FINAL DRAINAGE REPORT
FOR
STERLING RANCH RECYCLING FACILITY

Prepared For:

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PPR2341 & SF2325

Prepared By:

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Colorado Springs, CO 80919
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ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage letter has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

_____

Mike Bramlett, Colorado P.E. 32314
For and On Behalf of JR Engineering, LLC

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: SR Land, LLC

By: _____

Title: _____

Address: 20 Boulder Crescent, Suite 200
Colorado Springs, CO 80903

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

_____

County Engineer/ ECM Administrator

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APPENDICES

PURPOSE

This document is the Final Drainage Report for Sterling Ranch Recycling Facility. The purpose of this report is to identify on-site and off-site drainage patterns, areas tributary to the site, and compare existing and proposed drainage conditions.

GENERAL SITE DESCRIPTION

GENERAL LOCATION

Sterling Ranch Recycling Facility (hereby referred to as the "site") is a proposed development within the Sterling Ranch master planned community with a total area of approximately 32 acres. The site is presently used as a concrete and asphalt recycling facility.

The site is located in the north half of Section 5, Township 13 South, Range 65 West of the Sixth Principal Meridian in El Paso County, State of Colorado. The site is bounded by Marksheffel Road to the east, Pioneer Sand CO land to the west and south, and unplatted land to the north. Refer to the vicinity map in Appendix A for additional information.

DESCRIPTION OF PROPERTY

In the existing condition analysis, the property was analyzed at the time of the parcel sale in 2021. Before the sale of the site in 2021, the parcel had been used as a crushing facility for a nearby mining operation. The crushing business halted operations and vegetation was established on portions of the site prior to the sale. There was an asphalt access road and compacted gravel roads on the site at the time of sale. The site generally slope(s) to the south at 1 to 6% towards an existing 8' berm on the southern edge of the property. In the proposed interim condition, the property will be used as an asphalt and concrete recycling facility with asphalt drives, a staging area and some existing grasslands. In the ultimate condition, the site and surrounding properties are assumed to be developed per their land use which includes heavy industrial, multi-family residential, and commercial.

Soils located on the project site are Blakeland Loamy Sand (8) and Columbine Gravelly Sandy Loam (19). These soils are classified as Hydrologic Soil Group A. Group A soils exhibit high infiltration rates when thoroughly wet, and consist mainly of deep, well drained to excessively drained sands or gravelly sands. Refer to the soil survey map in Appendix A for additional information.

There are no known irrigation facilities located on the project site.

FLOODPLAIN STATEMENT

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, the entire site lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher

than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. Refer to the FIRM Map in Appendix A for additional information.

EXISTING DRAINAGE CONDITIONS

MAJOR BASIN DESCRIPTIONS

The site lies within the upper Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into 7 major sub-basins. The site is within the respective upper basin Sand Creek sub-basin as shown in Appendix D. Sand Creek ultimately enters Fountain Creek about two miles upstream of the Academy Boulevard bridge over Fountain Creek.

The site generally drains from north to southwest. Sand Creek is located to the east of the site and runs from north to south. This reach of drainage conveyance does not currently have any improvements. As of the date of this report, Kiowa is performing studies and plans to address Sand Creek stabilization adjacent to the site.

EXISTING SUB-BASIN DRAINAGE

The existing condition analyzes the parcel at the latest time of sale in 2021. The existing condition of the site was broken into seven sub-basins including six on-site basins and one off-site basin. The basin delineation is shown in the existing drainage map in Appendix E and is described as follows:

Basin EXA (Q_5=1.1 cfs, Q_{100}=5.4 cfs) is 2.68 acres with an 8 percent impervious and is located on the northwestern portion of the site. This basin is comprised of part of an existing paved access road, existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest onto the adjacent property to the west at design point (DP) 1. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin EXB (Q_5=0.6 cfs, Q_{100}=4.3cfs) is 2.60 acres with a 2 percent impervious and is located on the western portion of the site. This basin is comprised of existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest onto the adjacent property to the west at DP2. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin EXC (Q_5=1.0 cfs, Q_{100}=4.3 cfs) is 2.11 acres with a 14 percent impervious and is located on the southwest portion of the site. This basin is comprised of several existing gravel roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows southwest to DP3 located along the existing 8' berm. Runoff from DP3 infiltrates the ground along the berm's toe of slope.

Basin EXD (Q_5=7.6 cfs, Q_{100}=28.1 cfs) is 13.44 acres with a 17 percent impervious and is located on the western central portion of the site. This basin is comprised of part of an existing paved access road, several existing gravel roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows south to DP4 located along the existing 8' berm. Runoff from DP4 flows south across the existing berm via an existing 12" PVC pipe. Runoff follows historical drainage patterns off-site and outfalls to Sand Creek.

Basin OS1 (Q_5=1.5 cfs, Q_{100}=9.8 cfs) is 9.42 acres with a 2 percent impervious and is located to the north of the site. This basin is comprised of off-site undeveloped area tributary to the site. Runoff from this basin sheet flows south and then east along the existing off-site berm to DP5. Runoff from DP5 flows south entering into Basin EXE. Runoff follows historical drainage patterns within Basin EXE and combines at DP6.1.

Basin EXE (Q_5=2.0 cfs, Q_{100}=13.4 cfs) is 8.51 acres with a 2 percent impervious and is located on the eastern central portion of the site. This basin is comprised of part of several existing dirt access roads, existing vegetation and undeveloped area. Runoff from this basin sheet flows south and then east to DP6 located along the existing 8' berm. Runoff from DP5 and DP6 combine at DP6.1 (Q_5=2.8 cfs, Q_{100}=18.7 cfs). Runoff from DP6.1 continues to flow southeast through the neighboring property to the south. Flow becomes concentrated off-site in a natural stream section that ultimately follows the historical drainage patterns into Sand Creek.

Basin EXF (Q_5=0.8 cfs, Q_{100}=5.2 cfs) is 3.09 acres with a 2 percent impervious and is located on the eastern portion of the site. This basin is comprised of part of an existing dirt access road and undeveloped area. Runoff from this basin sheet flows southeast to DP7 located along the eastern side of the site. Runoff from DP7 continues to flow south through the neighboring sanitary lift station property to the east. Flow becomes concentrated off-site in a natural stream section that ultimately follows the historical drainage patterns into Sand Creek.

PROPOSED DRAINAGE CONDITIONS

PROPOSED CONVEYANCE

In general, developed flows are collected in proposed swales, which convey water to the proposed water quality and detention area. Proposed swale sections were designed to ensure they are stable and have required capacity to satisfy criteria. A swale is considered stable with a velocity of 5 ft/s of less. To ensure capacity, swales will have a minimum of 1 ft. of freeboard over the water surface for flows anticipated in a 100-year storm event. In addition to the swales, a proposed culvert also conveys flows under the access roadway. The culvert was sized to not overtop the roadways with flows from a 100-year storm event. Detailed swale calculations, sections, and culvert calculations are located in Appendix C.

In each basin's paragraph below, state how WQ treatment is or is not provided for each and any applicable WQ exclusions.

PROPOSED SUB-BASIN DRAINAGE

The proposed condition analyzes the parcel for the interim use of a recycling facility. The Rational Method produced flows that were used to design the proposed interim swales, culverts, storm sewer, and pond forebays. The proposed site was broken into eight basins including six on-site basins and two off-site basins. The proposed basin delineation is shown on the drainage basin map within Appendix E and is described as follows:

Basin A (Q_5=0.2 cfs, Q_{100}=1.0 cfs) is 0.30 acres with a 2 percent impervious and is located on the western property line of the site. This basin is comprised of proposed undeveloped area. Runoff from this basin sheet flows southwest to DP1 and then off-site to the adjacent property to the west. Runoff then follows historical drainage patterns off-site and outfalls to Sand Creek. In the existing condition, Basins EXA and EXB both flow off-site in this same direction for a total flow of Q_5=1.7 cfs, Q_{100}=9.7 cfs, which is more than is proposed.

What is drainage pattern? Swales, c&g, culverts, storm system, etc?

Basin B (Q_5=7.8 cfs, Q_{100}=26.0 cfs) is 14.43 acres with a 20 percent impervious and is located on the western central portion of the site. This basin is comprised of part of a paved roadway, raw concrete stockpile, raw concrete with rebar stockpile, asphalt stockpile, weighing station, mobile crusher, fence, part of temporary gravel road, swales and undeveloped land. Runoff from this basin sheet flows overland south to a proposed swale that directs flows east to DP2. Runoff from DP2 is combined at the proposed 30” FES at DP4.2.

Basin OS1 (Q_5=1.5 cfs, Q_{100}=9.8 cfs) is 9.42 acres with a 2 percent impervious and is located to the north of the site. This basin is comprised of off-site undeveloped area tributary to the site. Runoff from this basin sheet flows south and then east along the existing off-site berm to DP3. Runoff from DP3 flows south entering into Basin C. Runoff follows the drainage patterns within Basin C and combines at the proposed 24” RCP culvert at DP4.1.

Basin C (Q_5=3.5 cfs, Q_{100}=17.7 cfs) is 10.64 acres with a 7 percent impervious and is located on the eastern central portion of the site. This basin is comprised of a part of a paved roadway, swales and undeveloped land. Runoff from this basin sheet flows overland south to proposed swales that directs flows east to DP4. Runoff from DP4 is combined with flows from DP3 at the proposed 24” RCP culvert at DP4.1 (Q_5=3.9 cfs, Q_{100}=21.9 cfs). Runoff from DP4.1 enters the proposed culvert into Basin B and a proposed swale directs flows to the proposed 30” FES at DP4.2 (Q_5=9.7 cfs, Q_{100}=41.5 cfs). DP4.2 flows are piped to the west forebay within the pond and combine at DP8.1.

Basin D (Q_5=1.4 cfs, Q_{100}=5.6 cfs) is 2.69 acres with a 12 percent impervious and is located on the eastern boundary of the site. This basin is comprised of a part of a paved roadway, paved access, swale and undeveloped land. Runoff from this basin sheet flows overland southeast to a proposed swale that directs flows south to DP5. Runoff from DP5 is combined at the proposed Type C sump inlet at DP7.1 within Basin E.

Basin E (Q_5=1.3 cfs, Q_{100}=5.3 cfs) is 2.49 acres with a 13 percent impervious and is located on the eastern portion of the site. This basin is comprised of a part of a paved roadway, part of a temporary gravel road, swale and undeveloped land. Runoff from this basin sheet flows overland southeast to a proposed swale that directs flows east to DP6. Runoff from DP6 is combined at the proposed Type C sump inlet at DP7.1.

Basin OS2 (Q_5=0.1 cfs, Q_{100}=0.7 cfs) is 0.36 acres with a 2 percent impervious and is located to the east of the site. This basin is comprised of off-site undeveloped area tributary to the proposed pond. Runoff from this basin sheet flows west and then south along the property boundary to DP7. Runoff from DP7 is combined with DP5 and DP6 flows at the proposed Type C sump inlet at DP7.1 (Q_5=2.6 cfs, Q_{100}=10.8 cfs). DP7.1 flows are piped to the north forebay within the pond and combine at DP8.1.

Basin F (Q_5=0.6 cfs, Q_{100}=4.4 cfs) is 2.26 acres with a 2 percent impervious and is located on the southeast portion of the site. This basin is comprised of a proposed full-spectrum extended detention basin (EDB) within Tract A and the proposed off-site detention pond easement. Runoff from this basin sheet flows overland to a proposed trickle channel that directs flows east to DP8. Runoff from DP8 is combined with flows from DP4.2 and DP7.1 at the proposed full-spectrum EDB outlet structure at DP8.1 (Q_5=11.7 cfs, Q_{100}=50.5 cfs). DP8.1 represents the total proposed flows that will enter the proposed full-spectrum EDB in the interim condition. Flows will be released through the outlet structure at DP8.2 (Q_5=0.1 cfs, Q_{100}=8.0 cfs) and connect into the existing storm infrastructure sending the flows east where they will eventually follow the historical drainage patterns into Sand Creek.

ULTIMATE SUB-BASIN DRAINAGE

The ultimate condition analyzes the parcel and tributary properties for the future development based on the land use in order to design the ultimate full-spectrum EDB and spillway overflow path. The ultimate site was broken into five land uses. The land uses are shown on the proposed drainage map within Appendix E and is described as follows.

Note that the Final Plat Drawing has Lot #2 as 24.05ac

- Lot 1 is 24.06 acres and is zoned as Residential-1/8 Acre or Less (65% impervious)
- Urban Non-Residential Collector Roadway (80’ R.O.W.) is 1.78 acres (100% impervious for roadway, curb & gutter, and sidewalk width, 2% impervious for other areas)
- Lot 2 is 4.74 acres and is zoned as Heavy Industrial Area (90% impervious)
- Tract A is 1.85 acres and is used as detention pond area (2% impervious)
- Off-site vacant land to the north is 9.42 acres and is zoned as Commercial Area (95% impervious)
- Off-site Tract/ Lift Station land to the east is 1.87 acres and is zoned as Heavy Industrial Area (90% impervious)
- Off-site land to the east is 0.44 acres and is used as detention pond area (2% impervious)

- Total Area = 44.16 acres with 72.4% impervious

The ultimate condition was used overall to size the full-spectrum EDB and ensure it will operate for future developments.

DRAINAGE DESIGN CRITERIA

DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.

HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. On-site drainage improvements were designed based on the 5-year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One-hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

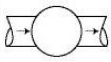
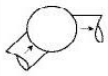
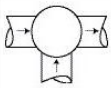
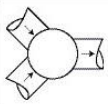
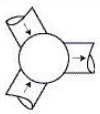
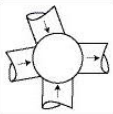
Table 1: 1-hr Point Rainfall Data

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Autodesk Hydraflow Express was used to size the overflow channel and drainage swales per criteria. The MHFD-Detention_v4.06 spreadsheet was utilized for evaluating proposed detention and water quality for Pond A. Bentley StormCAD v8i was used to analyze the hydraulic grade lines and energy grade lines for the storm sewer network. Manhole and pipe losses for the model were obtained from the standard head-loss coefficients (Table 2) as recommended by Bentley. Calculations can be found in Appendix C.

Table 2: StormCAD Head-loss Coefficients

Type of Manhole	Diagram	Headloss Coefficient
Trunkline only with no bend at the junction		0.5
Trunkline only with 45° bend at the junction		0.6
Trunkline only with 90° bend at the junction		0.8
Trunkline with one lateral		Small 0.6 Large 0.7
Two roughly equivalent entrance lines with angle < 90° between lines		0.8
Two roughly equivalent entrance lines with angle > 90° between lines		0.9
Three or more entrance lines		1.0

DRAINAGE FACILITY DESIGN

GENERAL CONCEPT

The project site is anticipated to be developed in phases, beginning with the development of the Sterling Ranch Recycling Facility portion of Lot 1. This is known as the "interim condition". In the future, it is anticipated that Lot 1 will develop as multi-family, Lot 2 will develop as a heavy industrial area, proposed Sterling Ranch Road R.O.W. will develop as an urban non-residential collector roadway, unplatted land to the north of the site will develop as a commercial area, tract land to the east of the site will develop as heavy industrial, and Tract A will develop as the full-spectrum EDB. The timing and specific site details are largely unknown at this time. The fully developed site and tributary properties is referred to as the "ultimate condition".

Discuss the small section of 2-ft trickle channel too. Is that just likely for the interim condition?

All on-site swales, culverts, and conveyances were designed for the interim phase. The proposed full-spectrum EDB was designed for the interim condition, although, to limit the amount of required modifications and re-work upon ultimate developed conditions, the outlet pipe, emergency spillway, pond volume, 6-ft trickle channel, and emergency overflow inlet structure, were all sized per the anticipated ultimate conditions. The forebays and orifice plate were all designed per the interim condition, to ensure the pond will function as required until the site further develops. Upon development of the remaining undeveloped lots, lot specific drainage report(s) must be submitted to ensure the proposed full-spectrum EDB and drainage system designs herein are adequate to accommodate the developed flows. The reports shall identify any proposed modification, if needed,

to ensure proposer functionality of the drainage system(s) and compliance with the current EPC criteria. Treated water will outfall to the existing storm infrastructure to the east of the site and will eventually outfall into Sand Creek. A proposed drainage map is provided in Appendix E.

FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: In the interim site development, the site will remain largely undeveloped. Runoff is routed by sheet flow and grass-lined swales to promote infiltration and reduce runoff. The ultimate site development partly consists of multi-family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

Step 2 – Stabilize Drainageways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the future channel stabilization being designed by Kiowa adjacent to the site and on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Sand Creek, therefore no downstream stabilization will be accomplished with this project.

Step 3 – Treat the WQCV: Water Quality treatment for this site is provided in a proposed full-spectrum extended detention basin (Pond A). The runoff from this site will be collected within swales to inlets and conveyed to the proposed pond via storm sewer. Upon entrance to the ponds, flows will be captured in forebays designed to promote settlement of suspended solids. A concrete trickle channel is also incorporated into the pond to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. Major flows released from the ponds will be reduced to less than historic rates.

Step 4 –BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated concrete truck washout basin, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMPs include asphalt drives, storm inlets, storm pipe, the full-spectrum EDB Pond A and permanent vegetation. Maintenance responsibilities and plans will be defined at the time of final platting.

Cutoff Walls: Provide a discussion with supporting data/calcs on whether cutoff walls are or are not necessary for onsite emergency spillways and/or drop structures.

WATER QUALITY

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full-spectrum water quality and detention are provided for all developed basins. The ultimate condition was used to size the full-spectrum EDB to ensure the required volume, outlet structure and orifice plate design to ensure drain times, trickle channels to ensure capacity for double the 2% peak inflow, and emergency spillway and overflow structure design to ensure freeboard and capacity. The emergency overflow structure (triple Type C sump inlets), was sized to have the capacity for the ultimate peak undetained 100-year flow for Pond A and connects to the existing storm infrastructure that crosses Marksheffel Rd. The interim condition will utilize the same pond grading design and outlet structure, but will have different inlet structures and orifice plate design to ensure the interim design meets criteria. The interim condition forebays (West and North) were sized per the tributary areas for each to ensure they had the required volumes and release rates. Upon development of the surrounding properties (unplatted land to the north and tract land to the east) and the ultimate site, a lot specific drainage report shall be prepared to confirm the adequacy of Pond A to accept, treat, and detain the developed flows per EPC requirements and acceptable criteria.

What about Basin A? Discuss applicable WQ exclusions.

Where possible, flows were routed through proposed swales to promote infiltration and reduce runoff. Flows for the interim site are routed through the proposed swales and the proposed storm sewer system to a proposed full-spectrum extended detention basin, Pond A. The proposed ultimate WQCV for the pond shall be released within 40 hours and the ultimate EURV shall be released within 72 hours. Proposed interim Basins B-F, OS1, and OS2 are tributary to the proposed Pond A. The table below provides the volumes required for the proposed pond, along with the release rates for the 5-year and 100-year storm. The proposed pond will utilize forebays, trickle channels, and an outlet structure to dissipate energy and treat flows. The proposed outlet structure for this pond shall reduce the release rates for the major storm events to less than historic rates to minimize adverse impacts to downstream stormwater facilities. For some minor storm events, the release rate is higher than the existing predevelopment flows. Due to the Type A soils on the site, the predevelopment calculated flows are low for the 2 through 10 year storms. Therefore, the outlet structure was designed to meet drain times for the WQCV, EURV, and 100-year events.

A broad crested weir lined with Type L buried soil riprap is provided as an emergency spillway for Pond A. The emergency spillway provided will convey flows into a proposed outfall channel that will direct flows to the proposed emergency overflow structure (Triple Type C sump inlet) to the south of the existing sanitary lift station. This will ensure that emergency flows are captured within existing infrastructure and are directed away from Aspen Meadows Subdivision Filing No. 2. The released flows from Pond A discharges into the proposed emergency overflow structure and then connects to an existing 10.33'x10.33' storm junction box. Flows upstream from the north of this junction within the existing 54" RCP storm line are Q_5=30.7 cfs, Q_{100}=233.4 cfs. The proposed released flows combine with these existing flows and then continues within an existing 66" RCP storm pipe. The existing 66" RCP has adequate capacity to convey the additional flows in both the interim and ultimate conditions per the StormCAD calculations presented in Appendix C. Pond A

Per ECM Chap 3.2.8.B, "The proposed project or developed land use shall not change historical runoff values, cause downstream damage, or adversely impact adjacent properties." Increases from the historical flowrates are allowable (with or without full spectrum detention) if it is shown (via text and/or calcs) that the flow increase can be accommodated downstream (i.e., show that there is a suitable outfall, per ECM Chap 3.2.4). If applicable, reference the downstream facilities in a DBPS or MDDP.

will be private and maintained by the property owner. Access shall be granted to the owner and El Paso County for maintenance of the private full-spectrum EDB.

	Required Volume (ac-ft)	Provided Volume (ac-ft)	WQCV (ac-ft)	EURV (ac-ft)	5-year Release (cfs)	100-year Release (cfs)
Interim	1.062	6.608	0.259	0.355	0.1	8.0
Ultimate	6.004	6.608	1.066	4.133	1.4	21.8

EROSION CONTROL PLAN

We respectfully request that the Erosion Control Plan be submitted in conjunction with the Grading and Erosion Control Plan prior to obtaining a grading permit.

OPERATION & MAINTENANCE

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. This includes swales, inlets, and storm sewer that is to be maintained by the property owner. Access is provided from on-site facilities and easements for proposed infrastructure located off-site. The maintenance road access is off future Sterling Ranch Road and wraps around the top of the pond providing access to the inflow pipes, wingwalls and outlet structure for the pond.

DRAINAGE AND BRIDGE FEES

Please correct fees

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees are presented below and will be due at time of platting (depending on date of plat submittal):

2023 DRAINAGE AND BRIDGE FEES – STERLING RANCH RECYCLING FACILITY				
Impervious Acres (ac)	Drainage Fee (Per Imp. Acre)	Bridge Fee (Per Imp. Acre)	~~Sterling Ranch~~ Drainage Fee	~~Sterling Ranch~~ Bridge Fee
~~4.3~~	$23,821	$9,743	~~$102,430~~	~~$41,895~~

Sand Creek

SUMMARY

The proposed Sterling Ranch Recycling
exceed the El Paso County Drainage C
the off-site drainage ways or surroundin
latest El Paso County Storm Drainage C

Provide calculations for impervious area for all lots with type use for each lot and impervious value assigned.
The entire parcel is being platted for two lots. The road and 24.05ac lot is missing drainage basin fees. If the plan is to develop small lot single family then calculate impervious based on this 24.05ac area at 65% as detailed on page 5 above. If not the area shall be assessed as industrial at 85% All lots and road must be included. The Tract A 1.85ac for the EDB is the only area excluded. The Letter of intent says Lot#1 will be developed as a min-warehouse. Appropriate Impervious values must be assigned between industrial and commercial uses at time of plat.

REFERENCES

1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".

2. Sand Creek Drainage Basin Planning Study, prepared Kiowa Engineering Corporation, January 1993, revised March 1996.

3. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.

COST ESTIMATE

Include a cost estimate for each PBMP with line items for all components (ex: riprap, road base, forebay, trickle channel, outlet structure, outlet pipe, spillway, etc). Input the total value into the FAE form under “Permanent Pond/BMP (provide engineer’s estimate)” in Section 1. The total should not include grading, which is a separate line item in Section 1: “Earthwork.”

Per PDF page 8 of the Soils Report, groundwater was encountered in two borings at only ~4-5ft below grade, which would mean it could surface into the pond (according to Section A-A Profile on Sht 9 of the GEC Plan, the pond depth is 9-10ft). See excerpts from MHFD's DCM volume 2 and 3 on the page below for potential concerns with groundwater in an EDB and the recommended mitigation options (like a clay or geomembrane liner).

Per CDPHE's "Low Risk Discharge Guidance - Discharges of Uncontaminated Groundwater to Land," discharging groundwater to a pond or other SW conveyance is prohibited unless properly permitted through CDPHE. Please review this guidance and the applicable permits. The guidance is linked below, the permits can be found on CDPHE's website.

Please discuss this potential shallow groundwater in the report text above.

Include a discussion on a suitable outfall. Does the storm system which the proposed pond ties into, release directly into Sand Creek? Or are there other conveyances prior to Sand Creek Channel?

- **Groundwater**: Shallow groundwater on a site presents challenges for BMPs that rely on infiltration and for BMPs that are intended to be dry between storm events. Shallow groundwater may limit the ability to infiltrate runoff or result in unwanted groundwater storage in areas intended for storage of the WQCV (e.g., porous sub-base of a permeable pavement system or in the bottom of an otherwise dry facility such as an extended detention basin). Conversely, for some types of BMPs such as wetland channels or constructed wetland basins, groundwater can be beneficial by providing saturation of the root zone and/or a source of baseflow. Groundwater quality protection is an issue that should be considered for infiltration-based BMPs. Infiltration BMPs may not be appropriate for land uses that involve storage or use of materials that have the potential to contaminate groundwater underlying a site (i.e., "hot spot" runoff from fueling stations, materials storage areas, etc.). If groundwater or soil contamination exists on a site and it will not be remediated or removed as a part of construction, it may be necessary to avoid infiltration-based BMPs or use a durable liner to prevent infiltration into contaminated areas.

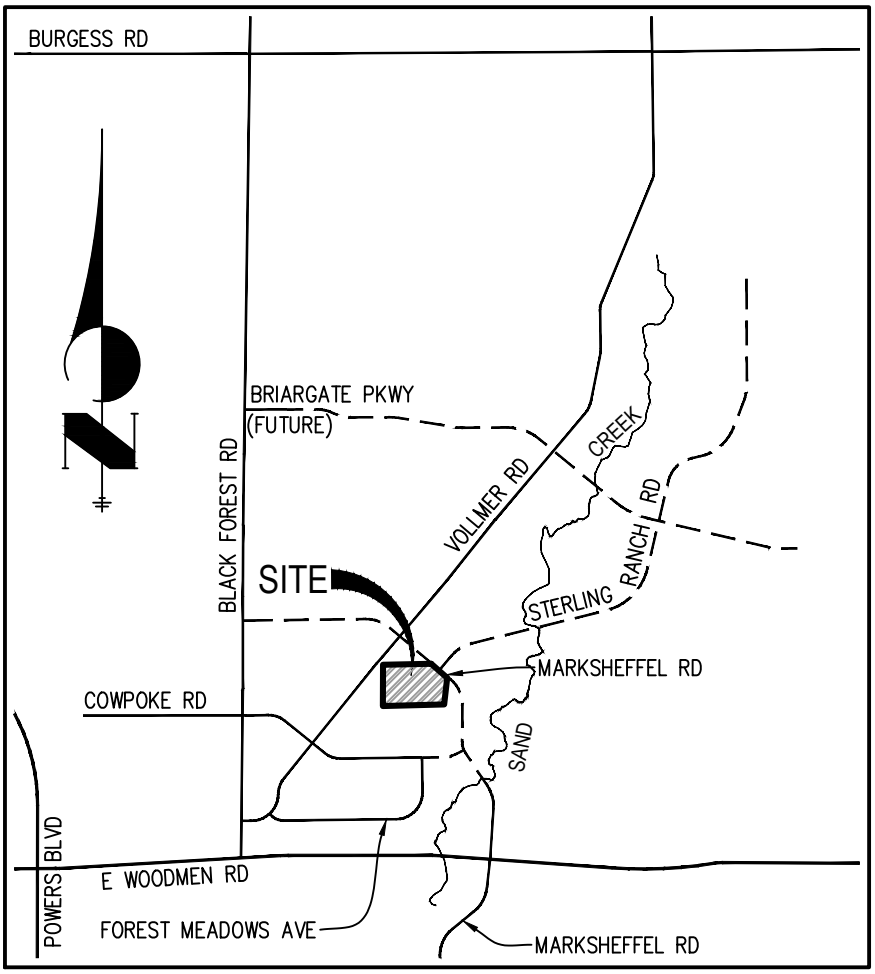
5.12 Linings

Sometimes an impermeable clay or synthetic liner is necessary. Stormwater detention and retention facilities have the potential to raise the groundwater level in the vicinity of the basin. Where there is concern for damage to adjacent structures due to rising ground water, consider lining the basin with an impermeable liner. An impermeable liner may also be warranted for a retention pond where the designer seeks to limit seepage from the permanent pool. Note that if left uncovered, synthetic lining on side slopes creates a serious impediment to egress and a potential drowning hazard. See the Retention Pond Fact Sheet in Volume 3 of the USDCM for guidance and benefits associated with the constructing a safety wetland bench.

Site Selection

EDBs are well suited for watersheds with at least five impervious acres up to approximately one square mile of watershed. Smaller watersheds can result in an orifice size prone to clogging. Larger watersheds and watersheds with baseflows can complicate the design and reduce the level of treatment provided. EDBs are also well suited where flood detention is incorporated into the same basin. The depth of groundwater should be investigated. Groundwater depth should be 2 or more feet below the bottom of the basin in order to keep this area dry and maintainable.

- Design foundation drains and other groundwater drains to bypass the water quality plate directing these drains to a conveyance element downstream of the EDB. This will reduce baseflows and help preserve storage for the WQCV.



VICINITY MAP

N.T.S.

STERLING RECYCLING FACILITY
VICINITY MAP
JOB NO. 25188.00
6/3/22
SHEET 1 OF 1

J·R ENGINEERING
A Westrian Company

Centennial 303-740-9393 • Colorado Springs 719-593-2593
Fort Collins 970-491-9888 • www.jrengineering.com

Hydrologic Soil Group—El Paso County Area, Colorado

Map Scale: 1:4,680 if printed on A portrait (8.5" x 11") sheet.

N

Meters
0 50 100 200 300

Feet
0 200 400 800 1200

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84

MAP LEGEND

Area of Interest (AOI)

- Area of Interest (AOI)

Soils

Soil Rating Polygons

- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

Soil Rating Lines

- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

Soil Rating Points

- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

Water Features

- Streams and Canals

Transportation

- Rails
- Interstate Highways
- US Routes
- Major Roads
- Local Roads

Background

- Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	46.2	51.5%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	43.6	48.5%
Totals for Area of Interest			**89.8**	**100.0%**

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, N/NGS12
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center** (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

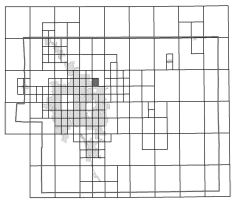
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined.
ZONE AE Base Flood Elevations determined.
ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodplain.
ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary
Floodway boundary
Zone D Boundary
CBRS and OPA boundary
Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
513 — Base Flood Elevation line and value; elevation in feet*
(EL 987) — Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

A — A — Cross section line
23 — 23 — Transect line
97° 07' 30.00" / 32° 22' 30.00" — Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
4275000 FT — 1000-meter Universal Transverse Mercator grid ticks, zone 13
6000000 FT — 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection
DX5510 — Bench mark (see explanation in Notes to Users section of this FIRM panel)
M1.5 — River Mile

MAP REPOSITORIES
Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'
250 0 500 1000 FEET
150 0 150 300 METERS

NFIP
NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0533G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 533 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	080060	0533	G
EL PASO COUNTY	080059	0533	G

Notice to User: The **Map Number** shown below should be used when placing map orders; the **Community Number** shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0533G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency

Appendix B
Hydrologic Calculations

COMPOSITE % IMPERVIOUS & COMPOSITE PRE-DEVELOPMENT RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/17/23

Basin ID	Total Area (ac)	Streets-Paved (100% Impervious)				Streets-Gravel (80% Impervious)				Historical Analysis (2% Impervious)				Basins Total Weighted C Values		Basins Total Weighted % Imp.
		C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	
EXA	2.68	0.90	0.96	0.16	6.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.52	1.9%	0.14	0.40	7.9%
EXB	2.60	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.60	2.0%	0.09	0.36	2.0%
EXC	2.11	0.90	0.96	0.00	0.0%	0.59	0.70	0.33	12.5%	0.09	0.36	1.78	1.7%	0.17	0.41	14.2%
EXD	13.44	0.90	0.96	0.86	6.4%	0.59	0.70	1.48	8.8%	0.09	0.36	11.10	1.7%	0.20	0.44	16.9%
EXE	8.51	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	8.51	2.0%	0.09	0.36	2.0%
EXF	3.09	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	3.09	2.0%	0.09	0.36	2.0%
OS1	9.42	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	9.42	2.0%	0.09	0.36	2.0%
TOTAL	41.85															7.8%

PRE-DEVELOPMENT
STANDARD FORM SF-2
TIME OF CONCENTRATION

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/17/23

SUB-BASIN DATA						INITIAL/OVERLAND (T_i)			TRAVEL TIME (T_t)					tc CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C_5	C_{100}	L (ft)	S_o (%)	t_i (min)	L_t (ft)	S_t (%)	K	VEL. (ft/s)	t_t (min)	COMP. t_c (min)	TOTAL LENGTH (ft)	Urbanized t_c (min)	t_c (min)
EXA	2.68	A	8%	0.14	0.40	300	4.0%	19.0	190	2.3%	10.0	1.5	2.1	21.1	490.0	26.7	21.1
EXB	2.60	A	2%	0.09	0.36	300	2.5%	23.3	240	2.5%	10.0	1.6	2.5	25.9	540.0	28.4	25.9
EXC	2.11	A	14%	0.17	0.41	300	2.6%	21.3	135	1.7%	15.0	2.0	1.2	22.4	435.0	25.2	22.4
EXD	13.44	A	17%	0.20	0.44	300	3.6%	18.5	810	3.4%	15.0	2.8	4.9	23.4	1110.0	29.6	23.4
EXE	8.51	A	2%	0.09	0.36	300	4.0%	20.0	800	3.0%	10.0	1.7	7.7	27.7	1100.0	34.0	27.7
EXF	3.09	A	2%	0.09	0.36	300	3.5%	20.9	400	4.3%	10.0	2.1	3.2	24.1	700.0	29.1	24.1
OS1	9.42	A	2%	0.09	0.36	150	2.0%	17.8	850	0.2%	10.0	0.4	31.7	49.4	1000.0	59.8	49.4

NOTES:

$$t_c = t_i + t_t$$ Equation 6-2

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$$ Equation 6-3

Where:

t_i = overland (initial) flow time (minutes)
C_5 = runoff coefficient for 5-year frequency (from Table 6-4)
L_i = length of overland flow (ft)
S_o = average slope along the overland flow path (ft/ft).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$ Equation 6-4

Where:

t_t = channelized flow time (travel time, min)
L_t = waterway length (ft)
S_o = waterway slope (ft/ft)
V_t = travel time velocity (ft/sec) = $K\sqrt{S_o}$
K = NRCS conveyance factor (see Table 6-2).

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$ Equation 6-5

Where:

t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.
L_t = length of channelized flow path (ft)
i = imperviousness (expressed as a decimal)
S_t = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

STANDARD FORM SF-3 - PRE-DEVELOPMENT

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County
Design Storm: 5-Year

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/17/23

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	tc (min)	C*A (ac)	I (in/hr)	Q (cfs)	$Q_{street/swale}$ (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	
	1	EXA	2.68	0.14	21.1	0.37	3.01	1.1															Sheet flows overland to DP1 Flows off-site to the west
	2	EXB	2.60	0.09	25.9	0.23	2.70	0.6															Sheet flows overland to DP2 Flows off-site to the west
	3	EXC	2.11	0.17	22.4	0.35	2.92	1.0															Sheet flows overland and along berm to DP3 Flows off-site to the south
	4	EXD	13.44	0.20	23.4	2.65	2.85	7.6															Sheet flows overland and along berm to DP4 Flows off-site to the south
	5	OS1	9.42	0.09	49.4	0.85	1.73	1.5															Sheet flows overland and along berm to DP5 Flows on-site and combines at DP6.1
	6	EXE	8.51	0.09	27.7	0.77	2.60	2.0															Sheet flows overland and along berm to DP6 Combines flows at DP6.1
	6.1								49.4	1.62	1.73	2.8											Combines the flows from DP5 and DP6 Flows off-site to the south
	7	EXF	3.09	0.09	24.1	0.28	2.81	0.8															Sheet flows overland to DP7 Flows off-site to the east

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

STANDARD FORM SF-3 - PRE-DEVELOPMENT

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County
Design Storm: 100-Year

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/17/23

Description	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	tc (min)	C*A (ac)	I (in/hr)	Q (cfs)	$Q_{street/swale}$ (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	
	1	EXA	2.68	0.40	21.1	1.06	5.05	5.4															Sheet flows overland to DP1 Flows off-site to the west
	2	EXB	2.60	0.36	25.9	0.94	4.54	4.3															Sheet flows overland to DP2 Flows off-site to the west
	3	EXC	2.11	0.41	22.4	0.87	4.90	4.3															Sheet flows overland and along berm to DP3 Flows off-site to the south
	4	EXD	13.44	0.44	23.4	5.86	4.79	28.1															Sheet flows overland and along berm to DP4 Flows off-site to the south
	5	OS1	9.42	0.36	49.4	3.39	2.90	9.8															Sheet flows overland and along berm to DP5 Flows on-site and combines at DP6.1
	6	EXE	8.51	0.36	27.7	3.06	4.37	13.4															Sheet flows overland and along berm to DP6 Combines flows at DP6.1
	6.1								49.4	6.45	2.90	18.7											Combines the flows from DP5 and DP6 Flows off-site to the south
	7	EXF	3.09	0.36	24.1	1.11	4.72	5.2															Sheet flows overland to DP7 Flows off-site to the east

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/20/23

Basin ID	Total Area (ac)	Streets-Paved (100% Impervious)				Streets-Gravel (80% Impervious)				Historical Analysis (2% Impervious)				Basins Total Weighted C Values		Basins Total Weighted % Imp.
		C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	
A	0.30	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.30	2.0%	0.09	0.36	2.0%
B	14.43	0.90	0.96	2.53	17.5%	0.59	0.70	0.10	0.6%	0.09	0.36	11.80	1.6%	0.24	0.47	19.7%
C	10.64	0.90	0.96	0.52	4.9%	0.59	0.70	0.00	0.0%	0.09	0.36	10.12	1.9%	0.13	0.39	6.8%
D	2.69	0.90	0.96	0.27	10.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.42	1.8%	0.17	0.42	11.8%
E	2.49	0.90	0.96	0.11	4.4%	0.59	0.70	0.22	7.1%	0.09	0.36	2.16	1.7%	0.17	0.42	13.2%
F	2.26	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.26	2.0%	0.09	0.36	2.0%
OS1	9.42	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	9.42	2.0%	0.09	0.36	2.0%
OS2	0.36	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.36	2.0%	0.09	0.36	2.0%
TOTAL (W. FOREBAY)	34.49															10.9%
TOTAL (N. FOREBAY)	5.18															12.5%
TOTAL (POND)	42.29															10.5%

Indicate which basins contribute to each forebay

How is overall imperviousness less than areas to each forebay?

PROPOSED
STANDARD FORM SF-2
TIME OF CONCENTRATION

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/20/23

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					tc CHECK			
DATA						(T_i)			(T_t)					(URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C_5	C_{100}	L (ft)	S_o (%)	t_i (min)	L_t (ft)	S_t (%)	K	VEL. (ft/s)	t_t (min)	COMP. t_c (min)	TOTAL LENGTH (ft)	Urbanized t_c (min)	t_c (min)
A	0.30	A	2%	0.09	0.36	20	33.0%	2.6	0	0.0%	10.0	0.0	0.0	2.6	20.0	25.7	5.0
B	14.43	A	20%	0.24	0.47	300	2.7%	19.5	1600	1.5%	15.0	1.8	14.5	34.0	1900.0	41.2	34.0
C	10.64	A	7%	0.13	0.39	300	2.7%	21.9	750	1.5%	15.0	1.8	6.8	28.7	1050.0	35.1	28.7
D	2.69	A	12%	0.17	0.42	245	3.0%	18.3	400	1.5%	15.0	1.8	3.6	21.9	645.0	29.1	21.9
E	2.49	A	13%	0.17	0.42	190	3.8%	14.9	440	1.5%	10.0	1.2	6.0	20.9	630.0	29.3	20.9
F	2.26	A	2%	0.09	0.36	40	25.0%	4.0	615	0.5%	10.0	0.7	14.5	18.5	655.0	41.3	18.5
OS1	9.42	A	2%	0.09	0.36	150	2.0%	17.8	850	0.2%	10.0	0.4	31.7	49.4	1000.0	59.8	49.4
OS2	0.36	A	2%	0.09	0.36	115	3.0%	13.6	300	3.0%	10.0	1.7	2.9	16.5	415.0	28.8	16.5

NOTES:

$$t_c = t_i + t_t$$ Equation 6-2

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$$ Equation 6-3

Where:

t_i = overland (initial) flow time (minutes)
C_5 = runoff coefficient for 5-year frequency (from Table 6-4)
L_i = length of overland flow (ft)
S_o = average slope along the overland flow path (ft/ft).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$ Equation 6-4

Where:

t_t = channelized flow time (travel time, min)
L_t = waterway length (ft)
S_o = waterway slope (ft/ft)
V_t = travel time velocity (ft/sec) = $K\sqrt{S_o}$
K = NRCS conveyance factor (see Table 6-2).

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$ Equation 6-5

Where:

t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.
L_t = length of channelized flow path (ft)
i = imperviousness (expressed as a decimal)
S_t = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

STANDARD FORM SF-3 - PROPOSED

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County
Design Storm: 5-Year

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/20/23

		DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	tc (min)	C*A (ac)	I (in/hr)	Q (cfs)	$Q_{street/swale}$ (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	A	0.30	0.09	5.0	0.03	5.17	0.2															Flows overland along the western site boundary to DP1 Flows off-site to the west
	2	B	14.43	0.24	34.0	3.40	2.29	7.8															Sheet flows overland to swale and then to DP2 Combines flow at FES at DP4.2
	3	OS1	9.42	0.09	49.4	0.85	1.73	1.5															Sheet flows overland and along berm to DP3 Flows on-site and combines at culvert at DP4.1
	4	C	10.64	0.13	28.7	1.38	2.55	3.5															Sheet flows overland to swale and then to DP4 Combines flow at culvert at DP4.1
	4.1								49.4	2.23	1.73	3.9											Combined flow of DP3 and DP4 within culvert Swale to FES at DP4.2
	4.2								49.4	5.63	1.73	9.7											Combined flow of DP2 and DP4.1 at sump inlet Piped to pond forebay, combines flow at DP8.1
	5	D	2.69	0.17	21.9	0.46	2.95	1.4															Sheet flows overland to swale and then to DP5 Combines flow at sump inlet at DP7.1
	6	E	2.49	0.17	20.9	0.42	3.02	1.3															Sheet flows overland to swale and then to DP6 Combines flow at sump inlet at DP7.1
	7	OS2	0.36	0.09	16.5	0.03	3.38	0.1															Sheet flows overland to DP7 Combines flow at sump inlet at DP7.1
	7.1								21.9	0.91	2.95	2.7											Combined flow of DP5, DP6, and DP7 at sump inlet Piped to pond forebay, combines flow at DP8.1
	8	F	2.26	0.09	18.5	0.20	3.21	0.6															Flows along trickle channel to DP8 at outlet structure Combines flow at DP8.1
	8.1								49.4	6.74	1.73	11.7											Combined flow of DP4.2, DP6.1, and DP8. Total interim pond inflow. Released though pond outlet structure at DP8.2
	8.2								-	-	-	0.1											Released flow through interim outlet structure from MHFD_Det Piped to existing junction box and storm infrastructure

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

STANDARD FORM SF-3 - PROPOSED

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County
Design Storm: 100-Year

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/20/23

Description	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	tc (min)	C*A (ac)	I (in/hr)	Q (cfs)	$Q_{street/swale}$ (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	
	1	A	0.30	0.36	5.0	0.11	8.68	1.0															Flows overland along the western site boundary to DP1 Flows off-site to the west
	2	B	14.43	0.47	34.0	6.75	3.85	26.0															Sheet flows overland to swale and then to DP2 Combines flow at FES at DP4.2
	3	OS1	9.42	0.36	49.4	3.39	2.90	9.8															Sheet flows overland and along berm to DP3 Flows on-site and combines at culvert at DP4.1
	4	C	10.64	0.39	28.7	4.14	4.28	17.7															Sheet flows overland to swale and then to DP4 Combines flow at culvert at DP4.1
	4.1								49.4	7.53	2.90	21.9											Combined flow of DP3 and DP4 within culvert Swale to FES at DP4.2
	4.2								49.4	14.28	2.90	41.5											Combined flow of DP2 and DP4.1 at sump inlet Piped to pond forebay, combines flow at DP8.1
	5	D	2.69	0.42	21.9	1.13	4.96	5.6															Sheet flows overland to swale and then to DP5 Combines flow at sump inlet at DP7.1
	6	E	2.49	0.42	20.9	1.04	5.08	5.3															Sheet flows overland to swale and then to DP6 Combines flow at sump inlet at DP7.1
	7	OS2	0.36	0.36	16.5	0.13	5.67	0.7															Sheet flows overland to DP7 Combines flow at sump inlet at DP7.1
	7.1								21.9	2.30	4.96	11.4											Combined flow of DP5, DP6, and DP7 at sump inlet Piped to pond forebay, combines flow at DP8.1
	8	F	2.26	0.36	18.5	0.81	5.38	4.4															Flows along trickle channel to DP8 at outlet structure Combines flow at DP8.1
	8.1								49.4	17.39	2.90	50.5											Combined flow of DP4.2, DP6.1, and DP8. Total interim pond inflow. Released though pond outlet structure at DP8.2
	8.2								-	-	-	8.0											Released flow through interim outlet structure from MHFD_Det Piped to existing junction box and storm infrastructure

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Recycling Facility
Location: El Paso County

Project Name: Sterling Ranch
Project No.: 25188.14
Calculated By: GAG
Checked By:
Date: 7/18/23

Basin ID	Total Area (ac)	Industrial-Heavy Areas (90% Impervious)				Business-Commercial Areas (95% Impervious)				Residential-1/8 Acre or Less (65% Impervious)				Streets-Paved (100% Impervious)				Historical Analysis (2% Impervious)				Basins Total Weighted C Values		Basins Total Weighted % Imp.
		C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	Area (ac)	Weighted % Imp.	C_5	C_{100}	
POND A	44.16	0.73	0.81	6.61	13.5%	0.81	0.88	9.42	20.3%	0.45	0.59	24.06	35.4%	0.90	0.96	1.40	3.2%	0.09	0.36	2.67	0.1%	0.56	0.68	72.4%
TOTAL	44.16																							72.4%

Appendix C
Hydraulic Calculations

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Swale DP2

Triangular

Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.60
Invert Elev (ft)	= 1.00
Slope (%)	= 1.00
N-Value	= 0.035

Calculations

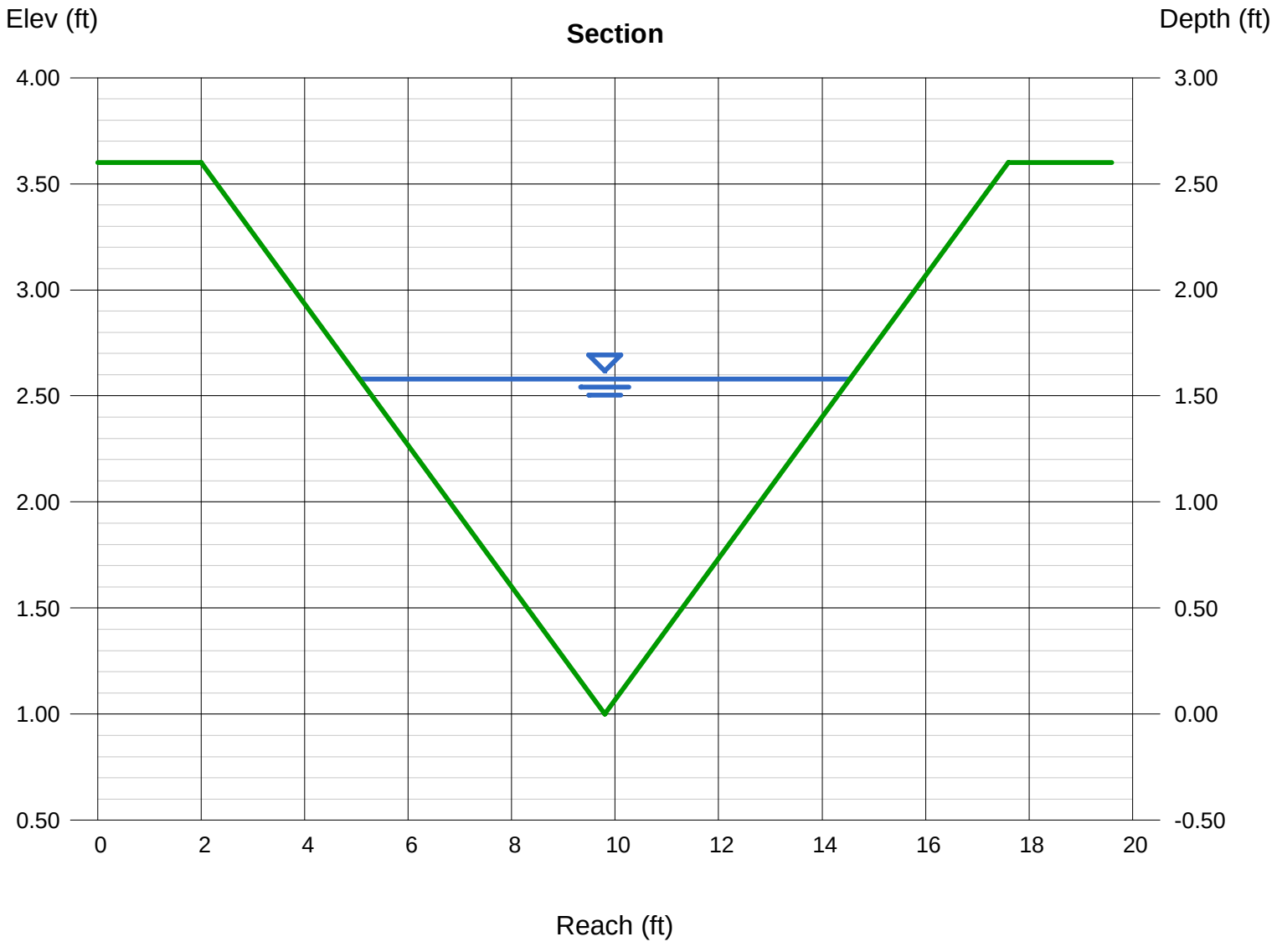
Compute by:	Known Q
Known Q (cfs)	= 26.00

Highlighted

Depth (ft)	= 1.58
Q (cfs)	= 26.00
Area (sqft)	= 7.49
Velocity (ft/s)	= 3.47
Wetted Perim (ft)	= 9.99
Crit Depth, Yc (ft)	= 1.37
Top Width (ft)	= 9.48
EGL (ft)	= 1.77

Per ECM 3.3.4.A, ditches in developments (roadside ditches excluded) that convey more than 15cfs should be in drainage easements. Please create drainage easements and reflect them on the plat.

Include what FR # is for each swale. If any are over 0.8, include what will be done to mitigate it.



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Swale DP4

Triangular

Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 2.50
Invert Elev (ft)	= 1.00
Slope (%)	= 1.00
N-Value	= 0.035

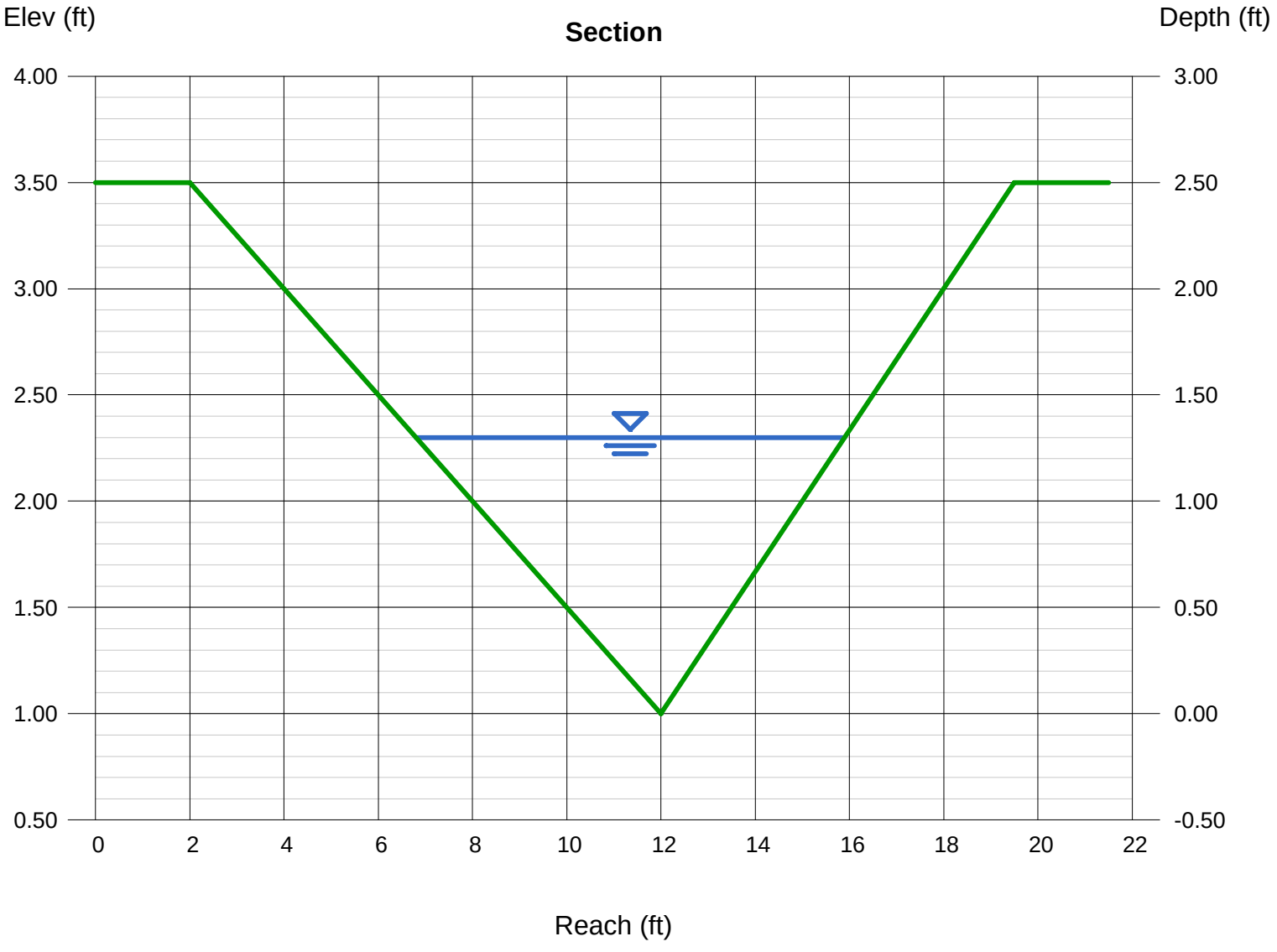
Calculations

Compute by:	Known Q
Known Q (cfs)	= 18.00

Highlighted

Depth (ft)	= 1.30
Q (cfs)	= 18.00
Area (sqft)	= 5.91
Velocity (ft/s)	= 3.04
Wetted Perim (ft)	= 9.47
Crit Depth, Yc (ft)	= 1.11
Top Width (ft)	= 9.10
EGL (ft)	= 1.44

Per ECM 3.3.4.A, ditches in developments (roadside ditches excluded) that convey more than 15cfs should be in drainage easements. Please create drainage easements and reflect them on the plat.



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Monday, Jul 31 2023

Swale DP4.1

Triangular

Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.50
Invert Elev (ft)	= 1.00
Slope (%)	= 2.00
N-Value	= 0.035

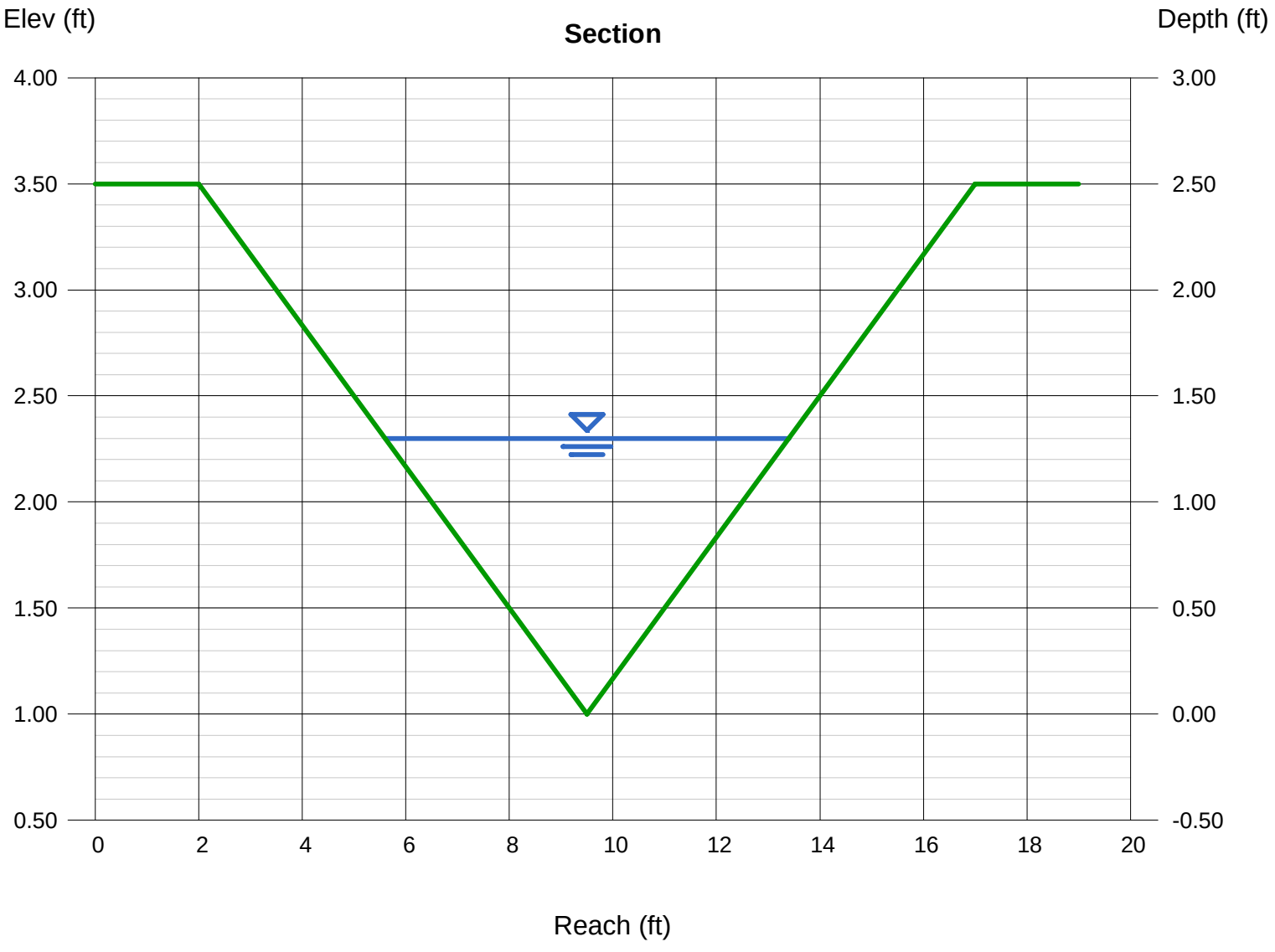
Calculations

Compute by:	Known Q
Known Q (cfs)	= 22.00

Highlighted

Depth (ft)	= 1.30
Q (cfs)	= 22.00
Area (sqft)	= 5.07
Velocity (ft/s)	= 4.34
Wetted Perim (ft)	= 8.22
Crit Depth, Yc (ft)	= 1.28
Top Width (ft)	= 7.80
EGL (ft)	= 1.59

Per ECM 3.3.4.A, ditches in developments (roadside ditches excluded) that convey more than 15cfs should be in drainage easements. Please create drainage easements and reflect them on the plat.



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

DP4.1 Culvert-5 year

Invert Elev Dn (ft)	=	6978.36
Pipe Length (ft)	=	75.70
Slope (%)	=	1.00
Invert Elev Up (ft)	=	6979.12
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	1
n-Value	=	0.013
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Groove end projecting (C)
Coeff. K,M,c,Y,k	=	0.0045, 2, 0.0317, 0.69, 0.2

Embankment

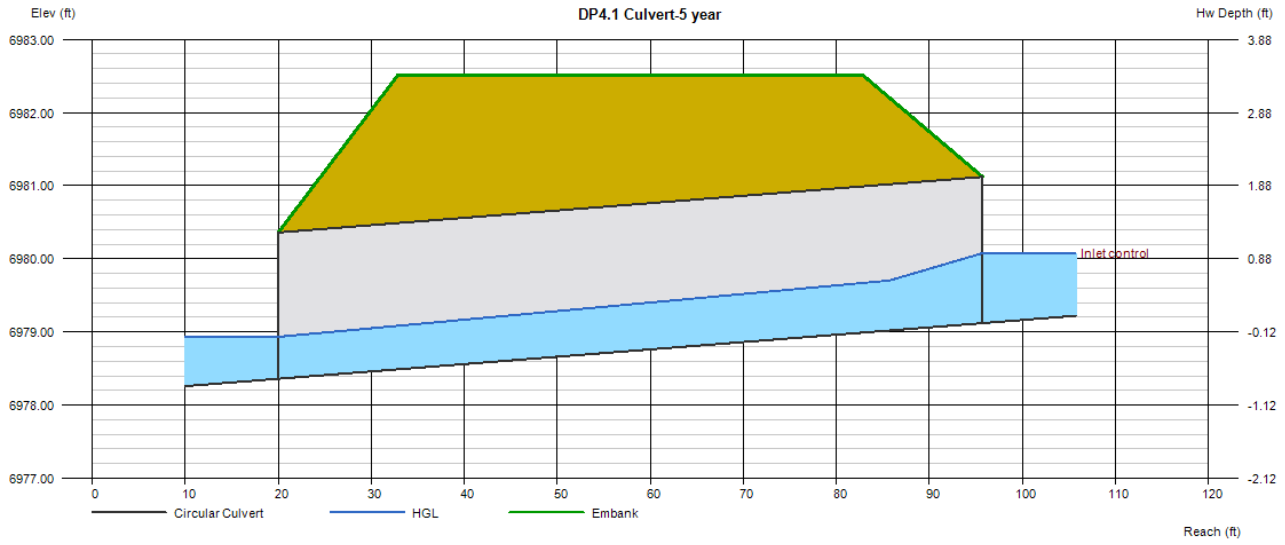
Top Elevation (ft)	=	6982.51
Top Width (ft)	=	50.00
Crest Width (ft)	=	125.00

Calculations

Qmin (cfs)	=	4.00
Qmax (cfs)	=	4.00
Tailwater Elev (ft)	=	0.00

Highlighted

Qtotal (cfs)	=	4.00
Qpipe (cfs)	=	4.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	5.38
Veloc Up (ft/s)	=	4.08
HGL Dn (ft)	=	6978.93
HGL Up (ft)	=	6979.82
Hw Elev (ft)	=	6980.08
Hw/D (ft)	=	0.48
Flow Regime	=	Inlet Control



Provide calculations for riprap outlet protection

Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

DP4.1 Culvert-100 year

Invert Elev Dn (ft)	=	6978.36
Pipe Length (ft)	=	75.70
Slope (%)	=	1.00
Invert Elev Up (ft)	=	6979.12
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	1
n-Value	=	0.013
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Groove end projecting (C)
Coeff. K,M,c,Y,k	=	0.0045, 2, 0.0317, 0.69, 0.2

Embankment

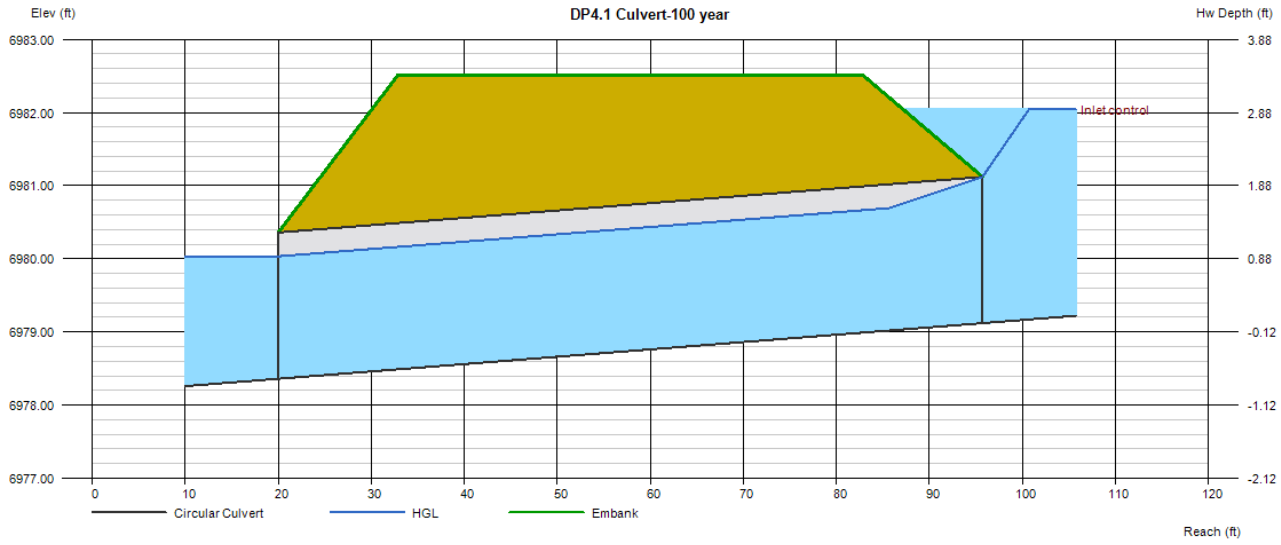
Top Elevation (ft)	=	6982.51
Top Width (ft)	=	50.00
Crest Width (ft)	=	125.00

Calculations

Qmin (cfs)	=	22.00
Qmax (cfs)	=	22.00
Tailwater Elev (ft)	=	0.00

Highlighted

Qtotal (cfs)	=	22.00
Qpipe (cfs)	=	22.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.83
Veloc Up (ft/s)	=	7.84
HGL Dn (ft)	=	6980.03
HGL Up (ft)	=	6980.79
Hw Elev (ft)	=	6982.04
Hw/D (ft)	=	1.46
Flow Regime	=	Inlet Control



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Tuesday, Jul 25 2023

DP4.2 Culvert to West Forebay-5 year

Invert Elev Dn (ft)	=	6969.19
Pipe Length (ft)	=	46.20
Slope (%)	=	3.33
Invert Elev Up (ft)	=	6970.73
Rise (in)	=	30.0
Shape	=	Circular
Span (in)	=	30.0
No. Barrels	=	1
n-Value	=	0.013
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Groove end projecting (C)
Coeff. K,M,c,Y,k	=	0.0045, 2, 0.0317, 0.69, 0.2

Embankment

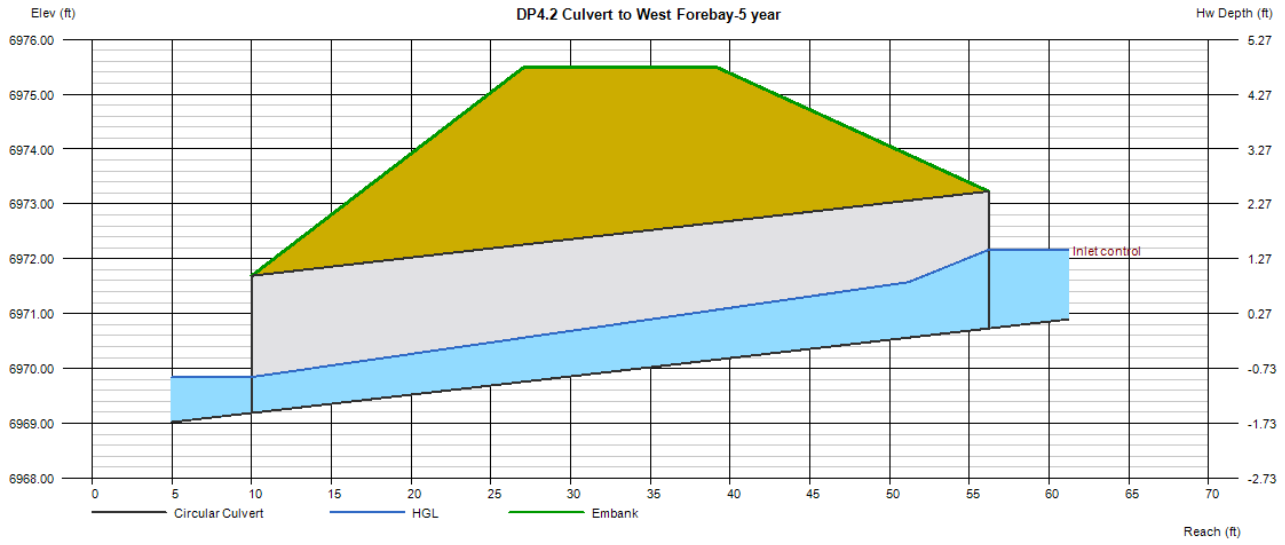
Top Elevation (ft)	=	6975.50
Top Width (ft)	=	12.00
Crest Width (ft)	=	78.00

Calculations

Qmin (cfs)	=	10.00
Qmax (cfs)	=	10.00
Tailwater Elev (ft)	=	6967.53

Highlighted

Qtotal (cfs)	=	10.00
Qpipe (cfs)	=	10.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	9.75
Veloc Up (ft/s)	=	5.08
HGL Dn (ft)	=	6969.85
HGL Up (ft)	=	6971.79
Hw Elev (ft)	=	6972.16
Hw/D (ft)	=	0.57
Flow Regime	=	Inlet Control



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, Jul 28 2023

DP4.2 Culvert to West Forebay-100 year

Invert Elev Dn (ft)	=	6969.19
Pipe Length (ft)	=	46.20
Slope (%)	=	3.33
Invert Elev Up (ft)	=	6970.73
Rise (in)	=	30.0
Shape	=	Circular
Span (in)	=	30.0
No. Barrels	=	1
n-Value	=	0.013
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Groove end projecting (C)
Coeff. K,M,c,Y,k	=	0.0045, 2, 0.0317, 0.69, 0.2

Embankment

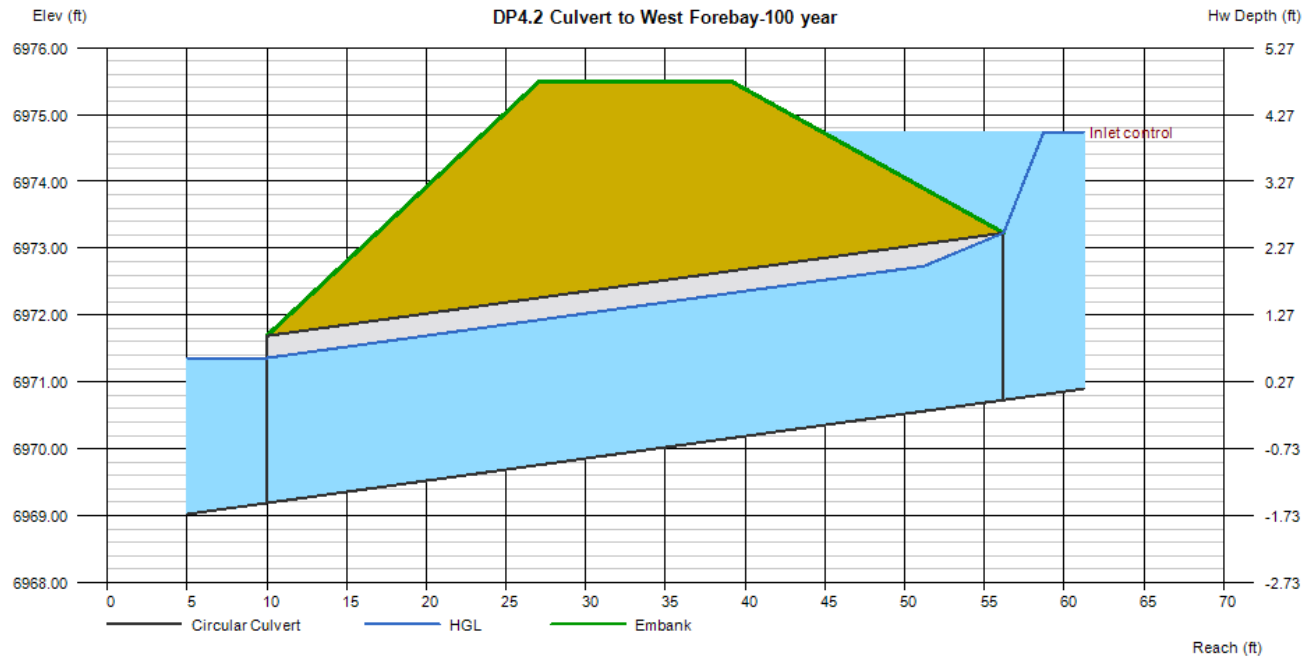
Top Elevation (ft)	=	6975.50
Top Width (ft)	=	12.00
Crest Width (ft)	=	78.00

Calculations

Qmin (cfs)	=	42.00
Qmax (cfs)	=	42.00
Tailwater Elev (ft)	=	6969.54

Highlighted

Qtotal (cfs)	=	42.00
Qpipe (cfs)	=	42.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	9.28
Veloc Up (ft/s)	=	9.29
HGL Dn (ft)	=	6971.36
HGL Up (ft)	=	6972.90
Hw Elev (ft)	=	6974.73
Hw/D (ft)	=	1.60
Flow Regime	=	Inlet Control



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Swale DP5

Triangular

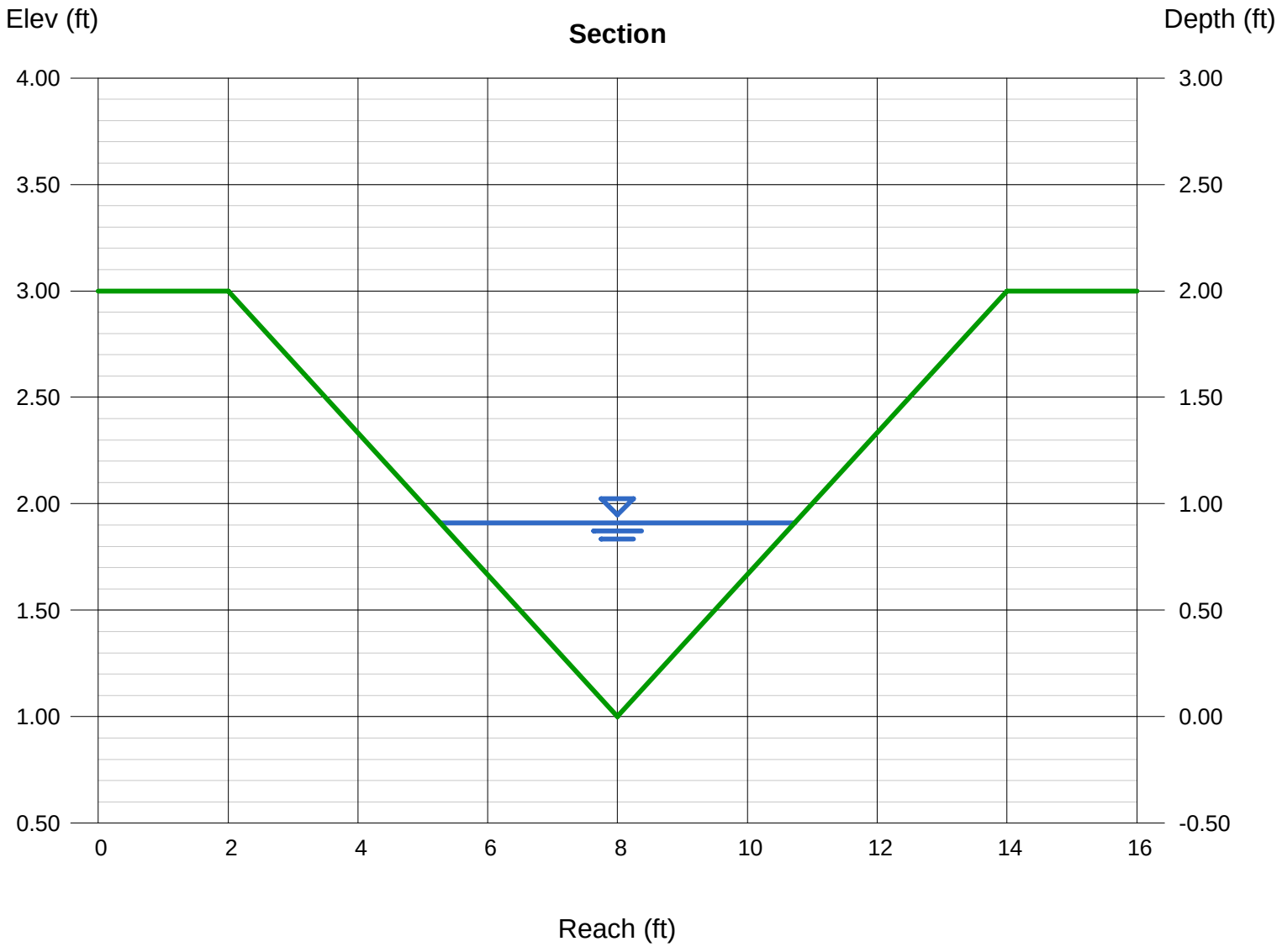
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 1.00
Slope (%)	= 1.00
N-Value	= 0.035

Calculations

Compute by:	Known Q
Known Q (cfs)	= 6.00

Highlighted

Depth (ft)	= 0.91
Q (cfs)	= 6.000
Area (sqft)	= 2.48
Velocity (ft/s)	= 2.42
Wetted Perim (ft)	= 5.76
Crit Depth, Yc (ft)	= 0.76
Top Width (ft)	= 5.46
EGL (ft)	= 1.00



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Swale DP6

Triangular

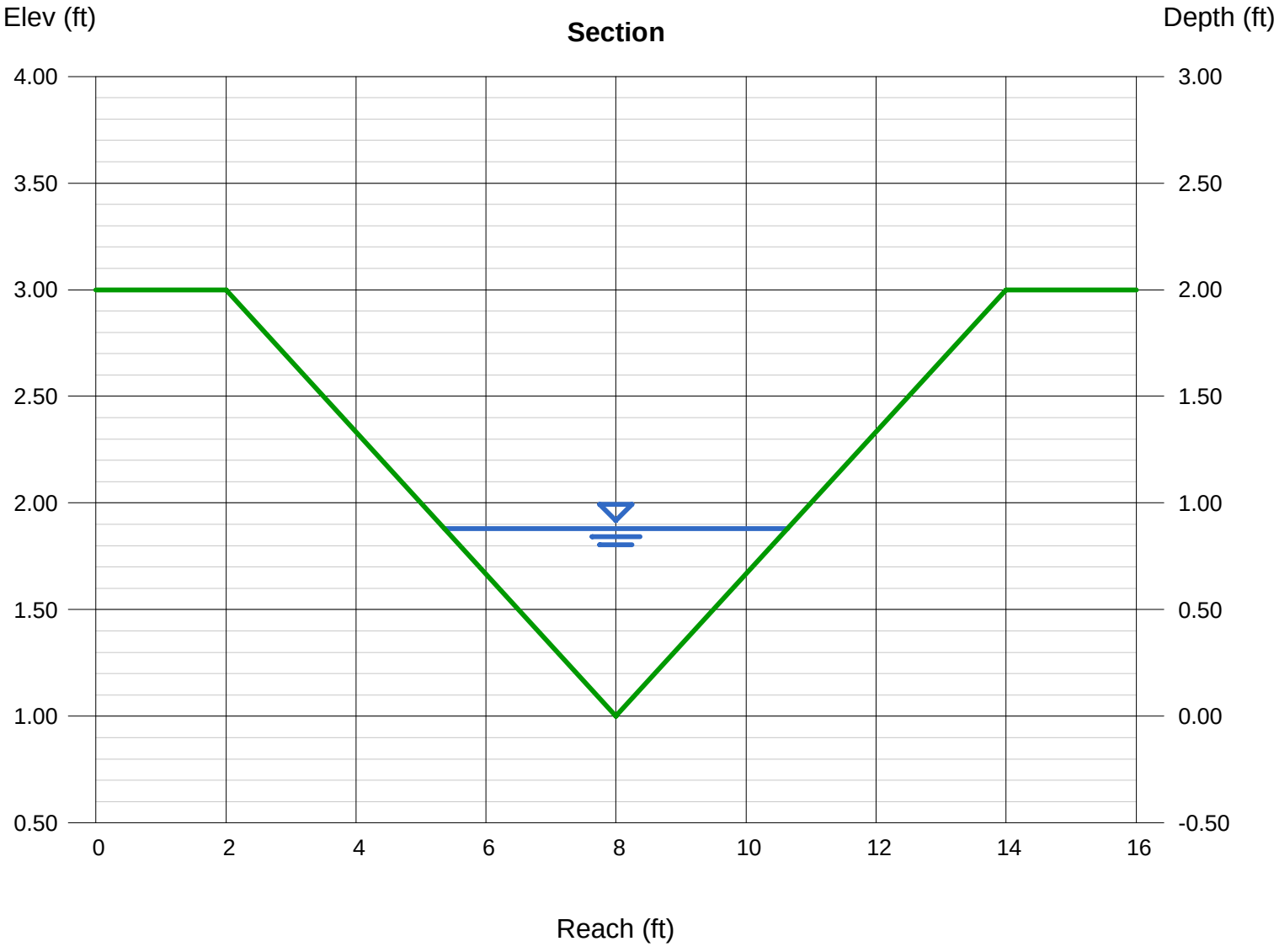
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 1.00
Slope (%)	= 1.00
N-Value	= 0.035

Calculations

Compute by:	Known Q
Known Q (cfs)	= 5.50

Highlighted

Depth (ft)	= 0.88
Q (cfs)	= 5.500
Area (sqft)	= 2.32
Velocity (ft/s)	= 2.37
Wetted Perim (ft)	= 5.57
Crit Depth, Yc (ft)	= 0.74
Top Width (ft)	= 5.28
EGL (ft)	= 0.97



Design Point 7.1 (Single Type C Grate)

Orifice Flow Calculation

Q = C*A* square root (2gH)

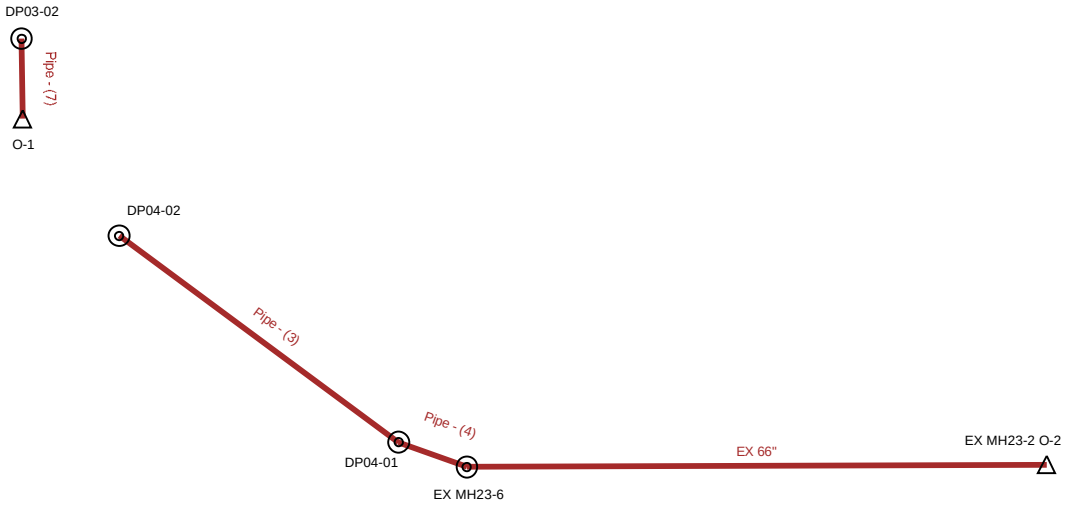
C = 0.6 A = 8.53 sq ft g = 32.2

Head (ft)	CA	(2GH)	Sqrt (2GH)	Capacity
1	5.118	64.40	8.025	41.1
2	5.118	128.80	11.349	58.1
3	5.118	193.20	13.900	71.1
4	5.118	257.60	16.050	82.1
5	5.118	322.00	17.944	91.8
6	5.118	386.40	19.657	100.6

Q_{100} DP7.1 = 11.4 cfs
Available Head = 2 ft

Use MHFD Inlet spreadsheet for Type C inlet

Scenario: 5-YEAR



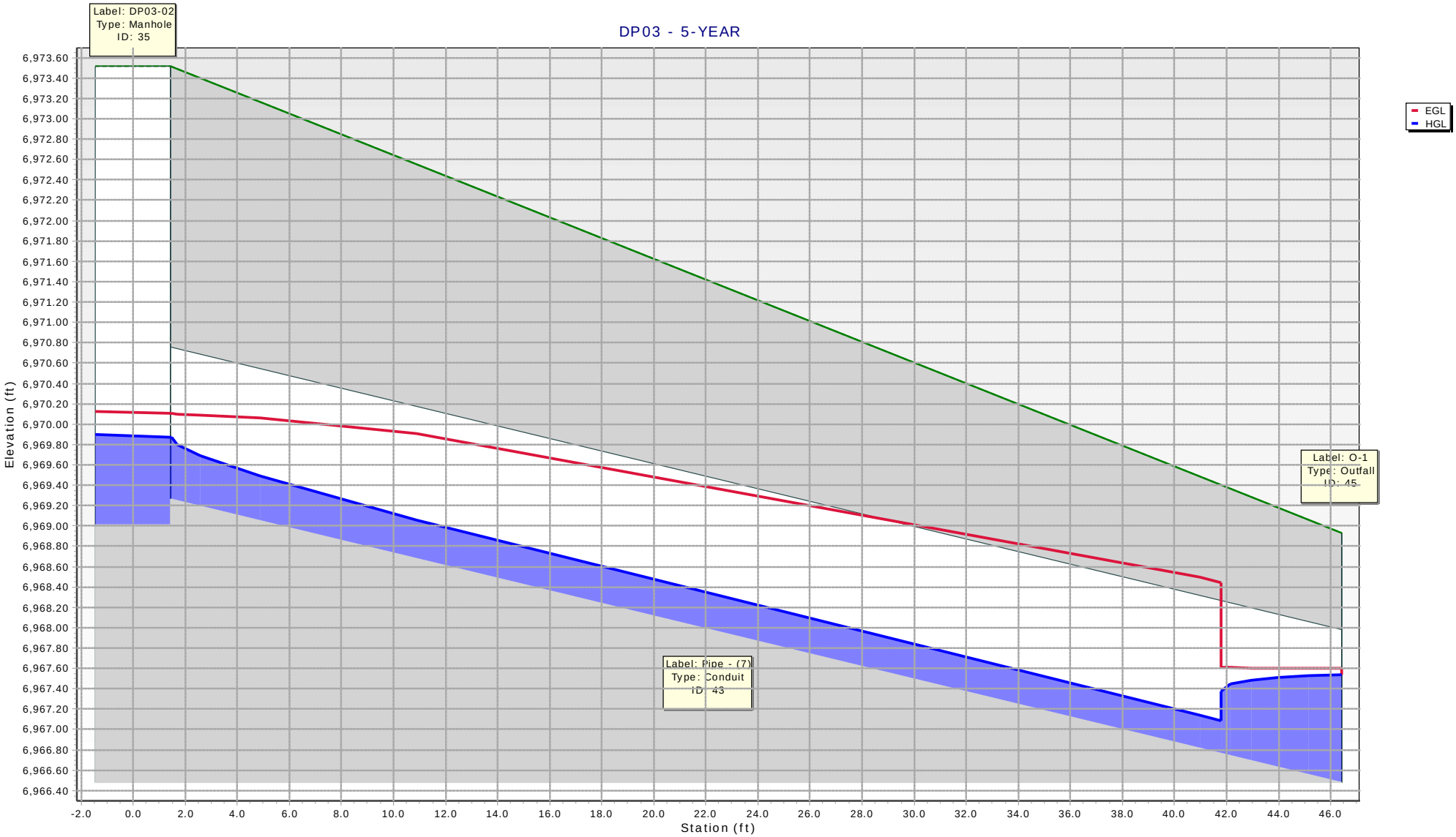
5-year Interim Report

Upstream Structure	Label	Flow (cfs)	Capacity (Full Flow) (cfs)	Diameter (in)	Manning's n	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	HGL (In) (ft)	HGL (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Velocity (ft/s)	Upstream Structure Headloss Coefficient
EX MH23-6	EX 66"	30.8	224.37	66	0.013	383	0.004	6,950.95	6,949.24	6,969.69	6,967.11	6,952.45	6,951.03	6,952.98	6,951.36	6.62	0.8
DP04-02	Pipe - (3)	0.1	37.87	24	0.013	200.3	0.028	6,962.51	6,956.90	6,972.35	6,967.70	6,962.62	6,956.98	6,962.66	6,957.08	2.58	0.1
DP04-01	Pipe - (4)	0.1	266.77	48	0.013	41.9	0.034	6,954.90	6,953.45	6,967.70	6,969.69	6,954.99	6,953.51	6,955.02	6,953.61	2.51	0.6
DP03-02	Pipe - (7)	2.6	25.71	18	0.013	46.4	0.06	6,969.26	6,966.48	6,973.52	6,968.93	6,969.87	6,967.54	6,970.10	6,967.60	9.34	0.1

100-year Interim Report

Upstream Structure	Label	Flow (cfs)	Capacity (Full Flow) (cfs)	Diameter (in)	Manning's n	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	HGL (In) (ft)	HGL (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Velocity (ft/s)	Upstream Structure Headloss Coefficient
EX MH23-6	EX 66"	241.4	224.37	66	0.013	383	0.004	6,950.95	6,949.24	6,969.69	6,967.11	6,959.38	6,957.40	6,960.98	6,959.00	10.16	0.8
DP04-02	Pipe - (3)	8.0	37.87	24	0.013	200.3	0.028	6,962.51	6,956.90	6,972.35	6,967.70	6,963.52	6,960.67	6,963.92	6,960.77	9.56	0.1
DP04-01	Pipe - (4)	8.0	266.77	48	0.013	41.9	0.034	6,954.90	6,953.45	6,967.70	6,969.69	6,960.66	6,960.66	6,960.67	6,960.67	0.64	0.6
DP03-02	Pipe - (7)	10.8	25.71	18	0.013	46.4	0.06	6,969.26	6,966.48	6,973.52	6,968.93	6,970.52	6,969.55	6,971.24	6,970.13	13.91	0.1

100-yr undetained flow from development is 50 cfs and flow in existing 54" RCP is 233 cfs. System needs to be able to handle 283 cfs.


DP03 - 5-YEAR
Label: DP03-02
Type: Manhole
ID: 35
Label: O-1
Type: Outfall
ID: 45
Label: Pipe - (7)
Type: Conduit
ID: 43
EGL
HGL
Elevation (ft)
Station (ft)
6,973.60
6,973.40
6,973.20
6,973.00
6,972.80
6,972.60
6,972.40
6,972.20
6,972.00
6,971.80
6,971.60
6,971.40
6,971.20
6,971.00
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6,970.00
6,969.80
6,969.60
6,969.40
6,969.20
6,969.00
6,968.80
6,968.60
6,968.40
6,968.20
6,968.00
6,967.80
6,967.60
6,967.40
6,967.20
6,967.00
6,966.80
6,966.60
6,966.40
-2.0
0.0
2.0
4.0
6.0
8.0
10.0
12.0
14.0
16.0
18.0
20.0
22.0
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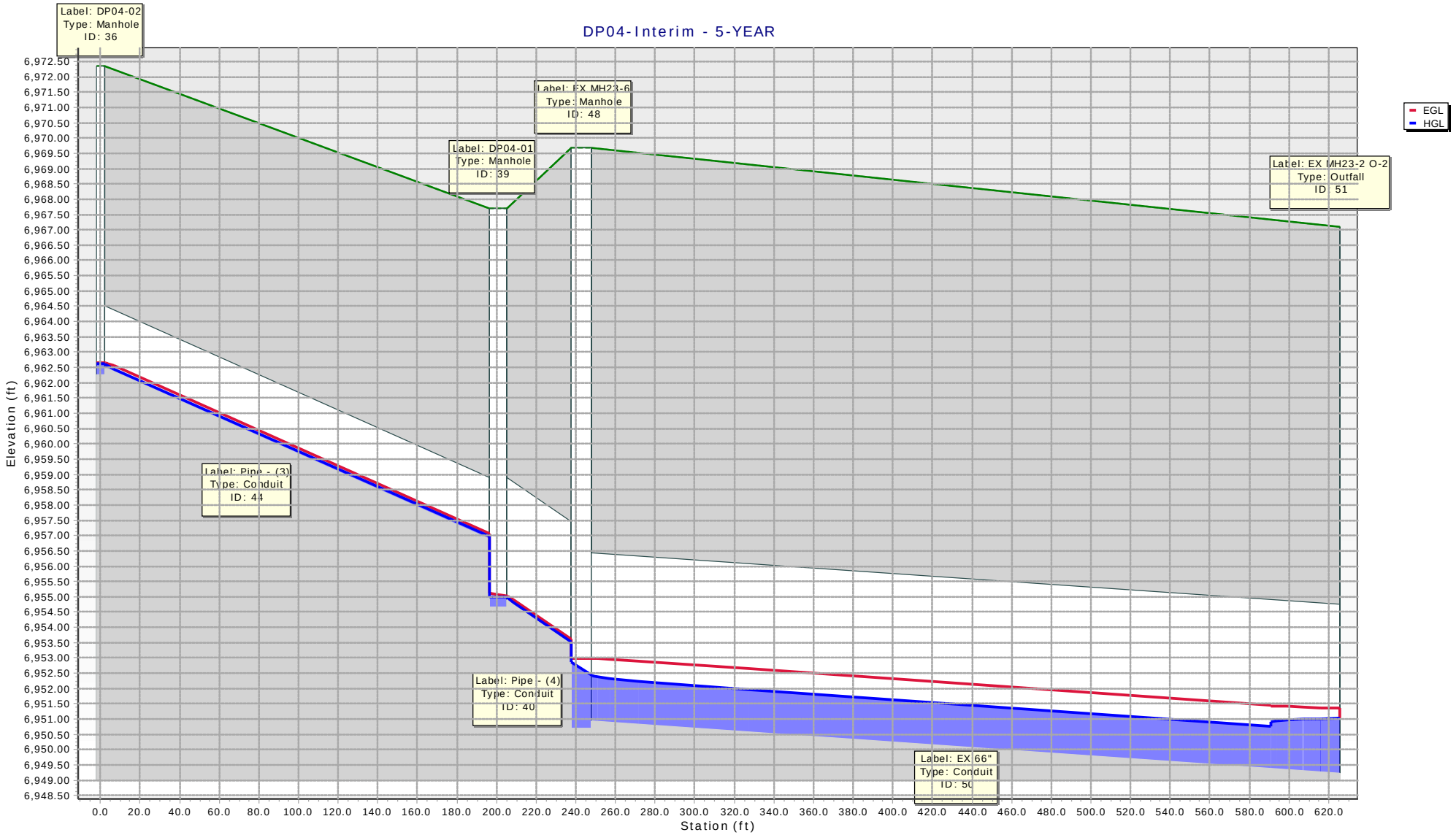
DP04-Interim - 5-YEAR
Label: DP04-02
Type: Manhole
ID: 36
Label: EX MH23-6
Type: Manhole
ID: 48
Label: DP04-01
Type: Manhole
ID: 39
Label: EX MH23-2 O-2
Type: Outfall
ID: 51
Label: Pipe - (3)
Type: Conduit
ID: 44
Label: Pipe - (4)
Type: Conduit
ID: 40
Label: EX 66"
Type: Conduit
ID: 50
EGL
HGL
Elevation (ft)
Station (ft)
6,972.50
6,972.00
6,971.50
6,971.00
6,970.50
6,970.00
6,969.50
6,969.00
6,968.50
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20.0
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80.0
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180.0
200.0
220.0
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260.0
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360.0
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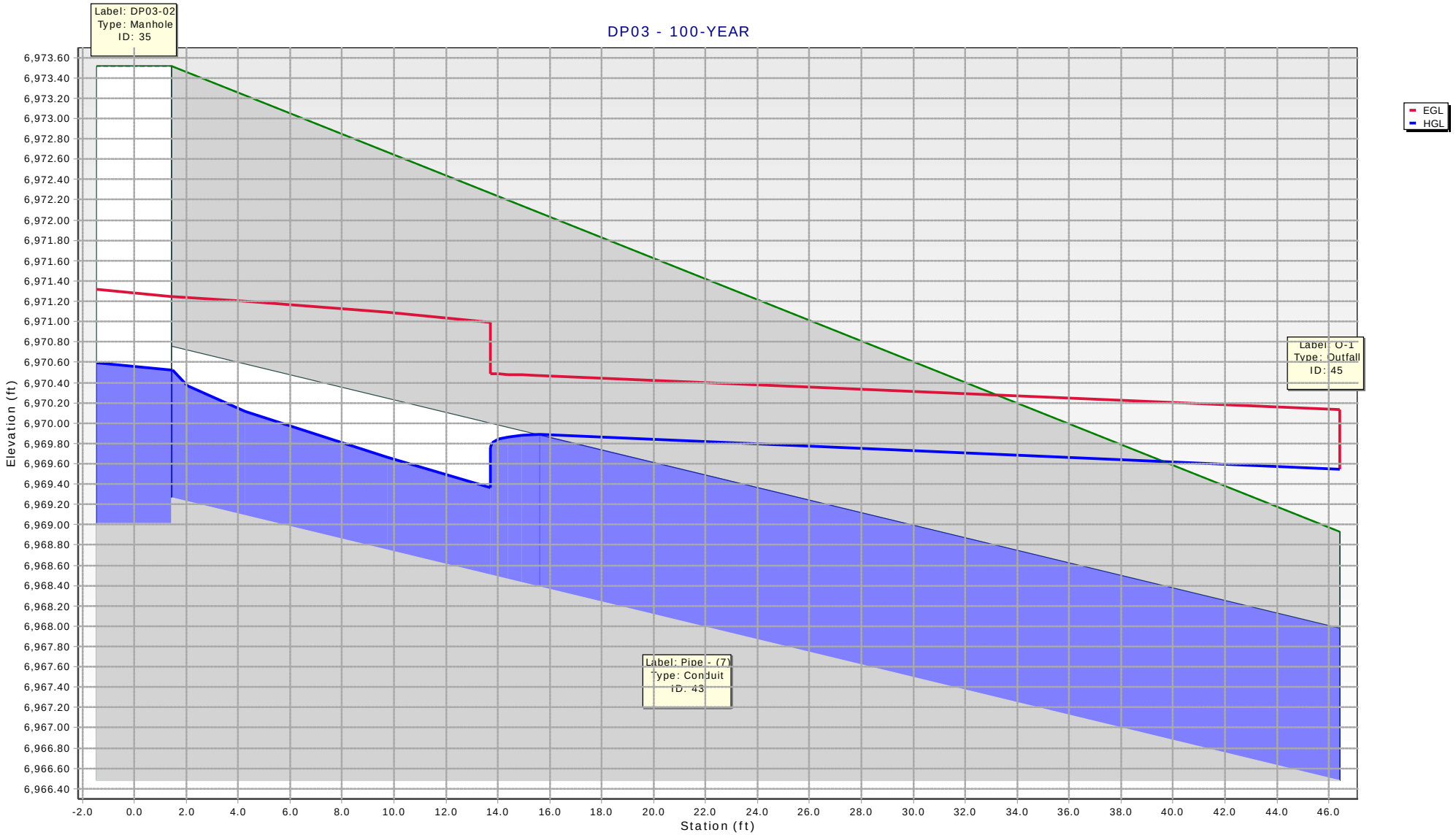
DP03 - 100-YEAR
Label: DP03-02
Type: Manhole
ID: 35
Label: O-1
Type: Outfall
ID: 45
Label: Pipe - (7)
Type: Conduit
ID: 43
EGL
HGL
Elevation (ft)
Station (ft)
6,973.60
6,973.40
6,973.20
6,973.00
6,972.80
6,972.60
6,972.40
6,972.20
6,972.00
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6,971.60
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6,966.80
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6,966.40
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2.0
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6.0
8.0
10.0
12.0
14.0
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18.0
20.0
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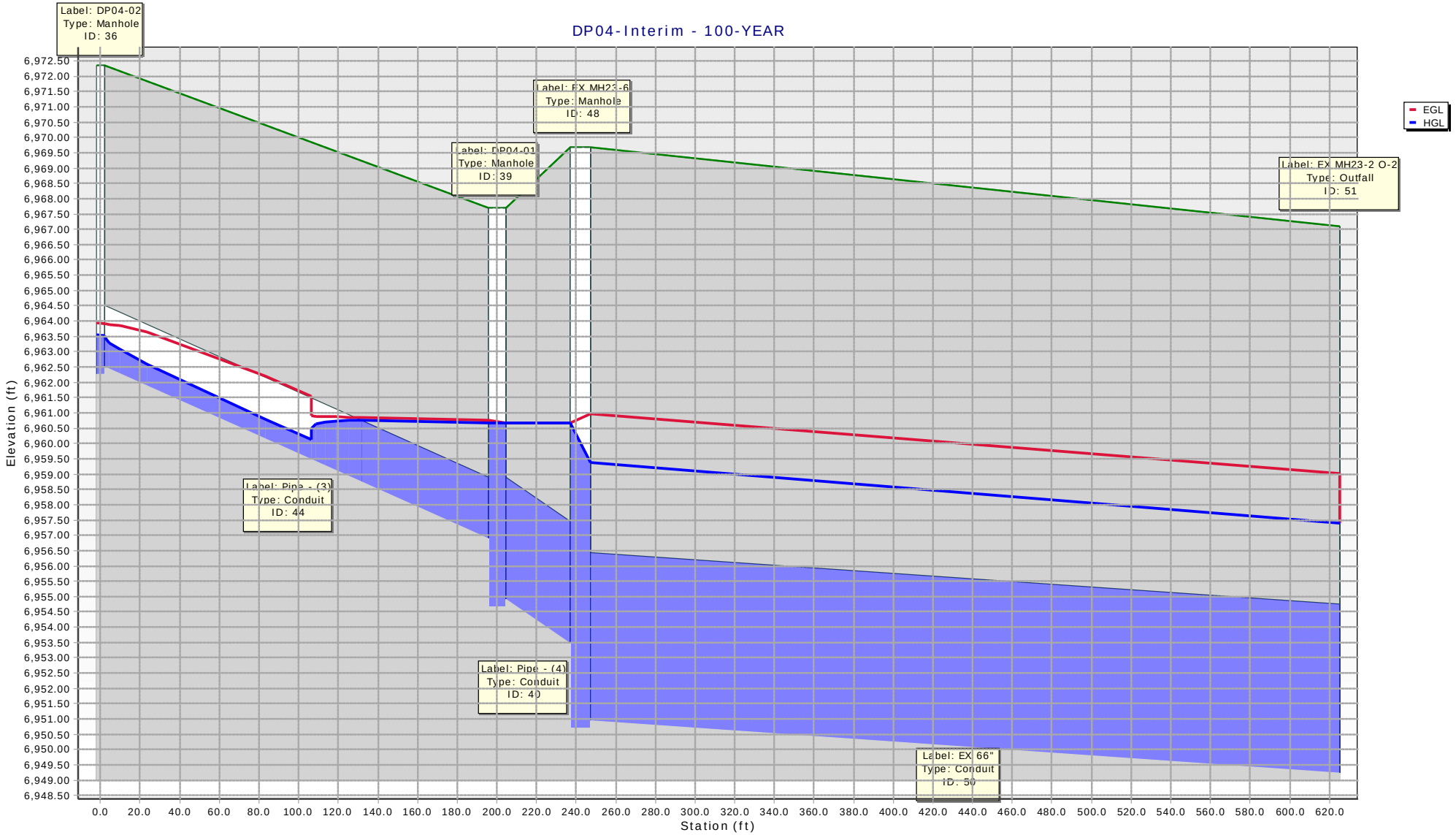
DP04-Interim - 100-YEAR
Label: DP04-02
Type: Manhole
ID: 36
Label: EX MH23-6
Type: Manhole
ID: 48
Label: DP04-01
Type: Manhole
ID: 39
Label: EX MH23-2 O-2
Type: Outfall
ID: 51
Label: Pipe - (3)
Type: Conduit
ID: 44
Label: Pipe - (4)
Type: Conduit
ID: 40
Label: EX 66"
Type: Conduit
ID: 50
EGL
HGL
Elevation (ft)
Station (ft)
6,972.50
6,972.00
6,971.50
6,971.00
6,970.50
6,970.00
6,969.50
6,969.00
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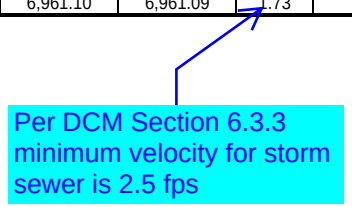
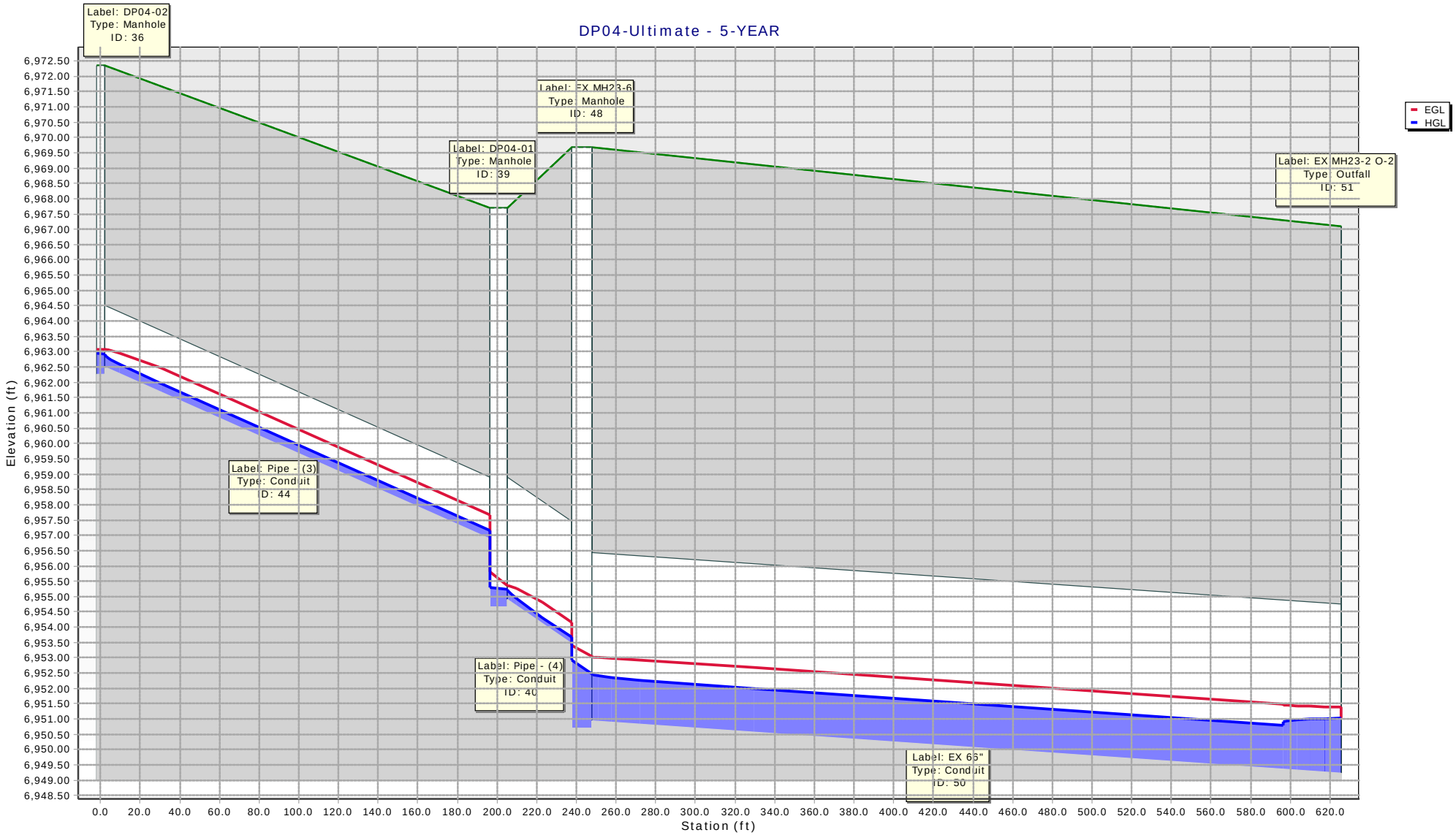
400.0
420.0
440.0
460.0
480.0
500.0
520.0
540.0
560.0
580.0
600.0
620.0

5-year Ultimate Report																	
Upstream Structure	Label	Flow (cfs)	Capacity (Full Flow) (cfs)	Diameter (in)	Manning's n	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	HGL (In) (ft)	HGL (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Velocity (ft/s)	Upstream Structure Headloss Coefficient
EX MH23-6	EX 66"	32.1	224.37	66	0.013	383	0.004	6,950.95	6,949.24	6,969.69	6,967.11	6,952.48	6,951.03	6,953.03	6,951.39	6.7	0.8
DP04-02	Pipe - (3)	1.4	37.83	24	0.013	200.7	0.028	6,962.51	6,956.90	6,972.35	6,967.70	6,962.92	6,957.16	6,963.07	6,957.67	5.74	0.1
DP04-01	Pipe - (4)	1.4	266.77	48	0.013	41.9	0.034	6,954.90	6,953.45	6,967.70	6,969.69	6,955.24	6,953.66	6,955.35	6,954.15	5.59	0.6

100-year Ultimate Report																	
Upstream Structure	Label	Flow (cfs)	Capacity (Full Flow) (cfs)	Diameter (in)	Manning's n	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	HGL (In) (ft)	HGL (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Velocity (ft/s)	Upstream Structure Headloss Coefficient
EX MH23-6	EX 66"	255.2	224.37	66	0.013	383	0.004	6,950.95	6,949.24	6,969.69	6,967.11	6,959.61	6,957.40	6,961.41	6,959.19	10.74	0.8
DP04-02	Pipe - (3)	21.8	37.83	24	0.013	200.7	0.028	6,962.51	6,956.90	6,972.35	6,967.70	6,964.18	6,961.08	6,965.12	6,961.83	12.47	0.1
DP04-01	Pipe - (4)	21.8	266.77	48	0.013	41.9	0.034	6,954.90	6,953.45	6,967.70	6,969.69	6,961.06	6,961.05	6,961.10	6,961.09	1.73	0.6

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Label: EX MH23-6
Type: Manhole
ID: 48
Label: DP04-01
Type: Manhole
ID: 39
Label: EX MH23-2 O-2
Type: Outfall
ID: 51
Label: Pipe - (3)
Type: Conduit
ID: 44
Label: Pipe - (4)
Type: Conduit
ID: 40
Label: EX 66"
Type: Conduit
ID: 50
EGL
HGL
Elevation (ft)
Station (ft)
6,972.50
6,972.00
6,971.50
6,971.00
6,970.50
6,970.00
6,969.50
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540.0
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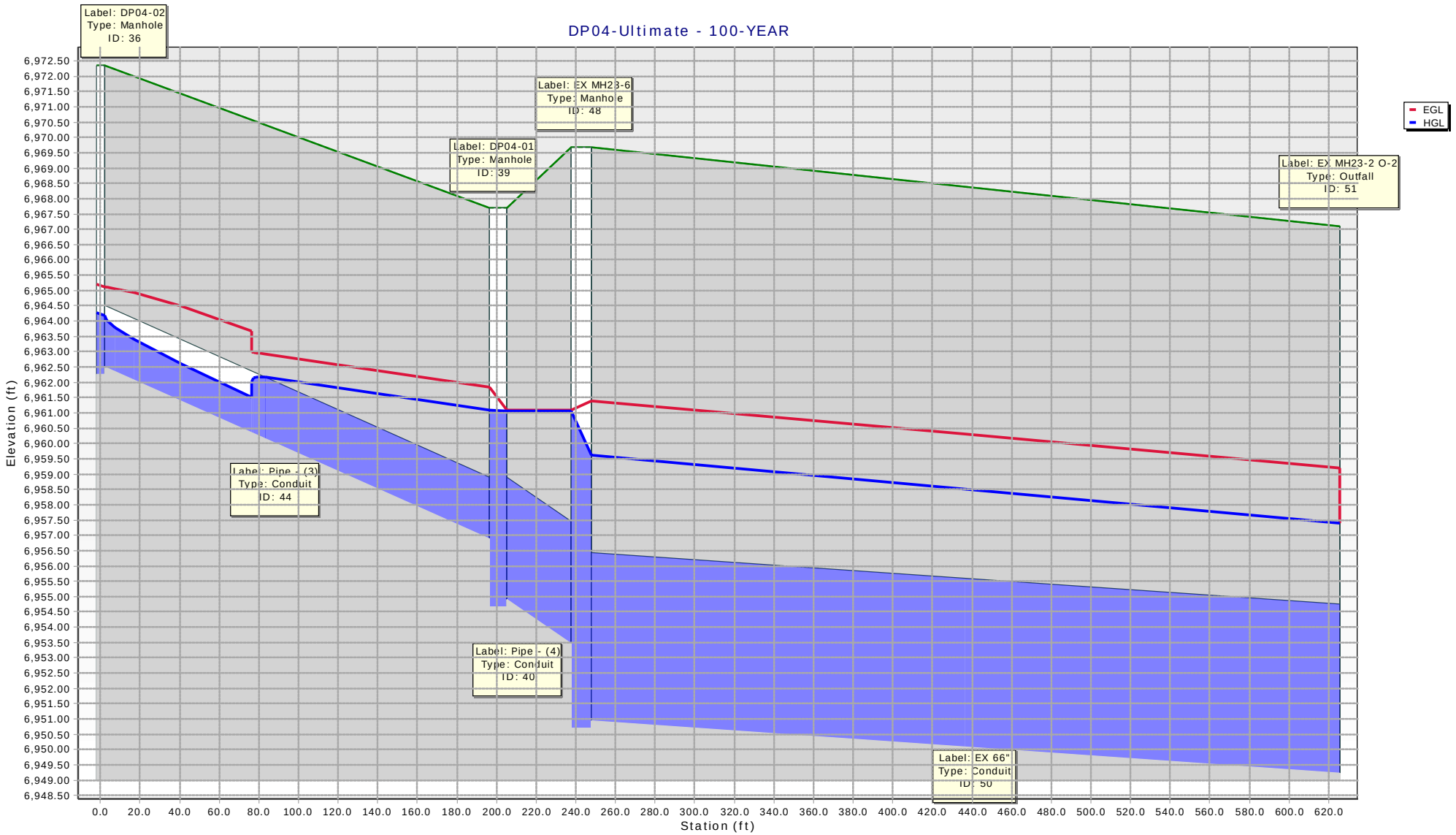
600.0
620.0


DP04-Ultimate - 100-YEAR
Label: DP04-02
Type: Manhole
ID: 36
Label: EX MH23-6
Type: Manhole
ID: 48
Label: DP04-01
Type: Manhole
ID: 39
Label: EX MH23-2 O-2
Type: Outfall
ID: 51
Label: Pipe - (3)
Type: Conduit
ID: 44
Label: Pipe - (4)
Type: Conduit
ID: 40
Label: EX 66"
Type: Conduit
ID: 50
EGL
HGL
Elevation (ft)
Station (ft)
6,972.50
6,972.00
6,971.50
6,971.00
6,970.50
6,970.00
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6,969.00
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220.0
240.0
260.0
280.0
300.0
320.0
340.0
360.0
380.0
400.0
420.0
440.0
460.0
480.0
500.0
520.0
540.0
560.0
580.0
600.0
620.0

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018) **Sheet 1 of 3**

Designer: Gabe Gonzales
Company: JR Engineering
Date: July 20, 2023
Project: Sterling Ranch Recycling Facility
Location: West Forebay

1. Basin Storage Volume

A) Effective Imperviousness of Tributary Area, I_a — I_a = 11.0 %

B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$) — i = 0.110

C) Contributing Watershed Area — Area = 34.490 ac

D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm — d_6 = ____ in

E) Design Concept (Select EURV when also designing for flood control)

Choose One
- ○ Water Quality Capture Volume (WQCV)
- ◉ Excess Urban Runoff Volume (EURV)

F) Design Volume (WQCV) Based on 40-hour Drain Time
($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area$) — V_{DESIGN} = 0.209 ac-ft

G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))$) — $V_{DESIGN\ OTHER}$ = ____ ac-ft

H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired) — $V_{DESIGN\ USER}$ = ____ ac-ft

I) NRCS Hydrologic Soil Groups of Tributary Watershed
- i) Percentage of Watershed consisting of Type A Soils — HSG_A = 100 %
- ii) Percentage of Watershed consisting of Type B Soils — HSG_B = 0 %
- iii) Percentage of Watershed consisting of Type C/D Soils — $HSG_{C/D}$ = 0 %

J) Excess Urban Runoff Volume (EURV) Design Volume
For HSG A: $EURV_A = 1.68 * i^{1.28}$
For HSG B: $EURV_B = 1.36 * i^{1.08}$
For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$
— $EURV_{DESIGN}$ = 0.286 ac-ft

K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired) — $EURV_{DESIGN\ USER}$ = ____ ac-ft

2. Basin Shape: Length to Width Ratio
(A basin length to width ratio of at least 2:1 will improve TSS reduction.) — L : W = 9.0 : 1

3. Basin Side Slopes

A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred) — Z = 4.00 ft / ft

4. Inlet

A) Describe means of providing energy dissipation at concentrated inflow locations:

5. Forebay

A) Minimum Forebay Volume (V_{FMIN} = 2% of the WQCV) — V_{FMIN} = 0.004 ac-ft

B) Actual Forebay Volume — V_F = 0.005 ac-ft

C) Forebay Depth (D_F = 18 inch maximum) — D_F = 18.0 in

D) Forebay Discharge

i) Undetained 100-year Peak Discharge — Q_{100} = 42.00 cfs

ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$) — Q_F = 0.84 cfs

E) Forebay Discharge Design

Choose One
- ○ Berm With Pipe
- ○ Wall with Rect. Notch
- ○ Wall with V-Notch Weir

Flow too small for berm w/ pipe

F) Discharge Pipe Size (minimum 8-inches) — Calculated D_P = ____ in

G) Rectangular Notch Width — Calculated W_N = ____ in

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018) **Sheet 1 of 3**

Designer: Gabe Gonzales
Company: JR Engineering
Date: July 20, 2023
Project: Sterling Ranch Recycling Facility
Location: North Forebay

1. Basin Storage Volume

A) Effective Imperviousness of Tributary Area, I_a — I_a = 13.0 %

B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$) — i = 0.130

C) Contributing Watershed Area — Area = 5.180 ac

D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm — d_6 = ____ in

E) Design Concept (Select EURV when also designing for flood control)

Choose One
- ○ Water Quality Capture Volume (WQCV)
- ◉ Excess Urban Runoff Volume (EURV)

F) Design Volume (WQCV) Based on 40-hour Drain Time
($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area$) — V_{DESIGN} = 0.036 ac-ft

G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))$) — $V_{DESIGN\ OTHER}$ = ____ ac-ft

H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired) — $V_{DESIGN\ USER}$ = ____ ac-ft

I) NRCS Hydrologic Soil Groups of Tributary Watershed
- i) Percentage of Watershed consisting of Type A Soils — HSG_A = 100 %
- ii) Percentage of Watershed consisting of Type B Soils — HSG_B = 0 %
- iii) Percentage of Watershed consisting of Type C/D Soils — $HSG_{C/D}$ = 0 %

J) Excess Urban Runoff Volume (EURV) Design Volume
For HSG A: $EURV_A = 1.68 * i^{1.28}$
For HSG B: $EURV_B = 1.36 * i^{1.08}$
For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$
— $EURV_{DESIGN}$ = 0.053 ac-ft

K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired) — $EURV_{DESIGN\ USER}$ = ____ ac-ft

2. Basin Shape: Length to Width Ratio

(A basin length to width ratio of at least 2:1 will improve TSS reduction.) — L : W = 9.0 : 1

3. Basin Side Slopes

A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred) — Z = 4.00 ft / ft

4. Inlet

A) Describe means of providing energy dissipation at concentrated inflow locations:

5. Forebay

A) Minimum Forebay Volume (V_{FMIN} = 0% of the WQCV) — V_{FMIN} = 0.000 ac-ft — **A FOREBAY MAY NOT BE NECESSARY FOR THIS SIZE SITE**

B) Actual Forebay Volume — V_F = ____ ac-ft

C) Forebay Depth (D_F = 12 inch maximum) — D_F = 12.0 in

D) Forebay Discharge
- i) Undetained 100-year Peak Discharge — Q_{100} = 11.00 cfs
- ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$) — Q_F = 0.22 cfs

Under the required effective impervious, sized for minimum volume constraints.
V_{Design} = 0.036 ac-ft
$V_{Required}$ = 1% of WQCV = **16 ft³**
$V_{Provided}$ = **46 ft³**

E) Forebay Discharge Design

Choose One
- ○ Berm With Pipe
- ○ Wall with Rect. Notch
- ○ Wall with V-Notch Weir

Flow too small for berm w/ pipe

F) Discharge Pipe Size (minimum 8-inches) — Calculated D_P = ____ in

G) Rectangular Notch Width — Calculated W_N = ____ in

Weir Report

West Forebay Interim Release Rate

Compound Weir

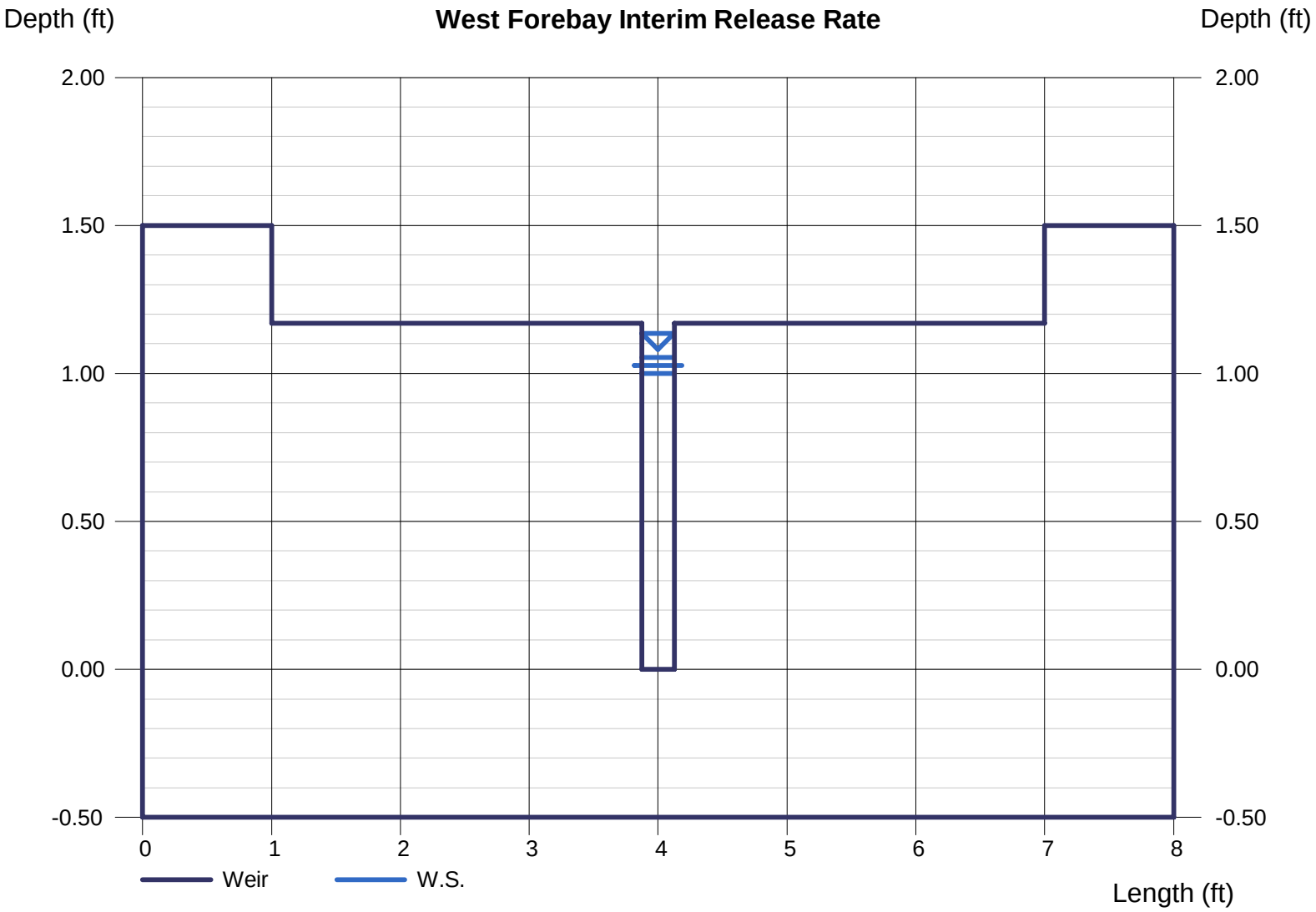
Crest	= Sharp
Bottom Length (ft)	= 6.00
Total Depth (ft)	= 1.50
Length, x (ft)	= 0.25
Depth, a (ft)	= 1.17

Highlighted

Depth (ft)	= 1.05
Q (cfs)	= 0.900
Area (sqft)	= 0.26
Velocity (ft/s)	= 3.42
Top Width (ft)	= 0.25

Calculations

Weir Coeff. Cw	= 3.33
Compute by:	Known Q
Known Q (cfs)	= 0.90



Weir Report

North Forebay Interim Release Rate

Compound Weir

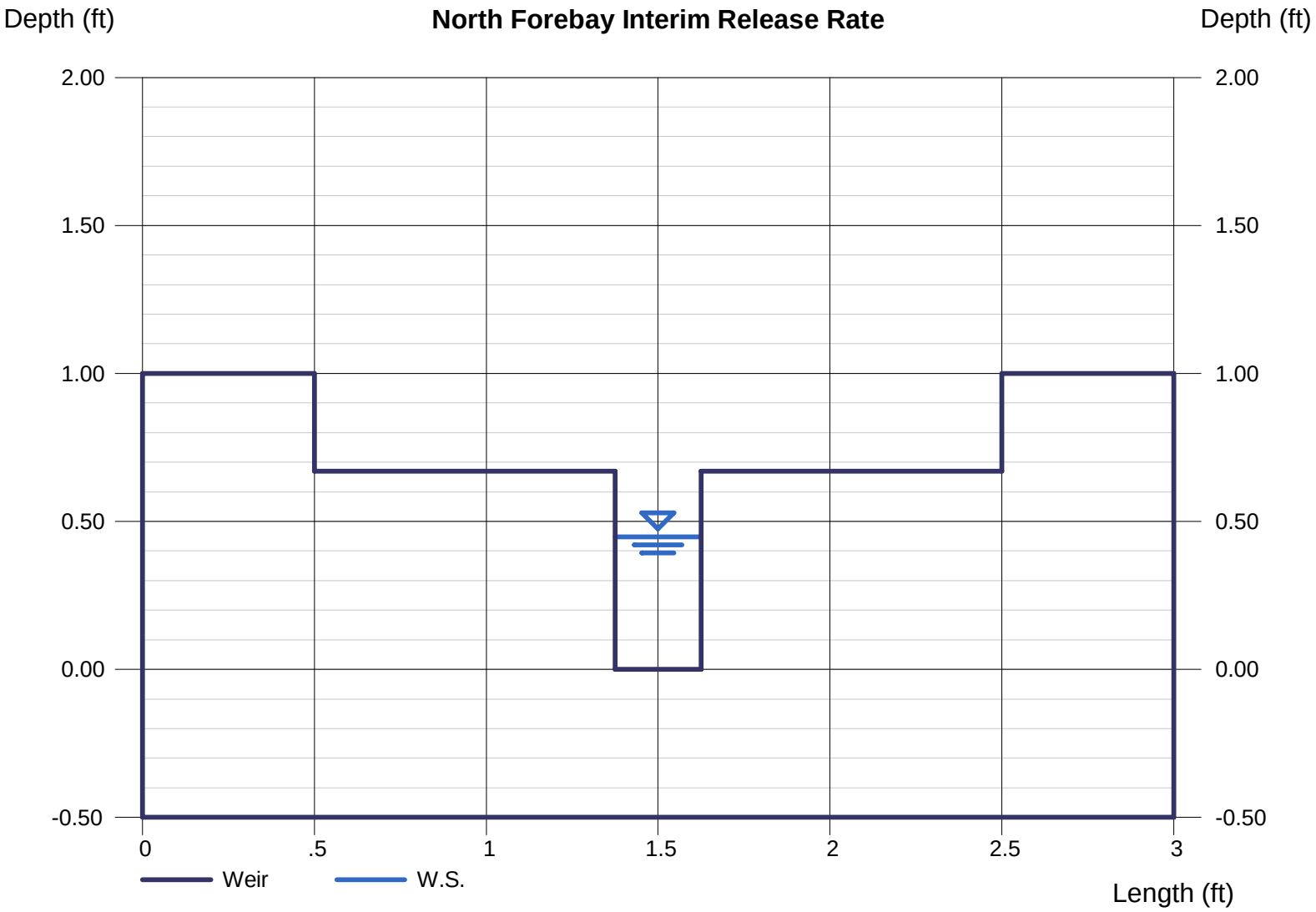
Crest	= Sharp
Bottom Length (ft)	= 2.00
Total Depth (ft)	= 1.00
Length, x (ft)	= 0.25
Depth, a (ft)	= 0.67

Highlighted

Depth (ft)	= 0.45
Q (cfs)	= 0.250
Area (sqft)	= 0.11
Velocity (ft/s)	= 2.23
Top Width (ft)	= 0.25

Calculations

Weir Coeff. Cw	= 3.33
Compute by:	Known Q
Known Q (cfs)	= 0.25



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Monday, Jul 31 2023

Trickle Channel Capacity-Interim

What about calcs for the 2ft wide trickle channel?

Rectangular

Bottom Width (ft)	= 6.00
Total Depth (ft)	= 0.50
Invert Elev (ft)	= 100.00
Slope (%)	= 0.50
N-Value	= 0.013

Calculations

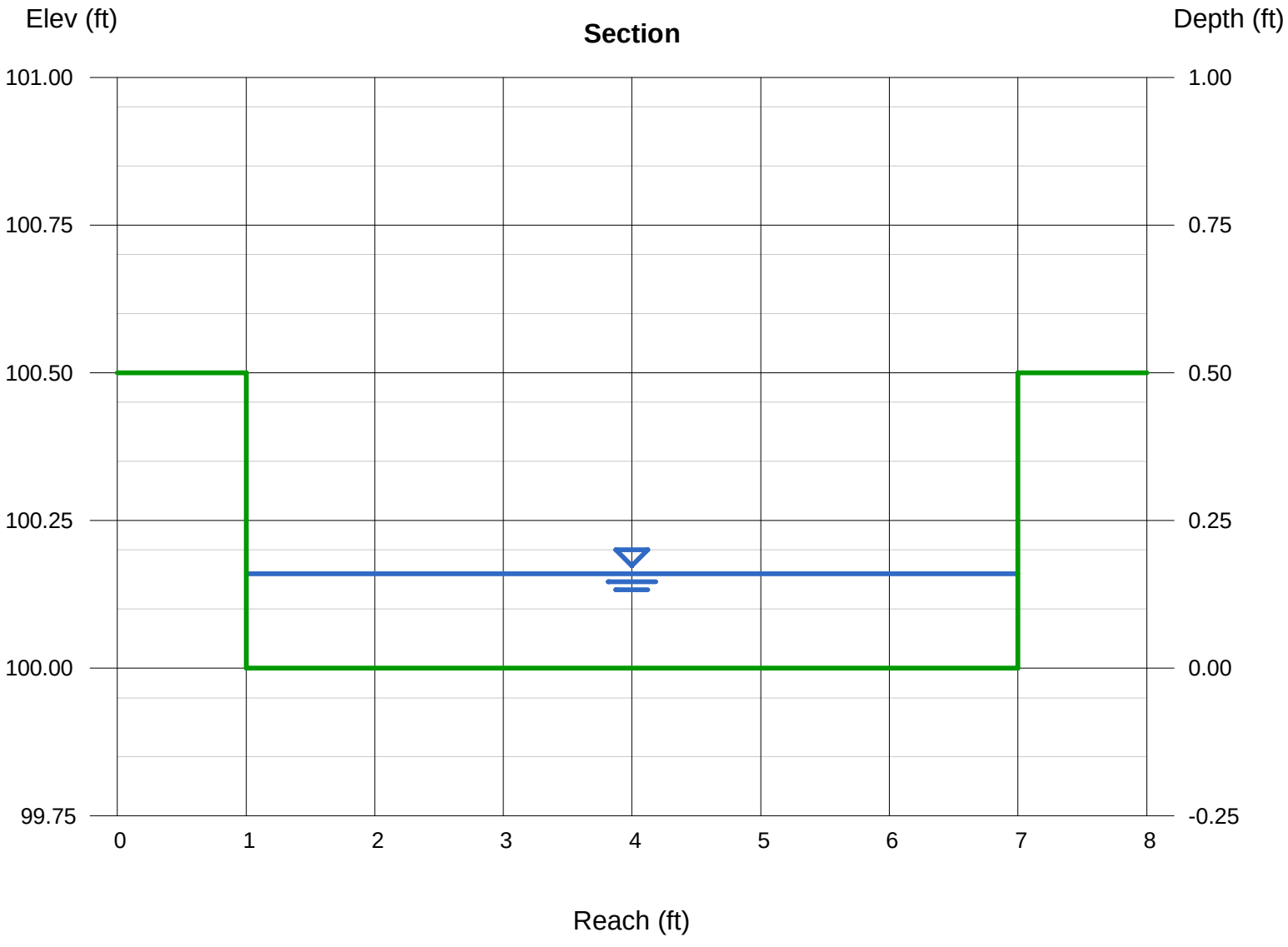
Compute by:	Known Q
Known Q (cfs)	= 2.00

Highlighted

Depth (ft)	= 0.16
Q (cfs)	= 2.000
Area (sqft)	= 0.96
Velocity (ft/s)	= 2.08
Wetted Perim (ft)	= 6.32
Crit Depth, Yc (ft)	= 0.16
Top Width (ft)	= 6.00
EGL (ft)	= 0.23

Interim Peak Inflow= 50.5 cfs

2% of Q_{100} = 51 * 0.02 = **1.0 cfs**
Double Value = 1.0 * 2 = **2.0 cfs**



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Trickle Channel Capacity-Ultimate

What about calcs for the 2ft wide trickle channel?

Rectangular

Bottom Width (ft)	= 6.00
Total Depth (ft)	= 0.50
Invert Elev (ft)	= 100.00
Slope (%)	= 0.50
N-Value	= 0.013

Calculations

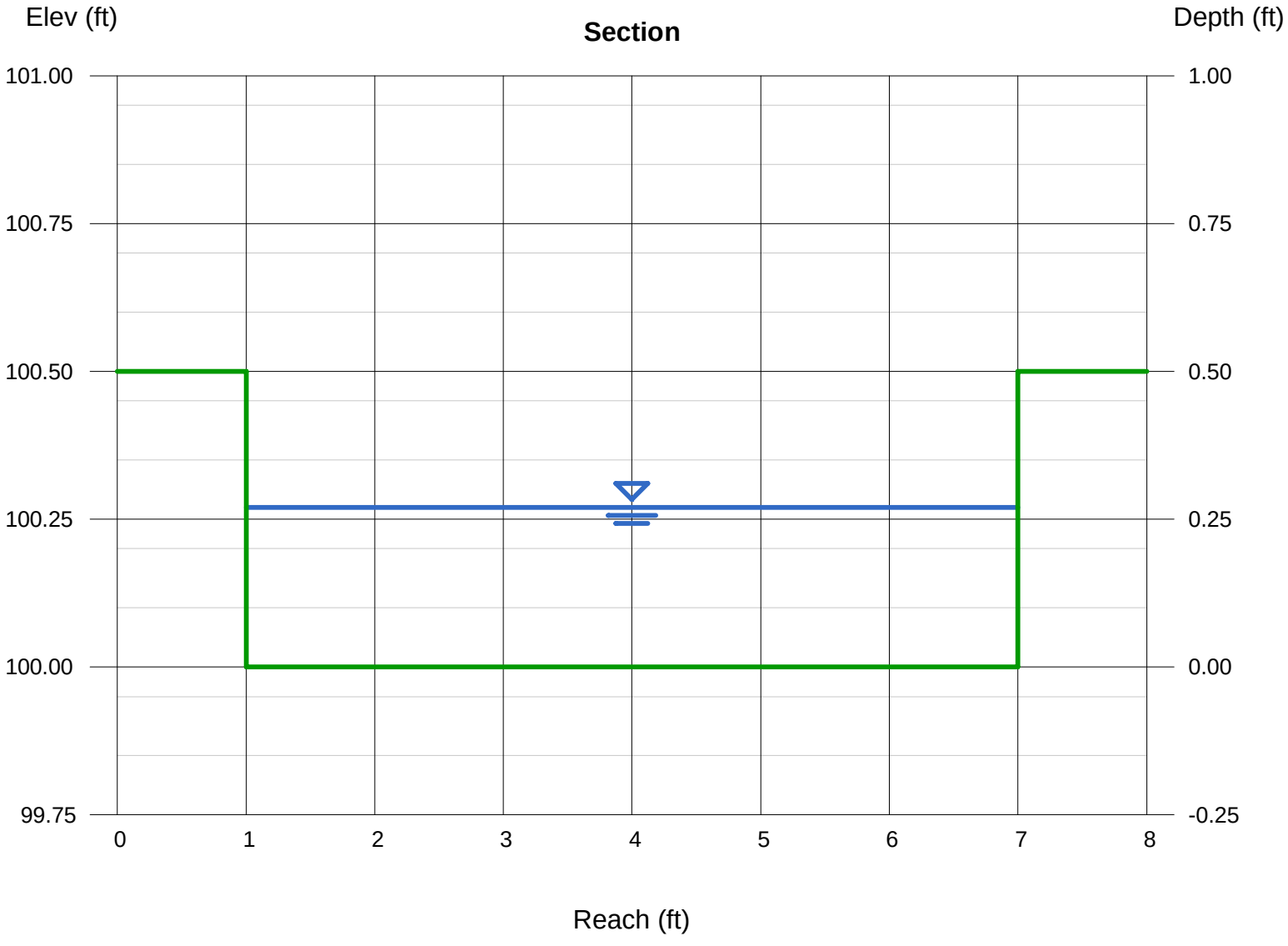
Compute by:	Known Q
Known Q (cfs)	= 5.00

Highlighted

Depth (ft)	= 0.27
Q (cfs)	= 5.000
Area (sqft)	= 1.62
Velocity (ft/s)	= 3.09
Wetted Perim (ft)	= 6.54
Crit Depth, Yc (ft)	= 0.28
Top Width (ft)	= 6.00
EGL (ft)	= 0.42

Ultimate Peak Inflow= 123.1 cfs

2% of Q_{100} = 125 * 0.02 = **2.5 cfs**
Double Value = 2.5 * 2 = **5.0 cfs**

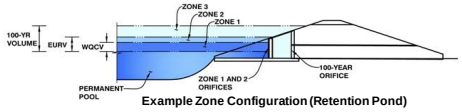


DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Sterling Ranch Recycling Facility

Basin ID: Pond A-Interim



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	42.29	acres
Watershed Length =	2,265	ft
Watershed Length to Centroid =	1,455	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	11.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

			Optional User Overrides
Water Quality Capture Volume (WQCV) =	0.256	acre-feet	acre-feet
Excess Urban Runoff Volume (EURV) =	0.351	acre-feet	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.181	acre-feet	1.19 inches
5-yr Runoff Volume (P1 = 1.5 in.) =	0.298	acre-feet	1.50 inches
10-yr Runoff Volume (P1 = 1.75 in.) =	0.397	acre-feet	1.75 inches
25-yr Runoff Volume (P1 = 2 in.) =	0.979	acre-feet	2.00 inches
50-yr Runoff Volume (P1 = 2.25 in.) =	1.558	acre-feet	2.25 inches
100-yr Runoff Volume (P1 = 2.52 in.) =	2.370	acre-feet	2.52 inches
500-yr Runoff Volume (P1 = 3.14 in.) =	4.158	acre-feet	inches
Approximate 2-yr Detention Volume =	0.211	acre-feet	
Approximate 5-yr Detention Volume =	0.289	acre-feet	
Approximate 10-yr Detention Volume =	0.379	acre-feet	
Approximate 25-yr Detention Volume =	0.510	acre-feet	
Approximate 50-yr Detention Volume =	0.674	acre-feet	
Approximate 100-yr Detention Volume =	1.062	acre-feet	

Define Zones and Basin Geometry

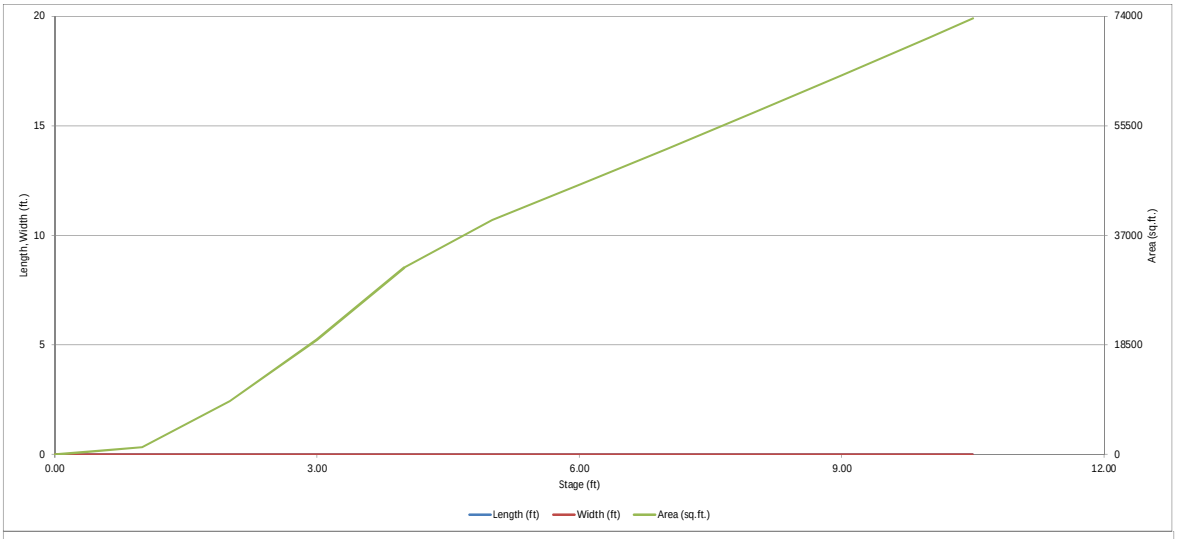
Zone 1 Volume (WQCV) =	0.256	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.095	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.711	acre-feet
Total Detention Basin Volume =	1.062	acre-feet
Initial Surcharge Volume (ISV) =	user	ft^3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio (R_{LW}) =	user	
Initial Surcharge Area (A_{ISV}) =	user	ft^2
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft^2
Volume of Basin Floor (V_{FLOOR}) =	user	ft^3
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft^2
Volume of Main Basin (V_{MAIN}) =	user	ft^3
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

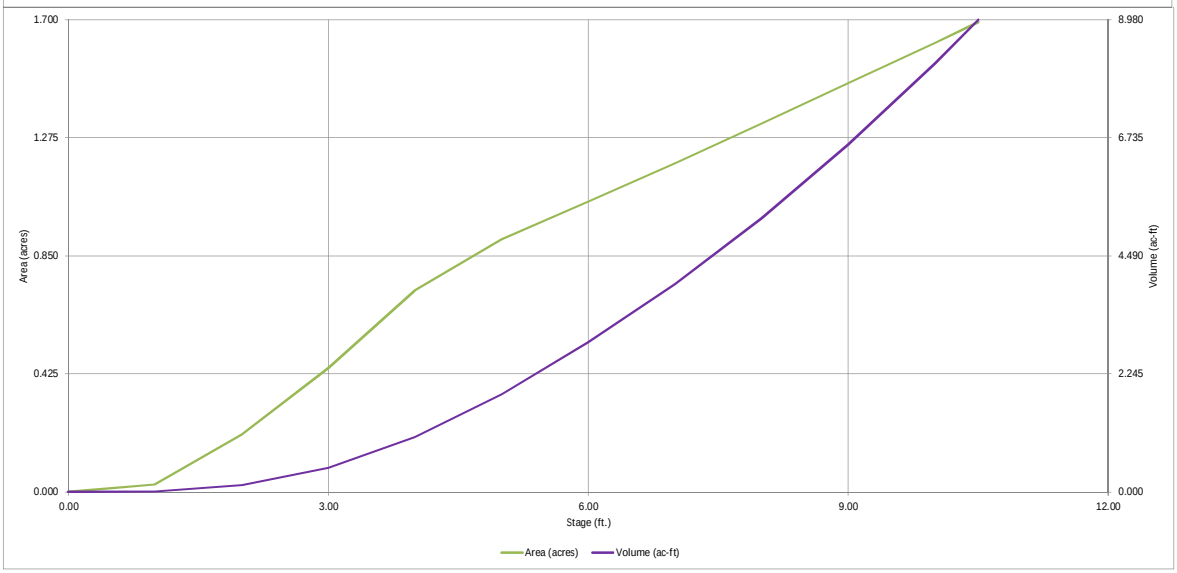
Depth Increment = ft

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Optional Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	10	0.000		
6966	--	1.00	--	--	--	1,237	0.028	623	0.014
6967	--	2.00	--	--	--	9,028	0.207	5,756	0.132
6968	--	3.00	--	--	--	19,414	0.446	19,977	0.459
6969	--	4.00	--	--	--	31,638	0.726	45,503	1.045
6970	--	5.00	--	--	--	39,589	0.909	81,116	1.862
6971	--	6.00	--	--	--	45,537	1.045	123,679	2.839
6972	--	7.00	--	--	--	51,596	1.184	172,246	3.954
6973	--	8.00	--	--	--	57,766	1.326	226,927	5.210
6974 (Crest)	--	9.00	--	--	--	64,047	1.470	287,833	6.608
6975	--	10.00	--	--	--	70,449	1.617	355,081	8.152
6975.5	--	10.50	--	--	--	73,681	1.691	391,114	8.979

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



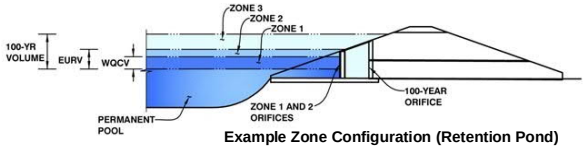


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: Sterling Ranch Recycling Facility

Basin ID: Pond A-Interim



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.48	0.256	Orifice Plate
Zone 2 (EURV)	2.75	0.095	Rectangular Orifice
Zone 3 (100-year)	4.03	0.711	Weir&Pipe (Restrict)
Total (all zones)		1.062	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft^2
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	N/A	ft^2
Depth at top of Zone using Orifice Plate =	2.75	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	sq. inches	Elliptical Slot Area =	N/A	ft^2

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00						
Orifice Area (sq. inches)	1.00	1.10						

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected			Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice =	2.80	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	1.75	N/A	ft^2
Depth at top of Zone using Vertical Orifice =	4.55	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.88	N/A	feet
Vertical Orifice Height =	21.00	N/A	inches				
Vertical Orifice Width =	12.00		inches				

Calculated Parameters for Vertical Orifice

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	7.35	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =	7.35	N/A	feet
Overflow Weir Front Edge Length =	4.00	N/A	feet	Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	4.03	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet	Overflow Grate Open Area w/o Debris =	12.66	N/A	ft^2
Overflow Grate Type =	Close Mesh Grate	N/A		Overflow Grate Open Area w/ Debris =	6.33	N/A	ft^2
Debris Clogging % =	50%	N/A	%				

Calculated Parameters for Overflow Weir

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	3.14	N/A	ft^2
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	1.00	N/A	feet
Restrictor Plate Height Above Pipe Invert =	24.00		inches	Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	9.00	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.48	feet
Spillway Crest Length =	120.00	feet	Stage at Top of Freeboard =	10.48	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	1.69	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	8.94	acre-ft

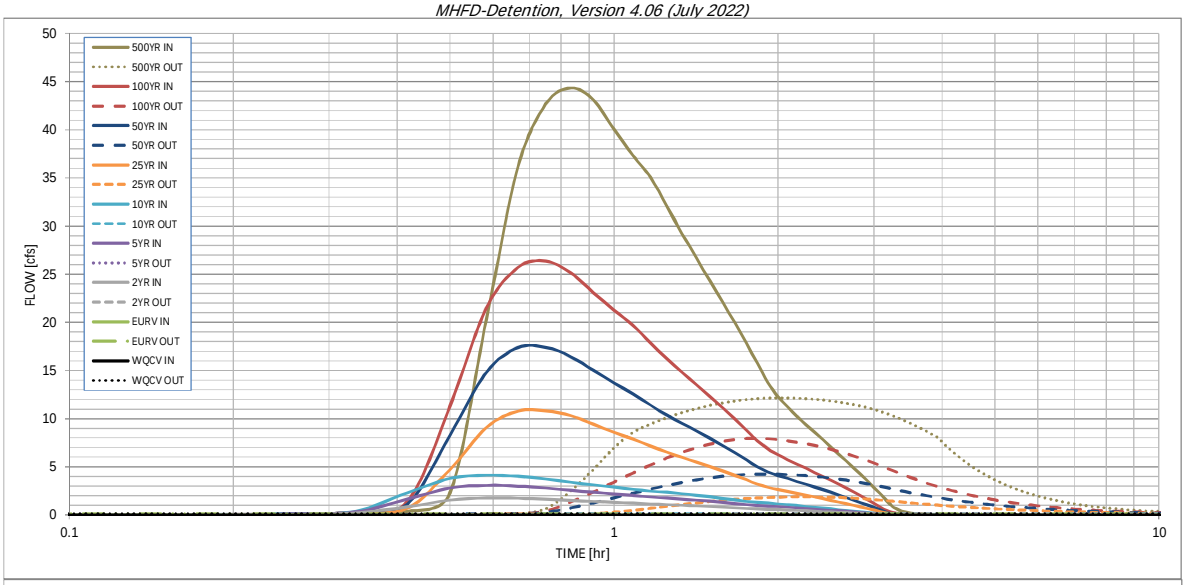
Calculated Parameters for Spillway

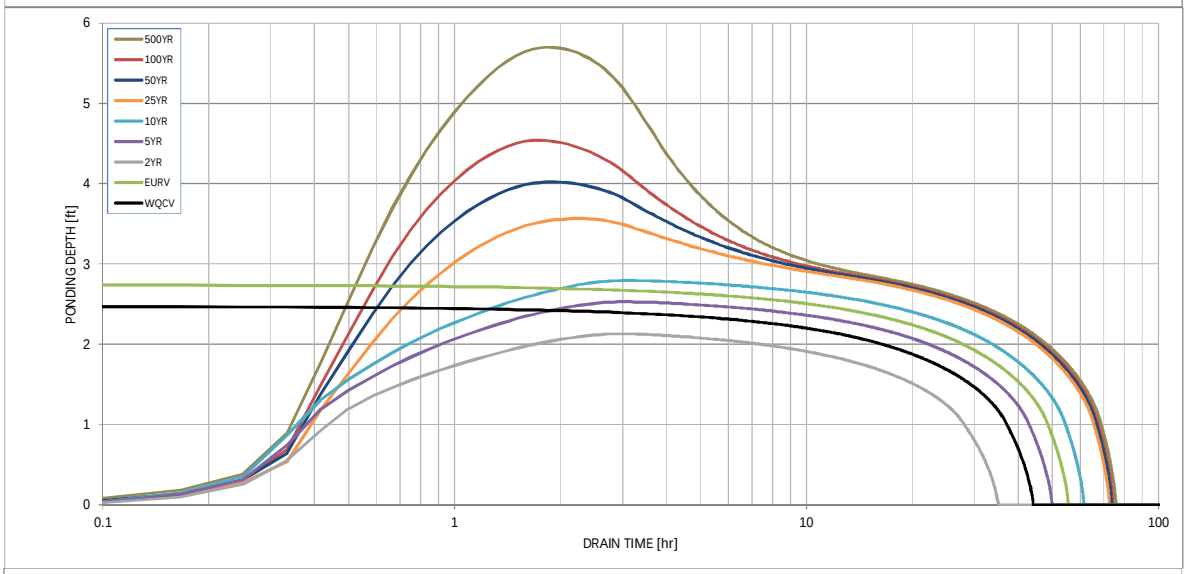
Routed Hydrograph Results *The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

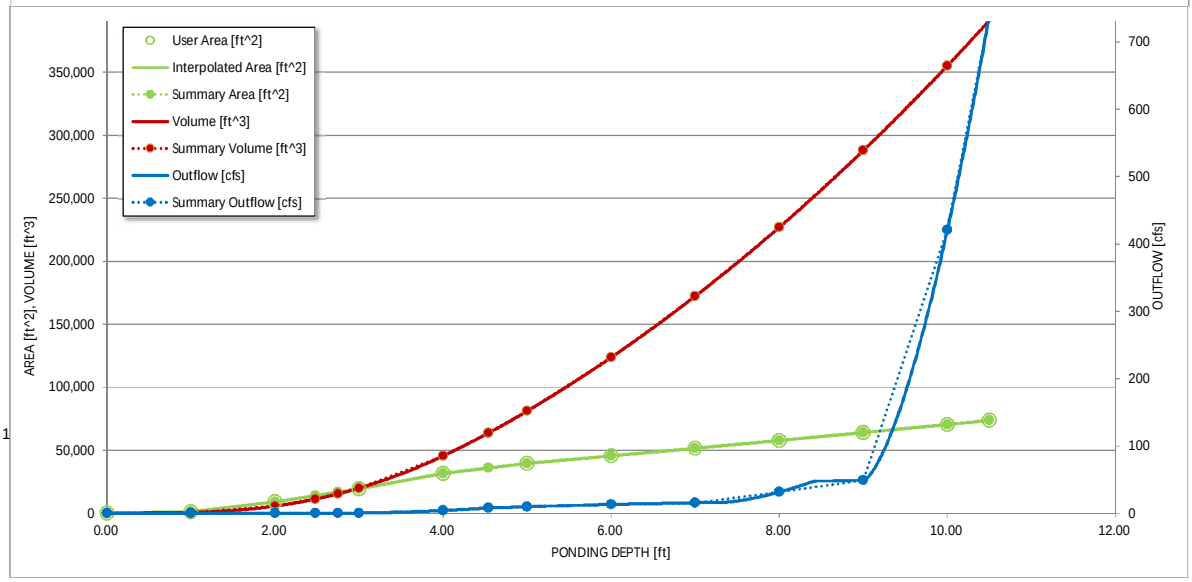
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.256	0.351	0.181	0.298	0.397	0.979	1.558	2.370	4.158
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.181	0.298	0.397	0.979	1.558	2.370	4.158
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.3	0.5	0.7	6.4	12.8	21.4	39.0
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.30	0.51	0.92
Peak Inflow Q (cfs) =	N/A	N/A	1.8	3.1	4.1	10.8	17.4	26.4	44.4
Peak Outflow Q (cfs) =	0.1	0.1	0.1	0.1	0.1	1.9	4.2	8.0	12.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.1	0.3	0.3	0.4	0.3
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	ertical Orifice
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	40	50	32	45	55	62	60	56	49
Time to Drain 99% of Inflow Volume (hours) =	42	53	34	48	59	67	66	65	63
Maximum Ponding Depth (ft) =	2.48	2.75	2.13	2.53	2.79	3.56	4.02	4.54	5.70
Area at Maximum Ponding Depth (acres) =	0.32	0.39	0.24	0.33	0.40	0.60	0.73	0.82	1.00
Maximum Volume Stored (acre-ft) =	0.259	0.355	0.159	0.272	0.370	0.752	1.059	1.463	2.532

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)







S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.02
	0:15:00	0.00	0.00	0.05	0.09	0.11	0.07	0.09	0.09	0.14
	0:20:00	0.00	0.00	0.22	0.29	0.35	0.22	0.26	0.28	0.37
	0:25:00	0.00	0.00	0.83	1.62	2.28	0.68	1.08	1.33	2.30
	0:30:00	0.00	0.00	1.54	2.80	3.78	4.72	8.32	11.31	20.33
	0:35:00	0.00	0.00	1.76	3.07	4.12	9.09	14.81	21.51	36.18
	0:40:00	0.00	0.00	1.74	2.99	4.01	10.78	17.39	25.70	42.69
	0:45:00	0.00	0.00	1.65	2.79	3.73	10.81	17.40	26.35	44.35
	0:50:00	0.00	0.00	1.52	2.55	3.39	10.30	16.44	25.12	43.09
	0:55:00	0.00	0.00	1.40	2.35	3.12	9.41	15.01	23.08	40.05
	1:00:00	0.00	0.00	1.31	2.18	2.89	8.57	13.71	21.26	37.33
	1:05:00	0.00	0.00	1.22	2.01	2.66	7.87	12.57	19.68	35.08
	1:10:00	0.00	0.00	1.14	1.87	2.47	7.16	11.41	17.89	32.09
	1:15:00	0.00	0.00	1.06	1.75	2.35	6.51	10.37	16.22	29.21
	1:20:00	0.00	0.00	1.00	1.64	2.21	5.97	9.50	14.81	26.68
	1:25:00	0.00	0.00	0.93	1.53	2.05	5.49	8.72	13.53	24.31
	1:30:00	0.00	0.00	0.87	1.42	1.89	5.02	7.95	12.31	22.08
	1:35:00	0.00	0.00	0.80	1.30	1.72	4.56	7.20	11.13	19.94
	1:40:00	0.00	0.00	0.74	1.18	1.56	4.10	6.45	9.97	17.84
	1:45:00	0.00	0.00	0.68	1.06	1.40	3.65	5.71	8.81	15.77
	1:50:00	0.00	0.00	0.63	0.97	1.29	3.21	4.99	7.70	13.78
	1:55:00	0.00	0.00	0.60	0.91	1.21	2.87	4.46	6.85	12.29
	2:00:00	0.00	0.00	0.56	0.86	1.14	2.64	4.10	6.25	11.20
	2:05:00	0.00	0.00	0.52	0.80	1.06	2.44	3.78	5.75	10.25
	2:10:00	0.00	0.00	0.47	0.73	0.97	2.24	3.48	5.28	9.39
	2:15:00	0.00	0.00	0.43	0.66	0.88	2.05	3.19	4.84	8.58
	2:20:00	0.00	0.00	0.39	0.60	0.79	1.87	2.90	4.41	7.80
	2:25:00	0.00	0.00	0.35	0.54	0.71	1.69	2.63	3.99	7.05
	2:30:00	0.00	0.00	0.31	0.48	0.63	1.52	2.35	3.58	6.34
	2:35:00	0.00	0.00	0.27	0.42	0.55	1.35	2.08	3.18	5.63
	2:40:00	0.00	0.00	0.24	0.36	0.48	1.18	1.82	2.78	4.93
	2:45:00	0.00	0.00	0.20	0.31	0.40	1.01	1.55	2.38	4.24
	2:50:00	0.00	0.00	0.17	0.25	0.33	0.84	1.29	1.98	3.54
	2:55:00	0.00	0.00	0.14	0.20	0.26	0.68	1.03	1.59	2.85
	3:00:00	0.00	0.00	0.11	0.15	0.19	0.51	0.77	1.19	2.16
	3:05:00	0.00	0.00	0.08	0.10	0.13	0.35	0.51	0.80	1.47
	3:10:00	0.00	0.00	0.06	0.08	0.10	0.20	0.27	0.43	0.84
	3:15:00	0.00	0.00	0.05	0.06	0.08	0.11	0.15	0.23	0.51
	3:20:00	0.00	0.00	0.04	0.05	0.07	0.08	0.10	0.15	0.33
	3:25:00	0.00	0.00	0.04	0.05	0.06	0.06	0.08	0.10	0.22
	3:30:00	0.00	0.00	0.03	0.04	0.05	0.05	0.06	0.08	0.15
	3:35:00	0.00	0.00	0.03	0.03	0.04	0.04	0.05	0.05	0.10
	3:40:00	0.00	0.00	0.02	0.03	0.04	0.03	0.04	0.04	0.06
	3:45:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	3:50:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	3:55:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	4:00:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	4:05:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	4:10:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	4:15:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft²]	Area [acres]	Volume [ft³]	Volume [ac-ft]	Total Outflow [cfs]
6965-Top of Micropool	0.00	10	0.000	0	0.000	0.00
6966	1.00	1,237	0.028	623	0.014	0.03
6967	2.00	9,028	0.207	5,756	0.132	0.08
6967.48-WQCV WSEL	2.48	14,013	0.322	11,286	0.259	0.10
6967.75-EURV WSEL	2.75	16,817	0.386	15,448	0.355	0.10
6968	3.00	19,414	0.446	19,977	0.459	0.27
6969	4.00	31,638	0.726	45,503	1.045	4.11
6969.54-100 yr WSEL	4.54	35,932	0.825	63,747	1.463	7.94
6970	5.00	39,589	0.909	81,116	1.862	9.85
6971	6.00	45,537	1.045	123,679	2.839	13.01
6972	7.00	51,596	1.184	172,246	3.954	15.54
6973	8.00	57,766	1.326	226,927	5.210	31.64
6974-Spillway Crest	9.00	64,047	1.470	287,833	6.608	49.02
6975	10.00	70,449	1.617	355,081	8.152	420.90
6976-Top of Pond	10.50	73,681	1.691	391,114	8.979	740.22

For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

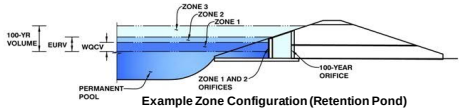
Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Sterling Ranch Recycling Facility

Basin ID: Pond A-Ultimate



Example Zone Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	44.16	acres
Watershed Length =	2,265	ft
Watershed Length to Centroid =	1,455	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	73.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

			Optional User Overrides
Water Quality Capture Volume (WQCV) =	1.064	acre-feet	acre-feet
Excess Urban Runoff Volume (EURV) =	4.132	acre-feet	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	3.020	acre-feet	1.19 inches
5-yr Runoff Volume (P1 = 1.5 in.) =	3.935	acre-feet	1.50 inches
10-yr Runoff Volume (P1 = 1.75 in.) =	4.670	acre-feet	1.75 inches
25-yr Runoff Volume (P1 = 2 in.) =	5.573	acre-feet	2.00 inches
50-yr Runoff Volume (P1 = 2.25 in.) =	6.455	acre-feet	2.25 inches
100-yr Runoff Volume (P1 = 2.52 in.) =	7.502	acre-feet	2.52 inches
500-yr Runoff Volume (P1 = 3.14 in.) =	9.804	acre-feet	inches
Approximate 2-yr Detention Volume =	2.702	acre-feet	
Approximate 5-yr Detention Volume =	3.522	acre-feet	
Approximate 10-yr Detention Volume =	4.222	acre-feet	
Approximate 25-yr Detention Volume =	5.044	acre-feet	
Approximate 50-yr Detention Volume =	5.530	acre-feet	
Approximate 100-yr Detention Volume =	6.004	acre-feet	

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.064	acre-feet
Zone 2 Volume (EURV - Zone 1) =	3.068	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.871	acre-feet
Total Detention Basin Volume =	6.004	acre-feet
Initial Surcharge Volume (ISV) =	user	ft^3
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio (R_{LW}) =	user	
Initial Surcharge Area (A_{ISV}) =	user	ft^2
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft^2
Volume of Basin Floor (V_{FLOOR}) =	user	ft^3
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft^2
Volume of Main Basin (V_{MAIN}) =	user	ft^3
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

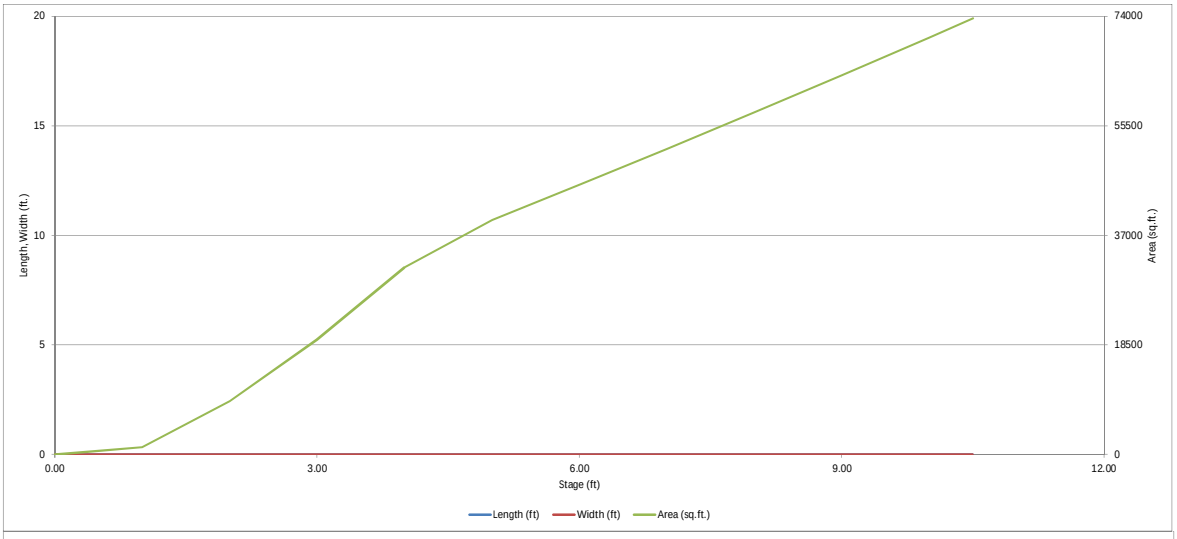
FYI - if this is adjusted to "5-yr - Zone 1" and then if you play with the orifice plate and vertical orifice inputs, some of the Ratio Peak Outflow exceedances can be eliminated. Just an FYI if you want to try.

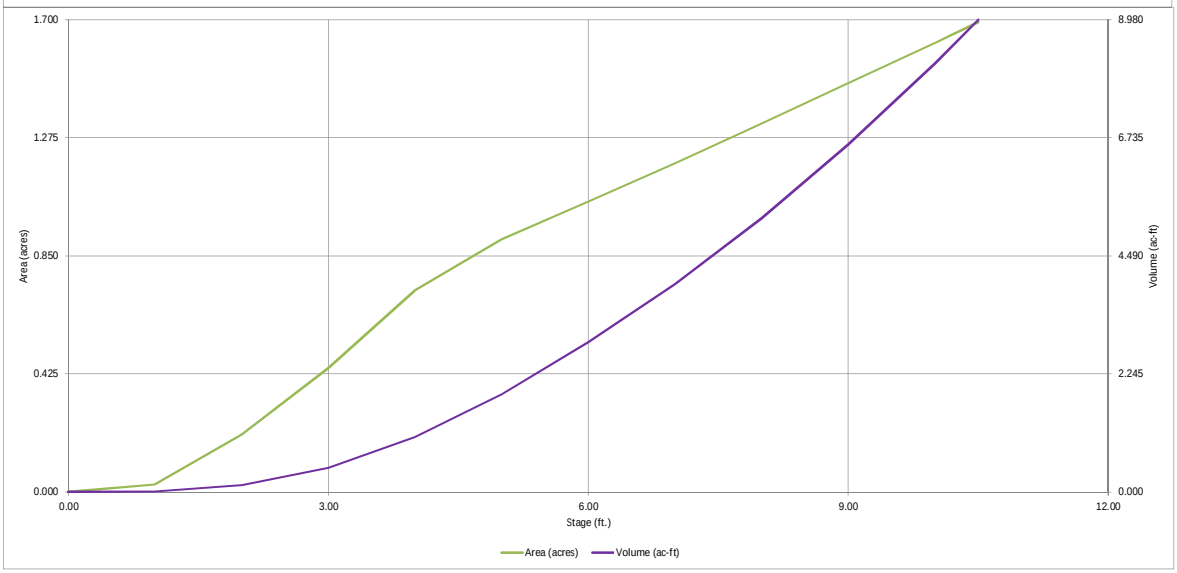
Depth Increment = ft

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Optional Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Top of Micropool	--	0.00	--	--	--	10	0.000		
6966	--	1.00	--	--	--	1,237	0.028	623	0.014
6967	--	2.00	--	--	--	9,028	0.207	5,756	0.132
6968	--	3.00	--	--	--	19,414	0.446	19,977	0.459
6969	--	4.00	--	--	--	31,638	0.726	45,503	1.045
6970	--	5.00	--	--	--	39,589	0.909	81,116	1.862
6971	--	6.00	--	--	--	45,537	1.045	123,679	2.839
6972	--	7.00	--	--	--	51,596	1.184	172,246	3.954
6973	--	8.00	--	--	--	57,766	1.326	226,927	5.210
6974 (Crest)	--	9.00	--	--	--	64,047	1.470	287,833	6.608
6975	--	10.00	--	--	--	70,449	1.617	355,081	8.152
6975.5	--	10.50	--	--	--	73,681	1.691	391,114	8.979

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



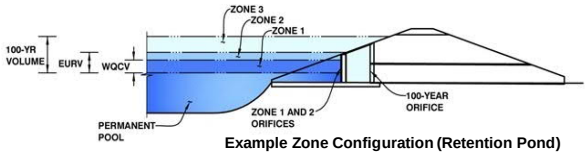


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: Sterling Ranch Recycling Facility

Basin ID: Pond A-Ultimate



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.03	1.064	Orifice Plate
Zone 2 (EURV)	7.15	3.068	Circular Orifice
Zone 3 (100-year)	8.59	1.871	Weir&Pipe (Restrict)
Total (all zones)		6.004	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)	Underdrain Orifice Area =	N/A	ft^2
Underdrain Orifice Diameter =	N/A	inches	Underdrain Orifice Centroid =	N/A	feet

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)	WQ Orifice Area per Row =	N/A	ft^2
Depth at top of Zone using Orifice Plate =	4.03	ft (relative to basin bottom at Stage = 0 ft)	Elliptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	Elliptical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	sq. inches	Elliptical Slot Area =	N/A	ft^2

Calculated Parameters for Plate

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.35	2.69					
Orifice Area (sq. inches)	3.00	3.00	3.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected			Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	4.03	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	0.10	N/A	ft^2
Depth at top of Zone using Vertical Orifice =	7.15	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	0.18	N/A	feet
Vertical Orifice Diameter =	4.20	N/A	inches				

Calculated Parameters for Vertical Orifice

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected			Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	7.35	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =	7.35	N/A	feet
Overflow Weir Front Edge Length =	4.00	N/A	feet	Overflow Weir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Grate Open Area / 100-yr Orifice Area =	9.01	N/A	
Horiz. Length of Weir Sides =	4.00	N/A	feet	Overflow Grate Open Area w/o Debris =	12.66	N/A	ft^2
Overflow Grate Type =	Close Mesh Grate	N/A		Overflow Grate Open Area w/ Debris =	6.33	N/A	ft^2
Debris Clogging % =	50%	N/A	%				

Calculated Parameters for Overflow Weir

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.40	N/A	ft^2
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.53	N/A	feet
Restrictor Plate Height Above Pipe Invert =	11.00		inches	Half-Central Angle of Restrictor Plate on Pipe =	1.49	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	9.00	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.48	feet
Spillway Crest Length =	120.00	feet	Stage at Top of Freeboard =	10.48	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	1.69	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	8.94	acre-ft

Calculated Parameters for Spillway

Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	1.064	4.132	3.020	3.935	4.670	5.573	6.455	7.502	9.804
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	3.020	3.935	4.670	5.573	6.455	7.502	9.804
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.3	0.5	0.8	6.8	13.6	22.7	41.4
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.31	0.51	0.94
Peak Inflow Q (cfs) =	N/A	N/A	47.1	60.8	71.0	88.8	104.1	123.1	161.3
Peak Outflow Q (cfs) =	0.5	1.5	1.3	1.4	1.7	8.7	16.0	21.8	57.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.7	2.3	1.3	1.2	1.0	1.4
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.6	1.1	1.6	1.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	67	60	66	71	71	69	68	65
Time to Drain 99% of Inflow Volume (hours) =	40	72	64	71	77	77	77	76	75
Maximum Ponding Depth (ft) =	4.03	7.15	5.99	6.79	7.38	7.77	8.01	8.45	9.21
Area at Maximum Ponding Depth (acres) =	0.73	1.21	1.04	1.15	1.24	1.29	1.33	1.39	1.50
Maximum Volume Stored (acre-ft) =	1.066	4.133	2.818	3.697	4.415	4.895	5.223	5.807	6.905

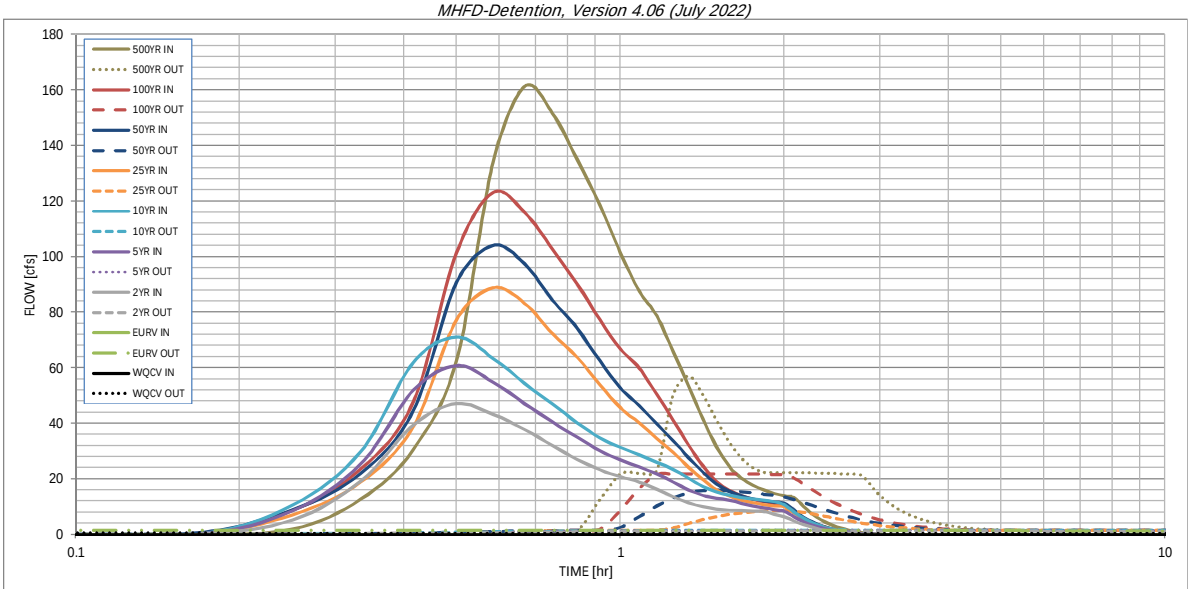
Ratio needs to be nearer to 1.0

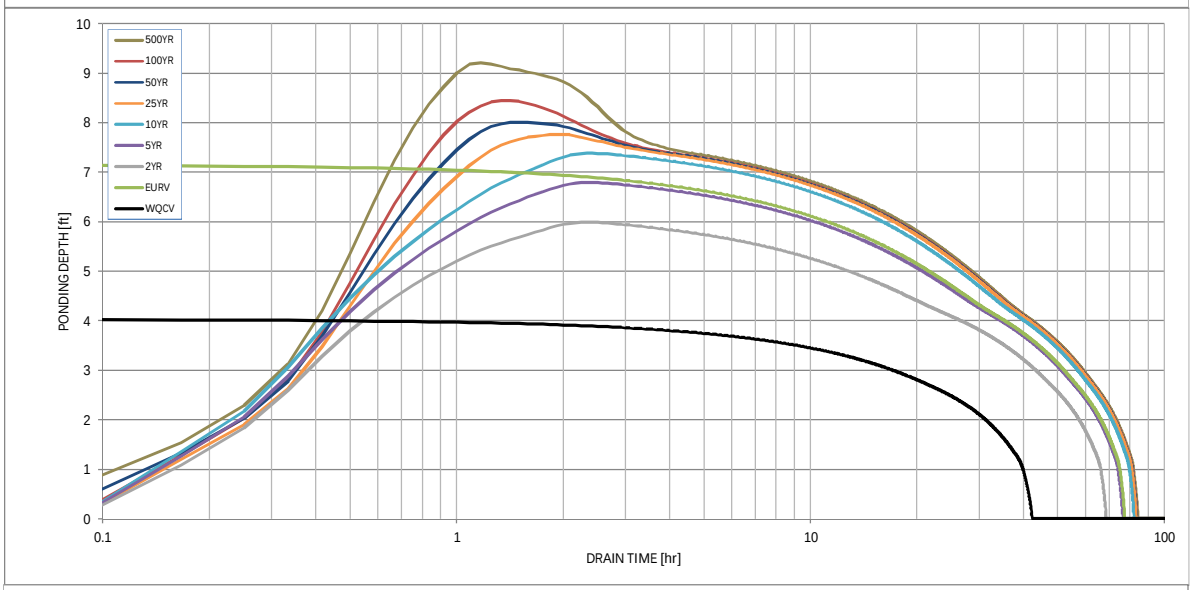
See my comment on PDF pg 12 above about these exceedances.

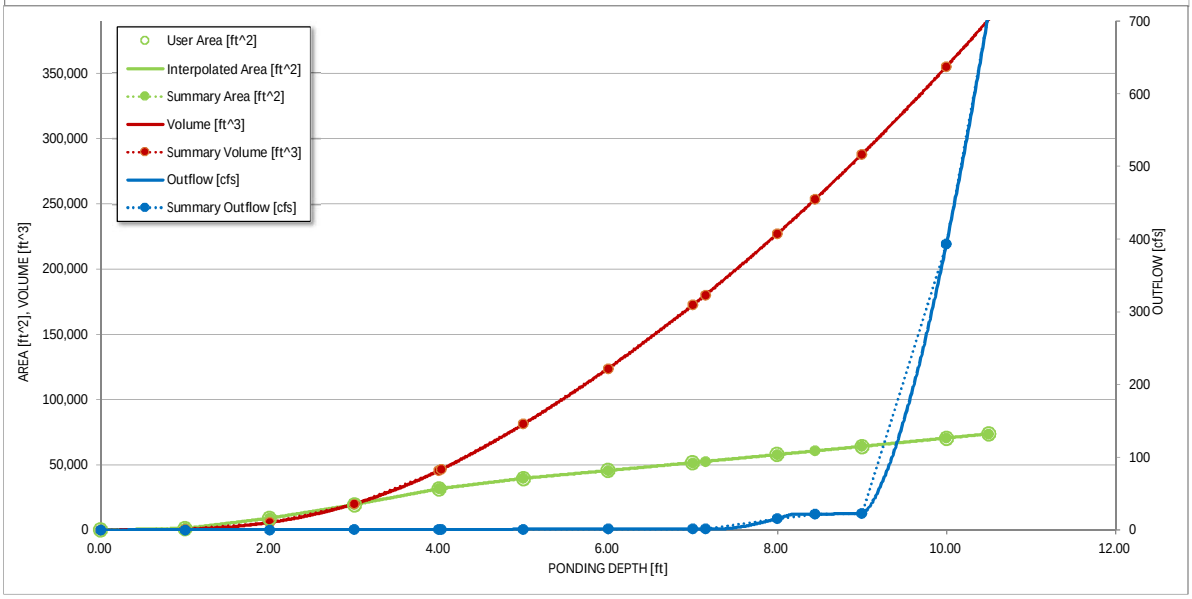
Per Basin sheet, required 100-year volume is 6.00 ac-ft

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)







S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.59	0.06	1.91
	0:15:00	0.00	0.00	5.25	8.54	10.58	7.11	8.93	8.67	12.63
	0:20:00	0.00	0.00	19.20	25.32	29.80	18.83	21.97	23.47	30.59
	0:25:00	0.00	0.00	39.45	51.94	61.97	38.88	44.61	47.85	62.61
	0:30:00	0.00	0.00	47.13	60.83	71.05	77.28	90.70	101.38	133.80
	0:35:00	0.00	0.00	43.24	54.87	63.48	88.83	104.10	123.11	161.33
	0:40:00	0.00	0.00	37.83	47.14	54.41	83.30	97.46	116.03	151.78
	0:45:00	0.00	0.00	32.03	40.50	47.05	72.36	84.47	102.89	134.92
	0:50:00	0.00	0.00	27.03	35.02	40.22	63.77	74.26	90.23	118.62
	0:55:00	0.00	0.00	23.25	30.13	34.78	53.91	62.53	77.27	101.40
	1:00:00	0.00	0.00	20.80	26.82	31.37	45.64	52.72	66.75	87.53
	1:05:00	0.00	0.00	18.89	24.26	28.66	40.15	46.30	59.93	78.69
	1:10:00	0.00	0.00	16.20	21.84	26.00	34.61	39.78	50.31	65.77
	1:15:00	0.00	0.00	13.60	18.95	23.42	29.53	33.82	41.23	53.60
	1:20:00	0.00	0.00	11.44	16.08	20.34	24.27	27.69	32.27	41.73
	1:25:00	0.00	0.00	9.96	14.06	17.28	19.82	22.50	24.68	31.73
	1:30:00	0.00	0.00	9.18	13.01	15.38	16.12	18.22	19.21	24.57
	1:35:00	0.00	0.00	8.78	12.43	14.20	13.82	15.59	15.99	20.34
	1:40:00	0.00	0.00	8.55	11.27	13.36	12.39	13.96	14.04	17.76
	1:45:00	0.00	0.00	8.40	10.25	12.75	11.44	12.88	12.69	15.97
	1:50:00	0.00	0.00	8.29	9.52	12.33	10.78	12.14	11.78	14.76
	1:55:00	0.00	0.00	7.32	8.98	11.75	10.34	11.64	11.12	13.90
	2:00:00	0.00	0.00	6.41	8.34	10.73	10.03	11.28	10.68	13.31
	2:05:00	0.00	0.00	4.89	6.39	8.17	7.74	8.71	8.20	10.21
	2:10:00	0.00	0.00	3.56	4.62	5.88	5.58	6.26	5.91	7.35
	2:15:00	0.00	0.00	2.58	3.35	4.25	4.03	4.53	4.29	5.34
	2:20:00	0.00	0.00	1.85	2.40	3.06	2.92	3.27	3.12	3.88
	2:25:00	0.00	0.00	1.31	1.66	2.16	2.05	2.30	2.20	2.73
	2:30:00	0.00	0.00	0.89	1.13	1.50	1.43	1.60	1.53	1.90
	2:35:00	0.00	0.00	0.59	0.77	1.02	1.00	1.12	1.07	1.32
	2:40:00	0.00	0.00	0.35	0.50	0.64	0.64	0.72	0.69	0.85
	2:45:00	0.00	0.00	0.18	0.28	0.35	0.37	0.41	0.39	0.48
	2:50:00	0.00	0.00	0.08	0.13	0.15	0.17	0.19	0.18	0.22
	2:55:00	0.00	0.00	0.02	0.04	0.04	0.05	0.05	0.05	0.06
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

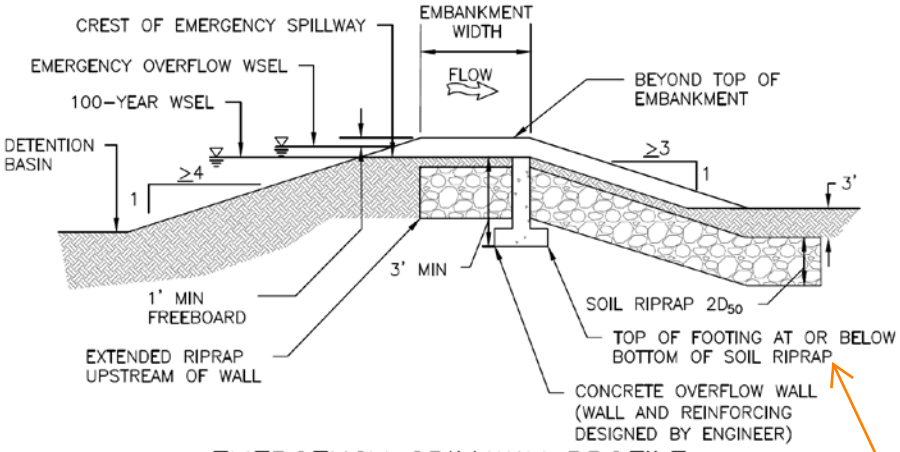
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Total Outflow [cfs]
6965-Top of Micropool	0.00	10	0.000	0	0.000	0.00
6966	1.00	1,237	0.028	623	0.014	0.10
6967	2.00	9,028	0.207	5,756	0.132	0.22
6968	3.00	19,414	0.446	19,977	0.459	0.36
6969	4.00	31,638	0.726	45,503	1.045	0.48
6969.03-WQCV WSEL	4.03	31,877	0.732	46,456	1.066	0.48
6970	5.00	39,589	0.909	81,116	1.862	0.98
6971	6.00	45,537	1.045	123,679	2.839	1.27
6972	7.00	51,596	1.184	172,246	3.954	1.49
6972.15-EURV WSEL	7.15	52,521	1.206	180,055	4.133	1.52
6973	8.00	57,766	1.326	226,927	5.210	15.61
6973.45-100 yr WSEL	8.45	60,592	1.391	253,557	5.821	21.83
6974-Spillway Crest	9.00	64,047	1.470	287,833	6.608	22.40
6975	10.00	70,449	1.617	355,081	8.152	392.99
6975.50-Top of Pond	10.50	73,681	1.691	391,114	8.979	711.69

For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

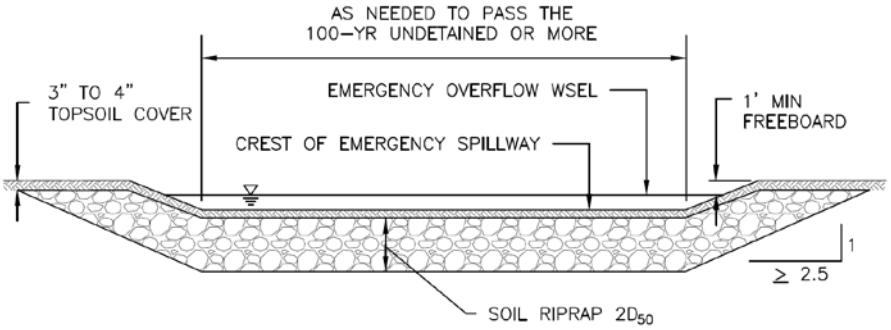
Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

SPILLWAY RIPRAP CALCULATION

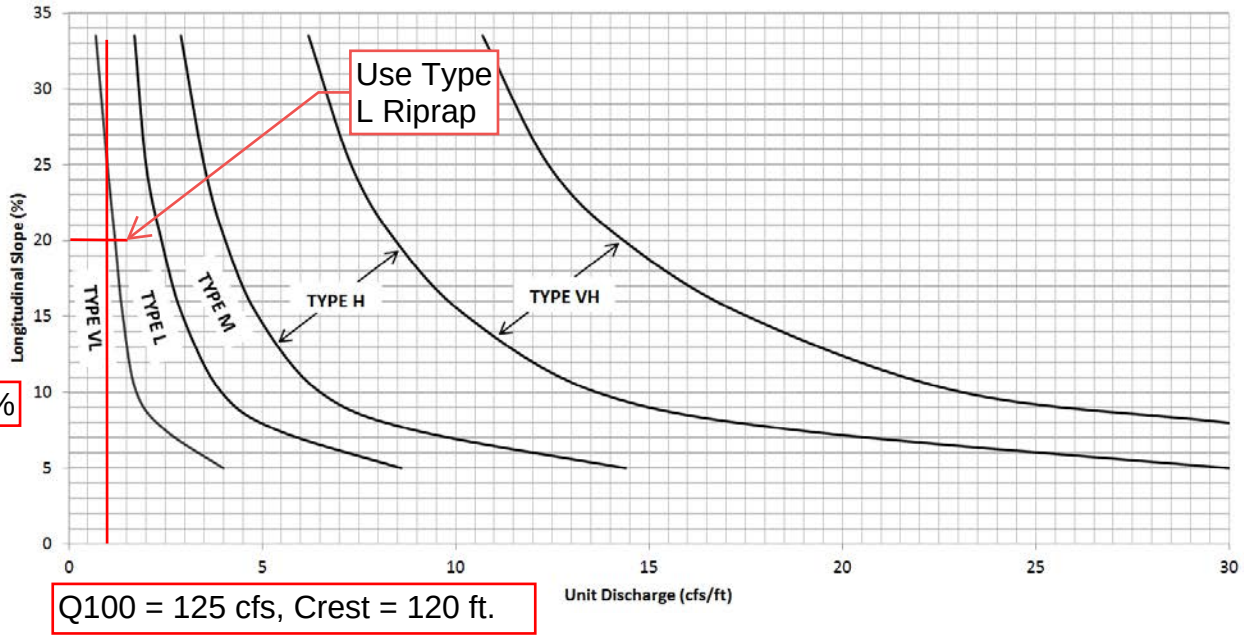


EMERGENCY SPILLWAY PROFILE

Will spillway have a cutoff wall? If not, cross off this text to avoid confusion or add a note on this page explaining that a cutoff wall will not be used.



EMERGENCY SPILLWAY SECTION AND SPILLWAY CHANNEL



Slope=20%

Q100 = 125 cfs, Crest = 120 ft.

Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Spillway Overflow Channel (Wide)

Trapezoidal

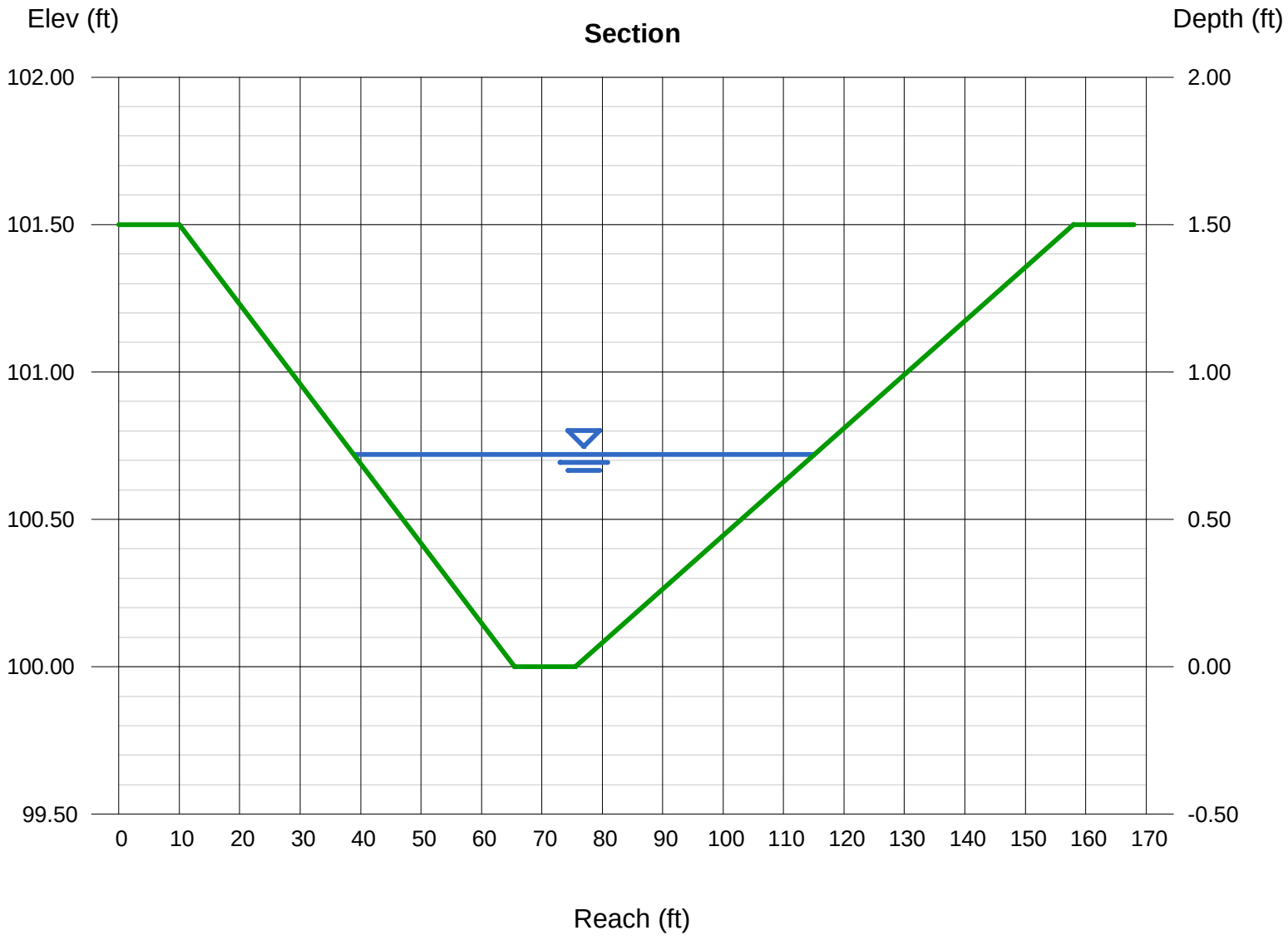
Bottom Width (ft)	= 10.00
Side Slopes (z:1)	= 37.00, 55.00
Total Depth (ft)	= 1.50
Invert Elev (ft)	= 100.00
Slope (%)	= 3.00
N-Value	= 0.035

Calculations

Compute by:	Known Q
Known Q (cfs)	= 125.00

Highlighted

Depth (ft)	= 0.72
Q (cfs)	= 125.00
Area (sqft)	= 31.05
Velocity (ft/s)	= 4.03
Wetted Perim (ft)	= 76.26
Crit Depth, Yc (ft)	= 0.76
Top Width (ft)	= 76.24
EGL (ft)	= 0.97



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Thursday, Jul 20 2023

Spillway Overflow Channel (Narrow)

Trapezoidal

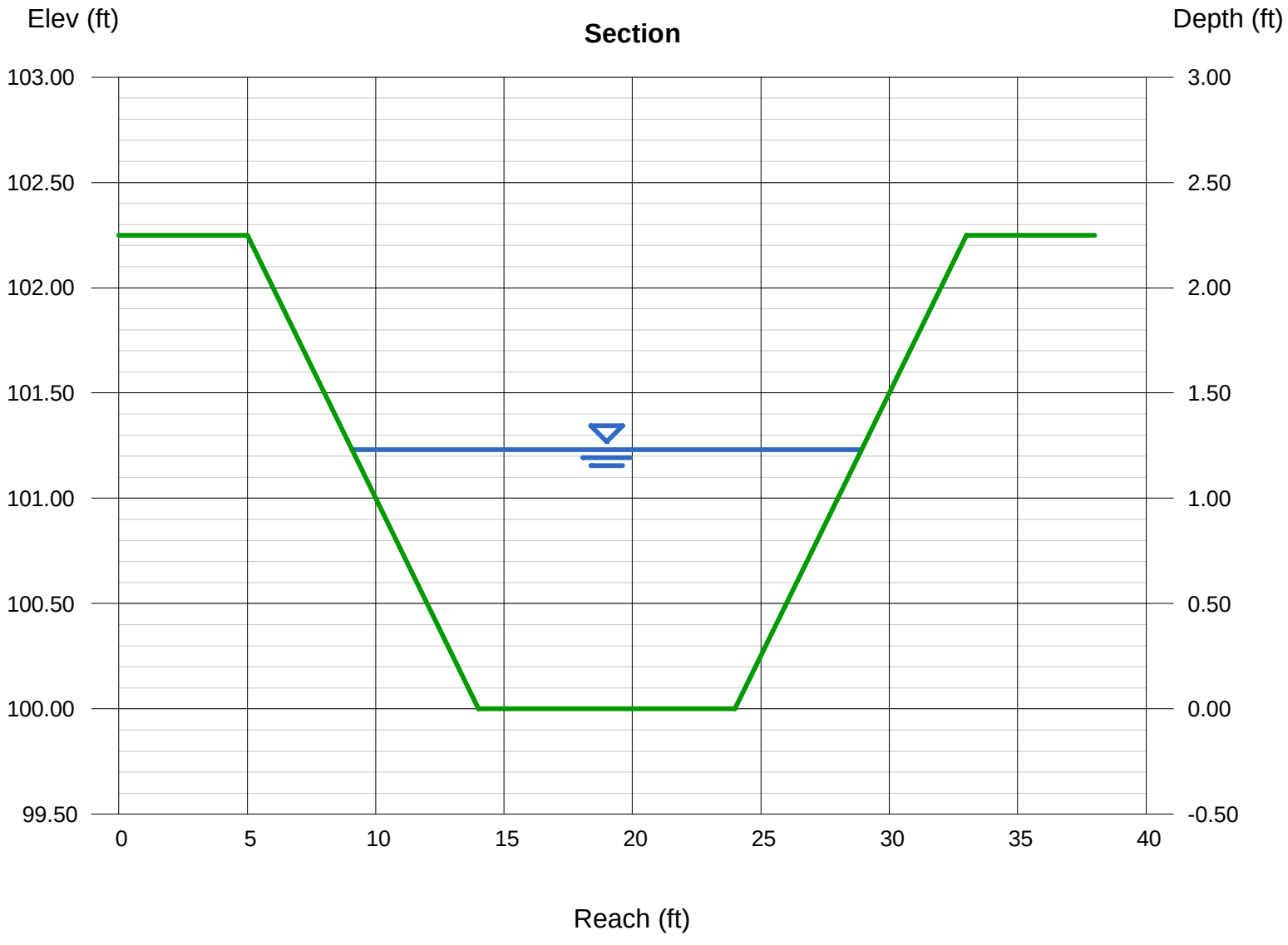
Bottom Width (ft)	= 10.00
Side Slopes (z:1)	= 4.00, 4.00
Total Depth (ft)	= 2.25
Invert Elev (ft)	= 100.00
Slope (%)	= 3.00
N-Value	= 0.035

Calculations

Compute by:	Known Q
Known Q (cfs)	= 125.00

Highlighted

Depth (ft)	= 1.23
Q (cfs)	= 125.00
Area (sqft)	= 18.35
Velocity (ft/s)	= 6.81
Wetted Perim (ft)	= 20.14
Crit Depth, Yc (ft)	= 1.40
Top Width (ft)	= 19.84
EGL (ft)	= 1.95



Label what inlet this is for

Emergency Spillway Overflow (Triple Type C Grate)
Orifice Flow Calculation

Q = C*A* square root (2gH)

C = 0.6 A = 25.58 sq ft g = 32.2

Head (ft)	CA	(2GH)	Sqrt (2GH)	Capacity
1	15.348	64.40	8.025	123.2
2	15.348	128.80	11.349	174.2
3	15.348	193.20	13.900	213.3
4	15.348	257.60	16.050	246.3
5	15.348	322.00	17.944	275.4
6	15.348	386.40	19.657	301.7

Use MHFD Inlet spreadsheet for Type C inlet

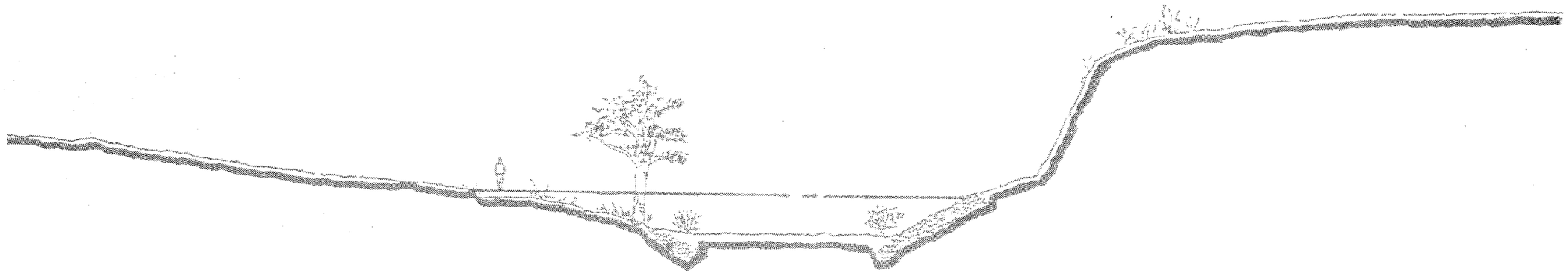
Peak Q_{100} Inflow = 123.1 cfs
Available Head = 2 ft

Appendix D
Reference Materials

SAND CREEK DRAINAGE BASIN PLANNING STUDY

PRELIMINARY DESIGN REPORT

CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO



PREPARED FOR:

City of Colorado Springs
Department of Comprehensive Planning, Development and Finance
Engineering Division
30 S. Nevada
Colorado Springs, Colorado 80903

PREPARED BY:

Kiowa Engineering Corporation
1011 North Weber
Colorado Springs, CO 80903

II. STUDY AREA DESCRIPTION

The Sand Creek drainage basin is a left-bank tributary to the Fountain Creek lying in the west-central portions of El Paso County. Sand Creek's drainage area at Fountain Creek is approximately 54 square miles of which approximately 18.8 square miles are inside the City of Colorado Springs corporate limits. The basin is divided into five major sub-basins, the Sand Creek mainstem, the East Fork Sand Creek, the Central Tributary to East Fork, the West Fork, and the East Fork Subtributary. Figure II-1 shows the location of the Sand Creek basin.

Basin Description

The Sand Creek basin covers a total of 54 square miles in unincorporated El Paso County and Colorado Springs, Colorado. Of this total, approximately 28 square miles is encompassed by the Sand Creek basin, and 26 square miles for the East Fork Sand Creek basin. The basin trends in generally a south to southwesterly direction, entering the Fountain Creek approximately two miles upstream of the Academy Boulevard bridge over Fountain Creek. Two main tributaries drain the basin, those being the mainstem of Sand Creek and East Fork Sand Creek. Development presence in most evident along the mainstream. At this time, approximately 25 percent of the basin is developed. This alternative evaluation focuses upon the Sand Creek basin only.

The maximum basin elevation is approximately 7,620 feet above mean sea level, and falls to approximately 5,790 feet at the confluence with Fountain Creek. The headwaters of the basin originate in the conifer covered areas of The Black Forest. The middle eastern portions of the basin are typified by rolling range land with fair to good vegetative cover associated with semi-arid climates.

Climate

This area of El Paso County can be described, in general as high plains, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry. Precipitation ranges from 14 to 16 inches per year, with the majority of this precipitation occurring in spring and summer in the form of rainfall. Thunderstorms are common during the summer months, and are typified by quick-moving low pressure cells which draw moisture from the Gulf of Mexico into the region. Average temperatures range from about 30^{O}F in the winter to 75^{O} in the summer. The relative humidity ranges from about 25 percent in the summer to 45 percent in the winter.

Soils and Geology

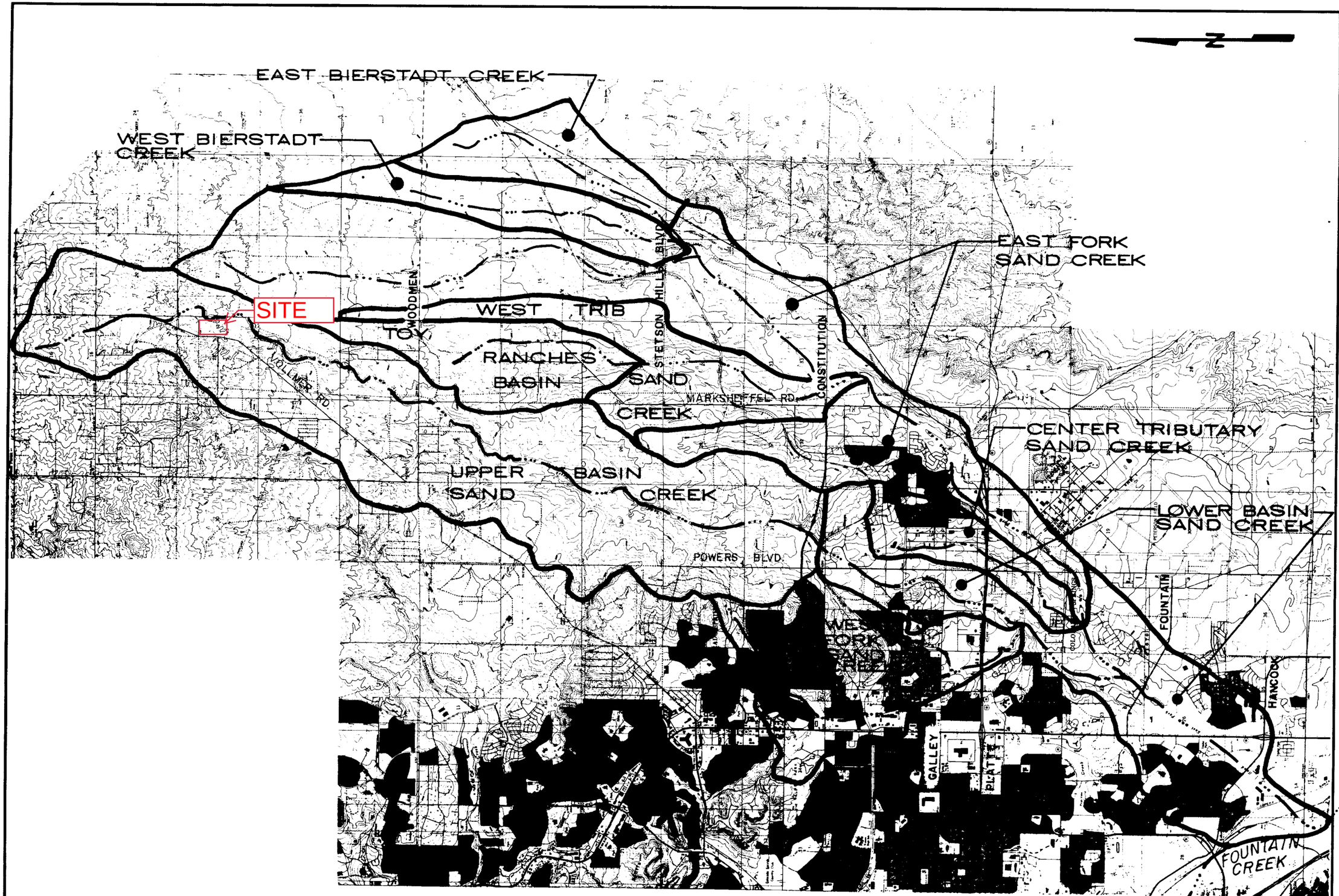
Soils within the Sand Creek basin vary between soil types A through D, as identified by the U. S. Department of Agriculture, Soil Conservation Service. The predominant soil groupings are in the Truckton and Bresser soil associations. The soils consist of deep, well drained soils that formed in alluvium and residium, derived from sedimentary rock. The soils have high to moderate infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. In undeveloped areas, the predominance of Type A and B soils give this basin a lower runoff per unit area as compared to basins with soils dominated by Types C and D. Presented on Figure II-2 is the Hydrologic Soil distribution map for the Sand Creek basin.

Property Ownership and Impervious Land Densities

Property ownership along the major drainageway within the Sand Creek basin vary from public to private. Along the developed reaches, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. Where development has not occurred, the drainageways remain under private ownership with no delineated drainage right-of-way or easements. There are several public parks which abut the mainstem of Sand Creek. Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin.

Land use information for the existing and future conditions were reviewed as part of the planning effort. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the creek. Presented on Figure II-3 is the proposed land use map used in the evaluation of impervious land densities discussed in the hydrologic section of this report. Figure II-3 is not intended to reflect the future zoning or land use policies of the City or the County.

The land use information within the Banning-Lewis Ranch property was obtained from Aries Properties during the time the draft East Fork Sand Creek Drainage Basin Planning Study was being prepared. The land use information was again reviewed with the City of Colorado Springs Department of Planning and was found to be appropriate for use in the estimation of hydrology for the East Fork Basin. The location of future arterial streets and roadways within



Kiowa Engineering Corporation
419 W. Bijou Street
Colorado Springs, Colorado
80905-1308

SAND CREEK DRAINAGE BASIN PLANNING STUDY

REGIONAL SUB-BASINS

Project No	90-04-09
Date:	11/90
Design:	
Drawn:	EAK
Check:	
Revisions:	

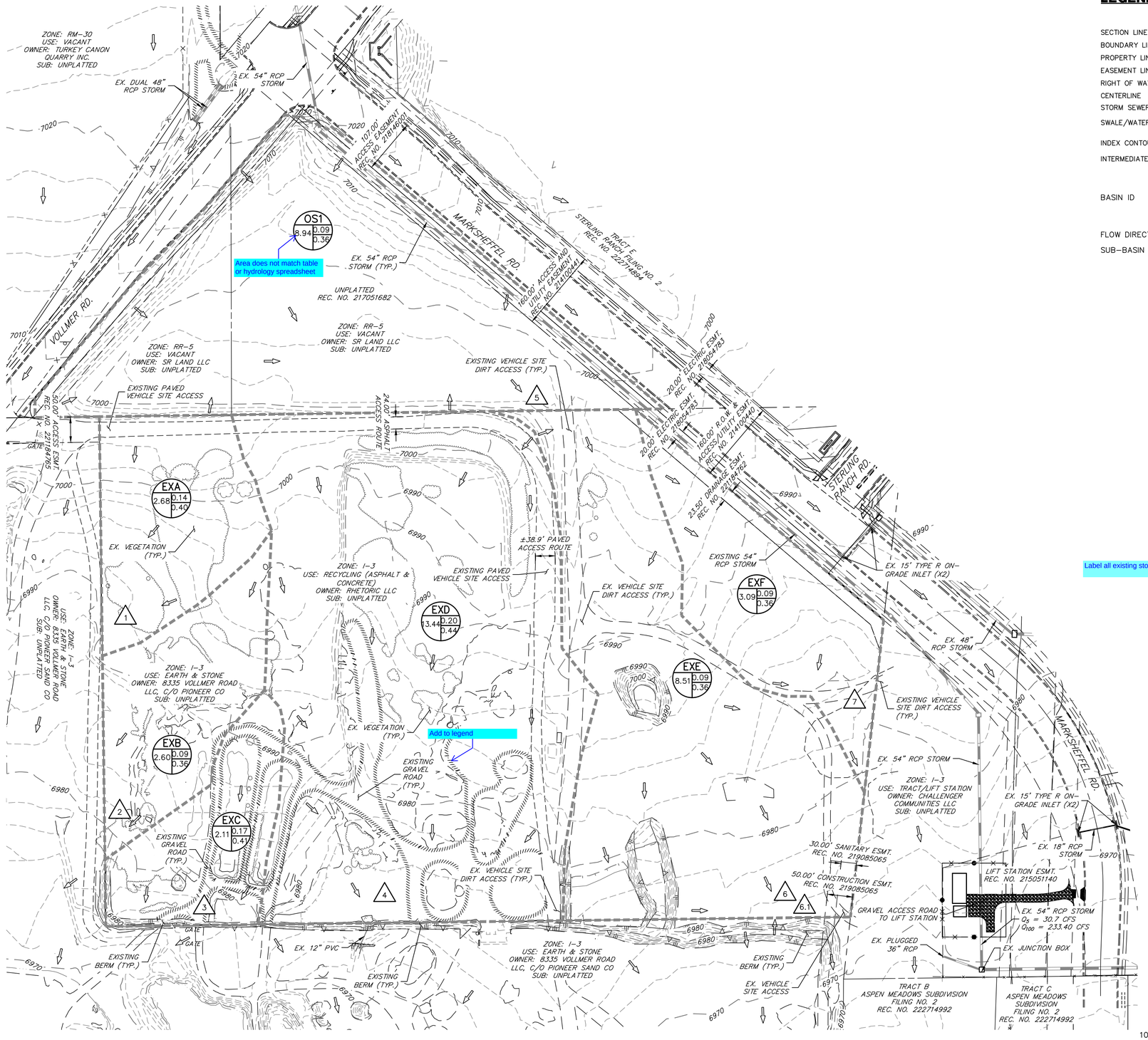
11

FIG. III-1

Appendix E
Drainage Maps

STERLING RANCH RECYCLING FACILITY

EXISTING DRAINAGE MAP



LEGEND

	EXISTING	PROPOSED
SECTION LINE		
BOUNDARY LINE		
PROPERTY LINE		
EASEMENT LINE		
RIGHT OF WAY		
CENTERLINE		
STORM SEWER		
SWALE/WATERWAY FLOWLINE		
INDEX CONTOUR	6100	6100
INTERMEDIATE CONTOUR		

BASIN ID — ID / AC / C5 / C100

DESIGN POINT DESIGNATION — 1

FLOW DIRECTION

SUB-BASIN DRAINAGE AREA

BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C_5	C_{100}	t_c (min)	Q_5 (cfs)	Q_{100} (cfs)
EXA	2.68	8%	0.14	0.40	21.1	1.1	5.4
EXB	2.60	2%	0.09	0.36	25.9	0.6	4.3
EXC	2.11	14%	0.17	0.41	22.4	1.0	4.3
EXD	13.44	17%	0.20	0.44	23.4	7.6	28.1
EXE	8.51	2%	0.09	0.36	27.7	2.0	13.4
EXF	3.09	2%	0.09	0.36	24.1	0.8	5.2
OS1	9.42	2%	0.09	0.36	49.4	1.5	9.8

DESIGN POINT

DP	Q5 Total	Q100 Total
1	1.1	5.4
2	0.6	4.3
3	1.0	4.3
4	7.6	28.1
5	1.5	9.8
6	2.0	13.4
6.1	2.8	18.7
7	0.8	5.2

PCD FILE NO. PPR-23-XXX
STERLING RANCH RECYCLING FACILITY
EXISTING DRAINAGE MAP
JOB NO. 25188.14
07/31/2023
SHEET 1 OF 1

J·R ENGINEERING
A Westrian Company
Centennial 303-740-9393 • Colorado Springs 719-593-2593
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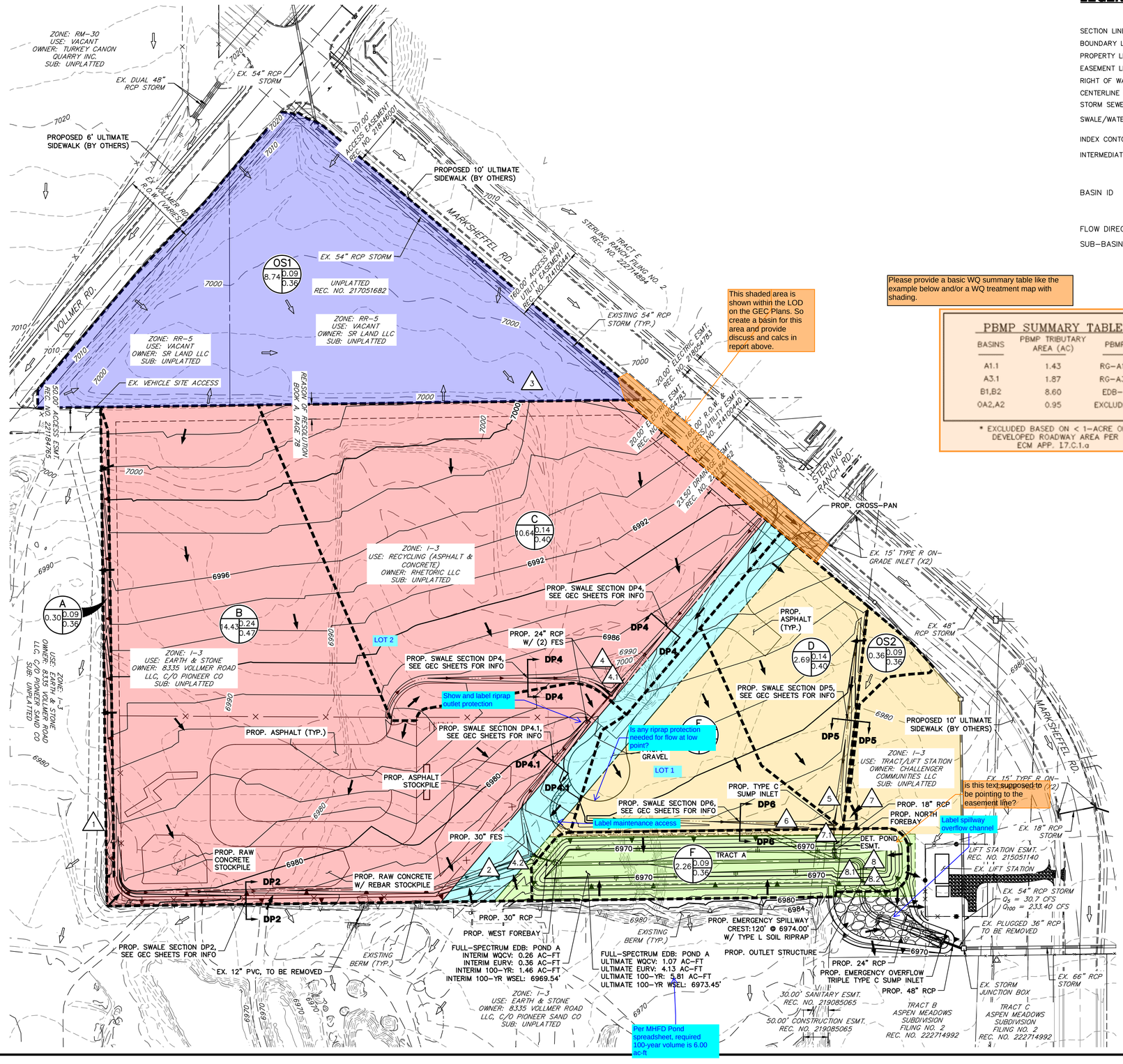
STERLING RANCH RECYCLING FACILITY

PROPOSED DRAINAGE MAP



Is any riprap protection needed for flow at low point?

This shaded area is shown within the LOD on the GEC Plans. So create a basin for this area and provide discuss and calcs in report above.

is this text supposed to be pointing to the easement line?

Label all storm facilities as public or private

LEGEND

	EXISTING	PROPOSED
SECTION LINE		
BOUNDARY LINE		
PROPERTY LINE		
EASEMENT LINE		
RIGHT OF WAY		
CENTERLINE		
STORM SEWER		
SWALE/WATERWAY FLOWLINE		
INDEX CONTOUR	6100	6100
INTERMEDIATE CONTOUR		

BASIN ID — ID / AC / C5 / C100

DESIGN POINT DESIGNATION — 1

FLOW DIRECTION

SUB-BASIN DRAINAGE AREA

Please provide a basic WQ summary table like the example below and/or a WQ treatment map with shading.

PBMP SUMMARY TABLE

BASINS	PBMP TRIBUTARY AREA (AC)	PBMP
A1.1	1.43	RG-A1.1
A3.1	1.87	RG-A3.1
B1,B2	8.60	EDB-B
OA2,A2	0.95	EXCLUDED*

* EXCLUDED BASED ON < 1-ACRE OF DEVELOPED ROADWAY AREA PER ECM APP. 17.C.1.a

ULTIMATE LAND USE LEGEND

INDUSTRIAL-HEAVY AREAS (90% IMPERVIOUS)	
BUSINESS COMMERCIAL AREAS (95% IMPERVIOUS)	
RESIDENTIAL-1/8 ACRE OR LESS (65% IMPERVIOUS)	
NON-RESIDENTIAL COLLECTOR-80' R.O.W. (100% AND 2% IMPERVIOUS)	
HISTORICAL ANALYSIS (2% IMPERVIOUS)	

BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C_5	C_{100}	t_c (min)	Q_5 (cfs)	Q_{100} (cfs)
A	0.30	2%	0.09	0.36	5.0	0.2	1.0
B	14.43	20%	0.24	0.47	34.0	7.8	26.0
C	10.64	7%	0.13	0.39	28.7	3.5	17.7
D	2.69	12%	0.17	0.42	21.9	1.4	5.6
E	2.49	13%	0.17	0.42	20.9	1.3	5.3
F	2.26	2%	0.09	0.36	18.5	0.6	4.4
OS1	9.42	2%	0.09	0.36	49.4	1.5	9.8
OS2	0.36	2%	0.09	0.36	16.5	0.1	0.7

DESIGN POINT

DP	Q5 Total	Q100 Total
1	0.2	1.0
2	7.8	26.0
3	1.5	9.8
4	3.5	17.7
4.1	3.9	21.9
4.2	9.7	41.5
5	1.4	5.6
6	1.3	5.3
7	0.1	0.7
7.1	2.7	11.4
8	0.6	4.4
8.1	11.7	50.5
8.2	0.1	8.0

N

100 50 0 100 200

ORIGINAL SCALE: 1" = 100'

PPR2341 & SF2325

PCD FILE NO. PPR-23-XXX
STERLING RANCH RECYCLING FACILITY
PROPOSED DRAINAGE MAP
JOB NO. 25188.14
07/31/23
SHEET 1 OF 1

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V1_Drainage Report - Final.pdf Markup Summary

Glenn Reese - EPC Stormwater (30)

Subject: SW - Textbox
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Author: Glenn Reese - EPC Stormwater
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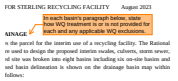
PPR2341 & SF2325



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Page Label: 7
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 8:22:54 AM
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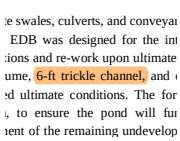
In each basin's paragraph below, state how WQ treatment is or is not provided for each and any applicable WQ exclusions.



Subject: SW - Highlight
Page Label: 10
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 8:25:18 AM
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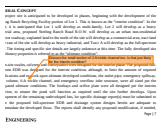
6-ft trickle channel,



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Page Label: 10
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 8:25:15 AM
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Discuss the small section of 2-ft trickle channel too. Is that just likely for the interim condition?

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Page Label: 12
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 9:47:41 AM
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For some minor storm events, the release rate is higher
than the existing predevelopment flows. Due to the Type A soils on the site, the predevelopment calculated flows are low for the 2 through 10 year storms. Therefore, the outlet structure was designed to meet drain times for the WQCV, EURV, and 100-year events.

Subject: SW - Textbox
Page Label: 12
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 8:25:43 AM
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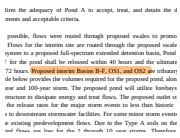
Cutoff Walls: Provide a discussion with supporting data/calcs on whether cutoff walls are or are not necessary for onsite emergency spillways and/or drop structures.



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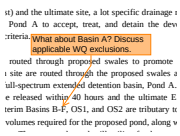
Proposed interim Basins B-F, OS1, and OS2 a



Subject: SW - Textbox with Arrow
Page Label: 12
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 8:27:03 AM
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What about Basin A? Discuss applicable WQ exclusions.

Subject: SW - Textbox with Arrow
Page Label: 12
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 9:47:37 AM
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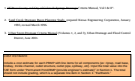
Per ECM Chap 3.2.8.B, “The proposed project or developed land use shall not change historical runoff values, cause downstream damage, or adversely impact adjacent properties.” Increases from the historical flowrates are allowable (with or without full spectrum detention) if it is shown (via text and/or calcs) that the flow increase can be accommodated downstream (i.e., show that there is a suitable outfall, per ECM Chap 3.2.4). If applicable, reference the downstream facilities in a DBPS or MDDP.



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Page Label: 14
Author: Glenn Reese - EPC Stormwater
Date: 10/17/2023 11:45:13 AM
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COST ESTIMATE

Include a cost estimate for each PBMP with line items for all components (ex: riprap, road base, forebay, trickle channel, outlet structure, outlet pipe, spillway, etc). Input the total value into the FAE form under “Permanent Pond/BMP (provide engineer’s estimate)” in Section 1. The total should not include grading, which is a separate line item in Section 1: “Earthwork.”

Subject: SW - Textbox
Page Label: 14
Author: Glenn Reese - EPC Stormwater
Date: 10/17/2023 11:45:16 AM
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Per PDF page 8 of the Soils Report, groundwater was encountered in two borings at only ~4-5ft below grade, which would mean it could surface into the pond (according to Section A-A Profile on Sht 9 of the GEC Plan, the pond depth is 9-10ft). See excerpts from MHFD's DCM volume 2 and 3 on the page below for potential concerns with groundwater in an EDB and the recommended mitigation options (like a clay or geomembrane liner).

Per CDPHE's "Low Risk Discharge Guidance - Discharges of Uncontaminated Groundwater to Land," discharging groundwater to a pond or other SW conveyance is prohibited unless properly permitted through CDPHE. Please review this guidance and the applicable permits. The guidance is linked below, the permits can be found on CDPHE's website.

Please discuss this potential shallow groundwater in the report text above.

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Date: 10/17/2023 11:45:17 AM
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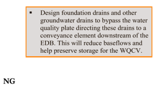

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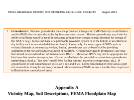

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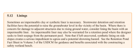

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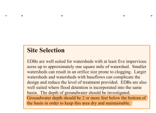

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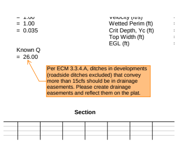

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Page Label: 1
Author: Glenn Reese - EPC Stormwater
Date: 10/17/2023 10:34:26 AM
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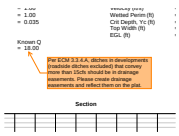
Per ECM 3.3.4.A, ditches in developments (roadside ditches excluded) that convey more than 15cfs should be in drainage easements. Please create drainage easements and reflect them on the plat.



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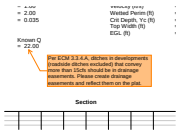

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Author: Glenn Reese - EPC Stormwater
Date: 10/17/2023 10:34:32 AM
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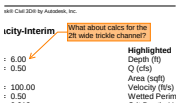
Per ECM 3.3.4.A, ditches in developments (roadside ditches excluded) that convey more than 15cfs should be in drainage easements. Please create drainage easements and reflect them on the plat.



Subject: SW - Textbox with Arrow
Page Label: 1
Author: Glenn Reese - EPC Stormwater
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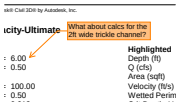
What about calcs for the 2ft wide trickle channel?



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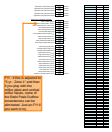
What about calcs for the 2ft wide trickle channel?



Subject: SW - Textbox with Arrow
Page Label: 2
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 9:48:51 AM
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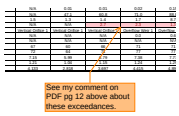
FYI - if this is adjusted to "5-yr - Zone 1" and then if you play with the orifice plate and vertical orifice inputs, some of the Ratio Peak Outflow exceedances can be eliminated. Just an FYI if you want to try.



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Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 9:48:39 AM
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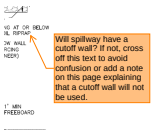
See my comment on PDF pg 12 above about these exceedances.



Subject: SW - Textbox with Arrow
Page Label: 2
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 9:49:13 AM
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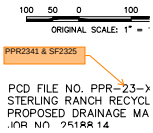
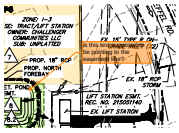
Space:

Will spillway have a cutoff wall? If not, cross off this text to avoid confusion or add a note on this page explaining that a cutoff wall will not be used.



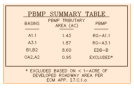
Subject: SW - Textbox
Page Label: [1] 24x36 Title Landscape
Author: Glenn Reese - EPC Stormwater
Date: 10/16/2023 2:34:38 PM
Status:
Color:
Layer:
Space:

PPR2341 & SF2325



Subject: SW - Textbox with Arrow
Page Label: [1] 24x36 Title Landscape
Author: Glenn Reese - EPC Stormwater
Date: 10/17/2023 5:06:11 PM
Status:
Color:
Layer:
Space:

is this text supposed to be pointing to the easement line?



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Page Label: [1] 24x36 Title Landscape
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Date: 10/17/2023 5:08:02 PM
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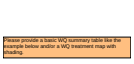


Subject: SW - Textbox
Page Label: [1] 24x36 Title Landscape
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 8:28:33 AM
Status:
Color:
Layer:
Space:

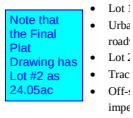
Please provide a basic WQ summary table like the example below and/or a WQ treatment map with shading.

Subject: Polygon
Page Label: [1] 24x36 Title Landscape
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 10:16:12 AM
Status:
Color:
Layer:
Space:

Subject: SW - Textbox with Arrow
Page Label: [1] 24x36 Title Landscape
Author: Glenn Reese - EPC Stormwater
Date: 10/18/2023 10:17:32 AM
Status:
Color:
Layer:
Space:

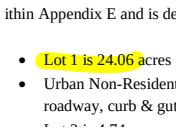
This shaded area is shown within the LOD on the GEC Plans. So create a basin for this area and provide discuss and calcs in report above.

eschoenheit (13)



Subject: Text Box
Page Label: 8
Author: eschoenheit
Date: 10/17/2023 8:14:11 AM
Status:
Color:
Layer:
Space:

Note that the Final Plat Drawing has Lot #2 as 24.05ac



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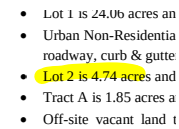

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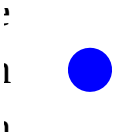

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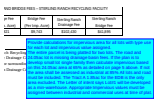
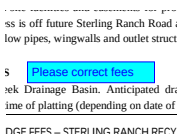


Subject: Text Box
Page Label: 13
Author: eschoenheit
Date: 10/18/2023 1:01:54 PM
Status:
Color:
Layer:
Space:

Provide calculations for impervious area for all lots with type use for each lot and impervious value assigned.
The entire parcel is being platted for two lots. The road and 24.05ac lot is missing drainage basin fees. If the plan is to develop small lot single family then calculate impervious based on this 24.05ac area at 65% as detailed on page 5 above. If not the area shall be assessed as industrial at 85% All lots and road must be included. The Tract A 1.85ac for the EDB is the only area excluded. The Letter of intent says Lot#1 will be developed as a min-warehouse. Appropriate Impervious values must be assigned between industrial and commercial uses at time of plat.



Subject: Text Box
Page Label: 13
Author: eschoenheit
Date: 10/18/2023 12:59:10 PM
Status:
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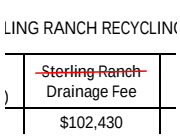
Please correct fees



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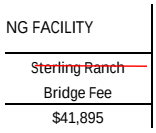

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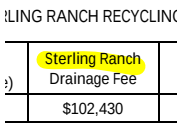

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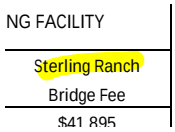

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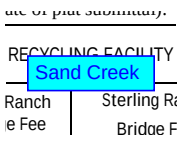

Subject: Text Box
Page Label: 13
Author: eschoenheit
Date: 10/18/2023 1:00:08 PM
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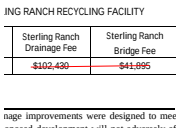
Sand Creek



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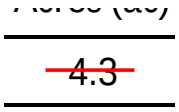

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Page Label: 13
Author: eschoenheit
Date: 10/18/2023 1:00:45 PM
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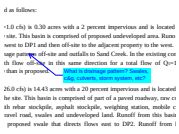
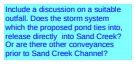
Layer:
Space:

CDurham (24)



Subject: Callout
Page Label: 7
Author: CDurham
Date: 10/19/2023 4:00:02 PM
Status:
Color:
Layer:
Space:

What is drainage pattern? Swales, c&g, culverts, storm system, etc?



Subject: Text Box
Page Label: 14
Author: CDurham
Date: 10/19/2023 4:13:01 PM
Status:
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Layer:
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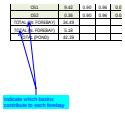
Include a discussion on a suitable outfall. Does the storm system which the proposed pond ties into, release directly into Sand Creek? Or are there other conveyances prior to Sand Creek Channel?



Subject: Callout
Page Label: 1
Author: CDurham
Date: 10/19/2023 3:51:26 PM
Status:
Color:
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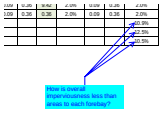
Indicate which basins contribute to each forebay



Subject: Callout
Page Label: 1
Author: CDurham
Date: 10/19/2023 3:52:23 PM
Status:
Color:
Layer:
Space:

How is overall imperviousness less than areas to each forebay?

= 9.48
= 1.77

Include what FR # is for each swale. If any are over 0.8, include what will be done to mitigate it.

Subject: Text Box
Page Label: 1
Author: CDurham
Date: 10/19/2023 2:14:11 PM
Status:
Color:
Layer:
Space:

Include what FR # is over 0.8, include what will be done to mitigate it.

Provide calculations for riprap outlet protection

Subject: Text Box
Page Label: 1
Author: CDurham
Date: 10/19/2023 3:49:09 PM
Status:
Color:
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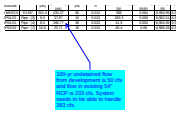
Space:

Provide calculations for riprap outlet protection

Use MHFD Inlet spreadsheet for Type C inlet

Subject: Text Box
Page Label: 1
Author: CDurham
Date: 10/19/2023 2:24:14 PM
Status:
Color:
Layer:
Space:

Use MHFD Inlet spreadsheet for Type C inlet



Subject: Callout
Page Label: 1
Author: CDurham
Date: 10/19/2023 5:31:05 PM
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Color:
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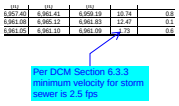
Space:

100-yr undetained flow from development is 50 cfs and flow in existing 54" RCP is 233 cfs. System needs to be able to handle 283 cfs.



Subject: Callout
Page Label: 6
Author: CDurham
Date: 10/19/2023 3:40:48 PM
Status:
Color:
Layer:
Space:

Per DCM Section 6.3.3 minimum velocity for storm sewer is 2.5 fps

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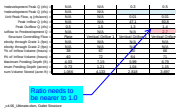

Subject: Callout
Page Label: 4
Author: CDurham
Date: 10/19/2023 3:29:55 PM
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Color:
Layer:
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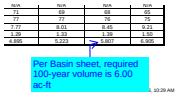
Ratio needs to be nearer to 1.0

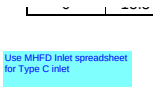


Subject: Callout
Page Label: 4
Author: CDurham
Date: 10/19/2023 3:34:27 PM
Status:
Color:
Layer:
Space:

Per Basin sheet, required 100-year volume is 6.00 ac-ft

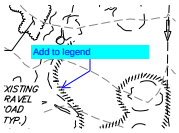
Subject: Text Box
Page Label: 5
Author: CDurham
Date: 10/19/2023 3:38:26 PM
Status:
Color:
Layer:
Space:

Label what inlet this is for



Subject: Text Box
Page Label: 5
Author: CDurham
Date: 10/19/2023 3:39:01 PM
Status:
Color:
Layer:
Space:

Use MHFD Inlet spreadsheet for Type C inlet

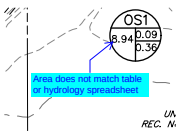


Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:42:10 PM
Status:
Color:
Layer:
Space:

Add to legend

Subject: Text Box
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:42:35 PM
Status:
Color:
Layer:
Space:

Label all existing storm facilities as public or private



Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:42:54 PM
Status:
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Layer:
Space:

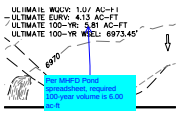
Area does not match table or hydrology spreadsheet

Subject: Text Box
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:44:27 PM
Status:
Color:
Layer:
Space:

LOT 2

Subject: Text Box
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:43:37 PM
Status:
Color:
Layer:
Space:

LOT 1



Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:45:46 PM
Status:
Color:
Layer:
Space:

Per MHFD Pond spreadsheet, required 100-year volume is 6.00 ac-ft

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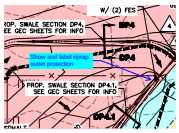
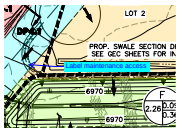


Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:46:08 PM
Status:
Color:
Layer:
Space:

Show and label riprap outlet protection

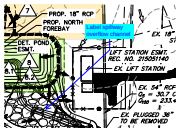


Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 4:27:37 PM
Status:
Color:
Layer:
Space:

Label maintenance access

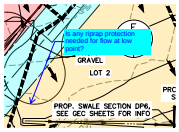
Subject: Text Box
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:47:21 PM
Status:
Color:
Layer:
Space:

Label all storm facilities as public or private



Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 3:49:44 PM
Status:
Color:
Layer:
Space:

Label spillway overflow channel



Subject: Callout
Page Label: [1] 24x36 Title Landscape
Author: CDurham
Date: 10/19/2023 4:27:43 PM
Status:
Color:
Layer:
Space:

Is any riprap protection needed for flow at low point?