# Preliminary Drainage Report 

> for

The Shire at Old Ranch<br>PPR2410

Prepared for KESS Properties
February 27, 2024
by
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Manitou Springs, CO 80829

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Verify with the state that they will allow holding the majority of the stormwater onsite. Water rights may be an issue with this approach.

Please submit correspondence from the state that allows the proposed storing/pumping of water.

## INTRODUCTION

This drainage report and it's proposed drainage solutions are unconventional versus typical developments. The owners have set intentions for the project that include best practices in water use and management. This drainage report and proposed strategies seek to treat storm water as an asset and intend to have as little stormwater leave the property as possible and prefer infiltrating. Our drainage strategies align with agricultural engineering more so than conventional civil engineering.

Our strategies focus on collecting stormwater from small basins that are adjacent to dedicated infiltration ponds. As such, conveyance needs are minimized and numerous vegetation lined ponds are proposed.

We've discussed our strategies for stormwater infiltration with our water attorney who indicates that pumping 'stored' water to other points on the property would certainly be considered as 'extracting a beneficial use' and would be considered contrary to Colorado water law. However, crops or commercial vegetation that gets 'watered' collaterally would not be a violation. Plantings in and around ponds would be helpful for erosion control and likely increase soil infiltration rates.

## Design Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.
[Name, P.E. \# ]Date

## Owner/Developer's Statement:

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.
[Name, Title]
[Business Name]
[Address]

## Date

| provide <br> the <br> County <br> standard <br> signature <br> block |
| :--- |

## El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer, P.E.

Date
County Engineer / ECM Administrator

## I PROJECT OVERVIEW

The Shire at Old Ranch is private development by the long time owners with the intent to create an educational and commercial experience focusing on gardening, health and wellness, and community. The project will include a garden center, cafe, meeting house, hand-craft workshops and agricultural endeavors including small animals and classes. The bulk of the land will be used for growing nursery and food crops.

## II. GENERAL LOCATION

The project is located east of the intersection of Powers Blvd and Old Ranch Road. It is bounded by Old Ranch Rd to the south, Howells Rd to the west, Ridgeway Ln. to the north and adjacent properties to the east.

Township12S Range 66W SW4SW4 Sec 23 El Paso County, Colorado
These parcels are at the very southwest corner of the Black Forest and located within the Kettle Creek Drainage Basin. Most of the land to the north and east of the Shire has not been developed beyond large-lot residential uses.

There are no drainageways on our property and there are no indications of anything other than sheet flow entering or leaving the property. The North Fork at Briargate to the west of this property has built three detention ponds. $\longleftarrow$ include more discussion of flows Surrounding Platted Developments include: entering the site and locations

1. Several small platted properties to the east
2. Academy High School Filing No. 5 and North Fork at Briargate Filing No. 6 to the west
3. Several Cordera Filings to the south
4. There aren't any new plattings filed to the north.
III.

## DESCRIPTION OF PROPERTY

The project is comprised of four contiguous 5 acre parcels, these parcels are at the very southwest corner of the Black Forest.:

3820 Old Ranch Rd \#6226000061
3890 Old Ranch Rd. \#6226000060
10655 Howells Rd. \#6226000059
10755 Howells Rd. \#6226000058
Each of the four properties has a single family residence with wells and individual septic systems. The land hasn't been reshaped over the years and has natural grasses, small trees and shrubs throughout. The land slopes generally to the west at $2-5 \%$. There are three sub-drainages within the 20 acres that flow to the northwest, west and south. The property is bound by Ridgeway Ln to the north, Howells Rd. to the west and Old Ranch Rd. to the south respectively.

The existing vegetation consists of trees (Blue Spruce, Sib Elm, Scrub Oak, Ponderosa, Black Locust...),

$$
\begin{aligned}
& \text { Will these septic systems still be used with the proposed site } \\
& \text { design? For separation requirements from septic systems } \\
& \text { and permanent water quality facilities, see ECM section I.7.6 } \\
& \text { and Colorado's Rules and Regulations for Water Well } \\
& \text { Construction, Pump Installation, and Monitoring and } \\
& \text { Observation Hole/Well Construction. }
\end{aligned}
$$

Shrubs (Juniper, Choke Cherry, Goji, Elderberry, American Plum, Sib. Pea, Currants, Goose Cherry...), all of which will be kept.


Based on geotechnical explorations that have been done, the soils beneath a few inches of top soil are fairly consistent fine sands, SW, SM. Sandstone was hit at 13 ' in just one test hole in the upper reach (east side). All other test bores showed sand/silt down to 20' maximum test depth. Percolation tests have found the soil capable of infiltrating water at 1.18 to 1.67 inches/hour.

USDA identifies this soils as sandy loam with some sand-clay loam (Peyton-Pring). The soil has a hydrologic Group B classification and a capacity of the most limiting layer to be 2.0-6.0 inches/hour. Areas to the east and north have similar soil (Group B) and slopes.

There are no drainageways or structures on the property and there is no sign that anything other than sheet flow may have ever entered the property along the east side or flowed off this property. There are no irrigation systems presently however the project will employ high efficiency irrigation methods when built. The only utilities within the property are those serving the existing residences.

## IV. MAJOR BASIN DESCRIPTION

The property is within the area studied by JR Engineering in April 2001 for the Kettle Creek Drainage Basin-Old Ranch Road Tributary Drainage Basin Planning Study and Master Development Plan. This in the first study to to address the entire Kettle Creek Watershed. Our property is within this study area near Basin Identifiers D10 \& D12. The drainage management plan proposed in this study 'calls for the major land owners/developers in the study area to construct the drainage infrastructure required to support the proposed development within the study area' and 'calls for several regional detention facilities'. The study acknowledges that much of the Kettle Creek Watershed is within the city limits of Colorado Springs and they would have jurisdiction. Also, since the watershed flows to the US Air Force Academy property, the City required $2,5,10,25,50$ and 100 year storm events to be analyzed.

Most of the land to the north and east of the Shire has not been developed beyond large lot residential. The Kettle Creek and Old Ranch Road Drainage Basin Planning Studies address drainage for the larger area whereas the a Drainage Report for the new subdivision (North Fork at Briargate Fil 2) is the nearest and most recent drainage study, albeit down stream from our project. Include project number for reference
The property is not within a designated floodplain and FEMA classifies our property as "Area of Minimal Flood Hazard" $\longleftarrow \quad$ Include FIRM grid number
V. SUB-BASIN DESCRIPTION

Historic drainage patterns within the property generally flow to the west. Three sub-basins have been identified: South, Middle and North for the pre-development analysis.


[^0]Analysis of the existing hydrologic conditions reveal a 10 year storm produces 1.27 Acre-Feet of runoff and 1.91 Acre-Feet for a 100 year storm. Flow rates are calculated for each sub-basin along with stormwater volume using the Rational Method. Hydrographs of these basins is found in the Appendix.


The Kettle Creek/ORR/DBPS used 2,5,10,25, 50 and 100 year storm events to be analyzed whereas our Not all of the proposed infiltration ponds appear to be accepting and treating disturbed areas since much of the site is undisturbed. Please clearly identify which VII. FOUR STEP Ponds are required to treat the disturbed areas. Discuss fourth step and applicability on site
Our runoff reduction methods will include : Limiting hardscape to heavy traffic areas, use of permeable pavers in most walkways, rooftop waters directed to ponds*, limited concrete curb and gutter (another hardscape), 'contour plowing' in crop areas, maintain many areas with dense vegetation.

Maintaining/stable drainageways will be simplified by employing ; numerous low volume, low velocity drainageways and allowing historic sheet flow to run directly to dedicated ponds. Some roof waters will be piped out most conveyances will be via small channels.

Our proposed WQCV would include all stormwaters infiltrated into the ground. We will be developing and implementing some unique 'best practices'.

* The term 'Rond' refers to infiltration ponds of various types and sizes, from vegetation lined pits scattered around, grass buffers and constructed basins.

The state must be contacted to verify the acceptability of infiltrating all stormwater.
For full infiltration BMPS, infiltration tests must show a field rate minimum of 2 times that required to drain the WQCV over 12 hours. If the percolation testing results indicate rates slower than 2 times what is required to drain the WQCV over 12 hours then an underdrain is required.

Design Storm for this report is the Rational Method and SCS Type II 24 hour storm for both 10 year and 100 year event. Hydrologic analysis was done using HYDROLOGY STUDIO v3.0.0.26 software. Rainfall data was downloaded from NOAA for Colorado Springs.

To size infiltration ponds, the Pond Design feature was utilized with the outflow volume reduced to 0.0001 cfs . This gives the required size of pond to capture $100 \%$ of a given storm flow entirely.

## IX. DRAINAGE FACILITY DESIGN CONCEPTS

A major objective of the project is to require the least amount of overlot grading and to maintain the historic drainage patterns. Our Drainage Strategies will reduce overall stormwater from flowing from the property. Using numerous mini-basins, basins will collect and infiltrate their waters $100 \%$ and some basins will allow a historic flow to continue. The net off-site flow will be reduced significantly.

The Plan view below shows enumerated surfaces and the general surface type in colors. Areas that will be runoff controlled will have their own pattern of runoff, conveyance and infiltration pond.


Most surface areas would utilize historic sheet flows directed to infiltration ponds (blue). Agricultural areas (green) would utilize strategies such as 'contour plowing'. Roofs are shown in orange color. White colored areas are paved surface (asphalt or gravel). Gray area around building groups is permeable
pavers. Purple areas are depressed gardens which would not contribute to runoff. please provide drainage analysis for any offsite improvements that are necessary. The previous traffic study done with the zoning application identified roadway improvements. These improvements shall be accounted for in your analysis. Coordinate with the developments traffic engineer for the recommended/required roadway improvements.

The spillways and their rundowns shall be contained within the property. Currently some ponds are shown at the property line. Shift the ponds as necessary and provide downstream analysis.

## E FACHITY DESIGN-DETAILS

a project guan is to mant water nuwny un property to volumes less than the historic, calculated volume.
Some of the identified mini-basins are easier to achieve that goak without significant disruption to existing landscaping and land use. Throughout the property variouscombinations of strategies for reducing run-off will be used.

All ponds should have an emergency
spillway designed for large storm events so that if the water overtops the ponds are intentionally designed to minimize downstream impacts and erosion.

1. Minimize grading
2. Use heavy vegetation and contour plowing to achieve lower run-of
3. Employ planters and gardens in small depressions to collect and infiltrate on the spot
4. Require the least curb and gutter
5. Maximize sheet flow directly into dedicated infiltration ponds

Different pond styles will be employed, both sloped side basins and some vertical wall ponds to conserve space. Details of the Pond Types is found in the Appendix.

Where curb and gutter is necessary, Owners wish to pursue a less carbon intensive manner as shown below. Uphill edges of roadways and parking would have no curb. Wheel stops would be used in parking areas. The 'barrier' noted in the diagram could be notched to allow water to spill over barrier and through the Gabion basket and then surface flow to it's dedicated pond. A similar detail could be used on the uphill side to route waters to a strategic road crossing.


Our drainage strategies will not adversely affect streets and utilities. Many intentions for the project will result in positive environmental elements that will enhance the visitor experience at the Shire. Since we will infiltrate rather than discharge to other drainage systems, we expect to have a very positive affect on downstream drainage systems.

Our drainage strategies involve numerous small collection and infiltration ponds which take advantage of the existing terrain with limited over-lot grading. The property has been broken into mini-basins that take advantage of proposed roadways, buildings and suffaces to allow waters to flow in small volumes to adjacent ponds. All surfaces have been colored and humbered.

## CALCULATION METHODS

For both the pre and post development runoff analysi\&, the contributing surfaces and their coefficient of runoff, slope and time of concentration were calculated.

Coefficients of Runoff used are as follows

| Undeveloped Land, Future Agricultural areas | 0.2 |
| :--- | :--- |
| Asphalt Roads and Parking spaces | 0.95 |
| Gravel Roads and Parking spaces, Pavers | 0.85 |
| Roofs | 0.95 |
| Ponds them selves, assumed full | 1.00 |

The Time of Concentration was typically quite long for pre-development flows and was adjusted for post development flows to find the surface that had the least and longest Tc. In some case's, if an Ag and Paved surface dominated the basin, Tc's for both surfaces were determined to find the largest flow (in cubic feet per second, cfs) to assess channel requirements.

## FREE FLOWING AREAS

Provide all calculations used in developing the analysis. Only the outputs have been provided in the tables below.
Some areas were found not to be good candidates for managing stormwater, usually areas at the bottom of the basins or areas with heavy vegetation. These areas are on the south and west sides of the property. Runoff from these areas was calculated for the 10 and 100 year storms to find there rate of flow and total runoff that would be discharged.

This is a summary of those areas which will be allowed to flow off site. Waters from these areas would tend to accumulate in borrow ditches along Old Ranch and Howells Roads. There no indications that anything other than sheet flow has ever occurred in off-site flows.

Include flows at
Basin 72, west side @ 10755 Howells Rd. these locations
Area 20 \& 21, low end of entry driveway, west side
Basin 70 southwest corner, 3820 Old Ranch Rd.
Area 16, 66 \& 67, south entrance driveway, garden and 3890 Old Ranch Road



## PONDED BASINS

The bulk of the property has been broken into (20) mini-basins with infiltration ponds dedicated to the runoff in that basin. Ponds are placed where they can collect surface flows without channels as often as possible. Grassed Swales are employed when needed to convey waters.

The ponds are sized based on two parameters : the total volume required to collect storm waters, and the required infiltrative area to 'perc' storm waters into the ground within 40 hours. The width on a horizontal plane at the bottom of the pond was generally used as the 'infiltrative surface area'. The ponds will be maintained as they will also serves other productive purposes such as cash crops, walking paths, wildlife habitat, replanted vegetation and historic vegetation.

Final design and details for the ponds required to provide water quality and flood control shall be provided at this stage. minor changes due to grading the site may happen but generally would
A copy of the Percolation be similar to the final design.

The infiltration ponds are rectangular, oval and triangular and possible organic shapes, geperally with 3:1 side slopes. Drawings attached show their design.

The pond sizes in this report may vary as the infiltration rate may differ, and pond shape maychange as development proceeds, hence we will work with the owner during construction and offer final design afterward. Pond sizes will be larger than the L1 \& L2 specified in this report as a $6 "$ high freeboard is required on all ponds and channels. Owner may ask to use $2: 1$ side slopes with vegetation or riprap.

The next page describes the format of results of the hydrologic analysis and the results.
Following that are individual basin calculations and solutions, beginning with the pre-development hydrology and the basin that will be allowed to flow freely off site. The Appendix includes Percolation Tests and Pond concepts.

The pond sizes shown on subsequent pages are based on full water surface dimensions. A page showing constructed sizes is included at the end of this file and on drawing sheet DR-2. These dimensions include a 6" free board.

Also attached is the spreadsheet of the many surface areas used in the analysis.

The following is the Pre-Develoment Hydrology

Provide an existing map with elements outlined in DCM section 4.4.A. 2

Provide design points for storm runoff for each basin.

PRE DEVELOPMENT RUN OFF



Hydrograph 10-yr Summary
Hydrology Studio v 3.0.0.26
03-29-2023

| Hyd. <br> No. | Hydrograph Type | Hydrograph Name | Peak Flow (cfs) | Time to Peak (hrs) | Hydrograph Volume (cuft) | Inflow Hyd(s) | Maximum Elevation (ft) | Maximum Storage (cuft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | North SubBasin | 1.496 | 2.07 | 11,128 | ---- |  |  |
| 2 | Reach |  | 0.000 | 0.00 | 0.000 | 1 |  |  |
| 3 | Rational | Mid SubBasin | 3.036 | 2.22 | 24,226 | ---- |  |  |
| 4 | Reach |  | 0.000 | 0.00 | 0.000 | 3 |  |  |
| 5 | Rational | South SubBasin | 2.303 | 2.43 | 20,178 | ---- |  |  |
| 6 | Reach |  | 0.000 | 0.00 | 0.000 | 5 |  |  |
|  |  |  |  |  |  |  |  |  |

North SubBasin

| Hydrograph Type | $=$ Rational |
| :--- | :--- |
| Storm Frequency | $=10-\mathrm{yr}$ |
| Time Interval | $=1 \mathrm{~min}$ |
| Drainage Area | $=3.956$ ac |
| Tc Method | $=$ User |
| IDF Curve | $=$ Colorado Spasin area) |
| Freq. Corr. Factor | $=1.00$ |

Does not match table, revise (appears to be South basin area)

| * Composite C Worksheet |  |  |
| :--- | :--- | :--- |
| AREA (ac) | C | DESCRIPTION |
| 0.041 | 0.95 | Roof |
| 0.122 | 0.85 | Road |
| 3.793 | 0.20 | Land |
| 3.956 | $\mathbf{0 . 2 3}$ |  |

$0.23 \quad 0$.
$Q p=1.50 \mathrm{cfs}$


## Mid SubBasin

Hyd. No. 3


## South SubBasin

Hyd. No. 5
Does not match table,

| Hydrograph Type | $=$ Rational | _revise (appears to be | Peak Flow | $=2.303 \mathrm{cfs}$ |
| :--- | :--- | :--- | :--- | :--- |
| Storm Frequency | $=10-\mathrm{yr}$ | North basin area) | Time to Peak | $=2.43 \mathrm{hrs}$ |
| Time Interval | $=1 \mathrm{~min}$ |  | Runoff Volume | $=20,178 \mathrm{cuft}$ |
| Drainage Area | $=6.806 \mathrm{ac}$ | Runoff Coeff. | $=0.23^{*}$ |  |
| Tc Method | $=$ User | Time of Conc. (Tc) | $=146.0 \mathrm{~min}$ |  |
| IDF Curve | $=$ Colorado Springs.idf | Intensity | $=1.47 \mathrm{in} / \mathrm{hr}$ |  |
| Freq. Corr. Factor | $=1.00$ | Asc/Rec Limb Factors $=1 / 1$ |  |  |

* Composite C Worksheet

| AREA (ac) | C | DESCRIPTION |
| :--- | :--- | :--- |
| 0.129 | 0.95 | Roof |
| 0.133 | 0.85 | Road |
| 6.544 | 0.20 | Land |
| 6.806 | $\mathbf{0 . 2 3}$ |  |

$Q p=2.30 \mathrm{cfs}$


## Storm Distribution: NRCS/SCS - Type II, 24-hr

| Storm <br> Duration | Total Rainfall Volume (in) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1-yr | 2-yr | 3-yr | 5-yr | $\checkmark$ 10-yr | 25-yr | 50-yr | 100-yr |  |
| 24 hrs | 1.62 | 1.89 | 0.00 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |  |


| Incremental Rainfall Distribution, 10-yr |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time (hrs) | Precip <br> (in) | Time (hrs) | Precip (in) | Time (hrs) | Precip <br> (in) | Time (hrs) | Precip <br> (in) | Time (hrs) | Precip (in) |
| 11.42 | 0.005412 | 11.60 | 0.016404 | 11.78 | 0.042662 | 11.97 | 0.040178 | 12.15 | 0.008210 |
| 11.43 | 0.005490 | 11.62 | 0.018325 | 11.80 | 0.048005 | 11.98 | 0.028020 | 12.17 | 0.008025 |
| 11.45 | 0.005567 | 11.63 | 0.020245 | 11.82 | 0.053347 | 12.00 | 0.015861 | 12.18 | 0.007840 |
| 11.47 | 0.005645 | 11.65 | 0.022166 | 11.83 | 0.058690 | 12.02 | 0.010016 | 12.20 | 0.007655 |
| 11.48 | 0.005723 | 11.67 | 0.024087 | 11.85 | 0.064032 | 12.03 | 0.009505 | 12.22 | 0.007470 |
| 11.50 | 0.005801 | 11.68 | 0.026008 | 11.87 | 0.069375 | 12.05 | 0.009320 | 12.23 | 0.007285 |
| 11.52 | 0.006822 | 11.70 | 0.027928 | 11.88 | 0.074717 | 12.07 | 0.009135 | 12.25 | 0.007101 |
| 11.53 | 0.008721 | 11.72 | 0.029849 | 11.90 | 0.080060 | 12.08 | 0.008950 | 12.27 | 0.006916 |
| 11.55 | 0.010642 | 11.73 | 0.031770 | 11.92 | 0.085402 | 12.10 | 0.008765 | 12.28 | 0.006731 |
| 11.57 | 0.012563 | 11.75 | 0.033690 | 11.93 | 0.055846 | 12.12 | 0.008580 | 12.30 | 0.006546 |
| 11.58 | 0.014483 | 11.77 | 0.037037 | 11.95 | 0.052337 | 12.13 | 0.008395 | 12.32 | 0.006361 |





## Mid SubBasin

Hyd. No. 3


| South SubBasin | Does not match table, | Hyd. No. 5 |  |
| :---: | :---: | :---: | :---: |
| Hydrograph Type | = Rational | Peak Flow | $=3.461 \mathrm{cfs}$ |
| Storm Frequency | $=100-\mathrm{yr}$ | Time to Peak | $=2.43 \mathrm{hrs}$ |
| Time Interval | $=1 \mathrm{~min}$ | Runoff Volume | = 30,315 cuft |
| Drainage Area | $=6.806 \mathrm{ac}$ | Runoff Coeff. | $=0.23$ * |
| Tc Method | = User | Time of Conc. (Tc) | $=146.0 \mathrm{~min}$ |
| IDF Curve | = Colorado Springs.idf | Intensity | $=2.21 \mathrm{in} / \mathrm{hr}$ |
| Freq. Corr. Factor | $=1.00$ | Asc/Rec Limb Facto | = $1 / 1$ |


| Composite C Worksheet |  |  |
| :--- | :--- | :--- |
| AREA (ac) | C | DESCRIPTION |
| 0.129 | 0.95 | Roof |
| 0.133 | 0.85 | Road |
| 6.544 | 0.20 | Land |
| 6.806 | $\mathbf{0 . 2 3}$ |  |

$Q p=3.46 \mathrm{cfs}$


## Storm Distribution: NRCS/SCS - Type II, 24-hr

| Storm <br> Duration | Total Rainfall Volume (in) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | $\checkmark$ 100-yr |  |
| 24 hrs | 1.62 | 1.89 | 0.00 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |  |



| Equation Coefficients | Intensity = B / (Tc + D)^E (in/hr) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |  |
| B | 0.0000 | 58.1215 | 0.0000 | 57.1446 | 58.8780 | 63.5498 | 67.7965 | 72.2003 |  |
| D | 0.0000 | 10.3000 | 0.0000 | 10.3000 | 10.3000 | 10.4000 | 10.5000 | 10.6000 |  |
| E | 0.0000 | 0.8106 | 0.0000 | 0.7542 | 0.7303 | 0.7097 | 0.6986 | 0.6898 |  |

Minimum $T c=5$ minutes


Cf $=$ Correction Factor applied to Rational Method runoff coefficient.
Sample IDF Curves


Hydrology Studio v 3.0.0.26 (Rainfall totals in Inches)
03-29-2023

|  | Active | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Active |  |  |  |  |  | $\checkmark$ |  |  | $\checkmark$ |
| SCS Storms | > SCS Dimensionless Storms |  |  |  |  |  |  |  |  |
| SCS 6hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| Type I, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type IA, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type II, 24-hr | $\checkmark$ | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type II FL, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type III, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Synthetic Storms | > IDF-Based Synthetic Storms |  |  |  |  |  |  |  |  |
| 1-hr |  | 0 | 1.85 | 0 | 2.31 | 2.64 | 3.10 | 3.47 | 3.83 |
| 2-hr |  | 0 | 2.24 | 0 | 2.90 | 3.36 | 4.01 | 4.51 | 5.01 |
| 3-hr |  | 0 | 2.48 | 0 | 3.27 | 3.82 | 4.60 | 5.20 | 5.79 |
| 6-hr |  | 0 | 2.89 | 0 | 3.96 | 4.70 | 5.73 | 6.53 | 7.32 |
| 12-hr |  | 0 | 3.33 | 0 | 4.75 | 5.73 | 7.08 | 8.13 | 9.17 |
| 24-hr |  | 0 | 3.82 | 0 | 5.66 | 6.94 | 8.70 | 10.07 | 11.42 |
| Huff Distribution | > 1st Quartile (0 to 6 hrs ) |  |  |  |  |  |  |  |  |
| 1-hr |  | 0.79 | 0.93 | 0 | 1.20 | 1.45 | 1.83 | 2.16 | 2.53 |
| 2-hr |  | 0.97 | 1.13 | 0 | 1.44 | 1.74 | 2.23 | 2.65 | 3.12 |
| 3-hr |  | 1.07 | 1.23 | 0 | 1.55 | 1.88 | 2.42 | 2.91 | 3.46 |
| 6-hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| Huff Distribution | > 2nd Quartile (>6 to 12 hrs ) |  |  |  |  |  |  |  |  |
| 8-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12-hr |  | 1.42 | 1.64 | 0 | 2.07 | 2.51 | 3.24 | 3.90 | 4.64 |
| Huff Distribution | > 3rd Quartile (>12 to 24 hrs ) |  |  |  |  |  |  |  |  |
| 18-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Custom Storms | > Custom Storm Distributions |  |  |  |  |  |  |  |  |
| Colorado Springs |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 2 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 3 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 4 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 5 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 6 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 7 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 8 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 9 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 10 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



Hydrograph 10-yr Summary

| Hyd. <br> No. | Hydrograph Type | Hydrograph Name | Peak Flow (cfs) | Time to Peak (hrs) | Hydrograph Volume (cuft) | Inflow Hyd(s) | Maximum Elevation (ft) | Maximum Storage (cuft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 0.691 | 1.43 | 3,567 | ---- |  |  |
| 2 | Rational | Post | 0.377 | 1.43 | 1,944 | ---- |  |  |
| 3 | Pond Route | Post \#72 Runs Free | 0.000 | 0.00 | 0.000 | 2 | 101.58 | 4,458 |
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Hydrograph 100-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. | $\begin{aligned} & \text { Hydrograph } \\ & \text { Type } \end{aligned}$ | Hydrograph <br> Name |  |  | $\begin{aligned} & \text { Hydrograph } \\ & \text { Volume } \\ & \text { (cuft) } \end{aligned}$ | (intow | $\begin{array}{\|l\|l\|} \hline \text { Haximum } \\ \text { (everation } \end{array}$ | $\begin{aligned} & \text { maximum } \\ & \text { Suratage } \\ & \text { cout } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 1.017 | ${ }^{1.43}$ | 5,250 | $\cdots$ |  |  |
| 2 | Rational | Post | 0.555 | ${ }^{1.43}$ | 2.861 | -- |  |  |
| 3 | Pond foute | Postifl R funs fiee | 0.000 | 0.00 | 0.000 | 2 | 10208 | ${ }^{6.563}$ |
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| Equation Coefficients | Intensity = B / ( $C$ c + D)^E (in/hr) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |  |
| B | 0.0000 | 58.1215 | 0.0000 | 57.1446 | 58.8780 | 63.5498 | 67.7965 | 72.2003 |  |
| D | 0.0000 | 10.3000 | 0.0000 | 10.3000 | 10.3000 | 10.4000 | 10.5000 | 10.6000 |  |
| E | 0.0000 | 0.8106 | 0.0000 | 0.7542 | 0.7303 | 0.7097 | 0.6986 | 0.6898 |  |

Minimum $T c=5$ minutes


Cf $=$ Correction Factor applied to Rational Method runoff coefficient.
Sample IDF Curves


Hydrology Studio v 3.0.0.26 (Rainfall totals in Inches)

|  | Active | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Active |  |  |  |  |  | $\checkmark$ |  |  | $\checkmark$ |
| SCS Storms | > SCS Dimensionless Storms |  |  |  |  |  |  |  |  |
| SCS 6hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| Type I, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type IA, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type II, 24-hr | $\checkmark$ | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type II FL, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Type III, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Synthetic Storms | > IDF-Based Synthetic Storms |  |  |  |  |  |  |  |  |
| 1-hr |  | 0 | 1.85 | 0 | 2.31 | 2.64 | 3.10 | 3.47 | 3.83 |
| 2-hr |  | 0 | 2.24 | 0 | 2.90 | 3.36 | 4.01 | 4.51 | 5.01 |
| 3-hr |  | 0 | 2.48 | 0 | 3.27 | 3.82 | 4.60 | 5.20 | 5.79 |
| 6-hr |  | 0 | 2.89 | 0 | 3.96 | 4.70 | 5.73 | 6.53 | 7.32 |
| 12-hr |  | 0 | 3.33 | 0 | 4.75 | 5.73 | 7.08 | 8.13 | 9.17 |
| 24-hr |  | 0 | 3.82 | 0 | 5.66 | 6.94 | 8.70 | 10.07 | 11.42 |
| Huff Distribution | > 1st Quartile (0 to 6 hrs) |  |  |  |  |  |  |  |  |
| 1-hr |  | 0.79 | 0.93 | 0 | 1.20 | 1.45 | 1.83 | 2.16 | 2.53 |
| 2-hr |  | 0.97 | 1.13 | 0 | 1.44 | 1.74 | 2.23 | 2.65 | 3.12 |
| 3-hr |  | 1.07 | 1.23 | 0 | 1.55 | 1.88 | 2.42 | 2.91 | 3.46 |
| 6-hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| Huff Distribution | > 2nd Quartile (>6 to 12 hrs ) |  |  |  |  |  |  |  |  |
| 8-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12-hr |  | 1.42 | 1.64 | 0 | 2.07 | 2.51 | 3.24 | 3.90 | 4.64 |
| Huff Distribution | > 3rd Quartile (>12 to 24 hrs ) |  |  |  |  |  |  |  |  |
| 18-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Custom Storms | > Custom Storm Distributions |  |  |  |  |  |  |  |  |
| Colorado Springs |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 2 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 3 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 4 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 5 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 6 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 7 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 8 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 9 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| My Custom Storm 10 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

$\begin{array}{ll}\text { Rainfall totals in Inches } & \text { 03-27-2023 }\end{array}$

|  | Active | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Active |  |  |  |  |  | $\checkmark$ |  |  | $\checkmark$ |
| Huff Indiana | > Indianapolis |  |  |  |  |  |  |  |  |
| 30-min |  | 0.61 | 0.73 | 0 | 0.95 | 1.15 | 1.44 | 1.68 | 1.93 |
| 1-hr |  | 0.79 | 0.93 | 0 | 1.20 | 1.45 | 1.83 | 2.16 | 2.53 |
| 2-hr |  | 0.97 | 1.13 | 0 | 1.44 | 1.74 | 2.23 | 2.65 | 3.12 |
| 3-hr |  | 1.07 | 1.23 | 0 | 1.55 | 1.88 | 2.42 | 2.91 | 3.46 |
| 6-hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| 12-hr |  | 1.42 | 1.64 | 0 | 2.07 | 2.51 | 3.24 | 3.90 | 4.64 |
| 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Huff Indiana | > Evansville |  |  |  |  |  |  |  |  |
| 30-min |  | 0.61 | 0.73 | 0 | 0.95 | 1.15 | 1.44 | 1.68 | 1.93 |
| 1-hr |  | 0.79 | 0.93 | 0 | 1.20 | 1.45 | 1.83 | 2.16 | 2.53 |
| 2-hr |  | 0.97 | 1.13 | 0 | 1.44 | 1.74 | 2.23 | 2.65 | 3.12 |
| 3-hr |  | 1.07 | 1.23 | 0 | 1.55 | 1.88 | 2.42 | 2.91 | 3.46 |
| 6-hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| 12-hr |  | 1.42 | 1.64 | 0 | 2.07 | 2.51 | 3.24 | 3.90 | 4.64 |
| 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Huff Indiana | > Fort Wayne |  |  |  |  |  |  |  |  |
| 30-min |  | 0.61 | 0.73 | 0 | 0.95 | 1.15 | 1.44 | 1.68 | 1.93 |
| 1-hr |  | 0.79 | 0.93 | 0 | 1.20 | 1.45 | 1.83 | 2.16 | 2.53 |
| 2-hr |  | 0.97 | 1.13 | 0 | 1.44 | 1.74 | 2.23 | 2.65 | 3.12 |
| 3-hr |  | 1.07 | 1.23 | 0 | 1.55 | 1.88 | 2.42 | 2.91 | 3.46 |
| 6-hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| 12-hr |  | 1.42 | 1.64 | 0 | 2.07 | 2.51 | 3.24 | 3.90 | 4.64 |
| 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| Huff Indiana | > South Bend |  |  |  |  |  |  |  |  |
| 30-min |  | 0.61 | 0.73 | 0 | 0.95 | 1.15 | 1.44 | 1.68 | 1.93 |
| 1-hr |  | 0.79 | 0.93 | 0 | 1.20 | 1.45 | 1.83 | 2.16 | 2.53 |
| 2-hr |  | 0.97 | 1.13 | 0 | 1.44 | 1.74 | 2.23 | 2.65 | 3.12 |
| 3-hr |  | 1.07 | 1.23 | 0 | 1.55 | 1.88 | 2.42 | 2.91 | 3.46 |
| 6-hr |  | 1.25 | 1.41 | 0 | 1.77 | 2.15 | 2.79 | 3.38 | 4.05 |
| 12-hr |  | 1.42 | 1.64 | 0 | 2.07 | 2.51 | 3.24 | 3.90 | 4.64 |
| 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
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$\begin{array}{ll}\text { Rainfall totals in Inches } & \text { 03-27-2023 }\end{array}$

|  | Active | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Active |  |  |  |  |  | $\checkmark$ |  |  | $\checkmark$ |
| NRCS Storms | > NRCS Dimensionless Storms |  |  |  |  |  |  |  |  |
| NRCS MSE1, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCS MSE2, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCS MSE3, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCS MSE4, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCS MSE5, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCS MSE6, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NOAA-A, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NOAA-B, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NOAA-C, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NOAA-D, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCC-A, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCC-B, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCC-C, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| NRCC-D, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| CA-1, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| CA-2, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| CA-3, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| CA-4, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| CA-5, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| CA-6, 24-hr |  | 1.62 | 1.89 | 0 | 2.41 | 2.92 | 3.72 | 4.43 | 5.21 |
| FDOT Storms | > Florida DOT Storms |  |  |  |  |  |  |  |  |
| FDOT, 1-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FDOT, 2-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FDOT, 4-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FDOT, 8-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FDOT, 24-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FDOT, 72-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SFWMD, 72-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Austin Storms > Austin Frequency Storms | > Austin Frequency Storms |  |  |  |  |  |  |  |  |
| Austin Zone 1, 24-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Austin Zone 2, 24-hr |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
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Old Ranch Road

## These Areas are have no Drainage Control

We need to know how much of the proposed area of disturbance is treated vs untreated and if there are any exclusions that apply to the untreated areas. So please create a basic overview map (or modify an existing drainage map) with color shading/hatching that shows areas tributary to each PBMP and those disturbed areas that are not treated by a PBMP, with the applicable exclusion labeled (ex: 20\% up to 1ac of development can be excluded per ECM App I.7.1.C. 1 and exclusions listed in ECM App I.7.1.B.\#). Identify all areas that will be undisturbed and don't require a PBMP. An accompanying summary table on this map would also be very helpful (example provided):

| Water Quality Treatment Summary Table |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Basin ID | Total Area (ac) | Total <br> Proposed <br> Disturbed <br> Area <br> (ac) | Area Trib to Pond A (ac) | Disturbed Area Treated via Runoff Reduction (ac) | Disturbed Area Excluded from WQ per ECM App 1.7.1.C. 1 (ac) | Disturbed Area Excluded from WQ per ECM App 1.7.1.B.\# (ac) | Applicable WQ Exclusions (App I.7.1.B.\#) |
| A | 4.50 | 4.50 | 4.50 |  |  |  |  |
| B | 1.25 | 1.25 |  | 1.25 |  |  |  |
| C | 6.00 | 4.00 |  |  |  | 4.00 | ECM App 1.7.1.B. 5 |
| D | 2.50 | 2.50 | 1.00 |  | 0.50 | 1.00 | ECM App 1.7.1.B. 7 |
| E | 3.00 |  | 3.00 |  |  |  |  |
| F | 8.25 |  |  |  |  |  |  |
| Total | 25.50 | 12.25 | 8.50 | 1.25 | 0.50 | 5.00 |  |
| comments |  | [For each row, the sum of the values in <br> Columns 4-7 must be greater than or equal to the value in Column 3 above.] | IValues in this column can be more than Column 3 if overtreating nondisturbed areas of the same landuse.] | (See RR calc spreadsheet.] | TTotal must be $<20 \%$ of site and <1ac.] |  |  |
|  |  | Total Proposed Disturbed Area (ac) | Total Proposed Treated Area (ac) |  | Total Proposed Disturbed Area Excluded from WQ (ac) |  | Minimum Area to be Treated (ac) |
|  |  | 12.25 | 9.75 |  | 5.50 |  | 6.75 |


what is the area? All disturbed areas require treatment. 20\% up to 1ac of development can be excluded per ECM App I.7.1.C.1, but this needs to be clearly identified.

This drainage area is comprised of asphalt roadway. Some of the flow from \#20 may be collected into the pond \#89. This area will run free.

| 10 yr Storm |  | 100 yr Storm |  | typical throughout the drainage plan/report |
| :---: | :---: | :---: | :---: | :---: |
| Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
| 0.93 | 668 | 1.28 | 920 |  |
|  | 120 |  | 165 |  |
| - Include design points on the map and table to show where these flows leave the project site <br> - Include area in table |  |  |  |  |

Hydrograph 10-yr Summary



Hydrograph 100-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. No. | Hydrograph Type | Hydrograph Name | Peak <br> Flow <br> (cfs) | Time to Peak (hrs) | Hydrograph Volume (cuft) | Inflow Hyd(s) | Maximum Elevation (ft) | Maximum <br> Storage <br> (cuft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 0.269 | 0.20 | 194 | ---- |  |  |
| 2 | Rational | Post | 1.277 | 0.20 | 920 | ---- |  |  |
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| Hydrograph Type | = Rational | Peak Flow | $=1.277 \mathrm{cfs}$ |
| :---: | :---: | :---: | :---: |
| Storm Frequency | $=100-\mathrm{yr}$ | Time to Peak | $=0.20 \mathrm{hrs}$ |
| Time Interval | $=1 \mathrm{~min}$ | Runoff Volume | $=920 \mathrm{cuft}$ |
| Drainage Area | $=0.16 \mathrm{ac}$ | Runoff Coeff. | = 0.95* |
| Tc Method | = User | Time of Conc. (Tc) | $=12.0 \mathrm{~min}$ |
| IDF Curve | = Colorado Springs.idf | Intensity | $=8.40 \mathrm{in} / \mathrm{hr}$ |
| Freq. Corr. Factor | $=1.00$ | Asc/Rec Limb Factors $=1 / 1$ |  |
| * Composite C Worksheet |  |  |  |
| $\begin{array}{lll} \text { AREA (ac) } & \text { C } & \text { DES } \\ 0.16 & 0.95 & \text { Roac } \\ 0.16 & 0.95 & \text { Ros } \end{array}$ | description Road-Asphatt |  |  |




Basin 72 dominate

This area will run free.

| Clarify if any new |
| :--- |
| disturbance/development will occur |


| 10 yr |  | Storm | 100 yr |  | Storm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |  |
| $\mathbf{0 . 8 6}$ | $\mathbf{4 , 4 5 8}$ | $\mathbf{1 . 2 7}$ | $\mathbf{6 , 5 6 3}$ |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration <br> Surface Area <br> Req'd (sf) | 801 |  |  |  |  |

Hydrograph 10-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. | ${ }_{\substack{\text { Hyper }}}^{\substack{\text { Hyprograph } \\ \text { Typ }}}$ |  | (eamk |  | $\begin{aligned} & \text { Hydrograph } \\ & \text { Volume } \\ & \text { (cuft) } \end{aligned}$ |  | Maximum Elevation <br> (ft) | $\begin{aligned} & \text { Maximum } \\ & \text { Storage } \\ & \text { (cuft) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Raional | Pre Pe | 0.691 | ${ }^{1.43}$ | ${ }^{3.567}$ | - |  |  |
| 2 |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  | Raional | Post | 0.864 | 1.43 | 4,458 | $\cdots$ |  |  |
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Hydrograph 100-yr Summary
Hydrology Studio v 3.0.0.26


| Hydrograph Type |  | = Rational | Peak Flow | $=1.272 \mathrm{cfs}$ |
| :---: | :---: | :---: | :---: | :---: |
| Storm Frequency |  | = 100-yr | Time to Peak | $=1.43 \mathrm{hrs}$ |
| Time Interval |  | $=1 \mathrm{~min}$ | Runoff Volume | $=6,563 \mathrm{cuft}$ |
| Drainage Area |  | $=1.649 \mathrm{ac}$ | Runoff Coeff. | $=0.25$ * |
| Tc Method |  | = User | Time of Conc. (Tc) | $=86.0 \mathrm{~min}$ |
| IDF Curve |  | = Colorado Springs.idf | Intensity | $=3.09 \mathrm{in} / \mathrm{hr}$ |
| Freq. Corr. Factor |  | $=1.00$ | Asc/Rec Limb Fact | = $1 / 1$ |
| * Composite C Worksheet |  |  |  |  |
| AREA (ac) C desa |  | description |  |  |
| $\begin{aligned} & 0.107 \\ & 1.542 \\ & 1.54 \end{aligned}$ | $\begin{array}{cc} 0.95 & \text { Roof } \\ 0.20 & \text { Land- } \end{array}$ | $\xrightarrow{\text { Roof }}$ Land-Undevel |  |  |
| 1.1.42 1.649 | 0.25 |  |  |  |



Basin 70


This basin in the SW corner of the project will have no drainage control. Within this basin are infiltration ponds collecting waters from adjacent pavement of other basins. A runoff coefficient of 0.2 , is probably low with extensive scrub oak and accumulated detritus.

Run off will continue in it's historical manner to the borrow ditch.
Are the ponds not drainage control? Clearly identify which sections of this basin do not drain to ponds. Clarify if any new disturbance/development will occur

| 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: |
| Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
| 0.86 | $\mathbf{4 , 9 0 7}$ | $\mathbf{1 . 2 7}$ | $\mathbf{7 , 2 5 1}$ |
|  |  |  |  |

Please clearly indicate how flows are being conveyed to the ponds. As stated before all development must be accounted for (i.e. walkways, paths). Developed flows must be treated and increase in flows must be mitigated. Downstream conveyance must also be analyzed.

Hydrograph 10-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. | ${ }_{\substack{\text { Hydrograph } \\ \text { Type }}}$ |  | $\begin{array}{\|l\|l} \substack{\text { Peagu } \\ \text { (cos } \\ \text { coss }} \end{array}$ |  |  |  | $\begin{aligned} & \text { Maximum } \\ & \text { Elevation } \\ & \text { (ft) } \end{aligned}$ | $\begin{aligned} & \text { Maximum } \\ & \text { Storage } \\ & \text { (cuft) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 0.792 | ${ }^{1.58}$ | 4,516 | -- |  |  |
|  |  |  |  |  |  |  |  |  |
| 2 | Rational | Post | 0.861 | ${ }^{1.58}$ | 4,907 | - |  |  |
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Hydrograph 100-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. No. | Hydrograph Type | Hydrograph Name | Peak <br> Flow <br> (cfs) | Time to Peak (hrs) | Hydrograph <br> Volume <br> (cuft) | Inflow Hyd(s) | Maximum Elevation (ft) | Maximum Storage (cuft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 1.171 | 1.58 | 6,672 | ---- |  |  |
| 2 |  | Post | 1.272 | 1.58 |  | ---- |  |  |
|  | Rational | Post | 1.272 | 1.58 | 7,251 | ---- |  |  |
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| Hydrograph Type |  | = Rational | Peak Flow | $=1.272 \mathrm{cfs}$ |
| :---: | :---: | :---: | :---: | :---: |
| Storm Frequency |  | $=100-\mathrm{yr}$ | Time to Peak | $=1.58 \mathrm{hrs}$ |
| Time Interval |  | $=1 \mathrm{~min}$ | Runoff Volume | = 7,251 cuft |
| Drainage Area |  | $=1.754 \mathrm{ac}$ | Runoff Coeff. | = 0.25* |
| Tc Method |  | = User | Time of Conc. (Tc) | $=95.0 \mathrm{~min}$ |
| IDF Curve |  | = Colorado Springs.idf | Intensity | $=2.90 \mathrm{in} / \mathrm{hr}$ |
| Freq. Corr. Factor |  | $=1.00$ | Asc/Rec Limb Fact | = $1 / 1$ |
| * Composite C Worksheet |  |  |  |  |
| area (ac) C desa |  | description |  |  |
| $\begin{array}{lll}0.126 \\ 1.628 & 0.95 & \text { Rood } \\ 0.20 & \text { Land }\end{array}$ |  | Land-Undevel |  |  |
| 1.754 | 0.25 |  |  |  |



## Basin 92 - Area $16+66+67$ to Free



This drainage area is comprised of asphalt roadway \#16 and undeveloped land \#66 \& 67 in the SE corner of the property. These areas will run free.

Clarify if any new disturbance/development will occur

|  | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.818 | 3044 | 1.19 | 4,426 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF |  |  |  |  |

Hydrograph 10-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. | ${ }_{\substack{\text { Hyprograph } \\ \text { Type }}}^{\substack{\text { a }}}$ |  | $\begin{array}{\|l\|l} \substack{\text { Peagu } \\ \text { (cos } \\ \text { coss }} \end{array}$ |  |  |  | $\begin{aligned} & \text { Maximum } \\ & \text { Elevation } \\ & \text { (ft) } \end{aligned}$ | $\begin{aligned} & \text { Maximum } \\ & \text { Storage } \\ & \text { (cuft) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 0.584 | ${ }^{1.03}$ | 2,174 | -- |  |  |
|  |  |  |  |  |  |  |  |  |
| 2 | Rational | Post | 0.818 | 1.03 | 3,044 | - |  |  |
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Hydrograph 100-yr Summary
Hydrology Studio v 3.0.0.26

| Hyd. No. | Hydrograph Type | Hydrograph Name | Peak <br> Flow <br> (cfs) | Time to Peak (hrs) | Hydrograph Volume (cuft) | Inflow Hyd(s) | Maximum Elevation (ft) | Maximum <br> Storage <br> (cuft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rational | Pre Pre | 0.850 | 1.03 | 3,161 | ---- |  |  |
| 2 | Rational | Post | 1.190 | 1.03 |  | ---- |  |  |
|  | Rational | Post | 1.190 | 1.03 | 4,426 | ---- |  |  |
|  |  |  |  |  |  |  |  |  |
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# Calculations for Areas with Dedicated Infiltration Ponds 

[^1]provide analysis of the spillway offsite

## Results Format



For each basin analyzed there is generally three pages of output. Below is the results of the Hydrology calculations these pages include.

Shows color coded surfaces and boundaries used for basin analysis

Shows expected total runoff volume in CF and flow in CFS for 10 yr and 100 yr storms Shows the size of the pond required to infiltrate runoff within 40 hours


Shows Basin number and Hydrology file name Shows contributing areas and \#'s
Shows areas, reach, slope and coefficient of runoff
Shows Time of Concentration used for Pre and Post developement or different surface flows
Shows Hydrology output Shows Pond Type
Shows pond size calculation
Shows Volume test as compared to req'd volume Shows infiltrative area test when pond is half full or empty


Shows Grassed Swale location and alignment
Shows Swale Type and size
Shows Pond Type and dimensions
Shows Pond location

## Basin 87



Area \#75 in Basin 87 will remain predominantly agricultural use and will be contour plowed to further reduce runoff. Greenhouse roof \#57 is included.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 1.42 | 8882 | 2.11 | 13,170 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 1,596 |  | 2,366 |

Basin 87


Type 2 Triangular Infiltration Pond


## Basin 87


provide froude number and identify if the flow is sub or super critical for all the proposed channels. Identify any protection that is needed. Refer to DCMV1 Ch10. for permissible velocities.
clarify whether roof \#56 will be conveyed to pond 87 or 86 as the boundary line for basin 87 does not include roof \#56

| , |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#87 | Hydrology File |  | 75+56+87 to 87.hys |  |  |
| , |  |  |  |  |  |
| , |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rafe (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166666667 |  |  |  |  |
| Receive Flows from: | 75, 54, 87 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (Min) |
| Roof \# 56 | 0.0201 |  |  | 0.95 |  |
| Roof \#54 | 0.1096 |  |  | 0.95 |  |
| Basin 75 | 2.4782 | 453 | 4.0\% | 0.2 | 103.8 |
| Pond \# 87 | 0.1410 |  |  | 1 |  |
| Total | 2.7489 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.2800 |  |  |  |  |
| Composite Area | 2.7490 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 103.8 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr St |  | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 1.42 | 8882 | 2.11 | 13,170 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 1,596 |  | 2,366 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Triangular Pyramid |  |  |  |  |  |
|  |  |  |  |  |  |
| Full Pyramid (defines top dimensions of pond) |  |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Base Length (ft) | 74 | L1 |  |  |  |
| Base Width (ft) | 104.7 | L2 |  |  |  |
| Height | 24.7 | h0 |  |  |  |
|  |  |  |  |  |  |
| Base Area (sf) | 7744.2 | BA |  |  |  |
| Volume (cf) | 63668.4 | Vol |  |  |  |
|  |  |  |  |  |  |
| Smaller Pyramid |  |  |  |  |  |
| Depth | 3.0 | h2 H |  |  |  |
| Base Length | 56.0 | I |  |  |  |
| Base Width (ft) | 86.7 | w |  |  |  |
| Top Cone Height (ft) | 21.7 | h1 |  |  |  |
| Top Cone Volume (cf) POND Size | 35042.3 |  |  |  |  |
|  |  |  |  |  |  |
| Bottom Truncated Cone Volume (cf) | 28626.1 | Greater Than | 13,170 |  |  |
| Base Area (sf) | 2426.3 | I x w /2 |  |  |  |
| Water Surface Area - FULL(sf) | 3872.1 |  |  |  |  |
| Water Surface Area at HALF FULL | 3149.2 | Greater Than | 2,366 |  |  |
| Water Surface Area - EMPTY | 2426.3 | Greater Than | 2,366 |  |  |
|  |  |  |  |  |  |

## Basin 89


please account for the imperviousness of the proposed path/walkway within this basin
Basin \#89, it's pond and conveyance swales is dedicated to reducing runoff from adversely affecting the OWTS Soil Treatment Area (\#95).

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.6 | 1923 | 0.87 | 2,780 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/R/40hr) = SF | Infiltration Surface Area Req'd (sf) | 345 |  | 499 |

## Basin 89





## Basin 95 is space reserved for the Soil Treatment Area of the

 OWTS. The uphill side of the STA is protected from runoff by Pond \#89. Swales will be created on the north and west sides to convey water to Pond \#95aaccount for the proposed walkway/path in this basin

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.42 | 1355 | 0.6 | 1,960 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 243 |  | 352 |

## Basin 95



| Channel Parameters |  |
| :---: | :---: |
| Bottom Width (tt) b | 0.50 |
| Side Slope X:1 | 3.00 |
| Depth (tt) h | 1.00 |
| Top Width (tt) T | 6.50 |
| Flow Area |  |
| Area (sf) | 3.50 |
| Wetted Perimeter | 6.82 |
| Hydraulic Radius | 0.51 |
| Flow Calc |  |
| Slope (\%) | 2.07\% |
| Mannings ( n ) | 0.03 |
| Velocity (tt/sec) | 4.58 |
| Area (sf) | 3.50 |
| Flow (cf/sec) | 16.03 |

## Swale Type 2 Tapered



|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#95 | Hydrology File |  | STA 95 to 95a.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | STA,95 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  | 0.95 |  |
| Roof |  |  |  | 0.95 |  |
| BasinSTA+95 | 0.5908 | 150 | 5.3\% | 0.2 | 54.2 |
| Pond | 0.0280 |  |  | 1 |  |
| Total | 0.6188 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.2100 |  |  |  |  |
| Composite Area | 0.6188 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 54.2 | 0.26 |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 0.42 | 1355 | 0.6 | 1,960 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 243 |  | 352 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Triangular Pyramid |  |  |  |  |  |
|  |  |  |  |  |  |
| Full Pyramid (defines top dimensions of pond) |  |  |  |  |  |
| Side Slope X:1 | 3.00 |  |  |  |  |
| Base Length | 38.00 | L1 |  |  |  |
| Base Width | 53.74 | L2 |  |  |  |
| Height | 12.67 | h0 |  |  |  |
|  |  |  |  |  |  |
| Base Area (sf) | 2042.12 | BA |  |  |  |
| Volume (cf) | 8621.44 | Vol |  |  |  |
|  |  |  |  |  |  |
| Smaller Pyramid |  |  |  |  |  |
| Depth | 3.00 | h2 H |  |  |  |
| Base Length | 20.00 | I |  |  |  |
| Base Width (ft) | 35.74 | W |  |  |  |
| Top Cone Height (ft) | 9.67 | h1 |  |  |  |
| Top Cone Volume (cf) POND Size | 2303.02 |  |  |  |  |
|  |  |  |  |  |  |
| Bottom Truncated Cone Volume (cf) | 6318.42 | Greater Than | 1,960 |  |  |
| Base Area (sf) | 357.40 | I x w/2 |  |  |  |
| Water Surface Area - FULL(sf) | 1021.06 |  |  |  |  |
| Water Surface Area at HALF FULL | 689.23 | Greater Than | 352 |  |  |
| Water Surface Area - EMPTY | 357.40 | Greater Than | 352 |  |  |
|  |  |  |  |  |  |



Pond 94 infiltrates waters from mostly undeveloped land \#73 and roof \#49. Runoff flows via sheet flow to low area of pond.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.53 | 2798 | 0.78 | 4,122 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 503 |  | 740 |

## Basin 94



Type 1 Rectangular Infiltration Pond


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#94 | Hydrology File |  | 49+73+94 to 94.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from : | 49,73,94 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof \#49 | 0.0500 |  |  | 0.95 |  |
| Roof |  |  |  | 0.95 |  |
| Basin \#73 | 0.7804 | 270 | 3.0\% | 0.2 | 88.3 |
| Pond \# 94 | 0.0550 |  |  | 1 |  |
| Total | 0.8854 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.2900 |  |  |  |  |
| Composite Area | 0.8854 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 88.3 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 0.53 | 2798 | 0.78 | 4,122 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 503 |  | 740 |  |
|  |  |  |  |  |  |
| Trapezoidal Pond Sizing | Input Values |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Pond Top Length (ft) | 80 | L |  |  |  |
| Pond Top Width (ft) | 30 | W |  |  |  |
| Pond Bottom Length (ft) | 65 | I |  |  |  |
| Pond Bottom Width (ft) | 15 | w |  |  |  |
| Depth (ft) | 2.5 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 2400 |  |  |  |  |
| Full Volume (cf) | 4,125 | Greater Than | 4,122 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 2400 |  |  |  |  |
| Water Surface Area at HALF FULL | 1687.5 | Greater than | 740 |  |  |
| Water Surface Area - EMPTY (sf) | 975 | Greater than | 740 |  |  |
|  |  |  |  |  |  |
| NOTES |  |  |  |  |  |

## Basin 86



Pond 86 infiltrates waters from the gravel roadway \#1 and a small shed \#56. Runoff flows via sheet flow to pond \#86.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 2.49 | 3432 | 3.49 | 4,821 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs $(C F / I R / 40 h r)=S F$ | Infiltration Surface Area Req'd (sf) | 617 |  | 866 |

## Basin 86



|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#86 | Hydrology File |  | 1+56+86.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 1, 56, 86 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  |  |  |
| Roof \#56 | 0.02 |  |  | 0.95 |  |
| Roads Gravel \#1 | 0.507 | 313 | 4.5\% | 0.85 | 23.1 |
| Roads Asphalt |  |  |  | 0.95 |  |
| Land |  | 313 | 4.5\% | 0.2 | 83.0 |
| Pond \# 86 | 0.094 |  |  | 1 |  |
| Total | 0.621 | ac |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.880 |  |  |  |  |
| Composite Area | 0.621 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) |  |  |  |  |
|  | 23.1 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 2.49 | 3432 | 3.49 | 4,821 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs $(\mathrm{CF} / \mathrm{IR} / 40 \mathrm{hr})=\mathrm{SF}$ | Infiltration Surface Area Req'd (sf) | 617 |  | 866 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Rectangular Pyramid |  |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Pond Top Length (ft) | 200 | L |  |  |  |
| Pond Top Width (ft) | 20 | W |  |  |  |
| Pond Bottom Length (ft) | 176 | 1 |  |  |  |
| Pond Bottom Width (ft) | 9.5 | W |  |  |  |
| Depth (ft) | 1.75 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 4000 |  |  |  |  |
| Full Volume (cf) | 4,890 | Greater than | 4,821 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 4000 |  |  |  |  |
| Water Surface Area at HALF FULL | 2836 | Greater than | 866 |  |  |
| Water Surface Area - EMPTY (sf) | 1672 |  |  |  |  |

## Basin 58



Pond 58 collects waters from paved area $\# 5$ and landscaped area \#76 via grassed swales and sheet flow from land. The six small buildings are earth sheltered and their area has been included as roofs.

|  | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
| From \#5 only | 1.67 | 1304 | 2.31 | 1801 |
| From \#76 only | 0.81 | 4418 | 1.19 | 6517 |
| Aggregate | 2.48 | 5,722 | 3.5 | 8,318 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 1,028 |  | 1,494 |

## Basin 58



## Pond 58 infiltrates waters and is generally trapezoidal with the dimensions

 shown. Both swales are Type 2 which begin a minimum of 2 ' wide and finish with the dimensions shown.| Channel Parameters |  | Channel Parameters |  |
| :---: | :---: | :---: | :---: |
| Bottom Width (tt) b | 1.5 | Bottom Width (tt) b | 1 |
| Side Slope X:1 | 3 | Side Slope X:1 | 3 |
| Depth (ft) H | 0.75 | Depth (ft) H | 1 |
| Top Width (ft) W | 6 | Top Width (ft) W | 7 |
| Flow Area |  | Flow Area |  |
| Area (sf) | 2.8125 | Area (sf) | 4 |
| Wetted Perimeter | 6.24341649 | Wetted Perimeter | 7.32455532 |
| Hydraulic Radius | 0.450474513 | Hydraulic Radius | 0.546108238 |
| Flow Calc |  | Flow Calc |  |
| Slope (\%) | 3.0\% | Slope (\%) | 4.2\% |
| Mannings ( n ) | 0.3 | Mannings ( n ) | 0.3 |
| Velocity (tt/sec) | 0.505789734 | Velocity (tt/sec) | 0.683753708 |
| Area (sf) | 2.8125 | Area (sf) | 4 |
| Flow (ct/sec) | 1.422533627 | Flow (cf/sec) | 2.735014831 |


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#58 | Hydrology File |  | 5+58+76 to | 58.hys |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate ( $\mathrm{IR}=\mathrm{ft} / \mathrm{hour} / \mathrm{sf}$ ) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 5, 58,76 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof \# ElH's | 0.0663 |  |  | 0.95 |  |
| Roof |  |  |  | 0.95 |  |
| Roads Gravel |  |  |  | 0.85 |  |
| Roads \#5 Asphalt | 0.299 | 245 | 3.5\% | 0.95 | 13.3 |
| Land \#76 | 0.866 | 305 | 3.3\% | 0.2 | 90.8 |
| Pond \# 58 | 0.141 |  |  | 1 |  |
| Total | 1.372 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.40 |  |  |  |  |
| Composite Area | 1.372 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) |  |  |  |  |
|  | 70.6 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
| From \#5 only | 1.67 | 1304 | 2.31 | 1801 |  |
| From \#76 only | 0.81 | 4418 | 1.19 | 6517 |  |
| Aggregate | 2.48 | 5,722 | 3.5 | 8,318 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 1,028 |  | 1,494 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Rectang | ular Pyramid |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Pond Top Length (ft) | 200 | L |  |  |  |
| Pond Top Width (ft) | 30 | W |  |  |  |
| Pond Bottom Length (ft) | 176 | 1 |  |  |  |
| Pond Bottom Width (ft) | 15 | w |  |  |  |
| Depth (ft) | 2.5 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 6000 |  |  |  |  |
| Full Volume (cf) | 8,350 | Greater than | 8,318 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 6000 |  |  |  |  |
| Water Surface Area at HALF FULL | 4320 | Greater than | 1,494 |  |  |
| Water Surface Area - EMPTY (sf) | 2640 | Greater than | 1,494 |  |  |

## Basin 85



Pond \#85 collects waters from mostly gravel road area \#24. Waters sheet flow to pond.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 2.42 | 1343 | 3.07 | 1,842 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Rea'd (sf) | 241 |  | 331 |

## Basin 85



| Infiltration Pond \#85 | Hydrology File |  | $24+85$ to 85.hys |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 24,85 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  | 0.95 |  |
| Asphalt \#24 | 0.2765 | 100 | 2.0\% | 0.95 | 10.2 |
| Basin |  | 100 | 2.0\% | 0.2 | 61.2 |
| Pond \#85 | 0.0799 |  |  | 1 |  |
| Total | 0.3564 |  |  |  |  |
|  |  | 0.02 |  |  |  |
| Flow Coefficient of Runoff | 0.9600 |  |  |  |  |
| Composite Area (ac) | 0.3564 |  |  |  |  |
| Composite Curve \# | 0.9600 |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 8 | 0.26 |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 2.42 | 1343 | 3.07 | 1,842 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 241 |  | 331 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Rectangular Pyramid | Input Values |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Pond Top Length (ft) | 175 | L |  |  |  |
| Pond Top Width (ft) | 15 | W |  |  |  |
| Pond Bottom Length (ft) | 167.5 | 1 |  |  |  |
| Pond Bottom Width (ft) | 7.5 | w |  |  |  |
| Depth (ft) | 1.25 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 2625 |  |  |  |  |
| Full Volume (cf) | 2,414 | Greater Than | 1,842 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 2625 |  |  |  |  |
| Water Surface Area at HALF FULL | 1940.625 | Greater than | 331 |  |  |
| Water Surface Area - EMPTY (sf) | 1256.25 |  |  |  |  |



Pond \#93 receives waters from land \#77,78, roof \#36 and pavement areas \#3,4

|  | 10 yr Storm |  | 100 yr Storm |  |
| :--- | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
| Infiltration | $\mathbf{1 . 1 3}$ | $\mathbf{4 , 2 6 9}$ | $\mathbf{1 . 6 4}$ | $\mathbf{6 , 2 1 1}$ |
| Infiltration Surface Area Req'd to drain within 40 hrs <br> (CF/IR/40hr) = SF | Infiltration <br> Surface Area <br> Req'd (sf) | $\mathbf{7 6 7}$ |  |  |

## Basin 93




## Basin 60



Pond \#60 infiltrates waters from pavements \#7, 8 .

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.94 | 564 | 1.29 | 774 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 101 |  | 139 |

## Basin 60



## Waters sheet flow to infiltration pond \#60



|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#60 | Hydrology File |  | 7+8+60 to 60.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 37, 7, 8, 60 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  |  |  |
| Roof |  |  |  | 0.95 |  |
| Roads Gravel \#7 | 0.055 | 130 | 4.6\% | 0.85 | 14.7 |
| Roads Asphalt \#8 | 0.081 | 130 | 4.6\% | 0.95 | 8.8 |
| Land |  |  |  | 0.2 |  |
| Pond \# 60 | 0.024 |  |  | 1 |  |
| Total | 0.159 | ac |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.910 |  |  |  |  |
| Composite Area | 0.159 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) |  |  |  |  |
|  | 14.7 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 0.94 | 564 | 1.29 | 774 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF $/ \mathrm{IR} / 40 \mathrm{hr})=\mathrm{SF}$ | Infiltration Surface Area Req'd (sf) | 101 |  | 139 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Rectangular Pyramid |  |  |  |  |  |
| Side Slope X:1 | 0.1 |  |  |  |  |
| Pond Top Length (ft) | 40 | L |  |  |  |
| Pond Top Width (ft) | 12 | W |  |  |  |
| Pond Bottom Length (ft) | 39.6 | I |  |  |  |
| Pond Bottom Width (ft) | 11.6 | w |  |  |  |
| Depth (ft) | 2 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 480 |  |  |  |  |
| Full Volume (cf) | 939 | Greater than | 774 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 480 |  |  |  |  |
| Water Surface Area at HALF FULL | 469.68 | Greater than | 139 |  |  |
| Water Surface Area - EMPTY (sf) | 459.36 | Greater than | 139 |  |  |

## Basin 61



Pond \#61 infiltrates waters from pavement \#9. The purple area shown is a depressed garden and does no impact the runoff.

|  | 10 yr Storm |  | 100 yr Storm |  |
| :--- | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.69 | 290 | 0.94 | 394 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain <br> within 40 hrs (CF/IR/40hr) = SF | Infiltration <br> Surface Area <br> Req'd (sf) | 52 |  |  |

## Basin 61



## Waters sheet flow directly to infiltration pond \#61





Pond \#59 receives waters from area \#79 which has a corral for goats etc. This is assumed to be fairly compacted soil so a runoff coefficient of .85 was used.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 1.93 | 1391 | 2.66 | 1,917 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF/IR/40hr) = SF | Infiltration Surface Area Req'd (sf) | 250 |  | 344 |

## Basin 59



| Channel Parameters |  |  |
| :--- | :--- | :--- |
| Bottom Width (ft) b | 1.00 b |  |
| Side Slope X:1 | 3.00 |  |
| Depth (ft) h | 0.50 H |  |
| Top Width (ft) W | Flow Area | 4.00 W |
|  |  |  |
| Area (sf) | Wetted Perimeter |  |
|  |  |  |
| Hydraulic Radius | 4.16 |  |
|  | 0.30 |  |
| Flow Calc |  |  |
| Slope (\%) | $1.25 \%$ |  |
| Mannings (n) | 0.03 |  |
| Velocity (ft/sec) | 2.49 |  |
| Area (sf) | 1.25 |  |
| Flow (cf/sec) | 3.12 |  |


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#59 | Hydrology File |  | 37+79+59 to 59-F2.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 79,59 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  |  |  |
| Roof \#37 | 0.0562 | 100 | 2.1\% | 0.95 | 10.0 |
| Roads Gravel |  |  |  | 0.85 |  |
| Roads Asphalt |  |  |  | 0.95 |  |
| Land \#79 | 0.270 | 108 | 3.8\% | 0.85 | 14.3 |
| Pond \# 59 | 0.034 |  |  | 1 |  |
| Total | 0.361 | ac |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.350 |  |  |  |  |
| Composite Area | 0.361 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) |  |  |  |  |
|  | 14.3 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 1.93 | 1391 | 2.66 | 1,917 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd to drain within $40 \mathrm{hrs}(\mathrm{CF} / \mathrm{IR} / 40 \mathrm{hr})=\mathrm{SF}$ | Infiltration Surface Area Req'd (sf) | 250 |  | 344 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Rec | tangular Pyramid |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Pond Top Length (ft) | 70 | L |  |  |  |
| Pond Top Width (ft) | 19 | W |  |  |  |
| Pond Bottom Length (ft) | 52 | I |  |  |  |
| Pond Bottom Width (ft) | 1 | w |  |  |  |
| Depth (ft) | 3 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 1330 |  |  |  |  |
| Full Volume (cf) | 1,911 | TOO SMALL | 1,917 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 1330 |  |  |  |  |
| Water Surface Area at HALF FULL | 691 | Greater than | 344 |  |  |
| Water Surface Area - EMPTY (sf) | 52 | TOO SMALL | 344 |  |  |



Pond \#88 collects waters from land \#82, roofs \#45, 46 and pavement \#6. Waters are conveyed to Pond 88 via grass swales. This pond is impounded by vegetated berms. See Plan and Detail DR-2

|  | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 0.92 | 2993 | 1.34 | 4,330 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs $(\mathrm{CF} / \mathrm{IR} / 40 \mathrm{hr})=\mathrm{SF}$ | Infiltration Surface Area Req'd (sf) | 538 |  | 778 |
|  |  |  |  |  |
|  |  |  |  |  |

## Basin 88




|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#88 | Hydrology File |  | 6+45+46+82 to 88.hys |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 6, 45, 46, 82, 8 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof \#45,\#46 | 0.1473 |  |  | 0.95 |  |
| Roof |  |  |  | 0.95 |  |
| Roads Gravel |  |  |  | 0.85 |  |
| Roads Asphalt \#6 | 0.069 |  |  | 0.95 |  |
| Land \#82 + . 5 * \#88 | 0.261 | 150 | 5.3\% | 0.2 | 54.2 |
| Pond \# $88 \times .5$ | 0.070 |  |  | 1 |  |
| Total | 0.547 | ac |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.200 |  |  |  |  |
| Composite Area | 0.547 |  |  |  |  |
| Composite Curve \# | 0.52 |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | 7.4 |  |  |  |
|  |  |  |  |  |  |
|  | 10 | yr Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 0.92 | 2993 | 1.34 | 4,330 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs $(\mathrm{CF} / \mathrm{R} / 40 \mathrm{hr})=\mathrm{SF}$ | Infiltration Surface Area Req'd (sf) | 538 |  | 778 |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Half Triangular Prism Volume |  |  |  |  |  |
| Side a | 134 |  |  |  |  |
| Side b | 90 |  |  |  |  |
| Side c | 97 |  |  |  |  |
| Height h | 2.2 |  |  |  |  |
| Semi Perimeter (lf) | 160.5 | $(a+b+c) / 2$ |  |  |  |
| Base Area (sf) | 6134.5 | sf |  |  |  |
| Volume = (cf) triangle based pyramid | 4494.1 | cf $=1 / 3 \times$ Base Are | $a \times h$ |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 6134.5 | far Greater than | 4,330 |  |  |
|  |  |  | 1 |  |  |
| Full Volume (cf) | 4494.1 | Greater than | 4,330 |  |  |

## Basin 71



Basin 71 is the largest collecting waters from roofs \#42,43,44, pavers \#26,27,28,29, pavement \#22 and the Nursery area \#71. The Nursery area is where 'ball and burlap' trees are staged for sale in wide rows separated by Gabion basket 'dams', all of which are infiltration ponds. Pond \#71a captures any waters that fall below the last 'dam'. It's irregular in shape and depth.

## Basin 71





## Basin 62



Pond 62 receives waters from plaza pavers \#25. All waters sheet flow to pond.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 1.66 | 1495 | 2.3 | 2,072 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF/R/40hr) = SF | Infiltration Surface Area Req'd (sf) | 269 |  | 372 |

## Basin 62



Waters sheet flow directly to infiltration pond \#62


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#62 | Hydrology File |  | 25+62 to 62.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from : | 25,62 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  | 0.95 |  |
| Roof |  |  |  | 0.95 |  |
| Roads Gravel / Pavers |  |  |  | 0.85 |  |
| Roads Concrete/Asphalt \#25 | 0.268 | 165 | 1.2\% | 0.95 | 15.5 |
| Land |  | 165 | 1.2\% | 0.2 | 93.0 |
| Pond \# 62 | 0.043 |  |  | 1 |  |
| Total | 0.311 | ac |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.910 |  |  |  |  |
| Composite Area | 0.311 |  |  |  |  |
| Composite Curve \# | 0.91 |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) |  |  |  |  |
|  | 7.4 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr S | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 1.66 | 1495 | 2.3 | 2,072 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF/IR/40hr) $=$ SF | Infiltration Surface Area Req'd (sf) | 269 |  | 372 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Rectangular Pyramid |  |  |  |  |  |
| Side Slope X:1 | 1 |  |  |  |  |
| Pond Top Length (ft) | 70 | L |  |  |  |
| Pond Top Width (ft) | 16 | W |  |  |  |
| Pond Bottom Length (ft) | 65.5 | I |  |  |  |
| Pond Bottom Width (ft) | 11.5 | w |  |  |  |
| Depth (ft) | 2.25 | h |  |  |  |
| Infiltation Surface Area - FULL (sf) | 1120 |  |  |  |  |
| Full Volume (cf) | 2,100 | Greater than | 2,072 |  |  |
|  |  |  |  |  |  |
| Water Surface Area - FULL (sf) | 1120 |  |  |  |  |
| Water Surface Area at HALF FULL | 936.625 | Greater than | 372 |  |  |
| Water Surface Area - EMPTY (sf) | 753.25 | Greater than | 372 |  |  |

## Pond 40c



Pond 40 c receives waters from loading dock pit \#12 and roofs \#40, 41, 42. All waters flow via underground pipe to pond.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 2.02 | 1,451 | 2.78 | 2,000 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF $\mathrm{IR} / 40 \mathrm{hr})=\mathrm{SF}$ | Infiltration Surface Area Req'd (sf) | 261 |  | 359 |

## Pond 40c



Pipe Flow, Full

| Slope (\%) 2' drop over 83' | 0.02 |  |  |
| :--- | :---: | :--- | :--- |
| Pipe Diameter (in) | 10 |  |  |
| Pipe Diameter (ft) | 0.8333 |  |  |
| Pipe Area (sf) | 0.5456 |  |  |
| Wetted Perimeter (ft) | 2.6190 |  |  |
| Hydraulic Radius (ft) Rh | 0.2083 |  |  |
| Velocity, Gravity Flow (tt/s) | 8.1150 |  |  |
| Flow Volume (cfs) | 4.486 |  |  |



## Basin 80a



Pond 80a collects waters from undeveloped Basin 80.

|  | 10 yr Storm |  | 100 yr Storm |  |
| :--- | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
| Infiltration | $\mathbf{0 . 2 8}$ | $\mathbf{6 6 7}$ | $\mathbf{0 . 4}$ | $\mathbf{9 5 4}$ |
| $\quad$ Infiltration Surface Area Req'd $(C F / I R / 40 h r)=$ SF | 2.17 off \#10 |  | 2.99 off \#10 |  |
|  |  |  |  |  |

## Basin 80a



|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#80a | Hydrology File |  | $80+80 \mathrm{a}$ to 80a |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate ( $\mathrm{IR}=\mathrm{ft} /$ hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | \#80,\#80a |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  | 0.95 |  |
| Asphalt |  |  |  |  |  |
| UnDeveloped Land \#80 | 0.3670 | 135 | 11.1\% | 0.2 | 40.4 |
| Pond \#80a | 0.0081 |  |  | 1 |  |
| Total | 0.3751 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.4100 |  |  |  |  |
| Composite Area (ac) | 0.3751 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 40.4 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 0.28 | 667 | 0.4 | 954 |  |
|  | 2.17 off \#10 |  | 2.99 off \#10 |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF |  | 120 |  | 171 |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Conical Ellipse - FULL |  |  |  |  |  |
| Full Cone (top dimensions) |  |  |  |  |  |
| Desired Depth | 2 |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Full Size (L1) | 37 |  |  |  |  |
| Base Length 'a' Long Axis radius (ft) | 18.5 | W |  |  |  |
| Full Size (L2) | 28 |  |  |  |  |
| Base Length 'b' Short Axis radius (ft) | 14 | L |  |  |  |
| Height of Full Cone (based on Side Slope) (ft) h1 | 4.7 | h1 |  |  |  |
| Volume (cf) | 1,266.1 |  |  |  |  |
|  |  |  |  |  |  |
| Missing Cone (bottom dimensions) |  |  |  |  |  |
| Missing Cone Height (ft) h2 | 2.7 |  |  |  |  |
| Base Length 'c' Long Axis radius (ft) | 10.6 | W |  |  |  |
| Base Length 'd' Short Axis radius (ft) | 8.0 | I |  |  |  |
| Volume (missing cone) (cf) | 236 |  |  |  |  |
|  |  |  |  |  |  |
| Truncated Pond Volume (cf) | 1,030 | Greater Than | 954 |  |  |
|  |  |  |  |  |  |
| Full Pond Surface Area (sf) | 814 | sf |  |  |  |
| Pond Bottom Surface Area (sf) | 266 | Greater Than | 171 |  |  |

## Basin 91



Pond \#91 receives waters from mostly undeveloped land, some pavement and roof. Pavement waters are conveyed via grassed swale to pond \#91

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 1.8 | 6486 | 2.62 | 9,420 |
|  | 2.17 off \#10 |  | 2.99 off \#10 |  |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF |  | 1,165 |  | 1,692 |

## Basin 91



Channel Parameters

| Bottom Width (tt) b | 1.00 b |
| :---: | :---: |
| Side Slope X:1 | 3.00 |
| Depth (tt) h | 0.50 H |
| Top Width (ft) W | 4.00 W |
| Flow Area |  |
| Area (sf) | 1.25 |
| Wetted Perimeter | 4.16 |
| Hydraulic Radius | 0.30 |
| Flow Calc |  |
| Slope (\%) | 1.25\% |
| Mannings ( n ) | 0.03 |
| Velocity (tt/sec) | 2.49 |
| Area (sf) | 1.25 |
| Flow (cf/sec) | 3.12 |



|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#91 | Hydrology File |  | $10+13+81+38+39+91$ to |  | 91.hys |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 10,13,81,38,39 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof \#38,\#39 | 0.0000 |  |  | 0.95 |  |
| Asphalt \#10, \#13 | 0.0000 | 215 | 0.0428 | 0.95 | 11.6 |
| UnDeveloped Land\#80,\#81 | 0.0000 | 450 | 3.3\% | 0.2 | 109.7 |
| Pond \#91 | 0.0000 |  |  | 1 |  |
| Total | 0.0000 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.4100 |  |  |  |  |
| Composite Area (ac) | 0.0000 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 109.7 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 1.77 | 6369 | 2.57 | 9,250 |  |
|  | 2.17 off \#10 |  | 2.99 off \#10 |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF |  | 1,144 |  | 1,662 |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Conical Ellipse |  |  |  |  |  |
| Full Cone (top dimensions) |  |  |  |  |  |
| Desired Depth | 4 |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Full Size (L1) | 90 | L |  |  |  |
| Base Length 'a' Long Axis radius (ft) | 45 | a |  |  |  |
| Full Size (L2) | 63 | W |  |  |  |
| Base Length 'b' Short Axis radius (ft) | 31.5 | b |  |  |  |
| Height of Full Cone (based on Side Slope) (ft) h1 | 10.5 | h1 |  |  |  |
| Volume (cf) | 15,590.9 |  |  |  |  |
|  |  |  |  |  |  |
| Missing Cone (bottom dimensions) |  |  |  |  |  |
| Missing Cone Height (ft) h2 | 6.5 |  |  |  |  |
| Base Length 'c' Long Axis radius (ft) | 27.9 | C |  |  |  |
| Base Length 'd' Short Axis radius (ft) | 19.5 | d |  |  |  |
| Volume (missing cone) (cf) | 3,699 |  |  |  |  |
|  |  |  |  |  |  |
| Truncated Pond Volume (cf) | 11,892 | Greater Than | 9,250 |  |  |
|  |  |  |  |  |  |
| Full Pond Surface Area (sf) | 4455 | sf |  |  |  |
| Pond Bottom Surface Area (sf) | 1707 | Greater Than | 1,662 |  |  |

## Basin 11a



Pond \#1 1a infiltrates waters from mostly concrete pavement and portion along the Basin 92.

| Hydrology Output | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 1.05 | 818 | 1.45 | 1,130 |
|  | 2.17 off \#10 |  | 2.99 off \#10 |  |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF |  | 147 |  | 203 |

## Basin 11a



Channel Parameters

|  |  |
| :---: | :---: |
| Bottom Width (ft) b | 1.00 b |
| Side Slope X:1 | 3.00 |
| Depth (ft) H | 1.50 H |
| Top Width (tt) W | 10.00 W |
| Flow Area |  |
| Area (sf) | 8.25 |
| Wetted Perimeter | 10.49 |
| Hydraulic Radius | 0.79 |
| Flow Calc |  |
| Slope (\%) | 3.00\% |
| Mannings ( n ) | 0.30 |
| Velocity (ft/sec) | 0.73 |
| Area (sf) | 8.25 |
| Flow (ct/sec) | 6.05 |



|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Infiltration Pond \#11a | Hydrology File |  | 11 to 11a-F2.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.139166667 |  |  |  |  |
| Receive Flows from: | 11+portion of \# |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
| Roof |  |  |  | 0.95 |  |
| Asphalt | 0.1403 | 250 | 0.038 | 0.95 | 13.0 |
| UnDeveloped Land | 0.0988 | 250 | 3.8\% | 0.2 | 78.3 |
| Pond \#11a | 0.0261 |  |  | 1 |  |
| Total | 0.2652 |  |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.4100 |  |  |  |  |
| Composite Area (ac) | 0.2652 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) | Composite Curve |  |  |  |
|  | 78.3 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr | Storm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 1.05 | 818 | 1.45 | 1,130 |  |
|  | 2.17 off \#10 |  | 2.99 off \#10 |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd (CF/IR/40hr) = SF |  | 147 |  | 203 |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Conical Ellipse - FULL |  |  |  |  |  |
| Full Cone (top dimensions) |  |  |  |  |  |
| Desired Depth | 2 |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Full Size (L1) | 40 |  |  |  |  |
| Base Length 'a' Long Axis radius (ft) | 20 | W |  |  |  |
| Full Size (L2) | 30 |  |  |  |  |
| Base Length 'b' Short Axis radius (ft) | 15 | L |  |  |  |
| Height of Full Cone (based on Side Slope) (ft) h1 | 5.0 | h1 |  |  |  |
| Volume (cf) | 1,571.3 |  |  |  |  |
|  |  |  |  |  |  |
| Missing Cone (bottom dimensions) |  |  |  |  |  |
| Missing Cone Height (ft) h2 | 3.0 |  |  |  |  |
| Base Length 'c' Long Axis radius (ft) | 12.0 | w |  |  |  |
| Base Length 'd' Short Axis radius (ft) | 9.0 | I |  |  |  |
| Volume (missing cone) (cf) | 339 |  |  |  |  |
|  |  |  |  |  |  |
| Truncated Pond Volume (cf) | 1,232 | Greater Than | 1,130 |  |  |
|  |  |  |  |  |  |
| Full Pond Surface Area (sf) | 943 | sf |  |  |  |
| Pond Bottom Surface Area (sf) | 339 | Greater Than | 203 |  |  |

## Basin 70a



This basin collects waters from paved areas $15,17,18$ and conveys waters via sheet flow to channels and then to pond \#70a. \#18 flows to a channel that discharges onto parking area \#17 and then flows to 70a

|  | 10 yr Storm |  | 100 yr Storm |  |
| :---: | :---: | :---: | :---: | :---: |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |
|  | 3.24 | 2,330 | 4.46 | 3,210 |
| Infiltration |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs $(C F / I R / 40 h r)=S F$ | Infiltration Surface Area Req'd (sf) | 419 |  | 577 |

Basin 70a


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pond 70a | Hydrology File |  | 15+17+18 to 70a.hys |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Infiltration Test | Entech PH2 |  |  |  |  |
| Infiltration Rate (inches / hour / sf ) | 1.67 |  |  |  |  |
| Infiltration Rate (IR = ft / hour /sf) | 0.13916666666667 |  |  |  |  |
| Receive Flows from: | 15, 17, 18 |  |  |  |  |
|  | Area (ac) | Reach Length (Ft) | Slope | Coeff (C) | Tc (min) |
|  |  |  |  |  |  |
| Roof |  | 330 | 3.3\% | 0.95 | 15.7 |
| Roads Gravel / Pavers |  |  |  | 0.85 |  |
| Roads Asphalt \#15,\#17,\#18,\#40b | 0.489 | 213 | 4.2\% | 0.95 | 11.6 |
| Land \#40a | 0.074 | 300 | 3.3\% | 0.2 | 89.6 |
| Pond \#70a | 0.054 |  |  | 1 |  |
| Total | 0.617 | ac |  |  |  |
|  |  |  |  |  |  |
| Flow Coefficient of Runoff | 0.950 |  |  |  |  |
| Composite Area | 0.617 |  |  |  |  |
| Composite Curve \# |  |  |  |  |  |
|  |  |  |  |  |  |
| Hydrology Input | Tc (min) |  |  |  |  |
|  | 7.7 |  |  |  |  |
|  |  |  |  |  |  |
|  | 10 yr St | orm | 100 yr | Storm |  |
| Hydrology Output | Qp (cfs) | Vol (cf) | Qp (cfs) | Vol (cf) |  |
|  | 3.24 | 2,330 | 4.46 | 3,210 |  |
|  |  |  |  |  |  |
| Infiltration |  |  |  |  |  |
| Infiltration Surface Area Req'd to drain within 40 hrs (CF/IR/40hr) $=$ SF | Infiltration Surface Area Req'd (sf) | 419 |  | 577 |  |
|  |  |  |  |  |  |
| Pond Sizing - Truncated Conical Ellipse |  |  |  |  |  |
| Full Cone (top dimensions) |  |  |  |  |  |
| Desired Depth | 2 |  |  |  |  |
| Side Slope X:1 | 3 |  |  |  |  |
| Full Size (L1) | 75 |  |  |  |  |
| Base Length 'a' Long Axis radius (ft) | 37.5 | W |  |  |  |
| Full Size (L2) | 40 |  |  |  |  |
| Base Length 'b' Short Axis radius (ft) | 20 | L |  |  |  |
| Height of Full Cone (based on Side Slope) (ft) h1 | 6.7 | h1 |  |  |  |
| Volume (cf) | 5,237.6 |  |  |  |  |
|  |  |  |  |  |  |
| Missing Cone (bottom dimensions) |  |  |  |  |  |
| Missing Cone Height (ft) h2 | 4.7 |  |  |  |  |
| Base Length 'a' Long Axis radius (ft) | 25.5 | W |  |  |  |
| Base Length 'b' Short Axis radius (ft) | 8 | I |  |  |  |
| Volume (missing cone) (cf) | 997 |  |  |  |  |
|  |  |  |  |  |  |
| Truncated Pond Volume (cf) | 4,240 | Greater Than | 3,210 |  |  |
|  |  |  |  |  |  |
| Full Pond Surface Area (sf) | 2357 | sf |  |  |  |
| Empty Pond Surface Area (sf) | 641 | Greater Than | 577 |  |  |


| Storm Runoff - Pre |  | Development |  | 10 Yr Storm |  | 100 Yr Storm |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Rate of Run -off | Volume of Run -off | Rate of Run-off | Volume of Run-off |  |
| Run Free | Basin |  |  | Composite Area (ac) | Composite Coeff RO | Q cfs 10yr | Volume cf 10 yr | Q cfs 100 yr | Volume cf 100yr | Includes |
| Pre Development | South | 3.956 | 0.23 | 2.303 | 20,178 | 3.461 | 30315 |  |
|  | Middle | 9.221 | 0.21 | 3.036 | 24,226 | 4.545 | 36,265 |  |
|  | North | 6.806 | 0.23 | 1.496 | 11,128 | 2.233 | 16,613 |  |
|  |  | Total Pre-Dev RO |  | 3.21 | 55,532 | 10.239 | 83,193 |  |
|  |  |  | Acre Feet |  | 1.27 |  | 1.91 |  |
|  |  |  |  |  |  |  |  |  |
| Storm Runoff - Post Development |  |  |  |  |  |  |  |  |
| Free Flowing off-site | Basin 72 |  |  | 0.86 | 4,458 | 1.27 | 6,563 | 51, 52, 72, 50 |
| Free Flowing off-site | Basin 70 |  |  | 0.86 | 4,907 | 1.27 | 7,251 | 53+54+55+48+70 |
| Free Flowing off-site | \#20+\#21 |  |  | 0.93 | 668 | 1.28 | 920 | 20,21 |
| Free Flowing of-site | Basin 92 |  |  | 0.818 | 3044 | 1.19 | 4426 | 16,66,67 |
|  |  |  |  |  |  |  |  |  |
|  |  | Total Po | st-Dev RO | 3.468 | 13,077 | 5.01 | 19,160 |  |
|  |  |  | duction of : | -0.258 | 42,455 | 5.229 | 64,033 |  |
|  |  |  |  | cfs | cf | cfs | cf |  |
|  |  |  | duction of : |  | 0.97 |  | 1.47 |  |
|  |  |  |  |  | acre-feet |  | acre-feet |  |




|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pond Construction Dimensions |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | From Drainage Plan * |  |  |  | Constructed w/ 6 " freeboard ** |  |  |  |  |
|  |  |  |  | Surface Dimensions, Full |  |  |  | Pond TOP <br> Dimensions |  | Free | Full Volume |  |
| Pond Number | Location | $\begin{aligned} & \text { Pond } \\ & \text { Type } \end{aligned}$ | Shape | L1 | L2 | H | $\begin{gathered} \text { Slope } \\ x: 1 \end{gathered}$ | L1 | L2 | H | CF |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11a | S | 3 | Oval | 40 | 30 | 2 | 3 | 44 | 31.5 | 2.5 | 1,130 |  |
| 40c | SW | 1 | Rectangular | 60 | 25 | 2 | 3 | 63 | 28 | 2.5 | 2,000 |  |
| 54a | SW | 3 | Oval | 20 | 15 | 2 | 3 | 23 | 18 | 2.5 | 1,014 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 58 | NW | 1 | $\sim$ Rectangular | 200 | 30 | 2.5 | 3 | 203 | 33 | 3 | 8,318 |  |
| 59 | E |  | ~ Rectangular | 70 | 19 | 2.25 | 3 | 73 | 22 | 2.75 | 1,917 |  |
| 60 | E | 4 | $\sim$ Rectangular | 40 | 12 | 2 | 3 | 43 | 15 | 2.5 | 774 |  |
| 61 | E | 4 | $\sim$ Rectangular | 50 | 13 | 1.75 | 1 | 53 | 16 | 2.25 | 394 |  |
| 62 | W |  | Rectangular | 70 | 16 | 2.25 | 3 | 73 | 19 | 2.75 | 2,072 |  |
| 70a | SW | 3 | Oval | 75 | 40 | 2 | 3 | 78 | 43 | 2.5 | 3,210 |  |
| 71a | W |  | Series of Pond |  |  |  | 3 | See D | tail |  |  |  |
| 80a | E | 3 | Oval | 37 | 28 | 2 | 3 | 40 | 31 | 2.5 | 954 |  |
| 85 | NW |  | $\sim$ Rectangular | 175 | 15 | 1.25 | 3 | 178 | 18 | 1.75 | 1,842 |  |
| 86 | NW | 1 | ~ Rectangular | 200 | 20 | 1.75 | 3 | 203 | 23 | 2.25 | 4,821 |  |
| 87 | NW | 2 | Triangular | 74 | 104.7 | 3.0 | 3 | 77 | 107.65 | 3.5 | 13,170 |  |
| 88 | Middle | 2 | Triangular |  |  |  | 3 | See D | tail |  | 4,330 |  |
| 89 | NW | 2 | Triangular | 43.00 | 60.81 | 3.00 | 3 | 46 | 63.811 | 3.5 | 2,780 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91 | SE | 3 | Oval | 90 | 63 | 4 | 3 | 93 | 66 | 4.5 | 9,250 |  |
| 93 | NE | 1 | ~ Rectangular | 113 | 30 | 3 | 3 | 116 | 33 | 3.5 | 6,211 |  |
| 94 | NW | 1 | Rectangular | 80 | 30 | 2.5 | 3 | 83 | 33 | 3 | 4,122 |  |
| 95 | NW | 2 | Triangular | 38 | 54 | 3 | 3 | 41 | 57 | 3.5 | 1,960 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Note | Based on | water | volume |  |  |  |  |  |  |  |  |  |
|  | ** Based 0 | const | ructed size |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


|  | Surface Areas List |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sub | Location | Type | Surface | Coeff of RO 10yr | Coeff of RO 100yr | Area (sf) | $\underset{(a c)}{\text { Area }}$ | Area (sq |
| 0 | Pre-Development |  |  |  |  |  |  |  |
| 1 | North Greenhouse (rd \& lot) | P \& D | Gravel | 0.8 | 0.85 | 22,074 | 0.5067 | 0.000792 |
| 2 | not used |  |  | 0.8 | 0.85 | 20,036 | 0.4600 | 0.000719 |
| 3 | NE Lot | P \& D | Paved | 0.9 | 0.95 | 3,243 | 0.0744 | 0.000116 |
| 4 | Maintenance Building Lot | P \& D | Gravel | 0.8 | 0.85 | 5,195 | 0.1193 | 0.000186 |
| 5 | North Lot | P \& D | Paved | 0.9 | 0.95 | 13,004 | 0.2985 | 0.000466 |
|  |  |  |  |  |  |  | 0.4922 |  |
| 6 | NE Gathering Driveway | Driving | Paved | 0.9 | 0.95 | 3,001 | 0.0689 | 0.000108 |
| 7 | Barn Driveway | Driving | Gravel | 0.8 | 0.85 | 2,395 | 0.0550 | 0.000086 |
| 8 | Barn Parking | Parking | Paved | 0.9 | 0.95 | 3,511 | 0.0806 | 0.000126 |
| 9 | East Lot north | P \& D | Paved | 0.9 | 0.95 | 4,044 | 0.0928 | 0.000145 |
| 10 | East Lot middle | P \& D | Paved | 0.9 | 0.95 | 3,222 | 0.0740 | 0.000116 |
| 11 | East Lot south \& South Lot | P \& D | Paved | 0.9 | 0.95 | 6,111 | 0.1403 | 0.000219 |
| 12 | Truck Dock @ Coop | Driving | Paved | 0.9 | 0.95 | 1,965 | 0.0451 | 0.000070 |
| 13 | Staging Area | Storage | Gravel | 0.8 | 0.85 | 3,146 | 0.0722 | 0.000113 |
| 14 | not used |  |  |  |  |  |  | 0.000000 |
| 15 | South Junction | Driving | Paved | 0.9 | 0.95 | 4,471 | 0.1026 | 0.000160 |
| 16 | South Entrance | Driving | Paved | 0.9 | 0.95 | 5,213 | 0.1197 | 0.000187 |
| 17 | SSW Parking | Parking | Paved | 0.9 | 0.95 | 5,209 | 0.1196 | 0.000187 |
| 18 | SW Parking | P \& D | Paved | 0.9 | 0.95 | 6,425 | 0.1475 | 0.000230 |
| 19 | West Entrance | Driving | Paved | 0.9 | 0.95 | 6,042 | 0.1387 | 0.000217 |
| 20 | Truck Dock | Driving | Paved | 0.9 | 0.95 | 5,638 | 0.1294 | 0.000202 |
| 21 | West Entrance (fork) | Driving | Paved | 0.9 | 0.95 | 1,311 | 0.0301 | 0.000047 |
| 22 | West Paking | Xeriscaped |  | 0.05 | 0.25 | 13,861 | 0.3182 | 0.000497 |
| 23 | not used |  |  |  |  |  |  | 0.000000 |
| 24 | NW \& Bathhouse | P \& D | Gravel | 0.8 | 0.85 | 12,045 | 0.2765 | 0.000432 |
| 25 | Main Courtyard | Walking | Pavers | 0.6 | 0.75 | 11,666 | 0.2678 | 0.000418 |
| 26 | Courtyard west of N coop | Walking | Pavers | 0.6 | 0.75 | 5,492 | 0.1261 | 0.000197 |
| 27 | Courtyard west of Vistor Ctr | Walking | Pavers | 0.6 | 0.75 | 992 | 0.0228 | 0.000036 |
| 28 | Courtyard north of Cafe | Walking | Pavers | 0.6 | 0.75 | 6,607 | 0.1517 | 0.000237 |
| 29 | Courtyard between Health \& Ca | Walking | Pavers | 0.6 | 0.75 | 3,153 | 0.0724 | 0.000113 |
|  |  |  |  |  |  |  |  | 0.000000 |
|  | ROOFS |  |  |  |  |  |  | 0.000000 |
|  |  |  |  |  |  |  |  | 0.000000 |
| 30 | EIH | Earth Sheltered |  |  |  | 400 | 0.0092 | 0.000014 |
| 31 | EIH | Earth Sheltered |  |  |  | 563 | 0.0129 | 0.000020 |
| 32 | ElH | Earth Sheltered |  |  |  | 400 | 0.0092 | 0.000014 |
| 33 | ElH | Earth Sheltered |  |  |  | 563 | 0.0129 | 0.000020 |
| 34 | EIH | Earth Sheltered |  |  |  | 400 | 0.0092 | 0.000014 |
| 35 | EIH 6= 2889sf= $5.5 \%$ of \#76 | Earth Sheltered |  |  |  | 563 | 0.0129 | 0.000020 |
| 36 | Maintenance Bldg | Roof |  | 0.9 | 0.95 | 4,752 | 0.1091 | 0.000170 |
| 37 | Barn Bldg | Roof |  | 0.9 | 0.95 | 2,448 | 0.0562 | 0.000088 |
| 38 | Well House | Roof |  | 0.9 | 0.95 | 384 | 0.0088 | 0.000014 |


| 39 | House @ 3890 ORR | Roof | 0.9 | 0.95 | 3,246 | 0.0745 | 0.000116 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | Greenhouse, South | Roof | 0.9 | 0.95 | 4,200 | 0.0964 | 0.000151 |
| 40a | Crescent of land below \#40 | Land |  |  | 3,224 | 0.0740 | 0.000116 |
| 40b | Hard walk below \#40 | Paving |  |  | 1,649 | 0.0379 | 0.000059 |
| 41 | Greenhouse, North | Roof | 0.9 | 0.95 | 4200 | 0.0964 | 0.000151 |
| 42 | Coop Bldg, South | Roof | 0.9 | 0.95 | 4,200 | 0.0964 | 0.000151 |
| 43 | Coop Bldg, North | Roof | 0.9 | 0.95 | 8,750 | 0.2009 | 0.000314 |
| 44 | Health Bldg | Roof | 0.9 | 0.95 | 2,609 | 0.0599 | 0.000094 |
| 45 | Gathering Bldg | Roof | 0.9 | 0.95 | 3,704 | 0.0850 | 0.000133 |
| 46 | Cafe | Roof | 0.9 | 0.95 | 2,712 | 0.0623 | 0.000097 |
| 47 | Visitor Ctr | Roof | 0.9 | 0.95 | 3,335 | 0.0766 | 0.000120 |
| 48 | House @ 3820 ORR | Roof | 0.9 | 0.95 | 2,177 | 0.0500 | 0.000078 |
| 49 | House @ 10855 Howells Rd | Roof | 0.9 | 0.95 | 1,550 | 0.0356 | 0.000056 |
| 50 | House @ 10755 Howells Rd | Roof | 0.9 | 0.95 | 1,932 | 0.0444 | 0.000069 |
| 51 | Bath House | Roof | 0.9 | 0.95 | 931 | 0.0214 | 0.000033 |
| 52 | Yurts $\times 4$ | Roof | 0.9 | 0.95 | 1,812 | 0.0416 | 0.000065 |
| 53 | Craft 1 |  | 0.9 | 0.95 | 1,100 | 0.0253 | 0.000039 |
| 54 | Craft 2 |  | 0.9 | 0.95 | 1,100 | 0.0253 | 0.000039 |
| 54a | Pond 54a |  |  |  | 1,571 | 0.0361 |  |
| 55 | Craft 3 |  | 0.9 | 0.95 | 1,100 | 0.0253 | 0.000039 |
| 56 | North Shed |  |  |  | 877 | 0.0201 | 0.000031 |
| 57 | North Greenhouse | Roof | 0.9 | 0.95 | 4,773 | 0.1096 | 0.000171 |
| 58 | Pond |  |  |  | 6,000 | 0.1377 | 0.000215 |
| 59 | Pond adjacent to Corral |  |  |  | 1,487 | 0.0341 | 0.000053 |
| 60 | Pond west of Barn |  |  |  | 1,024 | 0.0235 | 0.000037 |
| 61 | Pond west of Corral |  |  |  | 802 | 0.0184 | 0.000029 |
| 62 | Pond west of Plaza |  |  |  | 1,894 | 0.0435 | 0.000068 |
| 63 | Swale at south entrance |  |  |  |  | 0.0000 | 0.000000 |
| 64 | Swale at south entrance |  |  |  |  | 0.0000 | 0.000000 |
| 65 | Borders ORR near S Entrance |  |  |  | 2,219 | 0.0509 | 0.000080 |
| 66 | SE corner of 3890 |  |  |  | 13,332 | 0.3061 | 0.000478 |
| 67 | SEE Garden, South |  |  |  | 30,723 | 0.7053 | 0.001102 |
| 68 | Not used |  |  |  |  | 0.0000 | 0.000000 |
| 69 | LAND |  |  |  |  | 0.0000 | 0.000000 |
| 70 | LOT 3820 Old Ranch | Ag / Undevel'd | 0.15 | 0.2 | 73,253 | 1.6817 | 0.002628 |
| 70a | Pond at 3820 ORR |  |  |  | 2,357 | 0.0541 |  |
| 71 | Nursery Stock | Ag / Undevel'd | 0.15 | 0.2 | 56,613 | 1.2997 | 0.002031 |
| 71a | Pollinator Garden |  |  |  |  |  |  |
| 72 | LOT 10655 Howells | Ag / Undevel'd | 0.15 | 0.2 | 67,180 | 1.5422 | 0.002410 |
| 73 | LOT 10755 Howells | Ag / Undevel'd | 0.15 | 0.2 | 33,996 | 0.7804 | 0.001219 |
| 74 | East of Leach Field | Ag / Undevel'd | 0.15 | 0.2 | 15,355 | 0.3525 | 0.000551 |
| 75 | NE Garden | Ag / Undevel'd | 0.15 | 0.2 | 107,949 | 2.4782 | 0.003872 |
| 76 | Hobbit Town | Ag / Undevel'd | 0.15 | 0.2 | 46,774 | 1.0738 | 0.001678 |
| 77 | North of Shop | Ag / Undevel'd | 0.15 | 0.2 | 9,624 | 0.2209 | 0.000345 |
| 78 | Between Shop and Barn | Ag / Undevel'd | 0.15 | 0.2 | 12,665 | 0.2907 | 0.000454 |
| 79 | South of Barn | Ag / Undevel'd | 0.15 | 0.2 | 11,780 | 0.2704 | 0.000423 |
| 80 | Between Barn and 3890 | Ag / Undevel'd | 0.15 | 0.2 | 16,338 | 0.3751 | 0.000586 |
| 80a | Pond \#80a |  |  |  | 354 | 0.0081 |  |
| 81 | LOT 3890 Old Ranch | Ag / Undevel'd | 0.15 | 0.2 | 78,589 | 1.8042 | 0.002819 |
| 81R | LOT 3890 Old Ranch | Ag/Paved |  |  | 38,831 | 0.8914 |  |


| 82 | North of Cafe/Gathering | Ag / Undevel'd |  | 0.15 | 0.2 | 11,359 | 0.2608 | 0.000407 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 83 | 3890 ORR | \#81 subdivided |  |  |  | 33862 | 0.7774 |  |
| 84 | Pond |  |  |  |  |  | 0.0000 |  |
| 85 | Pond, west of corral | Retension |  |  |  |  | 0.0000 |  |
| 86 | Pond, west of \#1 near Bathhouse |  |  |  | 4,073 | 0.0935 |  |  |
| 87 | Pond east of Health |  |  |  |  | 6,119 | 0.1405 |  |
| 88 | Pond (triangular pyramid top) | N\&W of STA |  |  |  | 6134.5 | 0.1408 |  |
| 89 | Pond above STA |  |  |  |  |  | 0.0000 |  |
| 90 |  |  |  |  |  | 0.0000 |  |  |
| 91 | Pond at 3890 ORR |  |  |  |  | 4,455 | 0.1023 |  |
| 92 | Pond at South Entrance |  |  |  |  |  | 0.0000 |  |
| 93 | Pond near Maintenance |  |  |  |  | 2,960 | 0.0680 |  |
| 94 | Pond at 10755 Howells |  |  |  |  |  |  |  |
| 95 | Pond at STA |  |  |  |  |  | 0.6163 |  |
| 96 | Pond 96 in area 70 |  |  |  |  | 1,672 | 0.0384 |  |
| 97 |  |  |  |  |  |  |  |  |

Kess Properties

## Attn: Mark Phelan

Re: Infiltration Rates (Percolation Test Method)
The Shire at Old Ranch
10755 Howells Road
Colorado Springs, Colorado
Dear Mr. Phelan:
As requested, personnel of Entech Engineering, Inc. have performed percolation testing at the above referenced site to evaluate the site soils to determine the infiltration rate for the proposed detention pond.

The testing was performed on October 19 and November 3, 2021. The test locations are shown in Figure 1. The Test Boring Logs, Percolation Test results, Infiltration Rates, and Laboratory Test results are shown in Figures 2 through 6. Soils encountered in the profile and percolation holes consisted of silty sand.

The average percolation rates were 3 to 5 minutes/inch. The percolation rates correspond to adjusted average Infiltration Rate of 1.18 inches/hour for $\mathrm{PH}-1$, and 1.67 inches/hour for PH-2.

We trust that this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,
ENTECH ENGINEERING, INC.


Reviewed by:

Austin M. Nossokoff, P.E. Project Engineer

LLL_jr
Encl.
Entech Job No. 212362
AAprojects/2021/212362 Infiltration Rate


These bore holes are not all located where ponds are - there needs to be infiltration tests for all pond locations.

母TB- APPROXIMATE TEST BORING LOCATIONS AND NUMBERS
母-P- APPROXIMATE PERCOLATION BORING LOCATIONS AND NUMBERS

| TEST BORING LOCATION MAPTHE SHRE AT OLD RANCH1OTF5 HOWELLS RDCOLORAD SPRINGS COFOR: KESS PROPERTIES |  |  |  | JOB NO.: 212362 FIG NO.: |
| :---: | :---: | :---: | :---: | :---: |
| DRAWN: JHR | $12 / 1 / 21$ | $\begin{aligned} & \text { CHECKED: } \\ & \text { AMNN } \end{aligned}$ | DATE: |  |



| PROFILE HOLE LOG |  |  |  |
| :--- | :--- | :--- | :--- |
| DRAWN | DATE | CHECKED | DATE |

## PERCOLATION HOLES

Date Holes Prepared: 10/20/2021
Date Hole Completed:
11/3/2021

Hole No. 1A
Depth: 46"

|  | Time <br> Trial <br> 1 | Water <br> (min.) |
| :---: | :---: | :---: |
| Level <br> Change (in.) |  |  |
| 2 | 10 | 4 |
| 3 | 10 | 7 |
| 10 | 2 |  |

Perc Rate (min./in.): $\qquad$ 5

Hole No. 1B
Depth: 34"

| Trial | Time <br> (min.) | Water <br> Level <br> Change (in.) |
| :---: | :---: | :---: |
| 2 | 10 | 4 |
| 3 | 10 | 2 |
| 2 | 10 | 2 |

Average Perc Rate (min./in.)

Hole No. 2A
Hole No. 2B
Depth: 48"

| Trial | Time <br> (min.) | Water <br> Level <br> Change (in.) |
| :---: | :---: | :---: |
| 2 | 10 | 5 |
| 3 | 10 | 2 |
| 2 | 10 | 3 |

Perc Rate (min./in.): $\qquad$
Depth: 38"

| Trial | Time <br> (min.) | Water <br> Level <br> Change (in.) |
| :---: | :---: | :---: |
| $\frac{10}{3}$ | 10 | 5 |
| 3 | 10 | 2 |

Perc Rate (min./in.): 5

Observer: Nicholas S.
By:


Infiltration Rate (I) = Percolation Rate (P)/Reduction Factor(RF) $\mathrm{I}=\mathrm{P} / \mathrm{RF}$
$R_{f}=\left[\left(2 d_{1}-\Delta d\right) / d i a\right]+1$
$d_{1}=$ initial water depth (in.)
$\Delta d=$ final water level drop (in.)
dia $=$ diameter of the percolation hole (in.)

Test No. P1 (PH-1)

| Perc Rate $=$ | 12 |
| :--- | :---: |
| dia $=$ | 8 |

$\frac{P 1}{d_{1}}=$

$$
\Delta d=
$$

41.0
$R_{f}=$
5.0
$\mathrm{R}_{\mathrm{f}}=$
10.6

## $I=1.13 \quad \mathrm{in} / \mathrm{hr}$

$(\mathrm{PH}-1) \mid$ AVG $=1.19 \mathrm{in} / \mathrm{hr}$

## Test No. P1 (PH-2)

Perc Rate $=20 \mathrm{in} / \mathrm{hr}$
$\mathrm{dia}=\quad 8$
$\frac{P 1}{d}$
$\begin{array}{lc}d_{1}= & 39.0 \\ \Delta d= & 4.0\end{array}$
$R_{f}=\quad 10.3$
$1=1.95 \mathrm{in} / \mathrm{hr}$
$(P H-2) \mid$ AVG $=1.67 \mathrm{in} / \mathrm{hr}$

## CLIENT KESS PROPERTIES

PROJECT THE SHIRE AT OLD RANCH
JOB NO. 212362

Test No. P2 (PH-1)
$\begin{array}{lc}\text { Perc Rate }= & 12 \\ \text { in } & \text { hr } \\ \text { dia }= & 8\end{array}$

## $\frac{\mathrm{P} 2}{\mathrm{~d}_{1}}=$

$\Delta d=\quad 3.0$
$R_{f}=\quad 9.6$

$$
\mathrm{I}=1.25 \mathrm{in} / \mathrm{hr}
$$

Test No. P2 (PH-2)
Perc Rate $=12 \mathrm{in} / \mathrm{hr}$ $\mathrm{dia}=\quad 8$

| $\frac{P 2}{}$ |  |
| :--- | :---: |
| $d_{1}=$ | 33.0 |
| $\Delta d=$ | 5.0 |
| $R_{f}=$ | 8.6 |

$$
\mathrm{I}=1.39 \mathrm{in} / \mathrm{hr}
$$

| UNIFIED CLASSIFICATION | SM | CLIENT | KESS PROPERTIES |
| :--- | :--- | :--- | :--- |
| SOIL TYPE \# | 1 | PROJECT | THE SHIRE AT OLD RANCH |
| TEST BORING \# | P1 | JOB NO. | 212362 |
| DEPTH (FT) | $2-3$ | TESTBY | BL |



| U.S. <br> Sieve \# | Percent <br> Finer |
| :---: | :---: |
| $3^{\prime \prime}$ |  |
| $11 / 2^{\prime \prime}$ |  |
| $3 / 4^{\prime \prime}$ |  |
| $1 / 2^{\prime \prime}$ |  |
| $3 / 8^{\prime \prime}$ | $100.0 \%$ |
| 4 | $97.3 \%$ |
| 10 | $78.5 \%$ |
| 20 | $58.4 \%$ |
| 40 | $47.5 \%$ |
| 100 | $28.0 \%$ |
| 200 | $16.6 \%$ |


| Atterberg |  |
| :--- | :--- |
| Limits |  |
| Plastic Limit | NP |
| Liquid Limit | NV |
| Plastic Index | NP |
|  |  |
| Swell |  |
| Moisture at start |  |
| Moisture at finish |  |
| Moisture increase |  |
| Initial dry density (pcf) |  |
| Swell (psf) |  |


| UNIFIED CLASSIFICATION | SM | CLIENT | KESS PROPERTIES |
| :--- | :--- | :--- | :--- |
| SOIL TYPE \# | 1 | PROJECT | THE SHIRE AT OLD RANCH |
| TEST BORING \# | P2 | POB NO. | 212362 |
| DEPTH (FT) | $2-3$ | TEST BY | BL |



| U.S. <br> Sieve \# | Percent <br> Finer |
| :---: | :---: |
| $3^{\prime \prime}$ <br> $11 / 2^{\prime \prime}$ |  |
| $3 / 4^{\prime \prime}$ |  |
| $1 / 2^{\prime \prime}$ | $100.0 \%$ |
| $3 / 8^{\prime \prime}$ | $99.2 \%$ |
| 4 | $93.5 \%$ |
| 10 | $71.8 \%$ |
| 20 | $51.0 \%$ |
| 40 | $37.5 \%$ |
| 100 | $21.7 \%$ |
| 200 | $15.3 \%$ |

Atterberg
Limits
Plastic Limit Liquid Limit Plastic Index

## Swell

Moisture at start
Moisture at finish
Moisture increase
Initial dry density (pcf)
Swell (psf)


[^0]:    Discuss the proposed sub-basins as well as the historic. Explain in the narrative how water quality requirements are being addressed for all basins. Clearly identify which sub-basins have disturbance and which do not so it is clear which ponds are required for water quality treatment and which are superfluous.

[^1]:    Ponds will be reviewed in further detail once construction drawings are provided for all of the ponds. Ponds should have spillways designed for emergency overtopping.

