# FINAL DRAINAGE LETTER FOR LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY, COLORADO

# **Prepared for:**

DTV Meadowbrook LLC 106 S. Kyrene Road #2 Chandler, AZ 85226 (480) 313-2724

# Prepared by:

M&S Civil Consultants 212 N. Wahsatch Avenue Suite 305 Colorado Springs, CO 80903 (719) 955-5485

# February 2023

Project #10-025 PCD Filing No.: PPR2345



# FINAL DRAINAGE LETTER FOR LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY COLORADO

# DRAINAGE PLAN STATEMENTS

# ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

# DEVELOPER'S STATEMENT



I, the developer(s) have read and will comply with all the requirements specified in this drainage report and plan.

BY:\_

TITLE: Manager

DATE: 02-07-24

ADDRESS: Brian Zurek 106 S. Kryene Road Chandler, AZ 85226

# EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY:

DATE:\_\_\_\_\_

Joshua Palmer, P.E. County Engineer / ECM Administrator

CONDITIONS:



# FINAL DRAINAGE LETTER FOR CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY COLORADO

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# FINAL DRAINAGE LETTER FOR LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO. 2 EL PASO COUNTY COLORADO

# Purpose

This Final Drainage Letter for Lot 2 Claremont Business Park 2 Filing No. 2 is in support of the commercial layout for the south half of Lot 2 and Construction Drawings of the subject site and to show the general conformance with the drainage patterns established by the **Final Drainage Report for Claremont Business Park 2 Filing No. 2** prepared by M&S Civil Consultants, Inc. This letter functions to identify the existing and proposed runoff patterns and recommend proposed drainage improvements which are intended to safely convey runoff through the proposed development, while minimizing impacts to downstream facilities and adjacent properties. The analysis has been prepared in accordance with the requirements set forth by El Paso County and remains in compliance with the Final Drainage Report for Claremont for Claremont Business Park 2 Filing No. 2 by M&S Civil Consultants.

# **General Location and Description**

The Lot 2 Claremont Business Park 2 Filing No.2 is the commercial layout for the south half of Lot 2 of Claremont Business Park 2 Filing No.2. The site is located in the Northeast ¼ of the Northeast ¼ of Section 8, and the Southeast ¼ of the Southeast ¼ of Section 5, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The site is bordered to the northeast by N. Marksheffel Road, to the northwest by Meadowbrook Parkway, and to the south by Claremont Business Park 2 Filing No. 1 (Lots 1-7). See Vicinity Map in Appendix for details.

The site consists of 1.808 acres which is currently vacant land. The development project will connect with the existing drive entrance and construct a commercial building, drive thru, drive aisles, parking, landscaping and utilities through the south half of the site. The Claremont Business Park 2 Filing 2 site is currently zoned "CS" and the proposed principal use for the site will be neighborhood commercial and light industrial.

In addition to the construction of the commercial building, drive aisles and utilities, an existing storm sewer system was constructed that will function to collect runoff from the Lot 2 and route to an existing sand filter basin water quality pond 3 that will be provided to treat runoff from aforementioned improvements. Modifications are to be provided to the existing storm sewer, such as install a proposed 5' Type R inlet and remove sections of existing storm sewer to route Lot 2 runoff into the pond 3. The existing pond 3 will tie into an existing system near Meadowbrook Parkway, which ultimately conveys runoff southwest into the East Fork of Sand Creek.

Per Resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required. (Refer to appendix).



Individual drainage letter and/or report shall be required with the development of the north half of Lot 2.

# Soils

The Natural Resources Conservation Service, United States Department of Agriculture, Web Soil Survey, indicates that the soils for this project are: Blakeland Loamy Sand (8), Blendon Sandy Loam (10) and Ellicott Loamy Coarse Sand (28). These soils have been characterized as having Hydrologic Soil Types "A" & "B". The soils classification used for this study is "B". Refer to the Soils Map located in the Appendix of this report

# **Previous Studies**

The proposed site and surrounding existing drainage facilities have been included in multiple drainage letters and reports. The following is a list of existing documents that were pertinent to analyzing this site.

- Final Drainage Report for Claremont Business Park 2 Filing No. 1, by M&S Civil Consultants, approved 2/11/2021.
- Final Drainage Report for Claremont Business Park 2 Filing No. 2, by M&S Civil Consultants, approved 11/13/2023 PCD Filing No. VR233.
- Final Drainage Letter for Lot 5 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 03/03/2021.
- Final Drainage Letter for Lot 6 of Claremont Business Park 2 Filing No.1, by M&S Civil Consultants, approved 07/08/2021.

# **Drainage Criteria**

As required by El Paso County, Colorado, this report has been prepared in accordance to the criteria set forth in the El Paso County Drainage Criteria Manual Volume 1 & 2 (DCM), the El Paso County Engineering Criteria Manual (ECM), and El Paso County Resolutions 15-042 and 19-245.

# **Design Event Frequency**

The 100-year storm event was used as the major storm for the project, and the 5-year storm event was used as the minor storm.

# Method of Analysis

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres.

Where: Q=C\*i\*A

- Q = Maximum runoff rate in cubic feet per second (cfs)
- C = Runoff coefficient
- i = Average rainfall intensity (inches per hour)
- A = Area of drainage sub-basin (acres)



# **Runoff Coefficient**

Rational Method coefficients from Table 6-6 of the Drainage Criteria Manual for developed land were utilized in the Rational Method calculations. Composite percent impervious and C values were calculated using roofs, commercial areas, asphalt drives, landscaped areas and parks found within the aforementioned table.

# **Time of Concentration**

The time of concentration consists of the initial time of overland flow and the travel time (street or channel, etc) to a downstream structure or point of interest. A minimum time of concentrations of 5 minutes is utilized for urban areas.

# **Rainfall Intensity**

The hypothetical rainfall depths for the 1-hour storm duration were taken from Table 6-2 of the Drainage Criteria Manual.

Project 1-Hour Rainfall Depth Storm Recurrence Interval Rainfall Depth (inches) 5-year 1.50" 100-year 2.52"

The rainfall intensity equation for the Rational Method was taken from Drainage Criteria Manual Volume 1 Figure 6-5.

# Hydraulic Grade Line Analysis

StormCAD was utilized to analyze the proposed storm sewer system and determine the Hydraulic Grade Line (HGL's) profiles for the major and minor storms. The standard method was used to calculate head loss in the system with K coefficients taken from Table 9-4 of the Colorado Springs DCM.

In addition to the DCM, The Mile High Flood District BMP Sizing (UD-BMPv.3.07) and Detention Design (MHFD Detention v4.06) worksheets were utilized to verify the existing water quality ponds still functions with the revised tributary areas and impervious values. The MFHD-Inlet v5.02 worksheet was utilized to calculate both the street capacities and evaluate inlet capacities.

# **Floodplain Statement**

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0756G, revised December 7, 2018. No portion of this site is located within the 100-year floodplain. See Appendix.



# **Existing Drainage Conditions**

As the site has been graded previously with the development of Filing 1, the vegetation is sparse, consisting primarily of native grasses and weeds. Existing site terrain generally slopes from north to southwest at grade rates that vary between 1.2% and 2%. A soil retention wall runs along the eastside of the proposed site, next to U.S. Highway 24 and N. Marksheffel Road, and borders a large portion of the back of the proposed lot. An existing WQ Sand Filter Pond 3 has been constructed on the southwest corner and along the west edge of the site, which will serve as a singular water quality pond for Lot 2 and El Jefe Heights (private street). An existing 18"/24" ADS private storm drain has been constructed along the east side of Meadowbrook Parkway and into Claremont Business Park 2 Filing No.2 that extends to this existing WQ Sand Filter Pond 3.

The proposed project will construct a commercial building, drive thru, drive aisles, parking, landscaping and utilities through the south half of the site, the existing and proposed drainage analysis will be expanded to evaluate changes in drainage patterns to ensure no negative affects to downstream facilities. An existing conditions drainage map is included in the appendix of this report to accompany the following discussion.

Basins that have remained unchanged from the **Final Drainage Report for Claremont Business Park 2 Filing No. 2** prepared by M&S Civil Consultants, Inc., will herein be identified with \*\* within the report, rational sheets and drainage maps.

# **Existing Conditions Detailed Drainage Discussion**

**Design Point 1** (Q5 = 0.6 cfs, Q100 = 3.9 cfs) consists of runoff from undeveloped **Basins \*\*C**, **\*\*C1**, **D**, and **D1**. **Basins \*\*C** and **\*\*C1** are 0.12 and 0.17 acres of existing roadway embankment located generally between the subject site and existing Marksheffel Road. **Basins D** and **D1** are 0.77 and 0.63 acres of undeveloped portions of the subject site. Runoff from the four basins is conveyed to an existing 30" dome grate inline storm system, located south and west of the site at **DP1**. An existing 18" RCP (**Pipe Run 1 (PR1**)) will outfall the captured flows into an existing WQ Sand Filter Pond 3, located at the southwest corner of the site.

**Design Point 2** (Q5 = 2.2 cfs, Q100 = 6.9 cfs) consists of runoff from **Basin D2**, **Basin\*\*E1**, **\*\*E2** and **Design Point 1 (DP1)**. **Basin D2** is 0.15 acres of existing WQ Sand Filter Pond 3, **Basins \*\*E1** and **\*\*E2** consists 0.27 and 0.21 acres of existing EI Jefe Heights (asphalt paving, curb and gutter and landscaped areas) and **DP1**. Runoff from these basins flow into an existing WQ Sand Filter Pond 3 via existing 18" RCP pipes from EI Jefe Heights and from **DP1**. Runoff will be routed via an existing outfall structure and into the existing storm system which ultimately conveys runoff southwest into the East Fork of Sand Creek.

# Four Step Process

The development will follow the "Four Step Process" as outlined below:



# Step 1 - Employ Runoff Reduction Practices

The proposed development uses Low Impact Development (LID) practices to reduce runoff. When possible, runoff is to be directed to pervious areas to promote infiltration and limit directly connected impervious areas.

# Step 2 - Stabilize Drainageways

There are no drainageways on-site to stabilize. The site is upstream of an existing 42"/48" RCP storm sewer system that discharges directly into the Sand Creek Channel via an outlet structure with wingwalls (privately owned and maintained by the Central Marksheffel Metropolitan District). The Claremont Business Park 2 Filing No.2 site has a Sand Filter Water Quality Facility, that will be constructed and/or concurrently constructed with development of this site, that will treat runoff prior to discharging to the existing storm sewer system. There will be no adverse effects on downstream developments as a result of the development of this subdivision.

# Step 3 - Provide Water Quality Capture Volume

One (1) Sand Filter Basin Water Quality Facility is existing or will be constructed concurrently with the development of Lot 2 Claremont Business Park 2 Filing No.2 to provide WQCV at the time of the writing of this report.

# Step 4 - Consider Need for Industrial and Commercial BMP's

This submittal provides a Preliminary Grading and Erosion Control plan. A Final GEC plan with BMPs in place shall be required with final approval of this report, Grading Plan and construction drawings. The proposed project will use silt fence, a vehicle tracking control pad, a concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site.

# **Proposed Drainage Characteristics**

# **General Concept Drainage Discussion**

The "Final Drainage Report for Claremont Business Park 2 Filing No. 2", dated February 2023, by M&S Civil Consultants, Inc. indicated that flows discharged from the subject site were to be collected and conveyed to the East Fork of Sand Creek Channel via a storm system that was to parallel Meadowbrook Parkway. As a portion of the construction of Claremont Business Park 2 Filing No.2 the existing storm sewer system was extended along the eastern side of Meadowbrook Parkway to collect runoff from the Lots 1, 2 & 3 of Claremont Business Park 2 Filing No.2 re-plat and thus remain in compliance with the previous drainage plans and studies.

A permanent water quality pond (WQ Sand Filter Pond 3) has been constructed at the southwest corner of Lot 2 to provide treatment for the proposed roadway and Lot 2. An existing private 18" RCP has been installed to capture runoff from Lot 2 and outfalls into existing WQ Sand Filter Pond 3.



A proposed conditions drainage map is included in the Appendix of this report to accompany the following discussion.

Basins that have remained unchanged from the Final Drainage Report for Claremont Business Park 2 Filing No. 2 prepared by M&S Civil Consultants, Inc., approved 11/13/2023, will herein be identified with \*\* within the report, rational sheets and drainage maps. Basins that have changed from the Final Drainage Report for Claremont Business Park 2 Filing No. 2 prepared by M&S Civil Consultants, Inc., will herein be identified with # within the report, rational sheets and drainage maps. Basins, Design Points and Pipe Runs that are describing the ultimate build out (fully developed) of Lot 2, will herein be identified with \*\*\* within the report, rational sheets and drainage maps.

The ultimate build out models Lot 2 in the future should it get developed, showing the runoff coefficient for the 5- and 100-year events, as well as calculating proposed flows to the existing WQ Sand Filter Pond 3. The following Proposed Conditions Detailed Drainage Discussion Design Point 1, 2, and 3 describes the interim, where the interim includes only the proposed building shown in the Proposed Conditions Drainage Map and does not account for future development on Lot 2. The Design Point \*\*\*1 (Ultimate Build Out, 2 Ultimate Build Out (the same for interim and ultimate), and \*\*\*3 (Ultimate Build Out) models a proposed future development on Lot 2. There is no planned second development for Lot 2 at this time, however this Ultimate Build Out accounts for future development and proposed future flows to WQ Sand Filter Pond 3.

An individual drainage letter and/or report will be required with the development of the north half of Lot 2. The ultimate build out model is used to size and demonstrate the runoff routing and proposed storm system is designed properly if and when Lot 2 north gets developed. The drainage letter for the north half must demonstrate the same runoff routing and flow calculations or show the system still works if there are changes to this proposed design.

# **Proposed Conditions Detailed Drainage Discussion**

**Design Point 1** (Q5 = 0.3 cfs, Q100 = 1.6 cfs) consists of runoff from undeveloped **Basins #C** and partially developed **Basin #D**. **Basins #C** is 0.04 acres of existing roadway embankment located generally between the subject site and existing Marksheffel Road. **Basins #D** is 0.47 acres of partially developed land with asphalt roadway, a 5' Type R Inlet and curb and gutter, the majority of this basin is undeveloped. Runoff from these basins is routed to a proposed 5' Type R sump inlet. Runoff to this inlet will be conveyed via a proposed 15" PP pipe (**Pipe Run 1 (PR1,** Q5 = 0.3 cfs, Q100 = 1.6 cfs)) to **Design Point 2 (DP2)** and eventually to existing WQ Sand Filter Pond 3.

**Design Point 2** (Q5 = 3.7 cfs, Q100 = 7.2 cfs) consists of runoff from **Basin #C1** and developed **Basin #D1**. **Basin #C1** is 0.26 acres of existing roadway embankment located generally between the subject site and existing Marksheffel Road. **Basins #D1** is 0.93 acres of the developed portion of the subject site. Development includes connection with the existing drive entrance and construction of a commercial building, drive thru, drive aisles, parking, landscaping and utilities through the south half of the site. A small portion of the site is undeveloped. Runoff from these basins is routed to a proposed 5' Type R inlet.



Removal of approximately 12' of existing 18" RCP will be required to install the proposed inlet. The inlet shall be installed with non-shrink cementitious grout to fill voids and fasten the inlet and pipe together. The remaining existing 18" RCP (**Pipe Run 2** (**PR2**, Q5 = 4.0 cfs, Q100 = 8.8 cfs)) will route the combined captured flows from **DP1** and **DP2** and will outfall into an existing WQ Sand Filter Pond 3, located at the southwest corner of the site. The flows routed to existing WQ Sand Filter Pond 3 from Lot 2 are less than the flows cited in the approved Claremont Business Park 2 Filing No.2 Final Drainage Report (**PR6A**, Q5 = 6.0 cfs, Q100 = 11.6 cfs), hence there will be no negative impact on the downstream storm system.

**Design Point 3** (Q5 = 6.1 cfs, Q100 = 12.9 cfs) consists of runoff from **Basin #D2**, **Basin\*\*E1**, **\*\*E2** and **PR2**. **Basin D2** is 0.15 acres of existing WQ Sand Filter Pond 3, **Basins \*\*E1** and **\*\*E2** consists 0.27 and 0.21 acres of existing EI Jefe Heights (asphalt paving, curb and gutter and landscaped areas) and **PR2**. Runoff from these basins flow into an existing WQ Sand Filter Pond 3 via existing 18" RCP pipes from EI Jefe Heights and from **PR2**. Runoff will be treated and routed via an existing outfall structure and into the existing storm system which ultimately conveys runoff southwest into the East Fork of Sand Creek. The flows routed to existing WQ Sand Filter Pond 3 are less than the flows cited in the approved Claremont Business Park 2 Filing No.2 Final Drainage Report (DP6, Q5 = 7.8 cfs, Q100 = 14.6 cfs), hence there will be no negative impact on the existing WQ Pond 3 and the downstream storm system.

**Design Point \*\*\*1 (Ultimate Build Out)** (Q5 = 1.8 cfs, Q100 = 3.4 cfs) consists of runoff from undeveloped **Basins #C** and future developed **Basin \*\*\*D**. **Basins #C** is 0.04 acres of existing roadway embankment located generally between the subject site and existing Marksheffel Road. **Basins \*\*\*D** has no current builder but has been assigned a commercial area runoff coefficient number (5-yr 0.81 and 100-yr 0.88) applied to it. **Basins \*\*\*D** is 0.47 acres of future developed land and will route flows to a 5' Type R sump inlet. Runoff to this inlet will be conveyed via a proposed 15" PP pipe (**Pipe Run 1** (**PR1**, Q5 = 1.8 cfs, Q100 = 3.4 cfs)) to **Design Point 2 (DP2)** and eventually to existing WQ Sand Filter Pond 3.

**Design Point 2 (Ultimate Build Out)** (Q5 = 3.7 cfs, Q100 = 7.2 cfs) consists of runoff from **Basin #C1** and developed **Basin #D1**. **Basin #C1** is 0.26 acres of existing roadway embankment located generally between the subject site and existing Marksheffel Road. **Basins #D1** is 0.93 acres of the fully developed portion of the subject site. Development includes connection with the existing drive entrance and construction of a commercial building, drive thru, drive aisles, parking, landscaping and utilities through the south half of the site. Runoff from these basins is routed to a proposed 5' Type R sump inlet. Removal of approximately 12' of existing 18" RCP will be required to install the proposed inlet. The inlet shall be installed with non-shrink cementitious grout to fill voids and fasten the inlet and pipe together. The remaining existing 18" RCP (**Pipe Run \*\*\*2** (**PR\*\*\*2**, Q5 = 5.5 cfs, Q100 = 10.6 cfs)) will route the combined captured flows from **DP1** and **DP2** and will outfall into an existing WQ Sand Filter Pond 3, located at the southwest corner of the site. The flows routed to existing WQ Sand Filter Pond 3 from Lot 2 are less than the flows cited in the Claremont Business Park 2 Filing No.2 Final Drainage Report (**PR6A**, Q5 = 6.0 cfs, Q100 = 11.6 cfs), hence there will be no negative impact on the downstream storm system.

Design Point\*\*\*3 (Q5 = 7.3 cfs, Q100 = 14.6 cfs) consists of runoff from Basin #D2, Basin\*\*E1, \*\*E2 and PR\*\*\*2. Basin #D2 is 0.15 acres of existing WQ Sand Filter Pond 3, Basins \*\*E1 and \*\*E2 consists 0.27 and 0.21 acres of existing El Jefe Heights (asphalt paving, curb and gutter and landscaped areas) and



**PR\*\*\*2**. Runoff from these basins flow into an existing WQ Pond 3 via existing 18" RCP pipes from El Jefe Heights and from **PR\*\*\*2**. Runoff will be treated and routed via an existing outfall structure and into the existing storm system which ultimately conveys runoff southwest into the East Fork of Sand Creek. The flows routed to existing WQ Sand Filter Pond 3 are equivalent to the flows cited in the approved Claremont Business Park 2 Filing No.2 Final Drainage Report (**DP6**, Q5 = 7.8 cfs, Q100 = 14.6 cfs), hence there will be no negative impact on the existing WQ Sand Filter Pond 3 and the downstream storm system.

# Water Quality Provision and Maintenance

The subject site was previously analyzed within the Final Drainage Report for Claremont Business Park 2 Filing No. 2 prepared by M&S Civil Consultants, Inc. Per Resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Filing 2. The water quality volume required for the site has been determined using the MHFD UD-Detention workbook per the guidelines set forth in the City of Colorado Springs/El Paso County Drainage Criteria Manual - Volume II.

As previously discussed, water quality for the site will be provided by an existing WQ Sand Filter Basin Pond 3, PCD Filing NO. VR233. WQ Sand Filter Pond 3 is to be constructed prior to development of Lot 2 or concurrently with development of Lot 2 and will function to treat runoff from the newly constructed improvements (roadway, sidewalks) and Lot 2 or approximately 2.32 acres at 80.3% imperviousness. WQ Sand Filter Pond 3 will provide 0.051 acre-feet of water quality storage and shall be maintained by the property owners. Flows tributary to the WQ Sand Filter Pond 3 are released through outlet structure into an existing storm sewer system located along Meadowbrook Parkway. Access shall be granted to the owner and El Paso County for access and maintenance of the private WQ Sand Filter Basin Pond 3 facility. A private maintenance agreement document shall accompany the final drainage report submittal with construction of the WQ Sand Filter Pond 3.

# **Erosion Control**

It is the policy of the El Paso County that a grading and erosion control plan (GEC) with the drainage report. The GEC incorporates silt fence, vehicle traffic control, inlet and outlet controls, sediment basin and other best management practices (BMP's) as identified in the DCM Volume 2.

# **Construction Cost Opinion**

Private Drainage Facilities (NON-Reimbursable) Including Sand Filter WQ Pond 3:

Item	Description	Quantity	Unit Cost	Cost
	Remove 18" RCP & 30" Grate inline			
1.	storm	12 LF	\$50 /LF	\$600.00
2.	15" PP	66 LF	\$55 /LF	\$3,630.00
3.	Type R 5' Sump Inlet	1 EA	\$6,500 /EA	\$6,500.00
2.	Type R 5' Sump Inlet connect to Ex. RCP	1 EA	\$7,500 /EA	\$7,500.00



	\$18,230.00
Engineering Costs (10%)	\$1,823.00
Total	\$20,053.00

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost in 2023.

# **Drainage and Bridge Fees**

This site is in the Sand Creek Drainage Basin. The site was previously subdivided into ten commercial lots as a portion of Claremont Business Park 2, Filing No.1. The proposed site has been re-platted as Claremont Business Park 2, Filing No.2.

Drainage fees were paid at the time of the previous platting as Tract C of Claremont Business Park Filing No. 2 (Reception No. 207712506), therefore no additional Drainage Bridge and/or Pond fees are required.

# Summary

The proposed design meets the design assumptions utilized in the "Final Drainage Report for Claremont Business Park 2 Filing No. 2", by M&S Civil Consultants, Inc. The "Final Drainage Report for Claremont Business Park 2 Filing No. 2" calculated that DP 6 generated of (Q5=7.8 cfs and Q100=14.6). The proposed development (Lot 2, DP3) will generate Q5=6.1 cfs and Q100=12.9 which is less than what was anticipated by the Final Drainage Report for Claremont Business Park 2 Filing No. 2. Also, the ultimate build out of the proposed development (Lot 2, DP\*\*\*3) will generate Q5=7.5 cfs and Q100=14.6 which is less than what was anticipated by the Final Drainage Report for Claremont Business Park 2 Filing No. 2. Therefore, the proposed development shall not have a negative impact on the downstream storm system and is adequately sized to convey the proposed generated flows. Thus, the development of Lot 2 Claremont Business Park 2 Filing No.2 shall not adversely affect the surrounding development. The proposed drainage facilities will adequately convey, detain and route runoff from the onsite & offsite flows to existing facilities. Owner/developer of the lot shall comply with this final drainage report that will be submitted. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions.



640 220 00

# References

- 1. "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2. "Urban Storm Drainage Criteria Manual"
- Soil Survey Staff, Natural Resources Conservation Service, United States Department of Agriculture. Web Soil Survey. Available online at the following link: <u>http://websoilsurvey.sc.egov.usda.gov/</u>. Accessed: February 02, 2023.
- 4. Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective dated December 7, 2018.
- 5. "Final Drainage Report for Claremont Business Park 2 Filing No. 1", by M&S Civil Consultants, approved 2/11/2021.
- 6. Final Drainage Report for Claremont Business Park 2 Filing No. 2, by M&S Civil Consultants, approved 11/13/2023.
- 7. "Final Drainage Letter for Lot 5 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 03/03/2021.
- 8. "Final Drainage Letter for Lot 6 of Claremont Business Park 2 Filing No.1", by M&S Civil Consultants, approved 07/08/2021.



Appendix



Vicinity Map





8/5/2023 1:08 PM

Soils Map



LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO. 2



Map unit symbol	Map unit name	Rating
8	Blakeland loamy sand, 1 to 9 percent slopes	А
10	Blendon sandy loam, 0 to 3 percent slopes	В
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	А



FEMA FIRM Panel





8/5/2023 1:03 PM





# NOTES TO USERS

information and questions about this Flood FIRM, including historic versions, the curre he National Flood Insurance Program (NFIF 77-FEMA-MAP (1-877-336-2627) or visit th ance Study Rep firectly from the

nities annexing land on adjacent FIRM panels must obtain a current copy of the adjacent panel as well urrent FIRM Index. These may be ordered directly from the Flood Map Service Center at the number

Report for this junsaiction

Program at 1-800-638-6620. agent or call the National

nation shown on this FIRM was provided in digital format by the United States Geological Sun-hown is the USGS National Map: Ortholmagery. Last refreshed October, 2020.

tred from FEMA's National Flood Hazard Layer (NFHL) on 12/27/2022 3:40 PM and does or amendments subsequent to this date and time. The NFHL and effective information may superseded by new date over inne. For additional information, please are the Flood Hazard Powerview Fact Sheet at https://www.fema.gov/media-library/assets/documents/118418

FEMA's

A's standards for the use of digital flo ss with FEMA's basemap accuracy st elements do not appear: basemap in ty identifiers, FIRM panel number, an Ifood maps if it is not wold as described below, y standards. This map image is woid if the one to imagery, flood zone labels, legend, scale bar, and FIRM effective date.

# SCALE

Map Projection: GCS, Geodetic Reference System 1980; Vertical Datum: NAVD88

1:6,000

500 1,000 .500

tudy (FIS) Report for

200 300 400

50 100 2,000 Feet

 $\circ$ 

250 500

Scale in Feet FIRM MAP 1000

PARK 2 FILING NO. 2

SITE BOUNDARY

LEGEND

NATIONAL FLOOD INSURANCE PROGRAM PANEL 756 OF 1275

😻 FEMA

COMMUNITY EL PASO COUNTY CITY OF COLORADI SPRINGS

National Flood Insurance Program

MAP NUMBER 08041C0756G EFFECTIVE DATE December 07, 2018

3 500'

datum for elevation features, datum to create this map, please see the Flood nunity at https://msc.fema.gov

1 inch = 500 feet

# HYDROLOGIC CALCULATIONS



# FINAL DRAINAGE REPORT FOR LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO.2 EXISTING DRAINAGE CALCULATIONS (Area Runoff Coefficient Summary)

			R( ASPHA	00FS 0.73-0 LT DRIVES	).81 0.90-0.96	PARKS 0.12 YARD 0.3 AREAS 0. A	2-0.39 GRAVE 30-0.50 LIGHT 59-0.70 COM IREAS 0.81-0.4	L STORAGE F INDUST MERCIAL 88	GREEN	BELTS/AGRI.	WEIGHTED		
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
**C	5372.3	0.12	0.00	0.90	0.96	0.00	0.12	0.39	0.12	0.09	0.36	0.09	0.36
**C1	7457.3	0.17	0.00	0.90	0.96	0.00	0.12	0.39	0.17	0.09	0.36	0.09	0.36
D	33587.9	0.77	0.00	0.90	0.96	0.03	0.12	0.39	0.74	0.09	0.36	0.09	0.36
D1	27332.4	0.63	0.00	0.90	0.96	0.15	0.12	0.39	0.48	0.09	0.36	0.10	0.37
D2	6696.0	0.15	0.00	0.90	0.96	0.03	0.12	0.39	0.12	0.09	0.36	0.10	0.37
**E1	11683.7	0.27	0.22	0.90	0.96	0.05 0.81		0.81 0.88		0.09	0.36	0.88	0.95
**E2	9082.0	0.21	0.17	0.90	0.96	0.04	0.81	0.88	0.00	0.09	0.36	0.88	0.95

\*\*~ Claremont Business Park 2 Filing No.2 FDR, prepared by MS Civil Consultants, Inc.

Calculated by:	GT
Date:	8/2/2023
Checked by:	VAS

# (Area Drainage Summary)

From Area Runoff	Coefficient Summ	uary			OVERLA	IND		ST	REET / CH	ANNEL FLO	DW	Time of T	ravel (T <sub>t</sub> )	INTEN	SITY *	TOTAL FLOWS	
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	*TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
**C	0.12	0.09	0.36	0.09	40	16.0	3.4	0	0.0%	0.0	0.0	5.0	10.2	5.2	8.7	0.1	0.4
**C1	0.17	0.09	0.36	0.09	60	22.0	4.3	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.1	0.5
D	0.77	0.09	0.36	0.09	60	1.2	11.2	250	1.6%	1.9	2.2	13.4	11.7	3.9	6.5	0.3	1.8
D1	0.63	0.10	0.37	0.10	60	1.2	11.2	250	1.6%	1.9	2.2	13.4	11.7	3.9	6.5	0.2	1.5
D2	0.15	0.10	0.37	0.10	15	6.0	2.1	63	0.5%	0.7	1.5	5.0	10.4	5.2	8.7	0.1	0.5
**E1	0.27	0.88	0.95	0.88	30	0.6	1.7	280	2.0%	2.8	1.6	5.0	11.7	5.2	8.7	1.2	2.2
**E2	0.21	0.88	0.95	0.88	30	0.6	1.7	280	2.0%	2.8	1.6	5.0	11.7	5.2	8.7	1.0	1.7

\* Intensity equations assume a minimum travel time of 5 minutes.

\*\*~ Claremont Business Park 2 Filing No.2 FDR, prepared by MS Civil Consultants, Inc.

Calculated by: GT

Date: 8/2/2023 Checked by: VAS

# FINAL DRAINAGE REPORT FOR LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO.2 EXISTING DRAINAGE CALCULATIONS (Basin Routing Summary)

	From Area Runoff Coefficient Summary			OVERLAND				PIPE / CHANNEL FLOW				Time of Travel $(T_t)$	e of Travel (T <sub>t</sub> ) INTENSITY *		TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA100	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	*TOTAL	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>	COMMENTS
	DPS AND/OR PIPES				(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	**C, **C1, D, D1	0.16	0.61			Bas	in D Tc used	+ Basin D1 r	outing			12.3	3.8	6.4	0.6	3.9	Existing 30" Dome Grate
							11.7	56	1.0%	1.5	0.6						
2	D2, **E1, **E2, DP1	0.59	1.12			D	P1 Tc used +	Basin D2 rou	ting			13.8	3.6	6.1	2.2	6.9	Existing WQ Pond 3
							12.3	63	0.5%	0.7	1.5						

\* Intensity equations assume a minimum travel time of 5 minutes.

\*\*~ Claremont Business Park 2 Filing No.2 FDR, prepared by MS Civil Consultants, Inc.

Calculated by: GT

Date: 8/2/2023 Checked by: VAS

# (Storm Sewer Routing Summary)

					Inten	sity*	Fle	ow	Pipe Size
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA 100	Maximum T <sub>C</sub>	Ι <sub>5</sub>	I 100	<b>Q</b> 5	<b>Q</b> 100	
1	DP1	0.16	0.61	12.3	3.8	6.4	0.6	3.9	EX 18" RCP
* Intensity equat	ions assume a minimum travel time of 5 minu	ites.			C	alculated by:	GT		

DP - Design Point PR - Pipe Run FB- Flow By from Design Point INT- Intercepted Flow from Design Point Date: 8/2/2023 Checked by: VAS

# (Area Runoff Coefficient Summary)

			Ri ASPHAI	OOFS 0.73-0 LT DRIVES	0.81 0.90-0.96	P LANDSC GRAVEL S LIGHT IN COMMEN	ARKS 0.12-0.3 APED AREAS TORAGE YAH IDUST AREAS RCIAL AREAS	89 1 0.16-0.41 2D 0.30-0.50 5 0.59-0.70 5 0.81-0.88	GREEN	BELTS/AGRI.	WEIGHTED		
BASIN	TOTAL AREA <i>(SF)</i>	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
#C	1664.0	0.04	0.00	0.90	0.96	0.00	0.16	0.41	0.04	0.09	0.36	0.09	0.36
#C1	11176.5	0.26	0.00	0.90	0.96	0.00	0.16	0.41	0.26	0.09	0.36	0.09	0.36
# <b>D</b>	20496.0	0.47	0.03	0.90	0.96	0.07	0.12	0.39	0.37	0.09	0.36	0.15	0.40
***D	20496.0	0.47	0.00	0.90	0.96	0.47	0.81	0.88	0.00	0.09	0.36	0.81	0.88
# <b>D</b> 1	40410.0	0.93	0.00	0.90	0.96	0.93	0.81	0.88	0.00	0.09	0.36	0.81	0.88
#D2	6696.0	0.15	0.00	0.90	0.96	0.15	0.12	0.39	0.00	0.09	0.36	0.12	0.39
**E1	11683.7	0.27	0.22	0.90	0.96	0.05 0.81		0.88	0.00	0.09	0.36	0.88	0.95
**E2	9082.0	0.21	0.17	0.90	0.96	0.04	0.81	0.88	0.00	0.09	0.36	0.88	0.95

\*\*~ Claremont Business Park 2 Filing No.2 FDR Prepared by MS Civil Consultants, Inc.

#~ Basin area revised from Claremont Business Park 2 Filing No.2 FDR Prepared by MS Civil Consultants, Inc.

\*\*\*~ Ultimate build out. Development of Lot 2 (North half)

Calculated by: GT Date: 2/2/2024 Checked by: VAS

# (Area Drainage Summary)

From Area Runoff	Coefficient Summ	ary			OVERL	4ND		ST	REET / CH	ANNEL FLO	DW	Time of T	ravel $(T_t)$	INTEN	SITY *	TOTAL FLOWS							
BASIN	AREA TOTAL	C <sub>5</sub> C <sub>100</sub>		C <sub>5</sub> C <sub>100</sub>		C <sub>5</sub> C <sub>100</sub>		AREA TOTAL C5 C100		C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	*TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>
	(Acres)	5) From DCM Table 5-1			(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)						
#C	0.04	0.09	0.36	0.09	40	16.0	3.4	0	0.0%	0.0	0.0	5.0	10.2	5.2	8.7	0.0	0.1						
#C1	0.26	0.09	0.36	0.09	60	22.0	4.3	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.1	0.8						
#D	0.47	0.15	0.40	0.15	60	2.0	9.0	215	3.0%	2.6	1.4	10.3	11.5	4.1	6.8	0.3	1.3						
***D	0.47	0.81	0.88	0.81	40	1.5	2.1	268	2.6%	3.2	1.4	5.0	11.7	5.2	8.7	2.0	3.6						
#D1	0.93	0.81	0.88	0.81	30	2.0	1.5	250	1.4%	2.4	1.8	5.0	11.6	5.2	8.7	3.9	7.1						
#D2	0.15	0.12	0.39	0.12	15	6.0	2.0	63	0.5%	1.4	0.7	5.0	10.4	5.2	8.7	0.1	0.5						
**E1	0.27	0.88	0.95	0.88	30	0.6	1.7	280	2.0%	2.8	1.7	5.0	11.7	5.2	8.7	1.2	2.2						
**E2	0.21	0.88	0.95	0.88	30	0.6	1.7	280	2.0%	2.8	1.7	5.0	11.7	5.2	8.7	1.0	1.7						

\* Intensity equations assume a minimum travel time of 5 minutes.

\*\*~ Claremont Business Park 2 Filing No.2 FDR Prepared by MS Civil Consultants, Inc.

#~ Basin area revised from Claremont Business Park 2 Filing No.2 FDR Prepared by MS Civil Consultants, Inc.

\*\*\*~ Ultimate build out. Development of Lot 2 (North half)

Calculated by: GT Date: 2/2/2024 Checked by: VAS

# (Basin Routing Summary)

	From Area Runoff Coefficient Summary				OVE	ERLAND		PIPE	/ CHA	NNEL FLO	)W	Time of Travel (T <sub>1</sub> )	INTEN	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	Tt	*TOTAL	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>	COMMENTS
	DPS AND/OR PIPES				(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	#C, #D	0.07	0.20			Bas	in #C Tc + B	asin D routing	g used			6.4	4.8	8.1	0.3	1.6	Proposed 5' Type R Inlet
							5.0	215	3.0%	2.6	1.4						
***1	#C, ***D	0.38	0.43		-	Basin	#C Tc + Bas	sin ***D routi	ng used			6.4	4.8	8.1	1.8	3.4	Proposed 5' Type R Inlet
							5.0	268	2.6%	3.2	1.4						
2	#C1, #D1	0.77	0.91			Basin	#C1 Tc used	l + Basin #D1	routing			6.8	4.7	7.9	3.7	7.2	Proposed 5' Type R Inlet
							5.0	250	1.4%	2.4	1.8						
3	#D2, PR2, **E1, **E2	1.29	1.62				DP2	Tc used			•	6.8	4.7	7.9	6.1	12.9	Existing WQ Pond 3
***3	#D2, ***PR2, **E1, **E2	1.60	1.85	DP2				Tc used				6.8	4.7	7.9	7.5	14.6	Existing WQ Pond 3

\* Intensity equations assume a minimum travel time of 5 minutes.

\*\*~ Claremont Business Park 2 Filing No.2 FDR Prepared by MS Civil Consultants, Inc.

#~ Basin area revised from Claremont Business Park 2 Filing No.2 FDR Prepared by MS Civil Consultants, Inc.

\*\*\*~ Ultimate build out. Development of Lot 2 (North half)

MS CIVIL, INC. Prop Drainage Calculations 24-02-02.xls

Page 1 of 1

Calculated by: <u>GT</u> Date: 2/2/2024

Checked by: VAS

					Inter	nsity*	Fl	ow	Pipe Size
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA 100	Maximum T <sub>C</sub>	Ι <sub>5</sub>	I 100	Q 5	<b>Q</b> 100	
1	DP1	0.07	0.20	6.4	4.8	8.1	0.3	1.6	PROP 15" PP
***1	***DP1	0.38	0.43	6.4	4.8	8.1	1.8	3.4	PROP 15" PP
2	DP2, PR1	0.85	1.11	6.8	4.7	7.9	4.0	8.8	EX 18" RCP
***2	DP2, ***PR1	1.16	1.34	6.8	4.7	7.9	5.5	10.6	EX 18" RCP

(Storm Sewer Routing Summary)

\* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point PR - Pipe Run FB- Flow By from Design Point INT- Intercepted Flow from Design Point Calculated by: GT Date: 2/2/2024

Checked by: VAS

\*\*\*Ulitmate build out. Development of Lot 2 (north half)

HYDRAULIC CALCULATIONS / SFB WQCV CALCULATIONS



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



	DE	TENTION	Basin Out	LET STRU	CTURE DES	SIGN		
Project:	Claremont Busine	M ss Park 2 Filing No.	1HFD-Detention, V 2	ersion 4.06 (July 2	2022)			
Basin ID:	Lot 2 - Pond 3	EX WQ SAND FILTER PONI	3 DESIGNED AND CONST	RUCTED WITH PCD FILIN	G NO. VR 233)			
				Estimated	Estimated			
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type	I.	
			Zone 1 (WQCV)	1.44	0.051	Filtration Media		
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (100-year)	5.18	0.288	Weir&Pipe (Restrict)		
PERMANENT ORIFICES	Configuration (Re	tention Pond)	Zone 3				_	
		China - Filtratian Dh		Total (all zones)	0.339	l		have faulte danderin
User Input: Orifice at Underdrain Outlet (typical	y used to drain WQ	CV IN a FIITRATION BIN	<u>1P)</u> the filtration media	surface)	Under	train Orifice Area –		ers for Underdrain
Underdrain Orifice Diameter =	0.84	inches		surface)	Underdrair	Orifice Centroid =	0.04	feet
User Input: Orifice Plate with one or more orific	es or Elliptical Slot \	Neir (typically used	to drain WQCV and	I/or EURV in a sedir	mentation BMP)		Calculated Paramet	ters for Plate
Centroid of Lowest Orifice =	N/A	ft (relative to basin	bottom at Stage =	0 ft)	WQ Orifi	ice Area per Row =	N/A	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin	bottom at Stage =	0 ft)	Elli	ptical Half-Width =	N/A	feet
Orifice Plate: Orifice Area per Row -	N/A N/A	inches			Ellipt	illintical Slot Area -	N/A N/A	reet
Office Place. Office Area per Row -	N/A	sq. menes			L		N/A	ir.
User Input: Stage and Total Area of Each Orific	e Row (numbered fi	rom lowest to highe	<u>st)</u>					
	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
	Row 9 (optional)	Row 10 (ontional)	Row 11 (optional)	Row 12 (ontional)	Row 13 (optional)	Row 14 (ontional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
User Input: Vertical Orifice (Circular or Rectange	<u>ular)</u>		I				Calculated Paramet	ters for Vertical Orif
Invert of Vertical Orifica -	Not Selected	Not Selected	ft (rolativo to bacir	bottom at Stago -	0 ft) \/o	tical Orifica Araa -	Not Selected	Not Selected
Depth at top of Zone using Vertical Orifice =			ft (relative to basir	bottom at Stage =	0 ft) Vertica	I Orifice Centroid =		
Vertical Orifice Diameter =			inches	bottom ut Stuge -	vertice			LI
		1						
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoida	al Weir and No Outl	et Pipe)		Calculated Paramet	ters for Overflow W
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and Zone 2 Weir	Outlet Pipe OR Rect Not Selected	tangular/Trapezoida	al Weir and No Outl	et Pipe)	a linner Edge, H. –	Calculated Paramet Zone 2 Weir	ters for Overflow W Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	r Sloped Grate and Zone 2 Weir 1.45 3.00	Outlet Pipe OR Rect Not Selected	tangular/Trapezoida ft (relative to basin t	al Weir and No Outl	et Pipe) t) Height of Grate Overflow W	e Upper Edge, H <sub>t</sub> = /eir Slope Length =	Calculated Paramet Zone 2 Weir 1.45 3.00	ters for Overflow W Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00	Outlet Pipe OR Rect Not Selected	tangular/Trapezoida ft (relative to basin t feet H:V	al Weir and No Outl pottom at Stage = 0 f Gi	et Pipe) t) Height of Grate Overflow W rate Open Area / 10	e Upper Edge, H <sub>t</sub> = /eir Slope Length = )0-yr Orifice Area =	Calculated Paramet Zone 2 Weir 1.45 3.00 17.58	ters for Overflow W Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00	Outlet Pipe OR Rect Not Selected	tangular/Trapezoida ft (relative to basin t feet H:V feet	al Weir and No Outl pottom at Stage = 0 fi Gi O	et Pipe) t) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open	e Upper Edge, H <sub>t</sub> = /eir Slope Length = )0-yr Orifice Area = Area w/o Debris =	Calculated Paramet Zone 2 Weir 1.45 3.00 17.58 6.26	ters for Overflow W Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00 Type C Grate	Outlet Pipe OR Rec	tangular/Trapezoida ft (relative to basin t feet H:V feet	al Weir and No Outl pottom at Stage = 0 f Gi O O	<u>et Pipe)</u> t) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	e Upper Edge, H <sub>t</sub> = /eir Slope Length = )0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Calculated Paramet           Zone 2 Weir           1.45           3.00           17.58           6.26           1.88	ters for Overflow W. Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00 Type C Grate 70%	Outlet Pipe OR Rec	tangular/Trapezoida ft (relative to basin t feet H:V feet %	al Weir and No Outl bottom at Stage = 0 f G O O (	<u>et Pipe)</u> t) Height of Gratu Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Calculated Paramet Zone 2 Weir 1.45 3.00 17.58 6.26 1.88	ters for Overflow W Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00 Type C Grate 70%	Outlet Pipe OR Rec	tangular/Trapezoida ft (relative to basin t feet H:V feet %	al Weir and No Outl Nottom at Stage = 0 f Gi O O	et Pipe) t) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Calculated Paramet           Zone 2 Weir           1.45           3.00           17.58           6.26           1.88	ters for Overflow W. Not Selected
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00 Type C Grate 70% c (Circular Orifice, R Zone 2 Restrictor	Outlet Pipe OR Rec Not Selected	tangular/Trapezoida ft (relative to basin t feet H:V feet % ectangular Orifice)	al Weir and No Outl Nottom at Stage = 0 f Gi O O (	<u>et Pipe)</u> t) Height of Gratı Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Ope	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = liculated Parameters	Calculated Paramet           Zone 2 Weir           1.45           3.00           17.58           6.26           1.88           s for Outlet Pipe w/           Zone 2 Restrictor	ters for Overflow W Not Selected
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User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Deverflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Ne-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nesults Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00 Type C Grate 70% 2.75 18.00 4.60 Trapezoidal) 4.90 18.00 4.00 1.00 7 <i>The user can oven</i> WQCV N/A 0.051 N/A N/A N/A N/A N/A N/A N/A N/A	Outlet Pipe OR Rec Not Selected	tangular/Trapezoida ft (relative to basin to feet H:V feet % ectangular Orifice) ft (distance below basin inches bottom at Stage = 1/P hydrographs and 2 Year 1.19 0.161 0.161 0.161 0.161 0.161 0.02 3.7 2.2 N/A Overflow Weir 1 0.34 N/A 19 21 1.77	al Weir and No Outl sottom at Stage = 0 ff G O O asin bottom at Stage Half-Cent Half-Cent 0 ft) 1 runoff volumes by 5 Year 1.50 0.208 0.	et Pipe) t) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Ca = 0 ft) O Outle tral Angle of Restric Spillway D Stage at <sup>-</sup> Basin Area at Basin Volume at <sup>-</sup> entering new value 10 Year 1.75 0.249 0.25 	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /o-yr Orifice Area = Area w/o Debris = n Area w/o Debris = n Area w/ Debris = ilculated Parameters utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Top of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Area - 25 Year 2.00 0.297 1.4 0.61 7.0 3.8 2.7 Outlet Plate 1 0.6 N/A 18 20 2.39	Calculated Paramet           Zone 2 Weir           1.45           3.00           17.58           6.26           1.88           s for Outlet Pipe w/           Zone 2 Restrictor           0.36           0.23           1.06           Calculated Paramet           0.19           6.09           0.11           0.43           /rographs table (Col           50 Year           2.25           0.341           0.341           0.39           2.0           0.36           8.1           3.9           2.0           0.6           N/A           17           20           2.65	Flow Restriction Pla Not Selected Flow Restriction Pla Not Selected Not Selected N/A ters for Spillway feet feet acres acre-ft Umns W through Ar 100 Year 2.52 0.393 0.6 N/A
User Input: Overflow Weir (Dropbox with Flat o Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Deverflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Ne-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nesults Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (h) = Cime Tordin 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (h) =	r Sloped Grate and Zone 2 Weir 1.45 3.00 0.00 3.00 Type C Grate 70% 2.75 18.00 4.60 Trapezoidal) 4.90 18.00 4.00 1.00 7 <i>The user can oven</i> WQCV N/A 0.051 N/A N/A N/A N/A N/A N/A N/A N/A	Outlet Pipe OR Rec Not Selected	tangular/Trapezoida ft (relative to basin to feet H:V feet % ectangular Orifice) ft (distance below basin inches bottom at Stage = 1/P hydrographs and 2 Year 1.19 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.161 0.02 3.7 2.2 N/A 19 21 1.77 0.066	al Weir and No Outl sottom at Stage = 0 ff G O O ( asin bottom at Stage Half-Cent • 0 ft) ( <i>runoff volumes by</i> 5 Year 1.50 0.208	et Pipe) t) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Ca = 0 ft) O Outle tral Angle of Restrict Spillway D Stage at Basin Area at Basin Volume at entering new value 10 Year 1.75 0.249 0.25 	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/o Debris = in Area w/ Debris = ilculated Parameters utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Top of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Area 2 Year 2.00 0.297 1.4 0.61 7.0 3.8 2.7 Outlet Plate 1 0.6 N/A 18 20 2.39 0.07 0.17	Calculated Paramet           Zone 2 Weir           1.45           3.00           17.58           6.26           1.88           s for Outlet Pipe w//           Zone 2 Restrictor           0.36           0.23           1.06           Calculated Paramet           0.19           6.09           0.11           0.43           trographs table (Col           0 Year           2.25           0.341           0.341           0.39           0.06           N/A           17           20           2.65           0.07	Flow Restriction Pla Not Selected Flow Restriction Pla Not Selected Not Selected N/A ters for Spillway feet feet acres acre-ft Umns W through Ar 100 Year 2.52 0.393 0.40 1.20 0.40 1.20 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

ĺ	SOURCE	CLIHP	CLIHP	CLIHP	CLIHP	СШНР	CLIHP	СПНЬ	СШНР	CLIHP
Time Interval	TIME	WOCV [cfs]	FURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
E 00 min	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00			
5.00 min	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.05.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	1.22	0.00	1.00	0.99	1.35
	0:20:00	0.00	0.00	1.94	2.48	2.89	1.80	2.07	2.25	2.87
	0:25:00	0.00	0.00	3.68	4.78	5.69	3.59	4.13	4.41	5.68
	0:30:00	0.00	0.00	3.52	4.40	5.15	7.01	8.07	9.04	11.71
	0:35:00	0.00	0.00	2.58	3.17	3.69	6.24	7.15	8.62	11.03
	0:40:00	0.00	0.00	1.91	2.29	2.66	4.96	5.68	6.71	8.58
	0:45:00	0.00	0.00	0.90	1.64	1.94	3.59	4.12	5.18	5.03
	0:55:00	0.00	0.00	0.90	0.95	1.13	1.87	2.14	2.81	3.61
	1:00:00	0.00	0.00	0.66	0.86	1.05	1.46	1.67	2.31	2.98
	1:05:00	0.00	0.00	0.64	0.83	1.03	1.29	1.47	2.12	2.74
	1:10:00	0.00	0.00	0.54	0.81	1.03	1.07	1.22	1.52	1.95
	1:15:00	0.00	0.00	0.48	0.74	1.03	0.96	1.09	1.21	1.56
	1:20:00	0.00	0.00	0.45	0.67	0.91	0.80	0.91	0.88	1.12
	1:30:00	0.00	0.00	0.44	0.63	0.76	0.72	0.68	0.69	0.88
	1:35:00	0.00	0.00	0.43	0.60	0.63	0.55	0.62	0.56	0.70
	1:40:00	0.00	0.00	0.43	0.50	0.61	0.52	0.59	0.54	0.68
	1:45:00	0.00	0.00	0.43	0.45	0.60	0.51	0.57	0.54	0.67
	1:50:00	0.00	0.00	0.43	0.43	0.60	0.50	0.56	0.54	0.67
	1:55:00	0.00	0.00	0.33	0.41	0.57	0.50	0.56	0.54	0.67
	2:00:00	0.00	0.00	0.27	0.38	0.49	0.50	0.56	0.54	0.67
	2:10:00	0.00	0.00	0.14	0.20	0.20	0.20	0.15	0.15	0.18
	2:15:00	0.00	0.00	0.03	0.05	0.06	0.06	0.07	0.07	0.09
	2:20:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.03	0.03
	2:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

# MHFD-Inlet, Version 5.02 (August 2022)

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>Inlet 1 (DP1)</u>	Inlet 1 (DP1) Ultimate	Inlet 2 (DP2) Ultimate
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

### **USER-DEFINED INPUT**

User-Defined Design Flows			
Minor Q <sub>Known</sub> (cfs)	0.3	1.8	3.7
Major Q <sub>Known</sub> (cfs)	1.6	3.4	7.2
Bypass (Carry-Over) Flow from Upstream	Inlets must be organized from upstrea	am (left) to downstream (right) in order fo	or bypass flows to be linked.
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Watershed Characteristics			
Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			
Watershed Profile			
Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			
Minor Storm Rainfall Input			
Design Storm Return Period, T <sub>r</sub> (years)			
One-Hour Precipitation, P <sub>1</sub> (inches)			
Major Storm Rainfall Input			
Design Storm Return Period, T <sub>r</sub> (years)			
One-Hour Precipitation, P <sub>1</sub> (inches)			

# CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	0.3	1.8	3.7
Major Total Design Peak Flow, Q (cfs)	1.6	3.4	7.2
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A	N/A



# INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.02 (August 2022)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.6	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
	_			
Low Head Performance Reduction (Calculated)	-	MINOR	MAJOR	-
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.22	0.50	ft
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	$RF_{Curb} =$	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
	с Г	MINOR	MAJOR	-e-
I otal Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	2.8	9.3	CTS
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	V PEAK REQUIRED =	0.3	1.6	CTS



# INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.02 (August 2022)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.6	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
		MINOR		
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	<b>1</b> 0
Depth for Grate Midwidth	a <sub>Grate</sub> =	N/A	N/A	π c
Depth for Curb Opening Weir Equation	a <sub>Curb</sub> =	0.22	0.50	π
	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	_
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	2.8	9.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	1.8	3.4	cfs



# INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.02 (August 2022)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.5	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Hood Porformance Reduction (Calculated)		MINOR	MAIOR	
Low field Performance Reduction (Calculated)	d –	MINOR	MAJOR N/A	A
Depth for Curb Opening Weir Equation	d –	0.20	0.50	н А
Grated Inlet Performance Reduction Factor for Long Inlets	PE –	0.29 N/A	0.50 N/A	11
Curb Opening Performance Reduction Factor for Long Inlets	PE	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF	1.00 N/A	1.00 N/A	
combination fine renormance reduction ractor for Long filets	Combination -	IN/A	N/A	1
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	4.4	9.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	3.7	7.2	cfs

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.007 ft/ft	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Discharge	0.20 cfs	
Results		
Normal Depth	3.1 in	
Flow Area	0.2 ft <sup>2</sup>	
Wetted Perimeter	1.6 ft	
Hydraulic Radius	1.5 in	
Top Width	1.54 ft	
Critical Depth	2.3 in	
Critical Slope	0.031 ft/ft	
Velocity	1.02 ft/s	
Velocity Head	0.02 ft	
Specific Energy	0.27 ft	
Froude Number	0.501	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	3.1 in	
Critical Depth	2.3 in	
Channel Slope	0.007 ft/ft	
Critical Slope	0.031 ft/ft	

# Worksheet for East Swale Q100=0.2cfs

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.083 ft/ft	
Constructed Depth	15.0 in	
Constructed Top Width	25.00 ft	
Discharge	0.40 cfs	
Results		
Normal Depth	0.8 in	
Flow Area	0.2 ft <sup>2</sup>	
Wetted Perimeter	5.6 ft	
Hydraulic Radius	0.5 in	
Top Width	5.59 ft	
Critical Depth	0.9 in	
Critical Slope	0.035 ft/ft	
Velocity	1.72 ft/s	
Velocity Head	0.05 ft	
Specific Energy	0.11 ft	
Froude Number	1.481	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	0.8 in	
Critical Depth	0.9 in	
Channel Slope	0.083 ft/ft	
Critical Slope	0.035 ft/ft	

# Worksheet for North Swale Q100=0.4cfs

Project Description     Manning Formula       Solve For     Normal Depth       Input Data     Roughness Coefficient     0.030       Channel Slope     0.038 ft/ft       Constructed Depth     18.0 in       Constructed Top Width     30.00 ft       Discharge     0.20 cfs       Results     Image: Coefficient       Normal Depth     0.6 in       Flow Area     0.2 ft²       Wetted Perimeter     5.6 ft       Hydraulic Radius     0.4 in       Top Width     5.59 ft       Critical Depth     0.6 in       Critical Stope     0.040 ft/ft       Velocity     1.03 ft/s       Velocity Head     0.02 ft       Specific Energy     0.07 ft       Froude Number     0.973       Flow Type     Subcritical       GVF Input Data     0.0 in       Downstream Depth     0.0 in       Number Of Steps     0       GVF Output Data     0.00 ft       Upstream Depth     0.0 in       Profile Headloss     0.00 ft       Downstream Nelocity     Infinity ft/s       Upstream Velocity     Infinity ft/s       Upstream Velocity     Infinity ft/s       Upstream Velocity     0.6 in       Critical Gepth     0.6 in			
Friction Method     Manning Formula       Solve For     Normal Depth       Input Data     Roughness Coefficient     0.030       Roughness Coefficient     0.030     Channel Slope     0.038 ft/ft       Constructed Depth     18.0 in     Constructed Depth     18.0 in       Constructed Top Width     30.00 ft     Discharge     0.20 cfs       Results     Normal Depth     0.6 in     Flow Area     0.2 ft <sup>2</sup> Normal Depth     0.6 in     How Area     0.2 ft <sup>2</sup> Wetted Perimeter     5.6 ft     Hydraulic Radius     0.4 in       Top Width     5.59 ft     Critical Depth     0.6 in       Critical Slope     0.040 ft/ft     Velocity     1.03 ft/s       Velocity     1.03 ft/s     Velocity     Specific Energy       Velocity Head     0.02 ft     Specific Energy     0.07 ft       Froude Number     0.973     Flow Type     Subcritical       GVF Input Data     Downstream Depth     0.0 in     Length       Number Of Steps     0     In     Profile Description       N/A     Profile Description     N/A     Profile Description       N/A     Profile Description     N/A     Profile Description       Normal Depth     0.6 in     Critical Depth     0.6 in   <	Project Description		
Formula     Formula       Solve For     Normal Depth       Input Data     0.030       Roughness Coefficient     0.030       Channel Stope     0.038 ft/ft       Constructed Depth     18.0 in       Constructed Top Width     30.00 ft       Discharge     0.20 cfs       Results     Imput Data       Normal Depth     0.6 in       Flow Area     0.2 ft²       Wetted Perimeter     5.6 ft       Hydraulic Radius     0.4 in       Top Width     5.59 ft       Critical Stope     0.040 ft/ft       Velocity     1.03 ft/s       Velocity Head     0.02 ft       Specific Energy     0.07 ft       Froude Number     0.973       Flow Type     Subcritical       GVF Input Data     0.0 in       Downstream Depth     0.0 in       Length     0.0 ft       Number Of Steps     0       GVF Output Data     0.0 in       Upstream Depth     0.0 in       Profile Headloss     0.00 ft       Downstream Velocity     Infinity ft/s       Upstream Velocity     Infinity ft/s       Normal Depth     0.6 in       Critical Depth     0.6 in       Chonnel Stope     0.038 ft/ft <td>Friction Mothod</td> <td>Manning</td> <td></td>	Friction Mothod	Manning	
Solve For         Normal Depth           Input Data         Roughness Coefficient         0.030           Ronnel Slope         0.038 ft/ft         Constructed Depth         18.0 in           Constructed Top Width         30.00 ft         Discharge         0.20 cfs           Results         Normal Depth         0.6 in         Flow Area         0.2 ft²           Normal Depth         0.6 in         Flow Area         0.2 ft²           Wetted Perimeter         5.6 ft         Hydraulic Radius         0.4 in           Top Width         5.59 ft         Critical Depth         0.6 in           Critical Slope         0.040 ft/ft         Velocity         Velocity           Velocity         1.03 ft/s         Velocity         Velocity           Velocity Head         0.02 ft         Specific Energy         0.07 ft           Froude Number         0.973         Flow Type         Subcritical           GVF Input Data         Downstream Depth         0.0 in         Length           Downstream Depth         0.0 in         Profile Headloss         0.00 ft           Number Of Steps         0         0         Frofile Headloss         0.00 ft           Downstream Depth         0.0 in         Profile Headloss <t< td=""><td>Friction Method</td><td>Formula</td><td></td></t<>	Friction Method	Formula	
Input Data           Roughness Coefficient         0.030           Channel Slope         0.038 ft/ft           Constructed Depth         18.0 in           Constructed Top Width         30.00 ft           Discharge         0.20 cfs           Results	Solve For	Normal Depth	
Roughness Coefficient         0.030           Channel Slope         0.038 ft/ft           Constructed Depth         18.0 in           Constructed Top Width         30.00 ft           Discharge         0.20 dfs           Results            Normal Depth         0.6 in           Flow Area         0.2 ft²           Wetted Perimeter         5.6 ft           Hydraulic Radius         0.4 in           Top Width         5.9 ft           Critical Depth         0.6 in           Critical Depth         0.6 in           Critical Slope         0.040 ft/ft           Velocity         1.03 ft/s           Velocity Head         0.02 ft           Specific Energy         0.07 ft           Froude Number         0.973           Flow Type         Subcritical           GVF Input Data         0.0 in           Downstream Depth         0.0 in           Length         0.0 in           Length         0.0 in           Profile Description         N/A           Profile Headloss         0.00 ft           Downstream Depth         0.0 in           Profile Headloss         0.00 ft	Input Data		
Channel Slope       0.038 ft/ft         Constructed Depth       18.0 in         Constructed Top Width       30.00 ft         Discharge       0.20 cfs         Results       Image: Constructed Perimeter         Normal Depth       0.6 in         Flow Area       0.2 ft²         Wetted Perimeter       5.6 ft         Hydraulic Radius       0.4 in         Top Width       5.59 ft         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Slope       0.040 ft/ft         Velocity       1.03 ft/s         Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Downstream Depth       0.0 in         Length       0.0 in         Verice Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Depth       0.0 in         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s <tr< td=""><td>Roughness Coefficient</td><td>0.030</td><td></td></tr<>	Roughness Coefficient	0.030	
Constructed Depth       18.0 in         Constructed Top Width       30.00 ft         Discharge       0.20 cfs         Results       Normal Depth       0.6 in         Normal Depth       0.6 in         Flow Area       0.2 ft²         Wetted Perimeter       5.6 ft         Hydraulic Radius       0.4 in         Top Width       5.59 ft         Critical Depth       0.6 in         Critical Slope       0.040 ft/ft         Velocity       1.03 ft/s         Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 in         Length       0.0 in         Profile Description       N/A         Profile Description       N/A         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in <t< td=""><td>Channel Slope</td><td>0.038 ft/ft</td><td></td></t<>	Channel Slope	0.038 ft/ft	
Constructed Top Width Discharge         30.00 ft           Discharge         0.20 cfs           Results	Constructed Depth	18.0 in	
Discharge0.20 cfsResultsNormal Depth0.6 inFlow Area0.2 ft²Wetted Perimeter5.6 ftHydraulic Radius0.4 inTop Width5.59 ftCritical Stope0.040 ft/ftVelocity1.03 ft/sVelocity Head0.02 ftSpecific Energy0.07 ftFroude Number0.973Flow TypeSubcriticalGVF Input Data0.0 inDownstream Depth0.0 inLength0.0 ftNumber Of Steps0GVF Output Data0.0 inUpstream Depth0.0 inProfile DescriptionN/AProfile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream Depth0.6 inCritical Depth0.6 in/Critical	Constructed Top Width	30.00 ft	
Results         Normal Depth       0.6 in         Flow Area       0.2 ft <sup>2</sup> Wetted Perimeter       5.6 ft         Hydraulic Radius       0.4 in         Top Width       5.59 ft         Critical Depth       0.6 in         Critical Slope       0.040 ft/ft         Velocity       1.03 ft/s         Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0.0 in         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 ft/ft	Discharge	0.20 cfs	
Results           Normal Depth         0.6 in           Flow Area         0.2 ft <sup>2</sup> Wetted Perimeter         5.6 ft           Hydraulic Radius         0.4 in           Top Width         5.59 ft           Critical Depth         0.6 in           Critical Slope         0.040 ft/ft           Velocity         1.03 ft/s           Velocity Head         0.02 ft           Specific Energy         0.07 ft           Froude Number         0.973           Flow Type         Subcritical           GVF Input Data         0.00 in           Length         0.0 in           Length         0.0 in           Velocity Data         0.00 it           Upstream Depth         0.0 in           Profile Description         N/A           Profile Headloss         0.00 ft           Downstream Velocity         Infinity ft/s           Upstream Velocity         Infinity ft/s           Upstream Velocity         Infinity ft/s           Normal Depth         0.6 in           Critical Depth         0.6 in           Critical Depth         0.6 ft/ft			
Normal Depth0.6 inFlow Area0.2 ft²Wetted Perimeter5.6 ftHydraulic Radius0.4 inTop Width5.59 ftCritical Depth0.6 inCritical Slope0.040 ft/ftVelocity1.03 ft/sVelocity Head0.02 ftSpecific Energy0.07 ftFroude Number0.973Flow TypeSubcriticalGVF Input Data0.0 inLength0.0 ftNumber Of Steps0GVF Output Data0.0 inUpstream Depth0.0 inProfile DescriptionN/AProfile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sOwnstream Depth0.6 inCritical Depth0.6 inCritical Depth0.6 inCritical Depth0.6 inCritical Depth0.6 inCritical Depth0.6 inCritical Depth0.0 ft	Results		
Flow Area $0.2 ft^2$ Wetted Perimeter5.6 ftHydraulic Radius0.4 inTop Width5.59 ftCritical Depth0.6 inCritical Slope0.040 ft/ftVelocity1.03 ft/sVelocity Head0.02 ftSpecific Energy0.07 ftFroude Number0.973Flow TypeSubcriticalGVF Input DataGVF Output DataUpstream Depth0.0 inLength0.0 ftNumber Of Steps0GVF Output Data0.0 inUpstream Depth0.0 inProfile DescriptionN/AProfile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.038 ft/ft	Normal Depth	0.6 in	
Wetted Perimeter5.6 ftHydraulic Radius0.4 inTop Width5.59 ftCritical Depth0.6 inCritical Slope0.040 ft/ftVelocity1.03 ft/sVelocity Head0.02 ftSpecific Energy0.07 ftFroude Number0.973Flow TypeSubcriticalGVF Input DataDownstream Depth0.0 inLength0.0 ftNumber Of Steps0GVF Output DataUpstream Depth0.0 inProfile DescriptionN/AProfile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.6 inChannel Slope0.938 ft/ftCritical Depth0.406 ft/ft	Flow Area	0.2 ft <sup>2</sup>	
Hydraulic Radius         0.4 in           Top Width         5.59 ft           Critical Depth         0.6 in           Critical Slope         0.040 ft/ft           Velocity         1.03 ft/s           Velocity Head         0.02 ft           Specific Energy         0.07 ft           Froude Number         0.973           Flow Type         Subcritical           GVF Input Data           Downstream Depth         0.0 in           Length         0.0 ft           Number Of Steps         0           GVF Output Data           Upstream Depth           Upstream Depth         0.0 in           Profile Description         N/A           Profile Headloss         0.00 ft           Downstream Velocity         Infinity ft/s           Upstream Velocity         Infinity ft/s           Vestream Velocity         Infinity ft/s           Normal Depth         0.6 in           Critical	Wetted Perimeter	5.6 ft	
Top Width5.59 ftCritical Depth0.6 inCritical Slope0.040 ft/ftVelocity1.03 ft/sVelocity Head0.02 ftSpecific Energy0.07 ftFroude Number0.973Flow TypeSubcriticalGVF Input DataDownstream Depth0.0 inLength0.0 ftNumber Of Steps0GVF Output DataUpstream Depth0.0 inProfile DescriptionN/AProfile DescriptionN/AProfile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.038 ft/ft	Hydraulic Radius	0.4 in	
Critical Depth       0.6 in         Critical Slope       0.040 ft/ft         Velocity       1.03 ft/s         Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0.0 in         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in	Top Width	5.59 ft	
Critical Slope       0.040 ft/ft         Velocity       1.03 ft/s         Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0.0 in         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in	Critical Depth	0.6 in	
Velocity       1.03 ft/s         Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data         Downstream Depth       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0.0 in         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Vestream Velocity       Infinity ft/s         Upstream Velocity       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in	Critical Slope	0.040 ft/ft	
Velocity Head       0.02 ft         Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data	Velocity	1.03 ft/s	
Specific Energy       0.07 ft         Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Channel Slope       0.038 ft/ft	Velocity Head	0.02 ft	
Froude Number       0.973         Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Optimized Depth       0.6 in         Critical Depth       0.6 in         Channel Slope       0.038 ft/ft         Griffed Glares       0.004 ft/ft	Specific Energy	0.07 ft	
Flow Type       Subcritical         GVF Input Data       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0.0 in         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in         Critical Depth       0.6 in         Channel Slope       0.038 ft/ft	Froude Number	0.973	
GVF Input Data         Downstream Depth       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Vpstream Velocity       Infinity ft/s         Upstream Velocity       0.6 in         Critical Depth       0.6 in         Channel Slope       0.038 ft/ft	Flow Type	Subcritical	
Downstream Depth       0.0 in         Length       0.0 ft         Number Of Steps       0         GVF Output Data       0         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in         Channel Slope       0.038 ft/ft	GVF Input Data		
Length       0.0 ft         Number Of Steps       0         GVF Output Data	Downstream Depth	0.0 in	
Number Of Steps       0         GVF Output Data	Length	0.0 ft	
GVF Output Data         Upstream Depth       0.0 in         Profile Description       N/A         Profile Headloss       0.00 ft         Downstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Upstream Velocity       Infinity ft/s         Normal Depth       0.6 in         Critical Depth       0.6 in         Channel Slope       0.038 ft/ft	Number Of Steps	0	
Upstream Depth0.0 inProfile DescriptionN/AProfile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.6 inChannel Slope0.038 ft/ftCritical Conse0.040 ft/ft	GVF Output Data		
Profile Description     N/A       Profile Headloss     0.00 ft       Downstream Velocity     Infinity ft/s       Upstream Velocity     Infinity ft/s       Normal Depth     0.6 in       Critical Depth     0.638 ft/ft       Critical Slope     0.038 ft/ft	Unstream Denth	0 0 in	
Profile Headloss0.00 ftDownstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.6 inChannel Slope0.038 ft/ftCritical Cope0.040 ft/ft	Profile Description	N/A	
Downstream VelocityInfinity ft/sUpstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.6 inChannel Slope0.038 ft/ftCritical Class0.040 ft/ft	Profile Headloss	0.00 ft	
Upstream VelocityInfinity ft/sNormal Depth0.6 inCritical Depth0.6 inChannel Slope0.038 ft/ftCritical Class0.040 ft/ft	Downstream Velocity	Infinity ft/s	
Normal Depth0.6 inCritical Depth0.6 inChannel Slope0.038 ft/ftCritical Class0.040 ft/ft	Upstream Velocity	Infinity ft/s	
Critical Depth     0.6 in       Channel Slope     0.038 ft/ft       Critical Class     0.040 ft/ft	Normal Depth	0.6 in	
Channel Slope 0.038 ft/ft	Critical Depth	0.6 in	
	Channel Slope	0.038 ft/ft	
	Critical Slope	0.040 ft/ft	

# Parabolic West Swale Q100 = 0.2 cfs

# STORM 3 & LAT 1 INDEX MAP



Label	ID	Upstream Structure	Flow (cfs)	Length (Unified) (ft)	Velocity (ft/s)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
PR6A	631	5' TYPE R INLET	8.80	14.9	4.98	6,373.85	6,373.75	6,373.46	6,373.36
PR6B	635	45 DEG BEND	1.60	61.8	1.30	6,374.11	6,374.07	6,374.08	6,374.04
PR6C	637	5' TYPE R INLET	1.60	3.7	1.30	6,374.12	6,374.12	6,374.09	6,374.09
Headloss (ft)	Upstream Structure Energy Grade Line (In) (ft)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Manning's n	Friction Slope (ft/ft)	Slope (Calculated) (ft/ft)	Conduit Description
0.10	6,374.07	1.500	0.58	6,370.35	6,370.50	0.013	0.007	-0.010	Circle - 18.0 in
0.04	6,374.12	0.400	0.01	6,371.67	6,372.28	0.013	0.001	-0.010	Circle - 15.0 in
0.00	6,374.16	1.500	0.04	6,372.28	6,372.32	0.013	0.001	-0.011	Circle - 15.0 in

# FlexTable: Conduit Table





EXISTING DRAINAGE MAP





# FINAL DRAINAGE REPORT FOR LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO.2 EXISTING CONDITIONS DRAINAGE MAP



<u>LEGEND</u> BASIN DESIGNATION PIPE RUN REFERENCE 4 LABEL SURFACE DESIGN POINT BASIN BOUNDARY EXISTING CONTOUR PROP CONTOUR UNDERGROUND ELECTRICAL EXISTING GAS LINE Tc PATH OVERLAND UNDEVELOPED Tc PATH CHANNELIZED UNDEVELOPED STORM SEWER PIPE EXISTING STORM SEWER PIPE CROSSPAN INLET EXISTING FLOW DIRECTION ARROW EMERGENCY OVERFLOW DIRECTION FLOW DIRECTION FLARED END SECTION HIGH POINT LOW POINT

BASIN SUMMARY								
BASIN	AREA (ACRES)	<b>Q</b> <sub>5</sub>	Q <sub>100</sub>					
**C	0.12	0.1	0.4					
**C1	0.17	0.1	0.5					
D	0.77	0.3	1.8					
D1	0.63	0.2	1.5					
D2	0.15	0.1	0.5					
**E1	0.27	1.2	2.2					
**E2	0.21	1.0	0.1					

\*\*~CLAREMONT BUSINESS PARK 2 FILING NO.2 FDR PREPARED BY MS CIVIL CONSULTANTS, INC.

DESIGN POINT SUMMARY										
DESIGN POINT	<b>Q</b> <sub>5</sub>	Q <sub>100</sub>	BASIN	STRUCTURE						
1	0.6	3.9	**C, **C1, D, D1	EX 30" DOME GRATE						
2	2.2	6.9	D2, **E1, **E2, DP1	EX WQ SAND FILTER POND 3						

STORM SEWER SUMMARY								
PIPE RUN	$Q_5$	<b>Q</b> <sub>100</sub>	PIPE SIZE	CONTRIBUTING DP/BASIN/PIPES				
1	0.6	3.9	EX 18"	DP1				



	212 n. Wahsatch ave., ste 305	LOT2	CLA	AREM	ONT	BUSI	NESS	PARK	2	FIL.NO.2
	COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485	ΕX	(IST	ING	CON	DITIO	NS D	RAINA	GE	MAP
		PROJECT	NO.	10-025A	FILE: \	,dwg∖Eng E×	hibits\10025	5 EDM.dwg		
		DESIGNE	D BY:	GT	SC	ALE	DATE:	02-02-2024	4	
CONSULTANTS, INC.		drawn e Checked	3Y: ) BY:	DLM VAS	HORIZ: VERT:	1"=20' N/A	SHEET	Г 1 OF 1		EDM01

PROPOSED DRAINAGE MAP





# LOT 2 CLAREMONT BUSINESS PARK 2 FILING NO.2 PROPOSED CONDITIONS DRAINAGE MAP

\*\* CLAREMONT BUSINESS PARK2 FILING NO.2 FDR

& \*\*\* ULTIMATE BUILDOUT AND REVISED BASIN

# UNDEVELOPED BASIN

BASIN SUMMARY								
BASIN	AREA (ACRES)	<b>Q</b> <sub>5</sub>	Q <sub>100</sub>					
#C	0.4	0.0	0.1					
#C1	0.26	0.1	0.8					
#D	0.47	0.3	1.3					
***D	0.47	2.0	3.6					
#D1	0.93	3.9	7.1					
#D2	0.15	0.1	0.5					
**E1	0.27	1.2	2.2					
**E2	0.21	1.0	1.7					

\*\*~CLAREMONT BUSINESS PARK 2 FILING NO.2 FDR PREPARED BY MS CIVIL CONSULTANTS, INC. #~BASIN AREA REVISED FROM CLAREMONT BUSINESS PARK 2 FILING NO. 2 FDR PREPARED BY MS CIVIL CONSULTANTS, INC.

\*\*\*~ULTIMATE BUILD OUT. FULL DEVELOPMENT OF LOT 2.

# DESIGN POINT SUMMARY

DESIGN POINT	<b>Q</b> <sub>5</sub>	<b>Q</b> <sub>100</sub>	BASIN	STRUCTURE
1	0.3	1.6	#C, #D	PROP 5' TYPE R INLET
***1	1.8	3.4	#C, ***D	PROP 5' TYPE R INLET
2	3.7	7.2	#C1, #D1	PROP 5' TYPE R INLET
3	6.1	12.9	#D2, PR2, **E1, **E2	EX WQ SAND FILTERPOND 3
***3	7.5	14.6	#D2, ***PR2, **E1, **E2	EX WQ SAND FILTER POND 3

STORM SEWER SUMMARY									
PIPE RUN	$Q_5$	<b>Q</b> <sub>100</sub>	PIPE SIZE	CONTRIBUTING DP/BASIN/PIPES					
1	0.3	1.6	PROP 15"PP	DP1					
***1	1.8	3.4	PROP 15"PP	***DP1					
2	4.0	8.8	EX 18" RCP	DP2, PR1					
***2	5.5	10.6	EX 18"RCP	***DP2, ***PR1					

			EX F	POND 3 SA ENTION BA	AND FILTER ASIN DATA	
" = 20'			WQ WA WQ VC 100-Y SPILLW TOP O RATION MHFD MHFD	ATER SURFACE I DLUME=0.051 AC R WATER SURFA R VOLUME=0.15 IAY CREST EL=0 F EMBANKMENT NAL 100-YR INFLOW 100-YR INFLOW	EL = 6371.78 C-FT ACE EL=6373.36 53 AC-FT 6375.30 EL=6376.55 FLOW=14.8 CFS C = 9.0 CFS SE = 4.0 CFS	
) 20 40 Scale in Feet		PONI 2 FII CONS PCD	D DESIG LING NO SULTAN <sup>-</sup> FILING	N FROM CLAREN . 2 FDR PREPA IS, INC. APPRON NO. VR 233	MONT BUSINESS PARK RED BY MS CIVIL VED 11/13/2023	
	212 N. WAHSATCH AVE STE 305	LOT2 CLA	REM	ONT BUSI	NESS PARK	2 FIL.NO.2
	COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485	PRO	P. C	ONDITION	S DRAINAGE	MAP
		PROJECT NO. 1	0-025A	FILE: \dwg\Eng Ex	khibits\10025 PDM.dwg	
		DESIGNED BY:	GT	SCALE	DATE: 02-02-2024	
DNSULTANTS, INC.		DRAWN BY: CHECKED BY:	GT VAS	HORIZ: 1"=20' VERT: N/A	SHEET 1 OF 1	PDM01

# BOCC RESOLUTION 16-426

![](_page_53_Picture_1.jpeg)

60CL

![](_page_54_Picture_1.jpeg)

# **RESOLUTION NO. 16-426**

# **BOARD OF COUNTY COMMISSIONERS** COUNTY OF EL PASO, STATE OF COLORADO

Resolution Denying an Appeal by Hammers Construction LLC (APP-16-002) of the Administrative Determination made by the Planning and Community Development Department Executive Director regarding the requirement for permanent/post construction Water Quality (permanent stormwater quality best management practices or BMP's).

WHEREAS, pursuant to §§30-11-101(1)(e) and 30-11-107(1)(e), C.R.S., the Board of County Commissioners of El Paso County, Colorado (hereinafter "Board) has the legislative authority to manage the concerns of El Paso County when deemed by the Board to be in the best interests of the County and its inhabitants; and

WHEREAS, after consultation with the County Attorney's Office, the Executive Director of Planning and Community Development on August 4, 2016 issued an administrative determination finding made an administrative determination that all undeveloped lots within the Claremont Business Park are subject to installation of permanent stormwater management best management practices (BMP's) associated with development, and that the terms of a 2008 approved deviation relieving the developer of the requirements have not been met.; and

WHEREAS, an appeal of the administrative determination was filed by Hammers Construction on August 10, 2016, and a hearing date was set for September 27, 2016 to hear the appeal; and

WHEREAS, the hearing was continued to a date certain of November 22, 2016; and

WHEREAS, at the Applicant's appeal hearing on November 22, 2016, testimony from the Applicant and the Applicant's representatives was heard by the Board in favor of the appeal, testimony from representatives of Planning and Community Development Department and was presented, and such testimony and associated evidence was weighed by the Board; and

Resolution No. 16- 426 Page 2

WHEREAS, the Board, having reviewed the testimony and evidence, hereby finds and determines that the requested appeal of the administrative determination by the Planning and Community Development Executive Director by the Applicant did not satisfy the criteria of approval to overturn the administrative determination.

NOW, THEREFORE, BE IT RESOLVED that the Board of County Commissioners of El Paso County, Colorado, hereby denies the appeal of the administrative determination by Hammers Construction and determines that permanent stormwater management best management practices (BMP's) are required with new development within the Claremont Business Park: and

**BE** IT **FURTHER RESOLVED** that Sallie Clark, duly elected, qualified member and Chair of the Board of County Commissioners, or Darryl Glenn, duly elected, qualified member and Vice Chair of the Board of County Commissioners, be and is hereby authorized on behalf of the Board to execute any and all documents necessary to carry out the intent of the Board as described herein.

DONE THIS 22<sup>nd</sup> day of November, 2016, at Colorado Springs Colorado.

![](_page_55_Picture_5.jpeg)

BOARD OF COUNTY COMMISSIONERS EL PASO COUNTY, COLORADO

e ( Oal By:

Chair of the Board