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MEMORANDUM

DATE: September 27, 2024

TO: Adam Lancaster – CDOT R2 Permits Manager

FROM: Jeffrey C. Hodsdon, P.E. - LSC Transportation Consultants, Inc.

SUBJECT: Monument Ridge East
RE: Traffic Impact Study
Response to CDOT Comments Memorandum
LSC #S234450
EPC PCD File Nos. P245, P246, SP241

Following are the LSC Transportation Consultants, Inc. responses to the September 10, 2024 Comment Letter from CDOT – Region 2 – Traffic & Safety – Permits regarding the Monument Ridge East project.

COUNTY LINE ROAD/I-25 RAMP INTERSECTIONS LONG-TERM (2044) REVISED LOS ANALYSIS & QUEUING ANALYSIS

Per CDOT direction from the meeting on September 25, 2024, a separate, exclusive, northbound-right turn lane at the I-25 northbound off-ramp intersection with County Line Road has been added. The following presents updated level of service and vehicle queuing analysis at the northbound-ramp intersections with County Line Road. The analysis continues to show, as in the August 2024 TIS, the need for all-way stop control (AWSC) at the I-25 southbound ramp intersection to mitigate a projected LOS F for the southbound approach with TWSC.

Traffic Volumes

Volumes used in this analysis are shown in Figure 10 of the August 6, 2024 TIS report (copy attached for reference). The Long-Term “Total” (2044 Background plus Site-Generated) AM and PM peak-hour traffic volumes have been analyzed.

Level of Service Analysis

The following presents a summary of the results. For additional detail, please refer to the *HCM* TWSC and AWSC analysis reports, which have been attached for reference.

2044 Total AM

Assuming use of all-way stop control, all individual turning movements and single-lane approaches at the I-25 southbound ramp intersections are projected to operate at LOS D or better during the 2044 Total AM scenario.

With the addition of a northbound right turn lane at the I-25 northbound ramps, and assuming a stop sign on the northbound approach only (TWSC analysis procedure), all individual turning movements are projected to operate at LOS D or better during the 2044 Total AM scenario.

2044 Total PM

Assuming use of all-way stop control, all individual turning movements and single-lane approaches at the I-25 southbound ramp intersections are projected to operate at LOS D or better during the 2044 Total PM scenario.

With the addition of a northbound right-turn lane at the I-25 northbound ramps, and assuming a stop sign on the northbound approach only (TWSC analysis procedure), all individual turning movements are projected to operate at LOS D or better during the 2044 Total PM scenario.

Queuing Analysis

The following presents a summary of the results. For additional detail, please refer to the *HCM* TWSC and AWSC analysis reports.

No individual turn lanes or single-lane approaches at either I-25 ramp intersection are projected to experience any upstream or storage block time during the 2044 Total AM or PM scenarios. There are at least 300 feet for queuing between the ramp intersections. Projected queues would be accommodated on all approaches at both I-25 ramp intersections.

2044 Total AM

HCM AWSC queuing results for each individual turn lane or single-lane approach at the I-25 southbound ramp during the 2044 Total AM peak hour are summarized below:

| Queue Lengths I-25/County Line Road Southbound Ramp Intersection AM Peak Hour – 2044 Total Traffic | | | | |
|---|-----|-----|-----|----|
| Queuing Metric | EB | WBL | WBT | SB |
| 95th-Percentile Queue (vehicles) | 1.7 | 6.8 | 1.3 | 1 |

HCM TWSC queuing analysis results for each individual turn lane for yielding movements at the I-25 northbound-ramp intersection during the 2044 Total AM peak hour are summarized below:

| Queue Lengths I-25/County Line Road Northbound Ramp Intersection AM Peak Hour – 2044 Total Traffic - TWSC | | | |
|--|-----|-------|-----|
| Queuing Metric | EBL | NB LT | NBR |
| 95th-Percentile Queue (vehicles) | 0.3 | 0.9 | 0.4 |

2044 Total PM

HCM AWSC queuing results for each individual turn lane or single-lane approach at the I-25 southbound ramp intersection during the 2044 Total PM peak hour are summarized below:

| Queue Lengths I-25/County Line Road Southbound Ramp Intersection PM Peak Hour – 2044 Total Traffic - AWSC | | | | |
|--|-----|-----|-----|-----|
| Queuing Metric | EB | WBL | WBT | SB |
| 95th-Percentile Queue (vehicles) | 6.3 | 1.6 | 1.9 | 5.1 |

HCM TWSC queuing analysis results for each individual turn lane for yielding movements at the I-25 northbound ramp intersection during the 2044 Total PM peak hour are summarized below:

| Queue Lengths I-25/County Line Road Northbound Ramp Intersection PM Peak Hour – 2044 Total Traffic - TWSC | | | |
|--|-----|-------|-----|
| Queuing Metric | EBL | NB LT | NBR |
| 95th-Percentile Queue (vehicles) | 0.2 | 1.5 | 2.7 |

ALL-WAY STOP CONTROL WARRANTS EVALUATION

The following is an excerpt from the *MUTCD* regarding “warrants” for all-way stop control (AWSC):

Section 2B.12 All-Way Stop Control

Support:

01 The provisions in the following sections describe warrants for the recommended engineering study to determine all-way stop control. Warrants are not a substitute for engineering judgment. The fact that a warrant for a particular traffic control device is met is not conclusive justification to install or not install all-way stop control. Because each intersection will have unique characteristics that affect its operational performance or safety, it is the engineering study for a given intersection that is ultimately the basis for a decision to install or not install all-way stop control.

02 All-way stop controls at intersections with substantially differing approach volumes can reduce the effectiveness of these devices for all roadway users.

Guidance:

03 *The decision to establish all-way stop control at an unsignalized intersection should be based on an engineering study. The engineering study for all-way stop control should include an analysis of factors related to the existing operation and safety at the intersection, the potential to improve these conditions, and the applicable factors contained in the following all-way stop control warrants:*

- A. *All-Way Stop Control Warrant A: Crash Experience (see Section 2B.13)*
- B. *All-Way Stop Control Warrant B: Sight Distance (see Section 2B.14)*
- C. *All-Way Stop Control Warrant C: Transition to Signal Control or Transition to Yield Control at a Circular Intersection (see Section 2B.15)*
- D. *All-Way Stop Control Warrant D: 8-Hour Volume (Vehicles, Pedestrians, Bicycles) (see Section 2B.16)*
- E. *All-Way Stop Control Warrant E: Other Factors (see Section 2B.17)*

SOUTHBOUND I-25/COUNTY LINE ROAD INTERSECTION

The following presents evaluation of this intersection with respect to each AWSC warrant listed in the *MUTCD* section 2B.12

A. Crash Experience

For a four-leg intersection, there are five or more reported crashes in a 12-month period or six or more reported crashes in a 36-month period that were of a type susceptible to correction by the installation of all-way stop control

In the past 3 years, there has been one crash at the southbound-ramp intersection.

B. Sight Distance

The interchange has recently been improved and LSC presumes that sight distance meets CDOT standards.

C. Transition to Signal Control or Transition to Yield Control at a Circular Intersection

The implementation of AWSC in the future, once needed, to reduce delay and improve LOS for the southbound approach could be considered a “transitional” traffic control measure. The potential future need to signalize one or both of the ramp intersections in the future exists, but the timing would depend on both overall growth in traffic demand on County Line Road and the future land use (and associated trip generation) of the vacant parcels southwest of I-25 and County Line Road. If in the future signal warrants are met, a pair of roundabouts rather than traffic signals at the ramp terminals may be implemented.

D. Eight-Hour Volumes

Section 2B.16 All-Way Stop Control Warrant D: 8-Hour Volume (Vehicles, Pedestrians, Bicycles)

Option:

- 01 All-way stop control may be installed at an intersection where an engineering study indicates:
 - A. The combined motor vehicle, bicycle, and pedestrian volume entering the intersection from the major-street approaches is at least 300 units per hour for each of any 8 hours of a typical day; and
 - B. The combined motor vehicle, bicycle, and pedestrian volume entering the intersection from the minor-street approaches is at least 200 units per hour for each of any of the same 8 hours.
- 02 If the 85th-percentile approach speed of the major-street traffic exceeds 40 mph, the minimum vehicular volume warrants may be reduced to 70 percent of the values given in Items A and B in Paragraph 1 of this Section.

I-25 Northbound Ramp Intersection

Four hours of projected volumes were analyzed for this intersection. The volumes reflect motor-vehicle demand as pedestrian/bicycle demand is low. Three of the four hours analyzed would meet the *MUTCD*’s minimum-volume combination on major and minor streets to meet an AWSC warrant at the I-25 northbound ramp intersection (potentially, other hours of the day could meet both of these thresholds, but six additional hours would need to meet both minor and major street thresholds):

I-25 Southbound Ramp Intersection

Four hours of projected volumes were analyzed for this intersection. Two of the four hours analyzed would meet the *MUTCD*’s minimum volume combination on major and minor streets to meet AWSC Warrant Item D at the I-25 southbound ramp intersection (potentially other hours of the day could meet both of these thresholds, but six additional hours would need to meet both minor and major street thresholds to satisfy the Item D part of the warrant evaluation). Item D of the *MUTCD* AWSC warrant analysis at the I-25 southbound ramp intersection with County Line Road could be revisited at the future platting/access permitting stage of the development process for this development, which could include full evaluation of the off-peak hours as well (8-10 hours of the day).

| Analysis Period | | | Minor Street | | | Major Street | | | Overall |
|-----------------|-------|--|-------------------|---------------|-----------------|-------------------|---------------|-----------------|-----------------|
| Peak Period | Start | End | 2044 Total Volume | MUTCD Minimum | Meets Threshold | 2044 Total Volume | MUTCD Minimum | Meets Threshold | Meets Threshold |
| AM Hour 1 | 6:30 | 7:30 | 80 | 200 | X | 604 | 300 | ✓ | No |
| AM Hour 2 | 7:30 | 8:30 | 121 | 200 | X | 727 | 300 | ✓ | No |
| AM Overall | 7:10 | 8:10 | 125 | 200 | X | 821 | 300 | ✓ | No |
| PM Hour 1 | 16:00 | 17:00 | 347 | 200 | ✓ | 673 | 300 | ✓ | Yes |
| PM Hour 2 | 17:00 | 18:00 | 379 | 200 | ✓ | 598 | 300 | ✓ | Yes |
| PM Overall | 16:35 | 17:35 | 358 | 200 | ✓ | 689 | 300 | ✓ | Yes |
| 09/26/2024 | | # of hours of the 4 analyzed which meet the Major and minor street thresholds: | | | | | | | 2 hours |

E. Other Factors

| | |
|----|---|
| 01 | <p>All-way stop control may be installed at an intersection where an engineering study indicates that all-way stop control is needed due to other factors not addressed in the other all-way stop control warrants. Such other factors may include, but are not limited to, the following:</p> <ul style="list-style-type: none"> A. The need to control left-turn conflicts, B. An intersection of two residential neighborhood collector (through) streets of similar design and operating characteristics where all-way stop control would improve traffic operational characteristics of the intersection, or C. Where pedestrian and/or bicyclist movements support the installation of all-way stop control. |
|----|---|

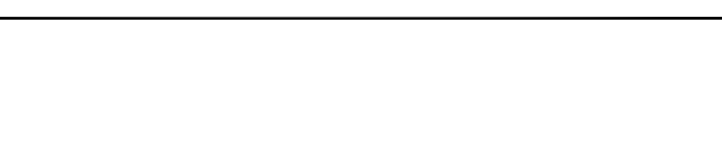
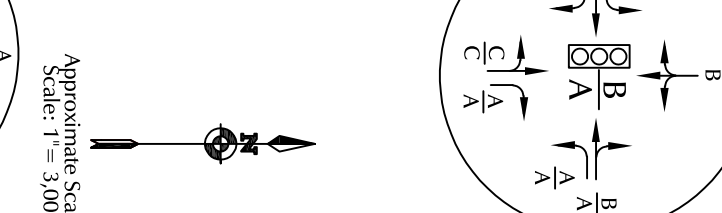
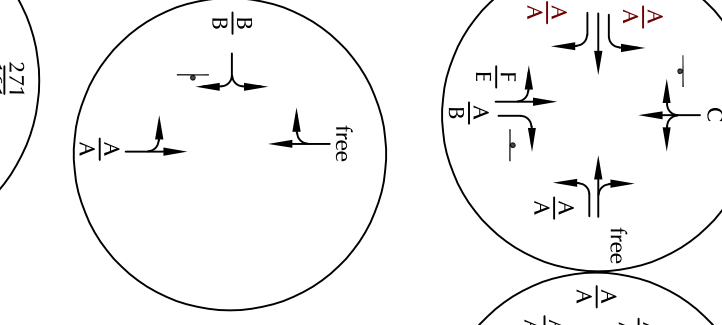
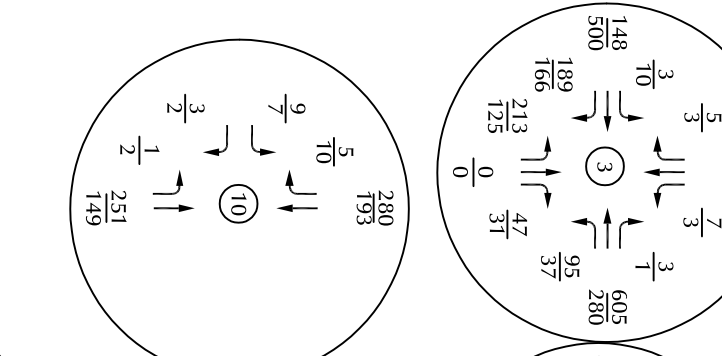
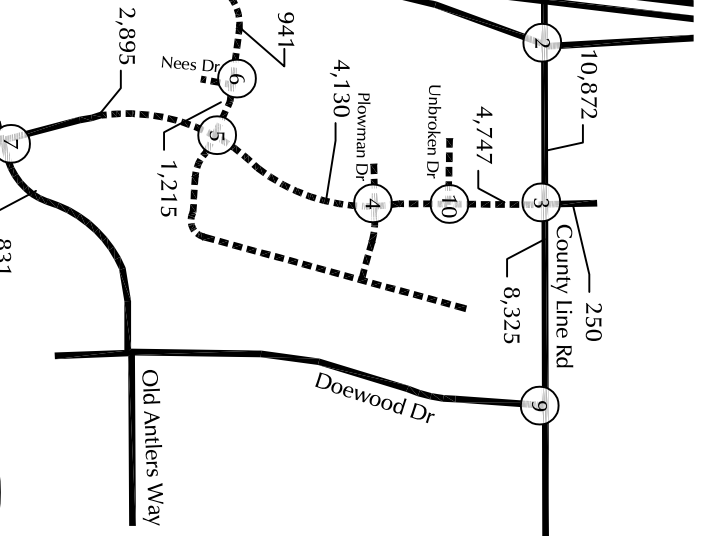
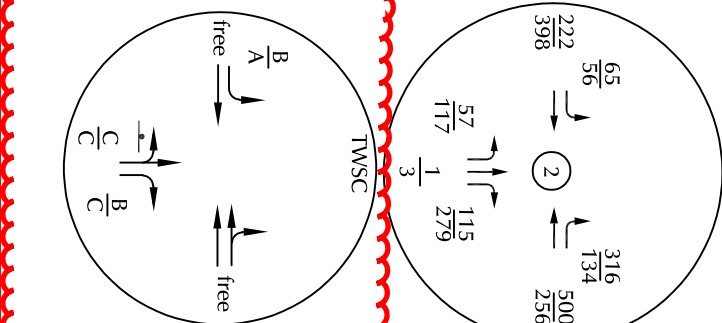
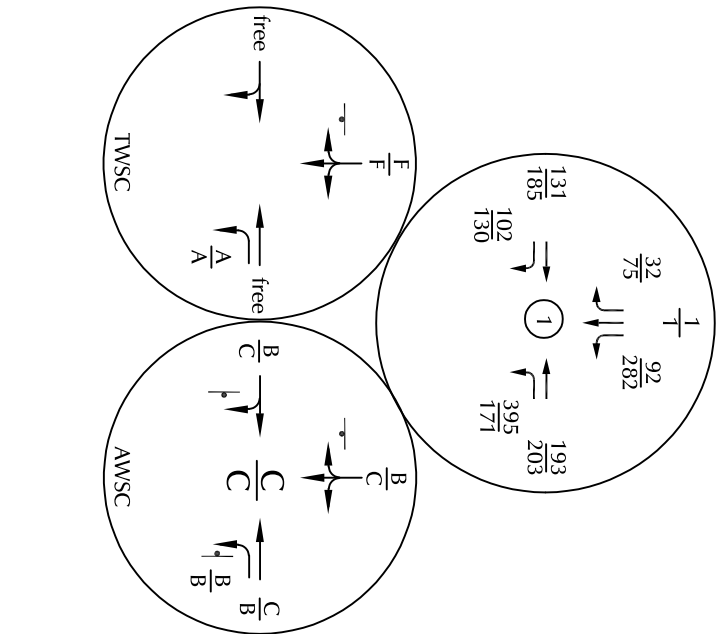
Part “A” may apply. There is a relatively heavy WBL volume at the southbound-ramp intersection during the morning peak hour. Additionally, there is a relatively heavy SBL volume during the afternoon peak hour.

Part “B” does not apply since neither I-25 ramp is in a residential neighborhood.

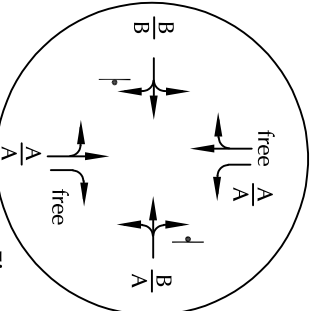
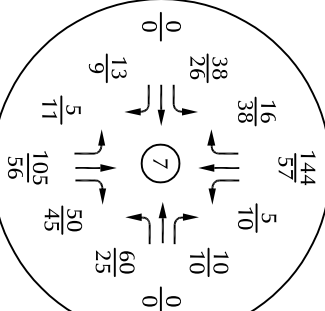
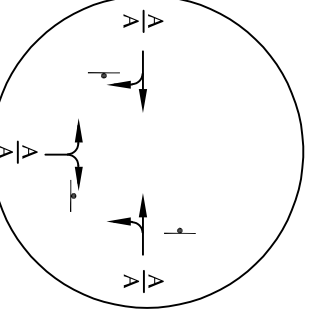
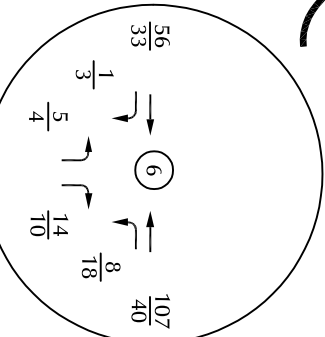
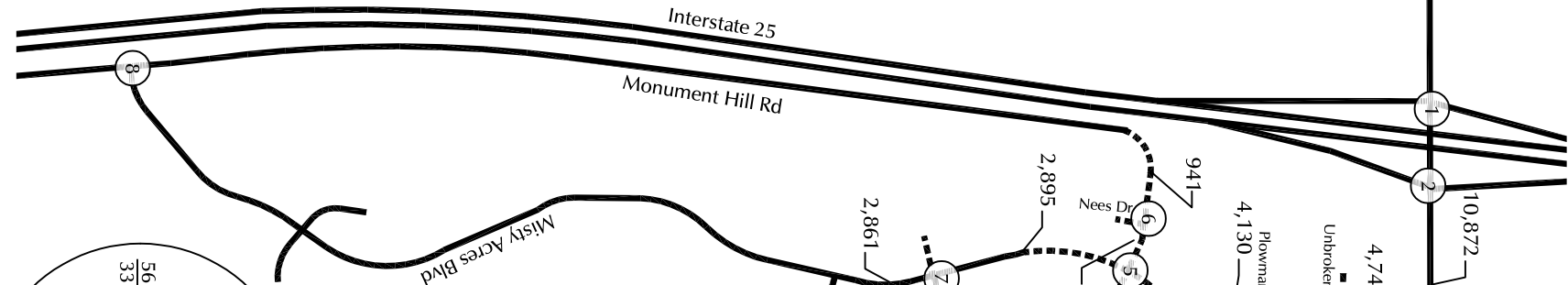
Part “C” may become more applicable in the future with growth in the area and any increase in non-motorized travel demand that may accompany such growth.

Additionally, with respect to future use of AWSC, as shown in the TIS, as mitigation at the southbound ramp intersection for the projected LOS below D:

- The projected 2044 total volumes in the TIS show relatively balanced volumes on all approaches for the PM peak hour.
- In the morning peak hour, the predominant volume movement is the westbound left turn and not either of the straight through movements on County Line Road.
- This intersection can be considered an “endpoint” or “breakpoint” intersection of the series of intersections along County Line Road to the east, which have heavier through volumes than County Line Road west of I-25. This is obviously subject to change if traffic demand changes west of the I-25 interchange in the future.



Revised per the CDOT comment letter and September 24th meeting.



X,XXX = Average Daily Traffic (vehicles per day)
XX/XX = AM Weekday Peak-Hour Traffic (vehicles per hour)
XX/XX = PM Weekday Peak-Hour Traffic (vehicles per hour)
X/X = AM Individual Movement Peak-Hour LOS
X/X = PM Individual Movement Peak-Hour LOS
X/X = AM Entire Intersection Peak-Hour LOS
X/X = PM Entire Intersection Peak-Hour LOS

⬡ = Traffic Signal | = Stop Sign

Roadways (as shown on Figure 3)

Existing Roadway segments (to remain)
Proposed New Roadway Segments

Approximate Scale
Scale: 1"= 3,000'







2044 Background + Site-Generated Traffic

Figure 10

HCM 6th TWSC
2: I-25 NB Ramps & County Line Rd

2044 Background + Site
AM

w/separate NB RT

| Intersection | | | | | | | | | | | | |
|--------------------------|---|---|------|------|---|---|------|---|---|------|------|------|
| Int Delay, s/veh | 2.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | | |  |  | |  |  | | | |
| Traffic Vol, veh/h | 65 | 222 | 0 | 0 | 500 | 316 | 57 | 1 | 115 | 0 | 0 | 0 |
| Future Vol, veh/h | 65 | 222 | 0 | 0 | 500 | 316 | 57 | 1 | 115 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | 300 | - | - | 0 | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 87 | 87 | 87 | 93 | 93 | 93 | 87 | 87 | 87 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 75 | 255 | 0 | 0 | 538 | 340 | 66 | 1 | 132 | 0 | 0 | 0 |

| Major/Minor | Major1 | | Major2 | | Minor1 | | |
|----------------------|--------|---|--------|---|--------|---|-------------------|
| Conflicting Flow All | 878 | 0 | - | - | - | 0 | 674 1283 255 |
| Stage 1 | - | - | - | - | - | - | 405 405 - |
| Stage 2 | - | - | - | - | - | - | 269 878 - |
| Critical Hdwy | 4.13 | - | - | - | - | - | 6.63 6.53 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.43 5.53 - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.83 5.53 - |
| Follow-up Hdwy | 2.219 | - | - | - | - | - | 3.519 4.019 3.319 |
| Pot Cap-1 Maneuver | 767 | - | 0 | 0 | - | - | 404 164 783 |
| Stage 1 | - | - | 0 | 0 | - | - | 673 598 - |
| Stage 2 | - | - | 0 | 0 | - | - | 753 365 - |
| Platoon blocked, % | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 767 | - | - | - | - | - | 364 0 783 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 364 0 - |
| Stage 1 | - | - | - | - | - | - | 607 0 - |
| Stage 2 | - | - | - | - | - | - | 753 0 - |







| Approach | EB | WB | NB |
|----------------------|-----|----|----|
| HCM Control Delay, s | 2.3 | 0 | 13 |
| HCM LOS | | | B |

| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | WBT | WBR |
|-----------------------|-------|-------|-------|-----|-----|-----|
| Capacity (veh/h) | 464 | 783 | 767 | - | - | - |
| HCM Lane V/C Ratio | 0.239 | 0.113 | 0.097 | - | - | - |
| HCM Control Delay (s) | 15.2 | 10.2 | 10.2 | - | - | - |
| HCM Lane LOS | C | B | B | - | - | - |
| HCM 95th %tile Q(veh) | 0.9 | 0.4 | 0.3 | - | - | - |

HCM 6th TWSC
2: I-25 NB Ramps & County Line Rd

2044 Background + Site
PM

w/separate NB RT





| Intersection | | | | | | | | | | | | |
|--------------------------|---|---|------|------|---|---|------|---|---|------|------|------|
| Int Delay, s/veh | 5.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | | |  |  | |  |  | | | |
| Traffic Vol, veh/h | 56 | 398 | 0 | 0 | 256 | 134 | 117 | 3 | 279 | 0 | 0 | 0 |
| Future Vol, veh/h | 56 | 398 | 0 | 0 | 256 | 134 | 117 | 3 | 279 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | 300 | - | - | 0 | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 61 | 433 | 0 | 0 | 278 | 146 | 127 | 3 | 303 | 0 | 0 | 0 |

| Major/Minor | Major1 | | Major2 | | Minor1 | | |
|----------------------|--------|---|--------|---|--------|---|-------------------|
| Conflicting Flow All | 424 | 0 | - | - | - | 0 | 694 979 433 |
| Stage 1 | - | - | - | - | - | - | 555 555 - |
| Stage 2 | - | - | - | - | - | - | 139 424 - |
| Critical Hdwy | 4.13 | - | - | - | - | - | 6.63 6.53 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.43 5.53 - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.83 5.53 - |
| Follow-up Hdwy | 2.219 | - | - | - | - | - | 3.519 4.019 3.319 |
| Pot Cap-1 Maneuver | 1133 | - | 0 | 0 | - | - | 392 249 622 |
| Stage 1 | - | - | 0 | 0 | - | - | 574 512 - |
| Stage 2 | - | - | 0 | 0 | - | - | 874 586 - |
| Platoon blocked, % | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1133 | - | - | - | - | - | 371 0 622 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 371 0 - |
| Stage 1 | - | - | - | - | - | - | 543 0 - |
| Stage 2 | - | - | - | - | - | - | 874 0 - |

| Approach | EB | WB | NB |
|----------------------|----|----|------|
| HCM Control Delay, s | 1 | 0 | 17.3 |
| HCM LOS | | | C |

| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | WBT | WBR |
|-----------------------|-------|-------|-------|-----|-----|-----|
| Capacity (veh/h) | 371 | 622 | 1133 | - | - | - |
| HCM Lane V/C Ratio | 0.352 | 0.488 | 0.054 | - | - | - |
| HCM Control Delay (s) | 19.9 | 16.2 | 8.4 | - | - | - |
| HCM Lane LOS | C | C | A | - | - | - |
| HCM 95th %tile Q(veh) | 1.5 | 2.7 | 0.2 | - | - | - |

| Intersection | |
|---------------------------|------|
| Intersection Delay, s/veh | 16.5 |
| Intersection LOS | C |

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------|------|---|------|---|---|------|------|------|------|------|---|------|
| Lane Configurations | |  | |  |  | | | | | |  | |
| Traffic Vol, veh/h | 0 | 131 | 102 | 395 | 193 | 0 | 0 | 0 | 0 | 92 | 1 | 32 |
| Future Vol, veh/h | 0 | 131 | 102 | 395 | 193 | 0 | 0 | 0 | 0 | 92 | 1 | 32 |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.83 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.83 | 0.83 | 0.83 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 151 | 117 | 476 | 208 | 0 | 0 | 0 | 0 | 111 | 1 | 39 |
| Number of Lanes | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |

| Approach | EB | WB | SB |
|----------------------------|------|------|----|
| Opposing Approach | WB | EB | |
| Opposing Lanes | 2 | 1 | 0 |
| Conflicting Approach Left | SB | | WB |
| Conflicting Lanes Left | 1 | 0 | 2 |
| Conflicting Approach Right | | SB | EB |
| Conflicting Lanes Right | 0 | 1 | 1 |
| HCM Control Delay | 10.9 | 19.9 | 11 |
| HCM LOS | B | C | B |

| Lane | EBLn1 | WBLn1 | WBLn2 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 0% | 100% | 0% | 74% |
| Vol Thru, % | 56% | 0% | 100% | 1% |
| Vol Right, % | 44% | 0% | 0% | 26% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 233 | 395 | 193 | 125 |
| LT Vol | 0 | 395 | 0 | 92 |
| Through Vol | 131 | 0 | 193 | 1 |
| RT Vol | 102 | 0 | 0 | 32 |
| Lane Flow Rate | 268 | 476 | 208 | 151 |
| Geometry Grp | 4a | 5 | 5 | 2 |
| Degree of Util (X) | 0.368 | 0.755 | 0.3 | 0.249 |
| Departure Headway (Hd) | 4.948 | 5.715 | 5.211 | 5.948 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 718 | 628 | 683 | 598 |
| Service Time | 3.035 | 3.497 | 2.993 | 4.043 |
| HCM Lane V/C Ratio | 0.373 | 0.758 | 0.305 | 0.253 |
| HCM Control Delay | 10.9 | 24.1 | 10.2 | 11 |
| HCM Lane LOS | B | C | B | B |
| HCM 95th-tile Q | 1.7 | 6.8 | 1.3 | 1 |

| Intersection | |
|---------------------------|------|
| Intersection Delay, s/veh | 19.7 |
| Intersection LOS | C |

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | ↕ | ↑ | | | | | | ↕ | |
| Traffic Vol, veh/h | 185 | 130 | 95 | 171 | 203 | 0 | 0 | 0 | 0 | 282 | 1 | 75 |
| Future Vol, veh/h | 185 | 130 | 95 | 171 | 203 | 0 | 0 | 0 | 0 | 282 | 1 | 75 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 201 | 141 | 103 | 186 | 221 | 0 | 0 | 0 | 0 | 307 | 1 | 82 |
| Number of Lanes | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |

| Approach | EB | WB | SB |
|----------------------------|------|------|------|
| Opposing Approach | WB | EB | |
| Opposing Lanes | 2 | 1 | 0 |
| Conflicting Approach Left | SB | | WB |
| Conflicting Lanes Left | 1 | 0 | 2 |
| Conflicting Approach Right | | SB | EB |
| Conflicting Lanes Right | 0 | 1 | 1 |
| HCM Control Delay | 23.8 | 13.8 | 21.2 |
| HCM LOS | C | B | C |

| Lane | EBLn1 | WBLn1 | WBLn2 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 45% | 100% | 0% | 79% |
| Vol Thru, % | 32% | 0% | 100% | 0% |
| Vol Right, % | 23% | 0% | 0% | 21% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 410 | 171 | 203 | 358 |
| LT Vol | 185 | 171 | 0 | 282 |
| Through Vol | 130 | 0 | 203 | 1 |
| RT Vol | 95 | 0 | 0 | 75 |
| Lane Flow Rate | 446 | 186 | 221 | 389 |
| Geometry Grp | 4a | 5 | 5 | 2 |
| Degree of Util (X) | 0.735 | 0.364 | 0.4 | 0.672 |
| Departure Headway (Hd) | 5.938 | 7.044 | 6.533 | 6.216 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 606 | 507 | 547 | 580 |
| Service Time | 4.014 | 4.834 | 4.323 | 4.29 |
| HCM Lane V/C Ratio | 0.736 | 0.367 | 0.404 | 0.671 |
| HCM Control Delay | 23.8 | 13.9 | 13.7 | 21.2 |
| HCM Lane LOS | C | B | B | C |
| HCM 95th-tile Q | 6.3 | 1.6 | 1.9 | 5.1 |