

PRELIMINARY DRAINAGE REPORT

FALCON MEADOWS AT BENT GRASS

El Paso County, Colorado

PREPARED FOR:

Challenger Homes 8605 Explorer Dr., Suite 250 Colorado Springs, CO 80920

PREPARED BY:

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DATE:

August 5, 2020 Revised December 2020 Revised February 2021

Engineering Review

EPC Planning & Community Development Department

Also see comment letter.



ENGINEER'S STATEMENT

to the best o established I plan of the d	d drainage plan and report were prepared unif my knowledge and belief. Said drainage by the County for drainage reports and said trainage basin. I accept responsibility for all my part in preparing this report.	report has been prepared according to the report is in conformity with the applicab	he criteria le master
	orham, P.E. #36727 Dehalf of Galloway & Company, Inc.	Date	
<u>DEVELOPE</u>	R'S CERTIFICATION		
I, The develo and plan.	oper, have read and will comply with all of t	he requirements specified in this drainag	ge report
Ву:		 Date	
Address:	Challenger Homes 8605 Explorer Dr., Suite 250 Colorado Springs, CO 80920	Date	
Ву:		_	
Address:	Better Land LLC 8605 Explorer Dr., Suite 250 Colorado Springs, CO 80920	Date	
EL PASO C	OUNTY CERTIFICATION		
	ordance with the requirements of the Draina ineering Criteria Manual and Land Develop	_	l Paso
Jennifer Irvir	ne, P.E. neer/ECM Administrator	Date	
Conditions:	HEEL/LOW AUTHINSTIALUI		

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I. Purpose

The purpose of this Preliminary Drainage Report is to identify on and offsite drainage patterns, locate and identify tributary or downstream drainage features and facilities that impact the site, and to identify which types of drainage facilities will be needed and where they will be located. This report will remain in general compliance with the MDDP submitted for review in January for the site prepared by Galloway & Company.

II. General Description

The project is a single-family residential development located in the Falcon area of El Paso County, Colorado. The site is located in the Northwest ¼ and Southwest ¼ of Section 1, Township 13S, Range 65W, of the Sixth Principal Meridian, County of El Paso, State of Colorado. The subject property is bounded by Bent Grass Meadows Filing No.2 to the east, Latigo Business Center Filing No. 1 to the south, The Meadows Filings No. 1 & 2 to the west, and The Meadows Filing No. 3 to the north. A Vicinity Map is included in Appendix A.

This preliminary drainage report was the basis for the drainage facility design contained within the previously approved MDDP for the site prepared by Galloway & Company. The site consists of approximately 66.6 acres and includes 267 dwelling units.

The existing soil types within the proposed site as determined by the NRCS Web Soil Survey for El Paso County Area consist of Columbine gravelly sandy loam, Blakeland-Fluvaquentic Haplaquolls, and Blakeland loamy sand. All soils are defined as having a hydrologic soil group of A. See the soils map included in Appendix A.

III. Previous Reports

The proposed site has been included in multiple drainage studies in the past. The following is a composite list of the existing reports pertaining to this site analysis.

- 1. Falcon Drainage Basin Planning Study, by Matrix Design Group, September 2015.
- 2. Master Development Drainage Plan Bent Grass Residential Subdivision, by Galloway & Company, Revision in Progress per Meridian Road Intersection Comments.
- 3. *Master Development Drainage Plan and Preliminary Drainage Plan Bent Grass Subdivision*, by Kiowa Engineering Corporation, December 2006.
- 4. Final Drainage Report for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2014.
- 5. Final Drainage Report Addendum for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2015.
- 6. *Master Development Drainage Plan for The Ranch*, by Classic Consulting Engineers & Surveyors, LLC, November 2018.
- 7. Falcon Highlands Master Development Drainage Plan & Preliminary Drainage Report & Final Drainage Report for Filing 1, by URS, January 2005.
- 8. Final Drainage Report and Erosion Control Plan Latigo Business Center Filing No. 1 A Resubdivision of a Portion of Latigo Business and Research Center Filing No. 1, by Kiowa Engineering Corporation, November 2004.
- 9. Final Drainage Letter Report for Lot 1, Latigo Business Center Filing No. 1, by Colorado Design Concepts, April 2005.

- 10. Final Drainage and Erosion Control for The Meadows Filing Three Subdivision, by LADD Engineering, July 2000.
- 11. Final Drainage Report for Bent Grass Residential (Filing No. 2), by Galloway & Company, May 2020

IV. Drainage Criteria

Hydrology calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.

The drainage calculations were based on the criteria manual Figure 6-5 and IDF equations to determine the intensity and are listed in Table 1 below.

Table 1 - Precipitation Data

Return Period	One Hour Depth (in).	Intensity (in/hr)
5-year	1.50	5.17
100-year	2.52	8.68

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has been proven to be accurate for basins of this size and is based on the following formula:

Q = CIA

Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff intensity (inches/hour)

A = Drainage area (acres)

The runoff coefficients are calculated based on land use, percent imperviousness, and design storm for each basin, as shown in the drainage criteria manual (Table 6-6). Composite percent impervious and C values were calculated using the residential, streets, roofs, and lawns coefficients found in Table 6-6 of the manual.

The 100-year event was used as the major storm event. The 5-year event was used as the minor event.

The UD-Detention v3.07 spreadsheet was utilized for the design of the proposed on-site water quality ponds, Pond (North) and Pond (South).

V. Existing Drainage Conditions

The site is contained fully within one major drainage basin; the West Falcon Tributary. The site generally drains from north to south with an average slope of 2% outside of the channel. The rational method was used to analyze the individual basins within the site because their size permits it.

In addition to the DBPS, The Ranch MDDP to the north and west of the site has revisited their existing conditions as well as existing conditions from the site directly to the north of them. Several detention ponds have been created within the Paint Brush Hills Subdivision which revise the offsite flow entering the site within the major drainageway. This is taken into account with The Ranch MDDP. While The Ranch is still in design stage, they are proposing detention ponds within their site to release at historic rates. This will revise the flow rates in their designed section of the RWT204 channel rates that are lower than those identified within the DBPS. An updated HEC-HMS model was submitted with the MDDP.

Per the DBPS the site lies within the basins, WT200, WT210, and WT220. These basins connect to channel reaches RWT202, RWT204, and RWT210. Both the RWT204 and RWT210 sections of channel currently exist and appear as a drainageway when visiting the site. With Bent Grass Filing No. 2, Reach RWT202 from Basin WT200 was "relocated and improved". The channel reach is now along the north border of the Bent Grass property and drains towards the east, where it combines with channel reach RWT204. The channel is a 26-ft bottom trapezoidal section with 4:1 side slopes and a longitudinal slope of 1.00%.

A historic basin map has been prepared for this site to analyze the existing basins as well as the offsite basins contributing to the site. The historic map is included in Appendix D and basins are described below.

Basin EX-1 (1.19 AC, $Q_5 = 0.4$ cfs, $Q_{100} = 2.5$ cfs): is associated with the northeastern portion of the proposed site east of the existing channel. The basin is currently undeveloped. Runoff from the basin generally flows to the southwest, into Basin EX-2 at **DP 4.**

Basin EX-2 (1.56 AC, $Q_5 = 0.5$ cfs, $Q_{100} = 3.7$ cfs): is along the eastern boundary portion of the proposed site and is south of Basin EX-1, east of the existing channel. The basin is currently undeveloped and receives flows from Basins OS-4 & OS-5. Runoff from the basin generally flows to the southeast into Basin EX-3 at **DP 5** combined with flows from **DP 1, 2, & 4**.

Basin EX-3 (0.62 AC, $Q_5 = 0.2$ cfs, $Q_{100} = 1.5$ cfs): is along the eastern boundary of the proposed site south of Basin EX-2 and east of the existing channel. The basin currently contains an existing WQCV pond created as part of Bent Grass Residential Filing No. 2. This basin receives flows from **DP 5** and **DP 3**.

Basin EX-4 (12.49 AC, $Q_5 = 3.7$ cfs, $Q_{100} = 25.1$ cfs): is located along the northern boundary, just south of the swale built with Bent Grass Meadows Drive and west of the existing channel. The basin is currently undeveloped. Runoff from the basin generally flows to the south onto Bent Grass Meadows Drive at **DP 6**. From there, it flows via curb & gutter to the east into an existing sump inlet, ultimately discharging into the existing WQCV pond located in Basin EX-3.

Basin EX-5 (5.15 AC, $Q_5 = 1.6$ cfs, $Q_{100} = 10.6$ cfs): is west of Basin EX-4 and north of Bent Grass Meadows Drive. The basin is currently undeveloped. Runoff from the basin generally flows to the south onto Bent Grass Meadows Drive at **DP 7**. From there, it flows via curb & gutter to the east into an existing sump inlet, ultimately discharging into the existing WQCV pond located in Basin EX-3.

Basin EX-6 (9.53 AC, $Q_5 = 2.7$ cfs, $Q_{100} = 17.8$ cfs): is along the west boundary of the site. The basin is currently undeveloped and receives off-site flows from Basins OS-2 & OS-3. Runoff from the basin

generally flows to the south into the existing drainage ditch entering an existing inlet at DP 11 and flowing under Bent Grass Meadows Drive and discharging into an existing drainage swale in Basin EX-8.

Basin EX-7 (9.16 AC, $Q_5 = 2.8$ cfs, $Q_{100} = 18.9$ cfs): is north & west of Bent Grass Meadows Drive, between Basins EX-5 & EX-6. The basin is currently undeveloped. Runoff from the basin generally flows to the southeast into Bent Grass Meadows Drive at **DP 8**. From there, it flows via curb & gutter to the south into an existing sump inlet, ultimately discharging into the existing sediment pond located in Basin EX-8.

Basin EX-8 (21.3 AC, $Q_5 = 6.6$ cfs, $Q_{100} = 43.9$ cfs): is a portion of the site south and east of Bent Grass Meadows Drive, north of the south property line and west of Bent Grass Filing No. 2. The basin is currently undeveloped and contains two drainage ditches, a sediment pond, and a portion of the creek associated with Basin WT200 from the Falcon DBPS. Runoff from the basin generally flows to the southeast into the existing channel.

Basin OS-1 (32.28 AC, Q5 = 15.1 cfs, Q100 = 65.1 cfs) is associated with The Meadows Filing No. 3 lots 14, 15, 16, and 17. Runoff from this basin sheet flows to the northern property line of the site and then flow, via an existing drainage ditch, into the existing channel associated with Basin WT200 from the Falcon DBPS.

Basin OS-2 (20.08 AC, Q5 = 9.0 cfs, Q100 = 43.4 cfs) is associated with The Meadows Filing No. 1 lots 1, 2, 3, 4, 5, and 6. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site at **DP 9**. The runoff will continue to sheet flow through Basin EX-6 to the south until entering the existing drainage swale on the southern boundary of Basin EX-6 at **DP 11**.

Basin OS-3 (10.62 AC, Q5 = 4.7 cfs, Q100 = 22.7 cfs) is associated with The Meadows Filing No. 1 lot 11 and The Meadows Filing No. 2 Lots 1 & 2. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site at **DP 10**. The runoff will continue to sheet flow through Basin EX-6 to the south until entering the existing drainage ditch on the southern boundary of Basin EX-6 at **DP 11**.

Basin OS-4 (4.46 AC, Q5 = 5.6 cfs, Q100 = 14.0 cfs) is associated with The Bent Grass Residential Filing No. 2, lots 152-160, lots 163-168, Tract D, and portions of Thedford Court & Willmore Drive. Runoff from this basin flows via curb & gutter south on Thedford Court then continues flowing west along the northern curb & gutter along Willmore Drive before discharging into southeast corner of Basin EX-2 at **DP 1**.

Basin OS-5 (0.46 AC, Q5 = 1.1 cfs, Q100 = 2.3 cfs): is associated with The Bent Grass Residential Filing No. 2, lots 161 & 162 along with a portion of Silky Thread Road. Runoff from this basin generally flows to the west via curb & gutter along Silky Thread Road before discharging into the northeast corner of Basin EX-2 at **DP 2**.

Basin OS-6 (1.17 AC, Q5 = 2.0 cfs, Q100 = 4.3 cfs): is associated with The Bent Grass Residential Filing No. 2, the northern halves of Lots 170-178 and a portion of the southern side of Willmore Drive. Runoff from this basin generally flows to the west via curb & gutter along Willmore Drive before discharging into the northeast corner of Basin EX-3 at **DP 3**.

Basins E-1 thru E-5, C-8 and I-1, are basins from the Bent Grass Filing No. 2 report, which are
within the Falcon Meadows project area. The basins were "developed" as part of the Filing No. 2
project and retain the same basin and flow characteristics. Brief summaries from the Filing No. 2
report are included here for reference.

Basin E-1 (1.71 AC, Q5 = 3.6 cfs, Q100 = 7.7 cfs): a basin that is east of Falcon Meadows and encompasses the north portion of Bent Grass Meadows Drive. A high point on the far East of the basin at the near the Filing No. 2 boundary, forces water to flow to a low point at **DP-8**, which represents an existing 20' CDOT Type R sump inlet, which conveys stormwater via proposed 36" RCP storm sewer to the existing Filing No. 2 north water quality detention pond. Emergency overflow will spill over the crown of the road and enter into an existing 10' CDOT Type R sump inlet on the south side of Bent Grass Meadows Drive.

Basin E-2 (0.68 AC, Q5 = 2.4 cfs, Q100 = 4.6 cfs): a basin that is in west of Basin E-1 and encompasses a portion of the north section Bent Grass Meadows Drive. A high point on the far West of the basin forces water to flow to a low point at **DP-8**, which represents an existing 20' CDOT Type R sump inlet, which conveys stormwater via a proposed 36" RCP storm sewer to the existing Filing No. 2 north water quality detention pond. Emergency overflow will spill over the crown of the road and enter into an existing 10' CDOT Type R sump inlet on the south side of Bent Grass Meadows Drive.

Basin E-3 (0.78 AC, Q5 = 2.9 cfs, Q100 = 5.3 cfs): a basin that is south of Basin E-2 and encompasses a portion of the south half of Bent Grass Meadows Drive. A high point on the far West of the basin forces water to flow to a low point, which is an existing 10' CDOT Type R sump inlet, which conveys stormwater via an existing 24" storm sewer to **DP-8**. This inlet receives emergency overflow from DP-8.

Basin E-4 (0.91 AC, Q5 = 3.0 cfs, Q100 = 5.7 cfs): a basin that is in the Southwest area of the Bent Grass Filing No. 2 site and encompasses a portion of the north and west sections of Bent Grass Meadows Drive. Runoff from this basin is captured by existing curb and gutter and then routed South where the 5 yr. and 100 yr. flows will be captured by an existing 25' CDOT Type R (1-10' and 1-15' inlet) on-grade inlet, **DP-24**. Captured flow will be routed by a 24" RCP storm drain piped to DP-25. A temporary water quality facility will treat this flow for the Bent Grass Filing No. 2 development and will remain in place until further development occurs.

Basin E-5 (0.89 AC, Q5 = 3.3 cfs, Q100 = 6.1 cfs): a basin that is in the Southwest area of the site and encompasses a portion of south and east sections Bent Grass Meadows Drive. Runoff from this basin is captured by existing curb and gutter and then routed South where the 5 yr. and 100 yr. flows will be captured by a proposed 25' CDOT Type R (1-10' and 1-15' inlet) on-grade inlet, **DP-25**. Captured flow will be routed by a 24" RCP storm drain piped to an outfall at DP-26, where a temporary sediment basin will provide water quality for the basin. Flows will then be routed East by Existing Swale – F until out-falling into RWT210.

Basin C-8 (0.42 AC, Q5 = 0.2 cfs, Q100 = 1.0 cfs): a basin that is in the South-central area of the site adjacent to RWT204 and RWT 210. It encompasses the rears of single-family residential Type B lots. Runoff will sheet flow West directly into RWT204 and RWT210.

Design Point CC is the location in channel reach RWT210, where flows exit the Bent Grass Site, including the offsite flows from RWT202, RWT204 and WT200. The minor flows are 302.4 cfs and the major flows are 1336.7 cfs.

269?

1040 per DBPS - pg 109 of MDDP?

If grass buffers are proposed they need to meet criteria, be within a PBMP easement and be shown on the WQCV Plan

VI. Four Step Process

The Four Step Process is used to minimize the adverse impacts of urbanization and is a vital component of developing a balanced, sustainable project. Below identifies the approach to the four-step process:

1. Employ Runoff Reduction Practices

This step uses low impact development (LID) practices to reduce runoff at the source. Generally, rather than creating point discharges that are directly connected to impervious areas runoff is routed through pervious areas to promote infiltration. Grass buffers have been utilized where possible. The Impervious Reduction Factor (IRF) method was used and calculations can be found in Appendix B.

2. Provide Water Quality Capture Volume (WQCV)

This step utilizes formalized water quality capture volume to slow the release of runoff from the site.

The EURV volume will release in 72 hours, while the WQCV will release in no less than 40 hours. Onsite water quality control volume detention ponds will provide water quality treatment for all but 0.86 acres of the developed areas, prior to the runoff being released into the channel. Refer to WQCV Plan in Appendix D.

See redlines; any areas net treated need to be justifiable

3. Stabilize Drainageways

This step implements stabilization to channels to accommodate developed flows while protecting infrastructure and controlling sediment loading from erosion in the drainageways. Erosion protection in the form of riprap pads at all outfall points to the channel to prevent scouring of the channel from point discharges. A HEC-RAS model will be created and used to evaluate the stability of the existing and proposed channels as part of the Final Drainage Report for the next phase of the site.

4. Consider Need for Industrial and Commercial BMPs

As this project as all residential development and no commercial or industrial development is proposed, there will be no need for any specialized BMPs which would be associated with an industrial or commercial site.

VII. Proposed Drainage Conditions

There have been very minor changes to the overall Falcon Area Basin delineation with the proposed condition. This will be discussed with the individual basins. All necessary calculations can be found within the appendices of the report.

According to the DBPS, there are two channels that run through the site. As was discussed within the Existing Conditions portion of the report both the RWT202 and RWT204 run through the site. In the Bent Grass Filing No. 2 report & CD's, the RWT202 channel was rerouted to run along the north boundary & combine with the existing RWT204 channel. The proposed development will drain to the RWT204 channel, which becomes RWT210 south of Bent Grass Meadows Drive.

The site will provide two WQCV Detention Ponds, North Pond & South Pond, to provide water quality treatment prior to discharging the runoff directly into the West Tributary channel RWT204 - RWT210.

As has been mentioned previously, the site is proposed to be single family residential. The site has been designed to provide a large lot buffer between the existing large lots to the north and west of the site and the proposed site. Beyond this buffer, the remainder of the site is smaller, approximately 1/8 acre lots.

address OS-2 and OS-3

Basin OS-1 (32.28 AC, Q5 = 15.1 cfs, Q100 = 65.1 cfs) is associated with The Meadows Filing No. 3 lots 14, 15, 16, and 17. Runoff from this basin sheet flows to the northern property line of the site and then flows, via an existing drainage swale, into the existing changel reach RWT204 from the Falcon DBPS at flows don't match plan

Basin OS-4 (4.46 AC, Q5 = 5.6 cfs, Q100 = 14.0 cfs) is associated with The Bent Grass Residential Filing No. 2, lots 152-160, lots 163-168, Tract D, and portions of Thedford Court & Willmore Drive. Runoff from this basin flows via curb & gutter south on Thedford Court then continues flowing west along the northern curb & gutter along Willmore Drive before discharging into Basin A-1 at **DP 1**.

Basin OS-5 (0.46 AC, Q5 = 1.1 cfs, Q100 = 2.3 cfs): is associated with The Bent Grass Residential Filing No. 2, lots 161 & 162 along with a portion of Silky Thread Road. Runoff from this basin generally flows to the west via curb & gutter along Silky Thread Road before discharging into Basin A-1 at DP 2.

Basin OS-6 (1.17 AC, Q5 = 2.0 cfs, Q100 = 4.3 cfs): is associated with The Bent Grass Residential Filing No. 2, the northern halves of Lots 170-178 and a portion of the southern side of Willmore Drive. Runoff from this basin generally flows to the west via curb & gutter along Willmore Drive before discharging into Basin A-1 at **DP 3**.

Basin A-1 (2.16 AC, Q5 = 4.9 cfs, Q100 = 11.7 cfs): a basin that includes residential lots, portions of 2 tracts & the east half of Lemon Grass Road. It encompasses single-family residential lots. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 4**. Flows will then enter a proposed CDOT Type 'R' inlet and will be piped into the existing Bent Grass Filing No. 2 WQCV pond located in Basin A-2 at **DP 6**.

Basin A-2 (0.86 AC, Q5 = 2.0 cfs, Q100 = 4.4 cfs); a basin that includes the back \(\frac{3}{2} \) of single-family residential lots. Runoff will flow from each lot into the existing channel (RWT204). These flows will not be detained but are less than 1.0 acre max allowed per criteria. justification is required and MDDP

Says all areas will be treated Basin A-3 (0.92 AC, Q5 = 2.6 cfs, Q100 = 5.2 cfs): a basin that includes the west half of Lemon Grass Road and the front 1/4 of single-family residential lots. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to DP 5. Flows will then enter a proposed CDOT Type 'R' inlet where it will be piped into the existing Bent Grass Filing No. 2 WQCV pond.

Basin A-4 (0.82 AC, Q5 = 0.4 cfs, Q100 = 2.6 cfs): a basin that includes the existing north water quality facility built with Bent Grass Filing No. 2 (Tract K). This basin will combine with the other flows being diverted to this facility and upon treatment, will be released into the existing channel (RWT204).

Basin C-6 (1.37 AC, Q5 = 2.1 cfs, Q100 = 5.1 cfs): a basin that includes a portion of residential lots between Henzlee Place and Channel RWT204. These lots drain towards the east, towards the channel. A proposed swale with intercept these flows at the top bank of the channel and divert the flows towards the south to DP 19, where an area inlet will capture the flows and release into the proposed north water quality pond.

Basin B-1 (4.32 AC, Q5 = 2.2 cfs, Q100 = 7.8 cfs): a basin that is in the center of the site and encompasses the existing rerouted channel RWT202 and existing improved channel RWT204. Flows will sheet flow into the existing channel where they will then be conveyed to DP 22.

- north-

Basin C-1 (9.07 AC, Q5 = 16.9 cfs, Q100 = 36.0 cfs): a basin that includes Sophia Lane, the west half of Henzlee Place, north portion of Kittrick Place, and encompasses single-family residential lots. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 15.** Flows will then enter a proposed CDOT Type 'R' inlet where it will be piped to the proposed north WQCV pond at **DP 13**.

Basin C-2 (1.11 AC, Q5 = 2.8 cfs, Q100 = 6.2 cfs): It encompasses single-family residential lots including the east half of Henzlee Place. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 12.** Flows will then enter a proposed CDOT Type 'R' inlet where it will be piped to the proposed north WQCV pond at **DP 13**.

Basin C-3 (1.52 AC, Q5 = 5.3 cfs, Q100 = 9.9 cfs): It encompasses Kittrick Place between Henzlee Place & Daelyn Drive, as well as single-family residential lots. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DF 8.** Flows will then enter an existing CDOT Type 'R' inlet on the north side of Bent Grass Meadows Drive, where it will then be released into the existing Filing No. 2 North WQCV Pond.

Basin C-4 (4.70 AC, Q5 = 8.0 cfs, Q100 = 21.0 cfs): It encompasses residential lots and open space between Henzlee Place & Bent Grass Meadows Drive. Runoff will flow from each lot onto the proposed open space, eventually releasing into the public R.O.W. of Bent Grass Meadows Drive, where existing curb and gutter will convey flows to **DP 8.** Flows will then enter an existing CDOT Type 'R' inlet where it will then be released into the existing Filing No. 2 North WQCV Pond.

Basin C-5 (0.51 AC, Q5 = 0.3 cfs, Q100 = 1.6 cfs): It encompasses the proposed north WQCV pond area. The stormwater within the proposed north WQCV pond will be released at a controlled rate, via an outlet structure with orifice holes, into the existing channel RWT204.

Basin OS-2 (20.07 AC, Q5 = 9.0 cfs, Q100 = 43.4 cfs): is associated with The Meadows Filing No. 1 lots 1, 2, 3, 4, 5, and 6. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site at **DP 15**. Flows will then be conveyed via a proposed drainage swale to the south where it will enter Basin D-3 and tie-into the existing drainage swale along the southern boundary of Basin D-3. It will then continue flowing east before entering an existing area inlet at **DP 11** where it will be piped, ultimately outfalling into the proposed south WQCV pond at **DP 31**.

Basin OS-3 (10.61 AC, Q5 = 4.7 cfs, Q100 = 24.3 cfs): is associated with The Meadows Filing No. 1 lot 11 and The Meadows Filing No. 2 Lots 1 & 2. Runoff from this basin sheet flows from the northwest to the southeast, crossing the west property line of the site into Basin D-3 at **DP 10**. Flows will then be conveyed via an existing drainage swale to the east where it will enter an existing area inlet at **DP 11** where it will be piped, ultimately outfalling into the proposed south WQCV pond at **DP 31**.

- DP9?

Basin D-1 (8.13 AC, Q5 = 10.0 cfs, Q100 = 23.8 cfs): a basin along the west property line of the site. It encompasses single-family residential lots, Isabel Place, & west half of Daelyn Drive. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 16.** Flows will then enter a proposed CDOT at grade Type 'R' inlet where captured flows will then be piped and ultimately outfall in the proposed south WQCV pond at **DP 31**. Bypass flows from the inlet will continue to the south in Bent Grass Meadows Drive to be intercepted by the existing CDOT Type R inlet at **DP 24**.

Basin D-2 (6.72 AC, Q5 = 14.3 cfs, Q100 = 29.6 cfs): a basin east of Basin D-1. It encompasses single-family residential lots, Isabel Place, Raylan Way, Jolie Court, as well as the east half of Daelyn Drive. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 14.** Flows will then enter a proposed at grade CDOT Type 'R' inlet where captured flows will then be piped and ultimately outfall in the proposed south WQCV pond at **DP 31**. Bypass flows from the inlet would overtop Rowena Way to **DP 16**. □ DP24?

Basin D-3 (2.93 AC, Q5 = 2.0 cfs, Q100 = 5.1 cfs): a basin that is in the southwest corner of the site, south of Basin D-1. It encompasses the backs of several proposed residential lots as well as an existing drainage ditch and proposed Swale D. Runoff will flow from basin OS-2 and OS-3 into Swale D, and convey flows to the existing drainage ditch which will convey flows to an existing area inlet at **DP 11**. From there, flows will be piped and ultimately outfall at the south WQCV pond at **DP 31**.

Basin D-4 (4.38 AC, Q5 = 7.8 cfs, Q100 = 16.6 cfs): a basin that is east of Bent Grass Meadows Drive. It encompasses single-family residential lots, Rowena Way, & portions of Linley Way, Jayla Trail, and Henzlee Place. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to DP 17. Overflow from this inlet would be to overtop the curb and then continue via a proposed swale, following the same path as the proposed pipe, to the east until flows are released into the proposed south water quality pond. Flows will then enter a proposed sump CDOT Type 'R' inlet where it will then be piped and ultimately out all in the proposed south WQCV pond at DP 31.

Basin D-5 (1.08 AC, Q5 = 2.2 cfs, Q100 = 4.6 cfs): a basin that is located at the southwest corner of Bent Grass Meadows Drive and Henzlee Place. It includes residential lots, as well as a portion of the north half of Nico Way and west half of Henzlee Place. Flows will be directed towards the public R.O.W. where proposed curb and gutter will convey flows to the south along Henzlee Place to **DP 18**. Flows will then enter a proposed CDOT Type 'R' inlet where it will then be piped and ultimately outfall in the proposed

— provide size

Basin D-6 (4.01 AC, Q5 = 8.2 cfs, Q100 = 17.2 cfs): a basin that is south of Basin D-5 & east of Basin D-4. It encompasses single-family residential lots & half of Linley Way, Jayla Trail, Henzlee Place, & Nico Way. Runoff will flow from each lot onto the proposed public R.O.W. where proposed mountable curb and gutter will convey flows to **DP 18.** Flows will then enter a proposed sump CDOT Type 'R' inlet where it will then be piped and ultimately outfall in the proposed south WQCV pond at **DP 31**.

Basin D-7 (6.39 AC, Q5 = 3.2 cfs, Q100 = 14.8 cfs): a basin that is in the south end of the site, east of Bent Grass Meadows Drive & west of the existing channel. It encompasses the back half of several single-family residential lots as well as proposed south WQCV pond, an existing sediment basin, and an existing drainage ditch. Runoff will flow, via sheet flow, until it enters the existing drainage ditch and is conveyed to the proposed south WQCV pond or will directly flow into the proposed south WQCV pond.

Basin D-8 (1.69 AC, Q5 = 1.3 cfs, Q100 = 4.5 cfs): a basin that is west of the existing channel & south of Bent Grass Meadows Drive. It encompasses the back half of single-family residential lots. Runoff will flow from each lot and discharge into a proposed drainage ditch. The drainage ditch (Swale C) will then convey flows, ultimately discharging into the proposed south WQCV pond at **DP 32**.

Basin B-2 (1.17 AC, Q5 = 0.4 cfs, Q100 = 2.5 cfs): a basin that is in the south area of the site and encompasses the existing channel RWT210. Flows will sheet flow into the existing channel where they will then be conveyed to **DP CC** exiting the site.

south WQCV pond at **PP 31**.

Basins E-1 thru E-5 are the same as discussed under the Existing Conditions Section, as these basins represent the already built Bent Grass Meadows Drive through the proposed site.

Basin RWT202 (1574.4 AC,Q5 = 200 cfs, Q100 = 1000 cfs), RWT204 (38.4 AC, Q5 = 7 cfs, Q100 = 43 cfs) and WT200 (192 AC, Q5 = 52 cfs, Q100 = 190 cfs) represent larger offsite basins to the north of the proposed project. These areas were studied as part of the Falcon Basin DBPS prepared by Matrix and were also part of the Bent Grass MDDP, submitted for review in January. There have been no changes to these basins as they are offsite and existing.

Provide combined flows

Design Point CC is the location in channel reach RWT210, where flows exit the Bent Grass Site, including the offsite flows from RWT202, RWT204 and WT200. The minor flows are 260.1 cfs and the major flows are 1137.6 cfs.

VIII. Storm Sewer System

All development is anticipated to be urban and will include storm sewer & street inlets. Storm sewers collect storm water runoff and convey the water to water quality facilities prior to discharging. Storm sewer systems will be designed to the 100-year storm and checked with the 5-year storm. Inlets will be placed at sump areas and intersections where street flow is larger than street capacity. UDFCD Inlet spreadsheet will be used to determine the size of all at-grade and sump inlets. There will be a minimum of 3 proposed storm systems within the site. One will collect flows on the north and east side of the project, prior to entering Bent Grass Meadows Drive. Intercepted flows will be released into the Bent Grass Filing No. 2 existing North water quality pond. Any bypass flows will travel west in Bent Grass Meadows Drive to an existing storm system in the roadway.

has been?

The second system will collect the north and west portion of the site, intercepting flows prior to entering Bent Grass Meadows Drive. These flows will be released into the proposed North water quality pond. Any flows bypassed from the storm system will enter Bent Grass Meadows Drive and travel east to the existing storm sewer system.

Or existing Filing 2 pond?

The final proposed system will be designed for the remaining south and west portion of the project. Flows intercepted by inlets will be released into the proposed South water quality pond.

state the proposed materials (RCP, CDOT type R inlets)
Final drainage report will include details concerning inlet location, street capacity, storm sewer sizing,
outlet protection and location.
The south pond will be constructed in

IX. Proposed Water Quality Detention Ponds requirements with the early grading.

Two Water Quality Capture Volume Detention Ponds will be provided for the proposed site. One will be provided for the area north of Bent Grass Meadows Drive and the other will be provided for the area to the south Both ponds are private and will be maintained by Bent Grass Metro District. These detention ponds will only provide water quality. The EURV and 100-year volumes will be conveyed via the emergency overflow weir, which will be lined. The water quality volume release will be controlled with an orifice plate that will release in 40 hours. Outlet structures, forebays, trickle channels, etc. will be designed with the final drainage report during final plat. The required WQCV volume of the North & South pond are 0.289 acre-feet & 0.875 acre-feet, relatively. The north water quality pond will release into RWT204 and the south will release into RWT210. Initial sizing of the ponds has been provided in Appendix C.

Address revisions to the existing F2 north pond

X. Proposed Channel Improvements

The channel design is anticipated to have a series of Grouted Sloping Boulder Drops within it. Final design and details of the channel and associated structures will be provided with the corresponding Final Drainage Reports.

Riprap protection will be provided at the individual outfalls from the site into the channel to prevent scouring from the point discharges if velocity constraints are not met.

Improvements to the existing channel are outlined in the Master Development Drainage Plan for Bent Grass Residential Subdivision (MDDP). As part of this development, improvements outlined in the MDDP for the existing channel will be implemented. Final design of the channel and all improvements associated with it will be completed with the Final Drainage Report, including channel grading, drop/check structure design, etc.

XI. Maintenance

You need to address whether the DBPS improvements will be adequate for the increased flows (~1300 vs ~900 cfs? and what the proposed revisions are.

The proposed channels are to be public facilities. A buffer has been provided along the north boundary of the site between the rerouted channel RWT202 and the back of the proposed lots. After completion of construction and upon the Board of County Commissioners acceptance the West Tributary channel is anticipated to be owned and maintained by EI Paso County along with all drainage facilities within the public Right-of-Way. Swale D, which is located along the west property line, will run through an existing easement through the back of several residential lots. The swale will be maintained by the Bent Grass Metro District.

proposed tract

The existing swale along the north property line, built as part of Bent Grass Filing No. 2, will have a maintenance access road constructed beginning at the north end of the Lemon Grass Road cul-de sacs

to be maintained

XII. Wetlands Mitigation by the district?

No wetlands are located on site.

Also address the swale from the northwest corner in Tract G

XIII. Floodplain Statement

A portion of the project site lies within Zone AE Special Flood Hazard Area as defined by the FIRM Map number 08041C0553G effective December 7, 2018. A copy of the FIRM Panel is included in Appendix A.

The portion of channel that has a floodplain designation is only the RWT210 and RWT204 portions of the channel. It is unknown why the western channel, RWT202 is unmapped since it is the larger contributor regarding flow rates. Discussions have occurred with PPRBD and a no rise certificate will be required for the existing channel. Models have been obtained from FEMA which show that the FEMA discharges are higher than the DBPS. Therefore, the culvert crossing at Bent Grass Meadows Parkway has been sized per the FEMA flows and not the DBPS. The no rise certification will be provided under a separate report.

XIV. Drainage Fees & Maintenance

Falcon Basin is part of the El Paso County drainage basin fee program all applicable fees well be presented in the final drainage report.

A presentation of accurate, complete, and current estimate of cost for proposed facilities will be presented with the final drainage report.

XV. Conclusion

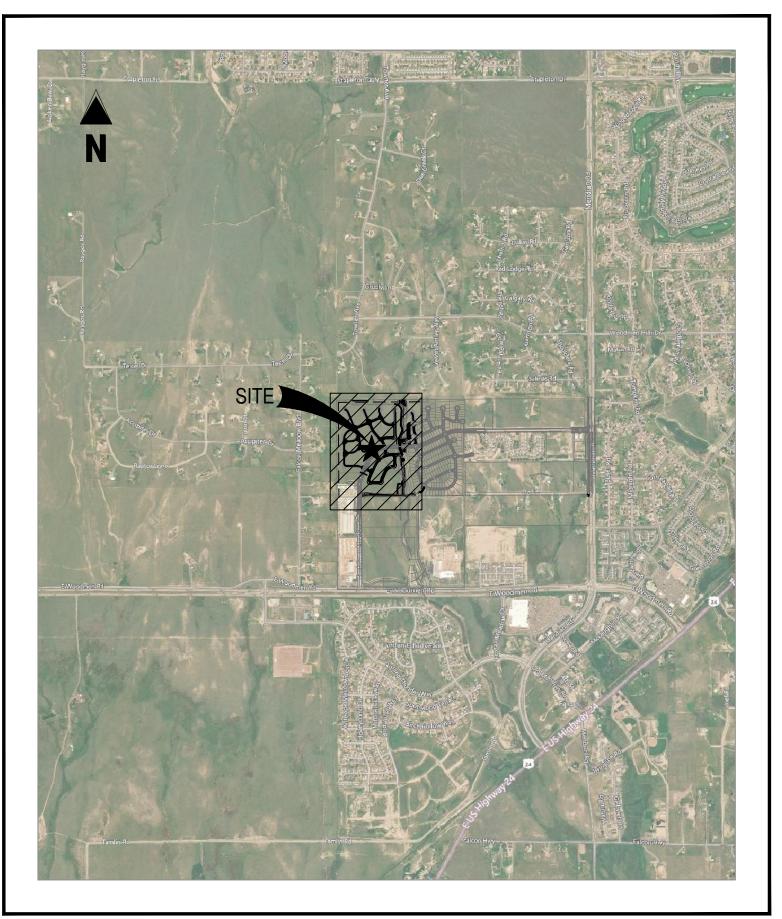
The Falcon Meadows at Bent Grass residential subdivision lies within the West Tributary of the Falcon Area Watershed. Recommendations are made within this report to establish and stabilize multiple drainageways through the project site. Water quality for the site is provided in two on-site WQCV ponds, North Pond & South Pond. All drainage facilities within this report were sized according to the El Paso County Drainage Criteria Manuals. The West Tributary channel segment is proposed to be publicly owned and maintained and shall be the responsibility of El Paso County. The two WQCV ponds and all of the swales will be maintained by Bent Grass Metro District. A Final Drainage Report will be submitted along with the final plat and construction drawings.

XVI. References

upon completion of the required improvements

- 1. City of Colorado Springs/County of El Paso Drainage Criteria Manual, October 1991.
- 2. Drainage Criteria Manual, Volume 2, City of Colorado Springs, November 2002.
- 3. *Urban Storm Drainage Criteria Manual*, Urban Drainage and Flood Control District, January 2016 (with current revisions).
- 4. Falcon Drainage Basin Planning Study, by Matrix Design Group, September 2015.
- 5. *Master Development Drainage Plan and Preliminary Drainage Plan Bent Grass Subdivision*, by Kiowa Engineering Corporation, December 2006.
- 6. Final Drainage Report for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2014.
- 7. Final Drainage Report Addendum for Bent Grass Residential (Filing No. 1), by Classic Consulting Engineers & Surveyors, LLC, August 2015.
- 8. *Master Development Drainage Plan for The Ranch*, by Classic Consulting Engineers & Surveyors, LLC, November 2018.
- 9. Falcon Highlands Master Development Drainage Plan & Preliminary Drainage Report & Final Drainage Report for Filing 1, by URS, January 2005.
- Final Drainage Report and Erosion Control Plan Latigo Business Center Filing No. 1 A Resubdivision of a Portion of Latigo Business and Research Center Filing No. 1, by Kiowa Engineering Corporation, November 2004.
- 11. Final Drainage Report for Bent Grass Residential (Filing No. 2), by Galloway & Company, May 2020.

APPENDIX A Exhibits and Figures



FALCON MEADOWS AT BENT GRASS

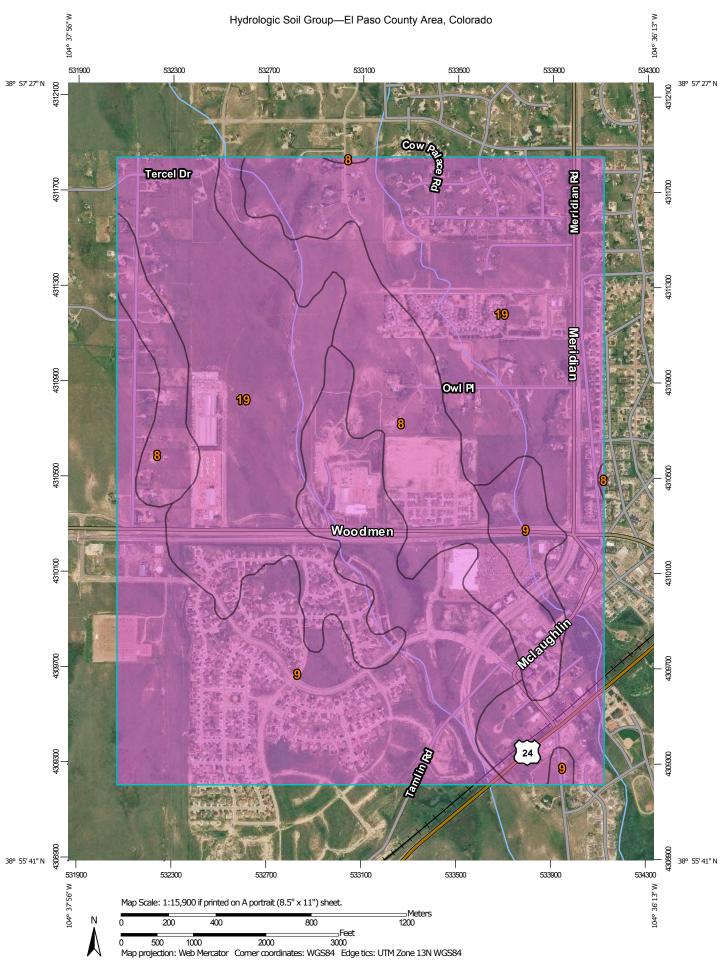
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BENT GRASS MEADOWS DRIVE SCALE: 1"=2,000' VICINITY MAP

Project No:	CLH000017.20
Drawn By:	TJE
Checked By:	CMD
Date:	06/19/2020



1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920 719.900.7220 • GallowayUS.com



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Please rely on the bar scale on each map sheet for map Soils D measurements. Soil Rating Polygons Not rated or not available Α Source of Map: Natural Resources Conservation Service Web Soil Survey URL: **Water Features** A/D Coordinate System: Web Mercator (EPSG:3857) Streams and Canals В Maps from the Web Soil Survey are based on the Web Mercator Transportation projection, which preserves direction and shape but distorts B/D Rails --distance and area. A projection that preserves area, such as the С Albers equal-area conic projection, should be used if more Interstate Highways accurate calculations of distance or area are required. C/D **US Routes** This product is generated from the USDA-NRCS certified data as D Major Roads of the version date(s) listed below. Not rated or not available -Local Roads Soil Survey Area: El Paso County Area, Colorado Soil Rating Lines Survey Area Data: Version 16, Sep 10, 2018 Background Aerial Photography Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. A/D Date(s) aerial images were photographed: Jun 7, 2016—Aug 17, 2017 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor C/D shifting of map unit boundaries may be evident. D Not rated or not available **Soil Rating Points** Α A/D B/D

Hydrologic Soil Group

	_			
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	А	214.3	16.0%
9	Blakeland-Fluvaquentic Haplaquolls	А	465.8	34.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	662.6	49.3%
Totals for Area of Inter	est		1,342.6	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

obtain more detailed information in areas where Base Flood Elevations (BFEs o obtain more detailed information in areas where Base Flood Elevations (BFEs didor floodways have been determined, users are encouraged to consult the Floo roffles and Floodway Data and/or Summary of Stillwater Elevations tables contains tithin the Flood Insurance Study (FIS) report that accompanies this FIRM. User hould be aware that BFEs shown on the FIRM represent rounded whole-for levations. These BFEs are intended for flood insurance rating purposes only an hould not be used as the sole source of flood elevation information. Accordingly considerations are sold to the sole source of flood elevation information. od elevation data presented in the FIS report should be utilized in conjunction w FIRM for purposes of construction and/or floodplain managemen

Coastal Base Flood Elevations shown on this map apply only landward of 0. North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be waver that coastal flood elevations are also provided in the Summary of Stillwate clevations table in the Flood Insurance Study report for this jurisdiction. Elevation thown in the Summary of Stillwater Elevations table should be used for construction. d/or floodplain management purposes when they are higher than the elevation own on this FIRM.

oundaries of the **floodways** were computed at cross sections and interpolate tween cross sections. The floodways were based on hydraulic considerations wit gard to requirements of the National Flood Insurance Program. Floodway to do ther pertinent floodway data are provided in the Flood insurance Study repo

The projection used in the preparation of this map was Universal Transvers Mercator (UTM) zone 13. The horizontal datum was NADB3, GRS80 spheroic Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positions differences in map features across jurisdiction boundaries. These differences do no affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure am argound elevations referenced to the same verifical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following nerforess:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Iver Spring, MD 20910-3282

o obtain current elevation, description, and/or location information for **bench mar** hown on this map, please contact the Information Services Branch of the Natio leodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Pas County, Colorado Springs Utilities, City of Fountain, Bureau of Land Managemen National Oceanic and Atmospheric Administration, United States Geological Survey and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations an floodplain delineations than those shown on the previous FIRM for this jurisdiction for floodplains and floodways that were transferred from the previous FIRM manave been adjusted to conform to these new stream channel configurations. As result, the Flood Profles and Floodway Data tables in the Flood Insurance Stud suit, rine ricota ricinies and ricotavay Data latines in the ricota insurance study peport (which contains authoritistive hydraulic data) may reflect stream channel stances that differ from what is shown on this map. The profile baselines depicted this map represent the hydraulic modeling baselines that match the flood profile this map represent the hydraulic modeling baselines that when the flood profile depicts are some stream of the profile selficies may deviate significantly from the new base map channel representation. nd may appear outside of the floodplair

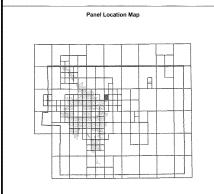
orporate limits shown on this map are based on the best data available at the tim publication. Because changes due to annexations or de-annexations may hav courred after this map was published, map users should contact appropriat ommunity officials to verify current corporate limit locations.

lease refer to the separately printed Map Index for an overview map of the count howing the layout of map panels; community map repository addresses; and a string of Communities table containing National Flood Insurance Program dates fo ach community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchang (FMIX) 1-877-336-2627 for information on available products associated with this FIRM, Available products may include previously issued Letters of Map Change, Flood Insurance Study Report, and/or digital versions of this map. The MSC mails be reached by Fax at 1-800-358-9620 and its website a http://www.msc.lena.gov/.

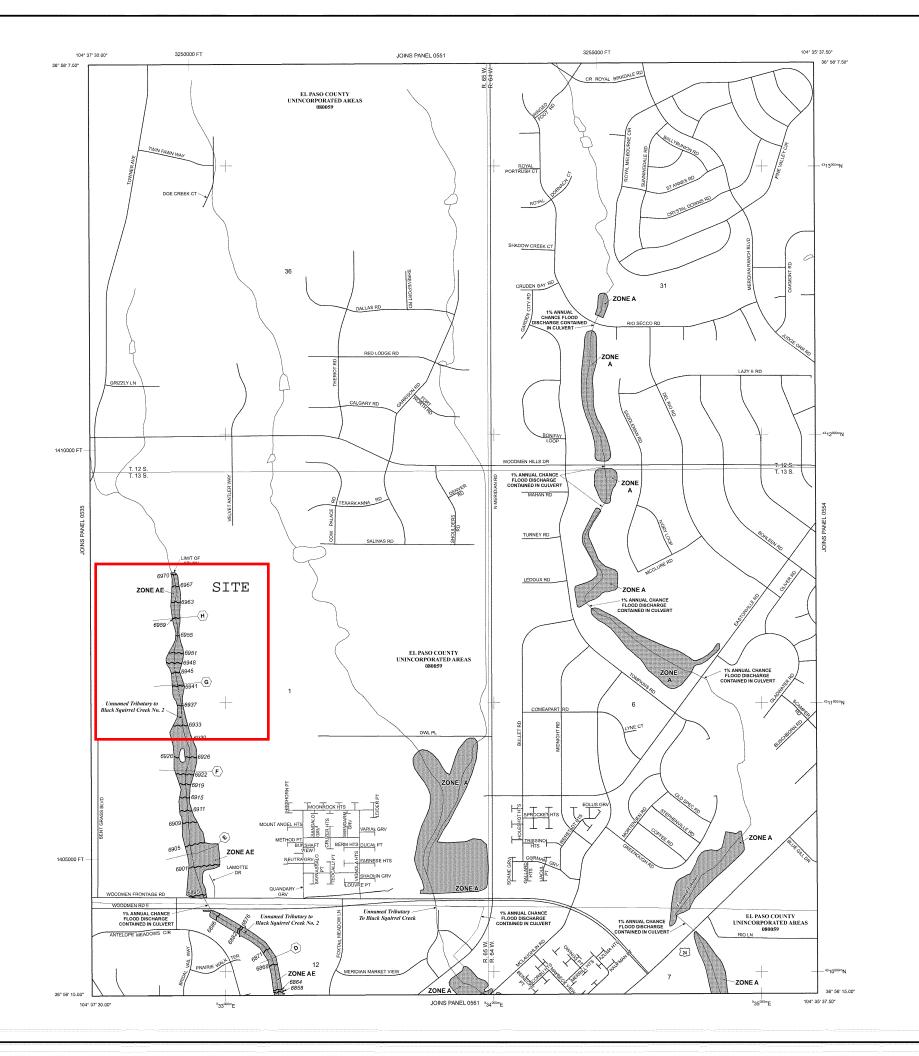
you have **questions about this map** or questions concerning the National Floc isurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) (sit the FEMA website at http://www.fema.gov/business/nfip.

El Paso County Vertical Datum Offset Table Flooding Source REFER TO SECTION 3.3 OF THE EL PASC FOR STREAM BY STREAM VERTICAL D



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Apaco





LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard annual chance flood on the 1% annual chance flood that of the 1% annual chance flood.

No Base Flood Elevations determined.
Base Flood Elevations determined.
Flood depths of 1 to 3 feet (usuality areas of ponding); Base Flood
Elevations determined.

Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodway boundary

Zone D Boundary CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

~~ 513 ~~ Base Flood Elevation line and value; elevation in feet Base Flood Elevation value where uniform within zone; elevation in feet*

 $\begin{picture}(100,0) \put(0,0){\line} \put(0,0){\li$

(23)-----(23)

97° 07' 30.00° 32° 22' 30.00° Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

_ M1.5

MAP REPOSITORIES Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elev Special Flood Hazard Areas, to update map format, to add roads and road na incorporate previously issued Letters of Map Revision.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500' 250 0 500 1000 FEET

PANEL 0553G

FIRM

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 553 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COMMUNITY

NUMBER PANEL SUFFIX



MAP NUMBER 08041C0553G MAP REVISED

DECEMBER 7, 2018 Federal Emergency Management Agency

FALCON DRAINAGE BASIN PLANNING STUDY SELECTED PLAN REPORT FINAL - SEPTEMBER 2015

Prepared for:



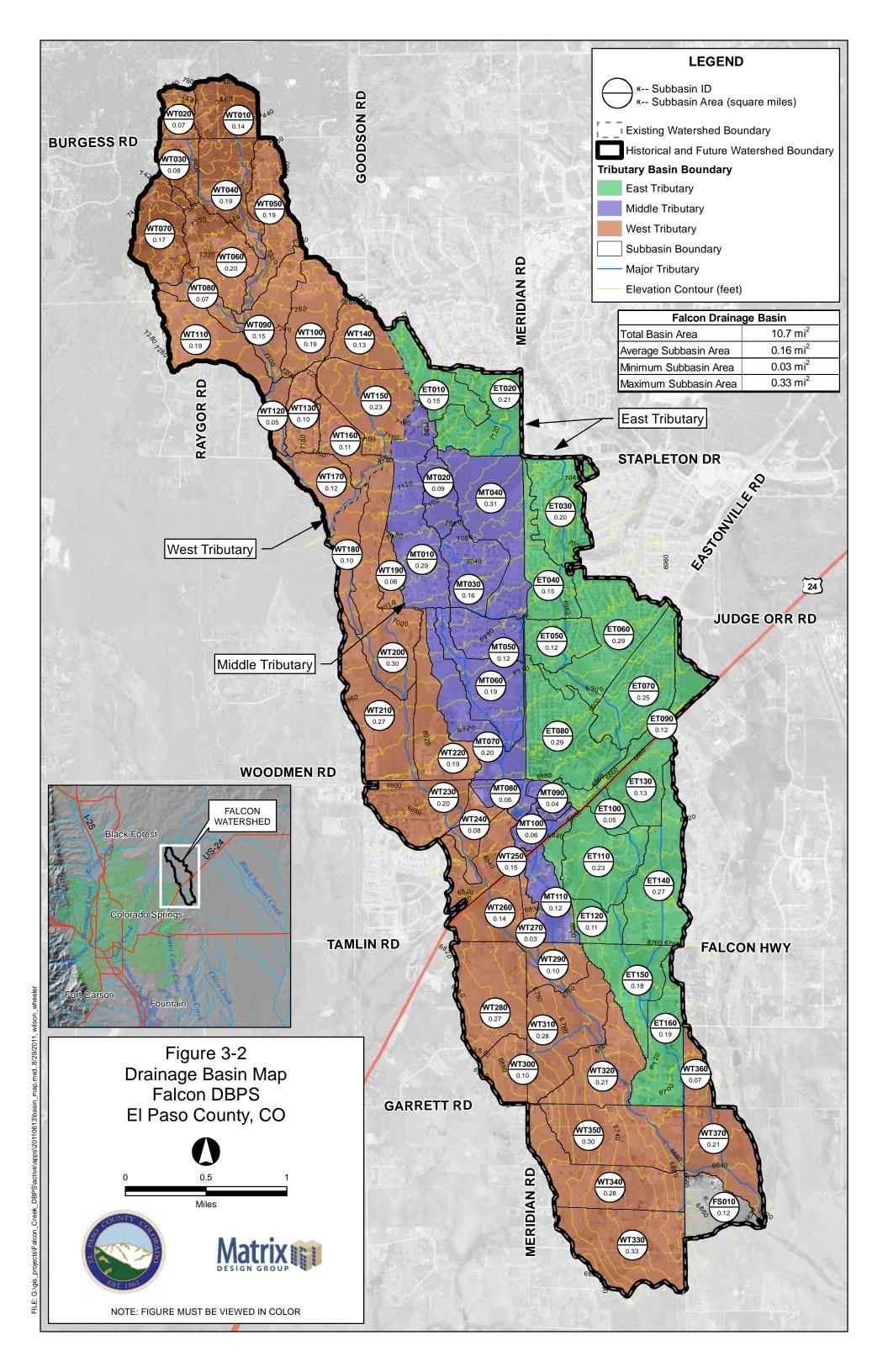
El Paso County Public Services Department 3275 Akers Drive Colorado Springs, CO 80922

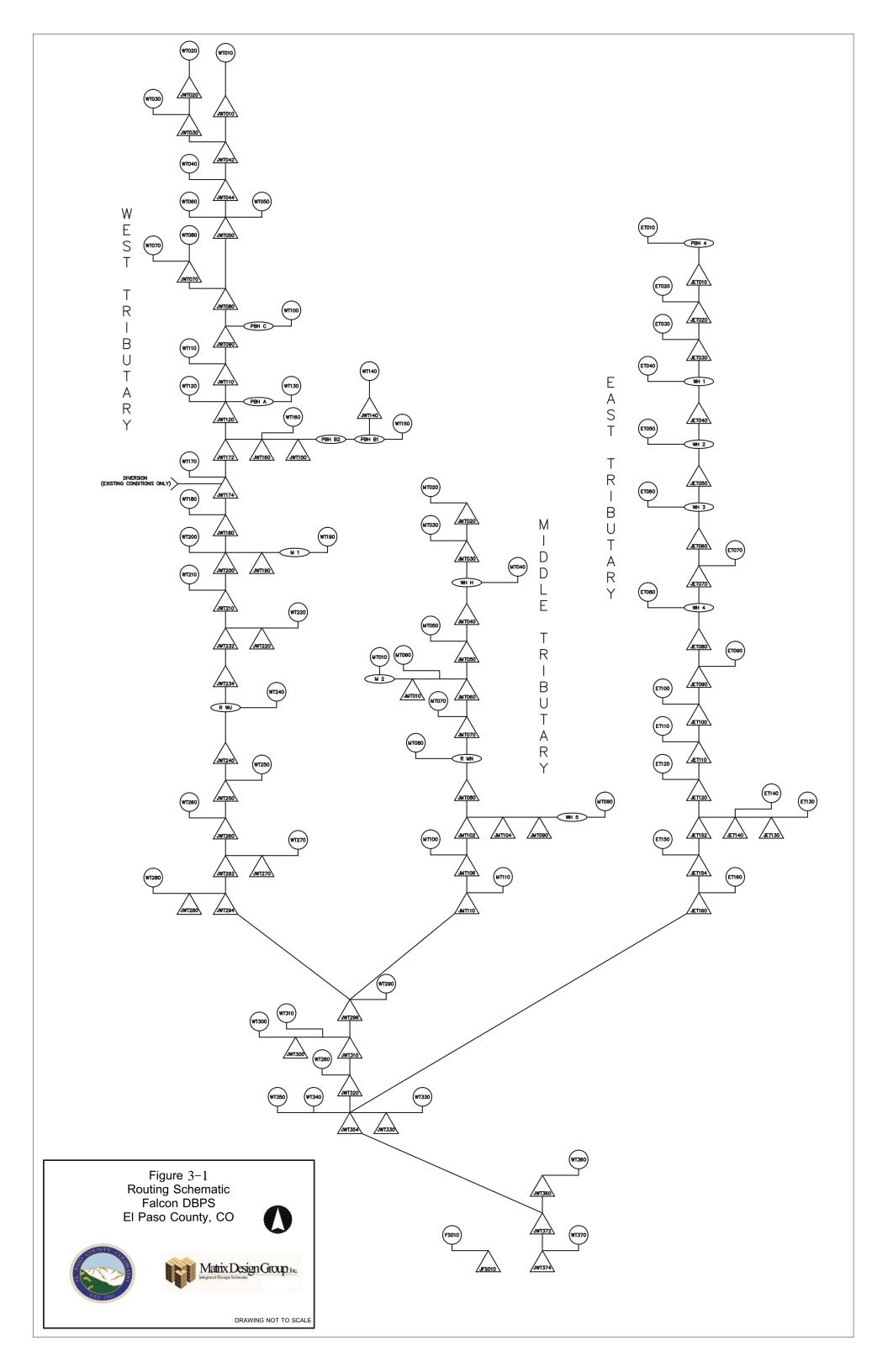
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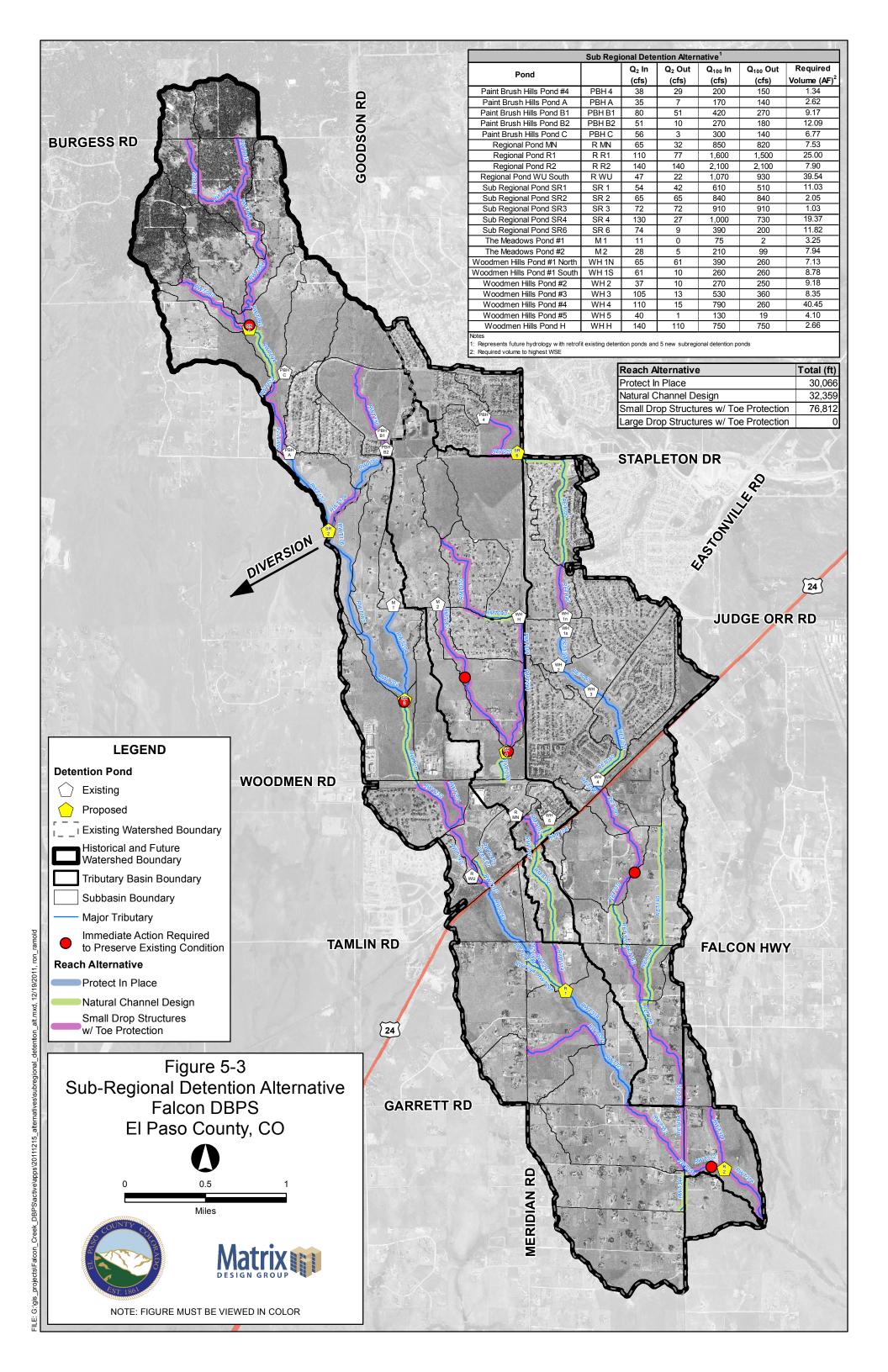


Matrix Design Group 2435 Research Parkway, Suite 300 Colorado Springs, CO 80920

Matrix Project No. 10.122.003







APPENDIX B Hydrologic Computations

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Designer: CMWJ Calculated cells Galloway & Co. Company: ***Design Storm: 1-Hour Rain Depth WQCV Event 0.60 inches February 9, 2021 ···Minor Storm: 1-Hour Rain Depth 5-Year Event 1.50 inches Falcon Meadows at Bent Grass ·--Major Storm: 1-Hour Rain Depth 100-Year Event 2.52 North WQ Pond inches Location: Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency 100-Year Event Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier Receiving Pervious Area Soil Type Sandy Loam Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 13.580 Directly Connected Impervious Area (DCIA, acres) 5.300 Unconnected Impervious Area (UIA, acres) 2.900 Receiving Pervious Area (RPA, acres) 0.000 Separate Pervious Area (SPA, acres) 5.380 RPA Treatment Type: Conveyance (C) С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) 13.580 Total Calculated Area (ac, check against input) Directly Connected Impervious Area (DCIA, %) 39.0% Unconnected Impervious Area (UIA, %) 21.4% Receiving Pervious Area (RPA, %) 0.0% Separate Pervious Area (SPA, %) 39.6% A_R (RPA / UIA) 0.000 I, Check 1 000 f / I for WQCV Event: 1.7 f / I for 5-Year Event 0.5 f / I for 100-Year Event: 0.3 f / I for Optional User Defined Storm CUHP. IRF for WQCV Event: 1.00 IRF for 5-Year Event: 1.00 IRF for 100-Year Event: 1.00 IRF for Optional User Defined Storm CUHP. Total Site Imperviousness: I_{total} 60.4% Effective Imperviousness for WQCV Event: 60.4% Effective Imperviousness for 5-Year Event: 60.4% Effective Imperviousness for 100-Year Event: 60.4% Effective Imperviousness for Optional User Defined Storm CUHP LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% N/A This line only for 10-Year Event N/A 100-Year Event CREDIT**: Reduce Detention By: 0.0% N/A User Defined CUHP CREDIT: Reduce Detention By Total Site Imperviousness: 60.4% Notes: Total Site Effective Imperviousness for WQCV Event: Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 60.4% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: $^{\star\star\star} \, \text{Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed}$ Total Site Effective Imperviousness for Optional User Defined Storm CUHP:

CLH17_IRF Calcs North Pond.xism, IRF

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: CMWJ Galloway & Co. Company: ***Design Storm: 1-Hour Rain Depth WQCV Event 0.60 inches February 9, 2021 ···Minor Storm: 1-Hour Rain Depth 5-Year Event 1.50 inches Project: Falcon Meadows at Bent Grass 100-Year Event 2.52 South WQ Pond ***Major Storm: 1-Hour Rain Depth inches Location: Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency 100-Year Event Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier D Off Site Receiving Pervious Area Soil Type Sandy Loam Sandy Loam Sandy Loan Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 35.330 30.680 1.800 Directly Connected Impervious Area (DCIA, acres) 11.900 1.800 2.400 Unconnected Impervious Area (UIA, acres) 4.900 0.000 0.000 Receiving Pervious Area (RPA, acres) 0.000 0.000 0.000 Separate Pervious Area (SPA, acres) 18.530 0.000 28.280 RPA Treatment Type: Conveyance (C) С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) 35.330 Total Calculated Area (ac, check against input) 1.800 30.680 Directly Connected Impervious Area (DCIA, %) 33.7% 100.0% 7.8% Unconnected Impervious Area (UIA, %) 13.9% 0.0% 0.0% Receiving Pervious Area (RPA, %) 0.0% 0.0% 0.0% Separate Pervious Area (SPA, %) 52.4% 0.0% 92.2% A_R (RPA / UIA) 0.000 0.000 I, Check 1 000 1.000 1 000 f / I for WQCV Event: 1.7 1.7 f / I for 5-Year Event 0.5 0.5 0.5 f / I for 100-Year Event: 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP. IRF for WQCV Event: 1.00 1.00 1.00 IRF for 5-Year Event: 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP. Total Site Imperviousness: I_{total} 47.6% 100.0% 7.8% Effective Imperviousness for WQCV Event: 100.0% 7.8% Effective Imperviousness for 5-Year Event: 47.6% 100.0% 7.8% Effective Imperviousness for 100-Year Event: 47.6% 100.0% 7.8% Effective Imperviousness for Optional User Defined Storm CUHP. LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% 0.0% 0.0% N/A This line only for 10-Year Event N/A 100-Year Event CREDIT**: Reduce Detention By: 0.0% 0.0% 0.0% N/A User Defined CUHP CREDIT: Reduce Detention By Total Site Imperviousness: 31.0% Notes: Total Site Effective Imperviousness for WQCV Event: 31.0% Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 31.0% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed Total Site Effective Imperviousness for Optional User Defined Storm CUHP.

CLH17_IRF Calcs South Pond.xism, IRF

Existing Computations

COMPOSITE % IMPERVIOUS CALCULATIONS: EXISTING

Subdivision: Falcon Meadows at Bent Grass
Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass
Project No.: CLH000017

Calculated By: TJE
Checked By: CMD
Date: 6/19/20

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
		Pa	ved/Gravel R	oads	La	wns/Undevelo	oped		Roofs		Res	sidential - 1/8	Acre	Res	idential - 1/4	Acre	Resi	idential - 1/3 A	Acre	Res	idential - 1/2 /	Acre	Re	sidential - 1 A	cre	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted	Weighted %
		/0 IIIp.	Area (ac)	% Imp.	∕o mip.	Alea (ac)	% Imp.	/0 mp.	Alea (ac)	% Imp.	/0 mp.	Area (ac)	% Imp.	∕o mip.	Area (ac)	% Imp.	/0 mp.	Area (ac)	% Imp.	70 mp.	Area (ac)	% Imp.	70 mp.	Area (ac)	% Imp.	Imp.
EX-1	1.19	100	0.00	0.0	2	1.19	2.0	2	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-2	1.56	100	0.00	0.0	2	1.56	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-3	0.62	100	0.00	0.0	2	0.62	2.0	1	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-4	12.49	100	0.00	0.0	2	12.49	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-5	5.15	100	0.00	0.0	2	5.15	2.0	10	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-6	9.53	100	0.00	0.0	2	9.53	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-7	9.16	100	0.00	0.0	2	9.16	2.0	18	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
EX-8	21.30	100	0.00	0.0	2	21.30	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
OS-1	32.28	100	2.15	6.7	2	29.25	1.8	90	0.88	2.5	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	11.0
OS-2	20.08	80	0.90	3.6	2	18.62	1.9	90	0.56	2.5	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
OS-3	10.62	80	0.48	3.6	2	9.84	1.9	19	0.30	0.5	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	6.0
OS-4	4.46	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	2.28	33.2	40	1.46	13.1	30	0.00	0.0	25	0.00	0.0	20	0.72	3.2	49.5
OS-5	0.46	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	0.46	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
OS-6	1.17	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	1.17	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
C-8	0.42	100	0.00	0.0	2	0.42	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
E-1	1.71	100	0.78	45.6	2	0.23	0.3	90	0.00	0.0	65.0	0.00	0.0	40	0.70	16.4	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.3
E-2	0.68	100	0.56	82.4	2	0.12	0.4	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	82.8
E-3	0.78	100	0.69	88.5	2	0.09	0.2	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	88.7
E-4	0.91	100	0.73	80.2	2	0.18	0.4	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.6
E-5	0.89	100	0.79	88.8	2	0.10	0.2	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	89.0
I-1	0.31	100	0.22	71.0	2	0.09	0.6	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	71.6

Lot Type Id	entification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	1/8 Acre
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32 671 43 560	1 Acre

NOTES:

% Impervious values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)

CLH17_EX-PDR-Drainage Calcs.xlsm Page 1 of 1 2/9/2021

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS: EXISTING

Subdivision: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass

Project No.: CLH000017

Calculated By: TJE

Checked By: CMD

Date: 6/19/20

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
		Pav	ed/Gravel R	oads	Lav	wns/Undevel	oped		Roofs	Residential - 1/8 Acre			Resi	dential - 1/4	Acre	Res	idential - 1/3	Acre	Resi	idential - 1/2	Acre	Res	sidential - 1	Acre			
Basin ID	Total Area (ac)	C_5	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C_{100}	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C_5	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	Composite C ₅	Composite C ₁₀₀
EX-1	1.19	0.90	0.96	0.00	0.09	0.36	1.19	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-2	1.56	0.90	0.96	0.00	0.09	0.36	1.56	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-3	0.62	0.90	0.96	0.00	0.09	0.36	0.62	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-4	12.49	0.90	0.96	0.00	0.09	0.36	12.49	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-5	5.15	0.90	0.96	0.00	0.09	0.36	5.15	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-6	9.53	0.90	0.96	0.00	0.09	0.36	9.53	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-7	9.16	0.90	0.96	0.00	0.09	0.36	9.16	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-8	21.30	0.90	0.96	0.00	0.09	0.36	21.30	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
OS-1	32.28	0.90	0.96	2.15	0.09	0.36	29.25	0.73	0.81	0.88	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.16	0.41
OS-2	20.08	0.90	0.96	0.90	0.09	0.36	18.62	0.73	0.81	0.56	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.14	0.40
OS-3	10.62	0.90	0.96	0.48	0.09	0.36	9.84	0.73	0.81	0.30	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.14	0.40
OS-4	4.46	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	2.28	0.30	0.50	1.46	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.72	0.36	0.54
OS-5	0.46	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.46	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.45	0.59
OS-6	1.17	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	1.17	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.45	0.59
C-8	0.42	0.90	0.96	0.00	0.09	0.36	0.42	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
E-1	1.71	0.90	0.96	0.78	0.09	0.36	0.23	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.70	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.55	0.69
E-2	0.68	0.90	0.96	0.56	0.09	0.36	0.12	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.76	0.85
E-3	0.78	0.90	0.96	0.69	0.09	0.36	0.09	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.81	0.89
E-4	0.91	0.90	0.96	0.73	0.09	0.36	0.18	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.74	0.84
E-5 I-1	0.89	0.90	0.96	0.79	0.09	0.36	0.10	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.81	0.89
1-1	0.31	0.90	0.96	0.22	0.09	0.36	0.09	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.66	0.79

Lot Type Ide	entification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	= 1/8 Acre</td
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32,671 - 43,560	1 Acre

C values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)

Coeffficients use HSG A&B soils - Refer to "Appendix A: Exhibits and Figures" for soil map

STANDARD FORM SF-2 TIME OF CONCENTRATION: EXISTING

Subdivision: Falcon Meadows at Bent Grass

Project Name: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Project No.: CLH000017

Calculated By: TJE

Checked By: CMD

Date: 6/19/20

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18

1	2	3	4	3	6	/	δ	9	10	11	12	13	14	15	16	17	18
		SUB-BA	ASIN			INITIA	L/OVER	LAND		TR	AVEL TI	ME			Tc CHECK		
		DAT	'A				(T_i)				$(\mathbf{T}_{\mathbf{t}})$			(UR	FINAL		
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S	T_{i}	L	S	Cv	VEL.	T_t	COMP. T _c	TOTAL	Urbanized T_c	T_c
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT)	(MIN)	(MIN)
EX-1	1.19	A	2.0	0.09	0.36	300	2.7	23.0	690	2.7	15	2.5	4.7	27.7	990.0	15.5	15.5
EX-2	1.56	A	2.0	0.09	0.36	200	2.7	18.8	100	2.7	15	2.5	0.7	19.5	300.0	11.7	11.7
EX-3	0.62	A	2.0	0.09	0.36	100	5.0	10.8	30	2.7	15	2.5	0.2	11.0	130.0	10.7	10.7
EX-4	12.49	A	2.0	0.09	0.36	100	2.7	13.3	1180	2.7	15	2.5	8.0	21.3	1280.0	17.1	17.1
EX-5	5.15	A	2.0	0.09	0.36	100	2.7	13.3	1000	2.7	15	2.5	6.8	20.0		16.1	16.1
EX-6	9.53	A	2.0	0.09	0.36	100	2.7	13.3	1700	2.7	15	2.5	11.5		1800.0	20.0	20.0
EX-7	9.16	A	2.0	0.09	0.36	90	2.7	12.6	1020	2.7	15	2.5	6.9	19.5	1110.0	16.2	16.2
EX-8	21.30	A	2.0	0.09	0.36	100	2.7	13.3	996	2.7	15	2.5	6.7	20.0	1095.5	16.1	16.1
OS-1	32.28	A	11.0	0.16	0.41	100	2.4	12.9	2100	2.2	15	2.2	15.7	28.6	2200.0	22.2	22.2
OS-2	20.08	A	8.0	0.14	0.40	100	2.3	13.3	1400	2.3	15	2.3	10.3	23.6	1500.0	18.3	18.3
OS-3	10.62	A	8.0	0.14	0.40	100	2.0		1500	2.0	15	2.1	11.8	25.7	1600.0	18.9	18.9
OS-4	4.46	A	49.5	0.36	0.54	100	2.0		910	1.2	20	2.2	6.9	17.7	1010.0	15.6	15.6
OS-5	0.46	A	65.0	0.45	0.59	15	2.0		190	1.0	20	2.0	1.6		205.0	11.1	5.2
OS-6	1.17	A	65.0	0.45	0.59	85	0.2	18.7	430	0.9	20	1.9	3.9		515.0	12.9	12.9
C-8	0.42	A	2.0	0.09	0.36	100	2.5	13.6	170	2.5	15	2.4	1.2		270.0	11.5	11.5
E-1	1.71	A	62.3	0.55	0.69	25	2.0	4.0	940	1.0	20	2.0	7.8		965.0	15.4	11.8
E-2	0.68	A	82.8	0.76	0.85	25	2.0		665	1.6	20	2.5	4.4	6.9	690.0	13.8	6.9
E-3	0.78	A	88.7	0.81	0.89	25	2.0		632	1.0	20	2.0	5.3		657.0	13.7	7.4
E-4	0.91	A	80.6	0.74	0.84	25	2.0		913	2.0	20	2.8	5.4			15.2	8.0
E-5	0.89	A	89.0	0.81	0.89	25	2.0		903	2.1	20	2.9	5.2	7.3	928.0	15.2	7.3
I-1	0.31	A	71.6	0.66	0.79	25	2.0	3.2	135	2.0	20	2.8	0.8	4.0	160.0	10.9	5.0

NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$, S in ft/ft

T_t=L/60V (Velocity From Fig. 501)

Velocity V=Cv*S^0.5, S in ft/ft

Tc Check = 10 + L/180

For Urbanized basins a minimum T_c of 5.0 minutes is required.

For non-urbanized basins a minimum T_c of 10.0 minutes is required

CLH17_EX-PDR-Drainage Calcs.xlsm Page 1 of 1 2/9/2021

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN: EXISTING

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Design Storm: 100-Year

 Project Name:
 Falcon Meadows at Bent Grass

 Project No.:
 CLH000017

 Calculated By:
 TJE

 Checked By:
 CMD

 Date:
 6/19/20

				DIRE	CT RUI	NOFF				TOTAL	RUNOF	F	STR	EET		PIPE		TRA	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		WT200	192.00									190.0									From Falcon DBPS by Matrix
	1	OS-4	4.46	0.54	15.6	2.41	5.81	14.0					1.2	14.0				910	2.2	6.9	Flow obtained from Bent Grass Filing No. 2 FDR.
	2	OS-5	0.46	0.59	5.2	0.27	8.56	2.3					1	2.3				190	2.0	1.6	Flow obtained from Bent Grass Filing No. 2 FDR.
	3	OS-6	1.17	0.59	12.9	0.69	6.30	4.3					0.86	4.3				430	1.9	3.9	Flow obtained from Bent Grass Filing No. 2 FDR.
	4	EX-1	1.19	0.36	15.5	0.43	5.83	2.5													
	5	EX-2	1.56	0.36	11.7	0.56	6.54	3.7	15.6	4.36	5.81	25.3									Total flows to DP 5 discharging into existing WQCV Pond.
		EX-3	0.62	0.36	10.7	0.22	6.76	1.5													Existing WQCV Pond.
			12.40	0.24	15.1	4.50	7.50	25.1													
	6	EX-4	12.49	0.36	17.1	4.50	5.58	25.1													
	7	EX-5	5.15	0.36	16.1	1.85	5.73	10.6	17.1	6.35	5.58	35.4									Total flow from DP 6 & EX-5 flowing onto Bent Grass Meadows Drive.
	8	EX-7	9.16	0.36	16.2	3.30	5.72	18.9													Flows from DP 8 go off-site into Bent Grass Meadows Drive.
		224 /	7.10	0.50	10.2	5.50	5.72	10.5													The state of the s
	9	OS-2	20.08	0.40	18.3	8.03	5.41	43.4													Flow obtained from Bent Grass Filing No. 2 FDR.
	10	OS-3	10.62	0.40	18.9	4.25	5.33	22.7													Flow obtained from Bent Grass Filing No. 2 FDR.
		EX-6	9.53	0.36	20.0	3.43	5.19	17.8													
	11								20.0	15.71	5.19	81.5									Total flows entering existing inlet at DP 11. (Basins OS-2, OS-3 & EX-6)
		EX-8	21.30	0.36	16.1	7.67	5.73	43.9													Existing flows from basin discharge into creek.
	12	OS-1	32.28	0.41	22.2	13.23	4.92	65.1													Existing off-site flows into creek via existing swale.
		E-1	1.71	0.69	11.8	1.18	6.51	7.7													
		E-2	0.68	0.85	6.9	0.58	7.89	4.6													
	4X								17.3	4.03	5.55	22.4									DP-4 from Bent Grass Filing No. 2 FDR (
	21								17.3	10.29	5.55	57.1									Combine Basins Ex-4, E-1 & E-2 at Existing Inlet from Bent Grass Filing No. 2 FDR
	15A											37.0									Release Rate from WQCV Pond North in Bent Grass Filing No. FDR
		E-3	0.78	0.89	7.4	0.69	7.70	5.3													
	AA	E 4	0.91	0.84	8.0	0.76	7.50	5.7				297.4									Combine Basins WT200 & E-3 w/Design Points 12 & 15A
		E-4 E-5	0.91	0.84	7.3	0.76	7.50	6.1													
		E-3	0.89	0.89	1.3	0.79	1.13	0.1													

Page 1 of 2 12/17/2020

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN: EXISTING

(RATIONAL METHOD PROCEDURE)

	Project Name: Falcon Meadows at Bent Grass
Subdivision: Falcon Meadows at Bent Grass	Project No.: CLH000017
Location: CO, Colorado Springs	Calculated By: TJE
Design Storm: 100-Year	Checked By: CMD
	Date: 6/19/20

				DIRE	ECT RUI	OFF	TOTAL RUNOFF				STREET			PIPE		TRAV	EL T	IME			
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		I-1	0.31	0.79	5.0	0.24	8.68	2.1													
	26								20.0	17.50	3.09	54.1									Combine Basins E-4, E-5 & I-1 w/DP 11 at Existing Inlet from Bent Grass Filing No. 2 FDR
	20B											64.9									Release Rate from WQCV Pond South in Bent Grass Filing No. FDR
		C-8	0.42	0.36	11.5	0.15	6.58	1.0													
	СС	•										417.4									Flows exiting site - Combined flows from Basin C-8 w/Design Points AA, 26 & 20B

CLH17_EX-PDR-Drainage Cales.xism

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN: EXISTING

(RATIONAL METHOD PROCEDURE)

Subdivision:
Subdivision:
Falcon Meadows at Bent GrassProject Non:
CLH000017CLH000017Location:
CO, Colorado SpringsCalculated By:
5-YearTJEDesign Storn:
5-YearChecked By:
6/19/20CMDDate:Object Non:
CLH000017CH000017Calculated By:
(MD)CMDDate:Object Non:
6/19/20

-						1								0/1//1							
		DIRECT RUNOFF						TOTAL RUNOFF					REET								
STREET	Design Point	3asin ID	Area (Ac)	Runoff Coeff.	ſc (min))*A (Ac)	(in/hr)	Q (cfs)	Tc (min)	∑*A (Ac)	(in/hr)	Q (cfs)	Slope (%)	street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	ength (ft)	Velocity (fps)	ft (min)	REMARKS
		RWT202	1574.40	, m					46.6	120.88	1.82	220.0	, , , , , , , , , , , , , , , , , , ,	3,		J,					From Falcon DBPS by Matrix
		RWT204	38.40						11.37	1.78	3.94	7.0									From Falcon DBPS by Matrix
		WT200	192.00						37.8	24.41	2.13	52.0									From Falcon DBPS by Matrix
	1	OS-4	4.46	0.36	15.6	1.61	3.46	5.6					1.2	5.6				910	2.2	6.9	Flows from Basin B-1 of Bent Grass Filing No. 2 FDR.
	2	OS-5	0.46	0.45	5.2	0.21	5.10	1.1					1	1.1				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR
	3	OS-6	1.17	0.45	12.9	0.53	3.75	2.0					0.86	2.0				430	1.9	3.9	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR.
	4	EX-1	1.19	0.09	15.5	0.11	3.47	0.4													
	5	EX-2	1.56	0.09	11.7	0.14	3.90	0.5	15.6	2.60	3.46	9.0									Total flows to DP 5 discharging into existing WQCV Pond.
		EX-3	0.62	0.09	10.7	0.06	4.02	0.2													Existing WQCV Pond.
P P																					
p p	6	EX-4	12.49	0.09	17.1	1.12	3.32	3.7													
p	7	EX-5	5.15	0.09	16.1	0.46	3.41	1.6	17.1	1.58	3.32	5.2									Total flow from DP 6 & EX-5 flowing onto Bent Grass Meadows Drive.
	8	EX-7	9.16	0.09	16.2	0.82	3.41	2.8													Flows from DP 8 go off-site into Bent Grass Meadows Drive.
	9	OS-2	20.08	0.14	18.3	2.81	3.22	9.0													Flow obtained from Bent Grass Filing No. 2 FDR.
	10	OS-3	10.62	0.14	18.9	1.49	3.18	4.7													Flow obtained from Bent Grass Filing No. 2 FDR.
	11	EX-6	9.53	0.09	20.0	0.86	3.09	2.7	20.0	5.16	3.09	15.9									Total flows entering existing inlet at DP 11. (Basins OS-2, OS-3 & EX-6)
		EX-8	21.30	0.09	16.1	1.92	3.42	6.6													Existing flows from basin discharge into creek.
	12	OS-1	32.28	0.16	22.2	5.16	2.93	15.1													Existing off-site flows into creek via existing swale.
		E-1	1.71	0.55	11.8	0.94	3.88	3.6													Existing Basin from Filing No. 2(East side of BGMD)
		E-2	0.68	0.76	6.9	0.52	4.70	2.4													Existing Basin from Filing No. 2(West side of BGMD)
	4X								17.3	2.60	3.31	8.6									DP-4 from Bent Grass Filing No. 2 FDR (
	21								17.3	5.18	3.31	17.1									Combine Basins Ex-4, E-1 & E-2 at Existing Inlet from Bent Grass Filing No. 2 FD
	15A		0.50	0.01		0.52	1.50	1	5.0	2.42	5.17	12.5									Release Rate from Ex WQCV Pond North in Bent Grass Filing No.2 FDR
		E-3	0.78	0.81	7.4	0.63	4.59	2.9													
	AA	F (0.01	0.7.	6.0	0.55	4.15	2.0	46.6	155.28	1.82	282.6									Combine Basins WT200 & E-3 w/Design Points 12 & 15A
		E-4	0.91	0.74	8.0	0.67	4.46	3.0													

CLH17_EX-PDR-Drainage Cales.xlsm

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN: EXISTING

(RATIONAL METHOD PROCEDURE)

	Project Name: Falcon Meadows at Bent Grass
Subdivision: Falcon Meadows at Bent Grass	Project No.: CLH000017
Location: CO, Colorado Springs	Calculated By: TJE
Design Storm: 5-Year	Checked By: CMD
	Date: 6/19/20

				DIRE	ECT RUI	NOFF			-	TOTAL:	RUNOF	F	STR	EET		PIPE		TRA	VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		E-5	0.89	0.81	7.3	0.72	4.60	3.3													
		I-1	0.31	0.66	5.0	0.20	5.17	1.0													
	26								20.0	6.75	3.09	20.9									Combine Basins E-4, E-5 & I-1 w/DP 11 at Existing Inlet from Bent Grass Filing No. 2 FDR
	20B								5.0	4.10	5.17	21.2									Release Rate from Ex WQCV Pond South in Bent Grass Filing No. FDR
		C-8	0.42	0.09	11.5	0.04	3.92	0.2													
	СС								46.6	166.17	1.82	302.4									Flows exiting site - Combined flows from Basin C-8 w/Design Points AA, 26 & 20B

CLH17_EX-PDR-Drainage Cales.xlsm

Proposed Computations

COMPOSITE % IMPERVIOUS CALCULATIONS: PROPOSED

Subdivision: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass

Project No.: CLH000017

Calculated By: TJE
Checked By: CMD

Date: 6/19/20

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
		Pav	ved/Gravel Ro	oads	La	wns/Undevelo	ped		Roofs			idential - 1/8	Acre	Res	idential - 1/4	Acre	Res	idential - 1/3			sidential - 1/2	Acre		sidential - 1 A	cre	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
A-1	2.16	100	0.50	23.1	2	0.00	0.0	90	0.00	0.0	65.0	0.93	28.0	40	0.00	0.0	30	0.73	10.1	25	0.00	0.0	20	0.75	6.9	68.1
A-2	0.86	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	0.86	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
A-3	0.92	100	0.64	69.6	2	0.28	0.6	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	70.2
A-4	0.82	100	0.00	0.0	2	0.82	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
B-1	4.32	100	0.00	0.0	2	4.32	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
B-2	4.16	100	0.00	0.0	2	4.41	2.1	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.1
C-1	9.07	100	2.14	23.6	2	0.33	0.1	90	0.00	0.0	65.0	4.56	32.7	40	1.70	7.5	30	0.34	1.1	25	0.00	0.0	20	0.00	0.0	65.0
C-2	1.11	100	0.37	33.3	2	0.19	0.3	90	0.00	0.0	65.0	0.30	17.6	40	0.00	0.0	30	0.25	6.8	25	0.00	0.0	20	0.00	0.0	58.0
C-3	1.52	100	0.94	61.8	2	0.00	0.0	90	0.00	0.0	65.0	0.58	24.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	86.6
C-4	4.70	100	0.36	7.7	2	1.85	0.8	90	0.00	0.0	65.0	2.49	34.4	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	42.9
C-5	0.51	100	0.00	0.0	2	0.51	2.0	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
C-6	1.37	100	0.00	0.0	2	0.30	0.4	90	0.00	0.0	65.0	1.07	50.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	51.2
D-1	8.13	100	1.52	18.7	2	0.69	0.2	90	0.00	0.0	65.0	1.85	14.8	40	1.42	7.0	30	1.53	5.6	25	1.12	3.4	20	0.00	0.0	49.7
D-2	6.72	100	2.31	34.4	2	0.76	0.2	90	0.00	0.0	65.0	3.65	35.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	69.9
D-3	2.93	100	0.00	0.0	2	0.28	0.2	90	0.00	0.0	65.0	1.26	28.0	40	0.17	2.3	30	0.12	1.2	25	0.00	0.0	20	0.00	0.0	31.7
D-4	4.38	100	1.21	27.6	2	0.63	0.3	90	0.00	0.0	65.0	2.53	37.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.4
D-5	1.08	100	0.22	20.4	2	0.11	0.2	90	0.00	0.0	65.0	0.75	45.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.7
D-6	4.01	100	0.91	22.7	2	0.09	0.0	90	0.00	0.0	65.0	3.01	48.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	71.5
D-7	6.39	100	0.00	0.0	2	5.59	1.7	90	0.00	0.0	65.0	0.80	8.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	9.8
D-8	1.69	100	0.00	0.0	2	1.13	1.3	90	0.00	0.0	65.0	0.56	21.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	22.8
E-1	1.71	100	0.78	45.6	2	0.23	0.3	90	0.00	0.0	65.0	0.00	0.0	40	0.70	16.4	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.3
E-2	0.68	100	0.56	82.4	2	0.12	0.4	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	82.8
E-3	0.78	100	0.69	88.5	2	0.09	0.2	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	88.7
E-4	0.91	100	0.73	80.2	2	0.18	0.4	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.6
E-5	0.89	100	0.79	88.8	2	0.10	0.2	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	89.0
I-1	0.31	100	0.22	71.0	2	0.09	0.6	90	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	71.6
OS-1	32.28	100	2.15	6.7	2	29.25	1.8	90	0.88	2.5	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	11.0
OS-2	20.07	80	0.90	3.6	2	18.62	1.9	90	0.56	2.5	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
OS-3	10.61	80	0.48	3.6	2	9.84	1.9	90	0.30	2.5	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	8.0
OS-4	4.46	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	2.28	33.2	40	1.46	13.1	30	0.00	0.0	25	0.00	0.0	20	0.72	3.2	49.5
OS-5	0.46	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	0.46	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0
OS-6	1.17	100	0.00	0.0	2	0.00	0.0	90	0.00	0.0	65.0	1.17	65.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.0

Lot Type Id	entification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	1/8 Acre
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32,671 - 43,560	1 Acre

NOTES:

% Impervious values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)

CLH17_PR-PDR-Drainage Calcs.xlsm Page 1 of 1 2/9/2021

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS: PROPOSED

Subdivision: Falcon Meadows at Bent Grass Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass

Project No.: CLH000017

Calculated By: TJE

Checked By: CMD

Date: 6/19/20

		Pa	ved/Gravel R	oads	La	wns/Undeve	loned		Roofs		Res	dential - 1/8	8 Acre	Resi	idential - 1/4	Acre	Res	sidential - 1/3	Acre	Resi	idential - 1/2	Acre	Re	sidential - 1 A	Acre		
Basin ID	Total Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	C ₅	C ₁₀₀	Area (ac)	Composite C ₅	Composite C ₁₀₀
A-1	2.16	0.90	0.96	0.50	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.93	0.30	0.50	0.00	0.25	0.47	0.73	0.22	0.46	0.00	0.20	0.44	0.75	0.56	0.79
A-2	0.86	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.86	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.45	0.59
A-3	0.92	0.90	0.96	0.64	0.09	0.36	0.28	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.65	0.78
A-4	0.82	0.90	0.96	0.00	0.09	0.36	0.82	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
B-1	4.32	0.90	0.96	0.00	0.09	0.36	4.32	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
B-2	4.16	0.90	0.96	0.00	0.09	0.36	4.41	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.10	0.38
C-1	9.07	0.90	0.96	2.14	0.09	0.36	0.33	0.73	0.81	0.00	0.45	0.59	4.56	0.30	0.50	1.70	0.25	0.47	0.34	0.22	0.46	0.00	0.20	0.44	0.00	0.51	0.65
C-2	1.11	0.90	0.96	0.37	0.09	0.36	0.19	0.73	0.81	0.00	0.45	0.59	0.30	0.30	0.50	0.00	0.25	0.47	0.25	0.22	0.46	0.00	0.20	0.44	0.00	0.49	0.65
C-3	1.52	0.90	0.96	0.94	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.58	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.73	0.82
C-4	4.70	0.90	0.96	0.36	0.09	0.36	1.85	0.73	0.81	0.00	0.45	0.59	2.49	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.34	0.53
C-5	0.51	0.90	0.96	0.00	0.09	0.36	0.51	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
C-6	1.37	0.90	0.96	0.00	0.09	0.36	0.30	0.73	0.81	0.00	0.45	0.59	1.07	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.37	0.54
D-1	8.13	0.90	0.96	1.52	0.09	0.36	0.69	0.73	0.81	0.00	0.45	0.59	1.85	0.30	0.50	1.42	0.25	0.47	1.53	0.22	0.46	1.12	0.20	0.44	0.00	0.41	0.58
D-2	6.72	0.90	0.96	2.31	0.09	0.36	0.76	0.73	0.81	0.00	0.45	0.59	3.65	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.56	0.69
D-3	2.93	0.90	0.96	0.00	0.09	0.36	0.28	0.73	0.81	0.00	0.45	0.59	1.26	0.30	0.50	0.17	0.25	0.47	0.12	0.22	0.46	0.00	0.20	0.44	0.00	0.23	0.34
D-4	4.38	0.90	0.96	1.21	0.09	0.36	0.63	0.73	0.81	0.00	0.45	0.59	2.53	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.52	0.66
D-5	1.08	0.90	0.96	0.22	0.09	0.36	0.11	0.73	0.81	0.00	0.45	0.59	0.75	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.51	0.64
D-6	4.01	0.90	0.96	0.91	0.09	0.36	0.09	0.73	0.81	0.00	0.45	0.59	3.01	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.54	0.67
D-7	6.39	0.90	0.96	0.00	0.09	0.36	5.59	0.73	0.81	0.00	0.45	0.59	0.80	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.14	0.39
D-8	1.69	0.90	0.96	0.00	0.09	0.36	1.13	0.73	0.81	0.00	0.45	0.59	0.56	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.21	0.44
E-1	1.71	0.90	0.96	0.78	0.09	0.36	0.23	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.70	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.55	0.69
E-2	0.68	0.90	0.96	0.56	0.09	0.36	0.12	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.76	0.85
E-3	0.78	0.90	0.96	0.69	0.09	0.36	0.09	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.81	0.89
E-4	0.91	0.90	0.96	0.73	0.09	0.36	0.18	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.74	0.84
E-5	0.89	0.90	0.96	0.79	0.09	0.36	0.10	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.81	0.89
I-1	0.31	0.90	0.96	0.22	0.09	0.36	0.09	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.66	0.79
OS-1	32.28	0.90	0.96	2.15	0.09	0.36	29.25	0.73	0.81	0.88	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.16	0.41
OS-2	20.07	0.90	0.96	0.90	0.09	0.36	18.62	0.73	0.81	0.56	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.14	0.40
OS-3	10.61	0.90	0.96	0.48	0.09	0.36	9.84	0.73	0.81	0.30	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.14	0.40
OS-4	4.46	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	2.28	0.30	0.50	1.46	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.72	0.36	0.54
OS-5	0.46	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.46	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.45	0.59
OS-6	1.17	0.90	0.96	0.00	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	1.17	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.45	0.59

Lot Type Ide	ntification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	= 1/8 Acre</td
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32 671 - 43 560	1 Acre

C values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)
Coeffficients use HSG A&B soils - Refer to "Appendix A: Exhibits and Figures" for soil map

STANDARD FORM SF-2: PROPOSED TIME OF CONCENTRATION

Subdivision: Falcon Meadows at Bent Grass	Project Name:	Falcon Meadows at Bent Grass

Checked By: CMD

Date: 6/19/20

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(MIN) 8 10.3 6 5.0
DATA Composite Total Composite Total Composite Compo	T _c T _c (MIN) 8 10.3 6 5.0
BASIN D.A. Hydrologic Impervious C.5 C. U.6 (FT) (%) (MIN) (FT) (%) (WIN) (FT) (%) (FT) (%) (MIN) (FT) (WIN) (FT) (MIN) (MIN) (MIN) (MIN) (LENGTH(FT) (MIN) (MIN) (LENGTH(FT) (MIN) (MIN	T _c T _c (MIN) 8 10.3 6 5.0
ID (AC) Soils Group (%) (%) (MIN) (MIN) (FT) (%) (MIN) (FFS) (MIN) (MIN) LENGTH(FT) (MIN) A-1 2.16 A 68.1 0.56 0.79 100 4.0 6.2 765 2.5 20 3.2 4.0 10.3 865.0 A-2 0.86 A 65.0 0.45 0.59 5 2.0 2.1 110 7.0 20 5.3 0.3 2.5 115.0 A-3 0.92 A 70.2 0.65 0.78 60 2.0 5.1 735 2.5 20 3.2 3.9 8.9 795.0 A-4 0.82 A 2.0 0.09 0.36 5 2.0 3.3 105 5.7 20 4.8 0.4 3.6 110.0 B-1 4.32 A 2.0 0.09 0.36 90 6.4 9.5 2000 1.7	(MIN) 8 10.3 6 5.0
A-1 2.16 A 68.1 0.56 0.79 100 4.0 6.2 765 2.5 20 3.2 4.0 10.3 865.0 A-2 0.86 A 65.0 0.45 0.59 5 2.0 2.1 110 7.0 20 5.3 0.3 2.5 115.0 A-3 0.92 A 70.2 0.65 0.78 60 2.0 5.1 735 2.5 20 3.2 3.9 8.9 795.0 A-4 0.82 A 2.0 0.09 0.36 5 2.0 3.3 105 5.7 20 4.8 0.4 3.6 110.0 B-1 4.32 A 2.0 0.09 0.36 90 6.4 9.5 2000 1.7 15 2.0 17.0 26.5 2090.0 B-2 1.17 A 2.1 0.10 0.38 160 11.0 10.4 920 1.6 15	8 10.3 6 5.0
A-2 0.86 A 65.0 0.45 0.59 5 2.0 2.1 110 7.0 20 5.3 0.3 2.5 115.0 A-3 0.92 A 70.2 0.65 0.78 60 2.0 5.1 735 2.5 20 3.2 3.9 8.9 795.0 A-4 0.82 A 2.0 0.09 0.36 5 2.0 3.3 105 5.7 20 4.8 0.4 3.6 110.0 B-1 4.32 A 2.0 0.09 0.36 90 6.4 9.5 2000 1.7 15 2.0 17.0 26.5 2090.0 B-2 1.17 A 2.1 0.10 0.38 160 11.0 10.4 920 1.6 15 1.9 8.1 18.5 1080.0 C-1 9.07 A 65.0 0.51 0.65 75 2.0 7.4 1160 2.3 2	6 5.0
A-3 0.92 A 70.2 0.65 0.78 60 2.0 5.1 735 2.5 20 3.2 3.9 8.9 795.0 A-4 0.82 A 2.0 0.09 0.36 5 2.0 3.3 105 5.7 20 4.8 0.4 3.6 110.0 B-1 4.32 A 2.0 0.09 0.36 90 6.4 9.5 2000 1.7 15 2.0 17.0 26.5 2090.0 B-2 1.17 A 2.1 0.10 0.38 160 11.0 10.4 920 1.6 15 1.9 8.1 18.5 1080.0 C-1 9.07 A 65.0 0.51 0.65 75 2.0 7.4 1160 2.3 20 3.0 6.4 13.9 1235.0 C-2 1.11 A 58.0 0.49 0.65 10 2.0 2.8 380 4.0 <t< td=""><td></td></t<>	
A-4 0.82 A 2.0 0.09 0.36 5 2.0 3.3 105 5.7 20 4.8 0.4 3.6 110.0 B-1 4.32 A 2.0 0.09 0.36 90 6.4 9.5 2000 1.7 15 2.0 17.0 26.5 2090.0 B-2 1.17 A 2.1 0.10 0.38 160 11.0 10.4 920 1.6 15 1.9 8.1 18.5 1080.0 C-1 9.07 A 65.0 0.51 0.65 75 2.0 7.4 1160 2.3 20 3.0 6.4 13.9 1235.0 C-2 1.11 A 58.0 0.49 0.65 10 2.0 2.8 380 4.0 20 4.0 1.6 4.4 390.0 C-3 1.52 A 86.6 0.73 0.82 10 2.0 1.7 945 2.5 <t< td=""><td>1 0.0</td></t<>	1 0.0
B-1 4.32 A 2.0 0.09 0.36 90 6.4 9.5 2000 1.7 15 2.0 17.0 26.5 2090.0 B-2 1.17 A 2.1 0.10 0.38 160 11.0 10.4 920 1.6 15 1.9 8.1 18.5 1080.0 C-1 9.07 A 65.0 0.51 0.65 75 2.0 7.4 1160 2.3 20 3.0 6.4 13.9 1235.0 C-2 1.11 A 58.0 0.49 0.65 10 2.0 2.8 380 4.0 20 4.0 1.6 4.4 390.0 C-3 1.52 A 86.6 0.73 0.82 10 2.0 1.7 945 2.5 20 3.2 5.0 6.7 955.0 C-4 4.70 A 42.9 0.34 0.53 5 2.0 2.5 575 2.5 <	4 8.9
B-2 1.17 A 2.1 0.10 0.38 160 11.0 10.4 920 1.6 15 1.9 8.1 18.5 1080.0 C-1 9.07 A 65.0 0.51 0.65 75 2.0 7.4 1160 2.3 20 3.0 6.4 13.9 1235.0 C-2 1.11 A 58.0 0.49 0.65 10 2.0 2.8 380 4.0 20 4.0 1.6 4.4 390.0 C-3 1.52 A 86.6 0.73 0.82 10 2.0 1.7 945 2.5 20 3.2 5.0 6.7 955.0 C-4 4.70 A 42.9 0.34 0.53 5 2.0 2.5 575 2.5 20 3.2 3.0 5.5 580.0 C-5 0.51 A 2.0 0.09 0.36 5 2.0 3.3 1.0 15 1.5	6 5.0
C-1 9.07 A 65.0 0.51 0.65 75 2.0 7.4 1160 2.3 20 3.0 6.4 13.9 1235.0 C-2 1.11 A 58.0 0.49 0.65 10 2.0 2.8 380 4.0 20 4.0 1.6 4.4 390.0 C-3 1.52 A 86.6 0.73 0.82 10 2.0 1.7 945 2.5 20 3.2 5.0 6.7 955.0 C-4 4.70 A 42.9 0.34 0.53 5 2.0 2.5 575 2.5 20 3.2 3.0 5.5 580.0 C-5 0.51 A 2.0 0.09 0.36 5 2.0 3.3 1.0 15 1.5 0.0 3.3 5.0 C-6 1.37 A 51.2 0.37 0.54 100 6.8 7.1 500 3.0 15 2.6	6 21.6
C-2 1.11 A 58.0 0.49 0.65 10 2.0 2.8 380 4.0 20 4.0 1.6 4.4 390.0 C-3 1.52 A 86.6 0.73 0.82 10 2.0 1.7 945 2.5 20 3.2 5.0 6.7 955.0 C-4 4.70 A 42.9 0.34 0.53 5 2.0 2.5 575 2.5 20 3.2 3.0 5.5 580.0 C-5 0.51 A 2.0 0.09 0.36 5 2.0 3.3 1.0 15 1.5 0.0 3.3 5.0 C-6 1.37 A 51.2 0.37 0.54 100 6.8 7.1 500 3.0 15 2.6 3.2 10.3 600.0	0 16.0
C-3 1.52 A 86.6 0.73 0.82 10 2.0 1.7 945 2.5 20 3.2 5.0 6.7 955.0 C-4 4.70 A 42.9 0.34 0.53 5 2.0 2.5 575 2.5 20 3.2 3.0 5.5 580.0 C-5 0.51 A 2.0 0.09 0.36 5 2.0 3.3 1.0 15 1.5 0.0 3.3 5.0 C-6 1.37 A 51.2 0.37 0.54 100 6.8 7.1 500 3.0 15 2.6 3.2 10.3 600.0	9 13.9
C-4 4.70 A 42.9 0.34 0.53 5 2.0 2.5 575 2.5 20 3.2 3.0 5.5 580.0 C-5 0.51 A 2.0 0.09 0.36 5 2.0 3.3 1.0 15 1.5 0.0 3.3 5.0 C-6 1.37 A 51.2 0.37 0.54 100 6.8 7.1 500 3.0 15 2.6 3.2 10.3 600.0	2 5.0
C-5 0.51 A 2.0 0.09 0.36 5 2.0 3.3 1.0 15 1.5 0.0 3.3 5.0 C-6 1.37 A 51.2 0.37 0.54 100 6.8 7.1 500 3.0 15 2.6 3.2 10.3 600.0	3 6.7
C-6 1.37 A 51.2 0.37 0.54 100 6.8 7.1 500 3.0 15 2.6 3.2 10.3 600.0	2 5.5
	0 5.0
D4 912 A 40.7 0.41 0.59 100 2.6 0.2 1000 1.2 20 2.2 12.0 22.1 2000.0	3 10.3
D-1 8.13 A 49.7 0.41 0.58 100 2.6 9.2 1900 1.3 20 2.5 13.9 23.1 2000.0	1 21.1
D-2 6.72 A 69.9 0.56 0.69 10 2.0 2.5 1355 1.3 20 2.3 9.9 12.4 1365.0	6 12.4
D-3 2.93 A 31.7 0.23 0.34 25 8.0 4.0 1960 1.0 15 1.5 21.8 25.8 1985.0	0 21.0
D-4 4.38 A 65.4 0.52 0.66 100 2.3 8.0 980 1.0 20 2.0 8.2 16.2 1080.0	0 16.0
D-5 1.08 A 65.7 0.51 0.64 100 2.0 8.6 300 1.1 20 2.1 2.4 11.0 400.0	2 11.0
D-6 4.01 A 71.5 0.54 0.67 45 2.0 5.5 835 1.0 20 2.0 7.0 12.4 880.0	9 12.4
D-7 6.39 A 9.8 0.14 0.39 200 7.5 12.7 665 1.0 15 1.5 7.4 20.1 865.0	8 14.8
D-8 1.69 A 22.8 0.21 0.44 125 3.7 11.8 600 1.0 15 1.5 6.7 18.4 725.0	0 14.0
E-1 1.71 A 62.3 0.55 0.69 25 2.0 4.0 940 1.0 20 2.0 7.8 11.8 965.0	4 11.8
E-2 0.68 A 82.8 0.76 0.85 25 2.0 2.5 665 1.6 20 2.5 4.4 6.9 690.0	8 6.9
E-3 0.78 A 88.7 0.81 0.89 25 2.0 2.1 632 1.0 20 2.0 5.3 7.4 657.0	7 7.4
E-4 0.91 A 80.6 0.74 0.84 25 2.0 2.6 913 2.0 20 2.8 5.4 8.0 938.0	2 8.0
E-5 0.89 A 89.0 0.81 0.89 25 2.0 2.1 903 2.1 20 2.9 5.2 7.3 928.0	2 7.3
I-1 0.31 A 71.6 0.66 0.79 25 2.0 3.2 135 2.0 20 2.8 0.8 4.0 160.0	9 5.0
OS-1 32.28 A 11.0 0.16 0.41 100 2.4 12.9 2100 2.2 15 2.2 15.7 28.6 2200.0	2 22.2
OS-2 20.07 A 8.0 0.14 0.40 100 2.3 13.3 1400 2.3 15 2.3 10.3 23.6 1500.0	3 18.3
OS-3 10.61 A 8.0 0.14 0.40 100 2.0 14.0 1500 2.0 15 2.1 11.8 25.7 1600.0	9 18.9
OS-4 4.46 A 49.5 0.36 0.54 100 2.0 10.8 910 1.2 20 2.2 6.9 17.7 1010.0	6 15.6
OS-5 0.46 A 65.0 0.45 0.59 15 2.0 3.7 190 1.0 20 2.0 1.6 5.2 205.0	
OS-6 1.17 A 65.0 0.45 0.59 85 0.2 18.7 430 0.9 20 1.9 3.8 22.5 515.0	1 5.2 9 12.9

NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$, S in ft/ft

 T_t =L/60V (Velocity From Fig. 501)

Velocity V=Cv*S^0.5, S in ft/ft

 $T_c Check = 10 + L/180$

For Urbanized basins a minimum T_c of 5.0 minutes is required.

For non-urbanized basins a minimum T_c of 10.0 minutes is required

CLH17_PR-PDR-Drainage Calcs.xlsm Page 1 of 1 2/9/2021

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Design Storm: 100-Year

 Project Name:
 Falcon Meadows at Bent Grass

 Project No.:
 CLH000017

 Calculated By:
 TJE

 Checked By:
 CMD

 Date:
 6/19/20

				DIRE	CT RUN	OFF			,	TOTAL 1	RUNOF	F	STR	EET		PIPE	E	TRAV	EL T	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		RWT202	1574.40						46.6	327.87	3.05	1000.0									From Falcon DBPS by Matrix
		RWT204	38.40						11.4	6.52	6.60	43.0									From Falcon DBPS by Matrix
		WT200	192.00						37.8	53.07	3.58	190.0									From Falcon DBPS by Matrix
		OS-1	32.28	0.41	22.2	13.23	4.92	65.1													Flows obtained from Bent Grass Filing No. 2 FDR. Q=65.1 CFS
		OS-4	4.46	0.54	15.6	2.41	5.81	14.0					1.2	14.0				910	2.2	6.9	Flows from Basin B-1 of Bent Grass Filing No. 2 FDR.
		OS-5	0.46	0.59	5.2	0.27	8.56	2.3					1	2.3				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR
		OS-6	1.17	0.59	12.9	0.69	6.30	4.3					0.9	4.3				430	1.9	3.8	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR.
		A-1	2.16	0.79	10.3	1.71	6.87	11.7					2.5	11.7				765	3.2	4.0	
		A-4	0.82	0.36	5.0	0.30	8.68	2.6													Existing North WQ Pond Bent Grass Filing No. 2
		A-3	0.92	0.78	8.9	0.72	7.21	5.2					2.5	5.2				735	3.2	3.9	Flow into proposed inlet.
		A-2	0.86	0.59	5.0	0.51	8.68	4.4													Releases directly to Channel
		C-4	4.70	0.53	5.5	2.49	8.44	21.0					2.5	21.0				575	3.2	3.0	Flow into Ex inlet in BGMD at DP 8
		E-1	1.71	0.69	11.8	1.18	6.51	7.7	11.8	1.18	6.51	7.7									Ex Basin from Filing No. 2(East side of BGMD)
		E-2	0.68	0.85	6.9	0.58	7.89	4.6													Ex Basin from Filing No. 2(West side of BGMD)
		B-1	4.32	0.36	21.6	1.56	4.99	7.8													
		C-6	1.37	0.54	10.3	0.74	6.87	5.1													
		C-2	1.11	0.65	5.0	0.72	8.68	6.2					4	6.25				380	4.0	1.583	Flow into proposed inlet.
		C-1	9.07	0.65	13.9	5.90	6.11	36.0					2.25	36.05				1160	3.0	6.4	Flow into proposed inlet.
		C-3	1.52	0.82	6.7	1.25	7.95	9.9					2.5	9.9				945	3.2	5.0	
		C-5	0.51	0.36	5.0	0.18	8.68	1.6													North Pond
		OS-2	20.07	0.40	18.3	8.03	5.41	43.4													Overland flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
		OS-3	10.61	0.40	18.9	4.24	5.33	24.3													Offsite flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
		D-3	2.93	0.34	21.0	1.00	5.06	5.1													Flows conveyed via existing ditch into proposed area inlet.
		D-2	6.72	0.69	12.4	4.64	6.39	29.6					1.3	29.65				1355	2.3	9.9	Flow into proposed inlet. Piped to DP 14.
		D-1	8.13	0.58	21.1	4.72	5.05	23.8					1.3	23.8				1900	2.3	13.9	Combined flows from D-1 into proposed inlet.
		D-4	4.38	0.66	16.0	2.89	5.75	16.6					1	16.6				980	2.0	8.2	Flow into proposed inlet.
		D-5	1.08	0.64	11.0	0.69	6.70	4.6					1.1	4.6				300	2.1	2.4	
		D-6	4.01	0.67	12.4	2.69	6.39	17.2					1	17.2				835	2.0	7.0	
		E-4	0.91	0.84	8.0	0.76	7.50	5.7					2	5.7				913	2.8	5.4	Flow into Ex inlet.
		E-5	0.89	0.89	7.3	0.79	7.73	6.1					2.1	6.1				903	2.9	5.2	Flow into Ex inlet.

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STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision:Falcon Meadows at Bent GrassFalcon Meadows at Bent GrassLocation:CO, Colorado SpringsCalculated By:TJEDesign Storn:100-YearChecked By:CMDDate:6/19/20

				DIRE	CT RUN	OFF				TOTAL I	RUNOF	F	STR	EET		PIPE		TRAV	EL TI	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		I-1	0.31	0.79	5.0	0.24	8.68	2.1					2	2.1				135	2.8	0.8	Flow into Ex inlet.
		D-7	6.39	0.39	14.8	2.49	5.94	14.8													
		D-8	1.69	0.44	14.0	0.74	6.08	4.5													Flow in Swale C (Basin D-8) into proposed south pond
		E-3	0.78	0.89	7.4	0.69	7.70	5.3					1	5.3				632	2.0	5.3	Flow into Ex Inlet in BGMD (South Side)
		B-2	1.17	0.38	16.0	0.44	5.75	2.5													

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STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Falcon Meadows at Bent Grass Location: CO, Colorado Springs Design Storm: 5-Year

Project Name: Falcon Meadows at Bent Grass
Project No.: CLH000017

				DIRE	CT RUN	OFF				TOTAL 1	RUNOF	F	STF	REET		PIPE		TRAV	EL T	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		RWT202	1574.40						46.6	120.88	1.82	220.0									From Falcon DBPS by Matrix
		RWT204	38.40						11.37	1.78	3.94	7.0									From Falcon DBPS by Matrix
		WT200	192.00						37.8	24.41	2.13	52.0									From Falcon DBPS by Matrix
		OS-1	32.28	0.16	22.2	5.16	2.93	15.1													Flows obtained from Bent Grass Filing No. 2 FDR. Q=65.1 CFS
		OS-4	4.46	0.36	15.6	1.61	3.46	5.6					1.2	5.6				910	2.2	6.9	Flows from Basin B-1 of Bent Grass Filing No. 2 FDR.
		OS-5	0.46	0.45	5.2	0.21	5.10	1.1					1	1.1				190	2.0	1.6	Flows from Basin B-2 of Bent Grass Filing No. 2 FDR
		OS-6	1.17	0.45	12.9	0.53	3.75	2.0					0.9	2.0				430	1.9	3.8	Flows from Basin B-3 of Bent Grass Filing No. 2 FDR.
		A-1	2.16	0.56	10.3	1.21	4.09	4.9					2.5	4.9				765	3.2	4.0	
		A-4	0.82	0.09	5.0	0.07	5.17	0.4					5.7	0.4				105	4.8	0.4	Existing North WQ Pond Bent Grass Filing No. 2
		A-3	0.92	0.65	8.9	0.60	4.30	2.6					2.5	2.6				735	3.2	3.9	Flow into proposed inlet.
		A-2	0.86	0.45	5.0	0.39	5.17	2.0					7.0	2.0				110	5.3	0.3	Releases directly to Channel
		C-4	4.70	0.34	5.5	1.60	5.03	8.0					2.5	8.0				575	3.2	3.0	Flow into Ex inlet in BGMD at DP 8
		E-1	1.71	0.55	11.8	0.94	3.88	3.6													Ex Basin from Filing No. 2(East side of BGMD)
		E-2	0.68	0.76	6.9	0.52	4.70	2.4													Ex Basin from Filing No. 2(West side of BGMD)
		B-1	4.32	0.09	21.6	0.39	2.97	1.2													
		C-6	1.37	0.37	10.3	0.51	4.09	2.1													
		C-2	1.11	0.49	5.0	0.54	5.17	2.8					4	2.792				380	4.0	1.6	Flow into proposed inlet.
		C-1	9.07	0.51	13.9	4.63	3.64	16.9					2.25	16.85				1160	3.0	6.4	Flow into proposed inlet.
		C-3	1.52	0.73	6.7	1.11	4.73	5.3					2.5	5.3				945	3.2	5.0	
		C-5	0.51	0.09	5.0	0.05	5.17	0.3													North Pond
		OS-2	20.07	0.14	18.3	2.81	3.22	9.0													Overland flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
		OS-3	10.61	0.14	18.9	1.49	3.18	4.7													Offsite flow into Basin D-3. Flow obtained from Bent Grass Filing No. 2 FDR
		D-3	2.93	0.23	21.0	0.67	3.01	2.0													Flows conveyed via existing ditch into proposed area inlet.
		D-2	6.72	0.56	12.4	3.76	3.81	14.3					1.3	14.3				1355	2.3	9.9	Flow into proposed inlet. Piped to DP 14.
		D-1	8.13	0.41	21.1	3.33	3.01	10.0					1.3	10.0				1900	2.3	13.9	Combined flows from D-1 into proposed inlet.
		D-4	4.38	0.52	16.0	2.28	3.42	7.8					1	7.8				980	2.0	8.2	Flow into proposed inlet.
		D-5	1.08	0.51	11.0	0.55	3.99	2.2					1.1	2.2				300	2.1	2.4	
		D-6	4.01	0.54	12.4	2.17	3.80	8.2					1	8.2				835	2.0	7.0	
		E-4	0.91	0.74	8.0	0.67	4.46	3.0													Flow into Ex inlet.
		E-5	0.89	0.81	7.3	0.72	4.60	3.3													Flow into Ex inlet.

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision:Falcon Meadows at Bent GrassFalcon Meadows at Bent GrassLocation:CO, Colorado SpringsCalculated By:TJEDesign Storn:5-YearChecked By:CMDDate:6/19/20

				DIRE	CT RUN	OFF				TOTAL :	RUNOF	F	STR	REET		PIPE		TRAV	EL T	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
		I-1	0.31	0.66	5.0	0.20	5.17	1.0													Flow into Ex inlet.
		D-7	6.39	0.14	14.8	0.89	3.54	3.2													
		D-8	1.69	0.21	14.0	0.35	3.62	1.3													Flow in Swale C (Basin D-8) into proposed south pond
		E-3	0.78	0.81	7.4	0.63	4.59	2.9													Flow into Ex Inlet in BGMD (South Side)
		B-2	1.17	0.10	16.0	0.12	3.42	0.4													

CLH17_PR-PDR-Drainage Cales.xlsm

provide current and proposed

BENT GRASS/MERIDIAN ROAD - PDR SURFACE ROUTING - CURRENT CONDITIONS

DESIGN	CONTRIBUTING	C A (e q u	ivalent)	Tc	INTEN	ISITY	TOTAL	FLOWS	NOTES
POINT	BASINS	CA(5)	CA(100)		I(5)	I(100)	Q(5)	Q(100)	
		` '		(min.)	(in/hr)	(in/hr)	(cfs)	(cfs)	
	RWT202	124.80	324.77	46.6	1.8	3.1	220.0	1000.0	
					TF	RAVEL TIN	ΛE		
		124.80	324.77	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	1
				CHANNEL	2000	5.0	6.7	53.3	
	RWT204	1.83	6.43	11.4	3.8	6.7	7.0	43.0	
					TR	RAVEL TIN			
		1.83	6.43	Type/flow	Length (ft)	, , ,	_ , ,	T. Time (min)	
				CHANNEL	800	5.0	2.7	14.1	
	WT200	25.81	54.00	37.8	2.0	3.5	52.0	190.0	
						RAVEL TIN			
		25.81	54.00	Type/flow	Length (ft)		d. Time (min)		
				CHANNEL	800	5.0	2.7	40.5	
21	OS-1	5.16	13.23	22.2	2.8	4.8	14.2	63.6	
						RAVEL TIN			
		5.16	13.23	Type/flow	Length (ft)		d. Time (min)		
				CHANNEL	800	5.0	2.7	24.9	
2	OS-4	1.61	2.41	15.6	3.3	5.8	5.3	13.9	
				- 10		RAVEL TIN		/	
		1.61	2.41	Type/flow	Length (ft)			T. Time (min)	
-	00.5	0.04	0.07	STREET	200	3.2	1.0	16.7	
1	OS-5	0.21	0.27	16.7	3.2	5.6 RAVEL TIN	5.8	15.0	
	DP 2	1.61	2.41	T /9				T Thur (!)	
		1.82	2.68	Type/flow STREET	Length (ft) 55	3.2	a. time (min) 0.3	T. Time (min) 16.9	
3	OS-6	0.53	0.69		3.2	5.5	7.5	18.7	
J	DP 1	1.82	2.68	10.9		SAVEL TIN		10.7	
	DI I	2.35		Type/flow	Length (ft)		d. Time (min)	T Timo (min)	
		2.33	3.37	STREET	115	3.2	0.6	17.5	
4	A-1	1.21	1.71	17.5	3.1	5.5	11.1	27.7	@ GRADE INLET
7	DP 3	2.35	3.37	17.5		RAVEL TIN		21.1	C OWNER INCE
	51 3	3.56		Type/flow	Length (ft)		d. Time (min)	T Time (min)	i
		3.30	3.00	STREET	40	2.4	0.3	17.8	
5	A-3	0.60	0.72		4.2	7.4	3.6		@ GRADE INLET
Ü	FB DP 4	0.26	1.51	0.7		RAVEL TIN		10.0	O OTTIBE INCE!
		0.86		Type/flow	Length (ft)			T. Time (min)	
		0.00	2.20	STREET	80	2.0	0.7	9.6	1
6	A-4	0.07	0.30		3.1	5.4	13.9	41.2	EX BG FIL NO. 2 WQ
-	DP 4	3.56	5.08						POND
	DP 5	0.86	2.23		TR	RAVEL TIN	ЛE		1
		4.49		Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	1
				-	J (1	2.0	0.0	17.8	1
15A	EX NORTH WQ	2.35	4.08	5.0	5.2	9.1	12.2	37.0	
	POND RELEASE					RAVEL TIN			1
		2.35	4.08	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	1
					J . /	2.6	0.0	5.0	

DESIGN	CONTRIBUTING	C A (equ	ivalent)	Tc	INTEI	VSITY	TOTAL	FLOWS	NOTES
POINT	BASINS	CA(5)	CA(100)		I(5)	I(100)	Q(5)	Q(100)	
				(min.)	(in/hr)	(in/hr)	(cfs)	(cfs)	
7	E-3	0.63	0.69	7.4	4.6	8.0	2.9	5.5	EX SUMP INLET
						RAVEL TIM			
		0.63	0.69	Type/flow	Length (ft)		d. Time (min)		
						2.6	0.0	7.4	
8	E-1	0.94	1.18	11.8	3.8	6.6	11.5	36.4	EX SUMP INLET
	E-2	0.52	0.58						
	C-4	1.60	2.49						
	FB DP 5	0.00	1.28	- 10		RAVEL TIM		/	
		3.06	5.53	Type/flow	Length (ft)		d. Time (min)		
	DIAITOOO	101.00	004.77	F0.0	1.1	2.6	0.0	11.8	
AA	RWT202	124.80	324.77	53.3	1.6	2.8	260.0	1143.5	CHANNEL FLOW & EX BOX CULVERTS @
	RWT204	1.83	6.43						BGMD
	WT200 OS-1	25.81 5.16	54.00 13.23						DGIVID
	B-1	0.39	13.23						
	DP 8	3.06	5.53		Т	RAVEL TIM	/ F		
	DP 15A	2.35	4.08		1.1	VAVEL III	VI L		
	1071	161.05	405.52	Type/flow	Length (ft)	Velocity (fns)	d. Time (min)	T Time (min)	
		101.00	100.02	CHANNEL	900	5.0	3.0	56.3	
12	C-2	0.54	0.72	5.0	5.2	9.1	9.7		@ GRADE INLET
	FB DP 15	1.33	2.73	0.0		RAVEL TIM		02	- 0.0.152 <u>-</u>
	· · ·	1.87		Type/flow	Length (ft)		d. Time (min)	T. Time (min)	
			01.10	STREET	350		2.3	7.3	
15	C-1	4.63	5.90	13.9	3.5	6.1	20.1	43.7	@ GRADE INLET
	C-3	1.11	1.25			RAVEL TIM			
		5.74	7.15	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
				STREET	40		0.3	14.2	
19	C-6	0.51	0.74	10.3	4.0	7.0	2.0	5.2	AREA INLET
					T F	RAVEL TIM	ИE		
		0.51	0.74	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						3.2	0.0	10.3	
13	DP 12	1.87	3.45	14.2	3.5	6.0	28.1		TOTAL FLOW INTO PR
	DP 15	5.74	7.15						NORTH WQ POND
	DP 19	0.51	0.74		TF	RAVEL TIM			
		8.12	11.34	Type/flow	Length (ft)	,	d. Time (min)	_ , ,	
						2.6	0.0	14.2	
13A	NORTH WQ	0.64	2.47	5.0	5.2	9.1	3.3	22.4	
	POND RELEASE					RAVEL TIM			
		0.64	2.47	Type/flow	Length (ft)		d. Time (min)		
						2.6	0.0	5.0	
9	OS-2	2.81	8.03	18.3	3.1	5.3	8.6	42.8	
						RAVEL TIM			
		2.81	8.03	Type/flow	Length (ft)		d. Time (min)		
				SWALE	1150		3.4	21.8	
10	OS-3	1.49	4.24	18.9	3.0	5.2	4.5	22.2	
						RAVEL TIM			
		1.49	4.24	Type/flow	Length (ft)		d. Time (min)		
				SWALE	3.33	6.1	0.0	18.9	

DESIGN	CONTRIBUTING	C A (e q u	ivalent)	Tc	INTEI	NSITY	TOTAL	FLOWS	NOTES
POINT	BASINS	CA(5)	CA(100)		I(5)	I(100)	Q(5)	Q(100)	
				(min.)	(in/hr)	(in/hr)	(cfs)	(cfs)	
11	D-3	0.67	1.00	21.8	2.8	4.9	13.8	64.5	AREA INLET
	DP 9	2.81	8.03						
	DP 10	1.49	4.24		T F	RAVEL TIM	ИE		
		4.97	13.27	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						6.0	0.0	21.8	
14	D-2	3.76	4.64	12.4	3.7	6.4	13.9	29.9	@ GRADE INLET
					ΤF	RAVEL TIM	ИE		
		3.76	4.64	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
				STREET	40	2.0	0.3	12.7	
16	D-1	3.33	4.72	21.1	2.8	4.9	12.0	36.4	@ GRADE INLET
	FB DP 14	0.92	2.65		TF	RAVEL TIM	ИE		
		4.25	7.37	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
				STREET	900	2.8	5.4	26.5	
17	D-4	2.28	2.89	16.0	3.3	5.7	7.5	16.5	SUMP INLET
					ΤF	RAVEL TIM	ИE		
		2.28	2.89	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	1
						6.1	0.0	16.0	
18	D-5	0.55	0.69	12.4	3.7	6.4	10.0	21.8	SUMP INLET
	D-6	2.17	2.69		TF	RAVEL TI	ИE		
		2.72	3.38	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
				,	, ,	6.2	0.0	12.4	
31	DP 17	2.28	2.89	26.5	2.5	4.4	32.5	79.7	FLOW INTO PR SOUTH
	DP 14	3.76	4.64						WQ POND
	DP 16	4.25	7.37						
	DP 18	2.72	3.38		ΤF	RAVEL TIM	ИE		
		13.01	18.28	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						6.0	0.0	26.5	
24	E-4	0.67	0.76	26.5	2.5	4.4	5.9	27.0	EX @ GRADE INLET
	FB DP 16	1.68	5.44		TF	RAVEL TI	ИE		
		2.35	6.20	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						2.6	0.0	26.5	
25	E-5	0.72	0.79	7.3	4.6	8.0	3.3	9.9	EX @ GRADE INLET
	FB DP 24	0.00	0.45		T F	RAVEL TII	M E		
		0.72	1.24	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
				71	, ,	2.6	0.0	7.3	
26	DP 24	2.35	6.20	26.5	2.5	4.4	7.7	32.4	FLOWS INTO SWALE F
	DP 25	0.72	1.24		TF	RAVEL TII	M E		
		3.07	7.44	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
				SWALE	740		3.5	30.0	
30	D-7	0.89	2.49	14.8	3.4	5.9	13.5	58.9	FLOW INTO PR SOUTH
	DP 26	3.07	7.44			RAVEL TII			WQ POND
		3.96	9.93	Type/flow	Length (ft)		d. Time (min)	T. Time (min)	1
		3.70	7.70	Jr	5 ()	2.6	0.0	14.8	
32	D-8	0.35	0.74	14.0	3.5		1.2		FLOW INTO PR SOUTH
	-	3.00	0.71	1110		RAVEL TII		1.0	WQ POND
		0.35	0.74	Type/flow	Length (ft)		d. Time (min)	T. Time (min)	
		0.00	0.77	. 100/11000	Longin (ii)	6.1	0.0	14.0	
						0.1	5.5		

DESIGN	CONTRIBUTING	C A (e q u	ivalent)	Tc	INTEI	NSITY	TOTAL	FLOWS	NOTES
POINT	BASINS	CA(5)	CA(100)		I(5)	I(100)	Q(5)	Q(100)	
				(min.)	(in/hr)	(in/hr)	(cfs)	(cfs)	
20	DP 30	3.96	9.93	26.5	2.5	4.4	43.2	126.1	TOTAL FLOW INTO PR
	DP 31	13.01	18.28						SOUTH WQ POND
	DP 32	0.35	0.74		T F	RAVEL TIM	ИE		
		17.32	28.95	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						2.6	0.0	26.5	
20A	PR SOUTH WQ	1.85	5.20	5.0	5.2	9.1	9.6	47.1	
	POND RELEASE				T F	RAVEL TIM	ИE		
		1.85	5.20	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						2.6	0.0	5.0	
20B	EX SOUTH WQ	4.11	7.28	5.0	5.2	9.1	21.3	66.0	
	POND RELEASE				T F	RAVEL TIM	ИE		
		4.11	7.28	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						2.6	0.0	5.0	
CC	B-2	0.12	0.44	56.3	1.6	2.7	260.1	1137.6	FLOWS EXITING SITE IN
	DP AA	161.05	405.52						CHANNEL
	DP 20A	1.85	5.20						
	DP 20B	4.11	7.28		TF	RAVEL TIM	ИE		
		167.13	418.44	Type/flow	Length (ft)	Velocity (fps)	d. Time (min)	T. Time (min)	
						2.6	0.0	56.3	

APPENDIX C Hydraulic Computations

Swale Calculations

Swales with supercritical designs highlighted.

Worksheet for Swale - A

Proi	ioct	Descri	ntion
Γ 10	IECL.	Descii	มแบบ

Manning Formula Friction Method Solve For Normal Depth

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.02580	ft/ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)
Discharge	5.20	ft³/s

Results

Normal Depth		0.61	ft
Flow Area		1.48	ft²
Wetted Perimeter		5.01	ft
Hydraulic Radius		0.29	ft
Top Width		4.86	ft
Critical Depth		0.64	ft
Critical Slope		0.01999	ft/ft
Velocity		3.52	ft/s
Velocity Head		0.19	ft
Specific Energy		0.80	ft
Froude Number		1.13	
Flow Type	Supercritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth

Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.61	ft
Critical Depth	0.64	ft
Channel Slope	0.02580	ft/ft
Critical Slope	0.01999	ft/ft

0.00 ft

Worksheet for Swale - C

Proi	ioct	Descri	ntion
Γ 10	IECL.	Descii	มแบบ

Manning Formula Friction Method Solve For Normal Depth

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.02400	ft/ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)
Bottom Width	1.00	ft
Discharge	4.50	ft³/s

Results

Normal Depth		0.47	ft
Flow Area		1.37	ft²
Wetted Perimeter		4.91	ft
Hydraulic Radius		0.28	ft
Top Width		4.79	ft
Critical Depth		0.49	ft
Critical Slope		0.02033	ft/ft
Velocity		3.28	ft/s
Velocity Head		0.17	ft
Specific Energy		0.64	ft
Froude Number		1.08	
Flow Type	Supercritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.47	ft
Critical Depth	0.49	ft
Channel Slope	0.02400	ft/ft
Critical Slope	0.02033	ft/ft

Worksheet for Swale - D

_		_	
Pro	IACT.	I)ASC	ription

Manning Formula Friction Method Solve For Normal Depth

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.02000	ft/ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)
Bottom Width	2.00	ft
Discharge	50.00	ft³/s

Results

Normal Depth		1.26	ft
Flow Area		8.91	ft²
Wetted Perimeter		12.42	ft
Hydraulic Radius		0.72	ft
Top Width		12.10	ft
Critical Depth		1.35	ft
Critical Slope		0.01474	ft/ft
Velocity		5.61	ft/s
Velocity Head		0.49	ft
Specific Energy		1.75	ft
Froude Number		1.15	
Flow Type	Supercritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	1.26	ft
Critical Depth	1.35	ft
Channel Slope	0.02000	ft/ft
Critical Slope	0.01474	ft/ft

Worksheet for Swale - E

_		_	
Pro	IACT.	I)ASC	ription

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.00500	ft/ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)
Bottom Width	3.00	ft
Discharge	64.50	ft³/s

Results

Normal Depth		1.79	ft
Flow Area	1	18.15	ft²
Wetted Perimeter	1	17.74	ft
Hydraulic Radius		1.02	ft
Top Width	1	17.30	ft
Critical Depth		1.42	ft
Critical Slope	0.0	1426	ft/ft
Velocity		3.55	ft/s
Velocity Head		0.20	ft
Specific Energy		1.98	ft
Froude Number		0.61	
Flour Type	Suboritical		

Flow Type Subcritical

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	1.79	ft
Critical Depth	1.42	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.01426	ft/ft

Worksheet for Swale - F

_			
ν_{r}	IDCt.	Descri	ntion
1 10		Descii	DUUI

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.01000	ft/ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)
Bottom Width	6.00	ft
Discharge	32.40	ft³/s

Results

Normal Depth		0.91	ft
Flow Area		8.73	ft²
Wetted Perimeter		13.48	ft
Hydraulic Radius		0.65	ft
Top Width		13.26	ft
Critical Depth		0.80	ft
Critical Slope		0.01592	ft/ft
Velocity		3.71	ft/s
Velocity Head		0.21	ft
Specific Energy		1.12	ft
Froude Number		0.81	
Flow Type	Subcritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.91	ft
Critical Depth	0.80	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.01592	ft/ft

Inlet Calculations

Inlet calculations not checked with this review.

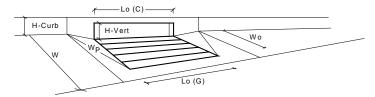
Version 4.06 Released August 2018

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 8 - Existing Sump Inlet (BG Filing No. 2) STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 26.0 Gutter Width W: 2.00 Street Transverse Slope S_X : 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP

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INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening ▼	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L ₀ (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	14.4	52.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	11.5	36.4	cfs

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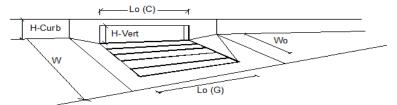
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 5 - At Grade Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb SBACK Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.051 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm 22.8 MAJOR STORM Allowable Capacity is based on Spread Criterion VARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management'

ajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

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INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input) Type of Inlet CDOT Type R Curb Opening	▼ Type =	MINOR CDOT Type F	MAJOR Curb Opening	7
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR STORM'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.6	9.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	7.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	56	%

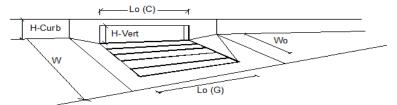
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 12 - At Grade Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 SBACK Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 14.2 NARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Mar ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management

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INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening ▼	_	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR & MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.7	16.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	1.0	14.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	90	52	%

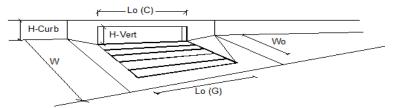
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 14 - At Grade Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb SBACK Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion NARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Mar ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management

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INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening	=1	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_fG =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f - C =$	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR & MAJOR STO	RM_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	11.3	16.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	2.6	13.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	82	56	%

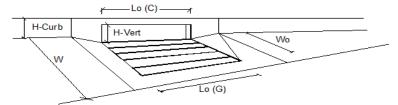
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 15 - At Grade Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 SBACK Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 14.2 NARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Mar ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management

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INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)	ODOTT DO O		MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to cor	ntinuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate	or Curb Opening)	L ₀ =	15.00	15.00	ft
Width of a Unit Grate (cannot be g	reater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit (Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit C	curb Opening (typical min. value = 0.1)	$C_f-C =$	0.10	0.10	
Street Hydraulics: WARNING: Q	> ALLOWABLE Q FOR MINOR & MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity		Q =	13.2	19.0	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	Q _b =	6.9	24.7	cfs
Capture Percentage = Q _a /Q _o =		C% =	66	43	%

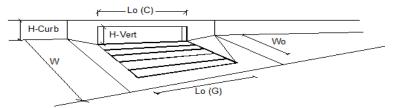
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 16 - At Grade Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb SBACK Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.013 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion NARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Mar ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management

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INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input) Type of Inlet CDOT Type R Curb Opening ▼	Type =	MINOR CDOT Type R	MAJOR Curb Opening	7
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR & MAJOR STORM		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	7.8	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	4.2	23.7	cfs
Capture Percentage = Q _a /Q _o =	C% =	65	35	%

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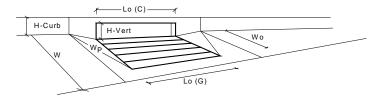
Version 4.06 Released August 2018

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 17 - Sump Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width W: 2.00 Street Transverse Slope S_X : 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 16.5 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP

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INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



Design Information (Input)	CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	CDO1 Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to c	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	lumber of Unit Inlets (Grate or Curb Opening)		2	2]
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	4.4	5.7	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grat	e (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical va	lue 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		_	MINOR	MAJOR	
Length of a Unit Curb Opening		$L_o(C) =$	15.00	15.00	feet
Height of Vertical Curb Opening i	n Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in I	nches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curt	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	1
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Eq	uation	d _{Curb} =	0.20	0.31	ft
Combination Inlet Performance R	Reduction Factor for Long Inlets	RF _{Combination} =	0.42	0.54	1
Curb Opening Performance Red	uction Factor for Long Inlets	RF _{Curb} =	0.67	0.77	
Grated Inlet Performance Reduct	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
			MINOR	MAJOR	_
Total Inlet Interception Ca	apacity (assumes clogged condition)	Q _a =	7.9	17.3	cfs
Inlet Capacity IS GOOD for Min	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	7.5	16.5	cfs

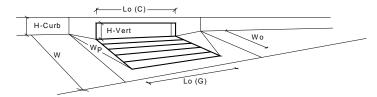
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 18 - Sump Inlet STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 16.5 Gutter Width W: 2.00 Street Transverse Slope S_X : 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 16.5 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP

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INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening ▼		MINOR	MAJOR	-
Type of fillet	Type =	,,	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	6.0	inches
Grate Information	. (0)	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L ₀ (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.23	0.33	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.45	0.57	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.70	0.79	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.4	19.9	cfs
WARNING: Inlet Capacity less than Q Peak for Major Storm	Q PEAK REQUIRED =	10.0	21.8	cfs

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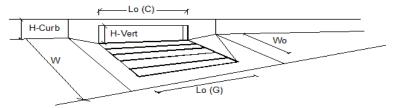
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 24 - Existing At Grade Inlet (BG Filing No. 2) STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 26.0 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.028 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm 55.5 MAJOR STORM Allowable Capacity is based on Spread Criterion 18.1 inor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Managen

ajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

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INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)	CDOT Trace B. Crist Opening		MINOR	MAJOR	_
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to con	tinuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (0	Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate	or Curb Opening)	L _o =	25.00	25.00	ft
Width of a Unit Grate (cannot be gr	eater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit G	Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit C	urb Opening (typical min. value = 0.1)	C_{f} - $C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allow	able Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity		Q =	5.9	23.4	cfs
Total Inlet Carry-Over Flow (flow	bypassing inlet)	Q _b =	0.0	3.6	cfs
Capture Percentage = Q _a /Q _o =		C% =	100	87	%

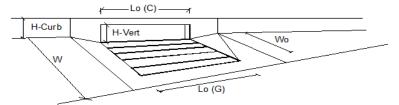
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Falcon Meadows at Bent Grass Project: Inlet ID: DP 25 - Existing At Grade Inlet (BG Filing No. 2) STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 26.0 Gutter Width w 2.00 Street Transverse Slope $\textbf{S}_{\textbf{X}}$ 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.028 Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 22.2 68.2 inor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager ajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

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INLET ON A CONTINUOUS GRADE

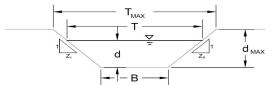
Version 4.06 Released August 2018



Design Information (Input)		_	MINOR	MAJOR	_
Type of Inlet CDOT Type R Curb Openi	ng 💌	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L ₀ =	25.00	25.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value	e = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		_	MINOR	MAJOR	_
Total Inlet Interception Capacity		Q =	3.3	9.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =		C% =	100	100	%

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Falcon Meadows at Bent Grass DP 11 - Type D Area Inlet (Relocated)

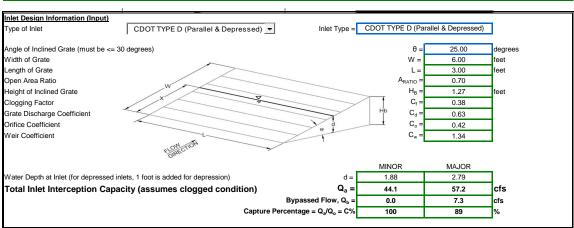


This worksheet uses the NRCS vegetal retardance method to determine Manning's n. For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method	_			
NRCS Vegetal Retardance (A, B, C, D, or E)	A, B, C, D or E			
Manning's n (Leave cell D16 blank to manually enter an n value)	n =	0.030		
Channel Invert Slope	S _O =	0.0050	ft/ft	
Bottom Width	B =	3.00	ft	
Left Side Slope	Z1 =	4.00	ft/ft	
Right Side Slope	Z2 =	4.00	ft/ft	
Check one of the following soil types:		Choose One:	_	7
Soil Type: Max. Velocity (V _{MAX}) Max Froude No. (F _{MAX})		O Non-Cohesive	•	ł
Non-Cohesive 5.0 fps 0.60		Cohesive		
Cohesive 7.0 fps 0.80		☐ Paved		
Paved N/A N/A		_		
	_	Minor Storm	Major Storm	_
Max. Allowable Top Width of Channel for Minor & Major Storm	T _{MAX} =	11.00	18.00	feet
Max. Allowable Water Depth in Channel for Minor & Major Storm	d _{MAX} =	1.00	2.00	feet
Allowable Channel Capacity Based On Channel Geometry		Minor Storm	Major Storm	
MINOR STORM Allowable Capacity is based on Depth Criterion	Q _{allow} =	17.9	72.2	cfs
MAJOR STORM Allowable Capacity is based on Top Width Criterion	d _{allow} =	1.00	1.88	ft
Water Depth in Channel Based On Design Peak Flow	_		<u>-</u>	
Design Peak Flow	Q ₀ =	13.8	64.5	cfs
200.3 0	d =	0.88	1.79	feet

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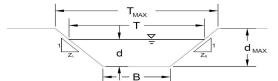
Falcon Meadows at Bent Grass DP 11 - Type D Area Inlet (Relocated)



Warning 04: Froude No. exceeds USDCM Volume I recommendation.

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Falcon Meadows at Bent Grass DP 19 - Type C Area Inlet



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method	A. B. C. D or E		1	
NRCS Vegetal Retardance (A, B, C, D, or E)				
Manning's n (Leave cell D16 blank to manually enter an n value)	n =	0.030		
Channel Invert Slope	S _o =	0.0260	ft/ft	
Bottom Width	B =	0.00	ft	
Left Side Slope	Z1 =	4.00	ft/ft	
Right Side Slope	Z2 =	4.00	ft/ft	
Check one of the following soil types:		Choose One:		7
Soil Type: Max. Velocity (V _{MAX}) Max Froude No. (F _{MAX})		Non-Cohesive	е	
Non-Cohesive 5.0 fps 0.60		Cohesive		
Cohesive 7.0 fps 0.80		○ Paved		
Paved N/A N/A	L			
	_	Minor Storm	Major Storm	_
Max. Allowable Top Width of Channel for Minor & Major Storm	T _{MAX} =	16.00	16.00	feet
Max. Allowable Water Depth in Channel for Minor & Major Storm	d _{MAX} =	1.00	1.00	feet
Allowable Channel Capacity Based On Channel Geometry		Minor Storm	Major Storm	
MINOR STORM Allowable Capacity is based on Depth Criterion	Q _{allow} =	19.8	19.8	cfs
MAJOR STORM Allowable Capacity is based on Depth Criterion	d _{allow} =	1.00	1.00	ft
Water Depth in Channel Based On Design Peak Flow				
Design Peak Flow	Q _o =	2.0	5.2	cfs
Water Depth	d =	0.42	0.61	feet

CLH17_UD-Inlet.xlsm, DP 19 2/9/2021, 1:57 PM

Falcon Meadows at Bent Grass DP 19 - Type C Area Inlet Inlet Design Information (Input) -CDOT Type C Type of Inlet CDOT Type C Inlet Type = Angle of Inclined Grate (must be <= 30 degrees) degrees Width of Grate Length of Grate Open Area Ratio $\mathsf{A}_{\mathsf{RATIO}}$ 0.70 Height of Inclined Grate 0.00 Clogging Factor 0.50 Grate Discharge Coefficient C_{d} 0.96 Orifice Coefficient C_o 0.64 Weir Coefficient 2.05 MINOR MAJOR Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) 0.42 0.61 Q_a = Total Inlet Interception Capacity (assumes clogged condition) 5.1 cfs 8.7 Bypassed Flow, Q_b = 0.0 0.0 cfs Capture Percentage = $Q_a/Q_o = C\%$ 100 100

Warning 04: Froude No. exceeds USDCM Volume I recommendation.

CLH17_UD-Inlet.xlsm, DP 19 2/9/2021, 1:57 PM

StormCAD

Proposed Smile - E Op 11 Op 11 Op 14 Op 14 Op 14 Op 14 Op 14 Op 15 Op 15 Op 16 Op 16 Op 16 Op 16 Op 17 Op 16 Op 17 Op 17 Op 18 Op

flow is higher than capacity - are watertight gasket joints proposed?

BG Filing No. 3 Storm

FlexTable: Conduit Table

Label	Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calc) (ft/ft)	Dia (in)	Manning's n	Flow (cfs)	yel (ft/s)	Capacity (Full Flow) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
P-12	MH-7	Outfall	6,927.48	6,926.00	296.0	0.005	48.0	0.013	128.81	10.25	101.57	6,932.05	6,929.40	6,933.68	6,931.39
P-1	DP 11	DP 16	6,940.50	6,939.59	96.5	0.009	42.0	0.013	56.02	10.50	97.69	6,943.92	6,943.63	6,944.46	6,944.16
P-2	DP 16	MH-1	6,939.29	6,939.24	5.0	0.010	42.0	0.013	86.57	9.00	100.60	6,943.00	6,942.97	6,944.26	6,944.22
P-3	DP 14	MH-1	6,942.50	6,941.24	27.5	0.046	24.0	0.013	24.85	15.52	48.44	6,944.26	6,942.46	6,945.38	6,944.85
P-4	MH-1	MH-2	6,938.74	6,936.65	211.5	0.010	48.0	0.013	106.07	12.45	142.80	6,941.86	6,940.56	6,943.44	6,941.68
P-5	MH-2	MH-3	6,936.35	6,935.03	132.1	0.010	48.0	0.013	105.37	12.49	143.59	6,939.46	6,938.93	6,941.03	6,940.04
P-6	MH-3	MH-4	6,934.73	6,933.99	75.2	0.010	48.0	0.013	104.93	12.40	142.45	6,937.83	6,937.91	6,939.40	6,939.01
P-7	MH-4	MH-5	6,933.69	6,933.08	61.2	0.010	48.0	0.013	104.68	12.45	143.39	6,936.88	6,936.97	6,938.36	6,938.06
P-8	MH-5	MH-6	6,932.78	6,929.88	235.3	0.012	48.0	0.013	104.48	13.53	159.45	6,935.88	6,934.72	6,937.43	6,935.79
P-9	MH-6	MH-7	6,929.58	6,927.78	119.8	0.015	48.0	0.013	103.76	8.26	176.10	6,933.98	6,933.35	6,935.04	6,934.41
P-10	DP 18	DP 17	6,931.23	6,930.63	35.0	0.017	18.0	0.013	13.85	7.83	13.75	6,934.04	6,933.43	6,934.99	6,934.38
P-11	DP 17	MH-7	6,928.13	6,928.08	9.2	0.005	48.0	0.013	29.99	2.39	105.77	6,933.36	6,933.35	6,933.44	6,933.44

FlexTable: Manhole Table

Label	Elevation (Rim) (ft)	Headloss Coefficient (Standard)	Headloss Method	Headloss (ft)	Hydraulic Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Diameter (in)
MH-1	6,947.98	0.700	Standard	1.11	6,941.86	6,942.97	6,945.35	6,943.44	84.0
MH-2	6,946.72	0.700	Standard	1.10	6,939.46	6,940.56	6,941.68	6,941.03	96.0
MH-3	6,945.39	0.700	Standard	1.10	6,937.83	6,938.93	6,940.04	6,939.40	96.0
MH-4	6,944.74	0.700	Standard	1.03	6,936.88	6,937.91	6,939.01	6,938.36	96.0
MH-5	6,944.50	0.700	Standard	1.09	6,935.88	6,936.97	6,938.06	6,937.43	96.0
MH-6	6,942.08	0.700	Standard	0.74	6,933.98	6,934.72	6,935.79	6,935.04	96.0
MH-7	6,941.75	0.800	Standard	1.31	6,932.05	6,933.35	6,934.41	6,933.68	96.0

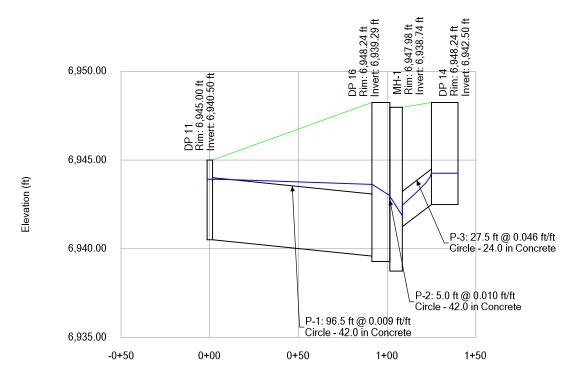
FlexTable: Outfall Table

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,929.00	6,926.00	User Defined Tailwater	6,928.46	6,929.40	6,929.40	127.32

Profile Report

Engineering Profile - Profile - 1 (BG Filing 3 StormCAD.stsw)

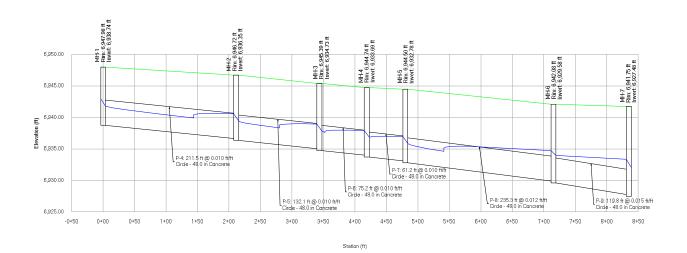
Active Scenario: 100 YR



Station (ft)

Profile Report

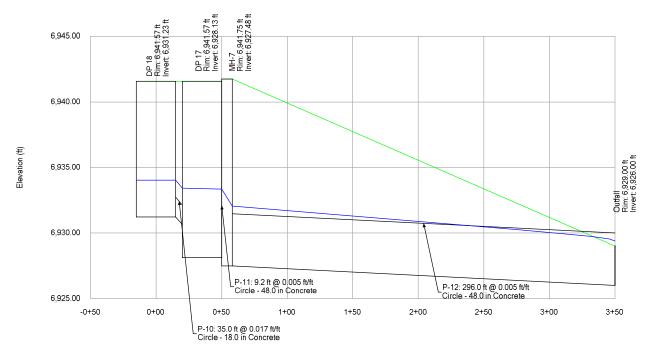
Engineering Profile - Profile - 2 (BG Filing 3 StormCAD.stsw)



Profile Report

Engineering Profile - Profile - 3 (BG Filing 3 StormCAD.stsw)

Active Scenario: 100 YR



Station (ft)

FlexTable: Conduit Table

Label	Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calc) (ft/ft)	Dia (in)	Manning's n	Flow (cfs)	Vel (ft/s)	Capacity (Full Flow) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
P-12	MH-7	Outfall	6,927.48	6,926.00	296.0	0.005	48.0	0.013	38.33	7.52	101.57	6,929.33	6,927.70	6,930.04	6,928.58
P-1	DP 11	DP 16	6,940.50	6,939.59	96.5	0.009	42.0	0.013	11.00	6.72	97.69	6,941.50	6,940.93	6,941.87	6,941.10
P-2	DP 16	MH-1	6,939.29	6,939.24	5.0	0.010	42.0	0.013	20.45	8.20	100.60	6,940.68	6,940.74	6,941.19	6,941.16
P-3	DP 14	MH-1	6,942.50	6,941.24	27.5	0.046	24.0	0.013	10.55	12.33	48.44	6,943.66	6,941.96	6,944.14	6,943.62
P-4	MH-1	MH-2	6,938.74	6,936.65	211.5	0.010	48.0	0.013	28.71	8.89	142.80	6,940.33	6,938.34	6,940.92	6,938.84
P-5	MH-2	MH-3	6,936.35	6,935.03	132.1	0.010	48.0	0.013	28.45	8.90	143.59	6,937.93	6,936.72	6,938.52	6,937.21
P-6	MH-3	MH-4	6,934.73	6,933.99	75.2	0.010	48.0	0.013	28.28	8.83	142.45	6,936.31	6,935.67	6,936.89	6,936.17
P-7	MH-4	MH-5	6,933.69	6,933.08	61.2	0.010	48.0	0.013	28.19	8.87	143.39	6,935.26	6,934.76	6,935.85	6,935.25
P-8	MH-5	MH-6	6,932.78	6,929.88	235.3	0.012	48.0	0.013	28.11	9.56	159.45	6,934.35	6,931.55	6,934.94	6,932.05
P-9	MH-6	MH-7	6,929.58	6,927.78	119.8	0.015	48.0	0.013	27.84	10.23	176.10	6,931.14	6,929.89	6,931.73	6,930.16
P-10	DP 18	DP 17	6,931.23	6,930.63	35.0	0.017	18.0	0.013	5.72	7.42	13.75	6,932.15	6,931.33	6,932.54	6,932.11
P-11	DP 17	MH-7	6,928.13	6,928.08	9.2	0.005	48.0	0.013	12.53	5.65	105.77	6,929.89	6,929.89	6,929.98	6,929.97

FlexTable: Manhole Table

Label	Elevation (Rim) (ft)	Headloss Coefficient (Standard)	Headloss Method	Headloss (ft)	Hydraulic Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Diameter (in)
MH-1	6,947.98	0.700	Standard	0.42	6,940.33	6,940.74	6,941.16	6,940.92	84.0
MH-2	6,946.72	0.700	Standard	0.41	6,937.93	6,938.34	6,938.84	6,938.52	96.0
MH-3	6,945.39	0.700	Standard	0.41	6,936.31	6,936.72	6,937.21	6,936.89	96.0
MH-4	6,944.74	0.700	Standard	0.41	6,935.26	6,935.67	6,936.17	6,935.85	96.0
MH-5	6,944.50	0.700	Standard	0.41	6,934.35	6,934.76	6,935.25	6,934.94	96.0
MH-6	6,942.08	0.700	Standard	0.41	6,931.14	6,931.55	6,932.05	6,931.73	96.0
MH-7	6,941.75	0.800	Standard	0.57	6,929.33	6,929.89	6,930.16	6,930.04	96.0

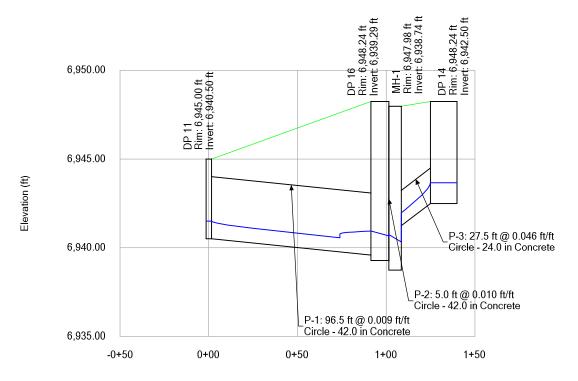
FlexTable: Outfall Table

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Energy Grade Line (ft)	Flow (Total Out) (cfs)
Outfall	6,929.00	6,926.00	User Defined Tailwater	6,926.78	6,927.70	6,927.70	37.72

Profile Report

Engineering Profile - Profile - 1 (BG Filing 3 StormCAD.stsw)

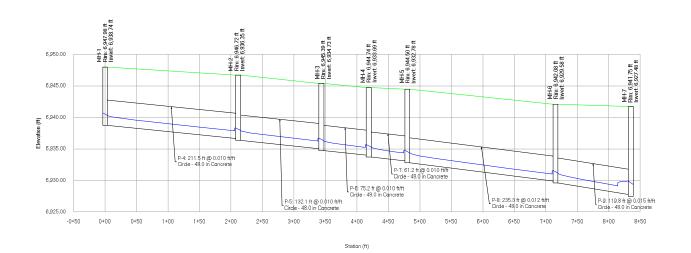
Active Scenario: 5 YR



Station (ft)

Profile Report

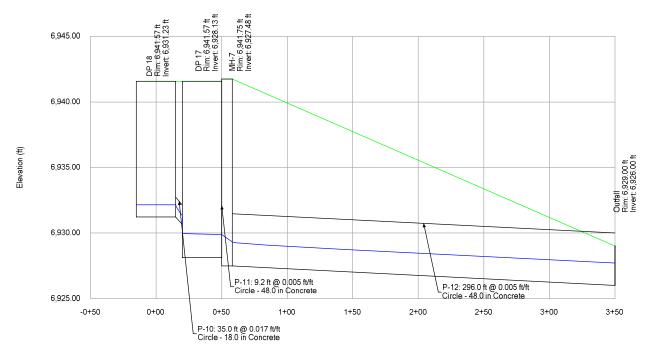
Engineering Profile - Profile - 2 (BG Filing 3 StormCAD.stsw)



Profile Report

Engineering Profile - Profile - 3 (BG Filing 3 StormCAD.stsw)

Active Scenario: 5 YR



Station (ft)

Pond Calculations

Detention Pond Tributary Areas

Subdivision: Falcon Meadows at Bent Grass

Location: CO, Colorado Springs

Project Name: Falcon Meadows at Bent Grass

Project No.: CLH000017

Calculated By: TJE
Checked By: CMD

Date: 6/19/20

Pond (North)

Basin	Area	% Imp
C-1	9.07	65
C-2	1.11	58
C-3	1.52	86.6
C-5	0.51	2
C-6	1.37	51.2
Total	13.58	63.1

Provide update for Filing 2 North pond

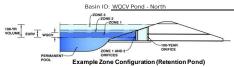
Pond (South)

Basin	Area	% Imp
D-1	8.13	49.7
D-2	6.72	69.9
D-3	2.93	31.7
D-4	4.38	65.4
D-5	1.08	65.7
D-6	4.01	71.5
D-7	6.39	9.8
D-8	1.69	22.8
E-4	0.91	80.6
E-5	0.89	89
OS-2	20.07	8
OS-3	10.61	8
Total	67.81	31.1

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

Project: Falcon Meadows at Bent Gras



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	13.94	acres
Watershed Length =	1,275	ft
Watershed Length to Centroid =	750	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	63.60%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.							
Water Quality Capture Volume (WQCV) =	0.289	acre-feet					
Excess Urban Runoff Volume (EURV) =	1.093	acre-feet					
2-yr Runoff Volume (P1 = 1.19 in.) =	0.798	acre-feet					
5-yr Runoff Volume (P1 = 1.5 in.) =	1.048	acre-feet					
10-yr Runoff Volume (P1 = 1.75 in.) =	1.248	acre-feet					
25-yr Runoff Volume (P1 = 2 in.) =	1.513	acre-feet					
50-yr Runoff Volume (P1 = 2.25 in.) =	1.774	acre-feet					
100-yr Runoff Volume (P1 = 2.52 in.) =	2.092	acre-feet					
500-yr Runoff Volume (P1 = 3.68 in.) =	3.418	acre-feet					
Approximate 2-yr Detention Volume =	0.711	acre-feet					
Approximate 5-yr Detention Volume =	0.930	acre-feet					
Approximate 10-yr Detention Volume =	1.122	acre-feet					
Approximate 25-yr Detention Volume =	1.352	acre-feet					
Approximate 50-yr Detention Volume =	1.491	acre-feet					
Approximate 100-yr Detention Volume =	1.638	acre-feet					

	acre-reet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.68	inches

Define Zones and Basin Geometry

Jefine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.289	acre-fee
Select Zone 2 Storage Volume (Optional) =		acre-fee
Select Zone 3 Storage Volume (Optional) =		acre-fee
Total Detention Basin Volume =	0.289	acre-fee
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

tasin Length-to-Width Ratio (R _{L/W}) =	user	
Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (LFLOOR) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft ²
Volume of Basin Floor (VELOOP) =	user	ft ³

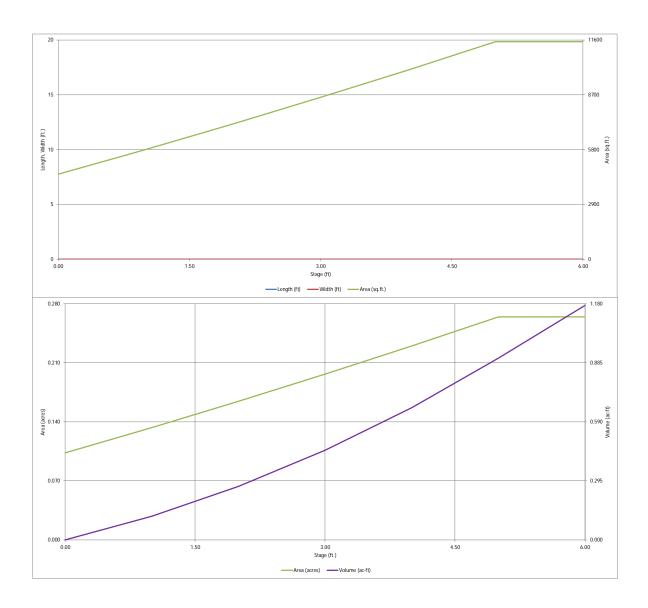
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =		ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L _{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft 2
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-fe

feet	
feet	Total detention
feet	volume is less than
feet	100-year volume.

YEAR PICE			1.							
FICE	Depth Increment =		ft Optional				Optional			
ention Pond)	Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
	Top of Micropool		0.00	-			4,501	0.103		
	6943		1.00				5,796	0.133	5,148	0.118
	6944		2.00				7,155	0.164	11,624	0.267
	6945		3.00				8,560	0.197	19,481	0.447
	6946		4.00				10,011	0.230	28,767	0.660
	6947		5.00				11,524	0.265	39,534	0.908
	6948		6.00				11,524	0.265	51,058	1.172
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Optional User Overrides										ļ
acre-feet										H
acre-feet 1.19 inches										H
1.19 Inches										-
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2.25 inches										
2.52 inches										
3.68 inches										
										
										
										
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Total detention										<u> </u>
volume is less than 100-year volume.										
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2/9/2021, 12:43 PM

CLH17 WQCV North_Detention_v4 03.xlsm, Basin



CLH17 WQCV North_Detention_v4 03.xlsm, Basin 2/9/2021, 12-43 PM

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: Falcon Meadows at Bent Grass
Basin ID: WQCV Pond - North

ZONE 2
ZONE 2
ZONE 2
ZONE 2
ORIFICE

Example Zone Configuration (Retention Pond)

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = If (distance below the filtration media surface) inches Underdrain Orifice Area = Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 1.94 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 9.00 inches

Orifice Plate: Orifice Area per Row = 1.92 sq. inches (diameter = 1-9/16 inches)

 $\frac{\text{3MP})}{\text{WQ Orifice Area per Row}} = \frac{\text{Calculated Parameters for Plate}}{1.332\text{E-02}} \text{ ft}^2$ $\text{Elliptical Half-Width} = \frac{\text{N/A}}{\text{Elliptical Slot Centroid}} = \frac{\text{N/A}}{\text{Elliptical Slot Area}} = \frac{\text{N/A}}{\text{Elliptical$

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.80	1.60					
Orifice Area (sq. inches)	1.92	1.92	1.92					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sg. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected		
Invert of Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	٧
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Verti
Vertical Orifice Diameter -			inches	

Vertical Orifice Area =
Vertical Orifice Centroid =

Calculated Parameters for Vertical Orifice

Not Selected Not Selected

ft²
feel

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)			Calculated Paramet	ers for Overflow W	eir	
	Not Selected	Not Selected		Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.50		ft (relative to basin bottom at Stage = 0 ft) $\frac{1}{2}$ Height of Grate Upper Edge, $\frac{1}{2}$	4.50		feet
Overflow Weir Front Edge Length =	6.00		feet Overflow Weir Slope Length =	3.00		feet
Overflow Weir Grate Slope =	0.00		H:V Grate Open Area / 100-yr Orifice Area =	7.13		
Horiz. Length of Weir Sides =	3.00		feet Overflow Grate Open Area w/o Debris =	12.60		ft ²
Overflow Grate Open Area % =	70%		%, grate open area/total area Overflow Grate Open Area w/ Debris =	6.30		ft ²
Overflow Grate Open Area % =	70%		%, grate open area/total area Overflow Grate Open Area w/ Debris =	6.30		ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Not Selected	Not Selected	
Depth to Invert of Outlet Pipe =	2.50		ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	18.00		inches

50%

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate						
	Not Selected	Not Selected				
Outlet Orifice Area =	1.77		ft ²			
Outlet Orifice Centroid =	0.75		feet			

N/A

N/A

radians

<u>User Input: Emergency Spillway (Rectangular or Trapezoidal)</u>

Debris Clogging % =

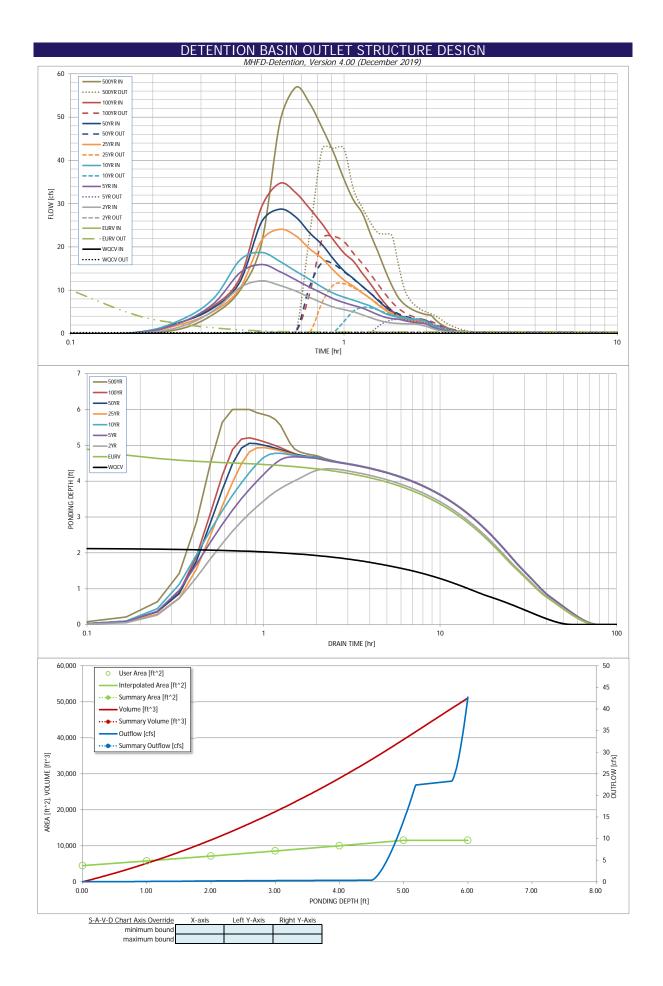
Spillway Invert Stage=	5.75	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	50.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	0.00	feet

	Calculated Parame	ters for Spillway
Spillway Design Flow Depth=	0.37	feet
Stage at Top of Freeboard =	6.12	feet
Basin Area at Top of Freeboard =	0.26	acres
sin Volume at Top of Freeboard =	1.17	acre-ft

Half-Central Angle of Restrictor Plate on Pipe =

Bas

Routed Hydrograph Results	The user can over	ride the default CUH	IP hydrographs and	runoff volumes by	entering new value	es in the Inflow Hyd	rographs table (Colu	umns W through Al	-).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.68
CUHP Runoff Volume (acre-ft) =	0.289	1.093	0.798	1.048	1.248	1.513	1.774	2.092	3.418
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.798	1.048	1.248	1.513	1.774	2.092	3.418
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.2	0.3	2.3	4.6	7.6	19.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.17	0.33	0.54	1.40
Peak Inflow Q (cfs) =	N/A	N/A	12.2	16.0	18.7	24.1	28.7	34.7	56.9
Peak Outflow Q (cfs) =	0.2	22.8	0.4	3.3	6.0	11.5	16.4	22.4	42.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	18.3	24.1	5.0	3.5	3.0	2.2
Structure Controlling Flow =	Plate	Outlet Plate 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	N/A
Max Velocity through Grate 1 (fps) =	N/A	1.81	N/A	0.2	0.5	0.9	1.3	1.7	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	45	56	58	57	55	53	51	48	40
Time to Drain 99% of Inflow Volume (hours) =	50	65	67	66	65	64	63	61	56
Maximum Ponding Depth (ft) =	2.14	5.71	4.34	4.68	4.78	4.93	5.05	5.21	6.00
Area at Maximum Ponding Depth (acres) =	0.17	0.26	0.24	0.25	0.26	0.26	0.26	0.26	0.26
Maximum Volume Stored (acre-ft) =	0.290	1.095	0.741	0.822	0.848	0.889	0.921	0.960	1.172



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	COURCE									CLILID
- · · ·	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]		500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.17	0.02	1.01
	0:15:00 0:20:00	0.00	0.00	1.50 5.29	2.44 6.91	3.03	2.03 5.12	2.53 5.96	2.48	4.48 10.00
	0:25:00	0.00	0.00	10.64	14.07	8.12 16.97	10.53	12.01	6.40 12.91	20.90
	0:30:00	0.00	0.00	12.18	15.95	18.74	21.53	25.83	29.30	48.97
	0:35:00	0.00	0.00	11.09	14.29	16.64	24.08	28.74	34.73	56.89
	0:40:00	0.00	0.00	9.81	12.39	14.38	22.55	26.89	32.49	53.12
	0:45:00	0.00	0.00	8.34	10.69	12.49	19.55	23.23	28.86	47.44
	0:50:00	0.00	0.00	7.09	9.29	10.70	17.30	20.48	25.25	41.77
	0:55:00	0.00	0.00	6.13	8.01	9.29	14.58	17.16	21.56	35.66
	1:00:00 1:05:00	0.00	0.00	5.51 5.03	7.16 6.51	8.40 7.70	12.38 10.91	14.47 12.71	18.60 16.68	30.85 27.81
	1:10:00	0.00	0.00	4.33	5.89	7.02	9.41	10.91	13.93	23.01
	1:15:00	0.00	0.00	3.67	5.12	6.33	8.07	9.32	11.49	18.79
	1:20:00	0.00	0.00	3.09	4.34	5.47	6.64	7.63	9.00	14.56
	1:25:00	0.00	0.00	2.67	3.77	4.60	5.43	6.19	6.90	11.00
	1:30:00	0.00	0.00	2.45	3.47	4.09	4.34	4.92	5.28	8.31
	1:35:00	0.00	0.00	2.34	3.31	3.78	3.70	4.18	4.34	6.75
	1:40:00 1:45:00	0.00	0.00	2.27	2.98	3.56 3.39	3.31	3.73 3.44	3.79 3.41	5.81 5.15
	1:50:00	0.00	0.00	2.23	2.72	3.39	2.87	3.44	3.41	4.71
	1:55:00	0.00	0.00	1.93	2.39	3.12	2.76	3.10	2.97	4.39
	2:00:00	0.00	0.00	1.70	2.22	2.84	2.67	3.00	2.85	4.17
	2:05:00	0.00	0.00	1.28	1.67	2.14	2.02	2.27	2.13	3.11
	2:10:00	0.00	0.00	0.95	1.23	1.56	1.47	1.66	1.56	2.27
	2:15:00	0.00	0.00	0.69	0.90	1.14	1.08	1.21	1.14	1.66
	2:20:00 2:25:00	0.00	0.00	0.50	0.65 0.45	0.82	0.78 0.56	0.88	0.84	1.22 0.86
	2:30:00	0.00	0.00	0.25	0.43	0.41	0.39	0.44	0.42	0.61
	2:35:00	0.00	0.00	0.17	0.22	0.29	0.28	0.31	0.30	0.43
	2:40:00	0.00	0.00	0.10	0.14	0.18	0.18	0.20	0.19	0.28
	2:45:00	0.00	0.00	0.05	0.08	0.10	0.11	0.12	0.11	0.16
	2:50:00	0.00	0.00	0.02	0.04	0.05	0.05	0.06	0.05	0.08
	2:55:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.02	0.02
	3:00:00 3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00 3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

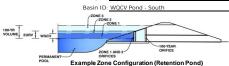
MHFD-Detention, Version 4.03 (May 2020)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of al outlets (e.g. vertical orifice,
							overflow grate and spillway
							overflow grate, and spillway where applicable).
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	67.81	acres
Watershed Length =	3,600	ft
Watershed Length to Centroid =	1,500	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	31.10%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.875	acre-feet
Excess Urban Runoff Volume (EURV) =	2.129	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.505	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	2.066	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.534	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	3.682	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	4.754	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	6.187	acre-feet
500-yr Runoff Volume (P1 = 3.68 in.) =	12.228	acre-feet
Approximate 2-yr Detention Volume =	1.341	acre-feet
Approximate 5-yr Detention Volume =	1.787	acre-feet
Approximate 10-yr Detention Volume =	2.230	acre-feet
Approximate 25-yr Detention Volume =	2.811	acre-feet
Approximate 50-yr Detention Volume =	3.239	acre-feet
Approximate 100-yr Detention Volume =	3.920	acre-feet

De

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.875	acre-feet
Select Zone 2 Storage Volume (Optional) =		acre-fee
Select Zone 3 Storage Volume (Optional) =		acre-fee
Total Detention Basin Volume =	0.875	acre-fee
Initial Surcharge Volume (ISV) =	user	ft 3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{LAV}) =	user	

Initial Surcharge Area (A_{ISV}) = user

Surcharge Volume Length (L_{ISV}) = user Surcharge Volume Width (W_{ISV}) = Depth of Basin Floor (H_{FLOOR}) = user Length of Basin Floor (L_{FLOOR}) = user Width of Basin Floor (W_{FLOOR}) =
Area of Basin Floor (A_{FLOOR}) = user Volume of Basin Floor (V_{FLOOR}) = user Depth of Main Basin (H_{MAIN}) = Length of Main Basin (L_{MAIN}) = user Width of Main Basin (W_{MAIN}) = Area of Main Basin (A_{MAIN}) = Volume of Main Basin (V_{MAIN}) = user user Calculated Total Basin Volume (Vtotal) = user

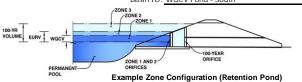
Total detention
volume is less than
100-year volume.

1.19 inches 1.50 inches 1.75 inches 2.00 inches 2.25 inches 2.52 inches 3.68 inches

\rightarrow	ı		1							
	Depth Increment =	1.00	ft Optional				Optional		I	
)	Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
	Description	(ft)	Stage (ft) 0.00	(ft)	(ft)	(ft ²)	Area (ft 2) 56	(acre) 0.001	(ft 3)	(ac-ft)
	Top of Micropool								0.047	0.047
	6924 6925		0.33				12,476 18,677	0.286	2,067 17,643	0.047
	6926		2.33				23,065	0.429	38,514	0.405
	6927		3.33				27,922	0.529	64,008	1.469
	6928		4.33				33,784	0.776	94,861	2.178
	6929		5.33				40,499	0.930	132,002	3.030
er Overrides		-		-	-	-				
acre-feet		-		-						
acre-feet										
inches										
inches										
inches										
inches										
inches										
inches										
						-				
ntion less than										
volume.										
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		-								
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		-		-						
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		-		1	-	1				
		-		1	1	-				
		1 1		1	1	-				

2/9/2021, 12:41 PM

CLH17 WQCV South_Detention_v4 03.xlsm, Basin



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.32	0.875	Orifice Plate
Zone 2			
Zone 3			
	Total (all zones)	0.875	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter : inches

alculated Parameters for Underdrain Underdrain Orifice Area Underdrain Orifice Centroid

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 9.00 inches Orifice Plate: Orifice Area per Row 5.00 sq. inches (use rectangular openings)

WQ Orifice Area per Row 3.472F-02 Elliptical Half-Width N/A Elliptical Slot Centroid N/A feet Elliptical Slot Area N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.80	1.60					
Orifice Area (sq. inches)	5.00	5.00	5.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sg. inches)								

Vertical Orifice Width =

USEL HIDUL. VELLICAL OFFICE (CITCUIAL OF RECLANGE	lidi)				U
	Not Selected	Not Selected			
Invert of Vertical Orifice =	2.32		ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	
Depth at top of Zone using Vertical Orifice =	4.27		ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	
Vertical Orifice Diameter or Height =	2.00		inches	_	

inches

	Calculated Parame	ters for Vertical Ori	fice
	Not Selected	Not Selected	
ea =	0.06		ft ²
oid =	0.08		fee

Calculated Parameters for Overflow Weir

Calculated Parameters for Plate

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

4.00

	Not Selected	Not Selected				Not Selected	Not Selected]
Overflow Weir Front Edge Height, Ho =	2.50		ft (relative to basin bottom at Stage =	0 ft)	Height of Grate Upper Edge, $H_t =$	2.50		feet
Overflow Weir Front Edge Length =	6.00		feet		Overflow Weir Slope Length =	3.00		feet
Overflow Weir Grate Slope =	0.00		H:V	Grate C	Open Area / 100-yr Orifice Area =	2.57		
Horiz. Length of Weir Sides =	3.00		feet	Overflo	ow Grate Open Area w/o Debris =	12.60		ft ²
Overflow Grate Open Area % =	70%		%, grate open area/total area	Overfl	low Grate Open Area w/ Debris =	6.30		ft ²
Debris Clogging % =	50%		%					-

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Not Selected	Not Selected			Not Selected	Not Selected	
Depth to Invert of Outlet Pipe =	2.50		ft (distance below basin bottom at Stage = 0 ft) Outlet O	rifice Area =	4.91		ft ²
Circular Orifice Diameter =	30.00		inches Outlet Orific	e Centroid =	1.25		feet
			Half-Central Angle of Restrictor Pla	te on Pipe =	N/A	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

4.33	ft (relative to basin bottom at Stage = 0 ft)
20.00	feet
4.00	H:V
0.00	feet
	20.00

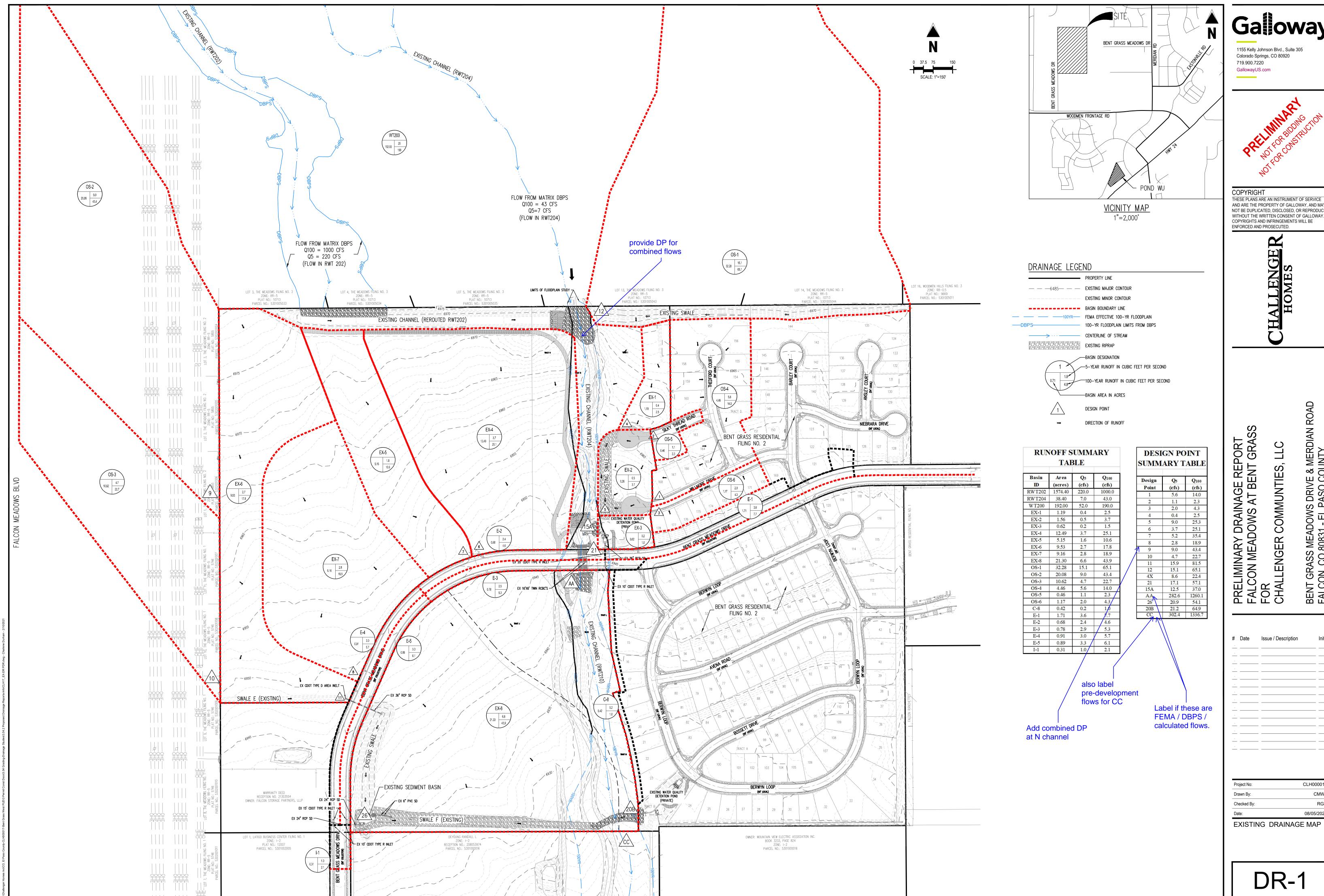
	Calculated Parame	ters for Spillwa
Spillway Design Flow Depth=	1.00	feet
Stage at Top of Freeboard =	5.33	feet
Basin Area at Top of Freeboard =	0.93	acres
Basin Volume at Top of Freeboard =	3.03	acre-ft

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Routed Hydrograph Results	The user can over	rride the default CUI	HP hydrographs and	runoff volumes by	entering new value	es in the Inflow Hyd	drographs table (Co	lumns W through A	F).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.68
CUHP Runoff Volume (acre-ft) =	0.875	2.129	1.505	2.066	2.534	3.682	4.754	6.187	12.228
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.505	2.066	2.534	3.682	4.754	6.187	12.228
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.4	0.8	1.1	10.1	20.3	33.7	87.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.30	0.50	1.30
Peak Inflow Q (cfs) =	N/A	N/A	14.2	19.8	24.5	40.0	53.5	70.5	139.1
Peak Outflow Q (cfs) =	0.6	46.3	5.0	9.6	13.8	27.0	36.9	47.1	118.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	12.3	12.6	2.7	1.8	1.4	1.3
Structure Controlling Flow =	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	3.82	0.32	0.7	1.0	2.1	2.8	3.6	4.7
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	40	39	43	42	40	36	33	30	20
Time to Drain 99% of Inflow Volume (hours) =	43	45	48	47	46	45	43	42	35
Maximum Ponding Depth (ft) =	2.32	4.27	2.72	2.87	2.98	3.27	3.57	4.11	5.23
Area at Maximum Ponding Depth (acres) =	0.53	0.77	0.57	0.59	0.60	0.63	0.67	0.75	0.91
Maximum Volume Stored (acre-ft) =	0.879	2.131	1.099	1.180	1.246	1.431	1.620	2.010	2.929

grate velocity is dangerous - larger box size is recommended

APPENDIX D Drainage Maps

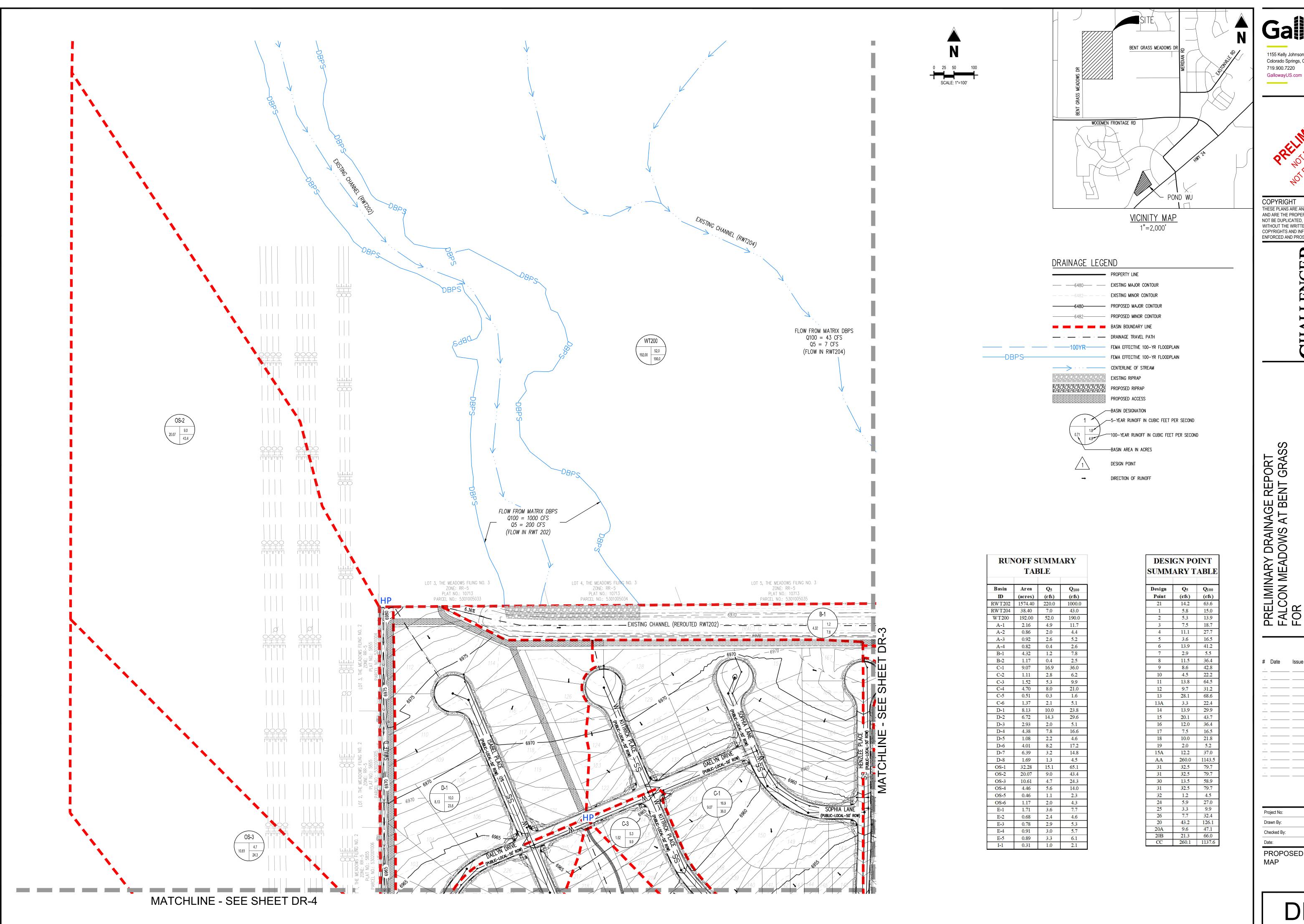


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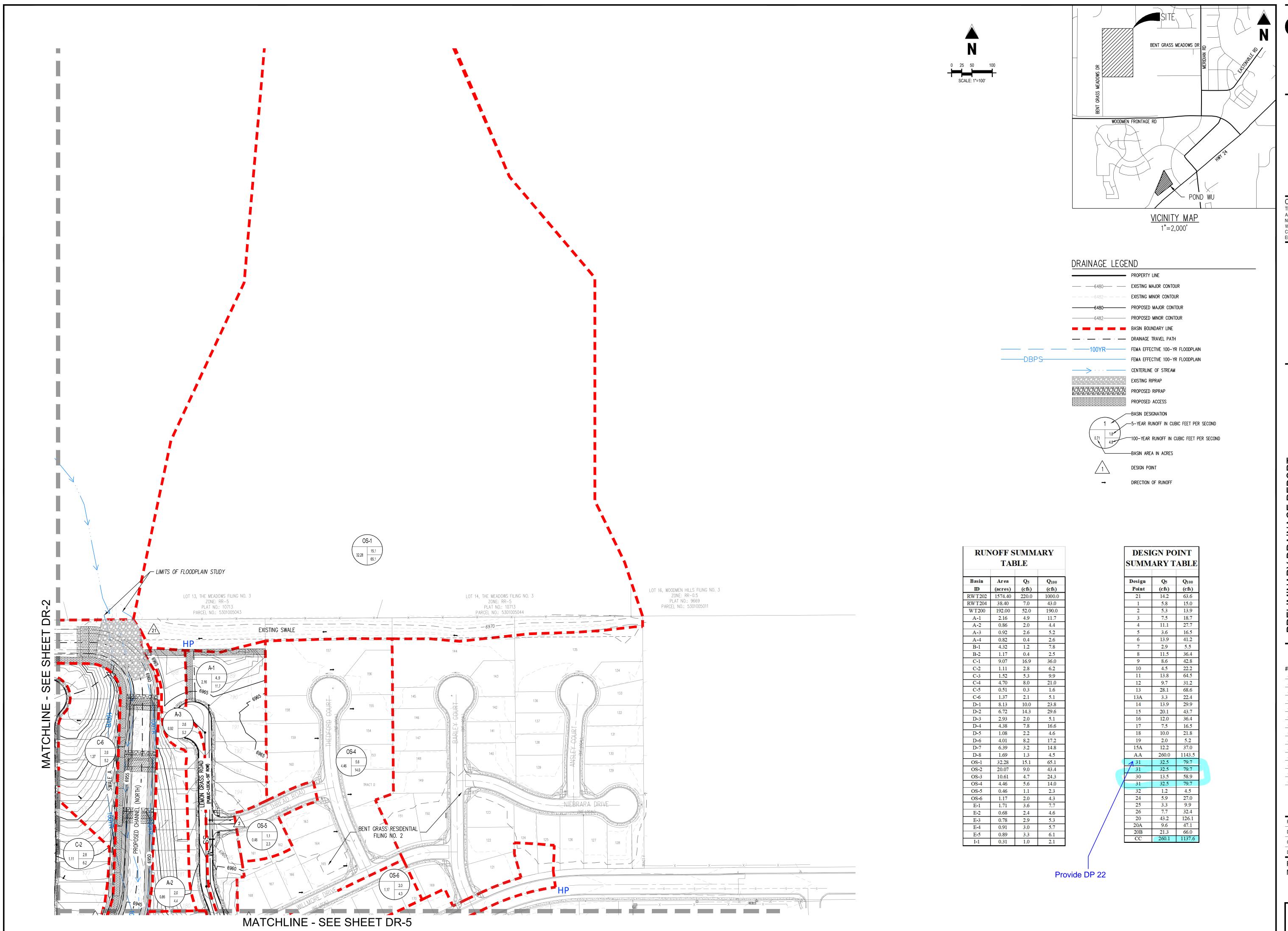
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PRELIMINARY DRAINAGE REF FALCON MEADOWS AT BENT FOR CHALLENGER COMMUNTIES,

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PROPOSED DRAINAGE

DR-2



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CHALLENGE R HOMES

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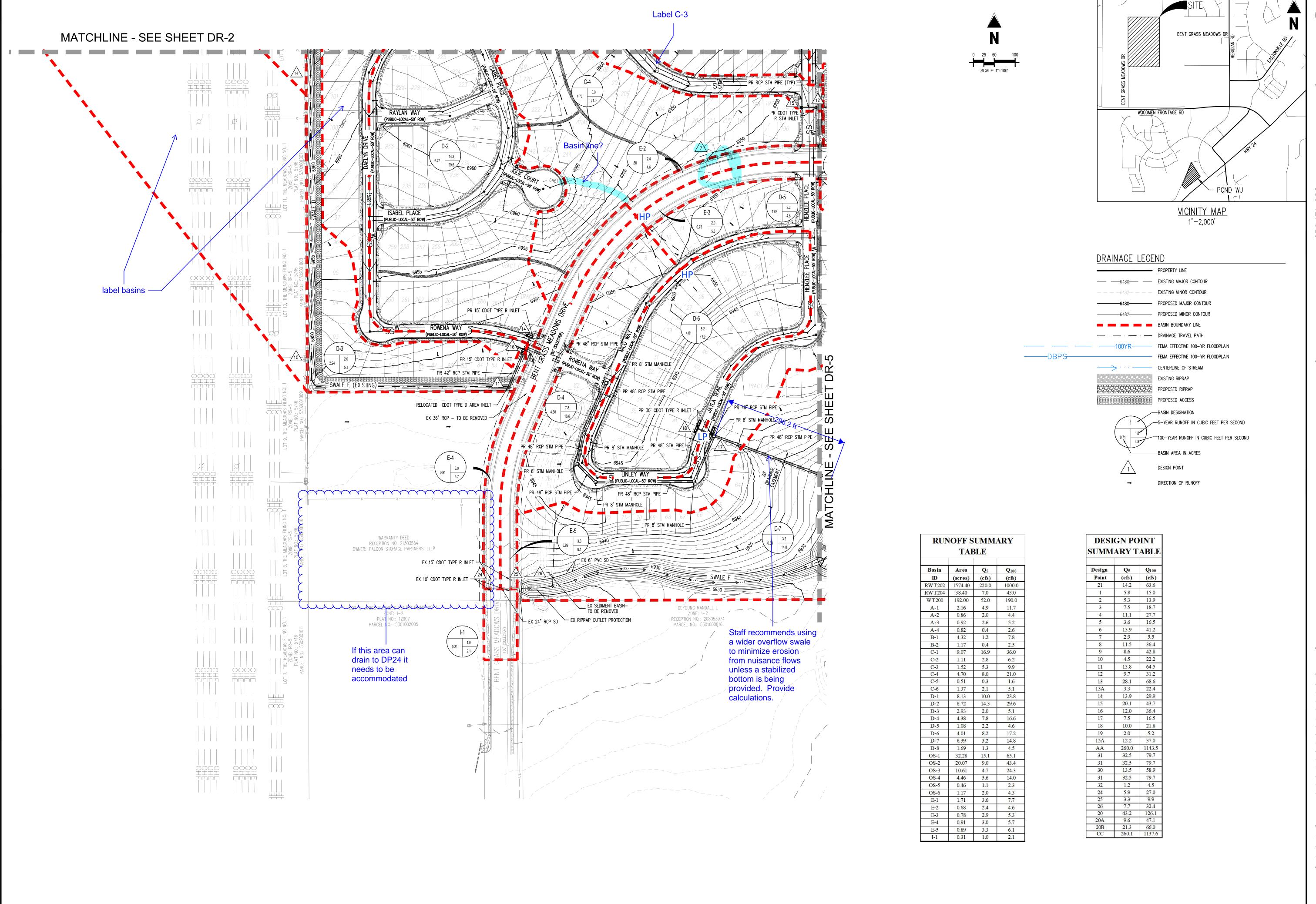
 Drawn By:
 CMWJ

 Checked By:
 RGD

 Date:
 08/05/2020

PROPOSED DRAINAGE MAP

DR-3



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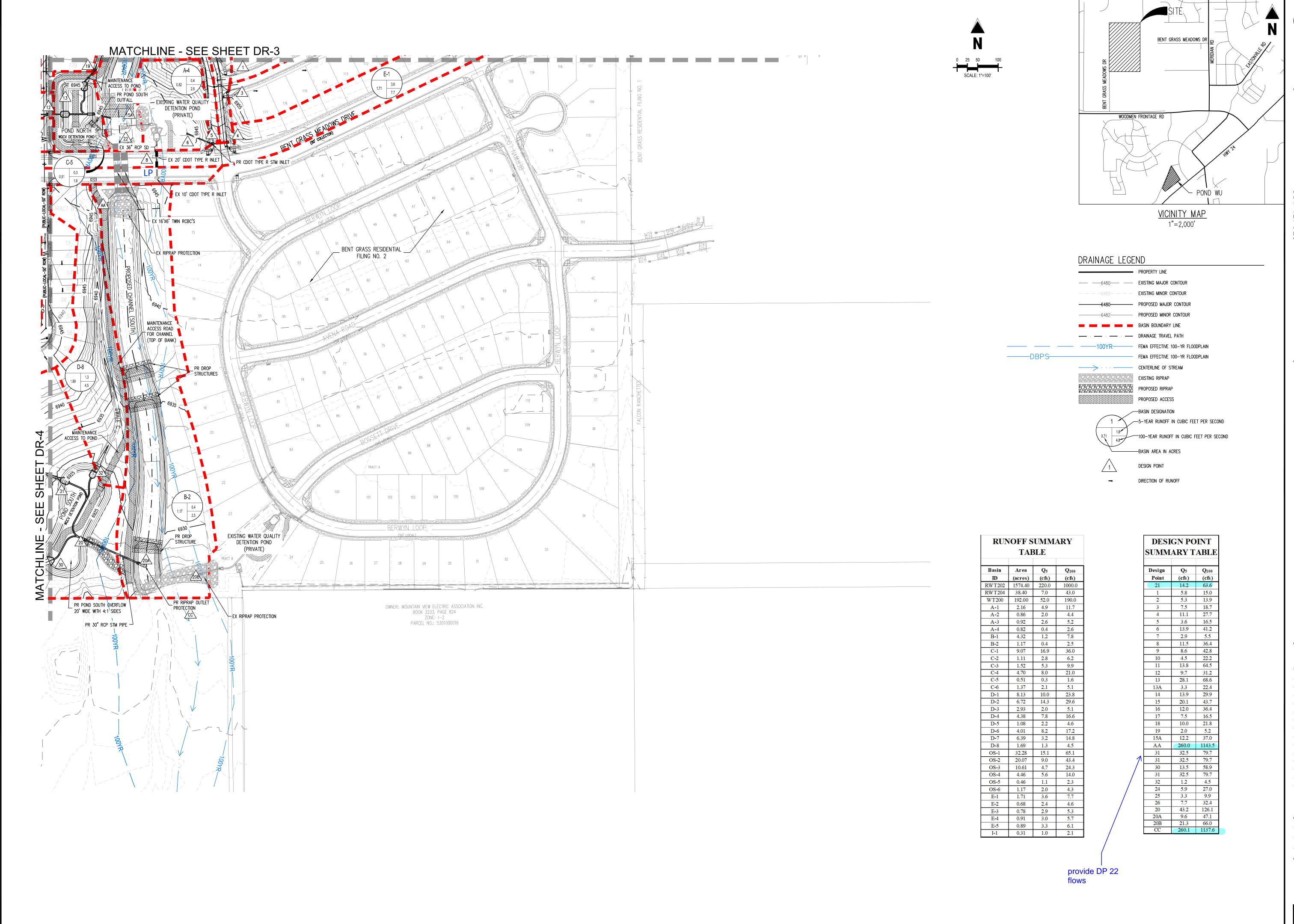
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PRELIMINARY DRAINAGE REF FALCON MEADOWS AT BENT FOR CHALLENGER COMMUNTIES,

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PROPOSED DRAINAGE MAP



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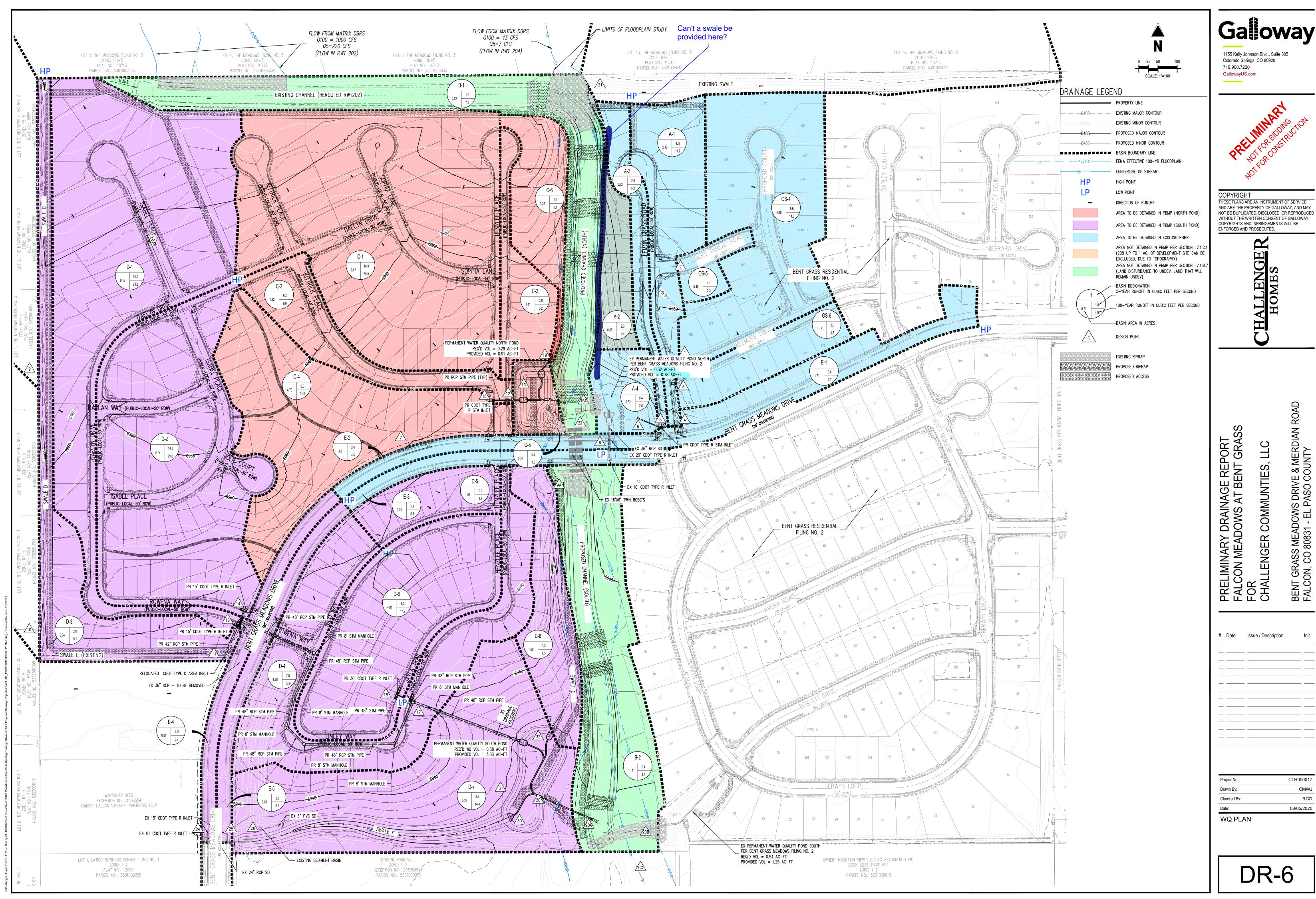
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CLH000017 Project No: CMWJ Checked By: RGD 08/05/2020

PROPOSED DRAINAGE MAP

DR-5



CLH000017 RGD