

**HomeLand Acres
FIRE PROTECTION REPORT**

April 2024

PREPARED FOR:

IBT PIMA LLC
1275 Village Ridge Pt
Monument, CO 80132

PREPARED BY:

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PROJECT NO. 0419-01

EXISTING CONDITIONS

General Location

The HomeLand Acres property is 57.09 acres in total. Consisting of 1 single family (A-5) 10 acre lot and a 46.66 acre tract. The site lies in Section 4 of Township 16 South, Range 65 West. The property is located at 8180 Kane Rd, Fountain Colorado south of the Eagleside Elementary School.

Land Use

The property is presently zoned A-5 and will remain so.

Topography and Floodplains

The topography of the site and surrounding area is typical of a high desert; short prairie grass and weeds with slopes generally ranging from 1% to 12%. The area generally drains to the south and east with a smaller portion draining west and north.

Drainage flow from the property will not be changed and will continue to outfall at historic rates and location.

The Flood Insurance Rate Map indicates that there is no floodplain adjacent to or on the site.

Geology

The site is comprised of several different soil types. From the Soil Survey of El Paso County, the site falls into the following soil types:

1. "2" Ascalon sandy loam, 1 to 3 percent slopes; Type B Soil
2. "3" Ascalon sandy loam, 3 to 9 percent slopes; Type B Soil
3. "101" Ustic Torrfluvents, loamy, 0 to 3 percent slopes; Type B Soil
4. "102" Valent Sand, 1 to 12 percent slopes; Type A Soil

Note: "#" indicates Soil Conservation Survey soil classification number.

Climate

Semi-arid climate with hot summers and cold winter, light precipitation; high evaporation and moderately high wind velocities characterize the climate of the study area.

The average annual monthly temperature is 50.6 F with an average monthly low of 39.4 F in the winter and an average monthly high of 64.8 F in the summer. Two years in ten will have

a maximum temperature higher than 98 F and a minimum temperature lower than –16 F. Precipitation averages 17 inches annually, with 80% of this occurring during the months of April through September. The average annual Class A pan evaporation is 45 inches.

FIRE PROTECTION

Fire protection services are provided by the City of Fountain Fire Department. The property relies on an existing well as its water source, the well is permitted for domestic-type uses, including fire protection. The property also falls within the City of Fountain Water service area. Fire hydrants connected to The City of Fountain water system are located north of the property within the Eagleside View Subdivision and the Eagleside Elementary School. The City of Fountain operates a centralized water system that meets both domestic and fire-related demands. The City of Fountain Fire Department utilizes this water system to maintain an ISO Rating of 2. Access to the property is unimpeded, as all roadways leading to it remain unchanged. Fire trucks can reach any part of the property, as it has street access from the North, West, and South. Furthermore, the property adheres to the requirements outlined in the City of Fountain Fire Department’s 2015 International Fire Code, including any relevant amendments.

GENERAL FIRE DEPARTMENT INFORMATION

HomeLand Acres is located within the City of Fountain Fire Department service area. The property is 2.3 miles from the nearest fire station.

The average response time including dispatch, turn out and travel for the first arriving engine company is 4.59 minutes.

The City of Fountain Fire Department has assets to equip the three current fire stations. Providing fire suppression, fire prevention and education, basic and advanced medical life support, ambulance transport, hazardous materials unit, heavy rescue unit, technical rescue team and wild land fire team

The City of Fountain Fire Department consists of 52 career firefighters on shifts 24/7 and 21 volunteer firefighters. These firefighters respond from three 24/7 staffed stations.

WILDFIRE HAZARDS ANALYSIS

From the included NFDR fuel model, it is estimated that the site falls within the “L” and “T” models, which represent western perennial grass and sagebrush-grass mixture, respectively. (See Appendix A) Fire can spread relatively quickly through grasses, due to large, exposed surface areas. Low intensity fires can burn out quickly. Effects of wind on a grass fire are significant, resulting in fast rates of spreading.

To determine the potential fire hazard at a particular time, there are several considerations. The essay included in Appendix A, “Fuel Models and Fire Potential from Satellite and Surface Observations,” by Robert Burgan, Robert Klaver and Jacqueline Klaver describes the procedure to determine relative wildland fire-danger at a particular time, and where up-to-date information is available. For example, as the Experimental Fire Potential Index shows for October 4, 2006, the observed fire potential is roughly in the 20% for the area and the

forecasted fire potential is approximately 30%. The fire danger map shows a “moderate” danger, along with the forecasted danger also in the “moderate” range. In general, this area is going to be subject to more fire hazards potential during summer months and drought years.

As development has been occurring in this area, wildfire potential has decreased with urbanization and removal of “prairie” type lands. However, homes and other structures could be potential fuel for any fire which may start. The structure owners will need to address their own fire hazard issues, but protection measures such as maintaining minimum distances from roofs to low-lying limbs and using fire retardant landscaping are recommended. Due to high erosion possibilities in this area, measures should be taken to avoid or minimize barren areas and the destruction of vegetation.

This development will be part of a central water system. Hydrants will be located on-site to provide an adequate minimum 500-foot radius, which will ensure proper coverage for proposed buildings. The location of the hydrants will be coordinated with the Security Fire Protection District.

Although precautions may be taken to prevent the spread of possible fires, there is always the chance of accident, carelessness or lightning causing a fire. When vegetation is dry and winds are strong, fire potential is at its highest.

FIRM Panel

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

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Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NNGS12
National Geodetic Survey
SSM-C-45202
1315 East-West Highway
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

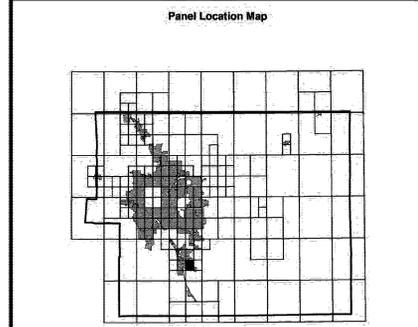
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-338-9620 and its website at <http://www.msc.fema.gov>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfp>.

El Paso County Vertical Datum Offset Table	
Flooding Source	Vertical Datum Offset (ft)

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



SITE



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined.

ZONE AE Base Flood Elevations determined.

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently deteriorated. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodplain.

ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary
Floodway boundary
Zone D boundary
CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
513 Base Flood Elevation line and value; elevation in feet*
987 Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

— Cross section line
— Transsect line

97° 07' 30.00"
32° 22' 30.00"
475000N
600000 FT
DX5510
M1.5

MAP REPOSITORIES
Refer to Map Repositories list on Map Index.
EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

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MAP SCALE 1" = 500'

250 0 500 1000
FEET
150 0 150 300
METERS

NFP

PANEL 0966G

FIRM

FLOOD INSURANCE RATE MAP

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 966 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
EL PASO COUNTY	08059	0886	G
FOUNTAIN, CITY OF	08061	0886	G

Notes to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0966G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 16 SOUTH, RANGE 65 WEST.

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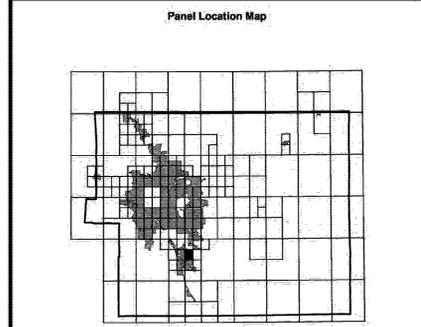
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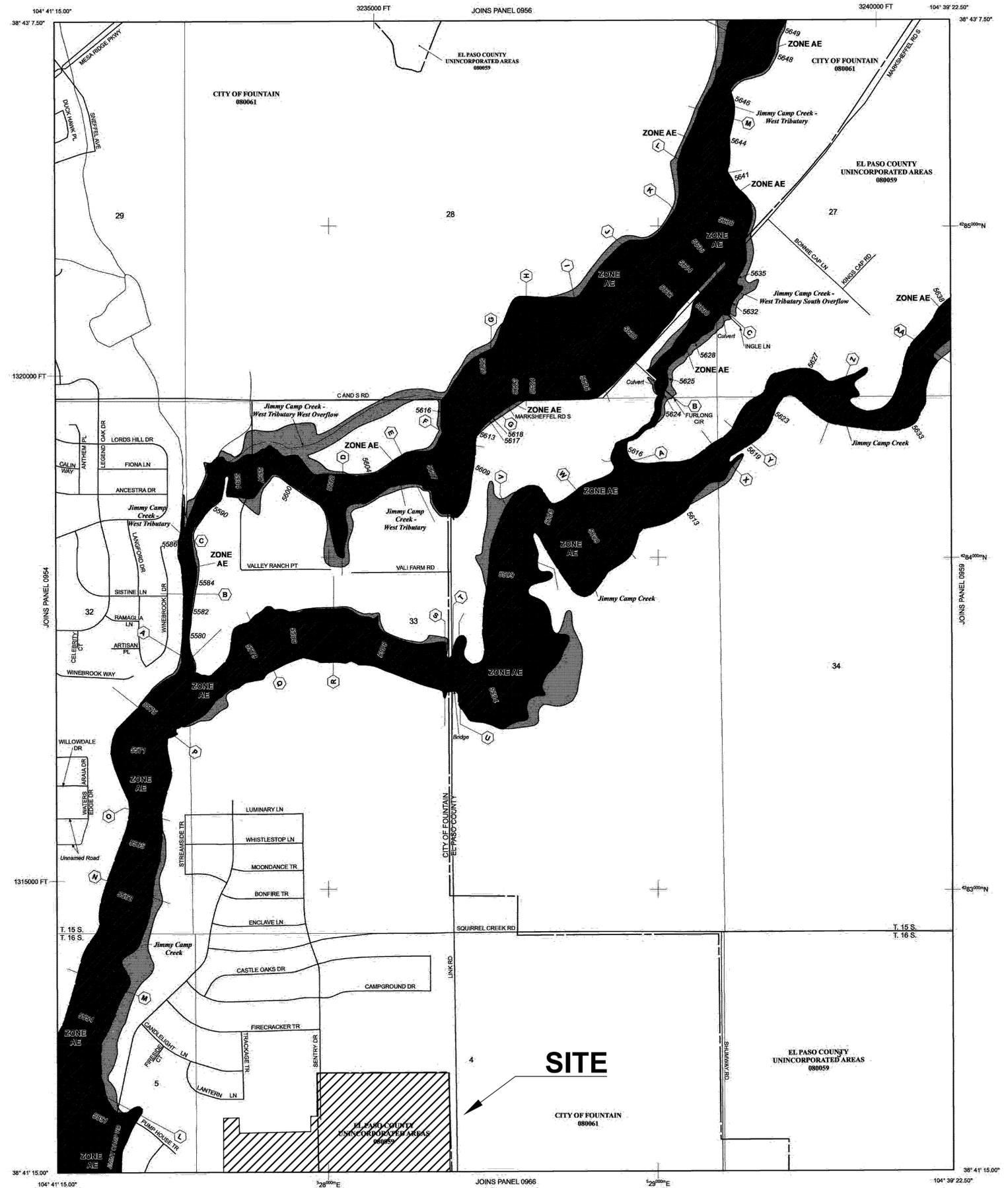
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- - - Floodway boundary
- - - Zone D boundary
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~ 513 (EL 987) Base Flood Elevation line and value; elevation in feet*
~ 513 (EL 987) Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

A A Cross section line
23 23 Transect line
97° 07' 30.00" 32° 22' 30.00" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
475mN 1000-meter Universal Transverse Mercator grid ticks, zone 13
6000000 FT 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (EPSZONE 6502), Lambert Conformal Conic Projection
DX5510 Bench mark (see explanation in Notes to Users section of this FIRM part)
M1.5 River Mile

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MARCH 17, 1997

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250 0 500 1000
FEET
150 0 150 300
METERS

PANEL 0958G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS

PANEL 958 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:	COMMUNITY	NUMBER	PANEL	SUFFIX
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FOUNTAIN, CITY OF	08061	0958	G	

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08041C0958G

MAP REVISED
DECEMBER 7, 2018
Federal Emergency Management Agency

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 15 SOUTH, RANGE 65 WEST, AND TOWNSHIP 16 SOUTH, RANGE 65 WEST.

APPENDIX A: Fuel Model and Fire Potential Essay and Maps

Fuel Models and Fire Potential from Satellite and Surface Observations

Robert E. Burgan, retired

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Robert W. Klaver

Science and Applications Branch, USGS EROS Data Center, Sioux Falls, SD 57198
Tel. 605-594-6067; FAX 605-594-6568; e-mail: bklaver@edcmail.cr.usgs.gov

Jacqueline M. Klaver

Science and Applications Branch, USGS EROS Data Center, Sioux Falls, SD 57198
Tel. 605-594-6961; FAX 605-594-6568; e-mail: jklaver@edcmail.cr.usgs.gov

Abstract

A national 1-km resolution fire danger fuel model map was derived through use of previously mapped land cover classes and Eco regions, and extensive ground sample data, then refined through review by fire managers familiar with various portions of the U.S. The fuel model map will be used in the next generation fire danger rating system for the U.S., but it also made possible immediate development of a satellite and ground based fire potential index map. The inputs and algorithm of the fire potential index are presented, along with a case study of the correlation between the fire potential index and fire occurrence in California and Nevada. Application of the fire potential index in the Mediterranean ecosystems of Spain, Chile, and Mexico will be tested.

Keywords

Fire potential; Fire danger; Fuels; Fire model; Satellite data

Introduction

The need for a method to rate wildland fire-danger was recognized at least as far back as 1940, in fire control conferences called by the Forest Service, U.S. Department of Agriculture, in Ogden, Utah. By 1954 several fire-danger rating systems were in use across the United States. In 1958 John Keetch, Washington Office, Aviation and Fire Management, headed a team to develop a national system. By 1964 most fire control organizations in the United States were using a "spread index" system. In 1968 another research effort was established in Fort Collins, Colorado to develop an analytical system based on the physics of moisture exchange, heat transfer and other known aspects of the problem (Bradshaw et al. 1983). The resulting fire spread model (Rothermel 1972) was used in the first truly National Fire Danger Rating System (NFDRS), introduced in 1972 (Deeming et al. 1972, revised in 1974). This system has since been revised twice, in 1978 (Deeming et al. 1977) and in 1988 (Burgan 1988).

Decisions fire managers must make depend on the temporal and spatial scales involved as well as management objectives. Presuppression decisions are often aimed at allocation of firefighting funds, personnel, and equipment. Such decisions usually have a large spatial context, encompassing millions of hectares, and a time scale of 1 to 3 days. Once a fire occurs initial attack and suppression decisions are directed at attaining cost-effective management of the fire. This may include a decision to not suppress the fire if it is burning within predefined constraints. These decisions have a spatial scale of a few thousand hectares and a temporal scale of 24 hours or less. Once a decision has been made to extinguish a fire, decisions are required on a spatial scale of several hundred hectares or less and a temporal scale of a few minutes to a few hours. The attitude toward wildland fire in the United States is changing from that of simply extinguishment to realization that fire must play a role in maintaining forest health, thus the need for prescribed fires is being recognized (Mutch 1994). Methods to assess fire potential both strategically and tactically must also evolve.

Assessment of fire potential at any scale requires basically the same information about the fuels, topography,

and weather conditions that combine to produce the potential fire environment. These factors have traditionally been measured for specific sites, with the resulting fire potential estimates produced as alpha-numeric text, and the results applied to vaguely defined geographic areas and temporal periods, with the knowledge that the further one is displaced (in time or space) from the point where such measurements have been taken, the less applicable the fire potential estimate is. This situation is rapidly changing because Geographic Information Systems (GIS) and space-borne observations are greatly improving the capability to assess fire potential at much finer spatial and temporal resolution.

Recent improvements to fire potential assessment technology include both broad scale fire-danger maps and local scale fire behavior simulations. In the context of local scale fire behavior, FARSITE (Finney 1994) and BEHAVE (Burgan and Rothermel 1984, Andrews 1986, Andrews and Chase 1989), provide methods to simulate fire behavior for areas up to several thousand hectares. In the broad area fire danger context, spot measurements of fire danger, calculated using the NFDRS at specific weather stations, are being interpolated and mapped on a national basis (Figure 1) through the Wildland Fire Assessment System (Burgan et al. 1997) (<http://www.fs.fed.us/land/wfas/welcome.html>).

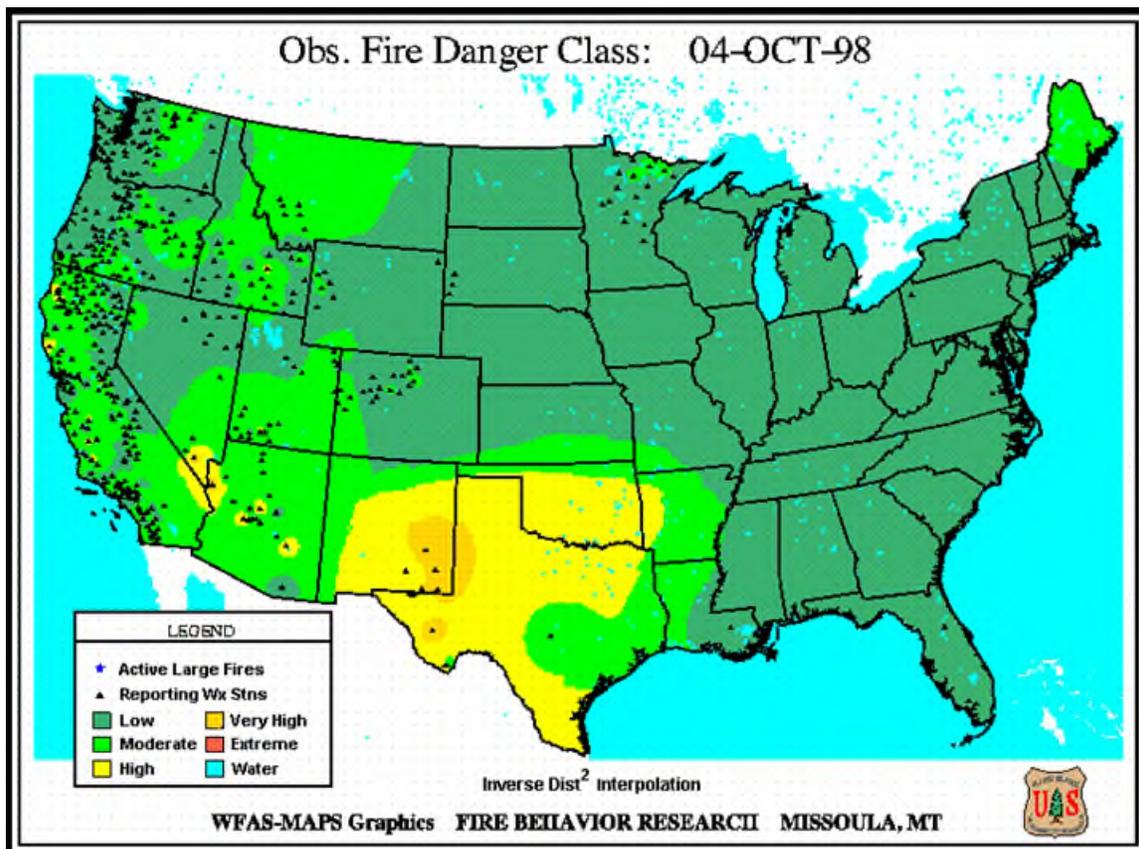


Figure 1. National Fire Danger Rating System indexes are calculated for each weather station, then the indicated staffing levels are interpolated and mapped on a national basis (http://www.fs.fed.us/land/wfas/fd_class.gif)

The Canadians publish similar maps for their fire danger system on the internet (<http://www.nofc.forestry.ca/fire/cwfis>) (Lee 1995) (Stocks et al. 1989). The U.S. maps are produced using an inverse distance squared weighting of staffing levels. Staffing level defines the readiness status of the suppression organization. It is based on comparison of current fire danger index values with historical values. The staffing (or readiness) level increases as the current index approaches historically high values. Because fire managers across the United States have not been consistent in their selection of an NFDRS index on which to base staffing levels, staffing level itself is the only common parameter with which to map fire danger. Staffing level normalizes all indexes against their historical values so it does not matter which of the several fire danger

indexes a fire manager selected. However this method neither addresses the effect of topography on fire potential, nor provides fire potential estimates for specific locations or landscape resolutions.

An operational process that does provide 1 km² landscape resolution is the Oklahoma Fire Danger Rating System (Carlson et al. 1996) (<http://radar.metr.ou.edu/agwx/fire/intro.html>), although it still does not recognize the effect of topography. The Oklahoma Fire Danger Rating System represents the direction of future fire-danger systems research for the United States, but the intensive weather network it relies upon could make this type of system difficult for others to apply.

A wildland fuel map, terrain data, and a reasonable sampling of weather are inputs to most fire danger systems. This paper discusses development of a national 1 km² fuel model map for the United States and describes a Fire Potential Index (FPI) model that can be used to assess fire hazard at 1 km² resolution.

The NFDR Fuel Model Map

Traditionally 1 to 4 fire danger fuel models (Deeming et al. 1977) have been assigned to each fire weather station. These fuel models represent the most common or most hazardous vegetation types occurring in the vicinity of the weather station. The exact geographic location represented by each fuel model has not been well defined. Progress in assessing fire potential across the landscape obviously requires much better fuels information.

In 1991, the U.S. Geological Survey's Earth Resources Observation Systems (EROS) Data Center, Sioux Falls, South Dakota, prepared a 159 class, 1 km² resolution, land cover characteristics database (Loveland et al. 1991) that portrayed vegetation patterns across the conterminous United States. The initial vegetation map was produced by unsupervised clustering of eight monthly composites of Normalized Difference Vegetation Index (NDVI) (Goward et al. 1990) data for 1990. A post classification refinement was accomplished through use of several ancillary data layers, however ground truth data was not used. It was obvious this map could provide the basis for a national fire danger fuel model map for the next generation National Fire Danger Rating System. However, because the vegetation map was designed to satisfy a wide range of applications, it was necessary to obtain ground sample data specifically for the purpose of developing an NFDRS fuel model map.

The first author and Colin Hardy of the Intermountain Fire Sciences Laboratory collaborated with the EROS Data Center to collect ground sample data for numerous locations across the U.S. Help was enlisted from numerous federal and state land management agencies to collect the ground data. (Burgan et al.1999). A total of 3500 1 km² ground sample plots were located on seven hundred 7½ minute USGS quadrangle maps (1:24000) (Figure 2).

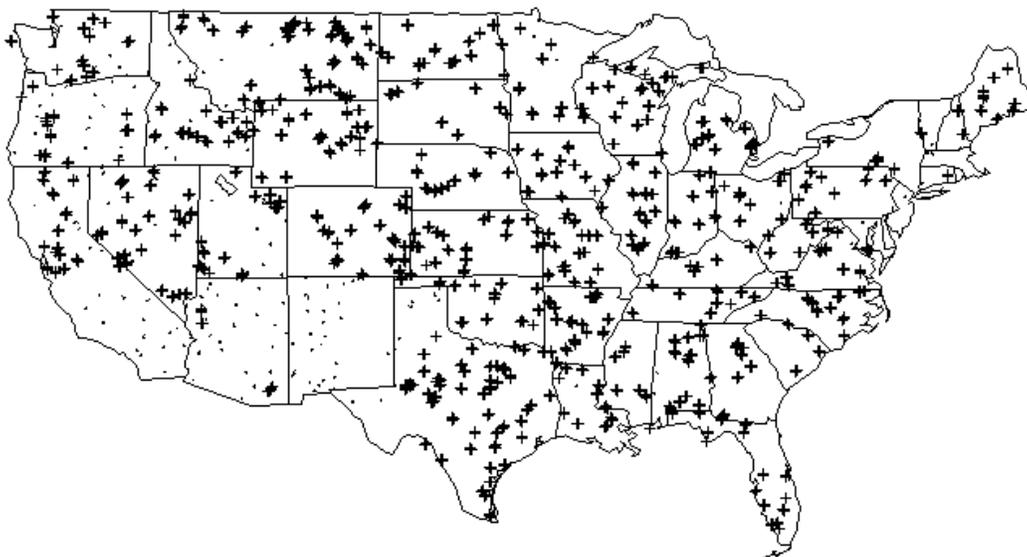


Figure 2. Ground sample data was collected from 2560 plots on these 7.5 minute USGS quadrangle maps. There were up to 5 plots per quadrangle map.

Data was obtained from 2560 of these plots. Percent cover, height, and diameter data were recorded on the four major tree and shrub species, and percent cover and depth were recorded for subshrubs, forbs, mosses and grass. Shrub and grass morphology and density classes were also recorded. Up to four 35 mm slides were taken for many of the plots. All data were entered into a database for analysis, and the slides and graphical analysis summaries were recorded on a CDROM and are available for viewing with a standard browser (Burgan et al. 1997).

Because a major objective of the ground sampling was to relate fire danger fuel models to the EROS Land Cover Classes, a fuel model assignment was required for each plot. The fuel model assignments were not made in the field however, because it was felt the diversity of people involved would produce large inconsistencies in making these assignments. Instead, one knowledgeable person was asked to review the data sheets and plot photographs to make the fuel model assignments, which were then added to the database. The Land Cover Characteristics Database also contained a map of Omernick Eco-regions (Figure 3) of the conterminous U.S. (Omernick 1987), so the eco-region for each plot was also recorded. With this data, a frequency count of fuel model by Omernick Eco-region and Land Cover Class was obtained through a contract with Statistical Sciences Incorporated, 1700 Westlake Ave. N., Seattle, WA 98109. The purpose of including eco-region data was to permit regionalizing fuel model assignments. The fuel model/eco-region/landcover associations were manually inspected and entered into a computer program that produced a 1 km² resolution fuel model map for the conterminous U.S. The program built the NFDR fuel model map by using the eco-region and landcover class values read from separate binary data files. With these inputs a table lookup method was used to determine the fuel model assignment for each 1 km square pixel. This became the "first draft" NFDR fuel model map.

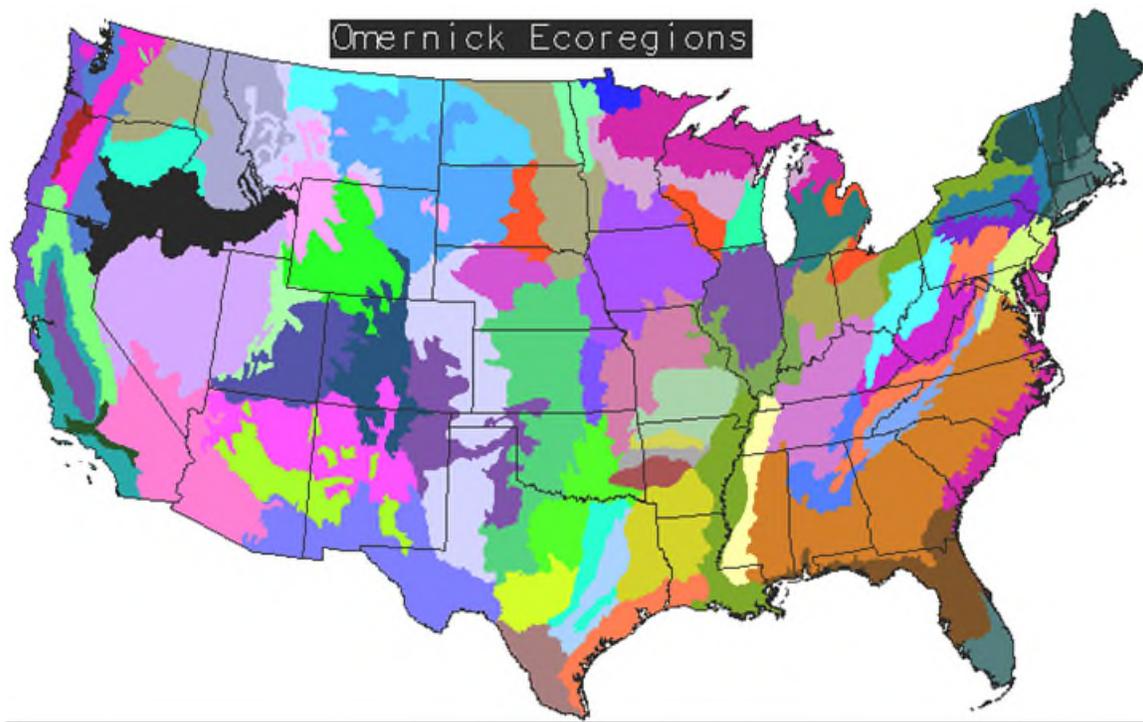


Figure3. Omernick eco-regions were used to localize refinements to the NFDRS fuel model map.

Because the ground data sample size was small for many fuel model/eco-region/landcover combinations, some fuel model assignments were made with inadequate data, thus it was felt that review by fire managers

from throughout the U.S. was necessary. This was accomplished by having individual fire managers come to the Intermountain Fire Sciences Laboratory to use the GRASS (U.S. Army Construction Engineering Research Laboratory 1988) GIS software for detailed review of the fuel model map within their area of knowledge. This process permitted alteration of fuel models by Land Cover Class within individual eco-regions by modifying the lookup table based on eco-regions and landcover class. Although there were changes, they were surprisingly limited considering the sparseness of the ground sample data. Fire danger fuel models E, I, J, and K (Deeming et al. 1977) were not used. Satellite observation of seasonal changes in vegetation greenness eliminates the need for using model E as a winter season substitute for model R, and the slash models I, J, and K don't cover sufficient area to be considered. The NFDR Fuel Model map (Figure 4) may undergo future revisions, but the most current version is on the Forest Service home page (<http://www.fs.fed.us/land/wfas/welcome.html>). The EROS Data Center has completed a 1-km resolution land cover database for the world (Belward 1996) (Loveland et al. In press). These data will provide the key to development of fuel model maps for many countries.

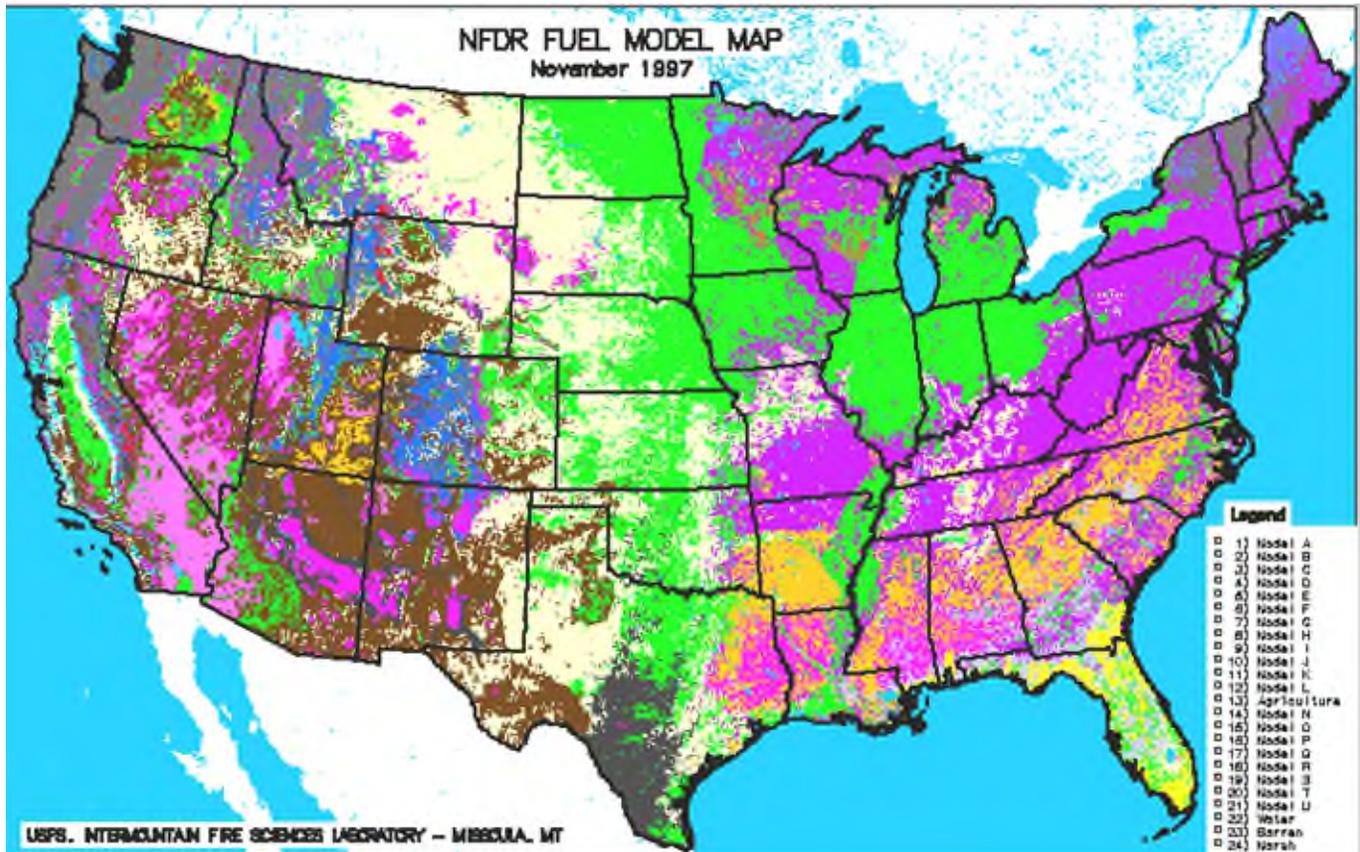


Figure4. The 1-km resolution fire danger fuel model map will be used in the next generation fire danger rating system (http://www.fs.fed.us/land/wfas/nfdr_map.htm)

The Fire Potential Index Model

Justification and Inputs

The Fire Potential Index (FPI) model was developed to incorporate both satellite and surface observations in an index that correlates well with fire occurrence and can be used to map fire potential from national to local scales through use of a GIS. The primary reasons for developing the model were: 1) to produce a method to depict fire potential at continental scale and at 1 km resolution, 2) provide a method of estimating fire potential that was simpler to operate than the current U.S. National Fire Danger Rating System.

The assumptions of the FPI model are: 1) fire potential can be assessed if the proportion of live vegetation is defined, and it is known how close the dead fine fuel moisture is to the moisture of extinction, 2) vegetation

greenness provides a useful parameterization of the quantity of high moisture content live vegetation, 3) ten hour time lag fuel moisture should be used to represent the dead vegetation because the moisture content of small dead fuels is critical to determination of fire spread, and 4) wind should not be included because it is so transitory. Thus the inputs to the FPI model are a 1-km resolution fuel model map, a Relative Greenness (RG) map (Burgan and Hartford 1993) that indicates current vegetation greenness compared to historical maximum and minimum values, a maximum vegetation greenness map, and 10 hour time lag dead fuel moisture (Fosberg and Deeming 1971) . Ten hour time lag fuels are defined as dead woody vegetation in the size range of 0.6 to 2.5 cm in diameter. These inputs must be in raster format and provided as byte data representing 1-km pixels. The output is a national scale, 1-km resolution map that presents FPI values ranging from 1 to 100.

Fuel Models

In the traditional sense, fuel models are a set of numbers that describe vegetation in terms that are required by the Rothermel fire model. Thus fuel models used in the U.S. National Fire Danger Rating System have numerous parameters that define live and dead fuel loads by size class, surface area to volume ratios of the various size classes, heat content, dead fuel moisture of extinction, wind reduction factors, and mineral and moisture damping coefficients. The FPI algorithm uses just the dead fuel extinction moisture parameter for the mapped NFDR fuel models (Table 1). Dead fuel moisture of extinction is defined as the fine dead fuel (0.6 to 2.5 cm dia) moisture content at which fires will no longer spread.

NFDR Model	Ext Moist (%)	Vegetation Represented
A	15	Western annual grasses
B	15	California mixed chaparral
C	20	Pine grass savanna
D	30	Southern rough
E	----	Hardwoods (winter)
F	15	Intermediate brush
G	25	Short needle conifers with heavy dead load
H	20	Short needle conifers with normal dead load
I	----	Heavy logging slash ¹
J	----	Intermediate logging slash ¹
K	----	Light logging slash ¹
L	15	Western perennial grasses
M	----	Agricultural land
N	25	Sawgrass or other thick stemmed grasses
O	30	High pocosin
P	30	Southern pine plantation
Q	25	Alaskan black spruce
R	25	Hardwoods (summer)
S	25	Alpine tundra
T	15	Sagebrush-grass mixture
U	20	Western long-needle conifer
V	----	Water ¹
W	----	Barren ¹
X	----	Water ¹

¹ Fire Potential Index not calculated for this case.

Table 1. Extinction moistures used in calculating the Fire Potential Index.

Maximum Live Ratio Map

In the original formulation of the FPI algorithm, maximum live ratios were determined as a function of the live and dead loads assigned to each fuel model. However, this resulted in similar live ratios for fuel models that represent very different vegetation types - not a realistic situation. The effect was to overestimate the FPI in the eastern U.S. during summer, when the vegetation is normally very green. This dilemma was resolved by deriving a maximum live ratio map from the maximum NDVI map of the conterminous United States, under the assumption of a direct relationship between the two. The algorithm used is:

$$LR_{mx} = 35 + 40 * (ND_{mx} - 100) / 80$$

where

LR_{mx} = Live ratio for a given pixel when the vegetation is at maximum greenness

ND_{mx} = historical maximum NDVI for a given pixel.

NDVI values were scaled to range from a minimum of 100 by multiplying the standard fractional NDVI data values by 100, then adding 100. This keeps NDVI within the range of binary byte data (0-255), making for efficient data compression. The value 35 is used as the lowest maximum percent green, even for arid areas of the west. That is, whatever amount of vegetation does exist, will be at least 35 percent green at its greenest, the remainder being dead vegetation from previous years growth. The value 40 scales the maximum live ratio from 35% to 75% as the maximum NDVI ranges from 100 to 180, the highest value recorded for the conterminous U.S.

Figure 5. Maximum live ratio map for the conterminous U.S.

The live ratios for the current date are determined as a function of the current Relative Greenness for each pixel, thus seasonally modifying the live/dead ratio. The 1-km fuel model map of the U.S. provides a key to the dead fuel extinction moisture value for each pixel.

Relative Greenness

Relative greenness is derived from the Normalized Difference Vegetation Index (NDVI) (Goward et al. 1990) which is calculated from data obtained by the Advanced Very High Resolution Radiometer (AVHRR) on board the National Oceanic and Atmospheric Administration's TIROS-N series of polar-orbiting weather satellites. The basis for calculating RG is historical NDVI data (1989 to present) that defines the maximum and minimum NDVI values observed for each pixel. Thus RG indicates how green each pixel currently is in relation to the range of historical NDVI observations for it. RG values are scaled from 0 to 100, with low values indicating the vegetation is at or near its minimum greenness. Specifically the algorithm is:

$$RG = (ND_o - ND_{mn}) / (ND_{mx} - ND_{mn}) * 100$$

where

ND_o = highest observed NDVI value for the 1 week composite period

ND_{mn} = historical minimum NDVI value for a given pixel

ND_{mx} = historical maximum NDVI value for a given pixel

The purpose of using relative greenness in the FPI model is to define the proportion of live and dead vegetation. The RG map has a 1-km resolution and is registered with the fuels map.

Ten Hour Time lag Fuel Moisture

Given an ignition source, the probability that a wildland fire will ignite and spread is strongly dependent on the moisture content of small dead vegetation. The U.S. National Fire Danger Rating System separates dead

fuel moisture response into time lag classes of 1, 10, 100, and 1000 hours (Deeming et al. 1977), meaning that their moisture content will change about 2/3 of the difference between initial and final conditions in one time lag period. Anderson (Anderson 1985) has shown that most dead wildland vegetation primarily involved in determining fire spread rate is in the 1 to 10 hour time lag response category, with only very fine fuels such as cheatgrass having response times of 1 hour or less. On this basis 10 hour time lag fuel moisture was selected to represent the moisture content of all dead vegetation in the 1 to 10 hour time lag size classes.

Ten hour fuel moisture is calculated from temperature, relative humidity, and state of the weather (cloudiness and occurrence of precipitation). These data are measured at surface weather stations and must be extrapolated across the landscape to meet the FPI model input requirement of 1-km resolution byte data. The process currently used to extrapolate this point data to a 1-km grid is an inverse distance squared algorithm. The advantage of this process is that it is convenient and simple to perform. The disadvantage is that it does not account for the influence of topography on fuel moisture. If the weather station network is reasonably dense, with weather stations at both high and low elevations, the resulting interpolations are quite useable. But if the weather station network is too sparse or all the weather stations are at low elevations, the interpolations are not adequate. Improvement of the process for calculating 10-h TLFM is the subject of further work.

The Model

The FPI model uses the proportion of the vegetation that is live, and the ratio of ten hour time lag dead fuel moisture to the moisture of extinction, for estimating relative fire potential. The fuel model map is used to reference the dead fuel extinction moisture for each pixel, and Relative Greenness is used to determine the proportion of the surface vegetation that is live (Fig 6a).

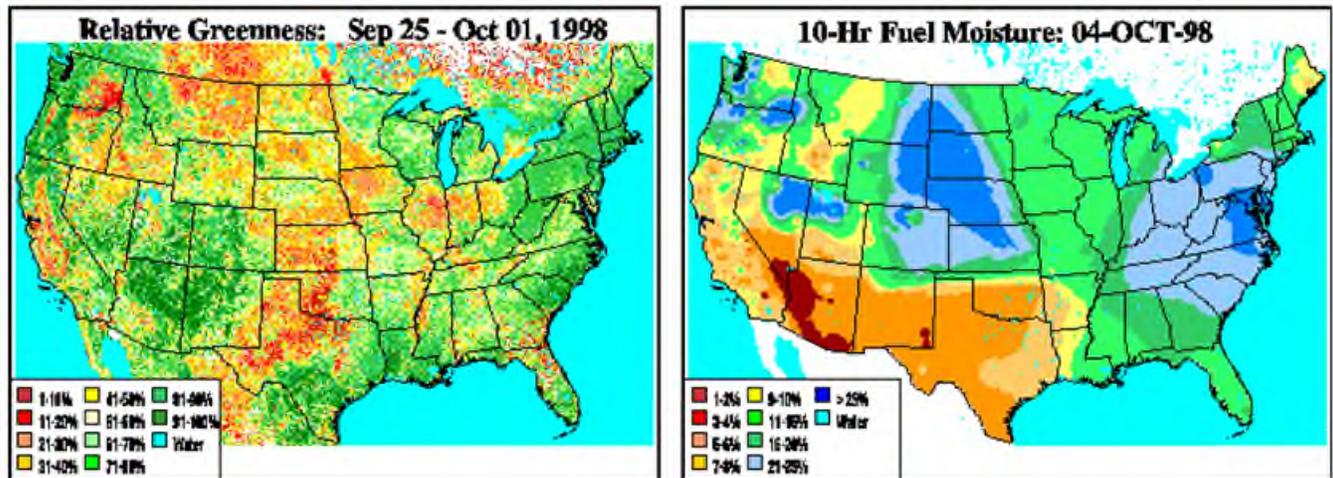


Figure 6a. Relative greenness, 10-hour fuel moisture maps, and NFDR fuel model (fig. 4) and the maximum live ratio (fig.5) maps are inputs to the FPI map calculation.

The FPI index is scaled from 1-100. The specific process for each pixel is to obtain the inputs from the 1-km fuel model, Relative Greenness, 10-h TLFM, and maximum live ratio maps, then perform the following calculations:

Set the FPI to a "no data" value greater than 100

- (1) $FPI = 105$

Convert RG to a fractional value

- (2) $RG_f = RG/100$

Relative greenness fraction is used to determine the current live fuel ratio (LR) for the pixel.

$$(3) LR = RG_f * LR_{mx} / 100$$

Fractional 10-h TLFM is normalized on dead fuel moisture of extinction (MX_d) for the fuel model, expressed as a percent (Table 1). Dead fuel moisture of extinction is defined as the dead fuel moisture at which a fire will not spread (Rothermel 1972). It varies from one vegetation or fuel type to another and is generally higher for moist climates such as the southeastern U.S. Ten hour fuel moisture (percent of dry weight) is normalized to the moisture of extinction to produce a fractional ten hour moisture scaled the same as fractional relative greenness (0-1). Ten hour fuel moisture is limited to a minimum of 2 percent, thus subtracting 2 from both the 10 hour moisture and the extinction moisture allows TN_f to reach zero when the ten hour moisture is at its minimum value and provides a convenient method of scaling the FPI from 0 to 100. The fractional ten hour moisture is smoothed near its minimum and maximum limits (0 and 1) to avoid discontinuities.

$$(4) TN_f = (FM_{10} - 2) / (MX_d - 2)$$

where

TN_f = fractional ten hour fuel moisture

FM_{10} = ten hour moisture (percent)

MX_d = dead fuel extinction moisture (percent)

The FPI calculation is performed only if the this pixel represents a valid fuel model, i.e. not agriculture, barren, etc. The live ratio (LR) defines the proportion of live vegetation, and inversely the proportion of dead vegetation (proportion dead equals 1 minus proportion live). Because live vegetation is green, it is assumed to have a high moisture content, thus reducing fire potential. The dead vegetation, as calculated from current weather data, has a relatively low moisture content -- less than 30%. Thus the FPI can be thought of as a "dryness" fraction times a "deadness" fraction.

$$(5) FPI = (1 - TN_f) * (1 - LR) * 100$$

where

FPI = fire potential index

Equation (5) produces FPI values that can range from 0 to 100. The FPI will equal 0 when the TN_f is 1 (the dead fuel moisture equals the moisture of extinction) or the LR value is 1 (the vegetation is fully green). These circumstances do occur, but the FPI is limited to a minimum value of 1 so that areas outside the United States can be identified as the value 0 (no data). The FPI will attain a value of 100 if the LR is 0 (all the vegetation is cured) and the 10 hour time lag fuel moisture is at its minimum value of 2 percent.

Fuel model map pixels that indicate agricultural lands are assigned an FPI value of 101. The RG image for the current composite period is processed by the EROS Data Center in a manner to indicate clouds, so pixels appearing cloudy in the RG map can be mapped as cloudy (102) in the FPI map. Pixels indicated as barren lands in the fuel model map are assigned an FPI value of 103, and marsh land pixels are assigned a value of 104. Water pixels are assigned a value of 255. A "C" program to perform these calculations is available from the author. The resulting output is a gridded raster file that can be displayed and analyzed using a GIS, or from which a graphics image can be prepared. Figure 6b illustrates the relationship between the FPI map and the standard NFDR map for October 4, 1998.

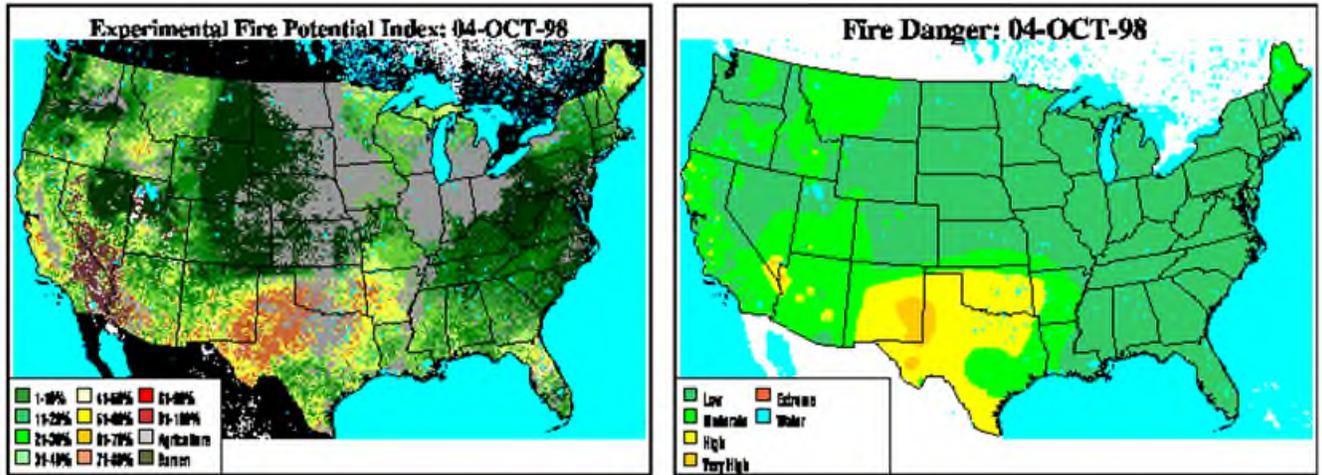


Figure 6b. The standard NFDRS map is provided for comparison with the fire potential index map (http://www.fs.fed.us/land/wfas/exp_fp_4.gif).

Model Application

Fire Potential Maps derived from this model were first introduced to fire managers in California and Nevada in 1996. Their response was very favorable, but anecdotal. In the fall of 1996 we required a simple method to assess fire potential in Mediterranean environments as part of a project sponsored by The Pan American Institute for Geography and History (PAIGH) (Klaver et al. 1997). PAIGH, in cooperation with the U.S. Geological Survey EROS Data Center, the Instituto Geografico Nacional, Spain, the Instituto Geografico Militar de Chile, and the Instituto Nacional De Estadística Geografía e Informática, Mexico is supporting the project "Digital Imagery for Forest Fire Hazard Assessment for the Mediterranean Regions of Chile, Mexico, Spain, and the U.S." In support of this effort we calculated daily FPI maps for mid-March to late October for the years 1990-1995, and performed statistical analyses of the correlation between fire occurrence and the FPI. The California Division of Forestry supplied the required weather data and the fire location data. We looked at the distribution of FPI values for 1990 -1994 in two contexts: 1) FPI for only those pixels in which a fire occurred (Fig. 7), and 2) FPI for all the pixels within the study area (Fig 8), which was basically California and Nevada.

Fire Potential of Fires 1990 - 1994

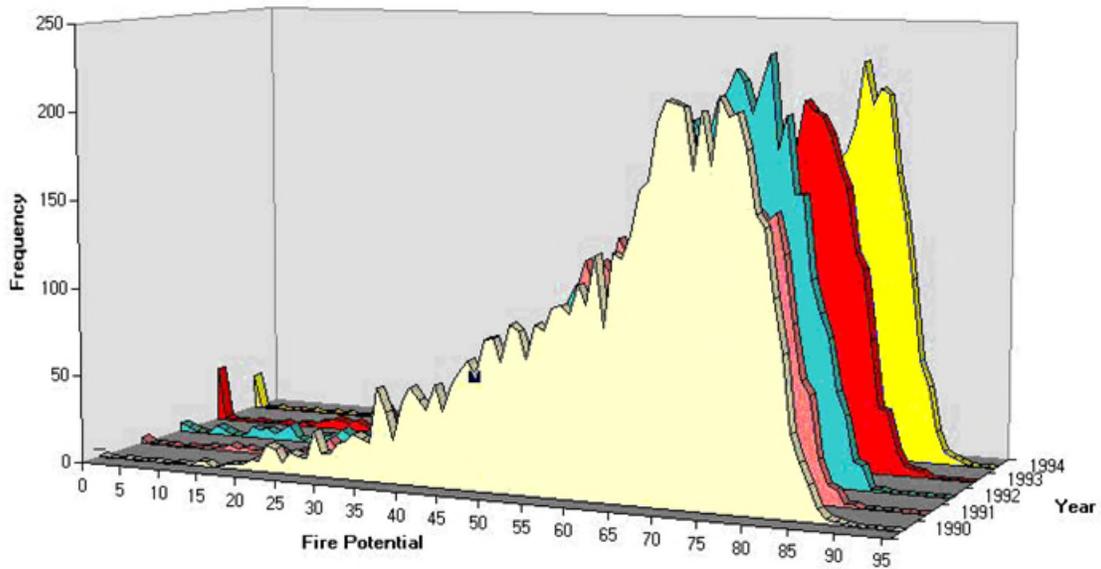


Figure 7. For only those pixels in which fires occurred, in the years 1990 to 1994, the frequency of FPI index values is shown.

Fire Potential of the Landscape 1990 - 1994

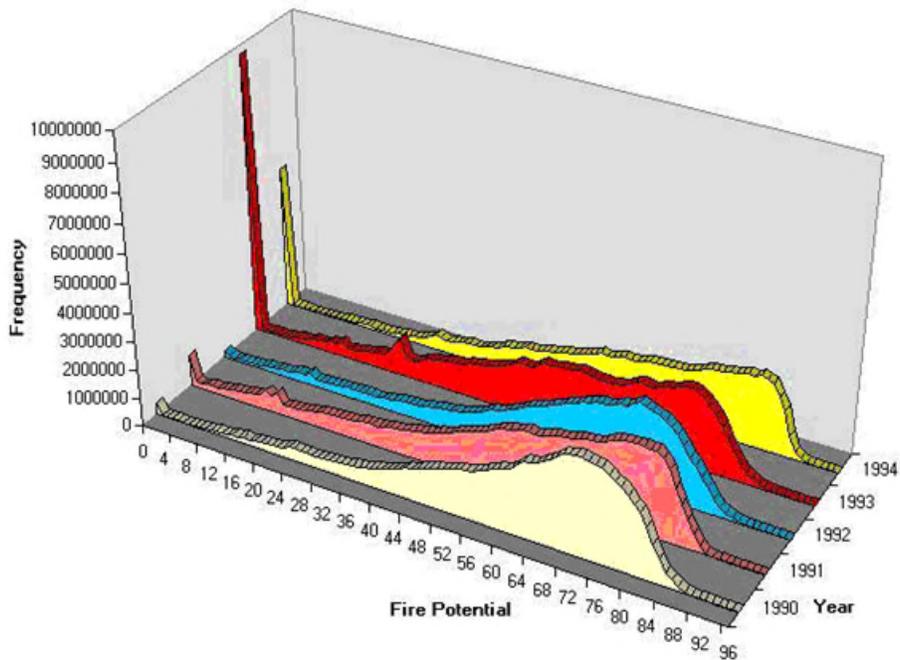


Figure 8. The frequency of pixels in the entire study area is shown for Fire Potential Index values calculated for 1990 to 1994.

For the first case the frequency distribution of FPI values was very similar for all years, indicating that in spite of fire season variability the relationship between fire occurrence and the FPI remains relatively constant. For the second case the frequency distribution of FPI values for all pixels varied between years, indicating that the FPI can discriminate fire season severity in the broad geographical sense. Correlation between the FPI and fire occurrence was very high, with r^2 values by year of: 1990, 0.44; 1991, 0.85; 1992, 0.87; 1993, 0.90; and 1994, 0.88. The r^2 value for all years combined was 0.72. The reason for the low correlation for 1990 is unknown, but could be due to changes in calibration of the AVHRR sensor, accuracy of fire location, or the two week rather than one week compositing period.

Annual comparisons show that the linear equations for the FPI and fire density were statistically identical for 1991, 1993, and 1994 ($r^2=0.825$, $df=1$ and 318 , $F=375.05$, $p=0.0$). The linear equation for 1990 was different from these years in both slope and intercept. The linear equation for 1992 had a greater intercept than the other years but the same slope (Figure 9). That is, fire occurrence was greater for a given FPI value in 1992 than for 1991, 1993, and 1994.

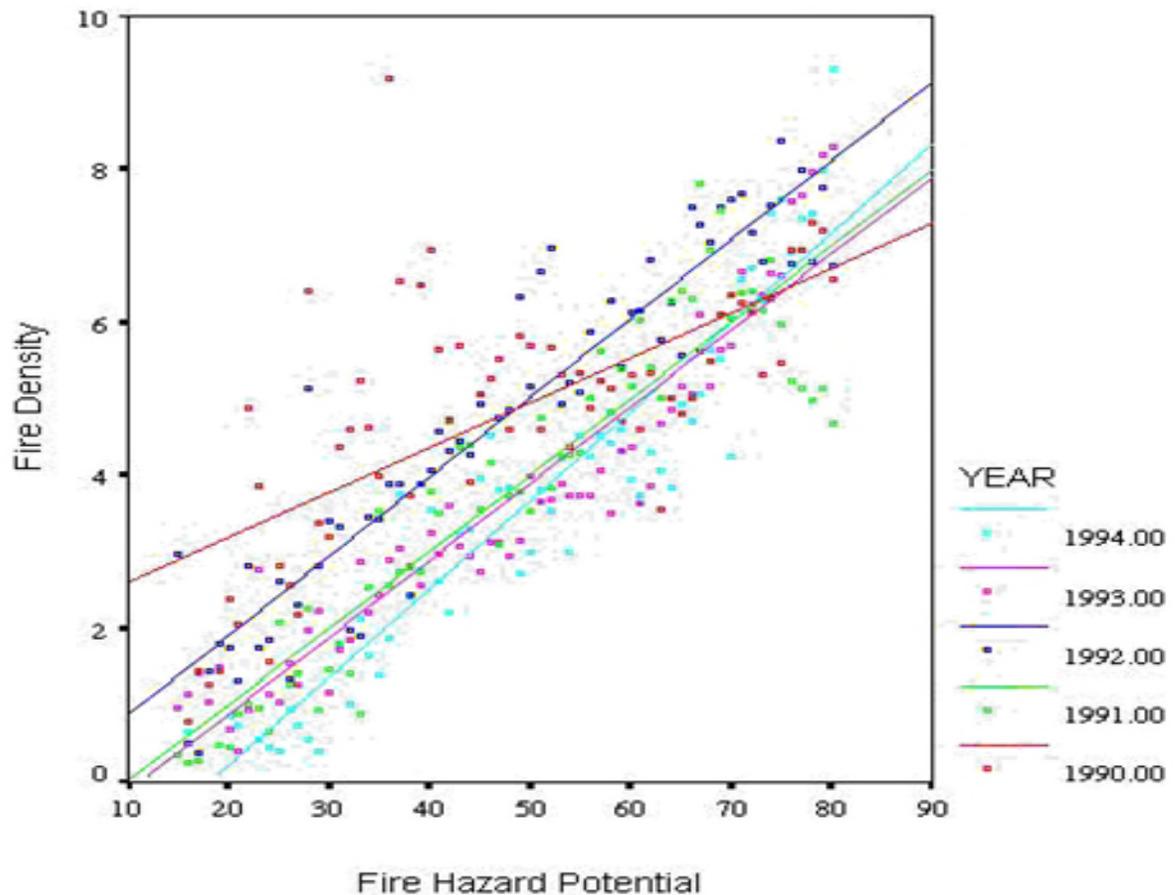


Figure 9. The slopes of the regression lines are very similar for all years except 1990.

The FPI map is also being tested, along with several NFDR indexes, for application to the problem of assessing seasonal fire severity for the United States. This is an important and difficult problem for which there is no standard procedure at this time. The problem is important because millions of dollars are made available to those Forest Service Regions that can show they expect to experience a fire season that is considerably more severe than average, and difficult because the decision of where to place the additional funds must be made 2-4 weeks in advance of the expected fire problems. The accuracy of these decisions depends on the accuracy of long range weather forecasting, so making the process simple in terms of weather requirements is important.

Conclusions

The FPI appears to be strongly correlated with fire occurrence and is well adapted to portraying fire potential across both large geographic areas and for local areas down to a few square kilometers. It is not a physically based model and thus requires enough historical data to develop the statistical relationships that can provide fire probability given a specific FPI value. Use of the FPI requires a fuel model map, a maximum live ratio map, access to current RG maps as calculated from AVHRR/NDVI data, and a reasonably dense network of surface weather stations. The 10-h time lag fuel moistures must be calculated from the weather station data and interpolated for all 1-km pixels. Efforts are underway to improve the interpolation procedure. The results of FPI tests for California and Nevada indicate that it may be a valuable tool for fire managers in other countries. This will be determined by future tests in the Mediterranean ecosystems of Spain, Chile, Argentina and Mexico.

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Update (5/2000).

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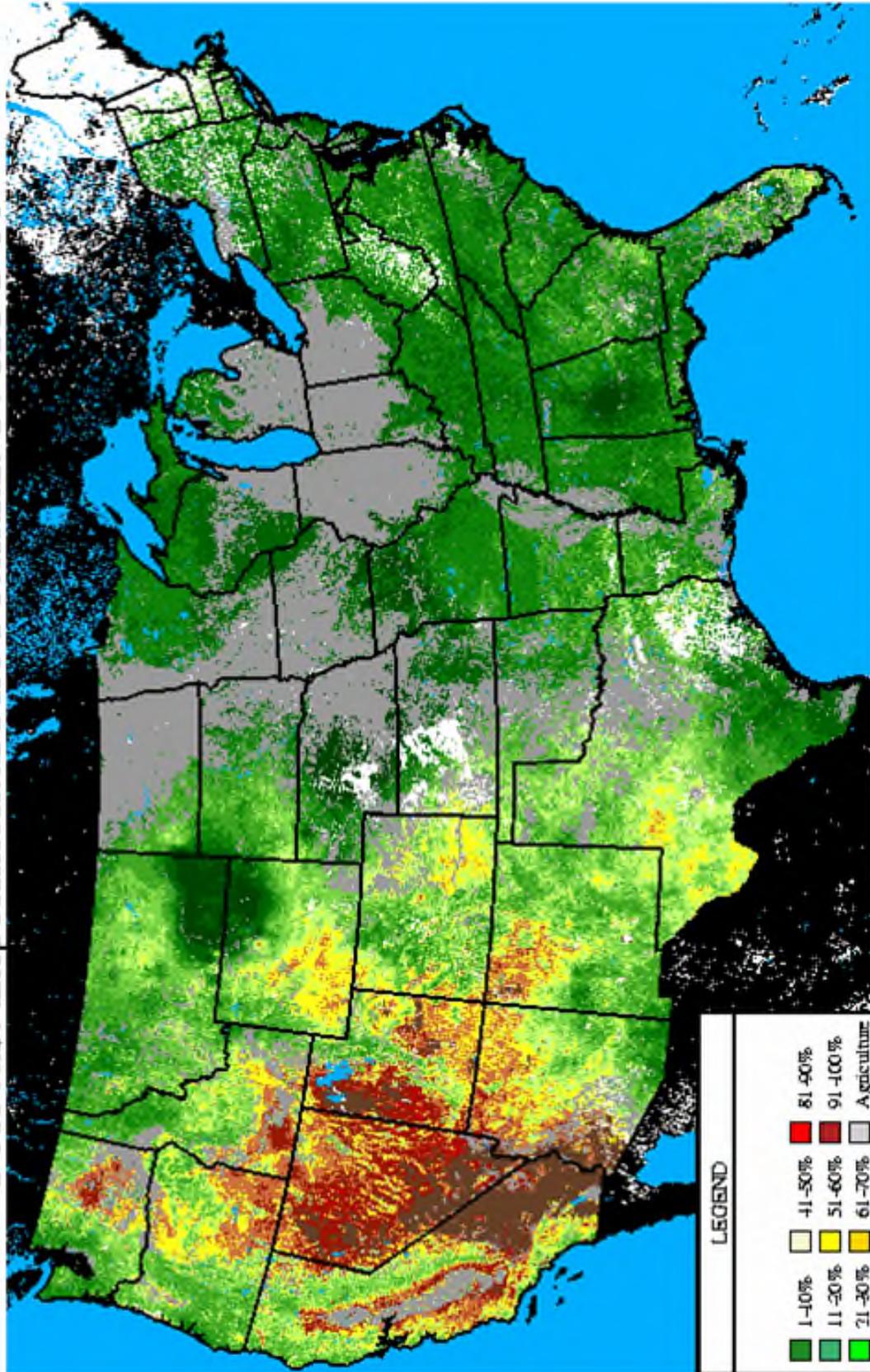
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Forecast Experimental Fire Potential: 14-AUG-08

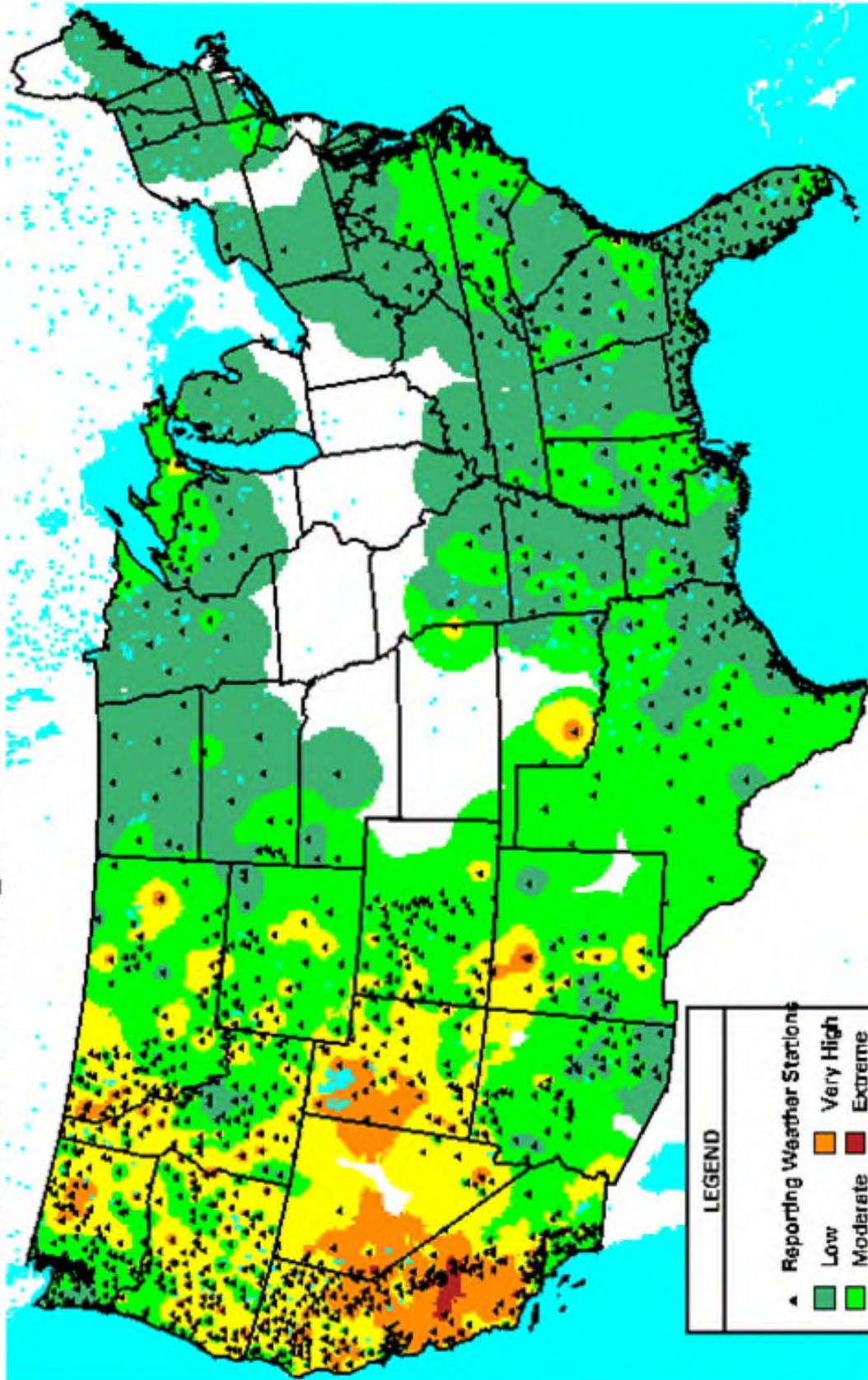


LEGEND

1-10%	41-50%	81-90%
11-20%	51-60%	91-100%
21-30%	61-70%	Agriculture
31-40%	71-80%	Bare

WFAS-MAPS Graphics FIRE BEHAVIOR RESEARCH MISSOULA, MT

Forecast Fire Danger Class: 14-AUG-08



LEGEND

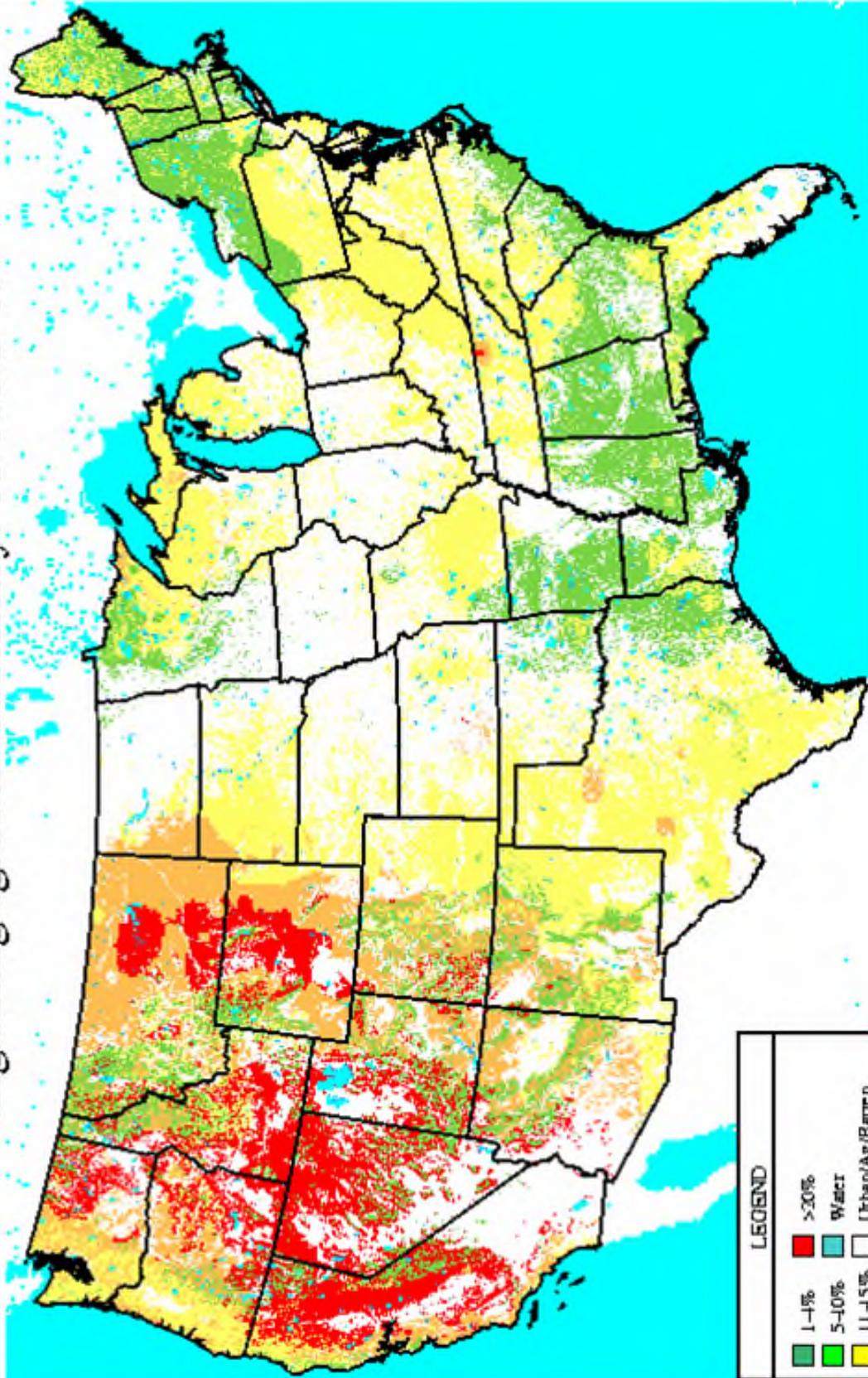
▲ Reporting Weather Stations	Low	Very High
Green	Moderate	Extreme
Yellow	High	Water

(Inv. Dist.² Interp.)

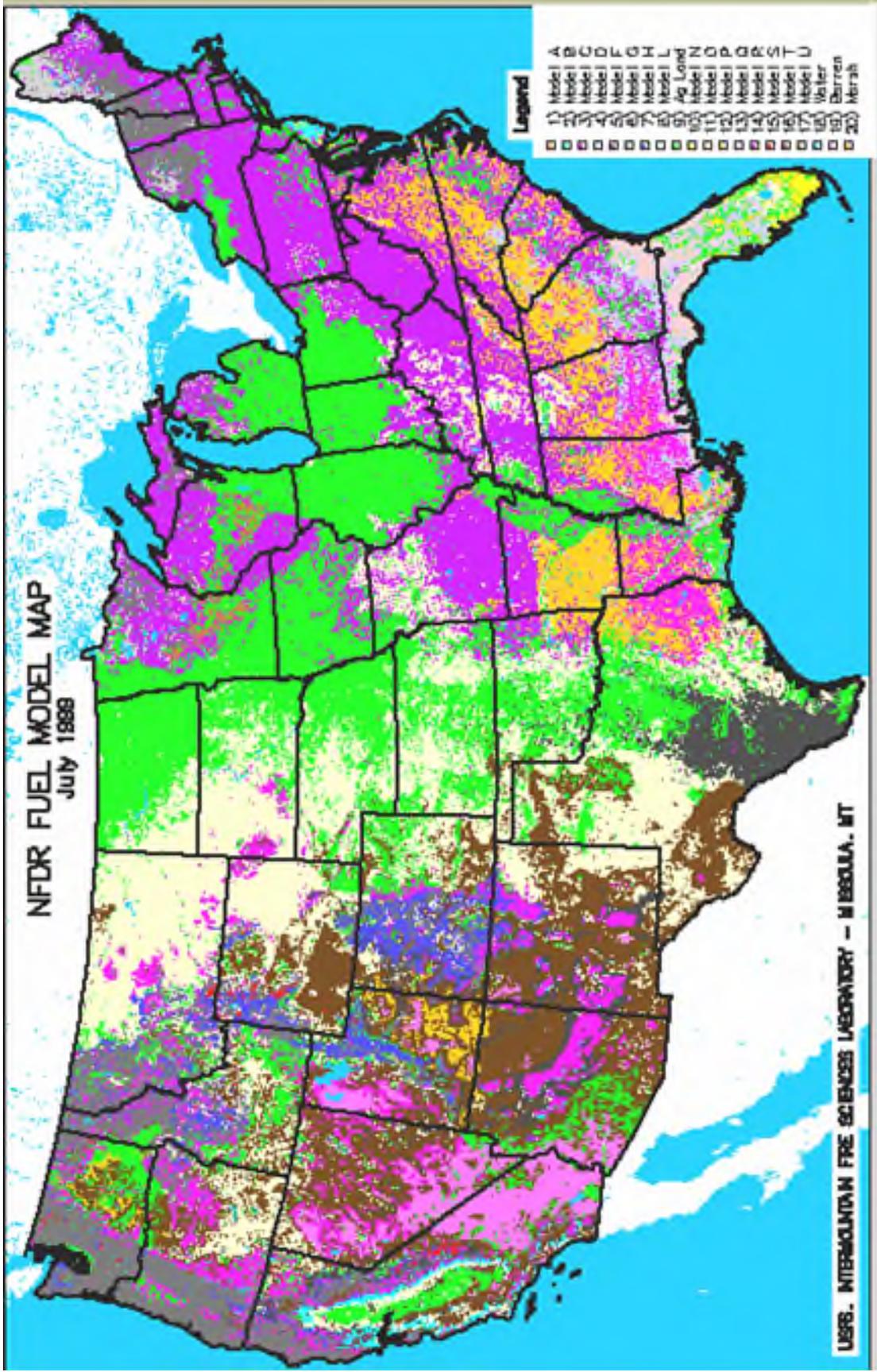


WFAS-MAPS Graphics FIRE BEHAVIOR RESEARCH MISSOULA, MT

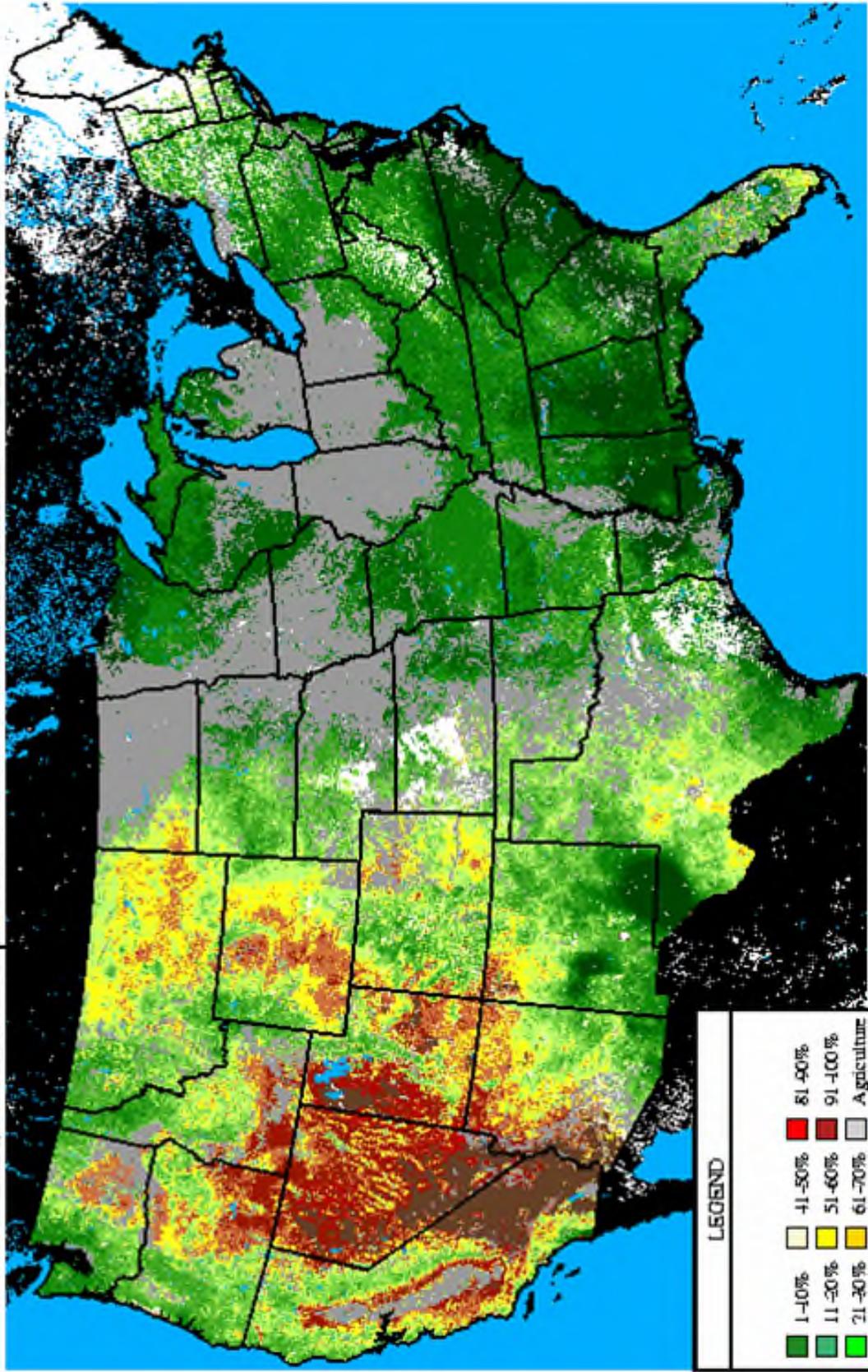
Lightning Ignition Efficiency: 13-AUG-08



WFAS-MAPS Graphics National Interagency Fire Center Boise, ID



Observed Experimental Fire Potential: 13-AUG-08

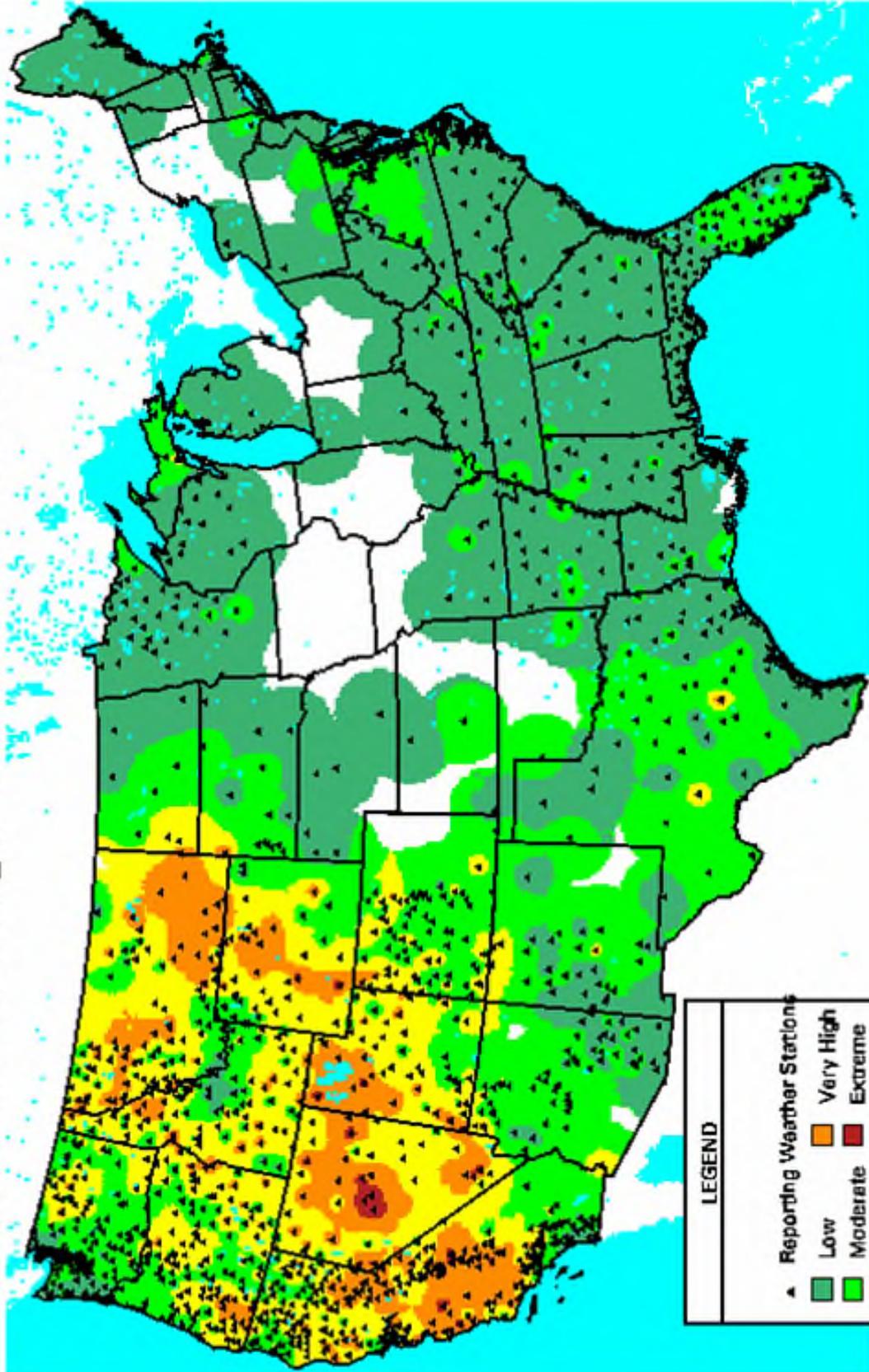


LEGEND

1-10%	41-50%	81-90%
11-20%	51-60%	91-100%
21-30%	61-70%	Agriculture
31-40%	71-80%	Barred

WFAS-MAPS Graphics FIRE BEHAVIOR RESEARCH MISSOULA, MT

Observed Fire Danger Class: 13-AUG-08



(Inv. Dist.² Interp.)
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