# FINAL DRAINAGE REPORT FOR STERLING RANCH FILING 3

**Prepared For:** 

SR Land, LLC 20 Boulder Crescent, Suite 200 Colorado Springs, CO 80903 (719) 491-3024

> April 2022 Project No. 25188.02 SF-2132

Prepared By: JR Engineering, LLC 5475 Tech Center Drive, Suite 235 Colorado Springs, CO 80919 719-593-2593



#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability canced by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. 32314 For and On Behalf of JR Engineering, LLC

#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

**Business Name:** 

By:

Title: Address:

SR Land, LLC 20 Boulder Crescent, Suite 200

Colorado Springs, CO 80903

#### El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

## APPROVED Engineering Department

06/09/2022 2:23:25 PM dsdnijkamp EPC Planning & Community Development Department County Engineer/ ECM Administrator

Date

Conditions:



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# PURPOSE

This document is the Final Drainage Report for Sterling Ranch Filing 3. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert and inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

# **GENERAL SITE DESCRIPTION**

# **GENERAL LOCATION**

Sterling Ranch Filing 3 (hereby referred to as the "site") is a proposed development within the Sterling Ranch master planned community with a total area of approximately 19.5 acres that are presently undeveloped.

The site is located in portions of the southwest quarter of Section 33, Township 12 South, Range 65 West of the Sixth Principal Meridian in El Paso County, State of Colorado. The site is bounded by Pawnee Rancheros Filing 2 to the south and un-platted land to the west, Sterling Ranch Road to the north, and Sand Creek borders the site to east. Refer to the vicinity map in Appendix A for additional information.

### **DESCRIPTION OF PROPERTY**

The property will be primarily be single-family residential development (approximately 12 acres), as well as open space and drainage tracts (approximately 7.5 acres). The site is comprised of variable sloping grasslands that generally slope(s) downward to the southeast at 3 to 8% towards the Sand Creek tributary basin and southwest toward existing Pond W-5 (constructed with Sterling Ranch Filing No. 2).

Soil characteristics are comprised of Type A and B hydrologic Soil groups. Refer to the soil survey map in Appendix A for additional information.

There are no major drainage ways running through the site, although a tributary to the Sand Creek basin is immediately to the east of the site. Currently, JR Engineering is performing studies and plans to address Sand Creek stabilization.

There are no known irrigation facilities located on the project site.

# FLOODPLAIN STATEMENT

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, the far eastern portion of the project site that is adjacent to the existing drainage way lies within Zone AE. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. The majority of



the proposed development lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. Grading is proposed in the floodplain at the northeast corner of the site to protect lots east of Dines Blvd. FIRM Maps have been presented in Appendix A.

# **EXISTING DRAINAGE CONDITIONS**

## MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into major sub-basins. The site is within the respective sub-basin is shown in Appendix E.

The Sand Creek DBPS assumed the Sterling Ranch Phase 2 property to have a "large lot residential" use for the majority of the site. The Sterling Ranch MDDP assumed a mix of commercial and single family residential lots ranging in size from 0.2 to 0.3 acres for the Sterling Ranch Phase 2 site. The proposed Sterling Ranch master plan is a mix of; school, multi-family, single-family, and commercial land uses, resulting in higher runoff. Any additional runoff will be provided for with the extended detention basin located at the southern edge of the site. The site generally drains from north to south consisting of rolling hills. Currently, the site is used as pasture land for cattle. Sand Creek is located east of the site running north to south. This reach of drainage conveyance is not currently improved. There are a few stock ponds within the creek channel used for cattle watering. Currently, JR Engineering is performing studies and plans to address Sand Creek stabilization adjacent to the site.

The proposed drainage on the site closely follows the approved "Master Development Drainage Plan for Sterling Ranch", (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018. The site is tributary to Pond W5 and full-spectrum detention for the site was previously analyzed and can be found in the Final Drainage Report for Sterling Ranch Filing 2.

# **EXISTING SUB-BASIN DRAINAGE**

The existing / predeveloped condition of the site was broken into two major basins: Basin A (western portion) and Basin B (Eastern Portion), as well as an offsite basin. The basin and sub-basin delineation is shown in the existing drainage map in Appendix E and is described as follows:

Sub-basin A1( $Q_5$ = 1.1cfs,  $Q_{100}$ =8.0cfs) is 5.17 acres and 0 percent impervious this basin is the east of the Sterling Ranch Filing 3 site. Runoff from this basin drains to the south west into the assumed existing storm sewer built with Filing 2 just east of Marksheffel Road located at design point 1.



Collected runoff is piped south to the existing detention pond built with Filing 2 and outfalls to Sand Creek.

Sub-basin A2 ( $Q_5$ = 4.6cfs,  $Q_{100}$ =33.6cfs) is 27.48 acres and 0 percent impervious and consists the central portion of Sterling Ranch Phase 2. Runoff from this basin drains south onsite into the assumed existing storm sewer built with Filing 2 located at design point 2. Collected runoff is piped south to the existing detention pond built with Filing 2 and outfalls to Sand Creek.

Sub-basin B1 ( $Q_5= 2.6cfs$ ,  $Q_{100}=19.0cfs$ ) is 11.78 and is 0 percent impervious and is located on the eastern portion of the site portion of the site. Runoff from this basin drains to the southeast into Sand Creek at design point 4.

Sub-basin OS1( $Q_5$ = 13.4cfs,  $Q_{100}$ =29.8cfs) is 9.27 acres is 30.7 percent impervious and is located to the south of the Sterling Ranch Filing 3 site. Runoff from this basin drains into the Sterling Ranch Filing 2 detention Pond in confluence with upstream flows from the eastern portion of Sub-basin A2. Collected runoff sheet flows south to the existing detention pond built with Filing 2 and outfalls to Sand Creek.

# **PROPOSED DRAINAGE CONDITIONS**

# **PROPOSED SUB-BASIN DRAINAGE**

The proposed site was broken into three major basins: Basin A and I (western-portion), Basin B (eastern-portion) and Basin D (offsite eastern-portion) of the site. The proposed basin (and subbasin) delineation is shown on the drainage basin map within Appendix E and is described as follows.

**Basin A1** ( $Q_5$ = 8.2cfs,  $Q_{100}$ =17.7cfs) is 4.37 acres and 64 percent impervious and is comprised of single-family residential lots, and a local road. Runoff from this basin drains to design point 15, a 15' type R on grade inlet at the southwest corner of the basin.

**Basin A5** ( $Q_5$ = 1.4cfs,  $Q_{100}$ =2.9cfs) is 0.45 acres and 78 percent impervious is comprised of future single-family residential lots and a local road. Runoff from this basin drains to an on grade 10' inlet at design point 16.

**Basin B1** ( $Q_5$ = 5.9 cfs,  $Q_{100}$ =11.8 cfs) is 2.44 acres and 77 percent impervious is comprised of singlefamily residential lots, local roads, two urban knuckles, and a cul-de sac. The runoff from basin B1 drains to a type 15' R sump inlet located at design point 13.



**Basin B2** ( $Q_5$ = 9.1cfs,  $Q_{100}$ =18.7cfs) is 4.33 acres and 73 percent impervious is comprised of single family residential lots. Runoff from basin B2 drains to a type 15' R sump inlet located at design point 12.

**Basin B3** ( $Q_5$ = 1.1 cfs,  $Q_{100}$ =2.4cfs) is 0.59 acres and 58 percent impervious is comprised of open space and sidewalk. Runoff from basin B3 drains to a 15' type R on grade inlet located west of the Sterling Ranch Filing 3 site at design point 9 in existing Sterling Ranch Road. All of the runoff is captured in the 100 year event. Runoff is piped and outfalls into pond W-5.

**Basin B4** ( $Q_5$ = 2.2cfs,  $Q_{100}$ =5.1cfs) is 1.59 acres and 56 percent impervious is comprised of single family residential lots and open space. Runoff from basin B4 drains to four rear lot type C area inlet(s) that confluence at DP 10.

**Basin B5** ( $Q_5=0.7$ cfs,  $Q_{100}=1.7$ cfs) is 0.45 acres and 51 percent impervious is comprised of single family residential lots and open space. Runoff from basin B4 drains to a rear lot area inlet at DP 11.

**Basin B6** ( $Q_5=0.8$ cfs,  $Q_{100}=2.2$ cfs) is 0.78 acres and 44 percent impervious is comprised of single family residential lots and open space. Runoff from basin B4 drains to a rear lot area inlet at DP 14.

**Basin D1**( $Q_5= 0.4cfs$ ,  $Q_{100}=1.2 cfs$ ) is 0.38 acres and 18 percent impervious is comprised of open space area. Runoff from basin D1 sheet flow to the, southeast and adjacent properties into Sandcreek as per the historic condition. Flows generated from this basin have been attributed to design point 28. The runoff is not treated and drains directly into Sand Creek. No residential development is within this basin. While the cumulative untreated area for Sterling Ranch Filing No.3 is more than 1 acre, a portion of this basin can be excluded per ECM APP1.7.1.B.9, given that the improvements within this basin include a trail and maintenance access road for Sand Creek. There is also a runoff reduction component in that runoff from the proposed trail sheet flow across grass areas.

**Basin D2** ( $Q_5= 2.5$ cfs,  $Q_{100}=11.9$  cfs) is 3.92 acres and 8 percent impervious is comprised of open space area and trail/access roads. Runoff from basin D2 sheet flows to the southeast into Sandcreek as per the historic condition. Flows generated from this basin have been attributed to design point 29. The runoff is not treated and drains directly into Sand Creek. No residential development is within this basin. While the cumulative untreated area for Sterling Ranch Filing No.3 is more than 1 acre, a portion of this basin can be excluded per ECM APP1.7.1.B.9 and APP1.7.1.B.8 given that the improvements within this basin include bank stabilization for Sand Creek and a trail/ maintenance access road for Sand Creek. The north part of this basin borders the future Sterling Ranch Road, wherein the interim conditions, the area will remain undeveloped, and when the road is built, the runoff will be conveyed east to a future water quality and detention pond where water quality will be provided for the street runoff. There is also a runoff reduction component in that runoff from the proposed trail sheet flow across grass areas.



**Basin I1** ( $Q_5$ = 5.2 cfs,  $Q_{100}$ =35.1 cfs) 24.5 acres and 1 percent impervious is comprised of open space, tail/ access roads and planned future development that has been accounted within pond W5's design in the Sterling Ranch Filing No. 2 Drainage Report as shown in Appendix D. The runoff from this basin sheet flows generally to the south and east into a temporary drainage channel where it is conveyed to an existing storm stub at design point I1.

**Basin I2** ( $Q_5= 0.7cfs, Q_{100}=4.9cfs$ ) 3.47 acres and 0 percent impervious is comprised of open space. The runoff from this basin sheet flows to the south and east into an existing drainage swale where it eventually enters a 42" existing storm stub provided from the Sterling Ranch Filing No 2. Project.

# **DRAINAGE DESIGN CRITERIA**

# **DEVELOPMENT CRITERIA REFERENCE**

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.

# HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the EPCSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the EPCSDCM. Time of concentrations were developed using equations from EPCSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

Table 2 -	1-hr	Point	Rainfall	Data
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# HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Sump and on-grade inlets were sized using UDFCD UD-Inlet v4.05. Autodesk Hydraflow express was used to size the overflow channel and an interim swale. Using Storm StormCAD V8i, a modeling program for stormwater drainage, the hydraulic grade lines and energy grade lines were determined for the storm sewer network. Manhole and pipe losses for the model were obtained from the <u>Modeling Hydraulic and Energy Gradients in Storm Sewers: A</u> <u>Comparison of Computation Methods</u>, by AMEC Earth & Environmental, Inc. The manhole loss coefficients used in the model can be seen in Table 2. StormCAD, Autodesk Hydraflow results along with street and inlet capacities are presented in Appendix C.

	StormCA	D Conversion Ta	ble								
	Bend Angle	K coefficient Conversion									
Bend Loss	0	0.05									
d L	22.5	0.1									
en	45	0.4									
•	60	0.64	1								
	90	1.32									
	1 Lateral K coefficient Conversion										
	Bend	Non									
	Angle	Surcharged	Surcharged								
SS	45	0.27	0.47								
Lateral Loss	60	0.52	0.9								
ag	90	1.02	1.77								
ate	2 Latera	Is K coefficient C	onversion								
_	45	0.96									
	60	1.10	6								
	90	1.52	2								

Table 2 - StormCAD Standard Method Conversions

# **DRAINAGE FACILITY DESIGN**

# **GENERAL CONCEPT**

The proposed stormwater conveyance system was designed to convey the developed Sterling Ranch Filing 3 runoff to an existing (Filing 2) full spectrum water quality and detention pond via storm sewer and swale. The proposed pond was designed to release at less than historic rates to minimize adverse impacts downstream. Treated water will outfall directly into the Sand Creek Drainage way, where it will eventually outfall into Fountain Creek. A proposed drainage map is presented in Appendix E showing locations of the pond. JR Engineering is working on a separate plan to stabilize Sand Creek directly adjacent to the site.



## FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the Engineering Manual County of El Paso, Colorado Appendix I, Section 7.2 this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes Employ Runoff Reduction Practices, Stabilize Drainageways, Provide Water Quality Capture Volume (WQCV), and Consider Need for Industrial and Commercial BMPs.

Step 1 – Employ Runoff Reduction Practices: The Sterling Ranch Filing 3 development project consists of single-family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

Step 2 – Stabilize Drainageways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the channel stabilization being designed by JR Engineering adjacent to the site and on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Sand Creek, therefore no downstream stabilization will be accomplished with this project.

Step 3 – Provide Water Quality Capture Volume (WQCV): Water Quality treatment for this site is provided in an existing full spectrum water quality detention pond (W5). The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer and swale. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the ponds will be reduced to less than historic rates.

Step 4 – Consider Need for Industrial and Commercial BMPs: There are no commercial or industrial facilities on the Sterling Ranch Filing 3 site. Other erosion control BMPs include asphalt drives and parking, storm inlets and storm pipe, the full spectrum detention pond W-5 and permanent vegetation. The interim channel for Sterling Ranch Filing 3 will be accessible for maintenance with the access trail to the east. Maintenance responsibilities and plans for pond W5 were provided with Filing 2. A channel maintenance agreement for Sand Creek will be provided with Filing 3.

# WATER QUALITY

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention are provided for all developed basins. This site will drain into an existing Full Spectrum Drainage Pond W5 developed during the Sterling Ranch Filing No. 2 Project. Further details as well as all pond volume, water quality, and outfall calculations are included in the Sterling Ranch Filing 2 Final Drainage Report. Pond W5 corresponds to pond FSD6 from the Master Development Drainage Plan



for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018. ( $Q_5=7.6$  cfs,  $Q_{100}=149.7$  cfs) and is releasing less than the MDDP values in the proposed design. A summary of Pond W-5 has been included below for reference.

	REQUIRED VOLUME	VOLUME PROVIDED	WQCV	EURV	5-YEAR RELEASE	100-YEAR RELEASE
	(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)	(CFS)	(CFS)
POND W5	18.217	18.441	3.29	11.71	2.7	137.1

Table 3. Pond Volumes & Release Rates

# **EROSION CONTROL PLAN**

The Erosion Control Plan and Cost Estimate have been submitted in conjunction with the grading and erosion control plan and construction assurances will be posted prior to obtaining a grading permit.

# **OPERATION & MAINTENANCE**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The district shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. A maintenance road was provided for the existing pond W5 and information on the road can be found in the Final Drainage Report for Sterling Ranch Filing No. 2. The maintenance road access is off of Marksheffel Road and wraps around the top of the pond providing access to the inflow pipe wingwalls and outlet structure for the pond.

# **DRAINAGE AND BRIDGE FEES**

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees are presented below and will be due at time of platting (depending on date of plat submittal):.

2021 DRAINAGE AND BRIDGE FEES – STERLING RANCH FILING 3												
Impervious Acres (ac)	Drainage Fee (Per Imp. Acre)	Bridge Fee (Per Imp. Acre)	Sterling Ranch Drainage Fee	Sterling Ranch Bridge Fee								
10.518	\$20,387	\$8,339	\$214,430.47	\$87,709.60								

The developed condition of tract C was used to calculate the overall impervious area. The total area used was 20.9116 Acres and the net impervious value is 50.3%.

# Construction Cost Opinion

The Drainage Criteria Manual specifies a Cost Estimate of proposed drainage facility improvements be submitted with the Final Drainage Report. A construction cost opinion has been provided below. The below cost opinion is only an estimate of facility and drainage infrastructure cost and may vary.



#### FINAL DRAINAGE REPORT FOR STERLING RANCH FILING 3

					-,	
Item	Description	Quantity	Unit	Ur	it Price	Cost
1	18" RCP	1138	L.F.	\$	67	\$ 76,246.00
2	24" RCP	126	L.F.	\$	81	\$ 10,206.00
3	36" RCP	512	L.F.	\$	124	\$ 63,488.00
4	36" FES	1	Ea.	\$	600	\$ 600.00
5	15' CDOT Type R At-Grade	3	Ea.	\$	11,005	\$ 33,015.00
6	10' CDOT Type R At-Grade	1	Ea.	\$	8,136	\$ 8,136.00
7	CDOT TYPE C	5	Ea.	\$	4,802	\$ 24,010.00
8	CDOT TYPE D	1	Ea.	\$	5,932	\$ 5,932.00
9	Storm Sewer MH, box base	1	Ea.	\$	12,034	\$ 12,034.00
				Su	b-Total	\$ 233,667.00

#### Sterling Ranch Filing No. 3 (Public Non-Reimbursable)

#### Sterling Ranch Filing No. 3 (Bridge - Reimbursable)

Item	Description	Quantity	Unit	Unit Price	Cost	
1	58S Bridge (see FAE CDR 22-6	1	1 Ea.		\$ \$ 750,000.00	
				Sub-Total	\$ 750,000.00	

The approved Sterling Ranch Filing 2 Final Drainage Report identified reimbursable improvements for both the pond W-4 and W-5 major drainage facilities in lieu of DBPS Segment 159 and 164 identified improvements. These reimbursable improvements are to be built per the approved Sterling Ranch Filing 2 Storm Sewer plans (SF-2015). The anticipated cost of these reimbursable improvements exceeded the Drainage Fees associated with Sterling Ranch Filing 2.

Per LDC section 8.5.5.C.3.b(ii) Fee Reductions, Credits or Reimbursement for Facilities, this development requests that no cash drainage fees or bridge fees are due at platting as the value of reimbursable DBPS improvements for the Sand Creek Tributary segment 159 and 164 shown in the below table minus deferments taken previously for Sterling Ranch Filing 2 exceed the drainage fee estimate for Sterling Ranch Filing 3. Additionally, the reimbursable bridge structure estimated value is well in excess of the bridge fees due for this subdivision

### Sterling Ranch Deferred Drainage Fees Analysis Reimbursable Costs associated with DBPS Segment 159 and 164

From Sterling Ranch Filing 2 FDR (SF-2015)

Reimbursable Cost estimate associated with Pond W-4 System	\$1,218,336.00
Reimbursable Cost estimate associated with Pond W-5 System	<u>\$699,729.00</u>
Subtotal Segment 159 and 164 E	\$1,918,065.00
Drainage Fees Deferred per LDC section 8.5.5.C.3.b(ii)	<u>\$400,855.70</u>
Excess Reimb. Costs associated with DBPS Segment 159 and 164	\$1,517,209.30
Sterling Ranch Filing 3 Drainage Fee Deferment	
Excess Reimb. Costs associated with DBPS Segment 159 and 164	\$1,517,209.30
Drainage Fees for Sterling Ranch Filing 3	\$214,430.47



# SUMMARY

The proposed Sterling Ranch Filing 3 drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainageways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.



# REFERENCES

- 1. Engineering Criteria Manual County of El Paso, Colorado, October, 14 2020
- 2. "Sand Creek Channel Design Report", prepared by JR Engineering, October, 2021 (under review)
- 3. "Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018.
- "MDDP Amendment No. 1 for Sterling Ranch", prepared JR Engineering, October 2021 (under review)
- "Sand Creek Drainage Basin Planning Study", prepared Kiowa Engineering Corporation, January 1993, revised March 1996.
- "Sterling Ranch Filing 2 Final Drainage Report", prepared by JR Engineering, dated August 2021 (Approved in November)
- 7. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- Sand Creek Stabilization at Aspen Meadows Subdivision Filing No. 1 100% Design Plans, April 2020



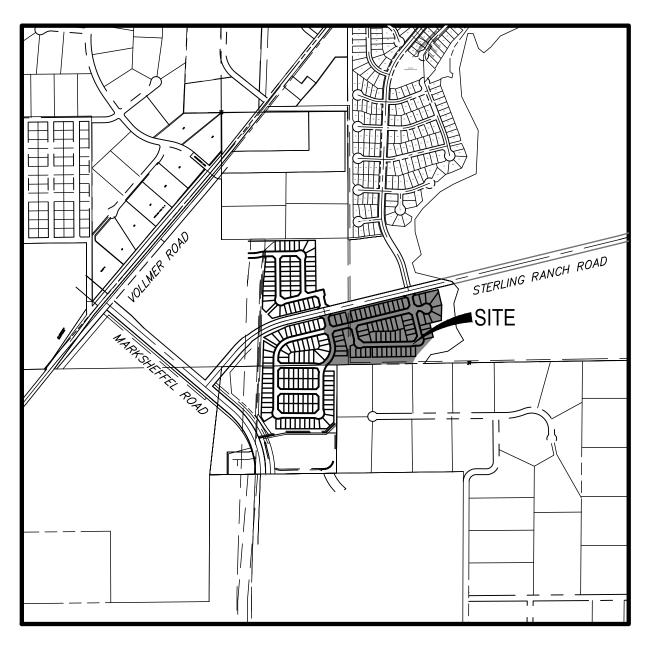
# REFERENCES

- 1. Engineering Criteria Manual County of El Paso, Colorado, October, 14 2020
- 2. "Sand Creek Channel Design Report", prepared by JR Engineering, October, 2021 (under review)
- 3. "Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018.
- "MDDP Amendment No. 1 for Sterling Ranch", prepared JR Engineering, October 2021 (under review)
- "Sand Creek Drainage Basin Planning Study", prepared Kiowa Engineering Corporation, January 1993, revised March 1996.
- "Sterling Ranch Filing 2 Final Drainage Report", prepared by JR Engineering, dated August 2021 (Approved in November)
- 7. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- Sand Creek Stabilization at Aspen Meadows Subdivision Filing No. 1 100% Design Plans, April 2020



Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map



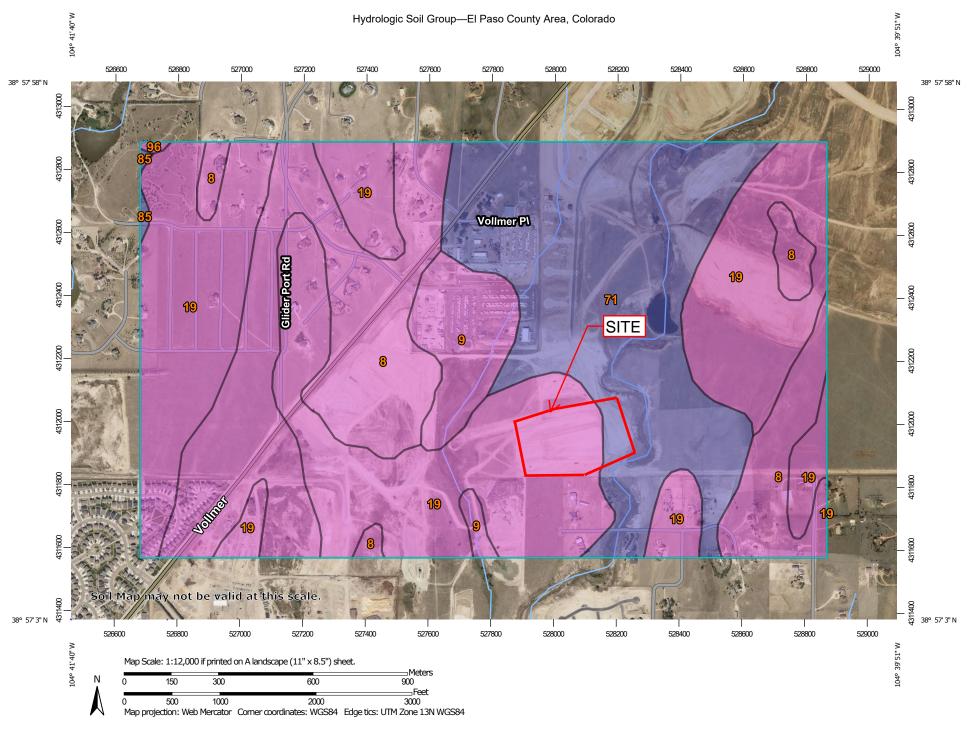




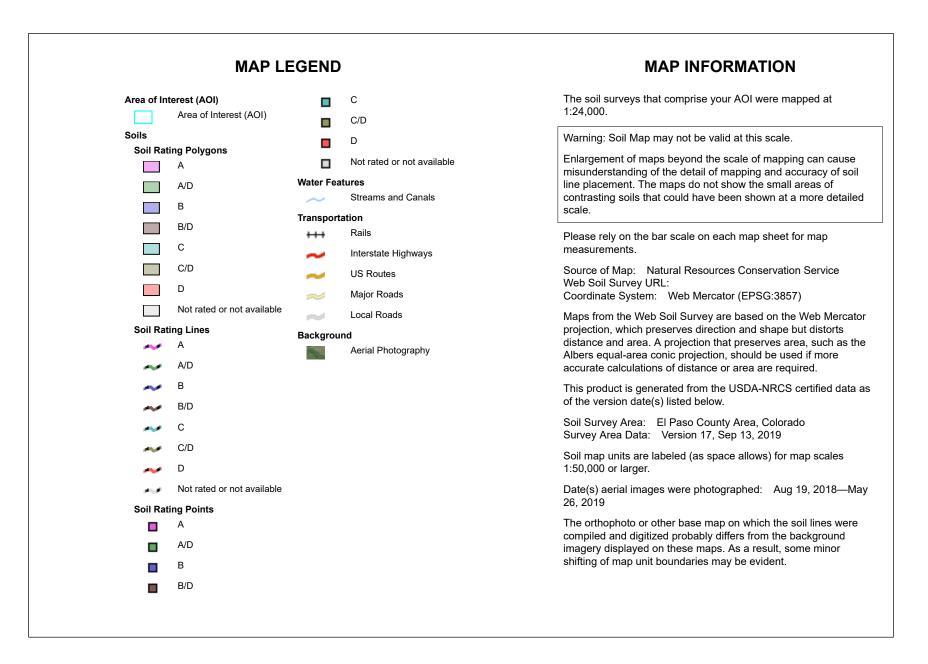
VICINITY MAP STERLING RANCH FILING 3 JOB NO. 25188.02 06/09/21 SHEET 1 OF 1



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI									
8	Blakeland loamy sand, 1 to 9 percent slopes	A	182.3	25.4%									
9	Blakeland-Fluvaquentic Haplaquolls	A	36.8	5.1%									
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	307.5	42.9%									
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	188.4	26.3%									
85	Stapleton-Bernal sandy loams, 3 to 20 percent slopes	В	1.2	0.2%									
96	Truckton sandy loam, 0 to 3 percent slopes	A	0.6	0.1%									
Totals for Area of Inter	rest		716.9	100.0%									

# Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

# **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

#### NOTES TO USERS

This map is for use in administring the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage curces of small size. The community map repository should be consulted for ossible updated or additional flood hazard information.

Location or detailed information in answer them taken the action flowed based information in answer the take Flood Elevations (RFEs) action flowed based and the flowed action of the Flood within the Flood taken as the state of the flowed within the Flood takenase. Budy (FIS) period that accompanies the FIRM. Uses a state of the flowed taken as the FIRM taken as the flowed taken as

Coastal Base Flood Elevations shown on this map apply only landward of 0.0° North Amarican Vertical Datum of 1989 (NAVD89), Users of this FIRM Hould be aware that coastal flood develosms are aired provided in the Summary of Sillwate Elevations table in the Flood Insurance Study report for this jurisdicion. Elevations shown in the Summary of Sillwate Elevations table should be used for construction and/or floodpian maragement purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway width and other partinent floodway data are provided in the Flood Insurance Study report for this jurisdicture.

Certain areas not in Special Flood Hazard Areas may be protected by **flood contrn** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insuranc Study report for information on flood control structures for this jurisdiction.

The projection used in the properties of this may was Universel Transverse Meanser (UTM) are 13. The hothcast attain was NARDS, GR585 spheroid. Differences in datum, spheroid, projection or UTM screes zones used in the production of FRMNs for adjacent juncticions may require uit, in slight positional differences in mag features across jurisdiction boundaries. These differences do not affect the accuracy of this FRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD68), Thesis flood elevations must be compared to structure are compared to structure and the structure of the structure and conversion between the National Geodelic Vertical Datum of 1528 and the North American Vertical Datum of 1988, visit the National Geodelic Survey at the Holm/ American Service and Service and Service and the Islaming Service and Service and

NGS Information Services NOAA, NINGS12 National Geodetic Survey SSMC-3, #9202 1315 East-Weast Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the information Services Branch of the National Seodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gow/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map infects more detailed and up-to-date stream channel configurations and modplain delineations than those shown on the previous FRM for this jurisdice, this way to be adjudged to confirm to these more stream channel configurations. As sets the besing disudder to confirm to these more stream channel configurations. As a sets the besing disudder to confirm to these more stream channel configurations. As a sets the besing disudder the stream channel configuration and disarces that offer from what is shown on the map. The profit baselines diplated disarces that offer from what is shown on the map. The profit baselines diplated baselines that offer from what is shown on the map. The profit baselines diplated baselines and the stream configuration that the FIS report. As a result, the profit baselines significantly from the new base map channel representation and may appear contact of the fore forem.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, may users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county howing the layout of map panels; community map repository addresses; and a siting of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is coted.

Contact FEMA Map Service Center (MSC) via tha FEMA Map information eXchange FMX) 1677-038227 for information on available products associated with the FRM. Available products may include prevauly issued Letters of Map Change, a food insurance Study Report, and/or diplail versions of his map. The MSC may also be reached by Fax at 1-800-358-9620 and its websile at try/invow.msc.fema.gov/.

f you have **questions about this map** or questions concerning the National Flood nsurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.





This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Water Conservation Board

tional Flood Hazaro Information and resource lable from local communities and the Col-



3235000 FT JOINS PANEL 0535 1047 307 33 607 104" 41" 15.00" 381 581 7 501 38" 58' 7 50" Sand Creek ZONEAE Ø EL PASO COUNTY UNINCORPORATED AREAS 080059 474 2000 mail (DC) VOLLMER F 33 32 34 ZONE (C) (cx) 4312000mN 1410000 F T. 12 S T. 13 S MOJAVE DR T. 12 S. T. 13 S. EL PASO COUNTY UNINCORPORATED AREAS 080059 (CII)-ZONEAE 070 C/p 3 ZONE AE SITE LOCATION KENOSHA DR EL PASO COUNTY CITY OF COLORADO SPRINGS PONCA RD 3 4 5 EL PASO COUNTY NINCORPORATED AREAS 080059 CITY OF COLORADO SPRINGS 1405000 F 6886 WOODMEN FRONTAGE RD E WOODMEN RD Bridge E WOODMEN DE co AREAS (000159 10 ZONE AE 8 43-10.000mN Sand Creek 381 561 15 00 381 561 15.001 104° 41' 15.00" JOINS PANEL 0545 104" 39' 22.50' \$-000mp NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.



Appendix B Hydrologic Calculations



### COMPOSITE % IMPERVIOUS & COMPOSITE EXISTING RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location: Sterling Ranch Subdivision- Existing El Paso County Project Name: Sterling Ranch Filing 3

Project No.: 25188.02 Calculated By: CJD

Checked By:

Date: 6/9/21

	Total Area (ac)	Str	eets (10	0% Impe	rvious)		Residential (65% Impervious) eighborhood Area (70% Impervious)				1 Acre lot Rersidential (20% Impervious) Light Commercial (80% Impervious)				•	pervious Impervio	,	Basins Total Weighted C Values		Basins Total Weighted %
Basin ID	Ai ea (ac)	C <sub>5</sub>	C <sub>100</sub>	Area	Weighted	C <sub>5</sub>	C <sub>100</sub>	Area	Weighted %	Cr	C <sub>5</sub> C <sub>100</sub>		Area Weighted		C <sub>100</sub>	Area	Weighted %	va	ues	Imp.
DasininD		05	♥100	(ac)	% Imp.	05	V100	(ac)	Imp.	05	C100	(ac)	% Imp.	$C_5$	0100	(ac)	Imp.	C <sub>5</sub>	C <sub>100</sub>	
A1	5.17	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	5.17	2.0%	0.08	0.35	2.0%
A2	27.48	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	27.48	0.0%	0.08	0.35	0.0%
B1	11.78	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	11.78	0.0%	0.08	0.35	0.0%
OS1	9.27	0.90	0.96	2.85	30.7%	0.45	0.59	0.00	0.0%	0.30	0.40	2.85	6.1%	0.08	0.35	3.57	0.0%	0.40	0.55	36.9%
TOTAL (A1-B1)	44.43																			0.2%
TOTAL	53.70																			6.6%

### **EXISTING STANDARD FORM SF-2** TIME OF CONCENTRATION

Subdivision: Sterling Ranch Subdivision- Existing

Location: El Paso County

Project Name: Sterling Ranch Filing 3 Project No.: 25188.02 Calculated By: CJD Checked By:

Equation 6-3

Equation 6-5

Date: 6/9/21

		SUB-I	BASIN			INITI	AL/OVERI	AND	TRAVEL TIME									
		DA	ATA				(T <sub>i</sub> )			(T <sub>t</sub> )					(URBANIZED BASINS)			
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>	
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)	
A1	5.17	А	2%	0.08	0.35	212	2.0%	21.4	517	2.1%	10.0	1.4	6.0	27.4	729.0	32.1	27.4	
A2	27.48	А	0%	0.08	0.35	297	2.5%	23.4	1475	2.4%	10.0	1.6	15.7	39.1	1772.0	43.5	39.1	
B1	11.78	А	0%	0.08	0.35	297	2.9%	22.4	380	5.2%	10.0	2.3	2.8	25.2	677.0	29.1	25.2	
OS1	9.27	А	37%	0.40	0.55	298	2.7%	15.7	737	2.4%	10.0	1.5	8.0	23.7	1035.0	25.4	23.7	

NOTES:

 $t_c = t_i + t_t$ 

concentration.

Where:

te = computed time of concentration (minutes)

Use a minimum t<sub>c</sub> value of 5 minutes for urbanized areas and a minimum t<sub>c</sub> value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of

ti = overland (initial) flow time (minutes)

 $t_t$  = channelized flow time (minutes).

 $t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$ 

ti = overland (initial) flow time (minutes)  $C_5$  = runoff coefficient for 5-year frequency (from Table 6-4)  $L_i =$ length of overland flow (ft)  $S_0$  = average slope along the overland flow path (ft/ft).

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$ 

Where:

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Where:  $t_t$  = channelized flow time (travel time, min)  $L_t$  = waterway length (ft) So = waterway slope (ft/ft)  $V_t$  = travel time velocity (ft/sec) = K $\sqrt{S_o}$ K = NRCS conveyance factor (see Table 6-2). Where:

Equation 6-4  $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$ 

Equation 6-2

 $t_c$  = minimum time of concentration for first design point when less than  $t_c$  from Equation 6-1.  $L_{\rm f}$  = length of channelized flow path (ft) i = imperviousness (expressed as a decimal)  $S_t =$  slope of the channelized flow path (ft/ft).

#### STANDARD FORM SF-3 - EXISTING STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name: Sterling Ranch Filing 3 Project No.: 25188.02 Calculated By: CJD Checked By:

Subdivision: Sterling Ranch Subdivision- Existing Location: El Paso County Design Storm: 5-Year

ecked By:	
Date:	6/9/21

				DIRE	CT RUI	NOFF			T	OTAL F	RUNOF	F	STRE	et/sw	/Ale		PI	PE		TRA\	VEL TIN	ЛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1	A1	5.17	0.08	27.4	0.41	2.62	1.1															
	2	A2	27.48	0.08	39.1	2.20	2.08	4.6															Basin A2
	3	OS1	9.27	0.40	23.7	3.71	2.83	10.5															Basin A1
	4	B1	11.78	0.08	25.2	0.94													1				Basin OS1

Notes:

Street and Pipe C\*A values are determined by O/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

#### STANDARD FORM SF-3 - EXISTING STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	El Pas	o Coun	h Subdiv ty	/ision-	Existin	ng										P	roject N Projec alculate Checke	lame: ct No.: ed By: ed By: Date:			nch Fi	ling 3	
				DIR	RECT RU	JNOFF			I	OTAL F	RUNO	FF	STRE	ET/SW	ALE		PIP	E		TRAV	'EL TII	ME	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	1	A1	5.17	0.35	27.4	1.81	4.39	8.0	)														
	2	A2	27.48	0.35	39.1	9.62	3.49	33.6	, ,														Basin A2
	3	OS1	9.27	0.55	23.7	5.13	4.76	24.4															Basin A1
	4	B1	11.78	0.35	25.2	4.12	4.60	19.0	)														Basin OS1
Notes:																							

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

#### COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location: Sterling Ranch Subdivision El Paso County Project Name: Sterling Ranch Filing 3

Project No.: 25188.02 Calculated By: CJD

Checked By:

Date: 4/12/22

	Total	Str	reets (10	0% Impe	rvious)	Re	sidentia	l (65% Im	ipervious)	0			npervious) pervious)		•	6 Impervi % Imperv		Basins Weigł		Basins Total Weighted %
Basin ID	Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighte d % Imp.	Val C <sub>5</sub>	ues C <sub>100</sub>	Imp.
A1	4.37	0.90	0.96	0.92	21.1%	0.45	0.59	2.86	42.5%	0.59	0.70	0.00	0.0%	0.08	0.35	0.59	0.0%	0.49	0.64	63.6%
A5	0.45	0.90	0.96	0.17	37.8%	0.45	0.59	0.28	40.4%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.62	0.73	78.2%
1	24.50	0.90	0.96	0.26	1.1%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	24.24	0.0%	0.09	0.36	1.1%
12	3.47	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	3.47	0.0%	0.08	0.35	0.0%
B1	2.44	0.90	0.96	1.04	42.6%	0.45	0.59	1.28	34.2%	0.59	0.70	0.00	0.0%	0.08	0.35	0.12	0.0%	0.62	0.74	76.8%
B2	4.33	0.90	0.96	0.94	21.7%	0.45	0.59	3.39	50.9%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.55	0.67	72.6%
B6	0.79	0.90	0.96	0.00	0.0%	0.45	0.59	0.53	43.6%	0.59	0.70	0.00	0.0%	0.08	0.35	0.26	0.0%	0.33	0.51	43.6%
B5	0.45	0.90	0.96	0.00	0.0%	0.45	0.59	0.35	50.6%	0.59	0.70	0.00	0.0%	0.08	0.35	0.10	0.0%	0.37	0.54	50.6%
B4	1.59	0.90	0.96	0.00	0.0%	0.45	0.59	1.36	55.6%	0.59	0.70	0.00	0.0%	0.08	0.35	0.23	0.0%	0.40	0.56	55.6%
B3	0.59	0.90	0.96	0.34	57.6%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.25	0.0%	0.55	0.70	57.6%
D1	0.38	0.90	0.96	0.07	17.6%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.31	0.0%	0.22	0.46	17.6%
D2	3.92	0.90	0.96	0.31	7.8%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	3.61	0.0%	0.14	0.40	7.8%
Impervious Area in Platted Filing 3	20.9116	0.90	0.96	3.99	19.1%	0.45	0.59	10.05	31.2%	0.59	0.70	0.00	0.0%	0.08	0.35	6.87	0.0%	0.41	0.58	50.3%
Basin A,B,D TOTAL	19.31																			53.4%
TOTAL	47.28																			22.4%

#### PROPOSED STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision:	Sterling Ranch Subdivision
Location:	El Paso County

Project Name:	Sterling Ranch Filing 3
Project No.:	25188.02
Calculated By:	CJD
Checked By:	
Date:	4/12/22

		SUB-	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(L	JRBANIZED BA	ASINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t <sub>i</sub>	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized t <sub>c</sub>	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	4.37	A	64%	0.49	0.64	79	1.7%	8.2	1007	3.7%	20.0	3.8	4.4	12.5	1086.0	20.1	12.5
A5	0.45	А	78%	0.62	0.73	54	3.7%	4.1	217	3.9%	20.0	4.0	0.9	5.0	271.0	13.6	5.0
11	24.50	А	1%	0.09	0.36	793	3.1%	35.4	627	3.7%	10.0	1.9	5.4	40.8	1420.0	31.8	31.8
12	3.47	А	0%	0.08	0.35	383	3.2%	24.6	394	1.0%	10.0	1.0	6.6	31.1	777.0	33.3	31.1
B1	2.44	А	77%	0.62	0.74	50	2.5%	4.5	1066	1.6%	20.0	2.5	7.1	11.6	1116.0	20.1	11.6
B2	4.33	А	73%	0.55	0.67	226	4.9%	8.8	346	0.7%	20.0	1.7	3.4	12.2	572.0	17.2	12.2
B6	0.79	А	44%	0.33	0.51	246	1.5%	19.2	0	1.0%	20.0	2.0	0.0	19.2	246.0	18.6	18.6
B5	0.45	А	51%	0.37	0.54	129	5.0%	8.8	0	1.0%	20.0	2.0	0.0	8.8	129.0	17.4	8.8
B4	1.59	В	56%	0.40	0.56	222	11.0%	8.6	914	1.1%	20.0	2.1	7.4	16.0	1136.0	25.4	16.0
B3	0.59	А	58%	0.55	0.70	165	3.4%	8.5	612	2.7%	10.0	1.6	6.2	14.7	777.0	19.9	14.7
D1	0.38	А	18%	0.22	0.46	16	2.0%	5.0	570	6.0%	10.0	2.4	3.9	8.9	586.0	26.4	8.9
D2	3.92	A	8%	0.14	0.40	105	25.0%	6.1	975	50.0%	15.0	10.6	1.5	7.6	1080.0	26.9	7.6

NOTES:

 $t_c = t_i + t_t$ Equation 6-2 Table 6-2. NRCS Conveyance factors, K Where:  $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_e^{0.033}}$ Type of Land Surface Conveyance Factor, K Equation 6-3  $t_c =$  computed time of concentration (minutes) Heavy meadow Tillage/field Where: 5  $t_l = \text{overland (initial) flow time (minutes)}$ Short pasture and lawn Nearly bare ground  $t_i = \text{overland (initial) flow time (minutes)}$   $C_S = runoff coefficient for 5-year frequency (from Table 6-4)$   $L_i = \text{length overland flow (ft)}$   $S_p = \text{average slope along the overland flow path (ft/ft)}.$ tr = channelized flow time (minutes). 10 Grassed waterway  $t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$ 15 Equation 6-4 Paved areas and shallow paved swales 20  $t_r = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$ Where: Equation 6-5  $\label{eq:linear} \begin{array}{l} t_t = \text{channelized flow time (travel time, min)} \\ L_t = \text{waterway length (ft)} \\ S_0 = \text{waterway slope (ft/ft)} \\ V_t = \text{travel time velocity (ft/sec)} = K \sqrt{S_0} \\ K = \text{NRCS conveyance factor (see Table 6-2)}. \end{array}$ Where:  $t_t$  = minimum time of concentration for first design point when less than t<sub>t</sub> from Equation 6-1.  $t_x$  = length of channelized flow path (fl) = imperviouses (expressed as a decimal)  $S_t$  = slope of the channelized flow path (fl/fl). Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### STANDARD FORM SF-3 - PROPOSED STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location:	Sterlin El Paso	ng Rani o Cour	ch Subd	livision	I											1	ject Na Project culatec	No.:	25188	ng Rar 3.02	nch Fil	ling 3	
Design Storm:			1													С	hecked	d By:	4/12/	22			
			1	DIRE	CT RU	NOFF			T	OTAL R	UNOF	F	STRE	et/SW	/ALE		PIP	ЪЕ		TRAV	EL TIN	ЛЕ	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	9	B3	0.59	0.55	14.7	0.33	3.55	1.2															Offsite flow to existing inlet in Sterling Ranch Road Piped to existing storm sewer in Sterling Ranch Road
	10	B4	1.59					2.2								2.2	0.63	1.0	12	380	4.7		Rear lot and area inlets Piped to DP 11.1
	11	B5	0.45					0.7															Area Inlet Piped to DP 14.1
	11.1								17.3	0.80	3.30	2.6				2.6	0.80	1.0	18	357	4.9	1.2	Piped to DP 14.1
	12	B2	4.33	0.55	12.2	2.37	3.83	9.1								9.1	2.37	1.0	18	38	6.7		Sump Inlet Piped to DP 13.1
	13	B1	2.44	0.62	11.6	1.52	3.91	5.9															Sump Inlet Piped to DP 13.1
	13.1								12.3	3.89	3.82	14.9				14.9	3.89	1.0	24	125	7.6	0.3	Piped to DP 14.1
	14	B6	0.79	0.33	18.6	0.26	3.20	0.8															Area Inlet Piped to DP 14.1
	14.1								18.6	4.95	3.20	15.8				15.8	4.95	1.0	24		7.7		Piped to DP 15.1
	15	A1	4.37	0.49	12.5	2.16	3.79	8.2					0.8	0.21	1.6	7.4				230	2.5		On-grade Inlet Captured Flows piped to DP 15.1, Bypass flow to DP 17
	15.1								19.5	7.11	3.13	22.2				22.2	7.11	1.0	24	45	8.2		On-grade Inlet Captured Flows piped to DP 16.1
	16	A5	0.45	0.62	5.0	0.28	5.16	1.4															On-grade Inlet Captured Flows piped to DP 16.1
	16.1								19.6	7.39	3.12	23.1				23.1	7.39	1.0	24	125	8.2	0.3	FES release to drainage channel
	11	11	24.50	0.09	31.8	2.17	2.40	5.2															FES
	11.1								31.8	9.56	2.40	22.9				22.9	9.56	0.4	42	62	6.1	0.2	Combined flow from DPI1 & DP16.1 Piped to Existing 84" RCP
	12	12	3.47	0.08	31.1	0.28	2.43	0.7															Piped to Existing 84" RCP
	28	D1	0.38	0.22	8.9	0.09	4.30	0.4															Sheet flow to Sand Creek
	29	D2	3.92	0.14	7.6	0.56	4.53	2.5															Sheet flow to Sand Creek

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

#### STANDARD FORM SF-3 - PROPOSED STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

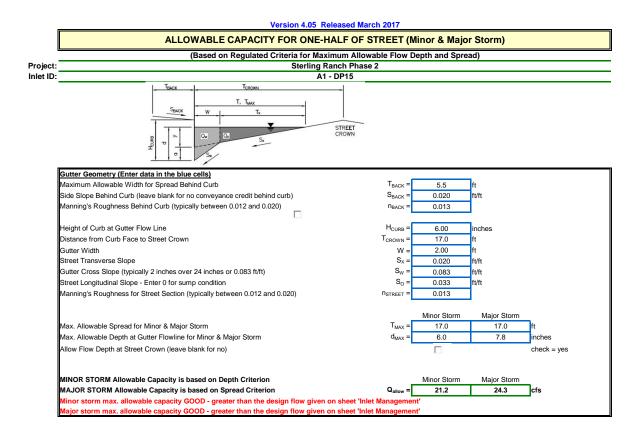
Subdivision:	Sterlin	n Rancl	h Subdi	vision												Pr	oject Na Project	ame:	Sterlin 25188	ng Ran	nch Fil	ing 3	
Location:	El Pas	o Count	y I	131011												Ca	alculated	d By:	CJD	.02			
Design Storm:	100-16	Edi															Checked E	Date:	4/12/	22			
				DIR	RECT R	UNOFF			T	OTAL RU	NOF	F	STRE	ET/SW/	ALE		PIPE			TRAV	EL TIN	ΛE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street/swale</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	9	B3	0.59	0.70	14.7	0.41	5.96	2.4															Offsite flow to existing inlet in Sterling Ranch Road Piped to existing storm sewer in Sterling Ranch Road
	10	B4	1.59	0.56	16.0	0.88	5.75	5.1								5.1	0.88	1.0	12	380	6.5		Rear lot and area inlets Piped to DP 11.1
	11	B5	0.45	0.54	8.8	0.24	7.24	1.7															Area Inlet Piped to DP 14.1
	11.1								17.0	1.12 5	5.60	6.3				6.3	1.12	1.0	18	357	6.2	1.0	Piped to DP 14.1
	12	B2	4.33	0.67	12.2	2.90	6.43	18.7								18.7	2.90				10.6		Sump Inlet Piped to DP 13.1
	13	B1	2.44	0.74	11.6	1.80	6.56	11.8															simp Inlet Piped to DP 13.1
	13.1								12.3	4.70	5.42	30.2				30.2	4.70	1.0	24	125	9.6		Piped to DP 14.1
	14	B6	0.79	0.51	18.6	0.40	5.37	2.1															Area Inlet Piped to DP 14.1
	14.1								18.6	6.22 5	5.37	33.4				33.4	6.22	1.0	24	415	10.6	0.7	Piped to DP 15.1
	15	A1	4.37	0.64	12.5	2.78	6.37	17.7					10.3	1.618	1.6	7.4				230	2.5	1.5	On-grade Inlet Captured Flows piped to DP 15.1, Bypass flow to DP 17
	15.1		1107	0.01	12.10	2.70	0.07		19.2	9.00 5	5 28	47.6				47.6	9.00	1.0	24	45	15.2		Captured Flows piped to DP 16.1
	16	A5	0.45	0.73	5.0	0.33	8.66	2.9	.,	7100		1710				1710	7100		2.	10	10.2		Captured Flows piped to DP 16.1
	16.1	7.0	0110	0.170	0.0	0.00	0.00	217	19.3	9.33 5	5.28	49.2				49.2	9.33	1.0	24	125	15.7		FES release to drainage channel
	1	11	24 50	0.36	31.8	8.73	4.02	35.1															FES
	11.1		21100	0.00	0.110	0170	1102	0011	31.8	18.06	1 02	72.6				72.6	18.06	0.4	42	62	7.6	01	Combined flow from DPI1 & DP16.1 Piped to Existing 84" RCP
	12	12	3.47	0.35	31.1	1.21	4.07	4.9															Piped to Existing 84" RCP
	28	D1	0.38				7.22	1.2															Sheet flow to Sand Creek
	29	D2	3.92	0.40			7.61	11.9															Sheet flow to Sand Creek

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value. All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

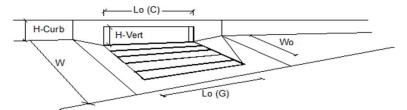
# Appendix C Hydraulic Calculations



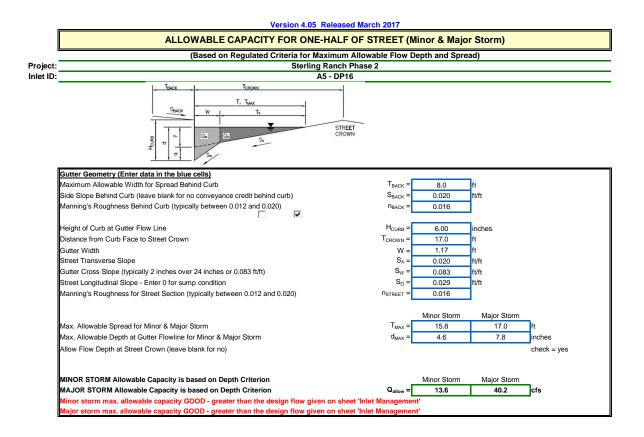


### INLET ON A CONTINUOUS GRADE



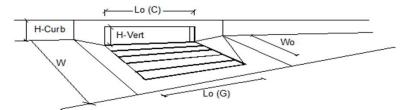


Design Information (Input)			MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	-	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a	LOCAL =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L <sub>o</sub> =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			MINOR	MAJOR	
Total Inlet Interception Capacity		Q =	7.8	12.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q <sub>b</sub> =	0.3	5.0	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =		C% =	96	71	%

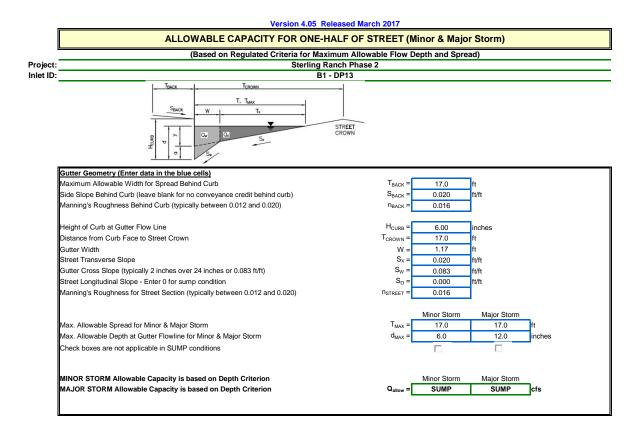


#### INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

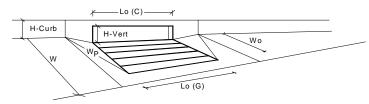


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.4	2.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.0	0.0	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	100	%

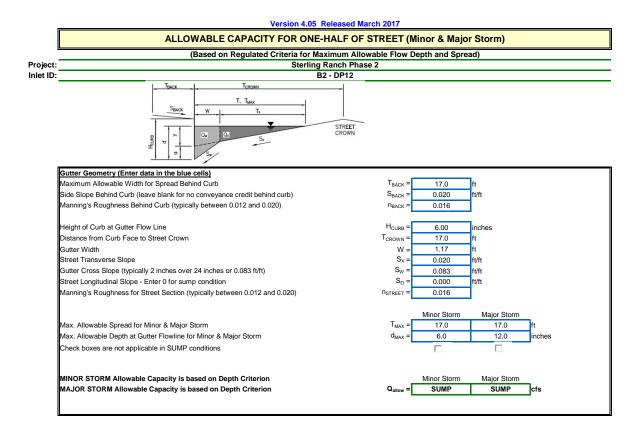


#### INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017

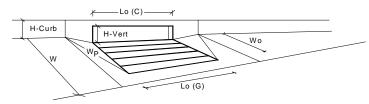


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.32	0.90	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.47	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.72	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	7.5	39.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.2	12.0	cfs



#### INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	7
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.37	0.90	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.53	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.76	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	13.1	52.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	9.1	18.7	cfs

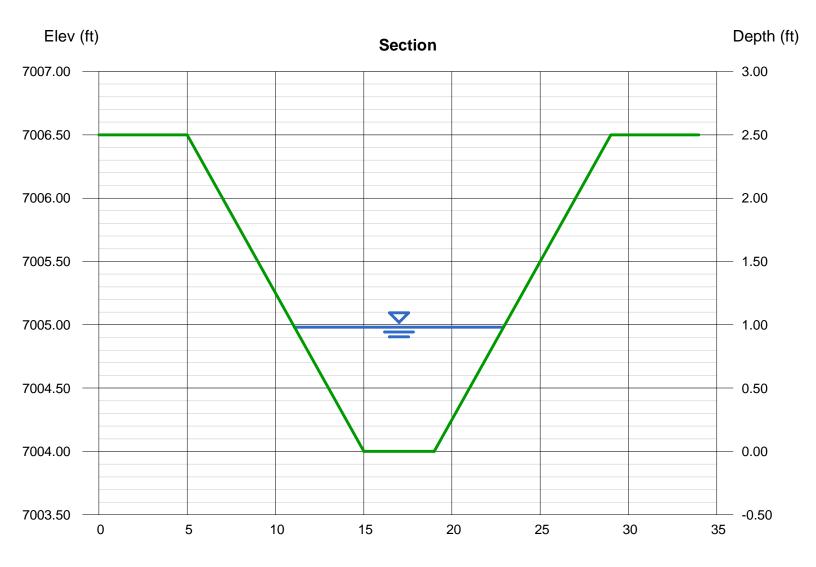
## **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Apr 12 2022

### **DP 13.1 - Emergency Overflow**

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.00	Depth (ft)	= 0.98
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 30.20
Total Depth (ft)	= 2.50	Area (sqft)	= 7.76
Invert Elev (ft)	= 7004.00	Velocity (ft/s)	= 3.89
Slope (%)	= 2.00	Wetted Perim (ft)	= 12.08
N-Value	= 0.040	Crit Depth, Yc (ft)	= 0.90
		Top Width (ft)	= 11.84
Calculations		EGL (ft)	= 1.22
Compute by:	Known Q		
Known Q (cfs)	= 30.20		



Reach (ft)

## **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Apr 27 2021

## **Interim Channel - DP I1**

# Triangular

Side Slopes (z:1) Total Depth (ft)	
Invert Elev (ft) Slope (%)	

# N-Value

## Calculations

Compute by: Known Q (cfs)

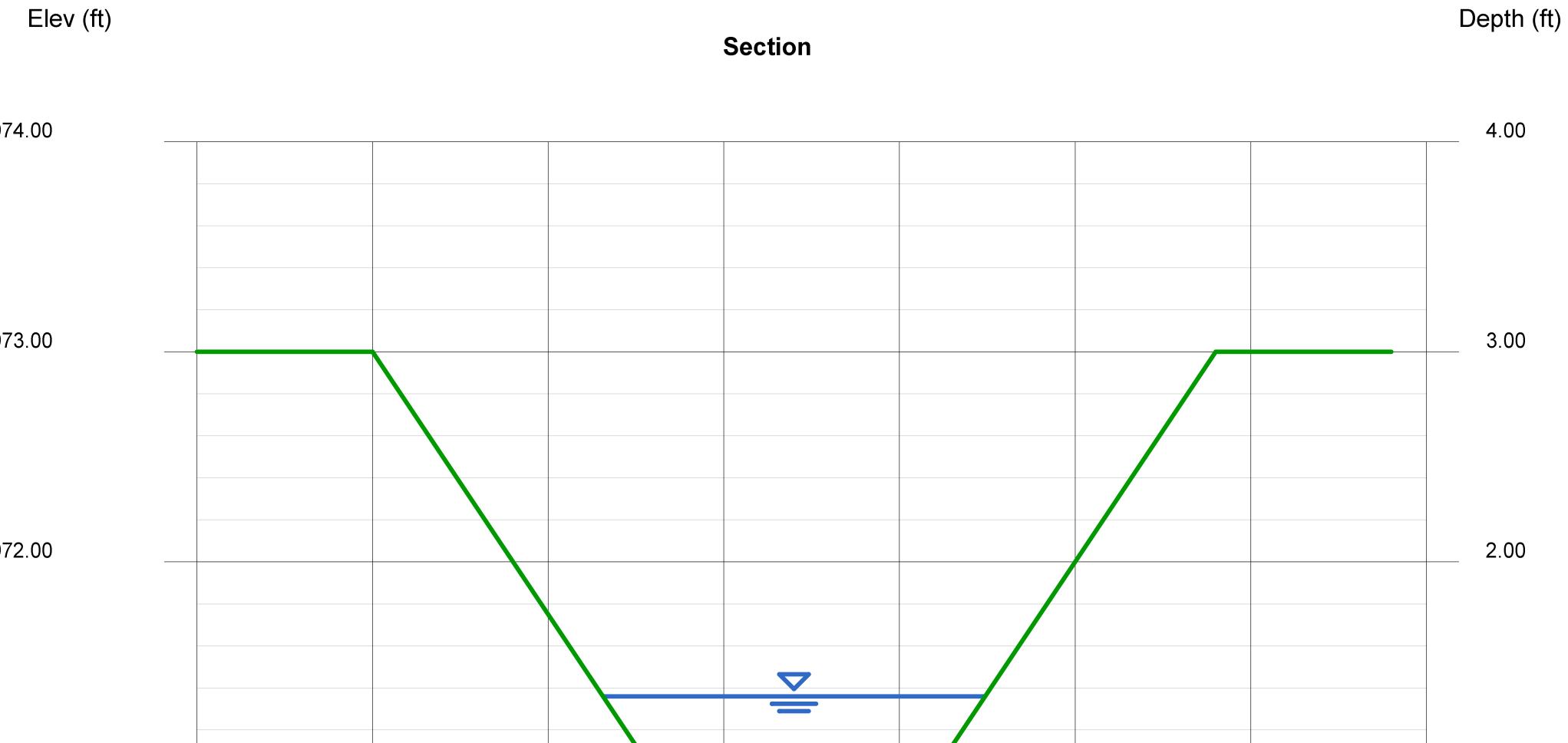
	4.00, 4.00 3.00
=	6970.00

- = 0.88
- = 0.025

Known Q = 31.20

## Highlighted

Depth (ft)	=	1.36
Q (cfs)	=	31.20
Area (sqft)	=	7.40
Velocity (ft/s)	=	4.22
Wetted Perim (ft)	=	11.21
Crit Depth, Yc (ft)	=	1.31
Top Width (ft)	=	10.88
EGL (ft)	=	1.64



Elev (ft)

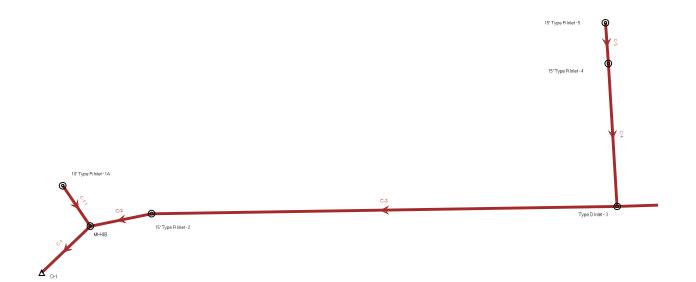
71	.00	

70.00

69.00

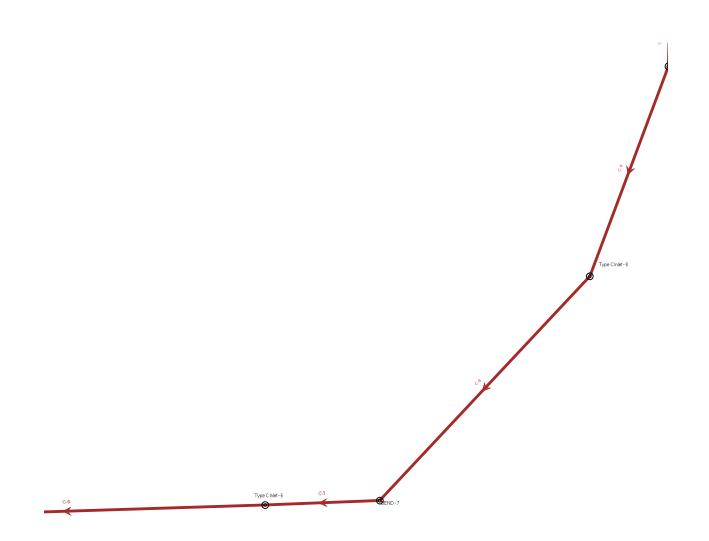
1.00								
0.00								
-1.00								
	35	30	25	20	15	10	5	0

Scenario: 100 YR



Phase 2 - Interim.stsw 12/10/2021

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 StormCAD [10.03.02.04] Page 1 of 1 Scenario: 100 YR



Phase 2 - Interim.stsw 12/10/2021

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 StormCAD [10.03.02.04] Page 1 of 1

#### Scenario: 100 YR



Phase 2 - Interim.stsw 12/10/2021

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 StormCAD [10.03.02.04] Page 1 of 1

Label	Flow (cfs)	Capacity (Full Flow) (cfs)	Velocity (ft/s)	Manning's n	Diameter (in)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
C-1	49.40	37.31	6.99	0.013	36.0	6,988.01	6,987.84	6,994.06	6,992.27	6,990.69	6,990.13	6,991.55	6,991.26
C-1.1	2.90	13.02	5.93	0.013	18.0	6,990.73	6,990.46	6,994.34	6,994.06	6,991.38	6,991.12	6,991.62	6,991.35
C-2	47.70	39.41	6.75	0.013	36.0	6,989.10	6,988.96	6,995.37	6,994.06	6,991.65	6,991.21	6,992.51	6,992.30
C-3	33.50	47.91	7.33	0.013	36.0	6,991.35	6,989.20	7,001.33	6,995.37	6,993.23	6,992.08	6,994.03	6,992.44
C-4	30.20	39.85	13.95	0.013	24.0	7,000.31	6,996.45	7,005.49	7,001.33	7,002.18	6,997.78	7,003.70	7,000.66
C-5	18.70	10.47	10.58	0.013	18.0	7,001.26	7,000.91	7,005.49	7,005.49	7,004.07	7,002.94	7,005.81	7,004.68
C-6	6.30	5.74	3.57	0.013	18.0	6,992.52	6,991.46	7,000.51	7,001.33	6,995.23	6,993.95	6,995.43	6,994.15
C-7	5.10	10.65	2.89	0.013	18.0	6,993.68	6,992.64	7,003.48	7,000.51	6,995.57	6,995.33	6,995.70	6,995.46
C-8	5.10	10.65	5.97	0.013	18.0	6,996.51	6,993.68	7,004.33	7,003.48	6,997.38	6,995.65	6,997.74	6,995.78
C-9	5.10	19.67	9.35	0.013	18.0	7,004.48	6,997.50	7,013.09	7,004.33	7,005.35	6,998.02	7,005.71	6,999.38
C-10	5.10	18.20	8.84	0.013	18.0	7,008.83	7,007.48	7,013.34	7,013.09	7,009.70	7,008.04	7,010.06	7,009.16
C-11	5.10	16.84	8.35	0.013	18.0	7,011.95	7,009.13	7,015.87	7,013.34	7,012.82	7,009.70	7,013.18	7,010.78

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Label	Flow (cfs)	Capacity (Full Flow) (cfs)	Velocity (ft/s)	Manning's n	Diameter (in)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
C-1	23.10	37.31	5.56	0.013	36.0	6,988.01	6,987.84	6,994.06	6,992.27	6,989.69	6,989.39	6,990.19	6,990.00
C-1.1	1.40	13.02	4.81	0.013	18.0	6,990.73	6,990.46	6,994.34	6,994.06	6,991.17	6,990.80	6,991.33	6,991.14
C-2	22.30	39.41	5.75	0.013	36.0	6,989.10	6,988.96	6,995.37	6,994.06	6,990.71	6,990.48	6,991.23	6,991.08
C-3	15.80	47.91	6.08	0.013	36.0	6,991.35	6,989.20	7,001.33	6,995.37	6,992.62	6,990.97	6,993.10	6,991.17
C-4	14.90	39.85	11.77	0.013	24.0	7,000.31	6,996.45	7,005.49	7,001.33	7,001.71	6,997.30	7,002.34	6,999.45
C-5	9.10	10.47	6.67	0.013	18.0	7,001.26	7,000.91	7,005.49	7,005.49	7,002.43	7,001.99	7,003.02	7,002.68
C-6	2.60	5.74	3.17	0.013	18.0	6,992.52	6,991.46	7,000.51	7,001.33	6,993.30	6,993.05	6,993.42	6,993.08
C-7	2.20	10.65	4.75	0.013	18.0	6,993.68	6,992.64	7,003.48	7,000.51	6,994.24	6,993.36	6,994.45	6,993.46
C-8	2.20	10.65	4.75	0.013	18.0	6,996.51	6,993.68	7,004.33	7,003.48	6,997.07	6,994.37	6,997.28	6,994.49
C-9	2.20	19.67	7.35	0.013	18.0	7,004.48	6,997.50	7,013.09	7,004.33	7,005.04	6,997.84	7,005.25	6,998.68
C-10	2.20	18.20	6.96	0.013	18.0	7,008.83	7,007.48	7,013.34	7,013.09	7,009.39	7,007.83	7,009.60	7,008.58
C-11	2.20	16.84	6.58	0.013	18.0	7,011.95	7,009.13	7,015.87	7,013.34	7,012.51	7,009.50	7,012.72	7,010.17

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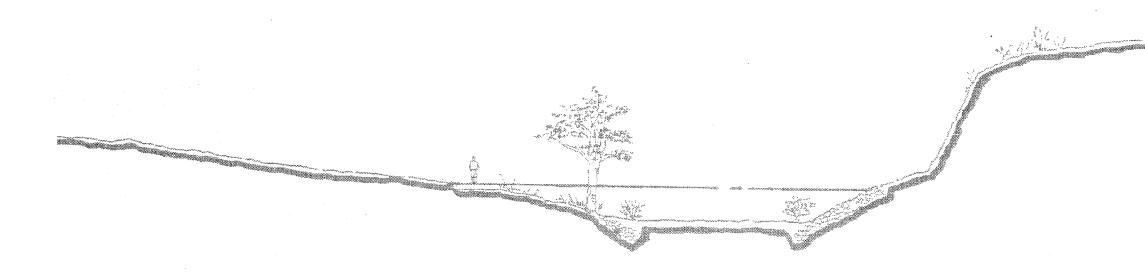
Appendix D Reference Material



## SAND CREEK DRAINAGE BASIN PLANNING STUDY

## PRELIMINARY DESIGN REPORT

## CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO



PREPARED FOR:

City of Colorado Springs Department of Comprehensive Planning, Development and Finance Engineering Division 30 S. Nevada Colorado Springs, Colorado 80903

#### PREPARED BY:

Kiowa Engineering Corporation 1011 North Weber Colorado Springs, CO 80903

#### **STUDY AREA DESCRIPTION** II.

The Sand Creek drainage basin is a left-bank tributary to the Fountain Creek lying in the west-central portions of El Paso County. Sand Creek's drainage area at Fountain Creek is approximately 54 square miles of which approximately 18.8 square miles are inside the City of Colorado Springs corporate limits. The basin is divided into five major sub-basins, the Sand Creek mainstem, the East Fork Sand Creek, the Central Tributary to East Fork, the West Fork, and the East Fork Subtributary. Figure II-1 shows the location of the Sand Creek basin.

#### **Basin Description**

The Sand Creek basin covers a total of 54 square miles in unincorporated El Paso County and Colorado Springs, Colorado. Of this total, approximately 28 square miles is encompassed by the Sand Creek basin, and 26 square miles for the East Fork Sand Creek basin. The basin trends in generally a south to southwesterly direction, entering the Fountain Creek approximately two miles upstream of the Academy Boulevard bridge over Fountain Creek. Two main tributaries drain the basin, those being the mainstem of Sand Creek and East Fork Sand Creek. Development presence in most evident along the mainstream. At this time, approximately 25 percent of the basin is developed. This alternative evaluation focuses upon the Sand Creek basin only.

The maximum basin elevation is approximately 7,620 feet above mean sea level, and falls to approximately 5,790 feet at the confluence with Fountain Creek. The headwaters of the basin originate in the conifer covered areas of The Black Forest. The middle eastern portions of the basin are typified by rolling range land with fair to good vegetative cover associated with semi-arid climates.

#### Climate

This area of El Paso County can be described, in general as high plains, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry. Precipitation ranges from 14 to 16 inches per year, with the majority of this precipitation occurring in spring and summer in the form of rainfall. Thunderstorms are common during the summer months, and are typified by quick-moving low pressure cells which draw moisture from the Gulf of Mexico into the region. Average temperatures range from about 30°F in the winter to 75° in the summer. The relative humidity ranges from about 25 percent in the summer to 45 percent in the winter.

#### Soils and Geology

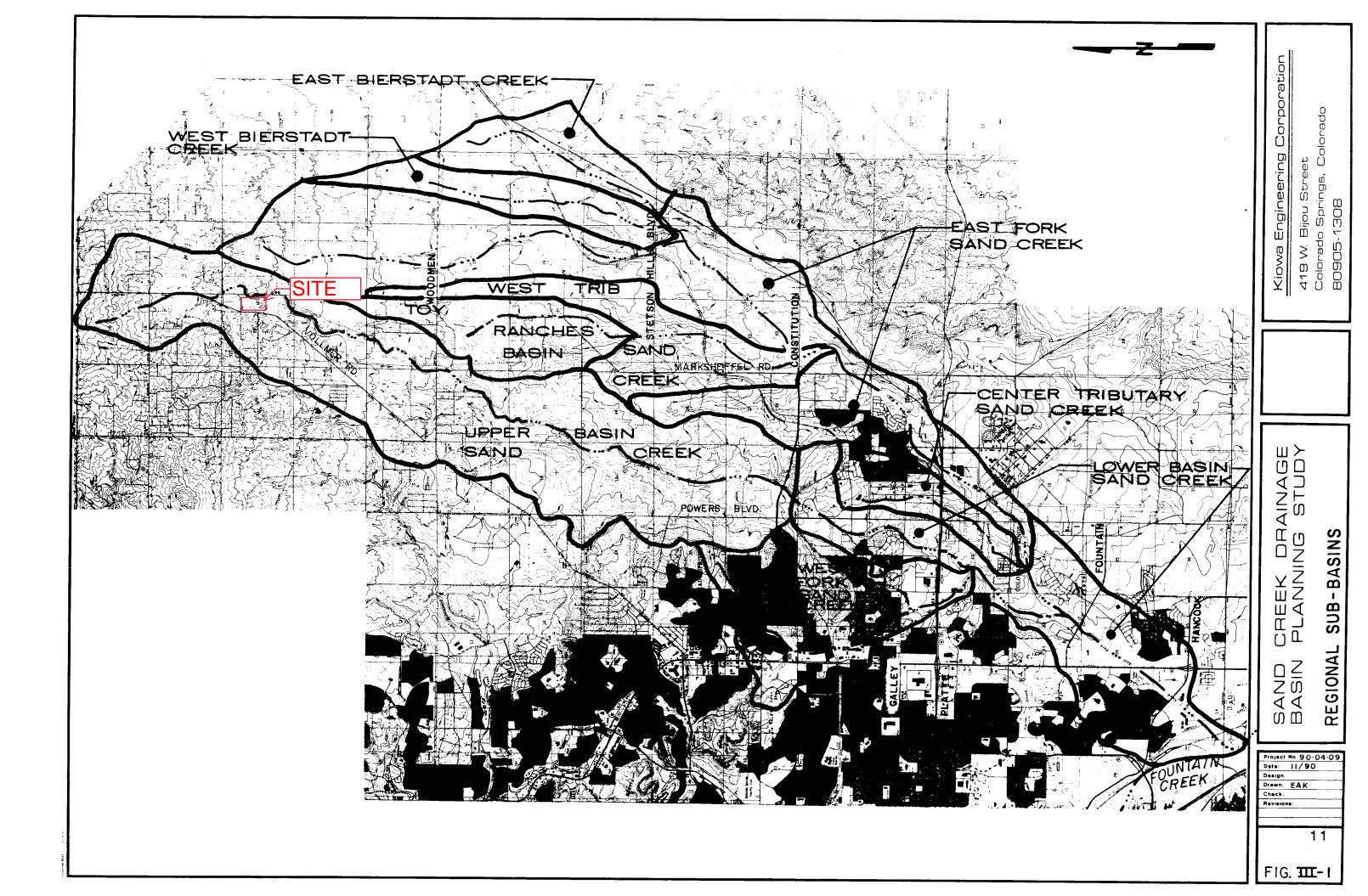
Soils within the Sand Creek basin vary between soil types A through D, as identified by the U.S. Department of Agriculture, Soil Conservation Service. The predominant soil groupings are in the Truckton and Bresser soil associations. The soils consist of deep, well drained soils that formed in alluvium and residium, derived from sedimentary rock. The soils have high to moderate infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. In undeveloped areas, the predominance of Type A and B soils give this basin a lower runoff per unit area as compared to basins with soils dominated by Types C and D. Presented on Figure II-2 is the Hydrologic Soil distribution map for the Sand Creek basin.

#### Property Ownership and Impervious Land Densities

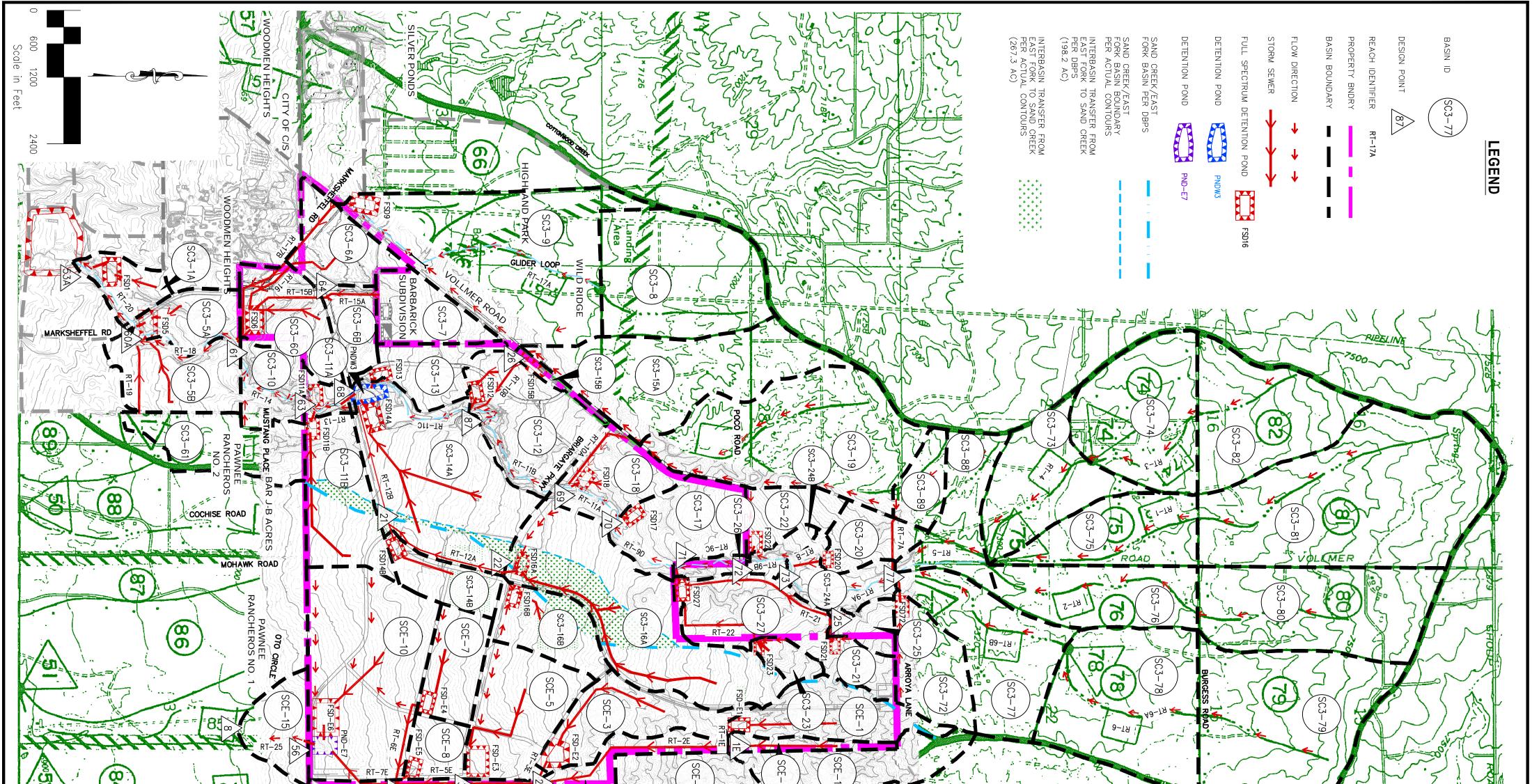
Property ownership along the major drainageway within the Sand Creek basin vary from public to private. Along the developed reaches, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. Where development has not occurred, the drainageways remain under private ownership with no delineated drainage right-of-way or easements. There are several public parks which abut the mainstem of Sand Creek. Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin.

Land use information for the existing and future conditions were reviewed as part of the planning effort. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the creek. Presented on Figure II-3 is the proposed land use map used in the evaluation of impervious land densities discussed in the hydrologic section of this report. Figure II-3 is not intended to reflect the future zoning or land use policies of the City or the County.

The land use information within the Banning-Lewis Ranch property was obtained from Aries Properties during the time the draft East Fork Sand Creek Drainage Basin Planning Study was being prepared. The land use information was again reviewed with the City of Colorado Springs Department of Planning and was found to be appropriate for use in the estimation of hydrology for the East Fork Basin. The location of future arterial streets and roadways within



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$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	BASIN CN AREA AREA AREA AREA (SS M) (GFS) Q5 (GFS) (GFS) Q5 (GFS)
	VATER QUALITY & DETENTION POND SUMMARY
Name <th< td=""><td>ALITY &amp; DETENTION POND SUMMARY</td></th<>	ALITY & DETENTION POND SUMMARY

#### **Worksheet for FSD Outlet Orifice Plate**

**Project Description** Solve For Diameter Input Data , 45.90 Hys (16.5 His+29.4 PLace) Discharge 4.70 ft Headwater Elevation **Centroid Elevation** 0.00 ft **Tailwater Elevation** 0.00 ft . **Discharge Coefficient** 0.60 Results 2.37 ft Diameter 4.70 ft Headwater Height Above Centroid Tailwater Height Above Centroid 0.00 ft Flow Area 4.40 ft<sup>2</sup> 10.43 ft/s Velocity

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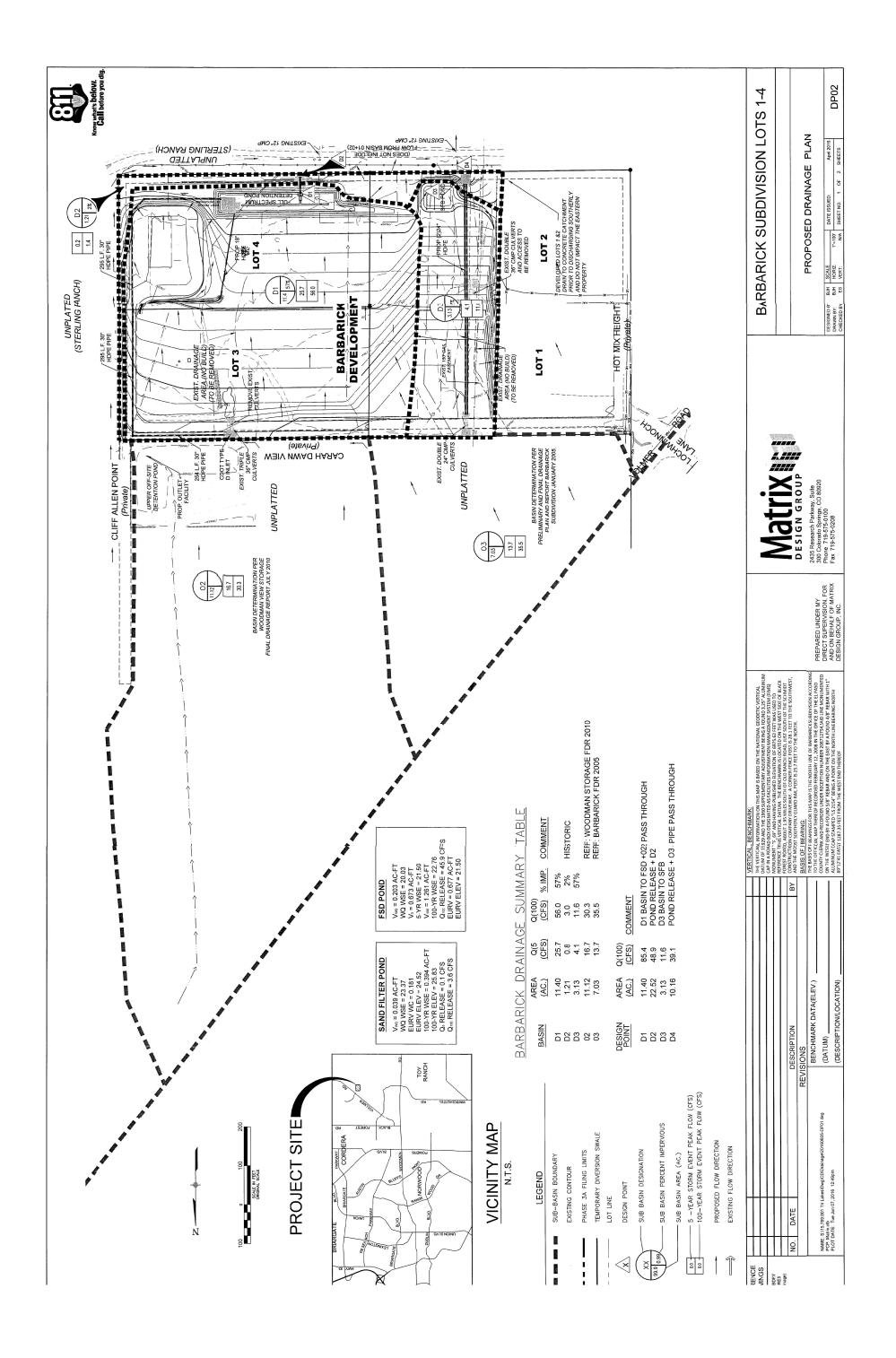
	Norksheet for	FSD Over	flow	v - Pass
Project Description				
Solve For	Discharge			
nput Data				
Headwater Elevation		0.90	ft	
Crest Elevation		0.00	ft	
<b>Failwater Elevation</b>		0.00	ft	
Crest Surface Type	Gravel			
Crest Breadth		12.00	ft	
Crest Length		36.00	ft	
Results	·			
Discharge		86.22	ft³/s	(55Dul+29.4 prec = 44.
leadwater Height Above Crest		0.90	ft	/
ailwater Height Above Crest		0.00	ft	
Veir Coefficient		2.80	US	
ubmergence Factor		1.00		
Adjusted Weir Coefficient		2.80	US	
low Area		32.40	ft²	
/elocity		2.66	ft/s	
Vetted Perimeter		37.80	ft	
Fop Width		36.00	ft	

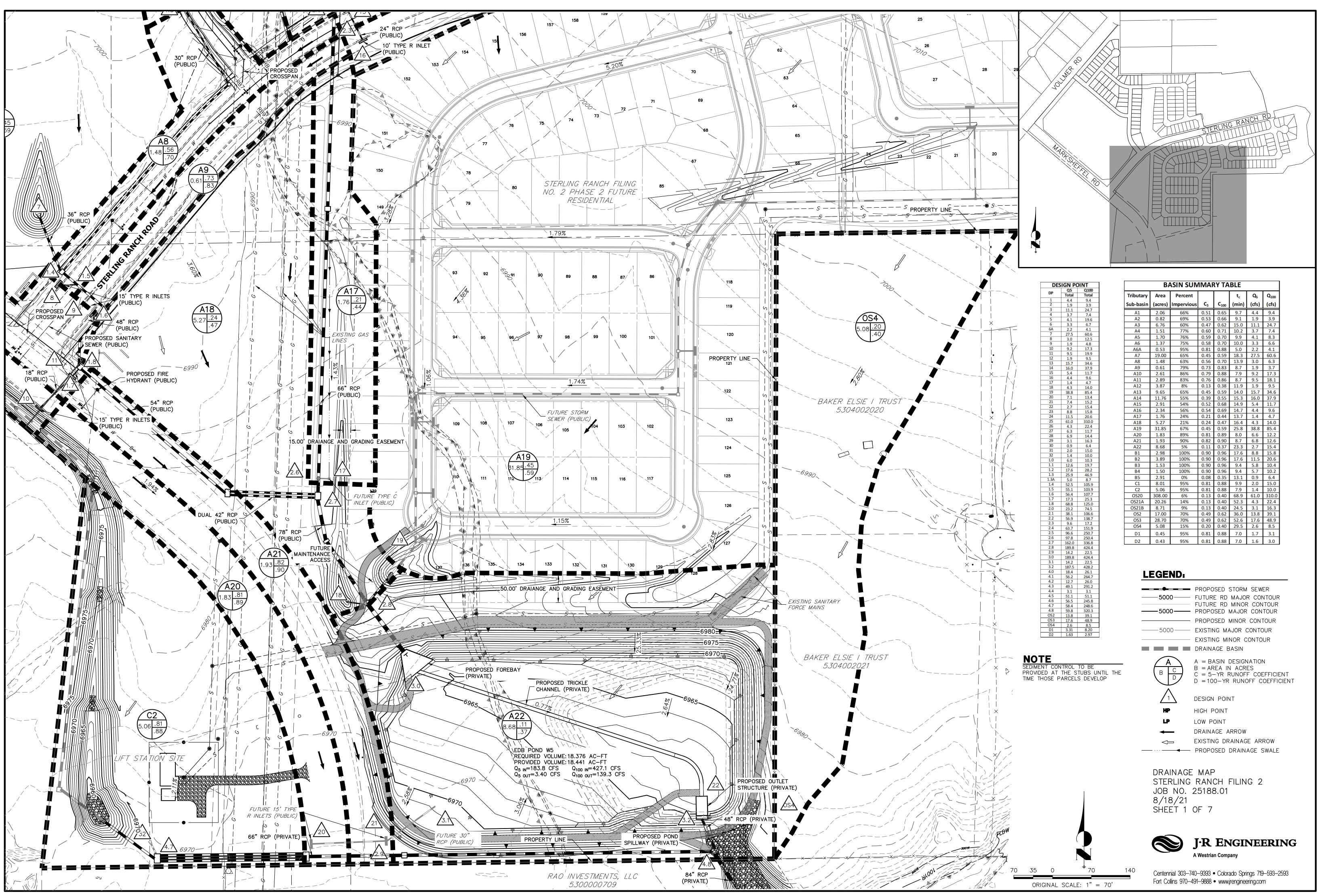
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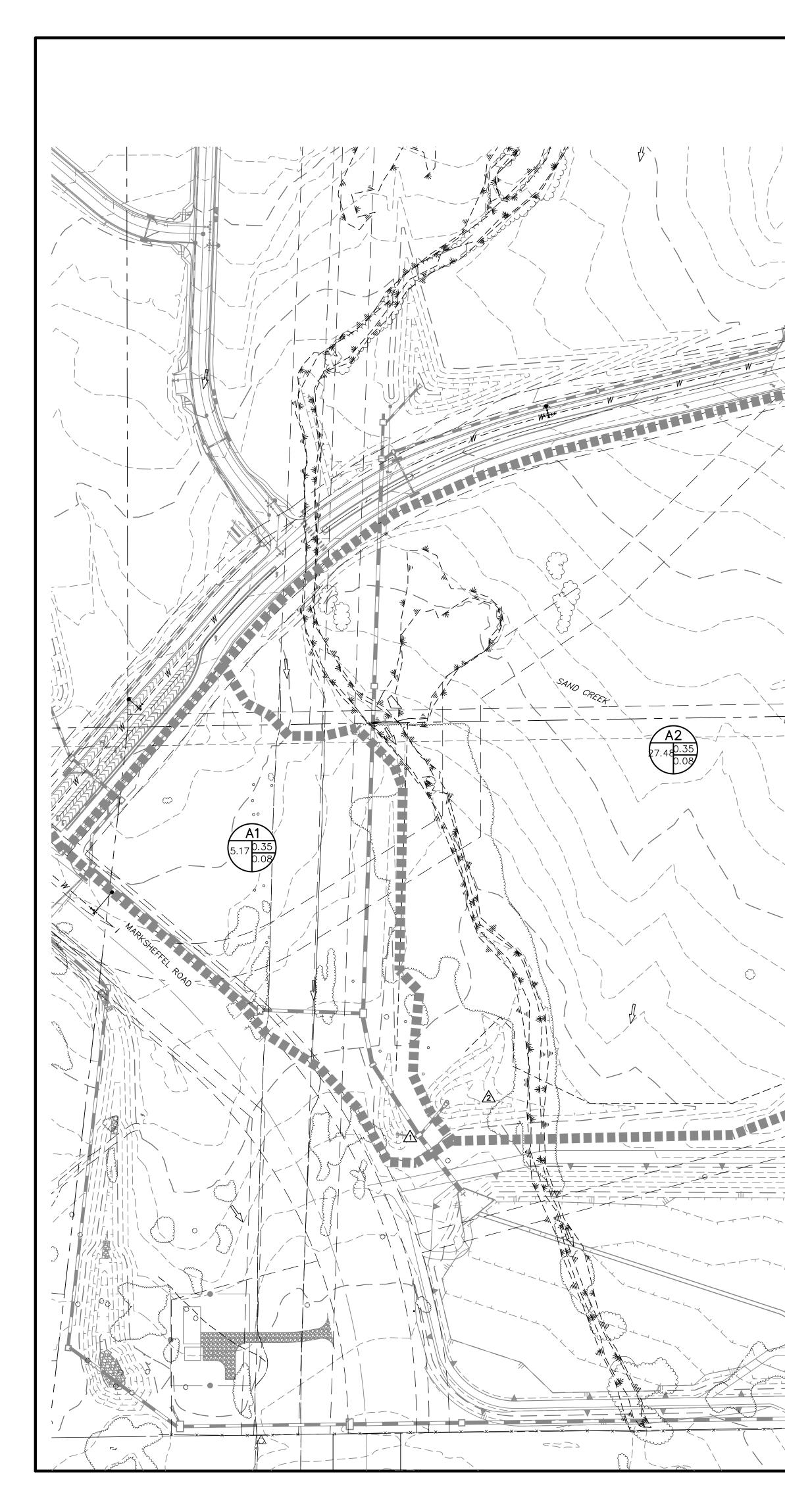


1	4.4	9.4
2	1.9	3.9
4	11.1	24.7
5	3.7 4.1	7.4 19.6
6	3.3	6.7
6A	2.2	4.1
7	27.5	60.6
8	3.0	12.5
9	1.9	4.8
10	9.2	17.3
11 12	9.5	19.9
12	1.9 15.7	9.5 34.6
15	16.0	37.9
15	5.4	11.7
16	4.4	9.6
17	1.4	4.7
18	4.3	14.0
19	38.8	85.4
20	7.1	13.4
21 22	7.4	15.2
22	2.7	15.4
23	8.8 11.5	15.8 20.6
25	61.0	310.0
26	4.3	22.4
27	6.3	11.7
28	6.9	14.4
29	3.1	16.3
30	0.9	6.4
31	2.0	15.0
32 1.0	1.4	10.0
1.1	6.0 12.6	10.3 19.7
1.2	17.6	28.2
1.3	25.9	46.9
1.3A	5.0	8.7
1.4	52.5	105.9
1.5	55.1	103.9
1.6	56.4	107.7
1.7 1.8	17.3	25.3
2.0	68.8 23.2	125.0 74.5
2.1	38.1	106.6
2.2	56.9	138.7
2.3	9.6	17.2
2.4	63.7	151.9
2.5	96.6	250.7
2.6	97.8	250.4
2.7	162.0	336.8
2.8	189.8 14.2	424.4 22.5
3.0	189.8	424.4
3.1	14.2	22.5
3.2	187.5	428.2
4.0	18.4	26.1
4.1	56.2	264.7
4.2	12.7	26.0
4.3 4.4	49.1	291.2
4.4	3.1 51.1	3.1 51.1
4.5	51.1 56.5	245.8
4.7	58.4	243.6
4.8	59.8	320.3
OS2	13.8	39.1
OS3	17.6	48.9
OS4	2.6	8.5
D1	3.31	8.20
D2	1.63	2.97

Tributary Area Percent					t <sub>c</sub>	Q₅	<b>Q</b> <sub>100</sub>
Sub-basin	(acres)	Impervious	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	(min)	(cfs)	(cfs)
A1	2.06	66%	0.51	0.65	9.7	4.4	9.4
A2	0.82	69%	0.53	0.66	9.1	1.9	3.9
A3	6.76	60%	0.47	0.62	15.0	11.1	24.7
A4	1.51	77%	0.60	0.71	10.2	3.7	7.4
A5	1.70	76%	0.59	0.70	9.9	4.1	8.3
A6	1.37	75%	0.58	0.70	10.0	3.3	6.6
A6A	0.53	95%	0.81	0.88	5.0	2.2	4.1
A7	19.00	65%	0.45	0.59	18.3	27.5	60.6
A8	1.48	63%	0.56	0.70	13.9	3.0	6.3
A9	0.61	79%	0.73	0.83	8.7	1.9	3.7
A10	2.61	86%	0.79	0.88	7.9	9.2	17.3
A11	2.89	83%	0.76	0.86	8.7	9.5	18.1
A12	3.87	8%	0.13	0.38	11.9	1.9	9.5
A13	9.65	65%	0.45	0.59	14.0	15.7	34.6
A14	11.76	55%	0.39	0.55	15.3	16.0	37.9
A15	2.91	54%	0.52	0.68	14.9	5.4	11.7
A16	2.34	56%	0.54	0.69	14.7	4.4	9.6
A17	1.76	24%	0.21	0.44	13.7	1.4	4.7
A18	5.27	21%	0.24	0.47	16.4	4.3	14.0
A19	31.85	67%	0.45	0.59	25.8	38.8	85.4
A20	1.83	89%	0.81	0.89	8.0	6.6	12.2
A21	1.93	90%	0.82	0.90	8.7	6.8	12.6
A22	8.68	5%	0.11	0.37	23.3	2.7	15.4
B1	2.98	100%	0.90	0.96	17.6	8.8	15.8
B2	3.89	100%	0.90	0.96	17.6	11.5	20.6
B3	1.53	100%	0.90	0.96	9.4	5.8	10.4
B4	1.50	100%	0.90	0.96	9.4	5.7	10.2
B5	2.91	0%	0.08	0.35	13.1	0.9	6.4
C1	8.01	95%	0.81	0.88	9.9	2.0	15.0
C2	5.06	95%	0.81	0.88	7.9	1.4	10.0
OS20	308.00	6%	0.13	0.40	68.9	61.0	310.0
OS21A	20.26	14%	0.13	0.40	52.3	4.3	22.4
OS21B	8.71	9%	0.13	0.40	24.5	3.1	16.3
OS2	17.00	70%	0.49	0.62	36.0	13.8	39.1
OS3	28.70	70%	0.49	0.62	52.6	17.6	48.9
OS4	5.08	15%	0.20	0.40	29.5	2.6	8.5
D1	0.45	95%	0.81	0.88	7.0	1.7	3.1
D2	0.43	95%	0.81	0.88	7.0	1.6	3.0

Appendix E Drainage Maps

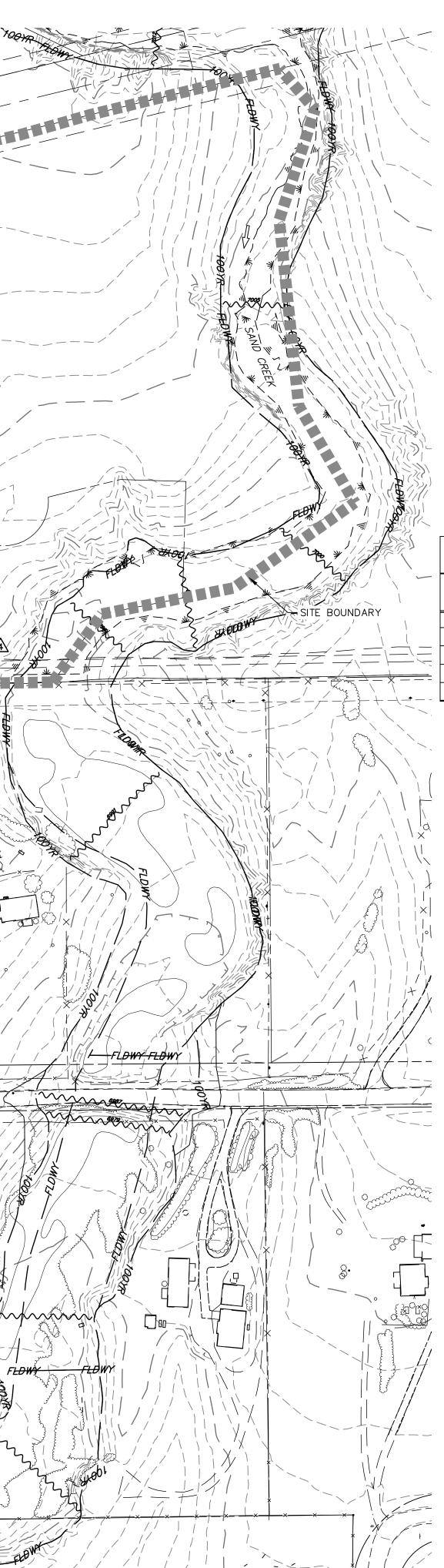




# **STERLING RANCH FILING 3** EXISTING DRAINAGE MAP

Renter and the second





## LEGEND

BASIN ID A: BASIN LABEL B: AREA C: C –100 YR D: C–5 YR	A B C D
DESIGN POINT	_#
EXISTING FLOW DIRECTION BASIN DRAINAGE AREA	
EXISTING STORM SEWER	
SITE BOUNDARY	
EXISTING PROPERTY LINE	
ROW EXISTING	
FL EXISTING	
SIDEWALK EXISTING	
DRAINAGE ACCESS & MAINTE EASEMENT	ENANCE — — — —

#### EXISTING

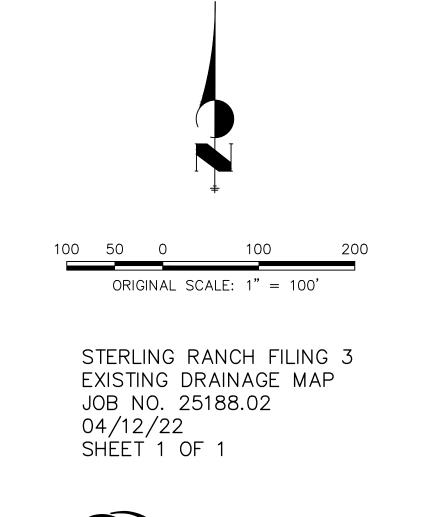
6100

#### BASIN SUMMARY TABLE

Tributary	Area	Percent			t <sub>c</sub>	Q₅	<b>Q</b> <sub>100</sub>
Sub-basin	(acres)	Impervious	<b>C</b> <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)
A1	5.17	2%	0.08	0.35	27.4	1.1	8.0
A2	27.48	0%	0.08	0.35	39.1	4.6	33.6
B1	11.78	0%	0.08	0.35	25.2	2.6	19.0
OS1	9.27	37%	0.40	0.55	23.7	10.5	24.4

DESIGN POINT				
	Q5	Q100		
DP	Total	Total		
1	1.1	8.0		
2	4.6	33.6		
3	10.5	24.4		
4	2.6	19.0		

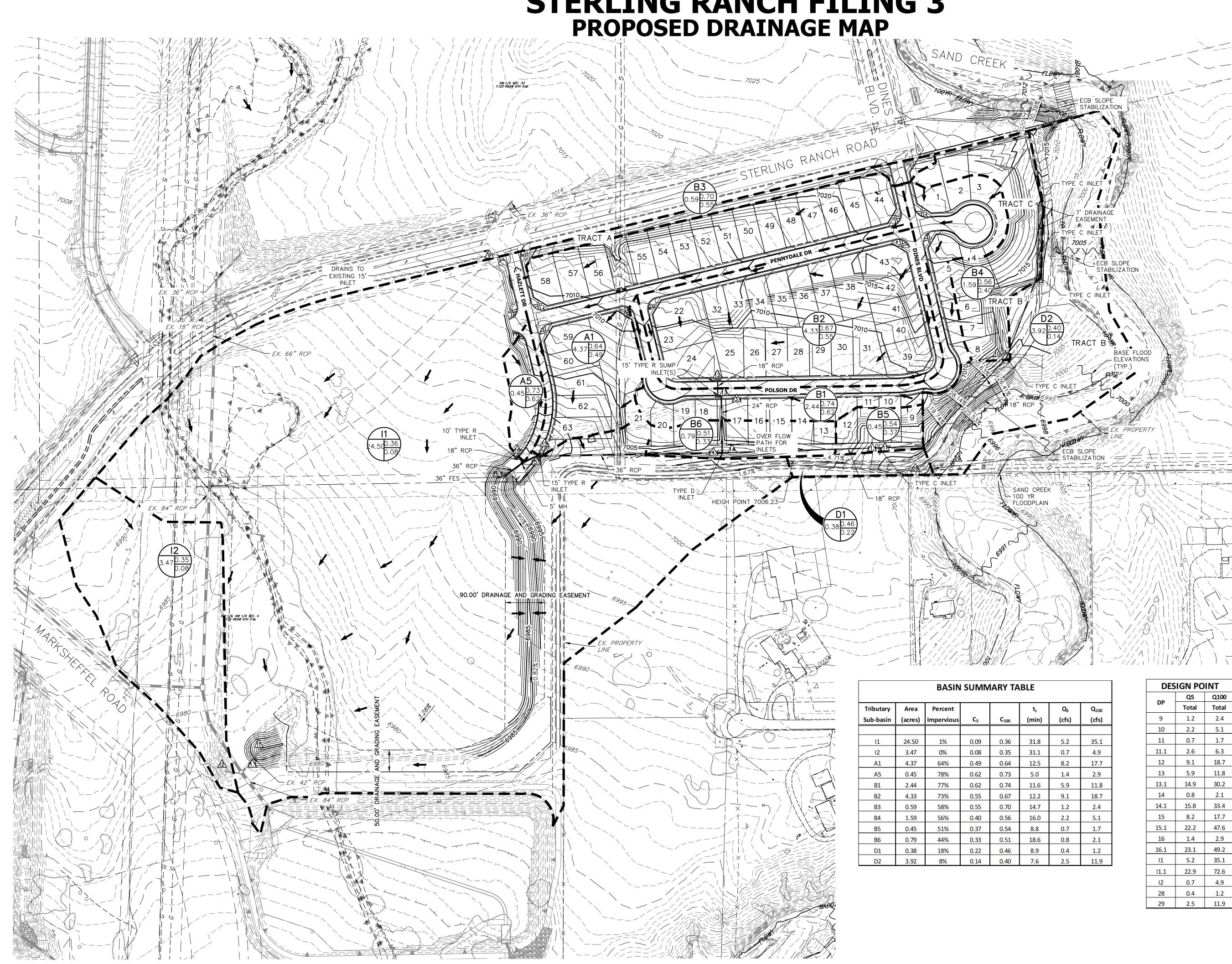
**NOTE** EXISTING GRADING ASSUMES FILING 2, STERLING RANCH ROAD, & MARKSHEFFEL ROAD ARE BUILT.





## J·R ENGINEERING A Westrian Company

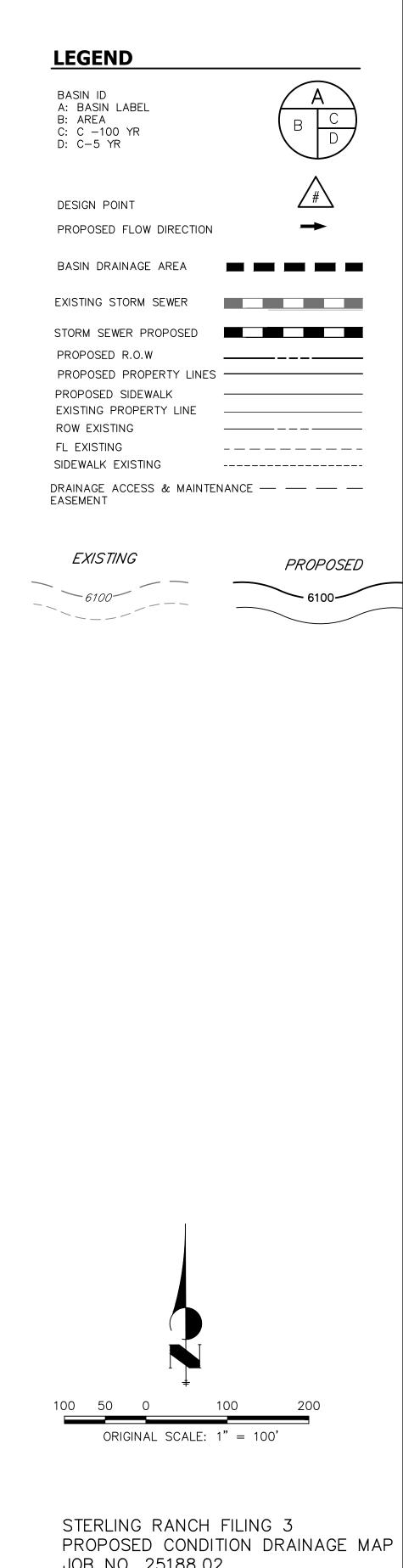
Centennial 303–740–9393 • Colorado Springs 719–593–2593 Fort Collins 970–491–9888 • www.jrengineering.com



# **STERLING RANCH FILING 3**

	t <sub>c</sub> (min)	Q₅ (cfs)	Q <sub>100</sub> (cfs)
Ť			
Ι	31.8	5.2	35.1
	31.1	0.7	4.9
	12.5	8.2	17.7
	5.0	1.4	2.9
	11.6	5.9	11.8
	12.2	9.1	18.7
	14.7	1.2	2.4
	16.0	2.2	5.1
	8.8	0.7	1.7
	<mark>18.</mark> 6	0.8	2.1
	<mark>8.</mark> 9	0.4	1.2
	7.6	2.5	11.9

DESIGN POINT			
DD	Q5	Q100	
DP	Total	Total	
9	1.2	2.4	
10	2.2	5.1	
11	0.7	1.7	
11.1	2.6	6.3	
12	9.1	18.7	
13	5.9	11.8	
13.1	14.9	30.2	
14	0.8	2.1	
14.1	15.8	33.4	
15	8.2	17.7	
15.1	22.2	47.6	
16	1.4	2.9	
16.1	23.1	49.2	
11	5.2	35.1	
11.1	22.9	72.6	
12	0.7	4.9	
28	0.4	1.2	
29	2.5	11.9	



JOB NO. 25188.02 04/12/22 SHEET 1 OF 1



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