# Pavement Study
# Trails at Aspen Ridge, Filing 4
# El Paso County, Colorado
# PCD File No. PAV2610

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**Project Number 252742-P1**
**July 7, 2026**
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## 1.0 EXECUTIVE SUMMARY

AGW completed the pavement study for the proposed streets to be constructed at the subject site. This study was revised to address the review comments provided by El Paso County. This study was conducted in general conformance with the El Paso County pavement design procedures. The following pavement study summarizes the field exploration, subsurface conditions encountered, laboratory tests performed, and the pavement recommendations.

The subsurface materials encountered in our test borings consisted of slightly sandy to sandy clay fill with varying portions of gravel overlying claystone bedrock. Ground water was not encountered at the time of drilling. Based on our sampling and laboratory testing, expansive subgrade mitigation per El Paso County is required.

The pavement recommendations for the local residential streets are a composite section of 5.5 inches of asphalt concrete overlying 19.0 inches of aggregate base course. The pavement recommendations for the residential collector are a composite section of 6.5 inches of asphalt concrete overlying 22.0 inches of aggregate base course. The pavement sections include 12.0 inches of aggregate base course for expansive subgrade mitigation. Chemical treatment of the subgrade is not planned to be performed. Therefore, we request a deviation (variance) to use aggregate base course for expansive subgrade mitigation. We encourage the Client to read this study in its entirety and not rely solely on the cursory information contained in this summary.

## 2.0 PURPOSE

The purpose of this study was to provide pavement thickness recommendations for the subject site in general conformance with the "El Paso County Engineering Criteria Manual" (Manual). This study was revised to address the review comments provided by El Paso County. This study presents the analysis of approximately 3,600 feet of local residential streets and 400 feet minor collector streets. Factual data gathered during the field and laboratory work and our analyses are summarized on Figures 1 through 6 and in Appendices A and B. Our opinions and recommendations shown in this study are based on the data generated during this field exploration, laboratory testing, and our experience with similar projects.

## 3.0 PROPOSED CONSTRUCTION

Based on the "Trails at Aspen Ridge Filing No. 4 - Roadway & Storm Improvement Plan" prepared by Matrix Design Group, Inc., Project No. 21.886.038, dated July 2025 (Plans), the local residential streets have a right-of-way (ROW) width of 50 feet with two travel lanes, curb, gutter, and attached sidewalks. The minor collector street has a ROW width of 80 feet with two travel lanes, a center turn lane, shoulders, curb, gutter, and detached sidewalks. These streets will be paved with asphalt concrete sloped with a 2% crown.

## 4.0 FIELD EXPLORATION

The subgrade soils were sampled by drilling 17 test borings within the proposed street alignments at the locations shown on Figure 1. The test borings were drilled after sanitary sewer installation to depths of 5 to 10 feet with disturbed bulk samples collected in the upper 5 feet of rough subgrade elevation. Samples of the subsurface materials were obtained using a Modified California sampler which was driven into the soil by dropping a 140-pound hammer through a free fall of 30 inches. The Modified California sampler is a 2.5-inch outside diameter by 2-inch inside diameter device. The number of blows required for the sampler to penetrate 12 inches and/or the number of inches that the sampler is driven by 50 blows gives an indication of the consistency or relative density of the soils and bedrock. Results of the penetration tests are presented on the "Test Boring Logs", Figures 3 through 6. Ground water was not encountered at the time of drilling.

## 5.0 LABORATORY TESTING

The samples obtained during drilling were returned to the laboratory where they were visually classified by a geotechnical engineer. Laboratory testing was then assigned to specific samples to evaluate their engineering properties. The laboratory tests included gradation analysis and Atterberg limits to evaluate grain size distribution and plasticity. Swell-consolidation testing was conducted to evaluate the effect of wetting under load on selected samples. Representative samples were tested for density, moisture content, and water-soluble sulfate concentration. Selected bulk samples were combined and tested for standard Proctor and resilient modulus to determine the subgrade support strength. The test results are summarized on Figures 3 through 6 and are included in Appendix A.

## 6.0 SUBSURFACE CONDITIONS

The subsurface materials encountered in our test borings consisted of slightly sandy to sandy clay fill with varying portions of gravel overlying claystone bedrock. According to the AASHTO Soil Classification system, the soils from the bulk samples collected classify as A-6 (17 to 24) and A-7-6 (22 to 28). Fill was encountered in all 17 test borings and was between 5 to 10 feet thick. AGW performed moisture-density testing during overlot grading and sanitary utility backfill operations (AGW Project Number 252742). Claystone bedrock was encountered in three of the test borings at depths ranging from 6 to 7 feet. Ground water was not encountered at the time of drilling.

## 7.0 WATER-SOLUBLE SULFATES

The Colorado Department of Transportation (CDOT) stipulates requirements for the risk of sulfate exposure on concrete structures based on Table 601-2 of the "Standard Specifications for Road and Bridge Construction (2023)". The water-soluble sulfate concentration of the samples tested ranged from 5,600 parts per million (ppm) to 7,800 ppm. Based on these results, the sulfate concentrations represent a Class 2 risk of sulfate exposure. We recommend concrete structures bearing upon onsite materials meet the requirements stipulated in Section 601.04 of the CDOT "Standard Specifications for Road and Bridge Construction". A high sulfate resistant Portland cement or double application will be required for chemical treatment of the subgrade. Chemical treatment of the subgrade is not planned for this site given the request for a variance included in Section 1.0.

## 8.0 EXPANSIVE SUBGRADE CONDITIONS

The Manual stipulates subgrade soils requiring expansive subgrade mitigation be discussed in the pavement design. Subgrade soils exhibiting 2% or greater swell potential require expansive subgrade mitigation. Swell-consolidation tests were conducted to determine expansion potential under a surcharge load of 200 pounds per square foot (psf). The test results exhibited swells ranging from 0.7 to 4.7%. Based on our sampling and laboratory testing, expansive subgrade mitigation per El Paso County is required. Expansive subgrade mitigation consists of removal of a minimum of 12.0 inches of subgrade and replacement with CDOT "Class 6" aggregate base course below the designed pavement section. Composite (multi-layered) pavements are considered less likely to exhibit edge line cracking. An intermediate layer creates a transition zone within the pavement system that aids in the distribution of stress over the weaker subgrade materials. Prior to placement of the aggregate base course, the subgrade should be prepared to a minimum depth of 12 inches.

## 9.0 SUBGRADE SUPPORT

The pavement subgrade support strength of soils is based on the resilient modulus ($M_R$). The resilient modulus is a measure of the elastic property of soil, which is dependent upon moisture content, density, and the applied stress level. Section D.2.4 of the Manual stipulates performing an R-value or California Bearing Ratio (CBR) to correlate the resilient modulus. The soils encountered at the site are considered to provide very poor subgrade support characteristics likely yielding an R-value of less than 5 or CBR less than 3. AGW typically performs an $M_R$ test based on AASHTO T307 the determine the subgrade support strength based on a specific dry density and moisture content. The soils encountered in Test Borings 5 and 10 as representative of A-7-6 (26 and 28) were combined and tested for standard Proctor and $M_R$. The $M_R$ testing was performed on a sample remolded to a minimum of 95% of standard Proctor (ASTM D698) maximum dry density at approximately 3% above optimum moisture content. The resilient modulus testing exhibited an $M_R$ of 3,964 psi. We found this value to be reasonable for the soils encountered. Based on Table 9-8 of the Mechanistic Empirical Pavement Design Guide (MEPDG), R-value Equation No. 2 ($M_R$ = 1,155 +555 (R-value)) correlates to an R-value of 5.

## 10.0 TRAFFIC CONSIDERATIONS

Based on the Manual and the Plans, the proposed streets at the site classify as local residential and collector. The Manual stipulates default Equivalent Single Axle Load (ESALs (18-kip)) values for each classification based on a 20-year design period. The default ESAL values appear higher than those typically adopted by other municipalities. However, Section D.3.2 of the Manual requires using the minimum ESAL default values if no actual traffic data is available. The following table summarizes the design criteria.

| Street Classification | ESALs | Reliability (%) | Serviceability Index |
|---|---|---|---|
| Local Residential | 292,000 | 80 | 2.5 |
| Minor Collector | 821,000 | 85 | 2.0 |

## 11.0 PAVEMENT THICKNESS RECOMMENDATIONS

The pavement thickness recommendations were calculated using the 1993 AASHTO Pavement Design, DARWin Pavement Design and Analysis System computer program. Based on the design criteria referenced above, the expansive subgrade mitigation, and the calculations included in Appendix B, the following pavement thicknesses are recommended. This pavement sections meet or exceed the minimum required by El Paso County. The pavement thicknesses are provided on the table below and are shown on Figure 2.

| Street Classification | Alternate | ACS (in) | ABC (in) | Total (in) |
|---|---|---|---|---|
| Local Residential (ESAL = 292,000; $M_R$ = 3,964 psi) | A | 5.5 | 19.0 | 24.5 |
| Residential Collector (ESAL = 821,000; $M_R$ = 3,964 psi) | A | 6.5 | 22.0 | 28.5 |

ACS – Asphalt Concrete Surface
ABC – Aggregate Base Course
Note: The alternates include the removal of 12.0 inches of subgrade and replacement with an additional 12.0 inches of CDOT "Class 6" aggregate base course for expansive subgrade mitigation.

Section D.4.1.F of the Manual limits the thickness of aggregate base course (ABC) credited in the structural pavement section to 2.5 times the asphalt thickness. Although the total ABC thickness shown for the alternatives in the table above exceeds this ratio, 12.0 inches of ABC is designated for expansive subgrade mitigation and is not credited toward the structural pavement thickness.

In our experience, the intermediate ABC layer provides a transition between the structural pavement section and the weaker subgrade, helping distribute pavement loads over a broader area. The recommended alternatives use this layer to provide a buffer between the structural pavement section and the underlying expansive soils.

Proper and timely maintenance will be required during the lifetime of the pavement to reach the designed service life. Pavement maintenance recommendations are provided in "Pavement Maintenance".

## 12.0 DRAINAGE CONSIDERATIONS

Long-term pavement performance is aided by proper drainage. Surface drainage is necessary for water to drain into the proper collection system instead of fully infiltrating into the subgrade soils below the pavement structure. If the pavement is not properly drained, the soils below the pavement structure may become saturated, and the subgrade will lose strength, ultimately affecting the performance of the pavement layers above (generally from imposed traffic loads). A drain system may aid pavement performance near irrigated areas. Excessive irrigation could negatively impact the pavement structure. In addition, xeriscaping the landscaped areas is recommended.

## 13.0 GENERAL DISCUSSION

Several municipalities in the region allow vertical residential construction prior to the completion of the designed pavement structure (i.e., after placement of the bottom lift of asphalt). Construction traffic during the buildout phase often exceeds the anticipated daily traffic volume on residential streets. Pavement distress may occur on incomplete pavement structures because of construction traffic. Full placement of the designed pavement structure prior to vertical residential construction should be considered or a minimum of two lifts of pavement should be paved before vertical construction begins. In addition, bottom lift only paving allows accumulation of water since the drainage structures cannot be effectively used. This could result in wetting of the subgrade soils and may result in weakening of the pavement structure.

## 14.0 CONSTRUCTION RECOMMENDATIONS

The following recommendations are intended as a guideline and not as replacement for the jurisdictional standards and specifications. It shall be the responsibility of the Contractor to abide by the standards and specifications stipulated in the Manual.

### 14.1 Subgrade

Prior to paving operations, the subgrade must be prepared in a manner that allows for adequate pavement support. The subgrade should only be prepared when ambient conditions will not prevent the Contractor from achieving the required density and moisture content. Frozen soil should never be used as subgrade fill. The entire subgrade should be proof-rolled with a loaded 988 front-end loader or similar heavy rubber-tired vehicle (GVW of 50,000 pounds with 18-kip per axle at tire pressures of 90 pounds per square inch (psi)) to detect any soft or loose areas. All areas exhibiting unstable subgrade conditions such as loose soils, pumping, or excessive movement, should be overexcavated to a firm soil layer or to a maximum depth of 2 feet, whichever is shallowest, and replaced with suitable compacted fill. If unstable subgrade conditions persist, AGW should be contacted for our opinion.

If no unstable areas are observed during the proof-roll or after removal and replacement of unsuitable soils, the entire subgrade may be prepared by windrowing, tilling, or by removing a minimum of 12 inches of subgrade from proposed pavement subgrade elevation. If necessary, add or reduce moisture to the required moisture content. The subgrade fill should be placed in maximum 8-inch loose lifts and compacted to a minimum of 95% of standard Proctor (ASTM D698) maximum dry density at optimum to +3.0% of optimum moisture content for A-6 and A-7-6 soils. The fill should be compacted to a minimum of 95% of modified Proctor (ASTM D1557) maximum dry density at −2.0% to +2.0% of optimum moisture content for other soil types. If additional fill is required to reach the pavement subgrade elevation, the fill should have a soil classification similar to or better than the poorest soils encountered during this study. The subgrade should be free of organics, vegetation, large rocks, or any other deleterious materials. The pavement subgrade should be crowned to the appropriate grade lines. Additional compactive effort should be applied along edged concrete structures such as curbs and crosspans.

### 14.2 Aggregate Base Course

Aggregate base course (ABC) should consist of aggregate which meets specifications for gradation, plasticity, abrasion wear, and strength. We recommend the use of material meeting CDOT "Class 6" specifications and having an R-value ≥ 78. The ABC should be tested to determine compliance with these specifications prior to use. The ABC should be placed in loose lifts not exceeding 8 inches and should be compacted to a minimum of 95% of modified Proctor maximum dry density (ASTM D1557). Aggregate thicknesses exceeding 8 inches should be placed and compacted in two separate lifts. The ABC should not be placed when weather conditions prevent achievement of the required compaction.

### 14.3 Asphalt Concrete Surface

Asphalt material should conform to an agency approved mix design that states the SHRP Gyratory design properties (i.e., maximum density, optimum asphalt content, job mix formula, recommended mixing and placing temperatures, etc.). We recommend that the aggregate used in the asphalt meet CDOT "Grading S", "Grading SX", or equivalent regulatory aggregate specifications. If the material does not meet or exceed these specifications, the asphalt thickness should be revised. The asphalt material should be placed in lifts a minimum of three times the aggregate size and should be compacted to 92 to 96% of Theoretical Maximum Specific Gravity for S and SX Super Pave mixes. The asphalt material should be compacted to 93 to 97% of Theoretical Maximum Specific Gravity for SMA Super Pave mixes. Materials standards and specifications in the Manual are required. Asphalt binder selection should be appropriate for each roadway classification. The paving contractor is responsible for mix submittal to the agency. Asphalt concrete should not be placed when weather conditions are such that the materials cannot be properly placed or compacted. The asphalt concrete should be placed on a prepared surface, graded to the appropriate elevation. In no case should the asphalt concrete be placed on frozen subgrade or base. When applicable, a tack coat should be applied at joints, adjacent to curbs, gutters or crosspans. The Contractor is responsible for establishing rolling patterns to determine the amount of effort required to meet the compaction requirements. Field testing conducted by AGW will not relieve the Contractor from proper compaction and construction of the pavement.

## 15.0 PAVEMENT MAINTENANCE

Flexible pavement structures are typically designed for a service period of 20 years. However, timely and proper maintenance during the life of the pavement is essential to reach the designed service period and to possibly extend the serviceability of the pavement. We recommend implementing a maintenance program aimed at preserving the structural integrity of the pavement. The implementation of available maintenance operations varies depending upon pavement type and on-site conditions. Flexible pavements will exhibit some type of pavement distress during their service life. Periodic maintenance and rehabilitation should be anticipated to reach the anticipated design life. Typically, minor cracks may develop within the first three years. Crack sealant should be used immediately upon recognition of these cracks to reduce further deterioration and/or potential moisture induced damage. The use of crack sealants may extend the life of the pavement by two to five years before any other treatment is applied. A variety of seal coats are available and can delay the need for a major surface structural treatment. However, careful engineering judgment should be used to determine the type of seal application that is most appropriate. Seal coats should not be

applied on pavements with severe cracks, raveling or potholes. Fog seals typically have an estimated service life of approximately one to two years but should only be used on structurally sound pavements. Slurry seals generally have a service life of four to seven years and are commonly used on pavements exhibiting no to low pavement distress. Chip seals aid in slowing surface oxidation, minor raveling, and sealing small cracks. Chip seals are considered to have a service life of approximately four to seven years. Structural mill and overlay are a rehabilitation technique that generally occurs within eight to 12 years after initial construction. This technique should only be used on stable pavements with minor surface distress and a strong base. Conventional structural mill and overlay operations are known to have a service life of eight to 14 years.

## 16.0 LIMITATIONS

This pavement study was based upon laboratory testing of samples obtained at widely spaced locations. Variations in subsoil conditions could occur between sample locations. We should evaluate and test the subgrade and pavement materials during construction to determine that our recommendations have been properly interpreted. However, AGW shall not be responsible for constant or exhaustive inspection of the work, the means and methods of construction or the safety procedures employed by Client's contractor. Client shall hold its contractor solely responsible for the quality and completion of the project, including construction in accordance with the construction documents. Any duty hereunder is for the sole benefit of the Client and not for any third party, including the contractor or any subcontractor. The Owner should be aware that this study was prepared utilizing the Manual standards. Highly plastic and expansive soils pose a significant risk to pavement structures. This risk includes heave and cracking upon wetting. In addition, utility backfill settlement is a risk of development that can affect pavement performance. The Client is aware that isolated to more wide-spaced damage may occur. Longitudinal cracking parallel to the curb line may be indicative of an expansive subgrade becoming wetted. The only positive solution is removal of the subgrade materials to the depth of wetting and replacement or treatment. The Manual specifications do not require that the Client take these measures, but the Client should be aware that these measures are the only solution to dealing with highly plastic and expansive soils. As this is generally economically unfeasible, this design may be used as an attempt to provide a reasonable cost-effective pavement structure. The Owner assumes all liability for the performance of this pavement structure. We are available to discuss the risks associated with this design.

A. G. Wassenaar, Inc.

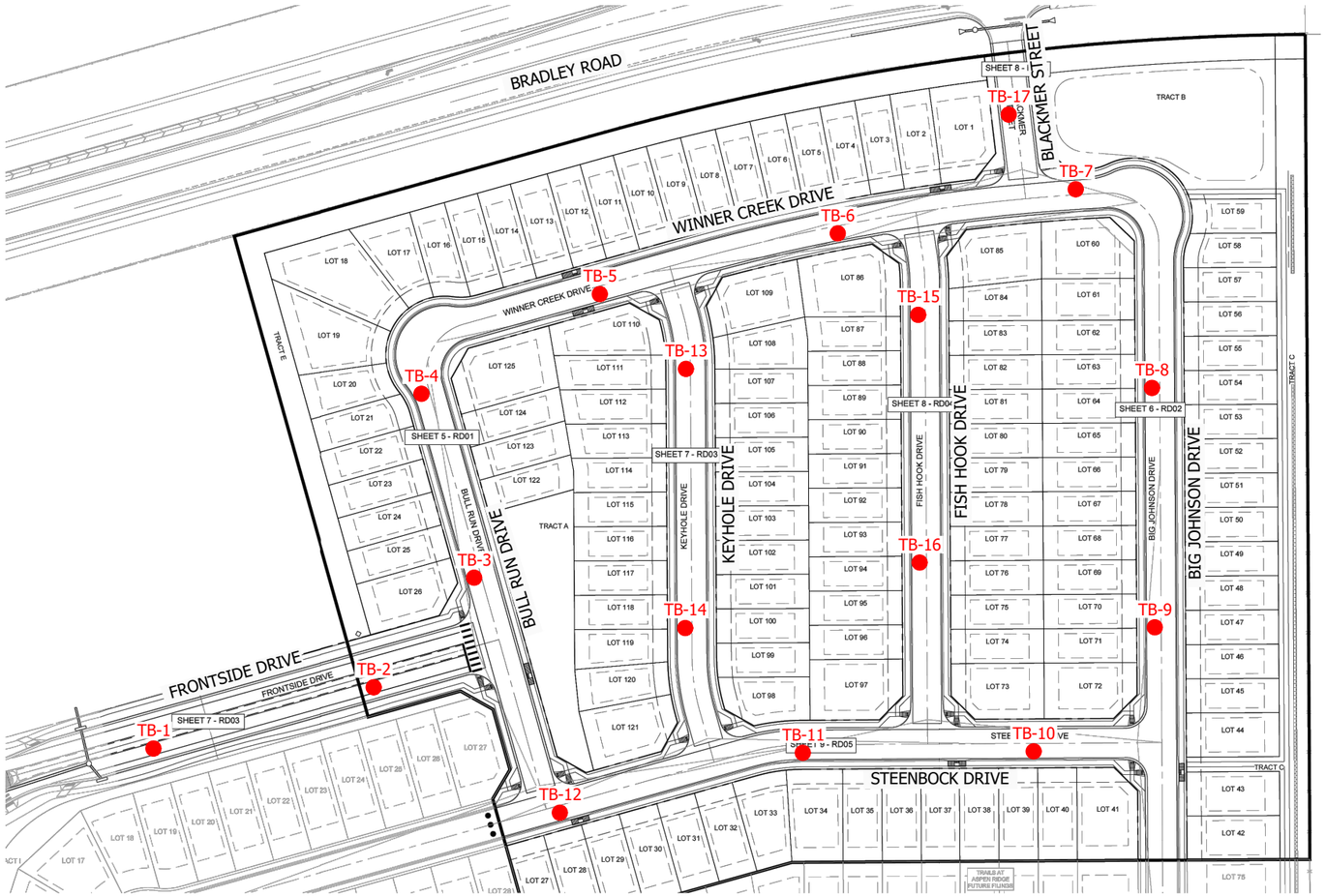
Pedro D. Manriquez, M.S., P.E.
Senior Geotechnical Engineer
Digitally signed by: Pedro D. Manriquez
Date: 2026.11.18 14:12:13 -07'00'

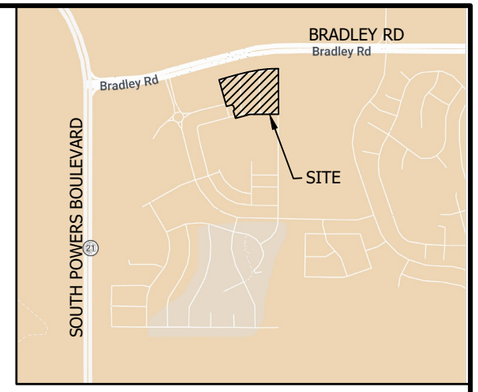
PDM/djp/pdm

# TRAILS AT ASPEN RIDGE, FILING 4
# EL PASO COUNTY, COLORADO

0 150 300

Scale in Feet




VICINITY MAP
NOT TO SCALE

NOTES:
1. TEST BORINGS ARE OVERLAID ON THE "TRAILS AT ASPEN RIDGE, FILING NO. 4, ROADWAY & STORM IMPROVEMENTS PLANS, ROAD CENTERLINE KEY MAP", SHEET 4 OF 32, PREPARED BY MATRIX DESIGN GROUP, INC., PROJECT NO. 21.886.038, DATED JANUARY, 2025.
2. ALL LOCATIONS ARE APPROXIMATE.

AGW

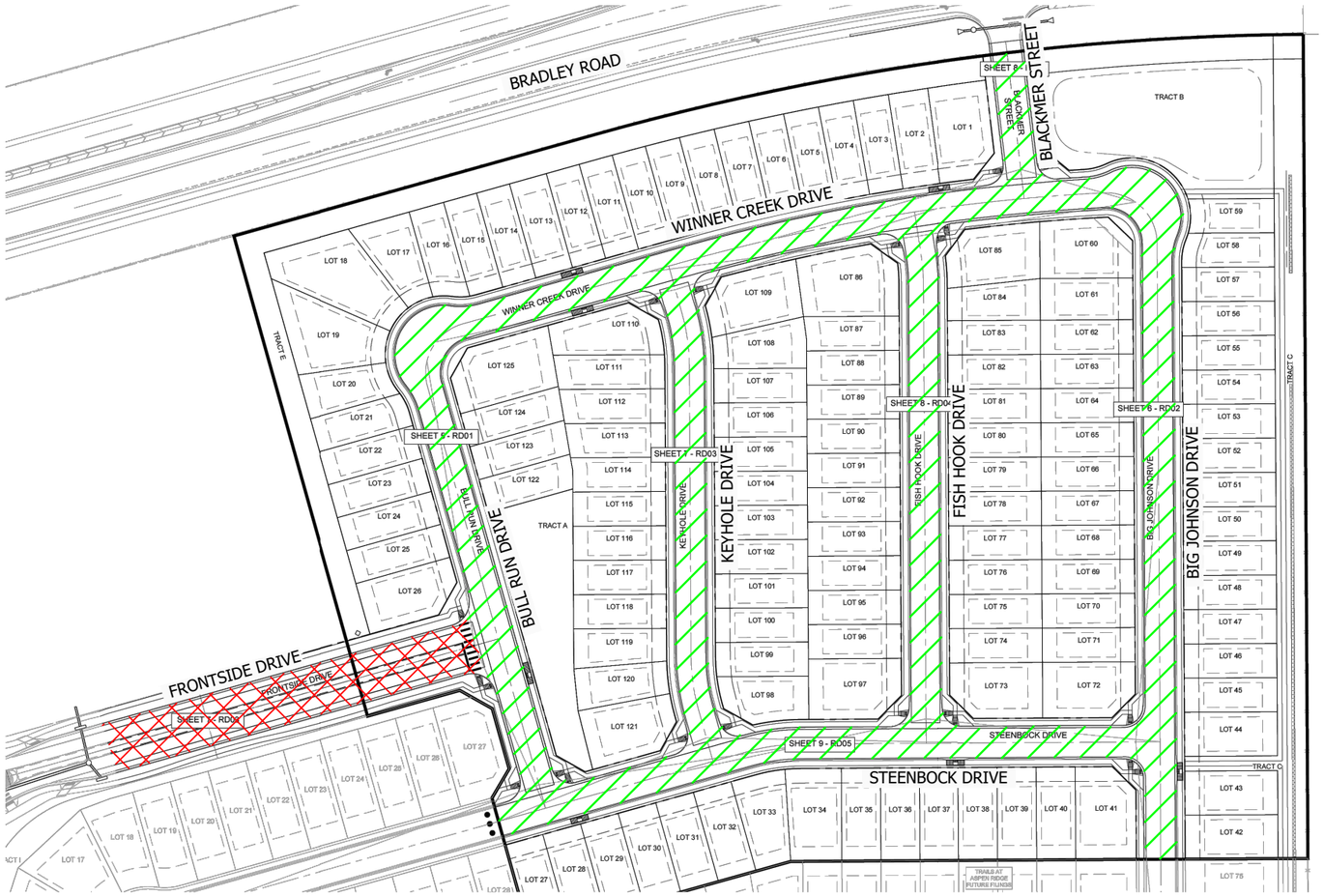
SITE PLAN
AND
VICINITY MAP

PROJECT NO. 252742-P1
FIGURE 1

# TRAILS AT ASPEN RIDGE, FILING 4
# EL PASO COUNTY, COLORADO

0 150 300

Scale in Feet




LOCAL RESIDENTIAL
(ESAL = 292,000; $M_R$ = 3,964 psi)

| ALT | ACS (IN) | ABC (IN) | TOTAL (IN) |
|---|---|---|---|
| A | 5.5 | 19.0 | 24.5 |

COLLECTOR
(ESAL = 821,000; $M_R$ = 3,964 psi)

| ALT | ACS (IN) | ABC (IN) | TOTAL (IN) |
|---|---|---|---|
| A | 6.5 | 22.0 | 28.5 |

ALT - ALTERNATE
ACS - ASPHALT CONCRETE SURFACE
ABC - AGGREGATE BASE COURSE

NOTE: THE ALTERNATES INCLUDE REMOVAL OF A MINIMUM OF 12.0 INCHES OF SUBGRADE AND REPLACEMENT WITH CDOT "CLASS 6" AGGREGATE BASE COURSE FOR EXPANSIVE SUBGRADE MITIGATION.

NOTES:
1. TEST BORINGS ARE OVERLAID ON THE "TRAILS AT ASPEN RIDGE, FILING NO. 4, ROADWAY & STORM IMPROVEMENTS PLANS, ROAD CENTERLINE KEY MAP", SHEET 4 OF 32, PREPARED BY MATRIX DESIGN GROUP, INC., PROJECT NO. 21.886.038, DATED JANUARY, 2025.
2. ALL LOCATIONS ARE APPROXIMATE.

AGW

PAVEMENT THICKNESS RECOMMENDATIONS

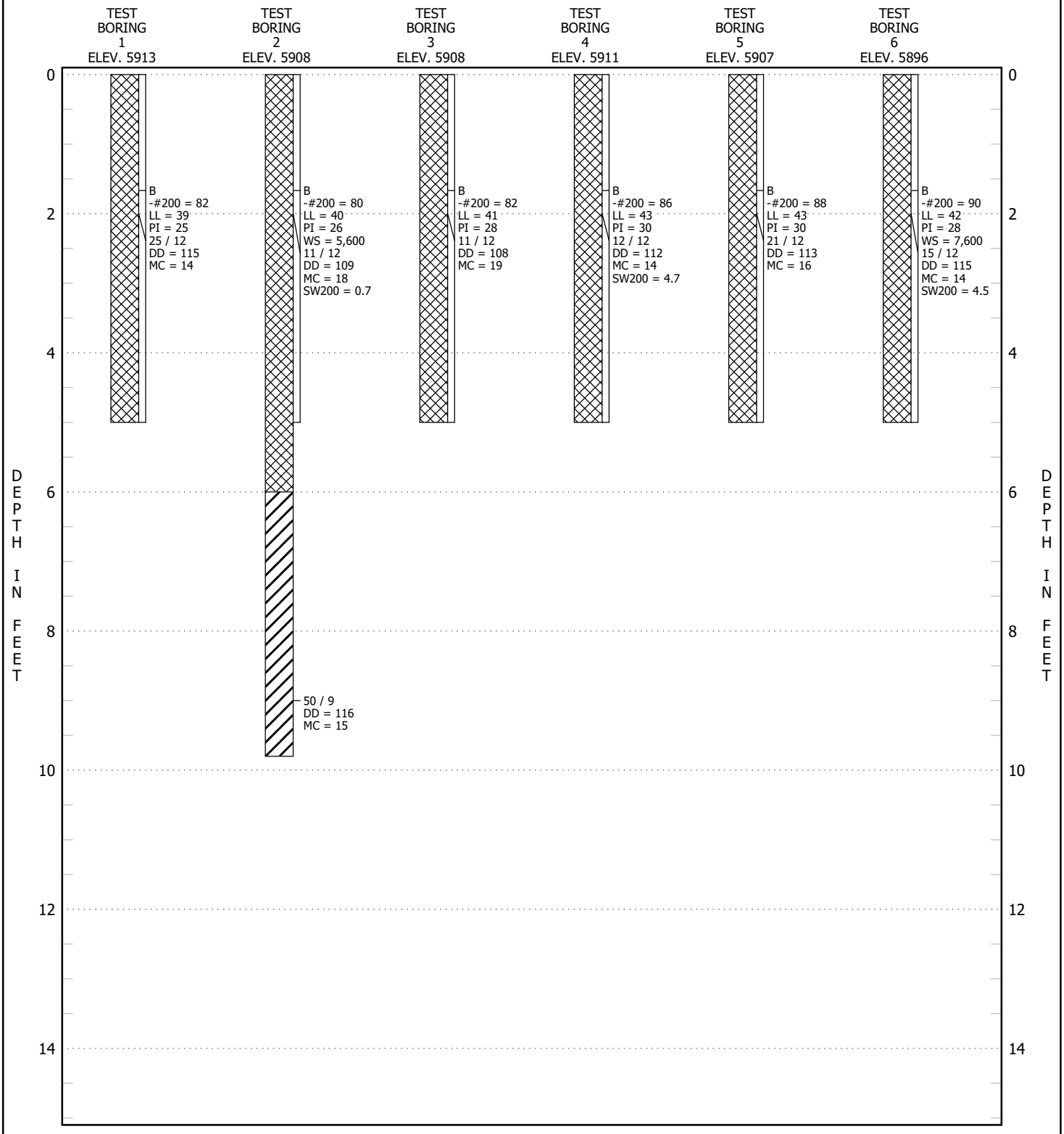
PROJECT NO. 252742-P1
FIGURE 2

**CLIENT** Richmond American Homes of Colorado, Inc.

**PROJECT NUMBER** 252742-P1

**PROJECT NAME** Trails at Aspen Ridge, Filing 4

**PROJECT LOCATION** El Paso County, Colorado




SEE FIGURE 6 FOR LEGEND AND NOTES

TEST BORING LOGS

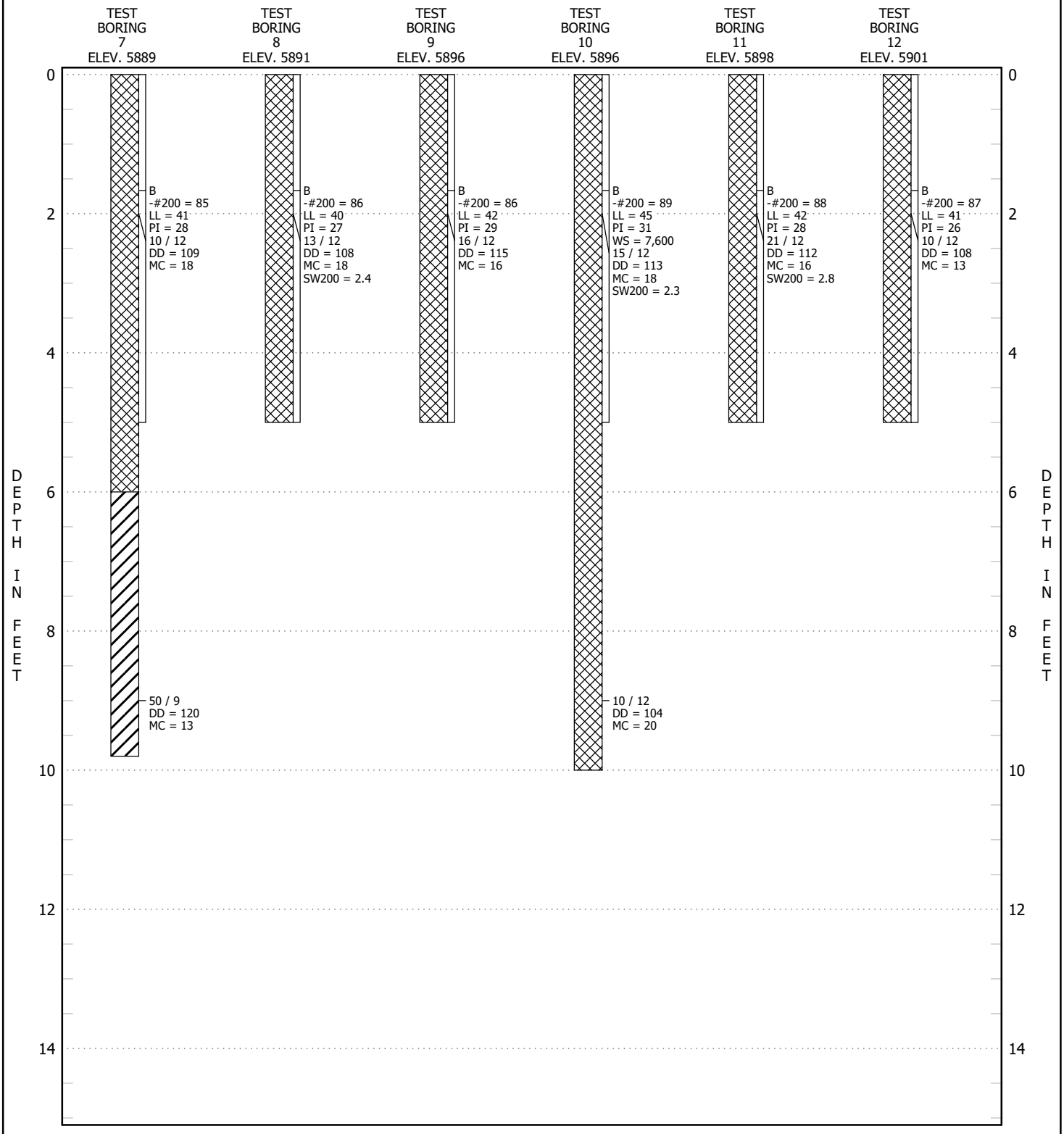
FIGURE 3

**CLIENT** Richmond American Homes of Colorado, Inc.

**PROJECT NUMBER** 252742-P1

**PROJECT NAME** Trails at Aspen Ridge, Filing 4

**PROJECT LOCATION** El Paso County, Colorado




SEE FIGURE 6 FOR LEGEND AND NOTES

TEST BORING LOGS

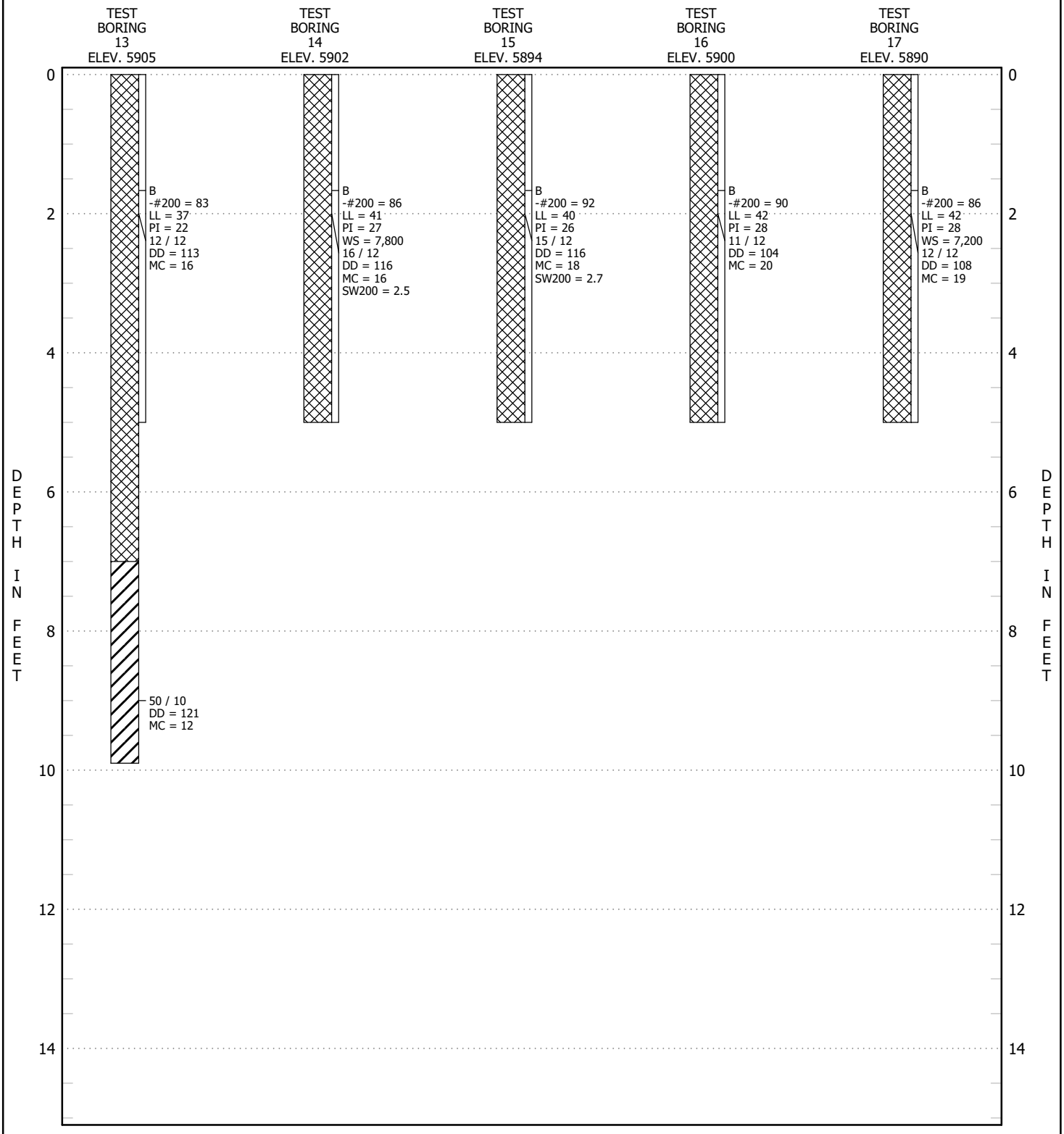
FIGURE 4

**CLIENT** Richmond American Homes of Colorado, Inc.

**PROJECT NUMBER** 252742-P1

**PROJECT NAME** Trails at Aspen Ridge, Filing 4

**PROJECT LOCATION** El Paso County, Colorado




SEE FIGURE 6 FOR LEGEND AND NOTES

TEST BORING LOGS

FIGURE 5

**CLIENT** Richmond American Homes of Colorado, Inc.

**PROJECT NUMBER** 252742-P1

**PROJECT NAME** Trails at Aspen Ridge, Filing 4

**PROJECT LOCATION** El Paso County, Colorado

## SOIL DESCRIPTIONS

Fill (moisture treated), clay, stiff to very stiff, sandy, with processed claystone and sandstone

Claystone (Bedrock), hard to very hard

## ABBREVIATIONS

| | |
|---|---|
| AC | Asphalt concrete (in) |
| CTS | Chemically treated subgrade (in) |
| GF | Granular fill (in) |
| DD | Dry density of sample, pounds per cubic foot (pcf) |
| MC | Moisture content, percentage of dry weight of soil (%) |
| SW200 | Swell under a surcharge of 200 pounds per square foot (psf) upon wetting (%) |
| COM200 | Compression under a surcharge of 200 psf upon wetting (%) |
| UC | Unconfined compressive strength (psf) |
| -#200 | Percent passing the No. 200 sieve (%) |
| LL | Liquid Limit |
| PI | Plasticity Index |
| NP | Nonplastic |
| NV | No Value |
| WS | Water soluble sulfates, parts per million (ppm) |
| x/y | x blows of a 140-pound hammer falling 30 inches were required to drive a 2.5-inch outside diameter sampler y inches |
| x/y SS | x blows of a 140-pound hammer falling 30 inches were required to drive a 2.0-inch outside diameter sampler y inches |
| C-x | Depth of cut to grade of x feet |
| F-x | Depth of fill to grade of x feet |
| FG | Finished grade |
| NR | No sample recovered |
| ND | No drive taken |
| Bounce | Sampler bounced during driving |
| B | Bulk sample |
| AS | Auger sample |
| | Well to very well cemented layer |
| | Practical drilling refusal |

Notes:

1. Test borings were drilled June 1, 2026.
2. Locations of the test borings were staked by others at locations chosen by AGW.
3. The horizontal lines shown on the logs differentiate materials and represent the approximate boundaries between materials. The transitions between materials may be gradual.
4. Elevations were obtained from information provided by others and were rounded to the nearest foot.
5. Test boring logs shown are subject to the limitations, explanations, and conclusions of this report.

LEGEND AND NOTES

FIGURE 6

# APPENDIX A
## LABORATORY TEST RESULTS

**SUMMARY OF LABORATORY TEST RESULTS.....TABLE A-1**

**GRADATION AND ATTERBERG TEST RESULTS.....FIGURES A-1 THROUGH A-9**

**SWELL-CONSOLIDATION TEST RESULTS .....FIGURES A-10 THROUGH A-13**

**STANDARD PROCTOR TEST RESULTS..... FIGURE A-14**

**RESILIENT MODULUS TEST RESULTS..... FIGURE A-15**

# TABLE A-1
# SUMMARY OF LABORATORY TEST RESULTS

July 7, 2026
Revised November 18, 2026



| Test Boring Number | Depth (feet) | Soil Type | AASHTO Soil Classification | Dry Density (pcf) | Moisture (%) | Swell / Consolidation (-) (%) [1] | % Passing #200 Sieve | Atterberg Limits | | | Water Soluble Sulfates (ppm) |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | Liquid Limit | Plastic Limit | Plasticity Index | |
| 1 | 0-5 | Fill, clay, sandy, trace gravel | A-6(19) | | | | 82 | 39 | 14 | 25 | |
| 1 | 2 | Fill, clay, sandy, trace gravel | | 115 | 14 | | | | | | |
| 2 | 0-5 | Fill, clay, sandy | A-6(19) | | | | 80 | 40 | 14 | 26 | 5,600 |
| 2 | 2 | Fill, clay, sandy | | 109 | 18 | 0.7 | | | | | |
| 2 | 9 | Claystone, slightly sandy | | 116 | 15 | | | | | | |
| 3 | 0-5 | Fill, clay, sandy | A-7-6(22) | | | | 82 | 41 | 13 | 28 | |
| 3 | 2 | Fill, clay, sandy | | 108 | 19 | | | | | | |
| 4 | 0-5 | Fill, clay, slightly sandy | A-7-6(25) | | | | 86 | 43 | 13 | 30 | |
| 4 | 2 | Fill, clay, slightly sandy | | 112 | 14 | 4.7 | | | | | |
| 5 | 0-5 | Fill, clay, slightly sandy | A-7-6(26) | | | | 88 | 43 | 13 | 30 | |
| 5 | 2 | Fill, clay, slightly sandy | | 113 | 16 | | | | | | |
| 6 | 0-5 | Fill, clay, slightly sandy | A-7-6(25) | | | | 90 | 42 | 14 | 28 | 7,600 |
| 6 | 2 | Fill, clay, slightly sandy | | 115 | 14 | 4.5 | | | | | |
| 7 | 0-5 | Fill, clay, slightly sandy, trace gravel | A-7-6(23) | | | | 85 | 41 | 13 | 28 | |
| 7 | 2 | Fill, clay, slightly sandy, trace gravel | | 109 | 18 | | | | | | |
| 7 | 9 | Claystone, slightly sandy | | 120 | 13 | | | | | | |
| 8 | 0-5 | Fill, clay, slightly sandy | A-6(22) | | | | 86 | 40 | 13 | 27 | |
| 8 | 2 | Fill, clay, slightly sandy | | 108 | 18 | 2.4 | | | | | |
| 9 | 0-5 | Fill, clay, slightly sandy | A-7-6(24) | | | | 86 | 42 | 13 | 29 | |
| 9 | 2 | Fill, clay, slightly sandy | | 115 | 16 | | | | | | |
| 10 | 0-5 | Fill, clay, slightly sandy | A-7-6(28) | | | | 89 | 45 | 14 | 31 | 7,600 |

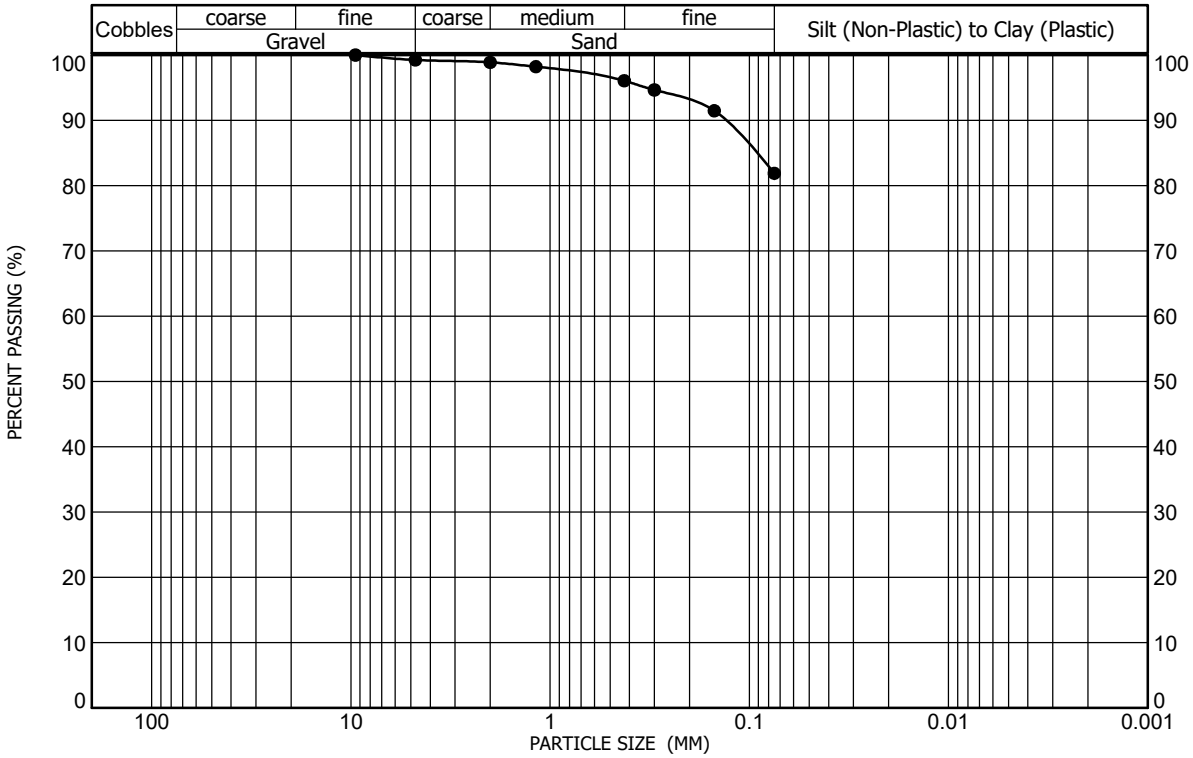
# TABLE A-1
# SUMMARY OF LABORATORY TEST RESULTS

July 7, 2026
Revised November 18, 2026



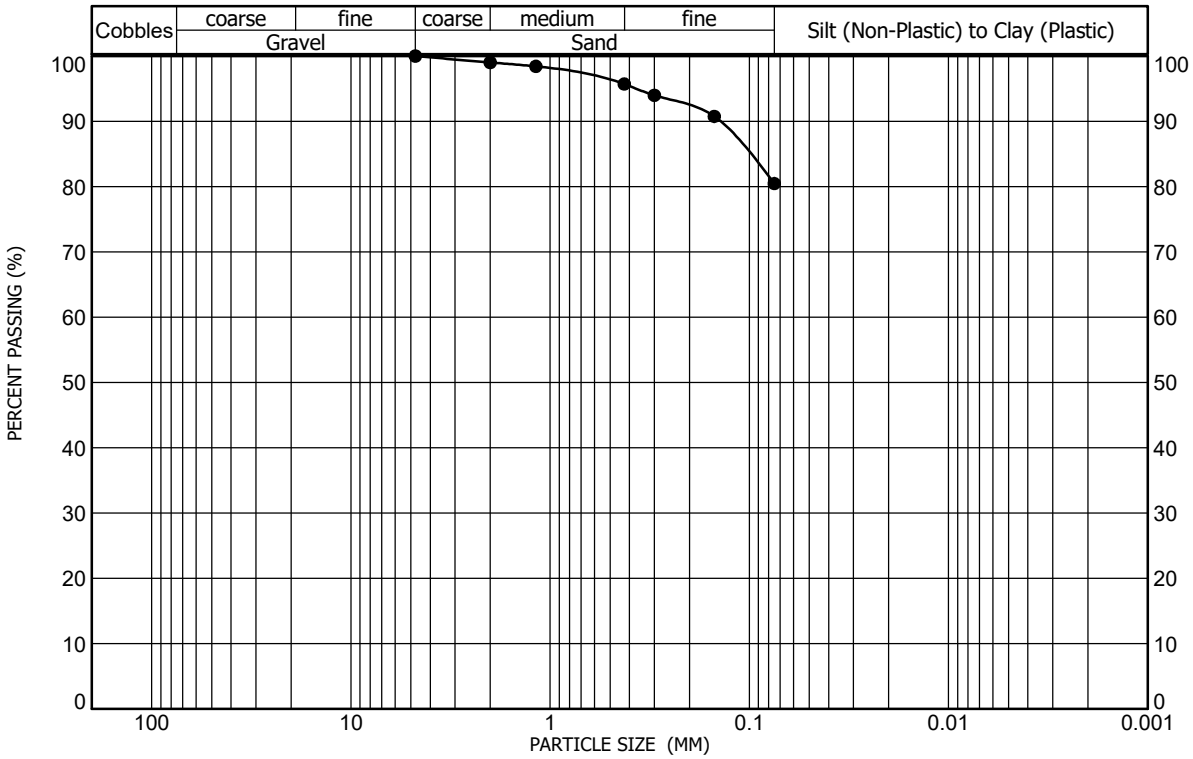
| Test Boring Number | Depth (feet) | Soil Type | AASHTO Soil Classification | Dry Density (pcf) | Moisture (%) | Swell / Consolidation (-) (%) [1] | % Passing #200 Sieve | Atterberg Limits | | | Water Soluble Sulfates (ppm) |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | Liquid Limit | Plastic Limit | Plasticity Index | |
| 10 | 2 | Fill, clay, slightly sandy | | 113 | 18 | 2.3 | | | | | |
| 10 | 9 | Fill, clay, slightly sandy | | 104 | 20 | | | | | | |
| 11 | 0-5 | Fill, clay, slightly sandy | A-7-6(24) | | | | 88 | 42 | 14 | 28 | |
| 11 | 2 | Fill, clay, slightly sandy | | 112 | 16 | 2.8 | | | | | |
| 12 | 0-5 | Fill, clay, slightly sandy | A-7-6(22) | | | | 87 | 41 | 15 | 26 | |
| 12 | 2 | Fill, clay, slightly sandy | | 108 | 13 | | | | | | |
| 13 | 0-5 | Fill, clay, sandy, trace gravel | A-6(17) | | | | 83 | 37 | 15 | 22 | |
| 13 | 2 | Fill, clay, sandy, trace gravel | | 113 | 16 | | | | | | |
| 13 | 9 | Claystone, slightly sandy | | 121 | 12 | | | | | | |
| 14 | 0-5 | Fill, clay, slightly sandy | A-7-6(23) | | | | 86 | 41 | 14 | 27 | 7,800 |
| 14 | 2 | Fill, clay, slightly sandy | | 116 | 16 | 2.5 | | | | | |
| 15 | 0-5 | Fill, clay, slightly sandy | A-6(24) | | | | 92 | 40 | 14 | 26 | |
| 15 | 2 | Fill, clay, slightly sandy | | 116 | 18 | 2.7 | | | | | |
| 16 | 0-5 | Fill, clay, slightly sandy | A-7-6(25) | | | | 90 | 42 | 14 | 28 | |
| 16 | 2 | Fill, clay, slightly sandy | | 104 | 20 | | | | | | |
| 17 | 0-5 | Fill, clay, slightly sandy | A-7-6(23) | | | | 86 | 42 | 14 | 28 | 7,200 |
| 17 | 2 | Fill, clay, slightly sandy | | 108 | 19 | | | | | | |
| Bulk [2] | 0-5 | Fill, clay, slightly sandy | A-7-6 (26 & 28) | 111.5 [3] | 16.3 [3] | | 89 | 44 | 14 | 31 | |

[1] Indicates Percent Swell or Consolidation (−) when wetted under a 200 psf load.
[2] Blended bulk sample from Test Borings 5 and 10 including average of %Passing -200 Sieve and Atterberg Limits
[3] Maximum Dry Density and Optimum Moisture Content




Sample Location: Test Boring No. 1 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, sandy, trace gravel
Classification: A-6(19), LEAN CLAY with SAND(CL)

Gravel (%): 1 | Sand (%): 17 | Clay/Silt (%): 82
Liquid Limit: 39 | Plasticity Index: 25



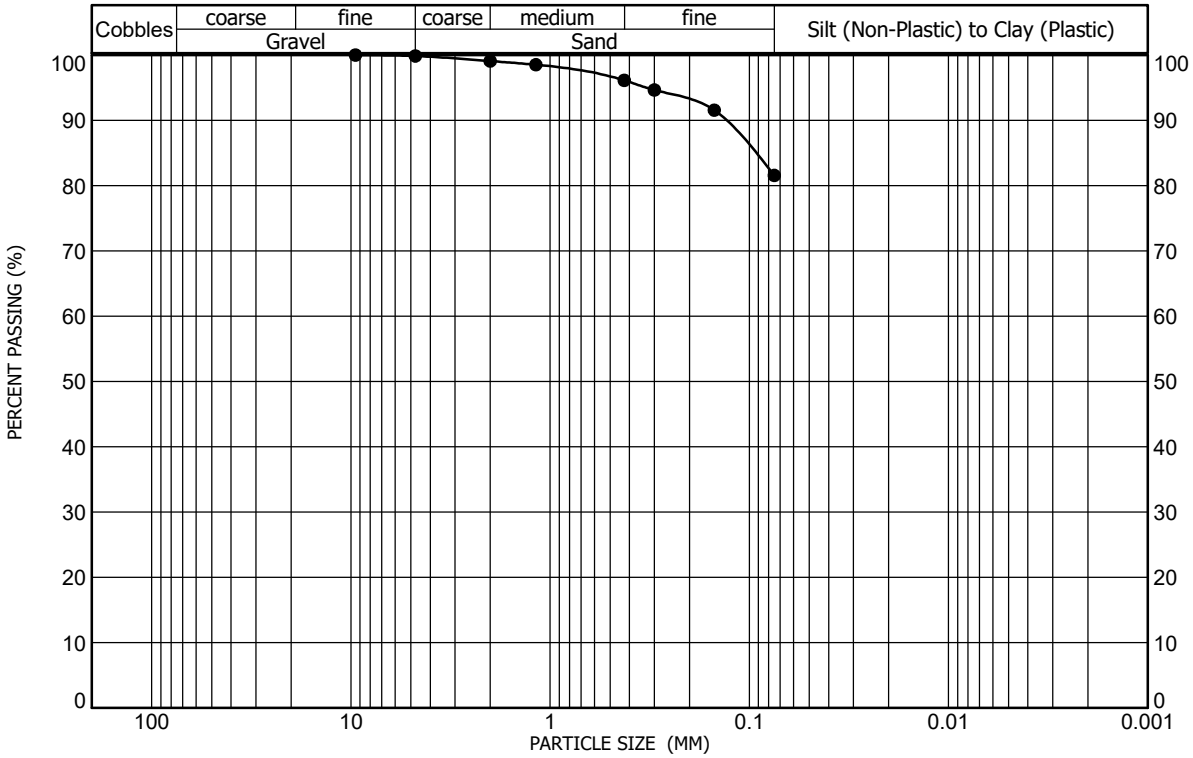

Sample Location: Test Boring No. 2 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, sandy
Classification: A-6(19), LEAN CLAY with SAND(CL)

Gravel (%): 0 | Sand (%): 20 | Clay/Silt (%): 80
Liquid Limit: 40 | Plasticity Index: 26

GRADATION AND ATTERBERG TEST RESULTS

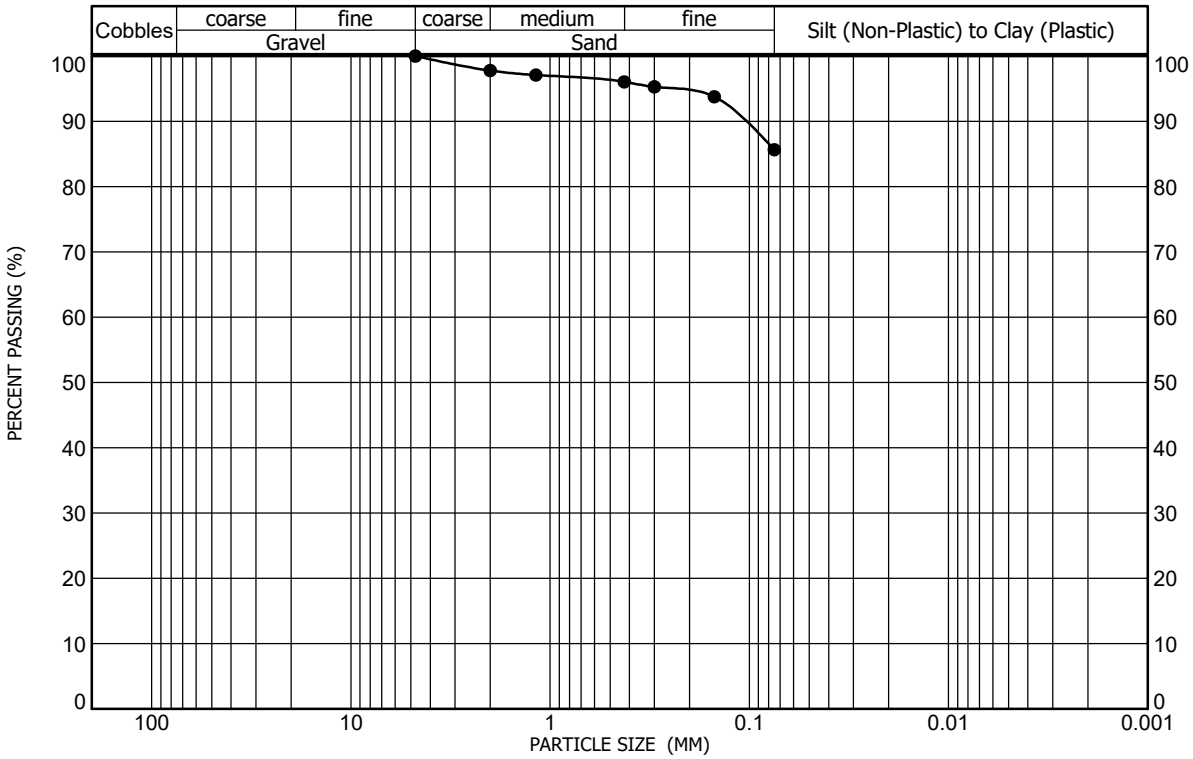
FIGURE A-1

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 3 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, sandy
Classification: A-7-6(22), LEAN CLAY with SAND(CL)

Gravel (%): 0 | Sand (%): 18 | Clay/Silt (%): 82
Liquid Limit: 41 | Plasticity Index: 28



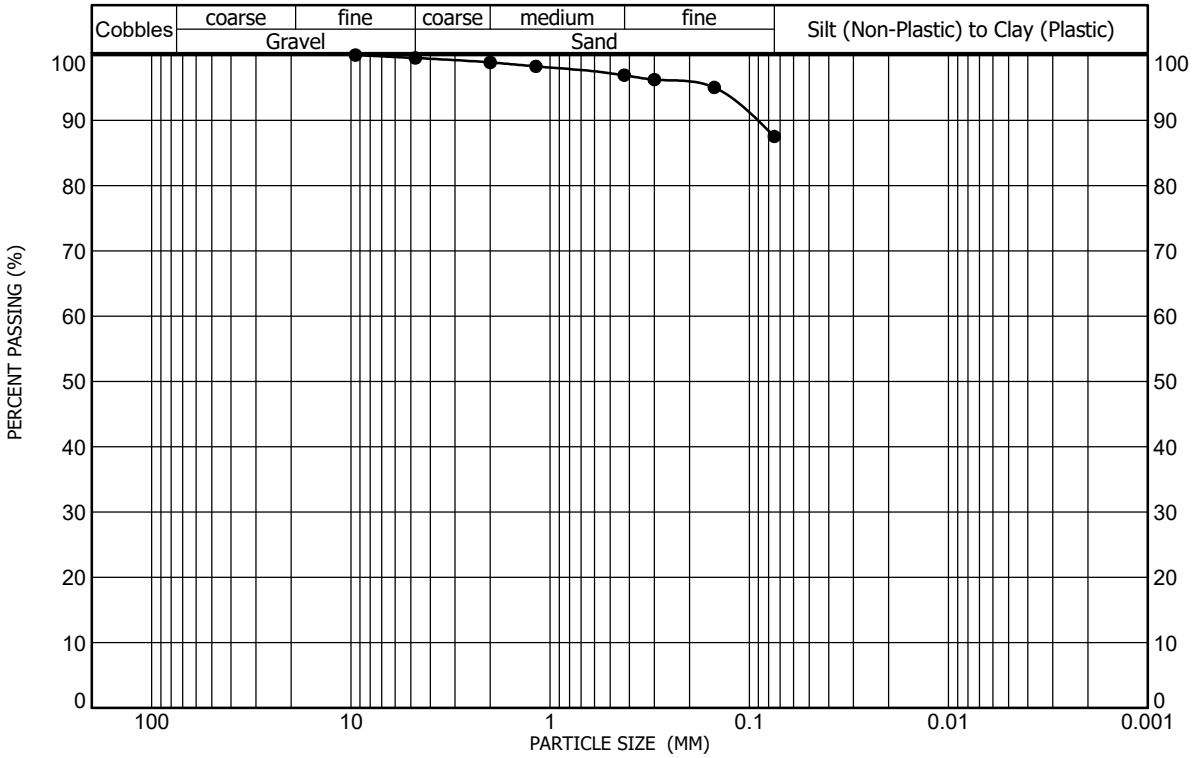

Sample Location: Test Boring No. 4 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(25), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 14 | Clay/Silt (%): 86
Liquid Limit: 43 | Plasticity Index: 30

GRADATION AND ATTERBERG TEST RESULTS

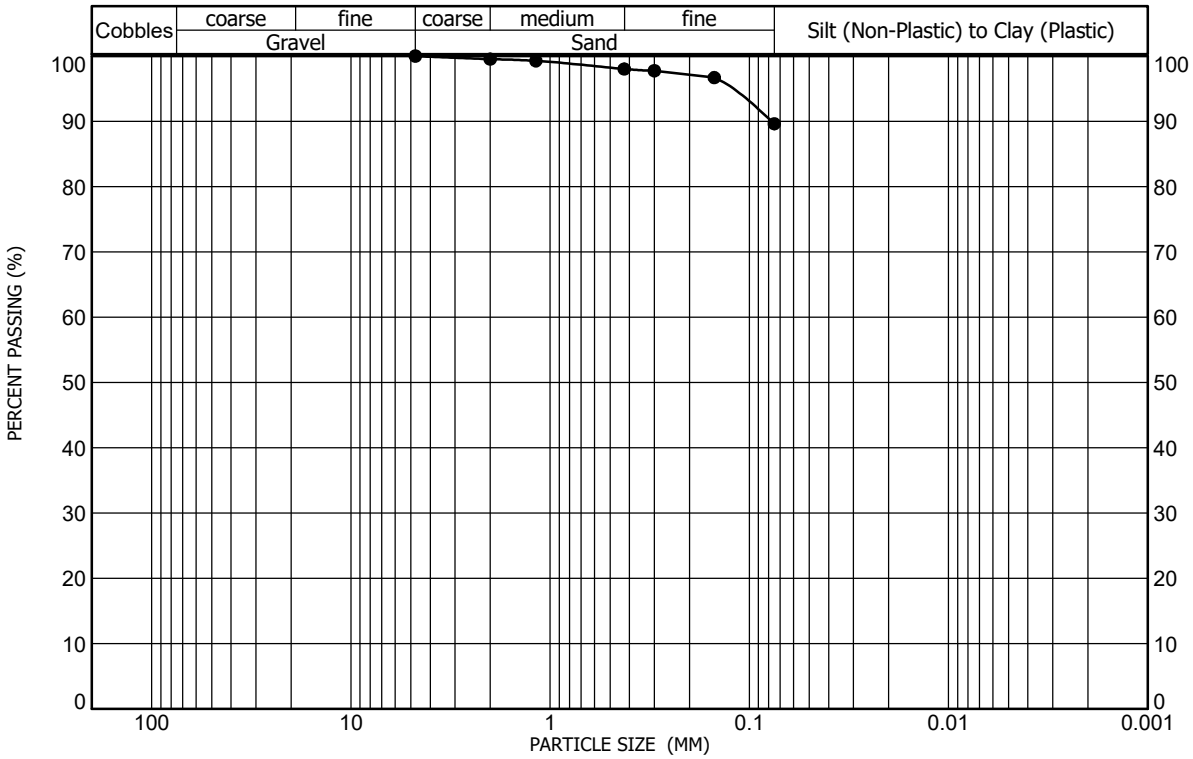
FIGURE A-2

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 5 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(26), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 12 | Clay/Silt (%): 88
Liquid Limit: 43 | Plasticity Index: 30



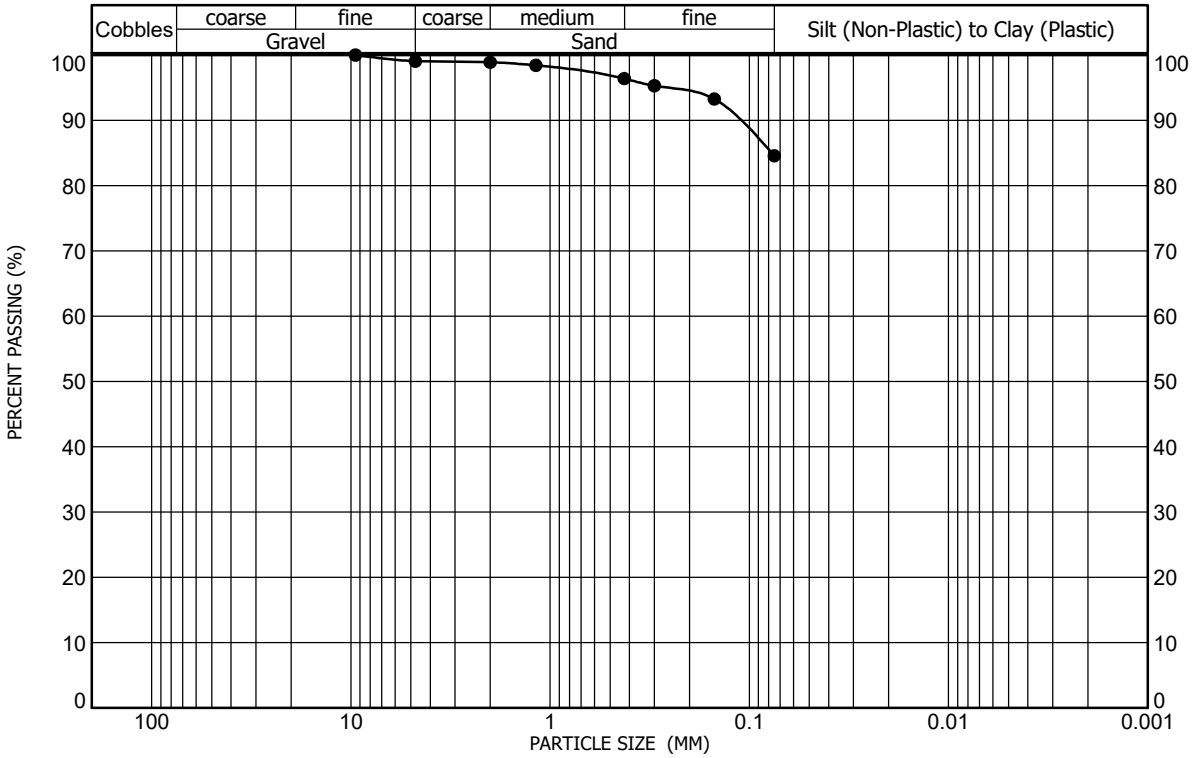

Sample Location: Test Boring No. 6 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(25), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 10 | Clay/Silt (%): 90
Liquid Limit: 42 | Plasticity Index: 28

GRADATION AND ATTERBERG TEST RESULTS

FIGURE A-3

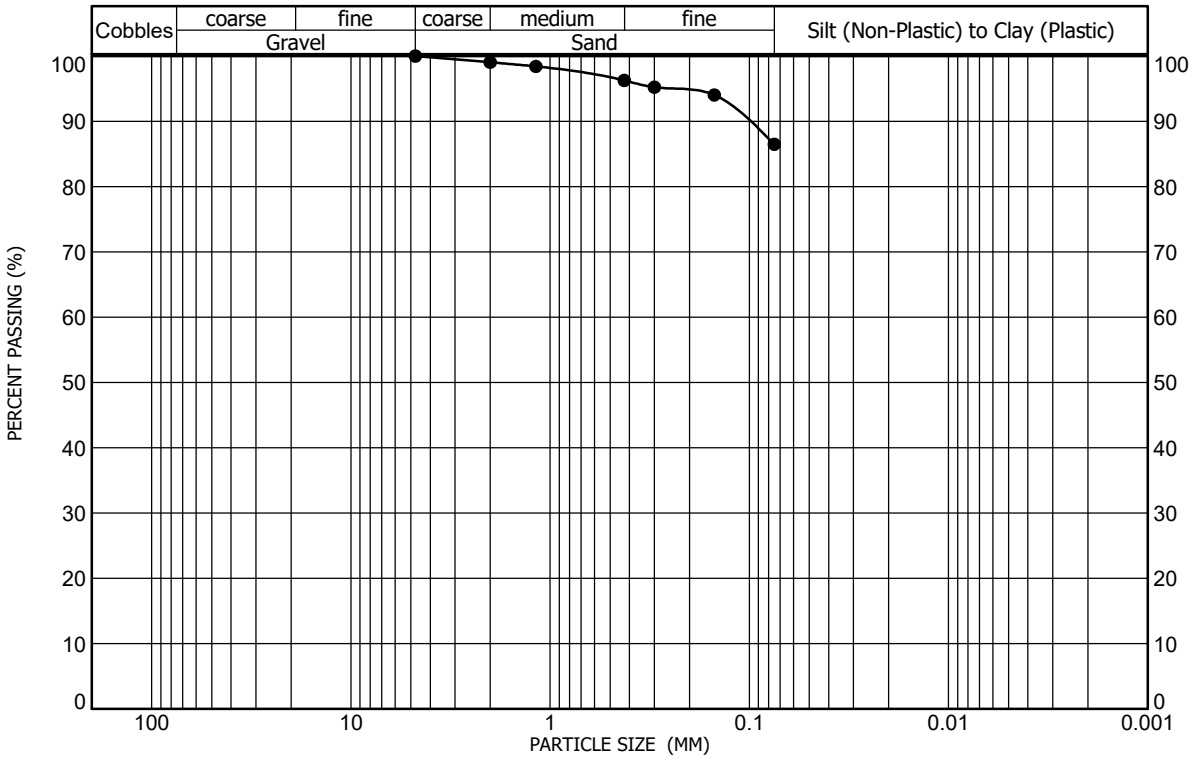
PROJECT NO. 252742-P1




Sample Location: Test Boring No. 7 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy, trace gravel
Classification: A-7-6(23), LEAN CLAY with SAND(CL)

Gravel (%): 1 | Sand (%): 14 | Clay/Silt (%): 85

Liquid Limit: 41 | Plasticity Index: 28




Sample Location: Test Boring No. 8 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-6(22), LEAN CLAY(CL)

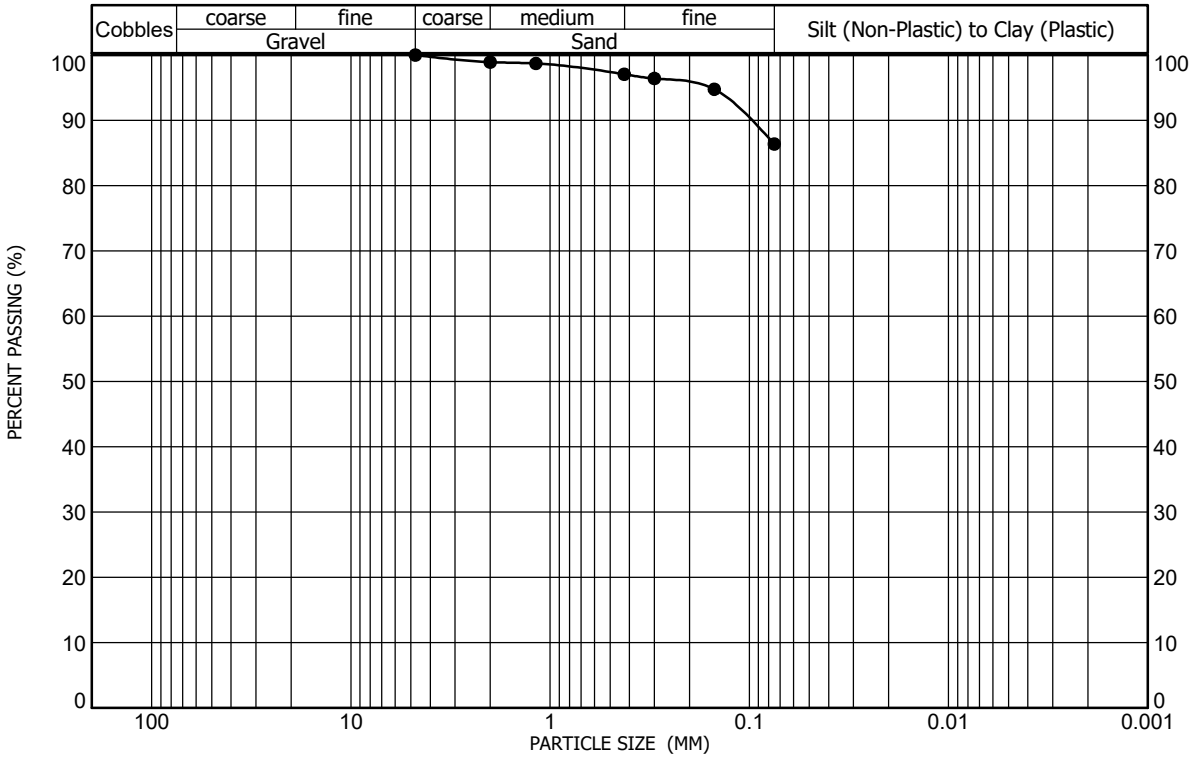
Gravel (%): 0 | Sand (%): 14 | Clay/Silt (%): 86

Liquid Limit: 40 | Plasticity Index: 27

GRADATION AND ATTERBERG TEST RESULTS

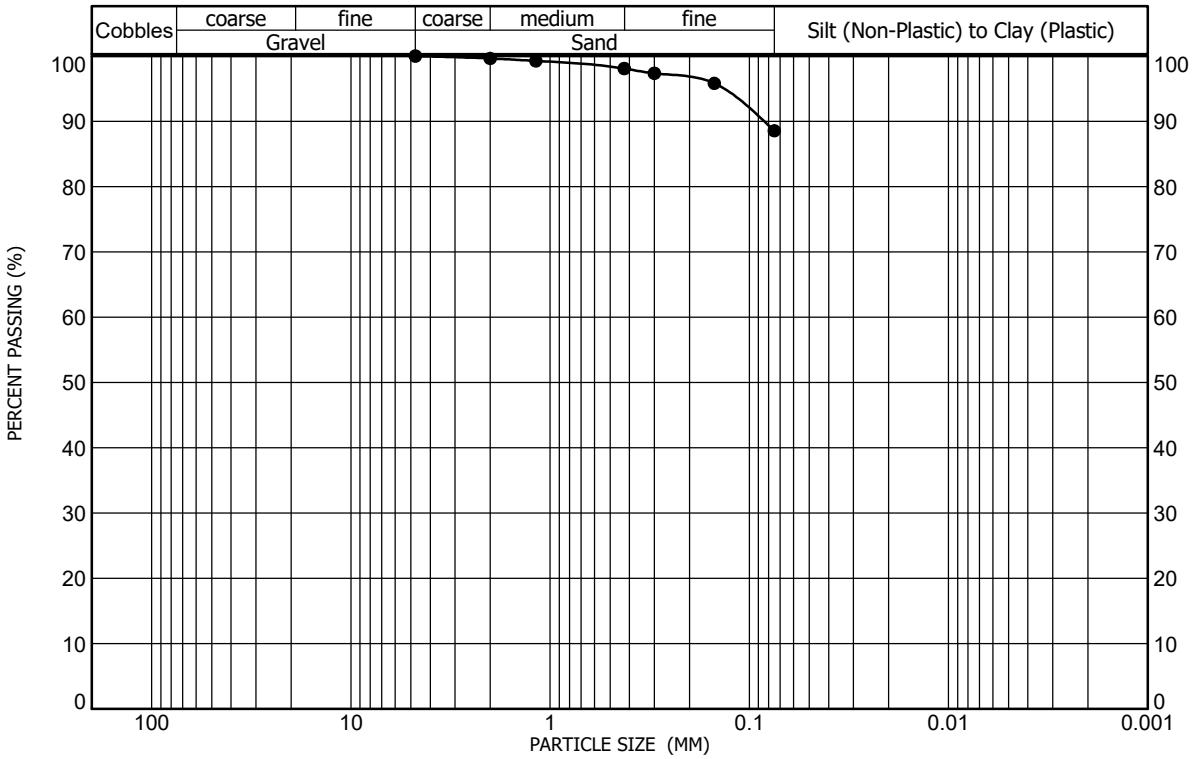
FIGURE A-4

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 9 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(24), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 14 | Clay/Silt (%): 86
Liquid Limit: 42 | Plasticity Index: 29



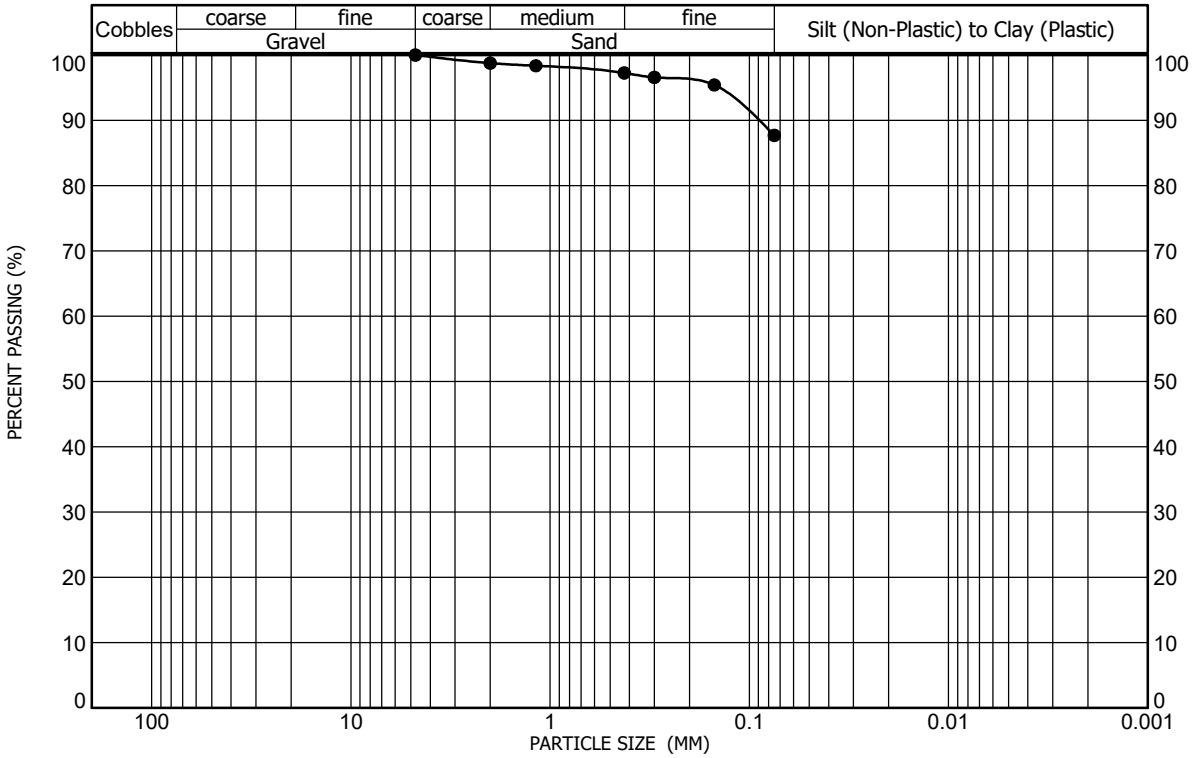

Sample Location: Test Boring No. 10 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(28), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 11 | Clay/Silt (%): 89
Liquid Limit: 45 | Plasticity Index: 31

GRADATION AND ATTERBERG TEST RESULTS

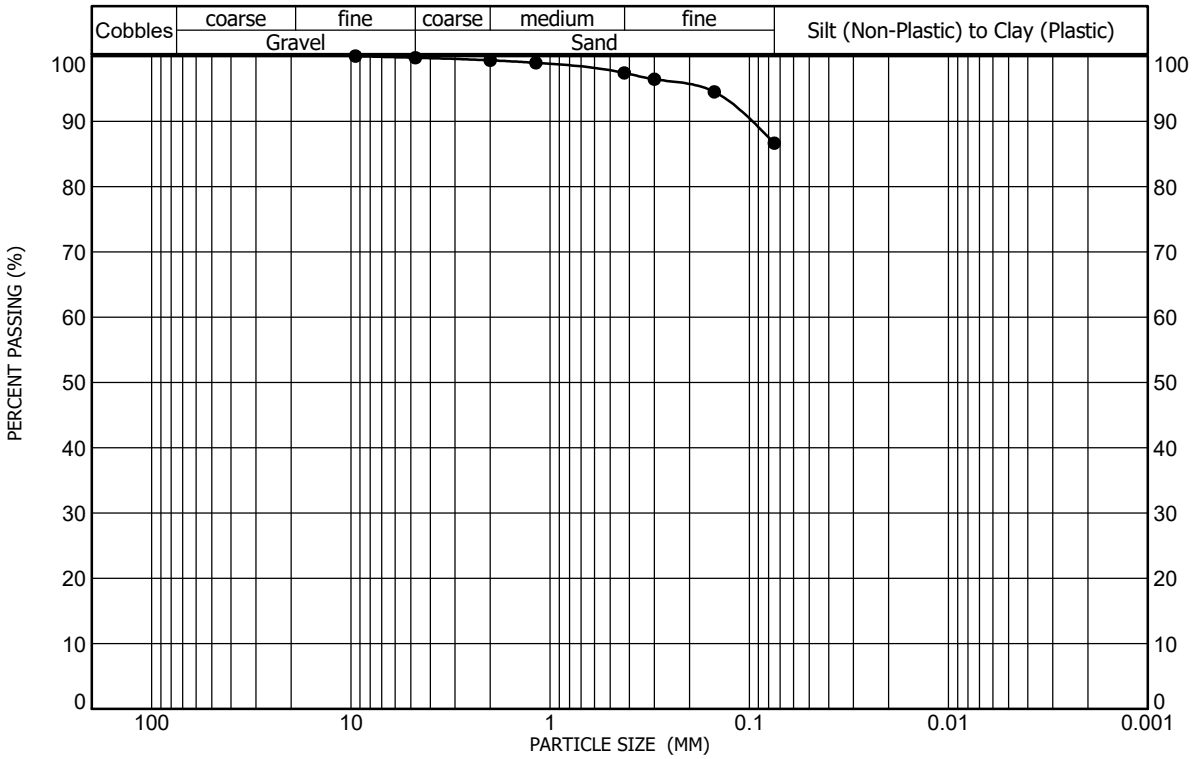
FIGURE A-5

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 11 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(24), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 12 | Clay/Silt (%): 88
Liquid Limit: 42 | Plasticity Index: 28



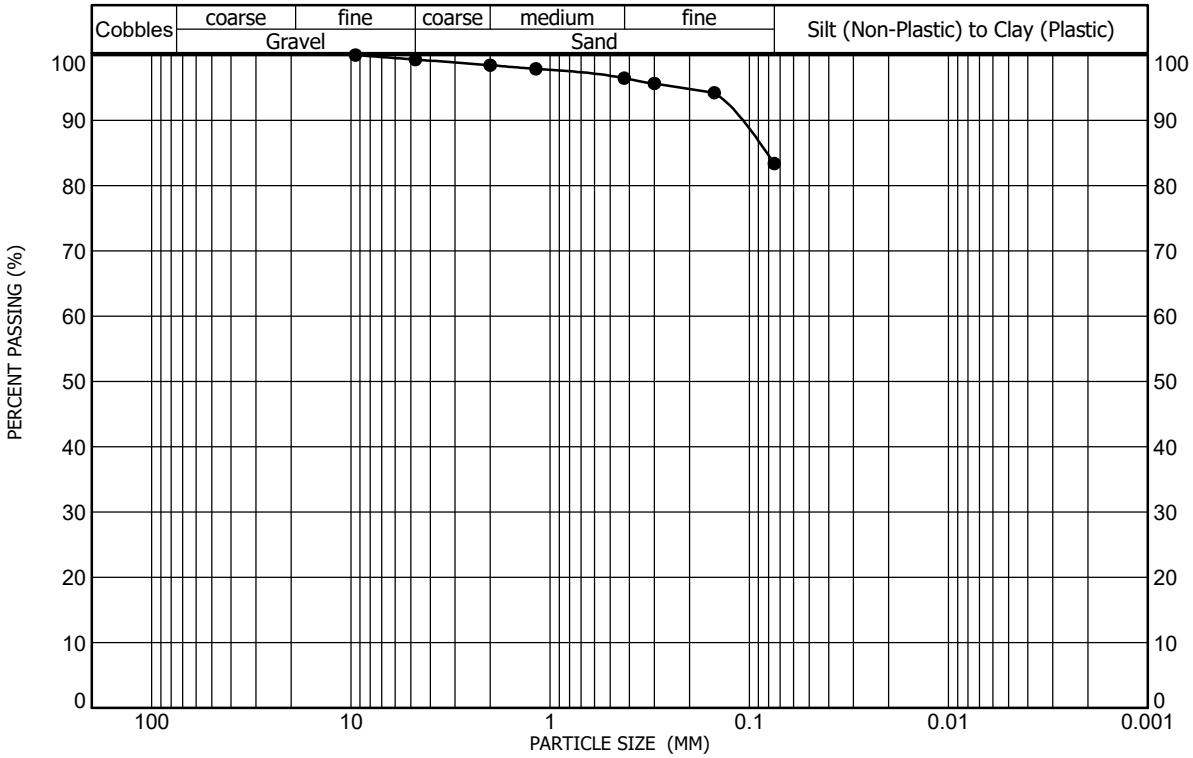

Sample Location: Test Boring No. 12 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(22), LEAN CLAY(CL)

Gravel (%): 0 | Sand (%): 13 | Clay/Silt (%): 87
Liquid Limit: 41 | Plasticity Index: 26

GRADATION AND ATTERBERG TEST RESULTS

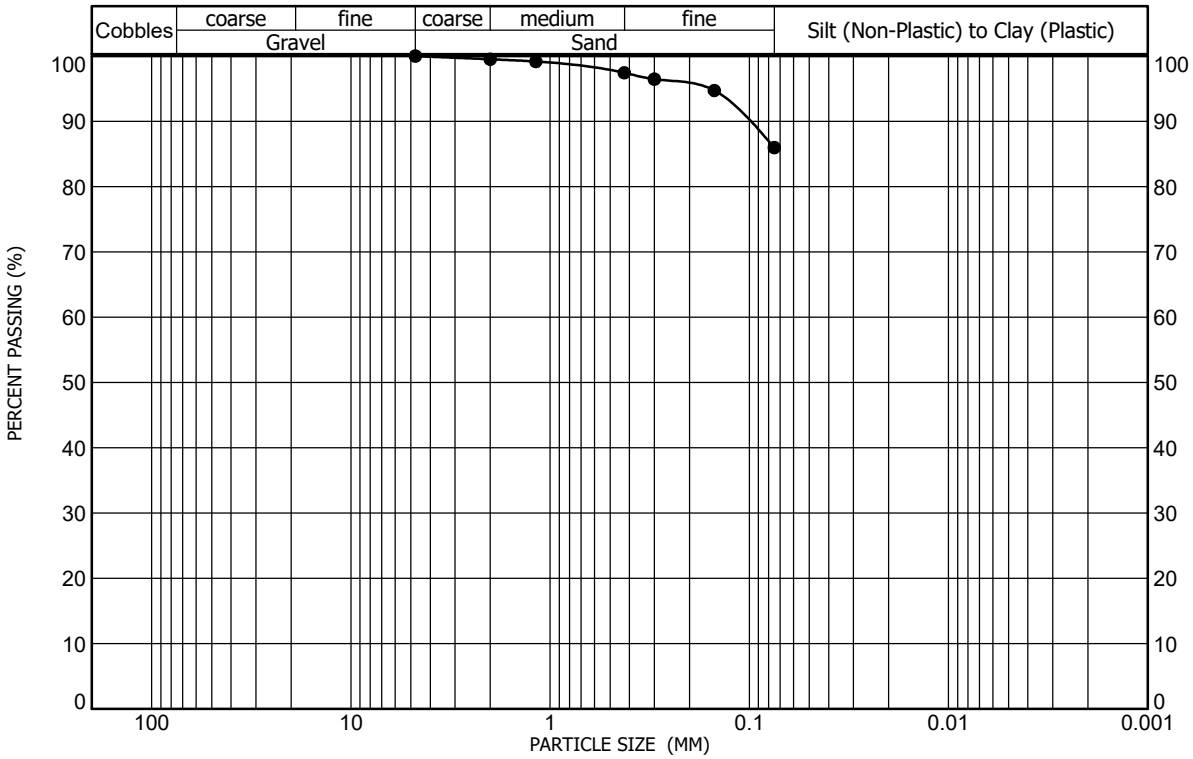
FIGURE A-6

PROJECT NO. 252742-P1




Sample Location Test Boring No. 13 at a depth of 0 feet to 5 feet
Sample Description Fill, clay, sandy, trace gravel
Classification A-6(17), LEAN CLAY with SAND(CL)

Gravel (%) 1 Liquid Limit 37
Sand (%) 16 Plasticity Index 22
Clay/Silt (%) 83



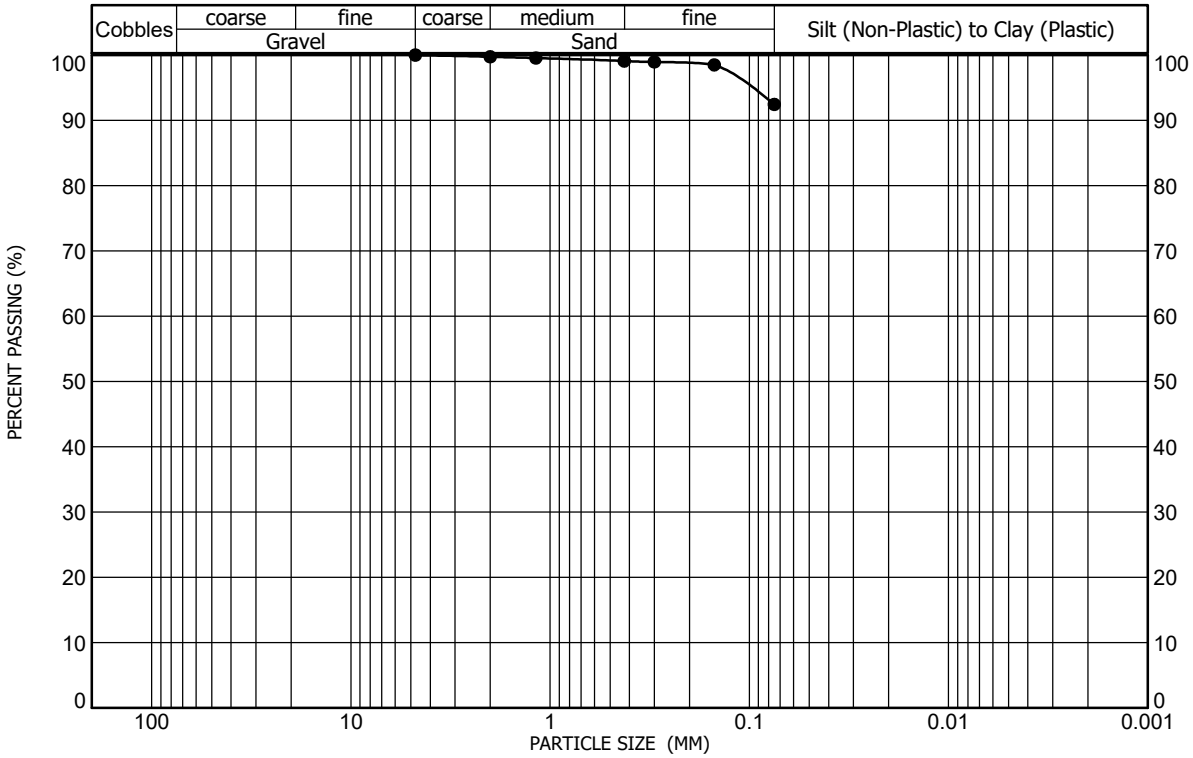

Sample Location Test Boring No. 14 at a depth of 0 feet to 5 feet
Sample Description Fill, clay, slightly sandy
Classification A-7-6(23), LEAN CLAY(CL)

Gravel (%) 0 Liquid Limit 41
Sand (%) 14 Plasticity Index 27
Clay/Silt (%) 86

GRADATION AND ATTERBERG TEST RESULTS

FIGURE A-7

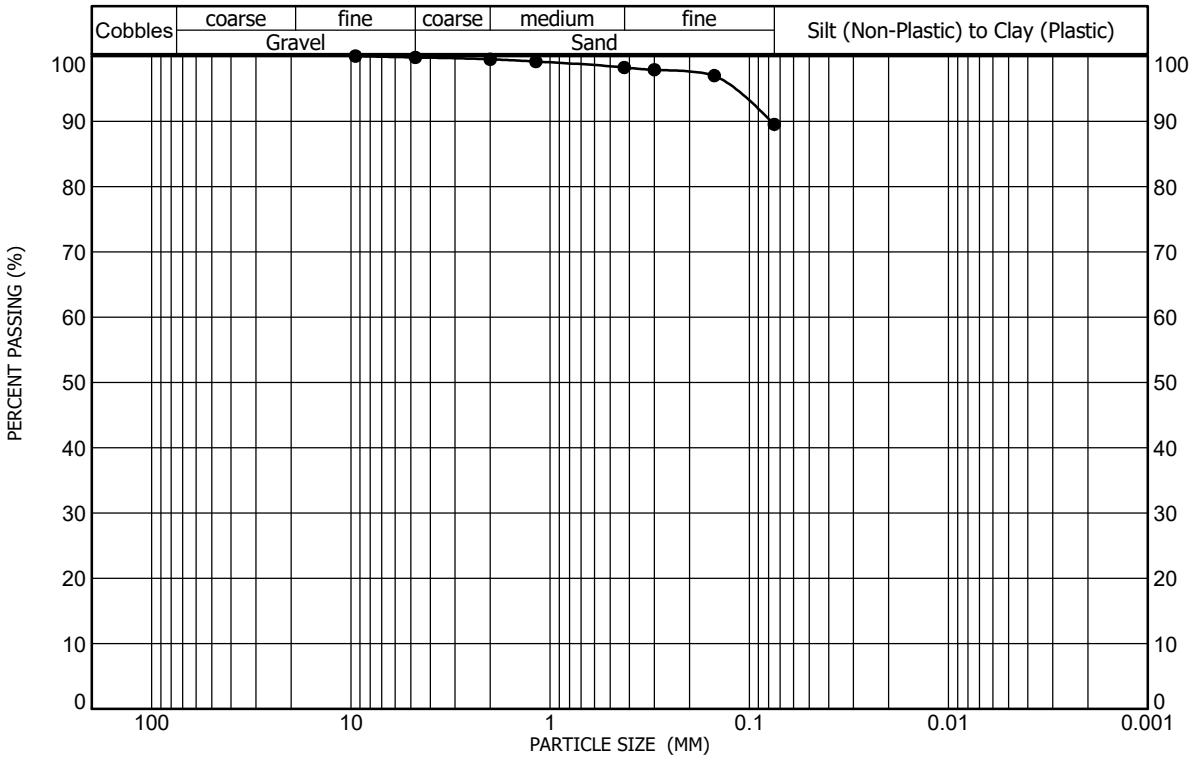
PROJECT NO. 252742-P1




Sample Location: Test Boring No. 15 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-6(24), LEAN CLAY(CL)

Gravel (%): 0
Sand (%): 8
Clay/Silt (%): 92

Liquid Limit: 40
Plasticity Index: 26




Sample Location: Test Boring No. 16 at a depth of 0 feet to 5 feet
Sample Description: Fill, clay, slightly sandy
Classification: A-7-6(25), LEAN CLAY(CL)

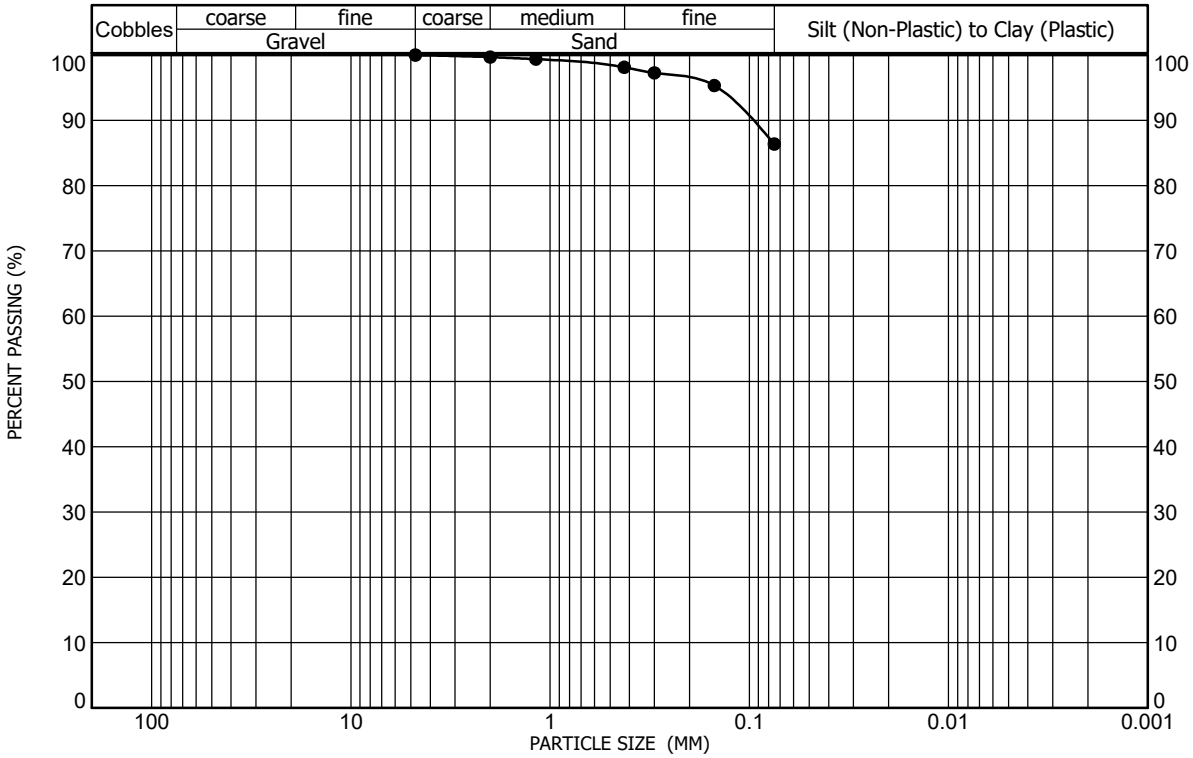
Gravel (%): 0
Sand (%): 10
Clay/Silt (%): 90

Liquid Limit: 42
Plasticity Index: 28

GRADATION AND ATTERBERG TEST RESULTS

FIGURE A-8

PROJECT NO. 252742-P1

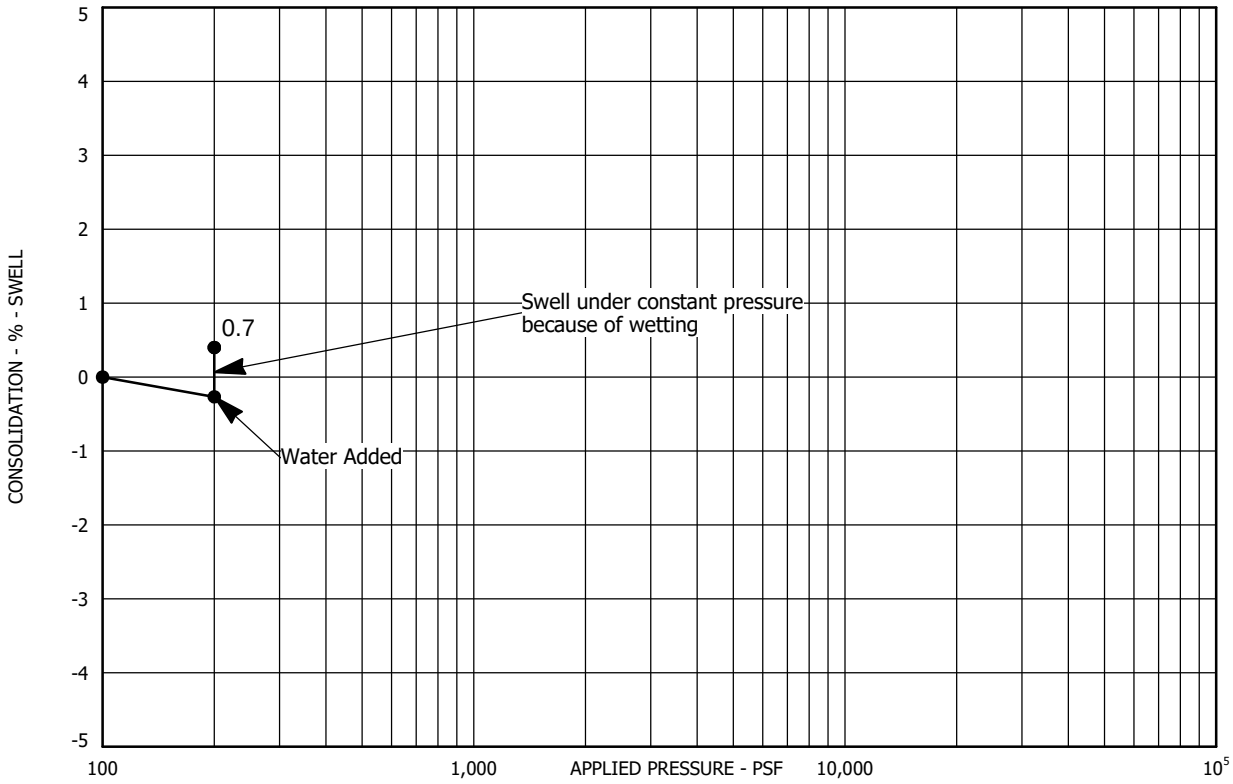



| | | | | | |
|---|---|---|---|---|---|
| Sample Location | Test Boring No. 17 at a depth of 0 feet to 5 feet | Gravel (%) | 0 | Liquid Limit | 42 |
| Sample Description | Fill, clay, slightly sandy | Sand (%) | 14 | Plasticity Index | 28 |
| Classification | A-7-6(23), LEAN CLAY(CL) | Clay/Silt (%) | 86 | | |

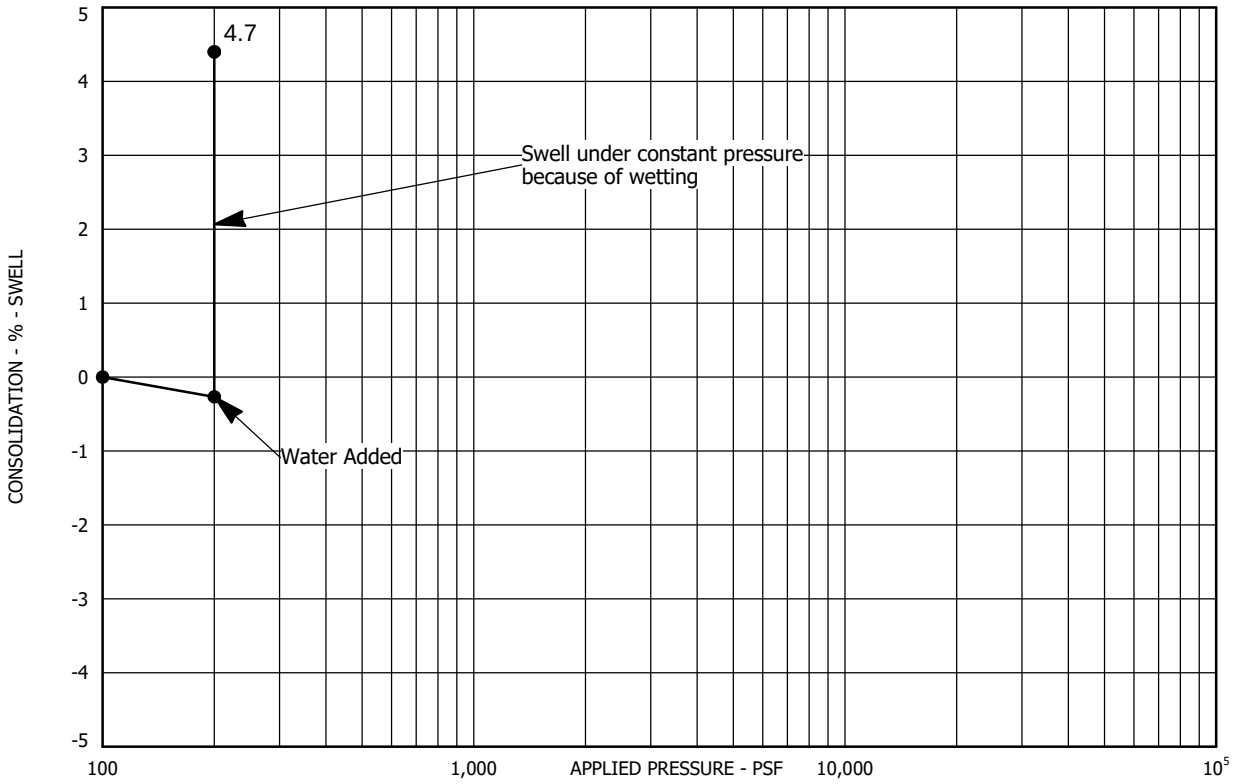
GRADATION AND ATTERBERG TEST RESULTS

FIGURE A-9

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 2 at a depth of 2 feet
Sample Description: Fill, clay, sandy
Dry Unit Weight (pcf): 109
Moisture Content (%): 18

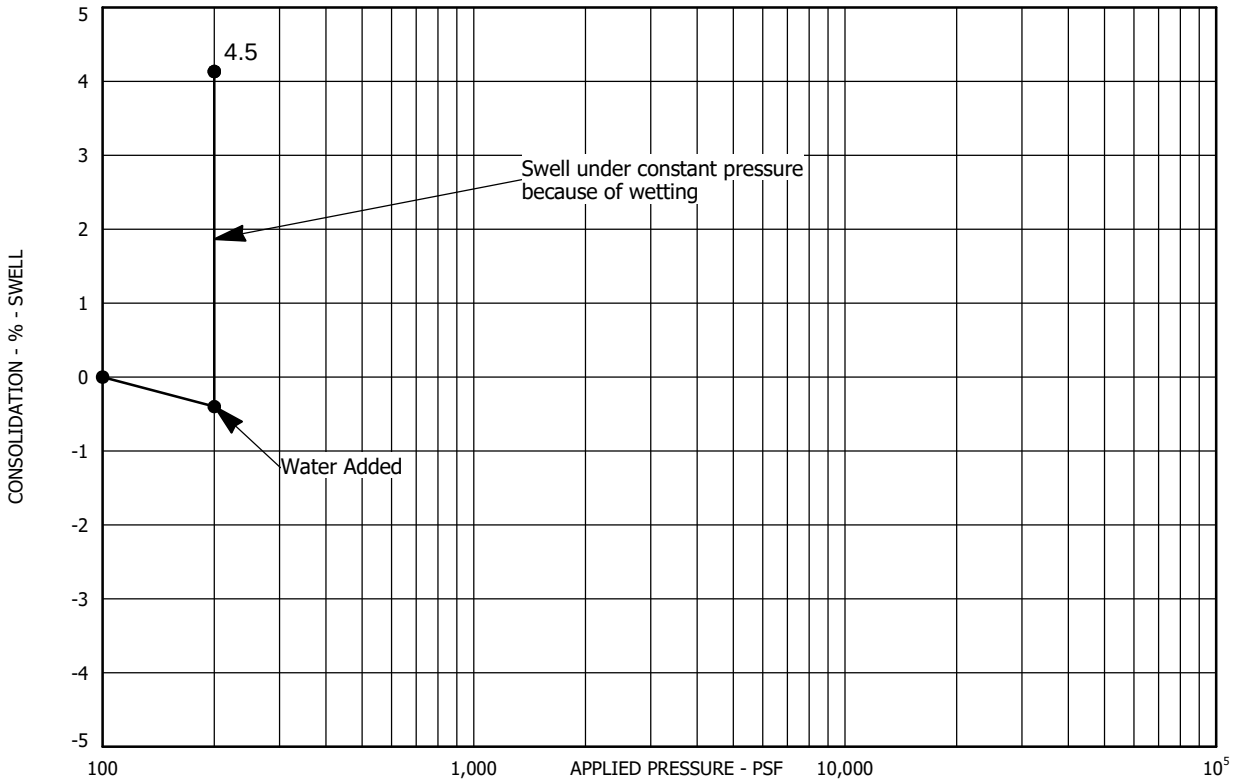



Sample Location: Test Boring No. 4 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 112
Moisture Content (%): 14

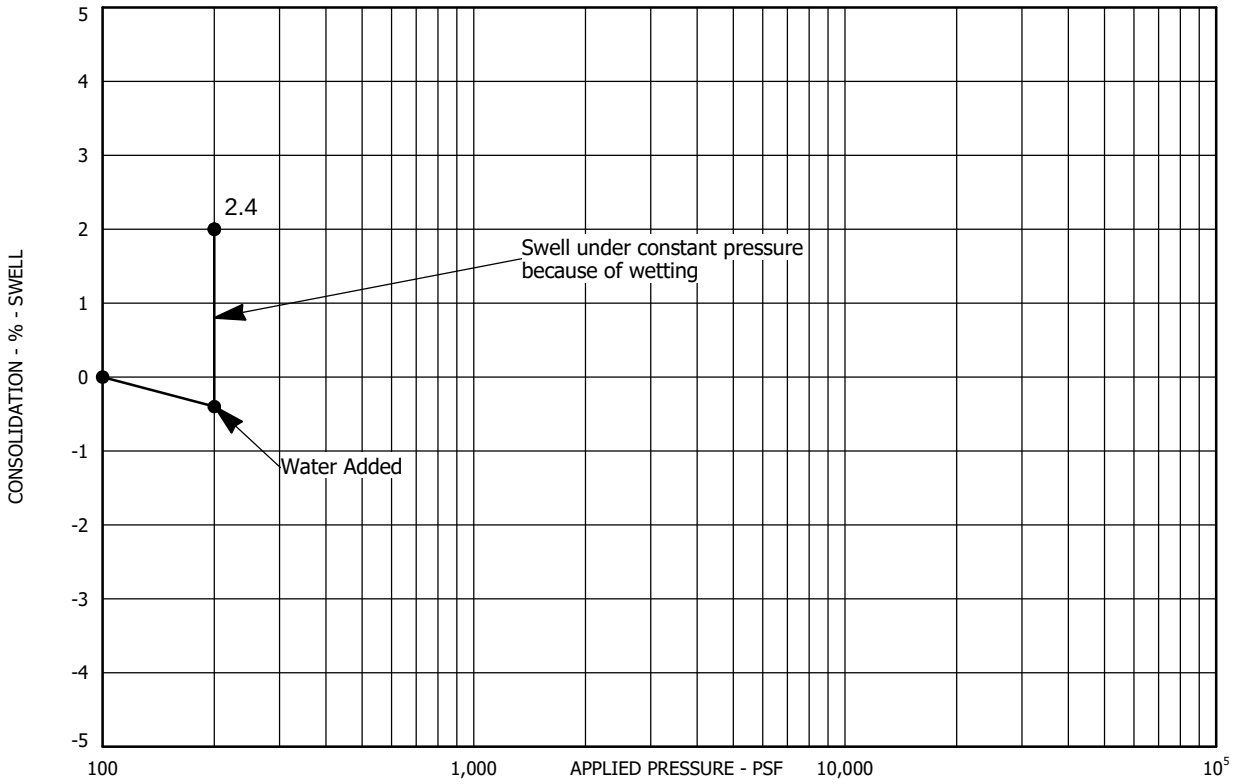
SWELL - CONSOLIDATION TEST RESULTS

FIGURE A-10

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 6 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 115
Moisture Content (%): 14

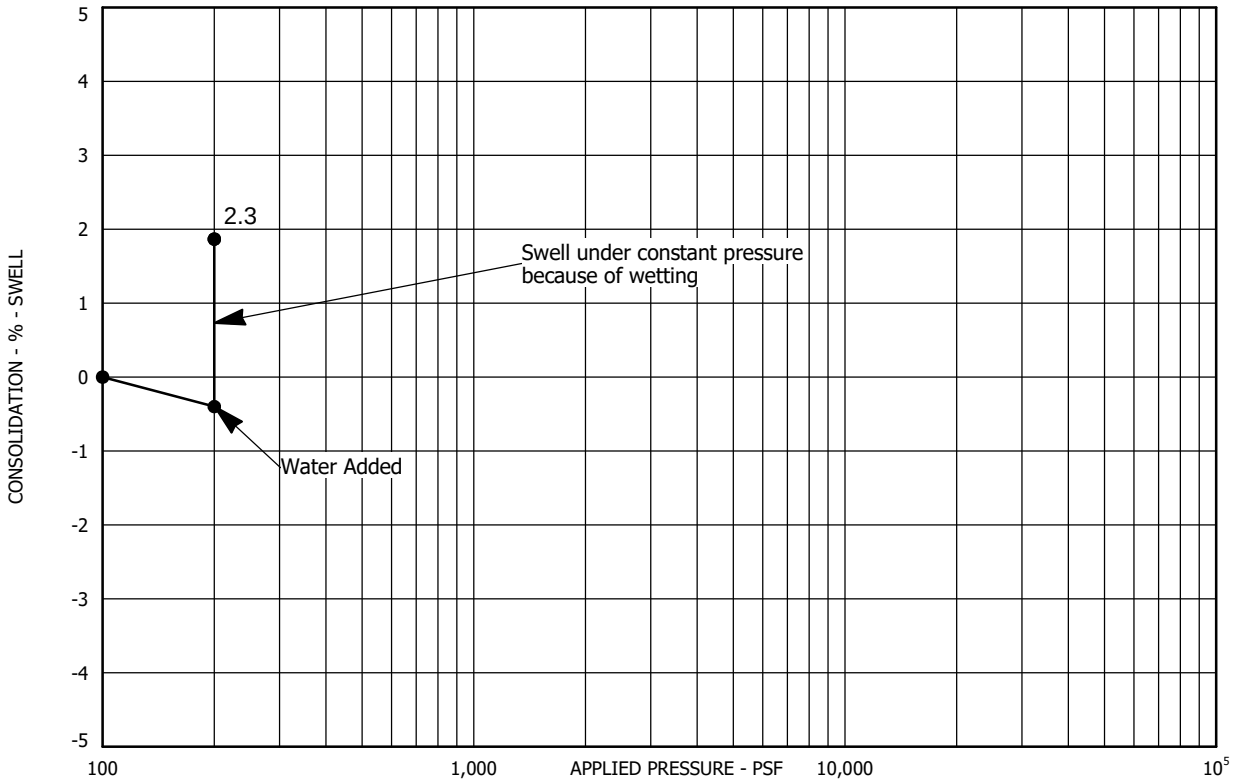



Sample Location: Test Boring No. 8 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 108
Moisture Content (%): 18

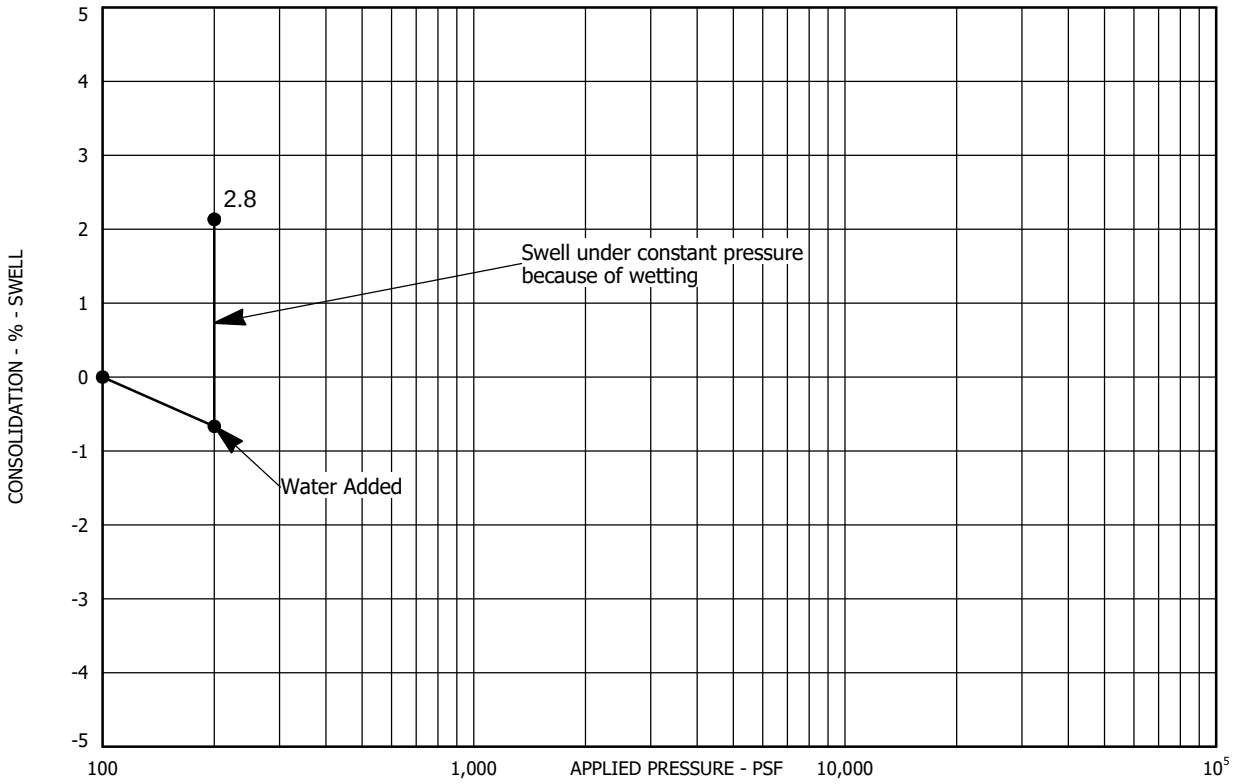
SWELL - CONSOLIDATION TEST RESULTS

FIGURE A-11

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 10 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 113
Moisture Content (%): 18

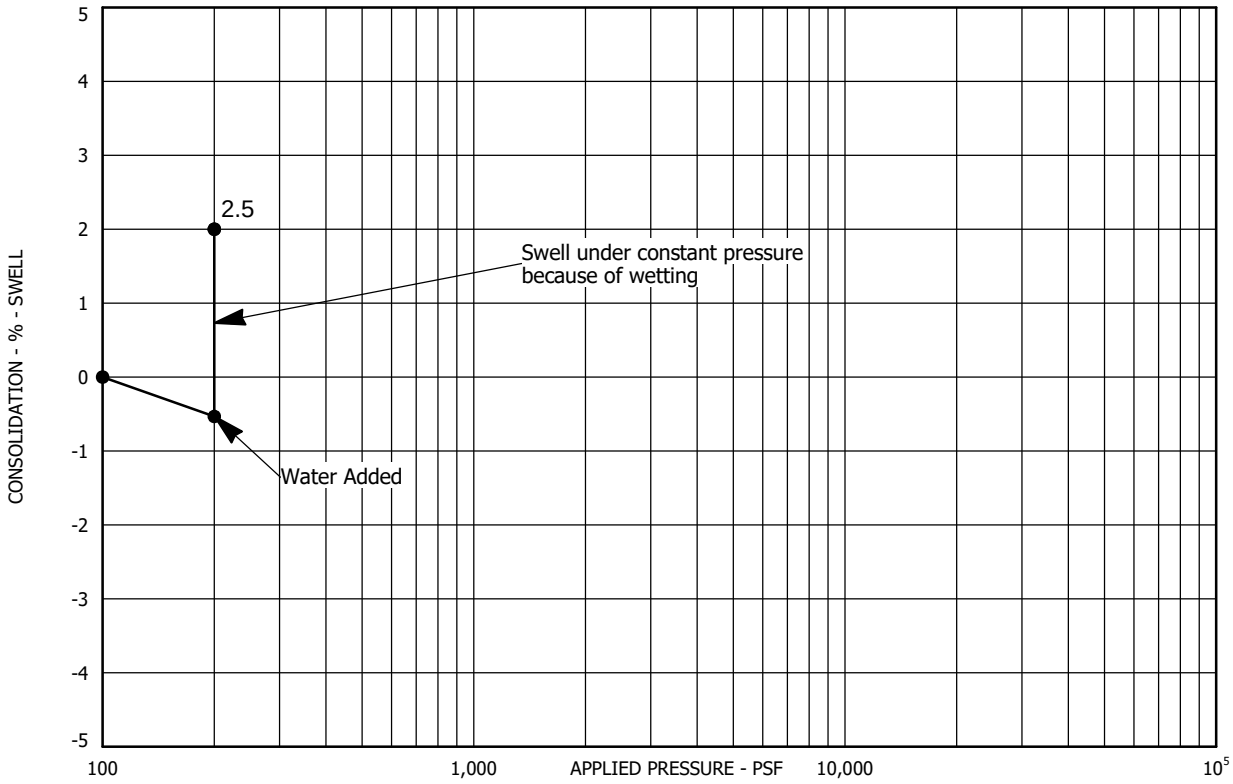



Sample Location: Test Boring No. 11 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 112
Moisture Content (%): 16

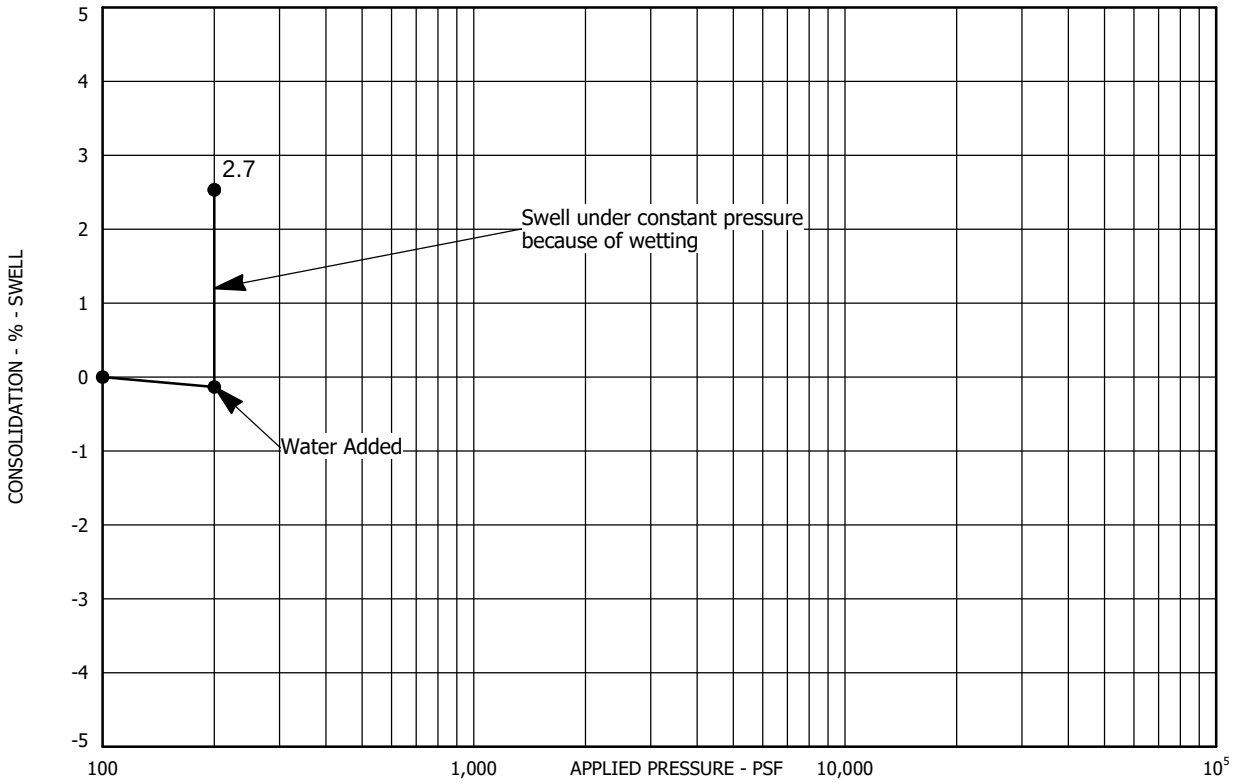
SWELL - CONSOLIDATION TEST RESULTS

FIGURE A-12

PROJECT NO. 252742-P1




Sample Location: Test Boring No. 14 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 116
Moisture Content (%): 16




Sample Location: Test Boring No. 15 at a depth of 2 feet
Sample Description: Fill, clay, slightly sandy
Dry Unit Weight (pcf): 116
Moisture Content (%): 18

SWELL - CONSOLIDATION TEST RESULTS

FIGURE A-13

PROJECT NO. 252742-P1

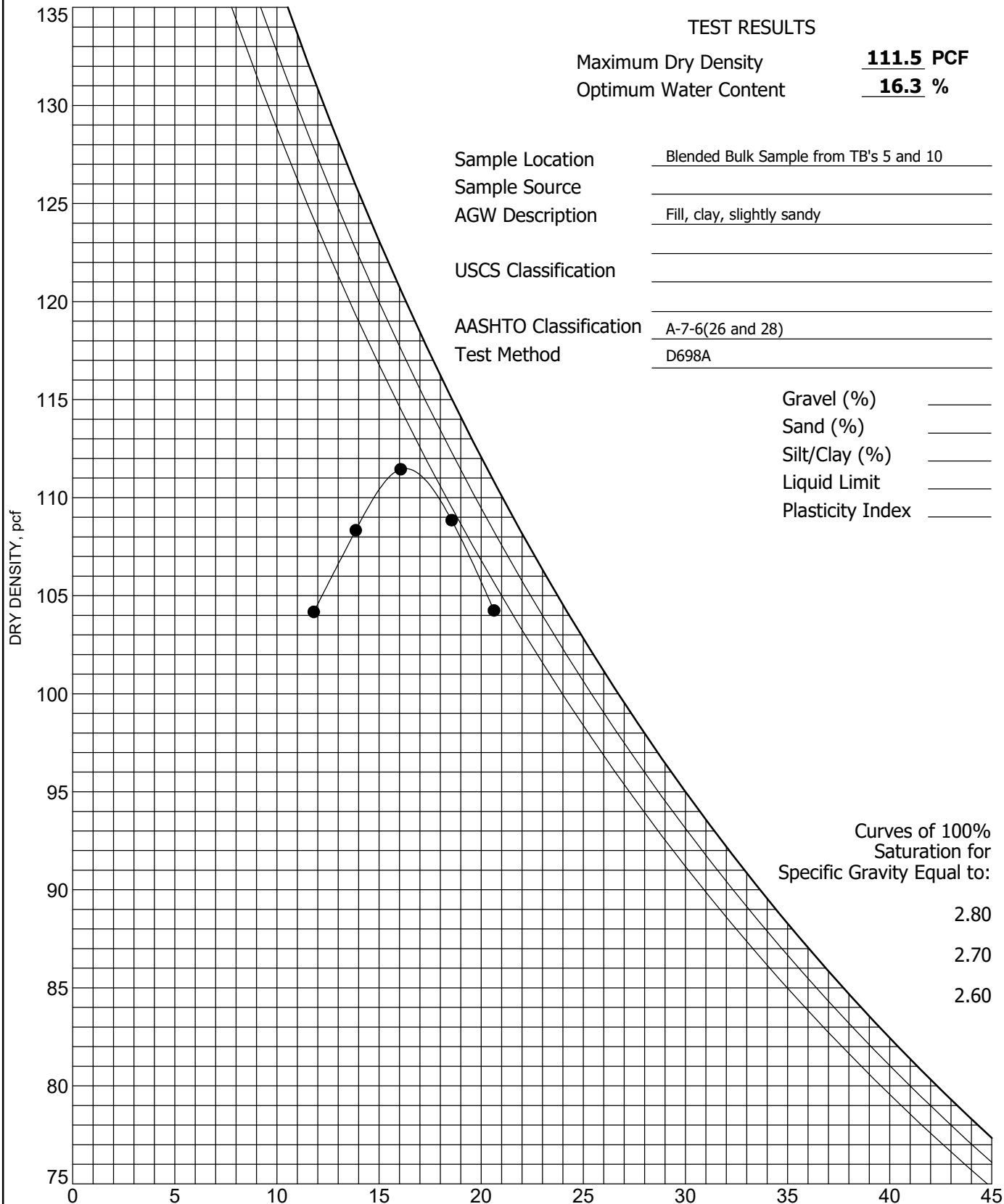
# MOISTURE-DENSITY RELATIONSHIP

**CLIENT** Richmond American Homes of Colorado, Inc.

**PROJECT NUMBER** 252742-P1

**PROJECT NAME** Trails at Aspen Ridge, Filing 4

**PROJECT LOCATION** El Paso County, Colorado




TEST RESULTS

| | |
|---|---|
| Maximum Dry Density | **111.5** PCF |
| Optimum Water Content | **16.3** % |

| | |
|---|---|
| Sample Location | Blended Bulk Sample from TB's 5 and 10 |
| Sample Source | |
| AGW Description | Fill, clay, slightly sandy |
| USCS Classification | |
| AASHTO Classification | A-7-6(26 and 28) |
| Test Method | D698A |

| | |
|---|---|
| Gravel (%) | |
| Sand (%) | |
| Silt/Clay (%) | |
| Liquid Limit | |
| Plasticity Index | |

Curves of 100% Saturation for Specific Gravity Equal to:

2.80

2.70

2.60

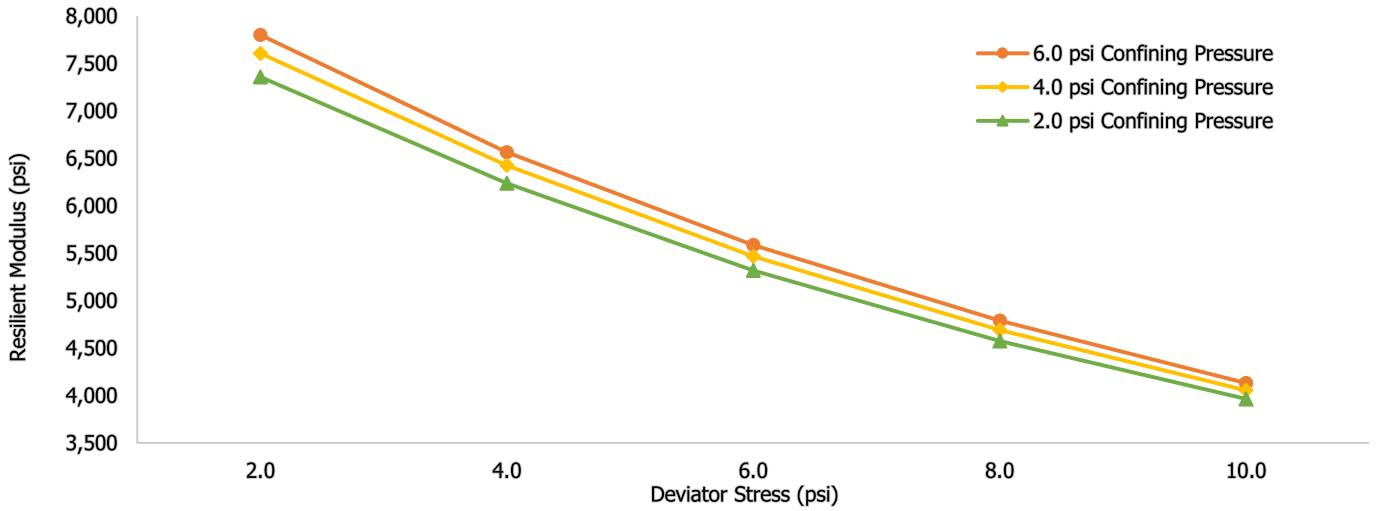
FIGURE A-14

## Resilient Modulus Testing - AASHTO T307

**Client** Richmond American Homes of Colorado, Inc.
4350 South Monaco Street
Denver, Colorado 80237

**Project Number** 252742-P1
**Project Name** Trails at Aspen Ridge, Filing 4
**Date** June 24, 2026

**Resilient Modulus Vs. Deviator Stress Graph**




| | | | |
|---|---|---|---|
| **Sample Location** | **Test Borings 5 and 10** | **AASHTO Classification** | **A-7-6 (26 and 28)** |
| **Soil Description** | **Fill, clay, slightly sandy** | **-No. 200 (%)** | **-** |
| **Height (in)** | **5.6** | **Liquid Limit** | **-** |
| **Diameter (in)** | **2.8** | **Plastic Limit** | **-** |
| **Area (in^2)** | **6.2** | **Plasticy Index** | **-** |
| **Volume (in^3)** | **34.5** | **Proctor Type** | **ASTM D698A** |
| **Remold Dry Density (pcf)** | **105.9** | **Max Dry Density (pcf)** | **111.5** |
| **Remold Moisture (%)** | **19.3** | **Optimum Moisture (%)** | **16.3** |
| **Percent Compaction (%)** | **95** | **Material Type** | **2** |
| **Water Content after (%)** | **19.3** | | |

**Loading Sequence and Test Results**

| Test Sequence | Actual Confining Pressure (psi) | Nominal Maximum Axial Stress (psi) | Actual Maximum Axial Load (lbs) | Actual Cyclic Load (lbs) | Actual Contact Load (lbs) | Actual Max Deviator Stress (psi) | Actual Cyclic Stress (psi) | Actual Contact Stress (psi) | Recoverable Deformation | | | Measured Resilient Strain (%) | Resilient Modulus (psi) |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | LVDT 1 (mils) | LVDT 2 (mils) | LVDT Average (mils) | | |
| 0 | 6.0 | 4.0 | 25.0 | 23.0 | 2.0 | 4.1 | 3.7 | 0.3 | 3.10 | 3.18 | 3.14 | 0.056 | N/A |
| 1 | 6.0 | 2.0 | 12.0 | 11.0 | 1.0 | 1.9 | 1.8 | 0.2 | 1.25 | 1.28 | 1.27 | 0.022 | 7,800 |
| 2 | 6.0 | 4.0 | 24.0 | 22.0 | 2.0 | 3.9 | 3.6 | 0.3 | 2.92 | 2.99 | 2.95 | 0.052 | 6,565 |
| 3 | 6.0 | 6.0 | 36.0 | 33.0 | 4.0 | 5.8 | 5.4 | 0.6 | 5.37 | 5.51 | 5.44 | 0.096 | 5,584 |
| 4 | 6.0 | 8.0 | 49.0 | 44.0 | 5.0 | 8.0 | 7.1 | 0.8 | 8.64 | 8.82 | 8.73 | 0.155 | 4,789 |
| 5 | 6.0 | 10.0 | 61.0 | 55.0 | 6.0 | 9.9 | 8.9 | 1.0 | 12.35 | 12.56 | 12.45 | 0.221 | 4,131 |
| 6 | 4.0 | 2.0 | 12.0 | 11.0 | 1.0 | 1.9 | 1.8 | 0.2 | 1.32 | 1.36 | 1.34 | 0.024 | 7,606 |
| 7 | 4.0 | 4.0 | 24.0 | 22.0 | 2.0 | 3.9 | 3.6 | 0.3 | 3.22 | 3.29 | 3.25 | 0.058 | 6,425 |
| 8 | 4.0 | 6.0 | 37.0 | 33.0 | 4.0 | 6.0 | 5.4 | 0.6 | 8.78 | 5.91 | 5.85 | 0.104 | 5,466 |
| 9 | 4.0 | 8.0 | 49.0 | 44.0 | 5.0 | 8.0 | 7.1 | 0.8 | 8.80 | 8.97 | 8.89 | 0.158 | 4,691 |
| 10 | 4.0 | 10.0 | 61.0 | 55.0 | 6.0 | 9.9 | 8.9 | 1.0 | 12.05 | 12.26 | 12.16 | 0.216 | 4,054 |
| 11 | 2.0 | 2.0 | 12.0 | 11.0 | 1.0 | 1.9 | 1.8 | 0.2 | 1.35 | 1.37 | 1.36 | 0.024 | 7,357 |
| 12 | 2.0 | 4.0 | 24.0 | 22.0 | 2.0 | 3.9 | 3.6 | 0.3 | 3.26 | 3.32 | 3.29 | 0.058 | 6,237 |
| 13 | 2.0 | 6.0 | 37.0 | 33.0 | 4.0 | 6.0 | 5.4 | 0.6 | 5.83 | 5.96 | 5.90 | 0.105 | 5,317 |
| 14 | 2.0 | 8.0 | 49.0 | 44.0 | 5.0 | 8.0 | 7.1 | 0.8 | 8.81 | 8.98 | 8.89 | 0.158 | 4,574 |
| 15 | 2.0 | 10.0 | 61.0 | 55.0 | 6.0 | 9.9 | 8.9 | 1.0 | 11.91 | 12.13 | 12.02 | 0.213 | 3,964 |

**Resilient Modulus** **3,964 psi** (result of test sequence 15)

**FIGURE A-15**

# APPENDIX B
## PAVEMENT THICKNESS CALCULATIONS

**DARWin FLEXIBLE PAVEMENT CALCULATIONS ..... FIGURES B-1 AND B-2**

1993 AASHTO Pavement Design

# DARWin Pavement Design and Analysis System

A Proprietary AASHTOWare
Computer Software Product

A. G. Wassenaar, Inc.

## Flexible Structural Design Module

Local Residential
Composite Section ACS / ABC
Trails at Aspen Ridge, Filing 4
El Paso County, Colorado
Project Number 252742-P1

## Flexible Structural Design

| | |
|---|---|
| 18-kip ESALs Over Initial Performance Period | 292,000 |
| Initial Serviceability | 4.5 |
| Terminal Serviceability | 2 |
| Reliability Level | 80 % |
| Overall Standard Deviation | 0.45 |
| Roadbed Soil Resilient Modulus | 3,964 psi |
| Stage Construction | 1 |
| | |
| Calculated Design Structural Number | 3.16 in |

## Specified Layer Design

| Layer | Material Description | Struct Coef. (Ai) | Drain Coef. (Mi) | Thickness (Di)(in) | Width (ft) | Calculated SN (in) |
|---|---|---|---|---|---|---|
| 1 | Hot Bituminous Asphalt | 0.44 | 1 | 5.5 | - | 2.42 |
| 2 | Aggregate Base Course | 0.11 | 1 | 19 | - | 2.09 |
| Total | - | - | - | 24.50 | - | 4.51 |

The structural section based on an SN of 3.16 would have yielded a structural section of 5.5 inches of asphalt overlying 7.0 inches of aggregate base course. The pavement section above includes 12.0 inches of aggregate base course for expansive subgrade mitigation.

FIGURE B-1

1993 AASHTO Pavement Design

# DARWin Pavement Design and Analysis System

A Proprietary AASHTOWare
Computer Software Product
A. G. Wassenaar, Inc.

## Flexible Structural Design Module

Collector
Composite Section ACS / ABC
Trails at Aspen Ridge, Filing 4
El Paso County, Colorado
Project Number 252742-P1

## Flexible Structural Design

| | |
|---|---|
| 18-kip ESALs Over Initial Performance Period | 821,000 |
| Initial Serviceability | 4.5 |
| Terminal Serviceability | 2.5 |
| Reliability Level | 85 % |
| Overall Standard Deviation | 0.45 |
| Roadbed Soil Resilient Modulus | 3,964 psi |
| Stage Construction | 1 |
| | |
| Calculated Design Structural Number | 3.94 in |

## Specified Layer Design

| Layer | Material Description | Struct Coef. (Ai) | Drain Coef. (Mi) | Thickness (Di)(in) | Width (ft) | Calculated SN (in) |
|---|---|---|---|---|---|---|
| 1 | Hot Bituminous Asphalt | 0.44 | 1 | 6.5 | - | 2.86 |
| 2 | Aggregate Base Course | 0.11 | 1 | 22 | - | 2.42 |
| Total | - | - | - | 28.50 | - | 5.28 |

The structural section based on an SN of 3.94 would have yielded a structural section of 6.5 inches of asphalt overlying 10.0 inches of aggregate base course. The pavement section above includes 12.0 inches of aggregate base course for expansive subgrade mitigation.

FIGURE B-2