

# **Falcon Highlands Filing No. 3**

## Master Development Drainage Plan

#### **Owner/Developer**

Challenger Homes 8605 Explorer Drive Ste. 250 Colorado Springs, CO 80920 (719) 598-5192 Contact: Jim Byers

#### Engineer

Atwell, LLC 143 Union Blvd., Suite 700 Lakewood, CO 80228 303-462-1100 Contact: Richard Lyon, PE

Atwell Project Number 21000656

Submitted by: Atwell, LLC

March 18, 2022

SKP-21-004

#### **Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Date

Richard D. Lyon, PE 53921

Seal:

## **Developer's Statement:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Challenger Homes

By:

Title:

Address:

#### **El Paso County Approval:**

Filed in accordance with requirements of the Drainage Criteria Manual, Volumes 1 & 2, El Paso County Engineering Criteria Manual and Land Development Code, as amended.

Jennifer Irvine / County Engineer, Director Conditions:

Date

## **Table of Contents**

| INTRODUCTION  | 1  |
|---|----|
| GENERAL LOCATION AND DESCRIPTION                    | 1  |
| SOILS AND EXISTING SITE CONDITIONS                  | 3  |
| FLOODPLAIN  | 3  |
| DRAINAGE DESIGN CRITERIA                            | 4  |
| EXISTING AND OFFSITE DRAINAGE BASINS                | 4  |
| PROPOSED DRAINAGE BASINS                            | 7  |
| STORM WATER CONVEYANCE AND STORAGE FACILITIES       | 13 |
| WATER QUALITY ENHANCEMENT BEST MANAGEMENT PRACTICES | 15 |
| MAINTENANCE   | 15 |
| FLOODPLAIN MODIFICATIONS                            | 15 |
| CONCLUSION  | 16 |
| REFERENCES  | 17 |

| APPENDIX A | VICINITY MAP                             |
|------------|--|
| APPENDIX B | SOILS SURVEY                             |
| APPENDIX C | FEMA FIRMETTE                            |
| APPENDIX D | HYDROLOGICAL CALCULATIONS                |
| APPENDIX E | HYDRAULIC CALCULATIONS                   |
| APPENDIX F | <b>REFERENCE CALCULATIONS &amp; MAPS</b> |
| APPENDIX G | DRAINAGE MAPS                            |
|            |  |

#### **INTRODUCTION**

This Master Development Drainage Plan Report has been completed for Challenger Homes in order to present an effective storm water management plan for the Falcon Highlands Filing No. 3 development, hereinafter referred to as the Site. This report is intended to guide the development of the site and recommend general drainage concepts that can be implemented as development progresses. Included within this report is a proposed drainage plan for the Site along with reference information for drainage basins and storm water conveyance facilities.

The Site was most recently studied in the *Falcon Highlands Filing No. 2 & 3 Final Drainage Report* by Terra Nova Engineering, Inc., latest revision August 2010 for the development of Filing No. 2. Prior to that Final Drainage Report, a Master Development Drainage Plan report entitled *Falcon Highlands Phase 2, Filing No. 2 & 3 Master Development Drainage Plan and Preliminary Drainage Report* by Terra Nova Engineering, Inc. latest revision September 2005 was developed. This new Master Development Drainage Plan (MDDP) acts as an update of the previous MDDP for the development of Falcon Highlands Filing No. 3 area and basins.

The entire site for Falcon Highlands Filing No. 3 is approximately 125.6 acres and will include a total of approximately 380 units. This is an additional 224 units from the previously approved reports of 156 units which had more quarter-acre and half-acre lots. In addition to greater lot density, roadway alignments have changed to accommodate the new lot layouts with approximately 2.75 miles of right-of-way improvements for paved roadways, curb and gutter, and attached sidewalks with 12.2 acres of open space interior to the subdivision not including tracts for drainage easements, with a dedicated park area central to the subdivision. This compares to the previously approved plans which had approximately 2.5 miles of right-of-way improvements and 7.0 acres of open space interior to the subdivision not including tracts for drainage easements, with no designated park areas. The drainage exhibits and calculations within the appendix present Filing No. 2 and other off-site basins consistent with that of previous reports. The total acreage of Filing No. 2 and 3 is approximately 257.7 acres and a portion of Filing No. 1 area totaling 10.6 acre was included for consistency in presenting tributary areas to existing detention ponds with that of previous studies.

Proposed herein is a network of storm infrastructure, ponds and channels that will meet the relevant criteria for storm water quality and detention, but also allow for aesthetically pleasing landscape and enjoyable green spaces within the PUD community.

#### **GENERAL LOCATION AND DESCRIPTION**

The Site is located within Section 12, Township 13 South, Range 65 West of the Sixth Principal Meridian, County of El Paso, State of Colorado. The Site is bounded by Tamlin Road to the south and east, Birch Hollow Way to the north and Bridal Vail Way to the west for the northern portion of the Site and Antelope Meadow Circle to the north for the western end of the Site. The Site, or Filing No. 3 specifically, is directly adjacent and south of Falcon Highlands Filing No. 2 and adjacent to the east and north of Banning Lewis Ranch subdivisions. The overall area consists of

approximately 125.6 acres that is proposed to be developed into approximately 380 single-family residential units including 24 nearly half-acre lots, 243 eighth-acre lots, 113 smaller (one-twelfth acre) lots. In addition to the single-family residential units and lots, there is proposed development for approximately 37 acres of open space, a well site, and associated roadways and landscaping. Of this 37 acres, approximately 12.2 acres is interior to the development which includes a park area of 3.53 acres. An off-site lift station property subject to potential upgrades to serve the development exists to the south central area of the Site.

The filing is initially planned to be built in three phases to plan for and accommodate water supply by the Metro District for what is anticipated to be approximately 55 water service taps in the initial Phase 1 of the development based on available water and an additional 191 taps following the new well connection, which includes Phases 1 and 2. Future Phases are included within this study to encompass the development of the entire Filing No. 3 as well as off-site, upstream Filing No. 2.

A map displaying the location and delineation of the Falcon Highlands Filings 1, 2, and 3 is shown below.



143 Union Boulevard, Suite 700, Lakewood, CO 80228 Tel: 303.462.1100 Fax: 303.825.7110 www.atwell-group.com

#### SOILS AND EXISTING SITE CONDITIONS

The majority of the Site is currently undeveloped. Of the development within the Site, there are existing dirt roadways and sanitary sewer infrastructure installed per the Preliminary Plan and Development Plan for Falcon Highlands Phase 2, Filing No. 2 & 3 prepared by Terra Nova Engineering, most recent revised date of September 15, 2005. The ALTA survey conducted by Atwell, LLC., shows the existing conditions of Filing No. 3 and adjacent development of Filing No. 2. The Site is nearly 100% existing natural grass vegetation typical of the eastern plains with sparse vegetative cover at its outer limits to the south and southeast. There is an existing regional drainage pond referred to as Pond WU, east of the Site within Falcon Highlands Filing No. 1, 2, and a small portion (Basin D) of Filing No. 3. There are two existing water quality and detention ponds to the south of the Site that were cut in during the construction of Filing No. 2 that were designed for development of both Filings Nos. 2 and 3. The on site slopes range from 0 percent to 10 percent and generally sheet flows from west to east. A Historic Drainage Map is included in Appendix F showing the delineated drainage basins.

The west edge of the Site has existing electric power lines and natural gas main within an existing utility easement. The south side of the Site has a 12" water main and a fiber optic line within what is considered future Tamlin Road right of way.

The Site is made up of mostly loamy sand soils with 100 percent of the soils being Hydrologic Soil Group A. The on-site soils are specified as Blakeland loamy sand (8), Blakeland Complex (8), and Columbine (19) as mapped by the Soil Conservation Service (SCS). The Natural Resources Conservation Service of the United State Department of Agriculture Web Soil Survey has been included in Appendix B for reference.

The western two thirds of the Site are contained within the Sand Creek Basin, the rest within the Falcon Basin.

Per previous drainage studies for the Site and the environmental study for Filing No. 1, there is a high ground water table that should be addressed with the final soils reports for this development. It is recommended that subsurface drains be installed for proposed structures.

Drainage improvements for the Site will include storm sewer infrastructure to capture runoff before street capacities are exceeded and at sump locations as well as channels and swales for potential overflow areas. The existing detention and water quality ponds south of the Site are assessed in this report and are to be constructed according to engineered construction drawings and a Final Drainage Report for Filing No. 3. More specific details regarding the proposed drainage improvements for the Site will be provided in the Final Drainage Report.

## **FLOODPLAIN**

According to the Federal Emergency Management Agency's (FEMA) Flood Insurance Rate Map No. 08041C0561G and 08041C0545G dated December 7, 2018, the vast majority of the Site lies

within Zone X, which is designated as "Areas determined to be outside the 0.2% annual chance flood hazard area", a portion of the site to the east that is proposed open space is located within a Zone A, which is designated as "Areas determined to be within the 0.2% annual chance flood hazard area". The Zone A designation to the east of Tamlin Road is comprised of an Unnamed Tributary that drains to the Black Squirrel Creek No. 2. The FEMA FIRM, Community Panels Nos. 08041 C 0561 G and 08041 C 0545 G (effective December 7,2018) are included in Appendix C for reference.

El Paso County is involved with the Colorado Hazard Mapping Program (CHAMP) because the CWCB delegates its authority to the County to enforce the regulatory floodplain. El Paso County is part of the NFIP (National Flood Insurance Program) which provides assistance to property owners affected by flooding. Inclusion into this program requires that the County enforce floodplain regulations and any changes made to the regulatory maps. Failure to implement these changes could result in the County losing its NFIP status as such a Preliminary FEMA FIRM panel is also included in Appendix C that was remapped as part of CHAMP. Drainage Maps of existing and proposed conditions can be found in Appendix F.

The site falls within the Sand Creek Drainage Basin as well as partially within the Falcon Drainage Basin. The Drainage Basin Planning Study (DBPS) for Sand Creek Drainage Basin by Stantec HDR Dewberry, dated January 2021 and the City of Colorado Springs Sand Creek Basin GIS website show that the nearest creek EF1R9-T1R1 is located approximately 400 feet west of the site, located on the Banning Lewis Ranch Property. The Falcon Drainage Study by Matrix Design Group, dated September 2015, shows no existing or future drainageway improvements within the Site. Drainage from the site will outflow per existing conditions.

## **DRAINAGE DESIGN CRITERIA**

The El Paso County Drainage Criteria Manual and El Paso County Engineering Criteria Manual were used in conjunction with the Mile High Flood District Criteria Manual. The rational method was used for drainage basin less than 100-acres. The 5-year design frequency was used for the minor storm and a 100-year design frequency was used for the major storm in calculating onsite storm facility hydraulics. The one-hour point rainfall depth used for the 5-year storm was 1.50 inches and 2.52 inches for the 100-year event. The City of Colorado Springs IDF Curve (Figure 6-5 of the Drainage Criteria Manual Volume 1) was used for calculating rainfall intensity.

#### **EXISTING AND OFFSITE DRAINAGE BASINS**

The Site has been assessed previously via the *Falcon Highlands Phase 2, Filing No. 2 & 3 Master Development Drainage Plan and Preliminary Drainage Report* developed by Terra Nova Engineering, Inc. latest revision September 2005 as well as a Final Drainage Report for Filing No. 2 & 3 by Terra Nova Engineering, Inc. dated August 2010.

The developments of Falcon Highlands Filing No. 1 & 2 remained consistent with their respective Master Development Drainage Plans and Final Drainage Reports and therefore offsite drainage basin descriptions and delineations provided in this report are based on those previous County

approved reports. The FDR for Filing No. 2 was utilized for off-site basin information within this MDDP. The FDR for Filing No. 2 was completed after the development of Filing No. 1 and therefore utilized the developed conditions for Filing No. 1 as the existing conditions within the Filing No. 2 report. Relevant excerpts from these reports including hydrologic calculations are included in Appendix D.

All off-site drainage basin runoff data and calculations have been updated for current codes and standards consistent with the El Paso County Drainage Criteria Manual. Part of the Site lies within the Sand Creek Basin and the other part within the Falcon Basin. Therefore, the *Sand Creek Drainage Basin Study* and the *Falcon Basin Drainage Basin Planning Study* were both referenced as well as the El Paso County Master Plan approved in May of 2021. Previous studies show the delineation between the two basins. This delineation is shown on the Drainage Basin Map.

The site has been broken down into eight major off-site basins upstream of Filing No. 3, within the existing development of Filing No. 2 and relatively small portions of Filing No. 1. Descriptions of the major basins and their respective sub-basins are below. The off-site basins match the naming convention of the previous Final Drainage Report for Filing No. 2 and 3 to be consistent. A drainage map is in the appendix.

**OS-1 (6.38 ac,**  $Q_5 = 10.7$  cfs,  $Q_{100} = 21.7$  cfs) is an off-site basin located on the northwestern part of Falcon Highlands Filing No. 2 and consists of the rear yard areas of PUD residential zoned lots. The historic drainage pattern sheet flows southwesterly where it is captured by basin OS-5 at **Design Point 7**.

**OS-2 (3.12 ac,**  $Q_5 = 7.8$  cfs,  $Q_{100} = 13.6$  cfs) is an off-site sub-basin within the developed area of Filing No. 1 for quarter-acre lots and is an off-site basin that was included in the MDDP for Filing No. 2. The basin's runoff sheet flows due south in Filing No. 2 and is captured by the roadways and storm system in Filing No. 2 that runs through Filing No. 3, and ultimately outfalls into the existing Pond 1. The basin flows to OS-5 at **Design Point 8**.

**OS-3 (1.14 ac,**  $Q_5 = 3.4$  cfs,  $Q_{100} = 6.0$  cfs) is an off-site basin within Filing No. 1 that includes the developed right-of-way of Rolling Thunder Way. This sub-basin was included in the previous MDDP as an off-site basin and represents a portion of the landscaped right-of-way on the south side of Rolling Thunder Way that sheet flows due south into the developed areas of Filing No. 2 at **Design Point 9** and ultimately into the public storm system shared with Filing No. 3, outfalling to existing Detention Pond 2.

**OS-4 (13.09 ac,**  $Q_5 = 12.3$  cfs,  $Q_{100} = 26.3$  cfs) is an off-site basin located on the southwestern part of Falcon Highlands Filing No. 2 and consists of mostly Tract A and portions of PUD residential zoned lots rear yard areas. The historic drainage pattern sheet flows south where it is captured by basin A at **Design Point 10**.

**OS-5 (59.62 ac,**  $Q_5 = 80.1$  cfs,  $Q_{100} = 160.7$  cfs) is an off-site basin that stretches from the eastern border of basin OS-4 to the eastern edge of Bridal Vail Way within Filing No. 2. The basin is zoned as PUD residential lots of about quarter-acre size. Runoff is carried in the public rights-of-

way where the flow travels south through a series of public curb and gutters, sump inlets and storm infrastructure within Filing No. 2. The flow outfalls into the existing Pond 1 through the public 60" RCP storm pipe that runs through Filing No. 3, the pipe run at **Design Point 11**.

**OS-6 (35.75 ac,**  $Q_5 = 31.9$  cfs,  $Q_{100} = 58.4$  cfs) is off-site basin located between Bridal Vail Way and Antelope Meadows Circle within Filing 2. This basin includes PUD residential zoned lots of half-acre size and contains drainage tracts. The basin is captured by a series of public curb and gutter systems in the rights-of-way where inlets and various size RCPs convey storm water to the end of the cul-de-sac of Wagon Track Drive where the public storm system of Filing No. 2 (**Design Point 12**) connects and daylights to Filing No. 3 within future Antelope Meadows Circle right-ofway.

In existing conditions, note that DP 12 releas the existing diversion ditch, running through I

**OS-7 (6.47 ac,**  $Q_5 = 5.2$  cfs,  $Q_{100} = 18.3$  cfs) is the off-site basis of Basin D of Filing 3. The basin includes PUD residential zoned tots of nan-acte size with **Language addee** of way. The basin runoff is captured in the public right-of-way curb and gutter where it travels south and is released at the road end at **Deign Point 13** where it continues south through Antelope Meadows Circle and then due east through Filing 3's Basin D in the existing access path where it outfalls to Pond WU.

**OS-8 (13.79 ac,**  $Q_5 = 4.6$  cfs,  $Q_{100} = 31.1$  cfs) is an off-site basin located east of Basin D. The basin consists of native grasses and an existing Regional Pond WU. Runoff within the basin flows into the Pond WU (**Design Point 4**) and drains to the northwest side of Highway 24 via the existing private 42" and three 60" RCP outlet pipes to the low point in the offsite grasslined swale at **Design Point 6**.

**Basin A (3.74 ac, Q\_5 = 1.2 cfs, Q\_{100} = 7.7 cfs)** is the basin located southwest of Antelope Meadow Circle, just below basin OS-4, west of Basin B. The majority of the basin is comprised of Tract A and consists of some rear yard runoff from the PUD lots at the western edge of Basin B. The storm water runoff sheet flows south and off-site at **Design Point 1** with the corper existing drainage patterns is not tributary to on-site detention ponds. Expand on existing drainage pattern. Is it sheetflow, and if so to where, or channel/swale, etc?

**Basin B** (38.93 ac,  $Q_5 = 10.2$  cfs,  $Q_{100} = 68.6$  cfs) is located south of Amerope meanow currec, adjacent to basin A. The site is covered in native grasses with limited grad Language added. Us development. Runoff from the site sheet flows southwesterly overland to existing Pond 1 (Design Point 2). The private 42" RCP outlet pipe from the outlet structure of the pond daylights at the grassland swale south of the abandoned future Tamlin Road right-of-way at Design Point 5.

**Basin** C (57.81 ac,  $Q_5 = 16.3$  cfs,  $Q_{100} = 109.7$  cfs) is located adjacent to Basin B and covered in native grasses and weeds. The site has limited grading due to work from a previous development that did not finish. Runoff from the site sheet flows southwesterly overland to an existing diversion ditch that spans from an existing public 24" RCP storm sewer main that daylights within Filing No. 3 south of Wagon Track Way. The diversion ditch flows directly to existing Pond 2 (**Design Point 3**).

**Basin D** (10.54 ac,  $Q_5 = 3.3$  cfs,  $Q_{100} = 22.4$  cfs) is located to the northeast of the Filing and consists of undeveloped area with native grasses. The basin's runoff drains directly to existing Pond WU (Design Point 4).

hydrology spreadsheet

**Basin E (3.14 ac, Q\_s = 1.1 cfs, Q\_{100} = 7.5 cfs)** is the undeveloped, natural landscaped area between Tamlin Road and the existing Pond 1. Runoff from **Summary calcs** point between the future Tamlin Road and Highw were correct, and its associated storm infrastructure is presented updated the intended plan. The 2010 FDR suggested that evidence that this was installed. The existing drain inserted. Iow point of the ditch that surcharges and is directed south through the grassland swale.

**Basin F (3.67 ac,**  $Q_5 = 1.2 \text{ cfs}$ ,  $Q_{100} = 8.0 \text{ cfs}$ **)** is the undeveloped area between Tamlin Road and the existing Detention Pond 2. The runoff from Basin F is directed to the low point in the downstream grasslined swale between the Site and Tamlin Road (**Design Point 6**). This drainage concept and its associated storm infrastructure is presented in the previous master plan and is to remain as the intended plan. The 2010 FDR suggested that a 4'x4' area inlet be constructed but there is no evidence that this was installed. The existing drainage pattern consists of pooling within the local low point of the ditch that surcharges and is directed south through the grassland swale.

**Basin G (8.84 ac, Q\_5 = 6.8 cfs, Q\_{100} = 16.0 cfs)** is the area east of Basin C that is not to be disturbed and remain as open, natural landscape. The runoff from Basin G is collected in a local topographic low point and when overtopping the low point, the runoff continues southeast to the low point in the grasslined swale along Highway 24, **Design Point 6**.

## **PROPOSED DRAINAGE BASINS**

This report has been prepared in accordance with the El Paso County Drainage Criteria Manual and the Mile High Flood District Criteria Manual. The 5-year storm was used as the minor storm event, while the 100-year storm was used as the major event. The one-hour point rainfall depth used for the 5-year storm was 1.50 inches and 2.52 inches for the 100-year event.

Grading design is preliminary or has not begun for much of the site. Due to this, the assumption has been made that the developed conditions drainage patterns presented in the previous MDDP (Terra Nova Engineering, Inc., September 2005) and FDR (Terra Nova Engineering, Inc., August 2010) will remain for all relevant developed areas consistent with the updated design plan and assumed drainage patterns within altered design areas will conform with the design intent. As design and development progress, this should be revisited to confirm the proposed drainage patterns used in this analysis are still applicable. Since the development of Filing No. 2, sketch plans for Filing No. 3 have been altered from the previous MDDP and FDR. Due to the change in the layout of Filing No. 3 from previous design plans and reports, this report serves to provide updated drainage information for the planned development based on new concept grading and drainage patterns. However, as mentioned previously, the drainage concept for the new layout aims to follow previous master plans as closely as possible including basin delineation areas and pond routing in order to keep with previous detention and water quality pond designs.

The overarching premise of the drainage design is to route overland flow from residential lots and units to adjacent rights-of-way where public storm infrastructure will be installed and ultimately convey the storm water to respective ponds to provide water quality treatment as well as flow attenuation and detention. Previous studies designed the existing Ponds 1 and 2 in order to provide full spectrum detention and water quality for Filing Nos. 2 and 3. The analysis within this report provides more defined pond sizing requirements due to the change in layout for Filing No. 3 as well as preliminary locations and sizes for culverts and/or open channels and the public storm system. This idea is intended to be followed for the entirety of the developed site. Basins which are not along the main drainageways within the proposed developed areas or which are expected to flow offsite have been analyzed. There are no engineered channels that exit the Site.

There is a proposed grass-lined, natural ditch to convey stormwater from the rear of B-lot sites within Basin C to existing Pond 2. The design of this swale is to be included in the Final Drainage Report. All Pond outlets daylight to the southern open space of the Site, but are not directed to any formal channels or drainageways.

Preliminary pond sizing and conveyance structures will be analyzed as development progresses to ensure that the final design meets the standards set forward in the El Paso County Engineering Criteria Manual as well as the Mile-High Flood Control Criteria Manual.

As with the existing conditions. the thirteen existing major drainage basins have been delineated into six major basins based on preliminary grading of the Site – basins A through G within the limits of Filing No. 3 and basins OS-1 through OS-6 for off-site basins consistent with the existing conditions for the developed areas of Filing No. 2 and relatively small developed area of Filing No. 1. Of the major basins within the Site, basins B, C, D, and E are consistent with previous reports for Filing Nos. 2 and 3 as those basins are not to be altered during the development of Filing No. 3. Basins B and C are the basins in which development of Filing No. 3 is to occur. Subbasin analysis within these major basins will be provided as a part of the hydrology calculations in the Preliminary and Final Drainage Reports for design of proposed storm infrastructure and channels on the Site.

The rational method was used to estimate runoff rates for the proposed development and are in accordance to El Paso County Drainage Criteria Manual and any references within the County criteria to the City of Colorado Springs Drainage Criteria Manuals, volumes 1, 2, and 3. These calculations can be found in Appendix D.

**OS-1 (6.38 ac,**  $Q_5 = 10.7$  cfs,  $Q_{100} = 21.7$  cfs) is an off-site basin located on the northwestern part of Falcon Highlands Filing No. 2 and consists of the rear yard areas of PUD residential zoned lots. The historic drainage pattern sheet flows southwesterly where it is captured by basin OS-5 at **Design Point 7**.

**OS-2 (3.12 ac,**  $Q_5 = 7.8$  cfs,  $Q_{100} = 13.6$  cfs) is an off-site sub-basin within the developed area of Filing No. 1 for quarter-acre lots and is an off-site basin that was included in the MDDP for Filing No. 2. The basin's runoff sheet flows due south in Filing No. 2 and is captured by the roadways

and storm system in Filing No. 2 that runs through Filing No. 3, and ultimately outfalls into the existing Pond 1. The basin flows to OS-5 at **Design Point 8**.

**OS-3 (1.14 ac,**  $Q_5 = 3.4$  cfs,  $Q_{100} = 6.0$  cfs) is an off-site basin within Filing No. 1 that includes the developed right-of-way of Rolling Thunder Way. This sub-basin was included in the previous MDDP as an off-site basin and represents a portion of the landscaped right-of-way on the south side of Rolling Thunder Way that sheet flows due south into the developed areas of Filing No. 2 at **Design Point 9** and ultimately into the public storm system shared with Filing No. 3, outfalling to existing Detention Pond 2.

**OS-4 (13.09 ac,**  $Q_5 = 14.9$  cfs,  $Q_{100} = 31.7$  cfs) is an off-site basin located on the southwestern part of Falcon Highlands Filing No. 2 and consists of mostly Tract A and portions of PUD residential zoned lots rear yard areas. The historic drainage pattern sheet flows south where it is captured by basin A at **Design Point 10**.

**OS-5 (59.62 ac,**  $Q_5 = 80.1$  cfs,  $Q_{100} = 160.7$  cfs) is an off-site basin that stretches from the eastern border of basin OS-4 to the eastern edge of Bridal Vail Way within Filing No. 2. The basin is zoned as PUD residential lots of about quarter-acre size. Runoff is carried in the public rights-ofway where the flow travels south through a series of public curb and gutters, sump inlets and storm infrastructure within Filing No. 2. The flow outfalls into the existing Pond 1 through the public 60" RCP storm pipe that runs through Filing No. 3, the pipe run at **Design Point 11**.

**OS-6 (35.75 ac,**  $Q_5 = 31.9$  cfs,  $Q_{100} = 58.4$  cfs) is offand Antelope Meadows Circle within Filing 2. This b half-acre size and contains drainage tracts. The basin gutter systems in the rights-of-way where inlets and v end of the cul-de-sac of Wagon Track Drive where the public s **Language added specifying Point 12)** connects and daylights to Filing No. 3 within future way. **Language added specifying conditions for Filing No. 3 prior to and after Phase 2.** 

**OS-7 (6.47 ac,**  $Q_5 = 5.2$  **cfs,**  $Q_{100} = 18.3$  **cfs)** is the off-site basin located within Filing 2, just north of Basin D of Filing 3. The basin includes PUD residential zoned lots of half-acre size with right of way. The basin runoff is captured in the public right-of-way curb and gutter where it travels south and is released at the road end at **Deign Point 13** wh Meadows Circle and across a cross pan adjacent to Basin I in a proposed public storm system that outfalls to Pond 2.

**OS-8 (13.79 ac,**  $Q_5 = 4.6$  cfs,  $Q_{100} = 31.1$  cfs) is an off-site basin locate Language added. basin consists of native grasses and an existing Regional Pond WU. Runoff within the basin flows into the Pond WU (Design Point 4) and drains to the northwest side of Highway 24 via the existing private 42" and three 60" RCP outlet pipes to the low poi Indicate roadside ditch will be analyzed for developed flows with PDR & FDR's.

**Basin A (3.74 ac, Q\_5 = 1.7 cfs, Q\_{100} = 8.2 cfs)** is the western most basin Language added. s of the open space Tract A and some small portions of the rear lots of the one-eighth acre single family

lots. The ranoff from Basin A Language added. site and onto the adjacent open space. Runoff reductions via grass buffers and natural landscape to Design Point 1 allow for no required detention of this basin.

**Basin B (40.37 ac,**  $Q_5 = 73.5$  **cfs,**  $Q_{100} = 176.7$  **cfs)** is the southwestern portion of Filing No. 3 consisting of the area south of Antelope Meadows Circle and west of Basin C. Basin B is laid out with several 50' public right of way roadways with curb and gutter, detached pedestrian sidewalk, and landscape areas. The PUD residential developments within Basin B are shown as 123 lots, varying from 50'x110' to 60'x110'. The roadways consist of high points at the eastern and western edges and low points central to the basin with a drainage Tract that flows north to south. The general drainage pattern is due south to the existing Pond 1. Within the roadways is a public storm system and a series of sump inlets at the low points to capture surface runoff and convey storm water to forebays within the existing Pond 1 (Design Point 2). A relatively small portion of the northern half-acre lots east of Bridal Vail Way are included in Basin B where a low point in the western cul-de-sac is to have a sump inlet for surface runoff collection that connects to the existing Pond 1 storm system.

**Basin** C (57.12 ac,  $Q_5 = 64.8$  cfs,  $Q_{100} = 170.6$  cfs) is the more central to east basin within Filing No. 3 that is tributary to Pond 2. The basin includes the majority of the half-acre PUD residential lots in the northern area south of Filing No. 2 and east of Bridal Vail Way, and stretches south to the very south and east edges of the Filing with the exception of Pond WU areas and Basin D. Basin C areas south of Antelope Meadows Circle consists of approximately 248 lots with some lots of 35'x110' and others of 50'x110' and 60'x110' in size. A public storm system is to be designed within the roadways to convey storm water from the off-site Basin OS-5 and Basin OS-6 within Filing No. 2 and the runoff from the entire Basin C areas. The storm system is to outfall into the existing Pond 2 (Design Point 3).

**Basin D** (7.96 ac,  $Q_5 = 9.8$  cfs,  $Q_{100} = 24.8$  cfs) is the northeast area of the Filing for one-eighth acre PUD residential lots at the extension of Birch Hollow Way. The basin is tributary to existing Pond WU which is an existing and recently improved pond under the jurisdiction of El Paso County. The basin depicted to the provident of the provident of

**Basin E** (3.14 ac,  $Q_5 = 1.1$  cfs,  $Q_{100} = 7.5$  cfs) is the undeveloped, natural landscaped area between. Tamlin Road and existing Detention Pond 1. Runoff from Basin E is directed by **Language added**. a low point where an inline inlet captures flow and direct it south offsit release rate of the existing pond. This drainage concept and its associa presented in the previous master plan and is to remain as the intende offsite is accounted for in existing Pond 1. The basin drains to Design Po at the southwest corner of the Filing.

**Basin F (5.50 ac,**  $Q_5 = 2.2 \text{ cfs}$ ,  $Q_{100} = 12.5 \text{ cfs}$ **)** is the area south of Basin C that is not to be disturbed and remain as open, natural landscape. The runoff from Basin F sheet flows downstream and is undetained. There is no increase runoff and the drainage pattern remains that of its existing flow

path in the channel south to the box culverts at Highway 24. The flow directed offsite is accounted for in existing Pond 1. The basin drains to Design Point 6 and is directed offsite through Tract K.

**Basin G (8.80 ac, Q\_5 = 6.8 cfs, Q\_{100} = 16.0 cfs)** is an open, undeveloped area east of Basin C within Tract Z that is to remain undisturbed. The basin drains southeast to the ditch between dedicated future Tamlin Road and Highway 24. The basin drains to Design Point 7 which and is dir offsite due southwest.

**Existing Pond 1:** The existing Detention Pond 1 (Design Point 2) was designed as a 17 acre-foot pond for water quality and detention basin for the 100-year storm event according to the 2010 FDR. The basins that are tributary to Pond 1 are Offsite Basins OS-1, OS-2, and OS-5 and On-site Basin B. The undetained storm water runoff from Basin A is accounted for within the pond as disturbance will occur within that basin.

Existing Pond 1 was sized using Haestad's Pondpack program in the previous study by Terra Nova, dated September of 2010. The pond will need to have more detail taken into account at the time of the Final Drainage Report when runoff calculations are finalized and the required pond volumes for WQCV (Water Quality Capture Volume), EURV (Excess Urban Runoff Volume), and 100-year detention and release rates are determined. The Existing Pond will be assessed for final conditions to determine if earthwork for volume adjustments is required and if retrofitting of existing pond infrastructure is required including the outlet structure, orifice plate, micropool, and spillway. The existing infrastructure will be as-built to verify elevations and sizes. The required WQCV, EURV, and 100-year detention volumes are listed in a table in the next section of this report.

An existing 42" RCP outlet pipe from the existing outlet structure discharges flow from existing Pond 1 due south under the future dedicated right-of-way of Tamlin Road (that has been abandoned) onto the adjacent undeveloped Banning Lewis Ranch property. Rip rap protection was to be constructed at the end of the outlet pipe at the time of final construction and is to be inspected for the Final Drainage Report as-built conditions. According to the previous study from 2010, "the released runoff drains south across a defined broad open grassland swale to Highway 24. A 72' wide emergency spillway set at 6817.00 will pass the complete 100-year developed flow safely over the proposed riprap lined weir." Downstream drainage patterns mentioned in the previous report are to be assessed in the Final Drainage Report. The previous FDR and Construction Drawings detailed an outlet structure and orifice plates to meet the required release rates of 40 hours for WQCV, approximately 68 hours for EURV, and 72 hours for the 100-year storm event. It is anticipated that new outlet structures with orifice plate, a micropool, and trickle channel will be required to be designed in order to satisfy release rate requirements for the proposed developed conditions. Some earthwork may be required to provide permanent stabilization of more defined contouring within the pond to ensure that runoff reaches the outlet structure. A maintenance path exists that accesses the outlet structure and future forebay areas but it may require alterations to meet current criteria for slopes and width.

Correcte

Preliminary calculations for the adjusted site layout can be found in Appendix E of this report including effective imperviousness calculations using the UD-BMP IRF calculator and WQCV, EURV, and 100-year detention calculations using the UD-Detention spreadsheet by the Mile High Flood District.

**Existing Pond 2:** The existing Detention Pond 2 (Design Point 3) was designed as a 7 acre-foot pond for water quality and detention basin for the 100-year storm event according to the 2010 FDR. The basins that are tributary to the existing pond are Offsite Basins OS-3 and OS-6 and Onsite Basin C.

Existing Pond 2 was sized using Haestad's Pondpack program in the previous study by Terra Nova, dated September of 2010. The pond will need to have more detail taken into account at the time of the Final Drainage Report when runoff calculations are finalized and the required pond volumes for WQCV, EURV, and 100-year detention and release rates are determined. The Existing Pond will be assessed for final conditions to determine if earthwork for volume adjustments is required and if retrofitting of existing pond infrastructure is required including the outlet structure, orifice plate, micropool, and spillway. The existing infrastructure will be as-built to verify elevations and sizes. The required WQCV, EURV, and 100-year detention volumes are listed in a table in the next section of this report.

The 2010 FDR proposed an 42" RCP outlet pipe from the existing outlet structure to discharge flow from existing Pond 2 due south under the future dedicated right-of-way of Tamlin Road onto the adjacent undeveloped Banning Lewis Ranch property. It was proposed that rip rap protection will need to be provided at the end of the outlet pipe at the time of final construction and this is to be verified for the Final Drainage Report. From here the runoff drains south to an existing channel and then is directed to an existing Highway 24 culvert. These proposed offsite improvements are to be assessed further in the Final Drainage Report. Current survey field data suggests that these improvements were not constructed as a part of Filing No. 2 and are to be verified in further studies. According to the 2010 study, "a 50' wide emergency spillway set at 6817.50 will pass the complete 100-year developed flow." Impervious factors and extended detention basin calculations for this pond can be found in Appendix E of this report. The previous FDR and Construction Drawings detailed an outlet structure and orifice plates to meet the required release rates of 40 hours for WQCV, approximately 68 hours for EURV, and 72 hours for the 100-year storm event. It is anticipated that new outlet structures with orifice plate, a micropool, and trickle channel will be required to be designed in order to satisfy release rate requirements for the proposed developed conditions. Some earthwork may be required to provide permanent stabilization of more defined contouring within the pond to ensure that runoff reaches the outlet structure. Maintenance paths are to be established for access to future forebays and the outlet structure.

**Existing Pond WU:** The existing Detention Pond WU is a recently improved storm water quality and detention facility that is owned and maintained by El Paso County. The previous MDDP called for developed flow conditions to drain to this existing facility and it was accounted for in the recent improvements by Galloway and Company. The new layout has more density and effective imperviousness in Basin D of Filing No. 3 but the developed conditions will route Offsite Basin

OS-7 due south in Antelope Meadows Circle instead of turning into Filing No. 3 at Basin D to drain directly to Pond WU. As a result, there is less runoff to Pond WU in the proposed plan, therefore there is no increase to water quality capture volume or 100-year detention volume from the previous study or from recent improvements. A table within Appendix E compares the developed conditions for the current proposed conditions to that of the 2010 FDR.

It may be warranted that pond infrastructure will need to be constructed within Pond WU to meet current criteria, particularly a concrete trickle channel. This is to be assessed in the Preliminary and Final Drainage Reports.

Due to the revised layout and grading of the site, approximately 31 acres of area that was tributary to the Falcon Basin will now be tributary to the Sand Creek Basin. This cross-basin transfer should not cause any downstream problems as detention of the additional runoff and release rates conforming to drainage standards will be implemented.

The Developed Condition's runoff flows are kept at or below historic flows by way of detention within existing Pond WU, existing Detention Pond 1, and existing Detention Pond 2; all of which are designed for water quality capture and to release storm water at rates conforming to the El Paso County Drainage Criteria Manual. It is anticipated that there will be no negative affects to downstream areas due to developed drainage conditions.

#### **STORM WATER CONVEYANCE AND STORAGE FACILITIES**

The proposed on-site conveyance facilities will consist of a combination of storm pipe, swales/channels, curb/gutter, and inlets. Proposed drainage patterns will generally follow the historic drainage patterns outlined in the previous sections of this report, including previous master plans and reports for upstream filings. Within the proposed roadway network, stormwater runoff will be conveyed overland via surface flow of streets in the curb and gutter until street capacities have been exceeded or where storm sewer inlets have been designed. At sump locations, inlets will be sized to collect 100-year flows. Runoff entering the inlets will be conveyed within the storm sewer system to detention and water quality ponds. The general onsite drainage paths and patterns were previously discussed in the Proposed Drainage Basins section of this report.

The existing pond outfalls are routed to the Sand Creek Basin. These outfalls have been preliminarily sized based on standard pond release rates required by the MHFD criteria. Release rates will be further evaluated during the preliminary and final drainage studies. The sizing of the facilities will be assessed in the Preliminary and Final Drainage Reports.

Detention and Water Quality Ponds for the Site have been preliminarily designed based on previous MDDP and FDR studies for off-site basins and for Filing No. 3 with the methods outlined in the MHFD Urban Storm Drainage Criteria Manual Volumes 1, 2 and 3 along with the MHFD MHFD-Detention\_v4.00. The ponds are designed to detain the EURV and the 100-year Detention Volume.

## existing evised.

The existing ponds have outlet structures that contain 2.5-ft deep micro-pools. EURV release rates will be controlled by an orifice plate designed to meet the MHFD release rate criteria. The 100-year storage volume is routed through a grate and restricted by a plate that was sized to limit the release rate to the allowable release rate.

The existing ponds have been previously designed using the runoff data from the Final Drainage Reports from Filing No. 1 and Filing No. 2 as well as assumed runoff data for Filing No. 3 via the most recent FDR in August of 2010 for the development of Filing No. 2. The existing infrastructure is to be assessed for final conditions within a Final Drainage Report to determine if retrofits are required.

This report provides more concise drainage calculations for Filing No. 3, consistent with the new layout and grading concept and thus for the tributary areas to Ponds 1 and 2. The MHFD UD-Detention calculator was used to determine existing Pond 1 and Pond 2's required WQCV, EURV, the 100-year detention volumes. The ponds are to be designed and updated to function as full-spectrum detention facilities as needed. These designs are to be presented in the Preliminary and Final Drainage Reports.

A summary of the required pond volumes is presented in the table below.

|        | Extended Detention Pond Volumes |                           |                              |                 |  |  |  |  |  |  |  |  |  |  |  |
|--------|---------------------------------|---------------------------|------------------------------|-----------------|--|--|--|--|--|--|--|--|--|--|--|
|        | Zone 1<br>(WQCV)                | Zone 2 (EURV<br>- Zone 1) | Zone 3 (100-<br>Year - Zones | Total<br>Volume |  |  |  |  |  |  |  |  |  |  |  |
|        |                                 |                           | 1 & 2)                       | Required        |  |  |  |  |  |  |  |  |  |  |  |
| Pond 1 | 1.855 ac-ft                     | 3.377 ac-ft               | 3.731 ac-ft                  | 8.962 ac-ft     |  |  |  |  |  |  |  |  |  |  |  |
| Pond 2 | 1.393 ac-ft                     | 2.235 ac-ft               | 2.824 ac-ft                  | 6.452 ac-ft     |  |  |  |  |  |  |  |  |  |  |  |

This MDDP consists of the most up to date calculations for percent imperviousness for the tributary areas to existing Ponds 1 and 2 and therefore has new, adjusted volume requirements compared to that of previous reports.

The existing Pond 1 was calculated to require 8.985 ac-ft and was sized for a 17 ac-ft pond using Haestad's Pondpack Program and HEC modeling according to the 2010 report. The as-built conditions for the constructed pond have the spillway weir at an elevation of 6416.5 and top of pond berm at 6817, yielding a total pond size of approximately 15.77 ac-ft. A Final Drainage Report for Filing No. 3 will require analysis of Pond 1's infrastructure to adjust to final hydrology and hydraulic conditions tributary to the pond for the new, more dense site layout.

Our calculations require 6.452 ac-ft within existing Pond 2 and the original report sized the pond for 9.43 ac-ft according to the Haestad's Pondpack Program and HEC modeling. The as-built conditions for the constructed pond have the spillway weir at an elevation of 6816.5 and top of pond berm at 6817.5 yielding a total pond size of approximately 10.45. A Final Drainage Report for Filing No. 3 will require analysis of Pond 2's size and infrastructure to adjust to final hydrology and hydraulic conditions tributary to the pond.

A Final Drainage Report for Filing No. 3 will require analysis of both existing ponds for size and infrastructure to adjust to final hydrology and hydraulic conditions tributary to the respective facilities.

Existing Regional Detention Pond WU was designed and built as a part of Filing No. 2 and accounted for the future development within Basin D of Filing No. 3 according to the previous MDDP and FDR. Total runoff from Basin D is reduced as a result of the new layout as shown in the hydrology tabulations. It is anticipated that a concrete trickle channel is to be installed within this regional pond and no other improvements are required.

#### WATER QUALITY ENHANCEMENT BEST MANAGEMENT PRACTICES

The existing detention ponds discussed in the previous section have been designed in accordance with the MHFD Urban Storm Drainage Criteria Manual Volumes 1, 2 and 3 as well as the El Paso County and City of Colorado Springs Drainage Criteria Manuals. The ponds are designed to provide WQCV and detain the EURV and the 100-year Detention Volume. Runoff from the upstream tributary areas will be conveyed to the ponds via storm sewer and designed channels as emergency overflow routes directed to the ponds.

Non-structural Best Management Practices that will be incorporated into the project are anticipated to include grass swales. Water quality is provided via side yard grass swales between lots in developed areas throughout the subdivision. It is provided for basins that drain directly offsite and are not tributary to the ponds by way of grass-lined swales, and by having minimal grading with no developed imperviousness in these areas as either open space or permanently seeded and landscaped rear yard areas.

Structural Best Management Practices that are incorporated in the Site design include storm infrastructure within the extended detention basins such as outlet structures and spillways.

#### **MAINTENANCE**

Maintenance of the existing Detention Ponds 1 and 2 shall be by the Falcon Highlands Metro District along with the outlet works for the pond. Public Pond WU will be maintained by El Paso County along with the channel on the east side of the property. The proposed storm sewer system in the internal streets will be owned and maintained by El Paso County once approved.

#### **FLOODPLAIN MODIFICATIONS**

A portion of the Site that is not to be developed is within a FEMA Flood Zone AE, within Basin G. Basin G is an open natural landscaped area not to be disturbed therefore there will be no modifications to the 100-year floodplain, nor will the development be impacted by said floodplain.

#### **CONCLUSION**

This Master Development Drainage Plan report covers the conceptual storm water management plan for the Falcon Highlands Filing No. 3 development. Detailed design will be required to develop individual portions of the site, but this document will provide guidance so that the drainage infrastructure constructed throughout the Falcon Highlands Filing No. 3 development will function efficiently and effectively. This report follows all standard criteria set forth by the El Paso County Drainage Criteria Manual, El Paso County Engineering Criteria Manual, the City of Colorado Springs Drainage Criteria Manuals Volumes 1, 2, and 3, and the Mile High Flood District Urban Storm Drainage Criteria Manual, with no requested variances. Downstream drainage facilities will not be negatively affected, as existing drainage patterns and allowable release rates are planned to be maintained. The Drainage Basin Planning Studies for both Sand Creek and Falcon have no existing or future plans within The Site. Furthermore, Pond WU will remain undisturbed and has the capacity for the basin that is to be developed in Filing No. 3 that is tributary to it.

#### **REFERENCES**

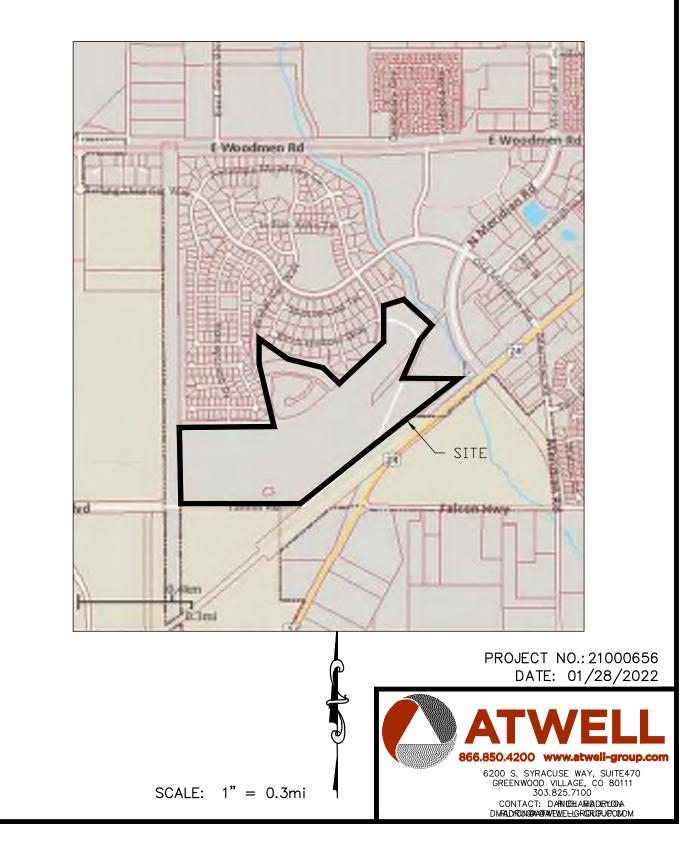
- 1) Urban Storm Drainage Criteria Manuals; Mile High Flood District; latest edition
- El Paso County Engineering Criteria Manual (ECM), latest revision 6 dated December 13, 2016
- 3) El Paso County Drainage Criteria Manual (DCM), latest revision October 31, 2018
- City of Colorado Springs Drainage Criteria Manuals, Volumes 1, 2, and 3, latest revision May 2014
- 5) Flood Insurance Rate Map of El Paso County Colorado, Federal Emergency Management Agency, Flood Insurance Rate Map No. 08041C0561G and 08041C0545G dated December 7, 2018.
- Hydrologic Soil Group El Paso County, Colorado, Web Soil Survey, National Cooperative Soils Survey, May 21, 2021
- 7) *Falcon Highlands Filing No. 2 & 3 Final Drainage Report* by Terra Nova Engineering, Inc., latest revision August 2010.
- Falcon Highlands Phase 2, Filing No. 2 & 3 Master Development Drainage Plan and Preliminary Drainage Report by Terra Nova Engineering, Inc. latest revision September 2005
- 9) URS Section for Regional Detention Pond WU, developed by Galloway & Company
- 10) Sand Creek DBPS, developed by Stantec, HDR, and Dewberry dated January 2021
- 11) Falcon DBPS, developed by Matrix Design Group dated September 2015

VICINITY MAP

**APPENDIX A** 

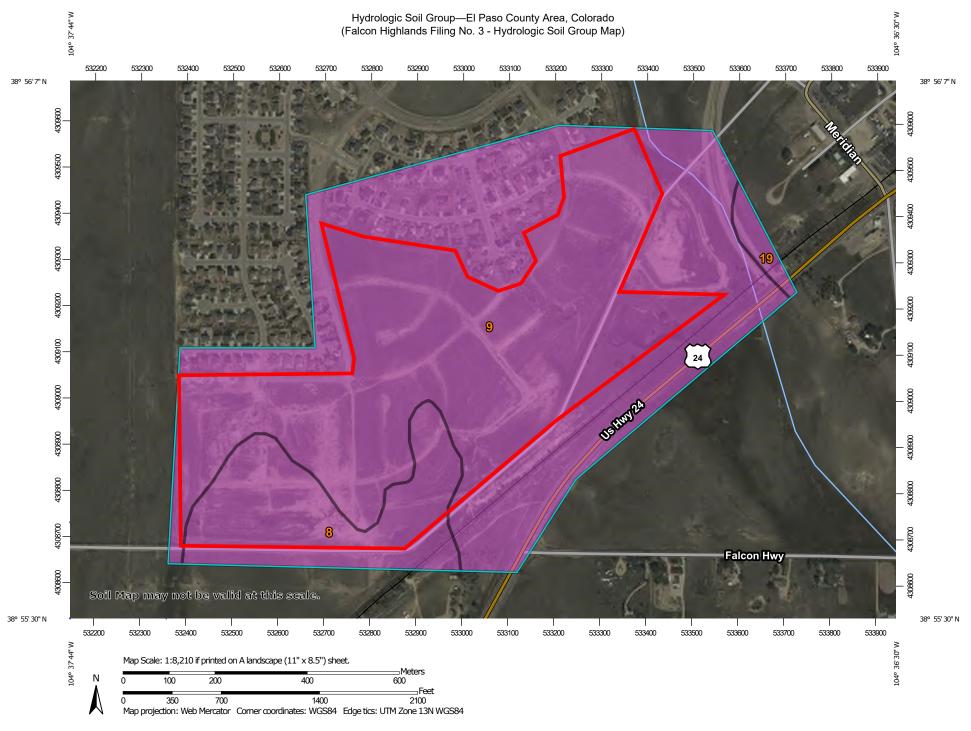
# Falcon Highlands - Filing No. 3

A PART OF SECTION 12, TOWNSHIP 13 SOUTH, RANGE 65 WEST OF THE SIXTH PRINCIPAL MERIDIAN, COUNTY OF EL PASO, STATE OF COLORADO



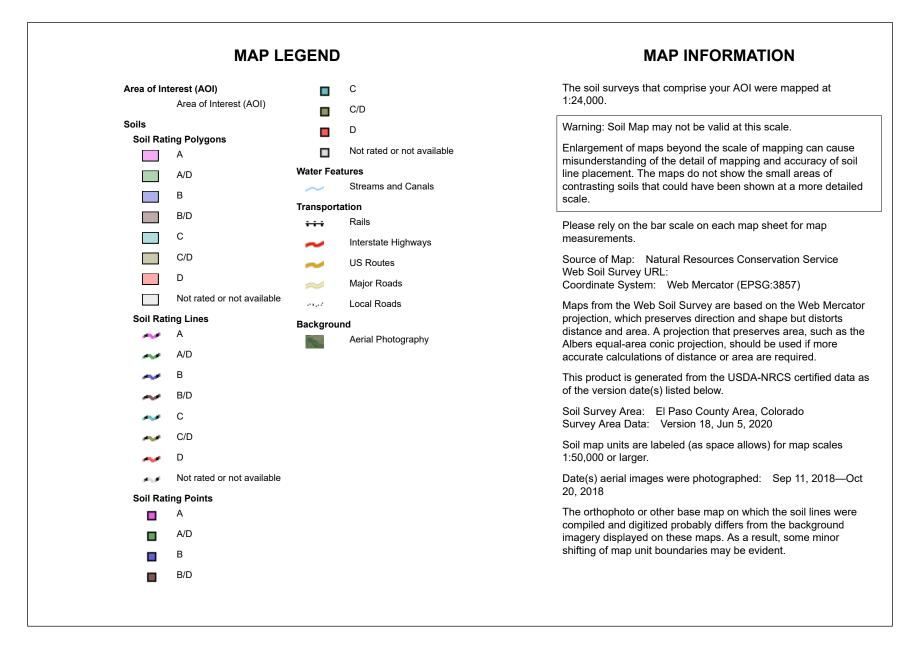
**APPENDIX B** 

**SOILS SURVEY** 



USDA Natural Resources

**Conservation Service** 



## Hydrologic Soil Group

| Map unit symbol          | Map unit name  | Rating | Acres in AOI | Percent of AOI |
|--------------------------|--|--------|--------------|----------------|
| 8                        | Blakeland loamy sand, 1<br>to 9 percent slopes             | A      | 31.0         | 14.2%          |
| 9                        | Blakeland-Fluvaquentic<br>Haplaquolls                      | A      | 184.2        | 84.5%          |
| 19                       | Columbine gravelly<br>sandy loam, 0 to 3<br>percent slopes | A      | 2.8          | 1.3%           |
| Totals for Area of Inter | rest   |        | 218.0        | 100.0%         |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



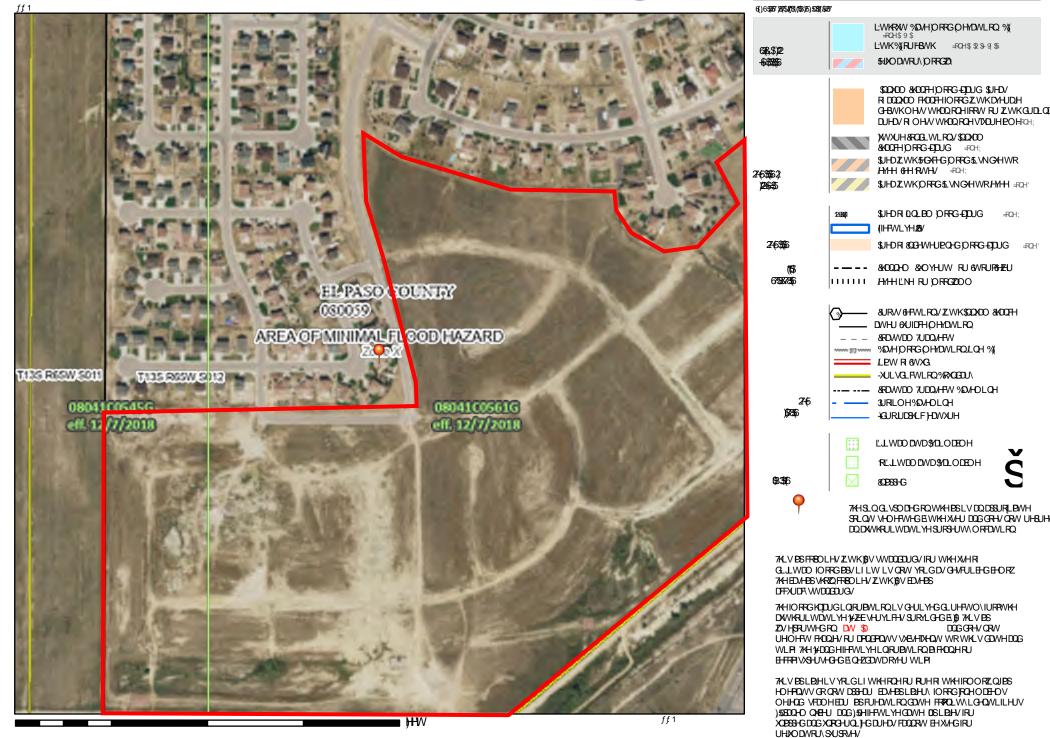
**APPENDIX C** 

**FEMA FIRMETTE** 

# DWLRODO ØRRGEDUGDHU )51WWH



## hhog



% DM-BS 865 DWL RODO DG 20WKRL BHU\ DWD UHUHMHG 2FWREHU

# NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202 1315 East-West Highway

Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channe distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

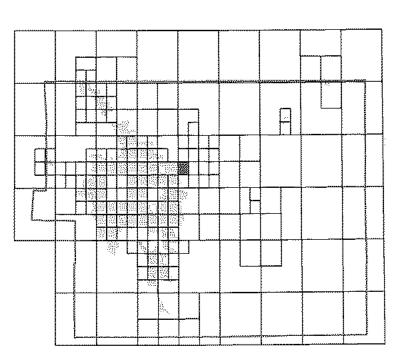
If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

> El Paso County Vertical Datum Offset Table Vertical Datum

Flooding Source Offset (ft) REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY

FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

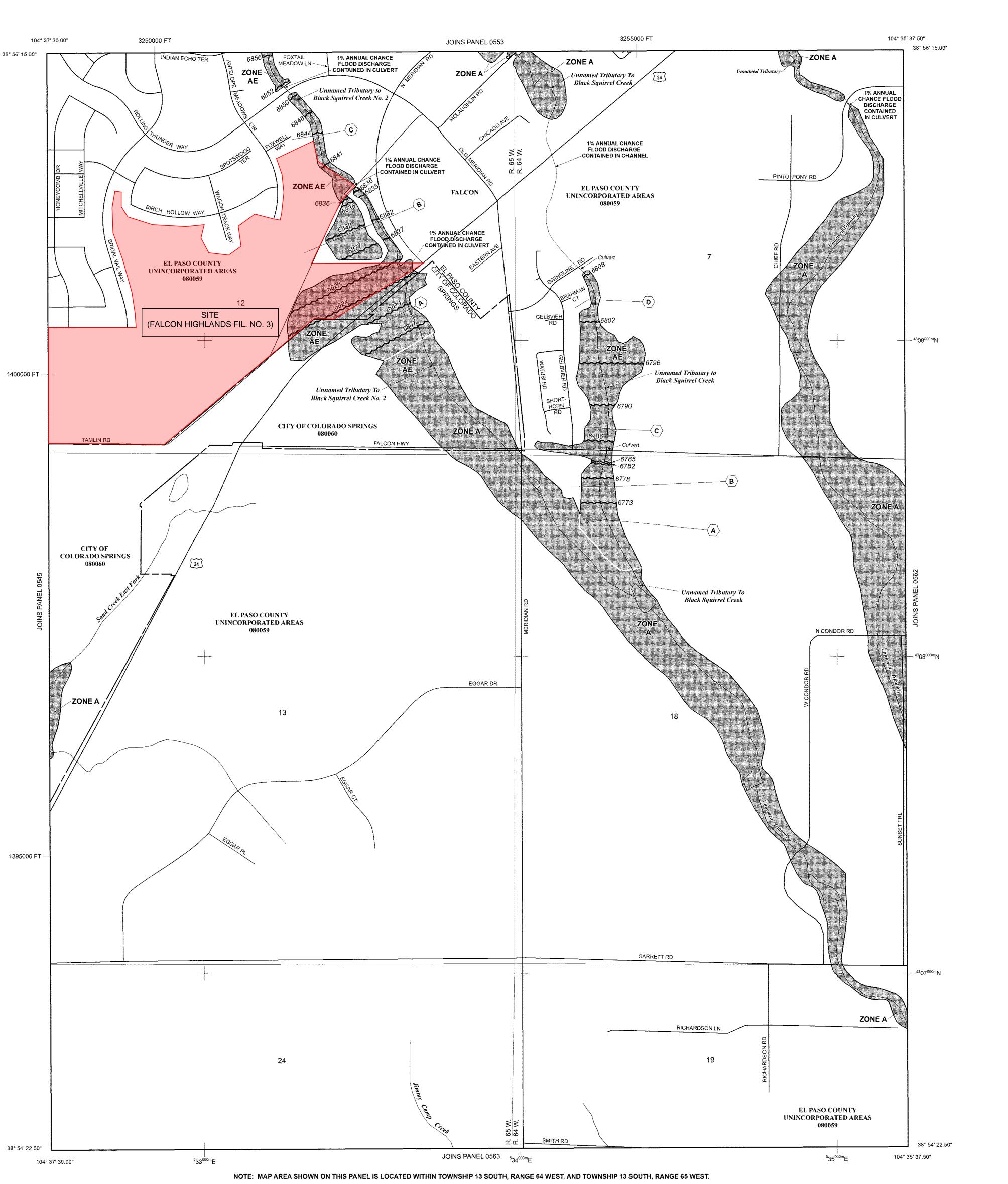
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



|   | INUNDATION BY  | LEGEND<br>D HAZARD AREAS (SFHAS) SUBJECT TO<br>(THE 1% ANNUAL CHANCE FLOOD   |
|---|--|--|
| that has a 1%<br>Hazard Area<br>Special Flood | 6 chance of being equ<br>is the area subject t<br>Hazard include Zones | year flood), also known as the base flood, is the flood<br>Jaled or exceeded in any given year. The Special Flood<br>to flooding by the 1% annual chance flood. Areas of<br>A, AE, AH, AO, AR, A99, V, and VE. The Base Flood<br>tion of the 1% annual chance flood. |
| ZONE A<br>ZONE AE                             | No Base Flood Eleva<br>Base Flood Elevation                            | is determined.   |
| ZONE AH                                       | Elevations determine   | to 3 feet (usually areas of ponding); Base Flood<br>ed.<br>3 feet (usually sheet flow on sloping terrain); average   |
|   | depths determined.<br>determined.                                      | For areas of alluvial fan flooding, velocities also  |
| ZONE AR                                       | flood by a flood con<br>AR indicates that t                            | d Area Formerly protected from the 1% annual chance<br>htrol system that was subsequently decertified. Zone<br>he former flood control system is being restored to<br>rom the 1% annual chance or greater flood.   |
| ZONE A99                                      | Area to be protecte<br>protection system                               | on the 1-% annual chance of greater hood.<br>ed from 1% annual chance flood by a Federal flood<br>under construction; no Base Flood Elevations   |
| ZONE V  | determined.<br>Coastal flood zone<br>Elevations determine              | with velocity hazard (wave action); no Base Flood<br>ed.   |
| ZONE VE                                       | Coastal flood zone<br>Elevations determine                             | e with velocity hazard (wave action); Base Flood<br>ed.  |
| The floodway                                  | FLOODWAY ARE   | AS IN ZONE AE<br>tream plus any adjacent floodplain areas that must be   |
| kept free of                                  |  | the 1% annual chance flood can be carried without  |
| 20115 2                                       | OTHER FLOOD  |  |
| ZONE X  | average depths of  | al chance flood; areas of 1% annual chance flood with<br>less than 1 foot or with drainage areas less than 1<br>leas protected by levees from 1% annual chance flood.  |
|   | OTHER AREAS  |  |
| ZONE X<br>ZONE D                              |  | be outside the 0.2% annual chance floodplain.<br>hazards are undetermined, but possible.   |
|   | COASTAL BARRI  | ER RESOURCES SYSTEM (CBRS) AREAS   |
|   | OTHERWISE PR   | OTECTED AREAS (OPAs)   |
| CBRS areas a                                  |  | located within or adjacent to Special Flood Hazard Areas.<br>ain boundary  |
|   | Floodw   | ay boundary<br>Boundary  |
| •••••   |  | nd OPA boundary  |
|   |  | ary dividing Special Flood Hazard Areas of different Base<br>Elevations, flood depths or flood velocities.   |
| 513<br>(EL 987                                | ') Base Fi   | ood Elevation line and value; elevation in feet*<br>ood Elevation value where uniform within zone;<br>m in feet*   |
| * Referenced                                  | *****  | n Vertical Datum of 1988 (NAVD 88)   |
| A>  | → → Cross s  | ection line  |
| <b>23</b>                                     | (23) Transed   | ct line<br>phic coordinates referenced to the North American   |
| 32° 22' 30                                    | .00" Datum   | of 1983 (NAD 83)<br>neter Universal Transverse Mercator grid ticks,  |
| 6000000                                       | zone 13  | •  |
|   | system   | , central zone (FIPSZONE 0502),<br>t Conformal Conic Projection  |
| DX5510  |  | mark (see explanation in Notes to Users section of<br>RM panel)  |
| ● M1.5  | 5 River M  | lie  |
|   | Refer to I   | MAP REPOSITORIES<br>Map Repositories list on Map Index   |
|   |  | CTIVE DATE OF COUNTYWIDE<br>OD INSURANCE RATE MAP<br>MARCH 17, 1997  |
|   | BER 7, 2018 - to upda<br>lood Hazard Areas, to                         | TE(S) OF REVISION(S) TO THIS PANEL<br>te corporate limits, to change Base Flood Elevations and<br>update map format, to add roads and road names, and to   |
| For communi                                   |  | eviously issued Letters of Map Revision.<br>y prior to countywide mapping, refer to the Community  |
| Map History                                   | Table located in the Flo   | od Insurance Study report for this jurisdiction.   |
|   |  | urance Program at 1-800-638-6620.  |
|   | *  |  |
|   | в<br>250 0<br>Н.Н.Н.   | AAP SCALE 1" = 500'<br>500 1000<br>FEET  |
| 1   | 50 0   | METERS<br>150 300  |
| (   |  | [  |
|   |  | PANEL 0561G  |
|   | MAN  | FIRM   |
|   |  | FLOOD INSURANCE RATE MAP   |
|   | Q  | EL PASO COUNTY,  |
|   | <b>N</b>   | COLORADO   |
|   |  | AND INCORPORATED AREAS   |
|   | Ð  | PANEL 561 OF 1300<br>(SEE MAP INDEX FOR FIRM PANEL LAYOUT)   |
|   |  | <u>CONTAINS:</u>   |
|   | A  | COMMUNITY   NUMBER   PANEL   SUFFIX     COLORADO SPRINGS. CITY OF   080060   0561   G  |
|   | Ø  | EL PASO COUNTY 060059 0561 G   |
|   | TE   |  |
|   |  |  |
|   | Ø  |  |
|   |  | Notice to User: The <b>Map Number</b> shown below should be<br>used when placing map orders: the <b>Community Number</b><br>shown above should be used on insurance applications for the<br>subject community.   |
|   |  | MAP NUMBER   |
|   | ME   | 08041C0561G  |
|   |  | MAP REVISED  |
|   | PER  | DECEMBER 7, 2018<br>Federal Emergency Management Agency  |
| ų   |  |  |
|   |  |  |

## **APPENDIX D**

## HYDROLOGICAL CALCULATIONS

| LAND USE OR SURFACE  | PERCENT    | "C" FREQU | JENCY |      |      |
|----------------------|------------|-----------|-------|------|------|
| CHARACTERISTICS      | IMPERVIOUS | 10        |       | 100  |      |
|                      |            | A&B*      | C&D*  | A&B* | C&D* |
| Business             |            |           |       |      |      |
| Commercial Areas     | 95         | 0.90      | 0.90  | 0.90 | 0.90 |
| Neighborhood Areas   | 70         | 0.75      | 0.75  | 0.80 | 0.80 |
| Residential          |            |           |       |      |      |
| 1⁄8 Acre or less     | 65         | 0.60      | 0.70  | 0.70 | 0.80 |
| ¼ Acre               | 40         | 0.50      | 0.60  | 0.60 | 0.70 |
| ⅓ Acre               | 30         | 0.40      | 0.50  | 0.55 | 0.60 |
| ½ Acre               | 25         | 0.35      | 0.45  | 0.45 | 0.55 |
| 1 Acre               | 20         | 0.30      | 0.40  | 0.40 | 0.50 |
| Industrial           |            |           |       |      |      |
| Light Areas          | 80         | 0.70      | 0.70  | 0.80 | 0.80 |
| Heavy Areas          | 90         | 0.80      | 0.80  | 0.90 | 0.90 |
| Parks and Cemeteries | 7          | 0.30      | 0.35  | 0.55 | 0.60 |
| Playgrounds          | 13         | 0.30      | 0.35  | 0.60 | 0.65 |
| Railroad Yard Areas  | 40         | 0.50      | 0.55  | 0.60 | 0.65 |

| LAND USE OR SURFACE                                  | PERCENT    | "C" FREQU | JENCY |      |      |
|--|------------|-----------|-------|------|------|
| CHARACTERISTICS                                      | IMPERVIOUS | 10        |       | 100  |      |
|  |            | A&B*      | C&D*  | A&B* | C&D* |
| Undeveloped Areas                                    |            |           |       |      |      |
| Historic Flow Analysis-<br>Greenbelts, Agricultural  | 2          | 0.15      | 0.25  | 0.20 | 0.30 |
| Pasture/Meadow                                       | 0          | 0.25      | 0.30  | 0.35 | 0.45 |
| Forest   | 0          | 0.10      | 0.15  | 0.15 | 0.20 |
| Exposed Rock   | 100        | 0.90      | 0.90  | 0.95 | 0.95 |
| Offsite Flow Analysis (when<br>land use not defined) | 45         | 0.55      | 0.60  | 0.65 | 0.70 |
| Streets  | 1          | 1         | 1     | 1    | 1    |
| Paved  | 100        | 0.90      | 0.90  | 0.95 | 0.95 |
| Gravel   | 80         | 0.80      | 0.80  | 0.85 | 0.85 |
| Drive and Walks                                      | 100        | 0.90      | 0.90  | 0.95 | 0.95 |
| Roofs  | 90         | 0.90      | 0.90  | 0.95 | 0.95 |
| Lawns  | 0          | 0.25      | 0.30  | 0.35 | 0.45 |
| *Hydrologic Soil Group                               |            |           |       |      |      |

#### RUNOFF COEFFICIENTS AND IMPERVIOUSNESS Falcon Highlands Filing No. 3 - EXISTING CONDITIONS El Paso County, Colorado

| Basin No | Hydrologic<br>Grouping | Total Area | 1/3  | 8 Acre or L | ess  |      | Paved |      |      | Drive and Walks |      |      | Lawns |      |      | 1/2 Acre |       |      | 1/4 Acre |       |      | c Flow Ana<br>belts, Agri |       | Runoff C | oefficient | Imperviousness |
|----------|------------------------|------------|------|-------------|------|------|-------|------|------|-----------------|------|------|-------|------|------|----------|-------|------|----------|-------|------|---------------------------|-------|----------|------------|----------------|
|          |                        |            |      | 65%         |      |      | 100%  |      |      | 100%            |      |      | 0%    |      | 25%  |          | 40%   |      |          | 2%    |      |                           |       |          |            |                |
|          |                        | (AC)       | C5   | C100        | (AC) | C5   | C100  | (AC) | C5   | C100            | (AC) | C5   | C100  | (AC) | C5   | C100     | (AC)  | C5   | C100     | (AC)  | C5   | C100                      | (AC)  | 5-Year   | 100-Year   | (%)            |
| A        | A                      | 3.74       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 3.74  | 0.09     | 0.36       | 2.0%           |
| В        | A                      | 38.93      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 38.93 | 0.09     | 0.36       | 2.0%           |
| С        | A                      | 57.81      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 57.81 | 0.09     | 0.36       | 2.0%           |
| D        | A                      | 10.54      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 10.54 | 0.09     | 0.36       | 2.0%           |
| E        | A                      | 3.14       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 3.14  | 0.09     | 0.36       | 2.0%           |
| F        | A                      | 3.67       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 3.67  | 0.09     | 0.36       | 2.0%           |
| G        | A                      | 8.84       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 8.84  | 0.09     | 0.36       | 2.0%           |
| OS-1     | A                      | 6.38       | 0.45 | 0.59        | 1.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 3.77  | 0.09 | 0.36                      | 1.61  | 0.27     | 0.48       | 34.3%          |
| OS-2     | A                      | 3.12       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 3.12  | 0.09 | 0.36                      | 0.00  | 0.30     | 0.50       | 40.0%          |
| OS-3     | A                      | 1.14       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 1.14 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 0.00  | 0.90     | 0.96       | 100.0%         |
| OS-4     | A                      | 13.09      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 7.50  | 0.09 | 0.36                      | 5.59  | 0.34     | 0.44       | 23.8%          |
| OS-5     | A                      | 59.62      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 63.24 | 0.09 | 0.36                      | 0.00  | 0.32     | 0.53       | 42.4%          |
| OS-6     | A                      | 35.75      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 35.75 | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 0.00  | 0.22     | 0.46       | 25.0%          |
| OS-7     | A                      | 6.47       | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 6.47  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 0.00  | 0.22     | 0.46       | 25.0%          |
| OS-8     | A                      | 13.79      | 0.45 | 0.59        | 0.00 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96            | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.50     | 0.00  | 0.09 | 0.36                      | 13.79 | 0.09     | 0.36       | 2.0%           |
| TOTAL    |                        | 266.0      |      |             | 1.0  |      |       | 0.0  |      |                 | 1.1  |      |       | 0.0  |      |          | 42.2  |      |          | 77.6  |      |                           | 133.9 |          |            | 17.3%          |
|          |                        |            |      |             |      |      |       |      |      |                 |      |      |       |      |      |          |       |      |          |       |      |                           |       |          |            |                |

#### TIME OF CONCENTRATION Falcon Highlands Filing No. 3 - EXISTING CONDITIONS El Paso County, Colorado

DATE: <u>3/18/2022</u> CALCULATED BY: <u>AMC/ARP</u> PROJECT: <u>21000656</u> DESIGN STORM: 5<u>Year</u>

|           |       |      | INITI  | AL/OVERL<br>TIME (ti) | AND   |        |       | TRAVEL TIME<br>(tt) |      | (URE  | tc CHECH<br>SANIZED B |        | FINAL<br>tc |       |
|-----------|-------|------|--------|-----------------------|-------|--------|-------|---------------------|------|-------|-----------------------|--------|-------------|-------|
| TRIBUTARY | AREA  | C5   | LENGTH | SLOPE                 | ti    | LENGTH | SLOPE | Conveyance          | VEL  | tt    | COMP.                 | TOTAL  | (L/180)+10  |       |
| BASINS    | Ac    |      | Ft     | %                     | Min.  | Ft.    | %     | Coefficient         | fps  | Min.  | tc                    | LENGTH | Min.        | Min.  |
|           | (2)   | (3)  | (4)    | (5)                   | (6)   | (7)    | (8)   |                     | (9)  | (10)  | (11)                  | (12)   | (13)        | (14)  |
| А         | 3.74  | 0.09 | 202    | 1.00                  | 25.92 | 910    | 1.00  | 15                  | 1.50 | 10.11 | 36.03                 | 1112   | 16.18       | 16.18 |
| В         | 38.93 | 0.09 | 1256   | 1.00                  | 64.63 | 979    | 1.00  | 15                  | 1.50 | 10.88 | 75.50                 | 2235   | 22.42       | 22.42 |
| С         | 57.81 | 0.09 | 1104   | 2.00                  | 48.20 | 571    | 1.00  | 15                  | 1.50 | 6.34  | 54.55                 | 1675   | 19.31       | 19.31 |
| D         | 10.54 | 0.09 | 540    | 1.00                  | 42.38 | 360    | 1.00  | 15                  | 1.50 | 4.00  | 46.38                 | 900    | 15.00       | 15.00 |
| E         | 3.14  | 0.09 | 90     | 6.00                  | 9.58  | 1080   | 1.00  | 15                  | 1.50 | 12.00 | 21.58                 | 1170   | 16.50       | 16.50 |
| F         | 3.67  | 0.09 | 125    | 3.00                  | 14.19 | 630    | 1.60  | 15                  | 1.90 | 5.53  | 19.72                 | 755    | 14.19       | 14.19 |
| G         | 8.84  | 0.09 | 200    | 3.00                  | 17.95 | 360    | 1.10  | 15                  | 1.57 | 3.81  | 21.76                 | 560    | 13.11       | 13.11 |
| OS-1      | 6.38  | 0.27 | 25     | 2.00                  | 5.96  | 650    | 2.00  | 20                  | 2.83 | 3.83  | 9.79                  | 675    | 13.75       | 9.79  |
| OS-2      | 3.12  | 0.30 | 50     | 2.00                  | 8.13  | 2180   | 1.00  | 20                  | 2.00 | 18.17 | 26.29                 | 2230   | 22.39       | 22.39 |
| OS-3      | 1.14  | 0.90 | 20     | 2.00                  | 1.28  | 1190   | 2.00  | 20                  | 2.83 | 7.01  | 8.30                  | 1210   | 16.72       | 8.30  |
| OS-4      | 13.09 | 0.34 | 80     | 2.00                  | 9.76  | 2300   | 2.00  | 20                  | 2.83 | 13.55 | 23.32                 | 2380   | 23.22       | 23.22 |
| OS-5      | 59.62 | 0.32 | 100    | 2.00                  | 11.23 | 608    | 2.00  | 20                  | 2.83 | 3.58  | 14.81                 | 708    | 13.93       | 13.93 |
| OS-6      | 35.75 | 0.22 | 100    | 2.00                  | 12.64 | 0      | 0.60  | 20                  | 1.55 | 0.00  | 12.64                 | 100    | 10.56       | 10.56 |
| OS-7      | 6.47  | 0.22 | 350    | 2.00                  | 23.65 | 300    | 0.60  | 15                  | 1.16 | 4.30  | 27.95                 | 650    | 13.61       | 13.61 |
| OS-8      | 13.79 | 0.09 | 550    | 2.00                  | 34.02 | 0      | 0.60  | 15                  | 1.16 | 0.00  | 34.02                 | 550    | 13.06       | 13.06 |

#### 5-YEAR RUNOFF CALCULATIONS Falcon Highlands Filing No. 3 - EXISTING CONDITIONS El Paso County, Colorado

| DATE:  | 3/18/2022 |     |
|--------|-----------|-----|
| CALCUL | ATED BY:  | RDL |

|           |        |         |      |       | FLOW T | O INLETS  |          |       |       | Minimum      | Maximum        | Under     |       |      |           | INLETS    |                |   |             |            | Carry-Over        |
|-----------|--------|---------|------|-------|--------|-----------|----------|-------|-------|--------------|----------------|-----------|-------|------|-----------|-----------|----------------|---|-------------|------------|-------------------|
| Sub-Basin | Design | Area    | С    | СхА   | Тс     | Intensity | Qd = CIA | Qco   | Qt    | Street Slope | Street/Paseo   | Capacity? | Inlet | Туре | Condition | Slope at  | Inlet          | R | Intercepted | Carry-Over | to Sub-basin/     |
|           | Point  | (acres) |      |       | (min)  | (in/hr)   | (cfs)    | (cfs) | (cfs) | (%)          | Capacity (cfs) |           |       |      |           | Inlet (%) | Capacity (cfs) |   | (cfs)       | (cfs)      | Design Point (DP) |
| Α         | 1      | 3.74    | 0.09 | 0.34  | 16.18  | 3.41      | 1.15     | 0.00  | 1.15  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| В         | 2      | 38.93   | 0.09 | 3.50  | 22.42  | 2.92      | 10.22    | 0.00  | 10.22 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| С         | 3      | 57.81   | 0.09 | 5.20  | 19.31  | 3.14      | 16.35    | 0.00  | 16.35 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| D         | 4      | 10.54   | 0.09 | 0.95  | 15.00  | 3.52      | 3.34     | 0.00  | 3.34  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| E         | 5      | 3.14    | 0.09 | 0.28  | 16.50  | 3.38      | 0.95     | 0.00  | 0.95  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| F         | 6      | 3.67    | 0.09 | 0.33  | 14.19  | 3.60      | 1.19     | 0.00  | 1.19  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| G         | 6      | 8.84    | 0.09 | 0.80  |        |           | 6.80     | 0.00  | 6.80  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-1      | 7      | 6.38    | 0.27 | 1.73  |        |           | 10.70    | 0.00  | 10.70 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-2      | 8      | 3.12    | 0.30 | 0.94  |        |           | 7.80     | 0.00  | 7.80  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-3      | 9      | 1.14    | 0.90 | 1.03  |        |           | 3.40     | 0.00  | 3.40  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-4      | 10     | 13.09   | 0.34 | 4.45  |        |           | 12.30    | 0.00  | 12.30 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-5      | 11     | 59.62   | 0.32 | 18.97 |        |           | 80.10    | 0.00  | 80.10 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-6      | 12     | 35.75   | 0.22 | 7.87  |        |           | 31.90    | 0.00  | 31.90 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-7      | 13     | 6.47    | 0.22 | 1.42  | 13.61  | 3.67      | 5.22     | 0.00  | 5.22  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-8      | 4      | 13.79   | 0.09 | 1.24  | 13.06  | 3.73      | 4.63     | 0.00  | 4.63  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |

Notes:

\*DATA IN RED REPRESENTS VALUES PER PREVIOUS DRAINAGE REPORTS FOR SUBDIVISION

Basin E corrected. This sheet replaced.

#### PROJECT: <u>21000656</u> DESIGN STORM: 5<u>-Year</u>

#### **100-YEAR RUNOFF CALCULATIONS** Falcon Highlands Filing No. 3 - EXISTING CONDITIONS El Paso County, Colorado

# DATE: 3/18/2022 CALCULATED BY: <u>RDL</u>

|           |        |         |      |       | FLOW T | O INLETS  |          |       |        | Minimum      | Maximum        | Under     |       |      |           | INLETS    |                |   |             |            | Carry-Over        |
|-----------|--------|---------|------|-------|--------|-----------|----------|-------|--------|--------------|----------------|-----------|-------|------|-----------|-----------|----------------|---|-------------|------------|-------------------|
| Sub-Basin | Design | Area    | С    | СхА   | Tc     | Intensity | Qd = CIA | Qco   | Qt     | Street Slope | Street/Paseo   | Capacity? | Inlet | Туре | Condition | Slope at  | Inlet          | R | Intercepted | Carry-Over | to Sub-basin/     |
|           | Point  | (acres) |      |       | (min)  | (in/hr)   | (cfs)    | (cfs) | (cfs)  | (%)          | Capacity (cfs) |           |       |      |           | Inlet (%) | Capacity (cfs) |   | (cfs)       | (cfs)      | Design Point (DP) |
| Α         | 1      | 3.74    | 0.36 | 1.35  | 16.18  | 5.72      | 7.70     | 0.00  | 7.70   | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| В         | 2      | 38.93   | 0.36 | 14.01 | 22.42  | 4.90      | 68.65    | 0.00  | 68.65  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| С         | 3      | 57.81   | 0.36 | 20.81 | 19.31  | 5.27      | 109.77   | 0.00  | 109.77 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| D         | 4      | 10.54   | 0.36 | 3.79  | 15.00  | 5.91      | 22.42    | 0.00  | 22.42  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| E         | 5      | 3.14    | 0.36 | 1.13  | 16.50  | 5.67      | 6.41     | 0.00  | 6.41   | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| F         | 6      | 3.67    | 0.36 | 1.32  | 14.19  | 6.05      | 7.99     | 0.00  | 7.99   | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| G         | 6      | 8.84    | 0.36 | 3.18  |        |           | 16.00    | 0.00  | 16.00  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-1      | 7      | 6.38    | 0.48 | 3.05  |        |           | 21.70    | 0.00  | 21.70  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-2      | 8      | 3.12    | 0.50 | 1.56  |        |           | 13.60    | 0.00  | 13.60  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-3      | 9      | 1.14    | 0.96 | 1.09  |        |           | 6.00     | 0.00  | 6.00   | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-4      | 10     | 13.09   | 0.44 | 5.76  |        |           | 26.30    | 0.00  | 26.30  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-5      | 11     | 59.62   | 0.53 | 31.62 |        |           | 160.70   | 0.00  | 160.70 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-6      | 12     | 35.75   | 0.46 | 16.45 |        |           | 58.40    | 0.00  | 58.40  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-7      | 13     | 6.47    | 0.46 | 2.98  | 13.61  | 6.16      | 18.32    | 0.00  | 18.32  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-8      | 4      | 13.79   | 0.36 | 4.96  | 13.06  | 6.26      | 31.08    | 0.00  | 31.08  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |

Notes: \*DATA IN RED REPRESENTS VALUES PER PREVIOUS DRAINAGE REPORTS FOR SUBDIVISION

Basin E corrected. This sheet replaced.

# PROJECT: 21000656 DESIGN STORM: 100<u>-Year</u>

| EXISTING C |              | RAINAG          | E BAS          | SIN S            | UMMAR    | Y                      |
|------------|--------------|-----------------|----------------|------------------|----------|------------------------|
| Basin      | Design Point | Area<br>(acres) | C <sub>5</sub> | C <sub>100</sub> | Q₅ (cfs) | Q <sub>100</sub> (cfs) |
| А          | 1            | 3.74            | 0.09           | 0.36             | 1.15     | 7.70                   |
| В          | 2            | 38.93           | 0.09           | 0.36             | 10.22    | 68.65                  |
| С          | 3            | 57.81           | 0.09           | 0.36             | 16.35    | 109.77                 |
| D          | 4            | 10.54           | 0.09           | 0.36             | 3.34     | 22.42                  |
| E          | 5            | 3.14            | 0.09           | 0.36             | 1.12     | 7.50                   |
| F          | 6            | 3.67            | 0.09           | 0.36             | 1.19     | 7.99                   |
| G          | 6            | 8.84            | 0.09           | 0.36             | 6.80     | 16.00                  |
| OS-1       | 7            | 6.38            | 0.27           | 0.48             | 10.70    | 21.70                  |
| OS-2       | 8            | 3.12            | 0.30           | 0.50             | 7.80     | 13.60                  |
| OS-3       | 9            | 1.14            | 0.90           | 0.96             | 3.40     | 6.00                   |
| OS-4       | 10           | 13.09           | 0.34           | 0.44             | 12.30    | 26.30                  |
| OS-5       | 11           | 59.62           | 0.32           | 0.53             | 80.10    | 160.70                 |
| OS-6       | 12           | 35.75           | 0.22           | 0.46             | 31.90    | 58.40                  |
| OS-7       | 13           | 6.47            | 0.22           | 0.46             | 5.22     | 18.32                  |
| OS-8       | 4            | 13.79           | 0.09           | 0.36             | 4.63     | 31.08                  |
| TOTAL      |              | 266.0           |                |                  | 196.2    | 576.1                  |

### - -

Flows do not ma hydrology spreadsheet

These #'s are correct on this page. Old #'s were in the calculations sheets.

| EXISTING CONDITIONS DESIGN POINT SUMMARY |
|--|
| (CUMULATIVE FLOW)                        |

| Design Point             | Contributing Basins                   | Q <sub>5</sub> (cfs) | Q <sub>100</sub> (cfs) |
|--------------------------|---------------------------------------|----------------------|------------------------|
| 1                        | A, DP 10 (OS-4)                       | 13.4                 | 34.0                   |
| Revised.                 | B, DP 11 (OS-2, OS-5)                 | 98.1                 | 242.9                  |
| 3                        | C, DP 12 (OS-3, OS-6) OS              | <mark>-7</mark> 51.6 | 174.2                  |
| 4                        | D, <del>OS-7,</del> OS-8              | 13.2                 | 71.8                   |
| 5                        | E, DP 2 (B, OS-2, OS-5)               | 99.2                 | 250.4                  |
| 6 <mark>F, G, D</mark> F | P 3 (C, OS-3, OS-6), DP 4(D, OS-7, OS | S-8) 3               | 246.0                  |
| 7                        | OS-1                                  | 10.7                 | 21.7                   |
| 8                        | OS-2                                  | 7.8                  | 13.6                   |
| 9                        | OS-3                                  | 3.4                  | 6.0                    |
| 10                       | OS-4                                  | 12.3                 | 26.3                   |
| 11                       | OS-2, OS-5                            | 87.9                 | 174.3                  |
| 12                       | OS-3, OS-6                            | 35.3                 | 64.4                   |
| 13                       | OS-7                                  | 5.2                  | 18.3                   |

Does OS-7 combine with D and OS-8 at DP 4 or travel through site down to DP 6? Clarify and update table.

Travels through down to DP3 (Pond 2) and DP6 (outlet of Pond 2). Revised.

#### RUNOFF COEFFICIENTS AND IMPERVIOUSNESS Falcon Highlands Filing No. 3 - PROPOSED CONDITIONS El Paso County, Colorado

| Basin No | Hydrologic<br>Grouping | Total Area | 1/   | 8 Acre or L | ess   |      | Paved |      | Dri  | ve and Wal | ks   |      | Lawns |      |      | 1/2 Acre |       |      | 1/4 Acre |       |      | c Flow Ana<br>pelts, Agrie |       | Runoff C | oefficient | Imperviousness |
|----------|------------------------|------------|------|-------------|-------|------|-------|------|------|------------|------|------|-------|------|------|----------|-------|------|----------|-------|------|----------------------------|-------|----------|------------|----------------|
|          |                        |            |      | 65%         |       |      | 100%  |      |      | 100%       |      |      | 0%    |      |      | 25%      |       |      | 40%      |       |      | 2%                         |       |          |            |                |
|          |                        | (AC)       | C5   | C100        | (AC)  | C5   | C100  | (AC) | C5   | C100       | (AC) | C5   | C100  | (AC) | C5   | C100     | (AC)  | C5   | C100     | (AC)  | C5   | C100                       | (AC)  | 5-Year   | 100-Year   | (%)            |
| A        | A                      | 3.74       | 0.45 | 0.59        | 0.50  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 3.24 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 0.00  | 0.13     | 0.38       | 8.7%           |
| В        | A                      | 40.37      | 0.45 | 0.59        | 31.28 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 4.23 | 0.22 | 0.46     | 4.86  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 0.00  | 0.38     | 0.55       | 53.4%          |
| С        | A                      | 57.12      | 0.45 | 0.59        | 34.24 | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 3.80 | 0.22 | 0.46     | 10.32 | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 8.75  | 0.33     | 0.52       | 43.8%          |
| D        | A                      | 7.96       | 0.45 | 0.59        | 5.74  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 2.22 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 0.00  | 0.35     | 0.52       | 46.9%          |
| E        | A                      | 3.14       | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 3.14  | 0.09     | 0.36       | 2.0%           |
| F        | A                      | 5.50       | 0.45 | 0.59        | 0.34  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 5.16  | 0.11     | 0.37       | 5.9%           |
| G        | A                      | 8.80       | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 8.80  | 0.09     | 0.36       | 2.0%           |
| OS-1     | A                      | 6.38       | 0.45 | 0.59        | 1.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 3.77  | 0.09 | 0.36                       | 1.61  | 0.27     | 0.48       | 34.3%          |
| OS-2     | A                      | 3.12       | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 3.12  | 0.09 | 0.36                       | 0.00  | 0.30     | 0.50       | 40.0%          |
| OS-3     | A                      | 1.14       | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 1.14 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 0.00  | 0.90     | 0.96       | 100.0%         |
| OS-4     | A                      | 13.09      | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 7.50  | 0.09 | 0.36                       | 5.59  | 0.34     | 0.44       | 23.8%          |
| OS-5     | A                      | 59.62      | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 59.62 | 0.09 | 0.36                       | 0.00  | 0.30     | 0.50       | 40.0%          |
| OS-6     | A                      | 35.75      | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 35.75 | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 0.00  | 0.22     | 0.46       | 25.0%          |
| OS-7     | A                      | 6.47       | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 6.47  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 0.00  | 0.22     | 0.46       | 25.0%          |
| OS-8     | A                      | 13.79      | 0.45 | 0.59        | 0.00  | 0.90 | 0.96  | 0.00 | 0.90 | 0.96       | 0.00 | 0.08 | 0.35  | 0.00 | 0.22 | 0.46     | 0.00  | 0.30 | 0.5      | 0.00  | 0.09 | 0.36                       | 13.79 | 0.09     | 0.36       | 2.0%           |
| TOTAL    |                        | 266.0      |      |             | 73.1  |      |       | 0.0  |      |            | 1.1  |      |       | 13.5 |      |          | 57.4  |      |          | 74.0  |      |                            | 46.8  |          |            | 35.2%          |
|          |                        |            |      |             |       |      |       |      |      |            |      |      |       |      |      |          |       |      |          |       |      |                            |       |          |            |                |

#### TIME OF CONCENTRATION Falcon Highlands Filing No. 3 - PROPOSED CONDITIONS El Paso County, Colorado

DATE: <u>3/18/2022</u> CALCULATED BY: <u>RDL</u> PROJECT: <u>21000656</u> DESIGN STORM: 5<u>Year</u>

|           |       |      | INITI  | AL/OVERL<br>TIME (ti) | AND   |        |       | TRAVEL TIME<br>(tt) |      |       | (URE  | tc CHECH<br>SANIZED B |            | FINAL<br>tc |
|-----------|-------|------|--------|-----------------------|-------|--------|-------|---------------------|------|-------|-------|-----------------------|------------|-------------|
| TRIBUTARY | AREA  | C5   | LENGTH | SLOPE                 | ti    | LENGTH | SLOPE | Conveyance          | VEL  | tt    | COMP. | TOTAL                 | (L/180)+10 |             |
| BASINS    | Ac    |      | Ft     | %                     | Min.  | Ft.    | %     | Coefficient         | fps  | Min.  | tc    | LENGTH                | Min.       | Min.        |
|           | (2)   | (3)  | (4)    | (5)                   | (6)   | (7)    | (8)   |                     | (9)  | (10)  | (11)  | (12)                  | (13)       | (14)        |
| А         | 3.74  | 0.13 | 100    | 2.00                  | 13.94 | 980    | 1.00  | 20                  | 2.00 | 8.17  | 22.11 | 1080                  | 16.00      | 16.00       |
| В         | 40.37 | 0.38 | 0      | 0.00                  | 0.00  | 907    | 1.30  | 20                  | 2.28 | 6.63  | 6.63  | 907                   | 15.04      | 6.63        |
| С         | 57.12 | 0.33 | 100    | 1.50                  | 12.18 | 924    | 1.00  | 20                  | 2.00 | 7.70  | 19.88 | 1024                  | 15.69      | 15.69       |
| D         | 7.96  | 0.35 | 100    | 1.00                  | 13.60 | 750    | 1.00  | 20                  | 2.00 | 6.25  | 19.85 | 850                   | 14.72      | 14.72       |
| E         | 3.14  | 0.09 | 75     | 2.00                  | 12.56 | 150    | 3.50  | 15                  | 2.81 | 0.89  | 13.45 | 225                   | 11.25      | 11.25       |
| F         | 5.50  | 0.11 | 125    | 3.00                  | 13.87 | 630    | 1.60  | 15                  | 1.90 | 5.53  | 19.41 | 755                   | 14.19      | 14.19       |
| G         | 8.80  | 0.09 | 200    | 3.00                  | 17.95 | 360    | 1.10  | 15                  | 1.57 | 3.81  | 21.76 | 560                   | 13.11      | 13.11       |
| OS-1      | 6.38  | 0.27 | 25     | 2.00                  | 5.96  | 650    | 2.00  | 20                  | 2.83 | 3.83  | 9.79  | 675                   | 13.75      | 9.79        |
| OS-2      | 3.12  | 0.30 | 50     | 2.00                  | 8.13  | 2180   | 1.00  | 20                  | 2.00 | 18.17 | 26.29 | 2230                  | 22.39      | 22.39       |
| OS-3      | 1.14  | 0.90 | 20     | 2.00                  | 1.28  | 1190   | 2.00  | 20                  | 2.83 | 7.01  | 8.30  | 1210                  | 16.72      | 8.30        |
| OS-4      | 13.09 | 0.34 | 80     | 2.00                  | 9.76  | 2300   | 2.00  | 20                  | 2.83 | 13.55 | 23.32 | 2380                  | 23.22      | 23.22       |
| OS-5      | 59.62 | 0.30 | 100    | 2.00                  | 11.49 | 608    | 2.00  | 20                  | 2.83 | 3.58  | 15.07 | 708                   | 13.93      | 13.93       |
| OS-6      | 35.75 | 0.22 | 100    | 2.00                  | 12.64 | 0      | 0.60  | 20                  | 1.55 | 0.00  | 12.64 | 100                   | 10.56      | 10.56       |
| OS-7      | 6.47  | 0.22 | 100    | 2.00                  | 12.64 | 550    | 0.60  | 20                  | 1.55 | 5.92  | 18.56 | 650                   | 13.61      | 13.61       |
| OS-8      | 13.79 | 0.09 | 100    | 2.00                  | 14.51 | 450    | 0.60  | 20                  | 1.55 | 4.84  | 19.35 | 550                   | 13.06      | 13.06       |

### 5-YEAR RUNOFF CALCULATIONS Falcon Highlands Filing No. 3 - PROPOSED CONDITIONS El Paso County, Colorado

| DATE:  | 3/18/2022 |     |
|--------|-----------|-----|
| CALCUL | ATED BY:  | RDL |

|           |        |         |      |       | FLOW T | O INLETS  |          |       |       | Minimum      | Maximum        | Under     |       |      |           | INLETS    |                |   |             |            | Carry-Over        |
|-----------|--------|---------|------|-------|--------|-----------|----------|-------|-------|--------------|----------------|-----------|-------|------|-----------|-----------|----------------|---|-------------|------------|-------------------|
| Sub-Basin | Design | Area    | С    | СхА   | Тс     | Intensity | Qd = CIA | Qco   | Qt    | Street Slope | Street/Paseo   | Capacity? | Inlet | Туре | Condition | Slope at  | Inlet          | R | Intercepted | Carry-Over | to Sub-basin/     |
|           | Point  | (acres) |      |       | (min)  | (in/hr)   | (cfs)    | (cfs) | (cfs) | (%)          | Capacity (cfs) |           |       |      |           | Inlet (%) | Capacity (cfs) |   | (cfs)       | (cfs)      | Design Point (DP) |
| Α         | 1      | 3.74    | 0.13 | 0.48  | 16.00  | 3.42      | 1.66     | 0.00  | 1.66  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| В         | 2      | 40.37   | 0.38 | 15.48 | 6.63   | 4.75      | 73.48    | 0.00  | 73.48 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| С         | 3      | 57.12   | 0.33 | 18.77 | 15.69  | 3.45      | 64.83    | 0.00  | 64.83 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| D         | 4      | 7.96    | 0.35 | 2.76  | 14.72  | 3.55      | 9.80     | 0.00  | 9.80  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| E         | 5      | 3.14    | 0.09 | 0.28  | 11.25  | 3.95      | 1.12     | 0.00  | 1.12  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| F         | 6      | 5.50    | 0.11 | 0.62  | 14.19  | 3.60      | 2.23     | 0.00  | 2.23  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| G         | 6      | 8.80    | 0.09 | 0.79  |        |           | 6.80     | 0.00  | 6.80  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-1      | 7      | 6.38    | 0.27 | 1.73  |        |           | 10.70    | 0.00  | 10.70 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-2      | 8      | 3.12    | 0.30 | 0.94  |        |           | 7.80     | 0.00  | 7.80  | -            | -              | -         |       |      |           |           |                |   |             |            |                   |
| OS-3      | 9      | 1.14    | 0.90 | 1.03  |        |           | 3.40     | 0.00  | 3.40  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-4      | 10     | 13.09   | 0.34 | 4.45  |        |           | 14.90    | 0.00  | 14.90 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-5      | 11     | 59.62   | 0.30 | 17.89 |        |           | 80.10    | 0.00  | 80.10 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-6      | 12     | 35.75   | 0.22 | 7.87  |        |           | 31.90    | 0.00  | 31.90 | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-7      | 13     | 6.47    | 0.22 | 1.42  | 13.61  | 3.67      | 5.22     | 0.00  | 5.22  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |
| OS-8      | 4      | 13.79   | 0.09 | 1.24  | 13.06  | 3.73      | 4.63     | 0.00  | 4.63  | -            | -              | -         | -     | -    | -         | -         | -              | - | -           | -          | -                 |

Notes:

\*DATA IN RED REPRESENTS VALUES PER PREVIOUS DRAINAGE REPORTS FOR SUBDIVISION

#### PROJECT: <u>21000656</u> DESIGN STORM: 5<u>-Year</u>

#### 100-YEAR RUNOFF CALCULATIONS Falcon Highlands Filing No. 3 - PROPOSED CONDITIONS El Paso County, Colorado

DATE: 3/18/2022 CALCULATED BY: <u>RDL</u>

|           |                 |                 |      |       | FLOW T      | O INLETS             |                   |              |             | Minimum             | Maximum                        | Under     |       |      |           | INLETS                |                         |   |                      |                     | Carry-Over                         |
|-----------|-----------------|-----------------|------|-------|-------------|----------------------|-------------------|--------------|-------------|---------------------|--------------------------------|-----------|-------|------|-----------|-----------------------|-------------------------|---|----------------------|---------------------|------------------------------------|
| Sub-Basin | Design<br>Point | Area<br>(acres) | С    | СхА   | Tc<br>(min) | Intensity<br>(in/hr) | Qd = CIA<br>(cfs) | Qco<br>(cfs) | Qt<br>(cfs) | Street Slope<br>(%) | Street/Paseo<br>Capacity (cfs) | Capacity? | Inlet | Туре | Condition | Slope at<br>Inlet (%) | Inlet<br>Capacity (cfs) | R | Intercepted<br>(cfs) | Carry-Over<br>(cfs) | to Sub-basin/<br>Design Point (DP) |
| •         | 1               | 3.74            | 0.29 | 1 4 2 | ()          | 5.75                 | 、 ,               | <u> </u>     | . ,         |                     |                                |           |       |      |           |                       |                         |   | . ,                  | . ,                 |                                    |
| A         |                 | -               | 0.38 | 1.43  | 16.00       |                      | 8.21              | 0.00         | 8.21        | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| В         | 2               | 40.37           | 0.55 | 22.17 | 6.63        | 7.97                 | 176.67            | 0.00         | 176.67      | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| С         | 3               | 57.12           | 0.52 | 29.43 | 15.69       | 5.80                 | 170.64            | 0.00         | 170.64      | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| D         | 4               | 7.96            | 0.52 | 4.16  | 14.72       | 5.96                 | 24.80             | 0.00         | 24.80       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| E         | 5               | 3.14            | 0.36 | 1.13  | 11.25       | 6.64                 | 7.50              | 0.00         | 7.50        | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| F         | 6               | 5.50            | 0.37 | 2.06  | 14.19       | 6.05                 | 12.46             | 0.00         | 12.46       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| G         | 6               | 8.80            | 0.36 | 3.17  |             |                      | 16.00             | 0.00         | 16.00       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-1      | 7               | 6.38            | 0.48 | 3.05  |             |                      | 21.70             | 0.00         | 21.70       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-2      | 8               | 3.12            | 0.50 | 1.56  |             |                      | 13.60             | 0.00         | 13.60       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-3      | 9               | 1.14            | 0.96 | 1.09  |             |                      | 6.00              | 0.00         | 6.00        | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-4      | 10              | 13.09           | 0.44 | 5.76  |             |                      | 31.70             | 0.00         | 31.70       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-5      | 11              | 59.62           | 0.50 | 29.81 |             |                      | 160.70            | 0.00         | 160.70      | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-6      | 12              | 35.75           | 0.46 | 16.45 |             |                      | 58.40             | 0.00         | 58.40       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-7      | 13              | 6.47            | 0.46 | 2.98  | 13.61       | 6.16                 | 18.32             | 0.00         | 18.32       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |
| OS-8      | 4               | 13.79           | 0.36 | 4.96  | 13.06       | 6.26                 | 31.08             | 0.00         | 31.08       | -                   | -                              | -         | -     | -    | -         | -                     | -                       | - | -                    | -                   | -                                  |

Notes:

\*DATA IN RED REPRESENTS VALUES PER PREVIOUS DRAINAGE REPORTS FOR SUBDIVISION

### PROJECT: 21000656 DESIGN STORM: 100<u>-Year</u>

| PROPO | PROPOSED CONDITIONS DRAINAGE BASIN SUMMARY |                 |                       |                  |          |                        |  |  |  |  |  |  |  |  |
|-------|--|-----------------|-----------------------|------------------|----------|------------------------|--|--|--|--|--|--|--|--|
| Basin | Design Point                               | Area<br>(acres) | <b>C</b> <sub>5</sub> | C <sub>100</sub> | Q₅ (cfs) | Q <sub>100</sub> (cfs) |  |  |  |  |  |  |  |  |
| Α     | 1  | 3.74            | 0.13                  | 0.38             | 1.7      | 8.2                    |  |  |  |  |  |  |  |  |
| В     | 2  | 40.37           | 0.38                  | 0.55             | 73.5     | 176.7                  |  |  |  |  |  |  |  |  |
| С     | 3  | 57.12           | 0.33                  | 0.52             | 64.8     | 170.6                  |  |  |  |  |  |  |  |  |
| D     | 4  | 7.96            | 0.35                  | 0.52             | 9.8      | 24.8                   |  |  |  |  |  |  |  |  |
| E     | 5  | 3.14            | 0.09                  | 0.36             | 1.1      | 7.5                    |  |  |  |  |  |  |  |  |
| F     | 6  | 5.50            | 0.11                  | 0.37             | 2.2      | 12.5                   |  |  |  |  |  |  |  |  |
| G     | 6  | 8.80            | 0.09                  | 0.36             | 6.8      | 16.0                   |  |  |  |  |  |  |  |  |
| OS-1  | 7  | 6.38            | 0.27                  | 0.48             | 10.7     | 21.7                   |  |  |  |  |  |  |  |  |
| OS-2  | 8  | 3.12            | 0.30                  | 0.50             | 7.8      | 13.6                   |  |  |  |  |  |  |  |  |
| OS-3  | 9  | 1.14            | 0.90                  | 0.96             | 3.4      | 6.0                    |  |  |  |  |  |  |  |  |
| OS-4  | 10   | 13.09           | 0.34                  | 0.44             | 14.9     | 31.7                   |  |  |  |  |  |  |  |  |
| OS-5  | 11   | 59.62           | 0.30                  | 0.50             | 80.1     | 160.7                  |  |  |  |  |  |  |  |  |
| OS-6  | 12   | 35.75           | 0.22                  | 0.46             | 31.9     | 58.4                   |  |  |  |  |  |  |  |  |
| OS-7  | 13   | 6.47            | 0.22                  | 0.46             | 5.2      | 18.3                   |  |  |  |  |  |  |  |  |
| OS-8  | 4  | 13.79           | 0.09                  | 0.36             | 4.6      | 31.1                   |  |  |  |  |  |  |  |  |
| TOTAL |  | 266.0           |                       |                  | 318.6    | 757.8                  |  |  |  |  |  |  |  |  |

|   | PR              | OPOSED CONDI<br>SUMMARY (CUN               |                                    |                                      |
|---|-----------------|--|------------------------------------|--------------------------------------|
|   | Design<br>Point | Contributing<br>Basins                     | Cumulative Q <sub>5</sub><br>(cfs) | Cumulative<br>Q <sub>100</sub> (cfs) |
| See comment under                       | 1               | A, DP 10 (OS-4)                            | 16.6                               | 39.9                                 |
| existing condition<br>summary table for |                 | 3, DP 11 (OS-2, OS-5                       | /                                  | 351.0                                |
| Basin OS-7. Revise                      | <u> </u>        | , DP 12 (OS-3, OS-6)                       | , DP 13 (OS-7)                     | 253.4                                |
| design point summary                    | 4               | → D, OS-8                                  | 14.4                               | 55.9                                 |
| here accordingly.                       | 5               | B, E, OS-2, OS-5                           | 162.5                              | 358.5                                |
|   | 6               | G, DP 3 (C, OS-3, O<br>OS-7), DP 4 (D, OS- |                                    | 325.2                                |
| Missing Basin F                         | 7               | OS-1                                       | 10.7                               | 21.7                                 |
| Missing Dasin I                         | 8               | OS-2                                       | 7.8                                | 13.6                                 |
|   | 9               | OS-3                                       | 3.4                                | 6.0                                  |
|   | 10              | OS-4                                       | 14.9                               | 31.7                                 |
|   | 11              | OS-5, DP 8 (OS-2)                          | 87.9                               | 174.3                                |
|   | 12              | OS-6, DP 9 (OS-3)                          | 35.3                               | 64.4                                 |
|   | 13              | OS-7                                       | 5.2                                | 18.3                                 |

Revised as suggested. Correct, OS-7 drains to DP3 as shown. Basin F added (drains to DP6).

| DEVELOPED CONDITIONS - SUMMARY OF FILING NO. 3, 2022 MDDP COMPARED TO 2010 FDR |  |            |                            |          |            |          |            |          |  |  |  |  |  |  |  |
|--|--|------------|----------------------------|----------|------------|----------|------------|----------|--|--|--|--|--|--|--|
| 2022 FIL NO. 3 MDDP (  | 2022 FIL NO. 3 MDDP (ATWELL) 2010 FDR (TERRA NOVA) DIFFERENCE ULTIMATE DESIGN PO |            |                            |          |            |          |            |          |  |  |  |  |  |  |  |
|  | Q5 (CFS)   | Q100 (CFS) |                            | Q5 (CFS) | Q100 (CFS) | Q5 (CFS) | Q100 (CFS) |          |  |  |  |  |  |  |  |
| BASIN A + OS-4   | 16.6   | 39.9       | BASIN A                    | 14.9     | 31.7       | 1.7      | 8.2        | OFF-SITE |  |  |  |  |  |  |  |
| BASIN B + E + OS-1 + OS-2 + OS-5   | 173.2  | 380.2      | BASIN B + E + OS-1 + OS-2  | 133.6    | 259.8      | 39.6     | 120.4      | POND 1   |  |  |  |  |  |  |  |
| BASIN C + F + G + OS-3 + OS-6 + OS-7   | 114.4  | 281.8      | BASIN C + D + F + G + OS-3 | 102.6    | 209.2      | 11.8     | 72.6       | POND 2   |  |  |  |  |  |  |  |
| BASIN D  | 9.8  | 24.8       | BASIN D (LESS D3)          | 20.0     | 40.3       | -10.2    | -15.5      | POND WU  |  |  |  |  |  |  |  |
| TOTAL  | 313.9  | 726.7      |                            | 271.1    | 541.0      | 42.8     | 185.7      |          |  |  |  |  |  |  |  |

### **APPENDIX E**

### HYDRAULIC CALCULATIONS

Put Pond Tributary Area and Imperviousness spreadsheets back into Appendix.

Provided as before. Included non-tributary basins for purposes of over-detention to account for developed areas that drain directly offsite.

| Site-Level   |                | •              | •              | ervious R             |               | •              |                | •              |                |               |                 |              |            |    |
|--|----------------|----------------|----------------|-----------------------|---------------|----------------|----------------|----------------|----------------|---------------|-----------------|--------------|------------|----|
|  |                |                |                | -BMP (Version         |               |                | ,              |                |                |               |                 |              |            |    |
| User Input   |                |                | 01             |                       | 5.00, 1000011 | 2010/          |                |                |                |               |                 |              |            |    |
|  |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| Calculated cells   |                |                |                | Designer:<br>Company: | Atwel         | d Lyon, PE     |                |                |                |               |                 |              |            |    |
| ***Design Storm: 1-Hour Rain Depth WQCV Event  | 0.60           | inches         |                | Date:                 |               | 18, 2022       |                |                |                |               |                 |              |            |    |
| +Minor Storm: 1-Hour Rain Depth 10-Year Event  | 1.19           | inches         |                | Project:              |               | Highlands      | - Pond 1 Ti    | ibutary Ba     | sins           |               |                 |              |            |    |
| ***Major Storm: 1-Hour Rain Depth 100-Year Event   | 2.52           | inches         |                | Location:             | El Pas        | o County       |                |                |                |               |                 |              |            |    |
| Optional User Defined Storm CUHP   |                |                |                | -                     |               |                |                |                |                |               |                 |              |            |    |
| (CUHP) NOAA 1 Hour Rainfall Depth and Frequency<br>for User Defined Storm 100-Year Event                       |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| Max Intensity for Optional User Defined Storm 0  |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| TE INFORMATION (USER-INPUT)  |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| Sub-basin Identifier   | A              | в              | OS-1           | 05-2                  | OS-4          | 05-5           |                |                |                |               |                 |              |            |    |
|  |                | -              |                |                       |               |                |                |                |                |               | <u> </u>        |              |            |    |
| Receiving Pervious Area Soil Type  | Clay Loam      | Sand           | Clay Loam      | Sand                  | Sand          | Sand           |                |                |                |               |                 |              |            |    |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)   | 3.740          | 40.370         | 6.380          | 3.120                 | 9.530         | 59.620         |                |                |                |               |                 |              |            |    |
| Directly Connected Impervious Area (DCIA, acres)   | 0.000          | 0.000          | 0.000          | 0.000                 | 0.000         | 0.000          |                |                |                |               |                 |              |            |    |
| Unconnected Impervious Area (UIA, acres)   | 0.551          | 18.972         | 2.158          | 1.248                 | 0.644         | 23.848         |                |                |                |               |                 |              |            |    |
| Receiving Pervious Area (RPA, acres)   | 0.000          | 21.398         | 4.222          | 1.872                 | 8.886         | 35.772         |                |                |                |               |                 | L            |            |    |
| Separate Pervious Area (SPA, acres)  | 3.189          | 0.000          | 0.000          | 0.000                 | 0.000         | 0.000          |                |                |                |               |                 |              |            |    |
| RPA Treatment Type: Conveyance (C),<br>Volume (V), or Permeable Pavement (PP)                                  | v              | v              | v              | v                     | v             | v              |                |                |                |               |                 |              |            |    |
|  |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| ALCULATED RESULTS (OUTPUT)   |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| Total Calculated Area (ac, check against input)  | 3.740          | 40.370         | 6.380          | 3.120                 | 9.530         | 59.620         |                |                |                |               |                 |              |            |    |
| Directly Connected Impervious Area (DCIA, %)   | 0.0%           | 0.0%           | 0.0%           | 0.0%                  | 0.0%          | 0.0%           |                |                |                |               |                 |              |            |    |
| Unconnected Impervious Area (UIA, %)   | 14.7%          | 47.0%          | 33.8%          | 40.0%                 | 6.8%          | 40.0%          |                |                |                |               |                 |              |            |    |
| Receiving Pervious Area (RPA, %)   | 0.0%           | 53.0%          | 66.2%          | 60.0%                 | 93.2%         | 60.0%          |                |                |                |               |                 |              |            |    |
| Separate Pervious Area (SPA, %)  | 85.3%          | 0.0%           | 0.0%           | 0.0%                  | 0.0%          | 0.0%           |                |                |                |               |                 |              |            |    |
| A <sub>R</sub> (RPA / UIA)   | 0.000          | 1.128          | 1.956          | 1.500                 | 13.798        | 1.500          |                |                |                |               |                 |              |            |    |
| I <sub>2</sub> Check   | 0.4            | 0.470<br>9.8   | 0.340          | 0.400<br>9.8          | 9.8           | 0.400<br>9.8   |                |                |                |               |                 |              |            |    |
| f / I for WQCV Event:  | 0.4            | 9.8            | 0.4            | 9.8<br>0.6            | 9.8           | 9.8<br>0.6     |                |                |                |               |                 |              |            |    |
| f / I for 10-Year Event:<br>f / I for 100-Year Event:  | 0.3            | 0.6            | 0.3            | 0.6                   | 0.6           | 0.6            |                |                |                |               |                 |              |            |    |
| f / I for Optional User Defined Storm CUHP:  | 0.1            | 0.0            | 0.1            | 0.0                   | 0.0           | 0.0            |                |                |                |               |                 |              |            |    |
| IRF for WQCV Event:  | 0.00           | 0.00           | 0.00           | 0.00                  | 0.00          | 0.00           |                |                |                |               |                 |              |            |    |
| IRF for 10-Year Event:   | 1.00           | 0.83           | 0.90           | 0.81                  | 0.25          | 0.81           |                |                |                |               |                 |              |            |    |
| IRF for 100-Year Event:  | 1.00           | 0.84           | 0.95           | 0.83                  | 0.25          | 0.83           |                |                |                |               |                 |              |            |    |
| IRF for Optional User Defined Storm CUHP:  |                |                |                |                       |               |                |                |                |                |               |                 |              |            | _  |
| Total Site Imperviousness: I <sub>total</sub>  | 14.7%          | 47.0%          | 33.8%          | 40.0%                 | 6.8%          | 40.0%          |                |                |                |               |                 |              |            |    |
| Effective Imperviousness for WQCV Event:   | 0.0%           | 0.0%           | 0.0%           | 0.0%                  | 0.0%          | 0.0%           |                |                |                |               |                 |              |            |    |
| Effective Imperviousness for 10-Year Event:<br>Effective Imperviousness for 100-Year Event:                    | 14.7%<br>14.7% | 39.0%<br>39.6% | 30.3%<br>32.0% | 32.4%<br>33.0%        | 1.7%          | 32.4%<br>33.0% |                |                |                |               |                 |              | <u> </u>   |    |
| Effective Imperviousness for 100-Year Event:<br>Effective Imperviousness for Optional User Defined Storm CUHP: | 14./70         | 53.0%          | 32.0%          | 33.0%                 | 1./70         | 33.0%          |                |                |                |               |                 | 1            | <u> </u>   |    |
|  | ļ              |                |                | ı – I                 |               | 1              |                | 1              | 1              |               |                 |              | I          |    |
| D / EFFECTIVE IMPERVIOUSNESS CREDITS   |                |                |                |                       |               |                |                |                |                |               |                 |              |            |    |
| D / EFFECTIVE IMPERVIOUSNESS CREDITS<br>WQCV Event CREDIT: Reduce Detention By:                                | N/A            | N/A            | N/A            | N/A                   | N/A           | N/A            | N/A            | N/A            | N/A            | N/A           | N/A             | N/A          | N/A        | N/ |
| 10-Year Event CREDIT**: Reduce Detention By:   | 0.0%           | 17.9%          | 11.0%          | 19.9%                 | 106.9%        | 19.9%          | N/A            | N/A            | N/A            | N/A           | N/A             | N/A          | N/A<br>N/A | N/ |
| 100-Year Event CREDIT**: Reduce Detention By:<br>User Defined CUHP CREDIT: Reduce Detention By:                | 0.0%           | 15.6%          | 5.4%           | 17.7%                 | 106.2%        | 17.7%          | N/A            | N/A            | N/A            | N/A           | N/A             | N/A          | N/A        | N/ |
| User Defined CUHP CREDIT: Reduce Detention By:   | L              | l              | I              | II                    |               | I              | l              | 1              | I              | I             | I               | 1            | I          |    |
|  | Total Site Im  | perviousness:  | 38.6%          |                       | Notes:        |                |                |                |                |               |                 |              |            |    |
| Total Site Effective Impe  | rviousness for | WQCV Event:    | 0.0%           | 1                     | * Use Green-  | Ampt average   | e infiltration | rate values fr | om Table 3-3   |               |                 |              |            |    |
| Total Site Effective Imper   |                |                | 31.5%          |                       | ** Flood cont | rol detention  | volume crec    | lits based on  | empirical equ  | ations from S |                 | ter of USDCM |            |    |
| Total Site Effective Impervi   | ousness for 10 | 0-Year Event:  | 32.2%          | 1                     | *** Method    | assumes that   | 1-hour raint   | all depth is e | quivalent to : | 1-hour intens | ity for calcula | tion purpose | d          |    |

Depth Increment = 0.50

ft

Stage - Storage Stage Override Length Width Area Override Area Volume Volume

MHFD-Detention, Version 4.04 (February 2021)

#### Project: FALCON HIGHLANDS FILING NO. 3 Basin ID: DETENTION POND 1 (BASINS A, B, OS-1, OS-2, OS-4, OS-5)

| T                   |           |
|---------------------|-----------|
| VOLUME, DATE ; MOOT | -         |
|                     | <br>- and |

3041 m0 3 same a Example Zone Configuration (Retention Pond)

#### -Watershed Information

| Selected BMP Type =                     | EDB        |         |
|---|------------|---------|
| Watershed Area =                        | 126.38     | acres   |
| Watershed Length =                      | 3,600      | ft      |
| Watershed Length to Centroid =          | 800        | ft      |
| Watershed Slope =                       | 0.010      | ft/ft   |
| Watershed Imperviousness =              | 38.60%     | percent |
| Percentage Hydrologic Soil Group A =    | 100.0%     | percent |
| Percentage Hydrologic Soil Group B =    | 0.0%       | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |
|   |            |         |

### After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

| the embedded colorado orban nyare      | graphinocedu | ile.      |
|--|--------------|-----------|
| Water Quality Capture Volume (WQCV) =  | 1.855        | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 5.232        | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 3.933        | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 5.308        | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 6.402        | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 8.551        | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 10.629       | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 13.365       | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 19.250       | acre-feet |
| Approximate 2-yr Detention Volume =    | 3.326        | acre-feet |
| Approximate 5-yr Detention Volume =    | 4.408        | acre-feet |
| Approximate 10-yr Detention Volume =   | 5.445        | acre-feet |
| Approximate 25-yr Detention Volume =   | 6.771        | acre-feet |
| Approximate 50-yr Detention Volume =   | 7.678        | acre-feet |
| Approximate 100-yr Detention Volume =  | 8.962        | acre-feet |
|  |              |           |

| Define | Zones | and | Basin  | Geomet   | ry |
|--------|-------|-----|--------|----------|----|
|        |       | ž   | Zone 1 | Volume ( | WQ |

| Zone 1 Volume (WQCV) =                                  | 1.855 | acre-feet       |
|---|-------|-----------------|
| Zone 2 Volume (EURV - Zone 1) =                         | 3.377 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 3.731 | acre-feet       |
| Total Detention Basin Volume =                          | 8.962 | acre-feet       |
| Initial Surcharge Volume (ISV) =                        | user  | ft <sup>3</sup> |
| Initial Surcharge Depth (ISD) =                         | user  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | user  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | user  | ft              |
| Slope of Trickle Channel (STC) =                        | user  | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | user  | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | user  |                 |
|   |       |                 |

acre-feet

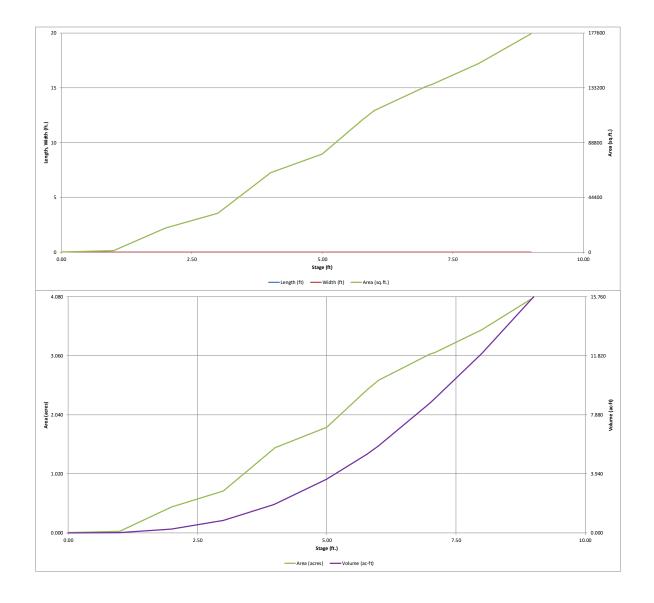
| Initial Surcharge Area (A <sub>ISV</sub> ) = | user | ft 2            |
|--|------|-----------------|
| Surcharge Volume Length $(L_{ISV}) =$        | user | ft              |
| Surcharge Volume Width $(W_{ISV}) =$         | user | ft              |
| Depth of Basin Floor $(H_{FLOOR}) =$         | user | ft              |
| Length of Basin Floor $(L_{FLOOR}) =$        | user | ft              |
| Width of Basin Floor $(W_{FLOOR}) =$         | user | ft              |
| Area of Basin Floor $(A_{FLOOR}) =$          |      | ft 2            |
| Volume of Basin Floor ( $V_{FLOOR}$ ) =      | user | ft <sup>3</sup> |
| Depth of Main Basin $(H_{MAIN}) =$           | user | ft              |
| Length of Main Basin $(L_{MAIN}) =$          | user | ft              |
| Width of Main Basin $(W_{MAIN}) =$           |      | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =    | user | ft 2            |
| Volume of Main Basin ( $V_{MAIN}$ ) =        | user | ft <sup>3</sup> |

Calculated Total Basin Volume (V<sub>total</sub>) = user acre-feet

| tion Pond)   |           | Stage - Storage  | Stage | Override   | Length | Width | Area               | Override                | Area   | Volume  | Volume   |
|--------------|-----------|------------------|-------|------------|--------|-------|--------------------|-------------------------|--------|---------|----------|
|              |           | Description      | (ft)  | Stage (ft) | (ft)   | (ft)  | (ft <sup>2</sup> ) | Area (ft <sup>2</sup> ) | (acre) | (ft 3)  | (ac-ft)  |
|              |           | Top of Micropool |       | 0.00       |        |       |                    | 0                       | 0.000  |         |          |
|              |           | 6808             |       | 0.01       |        |       | -                  | 130                     | 0.003  | 0       | 0.000    |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           | 6809             |       | 1.00       | -      |       | -                  | 1,115                   | 0.026  | 617     | 0.014    |
|              |           | 6810             |       | 2.00       |        |       |                    | 19,471                  | 0.447  | 10,909  | 0.250    |
|              |           | 6811             |       | 3.00       | -      |       | -                  | 31,417                  | 0.721  | 36,353  | 0.835    |
|              |           | WQCV: 6811.95    |       | 3.95       | -      |       |                    | 62,250                  | 1.429  | 80,845  | 1.856    |
|              |           |                  |       |            |        |       | -                  |                         |        |         |          |
|              |           | 6812             |       | 4.00       |        |       |                    | 64,054                  | 1.470  | 84,003  | 1.928    |
|              |           | 6813             |       | 5.00       |        |       |                    | 79,388                  | 1.822  | 155,724 | 3.575    |
|              |           | EURV: 6813.78    |       | 5.78       |        |       |                    | 107,566                 | 2.469  | 228,636 | 5.249    |
|              |           | 6814             |       | 6.00       |        |       |                    | 114,850                 | 2.637  | 253,102 | 5.810    |
|              |           |                  |       |            |        |       | -                  |                         |        |         |          |
|              |           | 6815             |       | 7.00       | -      |       |                    | 134,572                 | 3.089  | 377,813 | 8.673    |
|              |           | 100-YR: 6815.5   |       | 7.10       |        |       |                    | 135,660                 | 3.114  | 391,324 | 8.984    |
|              |           | 6816             |       | 8.00       | -      |       | -                  | 152,967                 | 3.512  | 521,206 | 11.965   |
|              |           | TOP: 6817        |       | 9.00       | -      |       | -                  | 177,276                 | 4.070  | 686,328 | 15.756   |
|              |           | 101.0017         |       | 5.00       |        |       |                    | 1/7,2/0                 | 4.070  | 000,520 | 15.750   |
| Optional Use |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              | acre-feet |                  |       |            |        |       |                    |                         |        |         |          |
|              | acre-feet |                  |       |            | -      |       | -                  |                         |        |         |          |
| 1.19         | inches    |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
| 1.50         | inches    |                  |       |            | -      |       |                    |                         |        |         |          |
| 1.75         | inches    |                  |       |            |        |       |                    |                         |        |         |          |
| 2.00         | inches    |                  |       |            |        |       |                    |                         |        |         |          |
| 2.25         | inches    |                  |       |            |        |       |                    |                         |        |         |          |
|              | +         |                  |       |            |        |       |                    |                         |        |         |          |
| 2.52         | inches    |                  |       |            |        |       |                    |                         |        |         |          |
|              | inches    |                  |       |            | -      | -     | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         | -      |         |          |
|              |           |                  |       |            | -      |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         | <u> </u> |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       | -                  |                         |        |         | <u> </u> |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         | <u> </u> |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        | i       |          |
|              |           |                  |       |            |        | -     | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         | _      |         |          |
|              |           |                  |       |            | 1 1    |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        | ĺ       | <u> </u> |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | 1 1    | 1 1   | 1 1                |                         |        |         |          |
|              |           |                  |       |            | -      | -     | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         | <u> </u> |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      | -     | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      | -     | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        | 1 1   |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         | <u> </u> |
|              |           |                  |       |            | 1 1    |       | 1 1                |                         |        |         | <u> </u> |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |
|              |           |                  |       |            | -      |       | -                  |                         |        |         |          |
|              |           |                  |       |            |        |       |                    |                         |        |         |          |

#### MHFD-Detention\_v4 04\_POND 1.xlsm, Basin

MHFD-Detention, Version 4.04 (February 2021)



| Site-Level  |  | •   | •   | n <mark>ent (Ll</mark><br>ervious R |                     | •           |                | •                               | ous Cal                        | culator       |              |              |            |            |
|---|--|---|---|-------------------------------------|---------------------|-------------|----------------|---------------------------------|--------------------------------|---------------|--------------|--------------|------------|------------|
|   |  |   |   | -BMP (Version                       |                     |             | ,              |                                 |                                |               |              |              |            |            |
| User Input  |  |   |   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Calculated cells  |  |   |   | Designer:                           | Richa               | d Lyon, PE  |                |                                 |                                |               |              |              |            |            |
| calculated cells  |  |   |   | Company:                            | Atwel               |             |                |                                 |                                |               |              |              |            |            |
| ••••Design Storm: 1-Hour Rain Depth WQCV Event  | 0.60   | inches  |   | Date:                               |                     | 15, 2022    |                |                                 |                                |               |              |              |            |            |
| ***Minor Storm: 1-Hour Rain Depth 10-Year Event   | 1.19   | inches  |   | Project:                            | Falco               | Highlands   | - Pond 2 T     | ributary Ba                     | sins                           |               |              |              |            |            |
| ***Major Storm: 1-Hour Rain Depth 100-Year Event  | 2.52   | inches  |   | Location:                           | El Pas              | o County    |                |                                 |                                |               |              |              |            |            |
| Optional User Defined Storm CUHP  |  |   |   | -                                   |                     |             |                |                                 |                                |               |              |              |            |            |
| (CUHP) NOAA 1 Hour Rainfall Depth and Frequency<br>for User Defined Storm 100-Year Event  |  |   |   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Max Intensity for Optional User Defined Storm 0   |  |   |   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| TE INFORMATION (USER-INPUT)   |  |   |   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Sub-basin Identifier  | с  | OS-3  | OS-6  |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Receiving Pervious Area Soil Type   | Sand   | Sand  | Sand  |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)  | 64.680   | 1.140   | 35.750  |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Directly Connected Impervious Area (DCIA, acres)  | 0.000  | 0.000   | 0.000   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Unconnected Impervious Area (UIA, acres)  | 24.836   | 1.140   | 8.938   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Receiving Pervious Area (RPA, acres)  | 39.844   | 0.000   | 26.813  |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Separate Pervious Area (SPA, acres)   | 0.000  | 0.000   | 0.000   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| RPA Treatment Type: Conveyance (C),<br>Volume (V), or Permeable Pavement (PP)   | v  | v   | v   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Directly Connected Impervious Area (DCIA, %)<br>Unconnected Impervious Area (DIA, %)<br>Receiving Pervious Area (RPA, %)<br>Separate Pervious Area (RPA, %)<br>, (RPA/ UIA)<br>, Check<br>f / I for UOC Vexent:<br>f / I for 10-Year Event:<br>f / I for 10-Year Event:<br>f / I for 10-Year Event:<br>IRF for 10-Year Event: | 0.0%<br>38.4%<br>61.6%<br>0.0%<br>1.604<br>0.380<br>9.8<br>0.6<br>0.6<br>0.6<br>0.0<br>0.00<br>0.80<br>0.82<br>38.4% | 0.0%<br>100.0%<br>0.0%<br>0.00%<br>0.000<br>1.000<br>9.8<br>0.6<br>0.6<br>0.6<br>0.00<br>1.00<br>1.00<br>1.00 | 0.0%<br>25.0%<br>75.0%<br>0.0%<br>3.000<br>0.250<br>9.8<br>0.6<br>0.6<br>0.6<br>0.00<br>0.73<br>0.75<br>25.0% |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Effective Imperviousness for WQCV Event:  | 0.0%   | 0.0%  | 0.0%  |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Effective Imperviousness for 10-Year Event:   | 30.8%  | 100.0%  | 18.4%   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| Effective Imperviousness for 100-Year Event:<br>Effective Imperviousness for Optional User Defined Storm CUHP:  | 31.3%  | 100.0%  | 18.7%   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| / EFFECTIVE IMPERVIOUSNESS CREDITS  |  |   |   |                                     |                     |             |                |                                 |                                |               |              |              |            |            |
| WQCV Event CREDIT: Reduce Detention By:   | N/A  | N/A   | N/A   | N/A                                 | N/A                 | N/A         | N/A            | N/A                             | N/A                            | N/A           | N/A          | N/A          | N/A        | N/#        |
| 10-Year Event CREDIT**: Reduce Detention By:<br>100-Year Event CREDIT**: Reduce Detention By:   | 21.0%<br>18.8%   | 0.0%  | 28.8%<br>26.7%  | N/A<br>N/A                          | N/A<br>N/A          | N/A<br>N/A  | N/A<br>N/A     | N/A<br>N/A                      | N/A<br>N/A                     | N/A<br>N/A    | N/A<br>N/A   | N/A<br>N/A   | N/A<br>N/A | N/A<br>N/A |
| User Defined CUHP CREDIT: Reduce Detention By:<br>Total Site Effective Imperv<br>Total Site Effective Impervi<br>Total Site Effective Imperviousness for Optiona  | Total Site Imp<br>viousness for V<br>iousness for 100<br>ousness for 100   | erviousness:<br>WQCV Event:<br>D-Year Event:<br>D-Year Event:   | 34.4%<br>0.0%<br>27.2%<br>27.7%   |                                     | Notes:<br>Use Green | Ampt averag | e infiltration | rate values fi<br>lits based on | rom Table 3-3<br>empirical equ | ations from S | itorage Chap | ter of USDCM |            |            |

Depth Increment = 0.50

Stage - Storage Stage Override

ft

Length

Width Area Override Area Volume Volume  $(f_{2}^{(0)})$   $(f_{2}^{(0)})$   $(f_{2}^{(0)})$   $(f_{2}^{(0)})$   $(f_{2}^{(0)})$   $(f_{2}^{(0)})$ 

#### Project: FALCON HIGHLANDS FILING NO. 3 Basin ID: DETENTION POND 2 (BASINS C, OS-3, OS-6)

|                   | ( dom: |   |
|-------------------|--------|---|
| where and weather |        |   |
|                   |        | 2 |
|                   | , / /  |   |

Example Zone Configuration (Retention Pond) ADD

#### Watershed Information

| EDB  |   |  |  |  |  |  |  |
|--|---|--|--|--|--|--|--|
| 101.57   | acres   |  |  |  |  |  |  |
| 2,450  | ft  |  |  |  |  |  |  |
| 1,500  | ft  |  |  |  |  |  |  |
| 0.010  | ft/ft   |  |  |  |  |  |  |
| 34.40%   | percent   |  |  |  |  |  |  |
| 100.0%   | percent   |  |  |  |  |  |  |
| 0.0%   | percent   |  |  |  |  |  |  |
| 0.0%   | percent   |  |  |  |  |  |  |
| 40.0   | hours   |  |  |  |  |  |  |
| Location for 1-hr Rainfall Depths = User Input |   |  |  |  |  |  |  |
|  | 101.57<br>2,450<br>1,500<br>0.010<br>34.40%<br>100.0%<br>0.0%<br>0.0%<br>40.0 |  |  |  |  |  |  |

### After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

| the embedded colorado orban nydrograph nocedare. |        |           |  |  |  |  |  |  |
|--|--------|-----------|--|--|--|--|--|--|
| Water Quality Capture Volume (WQCV) =            | 1.393  | acre-feet |  |  |  |  |  |  |
| Excess Urban Runoff Volume (EURV) =              | 3.628  | acre-feet |  |  |  |  |  |  |
| 2-yr Runoff Volume (P1 = 1.19 in.) =             | 2.642  | acre-feet |  |  |  |  |  |  |
| 5-yr Runoff Volume (P1 = 1.5 in.) =              | 3.596  | acre-feet |  |  |  |  |  |  |
| 10-yr Runoff Volume (P1 = 1.75 in.) =            | 4.369  | acre-feet |  |  |  |  |  |  |
| 25-yr Runoff Volume (P1 = 2 in.) =               | 6.102  | acre-feet |  |  |  |  |  |  |
| 50-yr Runoff Volume (P1 = 2.25 in.) =            | 7.738  | acre-feet |  |  |  |  |  |  |
| 100-yr Runoff Volume (P1 = 2.52 in.) =           | 9.913  | acre-feet |  |  |  |  |  |  |
| 500-yr Runoff Volume (P1 = 3.14 in.) =           | 14.576 | acre-feet |  |  |  |  |  |  |
| Approximate 2-yr Detention Volume =              | 2.295  | acre-feet |  |  |  |  |  |  |
| Approximate 5-yr Detention Volume =              | 3.051  | acre-feet |  |  |  |  |  |  |
| Approximate 10-yr Detention Volume =             | 3.789  | acre-feet |  |  |  |  |  |  |
| Approximate 25-yr Detention Volume =             | 4.746  | acre-feet |  |  |  |  |  |  |
| Approximate 50-yr Detention Volume =             | 5.426  | acre-feet |  |  |  |  |  |  |
| Approximate 100-yr Detention Volume =            | 6.452  | acre-feet |  |  |  |  |  |  |
|  |        |           |  |  |  |  |  |  |

| Define | Zones | and | Basin | Geometry |  |
|--------|-------|-----|-------|----------|--|
|        |       |     |       |          |  |

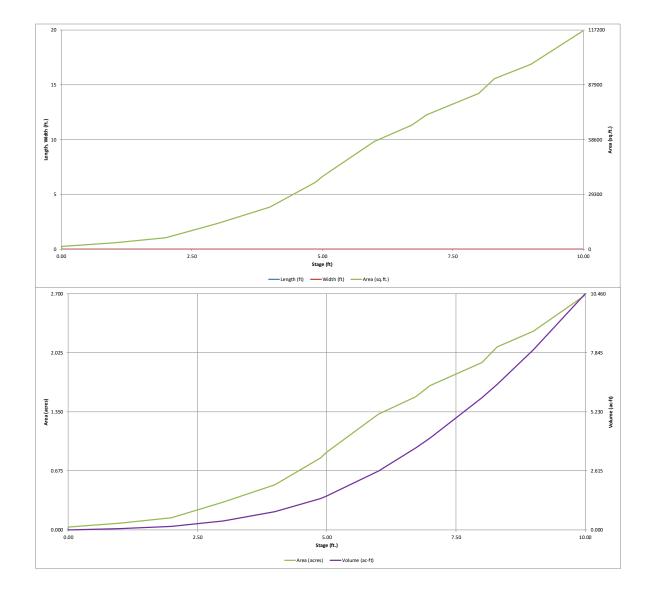
| Define Zones and Basin Geometry                         |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 1.393 | acre-feet       |
| Zone 2 Volume (EURV - Zone 1) =                         | 2.235 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 2.824 | acre-feet       |
| Total Detention Basin Volume =                          | 6.452 | acre-feet       |
| Initial Surcharge Volume (ISV) =                        | user  | ft <sup>3</sup> |
| Initial Surcharge Depth (ISD) =                         | user  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | user  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | user  | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | user  | ft/ft           |
| Slopes of Main Basin Sides (Smain) =                    | user  | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | user  |                 |
|   |       |                 |
|   |       |                 |

| Initial Surcharge Area $(A_{ISV}) =$            | user | ft <sup>2</sup> |
|---|------|-----------------|
| Surcharge Volume Length $(L_{ISV}) =$           | user | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =    | user | ft              |
| Depth of Basin Floor $(H_{FLOOR}) =$            | user | ft              |
| Length of Basin Floor $(L_{FLOOR}) =$           | user | ft              |
| Width of Basin Floor $(W_{FLOOR}) =$            | user | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =     | user | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =   | user | ft <sup>3</sup> |
| Depth of Main Basin $(H_{MAIN}) =$              | user | ft              |
| Length of Main Basin ( $L_{MAIN}$ ) =           | user | ft              |
| Width of Main Basin ( $W_{MAIN}$ ) =            | user | ft              |
| Area of Main Basin $(A_{MAIN}) =$               | user | ft <sup>2</sup> |
| Volume of Main Basin ( $V_{MAIN}$ ) =           | user | ft <sup>3</sup> |
| Calculated Total Basin Volume ( $V_{total}$ ) = | user | acre-feet       |
|   |      |                 |

| ition Pond)   |             | Description      | (ft) | Stage (ft) | (ft) | (ft) | (ft <sup>2</sup> ) | Area (ft <sup>2</sup> ) | (acre) | (ft <sup>3</sup> ) | (ac-ft) |
|---------------|-------------|------------------|------|------------|------|------|--------------------|-------------------------|--------|--------------------|---------|
|               |             | Top of Micropool |      | 0.00       |      |      | -                  | 0                       | 0.000  | ( )                | (,      |
|               |             | 6807.5           |      | 0.01       |      |      |                    | 1,425                   | 0.033  | 5                  | 0.000   |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             | 6808.5           |      | 1.00       |      |      | -                  | 3,320                   | 0.076  | 2,354              | 0.054   |
|               |             | 6809.5           |      | 2.00       |      |      |                    | 6,004                   | 0.138  | 7,016              | 0.161   |
|               |             | 6810.5           |      | 3.00       | -    |      | -                  | 13,803                  | 0.317  | 16,919             | 0.388   |
|               |             | 6811.5           |      | 4.00       | -    |      | -                  | 22,457                  | 0.516  | 35,049             | 0.805   |
|               |             | WQCV: 6812.38    |      | 4.88       | -    |      | -                  | 35,840                  | 0.823  | 60,700             | 1.393   |
|               |             | 6812.5           |      | 5.00       | -    |      | -                  | 38,755                  | 0.890  | 65,175             | 1.496   |
|               |             | 6813.5           |      | 6.00       | -    |      | -                  | 57,667                  | 1.324  | 113,386            | 2.603   |
|               |             | EURV: 6814.22    |      | 6.72       |      |      | -                  | 66,330                  | 1.523  | 158,025            | 3.628   |
|               |             | 6814.5           |      | 7.00       | -    |      |                    | 71,775                  | 1.648  | 177,360            | 4.072   |
|               |             | 6815.5           |      | 8.00       | -    |      |                    | 83,300                  | 1.912  | 254,897            | 5.852   |
|               |             | 100-YR: 6815.8   |      | 8.30       |      |      | -                  | 91,100                  | 2.091  | 281,057            | 6.452   |
|               |             | 6816.5           |      | 9.00       |      |      |                    | 98,912                  | 2.271  | 347,562            | 7.979   |
| Optional User | r Overrides | TOP: 6817.5      |      | 10.00      |      |      |                    | 116,945                 | 2.685  | 455,490            | 10.457  |
|               | acre-feet   | 1011001715       |      | 10.00      |      |      |                    | 110,515                 | 2.005  | 155,150            | 10.157  |
|               | acre-feet   |                  |      |            | -    |      | -                  |                         |        |                    |         |
| 1.19          |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
| -             | inches      |                  |      |            |      |      |                    |                         |        |                    |         |
|               | inches      |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               | inches      |                  |      |            |      |      | -                  |                         |        |                    |         |
|               | inches      |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               | inches      |                  |      |            | -    |      | -                  |                         |        |                    |         |
| 2.52          | inches      |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               | inches      |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | 1    | -    | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    | -    | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    | -    | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      |                    |                         |        |                    |         |
|               |             |                  | -    |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    | -    | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      |                    |                         | -      | -                  | -       |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         | -      | -                  | -       |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            |      | 1 1  | 1 1                |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | 1 1  |      |                    |                         | 1      |                    | 1       |
|               |             |                  |      |            |      |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        | L                  |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            | -    |      | -                  |                         |        |                    |         |
|               |             |                  |      |            |      |      |                    |                         |        |                    |         |

#### MHFD-Detention\_v4 04\_POND 2.xlsm, Basin

MHFD-Detention, Version 4.04 (February 2021)



### **APPENDIX F**

### **REFERENCE CALCULATIONS AND MAPS**

(SF-05-033)

### FALCON HIGHLANDS FILING NO. 2 PDR BASINS (Area Runoff Coefficient Summary)

|            |               | STREE   | TS / DEVEI | LOPED | OVERLAN | VD / UNDEV | ELOPED           | COMPO | SITE C |
|------------|---------------|---------|------------|-------|---------|------------|------------------|-------|--------|
| BASIN      | TOTAL<br>AREA | AREA    | C5         | C100  | AREA    | C,         | C <sub>100</sub> | C5    | C100   |
|            | (Acres)       | (Acres) |            |       | (Acres) |            |                  |       |        |
| A          | 13.09         | 4.67    | 0.50       | 0.60  | 8.41    | 0.25       | 0.35             | 0.34  | 0.44   |
| B1.1       | 7.39          | 7.39    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B1.2       | 7.22          | 7.22    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B2         | 4.00          | 4.00    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B3         | 7.97          | 7.97    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B4.1       | 4.13          | 4.13    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B4.2       | 13.98         | 13.36   | 0.50       | 0.60  | 0.62    | 0.25       | 0.35             | 0.49  | 0.59   |
| B5         | 11.63         | 11.63   | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B6.1       | 5.44          | 5.44    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B6.2       | 3.23          | 2.73    | 0.50       | 0.60  | 0.50    | 0.25       | 0.35             | 0.46  | 0.56   |
| B6.3       | 4.61          | 4.11    | 0.50       | 0.60  | 0.50    | 0.25       | 0.35             | 0.47  | 0.57   |
| B6.4       | 1.39          | 1.39    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B7.1       | 4.36          | 4.36    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B7.2       | 3.80          | 3.04    | 0.50       | 0.60  | 0.76    | 0.25       | 0.35             | 0.45  | 0.55   |
| B7.3       | 5.64          | 5.64    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| <b>B</b> 8 | 7.44          | 7.44    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B9,1       | 5.06          | 5.06    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B9.2       | 3.40          | 3.40    | 0.50       | 0.60  | 0.00    | 0.25       | 0.35             | 0.50  | 0.60   |
| B10.1      | 5.40          | 5.40    | 0.45       | 0.55  | 0.00    | 0.25       | 0.35             | 0.45  | 0.55   |
| B10.2      | 1.04          | 1.04    | 0.45       | 0.55  | 0.00    | 0.25       | 0.35             | 0.45  | 0.55   |

2010 FDR TABULATIONS WERE USED TO QUANTIFY FILING NO. 2 OFFSITE RUNOFF AS DEVELOPED CONDITIONS FOR THE EXISTING CONDITIONS OF THIS REPORT.

THESE CALCULATION SHEETS ARE FROM THE 2010 FINAL DRAINAGE REPORT BY TERRA NOVA. THE TITLE SAYS "PDR BASINS" BUT THESE ARE FDR CALCULATIONS WITHIN THE FDR.

### FALCON HIGHLANDS FILING NO. 2 PDR BASINS (Area Runoff Coefficient Summary)

| C1.1 | 7.80  | 7.04  | 0.45 | 0.55 | 0.75 | 0.25 | 0.35 | 0.43     | 0.53 |
|------|-------|-------|------|------|------|------|------|----------|------|
| C1.2 | 4.34  | 4.34  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C2.1 | 5.05  | 5.05  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C2.2 | 6.52  | 6.52  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C2.3 | 1.39  | 1.39  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| С3   | 2.52  | 2.52  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C4   | 13.26 | 10.01 | 0.45 | 0.55 | 3.25 | 0.25 | 0.35 | 0.40     | 0.50 |
| C5   | 8.68  | 7.47  | 0.45 | 0.55 | 1.21 | 0.25 | 0.35 | 0.42     | 0.52 |
| C6   | 4.81  | 4.81  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0,55 |
| C7   | 7.09  | 4.87  | 0.45 | 0.55 | 2.23 | 0.25 | 0.35 | 0.39     | 0.49 |
| C8.1 | 8.70  | 8.70  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C8.2 | 3.45  | 3.45  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C9.1 | 6.29  | 6.29  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| C9.2 | 3.14  | 3.14  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| CIØ  | 3.67  | 3.67  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| DI.I | 10.81 | 10.81 | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| D1.2 | 1.19  | 1.19  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| D2   | 4.48  | 4.48  | 0.45 | 0.55 | 0.00 | 0.25 | 0.35 | 0.45     | 0.55 |
| D3   | 14.62 | 14.62 | 0.90 | 0.95 | 0.00 | 0.25 | 0,35 | 0.90     | 0.95 |
| E    | 1.95  | 0.00  | 0.50 | 0.60 | 1.95 | 0.25 | 0.35 | 0.25     | 0.35 |
| F    | 6.51  | 0.00  | 0.50 | 0.60 | 6.51 | 0.25 | 0.35 | 0.25     | 0.35 |
| G    | 8.84  | 0.00  | 0.50 | 0.60 | 8.84 | 0.25 | 0.35 | 0.25     | 0.35 |
| 0S-1 | 6.38  | 6.38  | 0.50 | 0.60 | 0.00 | 0.25 | 0.35 | 0.50     | 0.60 |
| OS-2 | 3.12  | 3.12  | 0.90 | 0.95 | 0.00 | 0.25 | 0.35 | 0.90     | 0.95 |
| OS-3 | 1.14  | 1.14  | 0.90 | 0.95 | 0.00 | 0.25 | 0.35 | 0.90     | 0.95 |
|      |       | ····· |      |      |      |      |      | <u> </u> |      |

Calculated by: QNA

Date: 07/15/05

## (Area Drainage Summary)

|                  | ······ |                          | WEIG.                 | HTED                   |                | OVER           | LAND           |                         | STRE           | ET / CH      | ANNEL F           | LOW                     | T <sub>1</sub> | Te USED | INTE?         | VSITY                       | TOTAL                   | FLOWS         |
|------------------|--------|--------------------------|-----------------------|------------------------|----------------|----------------|----------------|-------------------------|----------------|--------------|-------------------|-------------------------|----------------|---------|---------------|-----------------------------|-------------------------|---------------|
|                  | BASIN  | AREA<br>TOTAL<br>(Acres) | C5<br>* For Colas Ser | C100<br>Runo/J Summory | C <sub>s</sub> | Length<br>(fl) | Height<br>(fl) | T <sub>C</sub><br>(min) | Length<br>(17) | Slope<br>(%) | Velocity<br>(fps) | T <sub>i</sub><br>(min) | TOTAL<br>(min) | (min)   | Is<br>(in/hr) | I <sub>100</sub><br>(in/hr) | Q <sub>5</sub><br>(cfs) | Q100<br>(cfs) |
| <mark>S-4</mark> | A      | 13.09                    | 0.34                  | 0.44                   | 0.25           | 105            | 2.1            | 13,0                    | 1625           | 1.5%         | 2.4               | 11.3                    | 24.2           | 24.2    | 2.8           | 4.6                         | 12.3                    | 26.3          |
|                  | B1.1   | 7.39                     | 0,50                  | 0,60                   | 0.25           | :70            | 3.4            | 16.5                    | 1700           | 1.5%         | 2.4               | 11,8                    | 28.3           | 28.3    | 2.6           | 4.2                         | 9.5                     | 18.6          |
|                  | B1.2   | 7.22                     | 0,50                  | 0,60                   | 0,25           | 170            | 3.4            | 16.5                    | 1400           | 2.0%         | 2.9               | 8.0                     | 24.5           | 24.5    | 2.8           | 4,6                         | 10.0                    | 19.7          |
|                  | B2     | 4.00                     | 0.50                  | 0.60                   | 0.25           | 200            | 4,0            | 17,9                    | 333            | 0.9%         | 1.9               | 2.9                     | 20.8           | 20,8    | 3.0           | 5.0                         | 6.0                     | 11.9          |
| /                | B3     | 7.97                     | 0,50                  | 0.60                   | 0.25           | 135            | 2,7            | 14.7                    | 885            | 0.9%         | 1.9               | 7,8                     | 22,5           | 22.5    | 2.9           | 4,8                         | 11.5                    | 22.8          |
| PIPE<br>SED      | B4.1   | 4.13                     | 0.50                  | 0.60                   | 0.25           | 165            | 3.3            | 16.2                    | 1550           | 1,3%         | 2.2               | 11.7                    | 28.0           | 28.0    | 2.6           | 4.2                         | 5.3                     | 10.5          |
|                  | B4.2   | 13.98                    | 0.49                  | 0.59                   | 0.25           | 165            | 3.3            | 16.2                    | 1551           | 1.3%         | 2.2               | 11,8                    | 28.0           | 28.0    | 2,6           | 4.2                         | 17.6                    | 34.7          |
|                  | B5     | 11.63                    | 0,50                  | 0.60                   | 0,25           | 210            | 4.2            | 18.3                    | 1100           | 2.0%         | 2.9               | 6,3                     | 24.6           | 24.6    | 2.8           | 4.5                         | 16.0                    | 31.7          |
|                  | B6.1   | 5.44                     | 0.50                  | 0.60                   | 0.25           | 160            | 3.2            | 16,0                    | 1180           | 0.7%         | 1.8               | 10.9                    | 26.9           | 26.9    | 2.6           | 4.3                         | 7.1                     | 14.1          |
|                  | B6.2   | 3.23                     | 0.46                  | 0.56                   | 0.25           | 140            | 2.8            | 15.0                    | 850            | 0.7%         | 18                | 7.9                     | 22.8           | 22.8    | 2.9           | 4.7                         | 4.3                     | 8.6           |
|                  | B6.3   | 4.61                     | 0.47                  | 0.57                   | 0.25           | 60             | 1,2            | 9.8                     | 1150           | 0.6%         | 16                | 12.0                    | 21.8           | 21.8    | 2.9           | 4.9                         | 6.4                     | 12.8          |
|                  | B6.4   | 1.39                     | 0.50                  | 0.60                   | 0.25           | 60             | 1.2            | 9.8                     | 700            | 0.7%         | 18                | 6.5                     | 16.3           | 16.3    | 3.3           | 5.7                         | 2.3                     | 4.7           |

O: RI

# (Area Drainage Summary)

|              |                          | WEIG                 | HTED             |                | OVER           | LAND          |                         | STRE           | ET / CH      | ANNEL F           | LOW                     | $T_t$          | Te USED | INTE                      | VSITY                       | TOTAL       | FLOWS         |
|--------------|--------------------------|----------------------|------------------|----------------|----------------|---------------|-------------------------|----------------|--------------|-------------------|-------------------------|----------------|---------|---------------------------|-----------------------------|-------------|---------------|
| BASIN        | AREA<br>TOTAL<br>(Acres) | C5<br>•For Cales See | C <sub>100</sub> | C <sub>5</sub> | Length<br>(fl) | Height<br>(1) | T <sub>C</sub><br>(min) | Length<br>(fl) | Slope<br>(%) | Velocity<br>(fps) | T <sub>1</sub><br>(min) | TOTAL<br>(min) | (min)   | I <sub>s</sub><br>(in/ht) | Ĭ <sub>100</sub><br>(in∕hr) | Qs<br>(cfs) | Q106<br>(cfs) |
| <b>B</b> 7.1 | 4.36                     | 0.50                 | 0.60             | 0.25           | 135            | 2.7           | 14.7                    | 660            | 1.0%         | 2.0               | 5.5                     | 20.2           | 20.2    | 3.0                       | 5.1                         | 6.6         | 13.2          |
| B7.2         | 3.80                     | 0,45                 | 0.55             | 0.25           | }40            | 2.8           | 15.0                    | 790            | 0.8%         | 1.9               | 6.9                     | 21.9           | 21.9    | 2.9                       | 4.8                         | 5.0         | 10.           |
| B7.3         | 5.64                     | 0.50                 | 0.60             | 0.25           | 175            | 3.5           | 16.7                    | 1165           | 0.9%         | 1.9               | 10.2                    | 26.9           | 26.9    | 2,6                       | 4.3                         | 7.4         | 14.0          |
| <u>88</u>    | 7,44                     | 0.50                 | 0.60             | 0.25           | 265            | 7.0           | 18.8                    | 860            | 0.9%         | 1.9               | 7.5                     | 26.3           | 26.3    | 2.7                       | 4,4                         | 9.9         | 19            |
| B9.1         | 5.06                     | 0.50                 | 0.60             | 0.25           | 112            | 5.0           | 10.3                    | 2500           | 1.3%         | 2.2               | 18.9                    | 29.2           | 29.2    | 2.5                       | 4.1                         | 6.4         | 12.           |
| B9.2         | 3.40                     | 0.50                 | 0.60             | 0,25           | 50             | 1.0           | 8.9                     | 1610           | 1.4%         | 2.3               | 11,7                    | 20.6           | 20,6    | 3.0                       | 5.0                         | 5.1         | 10.           |
| B10.1        | 5.40                     | 0.45                 | 0,55             | 0.25           | 250            | 5.0           | 20.0                    | 405            | 0.5%         | 1.5               | 4.5                     | 24.5           | 24.5    | 2.8                       | 4,6                         | 6.7         | 13.           |
| B10.2        | 1.04                     | 0,45                 | 0,55             | 0.25           | 50             | 1.0           | 8.9                     | 525            | 0.5%         | 1.5               | 5.8                     | 14.8           | 14.8    | 3.5                       | 5.9                         | 1.6         | 3.            |
| C1.1         | 7.80                     | 0.43                 | 0.53             | 0.25           | 180            | 3.6           | 17.0                    | 1145           | 1.4%         | 2,3               | 8.3                     | 25.3           | 25.3    | 2.7                       | 4.5                         | 9.1         | 18.           |
| C1.2         | 4.34                     | 0.45                 | 0,55             | 0.25           | 180            | 3.6           | 17.0                    | \$50           | 1.1%         | 2.1               | 4.4                     | 21.3           | 21.3    | 3.0                       | 4.9                         | 5.8         | 11.           |
| C2.1         | 5.05                     | 0.45                 | 0.55             | 0.25           | 150            | 3.0           | 15.5                    | 1485           | 1.1%         | 2.1               | 11.8                    | 27.3           | 27.3    | 2.6                       | 4.3                         | 5.9         | 11.           |
| C2.2         | 6.52                     | 0.45                 | 0.55             | 0,25           | 190            | 3.8           | 17.4                    | 780            | 1.0%         | 2.0               | 6.5                     | 23.9           | 23.9    | 2.8                       | 4.6                         | 8.2         | 16.           |
| C2.3         | 1.39                     | 0.45                 | 0,55             | 0.25           | 50             | 2.0           | 7.1                     | 900            | 1.6%         | 2.5               | 6.0                     | 13.1           | 13.1    | 3.7                       | 6.3                         | 2.3         | 4.            |
| <u>C3</u>    | 2.52                     | 0.45                 | 0.55             | 0.25           | 190            | 4.0           | 17.1                    | 140            | 1.6%         | 2.5               | 0.9                     | 18.1           | 18.1    | 3.2                       | 5.4                         | 3.6         | 7.            |

RUN

OS-7, PIP RUN USEI

## (Area Drainage Summary)

|                             |                  |               |                 |                  |                |        | <u></u> |                |        | ,<br>   |          |       |       |              |         |                  |       |                  |
|-----------------------------|------------------|---------------|-----------------|------------------|----------------|--------|---------|----------------|--------|---------|----------|-------|-------|--------------|---------|------------------|-------|------------------|
|                             |                  |               | WEIG.           | HTED             |                | OVER   | LAND    |                | STRE   | ET / CH | ANNEL F  | LOW   | $T_t$ | Te USED      | INTE    | VSITY            | TOTAL | FLOWS            |
|                             |                  |               |                 |                  |                |        |         |                |        |         |          |       |       |              |         |                  |       |                  |
|                             | BASIN            | AREA<br>TOTAL | C <sub>5</sub>  | C <sub>100</sub> | C <sub>5</sub> | Length | Height  | Τ <sub>c</sub> | Length | Slope   | Velocity | T,    | TOTAL |              | Iş      | 1 <sub>109</sub> | Qs    | Q <sub>100</sub> |
|                             |                  | (Acres)       | * For Coles See | Вино/J Биттагу   |                | (1)    | (fl)    | (min)          | (11)   | (%)     | (fps)    | (min) | (min) | (min)        | (in/hr) | (in/hr)          | (cfs) | (cfs)            |
| 7                           | C4               | 13.26         | 0,40            | 0.50             | 0.25           | 250    | 4.0     | 21.5           | 1530   | 1.0%    | 2.0      | 12.8  | 34.3  | 34.3         | 2.3     | 3,7              | 12.3  | 24.8             |
|                             | C5               | 8.68          | 0.42            | 0.52             | 0.25           | 300    | 7.0     | 20.8           | 286    | 1.7%    | 2.6      | 1,8   | 22.6  | 22.6         | 2.9     | 4.8              | 10.5  | 21.6             |
| OS-7, PIPE<br>RUN USED      | C6               | 4.81          | 0.45            | 0.55             | 0.25           | 180    | 3.6     | 17.0           | 390    | 8%      | 2.8      | 2.3   | 19.3  | 19.3         | 3.1     | 5.2              | 6.7   | 13.7             |
|                             | C7               | 7.09          | 0.39            | 0.49             | 0.25           | 180    | 3.6     | 17.0           | 670    | 1.0%    | 2.0      | 5.6   | 22.5  | 22,5         | 2.9     | 4.8              | 7.9   | 16.5             |
|                             | C8.1             | 8.70          | 0.45            | 0,55             | 0.25           | 200    | 4.0     | 17.9           | 1170   | 1.0%    | 2.0      | 9,8   | 27.6  | 27.6         | 2.6     | 4.3              | 10.2  | 20.3             |
|                             | C8.2             | 3.45          | 0.45            | 0.55             | 0.25           | 170    | 3,4     | 16.5           | 645    | 1.2%    | 2.2      | 4.9   | 21.4  | 21.4         | 3.0     | 4.9              | 4.6   | 9.3              |
|                             | C9.1             | 6.29          | 0.45            | 0.55             | 0.25           | 165    | 3.3     | 16.2           | 530    | 1.0%    | 2.9      | 4,4   | 20.7  | 20.7         | 3.0     | 5.0              | 8.5   | 17.3             |
|                             | C9.2             | 3,14          | 0.45            | 0.55             | 0.25           | 180    | 3.6     | 17.0           | 540    | 1.0%    | 2.0      | 4.5   | 21.5  | 21.5         | 2.9     | 4,9              | 4.2   | 8.5              |
|                             | C10              | 3.67          | 0,45            | 0,55             | 0.25           | 185    | 10.0    | 12.4           | 100    | 2.0%    | 2.3      | 0.7   | 13.1  | 13.1         | 3.7     | 6,3              | 6.1   | 12.7             |
|                             | D1.1             | 10.81         | 0.45            | 0.55             | 0.25           | 200    | 4.0     | 17.9           | 1340   | 1.2%    | 2.2      | 10.2  | 28.0  | <b>28</b> .0 | 2.6     | 4.2              | 12.5  | 25.1             |
| OS-7 AND<br>OS-8<br>REVISED | D1.2             | 1.19          | 0.45            | 0.55             | 0.25           | 180    | 3.6     | 17,0           | 630    | 1.0%    | 2.0      | 5.3   | 22.2  | 22.2         | 2.9     | 4.8              | 1.5   | 3.1              |
|                             | D2               | 4.48          | 0.45            | 0.55             | 0,25           | 200    | 4.0     | 17.9           | 320    | 1.6%    | 2.5      | 2.1   | 20.0  | 20.0         | 3.0     | 5,1              | 6.1   | 12.5             |
|                             | D3               | 14.62         | 0,90            | 0.95             | 0,25           | 185    | 10.0    | 12.4           | 103    | 1.9%    | 2.9      | 0.6   | 13.0  | 13.0         | 3,7     | 6.3              | 48.4  | 87.6             |
| BASIN E<br>RECALCULATE      | Ē                | 1.95          | 0,25            | 0.35             | 0.25           | 90     | 5.0     | 8.6            | 1080   | 1.0%    | 2.0      | 9,0   | 17.6  | 17.6         | 3.2     | 5.4              | 1.6   | 3.7              |
|                             | <mark>n -</mark> | L             | £               | L                | 1              | 1      | 1       | 1              |        | 1       | 1        | 1     | 1     | ł            | •       | 1                | ş     | 1                |

## (Area Drainage Summary)

|                         |             |               | WEIG            | HTED           |      | OVER   | LAND   |       | STRE   | ET / CH | ANNEL F  | LOW   | T,    | Te USED | INTE           | <b>SITY</b>      | TOTAL | FLOWS |
|-------------------------|-------------|---------------|-----------------|----------------|------|--------|--------|-------|--------|---------|----------|-------|-------|---------|----------------|------------------|-------|-------|
|                         | BASIN       | AREA<br>TOTAL | C <sub>5</sub>  | CLOG           | C₄   | Length | Height | Тc    | Leugth | Slope   | Velocity | Τ,    | TOTAL |         | I <sub>5</sub> | l <sub>190</sub> | Q5    | Q160  |
| ]                       |             | (Acres)       | * For Cales See | Runoff Summery |      | (1)    | (11)   | (min) | (1)    | (%)     | (fps)    | (min) | (min) | (min)   | (in/hr)        | (in/hr)          | (cfs) | (cfs) |
| BASIN F<br>RECALCULATED | F           | 6,51          | 0.25            | 0.35           | 0.25 | 125    | 4.0    | 12.1  | 630    | 1.6%    | 2.5      | 4.2   | 16,3  | 16.3    | 3.3            | 5,7              | 5.4   | 12.9  |
|                         | G           | 8.84          | 0.25            | 0.35           | 0.25 | 200    | 5.0    | 16.6  | 360    | 1.1%    | 2.1      | 2.9   | 19.5  | 19.5    | 3,1            | 5.2              | 6.8   | 16.0  |
| :                       | OS-1        | 6.38          | 0.50            | 0.60           | 0.25 | 100    | 2.0    | 12.6  | 608    | 2.0%    | 2.8      | 3.6   | 16.3  | 16.3    | 3.4            | 5,7              | 10.7  | 21.7  |
|                         | <i>OS-2</i> | 3.12          | 0,90            | 0.95           | 0.25 | 100    | 2.0    | 12.6  | 1525   | 1.2%    | 2.2      | 11.6  | 24.2  | 24.2    | 2.8            | 4.6              | 7.8   | 13.6  |
|                         | OS-3        | 1.14          | 0,90            | 0.95           | 0.25 | 20     | 0.4    | 5,7   | 1190   | 0.6%    | 1.8      | 11.0  | 16.7  | 16.7    | 3.3            | 5.6              | 3.4   | 6.0   |

Calculated by: QNA

Date: 07/15/05

# (Surface Routing Summary)

|                    |                            |                    |                      |                           | Inte           | nsity | Fl   | ow    |
|--------------------|----------------------------|--------------------|----------------------|---------------------------|----------------|-------|------|-------|
| Design<br>Point(s) | Contributing<br>Basins     | Equivalent<br>CA 5 | Equivalent<br>CA 100 | Maximum<br>T <sub>C</sub> | I <sub>5</sub> | I 100 | Qs   | Q 100 |
| 1                  | B1.1 B1.2 & OS-1           | 10.49              | 12.59                | 28.3                      | 2.6            | 4.2   | 26.9 | 52.8  |
| 2                  | B2 & DP1 F.B.              | 6.51               | 8.39                 | 28.3                      | 2.6            | 4.2   | 16.7 | 35.2  |
| 3                  | B3 AND DP2 F.B.            | 6.03               | 8.31                 | 28.3                      | 2.6            | 4.2   | 15.4 | 34.9  |
| 4                  | B4.1 & B4.2                | 8.90               | 10.71                | 28.0                      | 2.6            | 4.2   | 22.9 | 45.2  |
| 5                  | B5, DP 4 F.B. & DP 13 F.B. | 8.38               | 11.47                | 28.0                      | 2.6            | 4.2   | 21.6 | 48.4  |
| 3 & 5*             | DP-3 & 5                   | 14.41              | 19.79                | 28.3                      | 2.6            | 4.2   | 36.9 | 82.9  |
| 6                  | B6.1, B6.2, B6.3, & B6.4   | 7.08               | 8.55                 | 26.9                      | 2.6            | 4.3   | 18.6 | 36.9  |
| 7                  | B7.1, B7.2 & B7.3          | 6.71               | 8.09                 | 26.9                      | 2.6            | 4.3   | 17.6 | 34.9  |
| 8                  | C1.1 & C1.2                | 5.31               | 6.52                 | 25.3                      | 2.7            | 4.5   | 14.4 | 29.2  |
| 9                  | C2.1 , C2.2 & C2.3         | 5.83               | 7.13                 | 27.3                      | 2.6            | 4.3   | 15.2 | 30.5  |
| 10                 | C3, DP8 & DP9 F.B.         | 4.27               | 6.60                 | 27.3                      | 2.6            | 4.3   | 11.1 | 28.3  |
| 11                 | C4                         | 5.32               | 6.64                 | 34.3                      | 2.3            | 3.7   | 12.3 | 24.8  |
| 12                 | B10.1& B10.2               | 2.90               | 3.54                 | 24.5                      | 2.8            | 4.6   | 8.0  | 16.1  |
| 13                 | B9.1 & B9.2                | 4.23               | 5.07                 | 18.9                      | 3.1            | 5.2   | 13.2 | 26.6  |
| 14                 | C5                         | 3.66               | 4.53                 | 22.6                      | 2.9            | 4.8   | 10.5 | 21.6  |

## (Surface Routing Summary)

| [                  |                        |                    |                      |                           | Inte           | nsity | Fl    | ow    |
|--------------------|------------------------|--------------------|----------------------|---------------------------|----------------|-------|-------|-------|
| Design<br>Point(s) | Contributing<br>Basins | Equivalent<br>CA 5 | Equivalent<br>CA 100 | Maximum<br>T <sub>C</sub> | I <sub>5</sub> | I 100 | Qs    | Q 100 |
| 15                 | C6                     | 2.16               | 2.64                 | 19.3                      | 3.1            | 5.2   | 6.7   | 13.7  |
| 15A                | C7                     | 2.75               | 3.45                 | 22.5                      | 2.9            | 4.8   | 7.9   | 16.5  |
| 16                 | C8.1 & C8.2            | 5.47               | 6.69                 | 27.6                      | 2,6            | 4.3   | 14.2  | 28.4  |
| 17                 | C9.1 & C9.2            | 4.24               | 5.19                 | 21.5                      | 2.9            | 4.9   | 12.5  | 25.4  |
| 18                 | D1.1 & D1.2            | 5.40               | 6.60                 | 28.0                      | 2.6            | 4.2   | 13.9  | 27.8  |
| 19                 | D2                     | 2.02               | 2.47                 | 20.0                      | 3.0            | 5.1   | 6.I   | 12.5  |
| 20                 | E                      | 0.49               | 0.68                 | 17.6                      | 3.2            | 5.4   | 1.6   | 3.7   |
| 21                 | F                      | 1.63               | 2.28                 | 16.3                      | 3.3            | 5.7   | 5.4   | 12.9  |
| POND 1             | BASINS B1.1 THRU B10.2 | 52,64              | 63.35                | 29.2                      | 2.5            | 4.1   | 132.5 | 260.7 |
| POND 2             | BASINS C1.1 THRU C10   | 37.53              | 46.20                | 34.3                      | 2.3            | 3.7   | 86.5  | 172.7 |

\*Used to calculate the combined flow at DP-3 & DP-5 for split flow between inlets.

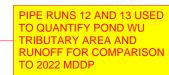
Calculated by: QNA Date: 07/15/05

Checked by:

PIPE RUN 5 USED TO QUANTIFY OS-5 RUNOFF MINUS OS-1 AND OS-2 RUNOFF

### FALCON HIGHLANDS FILING NO. 2 PDR BASINS (Pipe Routing Summary)

|                                    | l l            |                               |  |                      |                           | Inte | nsity | Fl          | ож    |
|------------------------------------|----------------|-------------------------------|--|----------------------|---------------------------|------|-------|-------------|-------|
|                                    | Pipe<br>Routes | Contributing<br>Design Points | Equivalent<br>CA 5                     | Equivalent<br>CA 100 | Maximum<br>T <sub>C</sub> | Ι,   | I 100 | Qs          | Q 100 |
|                                    | 1              | DP-1 & DP-4                   | 13.43                                  | 14.99                | 28.3                      | 2.6  | 4.2   | 34.4        | 62.8  |
|                                    | 2              | PR-1 & DP-2                   | 17.90                                  | 19.95                | 28.3                      | 2.6  | 4.2   | 45.8        | 83.7  |
| PIPE RUN 7 USED TO                 | 3              | PR-2, DP-3 & DP-5             | 32.31                                  | 39.74                | 28.3                      | 2.6  | 4.2   | 82.7        | 166.6 |
| QUANTIFY OS-6 RUNOFF<br>MINUS OS-3 | 4              | DP-12 & DP-13 PICK UP         | 6.21                                   | 7.01                 | 24.5                      | 2.8  | 4.6   | 17.1        | 31.9  |
|                                    | 5              | PR-3 & PR-4                   | 38.51                                  | 46.76                | 28.3                      | 2.6  | 4.2   | 98.6        | 196.0 |
|                                    | 6              | DP-8 & DP-9                   | 9.24                                   | 8.44                 | 27.3                      | 2.6  | 4,3   | 24.1        | 36.1  |
|                                    | 7              | PR-6 & DP-10                  | 13.51                                  | 15.04                | 27.3                      | 2.6  | 4.3   | 35.3        | 64.4  |
|                                    | 8              | PR-7 & DP-14                  | 17.17                                  | 19.57                | 27.3                      | 2.6  | 4.3   | 44.8        | 83.8  |
|                                    | 9              | PR-8 & DP-15                  | 19.34                                  | 22.21                | 27.3                      | 2.6  | 4.3   | 50.5        | 95.1  |
|                                    | 10             | PR-9 & DP-15A                 | 22.08                                  | 25.67                | 27.3                      | 2.6  | 4.3   | 57.6        | 109.9 |
|                                    | 11             | DP-11, DP-16 & DP-17          | 15.03                                  | 18.52                | 34.3                      | 2.3  | 3.7   | 34.6        | 69.2  |
|                                    | 12             | DP-18                         | 5.40                                   | 6.60                 | 28.03                     | 2.6  | 4.2   | 13.9        | 27.8  |
|                                    | 13             | DP-19                         | 2.02                                   | 2.47                 | 20.02                     | 3.0  | 5.1   | 6.1         | 12.5  |
|                                    | 14 <u>.</u>    |                               | ······································ |                      |                           |      | Са    | culated by: | QNA   |



Date: 07/15/05

Checked by:

### FALCON HIGHLANDS PHASE 2 FILING No. 2 and 3 MDDP MAJOR BASINS (Area Runoff Coefficient Summary)

THE 2010 FDR UTILIZED THE MDDP MAJOR BASINS FOR FILING NO. 1 DEVELOPED CONDITIONS / FILING NO. 2 & 3 EXISTING CONDITIONS FOR THE FILING NO. 1 OFFSITE AREAS.

|       |                          |                 | TS / DEVE      | LOPED            | OVERLAN         | ND / UNDE      | ELOPED | COMPO          | DSITE C          |
|-------|--------------------------|-----------------|----------------|------------------|-----------------|----------------|--------|----------------|------------------|
| BASIN | TOTAL<br>AREA<br>(Acres) | AREA<br>(Acres) | C <sub>5</sub> | C <sub>100</sub> | AREA<br>(Acres) | C <sub>5</sub> | Ci00   | C <sub>5</sub> | C <sub>10D</sub> |
| EX-1  | 21 75                    | 0 00            | 0 60           | 0 70             | 21 75           | 0 25           | 0 35   | 0 25           | 0 35             |
| EX-2  | 64 61                    | 0 00            | 0 60           | 0 70             | 64 61           | 0 25           | 0 35   | 0 25           | 0 35             |
| EX-3  | 99 57                    | 0 00            | 0 60           | 0 70             | 99 57           | 0 25           | 035    | 0 25           | 0 35             |
| EX-4  | 71 71                    | 0 00            | 0 60           | 0 70             | 71 71           | 0 25           | 0 35   | 0 25           | 0 35             |

EX-1 and EX-2 areas are part of Basin 78 from the Sand Creek DBPS and will use rational method to find the Historic Runoff EX-3 is the area in Phase 2 that is tributary to Design Point 38 of the Sand Creek DBPS, and will use rational method to find the Historic Runoff EX-4 is the area in Phase 2 that is tributary to Pond WU in the Falcon Basin DBPS

|             |                          |                 |           | PRO   | POSED           |            |                  |               |                  |  |
|-------------|--------------------------|-----------------|-----------|-------|-----------------|------------|------------------|---------------|------------------|--|
| BASIN       | TOTAL<br>AREA<br>(Acres) | STREE           | TS / DEVE | LOPED | OVERLAN         | VD / UNDEV | ELOPED           | COMPOSITE C   |                  |  |
|             |                          | AREA<br>(Acres) | C5        | C100  | AREA<br>(Acres) | Cs         | C <sub>100</sub> | Cs            | C <sub>100</sub> |  |
| A           | 14 81                    | 6 21            | 0 50      | 0 60  | 8 60            | 0 25       | 035              | 0.35          | 0 45             |  |
| B           | 105 45                   | 101 13          | 0 50      | 0 60  | 4 32            | 0 25       | 0 35             | 0 49          | 0 59             |  |
| С           | 88 47                    | 77 31           | 0 45      | 0 55  | 1116            | 0.25       | 0 35             | 0 42          | 0 52             |  |
| D           | 27 78                    | 27 00           | 0 45      | 0 55  | 0 78            | 0 25       | 0 35             | 0 44          | 0 54             |  |
| E           | 2 20                     | 0 00            | 0 50      | 0 60  | 2 20            | 0 25       | 0 35             | 0 25          | 0 35             |  |
| F           | 634                      | 0 00            | 0 50      | 0 60  | 634             | 0 25       | 0 35             | 0 25          | 0 35             |  |
| G           | 12 61                    | 0.00            | 0 50      | 0 60  | 12 61           | 0 25       | 0 35             | 0 25          | 0 35             |  |
| OS-1        | 6 38                     | 6 38            | 0 50      | 0 60  | 0 00            | 0 25       | 0 35             | 0 50          | 0 60             |  |
| OS-2        | 3 12                     | 3 12            | 0 90      | 0 95  | 0 00            | 0 25       | 0.35             | 0 90          | 0.95             |  |
| <b>OS-3</b> | 1 14                     | 1 14            | 0 90      | 0 95  | 0.00            | 0 25       | 0 35             | 0 90          | 0 95             |  |
|             |                          |                 |           |       |                 | ·          |                  | Calculated by | ONA              |  |

Calculated by <u>QNA</u>

Date 5/5/05

## FALCON HIGHLANDS PHASE 2 FILING No. 2 and 3 MDDP MAJOR BASINS (Area Drainage Summary) HISTORIC

|       |                          | WEIGHTED OVERLAND STREET / CHANNEL      |                           | ANNEL F | LOW            | Tr USED        |                         | INTENSITY      |              | TOTAL FLOWS       |                         |                |       |               |                             |                         |               |
|-------|--------------------------|---|---------------------------|---------|----------------|----------------|-------------------------|----------------|--------------|-------------------|-------------------------|----------------|-------|---------------|-----------------------------|-------------------------|---------------|
| BASIN | AREA<br>TOTAL<br>(Acres) | THE OWNER AND ADDRESS OF TAXABLE PARTY. | C190<br>Runpff Sutmittary | Ċ,      | Length<br>(it) | Height<br>(ft) | T <sub>C</sub><br>(min) | Length<br>(fl) | Slope<br>(%) | Velocitv<br>(fps) | T <sub>t</sub><br>(min) | TOTAL<br>(mun) | (min) | I₅<br>(ın∕hr) | I <sub>100</sub><br>(in/ht) | Q <sub>5</sub><br>(cfs) | Q100<br>(cfs) |
| EX-1  | 21 75                    | 0 25                                    | 0.35                      | 0 25    | 360            | 10.0           | 21.5                    | 0              | 0 0%         | 00                | 00                      | 21 5           | 21.5  | 29            | 49                          | 160                     | 372           |
| EX-2  | 64 61                    | 0 25                                    | 0 35                      | 0 25    | 300            | 100            | 185                     | 3750           | 1 5%         | 30                | 20.8                    | 39 3           | 39 3  | 2 1           | 34                          | 344                     | 776           |
| EX-3  | 99 S7                    | 0 25                                    | 0 35                      | 0 25    | 300            | 80             | 199                     | 2770           | 1 7%         | 32                | 14.4                    | 34 3           | 34 3  | 23            | 37                          | 573                     | 1301          |
| EX-4  | 71 71                    | 0 25                                    | 0 35                      | 0 25    | 280            | 80             | 188                     | 1900           | i 3%         | 27                | 117                     | 30 5           | 30 5  | 2 5           | 40                          | 44 0                    | 100 6         |

EX-1 and EX-2 area is planimetered from Sand Creek DBPS and will use rational method to find the Historic Runoff

EX-3 is the area in Phase 2 that is tributary to Design Point 38 of the Sand Creek DBPS

EX-4 is the area in Phase 2 that is tributary to Pond WU in the Falcon Basin DBPS

### PROPOSED

|       |                          |      |                                    |                |                |                |                         | $\overline{1}\overline{1}\overline{0}$ | <u>OSEI</u>  | <b>,</b>         |                         |       |         |                           |                          |             |                            |
|-------|--------------------------|------|------------------------------------|----------------|----------------|----------------|-------------------------|--|--------------|------------------|-------------------------|-------|---------|---------------------------|--------------------------|-------------|----------------------------|
|       |                          | WEIG | HTED                               |                | OVER           | LAND           |                         | STRE                                   | EET / CH     | IANNEL F         | LOW                     | Τ,    | Te USED | INTE/                     | VSITY                    | TOTAL       | FLOWS                      |
| BASIN | AREA<br>TOTAL<br>(Acres) |      | С <sub>196</sub><br>Ашпо/Г Summary | C <sub>s</sub> | Length<br>(ft) | Height<br>(fl) | T <sub>C</sub><br>(min) | Length<br>(fl)                         | Słope<br>(%) | Veiouts<br>((ps) | Т <sub>1</sub><br>(тип) | TOTAL | (min)   | l <sub>s</sub><br>(in∕hr) | l₁00<br>( <i>tn/hr</i> ) | Q3<br>(cfs) | Q <sub>100</sub><br>(cfs ) |
| A     | 14 8)                    | 0 35 | 0 45                               | 0 25           | 300            | 60             | 219                     | 233                                    | 3 0%         | 33               | 12                      | 23 1  | 23 1    | 28                        | 47                       | 149         | 317                        |
| B     | 105 45                   | 0 49 | 0 59                               | 0 25           | 170            | 34             | 16 5                    | 3890                                   | 2 5%         | 31               | 20 9                    | 37 4  | 37 4    | 2 2                       | 35                       | 113 3       | 220 :                      |
| С     | 88 47                    | 0 42 | 0 52                               | 0 25           | 110            | 40             | 109                     | 3255                                   | 13%          | 2.2              | 24 7                    | 35 5  | 35 5    | 23                        | 37                       | 84 9        | 169 7                      |

# FALCON HIGHLANDS PHASE 2 FILING No. 2 and 3 MDDP MAJOR BASINS

| <u></u>     |               | WEIG.           | HTED           |      | OVER   | LAND   |       | STRE   | ET / CH | ANNEL F  | LOW   | Τ,    | Te USED | INTE           | NSITY   | TOTAL | FLOWS |
|-------------|---------------|-----------------|----------------|------|--------|--------|-------|--------|---------|----------|-------|-------|---------|----------------|---------|-------|-------|
| BASIN       | AREA<br>TOTAL | C <sub>4</sub>  | C100           | C5   | Length | Height | Tc    | Length | Slope   | Velocity | Ť,    | TOTAL | IT USED | 1 <sub>5</sub> | I.00    | Q5    | Q100  |
|             | (Acres)       | * For Cales See | Вилоff Summary |      | (1)    | (n)    | (min) | (II)   | (%)     | (Ipv)    | (min) | (msn) | (mun)   | (in/hr)        | (in/hs) | (cfs) | (cfs) |
| D           | 27 78         | 0 44            | 0 54           | 0 25 | 180    | 36     | 170   | 1420   | 1 5%    | 24       | 99    | 26 8  | 26 8    | 26             | 43      | 325   | 65 4  |
| E           | 2 20          | 0 25            | 0 35           | 0 25 | 90     | 50     | 86    | 1080   | 10%     | 20       | 90    | 176   | 176     | 32             | 54      | 18    | 42    |
| F           | 6 34          | 0 25            | 0 35           | 0 25 | 125    | 40     | 121   | 630    | 16%     | 25       | 42    | 163   | 163     | 33             | 57      | 53    | 125   |
| G           | 12 61         | 0 25            | 0 35           | 0 25 | 300    | 70     | 20 8  | 285    | 18%     | 26       | 18    | 22.6  | 22.6    | 29             | 48      | 90    | 21 0  |
| <u> </u>    | 6 38          | 0 50            | 0.60           | 0 25 | 100    | 20     | 126   | 608    | 2.0%    | 28       | 36    | 163   | 163     | 34             | 57      | 107   | 217   |
| OS-2        | 3 12          | 0 90            | 0.95           | 0 25 | 100    | 20     | 126   | 1525   | 1 2%    | 22       | 11.6  | 24 2  | 24 2    | 28             | 46      | 78    | 13 6  |
| <b>OS-3</b> | 1 14          | 0 90            | 0 95           | 0 25 | 20     | 04     | 5 7   | 1190   | 0.6%    | 18       | 110   | 167   | 167     | 33             | 56      | 34    | 60    |

(Area Drainage Summary)

Calculated by QNA

Date 5/5/05

### FALCON HIGHLANDS PHASE 2 FILING No. 2 and 3 MDDP MAJOR BASINS (Surface Routing Summary)

### HISTORIC

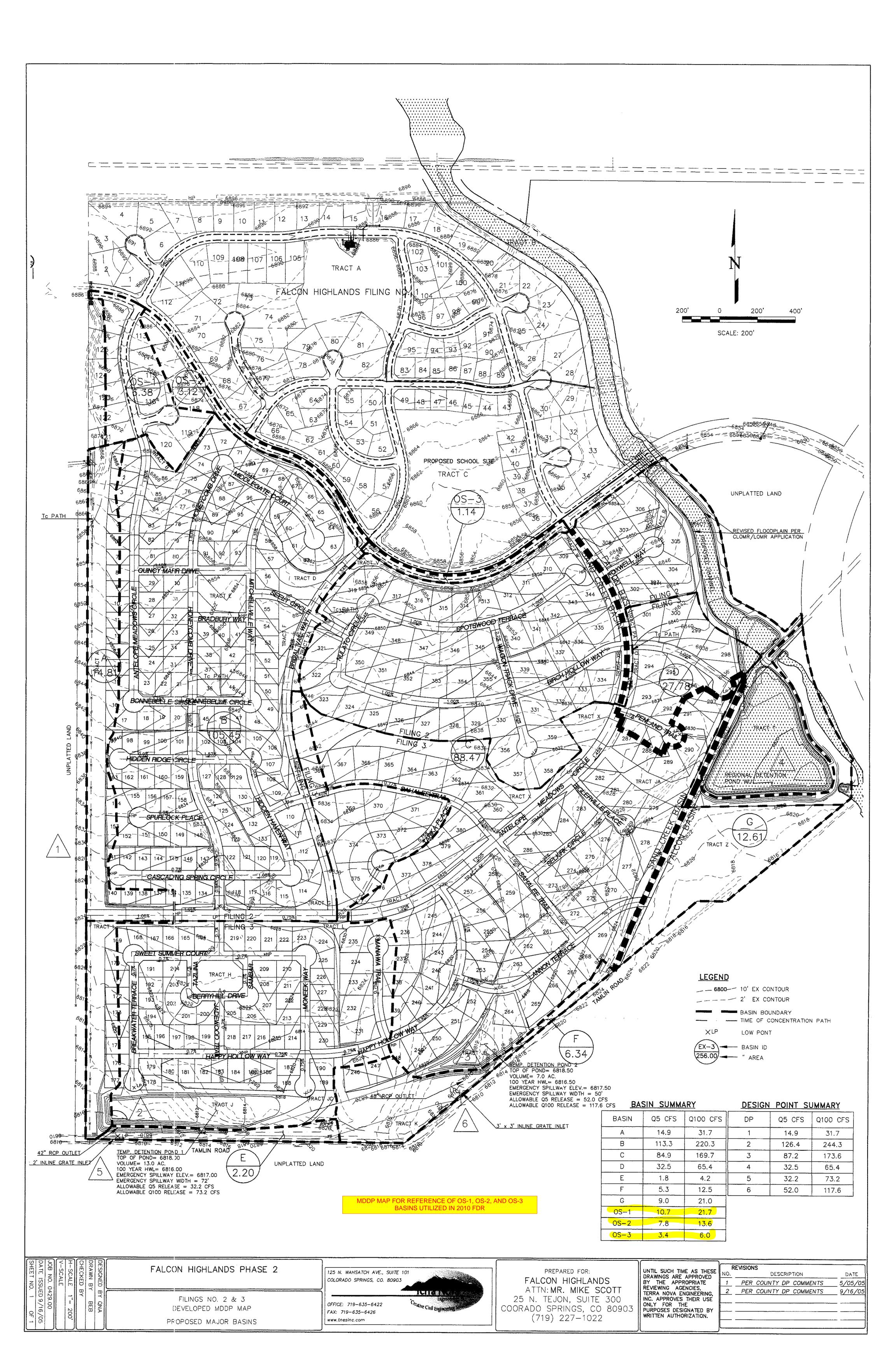
|                    |                        |                               |                      |                           | Inte | nsity | Flow |       |
|--------------------|------------------------|-------------------------------|----------------------|---------------------------|------|-------|------|-------|
| Design<br>Point(s) | Contributing<br>Basins | Equivalent<br>CA <sub>s</sub> | Equivalent<br>CA 100 | Maximum<br>T <sub>C</sub> | I s  | I 100 | Q5   | Q 100 |
| I                  | "EX-1"                 | 5 44                          | 761                  | 21 5                      | 29   | 49    | 160  | 372   |
| 2                  | "EX-2"                 | 16 15                         | 22 61                | 39 3                      | 21   | 34    | 34 4 | 776   |
| 3                  | "EX-3"                 | 24 89                         | 34 85                | 34 3                      | 2 3  | 37    | 573  | 130 1 |
| 4                  | "EX-4"                 | 17 93                         | 25 10                | 30 5                      | 25   | 40    | 44 0 | 100 6 |

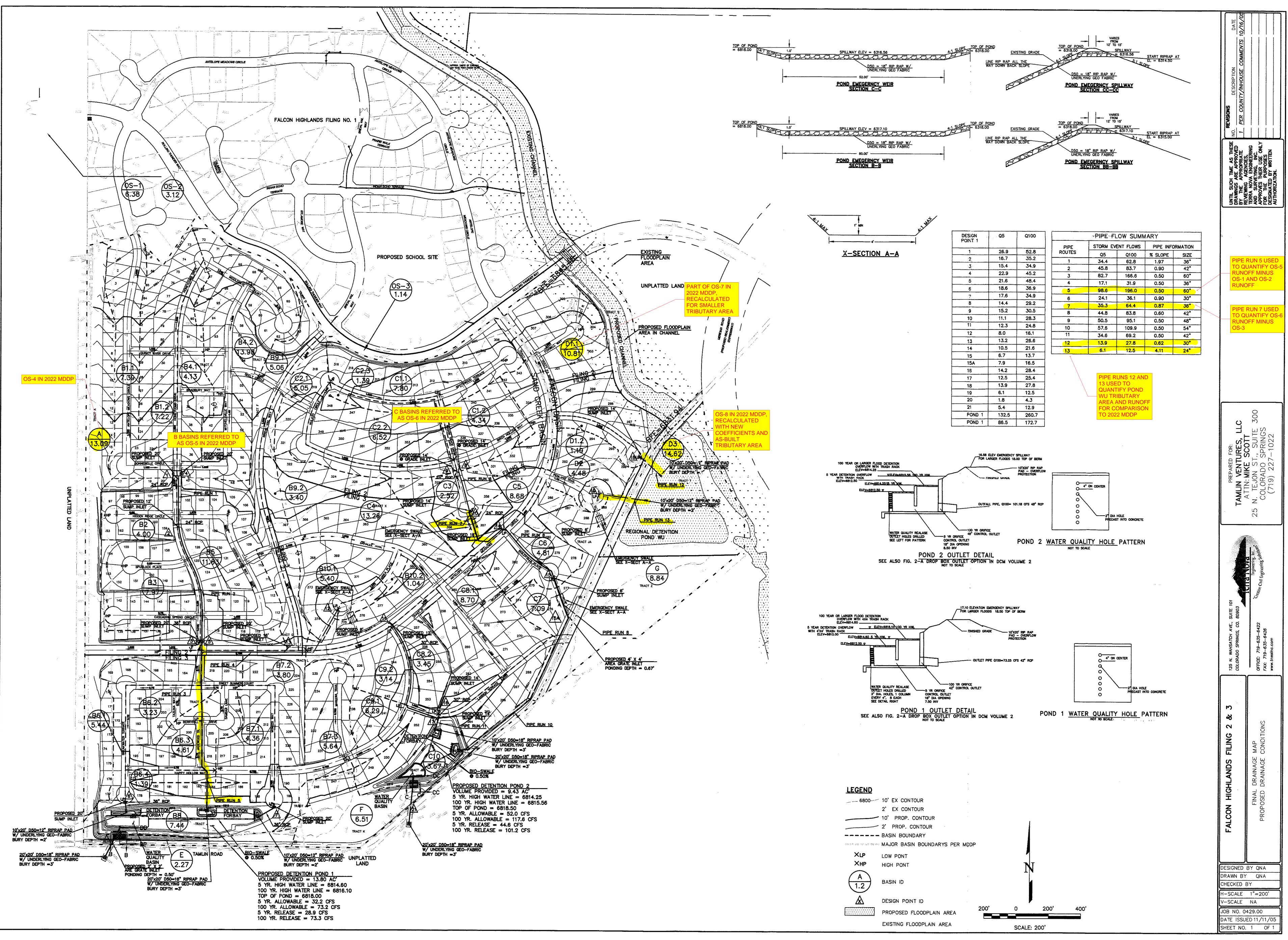
#### PROPOSED

|                    |                        |                    |                      |                           | Inte | nsity | <u> </u> | ow    |
|--------------------|------------------------|--------------------|----------------------|---------------------------|------|-------|----------|-------|
| Design<br>Point(s) | Contributing<br>Basins | Equivalent<br>CA 5 | Equivalent<br>CA 100 | Maximum<br>T <sub>C</sub> | Is   | I 100 | Qs       | Q 100 |
| 1                  | "A"                    | 5 2 5              | 6 73                 | 23 1                      | 28   | 4 7   | 149      | 317   |
| 2                  | "B", "OS-1" & "OS-2",  | 57 64              | 68 98                | 37 4                      | 22   | 35    | 126 4    | 244 3 |
| 3                  | "C", & "OS-3"          | 38 60              | 47 51                | 35 5                      | 23   | 37    | 872      | 173 6 |
| 4                  | "D"                    | 12 35              | 15 12                | 26 8                      | 26   | 43    | 325      | 65 4  |

Calculated by \_\_\_\_QNA

Date 5/5/05 Checked by

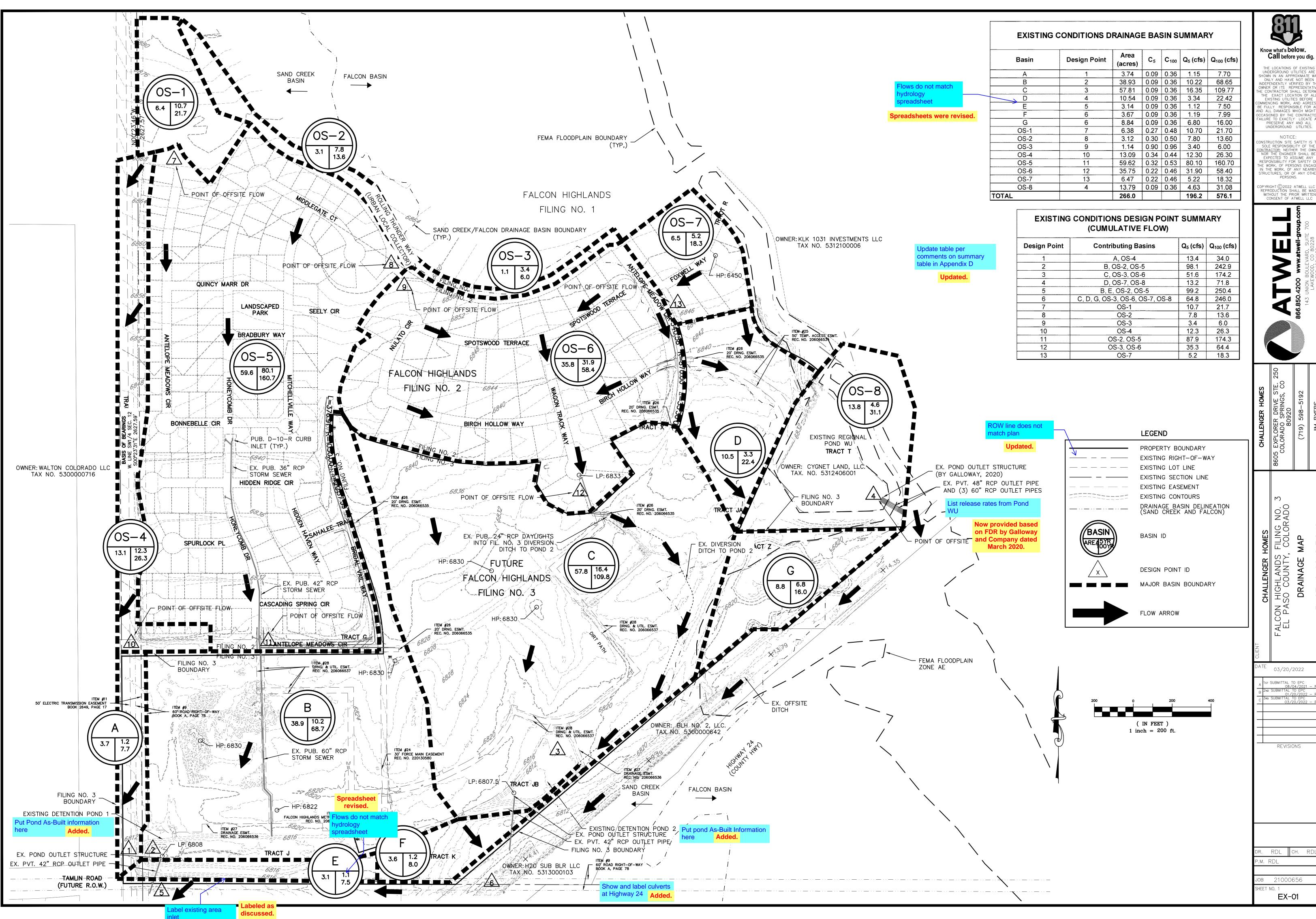




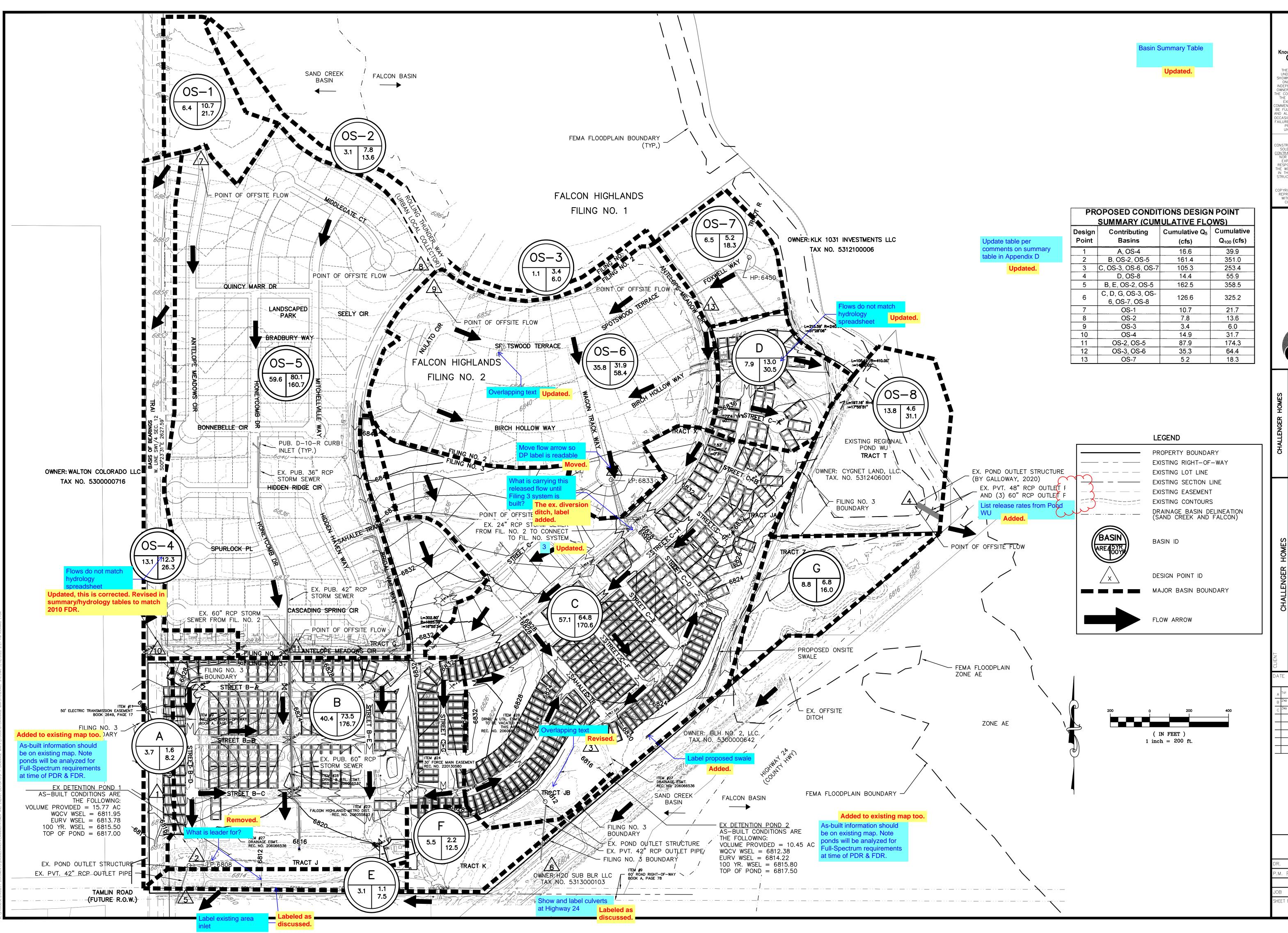
### **APPENDIX G**

### **DRAINAGE MAPS**

143 Union Boulevard, Suite 700, Lakewood, CO 80228 Tel: 303.462.1100 Fax: 303.825.7110 www.atwell-group.com



\PROJECT DOCUMENTS\ENGINEERING-PLANNING-PDWER AND ENERGY\REPORTS\F - DRAINAGE MAPS\21000656-DRAINAGE MAPS-EXISTING CONDITIONS.DWG 3/18/2022 1:53 PM RICHAR

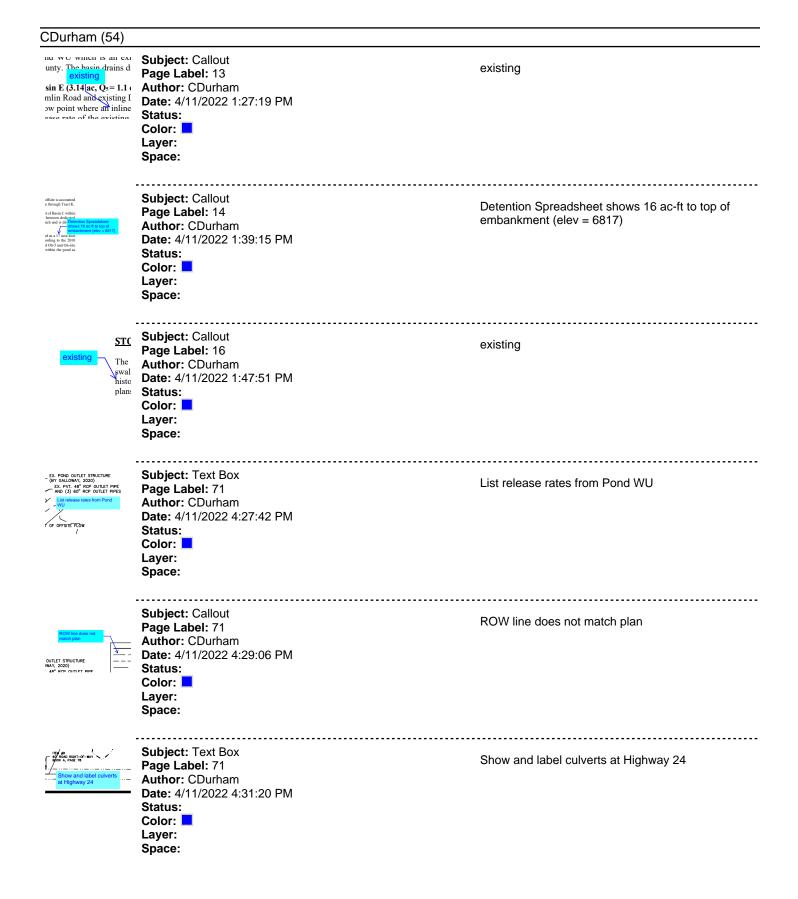


| Basin | Summary | Table |
|-------|---------|-------|
|       |         |       |

|   |  |  | _  |  |
|---|--|--|--|--|
|   | THE<br>UNDI<br>SHOWN<br>INDEPE<br>OWNER<br>THE CON<br>THE<br>EXX<br>COMMEN.<br>BE FUL<br>AND ALL<br>OCCASIO<br>FAILURE<br>FAILURE<br>CONSTRI<br>SOLE<br>CONTRA<br>NOR<br>EXP<br>RESPC<br>THE WCI<br>IN THIS<br>STRUC | what's be<br>call before<br>continues<br>erground u<br>in an apper<br>y and have<br>or ins re-<br>viractor se<br>exact loca<br>or exact<br>ing work,<br>instellity fo<br>perground<br>notice<br>responsibility fo<br>re-<br>visibility fo<br>re | e you d<br>OF EXIST<br>TILITIES<br>ROXIMATE:<br>NOT BE<br>RIFIED B<br>PRESENT<br>ITION OF<br>ES BEFO<br>AND AGE<br>CONTRA<br>Y LOCA<br>AND AGE<br>Y LOCA<br>Y LOCA<br>AND AGE<br>Y LOCA<br>Y | ING<br>ARE<br>E WAY<br>IEN<br>Y THE<br>ATIVE.<br>TERMINE<br>ALL<br>RE<br>CEES TO<br>RE ANY<br>GHT BE<br>SCTOR'S<br>TE AND<br>L<br>S.<br>IS THE<br>THE<br>OWNER<br>. BE<br>NY<br>Y OF<br>GAGED<br>ARBY<br>THER<br>LLC NO<br>MADE<br>TEN |
| T   lative   (cfs)   .9   1.0   3.4   .9   3.5   5.2   .7   .6   0   .7   4.3 |  | <b>ATWELL</b>  | 866.850.4200 www.atwell-group.com  | LAKEWOOD, CO 80228<br>303.462.1100   |
|   | CHALLENGER HOMES   | 8605 EXPLORER DRIVE STE. 250<br>COLORADO SPRINGS, CO<br>80920  | (719) 598–5192   | JIM BYERS  |
| ION<br>I)   | CLIENT<br>CHALLENGER HOMES   | FALCON HIGHLANDS FILING NO. 3<br>EL PASO COUNTY, COLORADO  | DRAINAGE MAP   | PROPOSED CONDITIONS  |
|   | DATE   | 08/0<br>SUBMITTAL T<br>01/2<br>SUBMITTAL T   | 0 EPC<br>04/2021<br>0 EPC<br>0/2022<br>0 EPC<br>0 EPC<br>0 2022  | - RDL<br>- RDL<br>- RDL  |
|   | DR.<br>P.M. F<br>JOB<br>SHEET N  | 210006   | \$56   | RDL  |

EX-02

### MDDP \_V3.pdf Markup Summary



| Sto ISWOOD TERRACE  | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:32:21 PM<br>Status:<br>Color: Layer:<br>Space:  | Overlapping text                      |
|---|--|---------------------------------------|
| EX. POND OUTLET STRUCTURE<br>(FY GALLOWAY, 2020)<br>EX. PVT. 48 'RCP OUTLET F<br>Last release rates from Pord<br>WU<br>WU<br>WO<br>VOID OFFSITE TOW | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:33:49 PM<br>Status:<br>Color: Layer:<br>Space: | List release rates from Pond WU       |
| SAU DOCED   | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:35:25 PM<br>Status:<br>Color: Layer:<br>Space:  | Label proposed swale                  |
| there a   | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:36:22 PM<br>Status:<br>Color: Layer:<br>Space:  | Overlapping text                      |
| Show and label cuverts<br>at Highway 24   | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:37:47 PM<br>Status:<br>Color: Layer:<br>Space: | Show and label culverts at Highway 24 |
| Label existing real   | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:39:01 PM<br>Status:<br>Color: Layer:<br>Space:  | Label existing area inlet             |

| Vitai a laster fo?   | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:41:04 PM<br>Status:<br>Color: Layer:<br>Space:  | What is leader for?   |
|--|--|---|
| PLING NO. 3<br>EXEMPLOYED PROD 1<br>PUT FOUL NO BUT INFORMATION<br>RECEIPTION OF THE STRUCTURE<br>EX. POT. 42° RCP. OUTLET PIPE  | Subject: Text Box<br>Page Label: 71<br>Author: CDurham<br>Date: 4/11/2022 4:41:45 PM<br>Status:<br>Color: Layer:<br>Space: | Put Pond As-Built information here                                  |
| p 2 Put pond As-Built Information  | Subject: Text Box<br>Page Label: 71<br>Author: CDurham<br>Date: 4/11/2022 4:42:01 PM<br>Status:<br>Color: Layer:<br>Space: | Put pond As-Built Information here                                  |
| 3  | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:43:52 PM<br>Status:<br>Color: Layer:<br>Space: | 3   |
| A second se | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 4:44:33 PM<br>Status:<br>Color: Layer:<br>Space:  | What is carrying this released flow until Filing 3 system is built? |
| E<br>31 1 25   | Subject: Callout<br>Page Label: 71<br>Author: CDurham<br>Date: 4/11/2022 4:45:58 PM<br>Status:<br>Color: Layer:<br>Space:  | Flows do not match hydrology spreadsheet                            |

| LUXI<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T<br>T                  | Subject: Callout<br>Page Label: 71<br>Author: CDurham<br>Date: 4/11/2022 4:46:16 PM<br>Status:<br>Color: Layer:<br>Space:      | Flows do not match hydrology spreadsheet                    |
|--|--|---|
| Update table per<br>comments on summary<br>table in Appendix D   | Subject: Text Box<br>Page Label: 71<br>Author: CDurham<br>Date: 4/11/2022 4:50:25 PM<br>Status:<br>Color: Layer:<br>Space:     | Update table per comments on summary table in<br>Appendix D |
| Label existing area  | Subject: Callout<br>Page Label: 71<br>Author: CDurham<br>Date: 4/11/2022 4:50:45 PM<br>Status:<br>Color: Layer:<br>Space:      | Label existing area inlet                                   |
| 10.22   00.05     16.35   109.77     3.34   22.42     1.12   7.50     1.19   7.99     6.80   16.00     10.70   21.70 | Subject: Highlight<br>Page Label: 38<br>Author: CDurham<br>Date: 4/11/2022 5:42:43 PM<br>Status:<br>Color:<br>Layer:<br>Space: | 1.12 7.50   |
|  | Subject: Callout<br>Page Label: 38<br>Author: CDurham<br>Date: 4/11/2022 5:43:07 PM<br>Status:<br>Color:<br>Layer:<br>Space:   | Flows do not match hydrology spreadsheet                    |
| ontributing Basins<br>A, DP 10 (OS-4)<br>B, OS-2, OS-5<br>C, OS-3, OS-6<br>D, OS-7, OS-8                             | Subject: Text Box<br>Page Label: 39<br>Author: CDurham<br>Date: 4/11/2022 5:50:16 PM<br>Status:<br>Color: Layer:<br>Space:     | A, DP 10 (OS-4)   |

| Contributing Basins   (     A, OS4   B, DP1 (OS2, OS-5)     C, OS4, OS-6   D, OS-7, OS-8     B, E, E, OS-2, OS-6   G, OS-3, OS-6                             | Subject: Text Box<br>Page Label: 39<br>Author: CDurham<br>Date: 4/11/2022 5:50:49 PM<br>Status:<br>Color: Layer:<br>Space: | B, DP 11 (OS-2, OS-5)                           |
|--|--|---|
| Contributing Basins     A, OS-4     B, OS-2, OS-5     C, DP 12 (OS-3, OS-6)     D, OS-7, OS-8     B, E, OS-2, OS-5     O, G, OS-3, OS-6, OS-7, OS-8     OS-1 | Subject: Text Box<br>Page Label: 39<br>Author: CDurham<br>Date: 4/11/2022 5:51:10 PM<br>Status:<br>Color: Layer:<br>Space: | C, DP 12 (OS-3, OS-6)                           |
| A. 05:4<br>B. 05:2, 05:5<br>C. 05:3, 05:6<br>D. 05:7, 05:8<br>E. DP 2 (8, 05:2, 05:5)<br>C. D. 6, 05:3, 05:6, 05:7, 05:8<br>05:1<br>05:2<br>05:3             | Subject: Text Box<br>Page Label: 39<br>Author: CDurham<br>Date: 4/11/2022 5:52:28 PM<br>Status:<br>Color: Layer:<br>Space: | E, DP 2 (B, OS-2, OS-5)                         |
| CURLENT ELSON<br>Deprint Constants James Alimento<br>2010/2011/2011/2011/2011/2011/2011/2011   | Subject: Text Box<br>Page Label: 39<br>Author: CDurham<br>Date: 4/11/2022 5:54:55 PM<br>Status:<br>Color: Layer:<br>Space: | F, G, DP 3 (C, OS-3, OS-6), DP 4(D, OS-7, OS-8) |
| Basin Summary Table  | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 5:56:02 PM<br>Status:<br>Color: Layer:<br>Space: | Basin Summary Table                             |
|  | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 5:56:14 PM<br>Status:<br>Color: Layer:<br>Space:  | Flows do not match hydrology spreadsheet        |

| Point of offster now   | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 5:56:28 PM<br>Status:<br>Color: Layer:<br>Space:     | Flows do not match hydrology spreadsheet                    |
|--|---|---|
| Update table per<br>commente or summary<br>table in Appendix D   | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 5:56:46 PM<br>Status:<br>Color: Layer:<br>Space:    | Update table per comments on summary table in<br>Appendix D |
| Contributing<br>Basins<br>A, DP 10 (OS-4)<br>B, OS-2, OS-5<br>C, OS-3, OS-6, OS-7<br>D, OS-8   | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/11/2022 5:57:58 PM<br>Status:<br>Color: Layer:<br>Space:    | A, DP 10 (OS-4)   |
| OS-2<br>OS-3<br>OS-4<br>OS-5. DP 8 (OS-2)<br>OS-3, OS-6<br>OS-7  | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/11/2022 5:58:53 PM<br>Status:<br>Color:<br>Layer:<br>Space: | OS-5, DP 8 (OS-2)   |
| 0S-3<br>0S-4<br>0S-2, 0S-5<br>0S-6, DP 9 (0S-3)<br>0S-7  | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/11/2022 5:59:20 PM<br>Status:<br>Color: Layer:<br>Space:    | OS-6, DP 9 (OS-3)   |
| sign   Contributing   Cum     bint   Basins   Cum     1   A. 05:4   Cum     2   B. 0P 11 (052, 06:5)   3     3   C. 05:3, 05:6, 05:7   4     4   D. 05:8   5     5   B. E. 05:2, 05:5   05:5 | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/11/2022 5:59:58 PM<br>Status:<br>Color: Layer:<br>Space:    | B, DP 11 (OS-2, OS-5)                                       |

| Reprinted Within the United States     SUMMARY (CUUL ATVEE COME)     Opage   Conclusion   Conclusion   Conclusion     0   Conclusion   Conclusio   | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/11/2022 6:00:49 PM<br>Status:<br>Color: Layer:<br>Space:     | C, DP 12 (OS-3, OS-6), DP 13 (OS-7)  |
|---|--|--|
| Does 05-7 conductor<br>with 0 part 05-8 at<br>DP 4 of zone fithtogs<br>with does not possible<br>block.   | Subject: Callout<br>Page Label: 39<br>Author: CDurham<br>Date: 4/11/2022 6:04:13 PM<br>Status:<br>Color: Layer:<br>Space:      | Does OS-7 combine with D and OS-8 at DP 4 or<br>travel through site down to DP 6? Clarify and<br>update table.     |
| <text><text><text><text></text></text></text></text>  | Subject: Text Box<br>Page Label: 9<br>Author: CDurham<br>Date: 4/11/2022 6:18:08 PM<br>Status:<br>Color: Layer:<br>Space:      | In existing conditions, note that DP 12 releases<br>into the existing diversion ditch, running through<br>Basin C. |
| 10.54 ac, Q <sub>2</sub> = 3.3 cfs, Q <sub>100</sub> = 22.4 cfs<br>undereloped area with native grasses.<br>Design Point 4, Q <sub>20</sub> = 7, 5, cfb is the<br>and the existing Pool 1. Runoff for<br>an the future Tranini Road and Highw<br>citated storm infrastructure is presented<br>d plan. The 2010 FDR suggested that i<br>at this start installed. The activities desire<br>with the start installed. The activities desire<br>of the start of the start of the start of the start<br>of the start of the start of the start of the start<br>of the start of the start of the start of the start<br>of the start of the start of the start of the start<br>of the start of the start of the start of the start<br>of the start of the start of the start of the start of the start<br>of the start of the start of the start of the start of the start<br>of the start of the s | Subject: Highlight<br>Page Label: 10<br>Author: CDurham<br>Date: 4/11/2022 6:18:35 PM<br>Status:<br>Color:<br>Layer:<br>Space: | Q5 = 1.1 cfs, Q100 = 7.5 cfs   |
| 1 cf. Que = 22.4 cf.1 is locard to the number of<br>the series graves. The hear's neural criteria disc<br>interaction of the series of the series of the<br>probability of the series of the series of the<br>Que 2 do not be not equal to the series of the<br>Board and Hayney 2 (Dodge Rund - S. Tha disc<br>Robert Rund - S.  | Subject: Callout<br>Page Label: 10<br>Author: CDurham<br>Date: 4/11/2022 6:19:29 PM<br>Status:<br>Color: Layer:<br>Space:      | Flows do not match hydrology spreadsheet   |
| In the determinent of the end of   | Subject: Callout<br>Page Label: 13<br>Author: CDurham<br>Date: 4/11/2022 6:23:46 PM<br>Status:<br>Color: Layer:<br>Space:      | replace detention with water quality treatment   |

| nm by the version and the set of   | Subject: Text Box<br>Page Label: 13<br>Author: CDurham<br>Date: 4/11/2022 6:24:48 PM<br>Status:<br>Color:<br>Layer:<br>Space: | Make note that if existing inlet wasn't installed, it<br>may need to be. It will be furthered analyzed in the<br>PDR & FDR's, as well as the capacity of the<br>existing swale. |
|---|---|---|
| <text></text>   | Subject: Text Box<br>Page Label: 12<br>Author: CDurham<br>Date: 4/11/2022 6:27:28 PM<br>Status:<br>Color: Layer:<br>Space:    | Flow from DP 12 was previously routed through a<br>diversion channel. How is it directed now, until<br>future system in Antelope Meadows Cir is built?                          |
| tion faunc Anticlop Madawa Chile right-of-<br>metric band bandt chile Filing 2, jan such<br>and and an of the Alfar service on single<br>englishesis on case and an anticloper service fragment<br>hands and the anticloper service and the service<br>service of the service of the service of the service<br>resource of the service 3 and the service<br>metric of the service service of the service<br>service and service 3 and the service of the<br>service service service 3 and the service<br>service and service 3 and the service of the<br>service service service of the service of the<br>service service service of the service of the service<br>service service service service service of the service<br>service service service service service service of the service<br>service service serv | Subject: Text Box<br>Page Label: 12<br>Author: CDurham<br>Date: 4/11/2022 6:28:44 PM<br>Status:<br>Color:<br>Layer:<br>Space: | From this description, Basin has been re-routed.<br>Ensure Pond design has accounted for additional<br>area and flow.   |
| <text><text><text></text></text></text>   | Subject: Text Box<br>Page Label: 12<br>Author: CDurham<br>Date: 4/11/2022 6:29:39 PM<br>Status:<br>Color:<br>Layer:<br>Space: | Indicate roadside ditch will be analyzed for developed flows with PDR & FDR's.  |
|   | Subject: Callout<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 6:31:46 PM<br>Status:<br>Color:<br>Layer:<br>Space:  | Move flow arrow so DP label is readable   |
| As-built Information should<br>be on existing map. Note<br>ponds will be analyzed for<br>ponds will be analyzed for<br>ponds will be analyzed for<br>at time of PDR & FDR.  | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 6:32:53 PM<br>Status:<br>Color:<br>Layer:<br>Space: | As-built information should be on existing map.<br>Note ponds will be analyzed for Full-Spectrum<br>requirements at time of PDR & FDR.  |

| FILMO IN 3<br>BOUNDARY<br>As-built information should<br>be on existing map. Note<br>ponds will be analyzed for<br>Full-Spectrum requirements<br>at time of PDR & FDR.<br>EX. DETENDER FORD. 1<br>AS-BUILT CONDITIONS ARE<br>THE FOLLOWING:  | Subject: Text Box<br>Page Label: 72<br>Author: CDurham<br>Date: 4/11/2022 6:32:58 PM<br>Status:<br>Color: Layer:<br>Space:    | As-built information should be on existing map.<br>Note ponds will be analyzed for Full-Spectrum<br>requirements at time of PDR & FDR. |
|--|---|--|
| southwest of Antelope Meadow<br>ir basin is comprised of Tract A<br>ten object of Basin B. The storm energy<br>proble galaxies in the storm energy of the<br>problem of the storm energy of the storm energy<br>in the storm energy of the storm energy of the<br>drawn energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the<br>storm energy of the storm energy of the storm energy of the storm energy of the<br>storm energy of the storm | Subject: Text Box<br>Page Label: 9<br>Author: CDurham<br>Date: 4/11/2022 9:10:47 AM<br>Status:<br>Color: Layer:<br>Space:     | Expand on existing drainage pattern. Is it sheetflow, and if so to where, or channel/swale, etc?                                       |
| Response   FROMULTION     Interpretent   State (State (St  | Subject: Callout<br>Page Label: 45<br>Author: CDurham<br>Date: 4/12/2022 9:23:21 AM<br>Status:<br>Color: Layer:<br>Space:     | See comment under existing condition summary<br>table for Basin OS-7. Revise design point<br>summary here accordingly.                 |
| C, OS-3, OS-6, OS-7   105     D, OS-8   14.     B, E, OS-2, OS-5   162     G, DP 3 (C, OS-3, OS-6, OS-7, DP 4 (D, OS-3)   126     OS-7, DP 4 (D, OS-3)   126     OS-3   3.     OS-4   14   | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/12/2022 9:23:34 AM<br>Status:<br>Color:<br>Layer:<br>Space: | G, DP 3 (C, OS-3, OS-6, OS-7), DP 4 (D, OS-8)  |
| Missing Basin F  | Subject: Text Box<br>Page Label: 45<br>Author: CDurham<br>Date: 4/12/2022 9:23:52 AM<br>Status:<br>Color:<br>Layer:<br>Space: | Missing Basin F  |
| HYDRAULIC C<br>Put Point Tobulary Assa and<br>the Appendix   | Subject: Text Box<br>Page Label: 47<br>Author: CDurham<br>Date: 4/12/2022 9:24:16 AM<br>Status:<br>Color: Layer:<br>Space:    | Put Pond Tributary Area and Imperviousness spreadsheets back into Appendix.  |