

**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

**FINAL DRAINAGE REPORT
FOR
TAMLIN ROAD RV & BOAT STORAGE**

**Prepared For:
C&M Properties, LLC
12748 Barossa Valley Road
Colorado Springs, CO 80921**

**January 17, 2020
Project No. 2513400**

**Prepared By:
JR Engineering, LLC
5475 Tech Center Drive, Suite 235
Colorado Springs, CO 80919
719-593-2593**

PCD FILE NO.: PPR1945



**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. # 32314
For and On Behalf of JR Engineering, LLC

Date

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: C&M Properties, LLC

By: Edward McDonald

Title: Manager

Address: 12748 Barossa Valley Road
Colorado Springs, CO 80921

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E.
County Engineer/ ECM Administrator

Date

Conditions:

**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

Table of Contents

Purpose 4
General Site Description 4
 Location 4
 Description of Property 4
Existing Drainage Conditions 5
 Major Basin Descriptions 5
 Existing Sub-basin Drainage 5
Proposed Drainage Conditions..... 6
 Proposed Sub-basin Drainage..... 6
 Development Criteria Reference 7
 Hydrologic Criteria..... 7
 Hydraulic Criteria..... 8
Drainage Facility Design 8
 Four Step Process to Minimize Adverse Impacts of Urbanization 8
 Water Quality..... 9
 Erosion Control Plan 9
 Operation & Maintenance..... 9
 Floodplain Statement 9
 Drainage and Bridge Fees..... 10
 Construction Cost Opinion 10
Summary 11
References..... 12

APPENDIX

- Appendix A – Vicinity Map, Soil Descriptions, FEMA Floodplain Map
- Appendix B – Hydrologic Calculations
- Appendix C – Hydraulic Calculations
- Appendix D – Water Quality & Detention Calculations
- Appendix E – Reference Material
- Appendix F – Drainage Maps

**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

PURPOSE

This document is the Final Drainage report for Tamlin Road Storage Yard. The purpose of this report is to:

1. Identify on-site and off-site drainage patterns.
2. Recommend storm water facilities to collect and convey storm runoff from the proposed development to appropriate discharge and/or detention locations.
3. Recommend water quality and detention facilities to control discharge release rates to below historic.
4. Demonstrate compliance with surrounding major drainage basin planning studies, master development drainage plans and flood insurance studies.

GENERAL SITE DESCRIPTION

LOCATION

Tamlin Road Storage Yard, known as ‘the site’ from herein, is currently vacant land located in a portion of Section 20, Township 13 South, Range 65 West of the Sixth Principal Meridian in unincorporated El Paso County, Colorado. The site is located northeast of the Tamlin Road and Marksheffel Road intersection. The site is bound by Tamlin Road to the west and north, vacant land owned by Norwood to the east and south. Stetson Hills Filing No. 3 and 4 is located adjacent to the site on the west side of Marksheffel Road. A vicinity map has been presented in Appendix A.

Sand Creek East Fork tributary is located approximately ¼ mile east of the site. The ultimate outfall of this drainageway is Fountain Creek. However, there are no existing stormwater facilities located on site.

DESCRIPTION OF PROPERTY

The site is approximately 16.5 acres and is covered with sparse trees and native vegetation. There are no existing structures on the site. An existing dirt road proceeds southeast from Tamlin Road through the site to service an existing water tank, located south of the site. There is a ridge that divides the drainage on the site. Roughly 6.5 acres drains southwest with slopes between 3-10% while the remaining 10 acres drains easterly with slopes up to 8%. In the developed condition, the site will be asphalt drive aisles, parking stalls and a single trash enclosure.

The site is comprised solely of Truckton sandy loam, which is classified as a Type A soil by the NRCS. Group A soils exhibit a high infiltration rate when thoroughly wet and consist chiefly of deep, well drained to excessively drained gravelly sands. These soils have a high rate of water transmission. A NRCS soil survey map is presented in Appendix A.



FINAL DRAINAGE REPORT FOR TAMLIN ROAD RV & BOAT STORAGE

There are no known irrigation facilities located on the project site. An existing water line (size unknown) runs north-south through the site in a 30' utility easement. Additionally, three gas mains (size unknown) cross the site. Two of the existing gas lines are parallel to the water main within two separate 50' easements. The third gas line runs parallel to Tamlin in a dedicated 50' easement. All existing utilities will remain and no grading will occur within the limits of the easements.

EXISTING DRAINAGE CONDITIONS

MAJOR BASIN DESCRIPTIONS

The site lies within the West Tributary Sand Creek regional sub basin within the Sand Creek Major Drainage Basin. The "*Sand Creek Drainage Basin Planning Study*" prepared by Kiowa Engineering revised in March 1996, evaluated the Sand Creek Major Drainage Basin, the existing facilities therein and provided recommendations for future development. A map of the Sand Creek regional sub basins is presented in Appendix B.

The Sand Creek Basin covers approximately 54 square miles in unincorporated El Paso County and Colorado Springs, CO. The undeveloped portions of the basin are typified by rolling range land with fair vegetative cover associated with semi-arid climates. The headwaters of the basin are in The Black Forest and general topography trends south to southwesterly towards its ultimate outfall into Fountain Creek. Per the *Sand Creek DBPS*, the Sand Creek East Fork Subtributary runs outside the western boundary of the site. This drainageway begins at the confluence with the mainstem of East Fork Sand Creek and runs north to Barnes Road.

Based on the FEMA FIRM Map number 08041C0543G and 08041C0545G, the site does not fall within a FEMA defined floodplain and is classified as Zone X, which are areas determined to be outside the 0.2% annual chance floodplain. FIRM maps of the site and surrounding areas have been presented in Appendix A.

EXISTING SUB-BASIN DRAINAGE

Existing drainage patterns are split on the site by a ridge running north-south. The eastern portion of the site drains across undeveloped land to Sand Creek East Fork Subtributary. The western portion of the site drains across Tamlin Road and Marksheffel road into Eastview Estates Filing No. 3 storm sewer. An existing drainage analysis and map are presented in Appendix C and F, respectively.



PROPOSED DRAINAGE CONDITIONS

PROPOSED SUB-BASIN DRAINAGE

In general, runoff generated from the site will be collected and conveyed to a full spectrum water quality and detention pond, Pond A. It should be noted that all proposed parking and drive aisles will be constructed of gravel. However, there is a possibility of the owner paving the drive aisles and parking stalls with asphalt in the future. Therefore, all calculations (hydrologic and hydraulic) have been performed per the future asphalt condition. The proposed basin delineation is as follows:

Basin A1 consists of approximately 0.38 acres of existing Tamlin Road pavement and undeveloped areas paralleling Tamlin Road. Runoff from these areas will sheet flow easterly to Design Point (DP) #1. From here, Basin A1 flows ($Q_5 = 0.7$ cfs and $Q_{100} = 1.8$ cfs) to DP#2 prior to being captured and detained in Full Spectrum Detention and Water Quality Pond A.

Basin A2 consists of approximately 4.42 acres of gravel drives, gravel parking stalls and landscaped areas. Runoff from this basin ($Q_5 = 13.3$ cfs and $Q_{100} = 26.5$ cfs) sheet flows southeasterly to DP #2 before being captured and detained in Full Spectrum Detention and Water Quality Pond A.

Basin A3 consists of approximately 4.72 acres of gravel drives, gravel parking stalls and landscaped areas. Runoff from this basin ($Q_5 = 16.0$ cfs and $Q_{100} = 30.0$ cfs) sheet flows northeasterly to DP #2 before being captured in Full Spectrum Detention and Water Quality Pond A.

Basin A4 consists of approximately 0.70 acres and consists of Full Spectrum Detention and Water Quality Pond A. Runoff from this basin ($Q_5 = 0.3$ cfs and $Q_{100} = 1.9$ cfs) will be captured within the pond. Full Spectrum Detention and Water Quality Pond A will release at less than historic rates and is detailed later in this report.

Basin A5 consists of approximately 1.14 acres of undeveloped land. Runoff from this basin ($Q_5 = 0.6$ cfs and $Q_{100} = 3.1$ cfs) will follow historic patterns and sheet flow southeasterly offsite. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A5 will not be detained in Full Spectrum Detention and Water Quality Pond A.

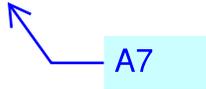
Basin A6 consists of approximately 0.26 acres of landscape area and undeveloped land. Runoff from this basin ($Q_5 = 0.1$ cfs and $Q_{100} = 0.8$ cfs) will follow historic patterns and sheet flow easterly offsite. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A5 will not be detained in Full Spectrum Detention and Water Quality Pond A.



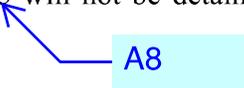
A6

**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

Basin A7 consists of approximately 0.39 acres of landscape area and undeveloped land. Runoff from this basin ($Q_5 = 0.2$ cfs and $Q_{100} = 1.2$ cfs) will follow historic patterns and sheet flow easterly offsite. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A7 will not be detained in Full Spectrum Detention and Water Quality Pond A.



Basin A8 consists of approximately 0.40 acres of landscape area and undeveloped land. Runoff from this basin ($Q_5 = 0.2$ cfs and $Q_{100} = 1.2$ cfs) will follow historic patterns and sheet flow easterly offsite. Per Section I.7.1.B.7 of the ECM – Stormwater Quality Policy and Procedures, the County may exclude sites with land disturbance to undeveloped land that will remain undeveloped from the WQCV standard. Therefore, Basin A8 will not be detained in Full Spectrum Detention and Water Quality Pond A.



Please provide discussion regarding off-site flow entering the site. If there is no off-site flow besides basin A1 due to the proposed grading please state it.

DEVELOPMENT CRITERIA REFERENCE

Storm Drainage Analysis and Design Criteria for this project were implemented from the El Paso County “Drainage Criteria Manual” (DCM) and the “Urban Storm Drainage Criteria Manual” by Urban Drainage and Flood Control District (USDCM).

Please also provide discussion/statement regarding the west side of the parcel and that it will not be developed and continue to follow historic patterns.

HYDROLOGIC CRITERIA

All hydrologic data was obtained from the “El Paso County Drainage Criteria Manual” Volumes 1 and 2, and the “Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual” Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the Colorado Springs Criteria. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the DCM. Time of concentrations were developed using equations from DCM. Water quality and detention pond will be sized per the full spectrum method presented in Chapter 13 of the DCM. All runoff calculations and applicable charts and graphs are included in Appendix A.

Table 1 - 1-hr Point Rainfall Data

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

Rock mulch islands are dispersed throughout the parking areas. Table 6-6 from the El Paso County DCM does not provide a composite percent impervious for rock mulch. The impervious value for



FINAL DRAINAGE REPORT FOR TAMLIN ROAD RV & BOAT STORAGE

gravel, of 80%, does not apply for rock mulch since the gravel impervious value is based upon compacted gravel used for roads. The rock mulch utilized on site will not be compacted and will have undisturbed soil underneath allowing percolation. Table 6-3 from Volume 1 of Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual proposes an impervious value of 40% for packed gravel. JR Engineering is proposing to use a value of 20% for rock mulch areas due to the void space and undisturbed area that increase perviousness.

HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD UD-Detention v3.07 spreadsheet was utilized for sizing the water quality and detention ponds as well as outlet structure. Manning's equation was used to size the proposed drainage swales in this report.

DRAINAGE FACILITY DESIGN

FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the Colorado Springs Drainage Criteria Manual, Volume 2 this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff: The Tamlin Road Storage Yard consists of gravel drive aisles and parking spaces with lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. The IRF worksheet can be found in Appendix C.

Step 2 – Treating the Water Quality Capture Volume: Water Quality treatment for this site is provided in two onsite full spectrum water quality and detention ponds. Runoff from the site will be collected in vegetated swales and conveyed to the detention ponds.

Step 3 – Stabilizing Drainageways: No drainage fees are due with this site development plan and final drainage report. If the site were to be platted in the future, drainage fees will be paid at that time in order to help fund major drainage improvements per the “Sand Creek Drainage Basin Planning Study”. These improvements help stabilize the drainage way.

Step 4 – Implementing Long Term Source Controls: BMP's will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated

a single pond is now proposed. Please revise.

The majority of the runoff is conveyed via sheet flow over the gravel/asphalt parking area.

It does not appear that there are any major drainageways on the site that need to be stabilized. I recommend stating that as well.



FINAL DRAINAGE REPORT FOR TAMLIN ROAD RV & BOAT STORAGE

I dont believe any inlets are identified on the drainage plan.

vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMP's include asphalt drives and parking, storm inlets and storm pipe.

gravel

basin B and its pond have been removed. Please update the narrative accordingly.

WATER QUALITY

Developed area within Basin A will be conveyed to Full Spectrum Water Quality and Detention Pond A, located along the site's eastern boundary. Developed area within Basin B will be conveyed to Full Spectrum Water Quality and Detention Pond B, located in the site's southwest corner along Tamlin Road. It should be noted that all proposed parking and drive aisles will be constructed of gravel. However, there is a possibility of the owner paving the drive aisles and parking stalls with asphalt in the future. Therefore, all water quality and detention calculations are per the asphalt condition.

The UD detention calculation indicates 10.22 acres tributary area. Please Revise accordingly.

Pond A has a total of 8.6 tributary acres for total detention basin volume of 1.288 ac-ft. Pond A utilizes a full spectrum outlet structure to detain the WQCV for a 40-hr period, the EURV for a 72-hour period and the 100-yr volume for 72-hr period. The outlet structure will release at less than historic rates. Pond A will discharge into a proposed energy dissipater located along the eastern property line. From here, discharge will maintain the sub-basins existing drainage patterns and discharge into a swale that conveys the flow across the vacant land to the east and eventually to Sand Creek East Fork. The pond is discharging at less than historic rates, therefore; downstream infrastructure has adequate capacity for discharge.

The drainage plan shows an existing riprap pad on the adjacent property downstream of your discharge. Is this sufficient? Although rates are at or below historic the downstream swale may not be adequate. Please see comment on the drainage plan

EROSION CONTROL PLAN

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate to be submitted with the Final Drainage Report. We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

OPERATION & MAINTENANCE

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities. An Inspection and Maintenance Manual will accompany the Final Drainage Report submittal package.

FLOODPLAIN STATEMENT

Based on the FEMA FIRM Map number 08041C0543G and 08041C0545G, the site does not fall within a FEMA defined floodplain and is classified as Zone X, which are areas determined to be



**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

outside the 0.2% annual chance floodplain. FIRM maps of the site and surrounding areas have been presented in Appendix A.

DRAINAGE AND BRIDGE FEES

The site lies within the Sand Creek Drainage Basin. See Table 2 below for required drainage basin fees. Per El Paso County processes, drainage fees are due at the time of platting. This development is not proposed to be platted and the fees shown in Table 2 below are for informational purposes only. The fees are based on a paved site and have not taken into consideration pond construction credits for the proposed detention pond.

Table 2 – Basin Fees

Tamlin Road Storage Yard Drainage Basin Fees					
Total Area	Site% Imperviousness	Impervious Acres	Drainage Fee/Impervious Acre	Bridge Fee/Impervious Acre	Total Fee
12.41	68%	8.44	\$18,940	\$5,559	\$206,742.16

CONSTRUCTION COST OPINION

See Table 3 below for cost opinion of private storm sewer infrastructure.

Table 3 – Construction Cost Opinion

Private Drainage Facilities				
Item	Quantity	Unit	Unit Price	Extended Cost
18" RCP	38	LF	\$ 45.00	\$ 1,710.00
18" FES	1	EA	\$ 1,500.00	\$ 1,500.00
SPILLWAY (TYPE M RIPRAP)	64	CY	\$ 125.00	\$ 8,000.00
RIPRAP PADS & TAIL WATER BASIN (TYPE M & L RIPRAP)	80	CY	\$ 125.00	\$ 10,000.00
AGG. BASE COURSE MAINT. ROAD	117	SY	\$ 45.00	\$ 5,265.00
FULL SPECTURM OUTLET STRUCTURE	1	LS	\$ 15,000.00	\$ 15,000.00
			Sub-Total	\$ 41,475.00
			10% Eng. And Contingency	\$ 4,147.50
			Grand Total	\$ 45,622.50



**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

SUMMARY

The proposed Tamlin Road RV Storage drainage improvements include storm sewer, a Full Spectrum Detention and Water Quality Pond, and an engineered outfall. The proposed development will not adversely affect the offsite major drainageways or surrounding developments. This report is in conformance with the latest El Paso County Storm Drainage Criteria requirements for this site.

**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

REFERENCES

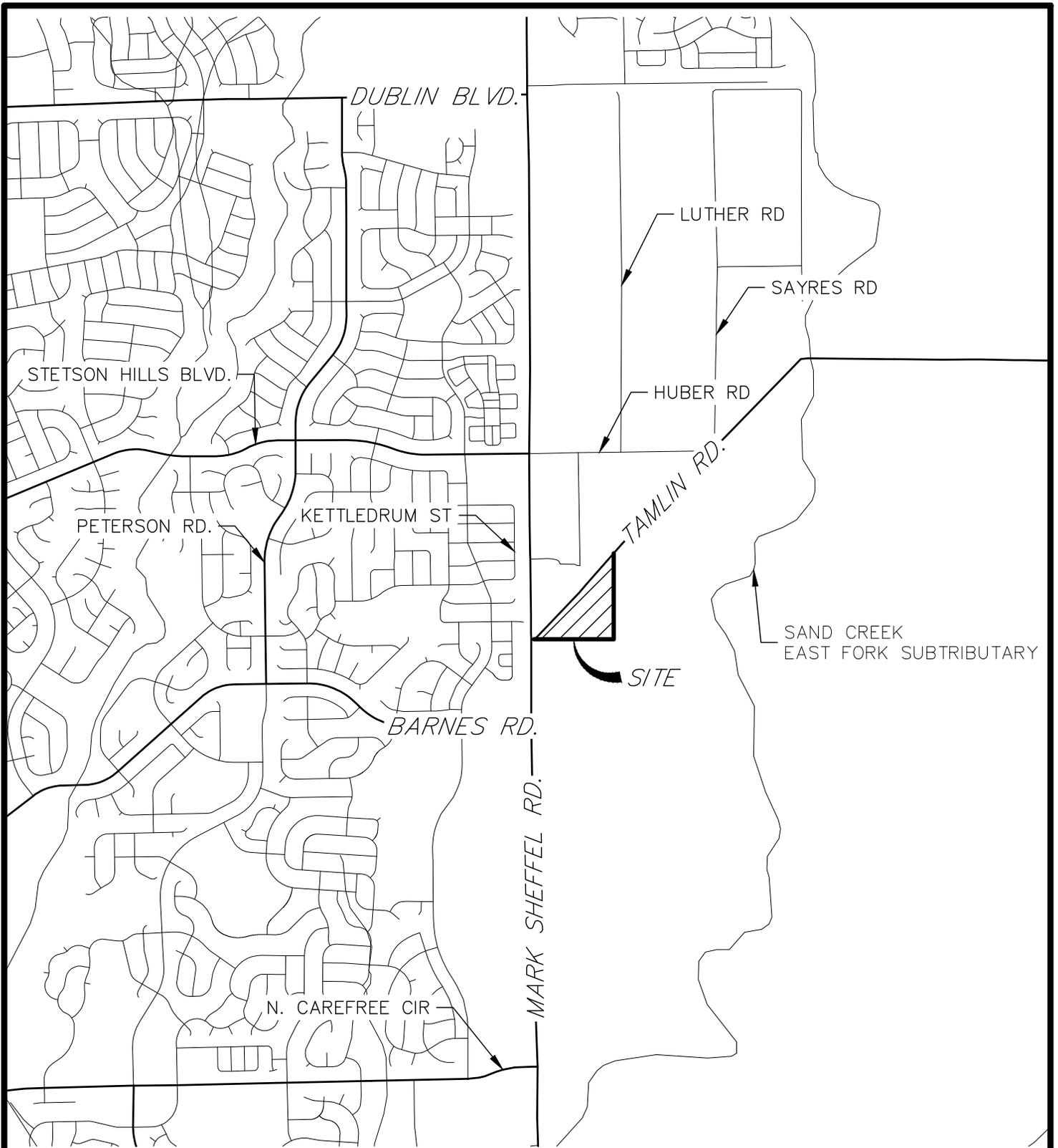
1. El Paso County Drainage Criteria Manual (Volumes I & II), El Paso County CO, Colorado, Updated May, 2014.
 2. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
 3. “Hydrologic Group Rating for El Paso County Area, Colorado”, USDA-Natural Resources Conservation Service, National Cooperative Soil Survey. Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>. [June 14, 2019]
 4. “Sand Creek Drainage Basin Planning Study Final Design Report”, Kiowa Engineering Corporation, March 1996.
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**FINAL DRAINAGE REPORT FOR
TAMLIN ROAD RV & BOAT STORAGE**

Appendix A

Vicinity Map, Soil Descriptions, FEMA Floodplain Map

X:\2510000.all\2513400\Drawings\Blocks\Vicinity Map.dwg, VIC. MAP, 6/14/2019 9:14:38 AM, CS



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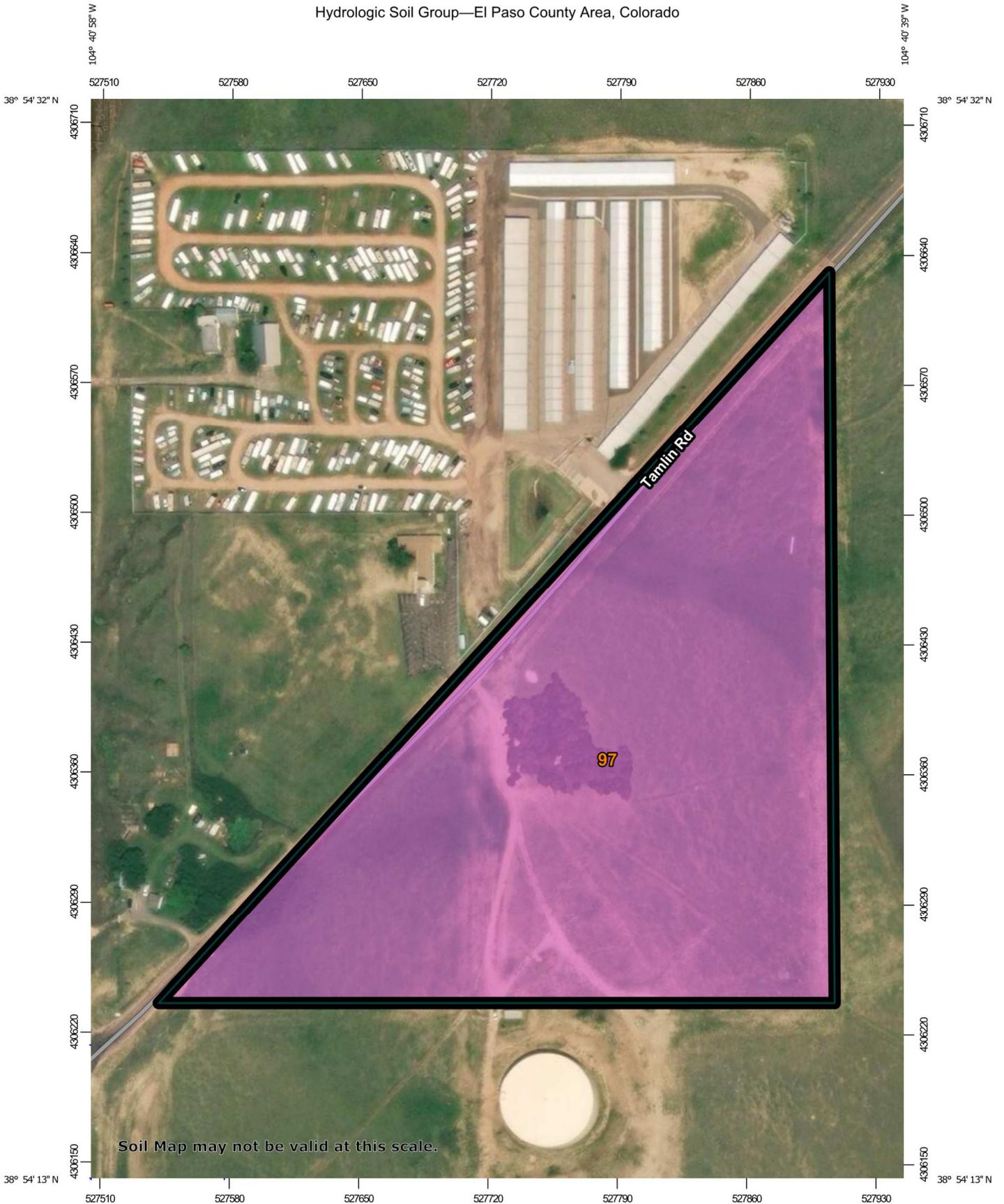
ORIGINAL SCALE: 1" = 2000'

VICINITY MAP
 TAMLIN ROAD STORAGE YARD
 2513400
 06/14/19
 SHEET 1 OF 1

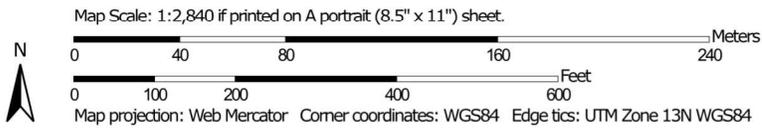


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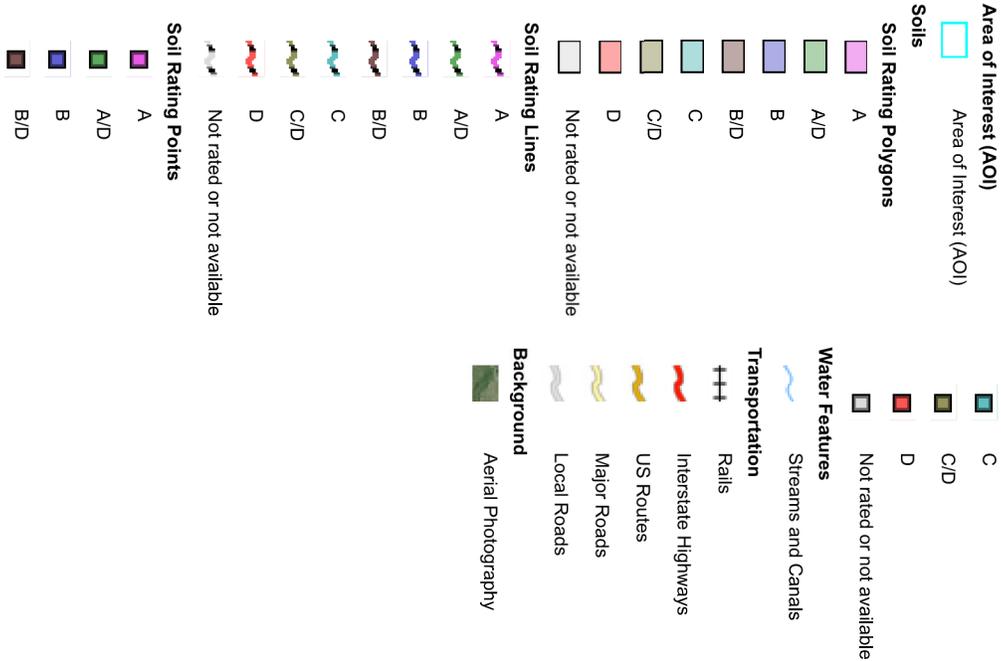
Hydrologic Soil Group—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



MAP LEGEND



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 16, Sep 10, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Apr 15, 2011—Aug 17, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
97	Truckton sandy loam, 3 to 9 percent slopes	A	17.9	100.0%
Totals for Area of Interest			17.9	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

	Without Base Flood Elevation (BFE) Zone A, V, A99
	With BFE or Depth Zone AE, AO, AH, VE, AR Regulatory Floodway

	0.2% Annual Chance Flood Hazard, Areas of 1% annual chance Flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
	Future Conditions 1% Annual Chance Flood Hazard Zone X
	Area with Reduced Flood Risk due to Levee, See Notes, Zone X
	Area with Flood Risk due to Levee Zone D

	Area of Minimal Flood Hazard Zone X
	Effective LOMIRs
	Area of Undetermined Flood Hazard Zone D
	Channel, Culvert, or Storm Sewer
	Levee, Dike, or Floodwall

	20.2 Cross Sections with 1% Annual Chance
	17.5 Water Surface Elevation
	Coastal Transect
	Base Flood Elevation Line (BFE)
	Limit of Study
	Jurisdiction Boundary
	Coastal Transect Baseline
	Profile Baseline
	Hydrographic Feature

	Digital Data Available
	No Digital Data Available
	Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **6/14/2019 at 10:33:46 AM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and undetermined areas cannot be used for regulatory purposes.



USGS The National Map: Orthoimagery, Data refreshed April, 2019.

0 250 500 1,000 1,500 2,000 Feet

104°40'29.24"W 38°54'2.78"N

104°41'6.69"W 38°54'30.77"N

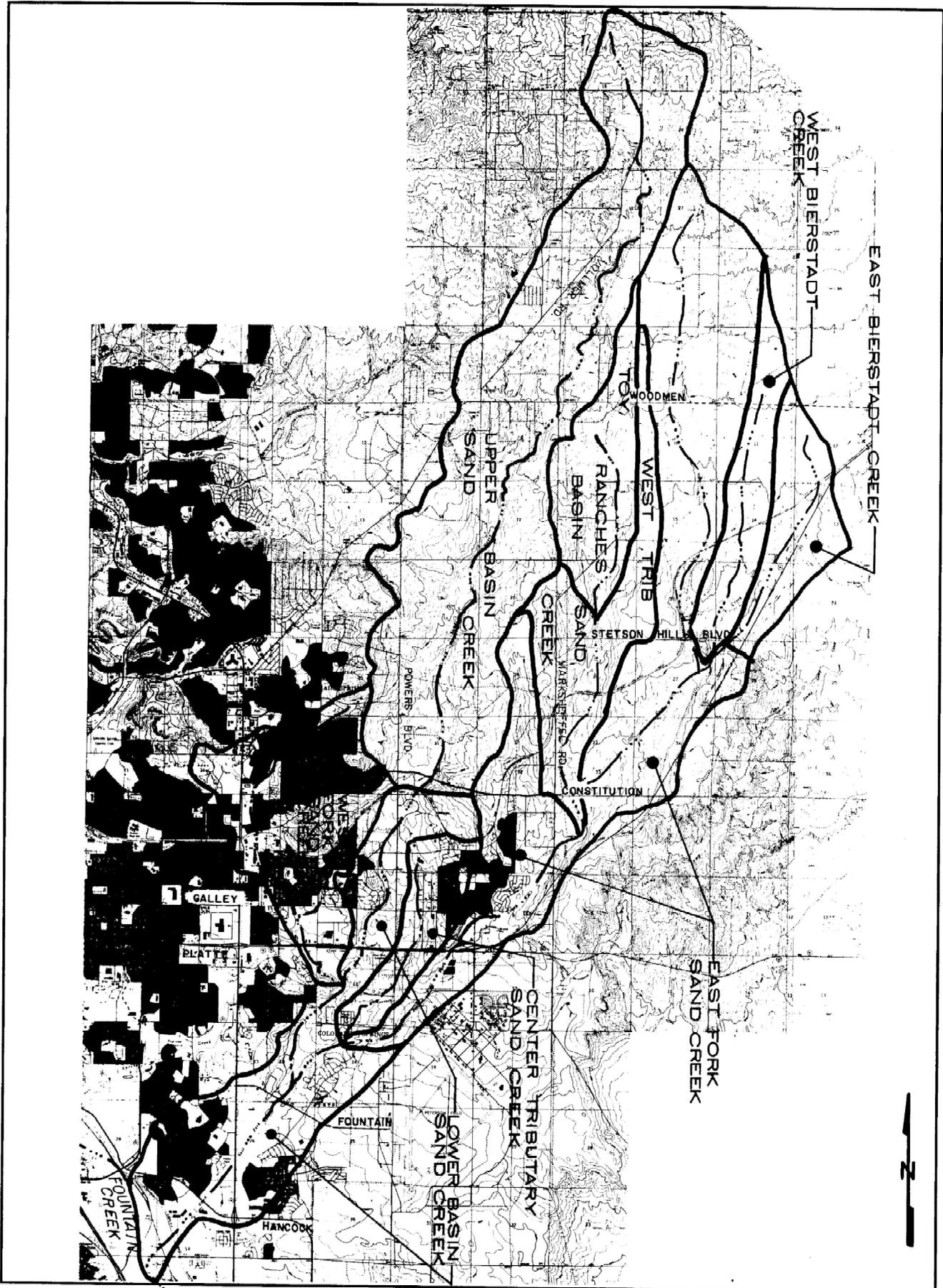
Appendix B
Reference Material

El Paso County Drainage Basin Fees

Resolution No. 18-470

Basin Number	Receiving Waters	Year Studied	Drainage Basin Name	2019 Drainage Fee (per Impervious Acre)	2019 Bridge Fee (per Impervious Acre)
<u>Drainage Basins with DBPS's:</u>					
CHMS0200	Chico Creek	2013	Haegler Ranch	\$10,324	\$1,524
CHWS1200	Chico Creek	2001	Bennett Ranch	\$11,558	\$4,433
CHWS1400	Chico Creek	2013	Falcon	\$29,622	\$4,069
FOFO2000	Fountain Creek	2001	West Fork Jimmy Camp Creek	\$12,564	\$3,717
FOFO2600	Fountain Creek	1991*	Big Johnson / Crews Gulch	\$18,350	\$2,370
FOFO2800	Fountain Creek	1988*	Widefield	\$18,350	\$0
FOFO2900	Fountain Creek	1988*	Security	\$18,350	\$0
FOFO3000	Fountain Creek	1991*	Windmill Gulch	\$18,350	\$275
FOFO3100 / FOFO3200	Fountain Creek	1988*	Carson Street / Little Johnson	\$11,192	\$0
FOFO3400	Fountain Creek	1984*	Peterson Field	\$13,235	\$1,004
FOFO3600	Fountain Creek	1991*	Fisher's Canyon	\$18,350	\$0
FOFO4000	Fountain Creek	1996	Sand Creek	\$18,940	\$5,559
FOFO4200	Fountain Creek	1977	Spring Creek	\$9,517	\$0
FOFO4600	Fountain Creek	1984*	Southwest Area	\$18,350	\$0
FOFO4800	Fountain Creek	1991	Bear Creek	\$18,350	\$1,004
FOFO5400	Fountain Creek	1977	21st Street	\$5,521	\$0
FOFO5600	Fountain Creek	1964	19th Street	\$3,611	\$0
FOFO5800	Fountain Creek	1964	Camp Creek	\$2,033	\$0
FOMO0400	Monument Creek	1986*	Mesa	\$9,598	\$0
FOMO1000	Monument Creek	1981	Douglas Creek	\$11,540	\$255
FOMO1200	Monument Creek	1977	Templeton Gap	\$11,847	\$275
FOMO1400	Monument Creek	1976	Pope's Bluff	\$3,676	\$627
FOMO1600	Monument Creek	1976	South Rockrimmon	\$4,314	\$0
FOMO1800	Monument Creek	1973	North Rockrimmon	\$5,521	\$0
FOMO2000	Monument Creek	1971	Pulpit Rock	\$6,085	\$0
FOMO2200	Monument Creek	1994	Cottonwood Creek / S. Pine	\$18,350	\$1,004
FOMO2400	Monument Creek	1966	Dry Creek	\$14,486	\$524
FOMO3600	Monument Creek	1989*	Black Squirrel Creek	\$8,331	\$524
FOMO3700	Monument Creek	1987*	Middle Tributary	\$15,312	\$0
FOMO3800	Monument Creek	1987*	Monument Branch	\$18,350	\$0
FOMO4000	Monument Creek	1996	Smith Creek	\$7,481	\$1,004
FOMO4200	Monument Creek	1989*	Black Forest	\$18,350	\$500
FOMO5200	Monument Creek	1993*	Dirty Woman Creek	\$18,350	\$1,004
FOMO5300	Fountain Creek	1993*	Crystal Creek	\$18,350	\$1,004
<u>Miscellaneous Drainage Basins: ¹</u>					
CHBS0800	Chico Creek		Book Ranch	\$17,217	\$2,492
CHEC0400	Chico Creek		Upper East Chico	\$9,380	\$272
CHWS0200	Chico Creek		Telephone Exchange	\$10,306	\$241
CHWS0400	Chico Creek		Livestock Company	\$16,976	\$202
CHWS0600	Chico Creek		West Squirrel	\$8,849	\$3,672
CHWS0800	Chico Creek		Solberg Ranch	\$18,350	\$0
FOFO1200	Fountain Creek		Crooked Canyon	\$5,540	\$0
FOFO1400	Fountain Creek		Calhan Reservoir	\$4,625	\$270
FOFO1600	Fountain Creek		Sand Canyon	\$3,342	\$0
FOFO2000	Fountain Creek		Jimmy Camp Creek ³	\$18,350	\$858
FOFO2200	Fountain Creek		Fort Carson	\$14,486	\$524
FOFO2700	Fountain Creek		West Little Johnson	\$1,209	\$0
FOFO3800	Fountain Creek		Stratton	\$8,801	\$394
FOFO5000	Fountain Creek		Midland	\$14,486	\$524
FOFO6000	Fountain Creek		Palmer Trail	\$14,486	\$524
FOFO6800	Fountain Creek		Black Canyon	\$14,486	\$524
FOMO4600	Monument Creek		Beaver Creek	\$10,970	\$0
FOMO3000	Monument Creek		Kettle Creek	\$9,909	\$0
FOMO3400	Monument Creek		Elkhorn	\$1,665	\$0
FOMO5000	Monument Creek		Monument Rock	\$7,953	\$0
FOMO5400	Monument Creek		Palmer Lake	\$12,717	\$0
FOMO5600	Monument Creek		Raspberry Mountain	\$4,278	\$0
PLPL0200	Monument Creek		Bald Mountain	\$9,116	\$0
<u>Interim Drainage Basins: ²</u>					
FOFO1800	Fountain Creek		Little Fountain Creek	\$2,346	\$0
FOMO4400	Monument Creek		Jackson Creek	\$7,263	\$0
FOMO4800	Monument Creek		Teachout Creek	\$5,044	\$758

1. The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies performed.
2. Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best available)
3. This is an interim fee and will be adjusted when a DBPS is completed. In addition to the Drainage Fee a surety in the amount of \$7,285 per impervious acre shall be provided. If the DBPS results in a fee greater than the current fee. Fees paid in excess of the future revised fee will be reimbursed. See Resolution 06-326 (9/14/06) and Resolution 18-470.



PROJECT NO. 90-03-09
 DATE: 11/90
 DRAWN: EAK
 CHECK: [blank]
 APPROVED: [blank]

**SAND CREEK DRAINAGE
 BASIN PLANNING STUDY**
REGIONAL SUB-BASINS

11

Kiowa Engineering Corporation
 419 W. Bijou Street
 Colorado Springs, Colorado
 80905-1308

Appendix C

Hydrologic Calculations

EX. DRAINAGE CALCS

BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C ₅	C ₁₀₀	t _c (min)	Q ₅ (cfs)	Q ₁₀₀ (cfs)
EX1	6.43	2%	0.05	0.36	13.4	1.2	14.3
EX2	10.08	2%	0.05	0.36	15.4	1.8	21.2

DESIGN POINT SUMMARY TABLE

Tributary Sub-basin	Q ₅ (cfs)	Q ₁₀₀ (cfs)
1	1.2	14.3
2	1.8	21.2

EX. COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: TAMLIN ROAD STORAGE YARD
 Location: Colorado Springs

Project Name: TAMLIN ROAD STORAGE YARD

Project No.: 25134.00

Calculated By: NOJ

Checked By:

Date: 11/1/19

Basin ID	Total Area (ac)	Historic Flow Analysis			Roofs			Paved Roads			Basins Total Weighted % Imp.
		% Imp.	Area (ac)	Weighted % Imp.	Area (ac)	Weighted % Imp.	Area (ac)	Weighted % Imp.	Area (ac)	Weighted % Imp.	
EX1	6.43	2%	6.43	2.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	2.0%
EX2	10.08	2%	10.08	2.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	2.0%
TOTAL	16.51										2.0%

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HS-CRB	HS-CBD	HS-CRB	HS-CBD	HS-CRB	HS-CBD	HS-CRB	HS-CBD	HS-CRB	HS-CBD	HS-CRB	HS-CBD
Business	50	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80
Commercial/Office	70	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80
Industrial	80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80	0.70	0.80
Light Areas	30	0.30	0.35	0.30	0.35	0.30	0.35	0.30	0.35	0.30	0.35	0.30	0.35
Medium Density Residential	20	0.20	0.25	0.20	0.25	0.20	0.25	0.20	0.25	0.20	0.25	0.20	0.25
High Density Residential	10	0.10	0.15	0.10	0.15	0.10	0.15	0.10	0.15	0.10	0.15	0.10	0.15
Fields and Pastures	10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
Forests	10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
Open Fields	10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
Offices (Flow Analysis taken from literature)	45	0.30	0.35	0.30	0.35	0.30	0.35	0.30	0.35	0.30	0.35	0.30	0.35
Streets	100	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
Driveways	100	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
Roofs and Walks	100	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
Lawns	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

EX. COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: TAMLIN ROAD STORAGE YARD
 Location: Colorado Springs

Project Name: TAMLIN ROAD STORAGE YARD
 Project No.: 25134.00
 Calculated By: NOJ
 Checked By: _____
 Date: 11/1/19

Basin ID	Total Area (ac)	Basins Total Weighted % Imp.	Hydrologic Soil Group				Land Use			Minor Coefficients			Major Coefficients			Basins Total Weighted C_s	Basins Total Weighted C_{100}
			Area A (ac)	Area B (ac)	Area C/D (ac)	Area Historic (ac)	Area Roofs (ac)	Area Paved Roads (ac)	$C_{S,A,HISTORIC}$	$C_{S,A,ROOFS}$	$C_{S,A,ROADS}$	$C_{100,A,HISTORIC}$	$C_{100,A,ROOFS}$	$C_{100,A,ROADS}$			
EX1	6.43	2.0%	6.43	0.00	0.00	6.43	0.00	0.00	0.05	0.73	0.90	0.36	0.81	0.96	0.05	0.36	
EX2	10.08	2.0%	10.08	0.00	0.00	10.08	0.00	0.00	0.05	0.73	0.90	0.36	0.81	0.96	0.05	0.36	
TOTAL	16.51	2.0%	16.51	0.00	0.00	16.51	0.00	0.00	0.05	0.73	0.90	0.36	0.81	0.96	0.05	0.36	

EX. STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: TAMLIN ROAD STORAGE YARD
Location: Colorado Springs

Project Name: TAMLIN ROAD STORAGE YARD
Project No.: 25134.00
Calculated By: NOJ
Checked By:
Date: 11/1/19

SUB-BASIN DATA					INITIAL/OVERLAND (T ₁)					TRAVEL TIME (T ₂)					t _c CHECK (URBANIZED BASINS)		FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	L (ft)	S ₀ (%)	t ₁ (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
EX1	6.43	A	2%	0.05	0.36	54	3.5%	9.2	550	4.7%	10.0	2.2	4.2	13.4	604.0	30.2	13.4
EX2	10.08	A	2%	0.05	0.36	76	3.9%	10.5	537	3.4%	10.0	1.8	4.9	15.4	613.0	30.9	15.4

NOTES:

$$t_c = t_1 + t_2$$

Where:

t_c = computed time of concentration (minutes)

t₁ = overland (initial) flow time (minutes)

t₂ = channelized flow time (minutes)

$$t_1 = \frac{L}{60K\sqrt{S_0}} = \frac{L}{60V}$$

Where:

- L = channelized flow time (travel time- min)
- L_t = watershed length (ft)
- S₀ = watershed slope (ft/ft)
- V = travel time velocity (ft/sec) = K√S₀
- K = NRCS conveyance factor (see Table 6-2)

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$\text{Equation 6-2}$$

$$t_1 = \frac{0.395(1-C_3)\sqrt{L}}{S_0^{0.33}}$$

Where:

- t₁ = overland (initial) flow time (minutes)
- C₃ = runoff coefficient for 2-year frequency (from Table 6-4)
- L_t = length of overland flow (ft)
- S₀ = average slope along the overland flow path (ft/ft)

$$\text{Equation 6-1}$$

$$t_2 = (26 - 1.7t_1) + \frac{L}{60(1.4t_1 + 9)\sqrt{S_2}}$$

Where:

- t₂ = minimum time of concentration for first design point when less than t_c from Equation 6-1
- L_t = length of channelized flow path (ft)
- t₁ = imperviousness (expressed as a decimal)
- S₂ = slope of the channelized flow path (ft/ft)

$$\text{Equation 6-3}$$

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

EX. STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
 (RATIONAL METHOD PROCEDURE)

Subdivision: TAMLIN ROAD STORAGE YARD
 Location: Colorado Springs
 Design Storm: 5-Year

Project Name: TAMLIN ROAD STORAGE YARD
 Project No.: 25134.00
 Calculated By: NJL
 Checked By:
 Date: 11/7/19

STREET	Design Point	DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME		REMARKS				
		Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)		Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)
	1	EX1	6.43	0.05	13.4	0.32	3.69	1.2															TOTAL FLOW DISCHARGING TO TAMLIN ROAD UNDEVELOPED LAND
	2	EX2	10.08	0.05	15.4	0.50	3.48	1.7															

Notes:
 Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

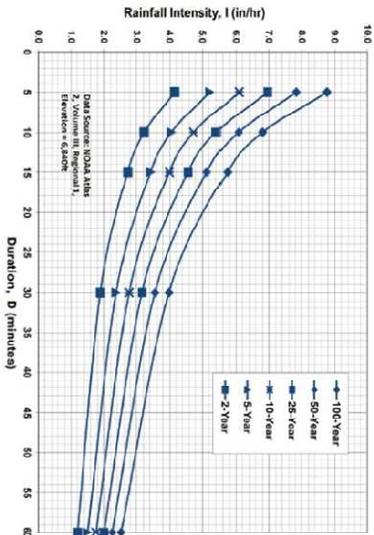


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 11.735$$

$$I_{50} = 2.35 \ln(D) + 11.775$$

$$I_{25} = 2.00 \ln(D) + 10.111$$

$$I_{10} = 1.75 \ln(D) + 8.817$$

$$I_{5} = 1.50 \ln(D) + 7.581$$

$$I_{2} = 1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

EX. STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: TAMULIN ROAD STORAGE YARD
Location: Colorado Springs
Design Storm: 100-Year

Project Name: TAMULIN ROAD STORAGE YARD
Project No.: 25134.00
Calculated By: NOJ
Checked By:
Date: 11/1/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF			STREET			PIPE			TRAVEL TIME		REMARKS			
		Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)		Length (ft)	Velocity (fps)	t_t (min)
	1	EX1	6.43	0.36	13.4	2.31	6.19	14.3															TOTAL FLOW DISCHARGING TO TAMULIN ROAD
	2	EX2	10.08	0.36	15.4	3.63	5.84	21.2															TOTAL FLOW DISCHARGING OFFSITE ALONG WESTERN PROPERTY LINE TO UNDEVELOPED PARCEL

Notes:
Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

**TAMLIN ROAD RV & BOAT
STORAGE - PROPOSED
DRAINAGE CALCS**

BASIN SUMMARY TABLE							
Tributary Sub-basin	Area (acres)	Percent Impervious	C₅	C₁₀₀	t_c (min)	Q₅ (cfs)	Q₁₀₀ (cfs)
A1	0.38	32%	0.34	0.54	5.0	0.7	1.8
A2	4.42	68%	0.66	0.78	7.4	13.3	26.5
A3	4.72	81%	0.78	0.86	8.5	16.0	30.0
A4	0.70	0%	0.08	0.35	7.0	0.3	1.9
A5	1.14	4%	0.12	0.38	8.7	0.6	3.1
A6	0.26	0%	0.08	0.35	5.0	0.1	0.8
A7	0.39	0%	0.08	0.35	5.0	0.2	1.2
A8	0.40	0%	0.08	0.35	5.0	0.2	1.2

DESIGN POINT SUMMARY TABLE		
Tributary Sub-basin	Q₅ (cfs)	Q₁₀₀ (cfs)
1	0.7	1.8
2	29.3	56.7
3	29.5	58.4
4	0.6	3.1
5	0.1	0.8
6	0.2	1.2
7	0.2	1.2

COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: TAMLIN ROAD RV STORAGE
 Location: Colorado Springs

Project Name: TAMLIN ROAD RV STORAGE
 Project No.: 25134.00
 Calculated By: NOJ
 Checked By: _____
 Date: 1/17/20

Basin ID	Total Area (ac)	Paved Roads (Asphalt)			Rock Mulch			Lawns		Basins Total Weighted % Imp.	
		% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)		Weighted % Imp.
A1	0.38	100%	0.12	31.6%	20%	0.00	0.0%	0%	0.26	0.0%	31.6%
A2	4.42	100%	2.96	67.0%	20%	0.28	1.3%	0%	1.18	0.0%	68.2%
A3	4.72	100%	3.74	79.2%	20%	0.38	1.6%	0%	0.60	0.0%	80.8%
A4	0.70	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.70	0.0%	0.0%
A5	1.14	100%	0.05	4.4%	20%	0.00	0.0%	0%	1.09	0.0%	4.4%
A6	0.26	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.26	0.0%	0.0%
A7	0.39	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.39	0.0%	0.0%
A8	0.40	100%	0.00	0.0%	20%	0.00	0.0%	0%	0.40	0.0%	0.0%
TOTAL	12.41										56.4%
POND A TOTAL	10.22										68.0%

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: TAMLIN ROAD RV STORAGE
 Location: Colorado Springs

Project Name: TAMLIN ROAD RV STORAGE
 Project No.: 25134.00
 Calculated By: NOJ
 Checked By: _____
 Date: 1/17/20

Basin ID	Total Area (ac)	Basins Total Weighted % Imp.	Hydrologic Soil Group				Land Use			Minor Coefficients					Major Coefficients			Basins Total Weighted C _s	Basins Total Weighted C ₁₀₀
			Area A (ac)	Area B (ac)	Area C/D (ac)	Area Roads (ac)	Area Roofs (ac)	Area Lawns (ac)	C _{s,A,ROADS}	C _{s,A,ROCK MULCH}	C _{s,A,LAWNS}	C _{100,A,ROADS}	C _{100,A,ROCK MULCH}	C _{100,A,LAWNS}	C _{s,B}	C _{s,C}	C _{s,D}		
A1	0.38	31.6%	0.38	0.00	0.00	0.12	0.00	0.26	0.90	0.20	0.08	0.96	0.36	0.35	0.34	0.54			
A2	4.42	68.2%	4.42	0.00	0.00	2.96	0.28	1.18	0.90	0.53	0.08	0.96	0.64	0.35	0.66	0.78			
A3	4.72	80.8%	4.72	0.00	0.00	3.74	0.38	0.60	0.90	0.66	0.08	0.96	0.74	0.35	0.78	0.86			
A4	0.70	0.0%	0.70	0.00	0.00	0.00	0.00	0.70	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35			
A5	1.14	4.4%	1.14	0.00	0.00	0.05	0.00	1.09	0.90	0.02	0.08	0.96	0.14	0.35	0.12	0.38			
A6	0.26	0.0%	0.26	0.00	0.00	0.00	0.00	0.26	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35			
A7	0.39	0.0%	0.39	0.00	0.00	0.00	0.00	0.39	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35			
A8	0.40	0.0%	0.40	0.00	0.00	0.00	0.00	0.40	0.90	0.00	0.08	0.96	0.11	0.35	0.08	0.35			
TOTAL	12.41	56.4%	12.41	0.00	0.00	6.87	0.24	4.88	---	---	---	---	---	---	0.56	0.71			

Table 6-6. Runoff Coefficients for Rational Method
 (Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A,B	HSG C,D	HSG A,B	HSG C,D	HSG A,B	HSG C,D	HSG A,B	HSG C,D	HSG A,B	HSG C,D	HSG A,B	HSG C,D
Residential	25	0.29	0.20	0.21	0.22	0.21	0.24	0.20	0.27	0.21	0.22	0.21	0.21
Commercial Areas	70	0.42	0.20	0.42	0.51	0.51	0.57	0.58	0.62	0.62	0.62	0.62	0.62
Industrial	60	0.42	0.42	0.42	0.40	0.40	0.42	0.42	0.50	0.42	0.42	0.50	0.42
Highway Areas	90	0.42	0.40	0.50	0.50	0.49	0.46	0.46	0.50	0.49	0.49	0.50	0.50
Developed Forestland	14	0.07	0.10	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
Unimproved Forestland	40	0.23	0.28	0.30	0.30	0.30	0.36	0.42	0.42	0.42	0.42	0.42	0.42
Urban Development Areas	2	0.49	0.49	0.49	0.44	0.44	0.44	0.44	0.49	0.44	0.44	0.49	0.44
Open Space	0	0.02	0.04	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.27	0.30	0.34	0.35	0.35
Barren Rock	100	0.90	0.90	0.90	0.90	0.90	0.94	0.94	0.95	0.95	0.95	0.95	0.95
Other Flow Analysis (when land use is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.48	0.48	0.48	0.51	0.50
Concrete	100	0.80	0.80	0.80	0.80	0.80	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Asphalt	80	0.17	0.00	0.10	0.03	0.03	0.06	0.06	0.06	0.06	0.06	0.06	0.06
Gravel	80	0.80	0.80	0.80	0.80	0.80	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Clay and Silt	100	0.80	0.80	0.80	0.80	0.80	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Rock	90	0.21	0.25	0.25	0.27	0.27	0.28	0.28	0.28	0.28	0.28	0.28	0.28
Grass	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.27	0.30	0.34	0.35	0.35

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

NRCS Soil Group	Storm Return Period				
	2-Year	5-Year	10-Year	25-Year	50-Year
A	$C_p = 0.84 / I^{0.01}$	$C_p = 0.86 / I^{0.04}$	$C_p = 0.87 / I^{0.03}$	$C_p = 0.84 / I^{0.04}$	$C_p = 0.85 / I^{0.025}$
B	$C_p = 0.84 / I^{0.08}$	$C_p = 0.86 / I^{0.08}$	$C_p = 0.87 / I^{0.057}$	$C_p = 0.83 / I^{0.249}$	$C_p = 0.56 / I^{0.328}$
C/D	$C_p = 0.83 / I^{0.122}$	$C_p = 0.83 / I^{0.035}$	$C_p = 0.74 / I^{0.132}$	$C_p = 0.58 / I^{0.319}$	$C_p = 0.49 / I^{0.393}$

Where:
 I = % imperviousness (expressed as a decimal)
 C_p = Runoff coefficient for Annual Resources Conservation Service (NRCS) HSG A soils
 C_s = Runoff coefficient for NRCS HSG B soils
 C₁₀₀ = Runoff coefficient for NRCS HSG C and D soils.

TABLE 6-4 UTILIZED TO CALCULATE 'C-VALUE' FOR ROCK MULCH

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: TAMLIN ROAD RV STORAGE
Location: Colorado Springs

Project Name: TAMLIN ROAD RV STORAGE

Project No.: 25134.00

Calculated By: NOJ

Checked By:

Date: 1/17/20

BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	INITIAL/OVERLAND			TRAVEL TIME				tc CHECK		FINAL t _c (min)		
						L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)		TOTAL LENGTH (ft)	Urbanized t _c (min)
A1	0.38	A	32%	0.34	0.54	11	2.0%	3.6	250	2.9%	20.0	3.4	1.2	4.8	261.0	22.5	5.0
A2	4.42	A	68%	0.66	0.78	125	5.6%	5.1	455	2.7%	20.0	3.3	2.3	7.4	580.0	16.9	7.4
A3	4.72	A	81%	0.78	0.86	105	1.0%	5.9	517	2.8%	20.0	3.3	2.6	8.5	622.0	14.8	8.5
A4	0.70	A	0%	0.08	0.35	25	25.0%	3.2	160	1.0%	7.0	0.7	3.8	7.0	185.0	29.0	7.0
A5	1.14	A	4%	0.12	0.38	37	5.2%	6.3	275	7.4%	7.0	1.9	2.4	8.7	312.0	27.0	8.7
A6	0.26	A	0%	0.08	0.35	20	22.0%	3.0	25	22.0%	7.0	3.3	0.1	3.1	45.0	26.1	5.0
A7	0.39	A	0%	0.08	0.35	20	25.0%	2.8	25	25.0%	7.0	3.5	0.1	3.0	45.0	26.1	5.0
A8	0.40	A	0%	0.08	0.35	20	18.0%	3.2	25	18.0%	7.0	3.0	0.1	3.3	45.0	26.1	5.0

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes)

$$t_i = \frac{L_i}{60 K \sqrt{S_o}} = \frac{L_i}{60 V_i}$$

Where:

L_i = channelized flow time (travel time, min)

L_t = waterway length (ft)

S_t = waterway slope (ft/ft)

V_i = travel time velocity (ft/sec) = K_SS_o

K_S = NRCS conveyance factor (see Table 6-3)

$$\text{Equation 6-2}$$

$$t_i = \frac{0.395(1 - C_1)\sqrt{L_i}}{S_o^{0.8}}$$

Where:

L_i = overland (initial) flow time (minutes)

C₁ = runoff coefficient for 2-year frequency (from Table 6-4)

L_i = length of overland flow (ft)

S_o = average slope along the overland flow path (ft/ft)

$$\text{Equation 6-3}$$

Where:

t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1

L_t = length of channelized flow path (ft)

f = imperviousness (expressed as a decimal)

S_t = slope of the channelized flow path (ft/ft)

Table 6.2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: TAMLIN ROAD RV STORAGE
Location: Colorado Springs
Design Storm: 5-Year

Project Name: TAMLIN ROAD RV STORAGE
Project No.: 25134.00
Calculated By: NGJ
Checked By:
Date: 1/17/20

STREET	Design Point	DIRECT RUNOFF						TOTAL RUNOFF			STREET			PIPE			TRAVEL TIME			REMARKS		
		Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)		Length (ft)	Velocity (fps)
	1	A1	0.38	0.34	5.0	0.13	5.17	0.7				0.7	0.13	2.0					406	2.8	2.4	BASIN A1 FLOW @ DP1, SHEET FLOW TO DP2
		A2	4.42	0.66	7.4	2.91	4.59	13.4														BASIN A2 FLOW @ DP2 (ROUTED IN SF2)
		A3	4.72	0.78	8.5	3.66	4.37	16.0														BASIN A3 FLOW @ DP2 (ROUTED IN SF2)
	2								8.5	6.70	4.37	29.3	6.7	25.0					35	10.0	0.1	DP1, BASIN A2-A3 FLOW @ DP2, SHEET FLOW TO DP3 (F.S.D. WQ POND)
		A4	0.70	0.08	7.0	0.06	4.67	0.3														BASIN A4 FLOW @ DP3 (ROUTED IN SF2)
	3								8.5	6.76	4.36	29.5										TOTAL BASIN A1-A4 FLOW ENTERING F.S.D. WQ POND
		A5	1.14	0.12	8.7	0.13	4.34	0.6														TOTAL BASIN A5 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
		A6	0.26	0.08	5.0	0.02	5.17	0.1														TOTAL BASIN A6 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
		A7	0.39	0.08	5.0	0.03	5.17	0.2														TOTAL BASIN A7 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
		A8	0.40	0.08	5.0	0.03	5.17	0.2														TOTAL BASIN A8 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS

Notes:
Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: TAMLIN ROAD RV STORAGE
Location: Colorado Springs
Design Storm: 100-Year

Project Name: TAMLIN ROAD RV STORAGE
Project No.: 25134.00
Calculated By: NGJ
Checked By:
Date: 1/17/20

STREET	Design Point	DIRECT RUNOFF						TOTAL RUNOFF			STREET			PIPE			TRAVEL TIME		REMARKS				
		Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)		Pipe Size (inches)	Length (ft)	Velocity (fps)	t_r (min)
	1	A1	0.38	0.54	5.0	0.21	8.68	1.8				1.8	0.21	2.0						406	2.8	2.4	BASIN A1 FLOW @ DP1, SHEET FLOW TO DP2
		A2	4.42	0.78	7.4	3.43	7.70	26.4															BASIN A2 FLOW @ DP2 (ROUTED IN SF2)
		A3	4.72	0.86	8.5	4.08	7.34	30.0															BASIN A3 FLOW @ DP2 (ROUTED IN SF2)
	2								8.5	7.72	7.34	56.7	7.72	25.0						35	10.0	0.1	DP1, BASIN A2-A3 FLOW @ DP2, SHEET FLOW TO DP3 (F.S.D. WQ POND)
		A4	0.70	0.35	7.0	0.25	7.83	2.0															BASIN A4 FLOW @ DP3 (ROUTED IN SF2)
	3								8.5	7.97	7.33	58.4											TOTAL BASIN A1-A4 FLOW ENTERING F.S.D. WQ POND
	4	A5	1.14	0.38	8.7	0.43	7.29	3.1															TOTAL BASIN A5 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	5	A6	0.26	0.35	5.0	0.09	8.68	0.8															TOTAL BASIN A6 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	6	A7	0.39	0.35	5.0	0.14	8.68	1.2															TOTAL BASIN A7 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS
	7	A8	0.40	0.35	5.0	0.14	8.68	1.2															TOTAL BASIN A8 FLOW (UNDEVELOPED), SHEET FLOW EAST FOLLOWING EX. DRAINAGE PATTERNS

Notes:
Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input

Calculated cells

--Design Storm: 1-Hour Rain Depth: **1.19** Inches

--Minor Storm: 1-Hour Rain Depth: **1.50** Inches

--Major Storm: 1-Hour Rain Depth: **2.52** Inches

Optional User Defined Storm: **CUIP**

(CUIP) NOAA 1-Hour Rainfall Depth and Frequency for User Defined Storm: **100-Year Event**

Max Intensity for Optional User Defined Storm: **0**

Designer: **NOI**

Company: **JR ENGINEERING**

Date: **January 21, 2020**

Project: **TAMULIN ROAD RV & BOAT STORAGE**

Location: **COLORADO SPRINGS**

SITE INFORMATION (USER-INPUT)

Sub-basin Identifier	A1	A2	A3	A4	A5	A6	A7	A8
Receiving Previous Area Soil Type	Sandy Loam							
Total Area (i.e., Sum of DCA, U/A, RPA & SPA)	0.380	4.420	4.720	0.700	1.140	0.260	0.390	0.400
Directly Connected Impervious Area (DCIA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Unconnected Impervious Area (UIA, acres)	0.380	4.420	4.720	0.000	0.000	0.000	0.000	0.000
Receiving Previous Area (RPA, acres)	0.000	0.000	0.000	0.700	0.000	0.000	0.000	0.000
Separate Previous Area (SPA, acres)	0.000	0.000	0.000	1.140	0.260	0.390	0.400	
RPA Treatment Type: Conveyance (C), Volume (V), or Permissible Pavement (P)	C	C	C	V	C	C	C	C

CALCULATED RESULTS (OUTPUT)

Total Calculated Area (i.e., check against input)	0.380	4.420	4.720	0.700	1.140	0.260	0.390	0.400
Directly Connected Impervious Area (DCIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Unconnected Impervious Area (UIA, %)	100.0%	100.0%	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Receiving Previous Area (RPA, %)	0.0%	0.0%	0.0%	100.0%	0.0%	0.0%	0.0%	0.0%
Separate Previous Area (SPA, %)	0.0%	0.0%	0.0%	0.0%	100.0%	100.0%	100.0%	100.0%
A _n (RPA / UIA)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
L-Check	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
f // For WQCV Event:	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9
f // For 5-Year Event:	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
f // For 100-Year Event:	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3
f // For Optional User Defined Storm CUIP:								
IRF for WQCV Event:	1.00	1.00	1.00	0.00	1.00	1.00	1.00	1.00
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
IRF for Optional User Defined Storm CUIP:								
Total Site Imperviousness: I _u	100.0%	100.0%	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Effective Imperviousness for WQCV Event:	100.0%	100.0%	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Effective Imperviousness for 5-Year Event:	100.0%	100.0%	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Effective Imperviousness for 100-Year Event:	100.0%	100.0%	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Effective Imperviousness for Optional User Defined Storm CUIP:								

LID / EFFECTIVE IMPERVIOUSNESS CREDITS

WQCV Event CREDIT: Reduce Detention By:	0.0%	0.0%	0.0%	N/A														
This site only, for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT: Reduce Detention By:	0.0% <td>0.0% <td>0.0% <td>N/A</td> </td></td>	0.0% <td>0.0% <td>N/A</td> </td>	0.0% <td>N/A</td>	N/A														
User Defined CUIP CREDIT: Reduce Detention By:																		

Total Site Imperviousness: **76.7%**

Total Site Effective Imperviousness for WQCV Event: **76.7%**

Total Site Effective Imperviousness for 5-Year Event: **76.7%**

Total Site Effective Imperviousness for 100-Year Event: **76.7%**

Total Site Effective Imperviousness for Optional User Defined Storm CUIP: **76.7%**

Notes:
 * Use Green Amps average infiltration rate values from Table 3.3
 ** Floor control detention volume credits based on empirical equations from Storage Chapter of USDCM.
 *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposes

Appendix D

Hydraulic Calculations

Weir Report

Pond A Spillway (Q_100_undetained = 39.9 cfs per UD-Detention Peak Inflow)

Trapezoidal Weir

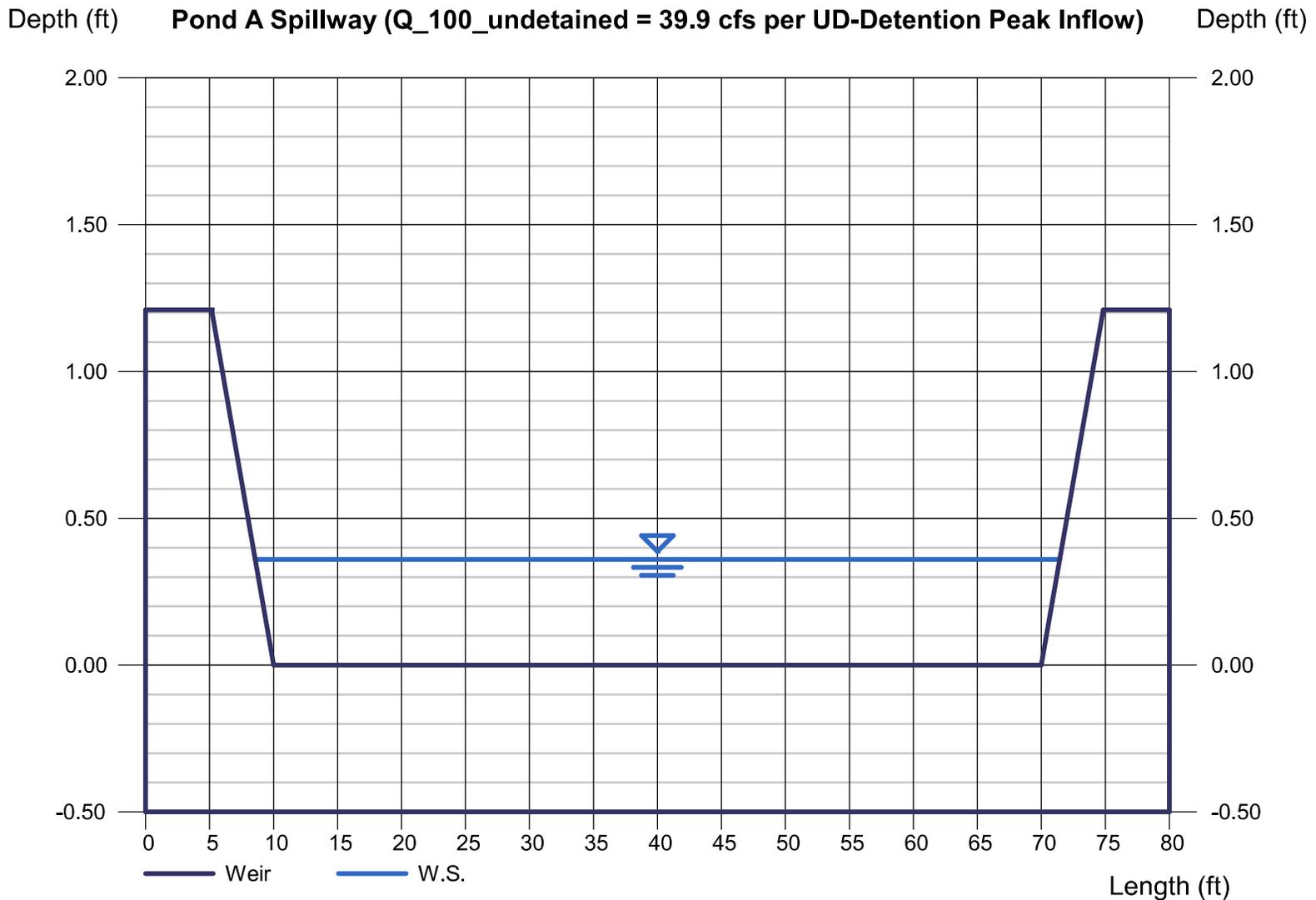
Crest = Sharp
Bottom Length (ft) = 60.00
Total Depth (ft) = 1.21
Side Slope (z:1) = 4.00

Highlighted

Depth (ft) = 0.36
Q (cfs) = 39.90
Area (sqft) = 22.12
Velocity (ft/s) = 1.80
Top Width (ft) = 62.88

Calculations

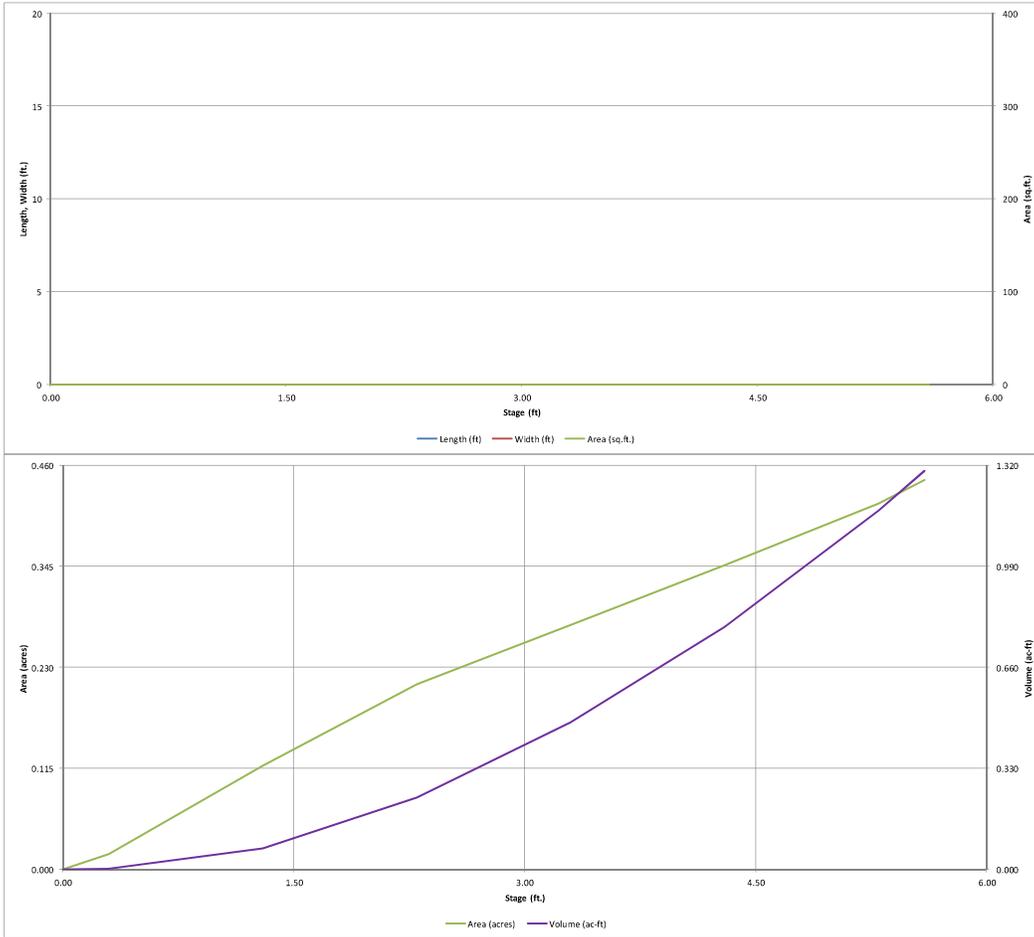
Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 39.90



Appendix E
Water Quality and Detention

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

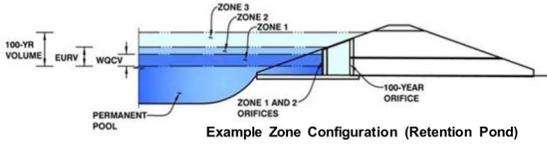
UD-Detention, Version 3.07 (February 2017)



Detention Basin Outlet Structure Design

UD- Detention, Version 3.07 (February 2017)

Project: **TAMLIN ROAD STORAGE YARD**
Basin ID: **BASIN A**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.27	0.227	Orifice Plate
Zone 2 (EURV)	4.54	0.647	Rectangular Orifice
Zone 3 (100-year)	5.58	0.415	Weir&Pipe (Restrict)
		1.288	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.27	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	1.14	sq. inches (diameter = 1-3/16 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row =	7.917E-03	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.76						
Orifice Area (sq. inches)	1.14	1.14						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.27	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	4.54	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.50	N/A	inches
Vertical Orifice Width =	1.25		inches

Calculated Parameters for Vertical Orifice

	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.02	N/A	ft ²
Vertical Orifice Centroid =	0.10	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.58	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	3.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	3.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H _g =	4.58	N/A	feet
Over Flow Weir Slope Length =	3.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	10.95	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	6.30	N/A	ft ²
Overflow Grate Open Area w/ Debris =	3.15	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.95	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	6.50		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.58	N/A	ft ²
Outlet Orifice Centroid =	0.32	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	1.29	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.65	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	60.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =	0.36	feet
Stage at Top of Freeboard =	7.01	feet
Basin Area at Top of Freeboard =	0.44	acres

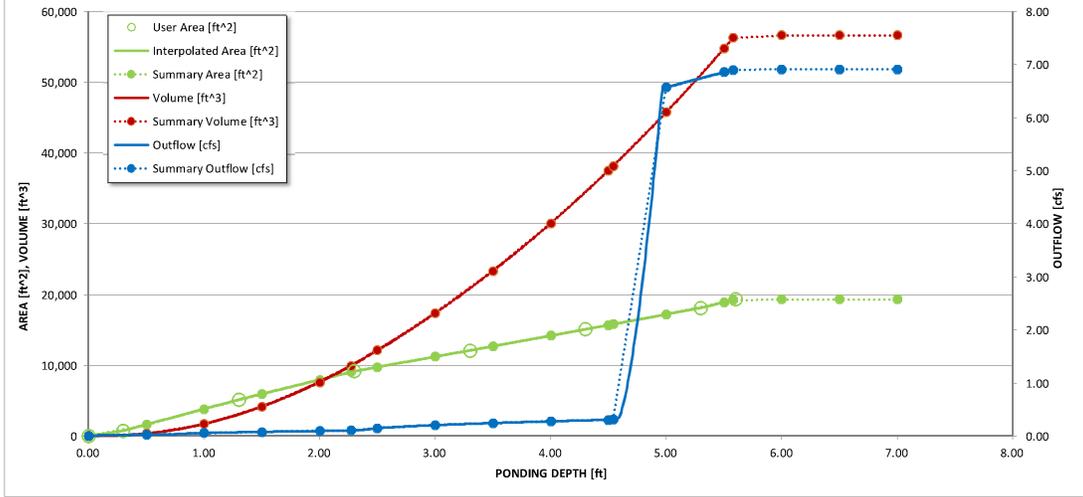
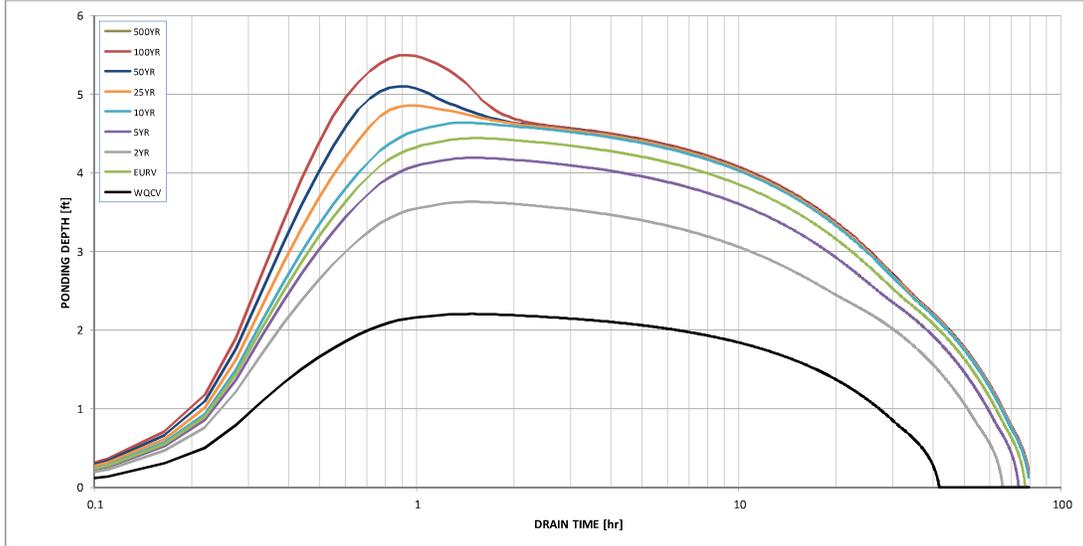
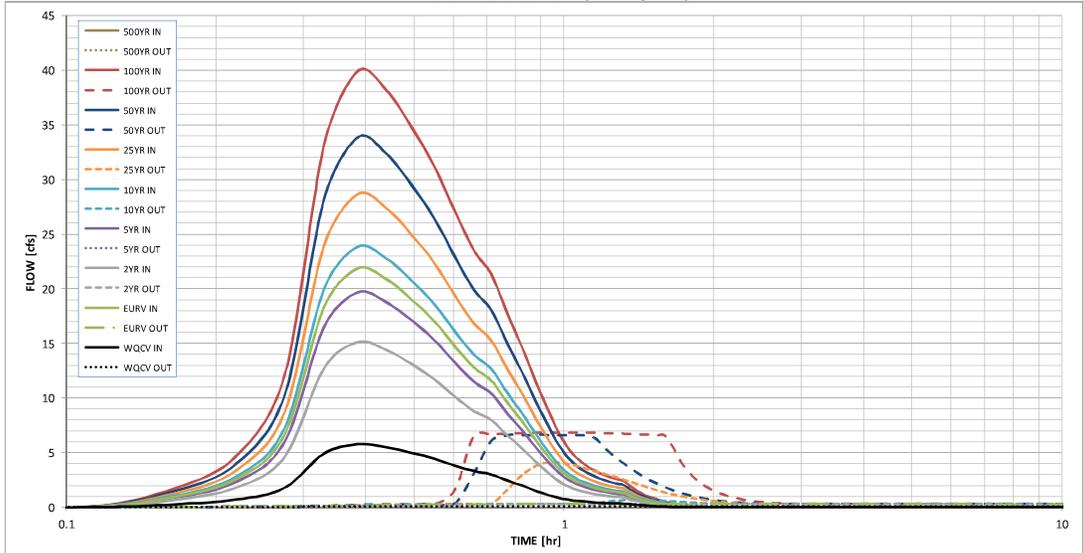
Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
One-Hour Rainfall Depth (in) =	0.227	0.873	0.601	0.785	0.953	1.149	1.359	1.606	0.000
Calculated Runoff Volume (acre-ft) =									
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.226	0.872	0.600	0.783	0.952	1.146	1.357	1.603	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.00	0.01	0.02	0.04	0.31	0.74	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.1	0.2	0.4	3.1	7.6	0.0
Peak Inflow Q (cfs) =	5.8	21.9	15.1	19.7	23.8	28.7	33.8	39.9	#N/A
Peak Outflow Q (cfs) =	0.1	0.3	0.3	0.3	0.7	4.1	6.6	6.9	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	3.5	3.5	9.4	2.1	0.9	#N/A
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.6	1.0	1.0	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	38	66	57	63	68	67	65	64	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	72	62	69	74	74	73	72	#N/A
Maximum Ponding Depth (ft) =	2.21	4.44	3.63	4.19	4.64	4.86	5.10	5.50	#N/A
Area at Maximum Ponding Depth (acres) =	0.20	0.36	0.30	0.34	0.37	0.38	0.40	0.43	#N/A
Maximum Volume Stored (acre-ft) =	0.214	0.840	0.574	0.753	0.909	0.992	1.090	1.253	#N/A

Adjust the design so that the release is equal to or less than pre-development

Detention Basin Outlet Structure Design

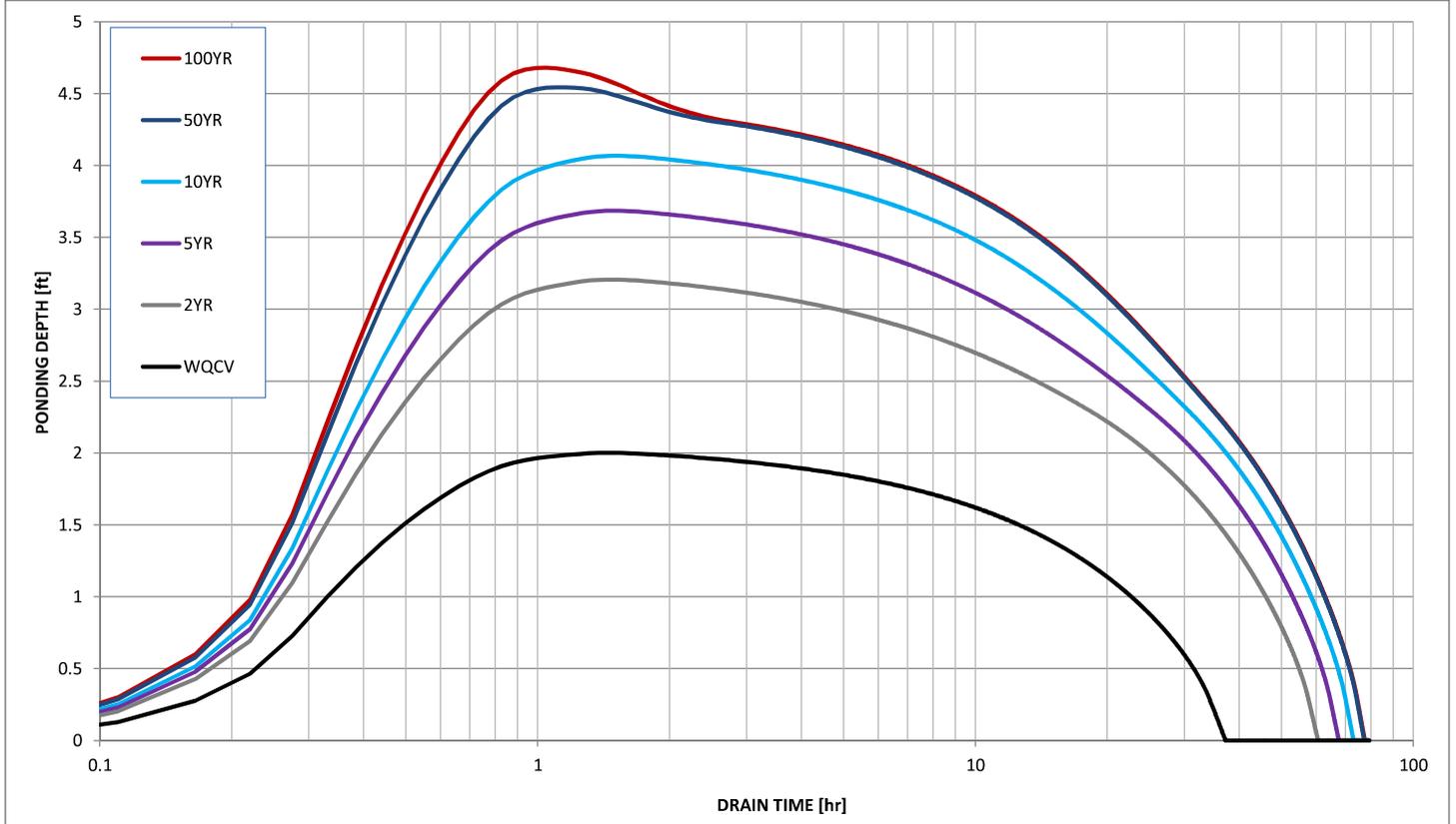
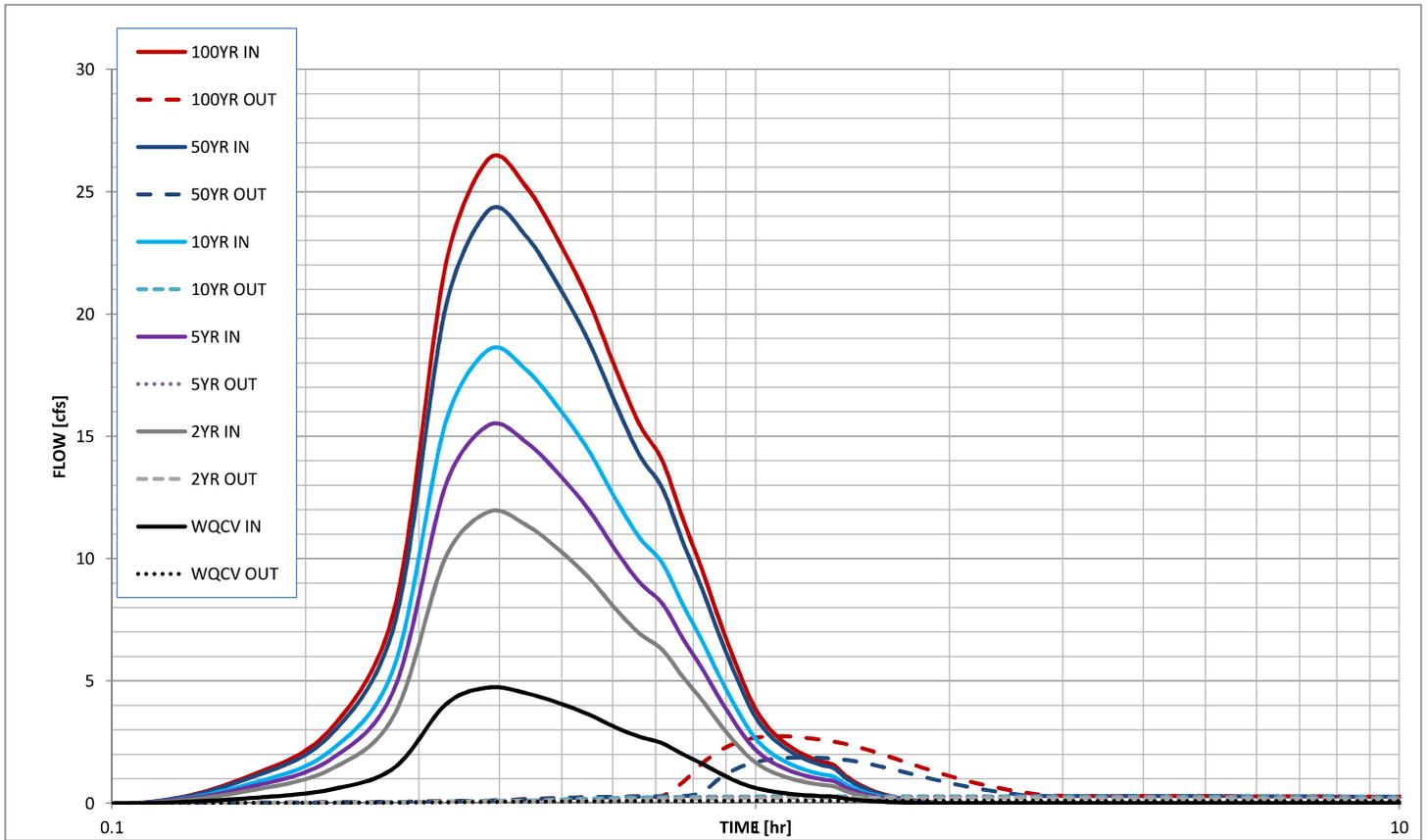
UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override

	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

Stormwater Detention and Infiltration Design Data Sheet



Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.06, November 2016)

Sheet 1 of 4

Designer: NICK JOKERST
 Company: JR ENGINEERING
 Date: January 21, 2020
 Project: TAMLIN ROAD RV STORAGE
 Location: UNINC. EL PASO COUNTY

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, I_b</p> <p>B) Tributary Area's Imperviousness Ratio ($i = I_b / 100$)</p> <p>C) Contributing Watershed Area</p> <p>D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>E) Design Concept (Select EURV when also designing for flood control)</p> <p>F) Design Volume (WQCV) Based on 40-hour Drain Time ($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)) / 12 * Area$)</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume ($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))$)</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p> <p>I) Predominant Watershed NRCS Soil Group</p> <p>J) Excess Urban Runoff Volume (EURV) Design Volume For HSG A: $EURV_A = 1.68 * i^{1.28}$ For HSG B: $EURV_B = 1.36 * i^{1.08}$ For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$</p>	<p>$I_b =$ <u>68.0</u> %</p> <p>$i =$ <u>0.680</u></p> <p>Area = <u>10.220</u> ac</p> <p>$d_6 =$ <u>0.42</u> in</p> <p>Choose One _____ <input type="radio"/> Water Quality Capture Volume (WQCV) <input checked="" type="radio"/> Excess Urban Runoff Volume (EURV)</p> <p>$V_{DESIGN} =$ <u>0.227</u> ac-ft</p> <p>$V_{DESIGN\ OTHER} =$ <u>0.222</u> ac-ft</p> <p>$V_{DESIGN\ USER} =$ _____ ac-ft</p> <p>Choose One _____ <input checked="" type="radio"/> A <input type="radio"/> B <input type="radio"/> C / D</p> <p>EURV = <u>0.873</u> ac-ft</p>
<p>2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.)</p>	<p>L : W = <u>0.8</u> : 1 INCREASE FLOW PATH FOR 2:1 RATIO</p>
<p>3. Basin Side Slopes</p> <p>A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>Z = <u>4.00</u> ft / ft</p>
<p>4. Inlet</p> <p>A) Describe means of providing energy dissipation at concentrated inflow locations:</p>	<p><u>Riprap rundowns down the side slopes of the podn at outfall locations</u> <u>and riprap pads extend into pond bottom.</u></p> <p>_____</p> <p>_____</p> <p>_____</p>

Design Procedure Form: Extended Detention Basin (EDB)

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<p>5. Forebay</p> <p>A) Minimum Forebay Volume ($V_{FMIN} =$ <u>3%</u> of the WQCV)</p> <p>B) Actual Forebay Volume</p> <p>C) Forebay Depth ($D_F =$ <u>18</u> inch maximum)</p> <p>D) Forebay Discharge</p> <p style="margin-left: 20px;">i) Undetained 100-year Peak Discharge</p> <p style="margin-left: 20px;">ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$)</p> <p>E) Forebay Discharge Design</p> <p>F) Discharge Pipe Size (minimum 8-inches)</p> <p>G) Rectangular Notch Width</p>	<p>$V_{FMIN} =$ <u>0.007</u> ac-ft</p> <p>$V_F =$ <u>0.007</u> ac-ft</p> <p>$D_F =$ <u>15.0</u> in</p> <p>$Q_{100} =$ <u>39.90</u> cfs</p> <p>$Q_F =$ <u>0.80</u> cfs</p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input type="radio"/> Berm With Pipe</p> <p><input checked="" type="radio"/> Wall with Rect. Notch</p> <p><input type="radio"/> Wall with V-Notch Weir</p> </div> <p align="right" style="color: blue; font-size: small;">(flow too small for berm w/ pipe)</p> <p>Calculated $D_p =$ <u> </u> in</p> <p>Calculated $W_N =$ <u>5.1</u> in</p>
<p>6. Trickle Channel</p> <p>A) Type of Trickle Channel</p> <p>F) Slope of Trickle Channel</p>	<div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input checked="" type="radio"/> Concrete</p> <p><input type="radio"/> Soft Bottom</p> </div> <p>$S =$ <u>0.0100</u> ft / ft</p>
<p>7. Micropool and Outlet Structure</p> <p>A) Depth of Micropool (2.5-feet minimum)</p> <p>B) Surface Area of Micropool (10 ft² minimum)</p> <p>C) Outlet Type</p> <p>D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)</p> <p>E) Total Outlet Area</p>	<p>$D_M =$ <u>2.5</u> ft</p> <p>$A_M =$ <u>21</u> sq ft</p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input checked="" type="radio"/> Orifice Plate</p> <p><input type="radio"/> Other (Describe):</p> </div> <hr style="border: 0.5px solid black; margin: 5px 0;"/> <hr style="border: 0.5px solid black; margin: 5px 0;"/> <p>$D_{orifice} =$ <u>1.14</u> inches</p> <p>$A_{ot} =$ <u>5.41</u> square inches</p>

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<p>8. Initial Surcharge Volume</p> <p>A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)</p> <p>B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)</p> <p>C) Initial Surcharge Provided Above Micropool</p>	<p>$D_{IS} =$ <u>4</u> in</p> <p>$V_{IS} =$ <u>28.9</u> cu ft</p> <p>$V_s =$ <u>7.0</u> cu ft</p>
<p>9. Trash Rack</p> <p>A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5 * (e^{-0.095D})$</p> <p>B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)</p> <p style="padding-left: 40px;">Other (Y/N): <u>N</u></p> <p>C) Ratio of Total Open Area to Total Area (only for type 'Other')</p> <p>D) Total Water Quality Screen Area (based on screen type)</p> <p>E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)</p> <p>F) Height of Water Quality Screen (H_{TR})</p> <p>G) Width of Water Quality Screen Opening ($W_{opening}$) (Minimum of 12 inches is recommended)</p>	<p>$A_t =$ <u>187</u> square inches</p> <p style="background-color: #e0ffe0; padding: 2px;"><i>S.S. Well Screen with 60% Open Area</i></p> <hr/> <hr/> <p>User Ratio =</p> <p>$A_{total} =$ <u>311</u> sq. in.</p> <p>$H =$ <u>4.54</u> feet</p> <p>$H_{TR} =$ <u>82.48</u> inches</p> <p>$W_{opening} =$ <u>12.0</u> inches</p>

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<p>10. Overflow Embankment</p> <p>A) Describe embankment protection for 100-year and greater overtopping:</p> <p>B) Slope of Overflow Embankment (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>24" Deep Type M Soil Riprap overflow weir w/ 1.36' total depth (design flow depth < 0.36') 60' crest width. 4:1 side slopes</p> <hr/> <p align="center">4.00</p>
<p>11. Vegetation</p>	<p>Choose One</p> <p><input type="radio"/> Irrigated</p> <p><input checked="" type="radio"/> Not Irrigated</p>
<p>12. Access</p> <p>A) Describe Sediment Removal Procedures</p>	<p>Pond will be maintained utilizing skid steer type equipment, trucks (when needed), and hand tools as needed.</p> <hr/> <hr/> <hr/>
<p>Notes:</p> <hr/> <hr/> <hr/>	

Appendix F Drainage Maps

