of approximately 0.40 acres of landscape area and undeveloped land. Runoff from this basin ( $Q_5 = 0.2$  cfs and  $Q_{100} = 1.2$  cfs) will follow historic patterns and sheet flow east offsite at DP#7. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A8 will not be detained in Full Spectrum Detention and Water Quality Pond A.

Total runoff released offsite along the eastern property line from Basins A5-A8, Basin E, and the Full Spectrum Detention and Water Quality Pond A at design points 4-7 ( $Q_{100} = 20.7$  cfs) is less than the



historic flow at the property line from Basin EX2 at existing design point 2 ( $Q_{100} = 21.2$  cfs). The existing wide grassed gently-sloped swale that receives the flow along the eastern property line is currently stable. Therefore, the proposed development will not negatively impact the receiving swale.

### **DEVELOPMENT CRITERIA REFERENCE**

Storm Drainage Analysis and Design Criteria for this project were implemented from the El Paso County "Drainage Criteria Manual" (DCM) and the "Urban Storm Drainage Criteria Manual" by Urban Drainage and Flood Control District (USDCM).

# HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "El Paso County Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the Colorado Springs Criteria. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the DCM. Time of concentrations were developed using equations from DCM. Water quality and detention pond will be sized per the full spectrum method presented in Chapter 13 of the DCM. All runoff calculations and applicable charts and graphs are included in Appendix A.

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

Table 1 - 1-hr Point Rainfall Data

Rock mulch islands are dispersed throughout the parking areas. Table 6-6 from the El Paso County DCM does not provide a composite percent impervious for rock mulch. The impervious value for gravel, of 80%, does not apply for rock mulch since the gravel impervious value is based upon compacted gravel used for roads. The rock mulch utilized on site will not be compacted and will have undisturbed soil underneath allowing percolation. Table 6-3 from Volume 1 of Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual proposes an impervious value of 40% for packed gravel. JR Engineering is proposing to use a value of 20% for rock mulch areas due to the void space and undisturbed area that increase perviousness.

# HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD UD-Detention v3.07 spreadsheet was



utilized for sizing the water quality and detention pond as well as outlet structure. Manning's equation was used to size the proposed drainage swales in this report.

# **DRAINAGE FACILITY DESIGN**

# FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the Colorado Springs Drainage Criteria Manual, Volume 2 this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff: The Tamlin Road Storage Yard consists of crushed asphalt drive aisles and parking spaces with lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. The IRF worksheet can be found in Appendix C.

Step 2 – Treating the Water Quality Capture Volume: Water Quality treatment for this site is provided in one onsite full spectrum water quality and detention pond. Runoff from the site will sheet flow over the proposed crushed asphalt parking area to the detention pond.

Step 3 – Stabilizing Drainageways: There are no major drainageways on the site that need to be stabilized. No drainage fees are due with this site development plan and final drainage report. If the site were to be platted in the future, drainage fees will be paid at that time in order to help fund major drainage improvements per the "*Sand Creek Drainage Basin Planning Study*". These improvements help stabilize major offsite drainage ways.

Step 4 – Implementing Long Term Source Controls: BMP's will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMP's include crushed asphalt drives and parking.

# WATER QUALITY

Runoff from Basins A1-A4 will be conveyed to Full Spectrum Water Quality and Detention Pond A, located along the site's eastern boundary. All proposed parking and drive aisles will be constructed of crushed asphalt. However, there is a possibility of the owner paving the drive aisles and parking stalls with asphalt in the future. Therefore, all water quality and detention calculations are per the asphalt condition.



Pond A has a total of 9.56 tributary acres for total detention basin volume of 1.262 ac-ft. The pond was designed to accommodate only the flows from Basins A1-A4, not the flow from the existing offsite Basin E, which will bypass the pond. Pond A utilizes a full spectrum outlet structure to detain the WQCV for a 42-hr period, the EURV for a 79-hour period and the 100-yr volume for 86-hr period. Per the UD-Detention spreadsheet found in Appendix E, the outlet structure releases at adequately functions for both Water Quality and EURV and releases at historic rates for the 25, 50 and 100-year storm. The 5-year and 10-year storm release at 0.2 cfs and 0.1 cfs above the historic rates, respectively. The author attempted to further restrict the 5 and 10-year release rate to historic through a variety of techniques but was unable to accomplish the reduction without increasing a second issue of excessive drain time. Please note the EURV release (0.3 cfs) is equal to the historic 10 year release rate (0.3 cfs).

Pond A will discharge into a proposed energy dissipater (low tailwater basin) located along the eastern property line. An existing riprap pad on the adjacent property was placed by others in the past. The pad shows no adverse effects from past storms and further helps disperse the flow. From here, stormwater will maintain historic drainage patterns and release these existing flows into a broad, well vegetated, gently sloping natural swale towards the Sand Creek East Fork Subtributary approximately 1,000 feet east. The downstream swale was analyzed in the 100-year condition assuming that all design points that release offsite (4, 5, 6 and 7), as well as Pond A, have found their way to the swale. The swale was found to have non-erosive velocities of under 2 feet per second. Therefore, the natural swale is adequate and does not require any protection or improvements. Refer to a channel report in Appendix D.

# **EROSION CONTROL PLAN**

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate to be submitted with the Final Drainage Report. We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

# **OPERATION & MAINTENANCE**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities. An Inspection and Maintenance Manual will accompany the Final Drainage Report submittal package.



# FLOODPLAIN STATEMENT

Based on the FEMA FIRM Map number 08041C0543G and 08041C0545G, the site does not fall within a FEMA defined floodplain and is classified as Zone X, which are areas determined to be outside the 0.2% annual chance floodplain. FIRM maps of the site and surrounding areas have been presented in Appendix A.

# **DRAINAGE AND BRIDGE FEES**

The site lies within the Sand Creek Drainage Basin. See Table 2 below for required drainage basin fees. Per El Paso County processes, drainage fees are due at the time of platting. This development is not proposed to be platted and the fees shown in Table 2 below are for informational purposes only. The fees are based on a paved site and have not taken into consideration pond construction credits for the proposed detention pond.

	Tamlin Road Storage Yard Drainage Basin Fees					
	Site% Bridge					
Total	Imperviousnes	Impervious	Drainage	Fee/Impervious		
Area	S	Acres	Fee/Impervious Acre	Acre	Total Fee	
12.41	71.70%	8.9	\$18,940	\$5,559	\$218,041.10	

Table 2 – Basin Fees

# **CONSTRUCTION COST OPINION**

See Table 3 below for cost opinion of private storm sewer infrastructure.

	Private Drainage	<b>Facilities</b>				
Item	Quantity	Unit		Unit Price	Ex	tended Cost
18" RCP	92	LF	\$	45.00	\$	4,140.00
18" FES	3	EA	\$	1,500.00	\$	4,500.00
SPILLWAY (TYPE M RIPRAP)	64	CY	\$	125.00	\$	8,000.00
RIPRAP PADS & TAIL WATER BASIN (TYPE M & L RIPRAP)	90	СҮ	\$	125.00	\$	11,250.00
AGG. BASE COURSE MAINT. ROAD	117	SY	\$	45.00	\$	5,265.00
FULL SPECTURM OUTLET STRUCTURE	1	LS	\$	15,000.00	\$	15,000.00
				Sub-Total	\$	48,155.00
	10% Eng. And Contingency				\$	4,815.50
			(	Grand Total	\$	52,970.50

 Table 3 – Construction Cost Opinion

# SUMMARY

The proposed Tamlin Road RV Storage drainage improvements include storm sewer, a Full Spectrum Detention and Water Quality Pond, and an engineered outfall. The proposed development will not adversely affect the offsite major drainageways or surrounding developments. This report is in conformance with the latest El Paso County Storm Drainage Criteria requirements for this site.



# REFERENCES

- 1. El Paso County Drainage Criteria Manual (Volumes I & II), <u>El Paso County CO, Colorado</u>, Updated May, 2014.
- 2. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), <u>Urban Drainage and Flood Control</u> <u>District</u>, June 2001.
- "Hydrologic Group Rating for El Paso County Area, Colorado", <u>USDA-Natural Resources</u> <u>Conservation Service, National Cooperative Soil Survey</u>. Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov. [June 14, 2019]
- 4. "Sand Creek Drainage Basin Planning Study Final Design Report", <u>Kiowa Engineering</u> <u>Corporation</u>, March 1996.



# Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map







**Conservation Service** 





# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
97	Truckton sandy loam, 3 to 9 percent slopes	A	17.9	100.0%
Totals for Area of Intere	st		17.9	100.0%

# Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

# **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

USDA

Tie-break Rule: Higher

# NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum** of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center** (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

> El Paso County Vertical Datum Offset Table Vertical Datum

> > Offset (ft)

Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

# **Panel Location Map**



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.





# NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

f you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

> El Paso County Vertical Datum Offset Table Vertical Datum

> > Offset (ft

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY

Flooding Source

FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

# Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



# National Flood Hazard Layer FIRMette



### Legend



Appendix B Reference Material



#### El Paso County Drainage Basin Fees Resolution No. <u>18-470</u>

		[	r		
Basin	Receiving	Year	Drainage Basin Name	2019 Drainage Fee	2019 Bridge Fee
Number	Waters	Studied		(per Impervious Acre)	(per Impervious Acre)
Drainage Basins with	DBPS's:				
CHMS0200	Chico Creek	2013	Haegler Ranch	\$10,324	\$1,524
CHWS1200	Chico Creek	2001	Bennett Ranch	\$11,558	\$4,433
CHWS1400	Chico Creek	2013	Falcon	\$29.622	\$4,069
FOFO2000	Fountain Creek	2001	West Fork Jimmy Camp Creek	\$12.564	\$3.717
FOF02600	Fountain Creek	1991*	Big Johnson / Crews Gulch	\$18,350	\$2.370
F0F02800	Fountain Creek	1988*	Widefield	\$18,350	\$0
F0F02900	Fountain Creek	1988*	Security	\$18,350	\$0
F0F03000	Fountain Creek	1991*	Windmill Gulch	\$18,350	\$275
FOFO3100 / FOFO3200	Fountain Creek	1988*	Carson Street / Little Johnson	\$11,192	\$0
FOF03400	Fountain Creek	1984*	Peterson Field	\$13,235	\$1,004
FOFO3600	Fountain Creek	1991*	Fisher's Canvon	\$18,350	\$0
FOFO4000	Fountain Creek	1996	Sand Creek	\$18,940	\$5,559
FOF04200	Fountain Creek	1977	Spring Creek	\$9.517	\$0
FOFO4600	Fountain Creek	1984*	Southwest Area	\$18,350	\$0
FOFO4800	Fountain Creek	1991	Bear Creek	\$18,350	\$1,004
FOFO5400	Fountain Creek	1977	21st Street	\$5.521	\$0
FOF05600	Fountain Creek	1964	19th Street	\$3,611	\$0
FOF05800	Fountain Creek	1964	Camp Creek	\$2.033	\$0
FOMO0400	Monument Creek	1986*	Mesa	\$9,598	\$0
FOMO1000	Monument Creek	1981	Douglas Creek	\$11,540	\$255
FOMO1200	Monument Creek	1977	Templeton Gap	\$11,847	\$275
FOMO1400	Monument Creek	1976	Pope's Bluff	\$3.676	\$627
FOMO1600	Monument Creek	1976	South Rockrimmon	\$4.314	\$0
FOMO1800	Monument Creek	1973	North Rockrimmon	\$5.521	\$0
FOMO2000	Monument Creek	1971	Pulpit Rock	\$6.085	\$0
FOMO2200	Monument Creek	1994	Cottonwood Creek / S. Pine	\$18.350	\$1.004
FOMO2400	Monument Creek	1966	Dry Creek	\$14,486	\$524
FOMO3600	Monument Creek	1989*	Black Squirrel Creek	\$8,331	\$524
FOMO3700	Monument Creek	1987*	Middle Tributary	\$15,312	\$0
FOMO3800	Monument Creek	1987*	Monument Branch	\$18,350	\$0
FOMO4000	Monument Creek	1996	Smith Creek	\$7,481	\$1,004
FOMO4200	Monument Creek	1989*	Black Forest	\$18,350	\$500
FOMO5200	Monument Creek	1993*	Dirty Woman Creek	\$18,350	\$1,004
FOMO5300	Fountain Creek	1993*	Crystal Creek	\$18,350	\$1,004
Miscellaneous Draina	age Basins: 1				
CHBS0800	Chico Creek		Book Ranch	\$17,217	\$2,492
CHEC0400	Chico Creek		Upper East Chico	\$9,380	\$272
CHWS0200	Chico Creek		Telephone Exchange	\$10,306	\$241
CHWS0400	Chico Creek		Livestock Company	\$16,976	\$202
CHWS0600	Chico Creek		West Squirrel	\$8,849	\$3,672
CHWS0800	Chico Creek		Solberg Ranch	\$18,350	\$0
FOFO1200	Fountain Creek		Crooked Canyon	\$5,540	\$0
FOF01400	Fountain Creek		Calhan Reservoir	\$4,625	\$270
	Fountain Creek			\$3,342	\$0
FOF02000	Fountain Creek		Jimmy Camp Creek	\$18,350	\$858
F0F02200	Fountain Creek		Fort Carson	\$14,486	\$524
	Fountain Creek			\$1,209	\$0
FOF05000	Fountain Creek		Midland	\$0,001 \$14,496	\$394 \$504
FOFO6000	Fountain Creek		Palmar Trail	\$ 14,400 \$14,400	\$024 \$504
FOFO6800	Fountain Creek		Black Canyon	\$14,480	\$024 \$524
FOMO4600	Monument Creek		Beaver Creek	\$10,970	\$0
FOMO3000	Monument Creek		Kettle Creek	\$9.909	\$0 \$0
FOMO3400	Monument Creek		Elkhorn	\$1.665	\$0
FOMO5000	Monument Creek		Monument Rock	\$7,953	\$0
FOMO5400	Monument Creek		Palmer Lake	\$12,717	\$0
FOMO5600	Monument Creek		Raspberry Mountain	\$4,278	\$0
PLPL0200	Monument Creek		Bald Mountain	\$9,116	\$0
Interim Drainage Bas	ins: 2				
FOFO1800	Fountain Creek		Little Fountain Creek	\$2,346	\$0
FOMO4400	Monument Creek		Jackson Creek	\$7,263	\$0
FOMO4800	Monument Creek		Teachout Creek	\$5,044	\$758

1. The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies perform

2. Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best available

3. This is an interim fee and will be adjusted when a DBPS is completed. In addition to the Drainage Fee a surety in the amount of \$7,285 per impervious acre shares the DBPS results in a fee greater than the current fee. Fees paid in excess of the future revised fee will be reimbursed. See Resolution 06-326 (9/14/06) and Resolution to the Drainage Fee a surety in the amount of \$7,285 per impervious acre shares a surety in

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# PRELIMINARY/FINAL DRAINAGE REPORT FOR EASTVIEW ESTATES FILING NO. 3

January 2005 Revised November 2005

Prepared For:

### LENNAR COMMUNITIES COLORADO

7222 Commerce Center Drive, Suite 118 Colorado Springs, CO 80919 (719) 593-8583

Prepared By:

#### **JR ENGINEERING**

4310 ArrowsWest Drive Colorado Springs, CO 80907-3449 (719) 593-2593

Job No. 8965.08

Hills subdivision at the varying grade of 2% - 10%. As reported in the "Preliminary/Final Drainage Report for Eastview Estates Filing No. 2" further area study revealed a 42" CMP located under Marksheffel Road, which deposits flow onto the Eastview Estates Filing No. 3. Investigation has lead to the belief that the offsite basin, approximately 23 acres shown as WW-13, will maintain at historic level,  $Q_5 = 14.8$  cfs and  $Q_{100} = 36.9$  cfs. The anticipated runoff from the 7.27 acre Eastview Estates Filing No. 3 will be directed to Antelope Ridge Drive where it is to be collected along with Eastview Estates Filing No. 2 runoff as the surface and subsurface flows mentioned above.

# PROPOSED DRAINAGE CHARACTERISTICS

#### East Fork Sand Creek Drainage Basin

Planned development for Eastview Estates Filing No. 3 is to construct 7.27 acres of planned single-family residential subdivision zoned R1-6000 DFOZ, located north of Willowind at Stetson Hills Filing No. 4, east of Eastview Estates Filing No. 2, and west of Marksheffel Road. Runoff from this single-family site will be intercepted into the existing storm system located in Antelope Ridge Drive, Eastview Estates Filing No. 2.

Per the "Master Development Drainage Plan for Eastview Estates", runoff from future Marksheffel Road, located to the east of the site, will be considered to comply with the assumptions made within the "Final Drainage Report and Plan for Willowind at Stetson Hills Filing Nos. 1, 2, and 3", which states runoff from future roadway will be conveyed to a planned inlet located within Marksheffel Road and conveyed to the existing 6'x 8' box culvert under Barnes Road, with a carryover conveyed to the low point within Barnes Road approximately 300' west of the Marksheffel intersection. Until this completion of Marksheffel Road, flows will be intercepted at the grated inlet of the Manhole at DP-11C.

# Eastview Estates Filing No. 3 Detailed Description

The proposed single-family development is contained within Basins F-1, F-2, F-3, and F-4. These basins are comprised of residential lots and public streets. "Preliminary/Final Drainage Report for Eastview Estates Filing No. 2" previously analyzed runoff flows from this area and

the impact Eastview Estates Filing No. 3 would have on the existing storm sewer and surface flows to off-site developments. Since then, changes in grading and roadway layout have altered the site to the now proposed Basins F-1, F-2, F-3, and F-4.

Basin F-1 is comprised of residential lots and streets. Basin F-1 (4.12 acres,  $Q_5 = 10.1 \text{ cfs}$ ,  $Q_{100} = 21.1 \text{ cfs}$ ), along with flow-by from the inlet at DP-9 (FB  $Q_5 = 1.5 \text{ cfs}$ , FB  $Q_{100} = 4.6 \text{ cfs}$ ) are combined and collected at DP-9B ( $Q_5 = 8.1 \text{ cfs}$ ,  $Q_{100} = 18.3 \text{ cfs}$ ) by an existing 20' D-10-R atgrade inlet. The flows are routed via an existing 18'' RCP storm pipe and combine with SD-2, in the existing 30'' RCP storm main within Antelope Ridge Drive at SD-3 ( $Q_5 = 29.9 \text{ cfs}$ ,  $Q_{100} = 59.7 \text{ cfs}$ ).

Offsite Basin OS-1 (2.98 Acres,  $Q_5 = 5.8$  cfs,  $Q_{100} = 13.9$  cfs) consists of portions of the existing Marksheffel Road and undeveloped land. This flow will be intercepted by a proposed city standard manhole with a Neenah 4342 Grated Inlet. A proposed berm will pond the water at the southern portion of Eastview Estates Filing No. 3. In the case that the inlet becomes clogged and unable to handle all of the flow, or basin WW-13 overtops Marksheffel Road, a spillway will be graded to convey excess flows onto the Steward Lane Cul-de-sac. The flows would then be carried in the street as surface flows. Basin OS-1 will contribute flows to the proposed system until Marksheffel Road is completed to its fully developed width. Upon this completion flows will be entirely contained within the basin WW-A6 (Discussed in the Final Drainage Report and Plan for Willowind at Stetson Hills Filing Nos. 1, 2, and 3), providing reduced runoff into the proposed system.

Offsite Basin WW-13 (23.42 Acres,  $Q_5 = 14.8$  cfs,  $Q_{100} = 36.9$  cfs) currently conveys historic flows that are collected in an existing 42" CMP under Marksheffel Road (Preliminary/Final Drainage Report for Eastview Estates Filing No. 2). This flow will be intercepted by a proposed city standard Type I manhole with grated inlet. This inlet also collects the flow prior to completion of Marksheffel Road in Basin OS-1 (2.98 Acres,  $Q_5 = 5.8$  cfs,  $Q_{100} = 13.9$  cfs). The flows are then routed via a proposed 30" RCP westerly where they combine with SD-3 ( $Q_5 =$ 29.9 cfs,  $Q_{100} = 59.7$  cfs) and SD-8 ( $Q_5 = 10$  cfs,  $Q_{100} = 18$  cfs, Preliminary/Final Drainage Report for Eastview Estates Filing No. 2) at SD-4 ( $Q_5 = 52.3$  cfs,  $Q_{100} = 109.9$  cfs).

BASIN	AREA (acres)	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (crs)
OS-C	7.2	14.2	29.7
OS-D	6.3	8.9	18.6
OS-E	3.9	6.3	13.1
OS-G	5.3	10,4	21.8
OS-H	3.5	5.2	11.0
0S-1	3.0	5.5	11.5
OS-J1	1.3	2.2	4.5
F-1	4.1	10.1	21.1
F-2	4.0	12.0	25.0
F-3	0.4	1.0	2.2
F-4	0.3	0.8	1.7
OS-1	1 3.0	5.8	13.9
WW-13	23.4	14.8	36.8

DESIGN	Q5 (CFS)	Q <sub>100</sub> (cfs)	
DP-9	6.2	13.1	
DP-9-B	8.1	18.3	
DP-10-A	5.2	11.0	Ĺ
DP-10-B	9.7	20.3	
DP-11-A	12.6	30.2	
DP-11-B	8.9	21.5	
DP-11-C	17.6	43.5	

STORM DRAIN	Q5 (CFS)	Q <sub>100</sub> (cfs)
SD-2	26	52
SD-3	29.9	59.7
SD-8	<u> </u>	18
SD-4	52.3	109.9
SD-5	58.3	122.1
SD-6	69	143



# EASTVIEW FILING NO. 3

CITY OF COLORADO SPRINGS, COUNTY CF EL PASO, STATE OF COLORADO

# DRAINAGE PLAN

JANUARY 2005

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EXIST: 42" RC STORM, SEAFE	WAY ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING	
	WORK. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FO ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS	
	ABOVE GROUND AND UNDERGROUND UTILITIES.	Q Z
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	CITY OF COLORADO SPRINGS DEPT. OF UTILITIES GAS, ELECTRIC, WATER AND WASTEWATER	TVIE
	PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF	
	OF JR ENGINEERING	
· ///		
	AARON B. EGBERT, COLORADO P.E. #34208 DATE	
		LOB NO. 28965.08

# EASTVIEW ESTATES FILING NO. 3

# GENERAL NOTES

- 1. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE EXISTENCE AND LOCATION OF ALL UNDERGROUND UTILITIES ALONG THE SITE. THE OMISSION FROM OR THE INCLUSION OF UTILITY LOCATIONS ON THE PLANS IS NOT TO BE CONSIDERED AS THE NONEXISTENCE OF OR A DEFINITE LOCATION OF EXISTING UNDERGROUND UTILITIES.
- 2. THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES, BUILDINGS, FENCES, AND ROADWAYS FROM DAMAGE DUE TO THIS OPERATION. ANY DAMAGE TO THE ABOVE WILL BE REPAIRED AT THE CONTRACTOR'S EXPENSE. AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.
- 3. OVERLOT GRADING SHALL BE COMPLETED TO A SUBGRADE TOLERANCE OF PLUS OR MINUS 0.2'.
- 4. CONTRACTOR SHALL OBTAIN COPIES OF THE SOILS REPORT FROM THE GEOTECHNICAL ENGINEER, AND THEY SHALL BE KEPT ONSITE DURING ALL EARTHWORK OPERATIONS.
- 5. THE SITE SHALL BE STRIPPED A MINIMUM OF 0.5' BELOW EXISTING GRADE.
- 6. MAXIMUM CUT/FILL SLOPES SHALL NOT EXCEED 3:1, UNLESS OTHERWISE NOTED.
- 7. DUST CONTROL SHALL BE SUPPLIED BY THE GRADING CONTRACTOR THROUGH THE DURATION OF OVERLOT GRADING ACTIVITIES PER THE COUNTY HEALTH DEPARTMENT SPECIFICATIONS.
- 8. BENCHMARKS:

A. 3-1/2" ALUMINUM CAP IN VALVE BOX AT THE NORTHEAST CORNER SECTION 20, T13S R65W. INTERSECTION MARKSHEFFEL ROAD AND STETSON HILLS BOULEVARD. EL = 6774.39

B. 1/4 CORNER SECTIONS 20/21, 3-1/2" ALUMINUM CAP IN VALVE BOX, MARKSHEFFEL ROAD. EL = 6700.59

# GRADING/EROSION CONTROL PLAN NOTES:

- 1. ANY LAND DISTURBANCE BY ANY OWNER, DEVELOPER, BUILDER, CONTRACTOR, OR OTHER PERSON SHALL COMPLY WITH THE BASIC GRADING, EROSION ADN STORMWATER QUALITY CONTROL REQUIREMENTS AND GENERAL PROHIBITIONS NOTED IN THE DRAINAGE CRITERIA MANUAL, VOLUME 2.
- 2. NO CLEARING, GRADING, EXCAVATION, FILLLING OR OTHER LAND DISTURBING ACTIVITES SHALL BE PERMITEED UNTIL SIGNOFF AND ACCEPTANCE OF THE GRADING PLAN AND EROSION AND STORMWATER QUALITY CONTROL PLAN IS RECEIVED FROM CITY ENGINEERING.
- 3. THE INSTALLATION OF THE FIRST LEVEL OF TEMPORARY EROSION CONTROL FACILITIES AND BMP'S SHALL BE INSTALLED AND INSPECTED PRIOR TO ANY EARTH DISTURBANCE OPERATIONS TAKING PLACE. CALL CITY STORMWATER INSPECTIONS, 385-5980, 48 HOURS PRIOR TO CONSTRUCTION.
- 4. SEDIMENT (MUD AND DIRT) TRANSPORTED ONTO A PUBLIC ROAD, REGARDLESS OF THE SIZE OF THE SITE, SHALL BE CLEANED AT THE END OF EACH DAY.
- CONCRETE WASH WATER SHAL NOT BE DISCHARGED TO OR ALLOWED TO RUNOFF TO STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR FACILITIES.
- 6. SOIL EROSION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, OR ANY DISTURBED LAND AREA SHALL BE COMPLETED WITHIN TWENTY-ONE (21) CALENDAR DAYS AFTER FINAL GRADING OR FINAL EARTH DISTURBANCE HAS BEEN COMPLETED. DISTURBED AREAS AND STOCKPILES WHICH ARE NOT AT FINAL GRADE BUT WILL REMAIN DORMANT FOR LONGER THAN 30 DAYS SHALL ALSO BE MULCHED WITHIN 21 DAYS AFTER INTERIM GRADING. AN AREA THAT IS GOING TO REMAIN IN AN INTERIM STATE FOR MORE THAN 60 DAYS SHALL ALSO BE SEEDED. ALL TEMPORARY SOIL EROSION CONTROL MEASURES AND BMP'S SHALL BE MAINTAINED UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED.
- THE GRADING AND EROSION CONTROL PLAN WILL BE SUBJECT TO RE-REVIEW AND RE-ACCEPTANCE BY THE CITY OF COLORADO SPRING ENGINEERING SHOULD ANY OF THE FOLLOWING OCCUR: GRADING DOES NOT COMMENCE WITH 12 MONTHS OF THE CITY ENGINEER'S ACCEPTANCE OF THE PLAN; A CHANGE IN PROPERTY OWNERSHIP; PROPOSED DEVELOPMENT CHANGES; OR PROPOSED GRADING REVISIONS.
- 8. THE PLAN SHALL NOT SUBSTANTIALLY CHANGE THE DEPTH OF COVER, OR ACCESS TO UTILITY FACILITIES. ADDITIONALLY, THE PLAN SHALL NOT INCREASE OR DIVERT WATER TOWARDS UTILITY FACILITIES. ANY CHANGES TO UTILITY FACILITES TO ACCOMMODATE THE PLAN MUST BE DISCUSSED AND AGREED TO BY THE AFFECTED UTILITY PRIOR TO IMPLEMENTING THE PLAN. THE RESULTING COST TO RELOCATE OR PROTECT UTILITIES, OR PROVIDE INTERIM ACCESS IS AT THE EXPENSE OF THE PLAN APPLICANT.
- TIMING: ANTICIPATED STARTING AND COMPLETION TIME PERIOD OF ALL GRADING: JAN. 2006 TO JULY 2006

EXPECTED DATE ON WHICH THE FINAL STABLIZATION WILL BE COMPLETED: AUG. 2006

AREAS: TOTAL AREA OF THE SITE TO BE CLEARED, EXCAVATED OR GRADED: 7.270 ACRES **RECEIVING WATERS:** 

NAME OF RECEIVING WATERS: SAND CREEK

# EROSION CONTROL COST ESTIMATE:

1.	770 LF SILT FENCE @ \$1.50/LF	\$ 1,155.00
2.	5 EACH - STRAW BALE CHECK DAM @ \$12.00/DAM INCL. LABOR	\$ 60.00
3.	2 EACH - VEHICLE TRACKING CONTROL @ \$500.00/EACH	\$ 1,000.00
4.	1 EACH - INLET PROTECTION @ \$40.00/EACH	\$ 40.00
	SUB TOTAL	\$ 2,255.00
5.	25% MAINTENANCE AND REPLACEMENT	\$ 564.00
5.	TOTAL	\$ 2.819.00

JR ENGINEERING, LLC CANNOT AND DOES NOT GUARANTEE THAT THE CONSTRUCTION COSTS WILL NOT VARY FROM THESE OPINIONS OR PROBABLE. CONSTRUCTION COSTS. THESE OPINIONS REPRESENT OUR BEST JUDGMENT AS A DESIGN PROFESSIONAL FAMILIAR WITH THE CONSTRUCTION INDUSTRY AND IN THIS DEVELOPMENT.

# SHEET INDEX

ITLE SHEET	SHEET 1 OF 4	
VERLOT GRADING PLAN	SHEET 2 OF 4	
ROSION CONTROL PLAN	SHEET 3 OF 4	
ETAIL SHEET	SHEET 4 OF 4	

CITY OF COLORADO SPRINGS, COUNTY OF EL PASO, STATE OF COLORADO

# **OVERLOT GRADING PLAN**

INCLUDING EROSION CONTROL

**JUNE 2005** 



# APPROV/

THIS EROSION SUPERVISION WORK IS PER THE WORK W ADVERSELY CHANNEL, OF

PREPARED U JR ENGINEERII



OWNER/ THE OWNER QUALITY CON CONSTRUCTIO (CDPS) PERM ÀCTIVITY.



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TITLE:

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	AULNUILS: DEVELOPER:	LENNAR COMMUNITIES COLORADO 9990 PARK MEADOWS DRIVE LONETREE, CO 80124 MS. KIM COOPER, (303) 754–0600			DLORADO		UKIVE 24	I	
	CIVIL ENGINEER:	JR ENGINEERING 4310 ARROWSWEST DRIVE COLORADO SPRINGS, COLORADO 80907-3449 MR. AARON B. EGBERT, P.E. (719) 593-2593		RED FOR	NITIES CO		CO 801		54.0600
	ENGINEERING DIVISION:	CITY OF COLORADO SPRINGS 30 S. NEVADA AVENUE, SUITE 702 COLORADO SPRINGS, COLORADO 80903 MR. TIM MITROS, (719) 385-5061		PREPA	COMMU		PARK N ONETREE		303.7
	TRAFFIC ENGINEERING	CITY OF COLORADO SPRINGS 30 S. NEVADA AVENUE COLORADO SPRINGS, COLORADO 80903 MR. DAVE KRAUTH, (719) 385-5908			LENNAR				
	DEVELOPMENT SERVICES:	WASTEWATER DIVISION: CITY OF COLORADO SPRINGS 111 S. CASCADE COLORADO SPRINGS, COLORADO 80905 MR. MATTHEW WILLIAMS, (719) 668-7211 WATER DIVISION: MR. AL JUVERA, (719) 668-8264	a	in ta	UNID			o Springs, C.O. 80907 th	2
	GAS DEPARTMENT:	CITY OF COLORADO SPRINGS 101 S. CONEJOS STREET COLORADO SPRINGS, COLORADO 80903 MR. CHARLES CHACON, (719) 668-3565			2INFE			rive • Colorado	) ) ) ) ) ) ) ) )
2	ELECTRIC DEPARTMENT:	CITY OF COLORADO SPRINGS 30 S. NEVADA AVENUE COLORADO SPRINGS, COLORADO 80903 MR. TONY SIDES, (719) 668-4967						ArrowsWest Dr 082593 • Fax	engineering.co
	TELEPHONE COMPANY:	U.S. WEST COMMUNICATIONS (LOCATORS) (800) 922-1987			1.1	A Uno		430 /	www.jr
		A.T.& T. (LOCATORS) (719)635–3674							
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JOB NO. 28965.08



# EASTVIEW ESTATES FILING NO. 3

CITY OF COLORADO SPRINGS, COUNTY OF EL PASO, STATE OF COLORADO

# **OVERLOT GRADING PLAN**

INCLUDING EROSION CONTROL

JUNE 2005

		THESE DRAWINGS ARE APPROVED BY THE	APPROPRIATE REVIEWING AGENCIES, JR ENCINEERING ADDOVVES THEID LISE	DESIGNATED BY WRITTEN	AUTHORIZATION.
	PREPARED FOR	LENNAR COMMUNITIES COLORADO	9990 PARK MEADOWS DRIVE	LONETREE, CO 80124	303.754.0600
CANTY SUBDIVISION		I-R ENGINEERING	A Westrian Company	4310 ArrowsWest Drive • Colorado Springs, CO 80907	7 <del>19-533-</del> 2533 • Fax: 7 <del>19-528-66</del> 13 www.jengineering.com
EX. 42" CULVERT UNDER MARKSHEFFEL AND THE EASTVIEW ESTATES FILING NO. 3 GRATED MANHOLE (INLET FOR MARKSHEFFEL AND FUTURE FLOWS)	BY DATE	kad 11/10/05	✓		
42" <u>CMP</u> A SEWER = 3 50 25 0 50 100	No. REVISION	1. PER CITY REVIEW COMMENTS			
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THE LOCATIONS OF EXISTING ABOVE GROUND AND UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL ABOVE GROUND AND UNDERGROUND UTILITIES. 48 HOURS BEFORE YOU DIG, CALL UTILITY LOCATORS 1-800-922-1987 UTILITY NOTIFICATION CENTER OF COLORADO GAS, ELECTRIC, WATER AND WASTEWATER PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF JR ENGINEERING A EGUINAL STORE	FACTMEW FCTATES FILING NO 3		OVERLOT GRADING PLAN	INCLUDING EROSION CONTROL	GRADING PLAN
AARON B. EGBENT COLORADO P.E. 454208 DATE	Sł JC	HEET B NO.	2	0F <b>8965</b>	4 5.08

# PARK ENGINEERING CONSULTANTS



# **Technical Memorandum**

To: Brad R Bonnet, Allred & Associates.

From: Joel Seamons, PE, Park Engineering Consultants

Date: 12/14/2015; Revised 01/18/2015, Revised 2/17/16, Revised 3/21/16, Revised 7/5/16

Re: Drainage Technical Memo – Trojan Storage 246-67

#### Design Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



7-5-16

Date

I, the owner/developer have read and will comply with all of the requirements specified in this drainage

ind plan. lenny Date Storage of Stets - Mills, UC Name, Title: 🖁 🕇 Business Name: ~ Blud #217 Address: 1732 Redondo Beach, CA 90228

#### El Paso County:

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Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

P. Brackin, P.E., BUNIFELE. JELLE County Engineer / ECM Administrator Conditions:

10142016 Date

The purpose of this memo is to verify the drainage concept and redesign of the detention pond due to site differing existing conditions for the development of Trojan Storage in Colorado Springs.

Trojan Storage is located at 5210 Tamlin Road Colorado Springs, CO 80938. Currently, this storage complex has 4 existing buildings with a total area of 51,114 sqft. It also has some gravel roads, parking and asphalt pavement at several locations. It also has an existing detention pond with a current capacity of 22,409 cuft plus 1' of freeboard.

The whole site consists of 16.9 acres and it is divided into 3 major basins (two offsite basins and one onsite basin). The West offsite basin (OSW) has 9.98 acres and consists mainly of gravel parking and drains offsite to the southwest. This basin has an imperviousness of 5%. The East offsite basin (OSE) has 1.37 acres it consists mainly of the landscape and swale areas along the edges of the east side of the property. It also includes the southern boundaries of the detention pond. This basin has an imperviousness of 7%.

The only basin that flows into the existing detention pond is basin E. It consists of 5.55 acres, and will have a final imperviousness of 86% after the proposed storage buildings and asphalt driveways get built. It drains into the existing detention pond located on the south of this basin.

The original drainage report titled "Final Drainage Report for a portion of Lot 3, Canty Subdivision No. 2 (Highfields Storage)," was prepared by Classic Consulting Engineers and dated May 2002. According to this report, the original detention pond was designed to hold 1.29 acre-feet (56,192 cuft) but for reasons out of our knowledge it was built smaller than than (estimated existing capacity 22,409 cuft). The existing outlet structure was designed to release 0.6 cfs on the minor 5 year storm and 8 cfs on the 100 year storm.

The expansion project consists of adding 5 additional storage buildings to the existing complex. Out of those 5 buildings only 3 are being planned to be constructed right now and the 3 buildings to the northeast are being considered for the future.

After performing the detention pond calculations by Full Spectrum method (100 yr + 1/2WQCV), it is determined that the new required capacity for the detention pond needs to be 0.92 acre-feet (40,075 cuft). The allowable release rate is 5.55 cfs and the outlet will be designed to drain in 72 hours EURV.

The existing detention pond will be expanded to the north and west in order to expand its capacity. A retaining wall is also being added around the perimeter of the expanded pond in order to obtain the required volume for water quality and detention requirements. The expanded detention pond, as it is being proposed, will have a stage storage capacity of 41,655 cuft plus 1' of freeboard which is more than the required capacity.

The existing pond is also being retrofitted by adding a 0.5% slope concrete trickle pan and a micropool. The micropool will be lined with 6" thick concrete, it will have a surface area of 64 sqft and 2.5' of depth, with an initial surcharge of 4".

The outlet structure is also being retrofitted. The new orifice plate will have 2 rows of 1.41"  $\emptyset$  orifices spaced 11" to drain the EURV in a period of 72 hours. It will also have an 9.0" orifice with an invert at 85.50 and a top weir 2.0' wide with an invert of 86.40 for 100 yr flow.

The existing 30" outlet RCP and flared end section have enough capacity to carry the 100 yr allowable flow (5.55 cfs). This existing pipe has a slope of 3.2% and on the 100 yr event it will only fill up to 0.44' as shown on the attached circular pipe flow calculation.

The existing emergency spillway will be retrofitted to be able to handle the 100 yr flow. The location of the emergency spillway is shown on the drainage plan and the new dimensions are 13' (Bottom width) by 6" high. This emergency spillway has a capacity for the 100 yr flow (24.86 cfs) with a high water elevation of .49' above the low part of the weir, which will still keep it below the top of pond elevation. The downstream face of the emergency spillway will be lined with type "M" riprap on a blanket 13' wide by 20' long.

At the bottom of the outlet pipe flared end section a riprap dissipater is being proposed. It is proposed to be 13' wide and 15' long. The detail for this flow dissipater can be found on the drainage drawings.

An 8' wide stabilized access is also being installed in the detention. This access will have a maximum slope of 15% as indicated on plans.

Please let me know if you have any questions.

#### GRADING & EROSION CONTROL PLANS TROJAN STORAGE

LOT 3. CANTY SUBDIVISION NO. 2

Located in a portion of Sec. 21, T13S, R65W of the 6TH P.M.

County of El Paso. State of Colorado

STANDARD NOTES FOR EL PASO COUNTY GRADING AND EROSION CONTROL

#### REVISED 7/07/10

1. CONSTRUCTION MAY NOT COMMENCE UNTIL A CONSTRUCTION FERMIT IS OBTAINED FROM DEVELOPMENT SERVICES AND A PRECONSTRUCTION CONFERENCE IS HELD WITH DEVELOPMENT SERVICES INSPECTIONS.

2.STORMWATER DISCHARGES FROM CONSTRUCTION STES SHALL NOT CAUSE OR THREATEN TO CAUSE POLLITION, CONTAMINATION, OR DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLITION OF ANY ON-SITE OR OFF SITE WATERS, INCLUDING WETLANDS.

SNOTPHISTNORM ANTINO DEPOTIO IN THESE PLANS IN WOOS OF GRAPHIC REPERINTATION, ALL DESIGN AND CONSTRUCTION RELATED TO RADAS, STORM DRAINAGE AND ERGISION CONTROL SHALL CONFORM TO THE STANDARDS AND FECUREWENTS OF THE WOOT FILL STANDARDS, NOLLINNO THE LAND DEVELOPMENT CODE, THE STANDARDS, NOLLINNO THE LAND DEVELOPMENT CODE, THE ENGINEERING OFFERA MANUAL, THE DRAINAGE OFFERA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS TO REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING.

4.A SERAATE STORWATER MANAGENET FUAN (SMM) FOR THS PROLECT SHALL BE COMPLETE NAM AN ROBORIN NAS STORMATER UALITY CONTROL PERMIT (ESCOP) ISSUED PROR TO COMMENNIA CONSTRUCTION, DURING CONSTRUCTION THE SWMP IS THE SHALL BE LOCATED ON STE AT ALL THES AND SHALL BE KEPT UP TO DATE WITH WORK PROGRESS AND CHARGES IN THE FED.

SONCE THE ESCOP MAS BEEN SSUED. THE CONTRACTOR MAY INSTALL THE INITIAL TAGE ERSONA MAS SOMENTS CONTROL, BMP SA INDICATED ON THE GEC. A PRECONSTRUCTION MEETING BETWEEN THE CONTRACTOR, ENGINEER, MAD EL PASO CONTY WILL BE HED APPLICANT TO COOPONATE THE MEETING THE AND PLACE WHY COUNTY DIS INSPECTIONS STAFF.

COUNTI DOB INSECTIONS JANF. 6 SOL ERGISION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, OR ANY DISTURBED LAND AREA SHALL BE COMPLETE STREAMS, IN ANY DISTURBED LAND AREA SHALL BE COMPLETE DISTURBANCE, HAS EPEN COMPLETED. DISTURBED REAFER AND STORMENT FOR LANS ERFO. COMPLETED. DISTURBED DISTURBANCE TO DORMANT FOR LONGER THAN 30 DAYS SHALL AS DIS BE WUICED TO REMAIN IN AN INTERN STATE FOR MORE THAN BO DAYS SHALL ALSO BE SEEDED. ALL TEMPORARY SOL ENGINE CONTROL MEASURES AND BAR'S SHALL BE MAINTANED UNTL, PERMARMIN SOL ENGINE

7. TEMPORARY SOIL EROSION CONTROL FACILITIES SHALL BE REMOVED AND EARTH DISTURBANCE AREAS GRADED AND STABILIZED WITH PERMANENT SOIL EROSION CONTROL MEASURES PURSUANT TO STANDARDS AND SPECIFICATION PRESCRIBED IN THE COM VOLUME II AND THE ENGINEERING CRITERIA MANUAL (ECM) APPENDIX I.

8.ALL PERSONS ENGAGED IN EARTH DISTURBANCE SHALL IMPLEMENT AND MAINTAN ACCEPTABLE SOIL EROSION AND SEDMENT CONTROL MEASURES INCLUDING BUPSI IN CONFORMACE WITH THE EROSON CONTROL TECHNICAL STANDARDS OF THE DRAINAGE CHITERIA MANUAL (LONG) VOLUME II AND IN ACCORDANCE WITH THE STORMWATER MANAGEMENT PLAN (SWMP)

9.ALL TEMPORARY EROSION CONTROL FACILITIES INCLUDING BMPS AND ALL PERMANENT FACULITES INTENDED TO CONTROL EROSION OF ANY EARTH DISTURBANCE OPERATIONS, SHALL BE INSTALLED AS DEFINED IN THE APPROVED PLANS, THESMMP AND THE DON VOLUME II AND MAINTAINED THROUGHOUT THE DURATION OF THE EARTH DISTURBANCE OPERATION

10. ANY FARTH DISTURBANCE SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVE REDUE ACCELERATIO SOLL ROSION AND RESULTING SEDURENTATION, ALL DISTURBANCES SHALL BE DESIONED, CONSTRUCTED, AND COMPLETE SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME:

ANY TEMPORARY OR PERMANENT FACILITY DESIGNED AND CONSTRUCTED FOR THE CONVEYANCE OF STORWWATER AROUND, THROUGH, OR FROM THE EARTH DISTURBANCE AREA SHALL BE DESIGNED TO LIMIT THE DISCHARGE TO A NON-EROSIVE VELOCIY.

13. EROSION CONTROL BLANKETING IS TO BE USED ON SLOPES STEEPER THAN 3:1.

14. BUILDING, CONSTRUCTION, EXCAVATION, OR OTHER WASTE MATERIAS SMAL INGT EE TEMPORARILY PACED OR STORED III THE MATERIA SMALL INGT EE TEMPORARILY PACED OR STORED III THE WITH AN APPROVED TRAFFIC CONTROL PLANE. BM/PS MAY BE REQUIRED BY EL PASO COUNTY ENGNEERING IF DEEMED NECESSARY, BASED ON SPECIFIC CONDITIONS AND CIRCUMSTANCES.

15. VEHICLE TRACKING OF SOILS AND CONSTRUCTION DEBRIS OFT-SITE SHALL BE MINIMIZED. MATERIALS TRACKED OFFSITE SHALL BE CLEANED UP AND PROPERLY DISPOSED OF IMMEDIATELY.

16. CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL WASTES FROM THE CONSTRUCTION SITE FOR DISPOSAL IN REMEMTS. NO CONSTRUCTION DEBRIS, THES SLASH, BULDING MATERIAL WASTES OR UNVSCD BULDING MATERIALS SHALL BE BURED, DUMPED, OR DISCHARED AT THE SITE.

17. THE OWNER, STE DEVELOPER, CONTRACTOR, AND/OR THEIR AUTHORIZED AGINTS SHALL BE RESPONSED FOR THE REMOVAL OF ALL CONSTRUCTION DEBRIS, DRT, TRASH, ROCK, SEDMENT, AND SAND THAT MAY ACCUMULATE IN THE STORM SETTER OR OTHER DRAINAGE CONVEYANCE SYSTEM AND STORMWATER APPURTENANCES AS A RESULT OF STE DEVELOPMENT.

18. THE QUANTITY OF MATERIALS STORED ON THE PROJECT SITE: IS THE BOARTHY AND THE MARKING STORED OF THE FROGED STREETS STALL BE LIMITED AS MUCH AS PRACTICAL, TO THAT GUARTITY REQUIRED TO PERFORM THE WORK IN AN ORDERLY SEQUENCE. ALL MATERIALS STORED IN STORED AN ANALY MANNER, IN THEIR ORIGINAL CONTAINERS, WITH ORIGINAL MANUFACTURER'S LABELS.

19. NO CHEMICALS ARE TO BE USED BY THE CONTRACTOR, WHICH 19. NO CHEMICALS ARE TO BE USED BY THE CUMINACION, WHICH HAVE THE POTENTIAL TO BE RELEASED IN STORMWATER UNLESSS PERMISSION FOR THE USE OF A SPECIFIC CHEMICAL IS GRANTED IN WRITING BY THE ECM ADMINISTRATOR. IN GRANTING THE USE (OF SUCH CHEMICALS, SPECIAL CONDITIONS AND MONITORING MAY [BE REQUIRED.

20. BULK STORAGE STRUCTURES FOR PETROLEUM PRODUCTS ANLD OTHER CHEMICALS SHALL HAVE ADEQUATE PROTECTION SO AS: TO CONTAIN ALL SPILLS AND PREVENT ANY SPILLED MATERIAL PROM ENTERING STATE WATERS, INCLUDING ANY SURFACE OR SUBSUFFIFACE STORN DRAINAGE SYSTEM OR FACILIES.

21. NO PERSON SHALL CAUSE THE IMPEDIMENT OF STORMWATER: FLOW IN THE FLOW LINE OF THE CURB AND GUTTER OR IN THE DITCHILINE.

22. INDIVIDUALS SHALL COMPLY WITH THE "COLORADO WATER OUJALITY 22. INDIVIDUALS SHALL COMPLY WITH THE COLORADO WATER OUALITY CONTROL ACT (INTE 25, ARTICLE 8, CR5), MOI THE CLEAN WATER ACT (ISI ISIC 1344), IM ADDITON TO THE REQUERTMENTS INCLUDED EXPLOSING ACT (ISIC 1344), IM ADDITON TO THE REQUERTMENTS INCLUDED FEMALE MALE DE GRIANEL BY THE CONTRACTOR PRORT TO CONSTRUCTION (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON CONTROL THESE REQUERTING MOIL LANG ADDITION THE CONTRACTOR PRORT TO THE REQUERT SMOLT LANG ADDITION (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON CONTONIST OF THEME REQUERTING MOLTANE ADDITION (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON CONTONIST OF THEME REQUERTING MOLTANE ADDITION (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON CONTONIST OF THEME REQUERTING MOLTANE ADDITION (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, FUDUTIVE DUST, ETC.), IN THE CONTON (MPGES, TLOODPLAN, 404, FUDUTIVE DUST, FUDUTIVE DUST, FUDUTIVE DUST, FUDUTIVE DUST, FUDUTIVE DUST, FUDUTIVE DUST, FUDUTIVE D

23. ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE AT APPROVED CONSTRUCTION ACCESS POINTS.

24. PRIOR TO ACTUAL CONSTRUCTION THE PERMITEE SHALL VERIRFY THE LOCATION OF EXISTING UTILITIES.

25. A WATER SOURCE SHALL BE AVAILABLE ON SITE DURING EARTHWORK OPERATIONS AND UTILIZED AS REQUIRED TO MINIMILIZE DUST FROM EARTHWORK EQUIPMENT AND WIND.

26. THE SOILS REPORT FOR THIS SITE HAS BEEN PREPARED BY HEPWORTH-PAWLAK GEOTECHNICAL INC, 215267A, 08/28/15 AND SHALL BE CONSIDERED A PART OF THESE PLANS.

27 AT LEASTING DOWN TO THE ALL DEVELOPED SAME TO CONTRACT THE DAY REPORT TO THE ALL DEVELOPE THAT DAY THE DAY REPORT OF CONSTRUCTION ACTIVITY SHALL SUBART A FEMIL TAPYLICATION FOR STOREMETER DISCLARES TO THE COLOROD INFLATIONED OF FUELE HEALTH AND ENVIRONMENT, AND THE DAY AND THE DAY AND ADDRESS TO THE DAY OF COMPLETION OF A STORMARTER MANAGEMENT PLAN (SWMP) OF MICH THIS GRADING AND REVELOP LAND THE ALL SAME APART. FOR MICHAELING AS APPLICATION ACTIVITY SHALL SAME APART. FOR MICHAELING AS APPLICATION ACTIVITY AND APPLICATION ACTIVITY SHALL SAME APART. FOR MICHAELING AS APPLICATION ACTIVITY SHALL SAME APART. FOR MICHAELING AS APPLICATION ACTIVITY SHALL SAME APART. FOR MICHAELING AS APPLICATION ACTIVITY AND APPLICATION ACTIVITY AND APPLICATION ACTIVITY APPLICATIO

COLORADO DEPARTMENT OF PUBLIC HEALTH AND

COLORADO DEPARTMENT OF POBLIC ENVIRONMENT WATER QUALITY CONTROL DIVISION WQCD – PERMITS 4300 CHERRY CREEK DRIVE SOUTH DENVER, CO 80246–1530 ATTN: PERMITS UNIT



VICINITY MAP NTS

SHEET INDEX: 1. COVER SHEET 2. GRADING & EROSION CONTROL PLAN 3. DETENTION POND DETAILS 4. EROSION CONTROL DETAILS

#### EL PASO COUNTY STANDARD SIGNATUE BLOCK

GRADING AND EROSION CONTROL PLANS (STANDLONE)

#### DESIGN ENGINEER'S STATEMENT:

THIS GRADING AND EROSION CONTROL PLAN WAS PREPAED UNDER MY DIRECTION AND SUPERVISION AND IS CORRECT TO THE EST OF MY KNOWLEDG AND BELIEF, SAUD PLAN HAS BEEN PREPARD ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR GRDING AND EROSION CONTROL-BLANS, IACCEPT RESPONSIBILITY FOR MAY LUMBULT EROSION CONTROL-PLANS. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSION ON MY PART IN PREPARING THIS PLAN.

DATE

01/18/16



I, THE OWNER/DEVELOPER HAVE READ AND WILL COMPL'WITH THE REQUIREMENTS OF THE GRADING AND EROSION CONTROLPLAN.

1732 AVIATION BLVD, SUITE 217 REDONDO BEACH, CA 90278

COUNTY PLAN REVIEW IS PROVIDED ONLY FOR CENERAL:ONFORMANCE WITH COUNTY USENG RETIRET, THE COUNTY IS NOT REPORTSIBLE FOR THE ACCURACY AND ADCULACY OF THE DESIGN, DIMENSINS, AND/ OR ELEVATIONS WHICH SHALL BE CONTINUED AT THE JOB SET. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASJMES NO RESPONSIBILITY FOR COMPLETENESS AND/ OR ACCURAC OF THIS DOCUMENT

FILED IN ACCORDANCE WITH THE REQUIREMENTS OF THEEL PASO COUNTY LAND DEVELOPMENT CODE, DRAINAGE CRITERIA IANUAL, VOLUMES I AND 2, AND ENCINEERING CRITERIA MANUAL'S AMENDED.

ANDRE P. BRACKIN, P.E., DATE S J. L. / 2 City COUNTY ENGINEER / ECM ADMINISTRATOR

PROJECT CONTACTS OWNER.

TROJAN STORAGE BRETT HENRY 310-372-8600 BHENRY@TROJANSTORAGE.COM 1732 AVIATION BLVD, SUITE 217 REDONDO BEACH, CA 90278

ARCHITECT: ANCHITECT: ALLRED & ASSOCIATES BRAD BONNET TEL: 303-465-4306 580 BURBANK ST, SUITE 125 BROMFIELD, CO 80020 BRAD@ALLREDARCH.COM

CIVIL ENGINEER: PARK ENGINEERING CONSULTANTS JOEL R. SEAMONS, P.E. 420 21ST AVENUE, SUITE 101 LONGMONT, CO 80501 303.651.6626 2# (0) 303.651.0331 (F) JOEL@PARKENGINEERING.NET

SURVEYOR. JOHN W. TOWNER 121 COUNTY ROAD 5, DIVIDE, CO 80814

#### CONTRACTOR

ABERDEEN CONSTRUCTION TEL: 303-635-2633 FAX: 303635-2297 4158 JASON ST DENVER, CO 80211 RH 286

COUNTY: EL PASO COUNTY DEVELOPMENT SERVICES 2880 INTERNATIONAL CIRCLE, SUITE 110 COLORADO SPRINGS, CO 80910 TELEPHONE: (719)520-6300 FAX: (719)520-6695

UTILITIES: COLORADO SPRINGS UTILITIES 111 S. CASCADE AVE. COLORADO SPRINGS, CO 80903 719-448-4800 800-238-5434



246-67 12/14/15 24667BASE 1 0E

NAME, P.E.

EL PASO COUNTY-COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE

OWNER/DEVELOPER STATEMENT:

fru 1 BRETT HENRY TROJAN STORAGE




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246-67 12/14/15 24



SC-5

Rock Sock (RS) Rock Sock (RS)

SC-5

Inlet Protection (IP)

SC-6

Inlet Protection (IP)

Appendix C Hydrologic Calculations



## **EX. DRAINAGE CALCS**

BASIN SUMMARY TABLE

Tributary	Area	Percent			t <sub>c</sub>	Q <sub>5</sub>	Q <sub>100</sub>
Sub-basin	(acres)	Impervious	C <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)
EX1	6.43	2%	0.05	0.36	13.4	1.2	14.3
EX2	10.08	2%	0.05	0.36	15.4	1.8	21.2

DESIGN POINT														
SUM	SUMMARY TABLE													
Tributary Q <sub>5</sub> Q <sub>100</sub>														
Sub-basin	(cfs)	(cfs)												
1	1.2	14.3												
2	2 1.8 21.2													

#### EX. COMPOSITE % IMPERVIOUS CALCULATIONS

Project Name: TAMLIN ROAD STORAGE YARD

Subdivision: TAMLIN ROAD STORAGE YARD Location: Colorado Springs

FIUJECT Name.	TAIVILIN KOAD STOKAGE TARD
Project No.:	25134.00
Calculated By:	NQJ
Checked By:	

Date: 11/1/19

		Histe	oric Flow Ar	nalysis		Roofs			Basins Total		
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
EX1	6.43	2%	6.43	2.0%	90%	0.00	0.0%	100%	0.00	0.0%	2.0%
EX2	10.08	2%	10.08	2.0%	90%	0.00	0.0%	100%	0.00	0.0%	2.0%
TOTAL	16.51										2.0%

#### Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

#### **Runoff Coefficients** Land Use or Surface Percent Characteristics 2-year 5-year 10-year 25-year 50-year 100-year HSG A&B HSG C&D usiness Commercial Areas Neighborhood Areas 0.79 0.80 0.45 0.49 0.82 0.83 0.84 0.53 0.53 0.57 0.85 0.87 0.87 0.88 0.88 0.89 0.58 0.62 0.60 0.65 0.62 0.68 95 70 0.81 0.49 Residential 65 0.41 0.45 0.49 0.49 0.54 0.54 0.59 0.57 0.62 0.59 0.57 40 0.23 0.23 0.30 0.35 0.46 0.42 0.42 0.49 0.54 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.57 0.62 0.59 0.67 0.57 0.62 0.59 0.67 0.57 0.62 0.59 0.67 0.57 0.62 0.59 0.67 0.57 0.62 0.59 0.67 0.57 0.62 0.59 0.67 0.51 0.52 0.59 0.67 0.51 0.57 0.47 0.57 30 0.12 0.39 0.47 0.51 0.47 0.51 0.47 0.51 1/8 Acre or less 1/4 Acre 1/3 Acre 1/2 Acre 1 Acre 0.15 0.20 0.22 0.28 0.30 0.36 0.37 0.46 0.41 0.51 0.46 0.56 0.12 0.17 0.20 0.26 0.27 0.34 0.35 0.44 0.40 0.50 0.44 0.55 25 20 ndustrial Light Areas Heavy Areas 80 0.57 0.60 0.59 0.63 0.63 0.66 0.66 0.70 0.68 0.72 0.70 0.74 90 0.71 0.73 0.73 0.75 0.75 0.77 0.78 0.80 0.82 0.81 0.83 7 0.05 0.09 0.12 0.19 0.20 0.29 0.30 0.40 0.34 0.46 0.39 0.52 13 0.07 0.13 0.16 0.23 0.34 0.31 0.32 0.42 0.57 0.48 0.41 0.54 40 0.23 0.28 0.30 0.55 0.42 0.52 0.46 0.54 0.51 Parks and Cemeteries Playgrounds Railroad Yard Areas Undeveloped Areas Undeveloped Areas Historic Flow Analysis---Greenbelts, Agriculture Pasture/Meadow Forest Exposed Rock Offsite Flow Analysis (when landuse is undefined) 2 0.03 0.05 0.09 0.16 0.17 0.26 0.26 0.38 0.31 0.45 0.36 0.51 0 0.02 0.04 0.08 0.15 0.15 0.25 0.37 0.30 0.44 0.38 0.50 0 0.20 0.04 0.08 0.15 0.15 0.25 0.37 0.30 0.44 0.35 0.50 0 0.20 0.04 0.08 0.15 0.15 0.25 0.37 0.30 0.44 0.35 0.50 0 0.20 0.044 0.08 0.15 0.15 0.25 0.37 0.30 0.44 0.35 0.51 100 0.89 0.89 0.90 0.92 0.92 0.94 0.94 0.95 0.96 0.96 2 45 0.26 0.31 0.32 0.37 0.38 0.44 0.44 0.51 0.48 0.55 0.51 0.59 Streets Paved 100 0.89 0.89 0.90 0.92 0.92 0.94 0.94 0.95 0.95 0.96 0.96 80 0.57 0.60 0.59 0.63 0.63 0.66 0.66 0.70 0.68 0.72 0.74 Gravel 100 0.89 0.89 0.90 0.90 0.92 0.92 0.94 0.94 0.95 0.95 0.96 0.96 90 0.71 0.73 0.73 0.75 0.77 0.76 0.80 0.80 0.82 0.81 0.83 0 0.02 0.04 0.06 0.15 0.15 0.25 0.37 0.30 0.44 0.83 0.64 0.63 0.64 0.63 0.64 0.64 0.64 0.64 0.63 0.64 0.64 0.64 0.64 0.65 0.65 0.65 0.64 0.64 0.64 Drive and Walks

## EX. COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: TAMLIN ROAD STORAGE YARD Location: Colorado Springs

Project Name: TAMLIN ROAD STORAGE YARD Project No.: 25134.00

Calculated By: NQJ

Checked By:

Date: 11/1/19

		Basins Total	Hydr	ologic Soil	Group		Land Use	!	Mi	nor Coeffici	ents	Ma	jor Coefficie	nts		
Basin ID	Total Area (ac)	Weighted % Imp.	Area A (ac)	Area B (ac)	Area C/D (ac)	Area Historic (ac)	Area Roofs (ac)	Area Paved Roads (ac)	C <sub>5,A,HISTORIC</sub>	C <sub>5,A,ROOFS</sub>	C <sub>5,A, ROADS</sub>	C <sub>100,A, HISTORIC</sub>	C <sub>100,A,ROOFS</sub>	C <sub>100,A, ROADS</sub>	Basins Total Weighted $C_5$	Basins Total Weighted C <sub>100</sub>
EX1	6.43	2.0%	6.43	0.00	0.00	6.43	0.00	0.00	0.05	0.73	0.90	0.36	0.81	0.96	0.05	0.36
EX2	10.08	2.0%	10.08	0.00	0.00	10.08	0.00	0.00	0.05	0.73	0.90	0.36	0.81	0.96	0.05	0.36
TOTAL	16.51	2.0%	16.51	0.00	0.00	16.51	0.00	0.00							0.05	0.36

## EX. STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: TAMLIN ROAD STORAGE YARD

Location: Colorado Springs

#### Project Name: TAMLIN ROAD STORAGE YARD

Project No.: 25134.00

Calculated By:	NQJ
Checked By:	
Date:	11/1/19

		SUB-	BASIN			INITI	AL/OVER	LAND		T	RAVEL TIM	E			tc CHECK				
		DA	٩ΤΑ			1	(T <sub>i</sub> )				(T <sub>t</sub> )			(U	(URBANIZED BASINS)				
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t c	TOTAL	Urbanized t <sub>c</sub>	t <sub>c</sub>		
ID	(ac)	Soils Group	(%)	ا ا		(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)		
	i			,,								1	,P						
EX1	6.43	A	2%	0.05	0.36	54	3.5%	9.2	550	4.7%	10.0	2.2	4.2	13.4	604.0	30.2	13.4		
EX2	10.08	A	2%	0.05	0.36	76	3.9%	10.5	537	3.4%	10.0	1.8	4.9	15.4	613.0	30.9	15.4		
, I	, i	1	í I	,			i I		1	1	I	, I	1	(	1 '	1			

NOTES:

	$t_{\perp} = t_{\perp} + t_{\perp}$	Equation 6.	$0.395(1.1-C_5)\sqrt{L_i}$	Employ 6.2	Table 6-2. NRCS Conve	yance factors, K
		Equation 0	$I_i = \frac{1}{S_0^{0.33}}$	Equation 0-3	Type of Land Surface	Conveyance Factor, K
Where	*				Heavy meadow	2.5
	$t_c =$ computed time of concentration (minutes)		Where:		Tillage/field	5
			$t_i = \text{overland (initial) flow time (minutes)}$		Short pasture and lawns	7
	$t_i$ = overland (initial) flow time (minutes)		$C_5$ = runoff coefficient for 5-year frequency (from Table 6-4)		Nearly bare ground	10
	$t_i$ = channelized flow time (minutes).		$S_o =$ average slope along the overland flow path (ft/ft).		Grassed waterway	15
			L.		Paved areas and shallow paved swales	20
	$I_t = \frac{-I_t}{60K\sqrt{S_o}} = \frac{-I_t}{60V_t}$	Equation 6-4	$t_{i} = (26 - 17i) + \frac{1}{60(14i + 9)\sqrt{S_{i}}}$	Equation 6-5		
Where			Where:			
	$t_i$ = channelized flow time (travel time, min) $L_i$ = waterway length (ft) $S_0$ = waterway slope (ft/ft) $V_i$ = travel time velocity (ft/sec) = K $\sqrt{S_0}$ K = NRCS conveyance factor (see Table 6-2).		$t_c$ = minimum time of concentration for first design point when less than $t_c$ $L_t$ = length of channelized flow path (ft) i = imperviousness (expressed as a decimal) $S_t$ = slope of the channelized flow path (ft/ft).	from Equation 6-1.		

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### **EX. STANDARD FORM SF-3** STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	TAML Color 5-Yea	.IN RO/ ado Sp r	AD STO rings	RAGE	YARD											Proj P Calc Cł	ect Na rojec sulate necke [	ame: t No.: d By: d By: Date:	TAM 2513 NQJ 11/1,	LIN RC 4.00 /19	DAD S	FORA	SE YARD
				DIR	ECT RUN	IOFF			T	OTAL I	RUNO	FF	0	STREE	T		PI	PE		TRAV	'EL TIN	ИE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1	EX1	6.43	0.05	13.4	0.32	3.69	1.2															TOTAL FLOW DISCHARGING TO TAMLIN ROAD
	2	EX2	10.08	0.05	15.4	0.50	3.48	1.7															TOTAL FLOW DISCHARGING OFFSITE TO UNDEVELOPED LAND

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



Notes: Street and Pipe  $\mbox{C*A}$  values are determined by  $\mbox{Q/i}$  using the catchment's intensity value.

#### IDF Equations $I_{100} = -2.52 \ln(D) + 12.735$ $I_{50} = -2.25 \ln(D) + 11.375$ $I_{25} = -2.00 \ln(D) + 10.111$ $I_{10} = -1.75 \ln(D) + 8.847$ $I_5 = -1.50 \ln(D) + 7.583$ $I_2 = -1.19 \ln(D) + 6.035$ Note: Values calculated by equations may not precisely duplicate values read from figure.

#### **EX. STANDARD FORM SF-3** STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name: TAMLIN ROAD STORAGE YARD Project No.: 25134.00 Calculated By: NOJ Checked By: Table Calculated By: Table Calculated Calculated By: Table Calculated Cal

Subdivision:	TAMLIN ROAD STORAGE YARD
Location:	Colorado Springs
Design Storm:	100-Year

Date: 11/1/19

				DIRE	CT RU	NOFF			T	OTAL	RUNO	FF		STREE	Т		PI	IPE		TRAV	'EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	O (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1	EX1	6.43	0.36	13.4	2.31	6.19	14.3															TOTAL FLOW DISCHARGING TO TAMLIN ROAD
	2	EX2	10.08	0.36	15.4	3.63	5.84	21.2															TOTAL FLOW DISCHARGING OFFSITE ALONG WESTERN PROPERTY LINE TO UNDEVELOPED PARCEL

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

### TAMLIN ROAD RV & BOAT STORAGE - PROPOSED DRAINAGE CALCS

	BASIN SUMMARY TABLE														
Tributary Sub-basin	Area (acres)	Percent Impervious	C <sub>5</sub>	C <sub>100</sub>	t <sub>c</sub> (min)	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)								
A1	0.09	33%	0.35	0.55	5.0	0.2	0.4								
A2	4.05	74%	0.71	0.81	6.8	13.5	26.0								
A3	4.72	81%	0.78	0.86	8.5	16.0	30.0								
A4	0.70	0%	0.08	0.35	7.0	0.3	1.9								
A5	1.84	9%	0.15	0.40	8.5	1.2	5.5								
A6	0.22	0%	0.08	0.35	5.0	0.1	0.7								
A7	0.39	0%	0.08	0.35	5.0	0.2	1.2								
A8	0.40	0%	0.08	0.35	5.0	0.2	1.2								
E 5.55 86% 0.79 0.84 n/a n/a 5.6															

DESIGN POINT										
SUMMARY TABLE										
DP#	Q <sub>5</sub>	Q <sub>100</sub>								
DF#	(cfs)	(cfs)								
1	0.2	0.4								
2	28.7	54.6								
3	28.8	56.3								
4	1.2	11.0								
5	0.1	0.7								
6	0.2	1.2								
7	0.2	1.2								
E1	n/a	5.6								

# COMPOSITE % IMPERVIOUS CALCULATIONS

## Subdivision: TAMLIN ROAD RV STORAGE

Location: Colorado Springs

## Project Name: TAMLIN ROAD RV STORAGE

Project No.: 25134.00 Calculated By: RPD

Checked By:

Date: 5/27/20

		Pave	ed Roads (A	sphalt)		Rock Mulch			Lawns		<b>Basins</b> Total
Basin ID	Total Area (ac)	% Imn	Area (ac)	Weighted	% lmn	Area (ac)	Weighted	% lmn	Area (ac)	Weighted	Weighted %
Dasin iD		<i>7</i> 0 mp.		% Imp.	<i>7</i> 0 mp.		% Imp.	<i>7</i> 0 mp.	Al Ca (ac)	% Imp.	Imp.
A1	0.09	100%	0.03	33.3%	20%	0.00	0.0%	0%	0.06	0.0%	33.3%
A2	4.05	100%	2.92	72.1%	20%	0.29	1.4%	0%	0.84	0.0%	73.5%
A3	4.72	100%	3.74	79.2%	20%	0.38	1.6%	0%	0.60	0.0%	80.8%
A4	0.70	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.70	0.0%	0.0%
A5	1.84	100%	0.16	8.7%	20%	0.00	0.0%	0%	1.68	0.0%	8.7%
A6	0.22	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.22	0.0%	0.0%
A7	0.39	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.39	0.0%	0.0%
A8	0.40	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.40	0.0%	0.0%
TOTAL	12.41										56%
POND A TOTAL	9.56									POND A	71%

### COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

#### Subdivision: TAMLIN ROAD RV STORAGE Location: Colorado Springs

Project Name: TAMLIN ROAD RV STORAGE

Project No.: 25134.00

Calculated By: RPD

Checked By:

Date: 5/27/20

	Total Area Basins T		Hydr	ologic Soil (	Group		Land Use		I	Vinor Coefficie	nts		Major Coefficien	ts		
Basin ID	Total Area (ac)	Weighted % Imp.	Area A (ac)	Area B (ac)	Area C/D (ac)	Area Roads (ac)	Area Rock Mulch (ac)	Area Lawns (ac)	C <sub>5,A,ROADS</sub>	$C_{5,A,ROCKMULCH}$	C <sub>5,A, LAWNS</sub>	C <sub>100,A. ROADS</sub>	C <sub>100,A,ROCK MULCH</sub>	C <sub>100,A, LAWNS</sub>	Basins Total Weighted $C_5$	Basins Total Weighted C <sub>100</sub>
A1	0.09	33.3%	0.09	0.00	0.00	0.03	0.00	0.06	0.90	0.21	0.08	0.96	0.37	0.35	0.35	0.55
A2	4.05	73.5%	4.05	0.00	0.00	2.92	0.29	0.84	0.90	0.58	0.08	0.96	0.68	0.35	0.71	0.81
A3	4.72	80.8%	4.72	0.00	0.00	3.74	0.38	0.60	0.90	0.66	0.08	0.96	0.74	0.35	0.78	0.86
A4	0.70	0.0%	0.70	0.00	0.00	0.00	0.00	0.70	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35
A5	1.84	8.7%	1.84	0.00	0.00	0.16	0.00	1.68	0.90	0.04	0.08	0.96	0.18	0.35	0.15	0.40
A6	0.22	0.0%	0.22	0.00	0.00	0.00	0.00	0.22	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35
A7	0.39	0.0%	0.39	0.00	0.00	0.00	0.00	0.39	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35
A8	0.40	0.0%	0.40	0.00	0.00	0.00	0.00	0.40	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35
TOTAL	12.41	56.3%	12.41	0.00	0.00	6.85	0.24	4.89							0.56	0.71

#### Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

I and like or furthers	Dessent						Runoff Co	refficients					
Characteristics	Impervious	2.9	rear	51	rear	10-	year	3	year	50-	year	100	year
		HSG ABS	HSG C&D	HSGARS	HSG C&D	HSG A&S	HSG C&D	HSG ABB	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HIG CRO
Business								1					
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential	-												
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial			<u> </u>			-		-					
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playerounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Indeveloped Areas		<u> </u>	<u> </u>	<u> </u>	-	<u> </u>	<u> </u>	<u> </u>					
Historic flow Apphric		<u> </u>	<u> </u>	<u> </u>		<u> </u>		<u> </u>	<u> </u>	<u> </u>		<u> </u>	<u> </u>
Greenheits Aariculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.76	0.38	0.31	0.45	0.36	12.0
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when													
landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets						-						<u> </u>	L
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawins	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

#### Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

NRCS				Storm Re	turn Period	- 25	
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year
A	C <sub>A</sub> = 0.84 <i>i</i> <sup>1.302</sup>	C <sub>A</sub> = 0.86 <i>i</i> <sup>1.276</sup>	C <sub>A</sub> = 0.87 <i>i</i> <sup>1.232</sup>	C <sub>A</sub> = 0.84 <i>i</i> <sup>1.124</sup>	C <sub>A</sub> = 0.85 <i>i</i> +0.025	C <sub>A</sub> = 0.78 <i>i</i> +0.110	C <sub>A</sub> = 0.65 <i>i</i> +0.254
В	C <sub>B</sub> = 0.84 <i>i</i> <sup>1.169</sup>	C <sub>B</sub> = 0.86 <i>i</i> <sup>1.088</sup>	C <sub>B</sub> = 0.81 <i>i</i> +0.057	C <sub>B</sub> = 0.63 <i>i</i> +0.249	C <sub>B</sub> = 0.56 <i>i</i> +0.328	C <sub>B</sub> = 0.47 <i>i</i> +0.426	C <sub>B</sub> = 0.37 <i>i</i> +0.536
C/D	C <sub>CD</sub> = 0.83 <i>i</i> <sup>1.122</sup>	C <sub>C/D</sub> = 0.82 <i>i</i> +0.035	C <sub>CD</sub> = 0.74 <i>i</i> +0.132	C <sub>CD</sub> = 0.56 <i>i</i> +0.319	C <sub>CD</sub> = 0.49 <i>i</i> +0.393	C <sub>CD</sub> = 0.41 <i>i</i> +0.484	C <sub>C/D</sub> = 0.32 <i>i</i> +0.588

#### TABLE 6-4 UTILIZED TO CALCULATE 'C-VALUE' FOR ROCK MULCH

#### Where:

i = % imperviousness (expressed as a decimal)

 $C_A$  = Runoff coefficient for Natural Resources Conservation Service (NRCS) HSG A soils

 $C_B = \text{Runoff coefficient for NRCS HSG B soils}$ 

 $C_{CD}$  = Runoff coefficient for NRCS HSG C and D soils.

### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: TAMLIN ROAD RV STORAGE

Location: Colorado Springs

Project Name: TAMLIN ROAD RV STORAGE

Project No.: 25134.00 Calculated By: RPD Checked By: Date: 5/27/20

		SUB-I	BASIN			INITI	AL/OVER	LAND		Т	RAVEL TIM	E			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	0.09	А	33%	0.35	0.55	11	2.0%	3.6	250	2.9%	20.0	3.4	1.2	4.8	261.0	22.1	5.0
A2	4.05	А	74%	0.71	0.81	125	5.6%	4.5	455	2.7%	20.0	3.3	2.3	6.8	580.0	15.9	6.8
A3	4.72	А	81%	0.78	0.86	105	1.0%	5.9	517	2.8%	20.0	3.3	2.6	8.5	622.0	14.8	8.5
A4	0.70	А	0%	0.08	0.35	25	25.0%	3.2	160	1.0%	7.0	0.7	3.8	7.0	185.0	29.0	7.0
A5	1.84	А	9%	0.15	0.40	37	5.2%	6.0	275	7.4%	7.0	1.9	2.4	8.5	312.0	26.2	8.5
A6	0.22	А	0%	0.08	0.35	20	22.0%	3.0	25	22.0%	7.0	3.3	0.1	3.1	45.0	26.1	5.0
A7	0.39	А	0%	0.08	0.35	20	25.0%	2.8	25	25.0%	7.0	3.5	0.1	3.0	45.0	26.1	5.0
A8	0.40	А	0%	0.08	0.35	20	18.0%	3.2	25	18.0%	7.0	3.0	0.1	3.3	45.0	26.1	5.0

#### NOTES:

	t = t + t	Fountion	$5.2$ 0.395(1.1-C <sub>5</sub> ) $\sqrt{L_i}$	The state of the	Table 6-2. NRCS Conve	eyance factors, K
	·c · · · · · ·	Equation	$t_i = \frac{S_0^{0.03}}{S_0^{0.03}}$	Equation 0-3	Type of Land Surface	Conveyance Factor, K
Wher	a.				Heavy meadow	2.5
	$t_c$ = computed time of concentration (minutes)		Where:		Tillage/field	5
			$t_i$ = overland (initial) flow time (minutes)		Short pasture and lawns	7
	$t_i$ = overland (initial) flow time (minutes)		$C_5$ = runoff coefficient for 5-year frequency (from Table 6-4) $L_1$ = length of overland flow (ff)		Nearly bare ground	10
	$t_t$ = channelized flow time (minutes).		$S_o =$ average slope along the overland flow path (ft/ft).		Grassed waterway	15
	L. L.			120702-002	Paved areas and shallow paved swales	20
	$t_t = \frac{t_t}{60K\sqrt{S_o}} = \frac{t_t}{60V_t}$	Equation 6-4	$t_{\rm c} = (26 - 17i) + \frac{1}{60(14i + 9)\sqrt{S_{\rm r}}}$	Equation 6-5		
Where			Where:			

Where:

 $t_t =$  channelized flow time (travel time, min)  $L_t$  = waterway length (ft)  $L_1$  – waterway length (h)  $S_0$  = waterway slope (ft/ft)  $V_i$  = travel time velocity (ft/sec) = K $\sqrt{S_0}$  K = NRCS conveyance factor (see Table 6-2).  $t_c$  = minimum time of concentration for first design point when less than t<sub>c</sub> from Equation 6-1.  $L_t$  = length of channelized flow path (ft) i = imperviousness (expressed as a decimal)  $S_t$  = slope of the channelized flow path (ft/ft).

Use a minimum te value of 5 minutes for urbanized areas and a minimum te value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	TAML Colora 5-Year	IN ROA ado Spi r	ND RV S rings	TORAC	GE											Pro I Cali C	ject N Projec culate hecke	ame: et No.: ed By: ed By: Date:	TAMI 2513 RPD 5/27/	<u>IN RO</u> 4.00 20	AD RV	' STOF	RAGE
				DIRE	CT RUI	NOFF			T	OTAL F	RUNO	FF		STREE	Т		PI	PE		TRAV	EL TIN	ΛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	E1	E	5.55	0.81	n/a	n/a	n/a	n/a															BASIN E POND OVERFLOW @ DPE1, SWALE ROUTES FLOW TO DP4
	1	A1	0.09	0.35	5.0	0.03	5.17	0.2					0.2	0.03	2.0					406	2.8	2.4	BASIN A1 FLOW @ DP1, SHEET FLOW TO DP2
		A2	4.05	0.71	6.8	2.86	4.71	13.5															BASIN A2 FLOW @ DP2 (ROUTED IN SF2)
		A3	4.72	0.78	8.5	3.66	4.37	16.0															BASIN A3 FLOW @ DP2 (ROUTED IN SF2)
	2								8.5	6.55	4.37	28.7	28.7	6.55	25.0					35	10.0	0.1	DP1, BASIN A2-A3 FLOW @ DP2, SHEET FLOW TO DP3 (F.S.D. WQ POND)
		A4	0.70	0.08	7.0	0.06	4.67	0.3															BASIN A4 FLOW @ DP3 (ROUTED IN SF2)
	3								8.5	6.61	4.36	28.8											TOTAL BASIN A1-A4 FLOW ENTERING F.S.D. WQ POND
	4	A5	1.84	0.15	8.5	0.28	4.38	1.2															TOTAL BASIN A5 (UNDEVELOPED) FLOW AND BASIN E POND OVERFLOW, SWALE DISCHARGES OFFSITE THRU LOW-TAILWATER BASIN
	5	A6	0.22	0.08	5.0	0.02	5.17	0.1															TOTAL BASIN A6 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	6	A7	0.39	0.08	5.0	0.03	5.17	0.2															TOTAL BASIN A7 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	7	A8	0.40	0.08	5.0	0.03	5.17	0.2															TOTAL BASIN A8 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name: TAMLIN ROAD RV STORAGE Project No.: 25134.00 Calculated By: RPD Checked By: Date: 5/27/20

Subdivision:	TAMLIN ROAD RV STORAGE
Location:	Colorado Springs
Design Storm:	100-Year

																		Juito.	0/2//	20			
				DIRE	CT RUN	IOFF			TC	DTAL F	RUNO	FF	S	TREE	Γ		PI	PE		TRAV	EL TIN	ΛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	E1	E	5.55	0.84	n/a	n/a	n/a	5.6															BASIN E POND OVERFLOW @ DPE1, SWALE ROUTES FLOW TO DP4
	1	A1	0.09	0.55	5.0	0.05	8.68	0.4					0.4	0.05	2.0					406	2.8	2.4	BASIN A1 FLOW @ DP1, SHEET FLOW TO DP2
		A2	4.05	0.81	6.8	3.30	7.90	26.1															BASIN A2 FLOW @ DP2 (ROUTED IN SF2)
		A3	4.72	0.86	8.5	4.08	7.34	30.0															BASIN A3 FLOW @ DP2 (ROUTED IN SF2)
	2								8.5	7.43	7.34	54.6	54.6	7.43	25.0					35	10.0	0.1	DP1, BASIN A2-A3 FLOW @ DP2, SHEET FLOW TO DP3 (F.S.D. WQ POND)
		A4	0.70	0.35	7.0	0.25	7.83	2.0															BASIN A4 FLOW @ DP3 (ROUTED IN SF2)
	3								8.5	7.68	7.33	56.3											TOTAL BASIN A1-A4 FLOW ENTERING F.S.D. WQ POND
	4	A5	1.84	0.40	8.5	0.74	7.36	5.4	n/a	n/a	n/a	11.0											TOTAL BASIN A5 (UNDEVELOPED) FLOW AND BASIN E POND OVERFLOW, SWALE DISCHARGES OFFSITE THRU LOW-TAILWATER BASIN
	5	A6	0.22	0.35	5.0	0.08	8.68	0.7															TOTAL BASIN A6 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	6	A7	0.39	0.35	5.0	0.14	8.68	1.2															TOTAL BASIN A7 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	7	A8	0.40	0.35	5.0	0.14	8.68	1.2															TOTAL BASIN A8 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

Site Lovel	lowIm	nact D	volopr	nont (L		ian Effe	octivo li	morvi	ous Cal	culator			Works	sheet Protect
Sile-Level	LOW III	LID Credi	it by Imp	ervious R	eduction	n Factor (	(IRF) Me	thod	Jus car	culator				
			UE	-BMP (Version	3.06, Novem	ber 2016)								
User Input														
Calculated cells				Designer:	RPD									
				Company:	JR EN	GINEERING								
***Design Storm: 1-Hour Rain Depth WQCV Event	1.19	inches		Date:	May 2	27, 2020								
Minor Storm: 1-Hour Rain Depth 5-Year Event	1.50	inches		Project:	TAML	IN ROAD R	V & BOAT S	TORAGE						
••••Major Storm: 1-Hour Rain Depth 100-Year Event	2.52	inches		Location:	COLO	RADO SPRI	NGS							
Optional User Defined Storm CUHP														
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency 100-Year Event for User Defined Storm 100-Year Event														
Max Intensity for Optional User Defined Storm 0														
TE INFORMATION (USER-INPUT)														
Sub-basin Identifier	A1	A2	A3	A4										
Receiving Pervious Area Soil Type	Sandy Loam	Sandy Loam	Sandy Loam	Sandy Loam										
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	0.085	4.050	4.622	0.699										
Directly Connected Impervious Area (DCIA, acres)	0.000	2.406	3.230	0.000										
Unconnected Impervious Area (UIA, acres)	0.024	0.571	0.551	0.000										
Receiving Pervious Area (RPA, acres)	0.061	0.625	0.251	0.000										
Separate Pervious Area (SPA, acres)	0.000	0.448	0.590	0.699										
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	с	С	С	v										
ALCULATED RESULTS (OUTPUT)														
Total Calculated Area (ac, check against input)	0.085	4.050	4.622	0.699										
Directly Connected Impervious Area (DCIA, %)	0.0%	59.4%	69.9%	0.0%										
Unconnected Impervious Area (UIA, %)	28.2%	14.1%	11.9%	0.0%										
Receiving Pervious Area (RPA, %)	71.8%	15.4%	5.4%	0.0%										
Separate Pervious Area (SPA, %)	0.0%	11.1%	12.8%	100.0%										
A <sub>R</sub> (RPA / UIA)	2.542	0.480	0.456	1.000										
f / I for WOCV Event	0.200	0.400	0.070	0.9										
f / I for 5-Year Event:	0.5	0.5	0.5	0.5										
f / I for 100-Year Event:	0.3	0.3	0.3	0.3										
f / I for Optional User Defined Storm CUHP:														
IRF for WQCV Event:	0.76	0.81	0.86	0.00										
IRF for 5-Year Event:	0.86	0.89	0.93	1.00										
IRF for 100-Year Event:	0.90	0.93	0.96	1.00										L
IRF for Optional User Defined Storm CUHP:		70.71												<u> </u>
Total Site Imperviousness: I <sub>total</sub>	28.2%	73.5%	81.8%	0.0%										⊢
Effective Imperviousness for E. Voor Event:	21.5%	70.8%	80.1%	0.0%										<u> </u>
Effective Imperviousness for 100.Vear Event:	24.3%	72.0%	81.3%	0.0%										
Effective Imperviousness for Optional User Defined Storm CUHP:														
WQCV Event CREDIT: Reduce Detention Bv:	16.6%	4.5%	3.2%	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT**: Reduce Detention By: User Defined CUHP CREDIT: Reduce Detention By:	10.4%	1.3%	0.6%	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
	Total Site Im	perviousness:	71.7%	]	Notes:									
Total Site Effective Impe	rviousness for	WQCV Event:	69.7%	1	* Use Green	Amnt average	e infiltration	rate values fi	om Table 3-3					
Total Site Effective Impe	rviousness for	5-Year Event:	70.6%	1	** Flood cont	trol detention	volume crec	lits based on	empirical eau	iations from S	Storage Chap	ter of USDCM		
Total Site Effective Impervi	ousness for 10	0-Year Event:	71.0%	1	*** Method	assumes that	t 1-hour rainf	all depth is e	quivalent to	1-hour intens	ity for calcula	ition purposed	ł	
Total Site Effective Imperviousness for Option	al User Defined	d Storm CUHP	·	J										

Appendix D Hydraulic Calculations



# Weir Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

# Pond A Spillway (Q\_100 = 34.4 cfs (Per UD-Detention Peak Inflow))

Trapezoidal Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 0.33
Bottom Length (ft)	= 60.00	Q (cfs)	= 34.40
Total Depth (ft)	= 1.21	Area (sqft)	= 20.24
Side Slope (z:1)	= 4.00	Velocity (ft/s)	= 1.70
		Top Width (ft)	= 62.64
Calculations			
Weir Coeff. Cw	= 3.10		
Compute by:	Known Q		
Known Q (cfs)	= 34.40		



# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# Pond A Spillway Channel Q100 = 34.4cfs (Per UD-Detention Peak Inflow)

Trapezoidal		Highlighted	
Bottom Width (ft)	= 60.00	Depth (ft)	= 0.12
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 34.40
Total Depth (ft)	= 1.21	Area (sqft)	= 7.26
Invert Elev (ft)	= 5000.00	Velocity (ft/s)	= 4.74
Slope (%)	= 25.00	Wetted Perim (ft)	= 60.99
N-Value	= 0.035	Crit Depth, Yc (ft)	= 0.22
		Top Width (ft)	= 60.96
Calculations		EGL (ft)	= 0.47
Compute by:	Known Q		
Known Q (cfs)	= 34.40		



Reach (ft)

#### TABLE 10-4

### MAXIMUM PERMISSIBLE VELOCITIES FOR EARTH CHANNELS WITH VARIED GRASS LININGS AND SLOPES

		Permiss: Mean Cha	ible annel
Channel Slope	Lining	Veloci	ity *
0 - 5%	Sodded grass	(10)	
	Bermudagrass	6	
	Reed canarygrass	5	
	Tall fescue	5	
	Kentucky bluegrass	5	
	Grass-legume mixture	4	
	Red fescue	2.	5
	Redtop	2.	5
	Sericea lespedeza	2.	5
	Annual lespedeza	2.	5
	Small grains	2.	5
	(temporary)		-
5 - 10%	Sodded grass	6	
	Bermudagrass	5	
	Reed canarygrass	4	
	Tall fescue	4	
	Kentucky bluegrass	4	
	Grass-legume mixture	3	
Greater than	Sodded grass	5	4.74 < 5 fps
10%	Bermudagrass	4	
	Reed canarygrass	3	
	Tall fescue	3	
	Kentucky bluegrass	3	
<ul> <li>For highly erod: 25%.</li> </ul>	ible soils, decrease perm	issible velocities	ьу
<ul> <li>Grass lined char continuous growt</li> </ul>	nnels are dependent upon a th and maintenance of gras	assurances of ss.	

Spillway Velocity with 100yr flow (34.4cfs) = 4.74fps

# **Channel Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

# Existing Swale Downstream of Pond A (Q\_100 = 20.7 cfs)

20.7 cfs = 6.6 (Pond A) + 11.0 (DP#4) + 0.7 (DP#5) + 1.2 (DP#6) + 1.2 (DP#7)

Triangular		Highlighted	
Side Slopes (z:1)	= 50.00, 50.00	Depth (ft)	= 0.47
Total Depth (ft)	= 1.00	Q (cfs)	= 20.70
		Area (sqft)	= 11.04
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 1.87
Slope (%)	= 1.00	Wetted Perim (ft)	= 47.01
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.41
		Top Width (ft)	= 47.00
Calculations		EGL (ft)	= 0.52
Compute by:	Known Q		
Known Q (cfs)	= 20.70		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# Riprap Rundown to Pond A at DP 2 (Q\_100 = 33.0 cfs per UD\_Detention Peak Inflow)

	Highlighted	
= 4.00	Depth (ft)	= 0.56
= 3.00, 3.00	Q (cfs)	= 33.00
= 1.00	Area (sqft)	= 3.18
= 1.00	Velocity (ft/s)	= 10.37
= 25.00	Wetted Perim (ft)	= 7.54
= 0.040	Crit Depth, Yc (ft)	= 1.00
	Top Width (ft)	= 7.36
	EGL (ft)	= 2.23
Known Q		
= 33.00		
	= 4.00 = 3.00, 3.00 = 1.00 = 1.00 = 25.00 = 0.040 Known Q = 33.00	= 4.00       Depth (ft)         = 3.00, 3.00       Q (cfs)         = 1.00       Area (sqft)         = 1.00       Velocity (ft/s)         = 25.00       Wetted Perim (ft)         = 0.040       Crit Depth, Yc (ft)         Top Width (ft)       EGL (ft)         Known Q       = 33.00



Reach (ft)

	Channel R	liprap S	izing Calcs	
Existing Channel Existing Channel Botte Char	Discharge om Width nnel Slope	33 4 0.2	CFS FT FT/FT	
for $S_{ch} \ge 0.10$ (10:1)	i.e. 5:1 o	r 0.20 f	t/ft	
D	$_{50} = \left[\frac{q_t(S)}{3.95}\right]$	$\frac{(h)^{0.58}}{(10)^{-2}}$	<u>1</u> 1.89	(Equation 2)
q E	ıt 050	10.3 11.5	1 FT 9 IN	
Type VL (D50 Type L (D50) Type M (D50 Type H (D50) Type VH (D50)	)) ))	1 1 2	6 IN 9 IN 2 IN 8 IN 4 IN	
Туре VH (D5	U)	2	4 IN	
Use	i ype M Ripr	ap for ch	nannel (D50	)=12")

Based on USDA's "Design procedures for rock-lined chute" https://data.nal.usda.gov/dataset/rock-chute-design

# **Channel Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

# Basin A5 Swale (Q\_100 = 11.0 cfs at DP#4)

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 0.85
Total Depth (ft)	= 1.00	Q (cfs)	= 11.00
		Area (sqft)	= 2.89
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.81
Slope (%)	= 2.00	Wetted Perim (ft)	= 7.01
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.86
		Top Width (ft)	= 6.80
Calculations		EGL (ft)	= 1.08
Compute by:	Known Q		
Known Q (cfs)	= 11.00		



Reach (ft)

Low Tailwater Ba	asin Riprap Sizing Calcs
Q	34.4 CFS
W	4 FT
H	1.5 FT
Yt	0.85 FT
Q/(WH^1.5)	2.24 <8.0
Q/(WH^0.5)	1.49
Yt/H	0.56

Use Type L Riprap for Low Tailwater Basin







Appendix E Water Quality and Detention



### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project:													
Basin ID:													
ZONE 3	2 ONE 1												
E CONT MOCA	-1	<u> </u>				1							
ZONE	1 AND 2	ORIFICE		Depth Increment =		ft Ontional				Optional		· · · · ·	
POOL Example Zone	e Configura	tion (Retention Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Makenak ad Information				Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft <sup>3</sup> )	(ac-ft)
watersned information	500	1	6716.7	100 01 MICropool		0.00				0	0.000	440	0.000
Selected BMP Type =	EDB 0.5(			6717		0.30				750	0.017	112	0.003
Watershed Longth	9.00	e		6718		2.20				0,149	0.211	3,062	0.070
Watershed Length =	261	ft.		6719		2.30				9,172	0.211	20.860	0.235
Watershed Slope =	0.023	ft/ft		6721		4.30				15,085	0.346	34,454	0.791
Watershed Imperviousness =	71.70%	percent		6722		5.30				18,119	0.416	51,056	1.172
Percentage Hydrologic Soil Group A =	100.0%	percent		6722.3		5.60				19,309	0.443	56,670	1.301
Percentage Hydrologic Soil Group B =	0.0%	percent											
Percentage Hydrologic Soil Groups C/D =	0.0%	percent											
larget WQCV Drain Time =	40.0	hours										-	
Location for 1-ni Rainiali Deptris =	user input											-	
After providing required inputs above inc depths, click 'Run CUHP' to generate run	cluding 1-hour off hydrograph	raintall is using											
the embedded Colorado Urban Hydro	graph Procedu	Jre. Optional Us	er Overrides										
Water Quality Capture Volume (WQCV) =	0.225	acre-feet	acre-feet										
Excess Urban Runoff Volume (EURV) =	0.874	acre-feet	acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) =	0.595	acre-feet 1.19	inches										ļ]
5-yr Runoff Volume (P1 = 1.5 in.) =	0.777	acre-feet 1.50	inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	0.922	acre feet 2.00	inches										
25-yr Runoff Volume (P1 = 2 ID.) = 50-yr Runoff Volume (P1 = 2 25 in.) =	1.102	acre-feet 2.00	inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	1.488	acre-feet 2.52	inches										
500-yr Runoff Volume (P1 = 3 in.) =	1.843	acre-feet 3.00	inches										
Approximate 2-yr Detention Volume =	0.571	acre-feet	-										
Approximate 5-yr Detention Volume =	0.745	acre-feet											
Approximate 10-yr Detention Volume =	0.894	acre-feet											
Approximate 25-yr Detention Volume =	1.069	acre-feet											
Approximate 50-yr Detention Volume =	1.173	acre-reet											
Approximate 100-yr Determon Volume =	1.275	acrester											
Define Zones and Basin Geometry													
Zone 1 Volume (WQCV) =	0.225	acre-feet											
Zone 2 Volume (EURV - Zone 1) =	0.649	acre-feet											
Zone 3 Volume (100-year - Zones 1 & 2) =	0.401	acre-feet											
Total Detention Basin Volume =	1.275	acre-feet											
Initial Surcharge Volume (ISV) =	user	ft 3											
Initial Surcharge Depth (ISD) =	user	π 0											
Depth of Trickle Channel (H <sub>m</sub> ) =	user	ft											
Slope of Trickle Channel (STC) =	user	ft/ft											
Slopes of Main Basin Sides (Smain) =	user	H:V											
Basin Length-to-Width Ratio ( $R_{L/W}$ ) =	user												
		1.											
Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>											
Surcharge Volume Length (L <sub>ISV</sub> ) =	user	Π 0											
Depth of Basin Floor (HELOOR) =	user	ft											
Length of Basin Floor $(L_{FLOOR}) =$	user	ft											
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft											
Area of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>											
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>											
Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft											
Width of Main Basin (Www) =	user	ft ft											
Area of Main Basin (Amain) =	user	ft <sup>2</sup>											
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>											
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet											
												<u> </u>	
						1							
												$\vdash$	

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)



# DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.03 (May 2020)

Project:			ni b beteintion, v	croion 4.00 (may .	2020)				
Basin ID:									
ZONE 3				Estimated	Estimated				
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type			
VOLUME EURV WOCV			Zone 1 (WQCV)	2.26	0.225	Orifice Plate			
	100-YEAR		Zone 2 (EURV)	4.54	0.649	Rectangular Orifice			
ZONE 1 AND 2 ORIFICES	ORIFICE		Zone 3 (100-vear)	5 55	0.401	Weir&Pine (Restrict)			
POOL Example Zone	Configuration (Re	ention Pond)	Zone 3 (100 year)	Total (all zonos)	1 275	non an ipo (nostriot)			
User Input: Orifice at Underdrain Outlet (typically )	used to drain WOCV	in a Eiltration PMD)		Total (all zones)	1.275	1	Calculated Baramot	ors for Undordrain	
Understrain Orifice Invert Denth -		ft (distance below t	he filtration modia s	urfaco)	Undor	drain Orifico Aroa -			
Underdrain Onlice Tivert Deptit =	IN/A	it (distance below t	ne nicración media su	ITACE)	Under		N/A	11 6	
Underdrain Onnice Diameter =									
User Input: Orifice Plate with one or more orifices	or Elliptical Slot Wei	(typically used to d	rain WOCV and/or FI	IDV in a sodimontat	ion BMP)		Coloulated Daramet	ora for Dioto	
Invert of Lowest Orifice -		ft (relative to basin	hottom at Stage - 0	(ff)	WO Ori	fice Area per Row -		ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate -	2.26	ft (relative to basin	bottom at Stage = 0	(ff)	FI	lintical Half-Width =	N/A	foot	
Orifice Plate: Orifice Vertical Spacing –	N/A	inches	bottom at Stage - c		Ellin	tical Slot Centroid -	N/A	feet	
Orifice Plate: Orifice Area per Row -	N/A	inches			Linp	Ellintical Slot Area -	N/A	ft <sup>2</sup>	
office flate. Office files per tow =	10/71	indica					10/7		
User Input: Stage and Total Area of Each Orifice R	ow (numbered from	lowest to highest)							
	Row 1 (required)	Row 2 (ontional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1
Stage of Orifice Controid (ft)	0.00	1.00	Row 5 (optional)	Row 4 (optional)	Row 5 (optional)	now o (optional)	(optional)	Now o (optional)	
	1.00	1.00							
Office Area (sq. inches)	1.23	1.23							1
	Row 9 (ontional)	Row 10 (ontional)	Row 11 (ontional)	Row 12 (ontional)	Row 13 (ontional)	Row 14 (ontional)	Row 15 (ontional)	Row 16 (ontional)	1
Stage of Orifice Centroid (ft)	Row 7 (optional)	Now To (optional)	Row IT (optional)	now 12 (optional)	Kow 13 (optional)	Row 14 (optional)	Now 13 (optional)	now re (optional)	
office Area (sq. incres)									1
User Input: Vertical Orifice (Circular or Rectangula	r)						Calculated Paramet	ers for Vertical Orific	e
·····	Zone 2 Rectangular	Not Selected	1				Zone 2 Rectangular	Not Selected	1
Invert of Vertical Orifice =	2.26	N/A	ft (relative to basin	bottom at Stage = 0	) ft) Ve	ertical Orifice Area =	0.02	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	4.54	N/A	ft (relative to basin	bottom at Stage = 0	) ft) Vertic	al Orifice Centroid =	0.05	N/A	feet
Vertical Orifice Height =	1.25	N/A	inches	5	,				1
Vertical Orifice Width =	2.50		inches						
	2.00								
User Input: Overflow Weir (Dropbox with Flat or S	loped Grate and Out	let Pipe OR Rectang	ular/Trapezoidal Wei	r (and No Outlet Pip	e)		Calculated Paramet	ers for Overflow Wei	r
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	1
Overflow Weir Front Edge Height, Ho =	4.54	N/A	ft (relative to basin b	ottom at Stage = 0 ft)	) Height of Grat	te Upper Edge, Ht =	4.54	N/A	feet
Overflow Weir Front Edge Length =	3.00	N/A	feet	5	Overflow V	Neir Slope Length =	3.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V		Grate Open Area / 1	00-vr Orifice Area =	2.55	N/A	
Horiz. Length of Weir Sides =	3.00	N/A	feet		Overflow Grate Oper	n Area w/o Debris =	4.50	N/A	ft <sup>2</sup>
Overflow Grate Open Area % =	50%	N/A	%, grate open area	/total area	Overflow Grate Ope	en Area w/ Debris =	1.35	N/A	ft <sup>2</sup>
Debris Clogging % =	70%	N/A	%						1
00 0			1						
User Input: Outlet Pipe w/ Flow Restriction Plate (0	Circular Orifice, Resti	ictor Plate, or Recta	ngular Orifice)		C	Calculated Parameter	s for Outlet Pipe w/	Flow Restriction Plat	te
	Zone 3 Restrictor	Not Selected			_		Zone 3 Restrictor	Not Selected	1
Depth to Invert of Outlet Pipe =	0.95	N/A	ft (distance below ba	sin bottom at Stage =	= 0 ft) C	Outlet Orifice Area =	1.77	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	18.00	N/A	inches	5	Outle	et Orifice Centroid =	0.75	N/A	feet
Restrictor Plate Height Above Pipe Invert =	18.00		inches	Half-Ce	entral Angle of Restri	ctor Plate on Pipe =	3.14	N/A	radians
- · ·					÷				•
User Input: Emergency Spillway (Rectangular or Tr	apezoidal)						Calculated Paramet	ers for Spillway	
Spillway Invert Stage=	5.65	ft (relative to basin	bottom at Stage = 0	ft)	Spillway [	Design Flow Depth=	0.31	feet	
Spillway Crest Length =	60.00	feet			Stage at	Top of Freeboard =	6.96	feet	
Spillway End Slopes =	4.00	H:V			Basin Area at	Top of Freeboard =	0.44	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at	Top of Freeboard =	1.30	acre-ft	
Devite d Under ments D	The		huden and the t			th - 1 - 61		A/ 46 453	
Routed Hydrograph Results	The user can overn	de the default CUHP	nydrographs and ru	not volumes by ent	ering new values in a	the Inflow Hydrograp	ons table (Columns I	V through AF).	500 V/
Design Storm Return Period =	N/A	EURV N/A	2 Year 1 10	5 Year	1 75	25 Year	2 25	2.52	3 00
CUHP Runoff Volume (acre-ft) =	0.225	0.874	0.595	0.777	0.922	1.102	1.278	1.488	1.843
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.595	0.777	0.922	1.102	1.278	1.488	1.843
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.2	0.3	2.6	4.9	8.0	12.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.00	0.00	0.07	0.50	0.01	1.00
Predevelopment Unit Peak How, q (cts/acre) =	N/A N/Δ	N/A	0.01	0.02 16.8	0.03	0.27	0.52	0.84 33.0	1.33
Peak Outflow O (cfs) =	0.1	0.3	0.3	0.3	0.3	1.7	3.2	5.8	8.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.4	1.1	0.7	0.6	0.7	0.7
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.3	0.6	1.2	1.8
Max Velocity through Grate 2 (fps) =	N/A 20	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A 41
Time to Drain 97% of Inflow Volume (nours) =	40	71	62	68	73	74	74	73	72
Maximum Pondina Depth (ft) =	10		52			, т	т,		
	2.26	4.54	3.58	4.13	4.54	4.79	4.94	5.20	5.60
Area at Maximum Ponding Depth (acres) =	2.26 0.21	4.54 0.36	3.58 0.30	4.13 0.33	4.54 0.36	4.79 0.38	4.94 0.39	5.20 0.41	5.60 0.44



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

	Inflow Hydrogr	aphs								
	The user can ov	erride the calcul	ated inflow hydr	ographs from th	is workbook with	inflow hydrogra	aphs developed i	n a separate prog	ram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.24	0.02	0.60
	0:15:00	0.00	0.00	2.11	3.44	4.25	2.86	3.48	3.47	4.45
	0:20:00	0.00	0.00	6.82	8.72	10.17	6.35	7.31	7.94	9.66
	0:25:00	0.00	0.00	12.70	16.76	20.09	12.56	14.32	15.38	19.06
	0:30:00	0.00	0.00	12.43	11.04	13.29	24.68	29.18	33.03	41.26
	0:40:00	0.00	0.00	7.26	8.82	10.08	18.51	21.70	26.10	32.32
	0:45:00	0.00	0.00	5.18	6.59	7.68	13.59	15.85	20.15	25.05
	0:50:00	0.00	0.00	3.80	5.09	5.70	10.84	12.59	15.52	19.37
	0:55:00	0.00	0.00	2.91	3.82	4.42	7.67	8.82	11.52	14.27
	1:00:00	0.00	0.00	2.56	3.32	3.97	5.71	6.51	8.93	11.06
	1:05:00	0.00	0.00	2.44	3.15	3.84	4.85	5.53	7.86	9.79
	1:10:00	0.00	0.00	2.05	3.08	3.79	4.04	4.58	5.75	5.64
	1:20:00	0.00	0.00	1.05	2.02	3.41	3.05	3.43	3.41	4 11
	1:25:00	0.00	0.00	1.67	2.40	2.89	2.76	3.11	2.75	3.31
	1:30:00	0.00	0.00	1.62	2.31	2.59	2.34	2.63	2.34	2.80
	1:35:00	0.00	0.00	1.60	2.26	2.42	2.12	2.38	2.14	2.55
	1:40:00	0.00	0.00	1.60	1.92	2.31	1.99	2.24	2.07	2.46
	1:45:00	0.00	0.00	1.60	1.74	2.26	1.93	2.17	2.04	2.42
	1:50:00	0.00	0.00	1.60	1.63	2.24	1.90	2.13	2.04	2.42
	2.00.00	0.00	0.00	1.25	1.57	2.13	1.88	2.12	2.04	2.42
	2:05:00	0.00	0.00	0.58	0.80	1.04	1.05	1.18	1.13	1.35
	2:10:00	0.00	0.00	0.31	0.44	0.57	0.59	0.66	0.63	0.75
	2:15:00	0.00	0.00	0.15	0.23	0.29	0.30	0.34	0.32	0.39
	2:20:00	0.00	0.00	0.06	0.11	0.13	0.15	0.16	0.16	0.18
-	2:25:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

# Stormwater Detention and Infiltration Design Data Sheet

Workbook Protected

-

Norksheet Protected

User Defined User Defined User Defined User Defined

Stormwater Facility Name: TAMLIN ROAD RV STORAGE - POND A

#### Facility Location & Jurisdiction: EL PASO COUNTY



WQCV Treatment Method = Extended Detention

Stage [ft]	Area [ft^2]	Stage [ft]	Discharge [cfs]
0.00	0	0.00	0.00
0.30	750	0.30	0.02
1.30	5.149	1.30	0.07
2.30	9,172	2.30	0.11
3.30	12,103	3.30	0.23
4.30	15,085	4.30	0.30
5.30	18,119	5.30	6.75
5.60	19,309	5.60	6.91

After completing and printing this worksheet to a pdf, go to: <u>https://maperture.digitaldataservices.com/gvh/?viewer=cswdif</u> create a new stormwater facility, and attach the pdf of this worksheet to that record.

	Routed Hydro	graph Results					_
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	1.19	1.50	1.75	2.00	2.25	2.52	in
Calculated Runoff Volume =	0.225	0.760	0.916	1.088	1.339	1.571	acre-ft
OPTIONAL Override Runoff Volume =	0.19	0.47	0.62	0.74	0.97	1.06	acre-ft
Inflow Hydrograph Volume =	0.185	0.473	0.615	0.739	0.970	1.055	acre-ft
Time to Drain 97% of Inflow Volume =	32.7	52.8	58.4	62.8	65.4	64.9	hours
Time to Drain 99% of Inflow Volume =	34.7	56.5	62.8	67.7	71.2	71.0	hours
Maximum Ponding Depth =	1.99	3.19	3.67	4.05	4.52	4.64	ft
Maximum Ponded Area =	0.18	0.27	0.30	0.33	0.36	0.37	acres
Maximum Volume Stored =	0.173	0.447	0.584	0.703	0.866	0.913	acre-ft



# Stormwater Detention and Infiltration Design Data Sheet

Design Procedure Form: Extended Detention Basin (EDB)				
Designer: Company: Date: Project: Location:	UD-BMP RYAN DEGROOT JR ENGINEERING July 10, 2020 TAMLIN ROAD RV STORAGE UNINC. EL PASO COUNTY	P (Version 3.06, November 2016) Sheet 1 of 4		
1. Basin Storage Volume				
A) Effective Imperviousness of Tributary Area, ${\rm I_a}$		l <sub>a</sub> = <u>71.0</u> %		
B) Tributary Are	ea's Imperviousness Ratio (i = $I_a/100$ )	i =		
C) Contributing	g Watershed Area	Area = <u>9.560</u> ac		
D) For Waters Runoff Proc	heds Outside of the Denver Region, Depth of Average ducing Storm	$d_6 = $ in		
E) Design Con (Select EUR	ncept VV when also designing for flood control)	Choose One O Water Quality Capture Volume (WQCV) Excess Urban Runoff Volume (EURV)		
F) Design Volu (V <sub>DESIGN</sub> = (	ume (WQCV) Based on 40-hour Drain Time 1.0 * (0.91 * i <sup>3</sup> - 1.19 * i <sup>2</sup> + 0.78 * i) / 12 * Area )	V <sub>DESIGN</sub> = 0.223 ac-ft		
G) For Waters Water Qual (V <sub>WQCV OTHE</sub>	heds Outside of the Denver Region, lity Capture Volume (WQCV) Design Volume $_{\rm IR} = (d_e^*(V_{\rm DESIGN}/0.43))$	V <sub>DESIGN OTHER</sub> = 0.218 ac-ft		
H) User Input ( (Only if a di	of Water Quality Capture Volume (WQCV) Design Volume fferent WQCV Design Volume is desired)	V <sub>DESIGN USER</sub> =ac-ft		
I) Predominant	t Watershed NRCS Soil Group	Choose One A B C C / D		
J) Excess Urba For HSG A For HSG B For HSG C	an Runoff Volume (EURV) Design Volume :: EURV <sub>A</sub> = 1.68 * i <sup>1.28</sup> :: EURV <sub>B</sub> = 1.36 * i <sup>1.08</sup> :/D: EURV <sub>CID</sub> = 1.20 * i <sup>1.08</sup>	EURV = <u>0.863</u> ac-f t		
2. Basin Shape: L (A basin length	length to Width Ratio to width ratio of at least 2:1 will improve TSS reduction.)	L : W = <u>0.8</u> : 1 INCREASE FLOW PATH FOR 2:1 RATIO		
3. Basin Side Slop	pes			
A) Basin Maxir (Horizontal	mum Side Slopes distance per unit vertical, 4:1 or flatter preferred)	Z = ft / ft		
4. Inlet A) Describe m inflow locati	eans of providing energy dissipation at concentrated	Riprap rundowns down the side slopes of the podn at outfall locations and riprap pads extend into pond bottom.		

Design Procedure Form: Extended Detention Basin (EDB)				
Destant DYAN D			Sheet 2 of 4	
Company: JR ENGL				
Date: July 10, 2	July 10, 2020			
Project: TAMLIN	TAMLIN ROAD RV STORAGE			
Location: UNINC. E	L PASO COUNTY			
5. Forebay				
A) Minimum Forebay Volur (V <sub>FMIN</sub> = <u>3%</u>	neof the WQCV)	V <sub>FMIN</sub> =0.007ac-ft		
B) Actual Forebay Volume		$V_{F} = 0.007$ ac-ft		
C) Forebay Depth $(D_F = 18)$	inch maximum)	D <sub>F</sub> = <u>15.0</u> in		
D) Forebay Discharge				
i) Undetai	ined 100-year Peak Discharge	Q <sub>100</sub> = <u>34.40</u> cfs		
ii) Foreba (Q <sub>F</sub> = 0	y Discharge Design Flow ).02 * Q <sub>100</sub> )	$Q_F = 0.69$ cfs		
E) Forebay Discharge Desi	gn	Choose One Berm With Pipe (flow Wall with Rect. Notch Wall with V-Notch Weir	r too small for berm w/ pipe)	
F) Discharge Pipe Size (mir	nimum 8-inches)	Calculated $D_P =$ in		
G) Rectangular Notch Widtl	ħ	Calculated W <sub>N</sub> = 4.8 in		
6. Trickle Channel		Choose One		
A) Type of Trickle Channel		O Soft Bottom		
F) Slope of Trickle Channe	k	S = <u>0.0100</u> ft / ft		
7. Micropool and Outlet Struct	ture			
A) Depth of Micropool (2.5-	-feet minimum)	D <sub>M</sub> = ft		
B) Surface Area of Micropo	ool (10 ft <sup>2</sup> minimum)	$A_{\rm M} = $ 21 sq ft		
C) Outlet Type				
		Choose One Orifice Plate Other (Describe):		
<ul> <li>D) Smallest Dimension of ( (Use UD-Detention)</li> </ul>	Orifice Opening Based on Hydrograph Routing	D <sub>orffice</sub> = <u>1.23</u> inches		
E) Total Outlet Area		A <sub>ot</sub> = <u>5.59</u> square inches		

Design Procedure Form: Extended Detention Basin (EDB)				
Designer: Company: Date: Project: Location:	RYAN DEGROOT JR ENGINEERING July 10, 2020 TAMLIN ROAD RV STORAGE UNINC. EL PASO COUNTY	Sheet 3 of 4		
8. Initial Surcharge Volume				
A) Depth of Init (Minimum re	ial Surcharge Volume commended depth is 4 inches)	D <sub>IS</sub> = in		
B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)		$V_{IS} = 28.4$ cu ft		
C) Initial Surcharge Provided Above Micropool		V <sub>s</sub> =7.0cu ft		
9. Trash Rack				
A) Water Quali	ty Screen Open Area: A <sub>t</sub> = A <sub>ot</sub> * 38.5*(e <sup>-0.095D</sup> )	A <sub>t</sub> = <u>191</u> square inches		
B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)		S.S. Well Screen with 60% Open Area		
	Other (Y/N): N			
C) Ratio of Tota	I Open Area to Total Area (only for type 'Other')	User Ratio =		
D) Total Water	Quality Screen Area (based on screen type)	A <sub>total</sub> = <u>319</u> sq. in.		
E) Depth of Des (Based on de	sign Volume (EURV or WQCV) sign concept chosen under 1E)	H= <u>4.54</u> feet		
F) Height of Wa	ter Quality Screen (H <sub>TR</sub> )	H <sub>TR</sub> = 82.48 inches		
G) Width of Wa (Minimum of 1	ter Quality Screen Opening (W <sub>opening</sub> ) 12 inches is recommended)	W <sub>opening</sub> = <u>12.0</u> inches		
Design Procedure Form: Extended Detention Basin (EDB)				
---	--	--	--	--
Designer: Company: Date: Project: Location:	RYAN DEGROOT JR ENGINEERING July 10, 2020 TAMLIN ROAD RV STORAGE UNINC. EL PASO COUNTY	Sheet 4 of 4		
<ol> <li>Overflow Emba</li> <li>A) Describe er</li> <li>B) Slope of Ov (Horizontal</li> </ol>	ankment nbankment protection for 100-year and greater overtopping: verflow Embankment distance per unit vertical, 4:1 or flatter preferred)	24" Deep Type M Soil Riprap overflow weir w/ 1.36' total depth (design flow depth < 0.36') 60' crest width. 4:1 side slopes 		
11. Vegetation		Choose One Irrigated Not Irrigated		
12. Access A) Describe Sediment Removal Procedures		Pond will be maintaned utilizing skid steer type equipment, trucks (when needed), and hand tools as needed.		
Notes:				

Appendix F Drainage Maps





## **TAMLIN ROAD RV & BOAT STORAGE EXISTING DRAINAGE MAP**



BASIN DESIGNATION <u>(1.D.</u> I.D.: BASIN IDENTIFIER A: BASIN AREA В B: C<sub>5</sub> C: C<sub>100</sub>

**BASIN SUMMARY TABLE** 

**C**<sub>5</sub>

0.05

0.05

Percent

mpervious

2%

2%

Tributary

Sub-basin

EX1

EX2

Area

(acres)

6.43

10.08

Q<sub>5</sub>

(cfs)

1.2

1.8

tc

(min)

13.4

15.4

C<sub>100</sub>

0.36

0.36

**Q**100

(cfs)

14.3

21.2

SUMMARY TABLE				
Tributary	Q₅	<b>Q</b> <sub>100</sub>		
Sub-basin	(cfs)	(cfs)		
1	1.2	14.3		
2	1.8	21.2		

DESIGN POINT



CS

7:42:49 AM,

BASIN DELINEATION

EXISTING INTERMEDIATE CONTOURS \_\_\_\_

PROPOSED INTERMEDIATE CONTOURS

EXISTING FLOW DIRECTION  $\Rightarrow$ 



TAMLIN ROAD RV & BOAT STORAGE EX. DRAINAGE MAP 2513400 01/20/2020 SHEET 1 OF 1



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## **TAMLIN ROAD RV & BOAT STORAGE**IRF MAP EXHIBIT

