



# Preliminary Drainage Report Meadow Lake Industrial Phase 1 El Paso County, Colorado

November 2024

HR Green Project No: 2202774

#### **Prepared For:**

Meadowlake Developments, LLC
Contact: Kevin O'Neil
PO Box 1385
Colorado Springs, CO 80901

#### Prepared By:

HR Green Development, LLC
Contact: Colleen Monahan, P.E., LEED AP
cmonahan@hrgreen.com
(719) 394-2433

PCD File No. SP236



# Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Colleen Monal	nan, P.E., LEED AP	Date
State of Colora	ado No. 56067	
For and on bel	nalf of HR Green Development, L	LC
Owner/D	eveloper's Statemen	i e e e e e e e e e e e e e e e e e e e
I, the owner/deplan.	eveloper have read and will comp	y with all of the requirements specified in this drainage report and
By:		
Authorized Sig	nature	Date
Address:	Meadowlake Developments, LI	С
	PO Box 1385	
	Colorado Springs, CO 80901	
El Paso (	County Statement	
	ance with the requirements of the riteria Manual and Land Develop	e Drainage Criteria Manual, Volumes 1 and 2, El Paso County ment code, as amended.
Joshua Palme	r, P.E.	Date
County Engine	er/ECM Administrator	
Conditions:		



#### > TABLE OF CONTENTS

l.	G	eneral Purpose, Location and Description	3
a	۱.	Purpose	3
b	).	Location	3
C	<b>:</b> .	Description of Property	3
C	۱.	Floodplain Statement	3
II.	D	rainage Design Criteria	3
a	١.	Drainage Criteria	3
III.		Drainage Basins and Subbasins	4
а	١.	Previous Drainage Studies	4
b	).	Existing Subbasin Description	4
C	<b>:</b> .	Proposed Subbasin Description	5
IV.		Drainage Facility Design	8
а	۱.	General Concept	8
b	).	Water Quality & Detention	9
C	<b>:</b> .	Inspection and Maintenance	9
C	l.	Four Step Method to Minimize Adverse Impacts of Urbanization	10
e	).	Drainage and Bridge Fees	10
f.		Opinion of Probable Cost	10
g	J.	Hydraulic Grade Line Analysis	10
٧.	S	ummary	11
VI.		Drawings	11
1/11		Poforoncos	11

#### > APPENDICES

- A. Vicinity Map, FEMA Map, NRCS Soil Survey
- B. Hydrologic Analysis
- C. Hydraulic Analysis
- D. Water Quality and Detention Calculations
- E. Drainage Maps



# I. General Purpose, Location and Description

#### a. Purpose

The purpose of the Preliminary Drainage Report (PDR) for Meadow Lake Industrial Phase 1 is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls.

#### b. General Location

Meadow Lake Industrial is 254 acres of undeveloped land. Meadow Lake Industrial Phase 1, referred to as 'the site' herein, is a 51.3-acre portion of the overall 254 acres that is zoned for Industrial and will be developed as an industrial subdivision. The remaining area will be undeveloped.

The site lies within a part of the east half of Section 9, Township 13 South, Range 64 West of the 6<sup>th</sup> P.M., El Paso County, Colorado. The site is bound to the north and west by undeveloped unplatted land, to the east by Curtis Road, and to the south by Falcon Highway. There are A vicinity map is presented in Appendix A.

#### c. Description of Property

The property is currently undeveloped and unplatted. Meadow Lake Industrial Phase 1 will plat 27 industrial lots and two drainage tracts on approximately 51.3 acres. The overall site is generally bisected by a ridge that directs stormwater east towards Curtis Road and west towards an unnamed tributary. The unnamed tributary runs north-south through the overall site, however; all development will occur east of the tributary.

The Phase 1 site is part of two major drainage basins: Haegler Ranch Basin and Solberg Ranch Basin. The basins are depicted on the drainage maps in Appendix E.

There are no existing utilities and no known irrigation facilities on the site. Onsite vegetation consists primarily of native grasses and weeds. The topography is gently sloping with 2-4% grades. Per a NRCS web soil survey, the site's soil is comprised of Type A soils: Blakeland loamy sand, Truckton loamy sand and Columbine gravelly sandy loam, Type B soil Stapleton sandy loam, and Type D soil Fluvaquentic Haplaquolls. A NRCS soil survey is presented in Appendix A.

#### d. Floodplain Statement

Based on FEMA FIRM 08041C0558G & 08041C0566G, revised December 7, 2018, there are no floodplains (Zone A or Zone X) within the Phase 1 boundary. Zone A areas are determined to be within the 1.0% annual chance flood but do not have base flood elevations established. Zone X are areas determined to be outside the 0.2% annual chance flood. The FIRM is presented in Appendix A.

# II. Drainage Design Criteria

#### a. Drainage Criteria

Hydrologic data and calculations were performed using the El Paso County Drainage Criteria Manual Volume 1 & 2 (EPCDCM), with current revisions.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from CCSDCM Table 6-2. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1. The detention pond allowable release rate will be limited to less than historic rates.



Table 6-2: Rainfall Depths for El Paso County							
Return Period (yr) 5 100							
1-hr Rainfall Depth (in)	1.50	2.52					

Inlets were sized per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer was sized per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

# III. Drainage Basins and Subbasins

#### a. Major Basin Descriptions

The site is part of two major drainage basins: Haegler Ranch Basin and Solberg Ranch Basin. The basins are depicted on the drainage maps in Appendix E. Of the 51.3 acres of Meadow Lake Industrial Phase 1, approximately 8.75 acres of the north part of the site drains to an existing roadside swale in Curtis Road that then travels northerly as part of Haegler Ranch Basin, ultimately draining to Chico Creek. The remainder of the south side of site, 42.55 acres, lies within Solberg Ranch Drainage Basin and drains to the unnamed tributary on the site to a culvert on the north side of Falcon Highway to under Falcon Highway and ultimately to Chico Creek.

The Haegler Ranch drainage basin was studied in the "Haegler Ranch Basin Drainage Basin Planning Study" in May 2009. The Solberg Ranch Basin does not have an associated Drainage Basin Planning Study.

#### b. Previous Drainage Studies

A portion of the site was previously studied as part of the Haegler Ranch Basin Drainage Basin Planning Study (DBPS), dated May 2009, by URS. Haegler Ranch is an unnamed tributary, eventually tributary to Black Squirrel Creek. The overall Haegler Ranch Basin flows to the southeast from north of Eastonville Road to McDaniels Road with a total of 16.6 sq mi in El Paso County, Colorado. Much of the existing basin consists of 2- and 5- acre residential lots surrounded by open space range land with gently rolling topography used for agriculture and later parcels with homes. Some higher density residential is planned in the northern part of the basin. The study did not identify any drainage concerns or recommendations for the site.

A portion of the site lies within Solberg Ranch Basin. Solberg Ranch does not have a Drainage Basin Planning Study (DBPS) on file with El Paso County.

#### c. Existing Subbasin Description

Basin EX1 is 8.75 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 3.4$  cfs  $Q_{100} = 18.3$  cfs) flows east offsite in a roadside ditch adjacent to Curtis Road to DP2. Flows from DP2 drain north offsite.

Basin EX2 is 30.77 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 9.5$  cfs  $Q_{100} = 57.8$  cfs) flows south in a roadside ditch adjacent to Curtis Road to DP4. Flows from DP4 are then conveyed south through Basin EX3 to DP6.

Basin EX3 is 13.39 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 4.5$  cfs  $Q_{100} = 25.4$  cfs) flows south in a roadside ditch adjacent to Curtis Road to DP6. Flows from DP6 are then conveyed south through Basin OS3 to DP7.



Basin EX4 is 7.03 acres of undeveloped area. Stormwater ( $Q_5 = 2.1$  cfs  $Q_{100} = 14.3$  cfs) flows west towards OS4 at DP8.

Basin OS1 is 2.83 acres of undeveloped area. Stormwater ( $Q_5 = 1.0$  cfs  $Q_{100} = 6.7$  cfs) flows east towards EX1 at DP1. Flows from DP1 are then conveyed east through Basin EX1, ultimately draining to DP2.

Basin OS2.1 is 5.34 acres of undeveloped area. Stormwater ( $Q_5 = 1.8$  cfs  $Q_{100} = 11.9$  cfs) flows southeast towards EX2 at DP3. Flows from DP3 are then conveyed southeast through Basin EX2 to DP4.

Basin OS2.2 is 0.37 acres of undeveloped area. Stormwater ( $Q_5 = 0.1$  cfs  $Q_{100} = 0.9$  cfs) flows southeast towards EX3 at DP5. Flows from DP5 are then conveyed southeast through Basin EX3 to DP6.

Basin OS3 is 3.96 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 2.1$  cfs  $Q_{100} = 9.2$  cfs) flows south in a roadside ditch adjacent to Curtis Road to DP7. Flows from DP7 are then conveyed west through Basin OS4, ultimately draining to DP9.

Basin OS4 is 40.63 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 10.7$  cfs  $Q_{100} = 64.7$  cfs) flows south towards an existing public box culvert and offsite at DP9.

Basin EROW4 is 1.48 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 2.1$  cfs  $Q_{100} = 4.6$  cfs) flows south in an existing roadside ditch adjacent to Curtis Road to DP10. Flows from DP10 continue south and are then conveyed west via an existing culvert underneath Curtis Road. The existing culvert (unknown size & material) outfalls into Basin OS4, ultimately draining to DP9.

#### d. Proposed Subbasin Description

Basin A is 5.78 acres of roadway and undeveloped area. Stormwater ( $Q_5 = 8.4$  cfs  $Q_{100} = 19.9$  cfs) is captured at DP1 in a public 10' Type R sump inlet. In the event of inlet failure at DP1, an overflow path is provided in Sundrop View to Pond A. Basin A will be treated and detained in Pond A.

Basin B is 1.10 acres of roadway and lot area. Stormwater ( $Q_5 = 3.6$  cfs  $Q_{100} = 6.6$  cfs) is captured at DP2 in a public 5' Type R sump inlet. In the event of inlet failure at DP2, an overflow path is provided in Sundrop View to Pond A. Basin B will be treated and detained in Pond A.

Basin C is 3.01 acres of industrial lots and roadway. Stormwater ( $Q_5 = 7.0$  cfs  $Q_{100} = 13.9$  cfs) is captured at DP3 in a private 20' Type R on-grade inlet in Sundrop View. In the event of inlet failure at DP3, an overflow path is provided in Sundrop View to Pond A. Basin C will be treated and detained in Pond A.

Basin D is 3.05 acres of industrial lots and roadway. Stormwater ( $Q_5 = 7.3$  cfs  $Q_{100} = 14.6$  cfs) is captured at DP4 in a private 20' Type R on-grade inlet in Sundrop View. In the event of inlet failure at DP4, an overflow path is provided in Sundrop View to Pond A. Basin D will be treated and detained in Pond A.

Basin E is 3.68 acres of industrial lots and roadway. Stormwater ( $Q_5 = 8.8$  cfs  $Q_{100} = 17.5$  cfs) is captured at DP5 in a private 15' Type R sump inlet in Sundrop View. In the event of inlet failure at DP5, an overflow path is provided in Sundrop View to Pond A by overtopping the curb and gutter at the knuckle. Basin E will be treated and detained in Pond A.

Basin F is 1.10 acres of industrial lots and roadway. Stormwater ( $Q_5 = 2.8$  cfs  $Q_{100} = 5.2$  cfs) is captured at DP6 in a private 15' Type R sump inlet in Sundrop View. In the event of inlet failure at DP6, an overflow path is provided in Sundrop View to Pond A by overtopping the curb and gutter at the knuckle. Basin F will be treated and detained in Pond A.



Basin G is 6.75 acres of industrial lots and undeveloped area. Stormwater ( $Q_5 = 2.0$  cfs  $Q_{100} = 13.5$  cfs) will remain undisturbed in this phase of development. Basin G will drain north offsite as part of the Haegler major drainage basin.

Basin H is 3.71 acres of industrial lots and undeveloped area. Stormwater ( $Q_5 = 7.7$  cfs  $Q_{100} = 15.8$  cfs) is conveyed southeast via sheet flow into a proposed swale. The proposed swale drains south to DP8, and continues to drain in the proposed swale south ultimately to the FES inlet at DP9 into Pond A. Basin H will be treated and detained in Pond A.

Basin I is 1.12 acres of industrial lots and undeveloped area. Stormwater ( $Q_5 = 2.1$  cfs  $Q_{100} = 4.6$  cfs) is conveyed southeast via sheet flow into a proposed swale. The proposed swale drains south to DP9, then into the FES inlet at DP9 into Pond A. Basin I will be treated and detained in Pond A.

Basin J is 3.14 acres and contains Pond A. Stormwater ( $Q_5 = 3.0$  cfs  $Q_{100} = 9.6$  cfs) sheet flows directly to Pond A. Basin J will be treated and detained in Pond A.

Basin K is 0.24 acres of roadway. Stormwater ( $Q_5 = 1.0$  cfs  $Q_{100} = 1.9$  cfs) is captured at DP11 in a public 10' Type R on grade inlet on Sagebrush Street. In the event of inlet failure at DP11, an overflow path is provided to Curtis Road. DP 11 drains south to DP 12, ultimately draining via a proposed swale to the FES inlet at DP 21.2. Basin K will be treated and detained in Pond B.

Basin L is 0.24 acres of roadway. Stormwater ( $Q_5 = 1.0$  cfs  $Q_{100} = 1.9$  cfs) is captured at DP12 in a public 10' Type R sump inlet in Sagebrush Street. In the event of inlet failure at DP12, an overflow path is provided to Curtis Road. DP 12 drains south to DP 12.1, ultimately draining via a proposed swale to the FES inlet at DP 21.2. Basin L will be treated and detained in Pond B.

Basin M and DP14 have been omitted as they are an old basin and design point that have been removed. In order to keep all calculations consistent within this report, the proceeding basin designations and design points have not changed and remain sequential.

Basin N1 is 2.07 acres of industrial lots and roadway. Stormwater ( $Q_5 = 4.9$  cfs  $Q_{100} = 9.8$  cfs) is captured at DP15 in a public 10' Type R on-grade inlet in Mariposa Lily Grove. In the event of inlet failure at DP15, an overflow path is provided within the adjacent public roadway and access road that drains south to Pond B. Basin N1 will be treated and detained in Pond B.

Basin N2 is 0.25 acres of industrial lots and roadway. Stormwater ( $Q_5 = 1.2$  cfs  $Q_{100} = 2.1$  cfs) is captured at DP15.1 in a public 5' Type R on-grade inlet in Mariposa Lily Grove. In the event of inlet failure at DP15.1, an overflow path is provided within the adjacent public roadway and access road that drains south to Pond B. Basin N1 will be treated and detained in Pond B.

Basin N3 is 1.84 acres of industrial lots and roadway. Stormwater ( $Q_5 = 4.8$  cfs  $Q_{100} = 9.6$  cfs) drains southwest onto Aspen Daisy Drive at DP15.2. Drainage then continues south on Aspen Daisy Drive in subbasin R to a public sump 10' Type R inlet at DP 19. See Basin N3 will be treated and detained in Pond B.

Basin O is 2.10 acres of industrial lots and roadway. Stormwater ( $Q_5 = 5.9$  cfs  $Q_{100} = 11.8$  cfs) is captured at DP16 in a private 10' Type R on-grade inlet in Zinnia Point. In the event of inlet failure at DP16, an overflow path is provided within the adjacent public roadway and access road that drains south to Pond B. Basin O will be treated and detained in Pond B.

Basin P1 is 0.25 acres of industrial lots and roadway. Stormwater ( $Q_5 = 1.2$  cfs  $Q_{100} = 2.1$  cfs) is captured at DP17 in a private 5' Type R on-grade inlet in Zinnia Point. In the event of inlet failure at DP17, an overflow



path is provided within the adjacent public roadway and access road that drains south to Pond B. Basin P1 will be treated and detained in Pond B.

Basin P2 is 2.05 acres of industrial lots and roadway. Stormwater ( $Q_5 = 2.4$  cfs  $Q_{100} = 11.4$  cfs) is captured at DP20.2 in a private Type C sump inlet at the southwest corner of the site. In the event of inlet failure at DP20.2, an overflow path is provided directly into Pond B. Basin P2 will be treated and detained in Pond B.

Basin Q is 1.02 acres of roadway. Stormwater (Q<sub>5</sub> = 3.2 cfs Q<sub>100</sub> = 6.2 cfs) is captured at DP18 in a public 5' Type R sump inlet in Aspen Daisy Drive. In the event of inlet failure at DP18, flows will overtop the sump and flow to Pond B along the maintenance access road. Basin Q will be treated and detained in Pond B.

Basin R is 1.43 acres of roadway. Stormwater ( $Q_5 = 2.1$  cfs  $Q_{100} = 6.8$  cfs) is captured at DP19 in a public 10' Type R sump inlet in Aspen Daisy Drive. In the event of inlet failure at DP19, flows will overtop the sump and flow to Pond B along the maintenance access road. Basin R will be treated and detained in Pond B.

Basin S1 is 1.16 acres of industrial lots and grass swale. Stormwater ( $Q_5 = 2.9$  cfs  $Q_{100} = 5.8$  cfs) is captured by a proposed swale and conveyed south to DP21. Runoff will continue south in the proposed swale, ultimately draining to an FES inlet structure at DP 21.2 and into Pond B. Basin S1 will be treated and detained in Pond B.

Basin S2 is 2.32 acres of industrial lots and grass swale. Stormwater ( $Q_5 = 5.3$  cfs  $Q_{100} = 10.6$  cfs) is captured by a proposed swale and conveyed south to DP21.1. Runoff will continue south in the proposed swale,

ultimately draining to an FES inlet structure identify that analysis of the roadside in Pond B.

ated and detained ditch will be required for the FDR. How Basin S3 is 1.16 acres of industrial lots and will the increase in flows be mitigated

9 cfs) is captured ucture at DP 21.2

by a proposed swale and conveyed south in the interim prior to development of and into Pond B. Basin S3 will be treated a lots 1 and 15 within basin G?

Basin T is 1.42 acres and contains Pond B Pond B. Basin T will be treated and detain

ows directly to

Basin OS1 2.83 acres of undeveloped land. Stormwater (Q<sub>5</sub> = 1.0 cfs Q<sub>100</sub> = 6.7 cfs) flows east into subbasin G at DP E1.

Basin ROW1 is 2.17 acres of right of way. Stormwater ( $Q_5 = 2.3$  cfs  $Q_{100} = 6.5$  cfs) flows north in a roadside ditch adjacent to Qurtis Road to DP E2. An additional 6' paved shoulder and 2' gravel shoulder has been added to Curtis Road in proposed conditions and accounted for in drainage calculations. There is a small increase in flow to DP E2 from basin ROW1. The future detention basin(s) within subbasin G should account for this increase and restrict flow from the future stormwater detention basins back to historic rates at DP E2. WQ for the improvements within basin ROW1 will be excluded from treatment per ECM exclusion I.7.1.B.2. The additional pavement proposed in this basin is part of a total additional pavement draining untreated offsite of 0.67 acres. The total additional paved area is less than 1 acre per mile draining offsite untreated.

Basin ROW2 is 3.25 acres of right of way. Stormwater ( $Q_5 = 3.6$  cfs  $Q_{100} = 9.6$  cfs) flows south in a roadside ditch adjacent to Curtis Road to DP 13. A widening resulting from the northbound turn lane & 6' paved shoulder and 2' gravel shoulder has been added to Curtis Road in proposed conditions and accounted for in drainage calculations. Runoff is captured in a 18" FES inlet which drains to the 10' Type R inlet at DP 11. Runoff ultimately drains south via a proposed drainage swale to Pond B. Basin ROW2 will be treated and detained in Pond B.



Basin ROW3 is 6.85 acres of right of way. Stormwater ( $Q_5 = 5.2$  cfs  $Q_{100} = 15.8$  cfs) flows south in a roadside ditch adjacent to Curtis Road to DP E9. A widening for a northbound turn lane & 6' paved shoulder and 2' gravel shoulder has been added to Curtis Road in proposed conditions and accounted for in drainage calculations. WQ for the improvements within basin ROW1 will be excluded from treatment per ECM exclusion I.7.1.B.2. The additional pavement proposed in this basin is part of a total additional pavement draining untreated offsite of 0.67 acres. The total additional paved area is less than 1 acre per mile draining offsite untreated.

should this be Falcon

Basin OS4 is 40.02 acres Hwy? water ( $Q_5 = 10.5$  cfs  $Q_{100} = 63.9$  cfs) flows south in the unnamed tributary to DP E9.

Basin ROW4 is 1.48 acres of undeveloped area and paved roadway. Stormwater ( $Q_5 = 2.3$  cfs  $Q_{100} = 4.9$  cfs) drains south to via an existing roadside ditch along Curtis Road to DP E10. An additional 2' paved and gravel shoulder on the east side of Curtis Road has been accounted for in drainage calculations. The proposed peak flow from drainage basin RQW4 to design point E10 is higher than historic flow rates due to the paved roadway of Curtis Road being widened for the shoulder. An analysis of the existing swale at DP E10 will be provided with the FDR. Flows from DP E10 continue south and are then conveyed west via an existing culvert underneath Curtis Road. The existing culvert (unknown size & material) outfalls into Basin ROW2, ultimately draining to DP9. WQ for the improvements within basin ROW4 will be excluded from treatment per ECM exclusion I.7.1.B.2. The additional pavement proposed in this basin is part of a total additional pavement draining untreated offsite of 0.67 acres. The total addit Revise statement as E2 does e draining offsite untreated.

increase as stated above and A total flow summary of existing vs. proposed design r listed in the table II not be

increased (Design points E2 & E9).

Table 1 – DP Flow Comparison								
DESIGN POINT	EX Q₅ (cfs)	PR Q <sub>100</sub> (cfs)						
E1	1.0	1.0	6.7	6.7				
E2	4.2	5.0	23.9	25.2				
E4	10.9	0.8	67.6	13.8				
E7	15.0	6.0	81.2	29.6				
E8	2.1	1.5	14.3	14.0				
E9	24.2	19.8	138.8	121.3				
E10	2.1	2.3	4.6	4.9				

# **Drainage Facility Design**

#### a. General Concept

For all Meadow Lake Phase 1 lots draining to Solberg Ranch Drainage Basin, storm water will be collected and conveyed by a series of inlets, swales and storm sewer to two full spectrum water quality and detention ponds. The full spectrum water quality and detention ponds will discharge at less than historic rates.

verify spillway



For all Meadow Lake Phase 1 lots draining to Haegler Ranch Drainage Basin, onsite water quality and detention shall be the responsibility of the future property owner and shall be designed at the time of site development plan application.

#### b. Water Quality & Detention

<u>Lots 1 & 15 (Basin G)</u> - Haegler Ranch Drainage Basin - Lots 1 and 15 (Basin G on proposed conditions map) will provide their own detention and water quality treatment at time of Site Development Plan that will discharge to the Haegler Ranch Drainage Basin as it has gone historically. The future detention basin(s) within subbasin G should account for the increase in flow from basin ROW1 and restrict flow from the future stormwater detention basins to historic rates at DP E2.

#### Pond A - Solberg Ranch Drainage Basin

Water quality and detention for Basins A – F, and H - J is provided in a full spectrum water quality and detention pond: Pond A. Pond A is located in Tract A. A total of 25.69 acres at 65% imperviousness will be detained in the pond. The WQCV is 0.544 ac-ft, the EURV is 2.012 ac-ft, and the approximate 100-year detention volume is 3.050 ac-ft. The WQCV, EURV and 100-year storms are released in 41, 71 and 73 hours, respectively. A forebay is located at the outfall into the pond and a 40" trickle channel conveys flow towards the outlet structure. A 15' wide ramp at a slope no greater than 12% slope is provided to the bottom of the pond to facilitate future maintenance. A 45' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Curtis Road. The spillway will be lined with Type L riprap. The outfall for the pond drains into a proposed roadside swale adjacent to Curtis Street. The total flow to this outfall point (DP E4) will remain at or less than existing flowrates for the minor and major storms. Analysis of the proposed roadside swale will be provided with the Food spillway on the drainage plan and

#### Pond B - Solberg Ranch Drainage Basin

Water quality and detention for Basins K – T and ROW2 is provided in a full detention pond: Pond B. Pond B is located in Tract B. A total of 20.80 acres at 68% imperviousness will be detained in the pond. The WQCV is 0.462 ac-ft, the EURV is 1.602 ac-ft, and the approximate 100-year detention volume is 2.496 ac-ft. The WQCV, EURV and 100-year storms are released in 40, 70, and 70 hours, respectively. A forebay is located at the outfall into the pond and a 40" trickle channel conveys flow towards the outlet structure. A 15' wide ramp at a slope no greater than 12% slope is provided to the bottom of the pond to facilitate future maintenance. A 85' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Curtis Road. The spillway will be lined with Type L riprap. The outfall for Pond B will be into a level spreader at DP8. The level spreader has been designed to drain runoff discharging from Pond B the same as existing conditions. Runoff draining from Pond B will be restricted so that there is no increase in the total runoff discharging to design point E8. The ultimate outfall of the pond is to DP E9, the un-named tributary. Pond design calculations are presented in Appendix D.

#### c. Inspection and Maintenance

The private detention ponds are to be owned and maintained by a metropolitan district, to be established with the project. Maintenance access for the full spectrum detention facilities will be provided through private drainage easements and tracts. A maintenance agreement with the County is required and will be provided with Final Drainage Report for this project.



#### d. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Two onsite full spectrum detention ponds provide water quality treatment for the majority of the site. The WQCV is released over a period of 40 hours.

Lots 1 and 15 (Basin G on proposed conditions map) will provide their own detention and water quality treatment at time of Site Development Plan that will discharge to the Haegler Ranch Drainage Basin as it has gone historically.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 – Consider the need for source controls: This project has no need for specialized source controls.

#### e. Drainage and Bridge Fees

Solberg Ranch - 2024 Drainage Basin / Bridge Fees										
Drainage Fee/Impervious Acre	Bridge Fee/Impervious Acre	Site Acreage	Site Impervious	Impervious Acres	Drainage Fee	Bridge Fee				
\$24,832.00	\$0	44.55	77%	34.30	\$851,737.60	\$0				

Haegler Ranch - 2024 Drainage Basin / Bridge Fees										
Drainage Fee/Impervious Acre	Bridge Fee/Impervious Acre	Site Acreage	Site Impervious	Impervious Acres	Drainage Fee	Bridge Fee				
\$13,971.00	\$2,062.00	6.75	77%	5.20	\$72,649.20	\$10,722.40				

#### f. Opinion of Probable Cost

An engineer's opinion of probable cost is presented will be provided with the Final Drainage Report submittal.

#### g. Hydraulic Grade Line Analysis

A hydraulic grade line analysis of the proposed storm will be provided with the Final Drainage Report submittal.



# V. Summary

Meadow Lake Industrial Phase 1 lies within the Solberg Ranch Drainage Basin and the Haegler Ranch Basin Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds for all lots draining to the Solberg Ranch Drainage Basin in Ponds A and B. For Lots 1 and 15 draining to the Haegler Ranch Drainage Basin, they will provide their own detention and water quality treatment at time of Site Development Plan that will discharge to the Haegler Ranch Drainage Basin as it has gone historically. The water quality and detention ponds will be owned and maintained by a metropolitan district, to be established with the project. All drainage facilities were sized per the El Paso County Drainage Criteria Manuals. Offsite basins will not be affected by this project. The existing unnamed channel west of the proposed development will not be affected or its condition modified. The runoff release of the site is less than existing rates to the ultimate outfall point into the channel and with appropriate controls as described herein. Downstream and surrounding properties will not be adversely affected by this developments flows.

# VI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.

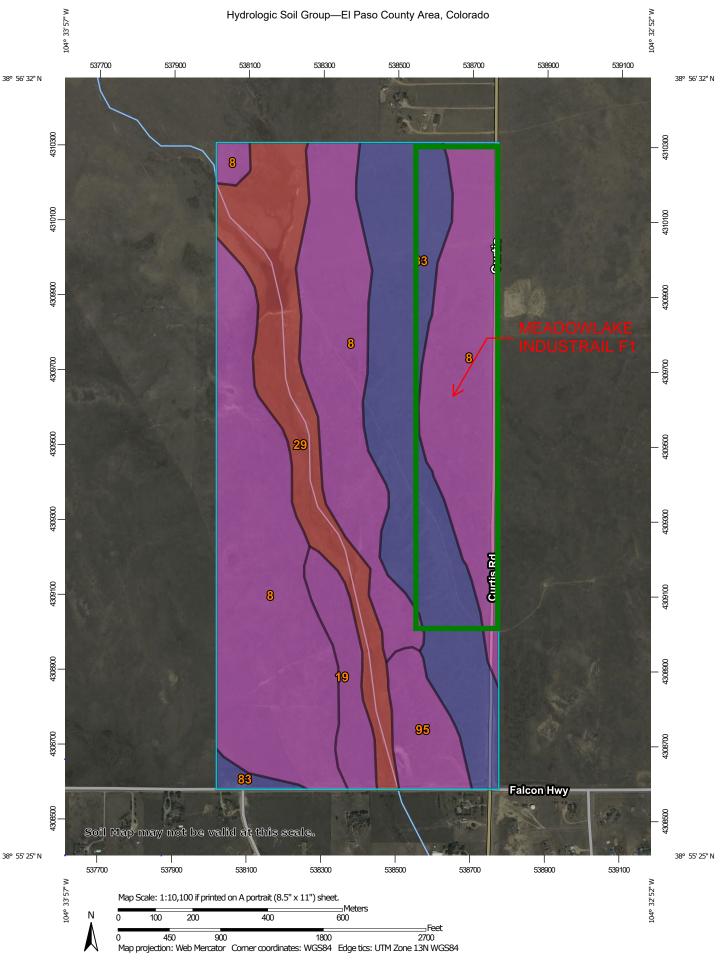
# VII. References

- 1. Haegler Ranch Basin Drainage Basin Planning Study (DBPS), dated May 2009, by URS
- 2. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 3. Drainage Criteria Manual of El Paso, Colorado, October 2018.
- 4. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.



APPENDIX A - VICINITY MAP, SOIL MAP, FEMA MAP

efs: EPC\_Parcels; 8.5x11\_Titleblock



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Sep 11, 2018—Oct 20. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

# **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	А	174.3	53.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	13.3	4.1%
29	Fluvaquentic Haplaquolls, nearly level	D	47.2	14.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	75.9	23.4%
95	Truckton loamy sand, 1 to 9 percent slopes	А	14.0	4.3%
Totals for Area of Inter	est		324.7	100.0%

#### **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

#### **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

#### NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for nossible undested or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) andorf Rodoways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summay of Stituted Elevations tables contained within the Flood insurance Subjuly (FIS) expert that excorragants the First III. Users the subjuly of the Flood of the Flood and the Flood and the Flood elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation formation. Accordingly, flood elevation data presented in the FIG report should be utilized in conjunction with the FRM for purpose of construction and for flood insurance flood manufactures.

Coastal Base Flood Elevations shown on his map apply only landward of 0.0" North Interest of the Coastal Board Co

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The **floodways** were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insuranc Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercatic (UTIN) zone 13. The horizontal datum was NADS3, GRS60 aphenot. GRS60 ap

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVOSS). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey webbing of the North Carbon (Programme Vertical Datum of 1988), visit the National Geodetic Survey webbing of the North Carbon (Programme Vertical Datum of 1988), visit the National Geodetic Survey web visit to the National Geodetic Survey with the National Geodetic Su

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench mark shown on this map, please contact the Information Services Branch of the Nationa Geodelic Survey at (301) 713-3242 or visit its website at http://www.ngs.noas.gow/.

Base Map information shown on this FIRM was provided in digital format by EI Past County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

The map reflects more detailed and up to date stream channel configurations and floodplain definestions than those shown on the previous FRDM for this jurisdiction. The production of the previous FRDM for this jurisdiction, the production of the

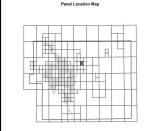
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Usiling of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information aCknape (FIXX) 14877-582672 for Information on available protects associated with the FIRM. Available products may include previously issued Letters of Map Change, a FIX of India March 1487-6426 (FIXED March 1487-6426) for Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

If you have questions about this map or questions concerning the National Floor Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

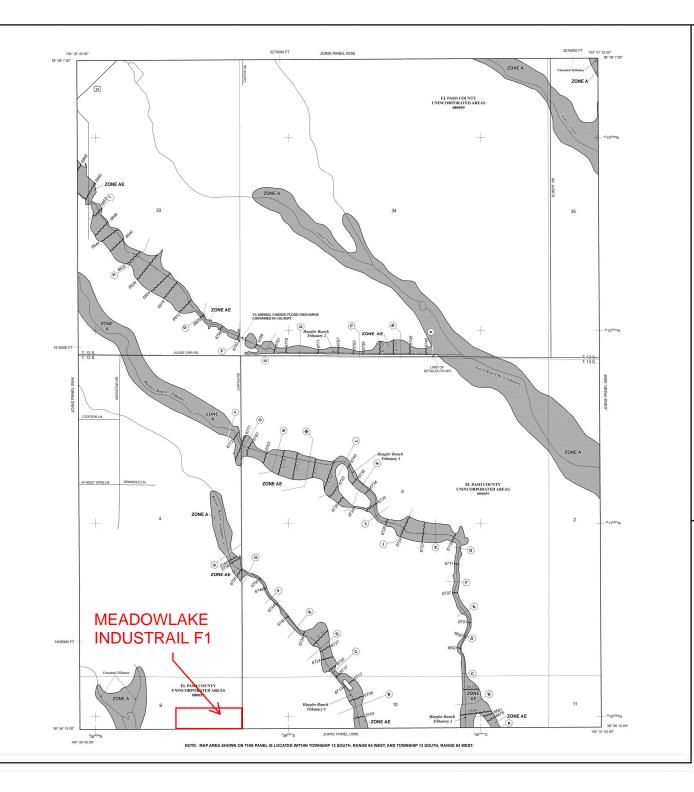
# Asist the FEMA website at http://www.foma.gov/business/nfp. EI Paso County Vertical Datum Offset Table Vertical Tolkium Flooding Source Flooding Source REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSUMANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (TEMA).



Additional Flood Hazard information and resources an available from local communities and the Colorado



**LEGEND** 

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard Area is A. A.E., A.H., A.M., A.M., A.W., A.W., A.W. A.W. A.W. The Base Flood Biraction is the water-surface elevation of the 1% annual chance flood.

The floodway is the channel of a stream plus any adjacent floodplain areas that must be largit free of encreachment so that the 1% annual chance flood can be carried without subctantial increases in flood healths

Areas in which flood hazards are undetermined, but possible

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
 Base Flood Elevation line and value; elevation in feet\*
 Base Flood Elevation value where uniform within zone; elevation in feet\*

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

for community map revision history prior to countywide mapping, refer to the Community rigo History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the historial Flood Insurance Program at 1-800-638-6620.

> 250 0 500 1000 HHH FEET

> > FIRM

CONTAINS:

COMMUNITY

PANEL 0558G

FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS
PANEL 558 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

NUMBER PANEL SUFFIX

MAP NUMBER 08041C0558G

DECEMBER 7, 2018

Federal Emergency Management Agency

Zone D Boundary

ZONE VE

OTHER AREAS

(A)—(A)

97° 07° 30.00° 32° 22° 30.00°

6000000 FT

DX5510\_

No Base Flood Elevations determined.
Base Flood Elevations determined.
Flood depits of 1 to 3 feet (usually areas of ponding); Base Flood
Elevations determined.

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

#### NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood instances Stady (FIS) great that accompanies the FIRM. Users that the Companies of the FIRM state of the Global state of the FIRM for purposes of construction and for flood instances rating purposes only and should not be used as the sale source of flood elevation formation. Accordingly, Stood elevation data presented in the FIRM for purpose of construction and for flooding in management.

Coastal Base Flood Elevations shown on his map apply only lands at 0 0.7 North the property of the property o

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Opecial Flood Hazard Areas may be protected by flood contro structures. Refer to section 2.4 "Flood Protection Measures" of the Flood insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTIN) zone 13. The horizontal datum was NADSS, GRSS0 aphrenic production of Filter for adjust instead to the production of Filter for adjust instead to product of filter for adjust instead to the production of Filter for adjust to adjust on the differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. Or information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1989, visit the National Geodetic Survey verbase is http://www.ngs.noaa.gov/ or contact the National Geodetic Survey verbase for coldresses.

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench mark** shown on this map, please contact the Information Services Branch of the Nation Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gow/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

The map reflects more detailed and up to date stream channel configurations and floodplain definestions than those shown on the previous FRDM for this jurisdiction. The production of the previous FRDM for this jurisdiction, the production of the

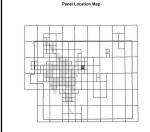
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Usiling of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (NSC) is the FEMA Map Information Acknaps (FMMX) 1477-382227 for information on available protects associated with the FIRM. Available products may include proviously issued Letters of Map Change, as Flood Insurance Study Report, and/or digital versions of this map. The NSC may also be reached by Fax at 1-800-359-9620 and its website at Intity/how/msc-fema.gov/.

If you have questions about this map or questions concerning the National Floor Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

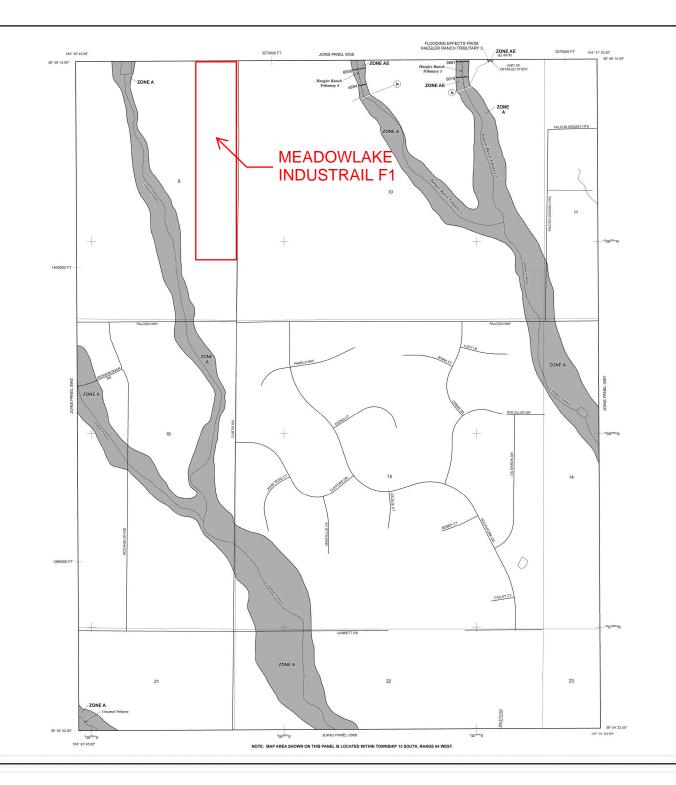
# E Pago County Vertical Datum Offset Table Flooding Source Flooding Flo



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEM).



Additional Flood Hazard information and resources an available from local communities and the Colorado







side to User. The Map Number shown below should be used en placing map orders. The Generality Number shows one placing map orders. The Generality Number shows one should be used on insurance applications for the subject morning.

MAP NUMBER
08041C0566G



MAP REVISED DECEMBER 7, 2018 Federal Emergency Management Agency



**APPENDIX B - HYDROLOGIC CALCULATIONS** 



MEADOWLAKE INDUSTRIAL	Calc'd by:	SPC
EXISTING CONDITIONS	Checked by:	СМ
EL PASO COUNTY, CO	Date:	10/25/2024

SUMMARY RUNOFF TABLE									
BASIN	AREA (ac)	Q <sub>100</sub> (cfs)							
EX1	8.75	5	3.4	18.3					
EX2	30.77	3	9.5	57.8					
EX3	13.39	5	4.5	25.4					
EX4	7.03	2	2.1	14.3					
OS1	2.83	2	1.0	6.7					
OS2.1	5.34	2	1.8	11.9					
OS2.2	0.37	2	0.1	0.9					
OS3	3.96	11	2.1	9.2					
OS4	40.63	3	10.7	64.7					
EROW4	1.48	53	2.1	4.6					

DESIGN POINT SUMMARY TABLE								
DESIGN POINT	CONTRIBUTING BASINS	$\Sigma Q_{100}$ (cfs)						
1	OS1	1.0	6.7					
2	EX1, DP1	4.2	23.9					
3	OS2.1	1.8	11.9					
4	EX2, DP3	10.9	67.6					
5	OS2.2	0.1	0.9					
6	EX3, DP5	13.2	79.9					
7	OS3, DP6, DP10	15.0	81.2					
8	EX4	2.1	14.3					
9	OS4, DP7, DP8	24.2	138.8					
10	EROW4	2.1	4.6					

**EL PASO COUNTY, CO** 

Calc'd by: SPC

Checked by: CM

Date: 10/25/2024

SOIL TYPE: HSG A&B

	COMPOSITE 'C' FACTORS																			
							LAND	USE	TYPE											
		c Flow An	-		Paved		Land (	Use Und	defined	Land	Use Und	defined	Land	Jse Un	defined			COMPOSITE		
	% <b>I</b>	C <sub>5</sub>	C <sub>100</sub>	%l	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>		IMPERVIOUSNESS & C FACTOR			
	2	0.09	0.36	100	0.90	0.96	0	0.00	0.00	0	0.00	0.00	0	0.00	0.00	TOTAL				
BASIN		ACRES	•		ACRES	•		ACRES	•	ACRES ACRES			ACRES	<b>%I</b>	C <sub>5</sub>	C <sub>100</sub>				
EX1		8.46			0.29											8.75	5	0.12	0.38	
EX2		30.35			0.42											30.77	3	0.10	0.37	
EX3		13.04			0.35											13.39	5	0.11	0.38	
EX4		7.03														7.03	2	0.09	0.36	
OS1		2.83														2.83	2	0.09	0.36	
OS2.1		5.34														5.34	2	0.09	0.36	
OS2.2		0.37														0.37	2	0.09	0.36	
OS3		3.61			0.35											3.96	11	0.16	0.41	
OS4		40.03			0.60											40.63	3	0.10	0.37	
EROW4	·	0.70	·		0.78			•				•		•	•	1.48	53	0.51	0.67	



MEADOWLAKE INDUSTRIAL	Calc'd by:	SPC
EXISTING CONDITIONS	Checked by:	СМ
EL PASO COUNTY, CO	Date:	10/25/2024

#### TIME OF CONCENTRATION

BAS	IN DATA		OVER	LAND TIM	E (T;)		TRAV	EL TIME (	T <sub>t</sub> )		TOTAL	tc=(L/180)+10	Design tc	
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	$C_{V}$	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	$t_c$ (min)	tc max	tc design (min)	
EX1	0.12	8.75	100	2.3	13.7	10	1270	3.0	1.7	12.2	25.9	17.6	17.6	
EX2	0.10	30.77	100	2.2	14.1	10	1820	2.1	1.4	20.9	35.0	20.7	20.7	
EX3	0.11	13.39	100	2.1	14.2	10	1889	1.9	1.4	22.8	37.0	21.1	21.1	
EX4	0.09	7.03	100	2.4	13.8	10	1086	4.1	2.0	8.9	22.8	16.6	16.6	
OS1	0.09	2.83	100	5.0	10.8	10	210	5.0	2.2	1.6	12.4	11.7	11.7	
OS2.1	0.09	5.34	100	2.0	14.7	10	527	1.7	1.3	6.7	21.4	13.5	13.5	
OS2.2	0.09	0.37	97	3.7	11.8	10	0	0.0	0.0	0.0	11.8	10.5	10.5	
OS3	0.16	3.96	100	2.0	13.7	10	1160	2.0	1.4	13.7	27.3	17.0	17.0	
OS4	0.10	40.63	100	5.5	10.4	10	3177	3.5	1.9	28.3	38.7	28.2	28.2	
EROW4	0.51	1.48	25	9.8	2.5	15	2685	1.6	1.9	24.0	26.5	25.1	25.1	

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
  $V = C_v S_w^{0.5}$ 

Table 6-7. Conveyance Coefficient, $C_1$
--

Type of Land Surface	$C_{\nu}$
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

\*For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.



MEADOWLAKE INDUSTRIAL	Calc'd by:	SPC
EXISTING CONDITIONS	Checked by:	СМ
DESIGN STORM: 5-YEAR	Date:	10/25/2024

						<b></b>						[	6=					_					REMARKS						
				DII	RECT	RUNO	FF		ТС	TAL F	RUNO	FF	Si	REET		-	PIP	Έ		TRA	AVEL	TIME	REMARKS						
	DESIGN POINT	BASIN ID	AREA (ac)	C <sub>5</sub>	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)		C <sub>5</sub> *A (a	SLOPE %	Q <sub>PIPE</sub> (cfs)	С <sub>5</sub> *А (ас)	% <b>3d0</b> 1S	PIPE SIZE (ft)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (mir							
1	1	004	0.00	0 00	44.7	0.05	0.00	4.0	11.7	0.25	3.89	1.0	1.0	0.25	3.0					940	3.5	4.52	BASIN OS1 DRAINS INTO EX1 VIA SHEET FLOW AT DP1						
2	2	OS1	2.83	0.09	11.7	0.25	3.89	1.0	17.6	1.28	3.28	4.2											BASIN EX1 DRAINS NORTH OFFSITE VIA CHANNLEIZED FLOW AT DP2						
		EX1	8.75	0.12	17.6	1.02	3.28	3.4		0	0.20																		
3	3								13.5	0.48	3.68	1.8	1.8	0.48	3.0					832	3.5	4.00	BASIN OS2.1 DRAINS INTO EX2 VIA SHEET FLOW AT DP3						
	1	OS2.1	5.34	0.09	13.5	0.48	3.68	1.8	20.7	3.59	3.04	10.0	10.0	3.59	1 7					1150	2.6	7.35	BASIN EX2 DRAINS INTO EX3 VIA CHANNELIZED FLOW AT DP4						
	<b>-</b>	EX2	30.77	0.10	20.7	3.11	3.04	9.5		3.33	3.04	10.5	10.3	3.33	1.7					1130	2.0	7.55	BAGIN EXE BIXAING INTO EXO VIA OTIANNELIZED FEOW AT BIT						
5	5								10.5	0.03	4.05	0.1	0.1	0.03	1.9					1285	2.8	7.77	BASIN OS3 DRAINS INTO OS4 VIA CHANNELIZED FLOW AT DP5						
	6	OS2.2	0.37	0.09	10.5	0.03	4.05	0.1	28.0	5.11	2.58	12.2	13.2	5.11	2.1					1015	2.0	5.84	BASIN EX3 DRAINS INTO OS3 VIA CHANNELIZED FLOW AT DP6						
'	٠	EX3	13.39	0.11	21.1	1.49	3.01	4.5		5.11	2.50	13.2	13.2	3.11	۷.۱					1013	2.3	5.04	BAGIN EAG BITAING INTO COS VIA GITAINNELIZED I EGW AT DEC						
7	7								33.9	6.51	2.30	15.0	15.0	6.51	3.7					853	3.8	3.70	BASIN OS3 DRAINS INTO OS4 VIA CHANNELIZED FLOW AT DP7 (INCLUDES DP 10)						
		OS3	3.96	0.16	17.0	0.64	3.33	2.1		0.00	0.07	0.4	0.4	0.00	4.4					4574	0.4	44.00	DACINI EVA DDAING INTO OCA VIA CHEET ELOW AT DDC						
3	ŏ	EX4	7.03	0.09	16.6	0.63	3.37	2.1	16.6	0.63	3.37	2.1	2.1	0.63	1.4					1571	2.4	11.06	BASIN EX4 DRAINS INTO OS4 VIA SHEET FLOW AT DP8						
9	9									11.29	2.14	24.2			$\top$								DP9 TOTAL FLOW OFFSITE AT EXISTING BOX CULVERTS (INCLUDES DP 10)						
		OS4	40.63	0.10	28.2	4.14	2.57	10.7																					
1	10	EROW4	1.48	0.51	25.1	0.76	2.75	2.1	25.1	0.76	2.75	2.1											DP10 TOTAL FLOW OFFSITE AT EXISTNG SWALE						

10/25/2024



MEADOWLAKE INDUSTRIAL	Calc'd by:	SPC
EXISTING CONDITIONS	Checked by:	СМ
DESIGN STORM: 100-YEAR	Date:	10/25/2024

			DIR	RECT F	RUNOF	F		то	TAL F	RUNOI	FF	S	TREE	Т		PII	PE		TR	AVEL	TIME	REMARKS
DESIGN POINT	BASIN ID	AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	% JODE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
1	OS1	2.83	0.36	11.7	1.02	6.52	6.7	11.7	1.02	6.53	6.7	6.7	1.02	3.0					940	3.5	4.52	BASIN OS1 DRAINS INTO EX1 VIA SHEET FLOW AT DP1
2	031	2.03	0.36	11.7	1.02	6.53	0.7	17.6	4.34	5.51	23.9											BASIN EX1 DRAINS NORTH OFFSITE VIA CHANNLEIZED FLOW AT DP2
	EX1	8.75	0.38	17.6	3.32	5.51	18.3															
3	OS2.1	5.34	0.36	10.5	1.00	6.40	11.0		1.92	6.18	11.9	11.9	1.92	3.0					832	3.5	4.00	BASIN OS2.1 DRAINS INTO EX2 VIA SHEET FLOW AT DP3
4	032.1	5.34	0.36	13.5	1.92	0.18	11.9		13.25	5.10	67.6	67.6	13.25	1.7					1150	2.6	7.35	BASIN EX2 DRAINS INTO EX3 VIA CHANNELIZED FLOW AT DP4
	EX2	30.77	0.37	20.7	11.33	5.10	57.8															
5	OS2.2	0.37	0.26	10.5	0.12	6.80	0.9		0.13	6.80	0.9	0.9	0.13	1.9					1285	2.8	7.77	BASIN OS3 DRAINS INTO OS4 VIA CHANNELIZED FLOW AT DP5
6	032.2	0.37	0.36	10.5	0.13	0.60	0.9		18.42	4.34	79.9	79.9	18.42	2.1					1015	2.9	5.84	BASIN EX3 DRAINS INTO OS3 VIA CHANNELIZED FLOW AT DP6
	EX3	13.39	0.38	21.1	5.03	5.06	25.4															
7	OS3	3.96	0.41	17.0	1 64	5.60	9.2		21.05	3.86	81.2	81.2	21.05	3.7					853	3.8	3.70	BASIN OS3 DRAINS INTO OS4 VIA CHANNELIZED FLOW AT DP7 (INCLUDES DP 10)
8	033	3.90	0.41	17.0	1.04	3.00	9.2		2.53	5.66	14.3	14.3	2.53	1.4					1571	2.4	11.06	BASIN EX4 DRAINS INTO OS4 VIA SHEET FLOW AT DP8
	EX4	7.03	0.36	16.6	2.53	5.66	14.3															
9	OS4	40.63	0.37	28.2	14.00	4 32	64.7		38.57	3.60	138.8											DP9 TOTAL FLOW OFFSITE AT EXISTING BOX CULVERTS (INCLUDES DP 10)
10	034	40.03	0.37	20.2	14.99	4.32	64.7		1.00	4.62	4.6											DP9 TOTAL FLOW OFFSITE AT EXISTING BOX CULVERTS
	EROW4	1.48	0.67	25.1	1.00	4.62	4.6															



MEADOWLAKE INDUSTRIAL	Calc'd by:	DH/AB
PROPOSED CONDITIONS	Checked by:	NQJ
EL PASO COUNTY, CO	Date:	10/25/2024

0. H H A D V D I II I D D D D D D D D D D D D D											
	SUMM	ARY RUNOF	F TABLE								
BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)							
Α	5.78	45	8.4	19.9							
В	1.10	96	3.6	6.6							
С	3.01	80	7.0	13.9							
D	3.05	80	7.3	14.6							
Е	3.68	80	8.8	17.5							
F	1.10	90	2.8	5.2							
G	6.75	2	2.0	13.5							
Н	3.71	74	7.7	15.8							
	1.12	67	2.1	4.6							
J	3.14	25	3.0	9.6							
K	0.24	90	1.0	1.9							
L	0.24	90	1.0	1.9							
N1	2.07	80	4.9	9.8							
N2	0.25	100	1.2	2.1							
N3	1.84	80	4.8	9.6							
0	2.10	80	5.9	11.8							
P1	0.25	100	1.2	2.1							
P2	2.05	80	2.4	11.4							
Q	1.02	80	3.2	6.2							
R	1.43	80	2.1	6.8							
S1	1.16	80	2.9	5.8							
S2	2.32	80	5.3	10.6							
S3	1.16	80	3.0	5.9							
Т	1.42	3	0.5	3.2							
OS1	2.83	2	1.0	6.7							
ROW1	2.17	28	2.3	6.5							
ROW2	3.25	33	3.6	9.6							
ROW3	6.85	24	5.2	15.8							
OS4	40.02	3	10.5	63.9							
ROW4	1.48	59	2.3	4.9							

	DESIGN POINT SUMMA	RY TABLE	
DESIGN POINT	CONTRIBUTING BASINS	$\Sigma Q_5$ (cfs)	ΣQ <sub>100</sub> (cfs)
E1	OS1	1.0	6.7
7	G, DP E1	2.9	19.2
E2	ROW 1, DP 7	5.0	25.2
1	А	8.4	19.9
2	E	3.6	6.6
2.1	DP 1, DP 2	11.4	25.3
3	С	7.0	13.9
4	D	7.3	14.6
4.1	DP 3, DP 4	13.7	27.2
5	E	8.8	17.5
5.1	DP 2.1, DP5	18.0	38.3
5.2	DP 4.1, DP 5.1	29.3	60.8
6	F, DP 5.2	31.8	65.5
6.1	DP 6	31.8	65.5
8	Н	7.7	15.8
9	I, DP 8	9.2	19.0
10	DP 6.1, DP 9	42.4	90.3
13	ROW2	3.6	9.6
E4	POND A RELEASE	0.8	13.8
11	K, DP 13	1.0	10.7
12	L, DP 11	2.0	11.9
12.1	DP 12	2.0	22.5
15	N1	4.9	9.8
15.1	N2	1.2	2.1
15.2	N3	4.8	9.6
16	0	5.9	11.8
17	P1	1.2	2.1
17.1	DP 16, DP 17	6.9	13.6
18	Q	3.2	6.2
19	R, DP 15.2	5.8	14.1
19.1	DP 18, DP 19	13.2	28.5
20.1	DP 17.1, DP 19.1	18.1	38.0
20.2	P2	2.4	11.4
20.3	DP 20.1, DP 20.2	19.2	44.9
21	S1, DP 12.1	4.6	25.3
21.1	S2, DP 21	9.2	30.8
21.2	S3, DP21.2	11.2	33.3
22	T, DP 20.3, DP 21.1	29.1	72.0
E7	ROW 2, DP E4	6.0	29.6
E8	POND B RELEASE	1.5	14.0
E9	OS4, DP E7, DP E8	19.8	110.9
E10	ROW4	2.3	4.9



#### MEADOWLAKE INDUSTRIAL DH/AB Calc'd by: PROPOSED CONDITIONS NQJ Checked by: HRGreen EL PASO COUNTY, CO 10/25/2024 Date:

#### **COMPOSITE 'C' FACTORS**

	COMPOSITE O TACTORS																
	UNDEVELOPED	INDUSTRIAL	PAVED	TOTAL	SOIL	UNI	DEVEL	OPED	IN	DUSTRIA	AL		P	AVED		MPOSI	
BASIN					TYPE										IMPERV		I
		ACRES				<b>%I</b>	C <sub>5</sub>	C <sub>100</sub>	<b>%I</b>	C <sub>5</sub>	C <sub>100</sub>	<b>%I</b>	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>
Α	3.27	0.00	2.51	5.78	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	45	0.44	0.62
В	0.00	0.23	0.87	1.10	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	96	0.84	0.91
С	0.00	3.01	0.00	3.01	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
D	0.00	3.05	0.00	3.05	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
E	0.00	3.68	0.00	3.68	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
F	0.00	0.57	0.53	1.10	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	90	0.74	0.83
G	6.75	0.00	0.00	6.75	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	2	0.09	0.36
Н	0.30	3.41	0.00	3.71	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	74	0.55	0.67
l	0.19	0.93	0.00	1.12	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	67	0.51	0.64
J	2.20	0.94	0.00	3.14	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	25	0.24	0.46
K	0.02	0.00	0.22	0.24	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	90	0.82	0.90
L	0.02	0.00	0.22	0.24	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	90	0.82	0.90
N1	0.00	2.07	0.00	2.07	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
N2	0.00	0.00	0.25	0.25	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	100	0.90	0.96
N3	0.00	1.84	0.00	1.84	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
0	0.00	2.10	0.00	2.10	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
P1	0.00	0.00	0.25	0.25	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	100	0.90	0.96
P2	0.00	2.05	0.00	2.05	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
Q	0.20	0.00	0.82	1.02	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.74	0.84
R	0.29	0.00	1.14	1.43	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.74	0.84
S1	0.00	1.16	0.00	1.16	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
S2	0.00	2.32	0.00	2.32	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
S3	0.00	1.16	0.00	1.16	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
Т	1.40	0.00	0.02	1.42	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	3	0.10	0.37
OS1	2.83	0.00	0.00	2.83	A/B	2	0.09	0.36	80	0.59	0.70	100		0.96	2	0.09	0.36
ROW1	1.60	0.00	0.57	2.17	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	28	0.30	0.52
ROW2	2.21	0.00	1.04	3.25	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	33	0.35	0.55
ROW3	5.32	0.00	1.53	6.85	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	24	0.27	0.49
ROW4	0.62	0.00	0.86	1.48	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	59	0.56	0.71
OS4	39.51	0.00	0.60	40.02	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	3	0.10	0.37
Pond A				25.69											65		
Pond B				20.80											68		



MEADOWLAKE INDUSTRIAL	Calc'd by:	DH/AB
PROPOSED CONDITIONS	Checked by:	ИДЈ
EL PASO COUNTY, CO	Date:	10/25/2024

TINAE	AE.		CENTR	ATION
	· ·	LLIN	LPNIR	

			•			_					TOTAL		
BAS												tc=(L/180)+10	Design tc
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	$C_V$	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	$t_c$ (min)	tc max	tc design (min)
Α	0.44	5.78	100	1.9	9.7	20	1360	2.2	3.0	7.6	17.4	18.1	17.4
В	0.84	1.10	100	1.9	3.9	20	1330	2.2	3.0	7.5	11.4	17.9	11.4
С	0.59	3.01	100	2.0	7.4	20	665	1.9	2.8	4.0	11.4	14.3	11.4
D	0.59	3.05	100	2.0	7.4	20	425	1.5	2.4	2.9	10.3	12.9	10.3
Е	0.59	3.68	100	2.0	7.4	20	470	1.6	2.5	3.1	10.5	13.2	10.5
F	0.74	1.10	100	1.9	5.3	20	1680	1.7	2.6	10.7	16.1	19.9	16.1
G	0.09	6.75	100	4.0	11.7	10	1200	0.4	0.7	30.2	41.8	17.2	17.2
Н	0.55	3.71	100	2.0	8.0	15	665	2.4	2.3	4.7	12.7	14.3	12.7
I	0.51	1.12	100	2.0	8.7	15	360	1.1	1.6	3.8	12.5	12.6	12.5
J	0.24	3.14	100	2.0	12.5	20	140	0.9	1.9	1.2	13.7	11.3	11.3
K	0.82	0.24	15	2.0	1.6	20	390	1.5	2.4	2.7	5.0	12.3	5.0
L	0.82	0.24	15	2.0	1.6	20	390	1.5	2.4	2.7	5.0	12.3	5.0
N1	0.59	2.07	100	2.0	7.4	20	460	1.5	2.4	3.1	10.6	13.1	10.6
N2	0.90	0.25	10	2.0	0.9	20	300	2.1	2.9	1.7	5.0	11.7	5.0
N3	0.59	1.84	100	2.0	7.4	20	167	4.0	4.0	0.7	8.1	11.5	8.1
0	0.59	2.10	100	4.5	5.7	20	215	4.5	4.2	0.8	6.5	11.8	6.5
P1	0.90	0.25	10	2.0	0.9	20	327	4.0	4.0	1.4	5.0	11.9	5.0
P2	0.59	2.05	100	4.6	5.6	20	279	4.6	4.3	1.1	6.7	12.1	6.7
Q	0.74	1.02	100	2.0	5.3	20	550	1.5	2.4	3.7	9.0	13.6	9.0
R	0.74	1.43	17	25.0	0.9	10	1160	1.5	1.2	15.8	16.7	16.5	16.5
S1	0.59	1.16	100	2.0	7.4	15	216	2.0	2.1	1.7	9.1	11.8	9.1
S2	0.59	2.32	100	2.0	7.4	15	491	1.7	2.0	4.2	11.6	13.3	11.6
S3	0.59	1.16	100	2.0	7.4	15	176	2.0	2.1	1.4	8.8	11.5	8.8
Т	0.10	1.42	100	2.0	14.5	20	540	2.5	3.2	2.8	17.4	13.6	13.6
OS1	0.09	2.83	100	5.0	10.8	10	210	5.0	2.2	1.6	12.4	11.7	11.7
ROW1	0.30	2.17	81	6.4	7.1	15	1012	0.5	1.1	15.9	23.0	16.1	16.1
ROW2	0.35	3.25	81	6.4	6.7	15	1494	1.9	2.1	12.0	18.7	18.8	18.7
ROW3	0.27	6.85	81	3.4	9.1	15	2515	1.2	1.6	25.5	34.6	24.4	24.4
ROW4	0.56	1.48	25	9.8	2.3	15	2685	1.6	1.9	24.0	26.3	25.1	25.1
OS4	0.10	40.02	300	5.5	17.9	15	2977	3.5	2.8	17.7	35.6	28.2	28.2

### FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient,  $C_{\nu}$ 

Type of Land Surface	$C_{\nu}$
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20
* F	

<sup>\*</sup>For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.



MEADOWLAKE INDUSTRIAL	Calc'd by:	DH/AB
PROPOSED CONDITIONS	Checked by:	ГДИ
DESIGN STORM: 5-YEAR	Date:	10/25/2024

				DII	RECT	RUNO	FF		T	OTAL	RUNOFF	:	S	TREE	т		PII	PE		TRA	VEL	ГІМЕ	REMARKS
STREET	DESIGN	BASIN ID	AREA (ac)	S.	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
	E1						2.00		11.7	0.25	3.89	0.99	1.0	0.25				, ,		228	4.4	0.87	DP E1 DRAINS VIA SHEETFLOW INTO BASIN G TO DP 7
	7	OS1	2.83	0.09		0.25	3.89		17.2	0.86	3.31	2.86	2.9	0.86	4.0					81	4.0	0.34	DP7 DRAINS VIA SHEETFLOW INTO BASIN ROW1 TO DP E2
	E2	G	6.75	0.09	17.2	0.61	3.31	2.0	17.6	1.52	3.28	5.00	5.0	1.52	4.0					81	4.0	0.34	DP E2 DRAINS NORTH OFFSITE
		ROW1	2.175	0.30	16.1	0.66	3.42	2.3															
	1	Α	5.78	0.44	17.4	2.55	3.30	8.4	17.4	2.55	3.30	8.42				8.4	2.55	1.2	1.5	40	6.5	0.10	DP1 CAPTURED W/ 10' TYPE R SUMP INELT, PIPE TO DP2.1
	2	Б	4.4	0.04	44.4	0.00	2.02	2.0	11.4	0.92	3.93	3.61				3.6	0.92	0.5	1.5	89	4.2	0.35	DP2 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP2.1
	2.1	В	1.1	0.84	11.4	0.92	3.93	3.0	17.5	3.47	3.29	11.43				11.4	3.47	0.5	1.5	305	4.2	1.21	DP2.1 FLOW, PIPE TO DP5.1
	3								11.4	1.78	3.93	6.97				7.0	1.78	2.0	1.5	427	8.4	0.85	DP3 CPATURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	3	С	3.01	0.59	11.4	1.78	3.93	7.0	11.4	1.70	ა.ყა	6.97				7.0	1.76	2.0	1.5	427	0.4	0.65	DP3 CPATURED W/ 20 TTPE R INLET, PIPE TO DP4.1
	4	D	3.05	0.59	10.3	1.80	4.08	7.3	10.3	1.80	4.08	7.35				7.3	1.80	1.0	1.5	6	5.9	0.02	DP4 CAPTURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4.1								12.3	3.58	3.82	13.66				13.7	3.58	2.0	1.5	500	8.4	0.99	DP4.1 FLOW, PIPE TO DP5.1
	5	E	3.68	0.59	10.5	2.17	4.05	8.8	10.5	2.17	4.05	8.80				8.8	2.17	3.0	1.5	6	10.3	0.01	DP5 CAPTURED W/ 15' TYPE R SUMP INLET, PIPE TO DP5.1
	5.1								18.7	5.64	3.19	18.00				18.0	5.64	0.4	2.0	50	4.6	0.18	DP5.1 FLOW, PIPE TO DP5.2
	5.2								18.9	9.22	3.18	29.28				29.3	9.22	0.8	2.0	36	6.2	0.10	DP5.2 FLOW, PIPE TO DP6.1
	6	F	1.1	0.74	16.1	0.81	3.42	2.8	19.0	10.03	3.17	31.78				31.8	0.81	1.0	2.0	12	7.2	0.03	DP6 CAPTURED IN 15' TYPE R SUMP INLET , PIPE TO DP6.1
	6.1								19.0	10.03	3.17	31 78											DP6.1, PIPE TO POND A
			0.74	0.55	40.7	0.04	0.70	7.7						2.04	1.7					360	2.6	2.30	SWALE TO BASIN I
	8	Н	3.71	0.55	12.7	2.04	3.76	1.1	12.7	2.04	3.76	7.68											
	9	I	1.12	0.51	12.5	0.57	3.80	2.1	15.1	2.60	3.52	9.16				9.2	2.60	0.5	1.5	40	4.2	0.16	SWALE TO DET POND A
	10	J	3.14	0.24	11.3	0.75	3.94	3.0	19.0	13.39	3.17	42.42											DP10 FLOW, TOTAL FLOW ENTERING POND A
	13	ROW2	3.25	0.35	18.7	1.14	3.19	3.6	18.7	1.14	3.19	3.63				3.6	1.14	0.5	1.5	56	4.2	0.22	DP13 FLOW, TOTAL FLOW TO INLET AT DP 11
	E4											0.80	0.8	0.00	1.4					2477	2.4	17.45	DP E4 FLOW, TOTAL FLOW TO ROADSIDE SWALE = POND A RELEASE



MEADOWLAKE INDUSTRIAL	Calc'd by:	DH/AB
PROPOSED CONDITIONS	Checked by:	NQJ
DESIGN STORM: 5-YEAR	Date:	10/25/2024

				DII	RECT	RUNO	FF		T	OTAL	RUNOFF		s	TREE	Т		PII	PE		TRA	VEL 1	ГІМЕ	REMARKS
STREET	DESIGN	BASIN ID	AREA (ac)	C <sub>5</sub>	$t_c$ (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	f <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>5</sub> *A (ac)	% <b>SCOPE</b> %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
	11	К	0.24	0.82	5.0	0.20	5.17	1.0	5.0	0.20	5.17	1.02				1.0	0.20	2.0	1.5	25	8.4	0.05	DP11 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP12.1
	12	ı	0.24	0.82	5.0	0.20	5.17	1.0	5.0	0.39	5.15	2.03				2.0	0.20		1.5	25	8.4	0.05	DP12 CAPTURED W/ 5' TYPE R SUMP INELT, PIPE TO DP12.1
	12.1		0.21	0.02	0.0	0.20	0			0.39		2.03	2.0	0.39	1.0	2.0	0.20	2.0	110	289	2.0	2.41	DP12.1 SWALE FLOW TO DP21
									5.0		5.15												
	15	N1	2.07	0.59	10.6	1.22	4.05	4.9	10.6	1.22	4.05	4.94				4.9	1.22	0.5	1.5	606	4.2	2.40	DP15 CAPTURED IN 10' TYPE R INLET, PIPE TO DP19.1
	15.1	N2	0.25	0.90	5.0	0.23	5.17	1.2	5.0	0.23	5.17	1.16				1.2	0.23	0.5	1.5	626	4.2	2.48	DP15.1 CAPTURED IN 5' TYPE R INLET, PIPE TO DP19.1
	15.2	N3	1.84	0.59	8.1	1.09	4.44	4.8	8.1	1.09	4.44	4.82	4.8	1.09	3.4					255	3.7	1.15	DP15.2 DRAINS INTO BASIN R, DRAINS TO DP 19
	16	0	2.1	0.59	6.5	1.24	4.77	5.9	6.5	1.24	4.77	5.91				5.9	1.24	1.0	1.5	45	5.9	0.13	DP16 CAPTURED IN 10' TYPE R INLET, PIPE TO DP17.1
	17	P1	0.25	0.90	5.0	0.23	5.17	1.2	5.0	0.23	5.17	1.16				1.2	0.23	2.0	1.5	27	8.4	0.05	DP17 CAPTURED IN 5' TYPE R INLET, PIPE TO DP17.1
	17.1								6.6	1.46	4.74	6.95				6.9	1.46	3.6	2.0	42	13.7	0.05	DP17.1 FLOW, PIPE TO DP20.1
	18	Q	1.02	0.74	9.0	0.75	4.29	3.2	9.0	0.75	4.29	3.23				3.2	0.75		1.5	50	4.2	0.20	DP18 CAPTURED IN 5' TYPE R INLET, PIPE TO DP19.1
	19	R	0.85	0.74	16.5	0.63	3.37	2.1	16.5	1.71	3.37	5.78			Н	5.8	0.63	1.0	1.5	6	5.9	0.02	DP19 CAPTURED IN 10' TYPE R SUMP INLET, PIPE TO DP19.1
	19.1								16.6	3.91	3.37	13.19			$\vdash$	13.2	3.91	0.5	2.0	42	5.1	0.14	DP19.1 FLOW, PIPE TO DP20.1
	20.1								16.7	5.38	3.36	18.07				18.1	5.38	0.5	2.5	370	5.9	1.04	DP20.1 PIPE FLOW TO POND B
	20.2	P2	0.85	0.59	6.7	0.50	4.73	2.4	6.7	0.50	4.73	2.37				2.4	0.50	0.5	1.0	15	3.2	0.08	DP20.1 PIPE FLOW TO POND B
	20.3								17.7	5.88	3.27	19.22				19.2	5.88	0.5	2.5	370	5.9	1.04	DP20.1 PIPE FLOW TO POND B
	21	S1	1.16	0.59	9.1	0.68	4.27	2.9	9.1	1.08	4.27	4.60	4.6	1.08	1.7					580	2.6	3.71	DP21 SWALE FLOW TO DP21.1
	21.1	S2	2.32				3.91		12.8	2.45	3.76			2.45						282	2.8	1.66	DP21 SWALE FLOW TO DP21.2
														2.43	2.0		0.40	<b>5</b> 0	0.0				
	21.2	S3		0.59					14.5	3.13		11.19				11.2	3.13	5.0	2.0	45	16.1	0.05	DP21 SWALE FLOW TO POND B
	22	Т	1.42	0.10	13.6	0.14	3.67	0.5	18.8	9.15	3.18	29.14	6.0	1.85	4.2					865	4.1	3.52	TOTAL FLOW ENTERING POND B
	E7	ROW3	6.848	0.27	24.4	1.85	2.79	5.2	24.4	1.85	2.79	5.97			$\vdash \vdash$			_		-			DP E7 SWALE FLOW TO DP E9
	E8											1.50			Щ								DP E8 FLOW TO DP E9 (POND B RELEASE)
	E9	OS4	40.02	0.10	28.2	4.10	2.57	10.5	28.2	6.78	2.57	19.76										<u> </u>	DP E9 TOTAL FLOW OFFSITE
	E10	ROW4	1.48	0.56	25.1	0.83	2.75	2.3	25.1	0.83	2.75	2.29										<u> </u>	DP E10 TOTAL FLOW OFFSITE



MEADOWLAKE INDUSTRIAL	Calc'd by:	DH/AB
PROPOSED CONDITIONS	Checked by:	NQJ
DESIGN STORM: 100-YEAR	Date:	10/25/2024

			DII	RECT	RUNOI	FF		т	TOTAL RUNOFF					Т		PII	PE		TR	AVEL	TIME	REMARKS	
STREET	DESIGN	BASIN ID	AREA (ac)	C <sub>100</sub>	<i>t<sub>c</sub> (</i> min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	<i>t<sub>c</sub> (</i> min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	E1	OS1	2.83	0.36	11.7	1.02	6.53	6.7	11.7	1.02	6.53	6.7	6.7	1.02	4.8					228	4.4	0.87	DP E1 DRAINS VIA SHEETFLOW INTO BASIN G TO DP 7
	7	G	6.75	0.36			5.56		17.2	3.45	5.56	19.2	19.2	3.45	4.0					81	4.0	0.34	DP7 DRAINS VIA SHEETFLOW INTO BASIN ROW1 TO DP E2
	E2		2.1745			1.13			17.6	4.58	5.51	25.2	25.2	4.58	4.0					81	4.0	0.34	DP E2 DRAINS NORTH OFFSITE
	1	A	5.78	0.62	17.4		5.54		17.4	3.59	5.54	19.9				19.9	3.59	1.2	1.5	40	6.5	0.10	DP1 CAPTURED W/ 10' TYPE R SUMP INELT, PIPE TO DP2.1
	2	В	1.1	0.02					11.4	1.00	6.60	6.6				6.6	1.00	0.5	1.5	89	4.2	0.35	DP2 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP2.1
	2.1			0.01		1100	0.00	0.0	17.5	4.58	5.52	25.3				25.3	4.58	0.5	1.5	305	4.2	1.21	DP2.1 FLOW, PIPE TO DP5.1
	3	С	3.01	0.70	11.4	2.11	6.59	13.9	11.4	2.11	6.59	13.9				13.9	2.11	2.0	1.5	427	8.4	0.85	DP3 CPATURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4	D	3.05	0.70	10.3	2.14	6.85	14.6	10.3	2.14	6.85	14.6				14.6	2.14	1.0	1.5	6	5.9	0.02	DP4 CAPTURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4.1								12.3	4.24	6.41	27.2				27.2	4.24	2.0	1.5	500	8.4	0.99	DP4.1 FLOW, PIPE TO DP5.1
	5	Е	3.68	0.70	10.5	2.58	6.81	17.5	10.5	2.58	6.81	17.5				17.5	2.58	3.0	1.5	6	10.3	0.01	DP5 CAPTURED W/ 15' TYPE R SUMP INLET, PIPE TO DP5.1
	5.1								18.7	7.16	5.36	38.3				38.3	7.16	0.4	2.0	50	4.6	0.18	DP5.1 FLOW, PIPE TO DP5.2
	5.2								18.9	11.40	5.33	60.8				60.8	11.40	0.8	2.0	36	6.2	0.10	DP5.2 FLOW, PIPE TO DP6.1
	6	F	1.1	0.83	16.1	0.91	5.74	5.2	19.0	12.31	5.32	65.5				65.5	0.91	1.0	2.0	12	7.2	0.03	DP6 CAPTURED IN 15' TYPE R SUMP INLET , PIPE TO DP6.1
	6.1								19.0	12.31	5.32	65.5		0.50								2.00	DP6.1, PIPE TO POND A
	8	Н	3.71	0.67	12.7	2.50	6.32	15.8	12.7	2.50	6.32	15.8	15.8	2.50	1.7					360	2.6	2.30	SWALE TO BASIN I
	9	I	1.12	0.64	12.5	0.72	6.38	4.6	15.1	3.21	5.90	19.0				19.0	3.21	0.5	1.5	40	4.2	0.16	SWALE TO DET POND A
	10	J	3.14	0.46	11.3	1.45	6.62	9.6	19.0	16.97	5.32	90.3											DP10 FLOW, TOTAL FLOW ENTERING POND A
	13	ROW2	3.25	0.55	18.7	1.80	5.35	9.6	18.7	1.80	5.35	9.6				9.6	1.80	0.5	1.5	56	4.2	0.22	DP13 FLOW, TOTAL FLOW TO INLET AT DP 11
	E4											13.8	13.8	0.00	1.4					2477	2.4	17.45	DP E4 FLOW, TOTAL FLOW TO ROADSIDE SWALE = POND A RELEASE



MEADOWLAKE INDUSTRIAL	Calc'd by:	DH/AB
PROPOSED CONDITIONS	<b>Checked by:</b>	NQJ
DESIGN STORM: 100-YEAR	Date:	10/25/2024

				DIF	RECT	RUNOF	F		тс	OTAL I	RUNOI	FF	S	TREE	т		PII	PE		TR	AVEL '	TIME	REMARKS
STREET	DESIGN	BASIN ID	AREA (ac)	C <sub>100</sub>	f <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	f <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	% <b>3401</b> S	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	11	K	0.24	0.90	5.0	0.22	8.68	1.9	18.9	2.01	5.32	10.7				10.7	2.01	2.0	1.5	25	8.4	0.05	DP11 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP12.1
	12	L	0.24	0.90	5.0	0.22	8.68	1.9	19.0	2.23	5.32	11.9				11.9	2.23	2.0	1.5	25	8.4	0.05	DP12 CAPTURED W/ 5' TYPE R SUMP INELT, PIPE TO DP12.1
	12.1								19.0	4.24	5.31		22.5	0.43	1.0					289	2.0	2.41	DP12.1 SWALE FLOW TO DP21
	15	N1	2.07	0.70	10.6	1.45	6.80	9.8			6.80					9.8	1.45	0.5	1.5	606	4.2	2.40	DP15 CAPTURED IN 10' TYPE R INLET, PIPE TO DP19.1
	15.1	N2	0.25	0.96	5.0	0.24		2.1			8.68									626		2.48	DP15.1 CAPTURED IN 5' TYPE R INLET, PIPE TO DP19.1
	15.2	N3	1.84	0.70	8.1			9.6			7.46		9.6	1.29	3.4					255	3.7	1.15	DP15.2 DRAINS INTO BASIN R, DRAINS TO DP 19
	16	0	2.1	0.70	6.5		8.01				8.01						1.47	1.0	1.5		5.9	0.13	DP16 CAPTURED IN 10' TYPE R INLET, PIPE TO DP17.1
	17	P1	0.25	0.96	5.0		8.68				8.68						0.24				8.4	0.05	DP17 CAPTURED IN 5' TYPE R INLET, PIPE TO DP17.1
	17.1			0.00			0.00				7.97						1.71				13.7	0.05	DP17.1 FLOW, PIPE TO DP20.1
	18	Q	1.02	0.84	9.0	0.86	7.20	6.2			7.20						0.86				4.2	0.20	DP18 CAPTURED IN 5' TYPE R INLET, PIPE TO DP19.1
	19	R	1.43	0.84	16.5		5.66	6.8			5.66						1.20				5.9	0.02	DP19 CAPTURED IN 10' TYPE R SUMP INLET, PIPE TO DP19.1
	19.1			0.0.			0.00	0.0			5.66						5.04				5.1	0.14	DP19.1 FLOW, PIPE TO DP20.1
	20.1										5.64									370		1.04	DP20.1 PIPE FLOW TO POND B
	20.2	P2	2.05	0.70	6.7	1.44	7 94	11 4												15			DP20.1 PIPE FLOW TO POND B
	20.3	12	2.00	0.70	0.7	1.44	7.04	11.4			5.49									370			DP20.1 PIPE FLOW TO POND B
	21	S1	1.16	0.70	9.1	0.81	7 17	5.8	21.4				25.3	1 2/	17		0.10	0.0	2.0	580		3.71	DP21 SWALE FLOW TO DP21.1
	21.1	S2	2.32			1.62														282		1.66	DP21 SWALE FLOW TO DP21.2
	21.2	S3	1.16	0.70					26.8				30.0	2.07	2.0		3 68	5.0	2.0	45	16.1		DP21 SWALE FLOW TO POND B
	22		1.42		13.6				26.9							33.3	3.00	3.0	2.0	45	10.1	0.03	TOTAL FLOW ENTERING POND B
	E7	ROW3											29.6	3.38	4.2					865	4.1	3.52	DP E7 SWALE FLOW TO DP E9
		ROVIS	0.0478	0.49	24.4	3.36	4.00	13.6	24.4	3.30	4.00												DP E8 FLOW TO DP E9 (POND B RELEASE)
	E8	004	40.00	0.07	20.0	14.00	4.20	60.0	20.0	10.00	4.00	14.0											
	E9	OS4	40.02			14.80																	DP E9 TOTAL FLOW OFFSITE
	E10	ROW4	1.48	0.71	25.1	1.05	4.62	4.9	25.1	1.05	4.62	4.9							ļ	<u> </u>	<u> </u>		DP E10 TOTAL FLOW OFFSITE



#### **APPENDIX C - HYDRAULIC CALCULATIONS**

TO BE PROVIDED WITH THE FDR

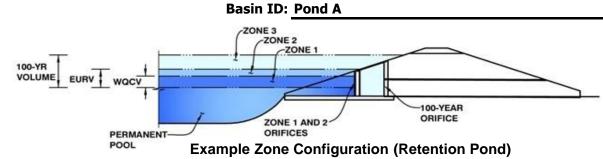


**APPENDIX D - WATER QUALITY & DETENTION** 

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)





#### Watershed Information

Selected BMP Type = **EDB** Watershed Area 25.69 acres Watershed Length 2,185 Watershed Length to Centroid = 1,100 Watershed Slope = 0.015 ft/ft 65.00% Watershed Imperviousness = percent 76.0% Percentage Hydrologic Soil Group A percent Percentage Hydrologic Soil Group B = 24.0% percent Percentage Hydrologic Soil Groups C/D = 0.0% percent Target WQCV Drain Time = 40.0 hours

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

Location for 1-hr Rainfall Depths = User Input

the embedded Colorado Urban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.544	acre-feet
Excess Urban Runoff Volume (EURV) =	2.012	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.564	acre-feet
5-yr Runoff Volume (P1 = $1.5$ in.) =	2.044	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.462	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	3.059	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.570	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.212	acre-feet
500-yr Runoff Volume (P1 = $3.14$ in.) =	5.571	acre-feet
Approximate 2-yr Detention Volume =	1.364	acre-feet
Approximate 5-yr Detention Volume =	1.794	acre-feet
Approximate 10-yr Detention Volume =	2.194	acre-feet
Approximate 25-yr Detention Volume =	2.567	acre-feet
Approximate 50-yr Detention Volume =	2.791	acre-feet
Approximate 100-yr Detention Volume =	3.050	acre-feet

#### **Define Zones and Basin Geometry**

		_
Zone 1 Volume (WQCV) =	0.544	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.468	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.038	acre-feet
Total Detention Basin Volume =	3.050	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel ( $H_{TC}$ ) =	user	ft
Slope of Trickle Channel ( $S_{TC}$ ) =	user	ft/ft
Slopes of Main Basin Sides $(S_{main}) =$	user	H:V
Basin Length-to-Width Ratio ( $R_{L/W}$ ) =	user	

		_
Initial Surcharge Area $(A_{ISV}) =$	user	ft <sup>2</sup>
Surcharge Volume Length ( $L_{ISV}$ ) =	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin $(V_{MAIN}) =$	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet

6761.5

**Optional User Overrides** 

1.19

1.50

1.75

2.00

2.25

2.52

acre-feet acre-feet

inches

inches

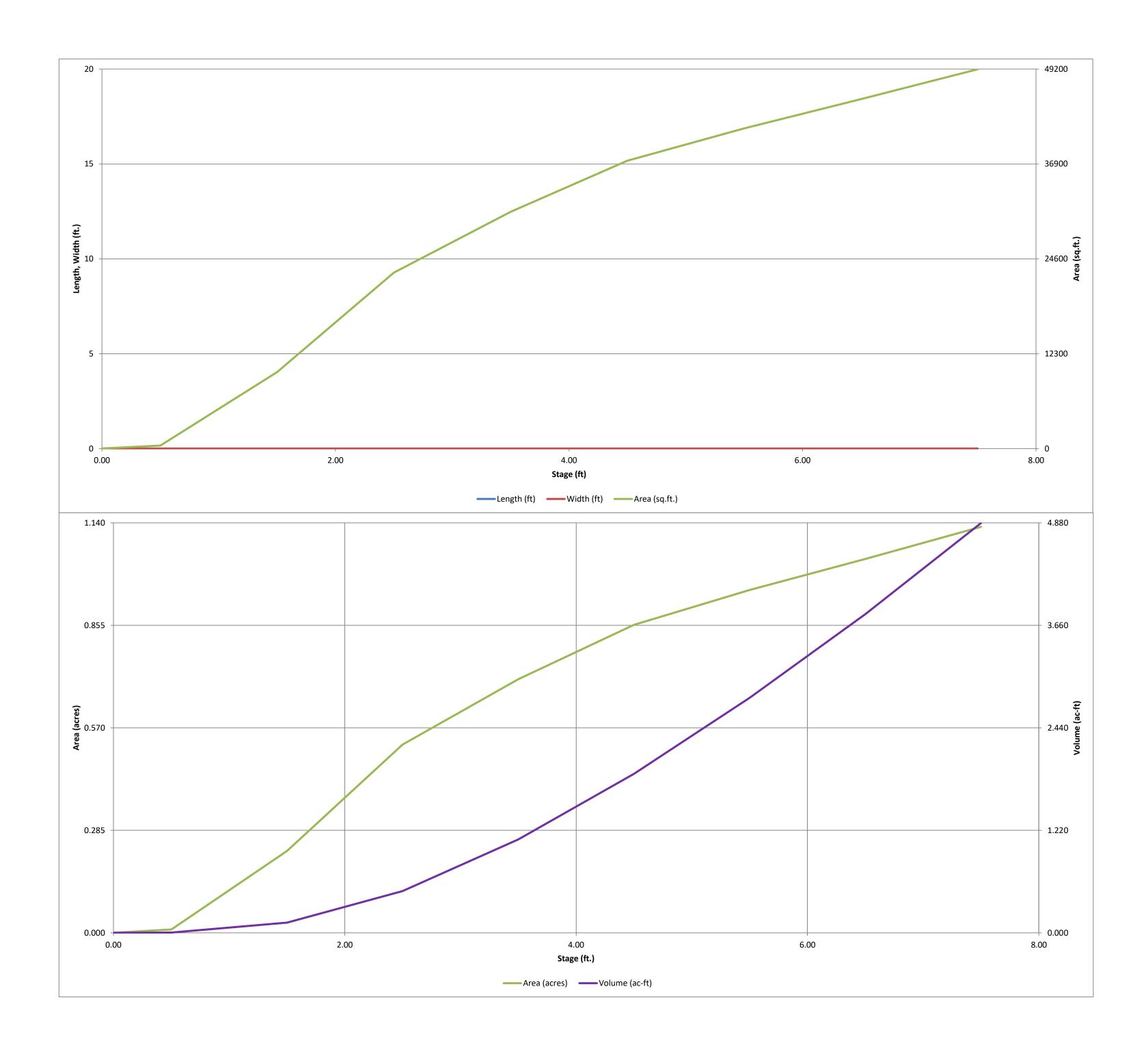
inches

inches

inches

inches inches

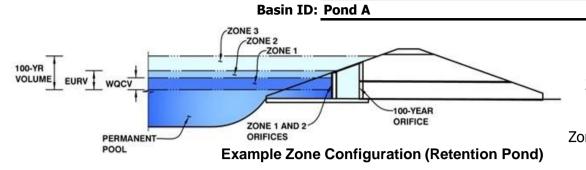
ĺ	Depth Increment =		ft			T.	Ontional		T.	I
1.5	Stage - Storage Description Top of Micropool	Stage (ft) 	Optional Override Stage (ft) 0.00	Length (ft) 	Width (ft) 	Area (ft <sup>2</sup> ) 	Optional Override Area (ft <sup>2</sup> )	Area (acre) 0.000	Volume (ft <sup>3</sup> )	Volume (ac-ft)
	6762		0.50				400	0.009	102	0.002
			1.50				9,930	0.228	5,267	0.121 0.497
	6,765.00		2.50 3.50				22,794 30,703	0.523 0.705	21,629 48,378	1.111
	0,703.00		4.50				37,312	0.857	82,385	1.891
			5.50				41,510	0.953	121,796	2.796
			6.50				45,283	1.040	165,193	3.792
	6,769.00		7.50				49,171	1.129	212,420	4.876
	•						·			
;										
									_	



10/25/2024, 1:25 PM

MHFD-Detention, Version 4.06 (July 2022)

**Project: Meadowlake Industrial F1** 



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.59	0.544	Orifice Plate
Zone 2 (EURV)	4.65	1.468	Circular Orifice
one 3 (100-year)	5.77	1.038	Weir&Pipe (Restrict)
•	Total (all zones)	3.050	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

N/A ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain N/A ft<sup>2</sup> Underdrain Orifice Area = N/A Underdrain Orifice Centroid = feet

<u>User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)</u>

Centroid of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 2.56 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing = N/A Orifice Plate: Orifice Area per Row = 1.90 sq. inches (diameter = 1-9/16 inches)

<u>Calculated Parameters for Plate</u> 1.319E-02 WQ Orifice Area per Row = Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

<u>User Input: Stage and Total Area of Each Orifice Row (numbered from lowest</u> to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.83	1.66					
Orifice Area (sq. inches)	1.90	1.90	1.90					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectang	<u>ular)</u>		_		Calculated Paramet	ters for Vertical Or	rifice
	Zone 2 Circular	Not Selected			Zone 2 Circular	Not Selected	]
Invert of Vertical Orifice =	2.60	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.06	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	4.64	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.14	N/A	feet
Vertical Orifice Diameter =	3.33	N/A	inches				-

User Input: Overflow Weir (Dropbox with Flat o	Calculated Paramet	ters for Overflow W	<u>Veir</u>			
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.67	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, $H_t$ =	4.67	N/A	feet
Overflow Weir Front Edge Length =	2.92	N/A	feet Overflow Weir Slope Length =	5.67	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	9.21	N/A	
Horiz. Length of Weir Sides =	5.67	N/A	feet Overflow Grate Open Area w/o Debris =	11.52	N/A	ft <sup>2</sup>
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris =	5.76	N/A	ft <sup>2</sup>

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice)</u>. Restrictor Plate. or Rectangular Orifice)

50%

N/A

ser Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, R	testrictor Plate, or	Rectangular Orifice)	<u>cangular Orifice</u> ) <u>Calculated Parameters for Outlet Pipe w/ Flow Restriction (Calculated Parameters for Outlet Parameters for Outlet Parameters for Outlet (</u>			
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.10	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.25	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.56	N/A	feet
Restrictor Plate Height Above Pipe Invert =	12.00		inches Half-Central Angle of	Restrictor Plate on Pipe =	1.91	N/A	radians

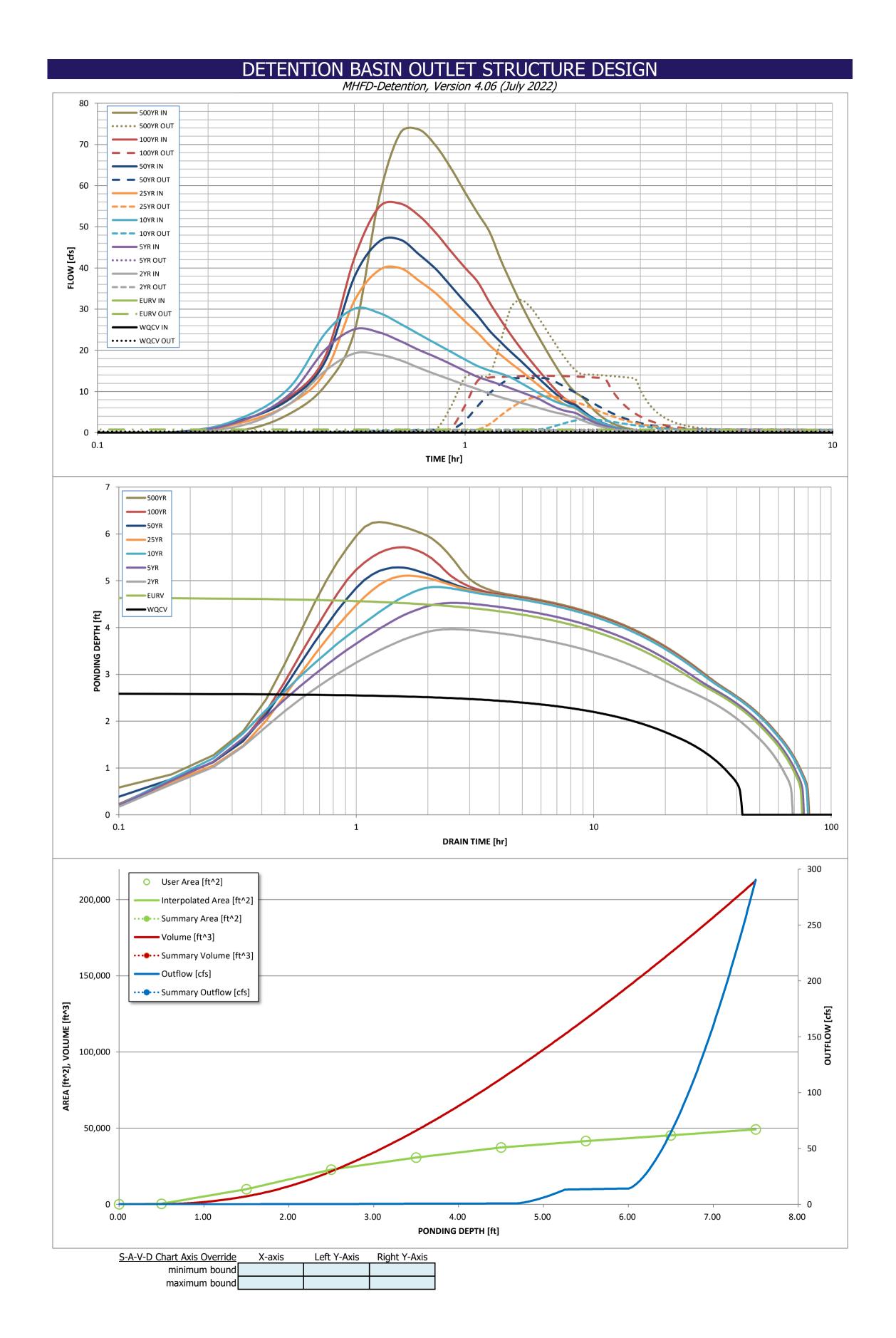
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Debris Clogging % =

inputer Errici gerief epinitra, (receariganar er		
Spillway Invert Stage=	6.00	ft (relative to basin bottom at Stage = $0$ ft)
Spillway Crest Length =	45.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

	Calculated Parameters for Spillw				
Spillway Design Flow Depth=	0.50	feet			
Stage at Top of Freeboard =		feet			
Basin Area at Top of Freeboard =	1.13	acres			
Basin Volume at Top of Freeboard =		acre-ft			

Routed Hydrograph Results	The user can over	ride the default CU	HP hydrographs and	d runoff volumes b	y entering new valu	ues in the Inflow Hy	ydrographs table (C	Columns W through	AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.544	2.012	1.564	2.044	2.462	3.059	3.570	4.212	5.571
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.564	2.044	2.462	3.059	3.570	4.212	5.571
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.2	0.3	1.5	6.7	10.0	14.9	24.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.06	0.26	0.39	0.58	0.96
Peak Inflow Q (cfs) =	N/A	N/A	19.3	25.1	30.1	40.0	46.9	55.6	73.6
Peak Outflow Q (cfs) =	0.2	0.8	0.7	0.8	3.2	8.9	13.2	13.8	32.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.4	2.1	1.3	1.3	0.9	1.3
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.2	0.7	1.1	1.1	1.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	65	60	67	68	67	65	64	60
Time to Drain 99% of Inflow Volume (hours) =	41	71	65	72	74	74	73	73	71
Maximum Ponding Depth (ft) =	2.59	4.64	3.96	4.53	4.87	5.11	5.29	5.71	6.26
Area at Maximum Ponding Depth (acres) =	0.54	0.87	0.77	0.86	0.89	0.91	0.93	0.97	1.02
Maximum Volume Stored (acre-ft) =	0.544	2.012	1.451	1.908	2.206	2.423	2.589	2.998	3.535



Outflow Hydrograph Workbook Filename:

### Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

I	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval										
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]		10 Year [cfs]				500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.21	0.02	0.69
ŀ	0:15:00	0.00	0.00	1.88	3.07	3.80	2.56	3.23	3.12	4.60
	0:20:00 0:25:00	0.00	0.00	7.01	9.34	11.01	6.97	8.17	8.69	11.43
	0:30:00	0.00	0.00	15.04 19.25	20.14 25.11	24.13 30.10	14.76 32.01	17.31 37.78	18.57 42.36	24.49 56.85
	0:35:00	0.00	0.00	18.98	24.37	29.09	39.46	46.38	54.75	72.76
	0:40:00	0.00	0.00	17.58	22.25	26.46	39.95	46.87	55.63	73.61
	0:45:00	0.00	0.00	15.74	20.08	23.90	36.89	43.28	52.69	69.67
	0:50:00	0.00	0.00	14.17	18.35	21.64	33.82	39.73	48.50	64.18
	0:55:00	0.00	0.00	12.84	16.63	19.63	30.29	35.57	44.00	58.38
	1:00:00	0.00	0.00	11.61	14.98	17.77	27.06	31.72	40.07	53.29
	1:05:00	0.00	0.00	10.55	13.56	16.17	24.21	28.33	36.59	48.74
	1:10:00	0.00	0.00	9.47	12.56	15.08	21.22	24.76	31.63	42.06
ŀ	1:15:00 1:20:00	0.00	0.00	8.61	11.68	14.37	18.91	22.03	27.45	36.48
	1:25:00	0.00	0.00	7.91 7.27	10.77 9.89	13.39 12.11	16.87 15.09	19.60 17.47	23.75 20.55	31.48 27.13
ŀ	1:30:00	0.00	0.00	6.67	9.06	10.86	13.27	15.33	17.77	23.36
	1:35:00	0.00	0.00	6.06	8.26	9.67	11.56	13.31	15.23	19.93
	1:40:00	0.00	0.00	5.48	7.22	8.58	9.97	11.44	12.88	16.76
	1:45:00	0.00	0.00	4.96	6.26	7.65	8.53	9.74	10.75	13.90
	1:50:00	0.00	0.00	4.59	5.54	6.99	7.28	8.28	8.93	11.47
	1:55:00	0.00	0.00	4.09	5.12	6.53	6.39	7.24	7.61	9.73
	2:00:00	0.00	0.00	3.67	4.76	6.03	5.87	6.64	6.82	8.68
	2:05:00	0.00	0.00	3.02	3.95	5.00	4.80	5.43	5.49	6.96
ŀ	2:10:00	0.00	0.00	2.42	3.15	4.01	3.80	4.28	4.26	5.39
	2:15:00	0.00	0.00	1.93	2.51	3.19	2.99	3.37	3.29	4.14
ŀ	2:20:00	0.00	0.00	1.53	1.99	2.53	2.35	2.65	2.53	3.17
	2:25:00 2:30:00	0.00	0.00	1.21 0.95	1.57 1.22	1.99 1.54	1.85	2.07	1.95 1.50	2.43 1.86
ŀ	2:35:00	0.00	0.00	0.93	0.94	1.18	1.43 1.10	1.61 1.23	1.15	1.43
	2:40:00	0.00	0.00	0.57	0.71	0.90	0.84	0.94	0.88	1.10
	2:45:00	0.00	0.00	0.44	0.54	0.70	0.65	0.72	0.69	0.85
	2:50:00	0.00	0.00	0.33	0.41	0.53	0.49	0.55	0.53	0.65
	2:55:00	0.00	0.00	0.23	0.29	0.38	0.36	0.41	0.39	0.48
	3:00:00	0.00	0.00	0.16	0.20	0.26	0.25	0.28	0.27	0.33
	3:05:00	0.00	0.00	0.09	0.13	0.16	0.16	0.18	0.17	0.21
	3:10:00	0.00	0.00	0.05	0.07	0.09	0.09	0.10	0.10	0.12
	3:15:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.04	0.05
	3:20:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:25:00 3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ľ	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
İ	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

# DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

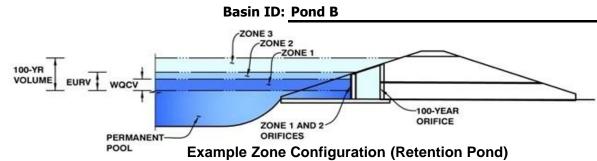
Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft <sup>3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor
							from the S-A-V table on Sheet 'Basin'.
							- Sheet basin.
							Also include the inverts of a
							outlets (e.g. vertical orifice,
							overflow grate, and spillway
							where applicable).
							-
							-
							-
							-
							1
							1
							1
							_
							4
							-
							-
							-
							-
							-
							1
							7
							1
							-
							-
							-
							-
							-
							1
							1
							_
							_
							-
							-
							-
							-
							-
							_
							-
							-
							-
							1
							]
							4
							4

## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Depth Increment =

### Project: Meadowlake Industrial F1



### Watershed Information

ersned information		
Selected BMP Type =	EDB	
Watershed Area =	20.80	acres
Watershed Length =	1,280	ft
Watershed Length to Centroid =	640	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	68.00%	percent
Percentage Hydrologic Soil Group A =	23.0%	percent
Percentage Hydrologic Soil Group B =	77.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Location for 1-hr Rainfall Depths = User Input

the embedded Colorado Urban Hydro	the embedded Colorado Urban Hydrograph Procedure.									
Water Quality Capture Volume (WQCV) =	0.462	acre-feet								
Excess Urban Runoff Volume (EURV) =	1.602	acre-feet								
2-yr Runoff Volume (P1 = 1.19 in.) =	1.338	acre-feet								
5-yr Runoff Volume (P1 = $1.5$ in.) =	1.813	acre-feet								
10-yr Runoff Volume (P1 = 1.75 in.) =	2.208	acre-feet								
25-yr Runoff Volume (P1 = 2 in.) =	2.708	acre-feet								
50-yr Runoff Volume (P1 = 2.25 in.) =	3.140	acre-feet								
100-yr Runoff Volume (P1 = 2.52 in.) =	3.668	acre-feet								
500-yr Runoff Volume (P1 = 3.14 in.) =	4.756	acre-feet								
Approximate 2-yr Detention Volume =	1.196	acre-feet								
Approximate 5-yr Detention Volume =	1.590	acre-feet								
Approximate 10-yr Detention Volume =	1.992	acre-feet								
Approximate 25-yr Detention Volume =	2.194	acre-feet								
Approximate 50-yr Detention Volume =	2.313	acre-feet								
Approximate 100-yr Detention Volume =	2.496	acre-feet								

#### **Define Zones and Basin Geometry**

anne Zones and Dasin Geometry		
Zone 1 Volume (WQCV) =	0.462	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.141	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.894	acre-feet
Total Detention Basin Volume =	2.496	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel ( $S_{TC}$ ) =	user	ft/ft
Slopes of Main Basin Sides $(S_{main}) =$	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
·		

Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length ( $L_{ISV}$ ) =	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin $(V_{MAIN}) =$	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet
•		•

6732.5 **T** 

**Optional User Overrides** 

1.19

1.50

1.75

2.00

2.25

acre-feet acre-feet

inches

inches

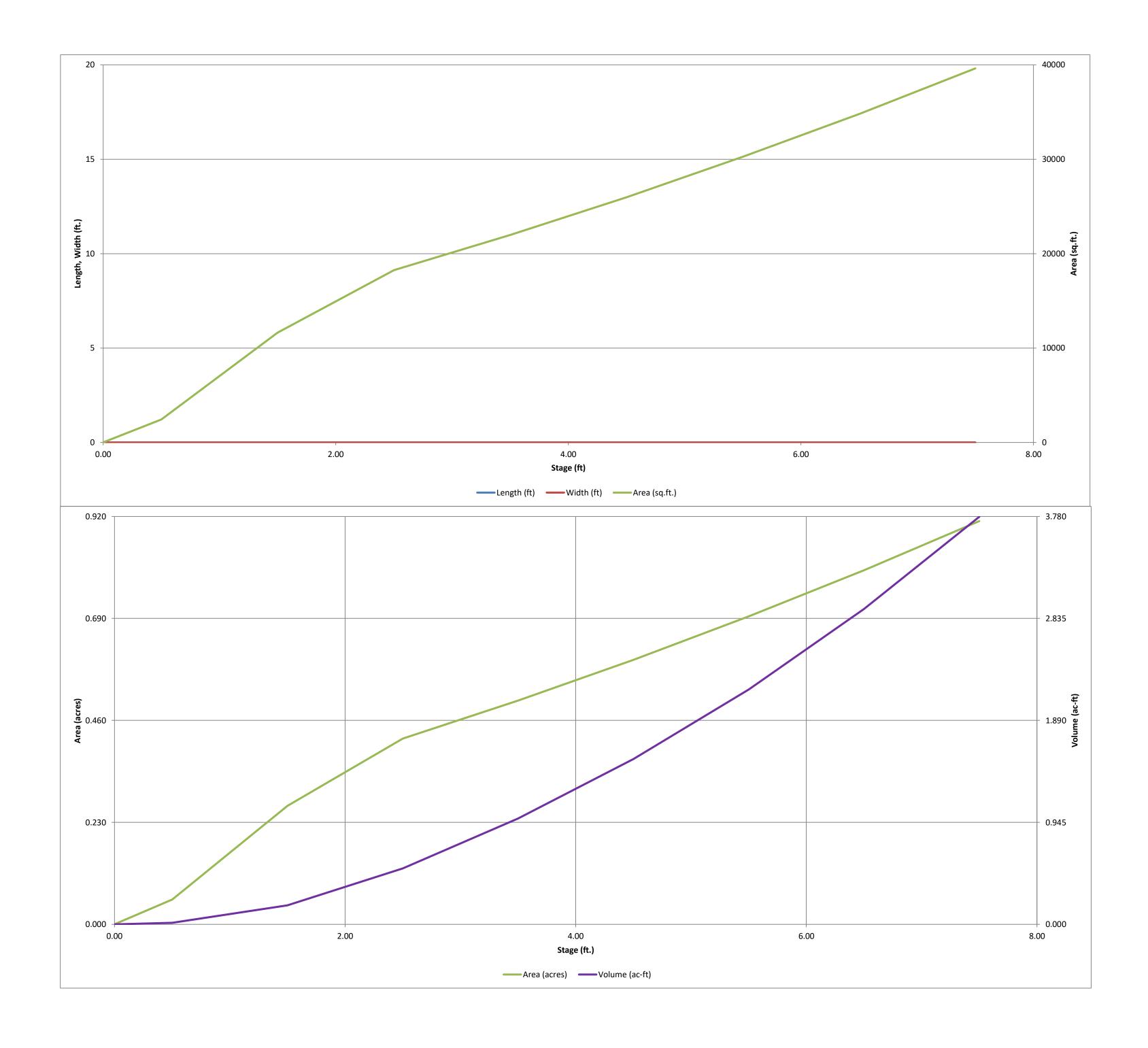
inches

inches inches

inches inches

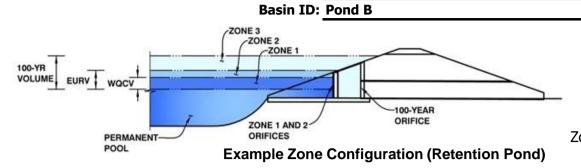
Бериі	Increment =		ft	1	1	1	Ontional	1	T	1
De:	e - Storage scription f Micropool	Stage (ft) 	Optional Override Stage (ft) 0.00	Length (ft) 	Width (ft) 	Area (ft ²) 	Optional Override Area (ft <sup>2</sup> )	Area (acre) 0.000	Volume (ft <sup>3</sup> )	Volume (ac-ft)
	6733		0.50				2,433	0.056	611	0.014
			1.50				11,642	0.267	7,648	0.176
	6735		2.50				18,245	0.419	22,592	0.519
			3.50				21,975	0.504	42,702	0.980
			4.50				25,977	0.596	66,678	1.531
			5.50				30,252	0.694	94,792	2.176
			6.50				34,801	0.799	127,319	2.923
	6740		7.50				39,622	0.910	164,530	3.777
										1
										<del>                                     </del>
										<del> </del>
										<u> </u>
										<u> </u>
										1
										<u> </u>
										<u> </u>
										-
										ļ
										ļ
										<u> </u>
										<u> </u>
										ļ
										<u> </u>
										<u>L</u>
										<del>                                     </del>
										<del> </del>
										<del> </del>
										<u> </u>
										ļ
										<del></del>
				<u></u>				<u> </u>	1	10/25/2024

MHFD-Detention\_v4-06-SOUTH\_POND.xlsm, Basin



MHFD-Detention, Version 4.06 (July 2022)

**Project: Meadowlake Industrial F1** 



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.37	0.462	Orifice Plate
Zone 2 (EURV)	4.62	1.141	Circular Orifice
Zone 3 (100-year)	5.95	0.894	Weir&Pipe (Restrict
•	Total (all zones)	2,496	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain ft<sup>2</sup> Underdrain Orifice Area = Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) 2.37 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) 10.00 Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row = 2.07 sq. inches (diameter = 1-5/8 inches)

Calculated Parameters for Plate 1.440E-02 WQ Orifice Area per Row = Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

<u>User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)</u>

and Total Area of Each office Now (nambered from lowest to highest)										
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)		
Stage of Orifice Centroid (ft)	0.00	0.80	1.60							
Orifice Area (sq. inches)	2.07	2.07	2.07							

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectang	Calculated Parameters for Vertical Orifice						
	Zone 2 Circular	Not Selected			Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.50	N/A	ft (relative to basin bottom at Stage = $0 \text{ ft}$ )	Vertical Orifice Area =	0.02	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	4.78	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.08	N/A	feet
Vertical Orifice Diameter =	2.00	N/A	linches				•

<u>User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)</u> Zone 3 Weir Not Selected ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge,  $H_t$  = 4.67 N/A Overflow Weir Front Edge Height, Ho = 4.67 Overflow Weir Front Edge Length = 2.92 N/A feet Overflow Weir Slope Length = 5.67

Overflow Weir Grate Slope = 0.00 N/A H:V Grate Open Area / 100-yr Orifice Area = 5.67 Horiz. Length of Weir Sides = N/A feet Overflow Grate Open Area w/o Debris = Type C Grate N/A Overflow Grate Open Area w/ Debris = Overflow Grate Type = 50% N/A Debris Clogging % =

Calculated Parameters for Overflow Weir Zone 3 Weir Not Selected N/A feet N/A feet 9.62 N/A 11.52 N/A 5.76 N/A

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice)</u>. Restrictor Plate. or Rectangular Orifice)

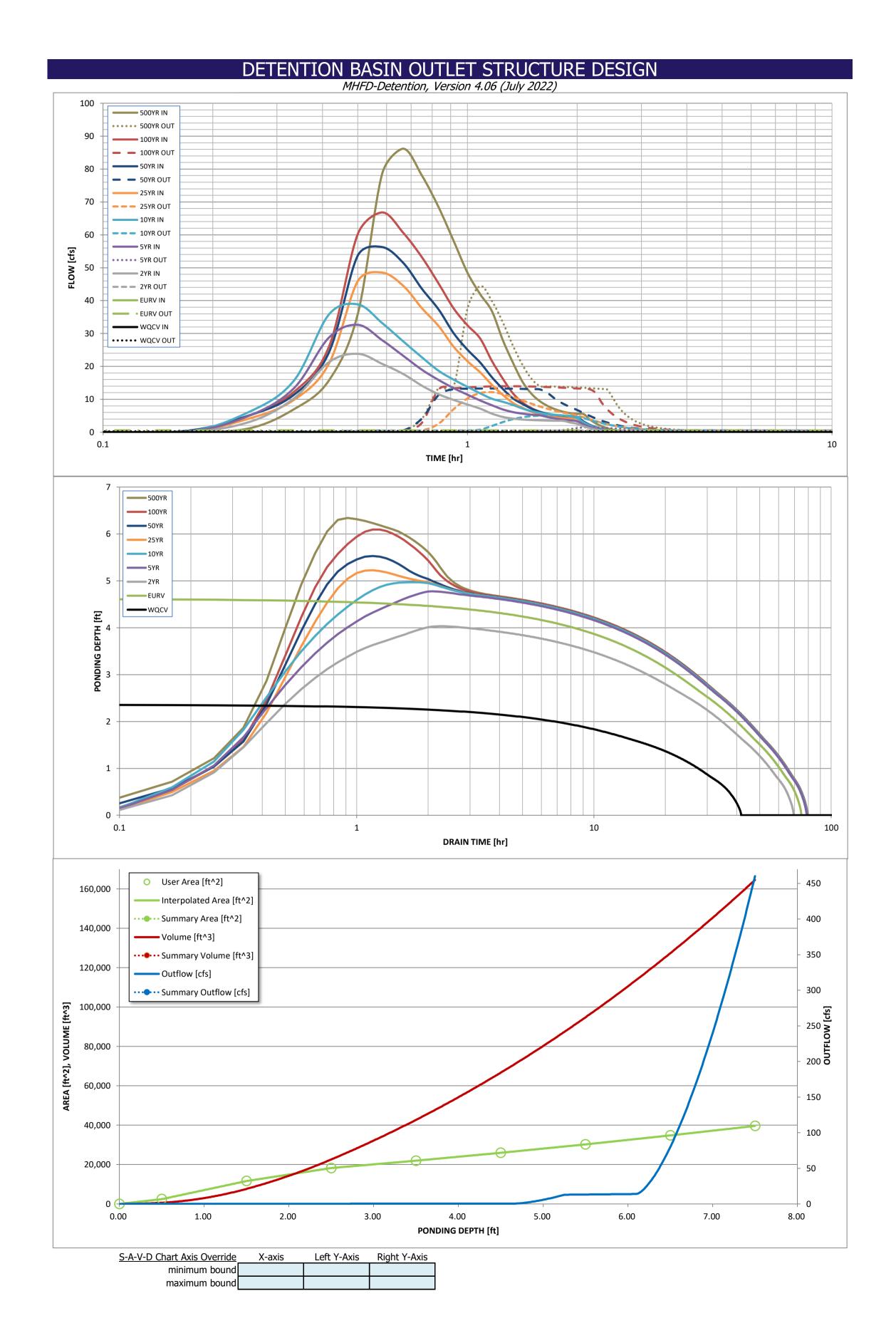
ser Input: Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice, R	estrictor Plate, or	Rectangular Orifice)	Calculated Parameters	Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate			
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected		
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.20	N/A	ft <sup>2</sup>	
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.47	N/A	feet	
Restrictor Plate Height Above Pipe Invert =	9.75		inches Half-Central Angle of R	Restrictor Plate on Pipe =	1.38	N/A	radians	

User Input: Emergency Spillway (Rectangular or Trapezoidal)

ipati Emergency opiniway (Neetangalai ol	Trapezolaarj	
Spillway Invert Stage=	6.10	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	85.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway Spillway Design Flow Depth= 0.40 feet 7.50 Stage at Top of Freeboard = feet Basin Area at Top of Freeboard = 0.91 acres Basin Volume at Top of Freeboard = 3.78 acre-ft

Routed Hydrograph Results	The user can ove	rride the default CU	HP hydrographs an	d runoff volumes h	v enterina new vali	ues in the Inflow Hu	ydrographs table ((	Columns W through	ΔE)
Design Storm Return Period =		EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	_	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.462	1.602	1.338	1.813	2.208	2.708	3.140	3.668	4.756
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.338	1.813	2.208	2.708	3.140	3.668	4.756
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.4	4.7	7.9	15.3	19.8	25.8	36.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.02	0.22	0.38	0.74	0.95	1.24	1.77
Peak Inflow Q (cfs) =	N/A	N/A	23.8	32.6	38.9	48.5	56.3	66.8	86.2
Peak Outflow Q (cfs) =	0.3	0.6	0.5	1.5	5.1	12.2	13.3	14.0	44.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.3	0.7	0.8	0.7	0.5	1.2
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.4	1.0	1.1	1.2	1.2
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	63	59	66	65	64	62	61	58
Time to Drain 99% of Inflow Volume (hours) =	40	70	65	73	73	72	71	70	68
Maximum Ponding Depth (ft) =	2.37	4.62	4.03	4.78	4.97	5.23	5.53	6.09	6.34
Area at Maximum Ponding Depth (acres) =	0.40	0.61	0.55	0.62	0.64	0.67	0.70	0.76	0.78
Maximum Volume Stored (acre-ft) =	0.465	1.603	1.261	1.695	1.815	1.986	2.197	2.604	2.789



Outflow Hydrograph Workbook Filename:

### Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]		25 Year [cfs]			500 Year [cfs]
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00 0.34	0.00	0.00 1.08
	0:15:00	0.00	0.00	2.98	4.86	6.02	4.04	4.99	4.91	6.90
	0:20:00	0.00	0.00	10.18	13.25	15.54	9.74	11.29	12.15	15.71
	0:25:00	0.00	0.00	21.27	28.75	35.77	20.78	24.21	25.93	35.87
	0:30:00	0.00	0.00	23.82	32.63	38.86	45.91	53.67	60.20	78.55
	0:35:00	0.00	0.00	20.77	27.97	33.18	48.53	56.28	66.81	86.19
	0:40:00	0.00	0.00	17.68	23.21	27.59	44.49	51.46	60.60	78.04
	0:45:00 0:50:00	0.00	0.00	14.13 11.53	18.97 15.87	22.76 18.66	37.68 32.28	43.59 37.32	53.19 45.20	68.40 58.13
	0:55:00	0.00	0.00	9.80	13.38	15.97	25.96	30.08	37.62	48.50
	1:00:00	0.00	0.00	8.41	11.40	13.79	21.59	25.08	32.50	41.98
	1:05:00	0.00	0.00	7.16	9.64	11.81	18.21	21.20	28.50	36.84
	1:10:00	0.00	0.00	5.64	8.19	10.17	14.41	16.73	21.68	28.02
	1:15:00	0.00	0.00	4.64	6.92	9.24	11.36	13.15	16.28	21.11
	1:20:00	0.00	0.00	4.12	6.10	8.27	8.87	10.27	11.80	15.28
	1:25:00	0.00	0.00	3.84	5.63	7.17	7.40	8.56	9.00	11.62
	1:30:00 1:35:00	0.00	0.00	3.68	5.32	6.41	6.19	7.13	7.27	9.34
	1:40:00	0.00	0.00	3.59 3.52	5.11 4.54	5.88 5.50	5.40 4.89	6.18 5.57	6.16 5.41	7.87 6.87
	1:45:00	0.00	0.00	3.47	4.12	5.25	4.55	5.16	4.90	6.20
	1:50:00	0.00	0.00	3.44	3.82	5.06	4.32	4.88	4.58	5.76
	1:55:00	0.00	0.00	2.93	3.60	4.78	4.19	4.72	4.43	5.57
	2:00:00	0.00	0.00	2.56	3.34	4.29	4.10	4.62	4.37	5.49
	2:05:00	0.00	0.00	1.80	2.34	3.00	2.88	3.24	3.08	3.87
	2:10:00 2:15:00	0.00	0.00	1.23	1.61	2.06	1.98	2.23	2.13	2.67
	2:20:00	0.00	0.00	0.83 0.55	1.08 0.70	1.40 0.92	1.36 0.90	1.53 1.01	1.46 0.96	1.83 1.21
	2:25:00	0.00	0.00	0.34	0.45	0.59	0.58	0.65	0.62	0.78
	2:30:00	0.00	0.00	0.20	0.28	0.36	0.37	0.41	0.39	0.49
	2:35:00	0.00	0.00	0.10	0.15	0.19	0.20	0.23	0.22	0.27
	2:40:00	0.00	0.00	0.04	0.06	0.08	0.09	0.10	0.09	0.11
	2:45:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00 3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00 4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

# DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft <sup>3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor
							from the S-A-V table on Sheet 'Basin'.
							Also include the inverts of a
							outlets (e.g. vertical orifice, overflow grate, and spillway
							where applicable).
							, ,
							_
							1
							1
							4
							-
							-
							_
							_
							_
							_
							-
							-
							-
							†
							1
							-
							1
							1
							<del></del> t



#### APPENDIX E - DRAINAGE MAPS

