



FINAL DRAINAGE REPORT

CONSTITUTION STORAGE DEVELOPMENT

El Paso County, Colorado

PREPARED FOR:

**Johnson Development Associates, Inc.
100 Dunbar Street, Suite 400
Spartanburg, SC 29306**

PREPARED BY:

**Galloway & Company, Inc.
1155 Kelly Johnson Blvd., Suite 305
Colorado Springs, CO 80920**

DATE:

July 8, 2022

PCD Filing No.: PPR-2224

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Brady A. Shyrock, PE #38164
For and on behalf of Galloway & Company, Inc.

Date

DEVELOPER'S CERTIFICATION

I, The developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By: _____

Date

Address: Johnson Development Associates, Inc.
101 N. Pacific Coast Hwy, Suite 308
El Segundo, CA 90245

EL PASO COUNTY CERTIFICATION

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer, P.E.
Interim County Engineer

Date

Conditions:

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I. Purpose

The purpose of this Final Drainage Report is to identify on and offsite drainage patterns, locate and identify tributary or downstream drainage features and facilities that impact the site, and to identify which types of drainage facilities will be needed and where they will be located. This report will remain in general compliance with the approved FDR prepared by Costin Engineering Company, dated February 2, 1983.

II. General Description

The project is a self-storage commercial development located in the Cimarron Hills area of El Paso County, Colorado. The site is located in a portion of Section 05, Township 14 South, Range 65 West of the 6th Principal Meridian, County of El Paso, State of Colorado. The subject property is bounded by Constitution Avenue to the north, Canada Drive to the east, Peterson Road to the west, and existing Northcrest Filing No. 3 residential development to the south. A Vicinity Map is included in **Appendix A**.

This final drainage report is the basis for the drainage facility design in conformance with the previously approved FDR for the site prepared by Costin Engineering Company, "*Amendment Number 1, Final Drainage Study, Cimarron Northcrest Filing No. 3*", Costin Engineering Company, February 1983 (**FDR**). The site consists of approximately 3.716 acres and includes 929 storage units.

The existing soil types within the proposed site as determined by the NRCS Web Soil Survey for El Paso County Area consist of Truckton Sandy Loam (hydrologic soil group A). See the soils map included in **Appendix A**.

III. Drainage Criteria

Hydrology calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.

The drainage calculations were based on the criteria manual Figure 6-5 and IDF equations to determine the intensity and are listed in Table 1 below.

Table 1 - Precipitation Data

Return Period	One Hour Depth (in.)	Intensity (in/hr)
5-year	1.50	5.17
100-year	2.52	8.68

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has been proven to be accurate for basins of this size and is based on the following formula:

$$Q = CIA$$

Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff intensity (inches/hour)

A = Drainage area (acres)

The runoff coefficients are calculated based on land use, percent imperviousness, and design storm for each basin, as shown in the drainage criteria manual (Table 6-6). Composite percent impervious and C values were calculated using the residential, streets, roofs, and lawns coefficients found in Table 6-6 of the manual.

The 100-year event was used as the major storm event. The 5-year event was used as the minor event. The UD-Inlets v5.01 spreadsheet was utilized for the sizing of the proposed sump inlets.

The UD-Detention v4.04 spreadsheet was utilized for the design of the proposed on-site water quality ponds, Ponds A, B, C, D, E.

IV. Existing Drainage Conditions

The site lies within the existing Sand Creek drainage basin (see Reference Map). Based on this report, existing topography, and proposed future developments, no off-site basins will impact the site.

Stormwater from this site generally drains to the southeast and southwest and will be routed to a single (1) private full spectrum detention facility designated as FSD-1 which has been sized to accommodate the developed flows from this site. The rational method was used to analyze the individual basins within the site because their size permits it.

The property presently discharges via sheet flow along the southern property line onto the adjacent Eight Line Inc. property and Alvarado property. Portions of the site along the eastern and western property lines also drain to the adjacent right-of-ways.

While the **FDR** shows a total of 26 basins that were analyzed as part of the overall Northcrest Filing No. 3 development, for the purposes of this report, only one (1) of the Basins within the FDR will be used for analysis. This Basin, C-4 (6.3 AC, $Q_5 = 7.0$ cfs, $Q_{100} = 18.30$ cfs) is located at the northwest corner of the approved FDR study area and drains through properties to the south to Allyn Way.

For a more in-depth analysis of existing tributary conditions as it pertains to this phase of development, an existing basin map has been prepared. The existing map can be found in **Appendix F** and basins are described below. The site has been divided into six (6) sub-basins to better show where runoff flows in the current conditions.

Basin EX-1 (0.05 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.1$ cfs): This basin encompasses a portion of the southwest of the site in the existing condition. This basin consists of un-developed land. Runoff from this basin will sheet flow to the south before outfalling onto the adjacent Eight Line Inc. property. **(DP 1)**.

Basin EX-2 (0.26 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.4$ cfs): This basin encompasses the southwest portion of the site in the existing condition. This basin consists of un-developed land. Runoff from this basin will sheet flow to the south before outfalling onto the adjacent Alvarado property. **(DP 2)**.

Basin EX-3 (0.39 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.7$ cfs): This basin encompasses the western portion of the site in the existing condition, as well as a portion of the Peterson Road right-of-way. This basin consists of un-developed land and a portion of existing sidewalk. Runoff from this basin will sheet flow to the southwest before outfalling into Peterson Road. **(DP 3)**.

Basin EX-4 (0.03 AC, $Q_5 = 0.1$ cfs, $Q_{100} = 0.2$ cfs): This basin encompasses a portion of the northwest of the site in the existing condition. This basin consists mostly of existing sidewalk. Runoff from this basin will sheet flow to the north before outfalling into Constitution Avenue. **(DP 4)**.

Basin EX-5 (2.69 AC, $Q_5 = 0.4$ cfs, $Q_{100} = 4.8$ cfs): This basin encompasses the majority of the site in the existing condition, as well as a portion of Constitution Avenue right-of-way that is currently undeveloped. This basin consists of un-developed land, access drive, and a single-family home. Runoff from this basin will sheet flow to the south before outfalling onto the adjacent Eight Line Inc. property. **(DP 5)**.

Basin EX-6 (0.36 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.5$ cfs): This basin encompasses the eastern portion of the site in the existing condition, as well as a portion of Constitution Avenue right-of-way that is currently undeveloped. This basin consists of un-developed land. Runoff from this basin will sheet flow to the southeast before outfalling into Canada Drive. **(DP 6)**.

V. Four Step Process

The Four Step Process is used to minimize the adverse impacts of urbanization and is a vital component of developing a balanced, sustainable project. Below identifies the approach to the four-step process:

1. Employ Runoff Reduction Practices

This step uses low impact development (LID) practices to reduce runoff at the source. Generally, rather than creating point discharges that are directly connected to impervious areas runoff is routed through pervious areas to promote infiltration. The Impervious Reduction Factor (IRF) method was used, and calculations can be found in **Appendix E**. For the majority of the site this is not practical, however portions of the site do drain through landscaped swales prior to entering the storm sewer system.

2. Stabilize Channels

This step implements stabilization to channels to accommodate developed flows while protecting infrastructure and controlling sediment loading from erosion in the drainageways. This project does not discharge to a channel. Flows are detained onsite to control release rates from the site down to existing rates and not adversely impact downstream facilities. The site is designed to release at or below the existing release rate for the site and will not negatively impact the downstream infrastructure.

3. Provide Water Quality Capture Volume (WQCV)

This step utilizes formalized water quality capture volume to slow the release of runoff from the site. The EURV volume will release in 72 hours, while the WQCV will release in no less than 12 hours because a sand filter is being utilized for water quality. An on-site water quality control volume detention pond will provide water quality treatment for all of the developed areas (utilizing a sand filter), prior to the runoff being released into existing curb flowlines at Canada Dr and Peterson Rd. Refer to WQCV Plan in **Appendix F**.

4. Consider Need for Industrial and Commercial BMPs

As this project is a commercial development, roof drains connecting directly to proposed water quality and detention facility, surface flows being routed to inlets that capture developed runoff and direct flows to proposed water quality and detention facility. Stockpile and concrete washout BMPs will be implemented onsite. At the Contractor's discretion, additional specialized BMPs which would be associated with an industrial or commercial site may be implemented.

VI. Proposed Drainage Conditions

The proposed development lies completely within the Sand Creek Drainage Basin and consists of eleven (11) sub-basins. Site runoff will be collected via sheet flows, roof drains, inlets & pipes and diverted to the one (1) proposed full spectrum detention pond (FSD-1). Within the pond, there will be a sand filter to infiltrate the water quality flows. All necessary calculations can be found within the appendices of this report.

According to the **FDR**, the proposed project site lies within Basin C-4 (6.3 AC, $Q_5 = 7.0$ cfs, $Q_{100} = 18.30$ cfs) is located at the northwest corner of the approved FDR study area. The property presently discharges via sheet flow along the southern property line onto the adjacent Eight Line Inc. property.

The site will provide one (1) Full Spectrum Sand Filter Basin (SFB). Ponds FSD-1 will discharge treated runoff at historic rates directly into the existing curb flowline at Canada Drive.

As has been mentioned previously, the site is proposed to have a land use of commercial self-storage. The site will consist of 929 storage units along with associated parking, drive aisles, RV storage, detention pond, and landscaping areas.

Basin PR-1 (0.24 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.3$ cfs): Located at the southwestern corner of the site, Basin PR-1 contains the proposed landscaping improvements immediately adjacent to the existing residential development (Northcrest Filing No. 3). Runoff from this basin will sheet flow to the existing southern boundary into the Alvarado property as it does in the existing condition (Basin EX-2) (**DP 1**).

Basin PR-2A (0.11 AC, $Q_5 = 0.1$ cfs, $Q_{100} = 0.3$ cfs): Located on the western boundary of the site, this basin consists of driveway and landscaping. Runoff from this basin will sheet flow from the driveway to proposed curb and gutter at the driveway and Peterson Rd. Flows will then be routed, via curb & gutter downstream to the existing curb & gutter at the southwestern corner of the project site (**DP 2A**).

Basin PR-2B (0.01 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.1$ cfs): Located on the northwestern corner of the site, this basin consists of sidewalk and landscaping. Runoff from this basin will sheet flow from the to existing curb and gutter at Peterson Rd. Flows will then be routed, via existing curb & gutter at the northwestern corner of the project site (**DP 2B**).

Basin PR-3 (0.22 AC, $Q_5 = 0.2$ cfs, $Q_{100} = 0.7$ cfs): Located on the northern boundary of the site, this basin consists of sidewalk and landscaping, as well as offsite areas within the Constitution right-of-way being developed. Runoff from this basin will sheet flow to existing curb and gutter in Constitution Ave. Flows will then be routed, via existing curb & gutter downstream to the northeastern corner of the project site (**DP 3**).

Basin PR-4 (0.24 AC, $Q_5 = 0.1$ cfs, $Q_{100} = 0.6$ cfs): Located on the eastern boundary of the site, this basin consists of driveway and landscaping. Runoff from this basin will sheet flow from the driveway to

proposed curb and gutter at the driveway and Canada Dr. Flows will then be routed, via curb & gutter downstream to the existing curb & gutter at the southeastern corner of the project site **(DP 4)**.

Basin PR-5 (1.32 AC, $Q_5 = 3.9$ cfs, $Q_{100} = 9.0$ cfs): Located on the northcentral portion of the site, this basin consists entirely of the proposed two-story building. Flows will be captured by roof drains and routed, via pipe **(DP 5)**, to the proposed (private) full spectrum detention (FSD-1) sand filter basin (SFB) located at the northeast corner of the site **(DP 10)**.

Basin PR-6 (0.83 AC, $Q_5 = 0.9$ cfs, $Q_{100} = 2.6$ cfs): Located on the central portion of the site, west and south of Basin PR-5. This basin consists of landscaping and driveway. Runoff from this basin will sheet flow from the driveway to the proposed curb and gutter to the proposed (private) 8' Colorado Springs D-10-R inlet **(DP 6A)** where flows will be routed, via pipe, to the proposed (private) full spectrum detention (FSD-1) sand filter basin (SFB) located at the northeast corner of the site **(DP 10)**. Emergency overflows will be routed downstream via proposed curb and gutter to Canada Drive.

Basin PR-7 (0.19 AC, $Q_5 = 0.6$ cfs, $Q_{100} = 1.3$ cfs): Located on the northcentral portion of the site east of Basin PR-5, this basin consists of landscaping, and RV storage. Runoff from this basin will sheet flow to the edge of the proposed RV storage area to a proposed (private) 18" Nyloplast Drain Basin inlet in sump condition **(DP 7)**, where flows will be routed, via pipe, to the proposed (private) full spectrum detention (FSD-1) sand filter basin (SFB) located at the northeast corner of the site **(DP 10)**. Emergency overflows will be routed downstream via proposed curb and gutter to Canada Drive.

Basin PR-8 (0.13 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.2$ cfs): Located on the northern portion of the site, this basin consists entirely of landscaped area and swale north of the building. Runoff from this basin will sheet flow to the proposed swale to the proposed (private) CDOT Type C inlet **(DP 8)** where flows will be routed, via pipe, to the proposed (private) full spectrum detention (FSD-1) sand filter basin (SFB) located at the northeast corner of the site **(DP 10)**. Emergency overflows will be routed downstream via proposed curb and gutter to Canada Drive.

Basin PR-9 (0.18 AC, $Q_5 = 0.5$ cfs, $Q_{100} = 1.3$ cfs): Located in the eastern portion of the site, this basin consists of drive aisle and parking. Runoff from this basin will sheet flow to a proposed (private) 4' Colorado Springs D-10-R inlet in sump conditions, located on the south side of the eastern most parking stalls **(DP 9)** where flows will be routed, via pipe, to the proposed (private) full spectrum detention (FSD-1) sand filter basin (SFB) located at the northeast corner of the site **(DP 10)**. Emergency overflows will be routed downstream via proposed curb and gutter to Canada Drive.

Basin PR-10 (0.31 AC, $Q_5 = 0.0$ cfs, $Q_{100} = 0.6$ cfs): Located at the northeastern corner of the site, Basin PR-8 contains the entirety of the proposed (private) full spectrum detention (FSD-1) and adjacent landscaped area. Runoff from this basin will sheet flow directly to the (private) full spectrum detention (FSD-1) **(DP 10)**.

VII. Storm Sewer System

All development is anticipated to be urban and will include storm sewer & street inlets. Storm sewers collect storm water runoff and convey the water to the water quality facility prior to discharging. Storm sewer systems will be designed to the 100-year storm and checked with the 5-year storm. Inlets will be placed at sump areas and locations where street flow is larger than street capacity. UDFCD Inlet spreadsheet has been used to determine the size of all sump inlets.

There will be a proposed storm system within the site. The storm sewer system will discharge storm water into the proposed private full spectrum detention facility (FSD-1). The proposed system will consist of HDPE pipe, CDOT Type C inlets, Colorado Springs D-10-R inlets, Nyloplast Drain Basins, and storm sewer manholes.

Additionally, there are two (2) proposed drainage swales that run along the north and west side of the proposed building, respectively within sub-basins PR-8 and PR-6. The swales were analyzed using the Bentley software FlowMaster to properly size a triangular channel to convey the 100-year flows from the basins to FSD-1, while providing 1.0-ft of freeboard. The sizing calculations can be found in **Appendix D**.

Subsequent submittals will include details concerning at-grade inlet locations, street capacity, storm sewer sizing, outlet protection and location. Preliminary sump inlets have been sized and the calculations can be found in **Appendix D**.

VIII. Proposed Water Quality Detention Ponds

One (1) Water Quality Capture Volume Detention Pond (FSD-1) will be provided for the proposed site. The proposed pond will be privately owned and maintained by Johnson Development Associates Inc., once established. This detention pond is proposed to be full spectrum and will provide water quality and detention. Flows will be routed into the pond with the proposed (private) storm sewer system and release onto riprap pads into the pond. The WQCV release will be controlled by infiltration within the sand filter basin (SFB). The release rates for the WQCV and EURV will be 25-hours and 32-hours, respectively, and will pond to depths of 6499.37 and 6500.16. Flows exceeding the WQCV will be controlled by orifices and a modified Type C Outlet Structure and will be designed to release at or below the pre-development flow rate. A proposed outlet structure has been designed with this report. See **Appendix E** for calculations.

Basins PR-5 through PR-10 drain to FSD-1, totaling 2.96 acres and 80% of the project site. Per ECM Section I.7.1.C.1, 20% of the site may free release offsite, not to exceed 1 acre. Basins PR-1 through PR-4 free release, totaling 0.76 acres and 20% of the site area.

FSD-1: Located at the northeastern corner of the site, just west of existing Canada Dr. This pond will discharge to the existing western curb line within Canada Dr. The required volume WQCV and EURV are 0.057 Ac-Ft & 0.275 Ac-Ft, respectively. The total required detention basin volume is 0.424 Ac-Ft. See **Appendix E** for volume calculations.

IX. Proposed Channel Improvements

There are no proposed channel improvements as part of this report.

X. Maintenance

After completion of construction, the drainage facility (FSD-1) will be privately owned and maintained by Johnson Development Associates, Inc.

XI. Wetlands Mitigation

There are no existing wetlands within the project site.

XII. Floodplain Statement

No portion of the project sit lies with the designated Flood Zone as defined by the FIRM Map number 08041C0752G effective December 7, 2018. A copy of the FIRM Panel is included in **Appendix A**.

XIII. Drainage Fees & Maintenance

Drainage fees do not apply for Site Development Plans and are therefore not applicable to this project.

Below is a cost estimate for the improvements proposed with this filing.

Item	Quantity	Unit	Unit Cost	Cost
Storm Drain Improvements (Private)				
CDOT Type C Inlet (Private)	1	EA	\$ 5,138.00	\$ 5,138.00
Nyoplast Area Inlet -Single (Private)	1	EA	\$ 2,750.00	\$ 2,750.00
4' Type D-10 R Inlet (Private)	1	EA	\$ 6,138.00	\$ 6,138.00
8' Type D-10 R Inlet (Private)	1	EA	\$ 8,447.00	\$ 8,447.00
Storm Sewer Manhole, Slab Base	3	EA	\$ 7,082.00	\$ 21,246.00
18" Storm Drain - RCP (Private)	355	LF	\$ 70.00	\$ 24,850.00
18" Storm Drain - HDPE (Private)	475	LF	\$ 60.00	\$ 28,500.00
18" FES	1	EA	\$ 420.00	\$ 420.00
Subtotal				\$ 119,188.00
WQCV Detention Ponds (Private)				
Pond (FSD-1)	1	EA	\$ 45,000.00	\$ 45,000.00
Subtotal				\$ 45,000.00
Total				\$ 164,188.00
Contingency			10%	\$ 16,418.80
Grand Total				\$ 180,606.80

XIV. Conclusion

The Constitution Storage commercial development lies within the Sand Creek Drainage Basin. Water quality for the site is provided in a single on-site, private, Full Spectrum Detention Pond; FSD-1. All drainage facilities within this report were sized according to the El Paso County Drainage Criteria Manuals. The private full spectrum detention facility (FSD-1) will be maintained by Johnson Development Associates, Inc. The Constitution Storage development will not adversely impact any downstream facilities.

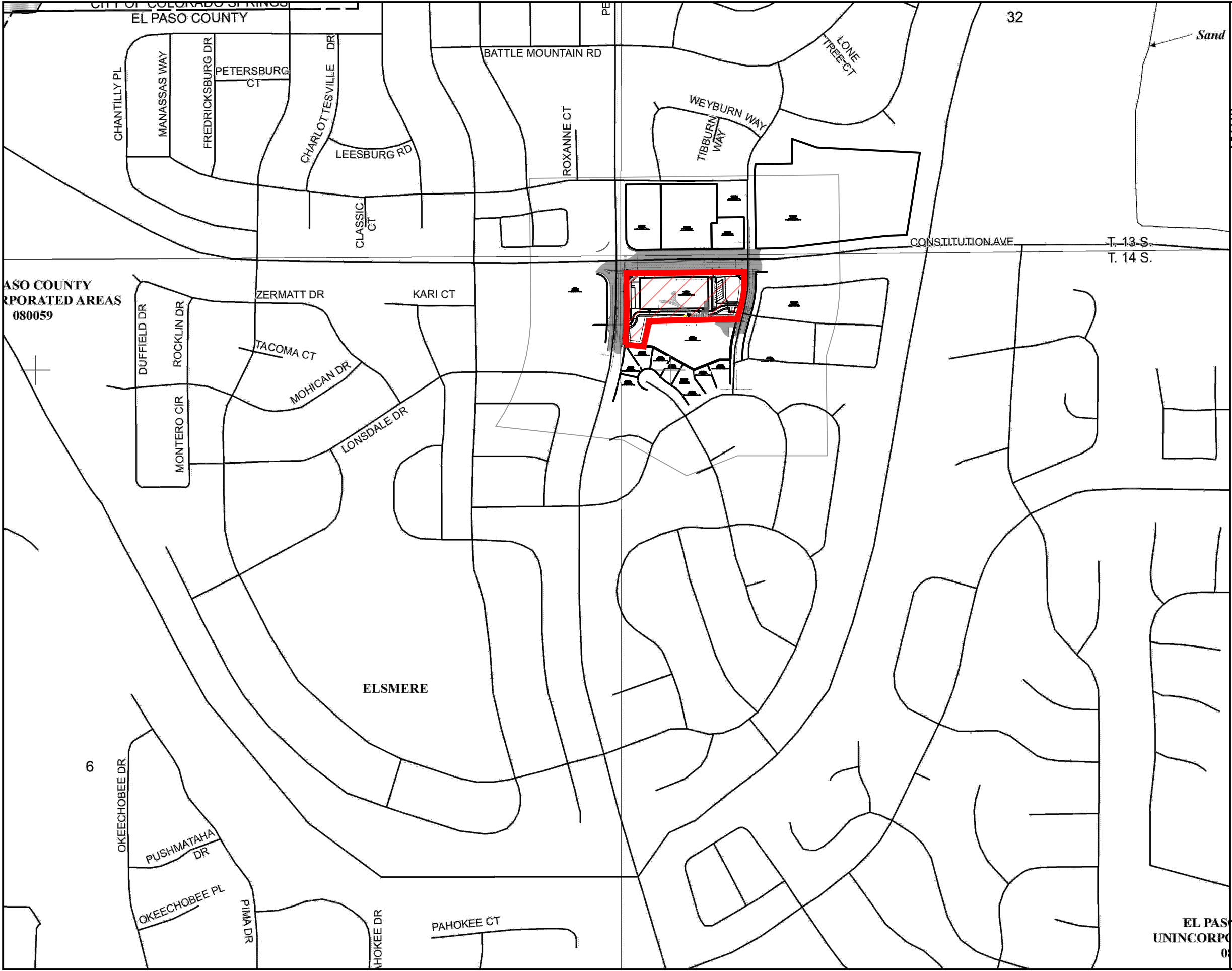
XV. References


1. *El Paso County Drainage Criteria Manual*, 1990.
2. *Drainage Criteria Manual, Volume 2*, City of Colorado Springs, 2002.
3. *El Paso County Drainage Criteria Manual Update*, 2015.
4. *El Paso County Engineering Criteria Manual*, 2020.

5. *Urban Storm Drainage Criteria Manual*, Urban Drainage and Flood Control District, January 2016 (with current revisions).
6. *Amendment Number 1, Final Drainage Study, Cimarron Northcrest Filing No. 3*", Costin Engineering Company, February 1983.

APPENDIX A

Exhibits and Figures






MAP SCALE 1" = 500'

250 0 500 1000
FEET

0 0 150 300
METERS



PANEL 0752G

FIRM

FLOOD INSURANCE RATE MAP

**EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS**

PANEL 752 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0752	G
EL PASO COUNTY	080059	0752	G


Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the Notice-to-User Letter that accompanied this correction for details.

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0752G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency



**EL PASO
UNINCORPORATED AREAS
080059**

This is an official FIRMette showing a portion of the above-referenced flood map created from the MSC FIRMette Web tool. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For additional information about how to make sure the map is current, please see the Flood Hazard Mapping Updates Overview Fact Sheet available on the FEMA Flood Map Service Center home page at <https://msc.fema.gov>.

El Paso County Area, Colorado

97—Truckton sandy loam, 3 to 9 percent slopes

Map Unit Setting

National map unit symbol: 2x0j2

Elevation: 5,300 to 6,850 feet

Mean annual precipitation: 14 to 19 inches

Mean annual air temperature: 48 to 52 degrees F

Frost-free period: 85 to 155 days

Farmland classification: Not prime farmland

Map Unit Composition

Truckton and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Truckton

Setting

Landform: Interfluves, hillslopes

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Re-worked alluvium derived from arkose

Typical profile

A - 0 to 4 inches: sandy loam

Bt1 - 4 to 12 inches: sandy loam

Bt2 - 12 to 19 inches: sandy loam

C - 19 to 80 inches: sandy loam

Properties and qualities

Slope: 3 to 9 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High
(2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 1 percent

Maximum salinity: Nonsaline (0.1 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 6.6 inches)

Interpretive groups

Land capability classification (irrigated): 6e

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Minor Components

Blakeland

Percent of map unit: 8 percent
Landform: Interfluves, hillslopes
Landform position (two-dimensional): Summit, shoulder, backslope
Landform position (three-dimensional): Side slope, crest
Down-slope shape: Convex, linear
Across-slope shape: Convex, linear
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

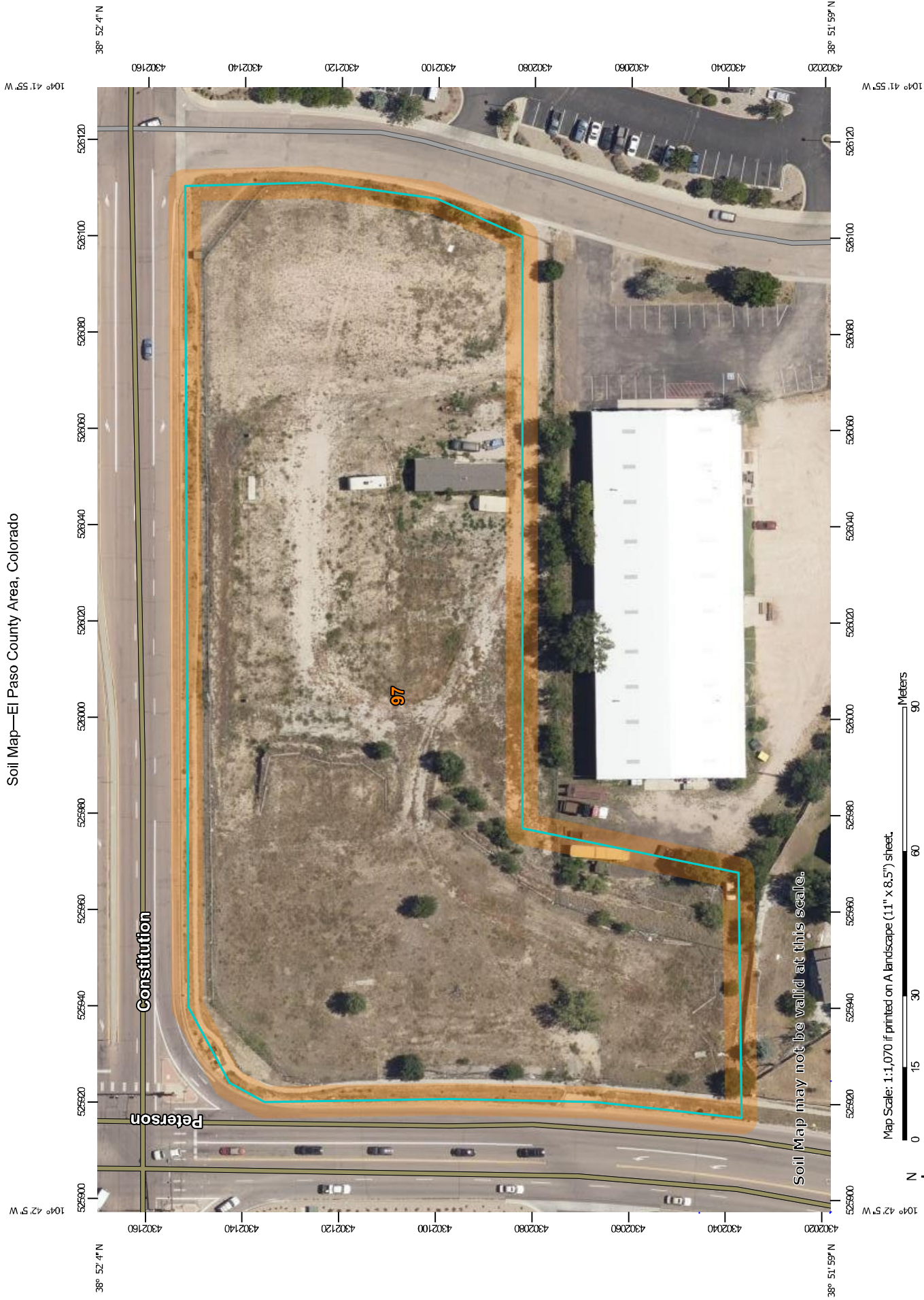
Bresser

Percent of map unit: 7 percent
Landform: Interfluves, low hills
Landform position (two-dimensional): Footslope, toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Ecological site: R049XB210CO - Sandy Foothill
Hydric soil rating: No

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

Soil Map—El Paso County Area, Colorado



Map Scale: 1:1,070 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84

















































Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

4/14/2022
Page 1 of 3

MAP LEGEND

Area of Interest (AOI)		Area of Interest (AOI)		Spoil Area
Soils		Soil Map Unit Polygons		Stony Spot
		Soil Map Unit Lines		Very Stony Spot
		Soil Map Unit Points		Wet Spot
Special Point Features		Blowout		Other
		Borrow Pit		Special Line Features
		Clay Spot		
		Closed Depression		
		Gravel Pit		
		Gravelly Spot		
		Landfill		
		Lava Flow		
		Marsh or swamp		
		Mine or Quarry		
		Miscellaneous Water		
		Perennial Water		
		Rock Outcrop		
		Saline Spot		
		Sandy Spot		
		Severely Eroded Spot		
		Sinkhole		
		Slide or Slip		
		Sodic Spot		

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
97	Truckton sandy loam, 3 to 9 percent slopes	3.8	100.0%
Totals for Area of Interest		3.8	100.0%

APPENDIX B

Standard Design Charts & Tables

Detailed descriptions of the curve number loss method and the dimensionless unit hydrograph can be found in these references:

- U.S. Department of Agriculture Natural Resources Conservation Service (NRCS) 1986. *Urban Hydrology for Small Watersheds*. Technical Release 55 (TR-55) (Second Edition). Prepared by Conservation Engineering Division.
- U.S. Army Corps of Engineers (USACE) 2010. *Hydrologic Modeling System HEC-HMS User's Manual*. Hydrologic Engineering Center, CPD-74A.

While it is possible to perform hydrograph analysis using the NRCS curve number loss method and dimensionless unit hydrograph using spreadsheet tools, it is cumbersome. More commonly, computer models such as the USACE HEC-HMS model are used. This section describes model input requirements for pre- and post-development modeling using HEC-HMS. Primary inputs include basin characteristics such as the drainage area, curve number and lag time. In addition, channel routing parameters are specified in HEC-HMS.

Other computer programs that use the NRCS loss method and dimensionless unit hydrograph may also be used, provided that the model results can be replicated using HEC-HMS. However, the curve number option for calculating rainfall losses in EPA SWMM is not acceptable because it is not an accurate implementation of the NRCS method and may produce results that vary significantly from HEC-HMS and TR-55.

4.1 NRCS Curve Numbers

NRCS curve numbers range from 0 to 100 (the recommended lower limit is 40) and can be used to calculate the volume of runoff from a storm event based on land use characteristics. A curve number of 0 would represent zero runoff (100% losses), and a curve number of 100 would represent zero losses (100% runoff).

The selection of a curve number value depends on the type of soil, identified by the NRCS hydrologic soil group (HSG), the land cover or treatment, and the antecedent runoff condition (ARC).

4.1.1 Hydrologic Soil Groups (HSG)

HSGs are determined by soil surveys published by the NRCS, which are generally done on a county-wide basis. The NRCS Soil Survey Geographic (SSURGO) Database is an online tool that may be used to characterize soils and HSGs.

The locations of each soil type for the drainage basin being studied must be identified by their HSG designation. The four hydrologic soil groups are defined by soil scientists, according to their runoff potential, as:

- **Group A: Low runoff potential.** Soils having low runoff potential and high infiltration rates even when thoroughly wetted. These consist chiefly of deep, well to excessively drained sand or gravel and have a high rate of water transmission (> 0.30 in/hr).
- **Group B: Moderate runoff potential.** Soils having moderate infiltration rates when thoroughly wetted and consist chiefly of moderately deep to deep, moderately well to well drained soils with moderately fine to moderately coarse textures. These soils have a moderate rate of water transmission (0.15-0.30 in/hr).

Assumed infiltration
rate for sand filter.
 $0.30 \text{ in/hr} * 6985 \text{ sf} =$
 $0.05 \text{ cfs infiltration}$

APPENDIX C

Hydrologic Computations

COMPOSITE % IMPERVIOUS CALCULATIONS

Existing Conditions

Subdivision: _____
Location: CO, Colorado Springs

Project Name: 6855 Constitution Ave Storage Site
Project No.: JDA000002
Calculated By: DDJ
Checked By: BS
Date: 7/8/22

Basin ID	Total Area (ac)	Paved Roads			Lawns			Roofs			Basins Total Weighted % Imp.
		% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	
EX-1	0.05	100	0.00	0.0	2	0.05	2.0	90	0.00	0.00	2.0
EX-2	0.26	100	0.00	0.0	2	0.26	2.0	90	0.00	0.00	2.0
EX-3	0.39	100	0.02	4.2	2	0.38	1.9	90	0.00	0.00	6.1
EX-4	0.03	100	0.02	77.0	2	0.01	0.5	90	0.00	0.00	77.5
EX-5	2.69	100	0.16	6.0	2	2.50	1.9	90	0.03	1.00	8.9
EX-6	0.36	100	0.00	0.0	2	0.36	2.0	90	0.00	0.00	2.0

STANDARD FORM SF-2
TIME OF CONCENTRATION

Existing Conditions

Subdivision: _____
Location: CO, Colorado Springs

Project Name: 6855 Constitution Ave Storage Site
Project No.: JDA000002
Calculated By: DDJ
Checked By: BS
Date: 7/8/22

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					T _c CHECK			FINAL
DATA						(T _i)			(T _t)					(URBANIZED BASINS)			
BASIN ID	D.A. (AC)	Hydrologic Soils Group	Impervious (%)	C ₁₀₀	C ₅	L (FT)	S (%)	T _i (MIN)	L (FT)	S (%)	C _v	VEL. (FPS)	T _t (MIN)	COMP. T _c (MIN)	TOTAL LENGTH (FT)	Urbanized T _c (MIN)	
EX-1	0.05	A	2.0	0.22	0.00	61	27.0	5.2	0	1.5	20.0	2.4	0.0	5.2	61.0	10.3	5.2
EX-2	0.26	A	2.0	0.22	0.00	100	3.0	14.0	130	7.3	15.0	4.1	0.5	14.5	230.0	11.3	11.3
EX-3	0.39	A	6.1	0.25	0.03	210	3.0	19.7	0	1.5	20.0	2.4	0.0	19.7	210.0	11.2	11.2
EX-4	0.03	A	77.5	0.63	0.53	16.5	2.0	3.4	16	1.5	20.0	2.4	0.1	3.5	32.5	10.2	5.0
EX-5	2.69	A	8.9	0.27	0.05	300	2.0	26.4	0	1.5	20.0	2.4	0.0	26.4	300.0	11.7	11.7
EX-6	0.36	A	2.0	0.22	0.00	200	5.0	16.7	0	1.5	20.0	2.4	0.0	16.7	200.0	11.1	11.1

NOTES:

$T_i = (0.395 * (1.1 - C_s) * (L)^{0.5}) / ((S)^{0.33})$, S in ft/ft

$T_t = L / 60V$ (Velocity From Fig. 501)

Velocity $V = C_v * S^{0.5}$, S in ft/ft

$T_c \text{ Check} = 10 + L / 180$

For Urbanized basins a minimum T_c of 5.0 minutes is required.

For non-urbanized basins a minimum T_c of 10.0 minutes is required

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)
Existing Conditions

Subdivision: _____
 Location: CO, Colorado Springs _____
 Design Storm: 2-Year _____

Project Name:	6855 Constitution Ave Storage Site
Project No.:	JDA000002
Calculated By:	DDJ
Checked By:	BS
Date:	7/8/22

[illegible]

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE) Existing Conditions

Subdivision: _____
Location: CO, Colorado Springs
Design Storm: 100-Year

Project Name: 6855 Constitution Ave Storage Site
Project No.: JDA000002
Calculated By: DDJ
Checked By: BS
Date: 7/8/22

[illegible]

COMPOSITE % IMPERVIOUS CALCULATIONS

Proposed Conditions

Subdivision: _____
Location: CO, Colorado Springs

Project Name: 6855 Constitution Ave Storage Site
Project No.: JDA000002
Calculated By: DDJ
Checked By: BS
Date: 7/8/22

Basin ID	Total Area (ac)	Paved Roads			Lawns			Roofs			Basins Total Weighted % Imp.
		% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	
PR-1	0.24	100	0.00	0.0	2	0.24	2.0	90	0.00	0.00	2.0
PR-2A	0.11	100	0.04	39.7	2	0.07	1.2	90	0.00	0.00	40.9
PR-2B	0.01	100	0.008	75.5	2	0.003	0.5	90	0.00	0.00	76.0
PR-3	0.22	100	0.07	30.8	2	0.15	1.4	90	0.00	0.00	32.2
PR-4	0.24	100	0.06	23.2	2	0.18	1.5	90	0.00	0.00	24.7
PR-5	1.32	100	0.00	0.0	2	0.00	0.0	90	1.32	90.00	90.0
PR-6	0.83	100	0.49	58.6	2	0.34	0.8	90	0.00	0.00	59.4
PR-7	0.19	100	0.17	91.7	2	0.02	0.2	90	0.00	0.00	91.9
PR-8	0.13	100	0.00	0.0	2	0.13	2.0	90	0.00	0.00	2.0
PR-9	0.18	100	0.17	90.9	2	0.02	0.2	90	0.00	0.00	91.1
PR-10	0.31	100	0.00	0.0	2	0.31	2.0	90	0.00	0.00	2.0

STANDARD FORM SF-2
TIME OF CONCENTRATION

Proposed Conditions

Subdivision: _____
Location: CO, Colorado Springs

Project Name: 6855 Constitution Ave Storage Site
Project No.: JDA000002
Calculated By: DDJ
Checked By: BS
Date: 7/8/22

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					T _c CHECK			FINAL
DATA						(T _i)			(T _t)					(URBANIZED BASINS)			
BASIN ID	D.A. (AC)	Hydrologic Soils Group	Impervious (%)	C ₁₀₀	C ₅	L (FT)	S (%)	T _i (MIN)	L (FT)	S (%)	C _v	VEL. (FPS)	T _t (MIN)	COMP. T _c (MIN)	TOTAL LENGTH (FT)	Urbanized T _c (MIN)	
PR-1	0.24	A	2.0	0.22	0.00	137	10.0	10.9	0	3.0	20.0	3.5	0.0	10.9	137.0	10.8	10.8
PR-2A	0.11	A	40.9	0.41	0.25	42	2.0	8.0	54	2.0	20.0	2.8	0.3	8.3	96.0	10.5	8.3
PR-2B	0.01	A	76.0	0.62	0.51												5.0
PR-3	0.22	A	32.2	0.38	0.20												5.0
PR-4	0.24	A	24.7	0.35	0.16	93	6.0	9.1	0	3.0	20.0	3.5	0.0	9.1	93.0	10.5	9.1
PR-5	1.32	A	90.0	0.79	0.71												5.0
PR-6	0.83	A	59.4	0.49	0.36	57	2.0	8.1	370	0.5	20.0	1.4	4.4	12.5	427.0	12.4	12.4
PR-7	0.19	A	91.9	0.81	0.74	42	2.0	3.4	47	0.5	20.0	1.4	0.6	3.9	89.0	10.5	5.0
PR-8	0.13	A	2.0	0.22	0.00	25	2.0	8.0	390	2.5	20.0	3.2	2.1	10.0	415.0	12.3	10.0
PR-9	0.18	A	91.1	0.80	0.73	96	4.0	4.2	59	4.0	20.0	4.0	0.2	4.4	155.0	10.9	5.0
PR-10	0.31	A	2.0	0.22	0.00												5.0

NOTES:

$T_i = (0.395 * (1.1 - C_s) * (L)^{0.5}) / ((S)^{0.33})$, S in ft/ft

$T_t = L / 60V$ (Velocity From Fig. 501)

Velocity $V = C_v * S^{0.5}$, S in ft/ft

$T_c \text{ Check} = 10 + L / 180$

For Urbanized basins a minimum T_c of 5.0 minutes is required.

For non-urbanized basins a minimum T_c of 10.0 minutes is required

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: _____
Location: CO, Colorado Springs _____
Design Storm: 2-Year _____

Project Name: 6855 Constitution Ave Storage Site _____
Project No.: JDA000002 _____
Calculated By: DDJ _____
Checked By: BS _____
Date: 7/8/22 _____

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	1	PR-1	0.24	0.00	10.8	0.00	3.21	0.0													Free Release to Alvarado property
	2A	PR-2A	0.11	0.25	8.3	0.03	3.51	0.1													Free Release to Peterson Road
	2B	PR-2B	0.01	0.51	5.0	0.01	4.12	0.0													Free Release to Peterson Road
	3	PR-3	0.22	0.20	5.0	0.04	4.12	0.2													Free Release to Constitution Avenue
	4	PR-4	0.24	0.16	9.1	0.04	3.40	0.1													Free Release to Canada Drive
	5	PR-5	1.32	0.71	5.0	0.94	4.12	3.9													Roof drains to DP-6B
	6A	PR-6	0.83	0.36	12.4	0.30	3.04	0.9													D-10R inlet to DP-6B
	6B								12.4	1.24	3.04	3.8									Max flow at DP-6B to DP-7
	7	PR-7	0.19	0.74	5.0	0.14	4.12	0.6	12.4	1.38	3.04	4.2									Area inlet & Maximum flow at DP-7 to DP-8
	8	PR-8	0.13	0.00	10.0	0.00	3.29	0.0	12.4	1.38	3.04	4.2									Area inlet & Flows from PR-5, PR-6, PR-7, PR-8 into FSD
	9	PR-9	0.18	0.73	5.0	0.13	4.12	0.5													Max flow at DP-9 into FSD
	10	PR-10	0.31	0.00	5.0	0.00	4.12	0.0	12.4	1.51	3.04	4.6									Maximum flow into FSD

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: _____
Location: CO, Colorado Springs _____
Design Storm: 100-Year _____

Project Name: 6855 Constitution Ave Storage Site _____
Project No.: JDA000002 _____
Calculated By: DDJ _____
Checked By: BS _____
Date: 7/8/22 _____

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	1	PR-1	0.24	0.22	10.8	0.05	6.75	0.3													Free Release to Alvarado property
	2A	PR-2A	0.11	0.41	8.3	0.04	7.39	0.3													Free Release to Peterson Road
	2B	PR-2B	0.01	0.62	5.0	0.01	8.68	0.1													Free Release to Peterson Road
	3	PR-3	0.22	0.38	5.0	0.08	8.68	0.7													Free Release to Constitution Avenue
	4	PR-4	0.24	0.35	9.1	0.08	7.16	0.6													Free Release to Canada Drive
	5	PR-5	1.32	0.79	5.0	1.04	8.68	9.0													Roof drains to DP-6B
	6A	PR-6	0.83	0.49	12.4	0.41	6.40	2.6													D-10R inlet to DP-6B
	6B								12.4	1.45	6.40	9.3									Max flow at DP-6B to DP-7
	7	PR-7	0.19	0.81	5.0	0.15	8.68	1.3	12.4	1.60	6.40	10.2									Area inlet & Maximum flow at DP-7 to DP-8
	8	PR-8	0.13	0.22	10.0	0.03	6.92	0.2	12.4	1.63	6.40	10.4									Area inlet & Flows from PR-5, PR-6, PR-7, PR-8 into FSD
	9	PR-9	0.18	0.80	5.0	0.15	8.68	1.3													Max flow at DP-9 into FSD
	10	PR-10	0.31	0.22	5.0	0.07	8.68	0.6	12.4	1.85	6.40	11.8									Maximum flow into FSD

APPENDIX D

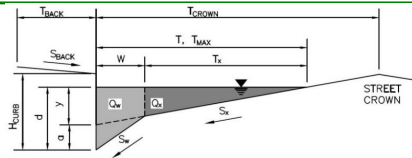
Hydraulic Computations

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: 6855 Constitution Ave Self Storage

Inlet ID: INLET DP-6A

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 5.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.013$

Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 120.0$ ft
 $W = 2.00$ ft
 $S_x = 0.005$ ft/ft
 $S_w = 0.083$ ft/ft
 $S_o = 0.000$ ft/ft
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	25.0	40.0	ft
$d_{MAX} =$	6.0	8.0	inches

☐ ☐

Maximum Capacity for 1/2 Street based On Allowable Spread

Water Depth without Gutter Depression (Eq. ST-2)
 Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")
 Gutter Depression ($d_c - (W * S_x * 12)$)
 Water Depth at Gutter Flowline
 Allowable Spread for Discharge outside the Gutter Section W ($T - W$)
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)
 Discharge outside the Gutter Section W , carried in Section T_x
 Discharge within the Gutter Section W ($Q_T - Q_x$)
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)
 Maximum Flow Based On Allowable Spread
 Flow Velocity within the Gutter Section
 $V*d$ Product: Flow Velocity times Gutter Flowline Depth

	Minor Storm	Major Storm	
$y =$	1.50	2.40	inches
$d_c =$	2.0	2.0	inches
$a =$	1.87	1.87	inches
$d =$	3.37	4.27	inches
$T_x =$	23.0	38.0	ft
$E_o =$	0.372	0.207	
$Q_x =$	0.0	0.0	cfs
$Q_w =$	0.0	0.0	cfs
$Q_{BACK} =$	0.0	0.0	cfs
$Q_T =$	SUMP	SUMP	cfs
$V =$	0.0	0.0	fps
$V*d =$	0.0	0.0	

Maximum Capacity for 1/2 Street based on Allowable Depth

Theoretical Water Spread
 Theoretical Spread for Discharge outside the Gutter Section W ($T - W$)
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)
 Theoretical Discharge outside the Gutter Section W , carried in Section T_{xTH}
 Actual Discharge outside the Gutter Section W , (limited by distance T_{CROWN})
 Discharge within the Gutter Section W ($Q_d - Q_x$)
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)
 Total Discharge for Major & Minor Storm (Pre-Safety Factor)
 Average Flow Velocity Within the Gutter Section
 $V*d$ Product: Flow Velocity Times Gutter Flowline Depth
 Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \geq 6"$) Storm
 Max Flow Based on Allowable Depth (Safety Factor Applied)
 Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)
 Resultant Flow Depth at Street Crown (Safety Factor Applied)

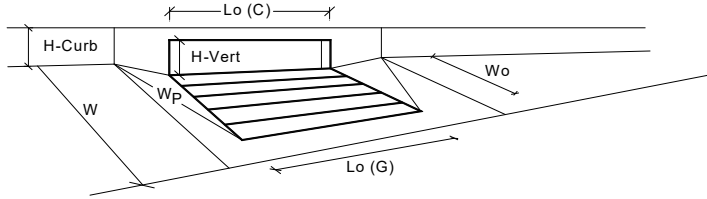
	Minor Storm	Major Storm	
$T_{TH} =$	68.8	102.1	ft
$T_{xTH} =$	66.8	100.1	ft
$E_o =$	0.104	0.065	
$Q_{xTH} =$	0.0	0.0	cfs
$Q_x =$	0.0	0.0	cfs
$Q_w =$	0.0	0.0	cfs
$Q_{BACK} =$	0.0	0.0	cfs
$Q =$	0.0	0.0	cfs
$V =$	0.0	0.0	fps
$V*d =$	0.0	0.0	
$R =$	SUMP	SUMP	
$Q_d =$	SUMP	SUMP	cfs
$d =$			inches
$d_{CROWN} =$			inches

MINOR STORM Allowable Capacity is based on Depth Criterion
 MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)



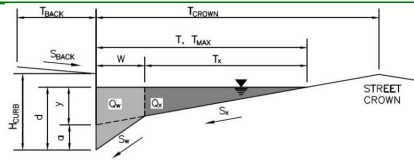
Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Springs D-10-R		
Local Depression (additional to continuous gutter depression 'a' from above)		a_{local} =	4.00	4.00	inches
Number of Unit Inlets (Grate or Curb Opening)		N_o =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	3.4	4.3	inches
Grate Information		MINOR		MAJOR	
Length of a Unit Grate		L_o (G) =	N/A	N/A	feet
Width of a Unit Grate		W_o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A_{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		C_f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C_o (G) =	N/A	N/A	
Curb Opening Information		MINOR		MAJOR	
Length of a Unit Curb Opening		L_o (C) =	8.00	8.00	feet
Height of Vertical Curb Opening in Inches		H_{vert} =	8.00	8.00	inches
Height of Curb Orifice Throat in Inches		H_{throat} =	8.00	8.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	81.00	81.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W_o =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		C_f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C_w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C_o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR		MAJOR	
Depth for Grate Midwidth		d_{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d_{Curb} =	0.12	0.19	ft
Combination Inlet Performance Reduction Factor for Long Inlets		$RF_{Combination}$ =	0.34	0.43	
Curb Opening Performance Reduction Factor for Long Inlets		RF_{Curb} =	0.81	0.89	
Grated Inlet Performance Reduction Factor for Long Inlets		RF_{Grate} =	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)		MINOR		MAJOR	
		Q_s =	1.2	2.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>0 PEAK)		$Q_{PEAK REQUIRED}$ =	0.9	2.6	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: 6855 Constitution Ave Self Storage

Inlet ID: INLET DP-9

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 5.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.013$

Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 27.0$ ft
 $W = 2.00$ ft
 $S_x = 0.040$ ft/ft
 $S_w = 0.083$ ft/ft
 $S_o = 0.000$ ft/ft
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	5.0	9.0	ft
$d_{MAX} =$	6.0	8.0	inches

☐ ☐

Maximum Capacity for 1/2 Street based On Allowable Spread

Water Depth without Gutter Depression (Eq. ST-2)
 Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")
 Gutter Depression ($d_c - (W * S_x * 12)$)
 Water Depth at Gutter Flowline
 Allowable Spread for Discharge outside the Gutter Section W ($T - W$)
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)
 Discharge outside the Gutter Section W , carried in Section T_x
 Discharge within the Gutter Section W ($Q_T - Q_x$)
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)
 Maximum Flow Based On Allowable Spread
 Flow Velocity within the Gutter Section
 $V*d$ Product: Flow Velocity times Gutter Flowline Depth

	Minor Storm	Major Storm	
$y =$	2.40	4.32	inches
$d_c =$	2.0	2.0	inches
$a =$	1.03	1.03	inches
$d =$	3.43	5.35	inches
$T_x =$	3.0	7.0	ft
$E_o =$	0.815	0.542	
$Q_x =$	0.0	0.0	cfs
$Q_w =$	0.0	0.0	cfs
$Q_{BACK} =$	0.0	0.0	cfs
$Q_T =$	SUMP	SUMP	cfs
$V =$	0.0	0.0	fps
$V*d =$	0.0	0.0	

Maximum Capacity for 1/2 Street based on Allowable Depth

Theoretical Water Spread
 Theoretical Spread for Discharge outside the Gutter Section W ($T - W$)
 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)
 Theoretical Discharge outside the Gutter Section W , carried in Section T_{xTH}
 Actual Discharge outside the Gutter Section W , (limited by distance T_{CROWN})
 Discharge within the Gutter Section W ($Q_d - Q_x$)
 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)
 Total Discharge for Major & Minor Storm (Pre-Safety Factor)
 Average Flow Velocity Within the Gutter Section
 $V*d$ Product: Flow Velocity Times Gutter Flowline Depth
 Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \geq 6"$) Storm
 Max Flow Based on Allowable Depth (Safety Factor Applied)
 Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)
 Resultant Flow Depth at Street Crown (Safety Factor Applied)

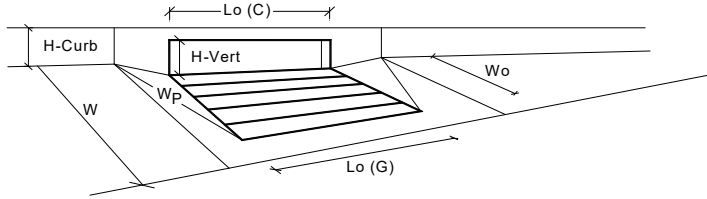
	Minor Storm	Major Storm	
$T_{TH} =$	10.4	14.5	ft
$T_{xTH} =$	8.4	12.5	ft
$E_o =$	0.482	0.356	
$Q_{xTH} =$	0.0	0.0	cfs
$Q_x =$	0.0	0.0	cfs
$Q_w =$	0.0	0.0	cfs
$Q_{BACK} =$	0.0	0.0	cfs
$Q =$	0.0	0.0	cfs
$V =$	0.0	0.0	fps
$V*d =$	0.0	0.0	
$R =$	SUMP	SUMP	
$Q_d =$	SUMP	SUMP	cfs
$d =$			inches
$d_{CROWN} =$			inches

MINOR STORM Allowable Capacity is based on Depth Criterion
 MAJOR STORM Allowable Capacity is based on Depth Criterion

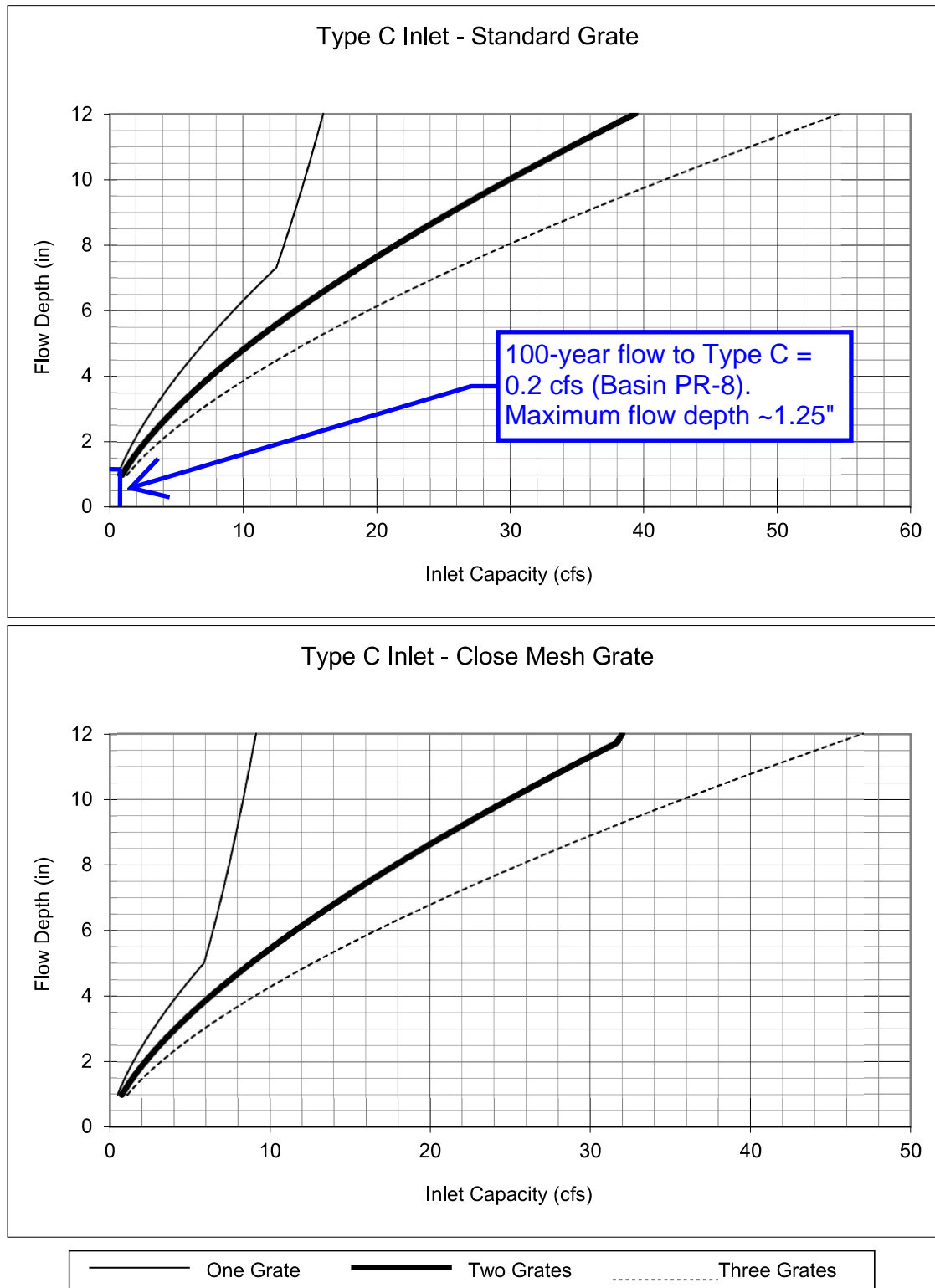
	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Springs D-10-R		
Local Depression (additional to continuous gutter depression 'a' from above)		a_{local} =	4.00	4.00	inches
Number of Unit Inlets (Grate or Curb Opening)		N_o =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	3.4	5.4	inches
Grate Information		MINOR		MAJOR	
Length of a Unit Grate		$L_o (G)$ =	N/A	N/A	feet
Width of a Unit Grate		W_o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A_{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		$C_f (G)$ =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		$C_w (G)$ =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		$C_o (G)$ =	N/A	N/A	
Curb Opening Information		MINOR		MAJOR	
Length of a Unit Curb Opening		$L_o (C)$ =	4.00	4.00	feet
Height of Vertical Curb Opening in Inches		H_{vert} =	8.00	8.00	inches
Height of Curb Orifice Throat in Inches		H_{throat} =	8.00	8.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	81.00	81.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W_o =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		$C_f (C)$ =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		$C_w (C)$ =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		$C_o (C)$ =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR		MAJOR	
Depth for Grate Midwidth		d_{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d_{Curb} =	0.12	0.28	ft
Combination Inlet Performance Reduction Factor for Long Inlets		$RF_{Combination}$ =	0.48	0.75	
Curb Opening Performance Reduction Factor for Long Inlets		RF_{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets		RF_{Grate} =	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)		MINOR		MAJOR	
		Q_s =	1.0	3.5	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>0 PEAK)		$Q_{PEAK REQUIRED}$ =	0.5	1.3	cfs

Figure 8-10. Inlet Capacity Chart Sump Conditions, Area (Type C) Inlet**Notes:**

1. The standard inlet parameters must apply to use these charts.



Nyloplast Inlet Capacity Table

DISCLAIMER: SAFETY FACTORS ARE NOT INCLUDED IN THESE CALCULATIONS. ACTUAL CALCULATIONS SHOULD BE CARRIED OUT AND VERIFIED BY THE DESIGN ENGINEER TAKING INTO ACCOUNT ALL LOCAL CONDITIONS. NYLOPLAST RECOMMENDS USING A MINIMUM SAFETY FACTOR OF 1.25 FOR PAVED AREAS AND 2.0 FOR TURF AREAS. ADS/NYLOPLAST IS NOT RESPONSIBLE FOR MISUSE OF THIS TOOL.

Input	
Type of Grate	18" Standard
Head (ft)	0.45
Properties	
Orifice Flow Area (in)	116.72
Orifice Flow Area (ft)	0.81
Weir Flow Perimeter (in)	52.04
Weir Flow Perimeter (ft)	4.34
Solution	
Capacity (cfs)	2.60
Capacity (gpm)	1167.00

maximum ponding
depth ~4.5"

Basin PR-7:
100-year flow =
1.3 cfs (doubled
to account for
50% clogging)

$$Q_{weir} = CLH^{3/2}$$

$C = 3.33$ Weir Discharge Coefficient

$L =$ Perimeter of Grate Opening (ft)

$H =$ Flow Height of Water Surface Above Weir (ft)

$$Q_{orifice} = CA\sqrt{2gh}$$

$C = 0.60$ Orifice Discharge Coefficient

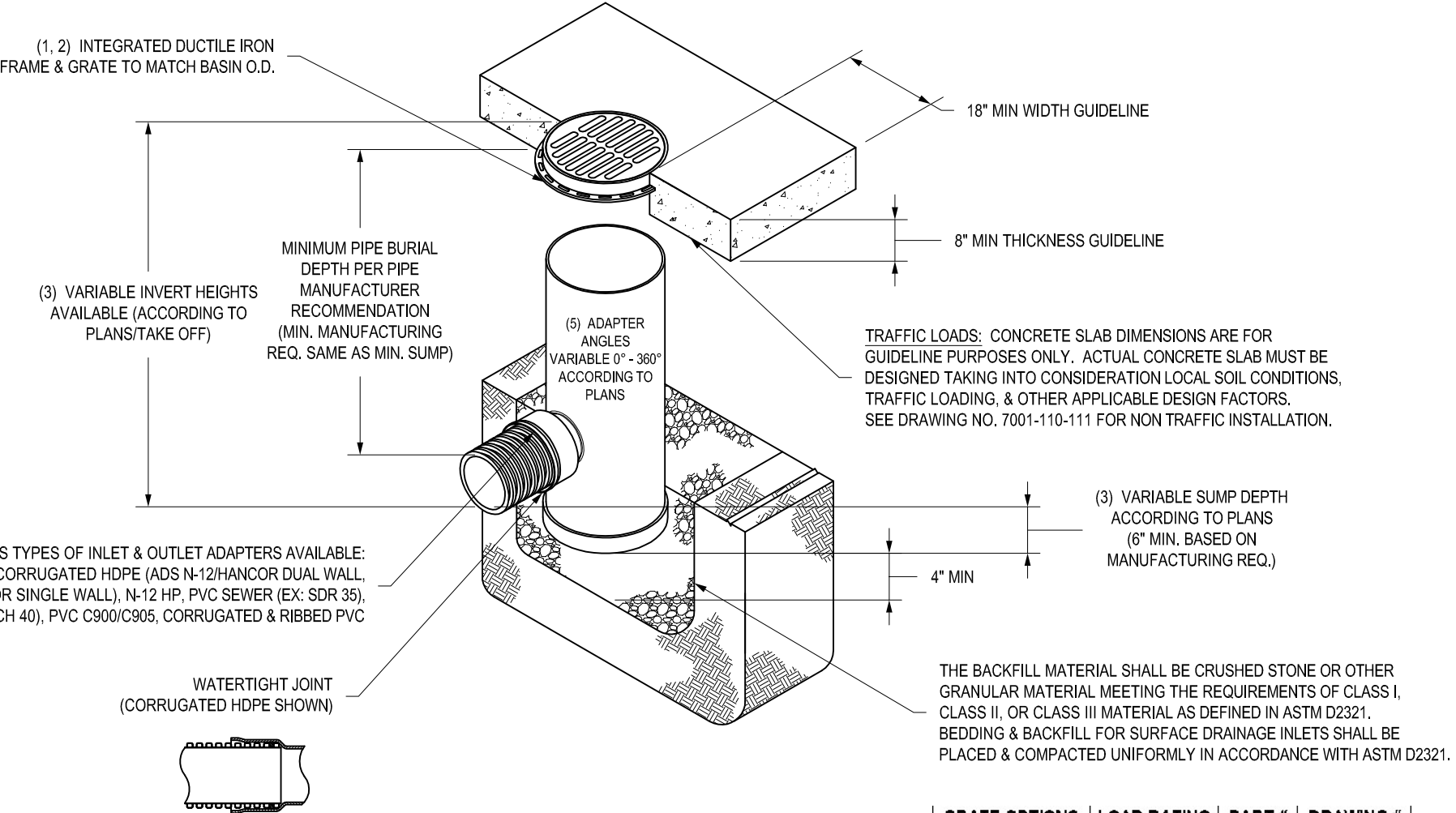
$A =$ Area of the Orifice (ft²)

$g =$ Gravitational Constant $\left(32.2 \frac{ft}{s^2}\right)$

$H =$ Depth of Water Above Center of Orifice (ft)

REV 2.1.21

NYLOPLAST 18" DRAIN BASIN: 2818AG __ X



- 1 - GRATES/SOLID COVER SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05.
- 2 - FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05.
- 3 - DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS. RISERS ARE NEEDED FOR BASINS OVER 84" DUE TO SHIPPING RESTRICTIONS. SEE DRAWING NO. 7001-110-065.
- 4 - DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 FOR CORRUGATED HDPE (ADS N-12/HANCOR DUAL WALL), N-12 HP, & PVC SEWER.
- 5 - ADAPTERS CAN BE MOUNTED ON ANY ANGLE 0° TO 360°. TO DETERMINE MINIMUM ANGLE BETWEEN ADAPTERS SEE DRAWING NO. 7001-110-012.

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DRAWN BY	EBC	MATERIAL
DATE	04-03-06	
REVISED BY	NMH	PROJECT NO./NAME
DATE	03-14-16	
DWG SIZE	A	SCALE 1:30 SHEET 1 OF 1

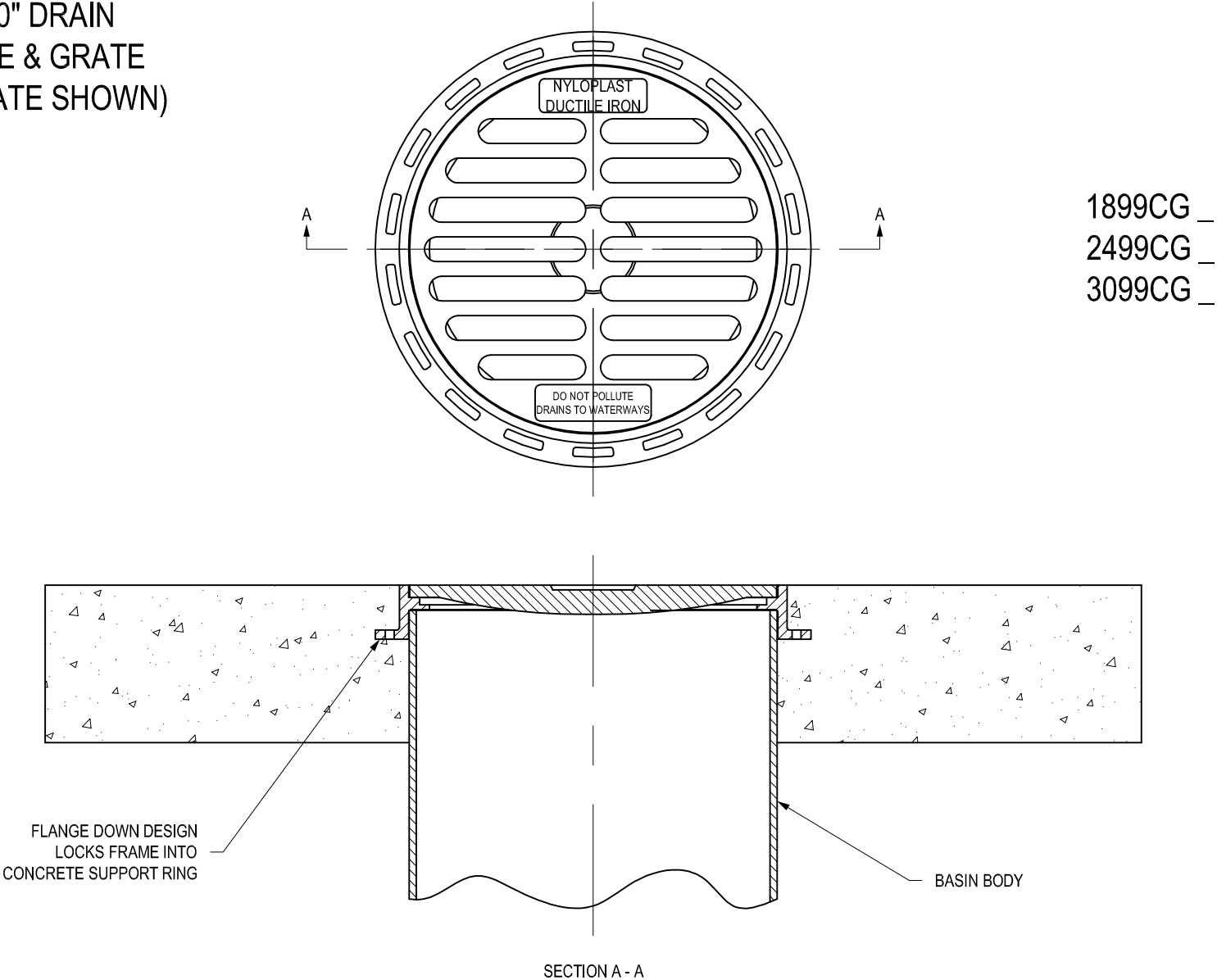



3130 VERONA AVE
BUFORD, GA 30518
PHN (770) 932-2443
FAX (770) 932-2490
www.nyloplast-us.com

TITLE	
18 IN DRAIN BASIN QUICK SPEC INSTALLATION DETAIL	
DWG NO.	7001-110-191
REV	E

GRATE OPTIONS	LOAD RATING	PART #	DRAWING #
PEDESTRIAN	MEETS H-10	1899CGP	7001-110-212
STANDARD	MEETS H-20	1899CGS	7001-110-213
SOLID COVER	MEETS H-20	1899CGC	7001-110-214
DOVE	N/A	1899CGD	7001-110-215
DROP IN GRATE	LIGHT DUTY	1801DI	7001-110-074

18" , 24" , & 30" DRAIN
 BASIN FRAME & GRATE
 (18" STD GRATE SHOWN)



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	DATE	12-10-99					
	APPD BY	CJA	PROJECT NO./NAME				TITLE
	DATE	12-10-99					18 IN, 24 IN, & 30 IN FRAME & GRATE EXAMPLE
	DWG SIZE	A	SCALE	1:8	SHEET	1 OF 1	DWG NO. 7001-110-005 REV D

12" @ 1% Capacity

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Normal Depth	1.00	ft
Diameter	1.00	ft
Discharge	3.56	ft ³ /s

Results

Discharge	3.56	ft ³ /s
Normal Depth	1.00	ft
Flow Area	0.79	ft ²
Wetted Perimeter	3.14	ft
Hydraulic Radius	0.25	ft
Top Width	0.00	ft
Critical Depth	0.81	ft
Percent Full	100.0	%
Critical Slope	0.01032	ft/ft
Velocity	4.54	ft/s
Velocity Head	0.32	ft
Specific Energy	1.32	ft
Froude Number	0.00	
Maximum Discharge	3.83	ft ³ /s
Discharge Full	3.56	ft ³ /s
Slope Full	0.01000	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%

12" @ 1% Capacity

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	1.00	ft
Critical Depth	0.81	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.01032	ft/ft

18" @ 1% Capacity

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Capacity

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Normal Depth	1.50	ft
Diameter	1.50	ft
Discharge	10.50	ft ³ /s

Results

Discharge	10.50	ft ³ /s
Normal Depth	1.50	ft
Flow Area	1.77	ft ²
Wetted Perimeter	4.71	ft
Hydraulic Radius	0.38	ft
Top Width	0.00	ft
Critical Depth	1.25	ft
Percent Full	100.0	%
Critical Slope	0.00977	ft/ft
Velocity	5.94	ft/s
Velocity Head	0.55	ft
Specific Energy	2.05	ft
Froude Number	0.00	
Maximum Discharge	11.30	ft ³ /s
Discharge Full	10.50	ft ³ /s
Slope Full	0.01000	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%

18" @ 1% Capacity

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	1.50	ft
Critical Depth	1.25	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.00977	ft/ft

Curb Chase Capacity

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Bottom Width	2.00	ft
Discharge	1.07	ft ³ /s

Results

Normal Depth	0.14	ft
Flow Area	0.27	ft ²
Wetted Perimeter	2.27	ft
Hydraulic Radius	0.12	ft
Top Width	2.00	ft
Critical Depth	0.21	ft
Critical Slope	0.00535	ft/ft
Velocity	3.93	ft/s
Velocity Head	0.24	ft
Specific Energy	0.38	ft
Froude Number	1.88	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.14	ft
Critical Depth	0.21	ft
Channel Slope	0.02000	ft/ft
Critical Slope	0.00535	ft/ft

Basin PR-6 Swale

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.04000 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Discharge 1.00 ft³/s

Results

Normal Depth 0.36 ft
Flow Area 0.38 ft²
Wetted Perimeter 2.26 ft
Hydraulic Radius 0.17 ft
Top Width 2.15 ft
Critical Depth 0.37 ft
Critical Slope 0.03362 ft/ft
Velocity 2.60 ft/s
Velocity Head 0.11 ft
Specific Energy 0.46 ft
Froude Number 1.08
Flow Type Supercritical

Note: Flow reduced from
PR-6 basin flow since
swale only captures small
portion of landscaped
flows

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 0.36 ft
Critical Depth 0.37 ft
Channel Slope 0.04000 ft/ft
Critical Slope 0.03362 ft/ft

Basin PR-8 Swale

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.035	
Channel Slope	0.02000	ft/ft
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Discharge	0.20	ft ³ /s

Results

Normal Depth	0.22	ft
Flow Area	0.15	ft ²
Wetted Perimeter	1.41	ft
Hydraulic Radius	0.11	ft
Top Width	1.34	ft
Critical Depth	0.19	ft
Critical Slope	0.04167	ft/ft
Velocity	1.34	ft/s
Velocity Head	0.03	ft
Specific Energy	0.25	ft
Froude Number	0.71	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.22	ft
Critical Depth	0.19	ft
Channel Slope	0.02000	ft/ft
Critical Slope	0.04167	ft/ft

APPENDIX E

Pond Computations

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input

Calculated cells

***Design Storm: 1-Hour Rain Depth	WQCV Event	0.60	inches
***Minor Storm: 1-Hour Rain Depth	5-Year Event	1.50	inches
***Major Storm: 1-Hour Rain Depth	100-Year Event	2.52	inches
Optional User Defined Storm	CUHP		
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm	100-Year Event		

Max Intensity for Optional User Defined Storm

0

Designer: DDJ

Company: Galloway & Co.

Date: July 8, 2022

Project: 6855 Constitution Ave Self Storage

Location: FSD

SITE INFORMATION (USER-INPUT)

Sub-basin Identifier	PR-5	PR-6	PR-7	PR-8	PR-9	PR-10									
Receiving Pervious Area Soil Type	Sandy Loam	Sandy Loam	Sandy Loam	Sandy Loam	Sandy Loam	Sandy Loam									
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	1.320	0.830	0.190	0.130	0.180	0.310									
Directly Connected Impervious Area (DCIA, acres)	1.320	0.490	0.170	0.000	0.170	0.000									
Unconnected Impervious Area (UIA, acres)	0.000	0.000	0.000	0.000	0.000	0.000									
Receiving Pervious Area (RPA, acres)	0.000	0.000	0.000	0.000	0.000	0.000									
Separate Pervious Area (SPA, acres)	0.000	0.340	0.020	0.130	0.010	0.310									
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	C	C	C	C	C	C									

CALCULATED RESULTS (OUTPUT)

Total Calculated Area (ac, check against input)	1.320	0.830	0.190	0.130	0.180	0.310									
Directly Connected Impervious Area (DCIA, %)	100.0%	59.0%	89.5%	0.0%	94.4%	0.0%									
Unconnected Impervious Area (UIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%									
Receiving Pervious Area (RPA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%									
Separate Pervious Area (SPA, %)	0.0%	41.0%	10.5%	100.0%	5.6%	100.0%									
A_t (RPA / UIA)	0.000	0.000	0.000	0.000	0.000	0.000									
I_a Check	1.000	1.000	1.000	1.000	1.000	1.000									
f / I for WQCV Event:	1.7	1.7	1.7	1.7	1.7	1.7									
f / I for 5-Year Event:	0.5	0.5	0.5	0.5	0.5	0.5									
f / I for 100-Year Event:	0.3	0.3	0.3	0.3	0.3	0.3									
f / I for Optional User Defined Storm CUHP:															
IRF for WQCV Event:	1.00	1.00	1.00	1.00	1.00	1.00									
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00									
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00									
IRF for Optional User Defined Storm CUHP:															
Total Site Imperviousness: I_{total}	100.0%	59.0%	89.5%	0.0%	94.4%	0.0%									
Effective Imperviousness for WQCV Event:	100.0%	59.0%	89.5%	0.0%	94.4%	0.0%									
Effective Imperviousness for 5-Year Event:	100.0%	59.0%	89.5%	0.0%	94.4%	0.0%									
Effective Imperviousness for 100-Year Event:	100.0%	59.0%	89.5%	0.0%	94.4%	0.0%									
Effective Imperviousness for Optional User Defined Storm CUHP:															

LID / EFFECTIVE IMPERVIOUSNESS CREDITS

WQCV Event CREDIT: Reduce Detention By:	N/A	0.0%	0.0%	0.0%	N/A	0.0%	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT**: Reduce Detention By:	N/A	0.0%	0.0%	0.1%	N/A	0.1%	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
User Defined CUHP CREDIT: Reduce Detention By:															

Total Site Imperviousness: 72.6%

Total Site Effective Imperviousness for WQCV Event: 72.6%

Total Site Effective Imperviousness for 5-Year Event: 72.6%

Total Site Effective Imperviousness for 100-Year Event: 72.6%

Total Site Effective Imperviousness for Optional User Defined Storm CUHP:

Notes:

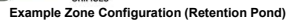
* Use Green-Ampt average infiltration rate values from Table 3-3.

** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCEM.

*** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

MHFD-Detention, Version 4.05 (January 2022)

Basin ID: FSD-1



Optional User Overrides

	acre-feet
	acre-feet
0.99	inches
1.27	inches
1.53	inches
1.94	inches
2.29	inches
2.67	inches
3.68	inches

Initial Surcharge Area (A_{ISV}) =		ft ²
Surcharge Volume Length (L_{ISV}) =		ft
Surcharge Volume Width (W_{ISV}) =		ft
Depth of Basin Floor (H_{FLOOR}) =		ft
Length of Basin Floor (L_{FLOOR}) =		ft
Width of Basin Floor (W_{FLOOR}) =		ft
Area of Basin Floor (A_{FLOOR}) =		ft ²
Volume of Basin Floor (V_{FLOOR}) =		ft ³
Depth of Main Basin (H_{MAIN}) =		ft
Length of Main Basin (L_{MAIN}) =		ft
Width of Main Basin (W_{MAIN}) =		ft
Area of Main Basin (A_{MAIN}) =		ft ²
Volume of Main Basin (V_{MAIN}) =		ft ³
Calculated Total Basin Volume (V_{OBS}) =		acre-feet

[illegible]

Required Detention Volumes

Stormwater Detention and Infiltration Design Data Sheet

Worksheet Protected

Watershed Slope =	0.020
-------------------	-------

Watershed Length = 520 ft

Watershed Area = 2.96 ac

and Imperviousness = 72.6% percent

Stage Hydrologic Soil Group A = 100.0% percent

Percentage Hydrologic Soil Group B =	0.0%	percent
--------------------------------------	------	---------

percentage Hydrologic Soil Groups C/D = 0.0% percent

Location for 1-hr Rainfall Depths (use dropdown):

User Input

[illegible]

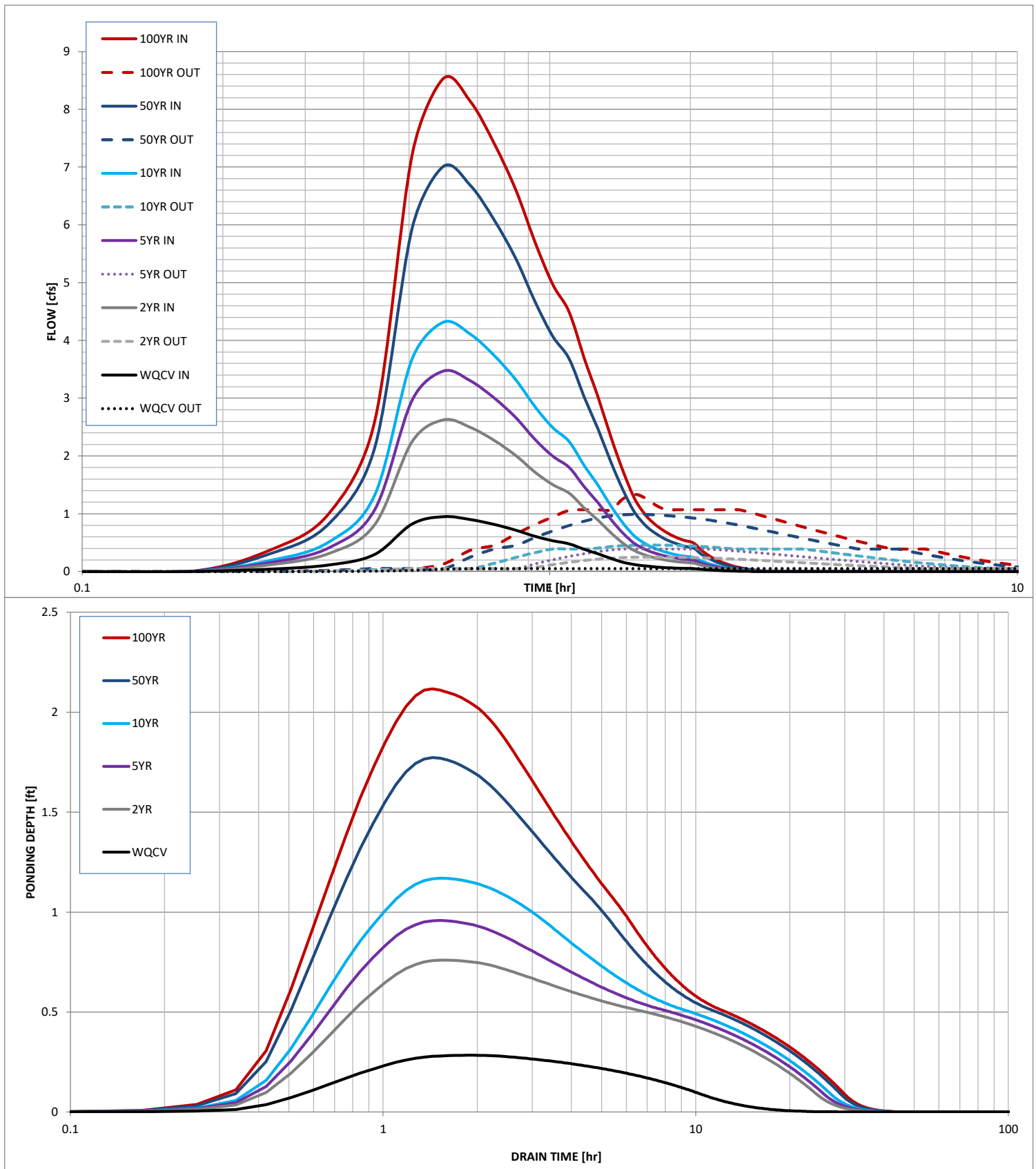
<https://maperture.digitaldataservices.com/gvh/?viewer=cswdif>

attach the pdf of this worksheet to that record.

WOCV	2 Year	5 Year	10 Year	50 Year	100 Year
------	--------	--------	---------	---------	----------

Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.60	0.99	1.27	1.53	2.29	2.67	in
Calculated Runoff Volume =	0.057	0.158	0.209	0.262	0.427	0.521	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.056	0.158	0.209	0.261	0.426	0.520	acre-ft
Time to Drain 97% of Inflow Volume =	18.3	28.6	28.9	29.4	29.7	29.8	hours
Time to Drain 99% of Inflow Volume =	22.2	32.5	32.8	33.4	33.7	33.8	hours
Maximum Ponding Depth =	0.28	0.76	0.96	1.17	1.77	2.12	ft
Maximum Ponded Area =	0.18	0.19	0.20	0.20	0.21	0.21	acres
Maximum Volume Stored =	0.048	0.134	0.173	0.216	0.339	0.410	acre-ft

Stormwater Detention and Infiltration Design Data Sheet



Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.06, November 2016)

Sheet 1 of 2

Designer: DDJ
Company: Galloway
Date: July 8, 2022
Project: 6955 Constitution Ave Self Storage
Location:

1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area, I_a
(100% if all paved and roofed areas upstream of sand filter)
- B) Tributary Area's Imperviousness Ratio ($i = I_a/100$)
- C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time
 $WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)$
- D) Contributing Watershed Area (including sand filter area)
- E) Water Quality Capture Volume (WQCV) Design Volume
 $V_{WQCV} = WQCV / 12 * \text{Area}$
- F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume
(Only if a different WQCV Design Volume is desired)

$I_a = 72.6 \%$

$i = 0.726$

$WQCV = 0.23$ watershed inches

$\text{Area} = 128,938$ sq ft

$V_{WQCV} = 2,469$ cu ft

$d_6 =$ in

$V_{WQCV \text{ OTHER}} =$ cu ft

$V_{WQCV \text{ USER}} =$ cu ft

2. Basin Geometry

- A) WQCV Depth
- B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.
- C) Minimum Filter Area (Flat Surface Area)
- D) Actual Filter Area
- E) Volume Provided

$D_{WQCV} = 0.46$ ft

$Z = 50.00$ ft / ft

$A_{\text{Min}} = 1170$ sq ft

$A_{\text{Actual}} = 2500$ sq ft

$V_T = 4478$ cu ft

3. Filter Material

Choose One

☒ 18" CDOT Class B or C Filter Material

☐ Other (Explain):

4. Underdrain System

- A) Are underdrains provided?
- B) Underdrain system orifice diameter for 12 hour drain time
- i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice
- ii) Volume to Drain in 12 Hours
- iii) Orifice Diameter, 3/8" Minimum

Choose One

☐ YES

☒ NO

$y = \text{N/A}$ ft

$\text{Vol}_{12} = \text{N/A}$ cu ft

$D_O = \text{N/A}$ in

Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

Designer: DDJ
Company: Galloway
Date: July 8, 2022
Project: 6955 Constitution Ave Self Storage
Location: _____

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

☐ YES

☒ NO

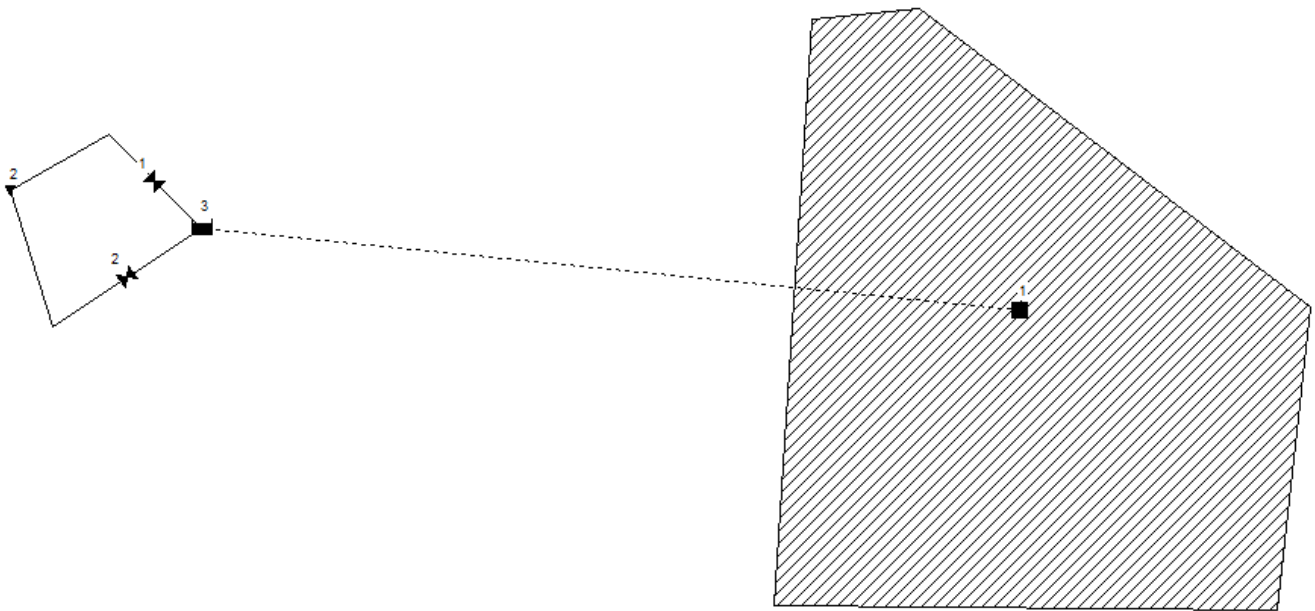
6-7. Inlet / Outlet Works

A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

Notes: _____

SWMM Layout

ColoradoSprings



SWMM Input Summary

```

1  [TITLE]
2  ;;Project Title/Notes
3
4  [OPTIONS]
5  ;;Option      Value
6  FLOW_UNITS    CFS
7  INFILTRATION  HORTON
8  FLOW_ROUTING  KINWAVE
9  LINK_OFFSETS  DEPTH
10 MIN_SLOPE      0
11 ALLOW_PONDING  NO
12 SKIP_STEADY_STATE NO
13
14 START_DATE     04/20/2022
15 START_TIME     00:00:00
16 REPORT_START_DATE 04/20/2022
17 REPORT_START_TIME 00:00:00
18 END_DATE       04/24/2022
19 END_TIME       00:00:00
20 SWEEP_START     01/01
21 SWEEP_END       12/31
22 DRY_DAYS        0
23 REPORT_STEP     00:15:00
24 WET_STEP        00:05:00
25 DRY_STEP        01:00:00
26 ROUTING_STEP    0:00:30
27 RULE_STEP       00:00:00
28
29 INERTIAL_DAMPING PARTIAL
30 NORMAL_FLOW_LIMITED BOTH
31 FORCE_MAIN_EQUATION H-W
32 VARIABLE_STEP    0.75
33 LENGTHENING_STEP 0
34 MIN_SURFAREA     12.566
35 MAX_TRIALS        8
36 HEAD_TOLERANCE    0.005
37 SYS_FLOW_TOL      5
38 LAT_FLOW_TOL      5
39 MINIMUM_STEP      0.5
40 THREADS           1
41
42 [EVAPORATION]
43 ;;Data Source    Parameters
44 ;;-----
45 CONSTANT         0.0
46 DRY_ONLY         NO
47
48 [RAINGAGES]
49 ;;Name           Format      Interval SCF      Source
50 ;;-----
51 ColoradoSprings  CUMULATIVE 0:05      1.0      TIMESERIES 100yr
52
53 [SUBCATCHMENTS]
54 ;;Name           Rain Gage      Outlet      Area      %Imperv  Width      %Slope
55 CurbLen  SnowPack
56 ;;-----
57
58 1              ColoradoSprings  3              2.96      72.6      20          2
59 0
60
61 [SUBAREAS]
62 ;;Subcatchment  N-Imperv  N-Perv      S-Imperv  S-Perv      PctZero      RouteTo
63 PctRouted
64 ;;-----
65 1              .011      .24          .1          .35          25          OUTLET
66
67 [INFILTRATION]
68 ;;Subcatchment  Param1      Param2      Param3      Param4      Param5

```

```

65 ;;;-----
66 1          5          1          2.52      7          0
67
68 [OUTFALLS]
69 ;;Name      Elevation  Type          Stage Data      Gated      Route To
70 ;;;-----
71 2          0          FREE          NO
72
73 [STORAGE]
74 ;;Name      Elev.      MaxDepth  InitDepth  Shape      Curve Name/Params
75 N/A      Fevap      Psi      Ksat      IMD
76 ;;;-----
77
78 3          0          5          0          TABULAR      FSB-1
79 0          0          0          .29      0
80
81 [ORIFICES]
82 ;;Name      From Node      To Node      Type      Offset      Qcoeff
83 Gated      CloseTime
84 ;;;-----
85
86 1          3          2          SIDE      .51      0.65
87 NO          0
88
89 [OUTLETS]
90 ;;Name      From Node      To Node      Offset      Type
91 QTable/Qcoeff      Qexpon      Gated
92 ;;;-----
93
94 2          3          2          2.09      FUNCTIONAL/DEPTH
95 10.0      0.5      NO
96
97 [XSECTIONS]
98 ;;Link      Shape      Geom1      Geom2      Geom3      Geom4
99 Barrels      Culvert
100 ;;;-----
101
102 1          CIRCULAR      .5          0          0          0
103
104 [CURVES]
105 ;;Name      Type      X-Value      Y-Value
106 ;;;-----
107 OutletStructure      Rating      0.00      0.00
108 OutletStructure      0.20      2.66
109 OutletStructure      0.40      7.53
110 OutletStructure      0.60      11.02
111 OutletStructure      0.80      11.77
112 OutletStructure      1.00      12.47
113 OutletStructure      1.20      13.13
114 OutletStructure      1.40      13.77
115 OutletStructure      1.60      14.37
116 OutletStructure      1.80      14.95
117 OutletStructure      2.00      15.51
118 OutletStructure      2.20      16.05
119 OutletStructure      2.40      16.57
120 OutletStructure      2.60      17.07
121 OutletStructure      2.80      17.56
122 OutletStructure      3.00      18.04
123 ;
124 FSB-1      Storage      0      6985
125 FSB-1      0.09      7526.48
126 FSB-1      1.09      8825.82
127 FSB-1      2.09      9119.29
128 FSB-1      3.09      9302.02
129 FSB-1      4.09      9464.61
130 FSB-1      5.09      9627
131
132 [TIMESERIES]
133 ;;Name      Date      Time      Value

```

123	;;-----		
124	5-yr	0:00	0
125	5-yr	0:05	0.01778
126	5-yr	0:10	0.05842
127	5-yr	0:15	0.10033
128	5-yr	0:20	0.1524
129	5-yr	0:25	0.22733
130	5-yr	0:30	0.32766
131	5-yr	0:35	0.53467
132	5-yr	0:40	0.90424
133	5-yr	0:45	1.04648
134	5-yr	0:50	1.13284
135	5-yr	0:55	1.18745
136	5-yr	1:00	1.23444
137	5-yr	1:05	1.27508
138	5-yr	1:10	1.29286
139	5-yr	1:15	1.3081
140	5-yr	1:20	1.32207
141	5-yr	1:25	1.33604
142	5-yr	1:30	1.35001
143	5-yr	1:35	1.36144
144	5-yr	1:40	1.37414
145	5-yr	1:45	1.38557
146	5-yr	1:50	1.397
147	5-yr	1:55	1.40843
148	5-yr	2:00	1.42113
149	;		
150	WQ	0:00	0
151	WQ	0:05	0.0084
152	WQ	0:10	0.0276
153	WQ	0:15	0.0474
154	WQ	0:20	0.072
155	WQ	0:25	0.1074
156	WQ	0:30	0.1548
157	WQ	0:35	0.2526
158	WQ	0:40	0.4272
159	WQ	0:45	0.4944
160	WQ	0:50	0.5352
161	WQ	0:55	0.561
162	WQ	1:00	0.5832
163	WQ	1:05	0.6024
164	WQ	1:10	0.6108
165	WQ	1:15	0.618
166	WQ	1:20	0.6246
167	WQ	1:25	0.6312
168	WQ	1:30	0.6378
169	WQ	1:35	0.6432
170	WQ	1:40	0.6492
171	WQ	1:45	0.6546
172	WQ	1:50	0.66
173	WQ	1:55	0.6654
174	WQ	2:00	0.6714
175	;		
176	100yr	0:00	0
177	100yr	0:05	0.03738
178	100yr	0:10	0.12282
179	100yr	0:15	0.21093
180	100yr	0:20	0.3204
181	100yr	0:25	0.47793
182	100yr	0:30	0.68886
183	100yr	0:35	1.12407
184	100yr	0:40	1.90104
185	100yr	0:45	2.20008
186	100yr	0:50	2.38164
187	100yr	0:55	2.49645
188	100yr	1:00	2.59524
189	100yr	1:05	2.68068
190	100yr	1:10	2.71806
191	100yr	1:15	2.7501

192	100yr	1:20	2.77947
193	100yr	1:25	2.80884
194	100yr	1:30	2.83821
195	100yr	1:35	2.86224
196	100yr	1:40	2.88894
197	100yr	1:45	2.91297
198	100yr	1:50	2.937
199	100yr	1:55	2.96103
200	100yr	2:00	2.98773

201
202 [REPORT]
203 ;;Reporting Options
204 SUBCATCHMENTS ALL
205 NODES ALL
206 LINKS ALL

207
208 [TAGS]

209
210 [MAP]
211 DIMENSIONS 0.000 0.000 10000.000 10000.000
212 Units None

213
214 [COORDINATES]
215 ;;Node X-Coord Y-Coord
216 ;;-----
217 2 -972.461 6075.731
218 3 -266.781 5938.038

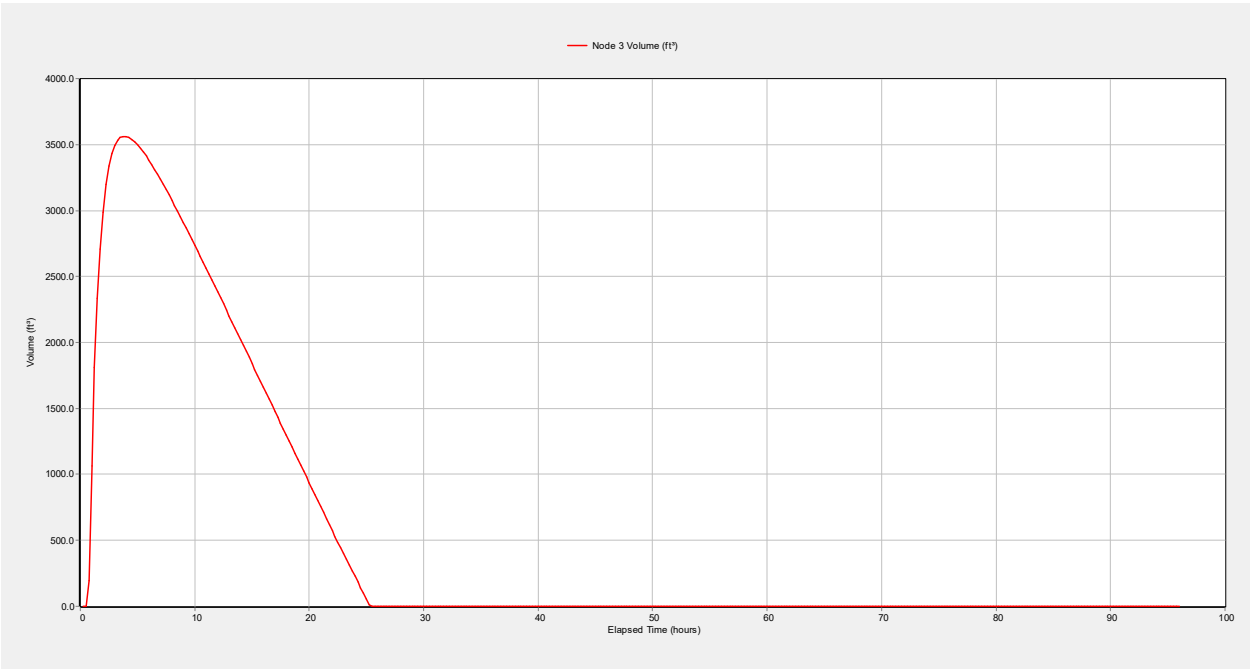
219
220 [VERTICES]
221 ;;Link X-Coord Y-Coord
222 ;;-----
223 1 -611.015 6282.272
224 2 -817.556 5576.592

225
226 [Polygons]
227 ;;Subcatchment X-Coord Y-Coord
228 ;;-----
229 1 2383.821 6746.988
230 1 3829.604 5645.439
231 1 3709.122 4526.678
232 1 1850.258 4543.890
233 1 1987.952 6712.565

234
235 [SYMBOLS]
236 ;;Gage X-Coord Y-Coord
237 ;;-----
238 ColoradoSprings 834.768 7228.916

239
240

Time to Drain WQCV



Water Quality Storm Report

 NOTE: The summary statistics displayed in this report are
 based on results found at every computational time step,
 not just on results from each reporting time step.

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed NO

Water Quality NO

Infiltration Method HORTON

Flow Routing Method KINWAVE

Starting Date 04/20/2022 00:00:00

Ending Date 04/24/2022 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 30.00 sec

	Volume acre-feet	Depth inches
*****	-----	-----
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	0.166	0.671
Evaporation Loss	0.000	0.000
Infiltration Loss	0.045	0.184
Surface Runoff	0.107	0.434
Final Storage	0.014	0.055
Continuity Error (%)	-0.165	

	Volume acre-feet	Volume 10 ⁶ gal
*****	-----	-----
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.107	0.035
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.000	0.000
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.107	0.035
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.000	0.000
Continuity Error (%)	0.000	

 Highest Flow Instability Indexes

All links are stable.

```

70 Routing Time Step Summary
71 *****
72 Minimum Time Step      :    30.00 sec
73 Average Time Step      :    30.00 sec
74 Maximum Time Step      :    30.00 sec
75 Percent in Steady State :     0.00
76 Average Iterations per Step :     1.00
77 Percent Not Converging  :     0.00

```

```

80 *****
81 Subcatchment Runoff Summary
82 *****

```

```

85 -----
86                                     Total      Total      Total      Total      Imperv
87                                     Perv      Total      Total      Peak      Runoff
88                                     Precip    Runon     Evap      Infil      Runoff
89 Subcatchment                      Runoff    Runoff    Runoff    Runoff    Coeff
90 in                               in          in        in        in        in
91                               10^6 gal      CFS

```

```

89 1                               0.67      0.00      0.00      0.18      0.43
90 0.00                          0.43      0.03      1.05      0.646

```

```

92 *****
93 Node Depth Summary
94 *****

```

```

96 -----
97                                     Average  Maximum  Maximum  Time of Max  Reported
98                                     Depth    Depth    HGL      Occurrence  Max Depth
99 Node                               Type      Feet     Feet     Feet     days hr:min  Feet
100 -----
101 2                                OUTFALL  0.00     0.00     0.00     0 00:00      0.00
102 3                                STORAGE   0.07     0.46     0.46     0 03:52      0.46

```

```

105 *****
106 Node Inflow Summary
107 *****

```

```

110 -----
111                                     Maximum  Maximum  Lateral
112                                     Total    Flow
113                                     Lateral  Total  Time of Max  Inflow
114                                     Inflow   Balance  Occurrence  Volume
115                                     Volume    Error
116 Node                               Type      CFS      CFS  days hr:min  10^6 gal  10^6
117 gal      Percent

```

```

115 2                                OUTFALL  0.00     0.00     0 00:00      0
116 0      0.000 gal
117 3                                STORAGE   1.05     1.05     0 00:55      0.0349
118 0.0349      -0.015

```

```

119 *****
120 Node Flooding Summary

```

No nodes were flooded.

Storage Volume Summary

Storage Unit	Average Max Volume Occurrence	Avg Maximum Pcnt	Evap Pcnt	Exfil Pcnt	Maximum Volume	Max Pcnt	Time of
hr:min	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days

3	0.514	1	0	100	3.563	8	0
03:51	0.05						

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
2	0.00	0.00	0.00	0.000
System	0.00	0.00	0.00	0.000

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
1	ORIFICE	0.00	0 00:00			0.00
2	DUMMY	0.00	0 00:00			

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Fri Jul 8 16:22:44 2022

Analysis ended on: Fri Jul 8 16:22:44 2022

Total elapsed time: < 1 sec

5-Year Storm Report

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed NO

Water Quality NO

Infiltration Method HORTON

Flow Routing Method KINWAVE

Starting Date 04/20/2022 00:00:00

Ending Date 04/24/2022 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 30.00 sec

Runoff Quantity Continuity

Volume

Depth

acre-feet

inches

Total Precipitation

0.351

1.421

Evaporation Loss

0.000

0.000

Infiltration Loss

0.096

0.389

Surface Runoff

0.242

0.980

Final Storage

0.014

0.055

Continuity Error (%)

-0.224

Flow Routing Continuity

Volume

Volume

acre-feet

10^6 gal

Dry Weather Inflow

0.000

0.000

Wet Weather Inflow

0.242

0.079

Groundwater Inflow

0.000

0.000

RDII Inflow

0.000

0.000

External Inflow

0.000

0.000

External Outflow

0.103

0.033

Flooding Loss

0.000

0.000

Evaporation Loss

0.000

0.000

Exfiltration Loss

0.139

0.045

Initial Stored Volume

0.000

0.000

Final Stored Volume

0.000

0.000

Continuity Error (%)

0.000

Highest Flow Instability Indexes

All links are stable.

Routing Time Step Summary

Minimum Time Step : 30.00 sec

Average Time Step : 30.00 sec

Maximum Time Step : 30.00 sec

% of Time in Steady State : 0.00

70 Average Iterations per Step : 1.00
71 % of Steps Not Converging : 0.00
72
73

74 *****
75 Subcatchment Runoff Summary
76 *****
77
78

79 Total Total Total Total Imperv
80 Perv Total Total Peak Runoff
81 Precip Runon Evap Infil Runoff
82 Runoff Runoff Runoff Runoff Coeff
83 in in in in in
84 10^6 gal CFS
85

83 1 1.42 0.00 0.00 0.39 0.98
84 0.00 0.08 3.35 0.690
85

86 *****
87 Node Depth Summary
88 *****
89

90
91 Average Maximum Maximum Time of Max Reported
92 Depth Depth HGL Occurrence Max Depth
93 Node Type Feet Feet Feet days hr:min Feet
94 -----
95 2 OUTFALL 0.00 0.00 0.00 0 00:00 0.00
96 3 STORAGE 0.13 0.93 0.93 0 02:13 0.93
97
98

99 *****
100 Node Inflow Summary
101 *****
102
103

104 Maximum Maximum Lateral
105 Total Flow Inflow
106 Lateral Total Time of Max Inflow
107 Inflow Balance Occurrence Volume
108 Volume Error
109 Node Type CFS CFS days hr:min 10^6 gal 10^6
110 gal Percent
111

109 2 OUTFALL 0.00 0.39 0 02:13 0
110 0.0335 0.000
111 3 STORAGE 3.35 3.35 0 00:50 0.0788
112 0.0788 0.005
113

114 *****
115 Node Flooding Summary
116 *****
117

118 No nodes were flooded.
119
120

Storage Volume Summary

Storage Unit hr:min CFS	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
----------------------------	---	--------------------------------	----------------------	-----------------------	-------------------------------	---------------------	-----------------

3 02:12 0.45	0.977	2	0	58	7.408	16	0
-----------------	-------	---	---	----	-------	----	---

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
2	9.51	0.14	0.39	0.033
System	9.51	0.14	0.39	0.033

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
1	ORIFICE	0.39	0 02:13			0.00
2	DUMMY	0.00	0 00:00			

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Fri Jul 8 16:58:35 2022
Analysis ended on: Fri Jul 8 16:58:35 2022
Total elapsed time: < 1 sec

100-Year Storm Report

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed NO

Water Quality NO

Infiltration Method HORTON

Flow Routing Method KINWAVE

Starting Date 04/20/2022 00:00:00

Ending Date 04/24/2022 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 30.00 sec

Runoff Quantity Continuity

Volume

Depth

acre-feet

inches

Total Precipitation

0.737

2.988

Evaporation Loss

0.000

0.000

Infiltration Loss

0.200

0.811

Surface Runoff

0.526

2.131

Final Storage

0.014

0.055

Continuity Error (%)

-0.308

Flow Routing Continuity

Volume

Volume

acre-feet

10^6 gal

Dry Weather Inflow

0.000

0.000

Wet Weather Inflow

0.526

0.171

Groundwater Inflow

0.000

0.000

RDII Inflow

0.000

0.000

External Inflow

0.000

0.000

External Outflow

0.375

0.122

Flooding Loss

0.000

0.000

Evaporation Loss

0.000

0.000

Exfiltration Loss

0.150

0.049

Initial Stored Volume

0.000

0.000

Final Stored Volume

0.000

0.000

Continuity Error (%)

0.051

Highest Flow Instability Indexes

All links are stable.

Routing Time Step Summary

Minimum Time Step : 30.00 sec

Average Time Step : 30.00 sec

Maximum Time Step : 30.00 sec

% of Time in Steady State : 0.00

70 Average Iterations per Step : 1.00
71 % of Steps Not Converging : 0.00
72
73

74 *****
75 Subcatchment Runoff Summary
76 *****
77
78

79 Total Total Total Total Imperv
80 Perv Total Total Peak Runoff
81 Precip Runon Evap Infil Runoff
82 Runoff Runoff Runoff Runoff Coeff
83 in in in in in
84 Subcatchment
85 in in 10^6 gal CFS

83 1 2.99 0.00 0.00 0.81 2.12
84 0.01 2.13 0.17 9.76 0.713
85

86 *****
87 Node Depth Summary
88 *****
89

90
91 Average Maximum Maximum Time of Max Reported
92 Depth Depth HGL Occurrence Max Depth
93 Node Type Feet Feet Feet days hr:min Feet
94 -----
95 2 OUTFALL 0.00 0.00 0.00 0 00:00 0.00
96 3 STORAGE 0.18 1.86 1.86 0 01:53 1.86
97

98
99 *****
100 Node Inflow Summary
101 *****
102
103

104 Maximum Maximum Lateral
105 Total Flow
106 Lateral Total Time of Max Inflow
107 Inflow Balance Occurrence Volume
108 Inflow Error
109 Volume CFS CFS days hr:min 10^6 gal 10^6
110 Node Type
111 gal Percent

109 2 OUTFALL 0.00 1.07 0 01:53 0
110 0.122 0.000
111 3 STORAGE 9.76 9.76 0 00:45 0.171
112 0.171 0.052
113

114 *****
115 Node Flooding Summary
116 *****
117

118 No nodes were flooded.
119
120

Storage Volume Summary

Storage Unit hr:min	CFS	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
------------------------	-----	--	--------------------------------	----------------------	-----------------------	-------------------------------	---------------------	-----------------

3 01:52	1.14	1.405	3	0	29	15.718	35	0
------------	------	-------	---	---	----	--------	----	---

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
2	12.00	0.39	1.07	0.122
System	12.00	0.39	1.07	0.122

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
1	ORIFICE	1.07	0 01:53			0.00
2	DUMMY	0.00	0 00:00			

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Fri Jul 8 17:00:44 2022
Analysis ended on: Fri Jul 8 17:00:44 2022
Total elapsed time: < 1 sec

STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

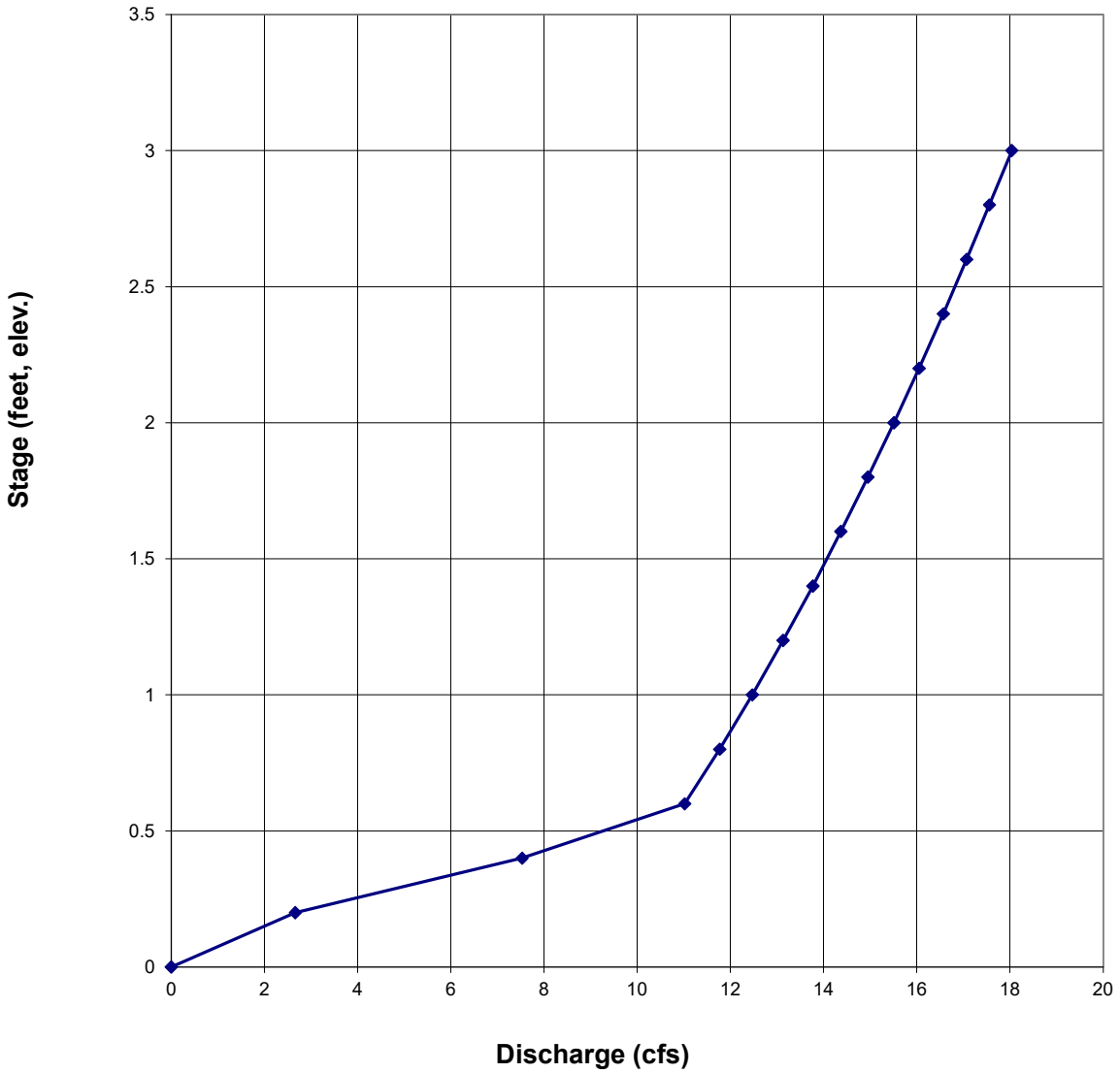
7/8/2022, 4:20 PM

STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

Project: _____

Basin ID: _____

STAGE-DISCHARGE CURVE FOR THE OUTLET STRUCTURE

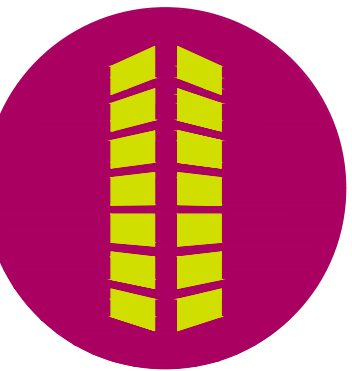


APPENDIX F

Drainage Maps

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6855 CONSTITUTION AVE. STORAGE SITE
COMMERCIAL DEVELOPMENT
DRAINAGE MAP
FOR JOHNSON DEVELOPMENT ASSOCIATES

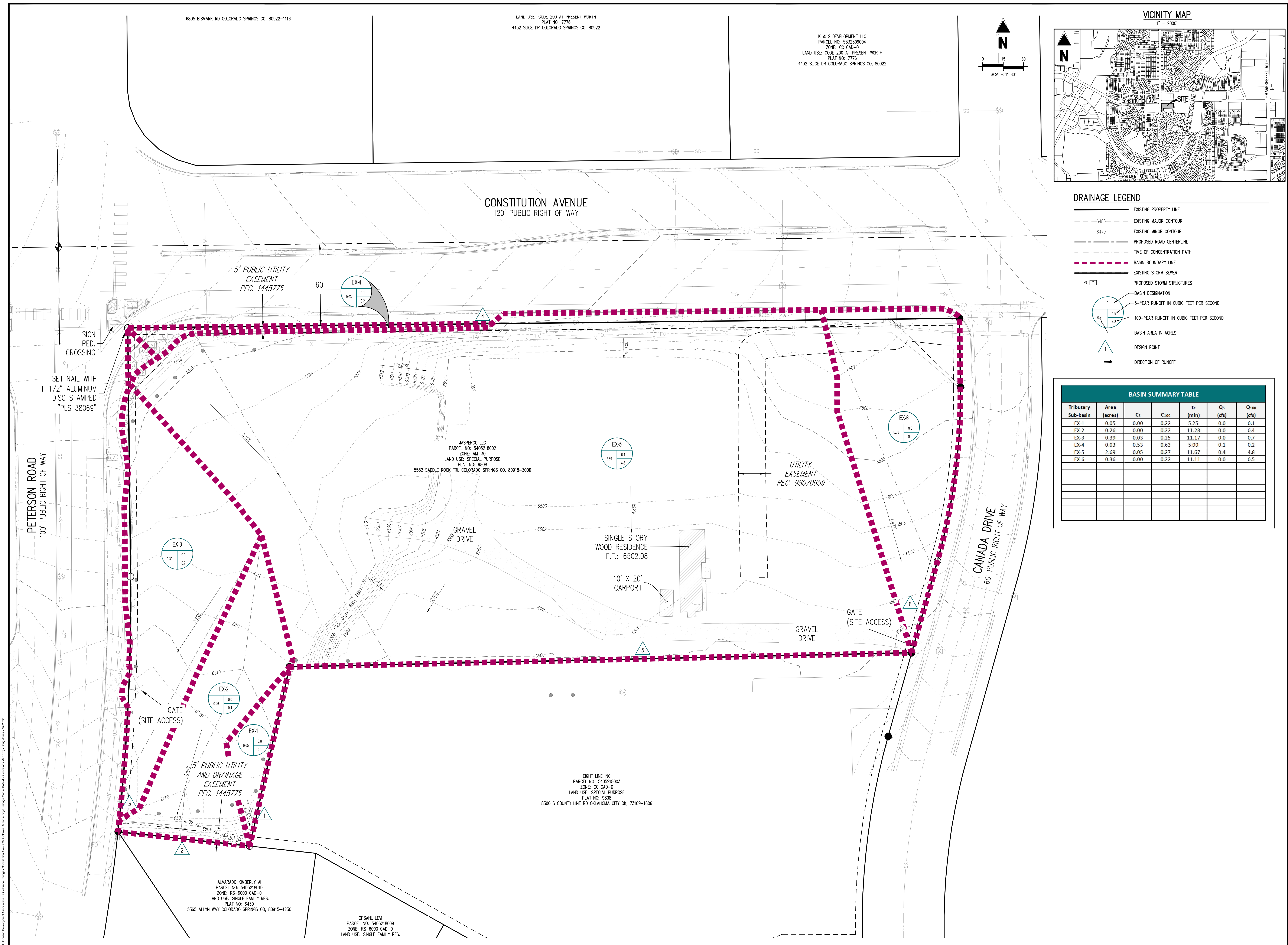
LOT 1 OF THE EIGHT LINE SUBDIVISION
COLORADO SPRINGS, CO 80915

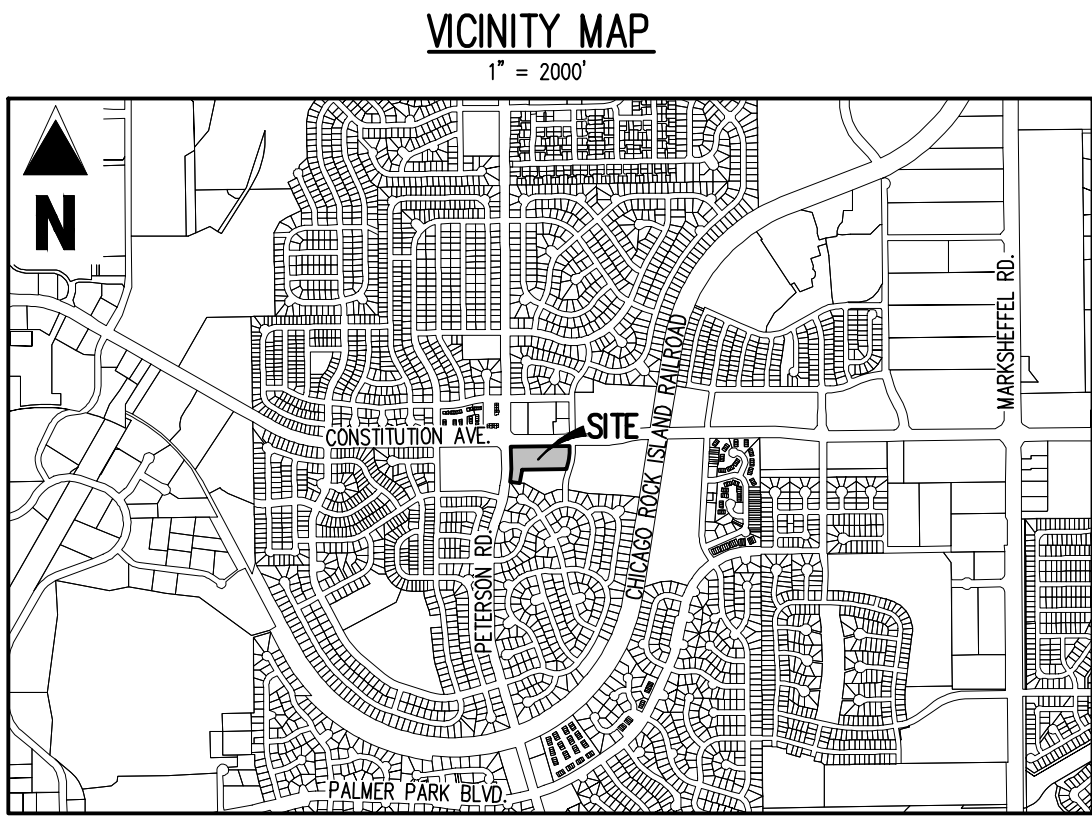
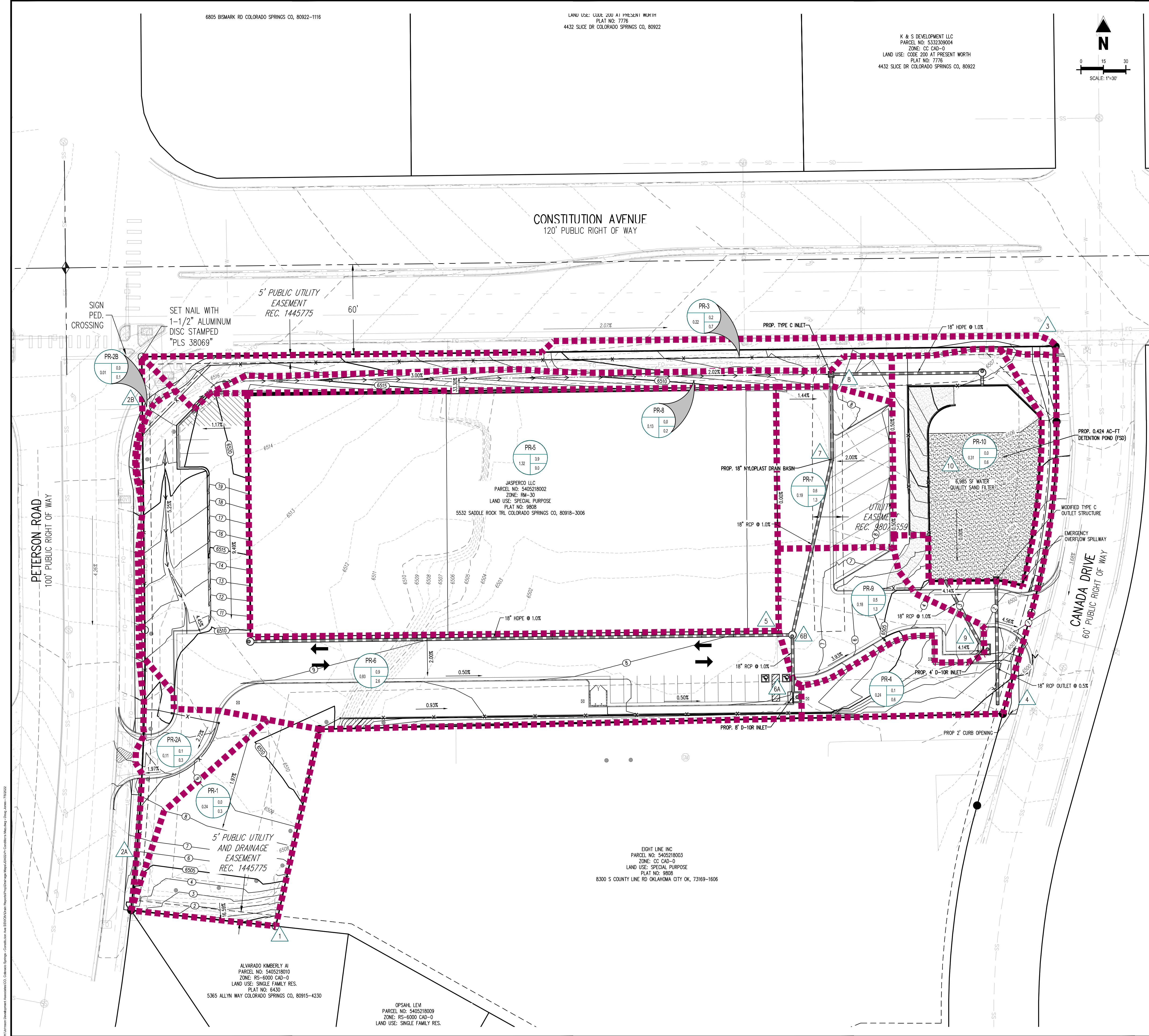
[illegible]

Project No:	JDA02.20
Drawn By:	BAS
Checked By:	BAS
Date:	07.08.2022

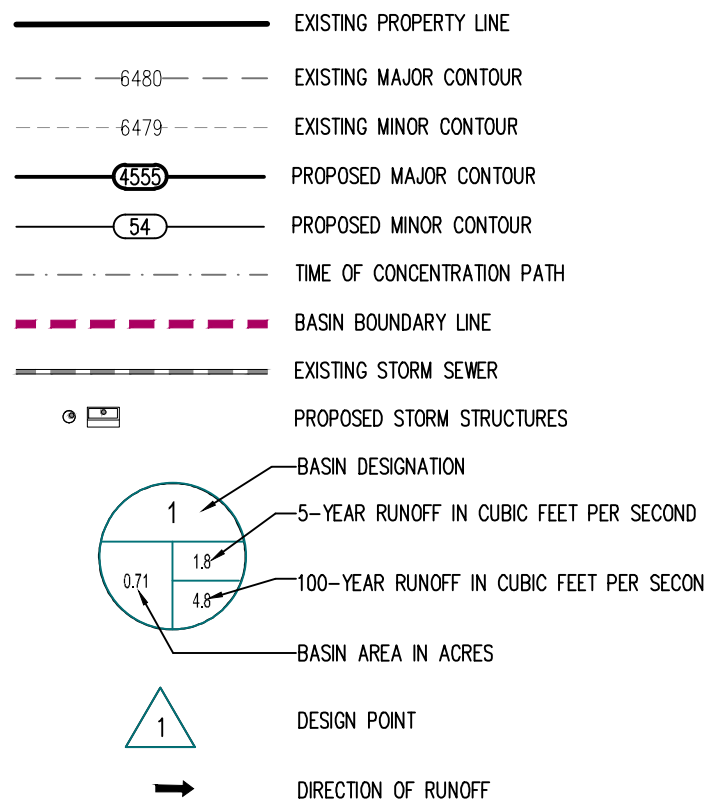
EXISTING DRAINAGE MAP

DR-1





DRAINAGE LEGEND



BASIN SUMMARY TABLE						
Tributary Sub-basin	Area (acres)	Cs	C100	tc (min)	Qs (cfs)	Q100 (cfs)
PR-1	0.24	0.00	0.22	10.8	0.0	0.3
PR-2A	0.11	0.25	0.41	8.3	0.1	0.3
PR-2B	0.01	0.51	0.62	5.0	0.0	0.1
PR-3	0.22	0.20	0.38	5.0	0.2	0.7
PR-4	0.24	0.16	0.35	9.1	0.1	0.6
PR-5	1.32	0.71	0.79	5.0	3.9	9.0
PR-6	0.83	0.36	0.49	12.4	0.9	2.6
PR-7	0.19	0.74	0.81	5.0	0.6	1.3
PR-8	0.13	0.00	0.22	10.0	0.0	0.2
PR-9	0.18	0.73	0.80	5.0	0.5	1.3
PR-10	0.31	0.00	0.22	5.0	0.0	0.6
Routed Flow to FSD (DP-10)					4.6	11.8
Total Offsite Free-Release (PR-1, PR-2A, PR-2B, PR-3, PR-4)					0.4	2.0

DESIGN POINT SUMMARY TABLE		
Design Point	Routed Flows	
	Qs (cfs)	Q100 (cfs)
1	0.0	0.3
2A	0.1	0.3
2B	0.0	0.1
3	0.2	0.7
4	0.1	0.6
5	3.9	9.0
6A	0.9	2.6
6B	3.8	9.3
7	4.2	10.2
8	4.2	10.4
9	0.5	1.3
10	4.6	11.8

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6855 CONSTITUTION AVE. STORAGE SITE
COMMERCIAL DEVELOPMENT
DRAINAGE MAP
FOR JOHNSON DEVELOPMENT ASSOCIATES
LOT 1 OF THE EIGHT LINE SUBDIVISION
COLORADO SPRINGS, CO 80915

#	Date	Issue / Description	Init.
1			
2			
3			
4			
5			
6			
7			
8			
9			
10			

Project No: JDA02.20
Drawn By: BAS
Checked By: BAS
Date: 07.08.2022

PROPOSED DRAINAGE
MAP