## PRELIMINARY/FINAL DRAINAGE REPORT

**FOR** 

## APPALOOSA HWY 24 SUBDIVISION FILING NO. 1A, LOTS 1, 2 & 3

Prepared For:
Platte Valley, LLC
1378 Promontory Bluff View
Colorado Springs, CO 80921
719-491-0801

Prepared By:
Associated Design Professionals, Inc.
3520 Austin Bluffs Parkway Suite 102
Colorado Springs, CO 80918
719.266-5212

ADP Project No. 160504 September 19, 2018

Please state when improvements will be completed and who will maintain all drainage and WQ structures, please include who currently and in the future is responsible to maintain the concrete channel.





#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Michael A. B	artusek, P.E. #23329	
I, the Develo	R'S STATEMENT: oper, have read and will comply with all of the port and plan.	requirements specified in this
Ву:	Ron Waldthausen	
Title: Presid		
Address:	Platte Valley, LLC 1378 Promontory Bluff View Colorado Springs, CO 80921	
	ordance the El Paso County Land Developmen and 2, and the Engineering Criteria Manual, as	
Jennifer Irv	ine, County Engineer/ECM Administrator	Date
Conditions:		

### PRELIMINARY/FINAL DRAINAGE REPORT APPALOOSA HWY 24 SUBDIVISION FILING No. 1A, Lots 1, 2 & 3

#### PROJECT DESCRIPTION

This drainage report is for the development of the Appaloosa Hwy 24 Subdivision, Filing No. 1A, Lots 1, 2 & 3. The currently vacant 4.67 acre site is located north of U.S. Hwy 24 and east of Amelia Street. It is further described as the southern portion of Section 7, Township 14 South, Range 65 West of the 6th Principal Meridian in El Paso County, Colorado.

All of this lot is located in Sand Creek drainage basin and drains into the central tributary of Sand Creek. An existing 4'x4' box culvert is located at the southeast corner of U.S. Hwy 24 and Amelia St. Also an existing concrete channel is located on the east side of proposed Lot 3.

#### **SOILS**

The soil on the site can be described as having a rapid permeability, medium-surface runoff, and moderate to high hazard of erosion. The soils within the site are Truckton sandy loams. These soils are classified as Hydrologic Group 'B'.

#### FLOODPLAIN STATEMENT

A small portion of the developed site is located within a designated FEMA 100-year floodplain according to the information published in the Federal Emergency Management Agency Flood Plain Map No. 08041CO754F, dated March 17, 1997, and LOMR 05-08-0368P dated May 23, 2007. This area falls within the existing concrete channel.

#### METHOD OF COMPUTATION

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual, Volumes 1*, dated May 2014. The Rational Method for computation of runoff was used for determining Sub-Basin flows.

Q = cia

Where

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration

required for the runoff to become established

a = drainage basin size in acres

#### **EXISTING DRAINAGE CONDITIONS**

The existing site has been overlot graded and is covered with rangeland grasses. The western portion of the site drains in a southerly direction toward the existing 4' x 4' box culvert under U.S. Hwy 24. The eastern portion of the site drains westerly toward the 4' x 4' box culvert. An existing concrete channel is located on the east side of the lot, but no flows from this parcel drain to the concrete channel. A portion of the concrete channel has failed with other portions showing signs of joint failure.

The existing sub-basin AEX produces flows of 0.8 cfs for the 5-year storm and 6.3 cfs for the 100-year storm.

These values do not match what is shown in the existing drainage map. Please confirm which is correct.

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#### **DEVELOPED DRAINAGE CONDITIONS**

The developed site will be divided into three (3) lots. Lots 1 and 2 will encompass 1.003 acres and 1.008 acres respectively and Lot 3 will encompass 2.655 acres. The proposed land is zoned I-2 (Limited Industrial). Drainage from each lot will be self-contained with flows intercepted by swales along the property lines and directed into proposed Type C inlets and transported to a proposed extended detention basin (EDB) facility in the southwest corner of Lot 3 through a private storm sewer

Lot 1, Sub-basin A1, is located in the northern portion of the site. Sub-basin A1 will produce flows of 1.6 cfs for the 5-year storm and 3.6 cfs for the 100-year storm. These flows will continue south and be intercepted by a proposed swale located along the southerly property line. The flows will then travel west to a proposed type 'C' inlet at the southwest corner of the lot. An 18" HDPE storm sewer will transport these flows through Lot 2.

#### southerly

Lot 2, Sub-basin A2, is located in the center of the site. Sub-basin A2 will produce flows of 1.6 cfs for the 5-year storm and 3.6 cfs for the 100-year storm. As with Lot 1 the site flows will be intercepted by a swale located along the property line. These flows will be intercepted by a type 'C' inlet at the southwest corner of the lot. These flows will combine with the flows from Sub-basin A1 at DP1 to produce flows of 3.2 cfs for the 5-year storm and 7.1 cfs for the 100-year storm. An 18" HDPE storm sewer will transport these flows into the proposed EDB in Lot 3.

Lot 3, Sub-basin A3, is located in the southern portion of the site. Sub-basin A3 will produce flows of 3.6 cfs and 7.9 cfs respectively. These flows will be intercepted by a proposed swale located along the south property line and into the proposed EDB. The combined flows into the basin at DP2 will be 6.4 cfs for the 5-year storm and 14.0 cfs for the 100-year storm.

The proposed 0.656 ac.ft. Private EDB will reduce the site flows into the existing 4' x 4' box culvert to 3.9 cfs for the 5-year storm and 5.3 cfs for the 100-year storm at DP3.

#### **CONCRETE CHANNEL REPAIR**

Approximately 120 If of the existing concrete channel will need to be removed and replaced. The channel section is 6 feet wide and 7 feet deep. The new concrete channel section will be doweled into the concrete channel sections which remain.

#### WATER QUALITY AND DETENTION

Water quality for the site will be achieved within by 0.118 acre-feet of storage, 1.85 ft deep within the 0.656 ac. ft. private extended detention basin (EDB)which will be maintained by the owner of Lot 3. The remainder of the basin will provide the storage volume required for detention. The facility will have an 18" RCP outlet pipe with a 12" restrictor plate located 6.5"above the pipe invert.

#### PRIVATE DRAINAGE FACILITIES

Item	Unit	Quantity	<b>Unit Cost</b>	Total Cost
18" HDPE FES	EA	1	\$450	\$ 450.00
18" HDPE	LF	346	\$45	\$ 15,570.00
Outlet Structure	EA	1	\$5,000	\$ 5,000.00
Emergency Spillway	EA	1	\$1,500	\$ 1,500.00
Type 'C' Inlet	EA	2	\$3,270	\$ 6,540.00
Concrete Channel	LF	120	\$150	\$18,000.00
Concrete Forebay	SF	102	\$10	\$ 1,020.00

please state who owns and maintains the concrete channel, and confirm that you have an easement to work on the entire width of the channel.

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Concrete Trickle Channel	LF	24	\$25	\$ 600.00
18" RCP FES	EA	1	\$500	\$ 500.00
18" RCP	LF	50	\$50	<u>\$ 2,500.00</u>
			Sub-Total	\$51,680.00
		15% Cont	tingency & Engineering	<u>\$ 7,752.00</u>
			TOTAL	\$59,432.00

#### **DRAINAGE BASIN FEES**

Based on a resolution, No. 16-336, passed by the Board of County Commissioners on September 29, 2016, drainage and bridge fees will only be assessed on the two (2) smaller lots in the replat. The area of the two (2) smaller lots is 2.011 acres.

The proposed development is located within the Sand Creek drainage basin. The 2018 drainage basin fee calculation is as follows:

Impervious Coverage	=	73.6%
Area Subject to Fee	=	0.736 x 2.011 acres = 1.480 acre
Sand Creek Basin Fee	=	\$17,197/acre
Drainage Basin Fee	=	\$17,197 x 1.480 = \$25,452
Sand Creek Bridge Fee	=	\$5,210
Bridge Fee	=	\$5,210 x 1.480 = \$7,711

#### CONCLUSION

The proposed development and subsequent lot developments follow the "Four Step Process" as mandated by the EPA as follows:

#### Step 1: Employ runoff reduction practices

Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

#### Step 2: Stabilize drainageways

All drainageways, ditches and channels have been stabilized by the following methods:

- Tributaries have been left in their relatively natural state where possible.
- New drainageways and swales have been stabilized with either riprap or erosion control fabric depending on the erosion potential.
- No new roadside ditches are proposed for the development.

#### Step 3: Provide water quality capture volume (WQCV)

The proposed development will disturb approximately 4.5 acres, although the initial disturbance will only be 0.7 acres.

#### Step 4: Consider need for industrial and commercial BMP's.

The development of this project will not affect sensitive waters.

The development of this site will have little impact on downstream properties once the EDB is constructed.

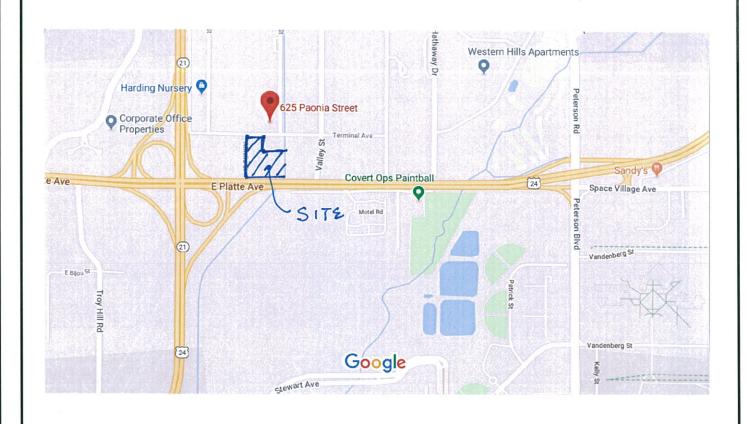
Elaborate further on how you are eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils. How are the impervious areas disconnected?

#### REFERENCES

- City of Colorado Springs and El Paso County (1994). Drainage Criteria Manual Volume 1 (DCM).
- 2. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume II* (DCM).
- 3. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
- 4. El Paso County (January 2006) Engineering Criteria Manual.
- 5. Urban Drainage and Flood Control District (June 2011). *Urban Storm Drainage Criteria Manual, Volume 1-3*.
- 6. Sand Creek Drainage Basin Planning Study (DBPS).
- 7. Preliminary/Final Drainage Plan and Report for the Appaloosa Hwy 24 Subdivision by Oliver E. Watts, Consulting Engineer, dated November, 2000.
- 8. Resolution No. 16-336. Board of County Commissioners, County of El Paso, State of Colorado.

## APPENDIX A

**MAPS** 





VICINITY MAP



3520 Austin Bluffs Pkwy, Suite 102 Colorado Springs, CO 80918 (719) 266-5212 fax: (719) 266-5341

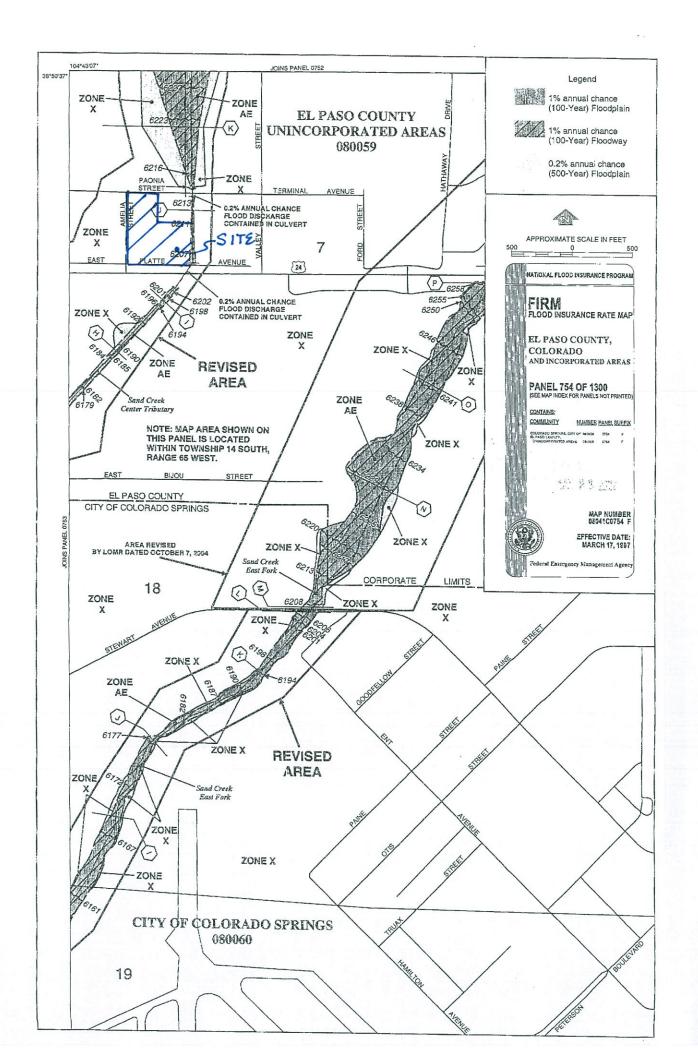




 $\frac{\text{SOILS MAP}}{\text{\tiny N.T.S.}}$ 



3520 Austin Bluffs Pkwy, Suite 102 Colorado Springs, CO 80918 (719) 266-5212 fax: (719) 266-5341



# APPENDIX B DESIGN CALCULATIONS

Maximum length of overland flow for urban areas is 100 feet.

be longer than calculated given the information provided.

Travel times appear to

APPALOOSA SUBDIVISION	BDIVISION											_				_					
PROJ. #160504																					
DRAINAGE CALCULATION SHEET	CULATION	SHEET														+					
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09/19/18																					
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000000000000000000000000000000000000000		3							Ħ	20.8 cfs		Ö	0.02 X 14.0 = 0.28 CFS	= 0.28 CF	S						
				Imperious	mperious Area Description	ription						3	W =0/(D^1.5XC)	exc)							
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		-	1						S = 1.5%	.5											
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A2	1.01	0.17	0.04			$\mid$	3		$Q \max = 15.0$	15.0 cfs	S.										
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									College	6.40	14.00	1.00	10.01	4.1	0.50	2.20	0.57	10.03	0.03 Use 6" Rock		
					1	- 			Chambre 1	- 1	22.7	١.	22.5								

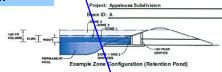
These values appear to be low for a Light Industrial use. Be advised, future site development plan applications will be limited to these values for percent impervious and weighted C values or the detention pond may need to be retro-fitted.

This value does not match the total site impervious percentage on the previous sheet. Revise to match.

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

Stage - Storage Description



danca tolalis oncasiron			
Selected BMP Type =	EDB	3	
Watershed Area =	4.58	acres	
Watershed Length =	550	ft	
Watershed Slope =	2 2	ft/ft	
Watershed Imperviousness =	76.70%	percent	
Percentage Hydrologic Soil Group A =	0.0%	percent	
Percentage Hydrologic Soil Group B =	100.0%	percent	
Percentage Hydrologic Soil Groups C/D =	0.0%	percent	
Desired WQCV Drain Time =	40.0	hours	
Location for 1-hr Rainfall Depths =	Denver - Cap	itol Building	
Water Quality Capture Volume (WQCV) =	0.118	acre-feet	Option
Excess Urban Runoff Volume (EURV) =	0.389	acre-feet	1-hr Pr
2-yr Runoff Volume (P1 = 1.19 in.) =	0.327	acre-feet	1
5-yr Runoff Volume (P1 = 1.5 in.) =	0.431	acre-feet	1
10-yr Runoff Volume (P1 = 1.75 in.) =	0.538	acre-feet	1
25-yr Runoff Volume (P1 = 2 in.) =	0.662	acre-feet	2
50-yr Runoff Volume (P1 = 2.25 in.) =	0.757	acre-feet	2
100-yr Runoff Volume (P1 = 2.52 in.) =	0.880	acre-feet	2
500-yr Runoff Volume (P1 = 3.01 in.) =	1.098	acre-feet	3
Approximate 2-yr Detention Volume =	0.307	acre-feet	
Approximate 5-yr Detention Volume =	0.405	acre-feet	
Approximate 10-yr Detention Volume =	0.506	acre-feet	
Approximate 25-yr Detention Volume =	0.542	acre-feet	

-hr Precipit	ation
1.19	inche
1.50	inche
1.75	inche
2.00	inche
2.25	inche
2.52	inche
3.01	inche

#### Stage-Storage Calculation

ac	0.118	Zone 1 Volume (WQCV) =
ac	0.271	Zone 2 Volume (EURV - Zone 1) =
ac	0.267	Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =
ac	0.656	Total Detention Basin Volume =
ft*	0	Initial Surcharge Volume (ISV) =
ft	0.33	Initial Surcharge Depth (ISD) =
ft	5.00	Total Available Detention Depth (H <sub>total</sub> ) =
ft	0.50	Depth of Trickle Channel (H <sub>TC</sub> ) =
ft/f	0.001	Slope of Trickle Channel (S <sub>TC</sub> ) =
H:	3	Slopes of Main Basin Sides (Smain) =
	2	Basin Length-to-Width Ratio (R <sub>LW</sub> ) =

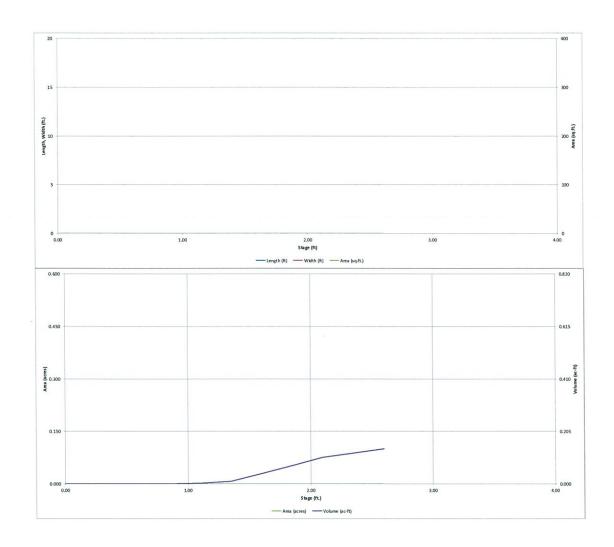
R*2	0	Initial Surcharge Area (A <sub>sv</sub> ) =
ft	0.3	Surcharge Volume Length (L <sub>SV</sub> ) =
ft	0.3	Surcharge Volume Width (Wsv) =
ft	0.10	Depth of Basin Floor (H <sub>FLOOR</sub> ) =
ft	99.9	Length of Basin Floor (L <sub>FLOOR</sub> ) =
ft	50.0	Width of Basin Floor (W <sub>FLOOR</sub> ) =
ft*2	4,997	Area of Basin Floor (A <sub>FLOOR</sub> ) =
ft*3	166	Volume of Basin Floor (V <sub>FLOOR</sub> ) =
ft	4.07	Depth of Main Basin (H <sub>MAIN</sub> ) =
ft	124.4	Length of Main Basin (L <sub>MAIN</sub> ) =
ft	74.4	Width of Main Basin (W <sub>MAIN</sub> ) =
ft^2	9,256	Area of Main Basin (A <sub>MAIN</sub> ) =
ft*3	28,568	Volume of Main Basin (V <sub>MAIN</sub> ) =
acre-	0.660	Calculated Total Basin Volume (V <sub>total</sub> ) =

Description	00	Statute (III)	(10)	(n)	(8.5)	Avea (It Z)	(acre)	(8.9)	(BC-R)
Top of Micropool	0.00					STREET, SE		STOREGE	
ISV	0.33	Sur annue				SACHES		0	0.000
	0.50								
	0.50	ESC. 1981				F-2-3/5		0	0.000
	0.75	A SALES						0	0.000
Floor	0.93	HAM BEEN				55.70		124	0.003
	1.00	Bronston				UNIXATED SE		471	0.011
	1.25	WELVEST !				September 1		1,762	0.040
	1.50					THE OWNER OF		3,111	0.071
	1.75							4,519	0.104
Zone 1 (WQCV)	1.86	0.74000000							_
Zone 1 (WCCV)		274120000				1000000		5,216	0.120
	2.00	250.000						5,987	0.137
	2.25	MATERIAL STATES				4 10 10 10 10 10 10 10 10 10 10 10 10 10		7,578	0.174
	2.50	PARTIES.				196912		9,171	0.211
	2.75	W/Constitution	110.9	60.9	6,754	tromp28	0.155	10,828	0.249
	3.00	LOS MAGA	112.4	62.4	7,014	Part of the Part	0.161	12,549	0.288
	3.25	865656b	113.9	63.9	7,279	C SERVICENSES	0.167	14,335	0.329
	3.50	1125-1164-0C11	115.4	65.4	7,548		0.173	16,189	0.372
Zone 2 (EURV)	3.61	100000000000000000000000000000000000000	116.0	66.1	7,668		0.176	17,026	0.391
ZDINE Z (LOKY)	3.75	100000000000000000000000000000000000000	-						_
			116.9	66.9	7,821		0.180	18,110	0.416
	4.00	170/1006	118.4	68.4	8,099	100-00-00-00-00-00-00-00-00-00-00-00-00-	0.186	20,100	0.461
	4.25	Serie Piece	119.9	9.99	8,382	THE STATE OF	0.192	22,160	0.506
	4.50	1927.00	121.4	71.4	8,669	SAVABLE S	0.199	24,291	0.558
	4.75	E6463954	122.9	72.9	8,960	7000000	0.206	26,494	0.608
Z3 (100+1/2WQCV)	5.00	10 33 33 3	124.4	74.4	9,256	10000	0.212	28,771	0.660
Z3 (100+1/2WQCV)	5.25	Townson.	125.9	75.9	9,556		0.219	31,123	0.714
	5.50	Calculation	127.4	77.4	9,861		0.216	33,550	0.770
		2000		2000	8.548.55	E HIELDS			_
	5.75	37402530	128.9	78.9	10,171		0.233	36,054	0.826
	6.00		130.4	80.4	10,485	THE PERSON	0.241	38,636	0.887
	6.25	1511000000	131.9	81.9	10,803	THE WAY	0.248	41,296	0.948
	6.50	STEEL STEEL	133.4	83.4	11,126	ALCOHOL: N	0.255	44,038	1.011
	6.75	Market St.	134.9	84.9	11,453	The second	0.263	46,860	1.076
	7.00	Jan Committee	136.4	86.4	11,785	Name and Address of the Owner, when the Owner, when the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, which	0.271	49,765	1,142
	7.25	San Carlotte	137.9	87.9	12,122		0.278	52,753	1.211
	7.50	100000000000000000000000000000000000000	139.4	89.4	12,463	PROCESS OF THE PARTY OF THE PAR	0.286	55,826	1.282
	7.75								
		File Control	140.9	90.9	12,808	0000000	0.294	58,985	1.35
	8.00		142.4	92.4	13,158		0.302	62,230	1.429
	8.25		143.9	93.9	13,513		0.310	65,564	1.50
	8.50	NAME OF STREET	145.4	95.4	13,872		0.318	68,987	1.584
	8.75	120-85	146.9	96.9	14,235	ALC: NO.	0.327	72,500	1.664
	9.00		148.4	98.4	14,603	2500000	0.335	76,105	1.74
	9.25	19 to 18 to 18	149.9	99.9	14,975	- CONTRACTOR	0.344	79,802	1.832
	9.50		151.4	101.4	15,352	101 P 10 P 100	0.352	83,593	1.919
	9.50		152.9						
		2011		102.9	15,734		0.361	87,479	2.000
	10.00	Sept. 198	154.4	104.4	16,120		0.370	91,460	2.100
	10.25	STEEL 28	155.9	105.9	16,510	-	0.379	95,539	2.193
	10.50	EVERTER C	157.4	107.4	16,905	HOLES	0.388	99,716	2.28
	10.75	17 (2.17)	158.9	108.9	17,305	1500000	0.397	103,992	2.38
	11.00		160.4	110.4	17,708		0.407	108,368	2.48
	11.25	0.00	161.9	111.9	18,117		0.416	112,847	2.50
	11.50		163.4						_
		Sent to the		113.4	18,530	Part of the last	0.425	117,427	2.69
	11.75		164.9	114.9	18,947		0.435	122,112	2.80
	12.00		166.4	116.4	19,369	THE SECOND	0.445	126,901	2.91
	12.25	100000000000000000000000000000000000000	167.9	117.9	19,796		0.454	131,797	3.02
	12.50		169.4	119.4	20,227	The collect	0.464	136,799	3.14
	12.75	7.000	170.9	120.9	20,662	102764107	0.474	141,910	3.25
	13.25		173.9	123.9	21,102	1912000	0.484	152,462	3.50
		The second second	175.4	125.4	21,995	ATT STREET	0.505	157,904	3.62
	13.50			126.9	22,449	Service Villa	0.515	163,460	3.75
	13.75	ALVALES CAN	176.9						
	13.75 14.00	STATE OF STA	178.4	128.4	22,907	350 FEE	0.526	169,129	
	13.75 14.00 14.25		178.4 179.9	128.4 129.9	23,369		0.536	169,129 174,914	4.01
	13.75 14.00 14.25 14.50		178.4 179.9 181.4	128.4 129.9 131.4	23,369 23,836		0.536 0.547	169,129 174,914 180,814	4.01
	13.75 14.00 14.25		178.4 179.9	128.4 129.9	23,369		0.536	169,129 174,914	4.01 4.15 4.28
	13.75 14.00 14.25 14.50 14.75		178.4 179.9 181.4 182.9	128.4 129.9 131.4 132.9	23,369 23,836 24,308		0.536 0.547 0.558	169,129 174,914 180,814 186,832	3.88 4.01 4.15 4.28 4.43

Input the optional override date for the stage and area so that the design volume will meet the minimum requirements.

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

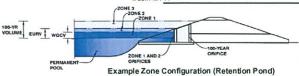
UD-Detention, Version 3.07 (February 2017)



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Basin ID: A



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.85	0.118	Orifice Plate
Zone 2 (EURV)	3.60	0.271	Orifice Plate
(100+1/2WQCV)	4.98	0.267	Weir&Pipe (Restrict)
A CONTRACTOR OF THE PARTY OF TH		0.656	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

Calculated Pa	arameters fo	r Underdrair
Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to
Depth at top of Zone using Orifice Plate = 1.50 ft (relative to
Orifice Plate: Orifice Vertical Spacing = 6.00 inches
Orifice Plate: Orifice Area per Row = 0.31 sq. inches (dia

ft (relative to basin bottom at Stage = 0 ft) ft (relative to basin bottom at Stage = 0 ft) inches sq. inches (diameter = 5/8 inch)

Calculat	ed Parameters	for Plate
VQ Orifice Area per Row =	2.153E-03	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.50	1.00					
Orifice Area (sq. inches)	0.31	0.31	0.31					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		Sell selles selle						
Orifice Area (sq. inches)	Section 1	<b>经过多过度</b>					NEW YORK BUILDING	THE REAL PROPERTY.

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated P	arameters for Vert	tical Orifice	
	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	N/A	N/A	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

ft (relative to basin bottom at Stage = 0 ft)
feet
H:V (enter zero for flat grate)
feet
%, grate open area/total area

Calculated Parameters for Overflow Weir Zone 3 Weir Height of Grate Upper Edge, H<sub>t</sub> Over Flow Weir Slope Length : 2.00 N/A feet Grate Open Area / 100-yr Orifice Area 4.87 N/A should be ≥ 4 Overflow Grate Open Area w/o Debris : 2.80 N/A Overflow Grate Open Area w/ Debris = 1.40 N/A

ser Input: Outlet Pine w / Flow Restriction Plate (Circular Oritice, Restrictor Plate or Rectang

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.00	N/A
Outlet Pipe Diameter =	18.00	N/A
Restrictor Plate Height Above Pipe Invert =	6.50	

Revise these values to match the design in the design in the design in vise incurrence.

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.58	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.32	N/A	feet
estrictor Plate on Pipe =	1.29	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= 5.00 ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = 5.00 feet
Spillway End Slopes = 4.00 H:V
Freeboard above Max Water Surface = 1.00 feet

 Calculated Parameters for Spillway

 Spillway Design Flow Depth=
 0.76
 feet

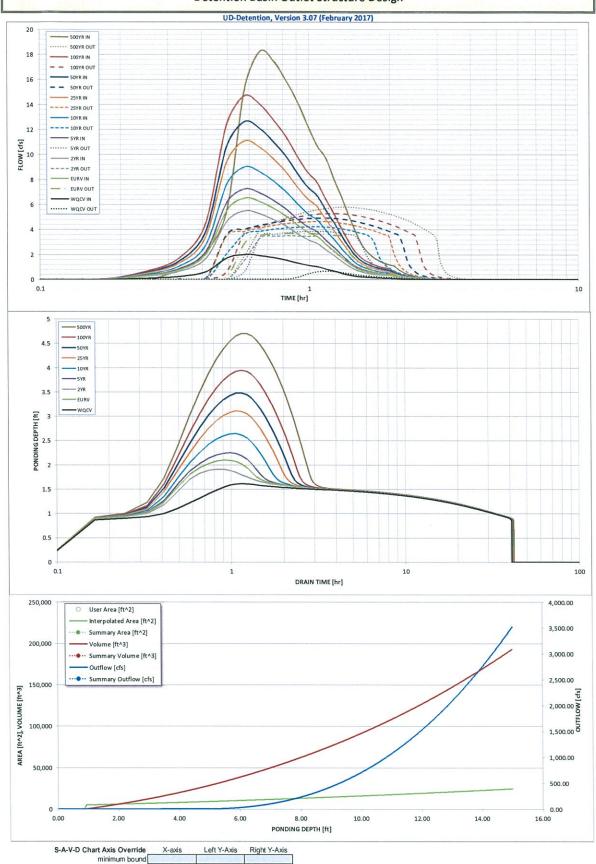
 Stage at Top of Freeboard =
 6.76
 feet

 Basin Area at Top of Freeboard =
 0.26
 acres

Routed Hydrograph Results

Mouted Hydrograph Mesuits_									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.01
Calculated Runoff Volume (acre-ft) =	0.118	0.389	0.327	0.431	0.538	0.662	0.757	0.880	1.098
OPTIONAL Override Runoff Volume (acre-ft) =								an algebraiche	H CHICAGO HAND SA
Inflow Hydrograph Volume (acre-ft) =	0.118	0.388	0.326	0.431	0.537	0.662	0.756	0.879	1.097
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.02	0.20	0.67	0.93	1.25	1.77
Predevelopment Peak Q (cfs) =	0.0	0.0	0.1	0.1	0.9	3.1	4.3	5.7	8.1
Peak Inflow Q (cfs) =	2.0	6.5	5.5	7.3	9.0	11.1	12.6	14.7	18.2
Peak Outflow Q (cfs) =	0.7	3.7	3.5	3.8	4.2	4.6	4.9	5.3	5.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	39.8	4.5	1.5	1.2	0.9	0.7
Structure Controlling Flow =	Overflow Grate 1	Outlet Plate 1							
Max Velocity through Grate 1 (fps) =	0.19	1.31	1.23	1.4	1.5	1.6	1.7	1.9	2.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	33	34	32	30	28	27	25	22
Time to Drain 99% of Inflow Volume (hours) =	40	38	39	38	38	37	36	36	34
Maximum Ponding Depth (ft) =	1.61	2.10	1.91	2.25	2.64	3.11	3.48	3.94	4.70
Area at Maximum Ponding Depth (acres) =		0.14	0.14	0.14	0.15	0.16	0.17	0.18	0.20
Maximum Volume Stored (acre-ft) =		0.151	0.127	0.173	0.232	0.304	0.366	0.450	0.598

Must release at or below the predeveloped rate. Revise.



maximum bound

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

_	The aser carro	verride the calcu	lated inflow riyul	ograpis nom ti	IIS WOINDOON WIL	ir ir ii iow riyarogi	apris developed	in a separate pit	yram.	
	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK
ime Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.96 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4.90 11111	0:04:58	Say Individual	water in the second of the sec	SWATTENSKATTENSKAT	AND PROPERTY AND ADDRESS.	Editor Distriction in the	CONTRACTION OF THE PARTY OF THE	ALIPATINA MARCONIES	DESCRIPTION OF PERSONS ASSESSED.	Date by the second second
Luderman	0:09:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Hydrograph Constant	0:09:53	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1.008	0:19:50	0.09	0.29	0.25	0.32	0.40	0.49	0.56 1.50	0.65 1.74	0.80 2.16
1.006	0:24:48	0.63	2.01	0.66 1.70	2.23	1.08 2.77	1.32 3.39	3.86	4.48	5.55
ŀ	0:29:46	1.73	5.54	4.68	6.14	7.61	9.32	10.62	12.31	15.26
ł	0:34:43	2.01	6.53	5.50	7.25	9.02	11.07	12.63	14.67	18.25
1	0:39:41	1.91	6.22	5.24	6.91	8.60	10.57	12.06	14.01	17.44
ŀ	0:44:38	1.74	5.66	4.77	6.29	7.83	9.62	10.98	12.76	15.88
	0:49:36	1.54	5.04	4.24	5.61	6.98	8.59	9.81	11.41	14.22
	0:54:34	1.31	4.34	3.65	4.83	6.02	7.42	8.48	9.87	12.32
	0:59:31	1.15	3.79	3.19	4.21	5.25	6.46	7.39	8.59	10.71
	1:04:29	1.04	3.43	2.88	3.81	4.76	5.86	6.69	7.79	9.71
İ	1:09:26	0.84	2.81	2.36	3.13	3.92	4.83	5.53	6.45	8.06
	1:14:24	0.67	2.29	1.92	2.55	3.19	3.95	4.52	5.28	6.61
	1:19:22	0.50	1.75	1.46	1.95	2.45	3.04	3.49	4.09	5.13
	1:24:19	0.36	1.29	1.07	1.44	1.82	2.27	2.61	3.06	3.86
	1:29:17	0.27	0.94	0.78	1.05	1.32	1.64	1.89	2.21	2.80
	1:34:14	0.21	0.73	0.61	0.82	1.03	1.27	1.46	1.70	2.15
	1:39:12	0.17	0.60	0.50	0.67	0.84	1.05	1.20	1.40	1.77
	1:44:10	0.15	0.51	0.43	0.57	0.72	0.89	1.02	1.19	1.50
	1:49:07	0.13	0.45	0.38	0.50	0.63	0.78	0.89	1.04	1.31
	1:54:05	0.12	0.41	0.34	0.45	0.57	0.70	0.80	0.94	1.18
	1:59:02	0.11	0.38	0.32	0.42	0.52	0.65	0.74	0.86	1.08
	2:04:00	0.08	0.28	0.23	0.31	0.38	0.47	0.54	0.63	0.80
	2:08:58	0.06	0.20	0.17	0.23	0.28	0.35	0.40	0.47	0.58
	2:13:55	0.04	0.15	0.12	0.16	0.21	0.26	0.29	0.34	0.43
	2:18:53	0.03	0.11	0.09	0.12	0.15	0.19	0.22	0.25	0.32
	2:23:50	0.02	0.08	0.06	0.09	0.11	0.13	0.15	0.18	0.23
	2:28:48	0.02	0.05	0.05	0.06	0.08	0.10	0.11	0.13	0.16
	2:33:46	0.01	0.04	0.03	0.04	0.05	0.07	0.08	0.09	0.12
()	2:38:43	0.01	0.02	0.02	0.03	0.04	0.04	0.05	0.06	0.08
	2:43:41	0.00	0.01	0.01	0.02	0.02	0.03	0.03	0.04	0.05
	2:48:38	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02
	2:53:36 2:58:34	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.01	0.01
	3:03:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:08:29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:13:26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:18:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:23:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:28:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:33:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:38:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:43:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:48:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:53:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:58:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:03:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:08:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:12:58	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0,00
	4:17:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:22:53 4:27:50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:32:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:37:46	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:42:43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:47:41 4:52:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:57:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:02:34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:07:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:12:29	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:17:26 5:22:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:27:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:32:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:37:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:42:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0,00
		100000000000000000000000000000000000000								
	5:47:12 5:52:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

UD-Detention, Version 3.07 (February 2017)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor)
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of all
	THE REST						outlets (e.g. vertical orifice,
	ADVENIENCE:						overflow grate, and spillway,
							where applicable).
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## APPENDIX C

## **DESIGN CHARTS**

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

and Use or Surface	Percent						Runoff Co	efficients						
haracteristics	impervious	2-year		5-y	5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	ISG ALB	HSG C&D	HSG A&B	HSG C&D	HIGALB	HSG C&D	HSG A&B	HSG C&D	
Business						<u> </u>								
Commercial Areas	95	0.79	0.80	0.81	0,82	0,83	0.84	0.85	0.87	0.87	0.88	0.88	0.89	
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0,62	0,60	0.65	0.62	0.68	
Residential		<del>                                     </del>	l				<u> </u>		İ	<b></b>			ļ	
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65	
1/4Acre	40	0.23	0,28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0,54	0.50	0.58	
1/3 Acre	80	0.18	0.22	0,25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57	
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.35	0.37	0,46	0.41	0.51	0.46	0.56	
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0,35	0.44	0,40	0.50	0.44	0.55	
Industrial	<del> </del>		<u> </u>	<u> </u>									-	
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.58	0.72	0.70	0,74	
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83	
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52	
Playgrounds	13	0.07	0.13	0,16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54	
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0,42	0.42	0.50	0,46	0.54	0.50	0.58	
Undeveloped Areas	1	+		+	<del> </del>		+	+	1					
Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51	
Pasture/Meadow	0	0.02	0.04	0,08	0,15	0.15	0.25	0.25	0,37	0.30	0.44	0.35	0.50	
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50	
Exposed Rock	100	0.89	0.89	0,90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.98	
Offsite Flow Analysis (when landuse is undefined)	45	0,26	0.31	0.32	0.37	0.38	0,44	0.44	0.51	0.48	0,55	0.51	0.59	
Streets	-	-	+	-					-		+	+-	+	
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.95	0.9	
Grave1	80	0.57	0,60	0.59	0,63	0,63	0.65	0.66	0.70	0.68	0.72	0.70	0.7	
Drive and Walks	100	0.89	0.89	0.90	0,90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.9	
Roofs	90	0.71	0.73			0.75	0.77	0.78	0.80	0.80	0.82	0.83	0.8	
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0,5	

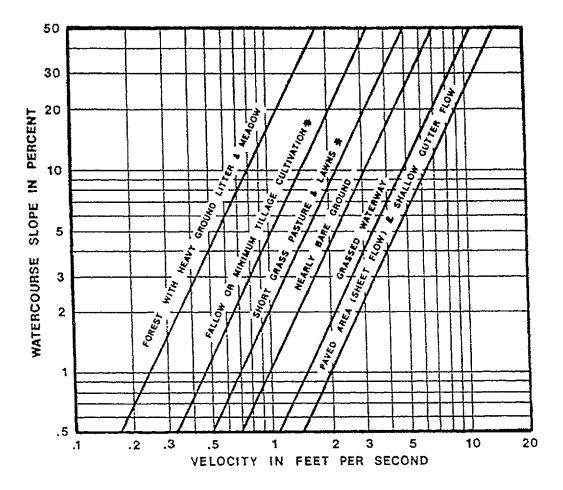


Figure 6-25. Estimate of Average Concentrated Shallow Flow

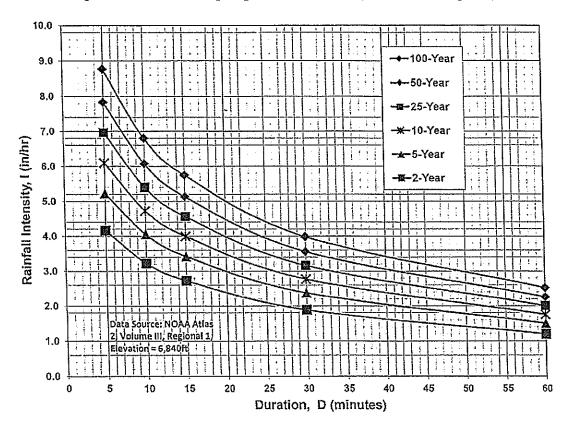


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

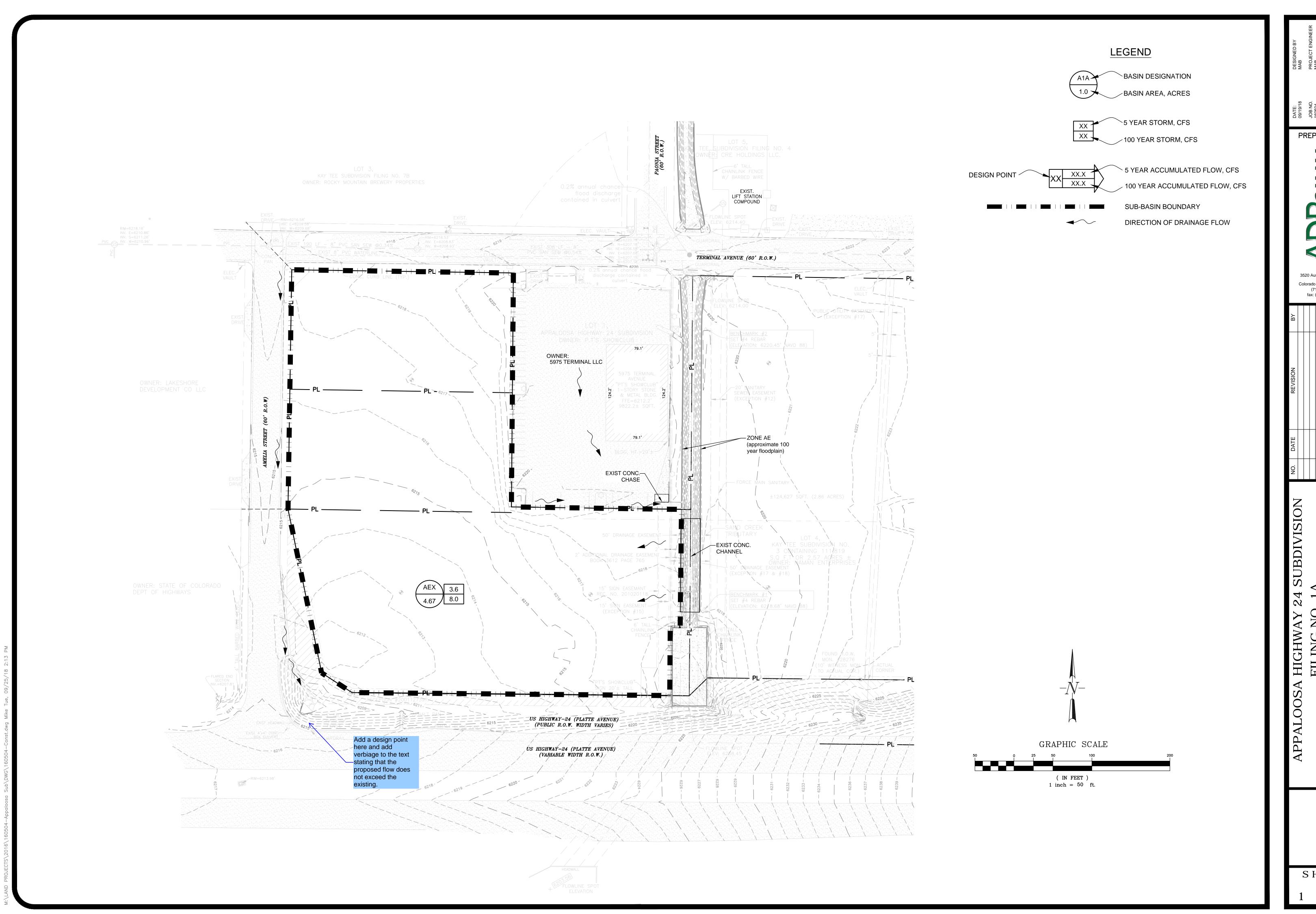
$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

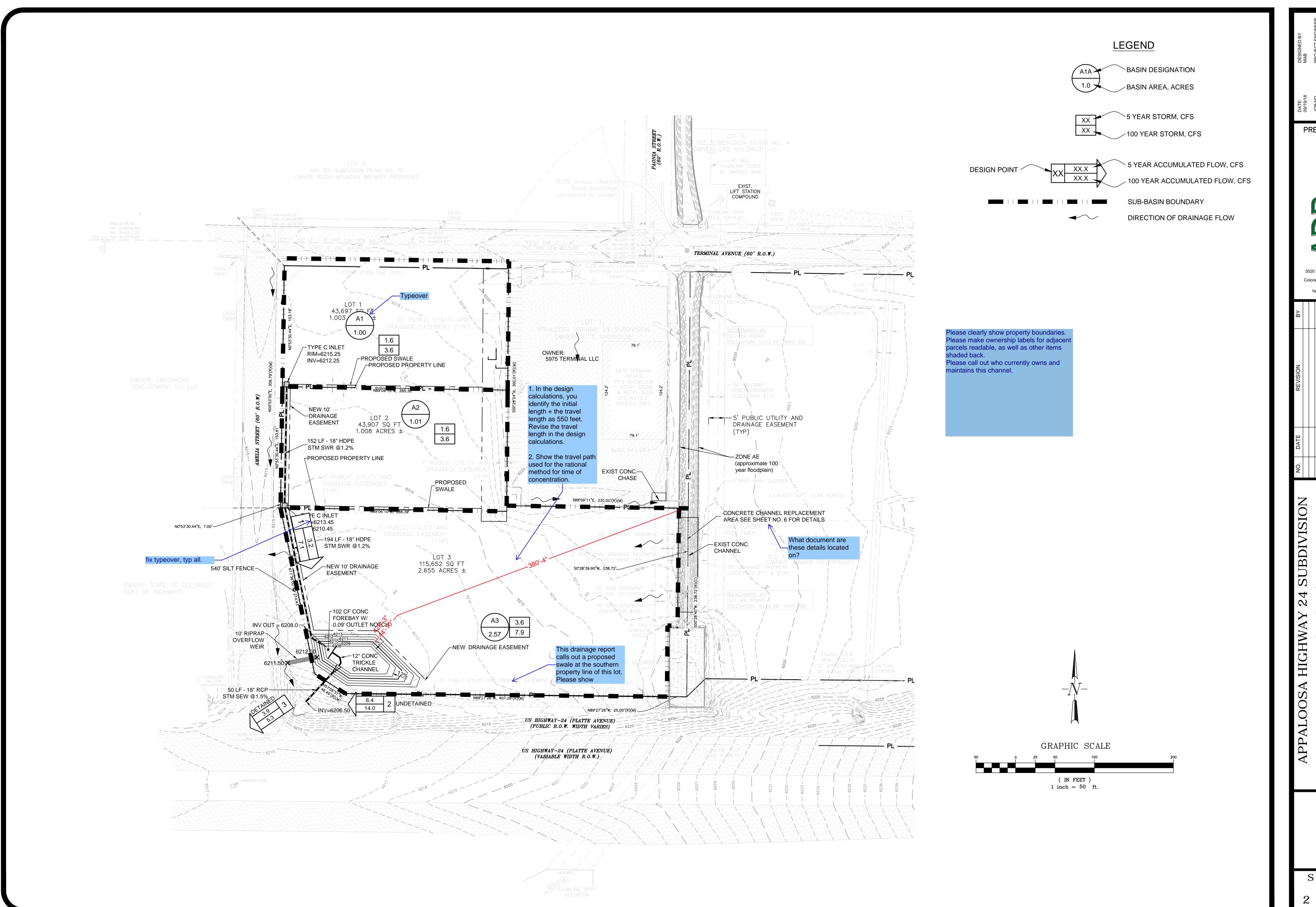
$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.



PREPARED BY: UTURE 3520 Austin Bluffs Parkway Suite 102 Colorado Springs, CO 80918 (719) 266-5212 fax: (719) 266-5341

SHEET



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FILING NO. 1A
COLORADO SPRINGS, COLORADO
PROPOSED DRAINAGE PLAN

SHEET

2 of 2

## Markup Summary

#### dsdgrimm (20)

works along the requiry lives and directed into perpendic elevated determine based (CDD) facility in private atoms severe.

Let 1.50-based a. It is located in the northern pertite flower of 1.6 of fix the 5-year enterm and 5.6 of fix of continues only and the intervenity by appropried to the continues continued to the continues continues to the continues of the continues continues to the continues

Subject: Engineer Page Label: 4 Lock: Unlocked Author: dsdgrimm

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control tables depending on the retrosio potential.

Step 1. Problek share audits cause volume (WOCO)

The proposed development will disturb approximately of
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that the constructed.

It is constructed.

It is constructed.

It is constructed.

Subject: Engineer Page Label: 5 Lock: Unlocked Author: dsdgrimm

Date: 10/24/2018 2:07:55 PM

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Elaborate further on how you are eliminating "unnecessary" impervious areas and encouraging infiltration into

suitable soils. How are the impervious

areas disconnected?

southerly

Input the optional op

Subject: Engineer Page Label: 13 Lock: Unlocked Author: dsdgrimm

Date: 10/25/2018 12:10:31 PM

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Input the optional override date for the stage and area so that the design volume will meet the minimum requirements.

of the site drains in a southerty direction toward the existing  $4^*$  x  $4^*$  box culvert uny y2-8. The eastern portion of the site drains westerfy oward the  $4^*$  x  $4^*$  box culvert., concrete channel is located on the east side of the lot, but no flows from this parce the concrete channel. A portion of the concrete channel has failed with other porting signs of joint failure.

ing sub-hasin AEX produces flows of 0.8 cfs for the 5-year storm and 6.3 cfs for th storm.

These values do not match what is shown in the existing dariange may Please confirm which is correct.

Subject: Engineer Page Label: 3 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 12:35:18 PM

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These values do not match what is shown in the existing drainage map. Please

confirm which is correct.



Subject: Engineer Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 2:34:32 PM

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This drainage report calls out a proposed swale at the southern property line of this

lot. Please show



Subject: Engineer Page Label: 4 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 4:29:57 PM

Color:

please state who owns and maintains the concrete channel, and confirm that you have an easement to work on the entire

width of the channel.



Subject: Engineer Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 4:38:37 PM

Color:

What document are these details located

on?



Subject: Engineer Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 4:39:30 PM

Color:

Please clearly show property boundaries. Please make ownership labels for adjacent parcels readable, as well as other items shaded back.

Please call out who currently owns and

maintains this channel.

ADP Project No. 16

Subject: Engineer Page Label: 1 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 5:20:07 PM

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Please state when improvements will be completed and who will maintain all drainage and WQ structures, please include who currently and in the future is responsible to maintain the concrete

channel.



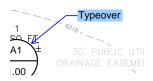
Subject: Engineer Page Label: 23 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 5:34:17 PM

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Add a design point here and add verbiage to the text stating that the proposed flow

does not exceed the existing.



Subject: Engineer Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 10/31/2018 7:19:46 AM

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Typeover



Subject: Engineer Page Label: 12 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 7:50:41 AM

Color: ■

These values appear to be low for a Light Industrial use. Be advised, future site development plan applications will be limited to these values for percent impervious and weighted C values or the

detention pond may need to be

retro-fitted.



Subject: Engineer Page Label: 13 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 7:53:20 AM

Color:

This value does not match the total site impervious percentage on the previous

sheet. Revise to match.



Subject: Engineer Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 7:56:28 AM

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fix typeover, typ all.



Subject: Engineer Page Label: 12 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 8:01:57 AM

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Maximum length of overland flow for

urban areas is 100 feet.

The state of the s

Subject: Polylength Measurement

Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 8:08:52 AM

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425'-3"



Subject: Engineer Page Label: 12 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 8:14:29 AM

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Travel times appear to be longer than calculated given the information provided.



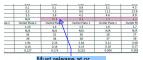
Subject: Group Page Label: 15 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 8:39:12 AM

Color:

Revise these values to match the design

in the GEC Plan or vise versa.



below the predeveloped rate.

Subject: Engineer Page Label: 15 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 8:47:10 AM

Color:

Must release at or below the predeveloped rate. Revise.



Subject: Engineer Page Label: 24 Lock: Unlocked Author: dsdgrimm

Date: 11/1/2018 8:58:19 AM

Color: ■

- 1. In the design calculations, you identify the initial length + the travel length as 550 feet. Revise the travel length in the design calculations.
- 2. Show the travel path used for the rational method for time of concentration.