

EPC STORMWATER REVIEW COMMENTS IN ORANGE BOXES WITH BLACK TEXT

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Preliminary Drainage Report Meadow Lake Industrial Filing No. 1 El Paso County, Colorado

August, 2023 HR Green Project No: 2202774

Prepared For:

Meadowlake Developments, LLC. Contact: Kevin O'Neil PO Box 1385 Colorado Springs, CO 80901

Prepared By:

HR Green Development, LLC Contact: Colleen Monahan, PE cmonahan@hrgreen.com (719) 394-2433

PCD File No. TBD SP236



Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Date

Colleen	Monahan,	PE
COllecti	wonanan,	

State of Colorado No.

For and on behalf of HR Green Development, LLC

Owner/Developer's Statement

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Authorized Signature

Date

Address: Meadowlake Developments, LLC. PO Box 1385

Colorado Springs, CO 80901

El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

Joshua Palmer, P.E.

Date

County Engineer/ECM Administrator

Conditions:



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I. General Purpose, Location and Description

a. Purpose

The purpose of the Preliminary Drainage Report (PDR) for Meadow Lake Industrial Filing No. 1 is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls.

b. Location

Meadow Lake Industrial Filing No. 1, referred to as 'the site' herein, is 254 acres of undeveloped land. A 51.3 acre portion of the site will be developed as an industrial subdivision, Filing No. 1, and the remaining area will be undeveloped. The site lies within a part of the east half of Section 9, Township 13 South, Range 64 West of the 6th P.M., El Paso County, Colorado. The site is bound to the north and west by undeveloped land, to the east by Curtis Road, and to the south by Falcon Highway. A vicinity map is presented in Appendix A.

c. Description of Property

The property is currently undeveloped and unplatted. The developed site will plat 27 industrial lots and two drainage tracts on approximately 51.3 acres. The site is generally bisected by a ridge that directs stormwater east towards Curtis Road and west towards an unnamed tributary. The unnamed tributary runs north-south through the site, however; all development will occur east of the tributary. There are no existing utilities on the site. Onsite vegetation consists primarily of native grasses and weeds. Per a NRCS web soil survey, the site's soil is comprised of Type A soils: Blakeland loamy sand, Truckton loamy sand and Columbine gravelly sandy loam, Type B soil Stapleton sandy loam, and Type D soil Fluvaquentic Haplaquolls. A NRCS soil survey is presented in Appendix A.

d. Floodplain Statement

Based on FEMA FIRM 08041C0558G & 08041C0566G, revised December 7, 2018, there are no floodplains (Zone A or Zone X) within the Filing No. 1 boundary. Zone A areas determined to be within the 1.0% annual chance flood but do not have base flood elevations established. Zone X are areas determined to be outside the 0.2% annual chance flood. The FIRM is presented in Appendix A.

II. Drainage Design Criteria

a. Drainage Criteria

Hydrologic data and calculations were performed using the El Paso County Drainage Criteria Manual Volume 1 & 2 (EPCDCM), with current revisions.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from CCSDCM Table 6-2. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1. The detention pond allowable release rate will be limited to less than historic rates.

Table 6-2: Rainfall Depths for El Paso County									
Return Period (yr)	5	100							
1-hr Rainfall Depth (in)	1.50	2.52							



Revise drainage report to include all of the offsite basins that drain to this site. Per the streamstats application there is a large area upstream of this site.

Inlets were sized per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer was sized per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

III. Drainage Basins and Subbasins

a. Previous Drainage Studies

These existing drainage basins are much larger than the proposed. The existing and proposed basins should be looking at approximately the same areas for comparison between the existing and developed conditions.

undeveloped area in basin B as it is

The site is primarily located within the Solberg Ranch Drainage Basin. Solberg Ranch does not have a Drainage Basin Planning Study (DBPS) on file with El Paso County.

b. Existing Subbasin Description

Basin EX1 is 200.66 acres of undeveloped area. Stormwater ($Q_5 = 18.9$ cfs $Q_{100} = 126.8$ cfs) flows south in the unnamed tributary to DP1.

Basin EX2 is 45.17 acres of undeveloped area. Stormwater ($Q_5 = 5.1$ cfs $Q_{100} = 26.7$ cfs) flows south in a roadside ditch adjacent to Curtis Road to DP2.

Basin EX3 is 8.49 acres of undeveloped area. Stormwater ($Q_5 = 1.5 \text{ cfs } Q_{100} = 9.8 \text{ cfs}$) flows north in aroadside ditch adjacent to Curtis Road to DP3.it does not appear that there is

c. Proposed Subbasin Description

all lots and roadway. revise Basin A is 4.79 acres of roadway and undeveloped area. Stormwater ($Q_5 = 5.3 \text{ cfs } Q_{100} = 14.1 \text{ cfs}$) is captured at DP1 in a public 10' Type R sump inlet. In the event of inlet failure at DP1, an overflow path is provided in Greenfield Avenue to Pond A. Basin A will be detained in Pond A.

Basin B is 1.68 acres of roadway and undeveloped area. Stormwater ($Q_5 = 5.7$ cfs $Q_{100} = 10.4$ cfs) is captured at DP2 in a public 5' Type R sump inlet. In the event of inlet failure at DP2, an overflow path is provided in Greenfield Avenue to Pond A. Basin B will be detained in Pond A.

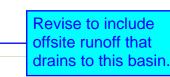
Basin C is 2.93 acres of industrial lots and roadway. Stormwater ($Q_5 = 6.8$ cfs $Q_{100} = 13.5$ cfs) is captured at DP3 in a private 20' Type R on-grade inlet in Wild Iris Way. Basin C will be detained in Pond A. In the event of inlet failure at DP3, an overflow path is provided in Wild Iris Way to Pond A.

Basin D is 2.92 acres of industrial lots and roadway. Stormwater ($Q_5 = 7.0$ cfs $Q_{100} = 14.0$ cfs) is captured at DP4 in a private 20' Type R on-grade inlet in Wild Iris Way. Basin D will be detained in Pond A. In the event of inlet failure at DP3, an overflow path is provided in Wild Iris Way to Pond A.

Basin E is 3.54 acres of industrial lots and roadway. Stormwater ($Q_5 = 8.5$ cfs $Q_{100} = 16.9$ cfs) is captured at DP5 in a private 15' Type R sump inlet in Wild Iris Way. Basin E will be detained in Pond A. In the event of inlet failure at DP3, an overflow path is provided in Wild Iris Way to Pond A by overtopping the curb and gutter at the knuckle.

Basin F is 1.70 acres of industrial lots and roadway. Stormwater ($Q_5 = 4.7$ cfs $Q_{100} = 8.7$ cfs) is captured at DP6 in a private 15' Type R sump inlet in Wild Iris Way. Basin F will be detained in Pond A. In the event of inlet failure at DP3, an overflow path is provided in Wild Iris Way to Pond A by overtopping the curb and gutter at the knuckle.

Basin G is 9.87 acres of industrial lots and undeveloped area. Stormwater ($Q_5 = 14.9$ cfs $Q_{100} = 30.3$ cfs) is captured at DP7 and conveyed in a swale to Pond A. Basin G will be detained in Pond A.





Basin H is 2.33 acres of industrial lots and undeveloped area. Stormwater ($Q_5 = 4.6$ cfs $Q_{100} = 9.6$ cfs) is captured at DP8 and conveyed in a swale to Pond A. Basin H will be detained in Pond A.

Basin I is 1.25 acres of industrial lots and undeveloped area. Stormwater ($Q_5 = 2.5$ cfs $Q_{100} = 5.2$ cfs) is captured at DP9 and conveyed in a swale to Pond A. Basin G will be detained in Pond A.

Basin J is 3.00 acres and contains Pond A. Stormwater ($Q_5 = 2.7$ cfs $Q_{100} = 8.6$ cfs) sheet flows directly to Pond A. Basin J will be detained in Pond A.

Basin K is 0.42 acres of roadway. Stormwater ($Q_5 = 1.8 \text{ cfs } Q_{100} = 3.3 \text{ cfs}$) is captured at DP11 in a public 5' Type R sump inlet in Sagebrush Street. In the event of inlet failure at DP11, an overflow path is provided in Swale B to Pond B. Basin K will be detained in Pond B.

Basin L is 0.42 acres of roadway. Stormwater ($Q_5 = 1.8 \text{ cfs } Q_{100} = 3.3 \text{ cfs}$) is captured at DP12 in a public 5' Type R sump inlet in Sagebrush Street. In the event of inlet failure at DP12, an overflow path is provided in Swale B to Pond B. Basin L will be detained in Pond B.

Basin M and DP14 have been omitted as they are an old basin and design point that have been removed. In order to keep all calculations consistent within this report, the proceeding basin designations and design points have not changed and remain sequential.

Basin N is 6.01 acres of industrial lots and roadway. Stormwater ($Q_5 = 14.4 \text{ cfs } Q_{100} = 28.6 \text{ cfs}$) is captured at DP15 in a public 15' Type R on-grade inlet in Mariposa Lily Court. Basin N will be detained in Pond B. In the event of inlet failure at DP15, an overflow path is provided in within the adjacent public roadway and access road that drain due south directly to Pond B.

Basin O is 3.04 acres of industrial lots and roadway. Stormwater ($Q_5 = 7.2 \text{ cfs } Q_{100} = 14.2 \text{ cfs}$) is captured at DP16 in a private 10' Type R on-grade inlet in Wildflower Court. Basin O will be detained in Pond B. In the event of inlet failure at DP16, an overflow path is provided in within the adjacent public roadway and access road that drain due south directly to Pond B.

Basin P is 3.20 acres of industrial lots and roadway. Stormwater ($Q_5 = 7.8 \text{ cfs } Q_{100} = 15.5 \text{ cfs}$) is captured at DP17 in a private 10' Type R on-grade inlet in Wildflower Court. Basin P will be detained in Pond B. In the event of inlet failure at DP17, an overflow path is provided in within the adjacent public roadway and access road that drain due south directly to Pond B.

Basin Q is 1.01 acres of roadway. Stormwater ($Q_5 = 4.0 \text{ cfs } Q_{100} = 7.6 \text{ cfs}$) is captured at DP18 in a public 5' Type R sump inlet in Greenfield Avenue. In the event of inlet failure at DP18, flows will overtop the sump and flow to Pond B along the maintenance access road. Basin Q will be detained in Pond B. In the event of inlet failure at DP18, an overflow path is provided in within the public roadway and access road that drain due south directly to Pond B.

Basin R is 1.11 acres of roadway. Stormwater ($Q_5 = 3.2$ cfs $Q_{100} = 6.2$ cfs) is captured at DP19 in a public 10' Type R sump inlet in Greenfield Avenue. In the event of inlet failure at DP19, flows will overtop the sump and flow to Pond B along the maintenance access road. Basin R will be detained in Pond B. In the event of inlet failure at DP19, an overflow path is provided in within the public roadway and access road that drain due south directly to Pond B.

Basin S is 0.85 acres of grass swale. Stormwater ($Q_5 = 0.3$ cfs $Q_{100} = 1.7$ cfs) is captured at DP21 and conveyed in a swale to Pond B. Basin S will be detained in Pond B.



Basin T is 1.19 acres and contains Pond B. Stormwater ($Q_5 = 0.4$ cfs $Q_{100} = 2.4$ cfs) sheet flows directly to Pond B. Basin T will be detained in Pond B.

IV. Drainage Facility Design

a. General Concept

Meadow Lake Industrial storm water will be collected and conveyed by a series of inlets, swales and storm sewer to two full spectrum water quality and detention ponds. The full spectrum water quality and detention ponds will discharge at less than historic rates.

b. Water Quality & Detention

Stabilized access ramp shall be a minimum of 15ft wide and no greater than 12% slope, in accordance with DCMv1, Chap 11.2.2.

Pond A

Water quality and detention for Basins A - J is provided in a full spectrum water quality and detention pond: Pond A. Pond A is located in Tract A. A total of 34.01 acres at 68% imperviousness will be detained in the pond. The WQCV is 0.755 ac-ft, the EURV is 2.133 ac-ft, and the 100-year volume is 4.274 ac-ft. The WQCV, EURV and 100-year storms are released in 40, 72 and 74 hours, respectively. A forebay is located at the outfall into the pond and a 2.0' trickle channel conveys flow towards the outlet structure. A 10' access and maintenance road is provided to the bottom of the pond to facilitate future maintenance. A 50' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Curtis Road. The spillway will be lined with Type L riprap. Pond design calculations are presented in Appendix D.

Pond B

Water quality and detention for Basins K - T is provided in a full spectrum water quality and detention pond: Pond B. Pond B is located in Tract B. A total of 17.81 acres at 74% imperviousness will be detained in the pond. The WQCV is 0.437 ac-ft, the EURV is 1.247 ac-ft, and the 100-year volume is 2.447 ac-ft. The WQCV, EURV and 100-year storms are released in 40, 72 and 73 hours, respectively. A forebay is located at the outfall into the pond and a 2.0' trickle channel conveys flow towards the outlet structure. A 10' access and maintenance road is provided to the bottom of the pond to facilitate future maintenance. An 18' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Curtis Road. The spillway will be lined with Type L riprap. Pond design calculations are presented in Appendix D.

c. Inspection and Maintenance A maintenance agreement with the County is required.

The private detention ponds are to be owned and maintained by a metropolitan district, to be established with the project. Maintenance access for the full spectrum detention facilities will be provided through private drainage easements and tracts.

d. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates.

For both narratives expand more on the ultimate outfall each pond will drain to. Per ECM 3.2.4 developed flows need to drain to a system that is hydraulically adequate. Analyze outfalls for each pond.



Step 2 - Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Onsite full spectrum detention pond provides water quality treatment for the site. The WQCV is released over a period of 40 hours.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 - Consider the need for source controls: Source controls will be required at the time of development for the industrial lots. Source control descriptions are discussed in the Stormwater Management Report for this project.

e. Drainage and Bridge Fees

This step is focused on permanent specialized source control, not the temp BMPs proposed. This project has no need of specialized source controls and that can be stated.

	d bridge fees fo platting.	r Meadow				ge fees will be paid			
	Solbo								
	e/Impervious Acre	Site Acreage	Site Impervious	Impervious Acres	Drainage Fee				
	\$23,078.00	51.3	77%	39.50	\$911,581.00				
	Probable (previously in the narrative it was stated that the site is primarily in the solberg ranch drainage basin. Per County GIS it appears that the northeast portion may be within the					
CURTIS RD	Grade Line ine analysis of		ed storm will b	Haegler Ranch drainage basin. Please indicate whether this development lies solely in the Solberg basin otherwise also include anticipated fees due for Haegler Ranch.					

Summary_A V.

Meadow Lake Industrial lies within the Solberg Ranch Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds. The water quality and detention ponds will be owned and maintained by a metropolitan district, to be established with the project. All drainage facilities were sized per the El Paso County Drainage Criteria Manuals.

VI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.

Discuss offsite flows that flow through the site. What is the condition of the natural channel labeled as the unnamed tributary where pond B outfalls. Determine if mitigation will be required because of the pond b outfall.

Revise to explain whether downstream facilities/ natural swales are hydraulically adequate to handle developed flows. What are the ultimate destinations for each outfall? Are developed flows a major increase compared to historic flows? Explain.



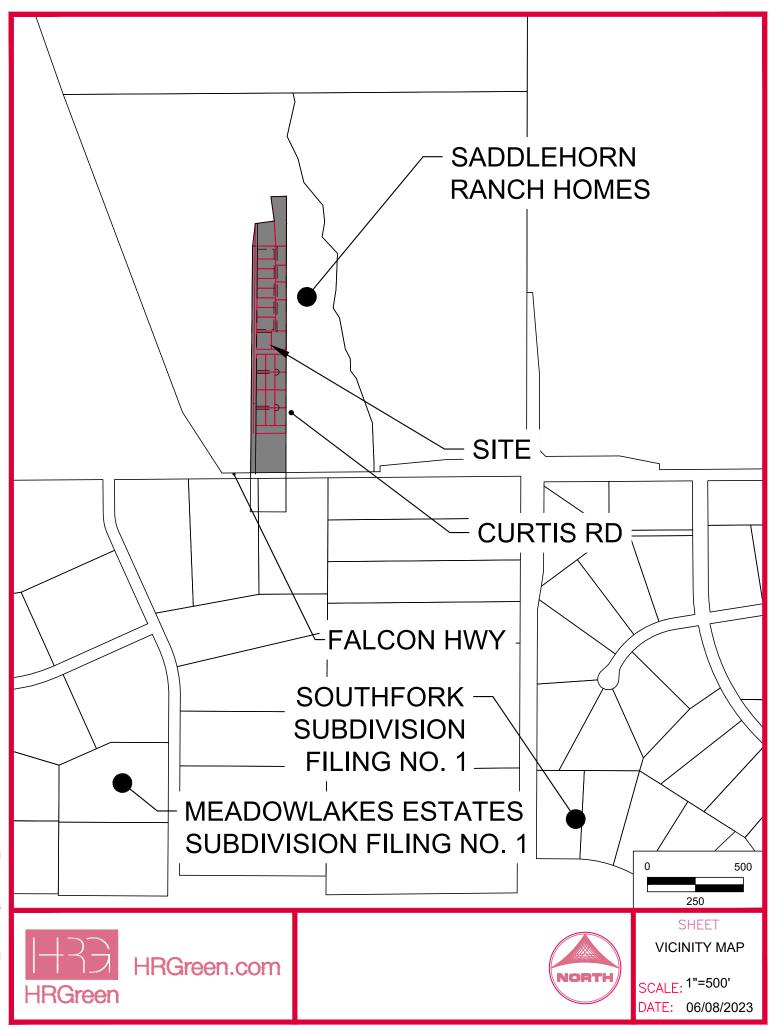
VII. References

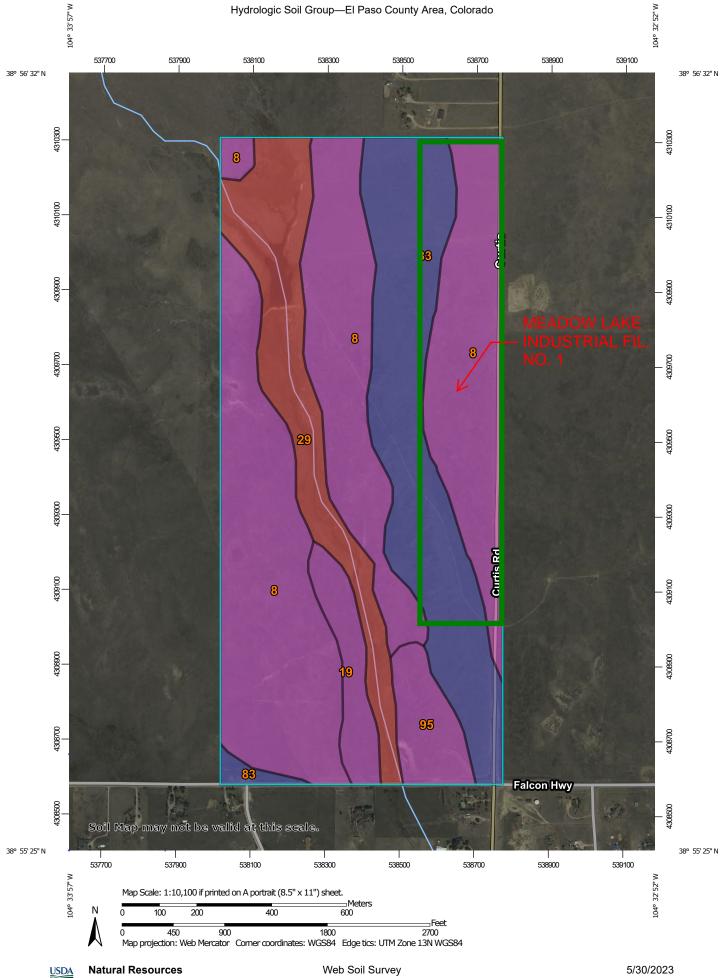
- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
- 3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.



Meadow Lake Industrial Filing No. 1 Preliminary Drainage Report Project No: 2202744

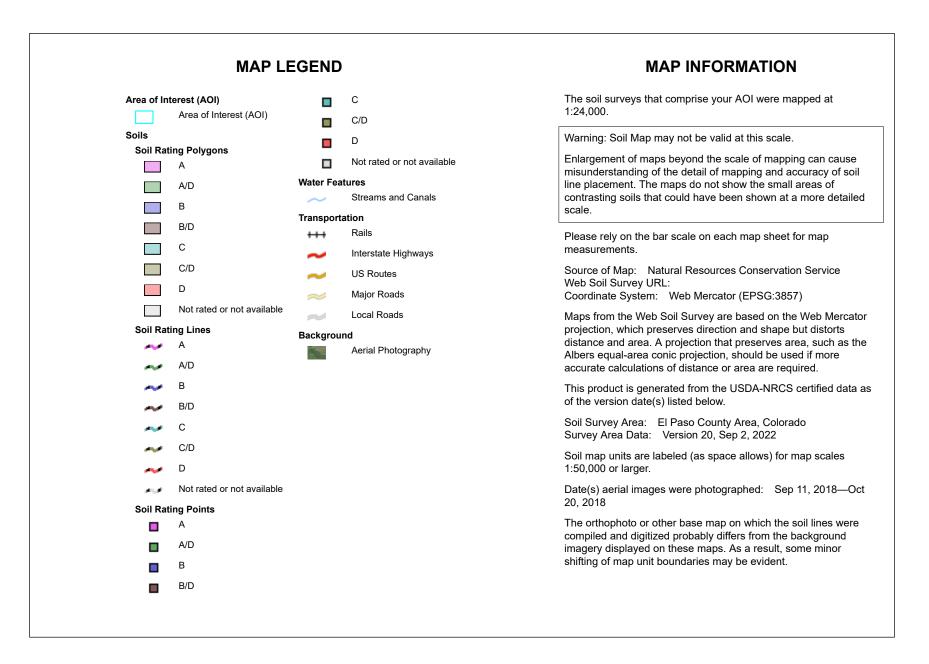
APPENDIX A - VICINITY MAP, SOIL MAP, FEMA MAP





National Cooperative Soil Survey

Conservation Service



Hydrologic Soil Group

		1		
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	174.3	53.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	13.3	4.1%
29	Fluvaquentic Haplaquolls, nearly level	D	47.2	14.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	75.9	23.4%
95	Truckton loamy sand, 1 to 9 percent slopes	A	14.0	4.3%
Totals for Area of Inter	rest		324.7	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

NOTES TO USERS

Program. It do This map is for use in administering the National Flood Insurance Program. It does to necessarily identify all areas subject to flooding, particularly from local drainage ources of small size. The community map repository should be consulted for ossible updated or additional flood hazard information.

obtain more detailed information in areas where Base Flood Elevations (BFE To obtain more detailed information in areas where Base Flood Elevations (EFEs) and/infording-base been determined, users are encouraged to consult the Flood within the Flood Insurance Study (FIS) (open that accompanies this FIRM. Users think due areas that EFEs along on the FIRM regresser to model whet been detaid on the used as the sole source of flood elevation information. According, flood elevations, These BFEs are infereded for flood elevation information. According, flood elevations, the FIRM regresser and a sole of according to the FIRM regression of and the FIRM to purpose of construction and the flood elevation information. According, flood elevation, and a presented in the FIRM regression to building elevation with the FIRM to purpose of construction and information.

Costal Base Flood Elevations shown on this map apply only landward of 0.0 North American Varical Claum of 1988 (NAVD28). Users of this FIRM should be average table in the Flood Insurance Study report for the jurisdician. Elevations shown in the Summary of Siltivater Elevations table should be used for construction and/or loog/aim management puppose when they are higher that the devations shown on the silter of the silter shown and the silter of the silter oodplain his FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolate between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Roodway width and other pertiment floodway data are provided in the Flood Insurance Study report if this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood cont** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurar Study report for information on flood control structures for this unisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NADB3. GR585 spin-rol production of HTMs for adjacent hyridicitions may result in light positional differences in map features across juridicition boundaries. These differences do not affect the accuracy of this FRM.

Flood elevations on this map are referenced to the North American Ve of 1988 (NAVD88). These flood elevations must be compared to a ground elevations referenced to the same vertical datum. For informat conversion between the National Geodetic Vertical Datum. For information regard conversion between the National Geodetic Vertical Datum of 1929 and the No American Vertical Datum of 1988, visit the National Geodetic Survey website http://www.ngs.noaa.gow/ or contact the National Geodetic Survey at the follow

ation Services GS Information 8 OAA, N/NGS12 NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench mark shown on this map, please contact the Information Services Branch of the Nationa Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

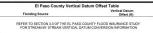
The may enforce more detailed and up to date etream channel coeffigurations and Bodglain delineations than increas shown on the previous FROM for this jurisdiction. How been adjusted to confrom to these new stream channel coeffigurations are result, the Road Profess and Roadway Data tables in the Flood Insurance Study Road (which contains authoritative induced data) may reflect stream channel show (which contains authoritative induced data) may reflect stream channel on this may represent the hydraulic code inny reflect stream channel and Floodway Data Tables i application. In the FIS report, the a result, the profess baselines may deviate adjusticity from the new base may channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel representation and may approximation of the flood inter the stream channel stream channel representation and may approximation of the flood inter the stream channel in the stream channel in

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a using of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is learned.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchang Cutilia: Food manage betwee Generating (in C) year and in Food Manage Textual textual regulation on available products associated with this FRM. Available products are included providuosly issued Laters of Mang Change, a Proof insurance Study Report and/or dylativersion of the map. The MSC may also be reached by Fax at 1-400-358-9620 and its website at the//www.mc.Emm.agovi.

f you have questions about this map or questions concerning the National Floor insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2827) o visit the FEMA website at http://www.fema.gov/business/nfip.





This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperaing Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



LEGEND SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD 3275000 FT 104" 31' 52.50" The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Haard Area is the area subject to flooding by the 1% arrunal chance flood. Areas of Special Flood Haard include Zones A, AE, AH, AD, AR, A93, V, and VE. The Base Flood Elevation is the water-sufroce devolution of the 1% annual chance flood. 3270000 FT JOINS PANEL 055 104" 33' 45.00 38' 58' 7.50" 18: 58: 7 50 ZONE A ZONE A ZONE AE ZONE AH No Base Flood Bevations determined. Base Flood Bevations determined. Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Beaution; determined ZONE A [24] Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also depths. ZONE AO EL PASO COUNTY UNINCORPORATED AREAS determined. Special Road Hazard Area Formerly protected from the 1% annual chance food by a flood control system that was subsequently descripted. Jone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. ZONE AR Area to be protected from 1% emails charge greater 1900. Area to be protected from 1% emails charce flood by a federal flood protection system under construction; no Base Flood Elevations determined. Caestal flood zone with velocity hazard (wave action); no Base Flood Bevators determined. ZONE A99 +ZONE V ZONE VE Coestal flood zone with velocity hazard (wave action); Base Flood Bevations determined. 11/1 FLOODWAY AREAS IN ZONE AE The floodway is the channel of a stream plus any adjacent floodplain areas that must be least free of encroachment so that the 1% annual chance flood can be carried without substantial increases in find heights. ZONE AE OTHER FLOOD AREAS ZONE A Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X 34 35 OTHER AREAS ZONE X ined to be outside the 0.2% annual chance floodple ZONE D Areas in which flood hazards are undetermined, but possible COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Specia Electricia boundary Floodway boundary Zone D Boundary CBRS and OPA bounda -Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. ~ 513~~ Base Rood Elevation line and value; elevation in feet* Base Rood Elevation value where uniform within zone; elevation in feet* (EL 987) ZONE AE American Vertical Datum of 1988 (NAVD 88 Cross section line 43 1 2000 11 23---23 Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 1410000 FT 97° 07' 30.00" 32" 22' 30.00" (E) T. 12 S. T. 13 S. T. 12 S. T. 13 S. 1000-meter Universal Transverse Mercator grid ticks zone 13 Ick Ranch New Telbun LIMIT OF DETAILED ST 6000000 FT 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Covic Projection DX5510 Bench mark (see exp • M1.5 River Mile MAP REPOSITORIES Refer to Map Repositories list on Map TATION LN EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL CEMBER 7, 2018 - to update corporate limits, to change Base Flood I cial Flood Hazard Anaza, to update map format, to add roads and road incorporate previously issued Latters of Man Brevious ZONE A community map revision history prior to countywide mapping, refer to the Cor History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620. SEMINOLE LN W WEST WIND LN ZONE AE EL PASO COUNTY UNINCORPORATED AREAS MAP SCALE 1" = 500" 250 0 500 1000 METERS ZONE A 2 + 43 1 1000mN PANEL 0558G 6 FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY, F COLORADO AND INCORPORATED AREAS PANEL 558 OF 1300 **MEADOW LAKE** (SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: **INDUSTRIAL FIL.** COMMUNITY NUMBER PANEL SUFFIX 1405000 FT NO. 1 EL PASO COUNTY INCORPORATED AREAS ZONE 8 Map Number sl ders: the Come ZONE A 11 Haegler Ranch Tributary 4 ZONE AE 431000mh ANOI Haegler Ranch Tributary 3 -ZONE AE (A) 38" 56' 15.00" 38" 56' 15.00" 104* 31* 52.50* MAP REVISED 539900#E JOINS PANEL 0566 \$38⁰⁰⁰E *A0000 104* 33' 45.00* DECEMBER 7, 2018 NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH. RANGE 64 WEST, AND TOWNSHIP 13 SOUTH. RANGE 64 WEST

munity Number shown

MAP NUMBER

08041C0558G

Federal Emergency Management Agency

NOTES TO USERS

Program. It doe This map is for use in administering the National Flood Insurance Program. It does to necessarily identify all areas subject to flooding, particularly from local drainage ources of small size. The community map repository should be consulted for ossible updated or additional flood hazard information.

o obtain more detailed information in areas where Base Flood Elevations (BFE To obtain more detailed information in areas where Base Flood Elevations (FES) and/or floodways have been determined, users are encouraged to consult the Flood within the Flood instructions (FLO) (FIG) (apport that accompanies this FIRM. Users should be avaited that EFEs alwoin on the FIRM regression that the FLO details are always hourd and a set the set of source of flood elevation information. Accordingly, flood elevations, These BFEs are intended for flood elevation information. Accordingly, flood elevation data presented in the FIRM regression due building in comparation with the FFRM for purposed orosituation and information.

Costal Base Flood Elevations shown on this map apply only landward of 0.0 North American Varical Claum of 1988 (NAVDB3). Users of this FIRM should be avera table in the Flood Insurance Study report for the jurisdician. Elevations shown in the Summary of Siltivater Elevations table should be used for construction and/or loopdain amagement puppose when they are higher that the devations shown on the silter of the silter shown in the silter loodplain r this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolate between cross sectors. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Theodorkey width and other pertiment floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood I lazard Areas may be protected by flood contro structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NACBS, GRSB0 sphreid, production of FIRMs for adjacent prioritications may result in sight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datu of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regardlin conversion between the National Geodetic Vertical Datum of 1929 and the Nor American Vertical Datum of 1989, visit the National Geodetic Survey website. http://www.ngs.noaa.gov/ or contact the National Geodetic Survey website addresse:

NGS Information Services NOAA, N/NGS12 NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the Nationa Seddelic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gow.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

The may effect more detailed and up to date etnam channels configurations and Bodglaan definietations thin those shown on the previous FRM for this jurisdiction. How been adjusted to confirm to these weterem channels on offigurations. As a result, the Road Profiles and Roadway Data tables in the Flood insurance Study Road (relind confism a advortative influenci data) may relind strate may and and Floodway Data Tables in the Flood insurance Study Road (relind confism) to these materials that match the flood profiles and Floodway Data Tables if applicable. In the FIS report, the a result, the profile baselines may deviate adjusticity from the new base map channel representation and may appresentation of the floodway.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

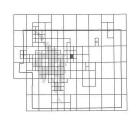
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a using of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is learned.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchang United Food and Section Comment (IndC) value in Food Angel (FMR) 1.877-352227 for information on available products associated with this FRM. Available products may include providuxly issued Laters of Map Change, a Proof insurance Study Report and/or digilal versions of the imap. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.Ema.gov/.

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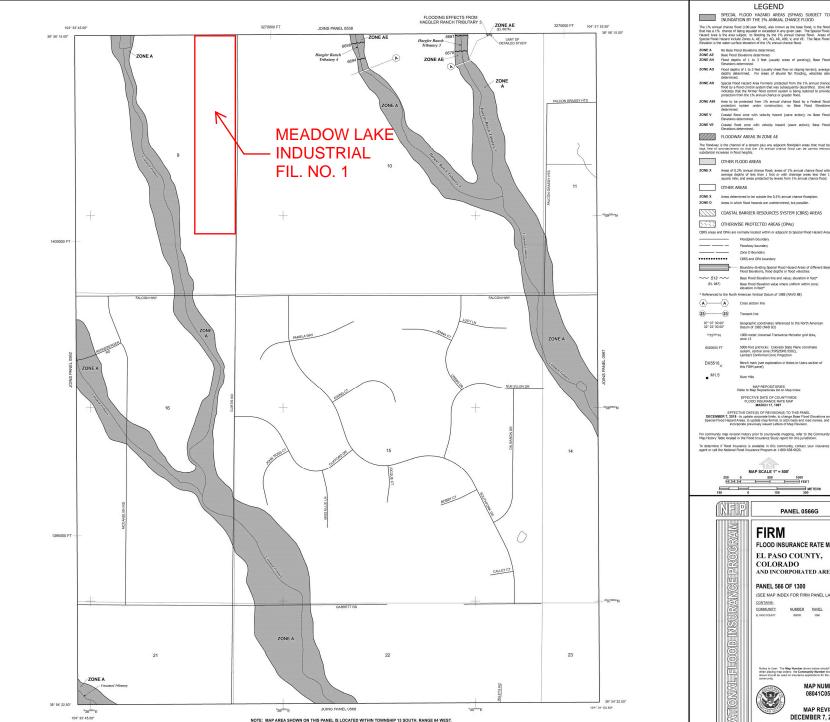
Panel Location Map



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The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% enrule chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AD, AR, A93, V, and VE. The Base Flood Elevation is the water-sufroce tendencion of the 1% annual chance flood. ZONE A No Base Flood Bevations determined. ZONE AE Base Flood Bevations determined. ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Bevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined. Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently descritted. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% ennual chance or greater flood. ZONE A99 Area to be protected from 1% e must diverse to getter index protection system under construction; no illese Nod Elevations deministic. ZONE V Cosstal flood zone with velocity hazard (wave action); no illese Nod Bestorins deterministic. ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Bevations determined. FLOODWAY AREAS IN ZONE AE The floodway is the channel of a stream plus any adjacent floodplain areas that must be logit, free of encroachment so that the 1% annual chance flood can be carried without substantial increases in find heights. OTHER FLOOD AREAS Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X Areas determined to be outside the 0.2% annual chance floo ZONE D Areas in which flood hazards are undetermined, but possible. nined to be outside the 0.2% annual chance floodplain COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Elopdolain boundary Floodway boundary Zone D Boundary CBRS and OPA bounda Boundary dividing Special Flood Hazard Areas of different Base Flood Bevations, flood depths or flood velocities. Base Rood Elevation line and value; elevation in feet* Base Rood Elevation value where uniform within zone; elevation in feet* * Referenced to the North American Vertical Datum of 1988 (NAVD 88) (A) Cross section line Transect line Geographic coordinates referenced to the North American Datum of 1963 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, zone 13 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection Bench mark (see explanation in Notes to Users section of this FIRM panel) River Mile MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Els Special Flood Hazard Areas, to update map format, to add roads and road in incorporate previously issued Latters of Man Revision. community map revision history prior to countywide mapping, refer to the Community o History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-900-638-6520. MAP SCALE 1" = 500" 250 0 500 1000 HHH FET METERS PANEL 0566G FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS PANEL 566 OF 1300 (SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: COMMUNITY NUMBER PANEL SUFFIX b User: The Map Number shown below should be use scing map orders: the Commanity Number shown hauld be used on insurance applications for the subject MAP NUMBER

08041C0566G

MAP REVISED

DECEMBER 7, 2018

Federal Emergency Management Agency

1

LEGEND



Meadow Lake Industrial Filing No. 1 Preliminary Drainage Report Project No: 2202744

APPENDIX B – HYDROLOGIC CALCULATIONS

	MEADOWLAKE INDUSTRIAL	<u>Calc'd by:</u>	NQJ
	EXISTING CONDITIONS	Checked by:	СМ
HRGreen	EL PASO COUNTY, CO	Date:	6/6/2023

SUMMARY RUNOFF TABLE													
BASIN	SIN AREA (ac) % IMPERVIOUS Q5 (cfs) Q100 (cfs)												
EX1	200.66	2	18.9	126.8									
EX2	45.17	6	5.1	26.7									
EX3	8.49	2	1.5	9.8									

DESIGN POINT SUMMARY TABLE												
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)									
1	EX1	18.9	126.8									
2	EX2	5.1	26.7									
3	EX3	1.5	9.8									

+イン	MEADOWLAK	ONDITIO						<u>Calc'c</u> <u>Checl</u> Date:	ked by:	NQJ CM 6/6/2023				
COMPOSITE 'C' FACTORS														
BASIN	UNDEVELOPED	PAVED	TOTAL	L SOIL	UNI	DEVEL	OPED		PA	VED	COMPOSITE IMPERVIOUSNESS & C			
	A	CRES	TYPE	%	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%	C ₅	C ₁₀₀		
EX1	200.66	0.00	200.66	A/B	2	0.09	0.36	100	0.90	0.96	2	0.09	0.36	
EX2	43.31	1.86	45.17	A/B	2	0.09	0.36	100	0.90	0.96	6	0.12	0.38	
EX3	8.49	0.00	8.49	A/B	2	0.09	0.36	100	0.90	0.96	2	0.09	0.36	
Total			254.32											

This area is significantly more than the proposed condition and as such the calculated flows are not comparable.

	MEAD	OWLAP	KE INDU	Calc'd by	y:	NQJ									
			ONDITIO	Checked	by:	СМ									
HRGreen	EL PAS		Date:		6/6/2023										
	TIME OF CONCENTRATION														
BAS	IN DATA		OVERI		E (T _i)		TRAV	EL TIME (TOTAL					
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)				
EX1	0.09	200.66	300	3.1	22.0	10	4252	1.6	1.3	56.0	78.0				
EX2	0.12	45.17	300	2.1	24.2	10	4000	1.2	1.1	60.9	85.1				
EX3	0.09	8.49	300	2.6	23.3	10	960	0.6	0.8	20.7	44.0				
	1						1								

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$

$$V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

* For buried riprap, select Cv value based on type of vegetative cover.

1 1	$\overline{)}$							ME	EADOV	VLAK	(E IND	UST	RIA	۱L							Calo	d by:	NQJ
			EXISTING CONDITIONS Checked b										ked by:	СМ									
1 1									DESIG	N ST	ORM: 5	5-YEA	R								D	ate:	6/6/2023
HR	Green																						
			DIRECT RUNOFF TOTAL RUNOFF SURFACE PIPE TRA							AVEL	TIME	REMARKS											
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ²	<i>t_c (</i> min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _e (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	% SLOPE	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	1	EX1	200.7	0.09	78.0	18.06	1.05	18.9															BASIN EX1 FLOW @ DP1
	2	EX2	45.17	0.12	85.1	5.57	0.92	5.1															BASIN EX2 FLOW @ DP2
	3	EX3	8.49	0.09	44.0	0.76	1.91	1.5															BASIN EX3 FLOW @ DP3



$\overline{}$	MEADOWLAKE INDUSTRIAL	<u>Calc'd by:</u>	DH/AB
ノ	PROPOSED CONDITIONS	Checked by:	NQJ
en	EL PASO COUNTY, CO	Date:	8/15/2023

	SUMM	ARY RUNOF	F TABLE	
BASIN	AREA (ac)	% IMPERVIOUS	$Q_5 (cfs)$	Q ₁₀₀ (cfs)
А	4.79	33	5.3	14.1
В	1.68	97	5.7	10.4
С	2.93	80	6.8	13.5
D	2.92	80	7.0	14.0
E	3.54	80	8.5	16.9
F	1.70	93	4.7	8.7
G	9.87	76	14.9	30.3
Н	2.33	70	4.6	9.6
- 1	1.25	68	2.5	5.2
J	3.00	26	2.7	8.6
К	0.42	90	1.8	3.3
L	0.42	90	1.8	3.3
N	6.01	<mark>8</mark> 0	14.4	28.6
0	3.04	80	7.2	14.2
Р	3.20	80	7.8	15.5
Q	1.01	96	4.0	7.6
R	1.11	96	3.2	6.2
S	0.85	2	0.3	1.7
Т	1.19	4	0.4	2.4

Impervious value for basin appears to be low. It includes lot 6, which will have an industrial use. Revise.

	DESIGN POINT SUMMA	ARY TABLE	
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ ₁₀₀ (cfs)
1	Α	5.3	14.1
2	В	5.7	10.4
2.1	DP1,DP2	9.9	22.2
3	С	6.8	13.5
4	D	7.0	14.0
4.1	DP3,DP4	13.2	24.8
5	E	8.5	16.9
5.1	DP2.1,DP5	16.0	32.6
5.2	DP4.1,5.1	26.5	51.6
6	F	4.7	8.7
6.1	DP5.2,DP6	30.6	58.3
7	G	14.9	30.3
8	DP7,H	15.9	32.5
9	I,DP8	16.7	34.1
10	DP6.1,J	32.9	64.9
11	К	1.8	3.3
12	L	1.8	3.3
13	OS1	1.6	6.1
15	Ν	14.4	28.6
16	0	7.2	14.2
17	Р	7.8	15.5
17.1	DP16,DP17	13.5	22.7
18	Q	4.0	7.6
19	DP15,DP16,R	6.3	17.1
21	DP12.1,S	2.5	59.6
22	DP20.1,DP21,T	30.3	68.9

	MEADOWLA	KE INDUST	RIAL						Calc'o	d by:				DH/AB			
1433	PROPOSED		IS						<u>Checl</u>	ked by:				NQJ			
HRGreen	EL PASO COUNT	Ύ, CO							Date:	_				8/15/2023			
				CO	MPOSI	Γ Ε '(C' F/	ACTOR	RS								
BASIN	UNDEVELOPED	INDUSTRIAL	PAVED	TOTAL	SOIL	UNI	DEVE	OPED	IN	DUSTRI	AL		P/	VED	CC IMPERV	MPOST IOUSNI	
		ACRES			TYPE	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀
А	3.27	0.00	1.52	4.79	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	33	0.35	0.55
В	0.00	0.23	1.45	1.68	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	97	0.86	0.92
С	0.00	2.93	0.00	2.93	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
D	0.00	2.92	0.00	2.92	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
E	0.00	3.54	0.00	3.54	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
F	0.00	0.57	1.13	1.70	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	93	0.80	0.87
G	0.50	9.37	0.00	9.87	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	76	0.56	0.68
Н	0.30	2.03	0.00	2.33	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	70	0.53	0.66
I	0.19	1.06	0.00	1.25	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	68	0.51	0.65
J	2.06	0.94	0.00	3.00	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	26	0.25	0.47
K	0.04	0.00	0.38	0.42	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	90	0.82	0.90
L	0.04	0.00	0.38	0.42	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	90	0.82	0.90
OS1	2.81	0.00	0.40	3.21	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	14	0.19	0.43
N	0.00	6.01	0.00	6.01	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
0	0.00	3.04	0.00	3.04	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
Р	0.00	3.20	0.00	3.20	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	80	0.59	0.70
Q	0.20	0.20	0.81	1.01	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	96	0.86	0.98
R	0.22	0.22	0.89	1.11	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	96	0.86	0.98
S	0.85	0.00	0.00	0.85	A/B	2	0.09	0.36	80	0.59	0.70		0.90	0.96	2	0.09	0.36
Т	1.17	0.00	0.02	1.19	A/B	2	0.09	0.36	80	0.59	0.70	100	0.90	0.96	4	0.10	0.37
Total				54.47											39		
North Pond				31.01											72		
				1/													
South Pond				21.85											62		

total draining to ponds = 52.86 ac, what basin is not draining to the pond? OS1? Adding that OS1 basin area to the combined pond areas you get 56.07 ac.

	MEAD	OWLAP	KE INDU	STRIAL	-			Calc'd b	y:	DI	H/AB
	PROP	OSED C	CONDITI	ONS				Checked	by:	P	1QJ
HRGreen	EL PAS		ry, co					Date:		8/1	5/2023
	<u> </u>			TIME O	F CONCE	NTRATI	ON			1	
BAS	IN DATA		EL TIME (T _t)		TOTAL					
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	<i>t</i> _c (min)
A	0.35	4.79	100	1.9	11.1	20	1360	2.2	3.0	7.6	18.8
В	0.86	1.68	100	1.9	3.6	20	1330	2.2	3.0	7.5	11.1
С	0.59	2.93	100	2.0	7.4	20	665	1.9	2.8	4.0	11.4
D	0.59	2.92	100	2.0	7.4	20	425	1.5	2.4	2.9	10.3
E	0.59	3.54	100	2.0	7.4	20	470	1.6	2.5	3.1	10.5
F	0.80	1.70	100	1.9	4.5	20	1680	1.7	2.6	10.7	15.2
G	0.56	9.87	100	4.0	6.2	15	1200	0.4	1.0	20.1	26.3
Н	0.53	2.33	100	2.0	8.4	15	665	2.4	2.3	4.7	13.1
	0.51	1.25	100	2.0	8.5	15	360	1.1	1.6	3.8	12.3
J	0.25	3.00	100	2.0	12.4	20	140	0.9	1.9	1.2	13.6
K	0.82	0.42	15	2.0	1.6	20	390	1.5	2.4	2.7	5.0
L	0.82	0.42	15	2.0	1.6	20	390	1.5	2.4	2.7	5.0
OS1	0.19	3.21	70	5.0	8.2	10	1490	1.6	1.3	19.6	27.8
N	0.59	6.01	100	2.0	7.4	20	460	1.5	2.4	3.1	10.6
0	0.59	3.04	100	2.0	7.4	20	525	1.5	2.4	3.6	11.0
P	0.59	3.20	40	2.0	4.7	20	1100	3.0	3.5	5.3	10.0
Q	0.86	1.01	100	2.0	3.6	20	550	1.5	2.4	3.7	7.3
R	0.86	1.11	17	25.0	0.6	10	1160	1.5	1.2	15.8	16.4
S	0.09	0.85	100	2.0	14.7	20	505	2.5	3.2	2.7	17.4
Т	0.10	1.19	100	2.0	14.5	20	540	2.5	3.2	2.8	17.3
1											

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

^{*} For buried riprap, select C_v value based on type of vegetative cover.



MEADOWLAKE INDUSTRIALCalc'd by:DH/ABPROPOSED CONDITIONSChecked by:NQJDESIGN STORM: 5-YEARDate:8/15/2023

				DII	RECT	RUNO	FF		т		UNOFF		S	REE	г		PIF	ΡE		TR/	AVEL 1	ГІМЕ	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	č	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
	1	А	4.79	0.35	18.8	1.66	3.18	5.3								5.3	1.66	1.2	1.5	40	6.5	0.10	DP1 CAPTURED W/ 10' TYPE R SUMP INELT, PIPE TO DP2.1
	2	В	1.68	0.86			3.98	5.7									1.44			89	4.2	0.35	DP2 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP2.1
									40.0	0.40	0.40												
	2.1								18.9	3.10	3.18	9.9				9.9	3.10	0.5	1.5	305	4.2	1.21	DP2.1 FLOW, PIPE TO DP5.1
	3	С	2.93	0.59	11.4	1.73	3.93	6.8								6.8	1.73	2.0	1.5	427	8.4	0.85	DP3 CPATURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4	D	2.92	0.59	10.3	1.72	4.08	7.0								7.0	1.72	1.0	1.5	6	5.9	0.02	DP4 CAPTURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4.1								12.3	3.45	3.82	13.2				13.2	3.45	2.0	1.5	500	8.4	0.99	DP4.1 FLOW, PIPE TO DP5.1
	5	E	3.54	0.59	10.5	2.09	4.05	8.5								8.5	2.09	3.0	1.5	6	10.3	0.01	DP5 CAPTURED W/ 15' TYPE R SUMP INLET, PIPE TO DP5.1
	5.1								20.1	5.19	3.08	16.0				16.0	5.19	0.4	2.0	50	4.6	0.18	DP5.1 FLOW, PIPE TO DP5.2
	5.2								20.3	8.64	3.07	26.5				26.5	8.64	0.8	2.0	36	6.2	0.10	DP5.2 FLOW, PIPE TO DP6.1
	6	F	1.7	0.80	15.2	1.35	3.50	4.7								4.7	1.35	1.0	2.0	12	7.2	0.03	DP6 CAPTURED IN 15' TYPE R SUMP INLET , PIPE TO DP6.1
	6.1								20.4	10.00	3.06	30.6											DP6.1, PIPE TO POND A
	7	G	9.87	0.56	26.3	5.57	2.68	14.9	20.4	10.00	0.00	30.0	14.9	5.57	0.7					665	1.7	6.62	SWALE TO BASIN H
	8	н	2.33	0.56	13.1	1.22	3.72	4.6	32.9	6.80	2.34	15.9	32.9	6.80	1.7					360	2.6	2.30	SWALE TO BASIN I
	9		1.25	0.51	12.3		3.81	2.5	35.2	7.44	2.24	16.7											SWALE TO DET POND A
	10		3	0.25		0.74	3.66	2.7		10.74	3.06	32.9											DP10 FLOW. TOTAL FLOW ENTERING POND A



MEADOWLAKE INDUSTRIAL DH/AB Calc'd by: **PROPOSED CONDITIONS** Checked by: NQJ DESIGN STORM: 5-YEAR 8/15/2023 Date:

				DII	RECT	RUNO	FF		т	DTAL F	RUNOFF		S	FREE	г		PIP	Е		TRA	VEL 1	IME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	Cs	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)		PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
	11	к	0.42	0.82	5.0	0.34	5.17	1.8								1.8	0.34	2.0	1.5	25	2.8	0.15	DP11 CAPTURED W/ 5' TYPE R SUMP INLET. PIPE TO DP12.1
	12	L	0.42	0.82	5.0	0.34	5.17	1.8								1.8	0.34	2.0	1.5	25	2.8	0.15	DP12 CAPTURED W/ 5' TYPE R SUMP INELT, PIPE TO DP12.1
	12.1								5.1	0.69	5.13	3.5	3.5	0.69	1.0					1150	2.0	9.58	DP12.1 SWALE FLOW TO DP21
	13	OS1	3.21	0.19	27.8	0.61	2.60	1.6															DP13 FLOWS TO PR CULVERT, FOLLOW HISTORIC DRAINAGE PATTERNS SOUTH ALONG CURTIS ROAD UNDER ACCESS ROAD NORTH
													2.6	0.63						550	3.5	2.65	DP15 BYPASS TO DP19
	15	N	6.01	0.59	10.6	3.55	4.05	14.4								11.8	2.91	3.6	1.5	32	11.3	0.05	DP15 CAPTURED IN 15' TYPE R INLET, PIPE TO DP15.1
						4 70							1.2	0.29						60	3.5	0.29	DP16 BYPASS TO DP19
	16	0	3.04	0.59	11.0	1.79	3.99	7.2								6.0	1.50	1.0	1.5	10	5.9	0.03	DP16 CAPTURED IN 10' TYPE R INLET, PIPE TO DP17.1
	17	Р	3.2	0.59	10.0	1.89	4.13	7.8								7.8	1.89	2.0	1.5	27	8.4	0.05	DP17 BYPASS OFFSITE DP17 CAPTURED IN 20' TYPE R INLET, PIPE TO DP17.1
	17.1								11.0	3.39	3.98	13.5				10 E	3.39	26	2.0	42	13.7	0.05	DP17.1 FLOW. PIPE TO DP20.1
	17.1								11.0	3.39	3.90	13.5				13.5	3.39	3.0	2.0	42	13.7	0.05	DP18 BYPASS OFFSITE
	18	Q	1.01	0.86	7.3	0.86	4.60	4.0								4.0	0.86	0.5	1.5	50	4.2	0.20	DP18 CAPTURED IN 5' TYPE R SUMP INLET, PIPE TO DP19.1
	19	R	1.11	0.86	16.4	0.95	3.39	3.2	16.4	1.87	3.39	6.3				3.2	0.95	1.0	1.5	6	5.9	0.02	DP19 CAPTURED IN 10' TYPE R SUMP INLET, PIPE TO DP19.1
	19.1								16.4	5.65	3.38	19.1				19.1	5.65	0.5	2.0	42	5.1	0.14	DP19.1 FLOW, PIPE TO DP20.1
															T.					070			
	20.1								16.4	9.04	3.38	30.6					9.04			370 151	5.9	1.04	DP20.1 PIPE FLOW TO POND B
	21	S	0.85	0.09	17.4	0.08	3.30	0.3	17.4	0.76	3.30	2.5				17.4	0.76	4.0	2.0	151	14.4	0.17	DP21 SWALE FLOW TO POND B
	22	т	1.19	0.10	17.3	0.12	3 30	0.4	17.4	9.17	3.30	30.3				Ī							TOTAL FLOW ENTERING POND B

F1+33
HRGreen

								DE	SIGN	I STO	RM:	100-	YEA	R							Da	ate:	8/15/2023
HF	Gree	ən																					
				DI	RECT	RUNO	FF		т		RUNO	FF	9	TREE	т		PI	PE		TR	AVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₁₀₀	ť _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	ť _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	1	А	4.79	0.55	18.8	2.64	5.34	14.1								14.1	2.64	1.2	1.5	40	2.2	0.30	DP1 CAPTURED W/ 10' TYPE R SUMP INELT, PIPE TO DP2.1
	2	В	1.68	0.92	11.1	1.55	6.68	10.4								10.4	1.55	0.5	1.5	89	1.4	1.05	DP2 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP2.1
	2.1								19.1	4.19	5.30	22.2				22.2	4.19	0.5	1.5	305	1.4	3.59	DP2.1 FLOW, PIPE TO DP5.1
	3	С	2.93	0.70	11.4	2.05	6.59	13.5					0.4	0.06	2.0	13.1	1.99	2.0	1.5	427	2.8 2.8	0.00 2.52	DP3 CPATURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4	D	2.92	0.70	10.3	2.04	6.85	14.0	11.4	2.10	6.59	13.9	0.2	0.03	1.6	13.7	2.07	1.0	1.5	6	2.5 2.0	0.00 0.05	DP4 CAPTURED W/ 20' TYPE R INLET, PIPE TO DP4.1
	4.1								14.0	4.06	6.09	24.8				24.8	4.06	2.0	1.5	500	2.8	2.95	DP4.1 FLOW, PIPE TO DP5.1
	5	E	3.54	0.70	10.5	2.48	6.81	16.9	10.5	2.51	6.81	17.1				17.1	2.51	3.0	1.5	6	3.5	0.03	DP5 CAPTURED W/ 15' TYPE R SUMP INLET, PIPE TO DP5.1
	5.1								22.7	6.70	4.87	32.6				32.6	6.70	0.4	2.0	50	1.3	0.66	DP5.1 FLOW, PIPE TO DP5.2
	5.2								23.3	10.76	4.80	51.6				51.6	10.76	0.8	2.0	36	1.7	0.35	DP5.2 FLOW, PIPE TO DP6.1
	6	F	1.7	0.87	15.2	1.48	5.87	8.7								8.7	1.48	1.0	2.0	12	2.0	0.10	DP6 CAPTURED IN 15' TYPE R SUMP INLET , PIPE TO DP6.1
	6.1								23.7	12.25	4.76	58.3											DP6.1, PIPE TO POND A
	7	G	9.87	0.68	26.3	6.74	4 50	30.3					30.3	6.74	0.7					665	1.7	6.62	SWALE TO BASIN H
	8	н	2.33	0.66	13.1	1.53	6.25	9.6	32.9	8 27	3.93	32.5	32.5	8.27	1.7					360	2.6	2.30	SWALE TO BASIN I
	9		1.25	0.65	12.3	0.81	6.40	5.2			3.76									1			SWALE TO DET POND A
	10	J	3	0.47	13.6			8.6															DP10 FLOW, TOTAL FLOW ENTERING POND A

MEADOWLAKE INDUSTRIAL

PROPOSED CONDITIONS

DH/AB

NQJ

Calc'd by:

Checked by:

	+	2	2	
H	IRO	Gre	een	

	T								FRUP												Cilec	kea by:	
								D	ESIGN	I STC	RM:	100-	YEA	R							Da	nte:	8/15/2023
HF	RGree	en																					
				DI	RECT	RUNO	FF		т	DTAL I	RUNO	FF	9	TREE	т		PII	PE		TR	AVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₁₀₀	f _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	f _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	11	к	0.42	0.90	5.0	0.38	8.68	3.3								3.3	0.38	2.0	1.5	25	8.4	0.05	DP11 CAPTURED W/ 5' TYPE R SUMP INLET, PIPE TO DP12.1
	12	L	0.42	0.90	5.0	0.38	8.68	3.3								3.3	0.38	2.0	1.5	25	8.4	0.05	DP12 CAPTURED W/ 5' TYPE R SUMP INELT. PIPE TO DP12.1
			0.12	0.00	0.0	0.00	0.00	0.0	5.0	0.70	0.05	0.5	6.5	0.76	1.0	0.0	0.00	2.0		1150		9.58	
	12.1								5.0	0.76	8.65	6.5											DP12.1 SWALE FLOW TO DP21
	13	OS1	3.21	0.43	27.8	1.40	4.36	6.1															DP13 FLOWS TO PR CULVERT, FOLLOW HISTORIC DRAINAGE PATTERNS SOU ALONG CURTIS ROAD UNDER ACCESS ROAD NORTH
													11.7	1.72	3.0					550		2.65	DP15 BYPASS TO DP19
	15	N	6.01	0.70	10.6	4.21	6.80	28.6					5.0	0.04		16.9	2.49	3.6	1.5	32	11.3	0.05	DP15 CAPTURED IN 15' TYPE R INLET, PIPE TO DP19.1
	16	0	3.04	0.70	11.0	2.13	6.69	14.2					5.6	0.84	3.0	06	1.28	10	15	60 10	3.5 5.9	0.29 0.03	DP16 BYPASS TO DP19 DP16 CAPTURED IN 10' TYPE R INLET, PIPE TO DP17.1
	10	0	5.04	0.70	11.0	2.15	0.03	14.2					0.9	0.14	3.0	0.0	1.20	1.0	1.5	10	5.5	0.05	DP17 BYPASS, FLOW TO POND B
	17	Р	3.2	0.70	10.0	2.24	6.94	15.5					0.0	0	0.0	14.6	2.10	2.0	1.5	27	8.4	0.05	DP17 CAPTURED IN 10' TYPE R INLET, PIPE TO DP17.1
	17.1								11.0	3.39	6.69	22.7				22.7	3.39	3.6	2.0	42	13.7	0.05	DP17.1 FLOW, PIPE TO DP21
													0.1	0.02	3.0								DP18 BYPASS OFFSITE
	18	Q	1.01	0.98	7.3	0.99	7.73	7.6								7.5	0.97	0.5	1.5	50	4.2	0.20	DP18 CAPTURED IN 5' TYPE R INLET, PIPE TO DP19.1
	19	R	1.11	0.98	16.4	1.09	5.68	6.2	24.5	3.65	4.68	17.1				6.2	1.09	1.0	1.5	6	5.9	0.02	DP19 CAPTURED IN 10' TYPE R SUMP INLET, PIPE TO DP19.1
	19.1								16.4	7 1 1	5.68	40.4				40.4	7.11	0.5	2.0	42	5.1	0.14	DP19.1 FLOW, PIPE TO DP20.1
	19.1								10.4	7.11	5.00	40.4				40.4	7.11	0.5	2.0	42	5.1	0.14	DF 19.11 LOW, FIFL TO DF20.1
	20.1		<u> </u>					<u> </u>	24.5	3.65	4.68	17.1				17.1	3.65	0.5	2.5	370	5.9	1.04	DP20.1 PIPE FLOW TO POND B
	21	S	0.85	0.36	17.4	0.31	5.54	1.7	16.4	10.50	5.68	59.6				59.6	10.50	0.5	2.5	370	5.9	1.04	DP21 SWALE FLOW TO POND B
	22	т	1.19	0.37	17.3	0.44	5.54	2.4	24.5	14.73	4.68	68.9											TOTAL FLOW ENTERING POND B

MEADOWLAKE INDUSTRIAL

PROPOSED CONDITIONS

DH/AB

NQJ

Calc'd by:

Checked by:



Meadow Lake Industrial Filing No. 1 Preliminary Drainage Report Project No: 2202744

APPENDIX C – HYDRAULIC CALCULATIONS

Provide riprap calculations for the culverts, pond outfall pipes, pond spillways, and any other riprap utilized onsite

MHFD-Inlet, Version 5.02 (August 2022)

INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP1	DP2	DP3	DP4
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening			

7.0

12.6

USER-DEFINED INPUT			
User-Defined Design Flows			
Minor Q _{Known} (cfs)	5.3	5.7	6.8
Major Q _{Known} (cfs)	14.1	10.4	13.5

Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.

Receive Bypass Flow from:	No Bypass Flow Received			
Minor Bypass Flow Received, Q _b (cfs)		0.0	0.0	0.0
Major Bypass Flow Received, Qb (cfs)		0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		
C ₁		
C ₂		
C ₃		
User-defined C		
User-defined 5-yr C₅		
User-defined T _c		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches)		
One-Hour Precipitation, P ₁ (inches)		
C ₁		
C ₂		
C ₃		
User-defined C		
User-defined C User-defined 5-yr C ₅ User-defined T _c		
User-defined T _c		

CALCULATED OUTPUT

5.3	5.7	6.8	7.0
14.1	10.4	13.5	12.6
N/A	N/A	0.0	0.0
N/A	N/A	2.2	0.2
-	5.3 14.1 N/A	5.3 5.7 14.1 10.4 N/A N/A	5.3 5.7 6.8 14.1 10.4 13.5 N/A N/A 0.0

MHFD-Inlet, Version 5.02 (August 2022)

INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP5	<u>DP6</u>	<u>DP15</u>	<u>DP16</u>	<u>DP17</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	On Grade	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening		CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows					
Minor Q _{Known} (cfs)	8.5	4.7	14.4	7.2	7.8
Major Q _{Known} (cfs)	17.5	8.7	28.6	14.2	15.5

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received				
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches)			
One-Hour Precipitation, P ₁ (inches)			
C ₁			
C2			
C3			
User-defined C			
User-defined C User-defined 5-yr C ₅ User-defined T _c			
User-defined T _c			

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)			
Design Storm Return Period, T_r (years) One-Hour Precipitation, P_1 (inches)			
C ₁			
C ₂			
C ₃			
User-defined C			
User-defined 5-yr C ₅			
User-defined C User-defined 5-yr C ₅ User-defined T_c			

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	8.5	4.7	14.4	7.2	7.8
Major Total Design Peak Flow, Q (cfs)	17.5	8.7	28.6	14.2	15.5
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A	2.6	1.2	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A	11.7	5.6	0.9

MHFD-Inlet, Version 5.02 (August 2022)

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>DP18</u>	<u>DP19</u>
Site Type (Urban or Rural)	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET
Hydraulic Condition	On Grade	On Grade
Inlet Type		

USER-DEFINED INPUT

User-Defined Design Flows		
Minor Q _{Known} (cfs)	4.0	3.2
Major Q _{Known} (cfs)	7.6	19.1

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)	
Percent Impervious	
NRCS Soil Type	

Watershed Profile

Overland Slope (ft/ft)	
Overland Length (ft)	
Channel Slope (ft/ft)	
Channel Length (ft)	

Minor Storm Rainfall Input

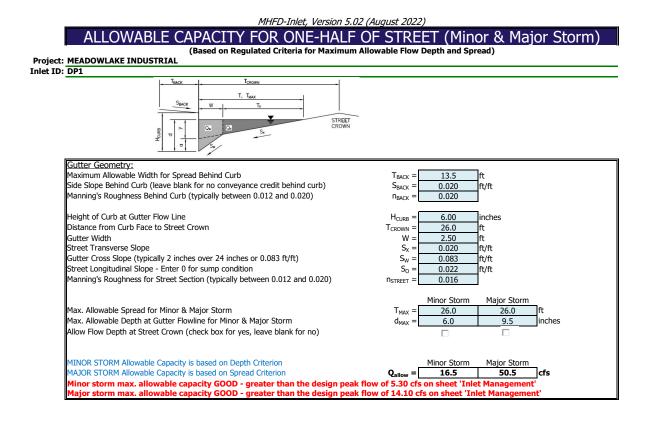
Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P_1 (inches)	
C ₁	
C ₂	
C ₃	
User-defined C	
User-defined 5-yr C ₅	
User-defined T _c	

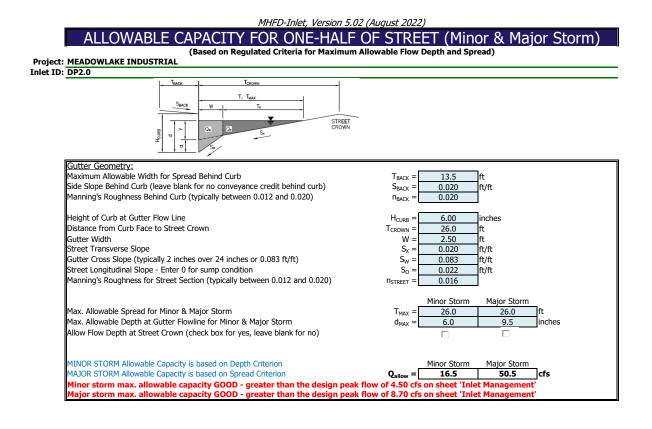
Major Storm Rainfall Input

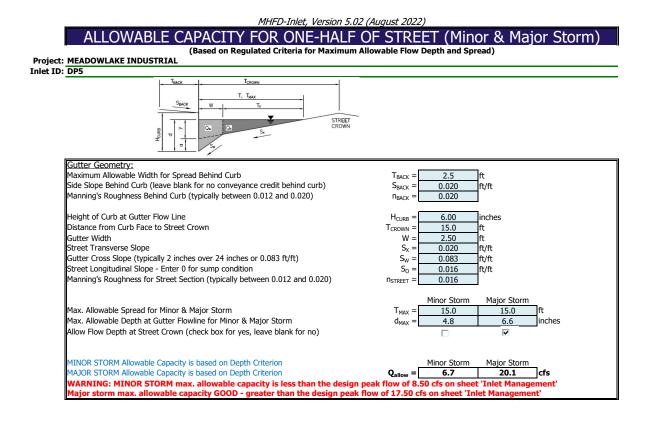
Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	
C ₁	
C ₂	
C₃	
User-defined C	
User-defined 5-yr C ₅	
User-defined T _c	

CALCULATED OUTPUT

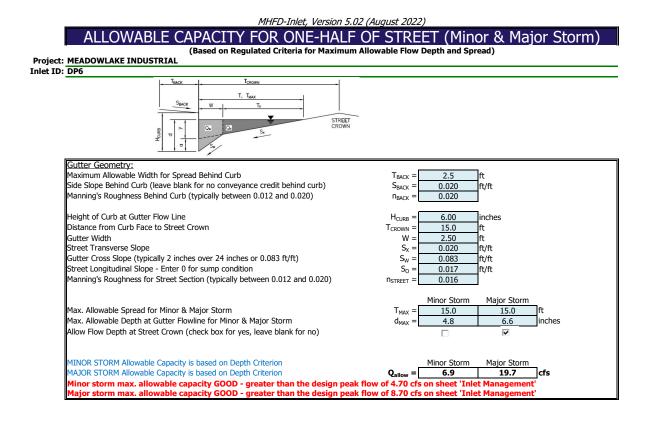
Minor Total Design Peak Flow, Q (cfs)	4.0	3.2
Major Total Design Peak Flow, Q (cfs)	7.6	19.1
Minor Flow Bypassed Downstream, Q _b (cfs)		
Major Flow Bypassed Downstream, Q _b (cfs)		

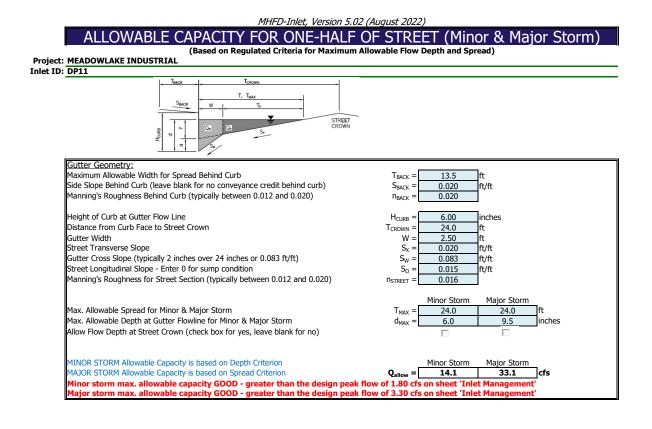


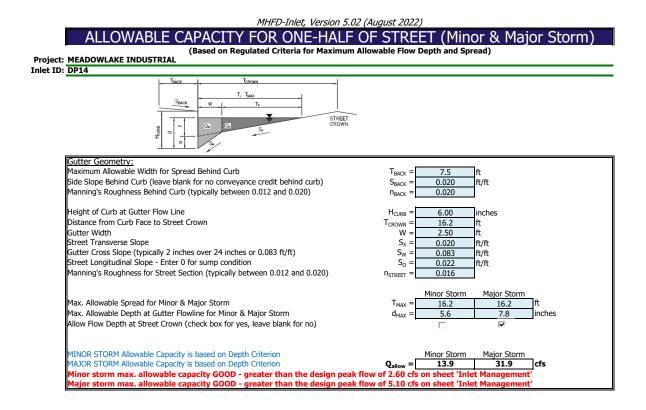


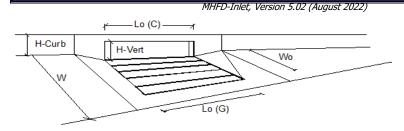


NOTE: IGNORE MINOR & MAJOR STREET CAPACITY WARNINGS. BASIN FLOWS ARE DIVIDED BETWEEN TWO SEPARATE STREETS.

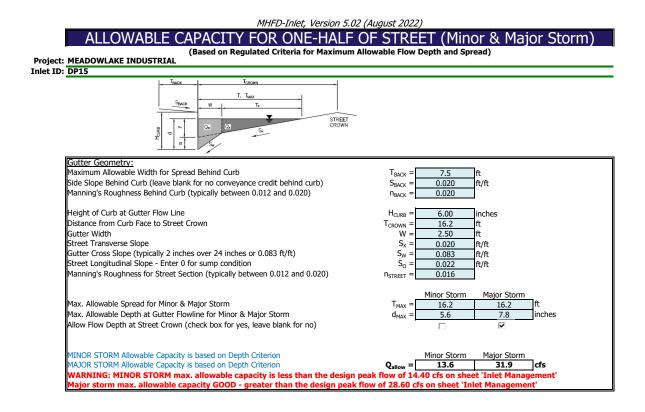


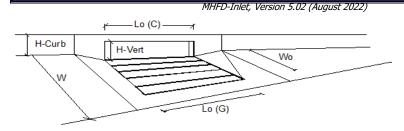




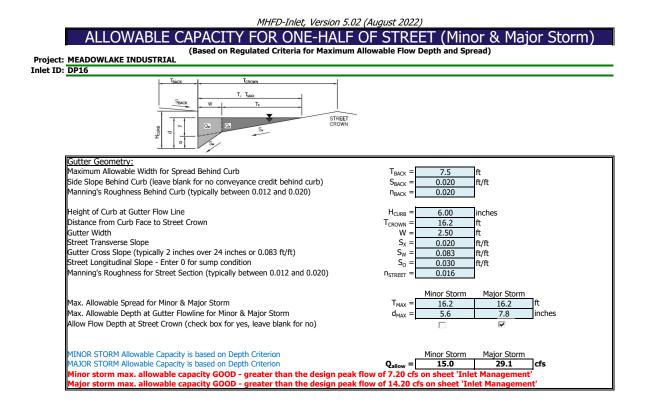


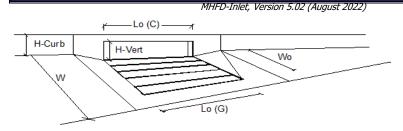
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.6	4.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.3	cfs
Capture Percentage = Q_a/Q_o	C% =	100	94	%



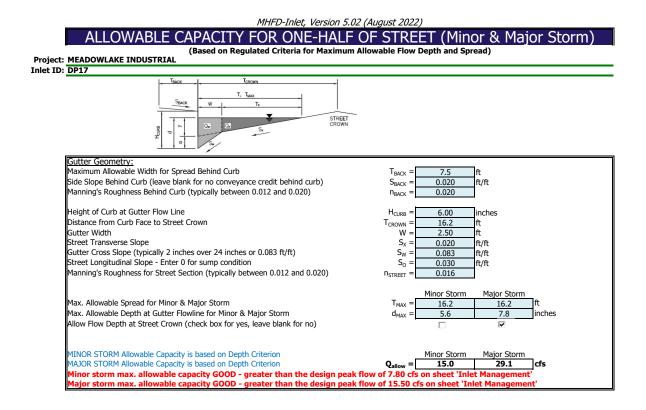


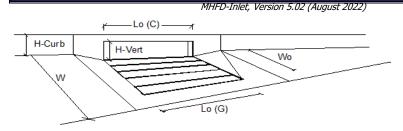
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR & MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	11.8	16.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	2.6	11.7	cfs
Capture Percentage = Q_a/Q_o	C% =	82	59	%



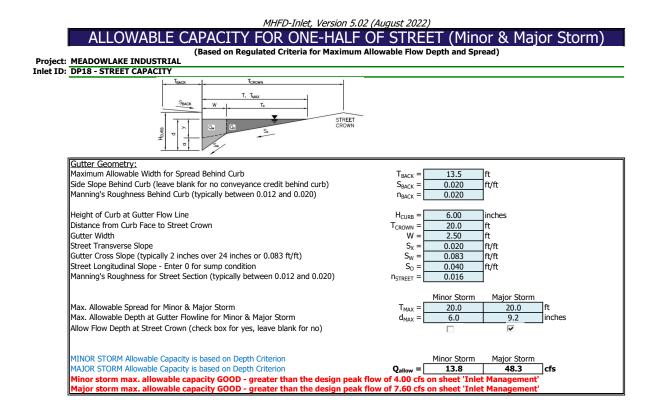


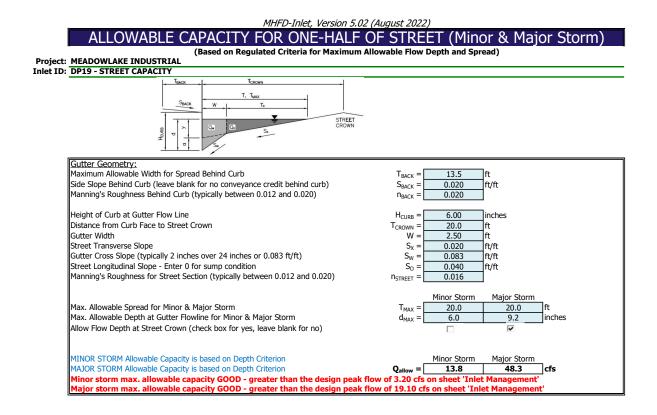
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	-	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.0	8.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	1.2	5.6	cfs
Capture Percentage = Q_a/Q_o	C% =	84	61	%





CDOT Type R Curb Opening	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	4	4	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_o =$	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.8	14.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.9	cfs
Capture Percentage = Q_a/Q_o	C% =	100	94	%





SUMP INLETS ON PRIVATE INDUSTRIAL ROADS (80' ROW, 48' PAVED WIDTH)

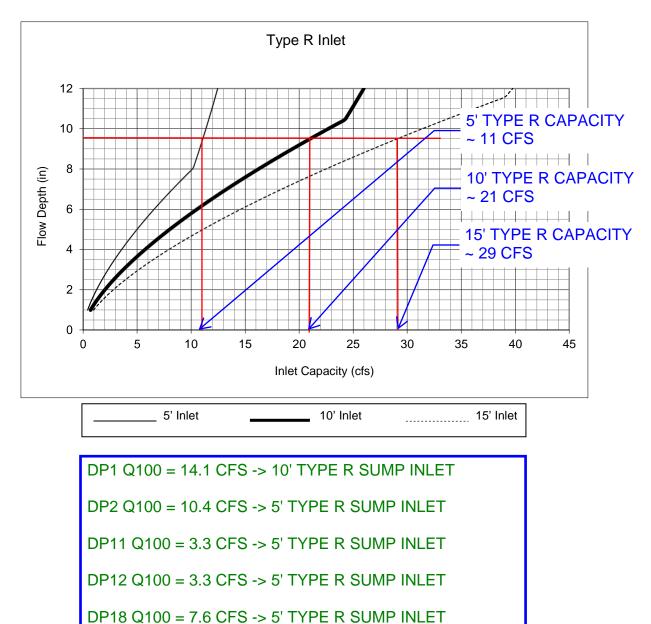


Figure 8-11. Inlet Capacity Chart Sump Conditions, Curb Opening (Type R) Inlet

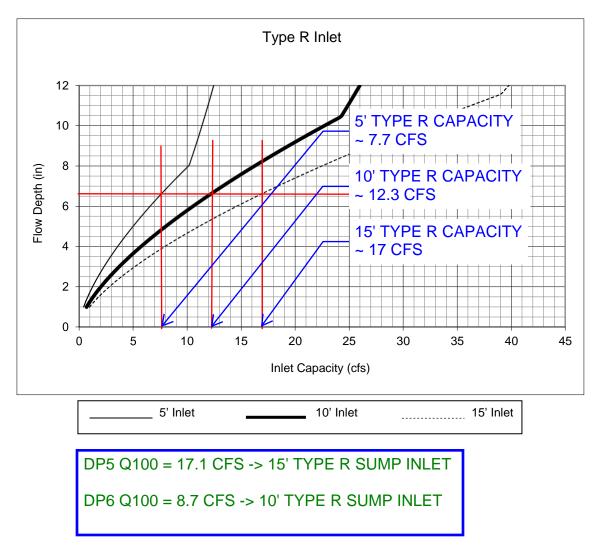
Notes:

1. The standard inlet parameters must apply to use this chart.

DP19 Q100 = 17.1 CFS -> 10' TYPE R SUMP INLET

SUMP INLETS ON PRIVATE ROADS (50' EASEMENT, 30' PAVED WIDTH)





Notes:

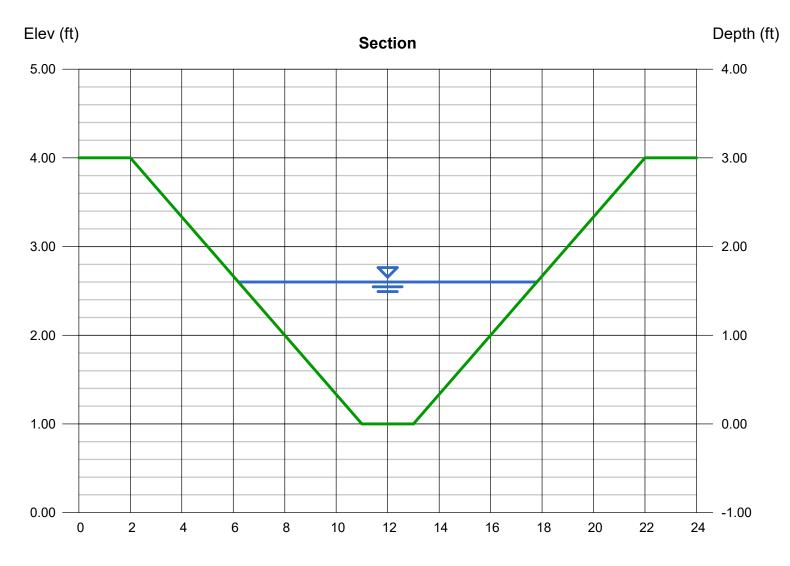
1. The standard inlet parameters must apply to use this chart.

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Thursday, Jun 8 2023

BASIN G SWALE A (Q100 = DP7 = 30.3 cfs)

Trapezoidal		Highlighted	
Bottom Width (ft)	= 2.00	Depth (ft)	= 1.60
Side Slopes (z:1)	= 3.00, 3.00	Q (cfs)	= 30.30
Total Depth (ft)	= 3.00	Area (sqft)	= 10.88
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 2.78
Slope (%)	= 0.50	Wetted Perim (ft)	= 12.12
N-Value	= 0.035	Crit Depth, Yc (ft)	= 1.16
		Top Width (ft)	= 11.60
Calculations		EGL (ft)	= 1.72
Compute by:	Known Q		
Known Q (cfs)	= 30.30		



Reach (ft)

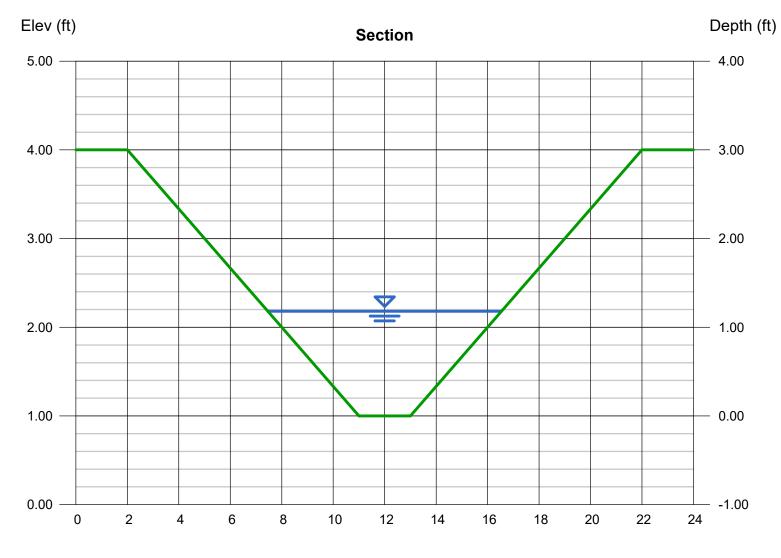
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Thursday, Jun 8 2023

= 1.18 = 32.50 = 6.54 = 4.97 = 9.46 = 1.20 = 9.08 = 1.56

BASIN H SWALE A (Q100 = DP7 = 30.3 cfs)

Trapezoidal		Highlighted
Bottom Width (ft)	= 2.00	Depth (ft)
Side Slopes (z:1)	= 3.00, 3.00	Q (cfs)
Total Depth (ft)	= 3.00	Area (sqft)
Invert Elev (ft)	= 1.00	Velocity (ft/s)
Slope (%)	= 2.25	Wetted Perim (ft)
N-Value	= 0.035	Crit Depth, Yc (ft)
		Top Width (ft)
Calculations		EGL (ft)
Compute by:	Known Q	
Known Q (cfs)	= 32.50	



Reach (ft)

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Jun 8 2023

BASIN I SWALE A (Q100 = DP7 = 30.3 cfs)

Trapezoidal	
Bottom Width (ft)	
Side Slopes (z:1)	
Total Depth (ft)	

= 3.00, 3.00 = 3.00 = 1.00 = 0.44 = 0.035

= 2.00

Calculations

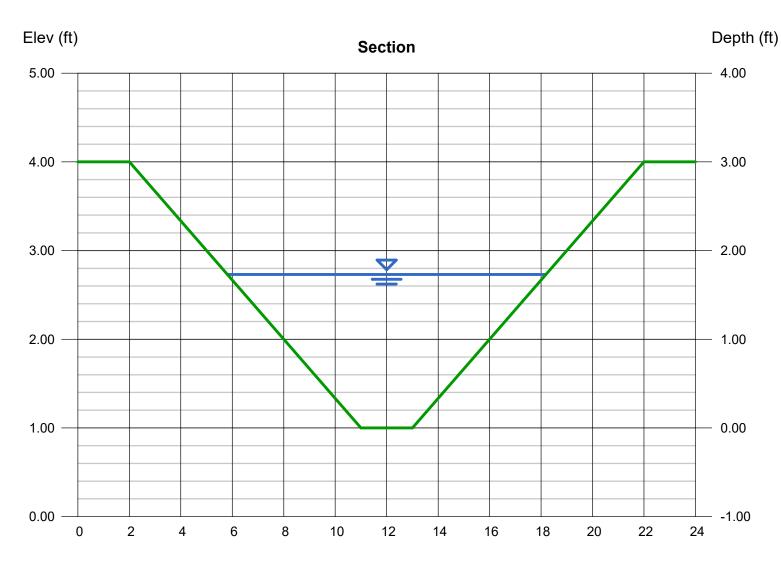
Invert Elev (ft)

Slope (%)

N-Value

Compute by:Known QKnown Q (cfs)= 34.10

Highlighted		
Depth (ft)	=	1.73
Q (cfs)	=	34.10
Area (sqft)	=	12.44
Velocity (ft/s)	=	2.74
Wetted Perim (ft)	=	12.94
Crit Depth, Yc (ft)	=	1.23
Top Width (ft)	=	12.38
EGL (ft)	=	1.85



Reach (ft)

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Jun 8 2023

BASIN S SWALE B (Q100 = 5.9 CFS)

Trapezoidal

Bottom Width (ft)	= 2.00
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.64
Invert Elev (ft)	= 5.00
Slope (%)	= 0.87
N-Value	= 0.030

Calculations

Compute by: Known Q (cfs) Known Q = 5.90

Highlighted		
Depth (ft)	=	0.62
Q (cfs)	=	5.900
Area (sqft)	=	2.39
Velocity (ft/s)	=	2.47
Wetted Perim (ft)	=	5.92
Crit Depth, Yc (ft)	=	0.51
Top Width (ft)	=	5.72
EGL (ft)	=	0.71

Fr = 2.74/(sqrt(32.17*0.62))=0.61 < 0.9

Elev (ft) Depth (ft) Section 8.00 -- 3.00 7.50 -- 2.50 7.00 -- 2.00 6.50 -- 1.50 6.00 -- 1.00 $\overline{}$ 5.50 -- 0.50 5.00 -- 0.00 4.50 -0.50 0 2 22 4 6 8 10 12 14 16 18 20

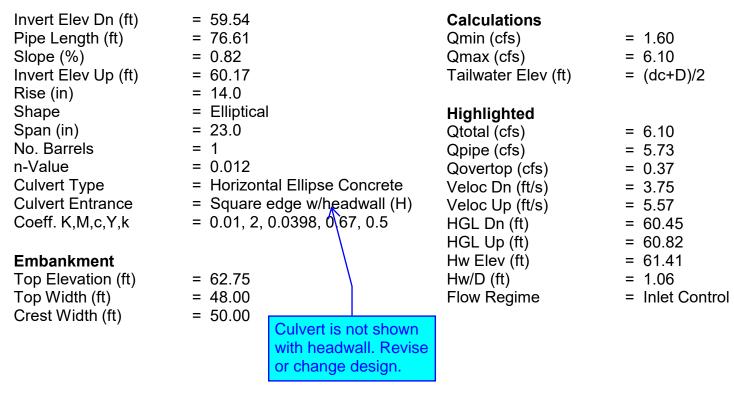
Reach (ft)

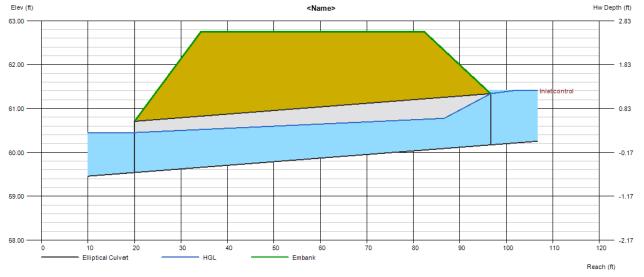
Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Jun 8 2023

Basin OS1 Culvert





Riprap Sizing - Pond A Spillway							
q (cfs/ft)	S (ft/ft)	C _f	n	D ₅₀ min. (in)			
1.62	0.33	2	0	7.41			

 Riprap Sizing - Pond B Spillway

 q (cfs/ft)
 S (ft/ft)
 C_f
 n
 D₅₀ min. (in)

 2.97
 0.33
 2
 0
 10.41

Type L Riprap (D₅₀ = 9") will be utilized for the spillway protection

Type M Riprap (D_{50} = 12") will be utilized for the spillway protection

Riprap Sizing - Pond A Outfall								
Pipe Dia (ft)	q (cfs/ft)	S (ft/ft)	C _f	n	D ₅₀ min. (in)	Length (ft, = 3x Pipe Dia)	Width (ft, = 3x Pipe Dia)	
1.5	53.87	0.005	2	0	8.71	4.5	4.5	

Type L Riprap (D₅₀ = 9") will be utilized for the outfall protection

Riprap Sizing - Pond B Outfall										
Pipe Dia (ft)	$\Gamma_{\alpha}(cts/ft) = S(ft/ft) = C_{\alpha} = n = D_{co} min (in)$									
1.5	35.60	0.005	2	0	6.91	4.5	4.5			

Type L Riprap (D₅₀ = 9") will be utilized for the outfall protection

 $D_{50} = 5.23 \ S^{0.43} \ (1.35 \, C_{\rm f} \, q)^{0.56}$

Where:

- D_{50} = median rock size (in)
- S = longitudinal slope (ft/ft)
- C_f = concentration factor (1.0 to 3.0)
- q = unit discharge (cfs/ft)

When:

 η (porosity) = 0.0 (i.e., for buried soil riprap)

Equation 13-9



Meadow Lake Industrial Filing No. 1 Preliminary Drainage Report Project No: 2202744

APPENDIX D – WATER QUALITY & DETENTION

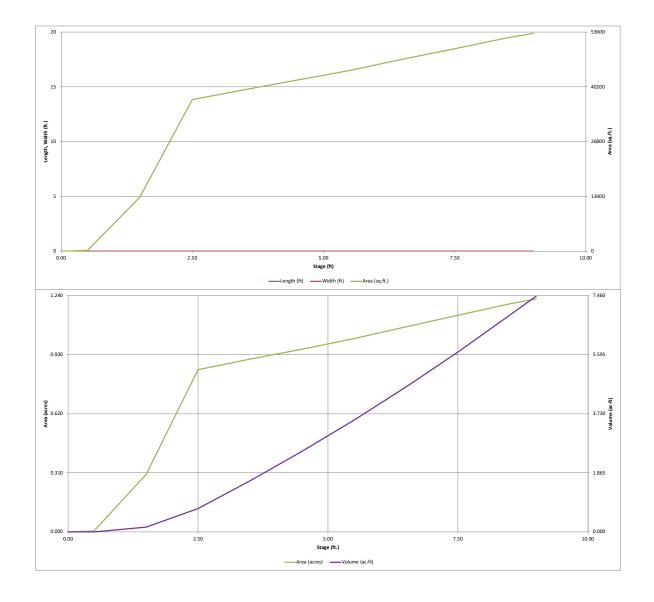
Provide forebay and trickle channel design calculations

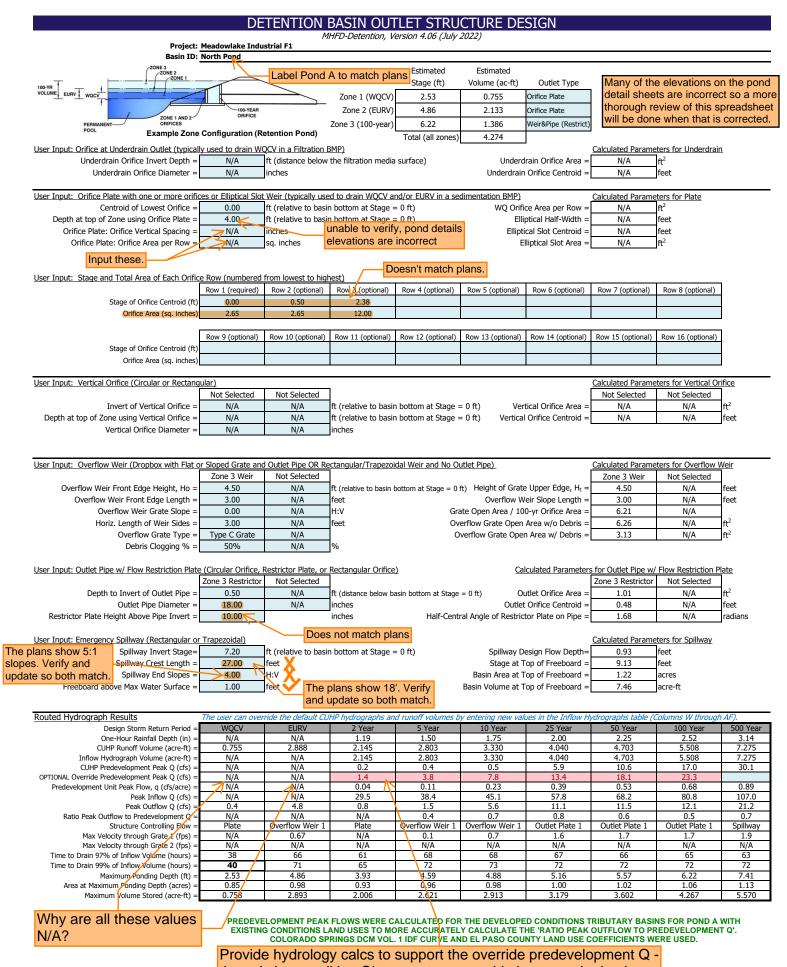
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project:	Meadowlak	e Industria	i F1	MHFL	D-Detention, Versio	ni 4.00 (Ji	uiy 2022)							
Basin ID:	North Pond													
	2 SONE 1	T												
	$ \rightarrow 1 $				٦		1							
	LI AND 2	100-YE ORIFIC			Depth Increment =		ft Optional			Area	Optional Override	• • •	Volume	
Example 201	e Configura	tion (Rete	ntion Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	(ft ²)	Area (ft ²)	Area (acre)	(ft ³)	Volum (ac-ft
Watershed Information Selected BMP Type =	EDB	1		6759.5	Top of Micropool 6760		0.00				11 215	0.000	56	0.001
Watershed Area =	34.01	acres			6761		1.50		-	-	13,184	0.303	6,756	0.001
Watershed Length =	2,185	ft			6762		2.50				37,092	0.852	31,893	0.732
Watershed Length to Centroid = Watershed Slope =	1,100	ft ft/ft			6763 6764		3.50 4.50				39,470 41,805	0.906	70,174 110,812	1.611 2.544
Watershed Imperviousness =	68.00%	percent			6765		5.50				44,176	1.014	153,802	3.531
Percentage Hydrologic Soil Group A =	95.0%	percent			6766		6.50				46,929	1.077	199,355	4.577
Percentage Hydrologic Soil Group B = Percentage Hydrologic Soil Groups C/D =	5.0% 0.0%	percent percent			6767 6768		7.50 8.50				49,516 52,190	1.137 1.198	247,577 298,430	5.684 6.851
Target WQCV Drain Time =	40.0	hours			6768.5		9.00				53,285	1.223	324,799	7.456
Location for 1-hr Rainfall Depths = After providing required inputs above inc		rainfall												
depths, click 'Run CUHP' to generate run	off hydrograpł	ns using								-				
the embedded Colorado Urban Hydro Water Quality Capture Volume (WQCV) =		acre-feet	Optional Us	er Overrides acre-feet										
Excess Urban Runoff Volume (EURV) =	2.888	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) = 5-yr Runoff Volume (P1 = 1.5 in.) =	2.145 2.803	acre-feet acre-feet	1.19	inches inches										
5-yr Runoff Volume (P1 = 1.5 in.) = 10-yr Runoff Volume (P1 = 1.75 in.) =	3.330	acre-feet acre-feet	1.50	inches						-				
25-yr Runoff Volume (P1 = 2 in.) =	4.040	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) = 100-yr Runoff Volume (P1 = 2.52 in.) =	4.703 5.508	acre-feet acre-feet	2.25 2.52	inches inches									-	
500-yr Runoff Volume (P1 = 3.14 in.) =	7.275	acre-feet		inches										
Approximate 2-yr Detention Volume = Approximate 5-yr Detention Volume =	1.898 2.482	acre-feet acre-feet												
Approximate 10-yr Detention Volume =	2.994	acre-feet												
Approximate 25-yr Detention Volume = Approximate 50-yr Detention Volume =	3.572 3.917	acre-feet acre-feet												
Approximate 100-yr Detention Volume =	4.274	acre-feet								-				
		-												
Define Zones and Basin Geometry Zone 1 Volume (WQCV) =	0.755	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	2.133	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	1.386 4.274	acre-feet acre-feet												
Initial Surcharge Volume (ISV) =	user	ft ³												
Initial Surcharge Depth (ISD) = Total Available Detention Depth (H _{total}) =	user	ft ft												
Depth of Trickle Channel $(H_{TC}) =$	user	ft												
Slope of Trickle Channel (S_{TC}) =	user	ft/ft												
Slopes of Main Basin Sides (S_{main}) = Basin Length-to-Width Ratio ($R_{L/W}$) =	user	H:V												
Initial Surcharge Area $(A_{ISV}) =$ Surcharge Volume Length $(L_{ISV}) =$	user user	ft² ft												
Surcharge Volume Width (W _{ISV}) =	user	ft								-				
Depth of Basin Floor (H_{FLOOR}) = Length of Basin Floor (L_{FLOOR}) =	user user	ft ft												
Width of Basin Floor $(W_{FLOOR}) =$	user	ft												
Area of Basin Floor (A _{FLOOR}) =	user	ft ²								-				
Volume of Basin Floor (V _{FLOOR}) = Depth of Main Basin (H _{MAIN}) =	user	ft ³ ft												
Length of Main Basin $(L_{MAIN}) =$	user	ft							-					
Width of Main Basin (W _{MAIN}) = Area of Main Basin (A _{MAIN}) =	user user	ft ft²												
Volume of Main Basin (V _{MAIN}) =	user	ft ³												
Calculated Total Basin Volume (V_{total}) =	user	acre-feet											<u> </u>	
									-					
									-				L	
													<u> </u>	
										1 1				

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

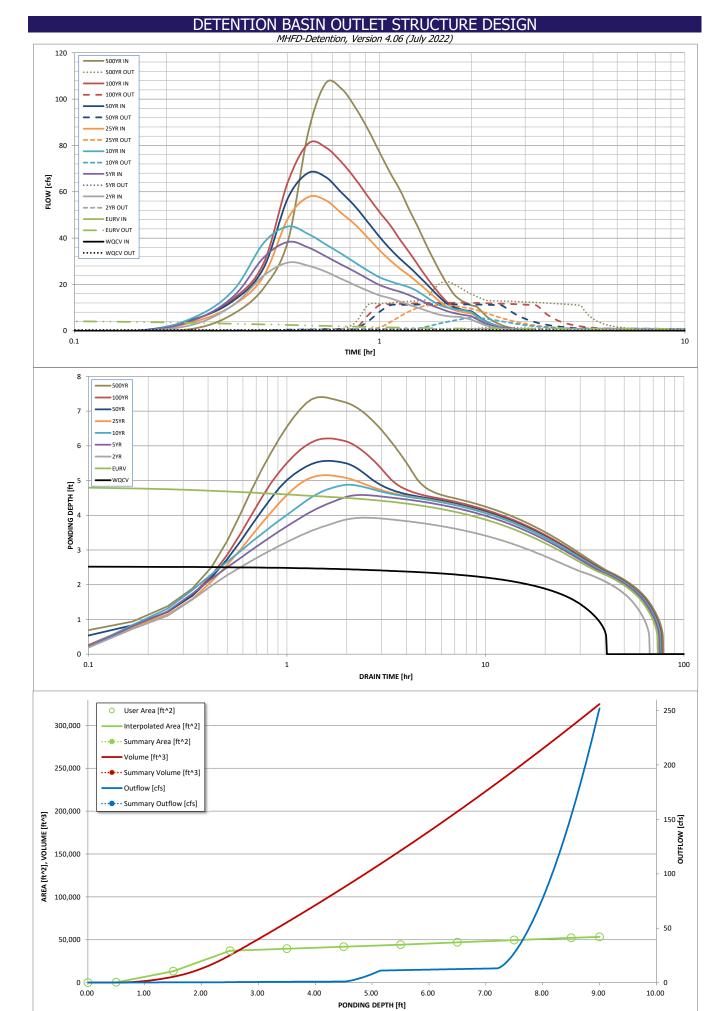




MHFD-Detention_v4-06-NORTH_POND, Outlet Structure

8/21/2023, 12:32 PM

the existing condition Q's are not comparable because the basins analyzed are drastically different from the proposed condition.



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program

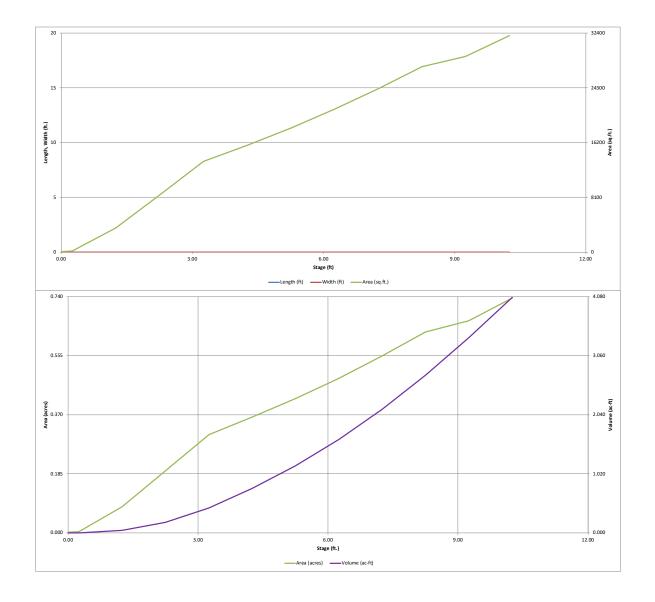
	The user can o	verride the calcu	lated inflow hyd	lrographs from t	his workbook w	ith inflow hydro	graphs develope	d in a separate p	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.35	0.03	1.12
	0:15:00	0.00	0.00	3.08	5.01	6.21	4.18	5.26	5.10	7.49
	0:20:00	0.00	0.00	11.42	15.11	17.83	11.29	13.20	14.07	18.43
	0:25:00	0.00	0.00	23.83	31.62	37.90	23.57	27.14	29.15	38.43
	0:30:00	0.00	0.00	29.48	38.37	45.06	48.36	57.15	64.09	85.59
	0:35:00	0.00	0.00	28.15	35.99	41.85	57.78	68.19	80.80	107.03
	0:40:00	0.00	0.00	25.54	32.15	37.29	56.30	66.32	79.13	104.54
	0:45:00	0.00	0.00	22.44	28.54	33.24	50.79	59.68	72.84	96.35
	0:50:00 0:55:00	0.00	0.00	19.66 17.28	25.46	29.38	45.74 40.08	53.59 46.82	65.48 57.94	86.90 76.96
	1:00:00	0.00	0.00	17.28	22.42 19.80	25.93 23.09	34.77	40.82	57.94	68.10
	1:05:00	0.00	0.00	14.06	19.00	21.35	30.40	35.32	45.57	60.77
	1:10:00	0.00	0.00	12.63	16.89	20.06	26.84	31.11	39.34	52.33
	1:15:00	0.00	0.00	11.25	15.43	18.82	23.91	27.61	33.94	44.90
	1:20:00	0.00	0.00	10.02	13.77	17.03	20.86	24.02	28.54	37.57
	1:25:00	0.00	0.00	8.83	12.14	14.72	17.94	20.59	23.58	30.91
	1:30:00	0.00	0.00	7.73	10.71	12.62	15.04	17.19	19.26	25.11
	1:35:00	0.00	0.00	6.87	9.58	10.98	12.40	14.10	15.44	19.99
	1:40:00	0.00	0.00	6.38	8.49	10.04	10.28	11.62	12.33	15.85
	1:45:00	0.00	0.00	6.15	7.69	9.48	9.06	10.22	10.56	13.51
	1:50:00	0.00	0.00	6.01	7.14	9.08	8.30	9.35	9.47	12.04
	1:55:00 2:00:00	0.00	0.00	5.41 4.81	6.72 6.26	8.65 7.99	7.82	8.80 8.40	8.73 8.20	11.04 10.32
	2:05:00	0.00	0.00	3.84	5.02	6.40	6.02	6.77	6.51	8.15
	2:10:00	0.00	0.00	2.95	3.84	4.90	4.58	5.14	4.87	6.08
	2:15:00	0.00	0.00	2.26	2.95	3.74	3.49	3.92	3.66	4.56
	2:20:00	0.00	0.00	1.73	2.24	2.83	2.65	2.97	2.78	3.46
	2:25:00	0.00	0.00	1.31	1.68	2.11	1.99	2.23	2.10	2.60
	2:30:00	0.00	0.00	0.98	1.24	1.56	1.47	1.65	1.56	1.94
	2:35:00	0.00	0.00	0.72	0.90	1.16	1.08	1.20	1.15	1.43
	2:40:00	0.00	0.00	0.52	0.65	0.86	0.81	0.90	0.86	1.07
	2:45:00	0.00	0.00	0.36	0.46	0.60	0.58	0.65	0.62	0.76
	2:50:00	0.00	0.00	0.23	0.31	0.39	0.39	0.43	0.41	0.51
	2:55:00 3:00:00	0.00	0.00	0.13	0.19	0.23	0.23	0.26	0.25	0.30
	3:05:00	0.00	0.00	0.06	0.09	0.11	0.12	0.13	0.12	0.15
	3:10:00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00 4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

				MHFD	D-Detention, Versio	on 4.06 (Ju	uly 2022)							
	Meadowlak	e Industria	al F1											
Basin ID:														
	2 ZONE 1													
T ZONE	1 AND 2	100-YE ORIFI	EAR CE		Depth Increment =		ft							
PERMANENT ORIFI POOL Example Zon	e Configura	tion (Rete	ntion Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
	J. J. J.	• • •	,		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)
Watershed Information	500	1		6729.75			0.00				100	0.002	22	0.001
Selected BMP Type = Watershed Area =	EDB 17.81	acres			6730 6731		1.25				161 3,554	0.004	33 1,890	0.001 0.043
Watershed Length =	1,280	ft			6732		2.25				8,459	0.194	7,897	0.181
Watershed Length to Centroid =	640	ft			6733		3.25				13,394	0.307	18,823	0.432
Watershed Slope =	0.020	ft/ft			6734		4.25				15,797	0.363	33,419	0.767
Watershed Imperviousness = Percentage Hydrologic Soil Group A =	74.00% 95.0%	percent percent			6735 6736		5.25 6.25				18,327 21,107	0.421	50,481 70,198	1.159 1.612
Percentage Hydrologic Soil Group B =	5.0%	percent			6737		7.25				24,138	0.554	92,820	2.131
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			6738		8.25				27,420	0.629	118,599	2.723
Target WQCV Drain Time =	40.0	hours			6739		9.25				28,927	0.664	146,773	3.369
Location for 1-hr Rainfall Depths =					6740		10.25				32,059	0.736	177,266	4.069
After providing required inputs above in depths, click 'Run CUHP' to generate run	cluding 1-hour hoff hydrograph	rainfall ns using								-				
the embedded Colorado Urban Hydro	ograph Proced	ure.	Optional Use	er Overrides										
Water Quality Capture Volume (WQCV) =		acre-feet		acre-feet										
Excess Urban Runoff Volume (EURV) = 2-yr Runoff Volume (P1 = 1.19 in.) =	1.684 1.208	acre-feet acre-feet	1.19	acre-feet inches										
2-yr Runoff Volume (P1 = 1.19 in.) = 5-yr Runoff Volume (P1 = 1.5 in.) =	1.572	acre-feet	1.19	inches									<u> </u>	
10-yr Runoff Volume (P1 = 1.75 in.) =	1.863	acre-feet	1.75	inches										
25-yr Runoff Volume (P1 = 2 in.) =	2.233	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) = 100-yr Runoff Volume (P1 = 2.52 in.) =	2.582	acre-feet acre-feet	2.25	inches inches										
500-yr Runoff Volume (P1 = 2.32 iii.) =	3.911	acre-feet	2.32	inches										
Approximate 2-yr Detention Volume =	1.111	acre-feet		-										
Approximate 5-yr Detention Volume =	1.449	acre-feet												
Approximate 10-yr Detention Volume = Approximate 25-yr Detention Volume =	1.741 2.066	acre-feet acre-feet												
Approximate 23-yr Detention Volume =	2.258	acre-feet							-					
Approximate 100-yr Detention Volume =	2.447	acre-feet												
		-												
Define Zones and Basin Geometry	0.427	1												
Zone 1 Volume (WQCV) = Zone 2 Volume (EURV - Zone 1) =	0.437	acre-feet acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =		acre-feet												
Total Detention Basin Volume =	2.447	acre-feet												
Initial Surcharge Volume (ISV) =	user	ft ³												
Initial Surcharge Depth (ISD) = Total Available Detention Depth (H _{total}) =	user	ft ft												
Depth of Trickle Channel $(H_{TC}) =$	user	ft												
Slope of Trickle Channel (S _{TC}) =	user	ft/ft								-				
Slopes of Main Basin Sides (S_{main}) =	user	H:V												
Basin Length-to-Width Ratio $(R_{L/W}) =$	user													
Initial Surcharge Area (A _{ISV}) =	user	ft ²												
Surcharge Volume Length $(L_{ISV}) =$	user	ft												
Surcharge Volume Width $(W_{1SV}) =$	user	ft												
Depth of Basin Floor (H _{FLOOR}) =	user	ft												
Length of Basin Floor $(L_{FLOOR}) =$ Width of Basin Floor $(W_{FLOOR}) =$	user	ft ft												
Area of Basin Floor (A _{FLOOR}) =	user	ft ²												
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³								-				
Depth of Main Basin (H _{MAIN}) =	user	ft											<u> </u>	
Length of Main Basin (L_{MAIN}) = Width of Main Basin (W_{MAIN}) =	user	ft ft												
Area of Main Basin (Amain) =	user	ft ²												
Volume of Main Basin (V _{MAIN}) =		ft ³												
Calculated Total Basin Volume (V_{total}) =	user	acre-feet											<u> </u>	
									-					
													1	
													1	
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

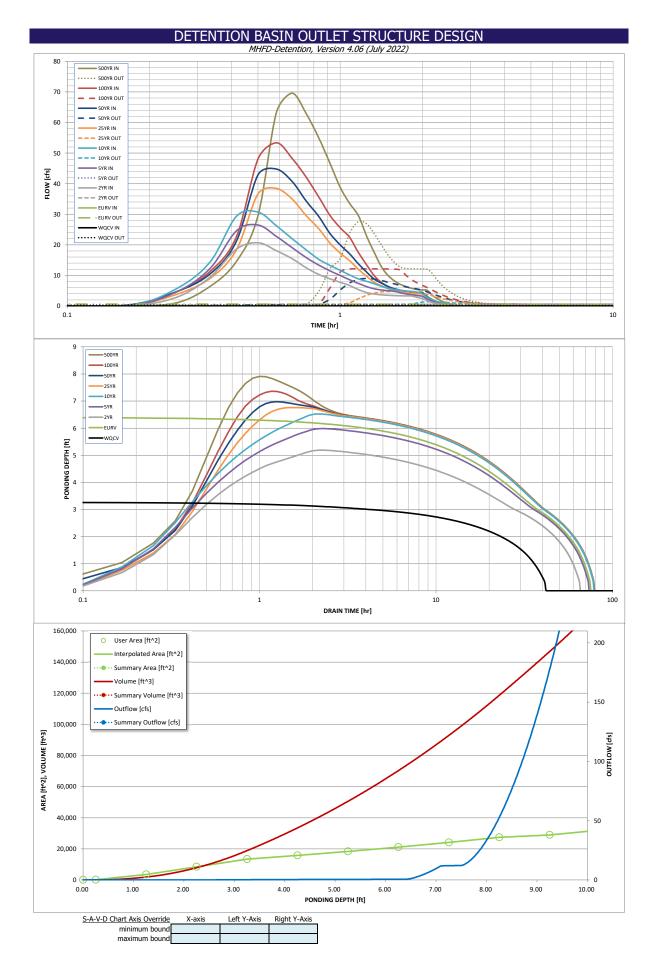


DETENTION BASIN OUTLET STRUCTURE DESIGN

	Meadowlake Indu	strial F1							
Basin ID:	Pona B			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type	Many of th	e elevations o	n the pond
			Zone 1 (WQCV)	3.27	0.437	Orifice Plate	detail shee	ets are incorre	ct so a mo
	100-YEAR		Zone 2 (EURV)	6.40	1.247	Orifice Plate	thorough re	eview of this s	preadshee
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	7.80	0.763	Weir&Pipe (Restrict)	will be don	e when that is	corrected
Example Zone Configuration (Retention Pond) Total (all zones) 2.447									
User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP).									
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underd	Irain Orifice Area =	N/A	ft ²	
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orifi	ces or Elliptical Slot	Weir (typically use	ed to drain WQCV a	nd/or EURV in a se	dimentation BMP)		Calculated Parame	eters for Plate	
Centroid of Lowest Orifice =	0.00	ft (relative to basi	n bottom at Stage =	= 0 ft)	WQ Orifi	ce Area per Row =	N/A	ft ²	
Depth at top of Zone using Orifice Plate =	3.50		n bottom at Stage =			ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A		highlighted va			ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A		atch plans or co date plan deta		erified.	lliptical Slot Area =	N/A	ft²	
		ev	erything match	· · · · · · · · · · · · · · · · · · ·	dsheet.				
User Input: Stage and Total Area of Each Orific									٦
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.50	3.00						
Orifice Area (sq. inches)	1.40	1.40	6.00						L
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)	(optional)		(optional)				. con 15 (optional)	(optional)	1
Orifice Area (sq. inches)			-						
User Input: Vertical Orifice (Circular or Rectand	<u>gular)</u>						Calculated Parame	eters for Vertical O	rifice
	Not Selected	Not Selected					Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage :	= 0 ft) Ver	tical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	n bottom at Stage =	= 0 ft) Vertical	Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						_
User Input: Overflow Weir (Dropbox with Flat			ectangular/Trapezoi T	dal Weir and No O	<u>utlet Pipe)</u>			eters for Overflow	<u>Neir</u>
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	6.40	N/A		oottom at Stage = 0	ft) Height of Grate		6.40	N/A	feet
Overflow Weir Front Edge Length =	3.00	N/A	feet	6		/eir Slope Length =	3.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V		ate Open Area / 10		7.63	N/A	ft ²
Horiz. Length of Weir Sides =	3.00	N/A N/A	feet		erflow Grate Open Iverflow Grate Oper		6.26 3.13	N/A N/A	ft ²
Overflow Grate Type = Debris Clogging % =	Type C Grate 50%	N/A	%	U	wernow Grate Oper	IT Aled w/ Deblis =	5.15	IN/A	In
	5070	14/1							
User Input: Outlet Pipe w/ Flow Restriction Plat	e (Circular Orifice, I	Restrictor Plate, or	Rectangular Orifice)	Cal	Iculated Parameter	s for Outlet Pipe w	/ Flow Restriction F	late
	Zone 3 Restrictor	Not Selected	1	*			Zone 3 Restrictor		1
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below ba	asin bottom at Stage	= 0 ft) Ou	utlet Orifice Area =	0.82	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches		Outlet	Orifice Centroid =	0.41	N/A	feet
Restrictor Plate Height Above Pipe Invert =	8.50		inches	Half-Cent	ral Angle of Restric	tor Plate on Pipe =	1.52	N/A	radians
User Input: Emergency Spillway (Rectangular o	r Trapezoidal)						Calculated Parame	eters for Spillway	
Spillway Invert Stage=	7.50	-	n bottom at Stage =	= 0 ft)		esign Flow Depth=	0.89	feet	
Spillway Crest Length =	18.00	feet			-	op of Freeboard =	9.39	feet	
Spillway End Slopes =	4.00	H:V				op of Freeboard =	0.67	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at T	op of Freeboard =	3.46	acre-ft	
Routed Hydrograph Results	The user can over	ride the default CL	IHP hydrographs an	d runoff volumes b	y entering new val		ydrographs table (Columns W througi	h AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	0.437 N/A	1.684 N/A	1.208 1.208	1.572 1.572	1.863 1.863	2.233 2.233	2.582 2.582	2.997 2.997	3.911 3.911
CUHP Predevelopment Peak Q (cfs) =	N/A N/A	N/A N/A	0.1	0.3	0.4	4.1	7.3	11.3	19.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	2.9	5.9	10.1	13.7	17.6	
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.06	0.16	0.33	0.57	0.77	0.99	1.12
Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	N/A 0.3	N/A 0.6	20.7 0.5	26.5 0.6	30.7 1.4	38.4 4.7	44.8 9.0	53.4 12.2	69.6 27.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	0.5 N/A	0.0	0.2	0.5	0.7	0.7	1.4
Structure Controlling Flow =	Plate	Øverflow Weir 1	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.7	1.3	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	38 40	66 71	58 62	65	69 74	68 73	66 73	65 72	62 71
Maximum Ponding Depth (ft) =	3.27	6.40	5.19	5.98	6.52	6.76	6.97	7.36	7.91
Area at Maximum Ponding Depth (acres) =	0.31	0.49	0.42	0,47	0.50	0.52	0.53	0.56	0.60
Maximum <mark>/</mark> olume Stored (acre-ft) =	0.438	1.685	1.130	1.483	1.745	1.862	1.978	2.187	2.507
	 								
Why are all these values			EAK FLOWS WER						
N/A?			S LAND USES TO S DCM VOL. 1 IDF						
							500-YEAR EVEN		

MHFD-Detention_v4-06-SOUTH_POND, Outlet Structure

Provide hydrology calcs to support the override predevelopment Q the existing condition Q's are not comparable because the basins analyzed are drastically different from the proposed condition.



DETENTION BASIN OUTLET STRUCTURE DESIGN

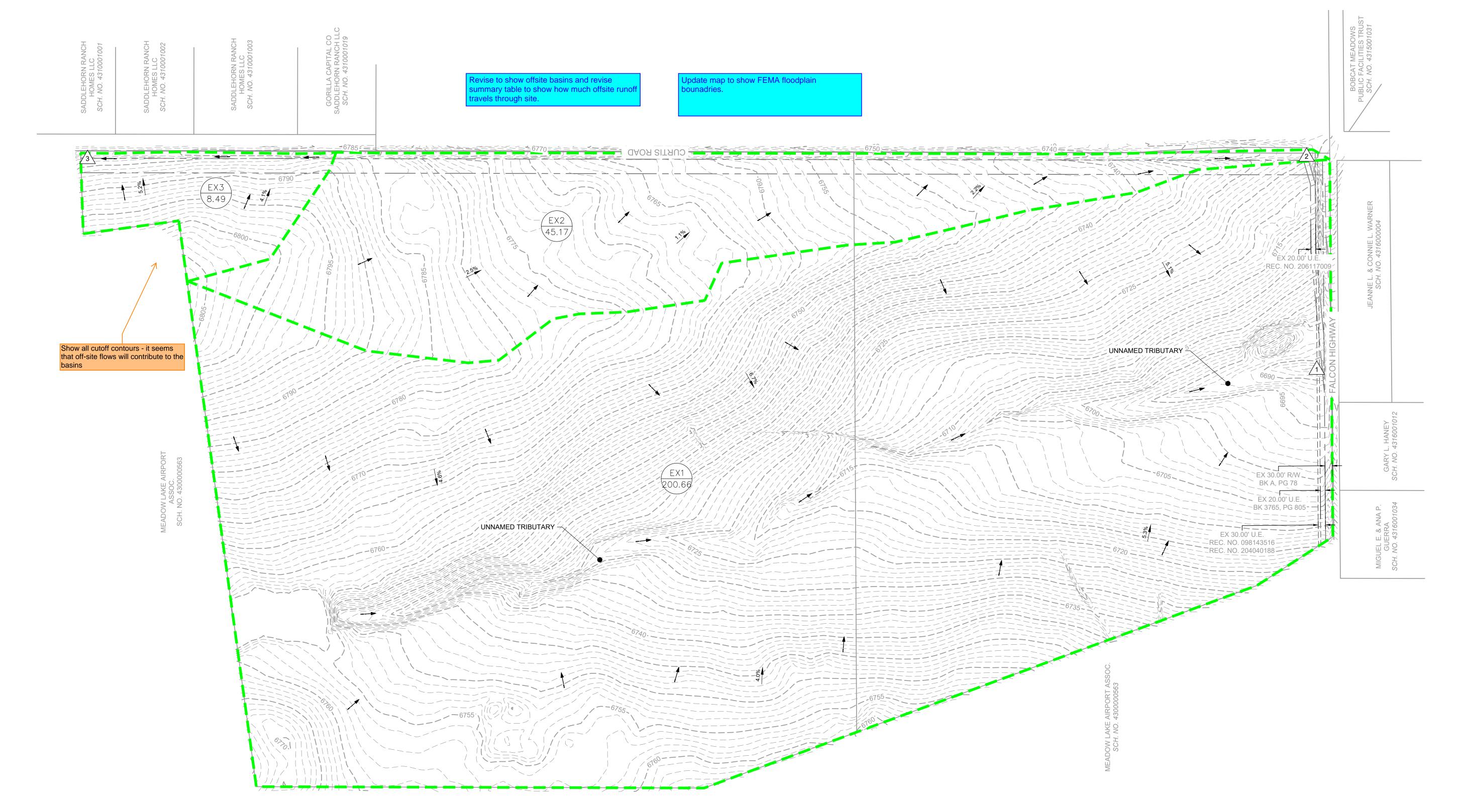
Outflow Hydrograph Workbook Filename:

	Inflow Hydrog									
ĺ								oed in a separate		0.00
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]		50 Year [cfs]		
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00 0:15:00	0.00	0.00	0.00	0.00 4.48	0.00	0.00 3.72	0.31 4.60	0.03 4.53	1.00 6.38
	0:20:00	0.00	0.00	9.43	12.25	14.35	9.01	10.45	11.24	14.55
	0:25:00	0.00	0.00	18.57	24.55	29.30	18.32	21.11	22.60	29.52
	0:30:00	0.00	0.00	20.69	26.47	30.70	36.61	42.87	48.03	63.23
	0:35:00	0.00	0.00	18.09	22.77	26.25	38.43	44.78	53.38	69.60
	0:40:00 0:45:00	0.00	0.00	15.47	19.11	22.00	34.98	40.75	48.31	62.98
	0:50:00	0.00	0.00	12.52 10.33	15.84 13.41	18.38 15.30	29.58 25.34	34.37 29.35	42.19 35.76	55.10 46.79
	0:55:00	0.00	0.00	8.89	11.50	13.30	20.60	23.77	29.67	38.82
	1:00:00	0.00	0.00	7.75	9.97	11.66	17.34	19.98	25.60	33.55
	1:05:00	0.00	0.00	6.69	8.57	10.13	14.79	17.03	22.45	29.53
	1:10:00	0.00	0.00	5.35	7.39	8.86	12.00	13.76	17.46	22.84
	1:15:00 1:20:00	0.00	0.00	4.40 3.91	6.32 5.63	8.04 7.28	9.72 7.74	11.08 8.78	13.46 9.89	17.50 12.80
	1:25:00	0.00	0.00	3.64	5.03	6.42	6.60	7.47	7.71	9.92
	1:30:00	0.00	0.00	3.49	4.97	5.83	5.63	6.35	6.38	8.14
	1:35:00	0.00	0.00	3.40	4.80	5.40	4.98	5.62	5.53	7.02
	1:40:00	0.00	0.00	3.33	4.28	5.11	4.55	5.13	4.96	6.25
	1:45:00	0.00	0.00	3.28	3.90	4.90	4.28	4.81	4.58	5.74
	1:50:00 1:55:00	0.00	0.00	3.25 2.78	3.62 3.42	4.76 4.51	4.08 3.96	4.59 4.45	4.32 4.18	5.39 5.21
	2:00:00	0.00	0.00	2.43	3.17	4.06	3.88	4.36	4.13	5.15
	2:05:00	0.00	0.00	1.72	2.25	2.87	2.75	3.09	2.93	3.65
	2:10:00	0.00	0.00	1.19	1.55	1.99	1.91	2.15	2.05	2.55
	2:15:00	0.00	0.00	0.81	1.06	1.37	1.32	1.48	1.42	1.76
	2:20:00 2:25:00	0.00	0.00	0.54 0.34	0.69 0.45	0.91 0.59	0.88	0.99 0.65	0.95	1.18 0.77
	2:30:00	0.00	0.00	0.34	0.45	0.39	0.38	0.65	0.62	0.50
	2:35:00	0.00	0.00	0.11	0.16	0.20	0.21	0.12	0.10	0.28
	2:40:00	0.00	0.00	0.04	0.07	0.09	0.10	0.11	0.10	0.13
	2:45:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.03	0.03
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00 3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00 4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



Meadow Lake Industrial Filing No. 1 Preliminary Drainage Report Project No: 2202744

APPENDIX E – DRAINAGE MAPS

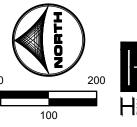


SUMMARY RUNOFF TABLE										
BASIN AREA (ac) % IMPERVIOUS Q ₅ (cfs) Q ₁₀₀ (cfs)										
EX1	200.66	2	18.9	126.8						
EX2	45.17 6 5.1 26.7									
EX3	8.49	8.49 2 1.5 9.8								

DESIGN POINT SUMMARY TABLE									
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)						
1	EX1	18.9	126.8						
2	EX2	5.1	26.7						
3	EX3	1.5	9.8						

These existing drainage maps are much larger than the proposed. The existing maps and proposed maps should be looking at approximately the same areas for comparison between the existing and developed conditions.

MEADOW LAKE INDUSTRIAL FILING NO. 1

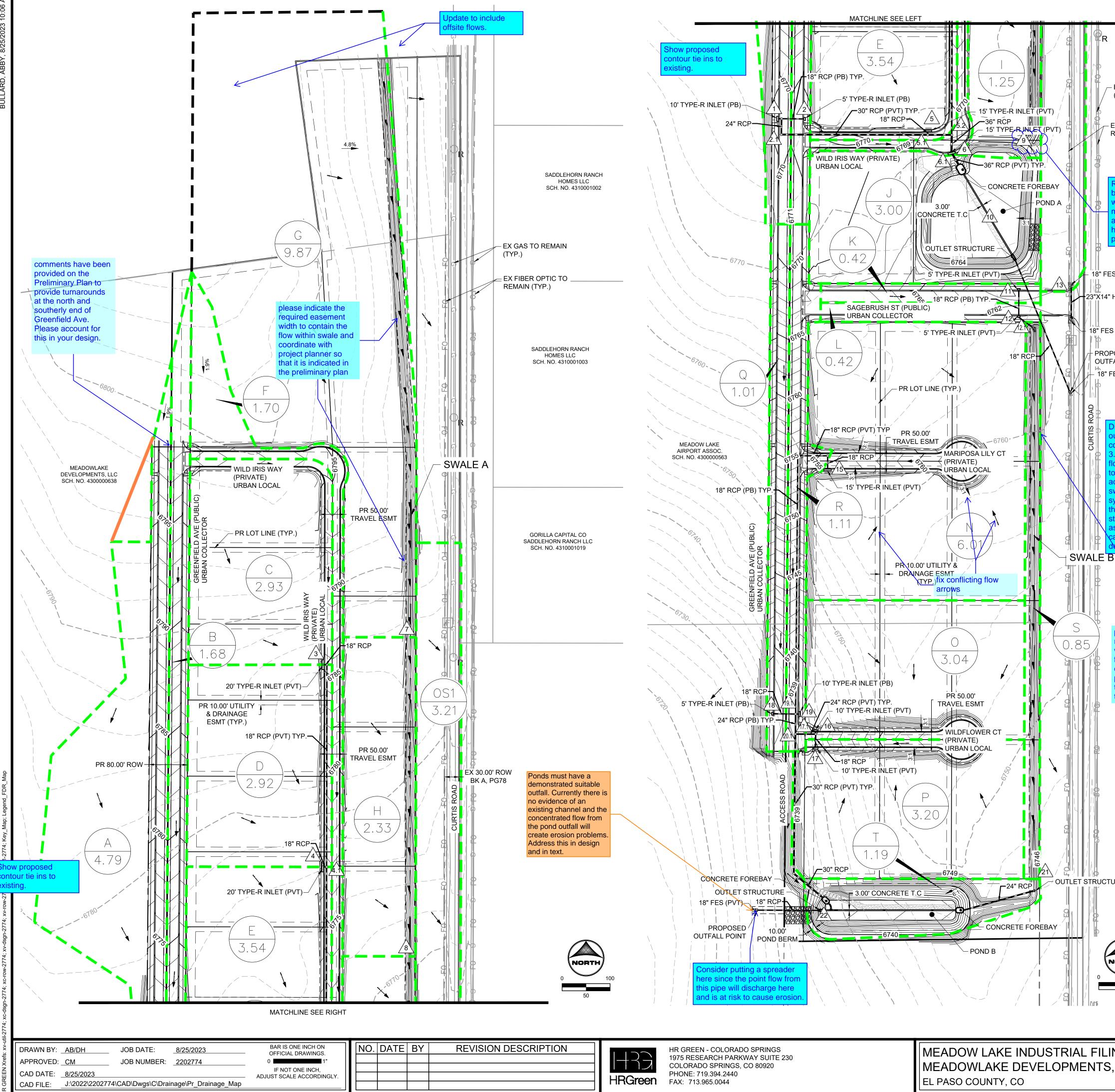




2202774 NQJ repared By: 8/24/2023

EX DRAINAGE MAP

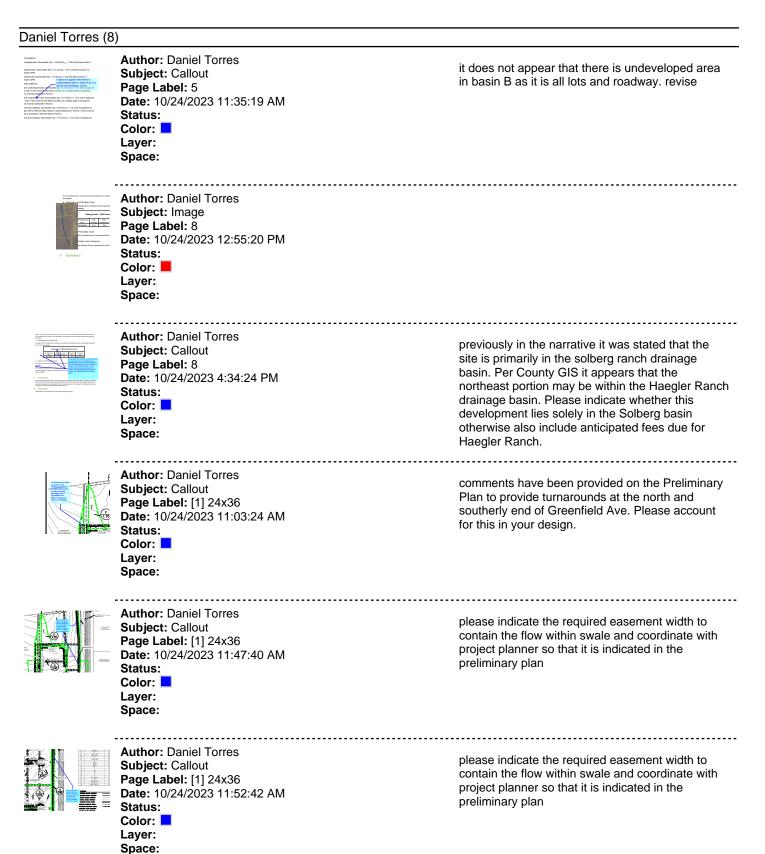




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	HRGroop

2		SUMMA	ARY RUNOF	F TABLE					
	BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)				
	A	4.79	33	5.3	14.1				
- EX GAS TO REMAIN	B	1.68	97	5.7	10.4				
(TYP.)	C D	2.93 2.92	80 80	6.8 7.0	13.5 14.0				
	E	3.54	80	8.5	14.0				
– EX FIBER OPTIC TO REMAIN (TYP.)	F	1.70	93	4.7	8.7				
	G H	9.87 2.33	76 70	14.9 4.6	30.3 9.6		\mathbb{N}		
	I	1.25	68	2.5	5.2	NORT	гн		
	J K	3.00 0.42	26 90	2.7 1.8	8.6 3.3				
Revise to show a	L	0.42	90	1.8	3.3			SCALE: NTS	
blowup of this section where the swale	N O	6.01 3.04	80 80	<u>14.4</u> 7.2	28.6 14.2				
meets pond. Need	Р	3.20	80	7.8	15.5				
additional clarity as to how swale will enter	Q R	1.01 1.11	96 96	4.0	7.6 6.2				
pond.	S	0.85	2	0.3	1.7				
			n the TIS to iden ed with this deve		2.4				
Curtis Ro	d roadway	cross section	. Coordinate with	the traffic					
your des		unt for any ne	cessary improver	nents in					
		irn is indicate	d as required at 9			Note, pe	er EC	M any	
Please a	iccount for	this in your a	d as required at S nalysis/design as	nt may	ARLE	swale th	hat co	onveys	
			h and the propos	ed outfall.	cfs) ∑Q ₁₀₀ (cfs) more th			
				· · · · · · · · · · · · · · · · · · ·	,	easeme			
	2		B	5.7					
	2.1	1	DP1,DP2	9.9) 22.2	2			
' FES (PVT)	3		C D	6.8 7.0					
	4.1	 [D DP3,DP4	13.2					
	5		E	8.5	5 16.9)			
Discuss/analyze	5.1 5.2		P2.1,DP5 DP4.1,5.1	16. 26.					
outfall in the report	6		F	4.7	7 8.7				
contents. Per ECM 3.2.4 developed	6.1 7		P5.2,DP6 G	30.					
flows shall discharge	8		DP7,H	15.	9 32.5	5			
to a hydraulically adequate natural	9		I,DP8	16.					
swale or manmade	10 11		DP6.1,J K	32.5					
system. Determine if this roadside ditch is	12		L	1.8	3 3.3				
stable enough as well	13 15		OS1 N	1.6 14.4					
as if it has enough capacity for	16		0	7.2					
developed flows.	17 17.1		P P16 DP17	7.8					
В	17.1	D	P16,DP17 Q	4.0					
	19		215,DP16,R	6.3	3 17.1				
	21 22		DP12.1,S 20.1,DP21,T	2.5					
please indicate the required easement width to contain the flow within swale and coordinate with project planner so that it is indicated in the preliminary plan	BROPOSE EXISTING EXISTING PROPOSE EXISTING PROPOSE EXISTING PROPOSE	D MAJOR CO MAJOR CO MAJOR CON MINOR CON D STORM SE DRAINAGE S D DRAINAGE D FLOW DIRE FLOW DIREC D DRAINAGE	NTOUR TOUR WER WALE SWALE ECTION TION BASIN		5250 - 5250 	Ν			
.ING NO. 1 S, LLC			GE MAPS	NAGE MA	P			SHEET DR	2

V1_Drainage Report - Preliminary.pdf Markup Summary 10-24-2023



Author: Daniel Torres Subject: Callout Page Label: [1] 24x36 Date: 10/24/2023 11:57:13 AM Status: Color: Layer: Space:



Author: Daniel Torres Subject: Text Box Page Label: [1] 24x36 Date: 10/24/2023 1:00:58 PM Status: Color: Layer: Space:

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Authory Incolumon

fix conflicting flow arrows

comments have been provided on the TIS to identify improvements that may be needed with this development to Curtis Rd roadway cross section. Coordinate with the traffic engineer and account for any necessary improvements in your design.

.....

A northbound left turn is indicated as required at Sagebrush. Please account for this in your analysis/design as it may impact the existing roadside ditch and the proposed outfall.

lpackman (16)



to O _M = 0 or and guard to O _M = 0 or a solution to O _M = 0 or a solution to	Author: Ipackman Subject: Callout Page Label: 5 Date: 10/16/2023 3:39:10 PM Status: Color: Layer: Space:	Revise to include offsite runoff that drains to this basin.
er moet fu bekak faster fu bekak te starsprese take de starsprese de starsprese de starsprese take	Author: Ipackman Subject: Callout Page Label: 5 Date: 10/17/2023 9:38:09 AM Status: Color: Layer: Space:	Revise drainage report to include all of the offsite basins that drain to this site. Per the streamstats application there is a large area upstream of this site.
	Author: lpackman Subject: Callout Page Label: 7 Date: 10/16/2023 3:06:52 PM Status: Color: Layer: Space:	For both narratives expand more on the ultimate outfall each pond will drain to. Per ECM 3.2.4 developed flows need to drain to a system that is hydraulically adequate. Analyze outfalls for each pond.

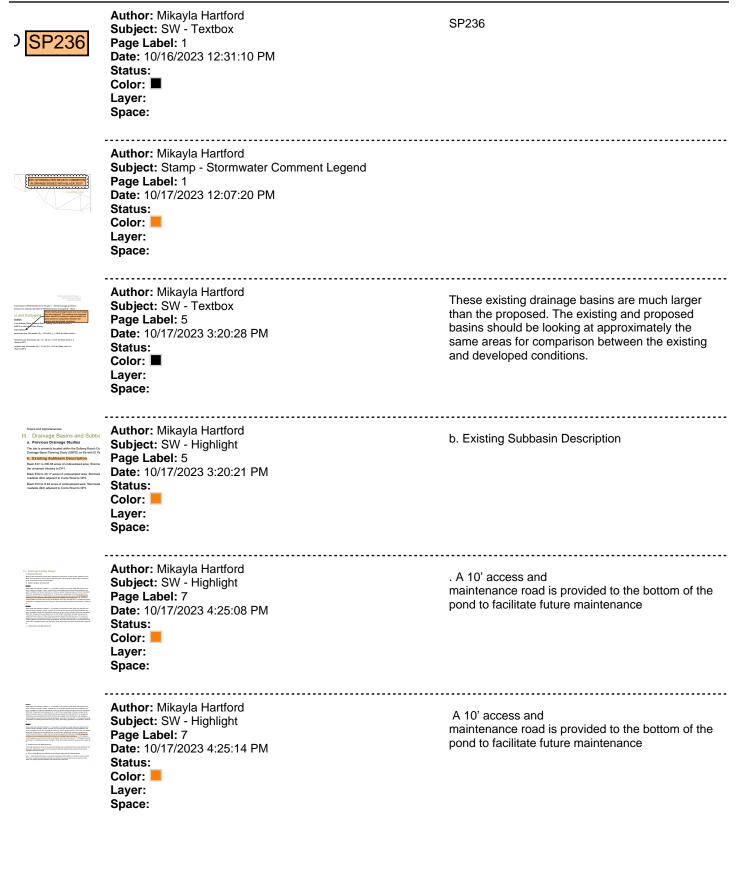
chang then belong these. These optimises of control has the set of adversion years, the set of period of the set of the chain, it is the adversion of the set of the period. If it densings having a chain, it is the adversion of the set of the period of the chain is the set. The set of the set of the period of the set of denses the set of the period of the set of the dense the set of the set of the set of the set of the dense to the set of the set of the set of the set of the dense to the set of the set of the set of the set of the dense to the set of the dense to the set of the dense to the set of the dense to the set of the dense to the set of the dense to the set of the dense to the set of the Author: Ipackman Subject: Callout Page Label: 8 Date: 10/17/2023 9:50:37 AM Status: Color: Layer: Space:

Revise to explain whether downstream facilities/ natural swales are hydraulically adequate to handle developed flows. What are the ultimate destinations for each outfall? Are developed flows a major increase compared to historic flows? Explain.

 V. Surveys, Surveys, Surveys, Surve	Author: Ipackman Subject: Callout Page Label: 8 Date: 10/24/2023 4:47:48 PM Status: Color: Layer: Space:	Discuss offsite flows that flow through the site. What is the condition of the natural channel labeled as the unnamed tributary where pond B outfalls. Determine if mitigation will be required because of the pond b outfall.
	Author: Ipackman Subject: Callout Page Label: 24 Date: 10/17/2023 1:12:06 PM Status: Color: Layer: Space:	Impervious value for basin appears to be low. It includes lot 6, which will have an industrial use. Revise.
Horizontal Elipse Concern Beare edge winderdentil (1) e 0.01.2.0.0348, 07.0.5 e 2.0.2 e	Author: Ipackman Subject: Callout Page Label: 52 Date: 10/17/2023 7:26:23 AM Status: Color: Layer: Space:	Culvert is not shown with headwall. Revise or change design.
And a time of the action of th	Author: Ipackman Subject: Text Box Page Label: 66 Date: 10/16/2023 3:40:03 PM Status: Color: Layer: Space:	Revise to show offsite basins and revise summary table to show how much offsite runoff travels through site.
	Author: Ipackman Subject: Text Box Page Label: 66 Date: 10/17/2023 9:43:29 AM Status: Color: Layer: Space:	Update map to show FEMA floodplain bounadries.
I OULET STRUCTURE I MERCENT - LE REC MENCENT - MERCENT PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTION PROPORTIONO	Author: Ipackman Subject: Callout Page Label: [1] 24x36 Date: 10/16/2023 3:14:18 PM Status: Color: Layer: Space:	Consider putting a spreader here since the point flow from this pipe will discharge here and is at risk to cause erosion.

	Author: Ipackman Subject: Cloud+ Page Label: [1] 24x36 Date: 10/24/2023 4:54:41 PM Status: Color: Layer: Space:	Revise to show a blowup of this section where the swale meets pond. Need additional clarity as to how swale will enter pond.
Show proposed contour tie ins to existing.	Author: Ipackman Subject: Text Box Page Label: [1] 24x36 Date: 10/16/2023 3:36:56 PM Status: Color: Layer: Space:	Show proposed contour tie ins to existing.
Show proposed contour tie ins to existing.	Author: Ipackman Subject: Text Box Page Label: [1] 24x36 Date: 10/16/2023 3:36:50 PM Status: Color: Layer: Space:	Show proposed contour tie ins to existing.
And an COM my more than 15 cfs rest that a submitter rest that a submitter restriction of the restriction of	Author: Ipackman Subject: Callout Page Label: [1] 24x36 Date: 10/16/2023 3:48:48 PM Status: Color: Layer: Space:	Note, per ECM any swale that conveys more than 15 cfs requires a drainage easement.
	Author: Ipackman Subject: Callout Page Label: [1] 24x36 Date: 10/16/2023 3:50:07 PM Status: Color: Layer: Space:	Update to include offsite flows.
	Author: Ipackman Subject: Callout Page Label: [1] 24x36 Date: 10/24/2023 4:53:23 PM Status: Color: Layer: Space:	Discuss/analyze outfall in the report contents. Per ECM 3.2.4 developed flows shall discharge to a hydraulically adequate natural swale or manmade system. Determine if this roadside ditch is stable enough as well as if it has enough capacity for developed flows.

Mikayla Hartford (53)



	Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: 7 Date: 10/18/2023 7:39:30 AM Status: Color: ■ Layer: Space:	Stabilized access ramp shall be a minimum of 15ft wide and no greater than 12% slope, in accordance with DCMv1, Chap 11.2.2.
	Author: Mikayla Hartford Subject: SW - Textbox Page Label: 7 Date: 10/18/2023 8:24:06 AM Status: Color: Layer: Space:	A maintenance agreement with the County is required.
<text><text><text><text></text></text></text></text>	Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: 8 Date: 10/18/2023 8:25:08 AM Status: Color: ■ Layer: Space:	This step is focused on permanent specialized source control, not the temp BMPs proposed. This project has no need of specialized source controls an d that can be stated.
4131 100 4017 AN 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: 20 Date: 10/17/2023 4:07:15 PM Status: Color: ■ Layer: Space:	This area is significantly more than the proposed condition and as such the calculated flows are not comparable.
	Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: 25 Date: 10/17/2023 4:09:15 PM Status: Color: ■ Layer: Space:	total draining to ponds = 52.86 ac, what basin is not draining to the pond? OS1? Adding that OS1 basin area to the combined pond areas you get 56.07 ac.
APPENDIX C - HIGHNILIC CALCULATIONS HIGHNING IN COMMUNICATION OF THE ADMINISTRATION OF	Author: Mikayla Hartford Subject: SW - Textbox Page Label: 31 Date: 10/17/2023 4:11:40 PM Status: Color: ■ Layer: Space:	Provide riprap calculations for the culverts, pond outfall pipes, pond spillways, and any other riprap utilized onsite

Author: Mikayla Hartford ENDIX D - WATER QUALITY & DETENTI Provide forebay and trickle channel design Subject: SW - Textbox calculations abay and trickle channel Page Label: 54 Date: 10/18/2023 9:09:19 AM Status: Color: Layer: Space: Author: Mikayla Hartford Provide hydrology calcs to support the override Subject: SW - Textbox with Arrow predevelopment Q - the existing condition Q's are Page Label: 57 not comparable because the basins analyzed are Date: 10/18/2023 8:33:03 AM drastically different from the proposed condition. Status: Color: Layer: Space: Author: Mikayla Hartford Why are all these values N/A? Subject: SW - Textbox with Arrow Page Label: 57 Date: 10/18/2023 8:35:10 AM Status: Color: Layer: Space: Author: Mikayla Hartford Label Pond A to match plans Subject: SW - Textbox with Arrow Page Label: 57 Date: 10/18/2023 8:37:21 AM Status: Color: Layer: Space: Author: Mikayla Hartford feet Subject: Checkmark H:V Page Label: 57 feet Date: 10/18/2023 8:41:14 AM Status: Color: Layer: Space: Ift (relative to basi Author: Mikayla Hartford Х Subject: Text Box feet Page Label: 57 H:V Date: 10/18/2023 8:41:25 AM feet Status: Color: Layer: Space:

27.00	Author: Mikayla Hartford	4.00
4.00	Subject: SW - Highlight Page Label: 57	
	Date: 10/18/2023 8:41:30 AM	
1.00	Status: Color:	
	Layer:	
	Space:	
the last don't file of file featies file Strate Origin to	Author: Mikayla Hartford	
Day 14 dealerster Day 15 to lavert of Outer Rys - 530 Outer Rys Dannes - 18.00 Rescitativ Rate High Robey Rys Invest + 19.00 Day 19.00 (States (Rstandard v Taccoold)	Subject: SW - Textbox with Arrow	The plans show 5:1 slopes. Verify and update so both match.
The plana show 3-1 spikes instructure - 2.20 s skopes. Very and service. C22.20 s update so both match FeetCort 2004 Max Water Surface + 1.20	Page Label: 57 Date: 10/18/2023 8:42:05 AM	both match.
Banket Hadronsch Banket The own processes Dengin Harm Reider Umpf REID Garetsaur Beind Lingeh REI Garetsaur Beind Lingeh REI Garetsaur Beind Lingeh REID Garetsaur Beind REID	Status:	
	Color:	
	Layer:	
	Space:	
7.20	Author: Mikayla Hartford Subject: SW - Highlight	27.00
27.00	Page Label: 57	
4.00	Date: 10/18/2023 8:46:50 AM	
	Status: Color:	
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	Space:	
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7.20 1 (niel/w to basin bottom at Stage = 0.1t) 27.00 set 4.00 Vev	Subject: SW - Textbox with Arrow Page Label: 57	match.
and update so both match. Take call central solution and update s	Date: 10/18/2023 8:47:25 AM	
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	Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: 62 Date: 10/18/2023 9:24:56 AM Status: Color: Layer: Space:	Provide hydrology calcs to support the override predevelopment Q - the existing condition Q's are not comparable because the basins analyzed are drastically different from the proposed condition.
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ne 3 Restrict 2.50 18.00	Author: Mikayla Hartford Subject: SW - Highlight Page Label: 62 Date: 10/18/2023 9:53:37 AM Status: Color: Layer: Space:	2.50
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Author: Mikayla Hartford Subject: SW - Textbox Page Label: 62 Date: 10/18/2023 9:55:18 AM Status: Color: Layer: Space:

All highlighted values either do not match plans or could not be verified. Update plan details and verify everything matches this spreadsheet.

Author: Mikayla Hartford Subject: SW - Textbox Page Label: 66 Date: 10/17/2023 3:14:11 PM Status: Color: ■ Layer: Space:

These existing drainage maps are much larger than the proposed. The existing maps and proposed maps should be looking at approximately the same areas for comparison between the existing and developed conditions.



Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: 66 Date: 10/17/2023 3:21:47 PM Status: Color: Layer: Space:

Show all cutoff contours - it seems that off-site flows will contribute to the basins



Author: Mikayla Hartford Subject: Line Page Label: [1] 24x36 Date: 10/17/2023 3:22:15 PM Status: Color: Layer: Space:

Author: Mikayla Hartford Subject: SW - Textbox with Arrow Page Label: [1] 24x36 Date: 10/17/2023 3:24:02 PM Status: Color: ■ Layer: Space:

Ponds must have a demonstrated suitable outfall. Currently there is no evidence of an existing channel and the concentrated flow from the pond outfall will create erosion problems. Address this in design and in text.