

**FINAL DRAINAGE REPORT
FOR
STERLING RANCH FILING NO. 2**

**Prepared For:
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**January 2021
Project No. 25188.01**

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PCD File No. SF-20-015

**Final Drainage Report
Sterling Ranch Filing No. 2**

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. # 32314
For and On Behalf of JR Engineering, LLC

Date

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: SR Land, LLC

By: _____

Title: _____

Address: 20 Boulder Crescent, Suite 210
Colorado Springs, CO 80903

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E.
County Engineer/ ECM Administrator

Date

Conditions:



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PURPOSE

This document is the Final Drainage Report for Sterling Ranch Filing No.2. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The following report is an analysis of the drainage for the entire development and surrounding areas.

GENERAL LOCATION AND DESCRIPTION

Location

Sterling Ranch Filing No. 2 is located in Section 32, Township 12 South, Range 65 West of the 6th Principal Meridian, Section 33, Township 12 South, Range 65 West of the 6th Principal Meridian and Section 4, Township 13 South, Range 65 West of the 6th Principal Meridian within unincorporated El Paso County, Colorado. The site is bound on the west by existing Vollmer Road. The site is bound on the north by the Barbarick Subdivision. The property is bound to the east by the Sterling Ranch Phase 2 and Vollmer Road to the west. The site is bound on the south by Sterling Ranch Road and Marksheffel Road. Sterling Ranch lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

Description of Property

Sterling Ranch Filing No. 2 consists of 49.5387 acres and is presently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from north to south at grade rates that vary between 2% and 8%.

Sterling Ranch Filing No. 2 is currently zoned "RS-5000" for residential single family development. Improvements proposed for the site include paved, streets, trails, utilities, and storm drainage improvements, drainage swales, and detention ponds as normally constructed for a residential development. Two full spectrum detention facilities are proposed to be constructed to provide water quality treatment and detain stormwater for the development. The proposed water quality and detention facilities will also be designed to incorporate the Sterling Ranch Phase 2 and Copper Chase at Sterling Ranch developments as well as other offsite areas. Approximately 174 acres are tributary to Pond W5 which includes all 49 acres of Sterling Ranch Filing No. 2. Approximately 350.74 acres of offsite area are tributary to Pond W-4.

Soils for this project are classified as Blakeland Loamy Sand (8), Flakeland-Fluvaquentic Haplaquolis (9) and Columbine Gravelly Sandy Loam (19). These soils are characterized as Hydrologic Soil Types "A". Group A soils exhibit high infiltration rates when thoroughly wet, and consist mainly of deep, well drained to excessively drained sands or gravelly sands. Pring Coarse Sandy Loam (71) is characterized as Hydrologic Soil Types "B". Group B soils exhibit moderate infiltration rate when thoroughly wet, and consist primarily of deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. A soil map of the site can be found in Appendix A.

Wetlands

Sterling Ranch was authorized under Section 404 of the Clean Water Act to discharge dredged and fill materials into waters of the United States to conduct work associated with construction of Sterling Ranch Residential Development in accordance with Action Number SPA-2015-00428-SCO. A copy of the permit is within the Appendix of this report. For the construction of Sterling Ranch Filing 2, ~17,582 square feet of wetlands will be displaced and will be mitigated. Wetlands that overlap with Sterling Ranch Filing 2 are located in Basin A8, A9, A22, and A13. The disturbance areas are located within the general area of Pond W5, which outfall into the Sand Creek Channel. A mitigation area is designated on the Sterling Ranch filing No. 2 construction drawings by JR Engineering. Coordination with the wetlands consultant and the Army Corp of Engineers will be in conformance with the wetland permit. The memo and map from Core Consultants showing intent to have wetlands delineated in the Filing No. 2 areas of wetland disturbance and mitigation can be found in the appendix.

Floodplain Statement

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, all of the proposed development lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. No grading operations are proposed within the Zone AE at this time. FIRM Maps have been presented in Appendix A.

DRAINAGE BASINS AND SUB-BASINS

Existing Major Basin Descriptions

The Sterling Ranch Filing No. 2 site consists of 49.5387 acres and is located in the Sand Creek Drainage Basin, but limits of this report consist of 538 acres. The site area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area was studied in the "Preliminary Drainage Report for Sterling Ranch-Phase 1", dated May 2015, by M&S Civil Consultants, Inc. The Sterling Ranch Area has recently been studied in the "Master Development Drainage Plan for Sterling Ranch" (MDDP), dated October 2018, by M&S Civil Consultants, Inc.

The Sand Creek DBPS assumed the Sterling Ranch property to have a "large lot residential" use for the majority of the site. However, the proposed master plan is a mix of; school, multi-family, single-family, and commercial land uses, resulting in higher runoff. The site generally drains from north to south consisting of rolling hills. Currently, the site is used as pasture land for cattle. Sand Creek is located east of the site running north to south. This reach of drainage conveyance is not currently improved. There are a few stock ponds within the creek channel used for cattle watering.

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An existing subdivision to the north of the proposed site known as Barbarick Subdivision will generate runoff that is collected by detention ponds and are released at the north property line of the proposed Sterling Ranch Filing No. 2 Phase 2 site. See “Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3 & 4, by Matrix Design Group, June 2016”. These offsite flows have been accounted for in order to ensure the proposed storm sewer infrastructure will have adequate capacity. If future offsite development occurs upstream of Sterling Ranch from the west, the properties will be required to detain to historic/ existing conditions per the County / City drainage criteria. A proposed drainage map showing these offsite basins can be found in Appendix E.

The following drainage basin narratives are based on information derived from field visits, USGS topographic mapping, aerial topography, field surveys and information provided by others familiar with the site. A “sheet flow” verses “concentrated ditch flow” designation was determined as best as possible from the available source topography, actual conditions may vary. A summary of peak runoff for the basins and designated design points are depicted on the Existing Conditions Drainage Map in the appendix.

Existing Sub-basin Drainage

Basin EXA1 ($Q_5=7.2$ cfs, $Q_{100}=12.1$ cfs) is 17.68 acres and is primarily open space and the existing Vollmer road. Runoff from this basin drains to the south east to DP 1 where it ultimately outfalls into the Sand Creek Drainageway.

Basin EXA2 ($Q_5=5.4$ cfs, $Q_{100}=9.0$ cfs) is 19.59 acres and is primarily open space and the existing Vollmer Road. Runoff from this basin drains to the south east to DP 2. Runoff is captured by an existing swale at DP 4.1 where it is conveyed to the Sand Creek Drainageway(See Sand Creek Drainage Basin Planning Study, Segment 159, page 47-48, anticipated flows=950 cfs).

Basin EXA3 ($Q_5=1.4$ cfs, $Q_{100}=2.3$ cfs) is 5.66 acres and is primarily open space. Runoff from this basin drains south to DP 3 where it ultimately outfalls into the Sand Creek Drainageway.

Basin EXA4 ($Q_5=10.6$ cfs, $Q_{100}=17.8$ cfs) is 50.72 and is primarily open space. Runoff from this basin drains to the south to DP 4. Runoff is then captured by an existing swale at DP 4.1 where it is conveyed to the Sand Creek Drainageway.

Basin EXB ($Q_5=3.0$ cfs, $Q_{100}=5.0$ cfs) is 11.78 acres and is comprised of open space and a portion of Sand Creek along the eastern most portion of the Sterling Ranch Filing No. 2 site. Runoff from this basin drains into Sand Creek.

Basin EXC1 ($Q_5=3.3$ cfs, $Q_{100}=5.5$ cfs) is 12.36 acres and is comprised of open space and a portion of Vollmer Road. Runoff from this basin drains south and does not flow onto the site.

Basin EXC2 ($Q_5=1.4$ cfs, $Q_{100}=2.3$ cfs) is 5.06 acres and is comprised of open space. Runoff from this basin drains south and does not flow onto the site.

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Basin OS1 ($Q_5=23.9$ cfs, $Q_{100}=40.1$ cfs) is 23.82 acres and is located just north of the site. Flows from this sub-basin flow directly onto basin EXA4. Runoff from this sub-basin eventually flow to the existing swale at DP 4.1 where it is conveyed into Sand Creek.

Basin OS2 ($Q_5=37.3$ cfs, $Q_{100}=62.6$ cfs) is comprised of 85.59 acres. Flows from this sub-basin flow directly onto basin A4. Runoff from this sub-basin eventually flow to the existing swale at DP 4.1 where it is conveyed into Sand Creek.

Basin OS3 ($Q_5=1.8$ cfs, $Q_{100}=3.1$ cfs) is 6.66 acres and is located just north of the site. Flows from this sub-basin flow directly onto basin A4. Runoff from this sub-basin eventually flow to the existing swale at DP 4.1 where it is conveyed into Sand Creek.

Basin OS4 ($Q_5=0.5$ cfs, $Q_{100}=0.9$ cfs) is 2.19 acres is comprised of open space just north of the site. Runoff from this basin drains south directly onto Basin B1 where it outfalls directly into Sand Creek.

Basin OS5 ($Q_5=7.5$ cfs, $Q_{100}=23.4$ cfs) is 9.27 acres and is comprised of existing single family residential. Runoff from this site drains southwest onto basin A4 where it eventually flows to the existing swale at DP 4.1. From here, it is conveyed south into Sand Creek.

Basin OS20 ($Q_5=33.7$ cfs, $Q_{100}=226.1$ cfs) is 308 acres and is comprised primarily of developed and undeveloped land with lots ranging from 2.5 to 90 acres in size. The ground cover is comprised of mainly native grasses. Runoff from this site drains southwest into basin via sheetflow and an existing drainage ditch along the west side of Volmer Road to OS21A.

Basin OS21B ($Q_5=2.1$ cfs, $Q_{100}=14.5$ cfs) is 8.71 acres and is comprised of undeveloped land covered with mainly native grasses. Runoff from this site sheet flows southeast onto basin OS21A.

Basin OS21A ($Q_5=2.8$ cfs, $Q_{100}=18.7$ cfs) is 20.26 acres and is comprised primarily of developed land with lots ranging from 2.5 to 5 acres in size. The ground cover is comprised of mainly native grasses. Runoff from this site drains southwest into basin via sheetflow and an existing drainage ditch along the west side of Volmer Road. Flows from basins OS21A combines with OS21B and OS20 where the combined flow generally sheet flows to the southeast where it eventually reaches Sand Creek. Offsite Basins OS20, OS21B and OS21A correspond to Basins SC3-8 ($Q_5=42.1$ cfs, $Q_{100}=166.2$ cfs) and SC3-9($Q_5=71.5$ cfs, $Q_{100}=254.0$ cfs) from the MDDP

Proposed Sub-basin Drainage

The following is a description of the offsite and onsite basins, offsite bypass flows and the overall future drainage characteristics for the development of Sterling Ranch Filing No. 2. Ponds W4 and W5 are sized for the ultimate development, therefore, future developments have been included. As the future sites develop, final drainage reports will be completed to confirm the assumptions made in this report. Calculations have been provided to show the proposed storm infrastructure will adequately convey flows in the ultimate condition. The following basins parameters and developed runoff were determined using the Rational Method. Surface flow is designated as design points with whole numbers (1) and storm sewer routing as design points with decimals (1.0). See Appendix B for all Rational Method calculations and storm water routing.

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Basin A consists of Sub-Basins A1-A22 combining for a total of 123.19 acres. This basin represents all 49.5387 acres of the proposed Sterling Ranch Filing 2 development. This basin is primarily single-family residential, roadway and minor open space. This basin also contains future commercial sites, the future Sterling Ranch Phase 2 development, the proposed Copper Chase at Sterling Ranch Development and a proposed school site. Stormwater runoff is conveyed via public streets where it is captured via a series of on-grade and sump inlets. Runoff is then piped to a proposed onsite Full Spectrum Detention Pond W5. From the detention pond, the treated flows are then released directly into the Sand Creek Drainageway at below historic rates.

Off-Site Conveyance

The existing drainage patterns on the west side of Vollmer Road will not change due to the development of Sterling Ranch. Vollmer Road construction will address the roadside ditch flows along the west side of the road and will install drainage culverts where indicated in this report. The majority of the flows from the west side of Vollmer Road are to be routed in the historical direction to the southwest along the roadway to proposed Pond W-4. Runoff produced from the remaining off-site watershed located along the west edge of the existing development will be routed along the west side of Vollmer Road to the southwest corner of the existing development and a proposed Pond W-4. At the northwest corner of Tahiti Drive and Vollmer Road a 66" RCP will be installed to collect and convey runoff under proposed Marksheffel Road before ultimately discharging into Sand Creek. Runoff reaching the development along the south boundary line of the Barbarick Subdivision will be conveyed through and around the proposed site by proposed temporary swales and proposed storm sewer until it ultimately reaches Pond W-5. At the time of final for Sterling Ranch Filing No. 2 Phase 2, JR will coordinate with Barbarick to determine a more specific design solution for conveying the flows from their site. In general, the sand filter and double barrel 24" RCP will discharge onto the Sterling Ranch Phase 2 site where it will be picked up in a sump inlet structure and conveyed through a 48" RCP through the Sterling Ranch Storm system to Pond W5. The eastern Barbarick EDB discharge pipe will be connected into a structure and into a 36" RCP where the flows will be routed to Pond W5. Specific design details can be found within the Sterling Ranch Phase 2 drainage report. Runoff reaching the northern boundary of Phase I at proposed Briargate Parkway will be redirected around the site via a temporary swale to Sand Creek. BMP's will be installed to prevent erosion of the temporary swale. The intention of the drainage design for Sterling Ranch is to not adversely affect any adjacent property within the developed flows from Sterling Ranch.

Sub-basin A1 ($Q_5=4.4$ cfs, $Q_{100}=9.4$ cfs) consists of approximately 2.06 acres and is the northern most portion of the Sterling Ranch Filing No. 2 Phase 1 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter then captured by a 10' on-grade inlet at DP 1. From here, the flow is piped to Pond W5.

Sub-basin A2 ($Q_5=1.9$ cfs, $Q_{100}=3.9$ cfs) consists of approximately 0.82 acres and is the north eastern most portion of the Sterling Ranch Filing No. 2 Phase 1 development. This basin is primarily singlefamily residential and minor open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter then captured by a 10' Type R on-grade inlet at DP 2. From here, the flow is piped to Pond W5.

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Sub-basin A3 ($Q_5=11.1$ cfs, $Q_{100}=24.7$ cfs) consists of approximately 6.76 acres and is the north western most portion of the Sterling Ranch Filing No. 2 Phase 1 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type-R on-grade inlet at DP 3. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1 & A2.

Sub-basin A4 ($Q_5=3.7$ cfs, $Q_{100}=7.4$ cfs) consists of approximately 1.51 acres and is the southern portion of Alzada Drive and this basin is primarily single-family residential(Copper Chase at Sterling Ranch) and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 10' Type-R on-grade inlet at DP 4. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A3.

Sub-basin A5 ($Q_5=4.1$ cfs, $Q_{100}=8.3$ cfs) consists of approximately 1.70 acres and is the western portion of Bynum Drive. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 5. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A4.

Sub-basin A6A ($Q_5=2.2$ cfs, $Q_{100}=4.1$ cfs) consists of approximately 0.53 acres. This basin will serve as a tract including mail kiosks, parking, landscaping and sidewalks. Runoff from this sub-basin will sheet flow to DP 6A where it flows via curb and gutter to the 15' Type R inlet at DP6. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A5.

Sub-basin A6 ($Q_5=3.3$ cfs, $Q_{100}=6.6$ cfs) consists of approximately 1.37 acres and is the eastern portion of Bynum Drive. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R inlet on-grade inlet at DP 6. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A6A.

Sub-basin A7 ($Q_5=27.5$ cfs, $Q_{100}=60.6$ cfs) represents the future Copper Chase at Sterling Ranch development and consists of approximately 19.00 acres. This basin is primarily single-family residential and open space. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 36" RCP storm sewer stub at DP 7 with sediment control structure. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A6. Prior to being developed, storm runoff from this sub-basin will overland flow to temporary swales, where the flows will be captured by an interim 36" FES and piped to Pond W5.

Sub-basin A8 ($Q_5=3.0$ cfs, $Q_{100}=6.3$ cfs) consists of approximately 1.48 acres and is the south western portion of Sterling Ranch Road. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 8. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A7.

Sub-basin A9 ($Q_5=1.9$ cfs, $Q_{100}=3.7$ cfs) consists of approximately 0.61 acres and is the south eastern portion of Sterling Ranch Road. This basin is comprised primarily of the proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 9. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A8.

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Sub-basin A10 ($Q_5=9.2$ cfs, $Q_{100}=17.3$ cfs) consists of approximately 2.61 acres and is the south eastern portion of Marksheffel Road. This basin is comprised primarily of the proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 10. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A9.

Sub-basin A11 ($Q_5=9.5$ cfs, $Q_{100}=18.1$ cfs) consists of approximately 2.89 acres and is the north portion of Marksheffel Road. This basin is comprised primarily of the proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 11. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A10.

Sub-basin A12 ($Q_5=1.9$ cfs, $Q_{100}=9.5$ cfs) consists of approximately 3.87 acres and represents the open space area between the Sterling Ranch Filing No. 2 Phases 1 & 2 developments. This basin is primarily open space. This basin also contains a 50' and 30' gas easement that contain 3 major gas lines. Runoff from this sub-basin will be conveyed via sheet flow and earthen swale to an area inlet at DP 12. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A11.

Sub-basin A13 ($Q_5=15.7$ cfs, $Q_{100}=34.6$ cfs) consists of approximately 9.65 acres and is the northern portion of the future Sterling Ranch Phase 2 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be captured by a storm sewer stub at DP 13. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A12. Prior to being developed, storm runoff from this sub-basin will overland flow to temporary swales, where the flows will be captured by an interim 36" FES and piped to Pond W5.

Sub-basin A14 ($Q_5=16.0$ cfs, $Q_{100}=37.9$ cfs) consists of approximately 11.76 acres and is the proposed future school site on the northern side of Sterling Ranch Road. Runoff from this sub-basin will be routed to a 36" RCP storm sewer stub at DP 14. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A13. Prior to being developed, storm runoff from this sub-basin will overland flow to temporary swales, where the flows will be captured by an interim 36" FES and piped to Pond W5.

Sub-basin A15 ($Q_5=5.4$ cfs, $Q_{100}=11.7$ cfs) consists of approximately 2.91 acres and is the north eastern portion of Sterling Ranch Road. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 15. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A14.

Sub-basin A16 ($Q_5=4.4$ cfs, $Q_{100}=9.6$ cfs) consists of approximately 2.34 acres and is the south eastern portion of Sterling Ranch Road. This basin is primarily single-family residential and proposed roadway. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 16. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A15.

Sub-basin A17 ($Q_5=1.4$ cfs, $Q_{100}=4.7$ cfs) consists of approximately 1.76 acres and is the open space located along the western portion of the sterling Ranch Phase 2 development south of Sterling Ranch Road. This basin is primarily single-family open space with a small amount of lot runoff. Runoff from this sub-basin will be captured by a future Type C inlet at DP 17 and conveyed via sheet flow

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and a drainage swale. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A16.

Sub-basin A18 ($Q_5=4.3$ cfs, $Q_{100}=14.0$ cfs) consists of approximately 5.27 acres and is anticipated to be a commercial site and open space located at the corner of Sterling Ranch Road and Marksheffel Road. This basin is primarily open space and a future commercial lot. Runoff from this sub-basin will sheetflow to a 24" RCP storm sewer stub located at DP 18. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A17.

Sub-basin A19 ($Q_5=38.8$ cfs, $Q_{100}=85.4$ cfs) consists of approximately 31.85 acres and is the southern portion of the future Sterling Ranch Phase 2 development. This basin is primarily single-family residential and minor open space. Runoff from this sub-basin will be routed to a 42" storm sewer stub at DP 19 via curb and gutter and storm sewer. From here, the flow is piped to Pond W5 along with the flows from Sub-basin A1-A18. Prior to being developed, stormwater runoff from this sub-basin will overland flow directly into Pond W5.

Sub-basin A20 ($Q_5=6.6$ cfs, $Q_{100}=12.2$ cfs) consists of approximately 1.83 acres and is the south western portion of Marksheffel Road. This basin is primarily proposed roadway and landscaping. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a future 15' Type R on-grade inlet at DP 20. From here, the flow is piped directly to Pond W5 along with the flows from Sub-basin A21.

Sub-basin A21 ($Q_5=6.8$ cfs, $Q_{100}=12.6$ cfs) consists of approximately 1.93 acres and is the south eastern portion of Marksheffel Road. This basin is primarily proposed roadway and landscaping. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a future 15' Type R on-grade inlet at DP 21. From here, the flow is piped directly to Pond W5 along with the flows from Sub-basin A20.

Sub-basin A22 ($Q_5=2.7$ cfs, $Q_{100}=15.4$ cfs) consists of approximately 8.68 acres and represents Pond W5. This basin is primarily singlefamily residential and open space. Runoff from this sub-basin will sheet flow directly into Pond W5 and be conveyed to DP 22. From here, the flow will combine with the runoff from Basin A. An outlet structure will release the treated flows directly into the Sand Creek Drainageway.

Basin B consists of Sub-Basins B1-B5 combining for a total of 13.77 acres. This basin represents Vollmer Road and Pond W4. This basin is primarily proposed roadway. Stormwater runoff is conveyed via Vollmer Road where it is captured via a series of on-grade and sump inlets. Runoff is then piped to a proposed roadside swale where it will ultimately outfall into the onsite Pond W4. From the detention pond, the treated flows are then released into a storm sewer system that conveys them directly into the Sand Creek Drainageway at below historic rates along with the treated flows from Pond W5.

Sub-basin B1 ($Q_5=8.8$ cfs, $Q_{100}=15.8$ cfs) consists of approximately 2.98 acres and is the north eastern portion of Vollmer Road located north of Lochwinnoch Lane. This basin is primarily proposed roadway and landscaping. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter to a 15' Type R on-grade inlet at DP 23. From here, the flow is piped to a proposed roadside swale. This swale will convey the runoff from Sub-basin B1 to Pond W4.

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Sub-basin B2 ($Q_5=11.5$ cfs, $Q_{100}=20.6$ cfs) consists of approximately 3.89 acres and is the north western portion of Vollmer Road north of Lochwinnoch Lane. This basin is primarily proposed roadway and landscaping. Runoff from this sub-basin will be conveyed via curb and gutter and sheet flow then captured by a 15' Typr R on-grade inlet at DP 24. From here, the flow is piped to a proposed roadside swale. This swale will convey the runoff from Sub-basin B1 and Sub-basin B2 to Pond W4.

Sub-basin B3 ($Q_5=7.8$ cfs, $Q_{100}=14.0$ cfs) consists of approximately 2.05 acres and is the south eastern portion of Vollmer Road located north of Marksheffel Road and south of Lochwinnoch Lane. This basin is primarily proposed of roadway and landscaping. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter then captured by a 15' Type R sump inlet at DP 27. From here, the flow is piped directly to Pond W4.

Sub-basin B4 ($Q_5=7.4$ cfs, $Q_{100}=13.2$ cfs) consists of approximately 1.94 acres and is the western portion of Vollmer Road located north of Marksheffel Road and south of Lochwinnoch Lane. This basin is primarily proposed roadway and landscaping. Runoff from this sub-basin will be conveyed via sheet flow and curb and gutter then captured by a 15' Type R sump inlet at DP 28. From here, the flow is piped directly to Pond W4.

Sub-basin B5 ($Q_5=0.9$ cfs, $Q_{100}=6.4$ cfs) consists of approximately 2.91 acres and represents Pond W4. This basin is primarily open space. Runoff from this sub-basin will sheet flow directly into Pond W4 and be conveyed to DP 30. From here, the flow will combine with the runoff from Basin B, and Basins OS20 & OS21. An outlet structure will release the treated flows directly into the Sand Creek Drainageway via 1070 linear foot of 66" RCP and 1610 linear foot of 72" RCP running southeast along the west side of Marksheffel road along with treated flows from Pond W5.

Basin C consists of Sub-Basins C1-C2 combining for a total of 13.07 acres. This basin represents the future commercial sites located along Marksheffel Road. This basin is primarily proposed roadway and future commercial developments. Stormwater runoff is conveyed via a drainage swale to a 66" RCP where it combines with treated flows from Pond W5 and is released into Sand Creek.

Sub-basin C1 ($Q_5=2.0$ cfs, $Q_{100}=15.0$ cfs) consists of approximately 8.01 acres and is the commercial lot located at the corner of Vollmer Road and Marksheffel Road. Runoff from this sub-basin will ultimately be captured by a future onsite full-spectrum pond, where it will release to a storm sewer stub located at DP 31. From here, the flow is piped directly to the Sand Creek Drainageway along with treated flows from Pond W5 and Pond W4. In the interim condition, flows will enter an earthen swale at DP 31 and will be routed through Sub-basin C2 to DP 32.

Sub-basin C2 ($Q_5=1.4$ cfs, $Q_{100}=10.0$ cfs) consists of approximately 5.06 acres located in the southwest corner of the development and has the already developed Sanitary Sewer Lift Station for Sterling Ranch as well as additional land to be developed as commercial in the future. A stub into the stormwater system has been provided to collect the flows from this site. The future commercial areas will be required to provide full-spectrum detention ponds but can use the storm sewer stub provided in this report. From here, the flow is piped directly to the Sand Creek Drainageway along with treated flows from Pond W4 and Pond W5. In the interim condition, flows generated within this basin combine with the flows from sub-basin C1 in an earthen swale where they will enter a 72" RCP where the flow is piped directly to the Sand Creek Drainageway along with treated flows from Pond W4 and Pond W5.

**Final Drainage Report
Sterling Ranch Filing No. 2**

Basin OS consists of Sub-Basins OS2-OS4, OS20, OS21A, and OS21B combining for a total of 387.75 acres. This basin represents the offsite flows that have been incorporated in the storm sewer and pond design. Sub-basins OS20, OS21A, and OS21B represent the low density residential land located to the west of the site along Vollmer Road. Sub-basins OS2 and OS3 represent the Barbarick Subdivision directly north of the site. Sub-basin OS4 represents the existing residential lots located just east of the Pond W5 location. Flows from these sub-basins enter the site or are captured directly by one of the proposed detention ponds. Each sub-basin is discussed in more detail below.

Sub-basin OS20 ($Q_5=33.7$ cfs, $Q_{100}=310$ cfs from MDDP) consists of approximately 308.0 acres and represents the offsite basin to the northwest of the site. This basin is comprised of partially developed low density residential. Runoff from this basin overland flows to a roadside swale along Vollmer Road. Flows in the swale will be routed through an existing 3.5' x 5.5' HECMP at DP 25 where it will outfall into Pond W4. A riprap apron will be constructed to dissipate energy and prevent local scour at the outlet. Offsite Basins OS20, OS21B and OS21A correspond to Basins SC3-8 ($Q_5=42.1$ cfs, $Q_{100}=166.2$ cfs) and SC3-9($Q_5=71.5$ cfs, $Q_{100}=254.0$ cfs) from the MDDP.

Sub-basin OS21A ($Q_5=4.2$ cfs, $Q_{100}=21.9$ cfs) consists of approximately 20.26 acres and represents the offsite basin to the west of the site. This basin is comprised of partially developed low density residential. Runoff from this basin overland flows to a roadside swale along Vollmer Road at DP 26. Flows in the swale will outfall directly into Pond W4. A riprap apron will be constructed to dissipate energy and prevent local scour at the outlet. Offsite Basins OS20, OS21B and OS21A correspond to Basins SC3-8 ($Q_5=42.1$ cfs, $Q_{100}=166.2$ cfs) and SC3-9($Q_5=71.5$ cfs, $Q_{100}=254.0$ cfs) from the MDDP.

Sub-basin OS21B ($Q_5=3.1$ cfs, $Q_{100}=16.3$ cfs) consists of approximately 8.71 acres and represents the offsite basin to the west of the site. This basin is comprised of partially developed low density residential. Runoff from this basin will overland flow to a propose Type D inlet at DP 29. Flows will then outfall directly into Pond W4 and will utilize a forebay to dissipate energy. From here, the flows will be treated and outfall into the Sand Creek Drainageway. Offsite Basins OS20, OS21B and OS21A correspond to Basins SC3-8 ($Q_5=42.1$ cfs, $Q_{100}=166.2$ cfs) and SC3-9($Q_5=71.5$ cfs, $Q_{100}=254.0$ cfs) from the MDDP.

Sub-basin OS2 ($Q_5=13.8$ cfs, $Q_{100}=39.1$ cfs) consists of approximately 17.0 acres and represents the western portion of the Barbarick Subdivision. Developed flows from this basin will be captured by an onsite sand filter and released directly onto the Sterling Ranch Phase 2 Site. A drainage swale and storm sewer grated inlet are being proposed as a part of Sterling Ranch Filing No. 2 Phase 2 to receive the discharge from the Barbarick sand filter as well as the 2 24" RCPs that are bypassing offsite flows through the Barbarick property. Sterling Ranch has provided the pond Outfalls for the Barbarick Subdivision. The specific emergency overflow path will be designed and described in more detail within the Sterling Ranch Phase 2 Drainage Report. In general the overflow path will be to the south parallel to the existing gas line to Sterling Ranch Road. Sterling Ranch Road will carry the flows to Marksheffel to the west where the flow will then travel south until entering Sand Creek. 5-year and 100-year flows have been taken from the Approved Final Drainage Report for Barbarick Subdivision which can be found in Appendix D.

Sub-basin OS3 ($Q_5=0.30$ cfs, $Q_{100}=45.9$ cfs) consists of approximately 28.7 acres and represents the eastern portion of the Barbarick Subdivision. Developed flows from this basin are captured by an onsite EDB and released directly onto the Sterling Ranch Phase 2 site. A structure will be connected to the outfall pipe from the EDB and convey the pipe releases through the Sterling Ranch storm

**Final Drainage Report
Sterling Ranch Filing No. 2**

system conveying flows to Pond W5. Sterling Ranch has provided the pond Outfalls for the Barbarick Subdivision. At the time of final platting for Phase 2, Sterling Ranch will coordinate with the owners of Barbarick. The specific emergency overflow path will be designed and described in more detail within the Sterling Ranch Phase 2 Final Drainage Report. In general the overflow path will be to the south into Sterling Ranch Road along an earthen swale. Sterling Ranch Road will carry the flows to Marksheffel to the west where the flow will then travel south until entering Sand Creek. 5-year and 100-year flows have been taken from the Approved Final Drainage Report for Barbarick Subdivision which can be found in Appendix D. The 100 year emergency overflow is 84.4 cfs and will be conveyed via drainage swale along the Phase 2 north property line to the east, then south where it can be safely conveyed via storm sewer. The detailed emergency overflow calculations are provided in the Phase 2 drainage report.

Sub-basin OS4 ($Q_5=2.6$ cfs, $Q_{100}=8.8$ cfs) consists of approximately 5.08 acres and represents the existing residential lots to the east of the proposed Pond W5. Existing flows from this basin will overland flow directly onto the Sterling Ranch Filing No. 2 Site into Pond W5. From here, the treated flows will outfall into the Sand Creek Drainage way.

There will be bank stabilization improvements to the Sand Creek Drainage Channel with the development of the Sterling Ranch Filing No. 2 site to maintain the integrity of Pond W5. However, channel improvements for Sand Creek (checks, drops, etc.) will be installed in accordance with the analysis performed by Kiowa Engineering.

DRAINAGE DESIGN CRITERIA

Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the “*City of Colorado Spring/El Paso County Drainage Criteria Manual*” Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the “*Urban Storm Drainage Criteria Manual*” Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the “*Colorado Springs Drainage Criteria Manual (CCSDCM)*”, dated May 2014, as adopted by El Paso County.

Hydrologic Criteria

All hydrologic data was obtained from the “*El Paso Drainage Criteria Manual*” Volumes 1 and 2, and the “*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*” Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. One hour point rainfall data for the storm events is identified in the table below. Rational Method calculations were prepared, in accordance with Section 3.0 of the EPCDCM, for the sub-basins that directly impact the sizing of the proposed storm sewer outfalls. Rational method calculations are presented in Appendix B. Sub-basin OS20 was evaluated using the MDDP flows for the sizing of the pond and the rational method for a more conservative sizing of the storm pipe infrastructure.

Table 1: 1-hr Point Rainfall Data

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

Hydraulic Criteria

Mile High Flood District’s MHFD-Detention, Version 4.03 workbook was used for pond sizing. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. Pond sizing spreadsheets are presented in Appendix C. The Mile High Flood District’s spreadsheet UD_Inlet v4.05, released March 2017, was also utilized to determine street and inlet capacities of the development. Using Storm StormCAD V8i, a modeling program for stormwater drainage, the hydraulic grade lines and energy grade lines were determined for the storm sewer network. Manhole and pipe losses for the model were obtained from the *Modeling Hydraulic and Energy Gradients in Storm Sewers: A Comparison of Computation Methods*, by AMEC Earth & Environmental, Inc. The manhole loss coefficients used in the model can be seen in Table 2. StormCAD results along with street and inlet capacities are presented in Appendix B.

Table 2 - StormCAD Standard Method Conversions

StormCAD Conversion Table			
Bend Loss	Bend Angle	K coefficient Conversion	
	0	0.05	
	22.5	0.1	
	45	0.4	
	60	0.64	
	90	1.32	
Lateral Loss	1 Lateral K coefficient Conversion		
	Bend Angle	Non Surcharged	Surcharged
	45	0.27	0.47
	60	0.52	0.9
	90	1.02	1.77
	2 Laterals K coefficient Conversion		
	45	0.96	
	60	1.16	
90	1.52		

DRAINAGE FACILITY DESIGN

General Concept

The proposed stormwater conveyance system was designed to convey the developed Sterling Ranch Filing No. 2 runoff to the proposed full spectrum water quality and detention pond W5 via storm sewer. Pond W4 will be utilized to detain and treat large portions of offsite area. The proposed ponds were designed to release at less than historic rates to minimize adverse impacts downstream. Treated

**Final Drainage Report
Sterling Ranch Filing No. 2**

water will outfall directly into the Sand Creek Drainageway, where it will eventually outfall into Fountain Creek. All Ponds will be owned and maintained by Sterling Ranch Metro District. A proposed drainage map is presented in Appendix E showing locations of the pond and channel outfall locations.

To maintain the integrity of Pond W5, there will be bank stabilization improvements to the Sand Creek Drainage Channel with the development of the Sterling Ranch Filing No. 2 site. The pond release location will be protected with riprap. However, channel improvements for Sand Creek (checks, drops, etc.) will be installed in accordance with the construction plans performed by Matrix Design Group. JR Engineering is coordinating with Matrix Design Group. The flows discharged from Pond W5 will outfall into the reach of Sand Creek designed by Matrix. The discharge point from Sterling Ranch Filing No. 2 into Sand Creek is shown on the Matrix Design Plans in Appendix D. The rerouting of flows to ponds W4 and W5 outfall location should cause no negative impacts to downstream reaches of Sand Creek. Per the DBPS, Reach SC-9, the recommended improvements to the channel include selective rip rap linings, grade control check structures, and drop structure improvements that are anticipated to stabilize the channel to prevent further degradation, scour and meandering. Full Spectrum Detention in ponds W4 and W5 will reduce peak flows within the channel there-by adding to the integrity of the Sand Creek Channel.

Provide documentation from the City that these flows and outfall are acceptable.

Specific Details

Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume (WQCV), and consider the need for Industrial Commercial BMP's.

Step 1, Reducing Runoff Volumes: The development of the project site is a proposed single-family development with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes.

Step 2, Stabilize Drainageways: Sterling Ranch Filing No. 2 utilizes storm sewer throughout the project site. This storm sewer directs the on-site development flows to the full spectrum detention Pond W5 that releases at or below historic rates into the Sand Creek Drainageway. Measures shall be implemented to prevent any negative impacts to the drainageway. Riprap at the outfall locations will be utilized to prevent any erosion. An emergency overflow spillway rundown has been designed from Pond W5 down into the Sand Creek Drainageway. The overflow channel will help protect and stabilize the drainageway by reducing channel degradation and erosion. The channel utilizes 4 foot deep "VH Soil Riprap" base with a minimum 4 inch overlay of topsoil, seed and mulch. A detailed analysis of the Sand Creek Drainageway is currently being conducted by Matrix Design Group. This report will cover stabilization measures and channel improvements needed for this reach of the Sand Creek Drainageway. The portions of Sand Creek to the south of the historic confluence point are to be stabilized per the Sand Creek Stabilization at Aspen Meadows Subdivision Filing No. 1 plans by Matrix Design Group, April 2020.

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Step 3, Treat the WQCV: Water Quality treatment is provided in two proposed full spectrum water quality detention ponds: Pond W4 and Pond W5. Pond W5 will receive all runoff generated within Sterling Ranch Filing No. 2 as well as future Sterling Ranch Phase 2 and Copper Chase at Sterling Ranch, a school site and a small portion of offsite areas. Pond W4 will receive runoff generated from portions of Vollmer Road and a large portion of offsite areas to the north and west of Vollmer road. In general, the runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structures have been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the ponds will be reduced to less than historic rates into the Sand Creek Drainageway. These ponds will facilitate pollutant removal for the site, while also reducing peak stormwater rates into the Sand Creek Drainageway.

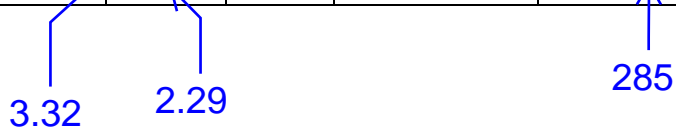
Step 4, Consider the need for Industrial and Commercial BMP's: future commercial sites are proposed within this development. Site specific storm water quality and erosion control plans will be required for each commercial tract prior to development. A site specific storm water quality and erosion control plan and narrative have also been prepared in conjunction with this final drainage report. Site specific temporary source control BMPs as well as permanent BMP's will be detailed in this plan and narrative to protect receiving waters.

Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention are provided for all developed basins. For this site, two detention ponds have been proposed. The WQCV for each pond shall be released within 40 hours and the EURV shall be released within 72 hours. The table below provides the volumes required for each pond, along with their respective release rates for the 5-year and 100-year storm. Both ponds will utilize forebays, trickle channels, and outlet structures to dissipate energy and treat flows. The outlet structure for these ponds shall reduce the release rates for all storm events to less than historic rates to minimize adverse impacts to downstream stormwater facilities. A broad crested weir is provided as an emergency spillway for each pond. The emergency spillway provided for Pond W5 will convey flows directly into the Sand Creek Drainageway. The emergency spillway provided for Pond W4 shall convey flows to the existing roadside swale along Vollmer Road. Both spillways will utilize riprap aprons to prevent scour at the outlets. Pond and outlet structure calculations and sizing can be found in Appendix C. The detention ponds will be private and shall be maintained by the Sterling Ranch Metropolitan District. Access shall be granted to the owner and El Paso County for access and maintenance of the private detention pond. Pond W5 corresponds to pond FSD6 from the MMDP ($Q_5=7.6$ cfs, $Q_{100}=149.7$ cfs) and is releasing less than the MDDP values in the proposed design.

Table 3. Pond Volumes & Release Rates

	REQUIRED VOLUME (AC-FT)	VOLUME PROVIDED (AC-FT)	WQCV (AC-FT)	EURV (AC-FT)	5-YEAR RELEASE (CFS)	100-YEAR RELEASE (CFS)
POND W5	18.376	18.441	3.311	11.843	3.40	139.3
INTERIM POND W4	12.211	7.64	2.281	3.710	20.7	281.3



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Per the MDDP, Pond W4 is sized to maximize the area on the site & could be potentially enlarged in the future if more land is purchased. A preliminary design for the ultimate configuration of Pond W4 has been used to calculate potential volume. Upon future development, an expansion of Pond W4 will need to be finalized. The pond is designed to treat approximately 352.2 acres and provide approximately 2.281 ac-ft of water quality storage. Modifications will be required to ensure the outlet structure complies with local and El Paso County criteria. A preliminary pond sizing for the ultimate condition can be found in the appendix. Pond W4 corresponds to pond FSD9 from the MMDP ($Q_5=24.9$ cfs, $Q_{100}=290$ cfs) and is releasing less than the MDDP values in the proposed design. The emergency overflow path will be through Marksheffel and a section can be found within Appendix B demonstrating the ability to pass 319.2 cfs.

Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted with each Final Drainage Report. The Erosion Control Plan for Sterling Ranch Filing No. 2 has been submitted with this report.

Operation & Maintenance

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within the any platted County ROW will be owned and maintained by El Paso County. All proposed drainage structures within the property or tracts will be owned and maintained by the Sterling Ranch Metro District. Vegetation in the natural and improved portions of Sand Creek Drainageway is the responsibility of Sterling Ranch Metro District. This includes all mowing, seeding and weed control activities. An Inspection & Maintenance Plan has been submitted concurrently with this final drainage report that details the required maintenance activities and intervals to ensure proper function of all stormwater infrastructures in the future. The full spectrum detention ponds will be owned & maintained by Sterling Ranch Metro District.

Sand Creek Drainageway Improvements

Per the Sand Creek DBPS, Sand Creek and connected tributaries in the area of the site will require improvements. The east tributary reaches within the site boundary (DBPS SEG: 169, 186, 164, 159) will not require improvements because they will no longer be present, as development in the areas will eliminate them, and replace them with, a storm sewer system to discharge into Sand Creek. Sand Creek itself will continue to be routed through the development. Per the DBPS, selective rip rap linings, grade control check structures, and drop structure improvements are required to stabilize the channel to prevent further degradation, scour and meandering. Full spectrum detention will also be used on its benefits to the integrity of the Sand Creek Drainageway. A separate analysis with detailed alternative sections, HEC-RAS analyses, and proposed improvements is currently being conducted by Kiowa Engineering. This analysis will outline the channel improvements that will be necessary for the section of Sand Creek Drainageway that is adjacent to the site.

Per the DBPS, the recommended improvements to reach SC-9 are selective rip rap linings, grade control check structures, and drop structure improvements. The peak flows to the channel are reduced due to the Full Spectrum Detention adding to the integrity of the channel. The portions of

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Sand Creek to the south of the historic confluence point are to be stabilized per the Sand Creek Stabilization at Aspen Meadows Subdivision Filing No. 1 plans by Matrix Design Group, April 2020. These plans propose improvements to Sand Creek from where Pond W5 outfalls all the way past the historic confluence. The Matrix Plans propose channel stabilization, stable slopes, drop structures, and cross vanes to ensure the quality of Sand Creek. The latest set of plans have been included within Appendix D for reference.

Drainage & Bridge Fees

The site lies within the Sand Creek Drainage Basin. An approximate estimate is presented below, exact fees to be determined at time of final plat. See full Drainage and Bridge fee worksheet in Appendix D for the fee calculation spreadsheet.

2020 DRAINAGE AND BRIDGE FEES – Sterling Ranch Filing No. 2				
Impervious Acres (ac)	Drainage Fee (Per Imp. Acre)	Bridge Fee (Per Imp. Acre)	Sterling Ranch Drainage Fee	Sterling Ranch Bridge Fee
33.905	\$20,387	\$8,339	\$691,246.82	\$282,738.30

Construction Cost Opinion

The City of Colorado Springs Drainage Criteria Manual specifies a Cost Estimate of proposed drainage facility improvements be submitted with the Final Drainage Report. A construction cost opinion has been provided below. The below cost opinion is only an estimate of facility and drainage infrastructure cost and may vary. Swapping of DBPS improvements for proposed improvements is being proposed for this project. A map demonstrating the DBPS improvements costs are being swapped for can be found in Appendix D.

Item	Description	Quantity	Unit Cost	Cost
1	18"RCP	731	\$65 /LF	\$ 47,515.00
2	24" RCP	464	\$78 /LF	\$ 36,192.00
3	30" RCP	492	\$97 /LF	\$ 47,724.00
4	36" RCP	651	\$120 /LF	\$ 78,120.00
5	42" RCP	598	\$160 /LF	\$ 95,680.00
6	48" RCP	1266	\$195 /LF	\$ 246,870.00
7	66" RCP	1915	\$332 /LF	\$ 635,780.00
8	72" RCP	2738	\$380 /LF	\$ 1,040,440.00
9	84" RCP	329	\$520 /LF	\$ 171,080.00
10	18" FES	1	\$390 /LF	\$ 390.00
11	24" FES	1	\$468 /EA	\$ 468.00
12	30" FES	2	\$582 /EA	\$ 1,164.00
13	36" FES	2	\$720 /EA	\$ 1,440.00
14	42" FES	2	\$960 /EA	\$ 1,920.00
15	66" FES (Temp.)	1	\$1992 /EA	\$ 1,992.00

**Final Drainage Report
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16	84" Headwall	2	\$10000 /EA	\$	20,000.00
17	15' CDOT Type R At-Grade	6	\$10633 /EA	\$	63,798.00
18	10' CDOT Type R At-Grade	10	\$7861 /EA	\$	78,610.00
19	2.9'x5.5' CDOT TYPE D	1	\$5731 /EA	\$	5,731.00
20	Storm Sewer MH, box base < 15 feet	24	\$11627 /EA	\$	279,048.00
21	Storm Sewer MH,slab base ~ 15 feet-20 feet	2	\$6395 /EA	\$	12,790.00
22	Storm Sewer MH, box base > 20 feet	1	\$20000 /EA	\$	20,000.00
23	*Detention Pond W5	1	\$75000 /EA	\$	75,000.00
24	*Detention Pond W4	1	\$65000 /EA	\$	65,000.00
25	Forebay Structure	1	\$15000 /EA	\$	15,000.00
26	Mod CDOT Outlet Structure	2	\$15000 /EA	\$	30,000.00
Total				\$	3,071,752.00

SUMMARY

Development of this site will not adversely affect the surrounding development per this final drainage report and will have no negative impact of the neighboring developments. Assumptions were made for the offsite future developments that utilize the drainage infrastructure within this report. As the future sites develop, final drainage reports will be completed to confirm the assumptions made in this report. The proposed drainage facilities will adequately convey, detain and route runoff from the tributary and onsite flows to the Sand Creek Drainage channel. Full spectrum detention and water quality ponds W4 and W5 will be used to discharge developed flows into Sand Creek per the Urban Drainage criteria flow rates, which are at or less than the historic flow. Care will be taken during construction to accommodate overland flow routes onsite and temporary drainage conditions. The development of the Sterling Filing No. 2 project shall not adversely affect adjacent or downstream property.

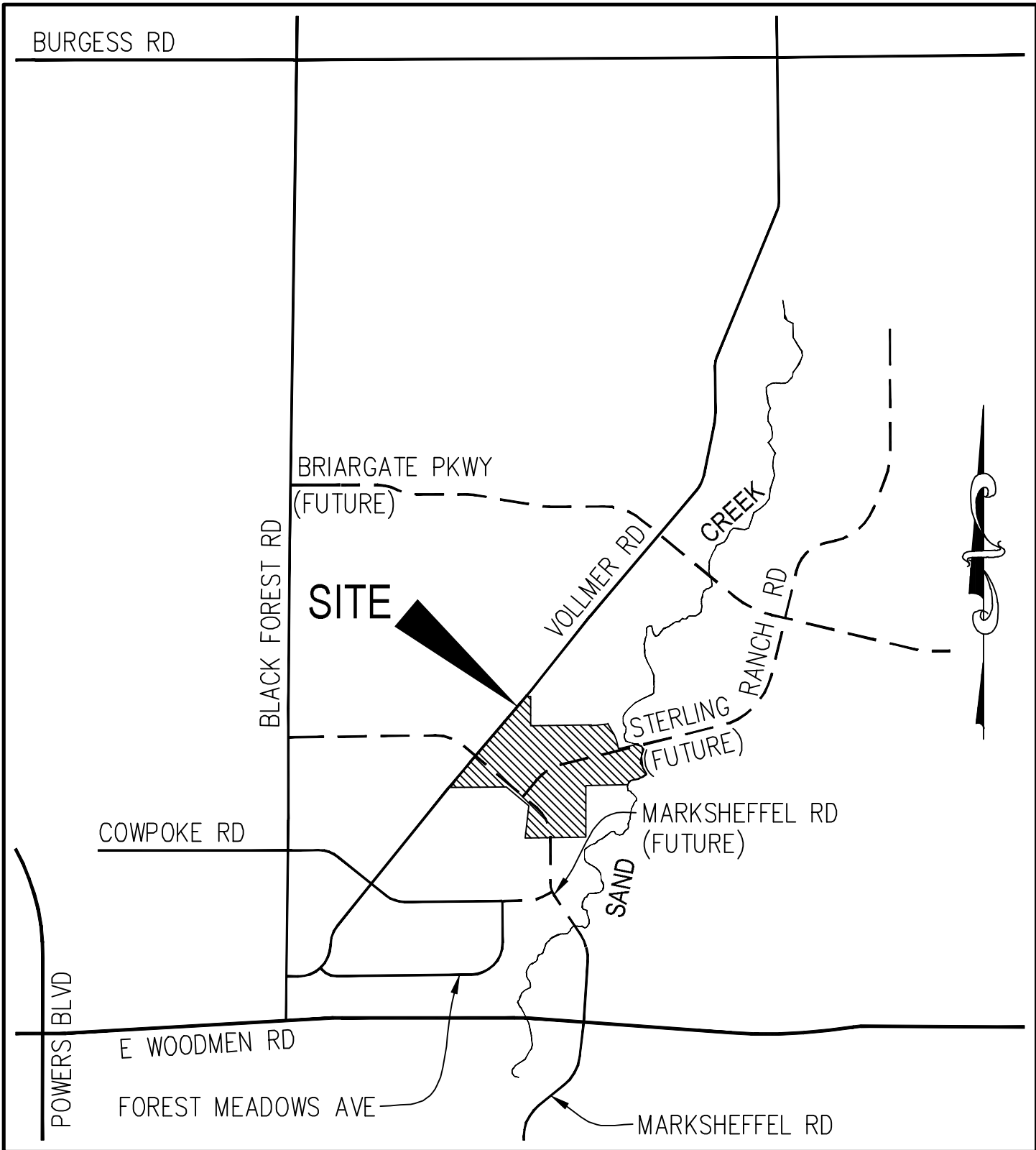
REFERENCES:

1. City of Colorado Springs Drainage Criteria Manual, Volume 1 & 2, Colorado Springs, CO, 2014.
2. El Paso County Drainage Criteria Manual Volume 1, El Paso County, CO, 1990.
3. El Paso County Drainage Criteria Manual Update (City Chapter 6), El Paso County, CO, 2015.

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Sterling Ranch Filing No. 2**

4. El Paso County Engineering Criteria Manual Revision 6, El Paso County, CO, 2016.
5. Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3 & 4, by Matrix Design Group, dated June 2016.
6. Final Drainage Report for Sterling Ranch Filing No. 2, by M&S Civil Consultants, dated March 2018.
7. Master Development Drainage Plan For Sterling Ranch, by M&S Civil Consultants, Inc., dated October 2018.
8. Sand Creek Drainage Basin Planning Study, Kiowa Engineering, January 1993.
9. Urban Storm Drainage Criteria Manual, Urban Drainage and Flood Control District, Latest Revision.

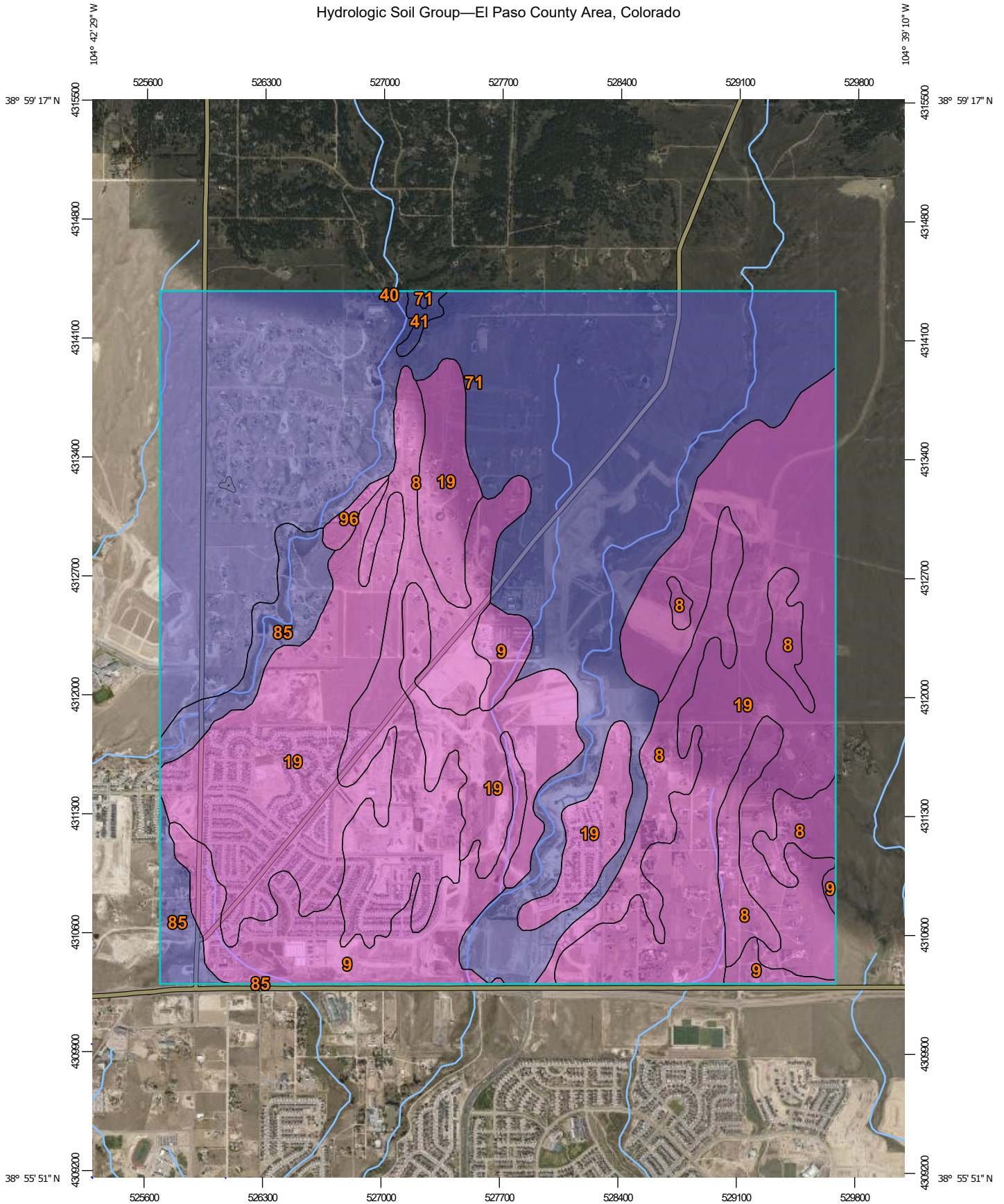
APPENDIX A
FIGURES AND EXHIBITS



VICINITY MAP

N.T.S.

Hydrologic Soil Group—El Paso County Area, Colorado



Map Scale: 1:30,900 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84




Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

8/31/2020
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—May 26, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	601.8	14.9%
9	Blakeland-Fluvaquentic Haplaquolls	A	267.7	6.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	1,430.7	35.4%
40	Kettle gravelly loamy sand, 3 to 8 percent slopes	B	0.5	0.0%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	B	11.1	0.3%
71	Pring coarse sandy loam, 3 to 8 percent slopes	B	1,577.2	39.1%
85	Stapleton-Bernal sandy loams, 3 to 20 percent slopes	B	136.3	3.4%
96	Truckton sandy loam, 0 to 3 percent slopes	A	12.4	0.3%
Totals for Area of Interest			4,037.6	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

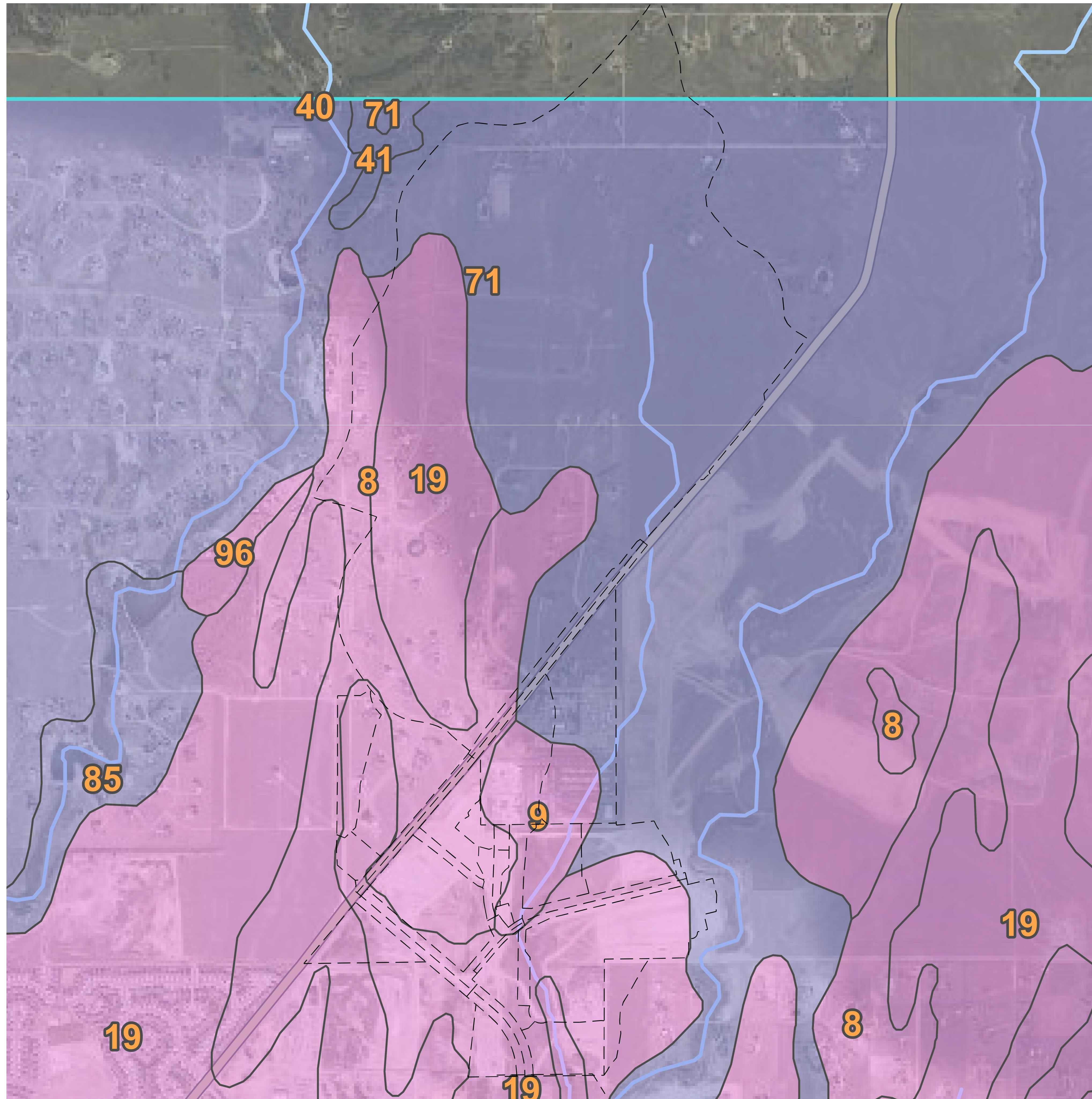
Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

STERLING RANCH FILING NO. 2



SOIL DELINEATION
STERLING RANCH FILING NO.2
JOB NO. 25188.01
9/1/20
SHEET 1 OF 1



Centennial 303-740-9393 • Colorado Springs 719-593-2593
Fort Collins 970-491-9888 • www.jrengineering.com

X:\25188\000_a\2518801 Drawings\Sheet Design\Drawings\Soil Delineation.dwg, 24:28 Title Landscape, 9/1/2020 2:21:22 PM, FC

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83. GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones across users in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
 NOAA, NNGS12
 National Geodetic Survey
 SSMC-3, #9222
 1315 East-West Highway
 Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (202) 773-3242 or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

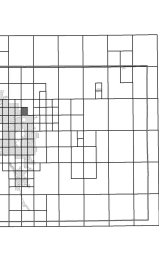
If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/inf>.

El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)

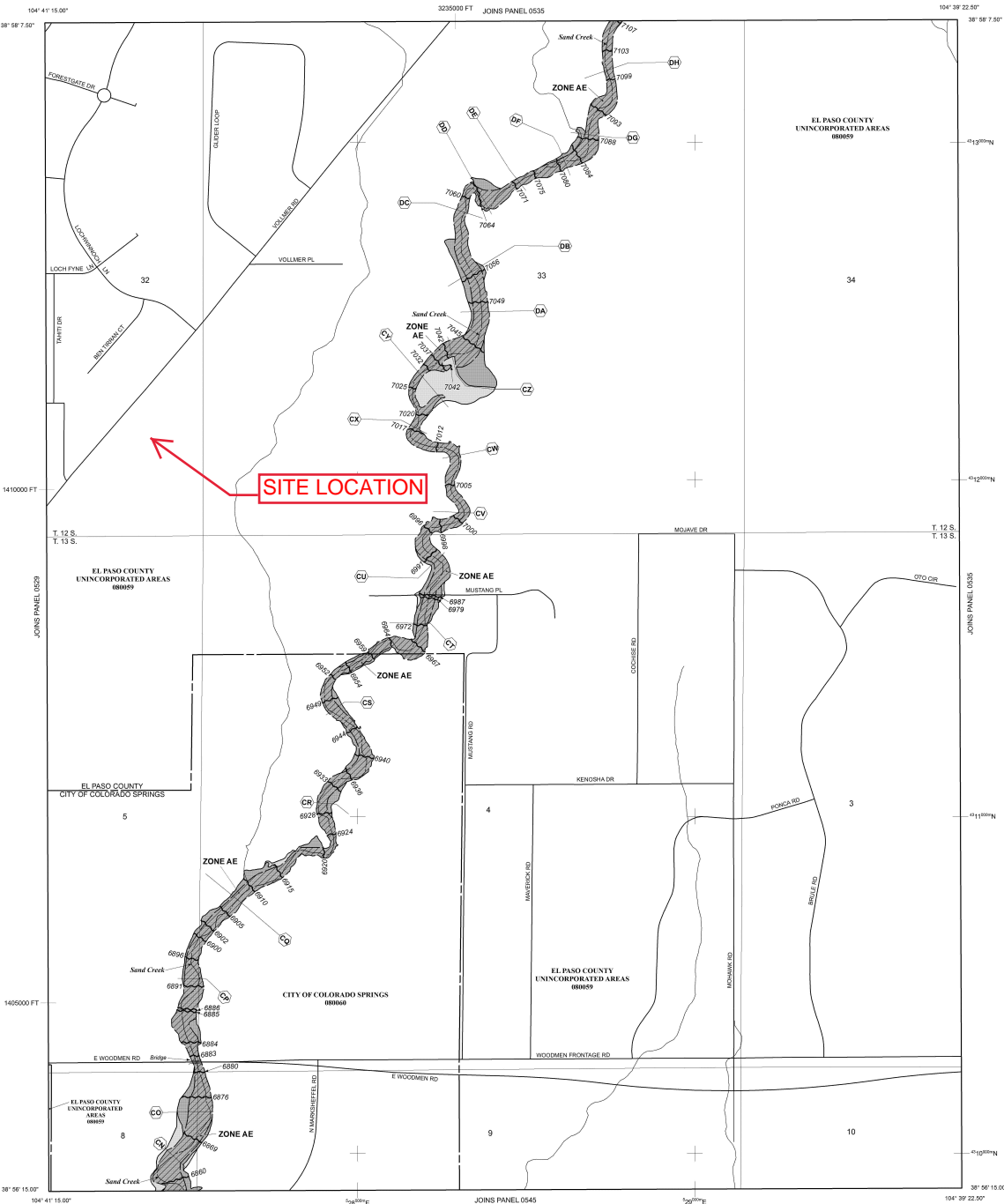
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM/STREAM VERTICAL DATUM CONVERSION INFORMATION.

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Plan (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



SITE LOCATION

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zone A, AE, AH, AO, AR, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was previously determined. Zone AR indicates that the former flood control system is being retained to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE
 The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increase in flood heights.

- OTHER FLOOD AREAS**
- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with velocities less than 1 square mile; and areas protected by levees from 1% annual chance flood.
- OTHER AREAS**
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER PROTECTED SYSTEM (CBRS) AREAS**
- OTHERWISE PROTECTED AREAS (OPA)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D Boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation line and value, elevation in feet (EL 587)
- Base Flood Elevation value where uniform within zone; elevation in feet

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

- Cross section line
- Transect line
- 97° 07' 30.00" 32° 22' 00.00" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 747° 12" 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 6000000 FT 5000-foot grid ticks; Colorado State Plane coordinate system; central zone (SPROJCOE2)
- Lambert Conformal Conic Projection
- DXS10 Bench mark (see explanation in Notes to Users section of this FIRM report)
- M1.5 River file

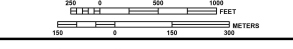
MAP REPOSITORIES
 Refer to Map Repository list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
 MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
 DECEMBER 7, 2018 To update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Change.

For community map revision history prior to courtswide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0533G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO
AND INCORPORATED AREAS

PANEL 533 OF 1300
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS CITY OF	08008	0033	0
EL PASO COUNTY	08008	0033	0

Notes to User: The Map Number shown below should be used when ordering map copies. The Community Number shown above should be used on insurance applications for the insured community.

MAP NUMBER
08041C0533G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency



REPLY TO
ATTENTION OF

DEPARTMENT OF THE ARMY
ALBUQUERQUE DISTRICT, CORPS OF ENGINEERS
200 SOUTH SANTA FE AVENUE, SUITE 301
PUEBLO, COLORADO 81003-4270

SIGNED

February 29, 2016

Regulatory Division

SUBJECT: Action No. SPA-2015-00428-SCO, Sterling Ranch Residential Development
Project, El Paso County, Colorado

Jim Morley
SR Land, LLC
20 Boulder Crescent Suite 201
Colorado Springs, CO 80903

Mr. Morley:

You are hereby authorized under Section 404 of the Clean Water Act to discharge dredged and fill material in to waters of the United States to conduct work in associated with construction of the Sterling Ranch Residential Development in accordance with Action Number SPA-2015-00428-SCO. A copy of the permit is enclosed.

To use this permit, you must ensure that the work is conducted in accordance with the terms and conditions of the permit. You must submit revised drawings to us for approval prior to construction should any changes be found necessary in either the location or plans for the work. Approval of revised plans may be granted if they are found not contrary to the public interest.

This permit is not an approval of the project design features, nor does it imply that the construction is adequate for its intended purpose. This permit does not authorize any injury to property or invasion of rights or a infringement of Federal, state or local laws or regulations. You must possess the authority, including property rights, to undertake the proposed work.

Enclosed is a compliance certification form. Upon completion of the project, please sign and date the form and return it to this office.

If you have any questions concerning our regulatory program, please contact me at 719-543-6915 or by e-mail at van.a.truan@usace.army.mil. At your convenience,

please complete a Customer Service Survey at
<http://per2.nwp.usace.army.mil/survey.html>.

Sincerely,



Van Truan
Chief, Southern Colorado
Regulatory Branch

Enclosure(s)



September 23, 2016

Mr. Virgil Sanchez
MS Civil Consultants, Inc.
20 Boulder Crescent, Suite 110
Colorado Springs, CO 80903

RE: Sand Creek Wetland Memo
Sterling Ranch Residential Development Project
El Paso County, Colorado

Dear Mr. Sanchez:

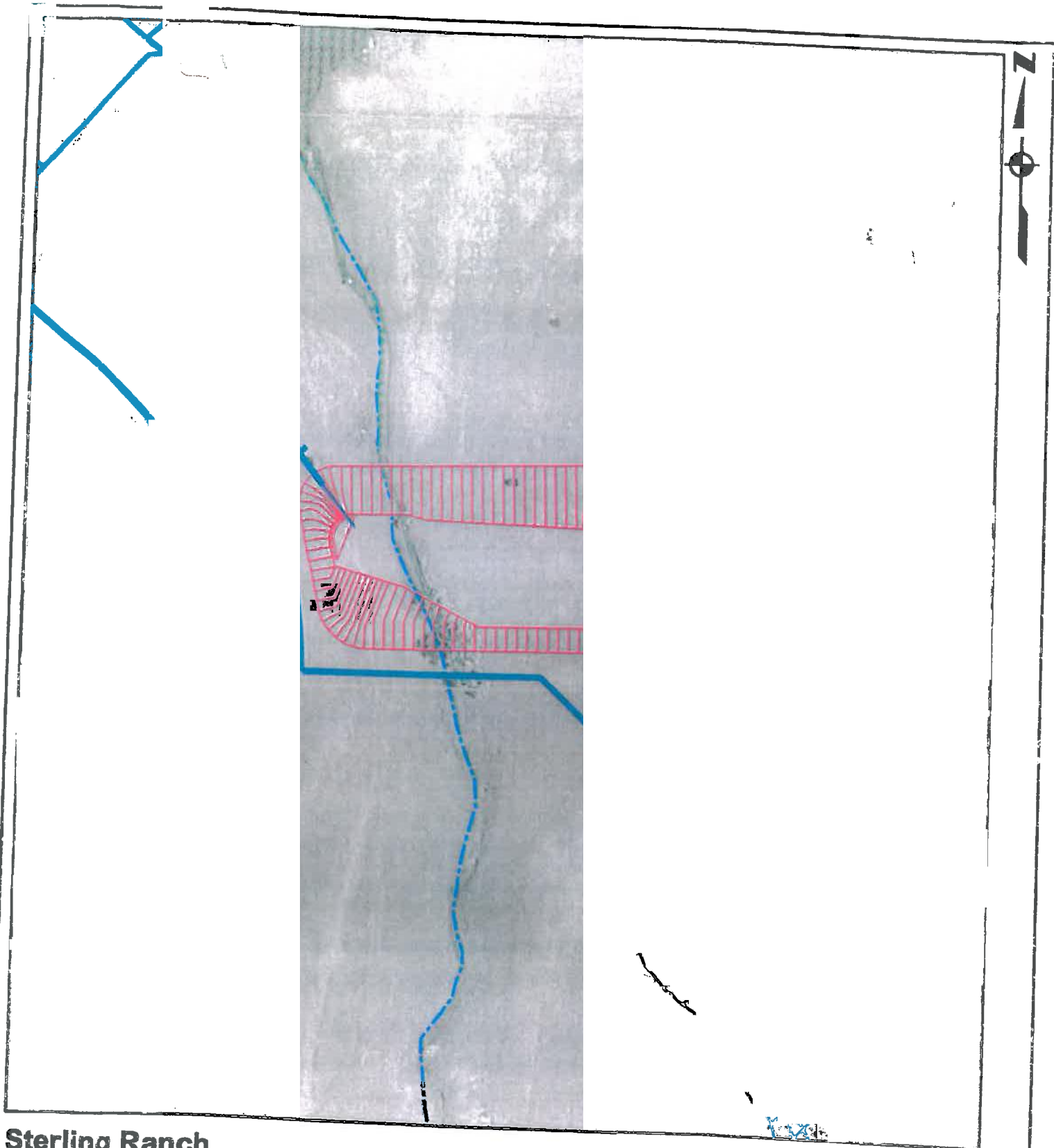
CORE Consultants, Inc. (CORE) was retained by MS Civil Consultants, Inc. to complete a wetland delineation for portions of the proposed Sterling Ranch Residential Development Project ("Project"). The Project is located on approximately 1,500 acres in unincorporated El Paso County (County), Colorado, and encompasses a portion of the perennial stream Sand Creek, its western tributaries, and adjacent uplands. CORE submitted a formal wetland delineation report to the U.S. Army Corps of Engineers (USACE) as a component of a Section 404 permit application for the Project (Permit Number SPA-2015-00428-SCO), which was approved by the USACE in February, 2016.

At the time of 404 permit issuance, CORE had performed wetland surveys in all areas of the Project covered by the permit. However, at the time of this writing, wetland surveys covering future phases of development have not been performed. Prior to development of future phases not covered under SPA-2015-00428-SCO, a formal wetland delineation will be performed in those areas and any necessary 404 permitting will be obtained. Based on CORE's findings throughout Sand Creek in the current permit area, CORE expects that wetlands may occur throughout the floodplain in portions of Sand Creek in future development areas further downstream (Attachment 1 - Wetland Location Map).

If you should have any questions, concerns, or require additional information, please feel free to contact our office directly at 303.703.4444.

Sincerely,
CORE Consultants, Inc.

Daniel Maynard
Senior Ecologist







Sterling Ranch
Wetland Location Map
 El Paso County, Colorado

0 250 500
 Feet
 1 inch = 250 feet

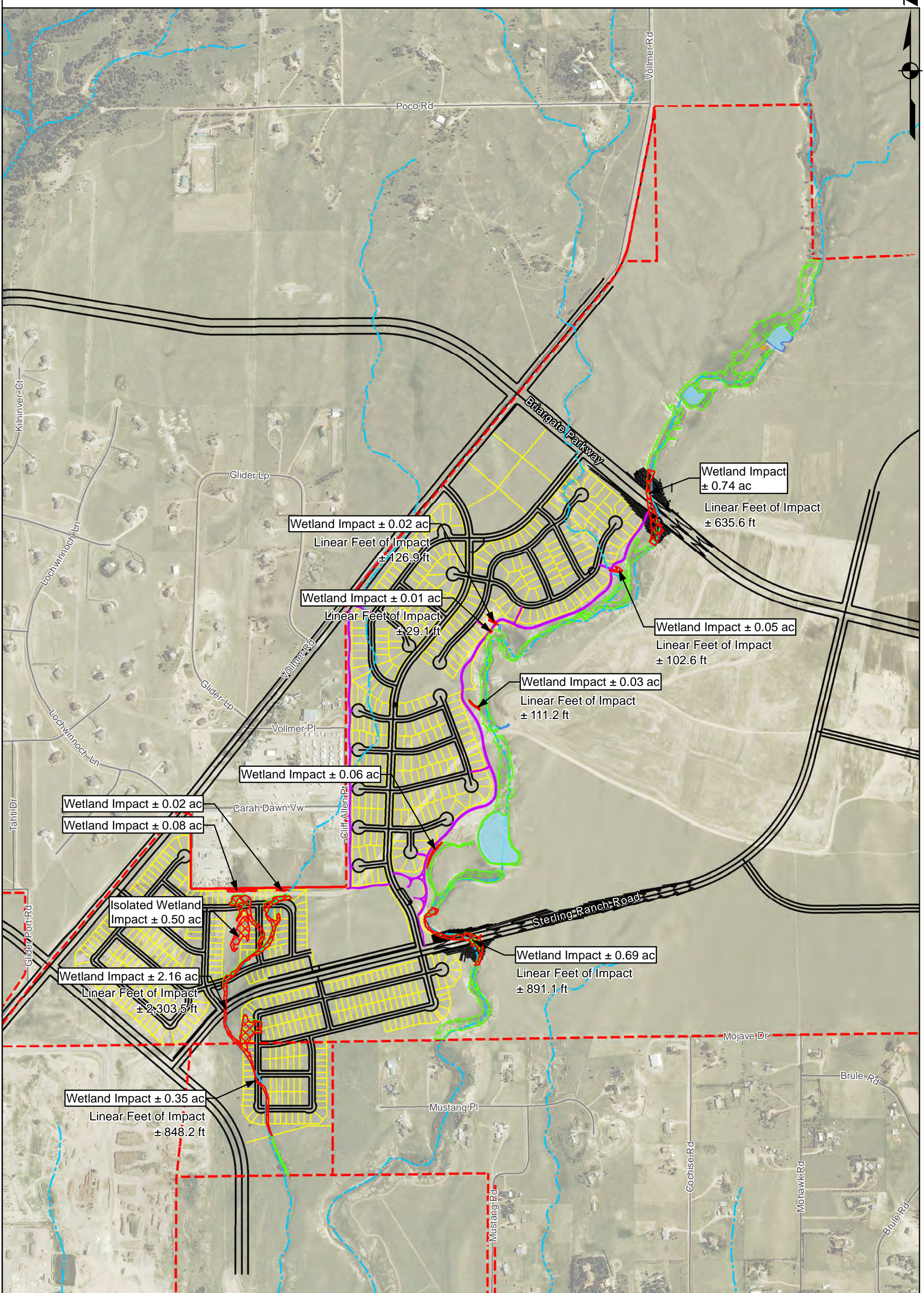
Date: 9/23/2016
 Project #: 15-001



CORE
CONSULTANTS

-  Proposed Storm Pipe
-  Proposed Detention Pond
-  Watercourse
-  100-year Floodplain

CIVIL ENGINEERING
 DEVELOPMENT CONSULTING
 NATURAL RESOURCES CONSULTING
 LAND SURVEYING
303.703.4444
 1850 W. Littleton Blvd., Ste. 105
 Littleton, CO 80120



Wetland Impact ± 0.74 ac
Linear Feet of Impact ± 635.6 ft

Wetland Impact ± 0.02 ac
Linear Feet of Impact ± 126.9 ft

Wetland Impact ± 0.01 ac
Linear Feet of Impact ± 29.1 ft

Wetland Impact ± 0.05 ac
Linear Feet of Impact ± 102.6 ft

Wetland Impact ± 0.03 ac
Linear Feet of Impact ± 111.2 ft

Wetland Impact ± 0.06 ac

Wetland Impact ± 0.02 ac

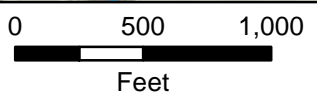
Wetland Impact ± 0.08 ac

Isolated Wetland Impact ± 0.50 ac

Wetland Impact ± 2.16 ac
Linear Feet of Impact $\pm 2,303.5$ ft

Wetland Impact ± 0.69 ac
Linear Feet of Impact ± 891.1 ft

Wetland Impact ± 0.35 ac
Linear Feet of Impact ± 848.2 ft



- Permanent Impact
- Pond
- Proposed Road
- Proposed Contour
- Existing Wetland
- Dry Wash
- Proposed Trail
- Parcel Boundary
- Existing Isolated Wetland
- NHD Watercourse
- Proposed Lot Lines

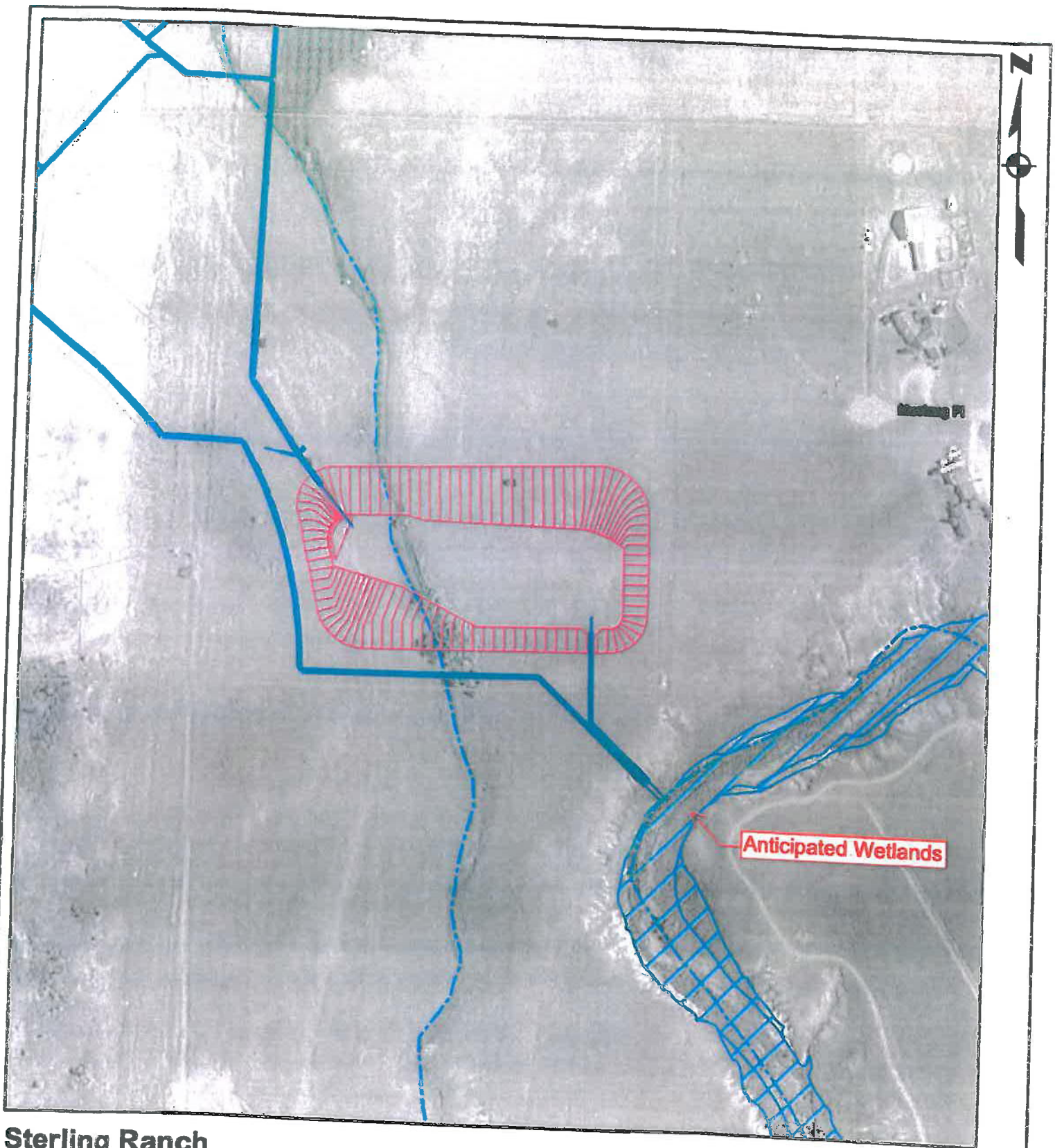


CIVIL ENGINEERING
DEVELOPMENT CONSULTING
LAND SURVEYING
303.703.4444
1950 W. Littleton Blvd., Ste. 109
Littleton, CO 80120

Sterling Ranch Wetland Impact Location Map

El Paso County, Colorado

Date: 10/13/2015
Project #: 15-001








Sterling Ranch
Wetland Location Map
 El Paso County, Colorado

0 250 500
 Feet
 1 inch = 250 feet

Date: 9/23/2016
 Project #: 15-001



CORE
 CONSULTANTS

-  Proposed Storm Pipe
-  Proposed Detention Pond
-  Wetland
-  NHD Watercourse
-  100-year Floodplain

CIVIL ENGINEERING
 DEVELOPMENT CONSULTING
 NATURAL RESOURCES CONSULTING
 LAND SURVEYING
303.703.4444
 1950 W. Littleton Blvd., Ste. 105
 Littleton, CO 80120

APPENDIX B

HYDROLOGIC/ HYDRAULIC CALCULATIONS

COMPOSITE % IMPERVIOUS & COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County

Project Name: Sterling Ranch Subdivision (Existing)
 Project No.: 25188.01
 Calculated By: CJD
 Checked By: _____
 Date: 5/15/20

Basin ID	Total Area (ac)	Streets (100% Impervious)				Residential (65% Impervious) Neighborhood Area (70% Impervious)				1 Acre lot Residential (20% Impervious) Light Commercial (80% Impervious)				Lawns (0% Impervious) School (55% Impervious)				Basins Total Weighted C Values		Basins Total Weighted % Imp.	
		C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀		
		EXA1	17.68	0.90	0.96	1.31	7.4%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	16.37	1.9%		0.15
EXA2	19.59	0.90	0.96	0.59	3.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	19.00	1.9%	0.11	0.38	5.0%	
EXA3	5.66	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	5.66	2.0%	0.09	0.36	2.0%	
EXA4	50.72	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	50.72	2.0%	0.09	0.36	2.0%	
EXB	11.78	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	11.78	2.0%	0.09	0.36	2.0%	
EXC1	12.36	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	12.36	2.0%	0.09	0.36	2.0%	
EXC2	5.06	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	5.06	2.0%	0.09	0.36	2.0%	
OS1	23.82	0.90	0.96	0.00	0.0%	0.45	0.59	11.03	30.1%	0.59	0.70	4.15	13.9%	0.09	0.36	8.64	0.7%	0.34	0.53	44.8%	
OS2	85.59	0.90	0.96	0.09	0.1%	0.45	0.59	5.09	3.9%	0.59	0.70	13.37	12.5%	0.09	0.36	67.04	1.6%	0.19	0.43	18.0%	
OS3	6.66	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	6.66	2.0%	0.09	0.36	2.0%	
OS4	2.19	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	2.19	2.0%	0.09	0.36	2.0%	
OS5	9.27	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	3.49	7.5%	0.09	0.36	5.78	1.2%	0.28	0.49	8.8%	
B5	2.91	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	3.49	24.0%	0.08	0.35	2.91	2.0%	0.79	1.19	26.0%	
TOTAL (A1-B1)	105.43																				3.8%
TOTAL (OS1-OS5)	127.53																				21.2%
TOTAL	250.38																				12.5%

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Filing No. 2
Location: El Paso County

Project Name: Sterling Ranch Subdivision (Existing)
Project No.: 25188.01
Calculated By: CJD
Checked By: _____
Date: 5/15/20

SUB-BASIN DATA						INITIAL/OVERLAND (T _i)			TRAVEL TIME (T _t)					t _c CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
EXA1	17.68	A	9%	0.15	0.40	225	3.5%	17.0	1417	2.0%	20.0	2.8	8.4	25.4	1642.0	40.7	25.4
EXA2	19.59	A	5%	0.11	0.38	300	2.3%	23.5	1568	2.7%	20.0	3.3	8.0	31.5	1868.0	41.6	31.5
EXA3	5.66	A	2%	0.09	0.36	300	2.5%	23.3	581	2.5%	20.0	3.1	3.1	26.4	881.0	32.3	26.4
EXA4	50.72	A	2%	0.09	0.36	221	4.1%	17.1	2510	1.7%	20.0	2.6	16.2	33.2	2731.0	60.5	33.2
EXB	11.78	A	2%	0.09	0.36	277	2.4%	22.7	326	7.0%	20.0	5.3	1.0	23.8	603.0	27.9	23.8
EXC1	12.36	A	2%	0.09	0.36	275	3.0%	21.0	115	1.0%	20.0	2.0	1.0	22.0	390.0	27.7	22.0
EXC2	5.06	A	2%	0.09	0.36	261	3.5%	19.5	195	2.0%	20.0	2.8	1.1	20.6	456.0	28.1	20.6
OS1	23.82	A	45%	0.34	0.53	300	3.0%	16.5	1197	2.8%	20.0	3.3	6.0	22.4	1497.0	26.2	22.4
OS2	85.59	A	18%	0.19	0.43	229	4.0%	15.7	3294	2.2%	20.0	3.0	18.3	34.1	3523.0	54.8	34.1
OS3	6.66	A	2%	0.09	0.36	197	2.9%	18.0	444	2.6%	20.0	3.2	2.3	20.3	641.0	30.6	20.3
OS4	2.19	A	2%	0.09	0.36	290	1.4%	27.9	72	1.8%	20.0	2.7	0.5	28.4	362.0	26.6	26.6
OS5	9.27	A	9%	0.28	0.49	300	2.7%	18.6	784	2.4%	20.0	3.1	4.2	22.8	1084.0	32.7	22.8
B5	2.91	A	26%	0.79	1.19	0	2.7%	0.0	300	2.4%	15.0	2.3	2.1	2.1	300.0	24.1	5.0

NOTES:

$$t_c = t_i + t_t$$

Where:

- t_c = computed time of concentration (minutes)
- t_i = overland (initial) flow time (minutes)
- t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

- t_t = channelized flow time (travel time, min)
- L_t = waterway length (ft)
- S_o = waterway slope (ft/ft)
- V_t = travel time velocity (ft/sec) = K√S_o
- K = NRCS conveyance factor (see Table 6-2).

Equation 6-2

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_o^{0.33}}$$

Where:

- t_i = overland (initial) flow time (minutes)
- C_s = runoff coefficient for 5-year frequency (from Table 6-4)
- L_i = length of overland flow (ft)
- S_o = average slope along the overland flow path (ft/ft).

Equation 6-4

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

- t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.
- L_t = length of channelized flow path (ft)
- i = imperviousness (expressed as a decimal)
- S_t = slope of the channelized flow path (ft/ft).

Equation 6-3

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use the minimum value even when calculations result in a longer time of

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County

Project Name: Sterling Ranch Subdivision (Existing)
 Project No.: 25188.01
 Calculated By: CJD
 Checked By: _____
 Date: 5/15/20

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					tc CHECK			FINAL
DATA						(T _i)			(T _t)					(URBANIZED BASINS)			
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
Values are not considered final. Use minimum values even when calculations result in a lesser time of concentration.																	

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
Location: El Paso County
Design Storm: 5-Year

Project Name: Sterling Ranch Subdivision (Existing)
Project No.: 25188.01
Calculated By: CJD
Checked By:
Date: 5/15/20

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	I (in/hr)	Q _i (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q _i (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_c (min)	
	1	EXA1	17.68	0.15	25.4	2.65	2.73	7.2															Existing Topography
	2	EXA2	19.59	0.11	31.5	2.24	2.41	5.4				5.4	2.24	1.7						1529	1.3	19.8	Existing Topography Swale conveyance to DP 4.1
	3	EXA3	5.66	0.09	26.4	0.51	2.67	1.4															Existing Topography
	4	EXA4	50.72	0.09	33.2	4.56	2.33	10.6															Existing Topography Overland flow to DP 4.1
		EXC1	12.36	0.09	22.0	1.11	2.95	3.3															
		EXC2	5.06	0.09	20.6	0.46	3.04	1.4															
	10	OS1	23.82	0.34	22.4	8.19	2.92	23.9				23.9	8.19	1.9						2779	1.4	33.3	Existing Topography Overland flow to DP 4.1
	9	OS2	85.59	0.19	34.1	16.29	2.29	37.3				37.3	16.29	1.9						2577	1.4	30.8	Existing Topography Overland flow to DP 4.1
	8	OS3	6.66	0.09	20.3	0.60	3.07	1.8				1.8	0.60	2.4						1785	1.5	19.3	Existing Topography Overland flow to DP 4.1
	5	OS5	9.27	0.28	22.8	2.58	2.90	7.5				7.5	2.58	2.4						399	1.5	4.3	Existing Topography Overland flow to DP 4.1
	4.1								64.9	34.46	1.32	45.6											Sum of DP 2, DP 4, DP 5, DP8, DP 9, & DP 10, Overland flow to the Sand Creek Drainageway
	7	OS4	2.19	0.09	26.6	0.20	2.66	0.5				0.5	0.20	4.5						660	2.1	5.2	Existing Topography Overland flow to DP 6.1
	6	EXB	11.78	0.09	23.8	1.06	2.83	3.0															Existing Topography Overland flow to DP 6.1
	6.1								31.8	1.26	2.39	3.0											Sum of DP 6 & DP 7, Overland flow to the Sand Creek Drainageway
	11	B5	2.91	0.79	5.0	2.29	5.17	11.8															Existing Pond W4 area flows southwest into drainage ditch along Vollmer offsite
		EXC1	12.36	0.09	22.0	1.11	2.95	3.3															
		EXC2	5.06	0.09	20.6	0.46	3.04	1.4															

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
Location: El Paso County
Design Storm: 100-Year

Project Name: Sterling Ranch Subdivision (Existing)
Project No.: 25188.01
Calculated By: CJD
Checked By:
Date: 5/15/20

Description	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	γ (in/hr)	Q (cfs)	t _c (min)	C*A (ac)	γ (in/hr)	Q (cfs)	Q _{direct/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _r (min)	
																							Existing Topography
	1	EXA1	17.68	0.15	25.4	2.65	4.58	12.1					9.0	2.24	1.7					1529	1.3	19.8	Existing Topography Swale conveyance to DP 4.1
	2	EXA2	19.59	0.11	31.5	2.24	4.04	9.0															Existing Topography Swaling Topography
	3	EXA3	5.66	0.09	26.4	0.51	4.49	2.3															Existing Topography Overland flow to DP 4.1
	4	EXA4	50.72	0.09	33.2	4.56	3.91	17.8															Existing Topography Overland flow to DP 4.1
		EXC1	12.36	0.09	22.0	1.11	4.95	5.5															
		EXC2	5.06	0.09	20.6	0.46	5.11	2.3															
	10	OS1	23.82	0.34	22.4	8.19	4.89	40.1				40.1	8.19	1.9					2779	1.4	33.3	Existing Topography Overland flow to DP 4.1	
	9	OS2	85.59	0.19	34.1	16.29	3.84	62.6				62.6	16.29	1.9					2577	1.4	30.8	Existing Topography Overland flow to DP 4.1	
	8	OS3	6.66	0.09	20.3	0.60	5.15	3.1				3.1	0.60	2.4					1785	1.5	19.3	Existing Topography Overland flow to DP 4.1	
	5	OS5	9.27	0.28	4.3	2.58	9.05	23.4				23.4	2.58	2.4					399	1.5	4.3	Existing Topography Overland flow to DP 4.1	
	4.1								64.9	34.46	2.22	76.5											Sum of DP 2, DP 4, DP 5, DP8, DP 9, & DP 10, Overland flow to the Sand Creek Drainageway
	7	OS4	2.19	0.09	26.6	0.20	4.46	0.9				0.9	0.20	4.5					660	2.1	5.2	Existing Topography Overland flow to DP 6.1	
	6	EXB	11.78	0.09	23.8	1.06	4.75	5.0															Existing Topography Overland flow to DP 6.1
	6.1								31.8	1.26	4.02	5.1											Sum of DP 6 & DP 7, Overland flow to the Sand Creek Drainageway
	11	B5	2.91	0.79	5.0	2.29	8.68	19.9															Existing Pond W4 area flows southwest into drainage ditch along Vollmer offsite

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

COMPOSITE % IMPERVIOUS & COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By: _____
 Date: 1/5/21

Basin ID	Total Area (ac)	Streets (100% Impervious)				Residential (65% Impervious) Neighborhood Area (70% Impervious)				Light Industrial (80% Impervious) Commercial (95% Impervious)				Lawns (0% Impervious) (55% Impervious) School Open Space (12%)				Basins Total Weighted C Values		Basins Total Weighted % Imp.
		C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	
A1	2.06	0.90	0.96	0.48	23.3%	0.45	0.59	1.34	42.3%	0.59	0.70	0.00	0.0%	0.08	0.35	0.24	0.0%	0.51	0.65	65.6%
A2	0.82	0.90	0.96	0.20	24.4%	0.45	0.59	0.56	44.4%	0.59	0.70	0.00	0.0%	0.08	0.35	0.06	0.0%	0.53	0.66	68.8%
A3	6.76	0.90	0.96	1.32	19.5%	0.45	0.59	4.16	40.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.28	0.0%	0.47	0.62	59.5%
A4	1.51	0.90	0.96	0.51	33.8%	0.45	0.59	1.00	43.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.60	0.71	76.8%
A5	1.70	0.90	0.96	0.51	30.0%	0.45	0.59	1.19	45.5%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.59	0.70	75.5%
A6	1.37	0.90	0.96	0.39	28.5%	0.45	0.59	0.98	46.5%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.58	0.70	75.0%
A6A	0.53	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.53	95.0%	0.08	0.35	0.00	0.0%	0.81	0.88	95.0%
A7	19.00	0.90	0.96	0.00	0.0%	0.45	0.59	19.00	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
A8	1.48	0.90	0.96	0.74	50.0%	0.45	0.59	0.29	12.7%	0.59	0.70	0.00	0.0%	0.08	0.35	0.45	0.0%	0.56	0.70	62.7%
A9	0.61	0.90	0.96	0.48	78.7%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.13	0.0%	0.73	0.83	78.7%
A10	2.61	0.90	0.96	2.25	86.2%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.36	0.0%	0.79	0.88	86.2%
A11	2.89	0.90	0.96	2.40	83.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.49	0.0%	0.76	0.86	83.0%
A12	3.87	0.90	0.96	0.00	0.0%	0.45	0.59	0.50	8.4%	0.59	0.70	0.00	0.0%	0.08	0.35	3.37	0.0%	0.13	0.38	8.4%
A13	9.65	0.90	0.96	0.00	0.0%	0.45	0.59	9.65	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
A14	11.76	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.00	0.0%	0.39	0.55	11.76	55.0%	0.39	0.55	55.0%
A15	2.91	0.90	0.96	1.57	54.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.34	0.0%	0.52	0.68	54.0%
A16	2.34	0.90	0.96	1.30	55.6%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.04	0.0%	0.54	0.69	55.6%
A17	1.76	0.90	0.96	0.00	0.0%	0.45	0.59	0.64	23.6%	0.59	0.70	0.00	0.0%	0.08	0.35	1.12	0.0%	0.21	0.44	23.6%
A18	5.27	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	1.18	21.3%	0.08	0.35	4.09	0.0%	0.24	0.47	21.3%
A19	31.85	0.90	0.96	0.00	0.0%	0.45	0.59	31.85	67.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	67.0%
A20	1.83	0.90	0.96	1.63	89.1%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.20	0.0%	0.81	0.89	89.1%
A21	1.93	0.90	0.96	1.73	89.6%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.20	0.0%	0.82	0.90	89.6%
A22	8.68	0.90	0.96	0.00	0.0%	0.45	0.59	0.70	5.2%	0.59	0.70	0.00	0.0%	0.08	0.35	7.98	0.0%	0.11	0.37	5.2%
B1	2.98	0.90	0.96	2.98	100.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B2	3.89	0.90	0.96	3.89	100.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B3	2.05	0.90	0.96	2.05	100.0%	0.45	0.59	0.00	0.0%	0.81	0.88	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B4	1.94	0.90	0.96	1.94	100.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.90	0.96	100.0%
B5	2.91	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	2.91	5.0%	0.08	0.35	5.0%

Basin ID	Total Area (ac)	Streets (100% Impervious)				Residential (65% Impervious) Neighborhood Area (70% Impervious)				Light Industrial (80% Impervious) Commercial (95% Impervious)				Lawns (0% Impervious) (55% Impervious) School Open Space (12%)				Basins Total Weighted C Values		Basins Total Weighted % Imp.
		C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	
C1	8.01	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	8.01	95.0%	0.08	0.35	0.00	0.0%	0.81	0.88	95.0%
C2	5.06	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.81	0.88	5.06	95.0%	0.08	0.35	0.00	0.0%	0.81	0.88	95.0%
OS20	308.00	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	308.00	9.0%	0.13	0.40	9.0%
OS21A	20.26	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	20.26	12.0%	0.13	0.40	12.0%
OS21B	8.71	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.09	0.36	8.71	12.0%	0.13	0.40	12.0%
OS2	17.00	0.90	0.96	0.00	0.0%	0.49	0.62	17.00	70.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.00	0.0%	0.49	0.62	70.0%
OS3	28.70	0.90	0.96	0.00	0.0%	0.49	0.62	28.70	70.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.00	0.0%	0.49	0.62	70.0%
OS4	5.08	0.90	0.96	0.00	0.0%	0.20	0.40	5.08	15.0%	0.59	0.70	0.00	0.0%	0.09	0.36	0.00	0.0%	0.20	0.40	15.0%
TOTAL (A1-A22,OS2-4)	173.97																			57.6%
TOTAL (B1-B5, OS20-21B)	350.74																			12.0%
TOTAL (C1-C2)	13.07																			95.0%
TOTAL	537.78																			29.4%

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By: _____
 Date: 1/5/21

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					t _c CHECK			FINAL
DATA						(T _i)			(T _t)					(URBANIZED BASINS)			
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	
A1	2.06	A	66%	0.51	0.65	100	2.5%	7.8	388	3.0%	20.0	3.5	1.9	9.7	488.0	16.9	9.7
A2	0.82	A	69%	0.53	0.66	100	2.5%	7.6	183	1.0%	20.0	2.0	1.5	9.1	283.0	15.9	9.1
A3	6.76	A	60%	0.47	0.62	100	2.5%	8.4	1186	2.3%	20.0	3.0	6.5	15.0	1286.0	23.4	15.0
A4	1.51	A	77%	0.60	0.71	78	2.0%	6.3	795	2.9%	20.0	3.4	3.9	10.2	873.0	16.9	10.2
A5	1.70	A	76%	0.59	0.70	100	2.5%	6.9	645	3.1%	20.0	3.5	3.1	9.9	745.0	16.3	9.9
A6	1.37	A	75%	0.58	0.70	100	2.5%	7.0	632	3.1%	20.0	3.5	3.0	10.0	732.0	16.3	10.0
A6A	0.53	A	95%	0.81	0.88	100	2.0%	4.2	30	2.0%	20.0	2.8	0.2	4.3	130.0	10.0	5.0
A7	19.00	A	65%	0.45	0.59	100	2.5%	8.7	1419	1.5%	20.0	2.4	9.7	18.3	1519.0	25.6	18.3
A8	1.48	A	63%	0.56	0.70	80	2.0%	6.9	646	0.6%	20.0	1.5	7.0	13.9	726.0	23.2	13.9
A9	0.61	A	79%	0.73	0.83	15	2.0%	2.1	661	0.7%	20.0	1.7	6.6	8.7	676.0	19.2	8.7
A10	2.61	A	86%	0.79	0.88	15	2.0%	1.7	1357	3.4%	20.0	3.7	6.1	7.9	1372.0	17.2	7.9
A11	2.89	A	83%	0.76	0.86	16	2.0%	1.9	1357	2.8%	20.0	3.3	6.8	8.7	1373.0	18.4	8.7
A12	3.87	A	8%	0.13	0.38	100	5.0%	10.3	267	3.4%	15.0	2.8	1.6	11.9	367.0	26.9	11.9
A13	9.65	A	65%	0.45	0.59	100	2.5%	8.7	934	2.1%	20.0	2.9	5.4	14.0	1033.6	20.9	14.0
A14	11.76	A	55%	0.39	0.55	100	2.0%	10.2	867	2.0%	20.0	2.8	5.1	15.3	967.0	22.8	15.3
A15	2.91	A	54%	0.52	0.68	34	2.0%	4.8	1621	1.8%	20.0	2.7	10.1	14.9	1655.0	29.0	14.9
A16	2.34	A	56%	0.54	0.69	35	2.0%	4.8	1594	1.8%	20.0	2.7	9.9	14.7	1629.0	28.4	14.7
A17	1.76	A	24%	0.21	0.44	100	5.0%	9.4	403	1.1%	15.0	1.6	4.3	13.7	503.0	27.2	13.7
A18	5.27	A	21%	0.24	0.47	100	2.0%	12.3	703	2.0%	20.0	2.8	4.1	16.4	803.0	29.3	16.4
A19	31.85	A	67%	0.45	0.59	100	2.5%	8.7	2675	1.7%	20.0	2.6	17.1	25.8	2775.0	33.2	25.8
A20	1.83	A	89%	0.81	0.89	15	2.0%	1.6	936	1.5%	20.0	2.4	6.4	8.0	951.0	16.8	8.0
A21	1.93	A	90%	0.82	0.90	15	2.0%	1.6	1049	1.5%	20.0	2.4	7.1	8.7	1064.0	17.4	8.7
A22	8.68	A	5%	0.11	0.37	185	3.0%	16.9	540	0.5%	20.0	1.4	6.4	23.3	725.0	38.2	23.3
B1	2.98	A	100%	0.90	0.96	17	2.0%	1.2	2561	1.7%	20.0	2.6	16.4	17.6	2578.0	23.2	17.6
B2	3.89	A	100%	0.90	0.96	17	2.0%	1.2	2561	1.7%	20.0	2.6	16.4	17.6	2578.0	23.2	17.6
B3	2.05	A	100%	0.90	0.96	17	2.0%	1.2	1394	2.0%	20.0	2.8	8.2	9.4	1411.0	16.1	9.4
B4	1.94	A	100%	0.90	0.96	17	2.0%	1.2	1394	2.0%	20.0	2.8	8.2	9.4	1411.0	16.1	9.4

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Filing No. 2
Location: El Paso County

Project Name: Sterling Ranch Subdivision
Project No.: 25188.01
Calculated By: AAM
Checked By: _____
Date: 1/5/21

SUB-BASIN DATA						INITIAL/OVERLAND (T _i)			TRAVEL TIME (T _t)					t _c CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
B5	2.91	A	5%	0.08	0.35	170	14.0%	10.1	259	0.5%	20.0	1.4	3.1	13.1	429.0	31.4	13.1
C1	8.01	A	95%	0.81	0.88	100	2.0%	4.2	965	2.0%	20.0	2.8	5.7	9.9	1065.0	14.9	9.9
C2	5.06	A	95%	0.81	0.88	100	2.0%	4.2	627	2.0%	20.0	2.8	3.7	7.9	727.0	13.2	7.9
OS20	308.00	A	9%	0.13	0.40	300	4.0%	19.2	6670	5.0%	10.0	2.2	49.7	68.9	6970.0	72.9	68.9
OS21A	20.26	A	12%	0.13	0.40	300	2.0%	24.1	2673	2.0%	10.0	1.4	31.5	55.6	2973.0	53.5	53.5
OS21B	8.71	A	12%	0.13	0.40	100	2.0%	13.9	1167	1.5%	15.0	1.8	10.6	24.5	1267.0	38.8	24.5
OS2	17.00	A	70%	0.49	0.62	300	1.0%	19.1	3020	1.5%	15.0	1.8	27.4	46.5	3320.0	36.0	36.0
OS3	28.70	A	70%	0.49	0.62	300	1.0%	19.1	4340	1.0%	15.0	1.5	48.2	67.3	4640.0	52.6	52.6
OS4	5.08	A	15%	0.20	0.40	300	1.0%	28.1	900	5.0%	10.0	2.2	6.7	34.9	1200.0	29.5	29.5

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

t_t = channelized flow time (travel time, min)

L_t = waterway length (ft)

S_o = waterway slope (ft/ft)

V_t = travel time velocity (ft/sec) = K√S_o

K = NRCS conveyance factor (see Table 6-2).

Equation 6-2

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S_o^{0.33}}$$

Where:

t_i = overland (initial) flow time (minutes)

C_s = runoff coefficient for 5-year frequency (from Table 6-4)

L = length of overland flow (ft)

S_o = average slope along the overland flow path (ft/ft).

Equation 6-4

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S_t = slope of the channelized flow path (ft/ft).

Equation 6-3

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County
 Design Storm: 5-Year

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By:
 Date: 1/5/21

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE			TRAVEL TIME			REMARKS	
		Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C* A (Ac)	I (in/hr)	Q (cfs)	t _c (min)	C* A (ac)	I (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C* A (ac)	Slope (%)	Q _{pipe} (cfs)	C* A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)		t _t (min)
	1	A1	2.06	0.51	9.7	1.05	4.17	4.4					0.2	0.04	3.3	4.2	1.01	2.0	18	652	3.6	3.0	On-grade inlet, carryover flow to DP 5 Piped to DP 1.0
	2	A2	0.82	0.53	9.1	0.44	4.27	1.9								1.9	0.44	2.0	18	27	5.8	0.1	On-grade inlet Piped to DP 1.0
	1.0								9.7	1.45	4.17	6.0				6.0	1.45	3.0	18	335	9.1	0.6	Sum of DP 1 & DP 2, piped to DP 1.2
	3	A3	6.76	0.47	15.0	3.16	3.53	11.1					1.6	0.47	2.9	9.5	2.69	4.7	18	426	3.4	2.1	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	4	A4	1.51	0.60	10.2	0.91	4.10	3.7					0.1	0.03	2.9	3.6	0.88	4.7	18	395	3.4	1.9	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	1.1								15.0	3.57	3.52	12.6				12.6	3.57	1.0	24	74	7.4	0.2	Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.2	5.02	3.50	17.6				17.6	5.02	3.3	24	319	12.5	0.4	Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.81	5.0	0.43	5.17	2.2															Overland Flow to DP1.3A
	6	A6	1.37	0.58	10.0	0.79	4.14	3.3								3.3	0.79	2.0	18	0	6.7	0.0	On-grade inlet Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.22	4.14	5.0				5.0	1.22	1.0	24	36	5.7	0.1	Sum of DP 6 & DP 6A, piped to DP 1.3
	5	A5	1.70	0.59	9.9	0.99	4.14	4.1	17.0	1.53	3.33	5.1				5.1	1.53	2.0	18	0	7.6	0.0	On-grade inlet Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	7.77	3.33	25.9				25.9	7.77	1.1	36	620	9.2	1.1	Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4
	7	A7	19.00	0.45	18.3	8.55	3.22	27.5								27.5	8.55	1.5	42	20	10.3	0.0	Future storm infrastructure from Copper Chase Subdivision Piped to DP 1.4
	1.4								18.4	16.32	3.22	52.5				52.5	16.32	0.5	48	26	8.2	0.1	Sum of DP 1.3 & DP 7, piped to DP 1.5
	8	A8	1.48	0.56	13.9	0.83	3.63	3.0								3.0	0.83	2.0	18	20	6.6	0.1	On-grade inlet, carryover flow to DP 11 Piped to DP 1.5
	1.5								18.4	17.15	3.21	55.1				55.1	17.15	0.5	48	91	8.3	0.2	Sum of DP 1.4 & DP 8, piped to DP 1.6
	9	A9	0.61	0.73	8.7	0.44	4.34	1.9	8.7	0.48	4.34	2.1				2.1	0.48	2.0	18	13	5.8	0.0	On-grade inlet Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								18.6	17.63	3.20	56.4				56.4	17.63	0.5	48	95	8.3	0.2	Sum of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.79	7.9	2.05	4.49	9.2					0.5	0.11	1.5	8.7	1.94	2.5	18	955	2.4	6.5	On-grade inlet, carryover flow to DP 20 Piped to DP 1.7
	11	A11	2.89	0.76	8.7	2.20	4.34	9.5					0.6	0.15	1.5	8.9	2.05	2.5	18	1049	2.4	7.1	On-grade inlet, carryover flow to DP 21 Piped to DP 1.7
	1.7								8.7	3.99	4.34	17.3				17.3	3.99	1.0	24	8	7.9	0.0	Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								18.8	21.63	3.18	68.8				68.8	21.63	2.0	54	517	14.4	0.6	Sum of DP 1.6 & DP 1.7, piped to DP 2.0
	OS2	OS2	17.00	0.49	14.0	6.25	2.20	13.8								13.8	6.25	1.0	30	787	7.5	1.7	Future flow released from Barbarick Subdivision Piped to DP 2.0
	12	A12	3.87	0.13	11.9	0.49	3.86	1.9								1.9	0.49	2.0	18	17	5.6	0.1	Type C inlet Piped to DP 2.0
	2.0								15.7	6.74	3.45	23.2				23.2	6.74	1.0	48	52	8.4	0.1	Sum of DP OS2 & DP 12, Piped to DP 2.1
	13	A13	9.65	0.45	14.0	4.34	3.62	15.7								15.7	4.34	1.5	30	200	9.1	0.4	Future storm infrastructure from Sterling Ranch Phase 2 Piped to DP 2.1

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County
 Design Storm: 5-Year

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By:
 Date: 1/5/21

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	
	2.1							15.9	11.08	3.44	38.1				38.1	11.08	1.6	48	65	11.4	0.1	Sum of DP 2.0 & DP 13, piped to DP 2.5
	OS3	OS3	28.70	0.49	19.0	14.06	1.25	17.6							17.6	14.06	1.0	30	719	8.0	1.5	Future flow released from Barbarick Subdivision Piped to DP 2.2
	14	A14	11.76	0.39	15.3	4.59	3.49	16.0							16.0	4.59	1.0	30	20	7.8	0.0	Future flow released from School Site Piped to DP 2.2
	2.2							20.5	18.65	3.05	56.9				56.9	18.65	1.5	48	773	12.4	1.0	Sum of DP OS3 & DP 14, piped to DP 2.3
	15	A15	2.91	0.52	14.9	1.52	3.53	5.4							5.4	1.52	1.3	18	35	6.5	0.1	On-grade inlet Piped to DP 2.3
	16	A16	2.34	0.54	14.7	1.25	3.55	4.4				0.1	0.04	0.8	4.3	1.21	2.0	18	697	1.8	6.5	On-grade inlet, carryover flow to DP 9 Piped to DP 2.3
	2.3							15.0	2.73	3.52	9.6				9.6	2.73	1.6	48	51	7.6	0.1	Sum of DP 15 & DP 16, piped to DP 2.4
	2.4							21.5	21.38	2.98	63.7				63.7	21.38	1.6	48	19	13.1	0.0	Sum of DP 2.2 & DP 2.3, piped to DP 2.5
	2.5							21.6	32.46	2.98	96.6				96.6	32.46	2.0	60	839	15.8	0.9	Sum of DP 2.1 & DP 2.4 piped to DP 2.6
	17	A17	1.76	0.21	13.7	0.38	3.66	1.4							1.4	0.38	1.0	18	24	4.1	0.1	Type C inlet Piped to DP 2.6
	2.6							21.6	32.84	2.98	97.8				97.8	32.84	2.0	60	32	15.8	0.0	Sum of DP 2.5 & DP 17, piped to DP 2.7
	2.7							21.6	54.47	2.97	162.0				162.0	54.47	0.6	78	220	11.5	0.3	Sum of DP1.8 & DP 2.6, piped to DP 2.8
	18	A18	5.27	0.24	16.4	1.28	3.38	4.3							4.3	1.28	1.0	18	24	5.6	0.1	Area inlet Piped to DP 2.6
	19	A19	31.85	0.45	25.8	14.33	2.71	38.8							38.8	14.33	1.0	18	24	22.0	0.0	Area inlet Piped to DP 2.6
	2.8							25.8	70.08	2.71	189.8				189.8	70.08	0.6	78	145	12.1	0.2	Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0.
	3.0							25.8	70.08	2.71	189.8	189.8	70.08	0.5					584	1.4	6.9	Detention Pond Trickle channel conveyance to DP 3.2
	20	A20	1.83	0.81	8.0	1.48	4.47	6.6	8.0	1.59	4.47	7.1			7.1	1.59	1.0	24	105	6.4	0.3	On-grade inlet Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0
	21	A21	1.93	0.82	8.7	1.57	4.33	6.8	8.7	1.72	4.33	7.4	0.1	0.03	7.3	1.68	2.5	18	0	9.0	0.0	On-grade inlet Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9
	2.9							8.7	3.27	4.33	14.2				14.2	3.27	2.0	24	58	9.8	0.1	Sum of DP 20 & DP 21, piped to DP 3.1
	3.1							8.7	3.27	4.33	14.2	14.2	3.27	0.5					568	1.4	6.7	Detention Pond Trickle channel conveyance to DP 3.2
	22	A22	8.68	0.11	23.3	0.95	2.86	2.7														Detention Pond Overland flow to DP 3.2
	OS4	OS4	5.08	0.20	29.5	1.02	2.51	2.6				2.6	1.02	13.0					113	5.4	0.3	Existing topography Overland flow to DP 4.1
	3.2							29.8	75.32	2.49	187.5											Outlet Structure Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8
	Pond W5							29.8	1.45	2.49	3.6				3.6	1.45	2.0	48	58	6.2	0.2	Outlet structure release to DP 4.8
	23	B1	2.98	0.90	17.6	2.68	3.29	8.8				0.4	0.12	2.0	8.4	2.56	0.5	30	1399	2.0	12.0	On-grade inlet Piped to DP 4.0

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County
 Design Storm: 5-Year

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By:
 Date: 1/5/21

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE			TRAVEL TIME			REMARKS	
		Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)		t _t (min)
	24	B2	3.89	0.90	17.6	3.50	3.29	11.5					1.4	0.43	2.0	10.1	3.07	2.0	30	1399 0	2.0 8.8	12.0 0.0	On-grade inlet Piped to DP 4.0
	4.0								17.8	5.63	3.26	18.4				18.4	5.63	3.0	30	40	12.1	0.1	Sum of DP 23 & DP 24, piped to DP 4.1
	25	OS20	308.00	0.13	68.9	40.04	1.23	49.4					49.4	40.04	2.0					24	2.1	0.2	Existing topography Overland flow to DP 4.1
	4.1								69.1	45.67	1.23	56.2	56.2	45.67	1.0					1263	1.5	14.0	Sum of DP 4.0 & DP 25, piped to DP 4.3
	26	OS21A	20.26	0.13	53.5	2.63	1.61	4.2					4.2	2.63	1.0					0	2.0	0.0	Existing topography Overland flow to DP 4.3
	27	B3	2.05	0.90	9.4	1.85	4.22	7.8	9.4	1.97	4.22	8.3				8.3	1.97	1.0	30	70	6.5	0.2	Sump inlet Piped to DP 4.2
	28	B4	1.94	0.90	9.4	1.75	4.22	7.4	12.0	2.18	3.86	8.4				8.4	2.18	1.0	30	0	6.5	0.0	Sump inlet Piped to DP 4.2
	4.2								12.0	4.15	3.86	16.0				16.0	4.15	1.0	30	110	7.8	0.2	Sum of DP 27 & DP 28, piped to DP 4.3
	4.3								83.1	52.45	0.95	49.9	49.9	52.45	0.5					192	1.1	3.0	Sum of DP 4.1, DP 4.2, & DP 26, piped to DP 4.5
	29	OS21B	8.71	0.13	24.5	1.13	2.78	3.1								3.1	1.13	1.0	30	719	4.9	2.4	Type D Inlet Piped to DP 4.4
	4.4								24.5	1.13	2.78	3.1	3.1	1.13	0.5					289	1.4	3.4	Detention Pond Trickle channel conveyance to DP 4.5
	30	B5	2.91	0.08	13.1	0.23	3.72	0.9															Detention Pond Overland flow to DP 4.5
	4.5								83.1	53.81	0.95	51.2				51.2	53.81						Outlet Structure Sum of DP 4.3, DP 4.4, & DP 30, outlet structure release to DP 4.6
	Pond W4								83.1	10.09	0.95	9.6				9.6	10.09	1.7	66	311	7.4	0.7	Outlet structure release to DP 4.6
	31	C1	8.01	0.81	9.9	6.49	0.32	2.0								2.0	6.49	2.0	36	52	5.3	0.2	Future Commercial Site, Full spectrum pond release Piped to DP 4.6
	4.6								83.8	60.30	0.94	56.7				56.7	60.30	2.5	60	1598	14.6	1.8	Sum of Pond B & DP 31, piped to DP 4.7
	32	C2	5.06	0.81	7.9	2.00	0.70	1.4								1.4	2.00	2.0	36	52	4.7	0.2	Future Commercial Site, Full spectrum pond release Piped to DP 4.7
	4.7								83.8	62.30	0.94	58.5				58.5	62.30	0.5	66	1004	8.3	2.0	Sum of DP 4.6 & DP 32, piped to DP 4.8
	4.8								83.8	63.75	0.94	59.9				59.9	63.75	0.5	72				Sum of DP DP 4.7 & Pond A, Outfall to Sandcreek Drainageway

Notes:
 Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
 All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County
 Design Storm: 100-Year

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By:
 Date: 1/5/21

Description	Design Point	DIRECT RUNOFF						TOTAL RUNOFF				STREET/SWALE			PIPE			TRAVEL TIME			REMARKS		
		Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (Inches)	Length (ft)		Velocity (fps)	t _t (min)
	1	A1	2.06	0.65	9.7	1.34	7.01	9.4					2.8	0.40	3.3	6.6	0.94	2.0	18	652	3.6	3.0	On-grade inlet, carryover flow to DP 5 0.0 Piped to DP 1.0
	2	A2	0.82	0.66	9.1	0.54	7.17	3.9					0.1	0.01	3.3	3.8	0.53	2.0	18	639	3.6	2.9	On-grade inlet, carryover flow to DP 6 0.1 Piped to DP 1.0
	1.0								9.7	1.47	7.00	10.3				10.3	1.47	3.0	18	335	10.6	0.5	Sum of DP 1 & DP 2, piped to DP 1.2
	3	A3	6.76	0.62	15.0	4.17	5.92	24.7					10.0	1.69	2.9	14.7	2.48	4.7	18	426	3.4	2.1	On-grade inlet, carryover flow to DP 5 0.0 Piped to DP 1.1
	4	A4	1.51	0.71	10.2	1.08	6.88	7.4					1.6	0.24	2.9	5.8	0.84	4.7	18	395	3.4	1.9	On-grade inlet, carryover flow to DP 5 0.0 Piped to DP 1.1
	1.1								15.0	3.33	5.91	19.7				19.7	3.33	1.0	24	74	8.1	0.2	Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.1	4.80	5.89	28.2				28.2	4.80	3.3	24	319	13.9	0.4	Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.88	5.0	0.47	8.68	4.1															Overland Flow to DP1.3A
	6	A6	1.37	0.70	10.0	0.95	6.94	6.6	10.0	0.96	6.94	6.7	1.3	0.18	0.7	5.4	0.78	2.0	18	696	1.7	7.0	On-grade inlet, carryover flow to DP 8 0.0 Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A								10.0	1.25	6.94	8.7				8.7	1.25	1.0	24	36	6.7	0.1	Sum of DP 6 & DP 6A, piped to DP 1.3
	5	A5	1.70	0.70	9.9	1.19	6.95	8.3	17.0	3.51	5.59	19.6	6.5	1.17	0.7	13.1	2.34	2.0	18	664	1.7	6.6	On-grade inlet, carryover flow to DP 8 0.0 Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	8.39	5.59	46.9				46.9	8.39	1.1	36	620	10.7	1.0	Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4
	7	A7	19.00	0.59	18.3	11.21	5.41	60.6								60.6	11.21	1.5	42	20	12.7	0.0	Future storm infrastructure from Copper Chase Subdivision Piped to DP 1.4
	1.4								18.4	19.60	5.40	105.9				105.9	19.60	0.5	48	26	9.2	0.0	Sum of DP 1.3 & DP 7, piped to DP 1.5
	8	A8	1.48	0.70	13.9	1.04	6.10	6.3	23.7	2.63	4.76	12.5	1.9	0.41	0.7	10.6	2.23	2.0	18	195	1.7	1.9	On-grade inlet, carryover flow to DP 11 0.0 Sum of Sub-basin A8 & Carryover flows from DP5, DP 6 & DP 15, Piped to DP 1.5
	1.5								23.7	21.83	4.76	103.9				103.9	21.83	0.5	48	91	9.2	0.2	Sum of DP 1.4 & DP 8, piped to DP 1.6
	9	A9	0.61	0.83	8.7	0.51	7.29	3.7	21.2	0.95	5.04	4.8	0.3	0.05	0.7	4.5	0.89	2.0	18	140	1.7	1.4	On-grade inlet, carryover flow to DP 11 0.0 Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								23.9	22.72	4.74	107.7				107.7	22.72	0.5	48	13	7.3	0.0	Sum of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.88	7.9	2.29	7.53	17.3					4.5	0.59	1.5	12.8	1.70	2.5	18	955	2.4	6.5	On-grade inlet, carryover flow to DP 20 0.2 Piped to DP 1.7
	11	A11	2.89	0.86	8.7	2.48	7.28	18.1	10.6	2.94	6.77	19.9	6.1	0.90	1.5	13.8	2.04	2.5	18	1049	2.4	7.1	On-grade inlet, carryover flow to DP 21 0.0 Sum of Sub-basin A11 & carryover flows from DP 8 & DP 9, piped to DP 1.7
	1.7								10.6	3.74	6.77	25.3				25.3	3.74	1.0	24	8	8.1	0.0	Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								24.0	26.45	4.72	125.0				125.0	26.45	2.0	54	517	17.0	0.5	Sum of DP 1.6 & DP 1.7, piped to DP 2.7
	OS2	OS2	17.00	0.62	12.0	10.54	3.71	39.1								39.1	10.54	1.0	30	787	9.5	1.4	Future flow released from Barbarick Subdivision Piped to DP 2.0
	12	A12	3.87	0.38	11.9	1.47	6.49	9.5								9.5	1.47	2.0	18	17	8.9	0.0	Type C inlet Piped to DP 2.0
	2.0								13.4	12.01	6.20	74.5				74.5	12.01	1.0	48	52	11.6	0.1	Sum of DP OS2 & DP 12, Piped to DP 2.1
	13	A13	9.65	0.59	14.0	5.69	6.08	34.6								34.6	5.69	1.5	30	200	11.0	0.3	Future storm infrastructure from Sterling Ranch Phase 2 Piped to DP 2.1

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County
 Design Storm: 100-Year

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AAM
 Checked By:
 Date: 1/5/21

Description	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (Inches)	Length (ft)	Velocity (fps)	t _t (min)	
	2.1							14.3	17.70	6.02	106.6				106.6	17.70	1.6	48	65	15.1	0.1	Sum of DP 2.0 & DP 13, piped to DP 2.5 Future flow released from Barbarick Subdivision	
	OS3	OS3	28.70	0.62	15.0	17.79	2.75	48.9							48.9	17.79	1.0	30	719	10.0	1.2	Piped to DP 2.2 Future flow released from School Site	
	14	A14	11.76	0.55	15.3	6.47	5.86	37.9							37.9	6.47	1.0	30	20	9.5	0.0	Piped to DP 2.2	
	2.2							16.2	24.26	5.72	138.7				138.7	24.26	1.5	48	773	15.5	0.8	Sum of DP OS3 & DP 14, piped to DP 2.3 On-grade inlet, carryover flow to DP 8	
	15	A15	2.91	0.68	14.9	1.98	5.93	11.7				1.4	0.24	0.7	10.3	1.74	1.3	18	724	1.7	7.2	Piped to DP 2.3 On-grade inlet, carryover flow to DP 9	
	16	A16	2.34	0.69	14.7	1.61	5.96	9.6				2.6	0.44	0.8	7.0	1.17	2.0	18	697	1.8	6.5	On-grade inlet, carryover flow to DP 9 Piped to DP 2.3	
	2.3							15.0	2.91	5.91	17.2				17.2	2.91	1.6	48	15	9.0	0.0	Sum of DP 15 & DP 16, piped to DP 2.4	
	2.4							17.0	27.17	5.59	151.9				151.9	27.17	1.6	48	19	16.2	0.0	Sum of DP 2.2 & DP 2.3, piped to DP 2.5	
	2.5							17.1	44.87	5.59	250.7				250.7	44.87	2.0	60	839	20.1	0.7	Sum of DP 2.1 & DP 2.4 piped to DP 2.6 Type C inlet	
	17	A17	1.76	0.44	13.7	0.77	6.14	4.7							4.7	0.77	1.0	18	24	5.7	0.1	Piped to DP 2.6	
	2.6							17.7	45.64	5.49	250.4				250.4	45.64	2.0	60	32	20.2	0.0	Sum of DP 2.5 & DP 17, piped to DP 2.7	
	2.7							24.5	72.10	4.67	336.8				336.8	72.10	0.6	78	220	13.7	0.3	Sum of DP 1.8 & DP 2.6, piped to DP 2.8 Area inlet	
	18	A18	5.27	0.47	16.4	2.47	5.68	14.0							14.0	2.47	1.0	18	24	7.9	0.1	Piped to DP 2.6 Area inlet	
	19	A19	31.85	0.59	25.8	18.79	4.55	85.4							85.4	18.79	1.0	18	24	48.4	0.0	Piped to DP 2.6	
	2.8							25.8	93.36	4.55	424.4				424.4	93.36	0.6	78	145	13.9	0.2	Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0. Detention Pond	
	3.0							25.8	93.36	4.55	424.4	424.4	93.36	0.5					564	1.4	6.6	Trickle channel conveyance to DP 3.2 On-grade inlet	
	20	A20	1.83	0.89	8.0	1.63	7.50	12.2	14.4	2.22	6.02	13.4	2.3	0.38	1.5	11.1	1.84	1.0	24	105	7.2	0.2	Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0 On-grade inlet
	21	A21	1.93	0.90	8.7	1.73	7.28	12.6	15.8	2.63	5.77	15.2	3.3	0.57	1.5	11.9	2.06	2.5	18	0	10.2	0.0	Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9
	2.9							15.8	3.91	5.77	22.5				22.5	3.91	2.0	24	58	11.0	0.1	Sum of DP 20 & DP 21, piped to DP 3.1 Detention Pond	
	3.1							15.8	3.91	5.77	22.5	22.5	3.91	0.5					568	1.4	6.7	Trickle channel conveyance to DP 3.2 Detention Pond	
	22	A22	8.68	0.37	23.3	3.21	4.80	15.4														Overland flow to DP 3.2	
	OS4	OS4	5.08	0.40	29.5	2.03	4.21	8.5				8.5	2.03	13.0					113	5.4	0.3	Existing topography Overland flow to DP 3.2	
	3.2							29.8	102.50	4.18	428.2											Outlet Structure Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8	
	Pond W5							29.8	34.84	4.18	145.5				145.5	34.84	2.0	48	58	17.5	0.1	Outlet structure release to DP 4.8 On-grade inlet	
	23	B1	2.98	0.96	17.6	2.86	5.51	15.8				3.6	0.65	2.0	12.2	2.21	0.5	30	1394	2.1	11.0	Piped to DP 4.0 On-grade inlet	
	24	B2	3.89	0.96	17.6	3.73	5.51	20.6				6.5	1.17	2.0	14.1	2.56	2.0	30	1394	2.1	11.0	On-grade inlet Piped to DP 4.0	

STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2
Location: El Paso County
Design Storm: 100-Year

Project Name: Sterling Ranch Subdivision
Project No.: 25188.01
Calculated By: AAM
Checked By:
Date: 1/5/21

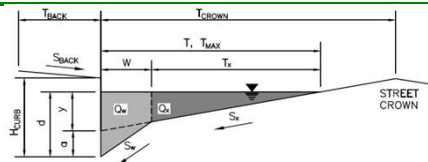
Description	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET/SWALE			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	$Q_{street/swale}$ (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (Inches)	Length (ft)	Velocity (fps)	t_t (min)	
	4.0							17.8	4.77	5.48	26.1				26.1	4.77	3.0	30	40	13.4	0.0	Sum of DP 23 & DP 24, piped to DP 4.1	
	25	OS20	308.00	0.40	68.9	123.20	2.07	310.0				310.0	123.20	2.0					24	2.1	0.2	FLOW TAKEN FROM MDDP Overland flow to DP 4.1	
	4.1							68.9	127.97	2.07	264.7	264.7	127.97	1.0					1263	1.5	14.0	Sum of DP 4.0 & DP 25, piped to DP 4.3	
	26	OS21A	20.26	0.40	53.5	8.10	2.71	21.9				21.9	8.10	1.0					0	2.0	0.0	Existing topography Overland flow to DP 4.3	
	27	B3	2.05	0.96	9.4	1.97	7.09	14.0	17.6	2.62	5.51	14.4			14.4	2.62	1.0	30	70	7.6	0.2	Sump inlet Piped to DP 4.2	
	28	B4	1.94	0.96	9.4	1.86	7.09	13.2	17.6	3.03	5.51	16.7			16.7	3.03	1.0	30	0	8.0	0.0	Sump inlet Piped to DP 4.2	
	4.2							17.7	5.65	5.49	31.0				31.0	5.65	1.0	30	110	9.2	0.2	Sum of DP 27 & DP 28, piped to DP 4.3	
	4.3							68.9	141.72	2.07	293.1	293.1	141.72	0.5					192	1.1	3.0	Sum of DP 4.1, DP 4.2, & DP 26, piped to DP 4.5	
	29	OS21B	8.71	0.40	24.5	3.48	4.67	16.3							16.3	3.48	1.0	30	719	7.8	1.5	Type D Inlet Piped to DP 4.4	
	4.4							24.5	3.48	4.67	16.3	16.3	3.48	0.5					289	1.4	3.4	Detention Pond Trickle channel conveyance to DP 4.5	
	30	B5	2.91	0.35	13.1	1.02	6.25	6.4														Detention Pond Overland flow to DP 4.5	
	4.5							68.9	146.22	2.07	302.4				302.4	146.22						Outlet Structure Sum of DP 4.3, DP 4.4, & DP 30, outlet structure release to DP 4.6	
	Pond W4							68.9	112.40	2.07	232.5				232.5	112.40	1.7	66	311	18.7	0.3	Outlet structure release to DP 4.6	
	31	C1	8.01	0.88	9.9	7.05	2.13	15.0							15.0	7.05	2.0	36	52	9.8	0.1	Future Commercial Site, Full spectrum pond release Piped to DP 4.6	
	4.6							69.2	119.45	2.06	245.8				245.8	119.45	2.5	60	1598	21.9	1.2	Sum of Pond B & DP 31, piped to DP 4.7	
	32	C2	5.06	0.88	7.9	1.32	7.54	10.0							10.0	1.32	2.0	36	52	8.6	0.1	Future Commercial Site, Full spectrum pond release Piped to DP 4.7	
	4.7							69.2	120.77	2.06	248.6				248.6	120.77	0.5	66	1004	11.4	1.5	Sum of DP 4.6 & DP 32, piped to DP 4.8	
	4.8							69.2	155.61	2.06	320.3				320.3	155.61	0.5	72				Sum of DP DP 4.7 & Pond A, Outfall to Sandcreek Drainageway	

Notes:
Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

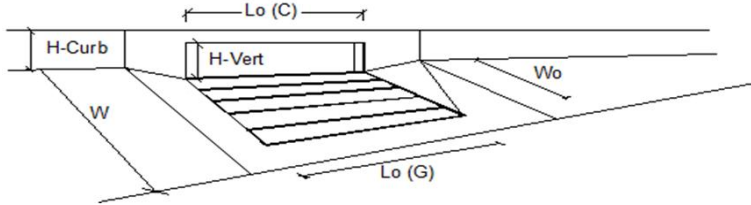
Project: Sterling Ranch Filing No. 2
 Inlet ID: A1



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 8.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 17.0$ ft												
Gutter Width	$W = 1.17$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.027$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>15.8</td> <td>17.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>4.6</td> <td>7.8</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	15.8	17.0	ft	$d_{MAX} =$	4.6	7.8	inches
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$T_{MAX} =$	15.8	17.0	ft										
$d_{MAX} =$	4.6	7.8	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Spread Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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	Minor Storm	Major Storm											
	13.1	16.7	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

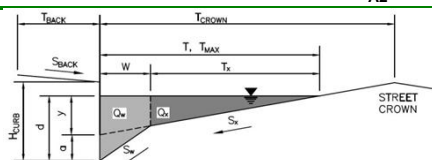


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity.			
Total Inlet Interception Capacity	4.2	6.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.2	2.8	cfs
Capture Percentage = Q_c/Q_o =	95	70	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

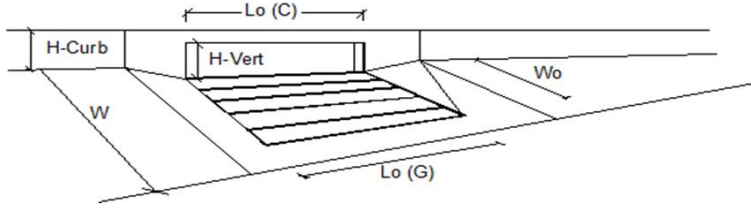
Project: Sterling Ranch Filing No. 2
 Inlet ID: A2



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 8.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) <input type="checkbox"/>	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 17.0$ ft												
Gutter Width	$W = 1.17$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.027$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>15.8</td> <td>17.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>4.6</td> <td>7.8</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	15.8	17.0	ft	$d_{MAX} =$	4.6	7.8	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	15.8	17.0	ft										
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Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no) <input type="checkbox"/>	check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Spread Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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	Minor Storm	Major Storm											
$Q_{allow} =$	13.1	16.7	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		a_{LOCAL} =	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		L_o =	10.00	10.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W_o =	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C_r-G =	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C_r-C =	0.10	0.10
Street Hydraulics: OK - Q < Allowable Street Capacity.				
Total Inlet Interception Capacity		Q =	1.9	3.8
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q_b =	0.0	0.1
Capture Percentage = Q_c/Q_o =		C% =	100	97

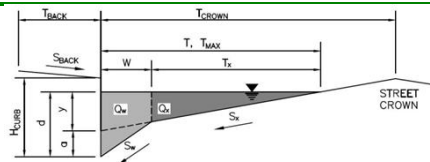
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2

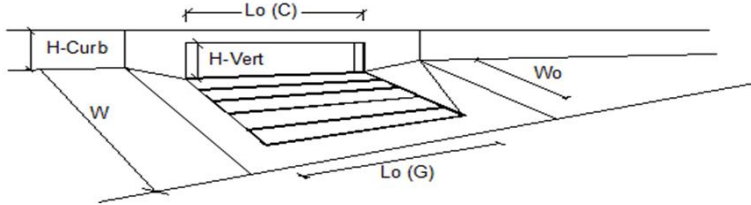
A3



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 8.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 17.0$ ft												
Gutter Width	$W = 1.17$ ft												
Street Transverse Slope	$S_X = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.026$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>15.8</td> <td>17.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>4.6</td> <td>7.8</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	15.8	17.0	ft	$d_{MAX} =$	4.6	7.8	inches
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Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input checked="" type="checkbox"/> check = yes												
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Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



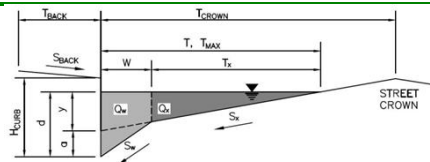
Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity.			
Total Inlet Interception Capacity	9.5	14.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	1.6	10.0	cfs
Capture Percentage = Q_i/Q_o =	86	60	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2
A4



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 8.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 17.0$ ft

Gutter Width

$W = 1.17$ ft

Street Transverse Slope

$S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

$S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

$S_O = 0.026$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	15.8	17.0	ft
$d_{MAX} =$	4.6	7.8	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

check = yes

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

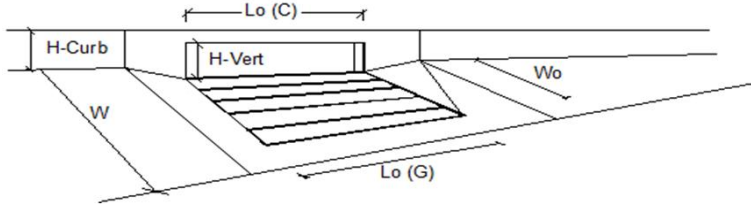
	Minor Storm	Major Storm	
$Q_{allow} =$	12.9	41.5	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

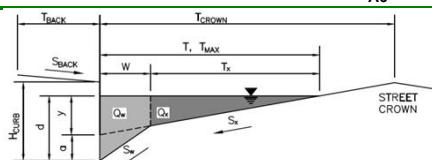


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity.			
Total Inlet Interception Capacity	3.6	5.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.1	1.6	cfs
Capture Percentage = Q_c/Q_o =	98	78	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

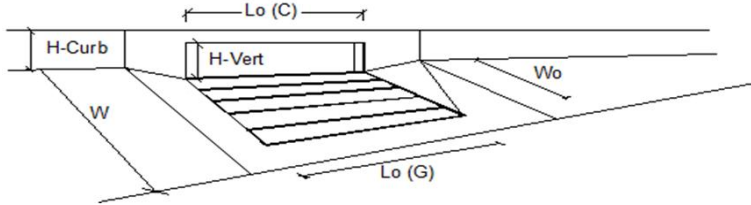
Project: Sterling Ranch Filing No. 2
 Inlet ID: A6



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 8.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 17.0$ ft												
Gutter Width	$W = 1.17$ ft												
Street Transverse Slope	$S_X = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.026$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>15.8</td> <td>17.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>4.6</td> <td>7.8</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	15.8	17.0	ft	$d_{MAX} =$	4.6	7.8	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	15.8	17.0	ft										
$d_{MAX} =$	4.6	7.8	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input checked="" type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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	Minor Storm	Major Storm											
$Q_{allow} =$	12.9	41.5	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	10.00	10.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	3.3	5.4
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.0	1.3
Capture Percentage = $Q_c/Q_o =$		C% =	100	81
				%

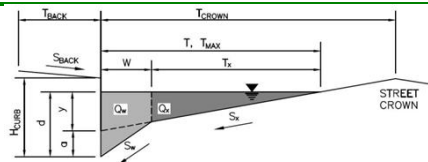
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2

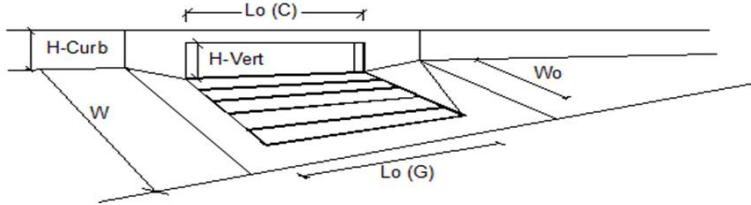
A5



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 8.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 17.0$ ft												
Gutter Width	$W = 1.17$ ft												
Street Transverse Slope	$S_X = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.029$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>15.8</td> <td>17.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>4.6</td> <td>7.8</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	15.8	17.0	ft	$d_{MAX} =$	4.6	7.8	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	15.8	17.0	ft										
$d_{MAX} =$	4.6	7.8	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input checked="" type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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	Minor Storm	Major Storm											
$Q_{allow} =$	13.6	40.2	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	5.1	13.1
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.0	6.5
Capture Percentage = $Q_c/Q_o =$		C% =	100	67
				%

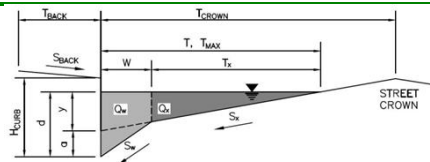
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2

A8



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 7.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 26.0$ ft

Gutter Width

$W = 2.00$ ft

Street Transverse Slope

$S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

$S_w = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

$S_o = 0.007$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	19.3	26.0	ft

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

	Minor Storm	Major Storm	
$d_{MAX} =$	6.0	7.7	inches

Allow Flow Depth at Street Crown (leave blank for no)

check = yes

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

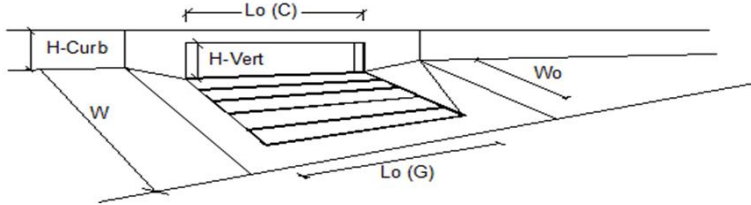
	Minor Storm	Major Storm	
$Q_{allow} =$	11.5	26.7	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



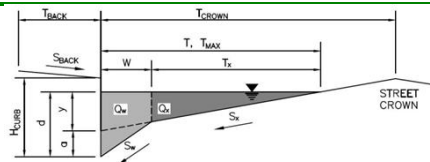
Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	3.0	10.6
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.0	1.9
Capture Percentage = $Q_c/Q_o =$		C% =	100	85
				cfs
				cfs
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing No. 2

Inlet ID: A15



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 7.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 26.0$ ft
 $W = 2.00$ ft
 $S_x = 0.020$ ft/ft
 $S_w = 0.083$ ft/ft
 $S_o = 0.023$ ft/ft
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	19.3	26.0	ft
$d_{MAX} =$	6.0	7.7	inches
	<input type="checkbox"/>	<input type="checkbox"/>	check = yes

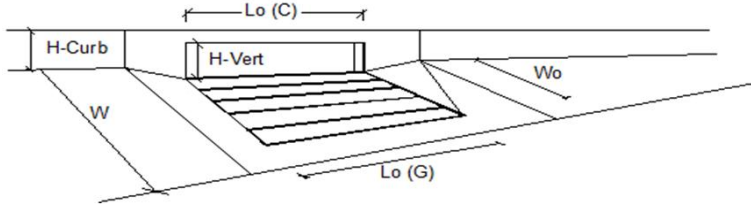
MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	19.2	36.4	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'
 Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

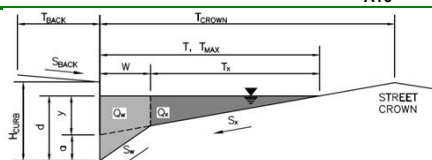


Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	5.4	10.3
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.0	1.4
Capture Percentage = $Q_c/Q_o =$		C% =	100	88
				cfs
				cfs
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

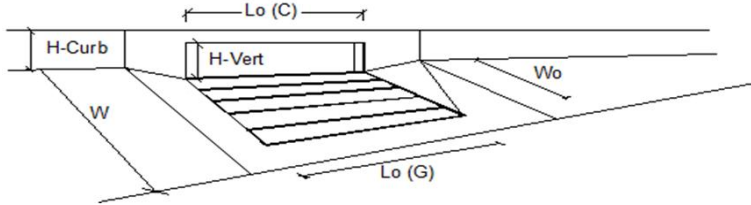
Project: Sterling Ranch Filing No. 2
 Inlet ID: A16



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 7.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 26.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.023$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>19.3</td> <td>26.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>6.0</td> <td>7.7</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	19.3	26.0	ft	$d_{MAX} =$	6.0	7.7	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	19.3	26.0	ft										
$d_{MAX} =$	6.0	7.7	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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	Minor Storm	Major Storm											
$Q_{allow} =$	19.2	36.4	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

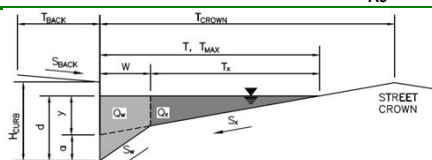


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity.			
Total Inlet Interception Capacity	4.3	7.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.1	2.6	cfs
Capture Percentage = $Q_i/Q_o =$	97	73	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

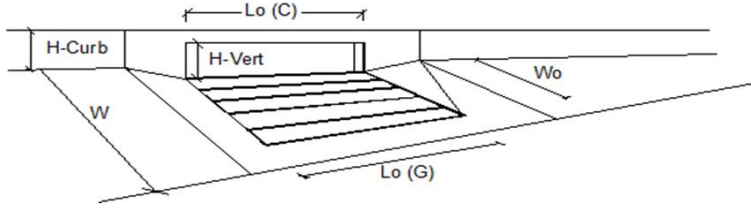
Project: Sterling Ranch Filing No. 2
 Inlet ID: A9



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 7.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 26.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.007$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>19.3</td> <td>26.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>6.0</td> <td>7.7</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	19.3	26.0	ft	$d_{MAX} =$	6.0	7.7	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	19.3	26.0	ft										
$d_{MAX} =$	6.0	7.7	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
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	Minor Storm	Major Storm											
$Q_{allow} =$	11.5	26.9	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

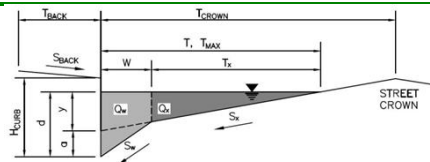


Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	10.00	10.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	2.1	4.5
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.0	0.3
Capture Percentage = $Q_c/Q_o =$		C% =	100	94
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

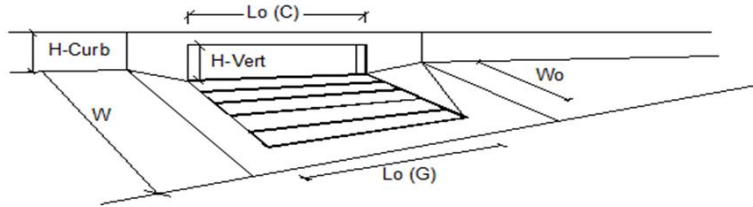
Project: Sterling Ranch Filing No. 2
 Inlet ID: A10



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 15.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 38.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_x = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.012$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>33.0</td> <td>38.0</td> <td>ft</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>6.0</td> <td>9.1</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	33.0	38.0	ft	$d_{MAX} =$	6.0	9.1	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	33.0	38.0	ft										
$d_{MAX} =$	6.0	9.1	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Depth Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$Q_{allow} =$</td> <td>15.2</td> <td>63.8</td> <td>cfs</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$Q_{allow} =$	15.2	63.8	cfs				
	Minor Storm	Major Storm											
$Q_{allow} =$	15.2	63.8	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

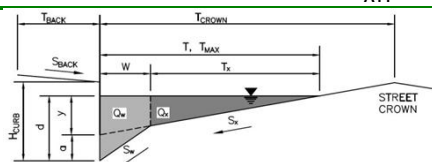


Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		a_{LOCAL} =	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		L_o =	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W_o =	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C_r-G =	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C_r-C =	0.10	0.10
Street Hydraulics: OK - Q < Allowable Street Capacity.				
Total Inlet Interception Capacity		Q =	8.7	12.8
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q_b =	0.5	4.5
Capture Percentage = Q_c/Q_o =		C% =	94	74
				cfs
				cfs
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing No. 2
 Inlet ID: A11



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 15.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 38.0$ ft
 $W = 2.00$ ft

Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition

$S_X = 0.020$ ft/ft
 $S_W = 0.083$ ft/ft
 $S_0 = 0.012$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	33.0	38.0	ft
$d_{MAX} =$	6.0	9.1	inches
	<input type="checkbox"/>	<input type="checkbox"/>	check = yes

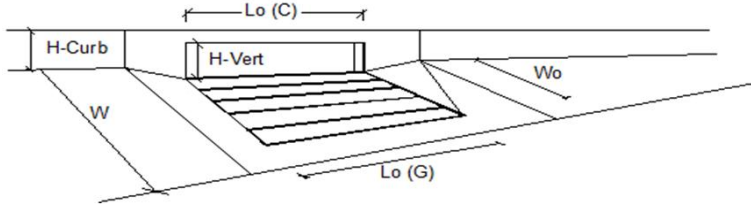
MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	15.1	63.3	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017

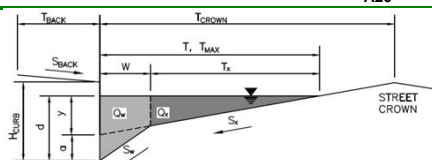


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity.			
Total Inlet Interception Capacity	8.9	13.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.6	6.1	cfs
Capture Percentage = Q_i/Q_o	93	69	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing No. 2
 Inlet ID: A20



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 15.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 38.0$ ft
 $W = 2.00$ ft
 $S_x = 0.020$ ft/ft
 $S_w = 0.083$ ft/ft
 $S_o = 0.015$ ft/ft
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	33.0	38.0	ft
$d_{MAX} =$	6.0	9.1	inches
	<input type="checkbox"/>	<input type="checkbox"/>	check = yes

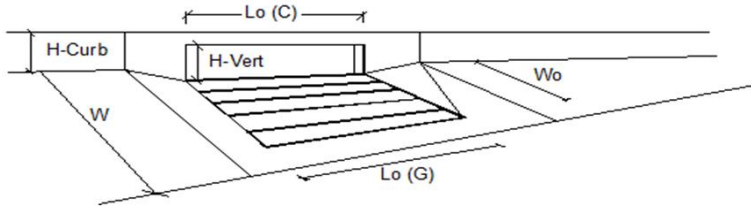
MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	16.9	70.8	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



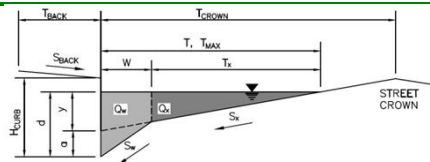
Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		a_{LOCAL} =	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		L_o =	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W_o =	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		C_r-G =	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		C_r-C =	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		Q =	7.1	11.1
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q_b =	0.0	2.3
Capture Percentage = Q_c/Q_o =		C% =	100	83
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

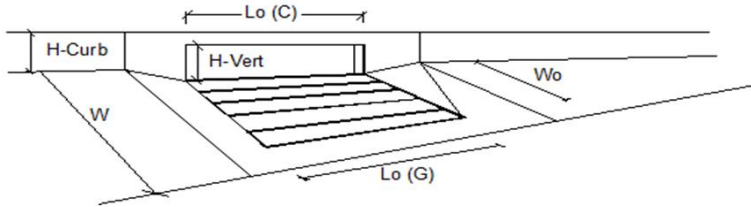
Sterling Ranch Filing No. 2
A21



Gutter Geometry (Enter data in the blue cells)									
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} =$ <input style="width: 50px;" type="text" value="15.0"/> ft								
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} =$ <input style="width: 50px;" type="text" value="0.020"/> ft/ft								
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} =$ <input style="width: 50px;" type="text" value="0.016"/>								
Height of Curb at Gutter Flow Line	$H_{CURB} =$ <input style="width: 50px;" type="text" value="6.00"/> inches								
Distance from Curb Face to Street Crown	$T_{CROWN} =$ <input style="width: 50px;" type="text" value="38.0"/> ft								
Gutter Width	$W =$ <input style="width: 50px;" type="text" value="2.00"/> ft								
Street Transverse Slope	$S_X =$ <input style="width: 50px;" type="text" value="0.020"/> ft/ft								
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W =$ <input style="width: 50px;" type="text" value="0.083"/> ft/ft								
Street Longitudinal Slope - Enter 0 for sump condition	$S_O =$ <input style="width: 50px;" type="text" value="0.015"/> ft/ft								
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} =$ <input style="width: 50px;" type="text" value="0.016"/>								
Max. Allowable Spread for Minor & Major Storm	<table style="width: 100%; border: none;"> <tr> <td style="width: 50%;"></td> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td>$T_{MAX} =$</td> <td style="border: 1px solid black; text-align: center;">33.0</td> <td style="border: 1px solid black; text-align: center;">38.0</td> <td>ft</td> </tr> </table>		Minor Storm	Major Storm		$T_{MAX} =$	33.0	38.0	ft
	Minor Storm	Major Storm							
$T_{MAX} =$	33.0	38.0	ft						
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table style="width: 100%; border: none;"> <tr> <td style="width: 50%;"></td> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td>$d_{MAX} =$</td> <td style="border: 1px solid black; text-align: center;">6.0</td> <td style="border: 1px solid black; text-align: center;">9.1</td> <td>inches</td> </tr> </table>		Minor Storm	Major Storm		$d_{MAX} =$	6.0	9.1	inches
	Minor Storm	Major Storm							
$d_{MAX} =$	6.0	9.1	inches						
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input type="checkbox"/> check = yes								
MINOR STORM Allowable Capacity is based on Depth Criterion									
MAJOR STORM Allowable Capacity is based on Depth Criterion									
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'									
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'									
	<table style="width: 100%; border: none;"> <tr> <td style="width: 50%;"></td> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td>$Q_{allow} =$</td> <td style="border: 1px solid black; text-align: center;">16.9</td> <td style="border: 1px solid black; text-align: center;">70.8</td> <td>cfs</td> </tr> </table>		Minor Storm	Major Storm		$Q_{allow} =$	16.9	70.8	cfs
	Minor Storm	Major Storm							
$Q_{allow} =$	16.9	70.8	cfs						

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	7.3	11.9
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.1	3.3
Capture Percentage = $Q_c/Q_o =$		C% =	99	79
				%

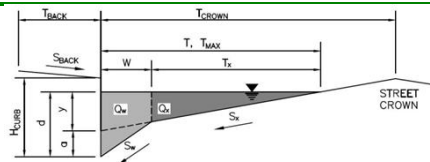
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2

B1



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} =$ 17.0 ft
 $S_{BACK} =$ 0.020 ft/ft
 $n_{BACK} =$ 0.016

Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} =$ 6.00 inches
 $T_{CROWN} =$ 33.0 ft
 $W =$ 2.00 ft
 $S_X =$ 0.020 ft/ft
 $S_W =$ 0.083 ft/ft
 $S_0 =$ 0.017 ft/ft
 $n_{STREET} =$ 0.016

Max. Allowable Spread for Minor & Major Storm
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
Allow Flow Depth at Street Crown (leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	28.0	33.0	ft
$d_{MAX} =$	6.0	10.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	check = yes

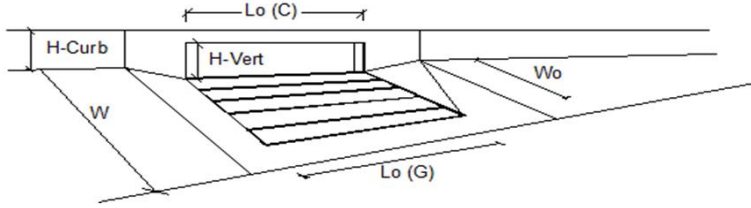
MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Spread Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	18.0	85.4	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



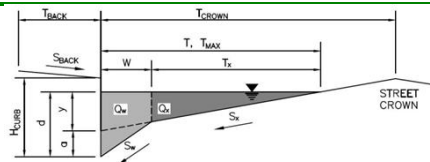
Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	8.4	12.2
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	0.4	3.6
Capture Percentage = $Q_c/Q_o =$		C% =	96	77
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

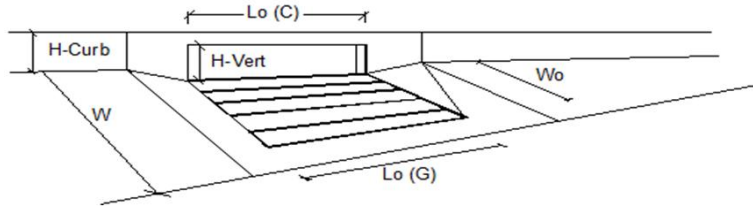
Sterling Ranch Filing No. 2
B2



Gutter Geometry (Enter data in the blue cells)													
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 17.0$ ft												
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft												
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.016$												
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches												
Distance from Curb Face to Street Crown	$T_{CROWN} = 33.0$ ft												
Gutter Width	$W = 2.00$ ft												
Street Transverse Slope	$S_X = 0.020$ ft/ft												
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft												
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.017$ ft/ft												
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$												
Max. Allowable Spread for Minor & Major Storm	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$T_{MAX} =$</td> <td>28.0</td> <td>33.0</td> <td>ft</td> </tr> <tr> <td>$q_{MAX} =$</td> <td>6.0</td> <td>10.0</td> <td>inches</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$T_{MAX} =$	28.0	33.0	ft	$q_{MAX} =$	6.0	10.0	inches
	Minor Storm	Major Storm											
$T_{MAX} =$	28.0	33.0	ft										
$q_{MAX} =$	6.0	10.0	inches										
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm													
Allow Flow Depth at Street Crown (leave blank for no)	<input type="checkbox"/> <input type="checkbox"/> check = yes												
MINOR STORM Allowable Capacity is based on Depth Criterion													
MAJOR STORM Allowable Capacity is based on Spread Criterion													
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													
	<table border="1"> <thead> <tr> <th></th> <th>Minor Storm</th> <th>Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>$Q_{allow} =$</td> <td>18.0</td> <td>85.4</td> <td>cfs</td> </tr> </tbody> </table>		Minor Storm	Major Storm		$Q_{allow} =$	18.0	85.4	cfs				
	Minor Storm	Major Storm											
$Q_{allow} =$	18.0	85.4	cfs										

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



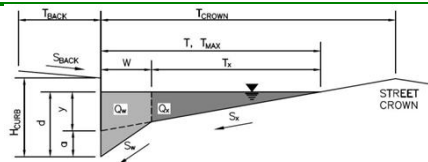
Design Information (Input)	CDOT Type R Curb Opening	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	3.0	3.0
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	15.00	15.00
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	N/A	N/A
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	N/A	N/A
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	0.10	0.10
Street Hydraulics: OK - $Q < Q_{allowable}$ Street Capacity.				
Total Inlet Interception Capacity		$Q =$	10.1	14.1
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b =$	1.4	6.5
Capture Percentage = $Q_c/Q_o =$		C% =	88	68
				%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2
B3



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 17.0$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 33.0$ ft
 $W = 2.00$ ft
 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$S_W = 0.083$ ft/ft
 $S_0 = 0.000$ ft/ft
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
Check boxes are not applicable in SUMP conditions

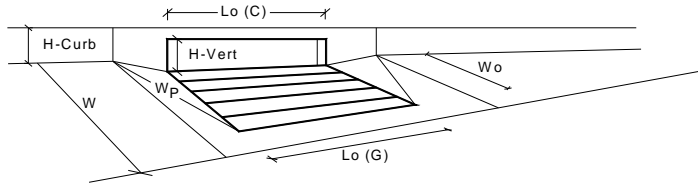
	Minor Storm	Major Storm	
$T_{MAX} =$	28.0	33.0	ft
$d_{MAX} =$	6.0	10.0	inches

MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	8.0	inches
Grate Information	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.34	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets	0.57	0.75	
Curb Opening Performance Reduction Factor for Long Inlets	0.94	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	MINOR	MAJOR	
Q_a	8.4	16.3	cfs
Q _{PEAK REQUIRED}	8.3	14.4	cfs

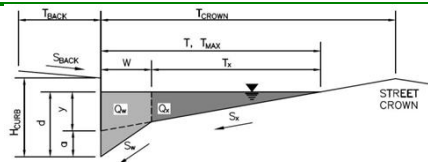
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:
Inlet ID:

Sterling Ranch Filing No. 2
B4



Gutter Geometry (Enter data in the blue cells)

Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} =$ 17.0 ft
 $S_{BACK} =$ 0.020 ft/ft
 $n_{BACK} =$ 0.016

Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width

$H_{CURB} =$ 6.00 inches
 $T_{CROWN} =$ 33.0 ft
 $W =$ 2.00 ft

Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$S_X =$ 0.020 ft/ft
 $S_W =$ 0.083 ft/ft
 $S_O =$ 0.000 ft/ft
 $n_{STREET} =$ 0.016

Max. Allowable Spread for Minor & Major Storm
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
Check boxes are not applicable in SUMP conditions

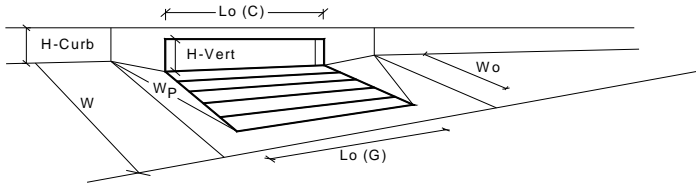
	Minor Storm	Major Storm	
$T_{MAX} =$	28.0	33.0	ft
$d_{MAX} =$	6.0	10.0	inches

MINOR STORM Allowable Capacity is based on Depth Criterion
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



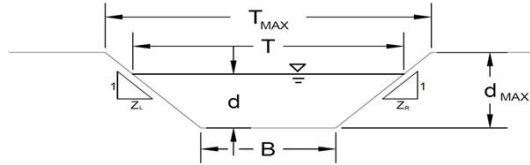
Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	1	1	
Water Depth at Flowline (outside of local depression)	6.0	9.4	inches
Grate Information	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate	N/A	N/A	feet
Width of a Unit Grate	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A	
Curb Opening Information	MINOR	MAJOR	
Length of a Unit Curb Opening	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67	
Low Head Performance Reduction (Calculated)	MINOR	MAJOR	
Depth for Grate Midwidth	N/A	N/A	ft
Depth for Curb Opening Weir Equation	0.34	0.62	ft
Combination Inlet Performance Reduction Factor for Long Inlets	0.57	0.89	
Curb Opening Performance Reduction Factor for Long Inlets	0.94	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition)	MINOR	MAJOR	
Q_a	8.5	21.0	cfs
Q _{PEAK REQUIRED}	8.4	16.7	cfs

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

AREA INLET IN A SWALE

Sterling Ranch Filing No. 2

A12



This worksheet uses the NRCS vegetative retardance method to determine Manning's n.
For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method													
NRCS Vegetal Retardance (A, B, C, D, or E) Manning's n (Leave cell D16 blank to manually enter an n value) Channel Invert Slope Bottom Width Left Side Slope Right Side Slope Check one of the following soil types:	A, B, C, D or E <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="text-align: center;">A</td></tr> <tr><td style="text-align: center;">see details below</td></tr> <tr><td style="text-align: center;">0.0200</td></tr> <tr><td style="text-align: center;">ft/ft</td></tr> <tr><td style="text-align: center;">2.00</td></tr> <tr><td style="text-align: center;">ft</td></tr> <tr><td style="text-align: center;">4.00</td></tr> <tr><td style="text-align: center;">ft/ft</td></tr> <tr><td style="text-align: center;">4.00</td></tr> <tr><td style="text-align: center;">ft/ft</td></tr> </table>	A	see details below	0.0200	ft/ft	2.00	ft	4.00	ft/ft	4.00	ft/ft		
A													
see details below													
0.0200													
ft/ft													
2.00													
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4.00													
ft/ft													
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Soil Type:	Max. Velocity (V_{MAX})	Max Froude No. (F_{MAX})											
Non-Cohesive	5.0 fps	0.60											
Cohesive	7.0 fps	0.80											
Paved	N/A	N/A											
Max. Allowable Top Width of Channel for Minor & Major Storm Max. Allowable Water Depth in Channel for Minor & Major Storm	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Minor Storm</th> <th style="text-align: center;">Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>T_{MAX} =</td> <td style="text-align: center;">18.00</td> <td style="text-align: center;">18.00</td> <td style="text-align: right;">feet</td> </tr> <tr> <td>d_{MAX} =</td> <td style="text-align: center;">2.00</td> <td style="text-align: center;">2.00</td> <td style="text-align: right;">feet</td> </tr> </tbody> </table>		Minor Storm	Major Storm		T_{MAX} =	18.00	18.00	feet	d_{MAX} =	2.00	2.00	feet
	Minor Storm	Major Storm											
T_{MAX} =	18.00	18.00	feet										
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d_{allow} =	2.00	2.00	ft										
Water Depth in Channel Based On Design Peak Flow Design Peak Flow Water Depth	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Minor Storm</th> <th style="text-align: center;">Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>Q_c =</td> <td style="text-align: center;">1.9</td> <td style="text-align: center;">9.5</td> <td style="text-align: right;">cfs</td> </tr> <tr> <td>d =</td> <td style="text-align: center;">0.85</td> <td style="text-align: center;">1.79</td> <td style="text-align: right;">feet</td> </tr> </tbody> </table>		Minor Storm	Major Storm		Q_c =	1.9	9.5	cfs	d =	0.85	1.79	feet
	Minor Storm	Major Storm											
Q_c =	1.9	9.5	cfs										
d =	0.85	1.79	feet										
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'													

AREA INLET IN A SWALE

Sterling Ranch Filing No. 2

A12

Inlet Design Information (Input)

Type of Inlet

CDOT Type C

Inlet Type =

CDOT Type C

Angle of Inclined Grate (must be <= 30 degrees)

Width of Grate

Length of Grate

Open Area Ratio

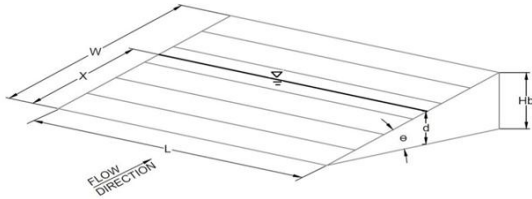
Height of Inclined Grate

Clogging Factor

Grate Discharge Coefficient

Orifice Coefficient

Weir Coefficient



θ =	0.00	degrees
W =	3.00	feet
L =	3.00	feet
A _{RATIO} =	0.70	
H _B =	0.00	feet
C _f =	0.50	
C _d =	0.96	
C _o =	0.64	
C _w =	2.05	

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

	MINOR	MAJOR	
d =	0.85	1.79	
Q_a =	14.5	21.6	cfs
Bypassed Flow, Q_b =	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o = C%	100	100	%

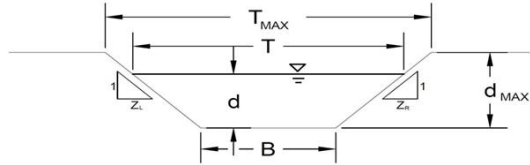
Total Inlet Interception Capacity (assumes clogged condition)

Capture Percentage = $Q_a/Q_o = C\%$

AREA INLET IN A SWALE

Sterling Ranch Filing No. 2

A17



This worksheet uses the NRCS vegetative retardance method to determine Manning's n.
For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method														
NRCS Vegetal Retardance (A, B, C, D, or E)	A, B, C, D or E													
Manning's n (Leave cell D16 blank to manually enter an n value)	n = see details below													
Channel Invert Slope	S ₀ = 0.0130 ft/ft													
Bottom Width	B = 2.00 ft													
Left Side Slope	Z1 = 4.00 ft/ft													
Right Side Slope	Z2 = 4.00 ft/ft													
Check one of the following soil types:	Choose One: <input type="radio"/> Non-Cohesive <input type="radio"/> Cohesive <input type="radio"/> Paved													
<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left;">Soil Type:</th> <th style="text-align: left;">Max. Velocity (V_{MAX})</th> <th style="text-align: left;">Max Froude No. (F_{MAX})</th> </tr> </thead> <tbody> <tr> <td>Non-Cohesive</td> <td>5.0 fps</td> <td>0.60</td> </tr> <tr> <td>Cohesive</td> <td>7.0 fps</td> <td>0.80</td> </tr> <tr> <td>Paved</td> <td>N/A</td> <td>N/A</td> </tr> </tbody> </table>	Soil Type:	Max. Velocity (V _{MAX})	Max Froude No. (F _{MAX})	Non-Cohesive	5.0 fps	0.60	Cohesive	7.0 fps	0.80	Paved	N/A	N/A		
Soil Type:	Max. Velocity (V _{MAX})	Max Froude No. (F _{MAX})												
Non-Cohesive	5.0 fps	0.60												
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MAJOR STORM Allowable Capacity is based on Depth Criterion	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Minor Storm</th> <th style="text-align: center;">Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>d_{allow} =</td> <td style="text-align: center;">2.00</td> <td style="text-align: center;">2.00</td> <td style="text-align: right;">ft</td> </tr> </tbody> </table>			Minor Storm	Major Storm		d _{allow} =	2.00	2.00	ft				
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Water Depth in Channel Based On Design Peak Flow														
Design Peak Flow	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Minor Storm</th> <th style="text-align: center;">Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>Q_c =</td> <td style="text-align: center;">1.4</td> <td style="text-align: center;">4.7</td> <td style="text-align: right;">cfs</td> </tr> </tbody> </table>			Minor Storm	Major Storm		Q _c =	1.4	4.7	cfs				
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Q _c =	1.4	4.7	cfs											
Water Depth	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Minor Storm</th> <th style="text-align: center;">Major Storm</th> <th></th> </tr> </thead> <tbody> <tr> <td>d =</td> <td style="text-align: center;">0.79</td> <td style="text-align: center;">1.46</td> <td style="text-align: right;">feet</td> </tr> </tbody> </table>			Minor Storm	Major Storm		d =	0.79	1.46	feet				
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d =	0.79	1.46	feet											
<p style="color: red; font-weight: bold;">Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</p> <p style="color: red; font-weight: bold;">Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</p>														

AREA INLET IN A SWALE

Sterling Ranch Filing No. 2

A17

Inlet Design Information (Input)

Type of Inlet: Inlet Type =

Angle of Inclined Grate (must be <= 30 degrees): $\theta =$ degrees

Width of Grate: $W =$ feet

Length of Grate: $L =$ feet

Open Area Ratio: $A_{RATIO} =$

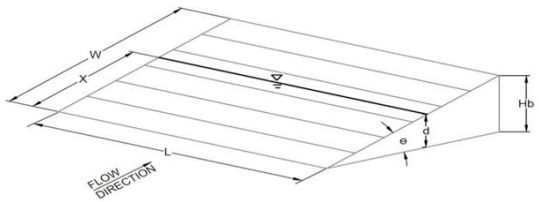
Height of Inclined Grate: $H_B =$ feet

Clogging Factor: $C_f =$

Grate Discharge Coefficient: $C_d =$

Orifice Coefficient: $C_o =$

Weir Coefficient: $C_w =$



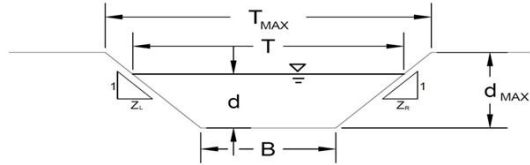
	MINOR	MAJOR	
$d =$	0.79	1.46	
$Q_a =$	13.1	19.5	cfs
Bypassed Flow, $Q_b =$	0.0	0.0	cfs
Capture Percentage = $Q_a/Q_o = C\%$	100	100	%

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

Total Inlet Interception Capacity (assumes clogged condition)

AREA INLET IN A SWALE

Sterling Ranch Filing No. 2
OS21B



This worksheet uses the NRCS vegetative retardance method to determine Manning's n.
For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method																									
NRCS Vegetal Retardance (A, B, C, D, or E) Manning's n (Leave cell D16 blank to manually enter an n value) Channel Invert Slope Bottom Width Left Side Slope Right Side Slope Check one of the following soil types:	A, B, C, D or E <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="text-align: center;">A</td></tr> <tr><td style="text-align: center;">see details below</td></tr> <tr><td style="text-align: center;">0.0200</td></tr> <tr><td style="text-align: center;">ft/ft</td></tr> <tr><td style="text-align: center;">10.00</td></tr> <tr><td style="text-align: center;">ft</td></tr> <tr><td style="text-align: center;">4.00</td></tr> <tr><td style="text-align: center;">ft/ft</td></tr> <tr><td style="text-align: center;">4.00</td></tr> <tr><td style="text-align: center;">ft/ft</td></tr> </table> Choose One: <input type="radio"/> Non-Cohesive <input checked="" type="radio"/> Cohesive <input type="radio"/> Paved	A	see details below	0.0200	ft/ft	10.00	ft	4.00	ft/ft	4.00	ft/ft														
A																									
see details below																									
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	Minor Storm	Major Storm																							
Q _{allow}	56.1	56.1	cfs																						
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	Minor Storm	Major Storm																							
Q _c	2.1	14.5	cfs																						
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Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'																									

AREA INLET IN A SWALE

Sterling Ranch Filing No. 2
OS21B

Inlet Design Information (Input)

Type of Inlet: Inlet Type =

Angle of Inclined Grate (must be <= 30 degrees): $\theta = 0.00$ degrees

Width of Grate: $W = 3.00$ feet

Length of Grate: $L = 6.00$ feet

Open Area Ratio: $A_{RATIO} = 0.70$

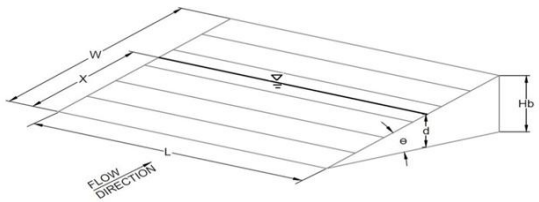
Height of Inclined Grate: $H_B = 0.00$ feet

Clogging Factor: $C_f = 0.38$

Grate Discharge Coefficient: $C_d = 0.78$

Orifice Coefficient: $C_o = 0.52$

Weir Coefficient: $C_w = 1.67$

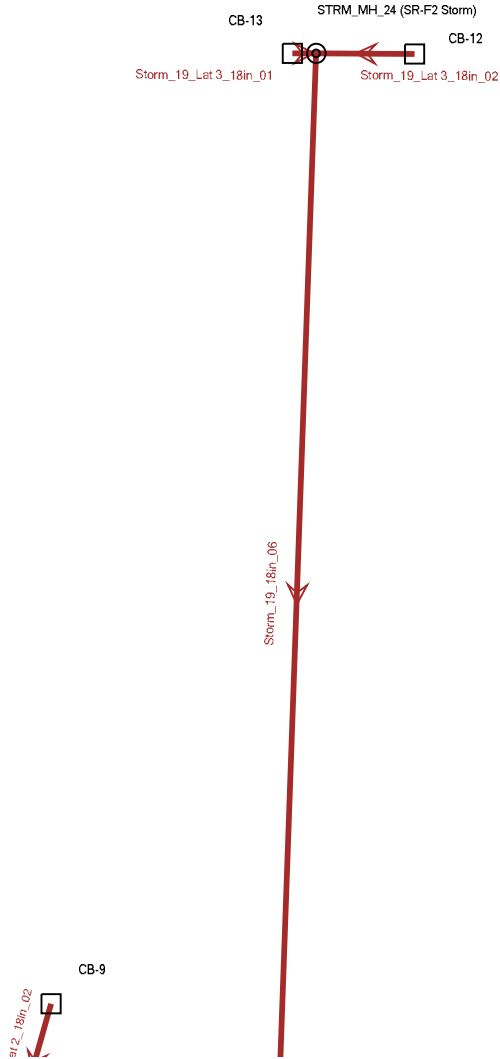


Water Depth at Inlet (for depressed inlets, 1 foot is added for depression):

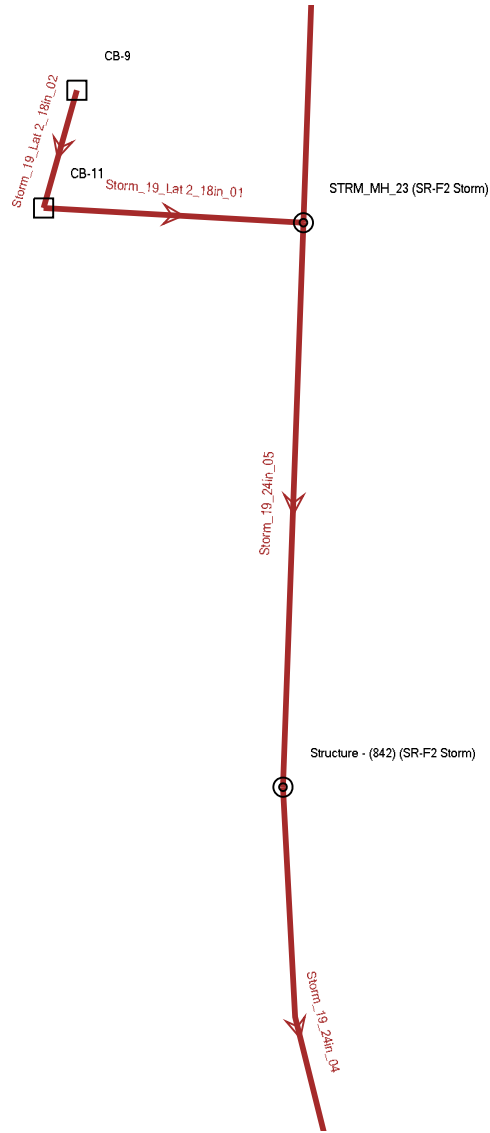
	MINOR	MAJOR
d =	0.47	1.45
$Q_a =$	9.5	39.6
Bypassed Flow, $Q_b =$	0.0	0.0
Capture Percentage = $Q_a/Q_o = C\%$	100	100

Total Inlet Interception Capacity (assumes clogged condition)

Sterling Ranch 5yr

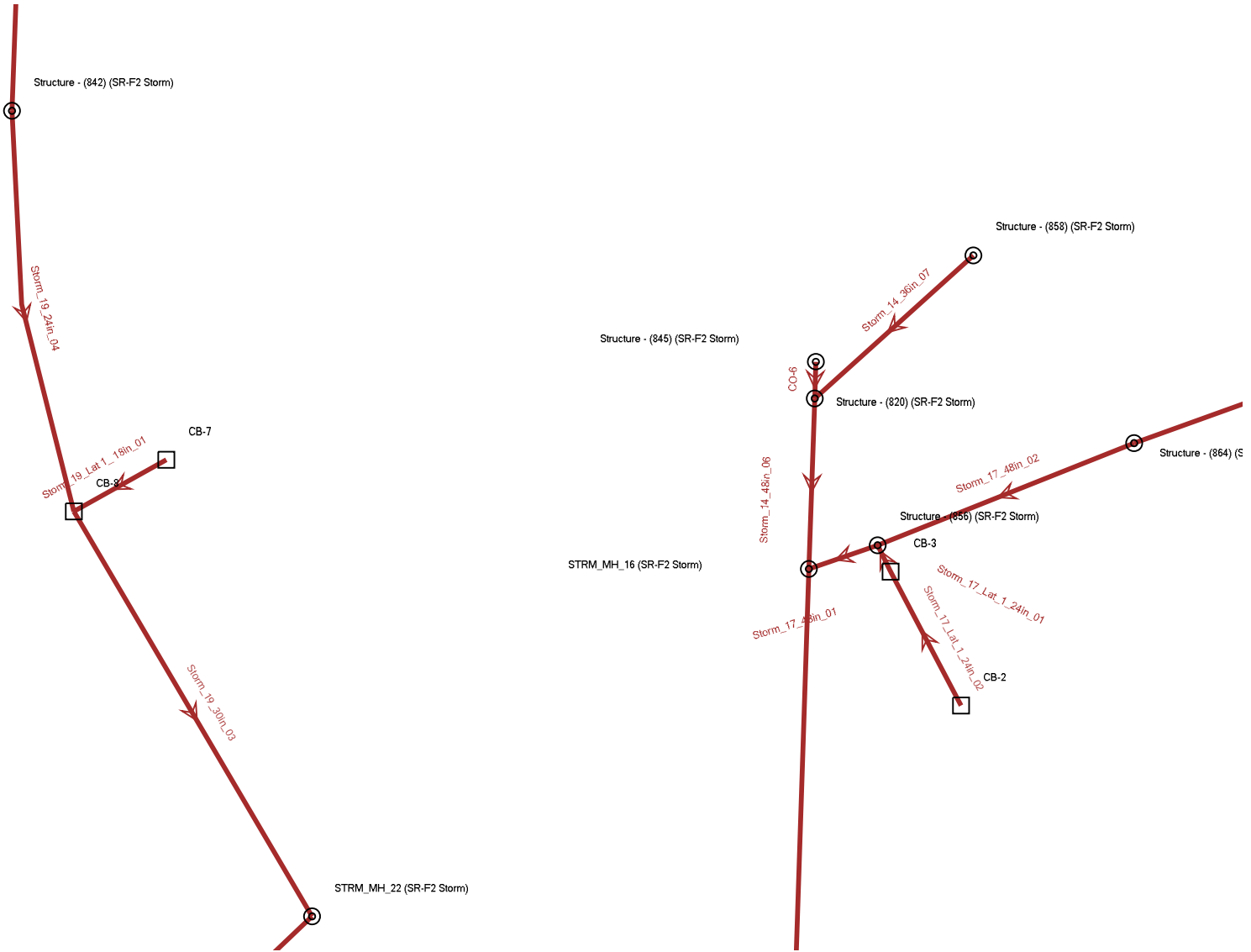


Sterling Ranch 5yr

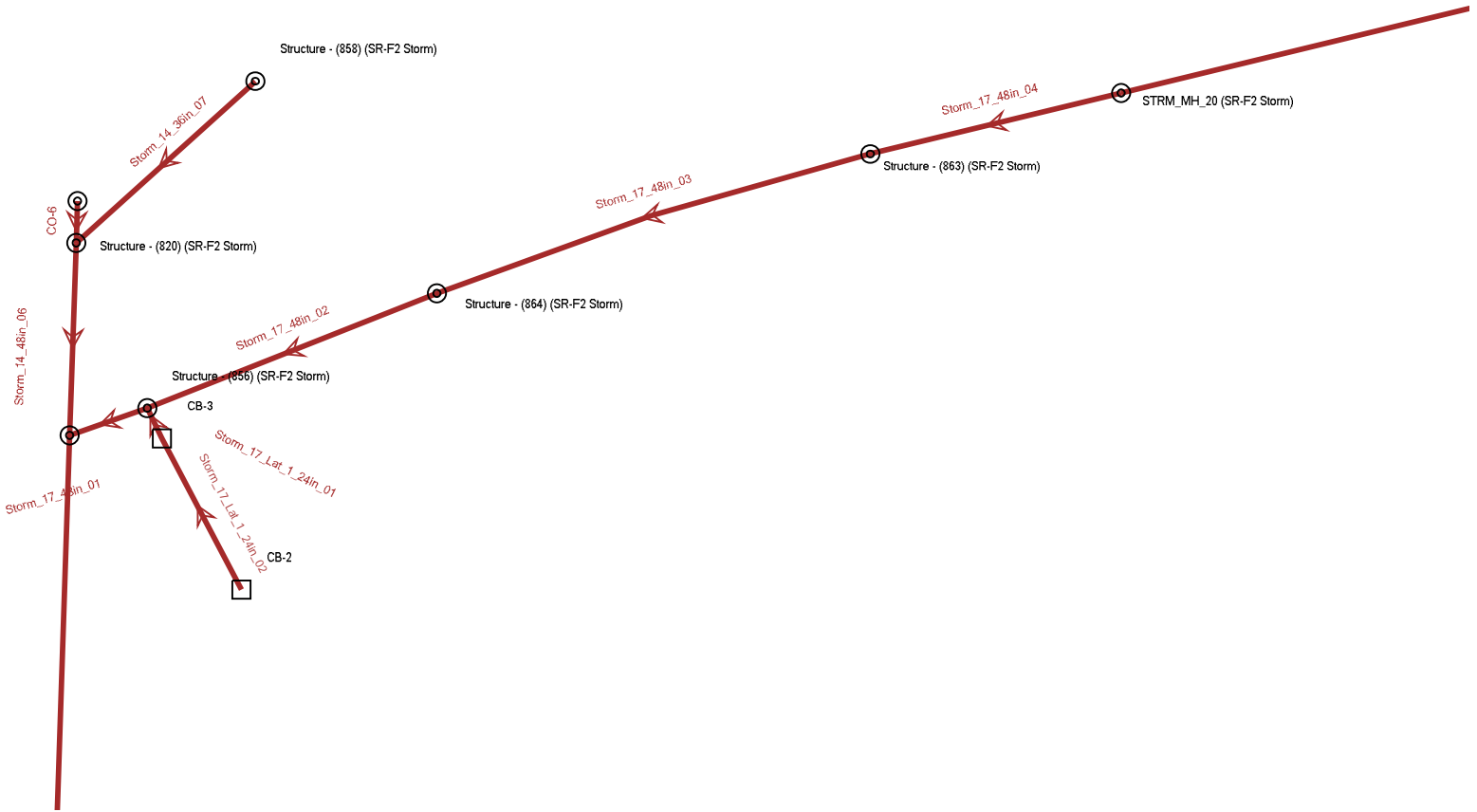


Structure - (845) (SR-F2 Storm)

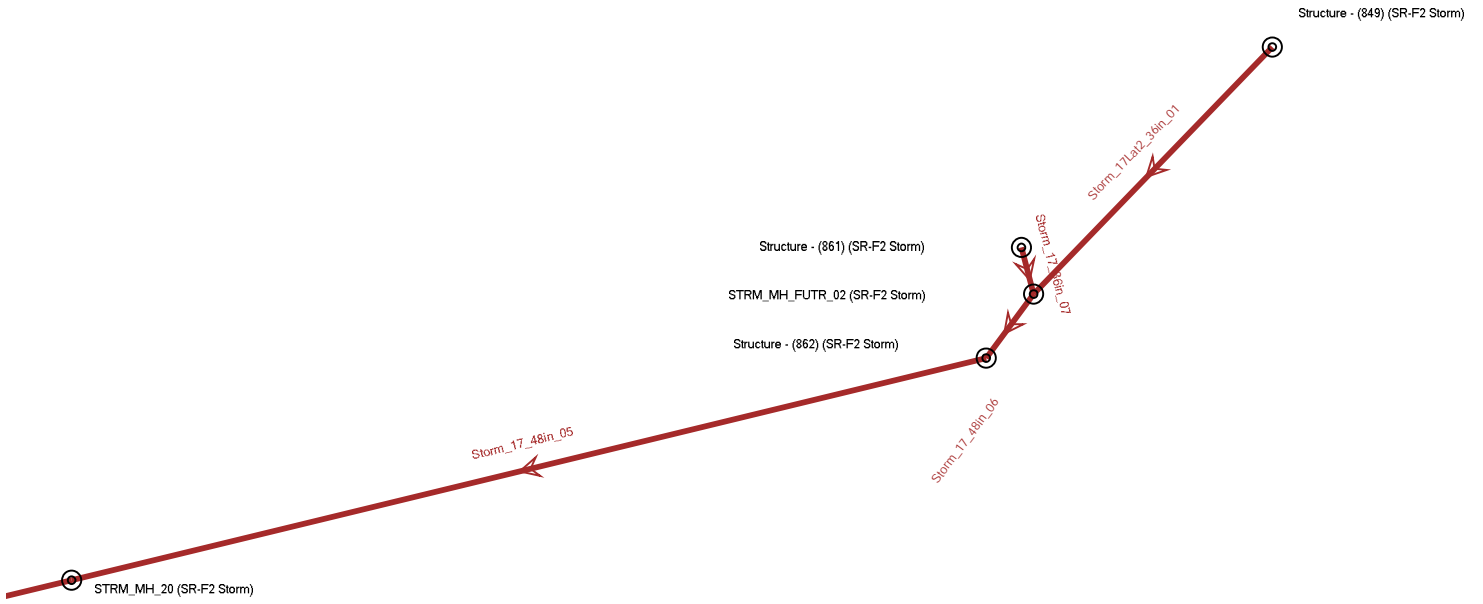
Sterling Ranch 5yr



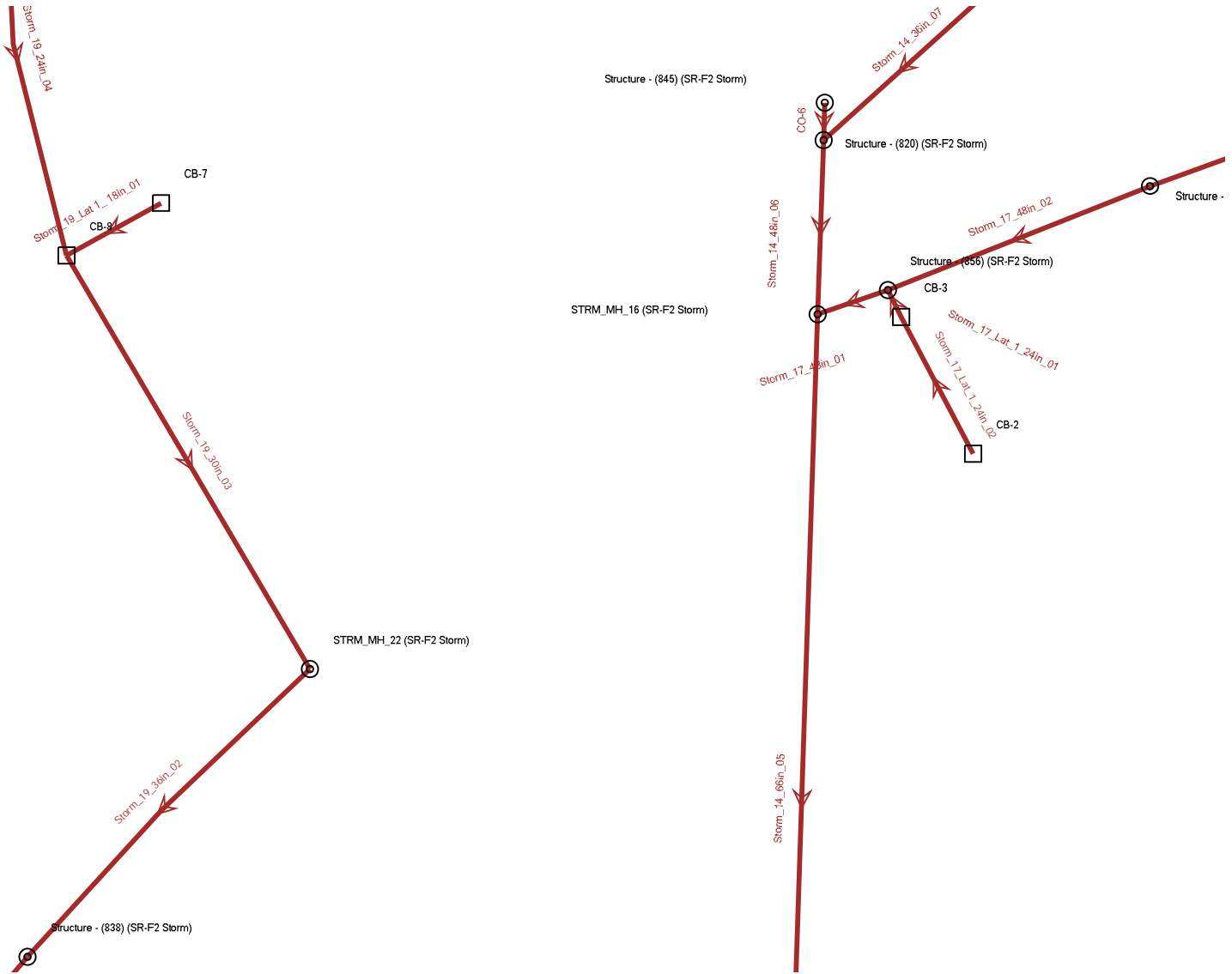
Sterling Ranch 5yr



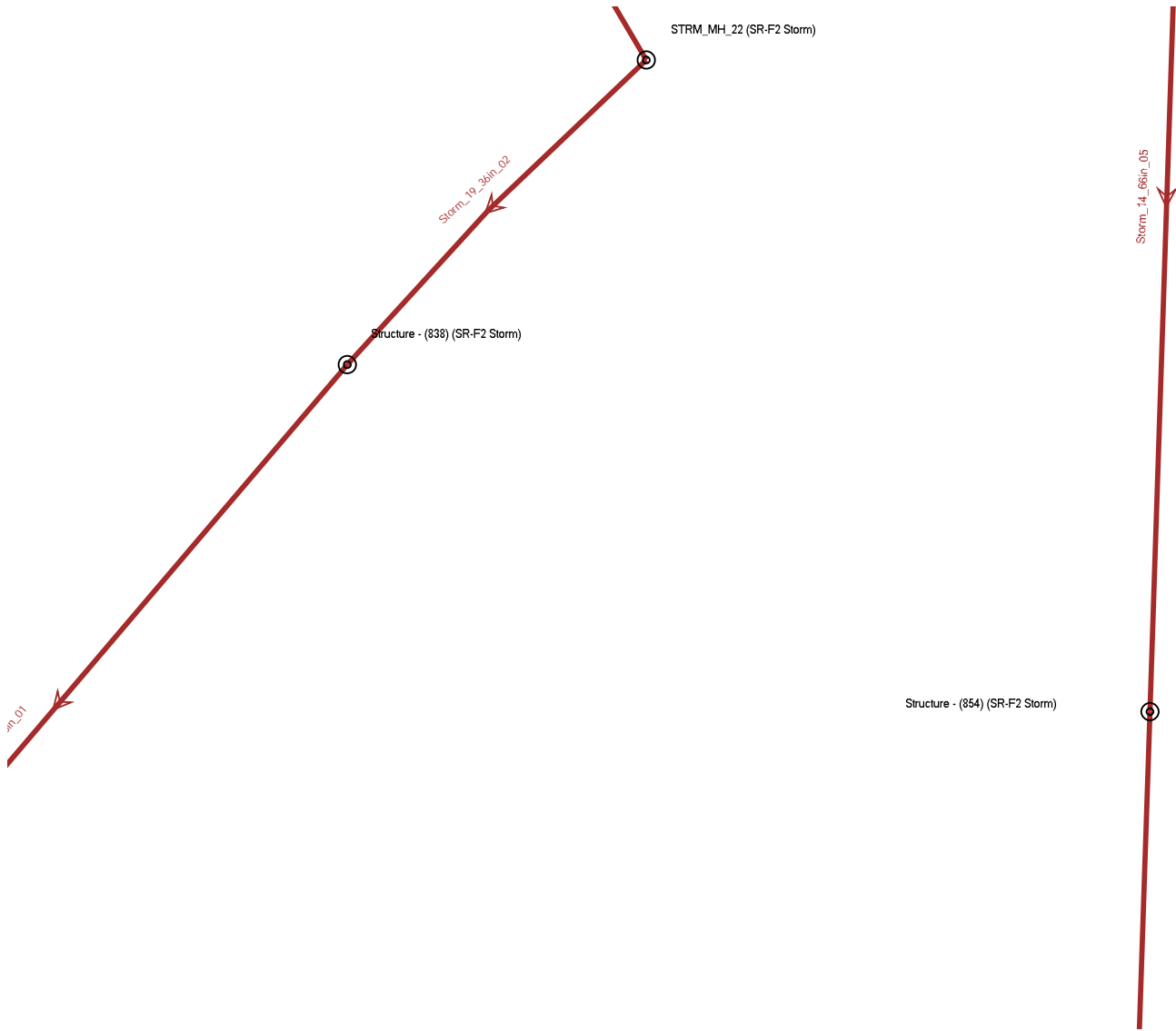
Sterling Ranch 5yr



Sterling Ranch 5yr



Sterling Ranch 5yr

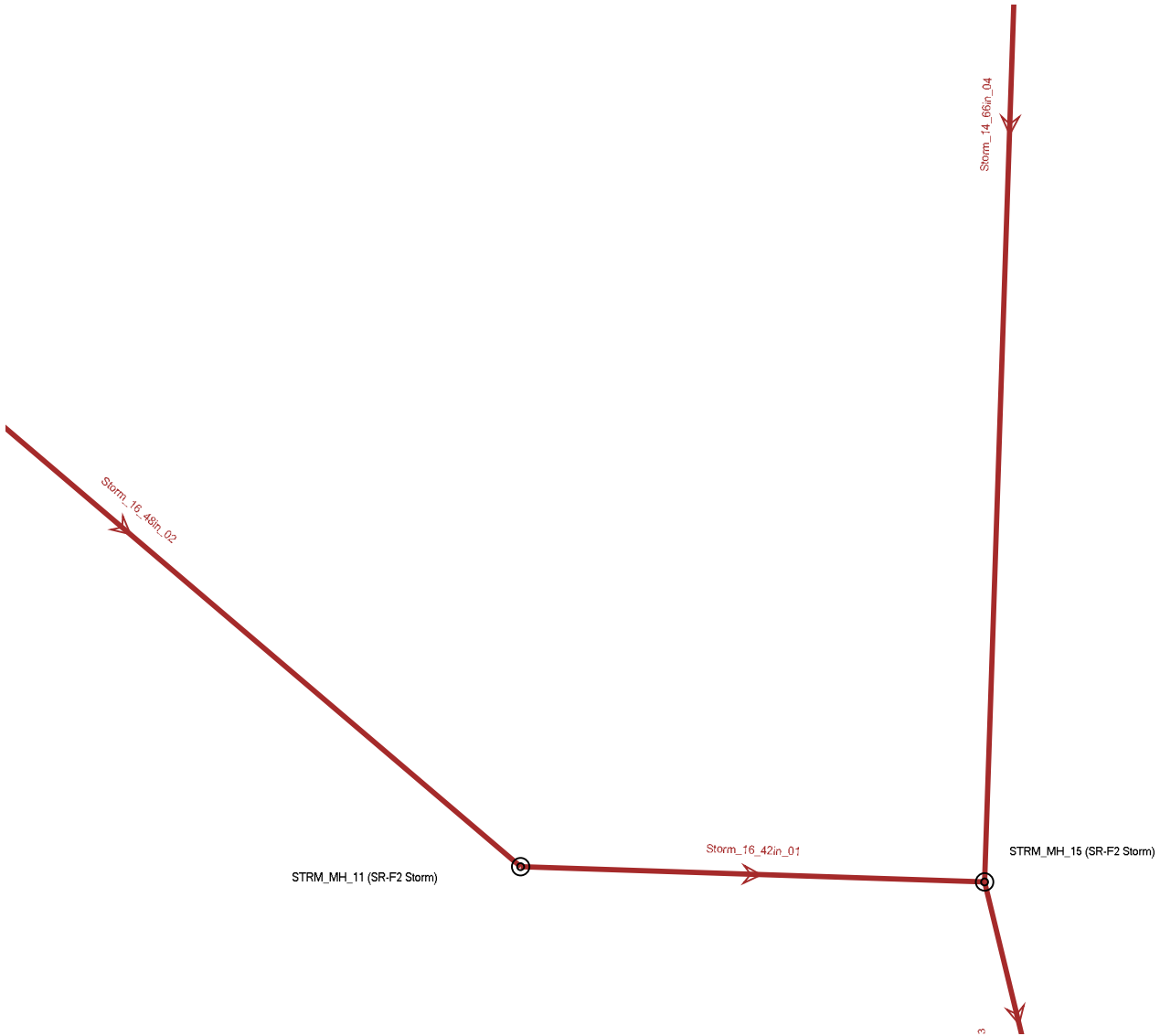


Sterling Ranch 5yr

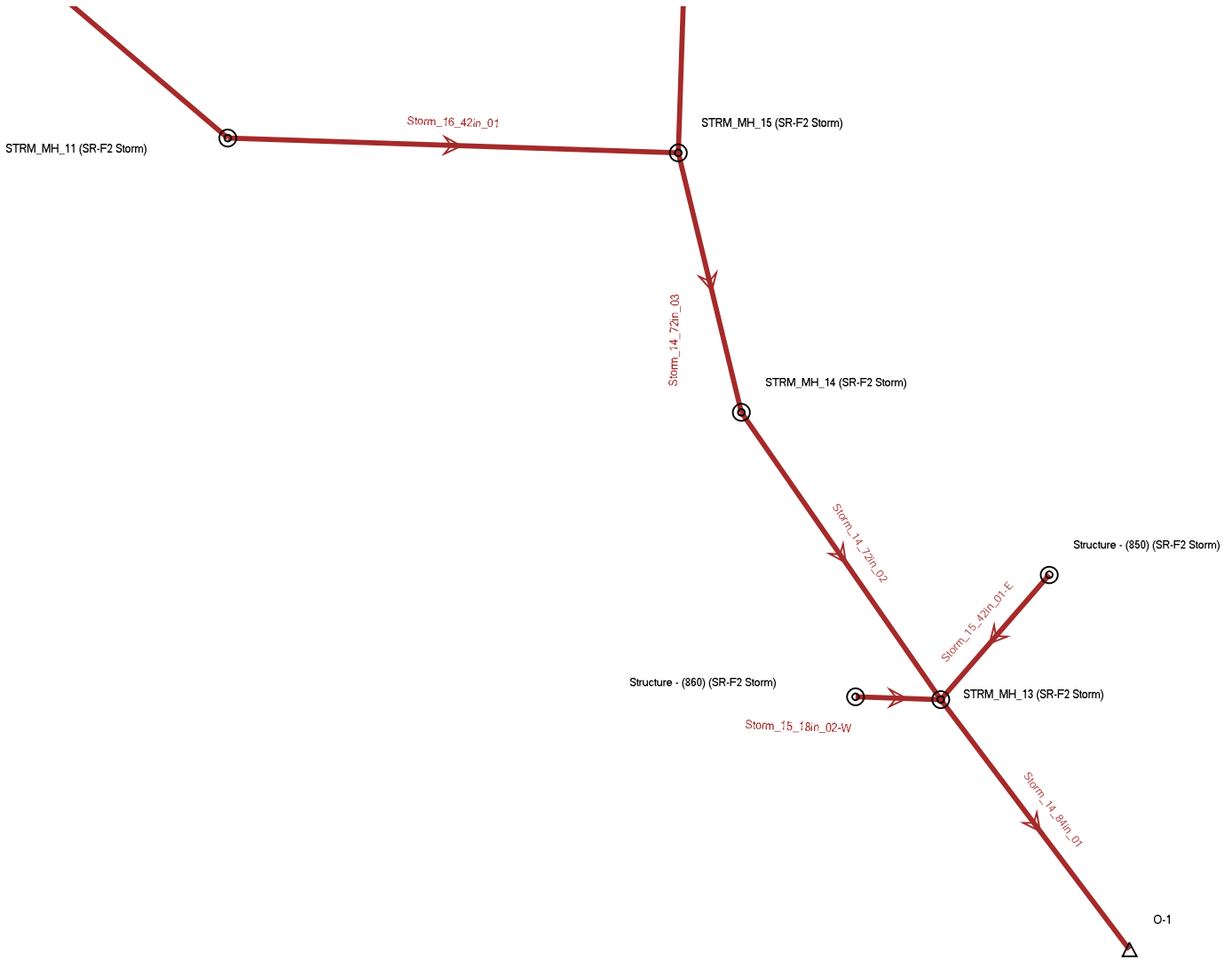
Structure - (854) (SR-F2 Storm)



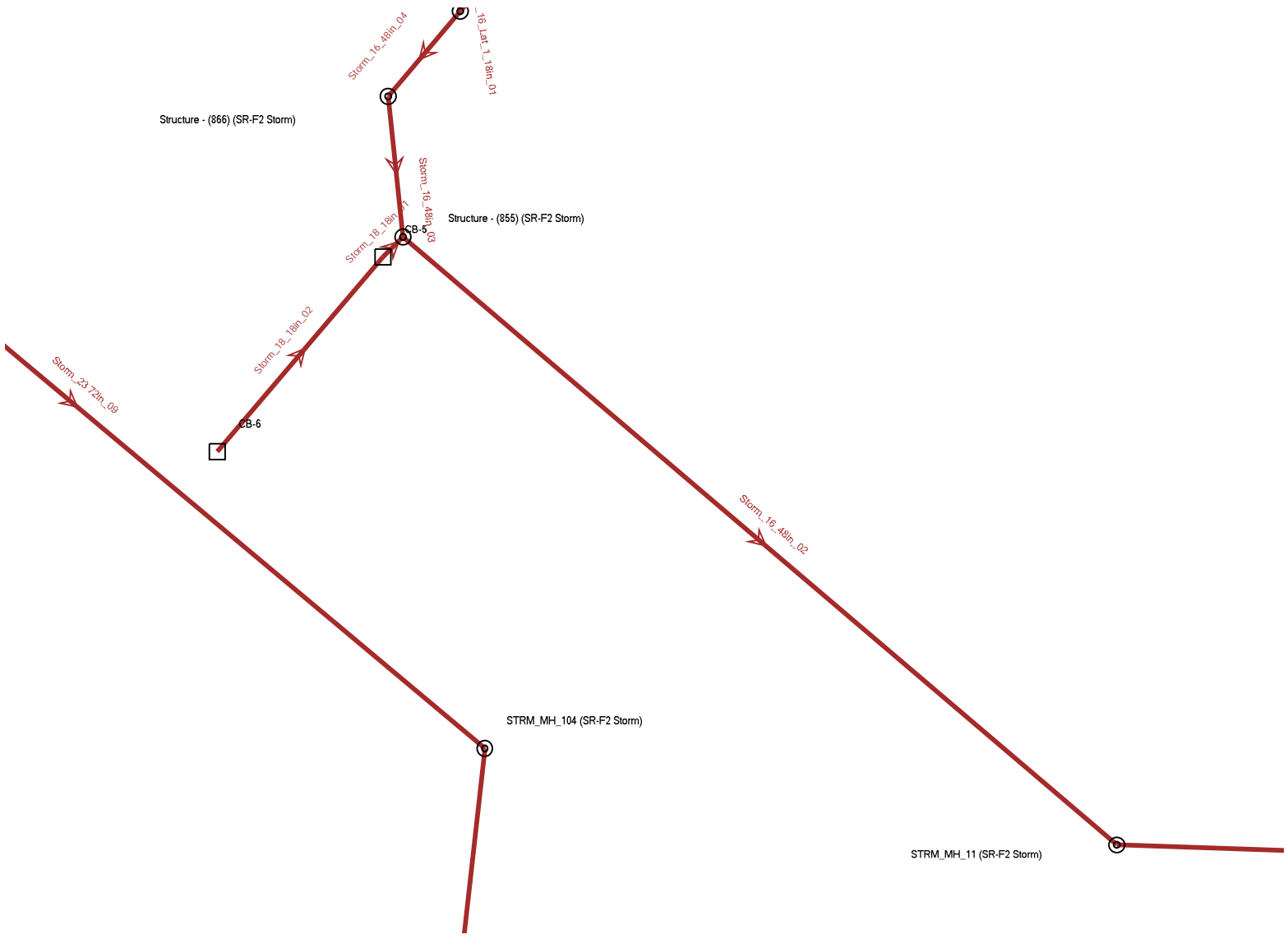
Sterling Ranch 5yr



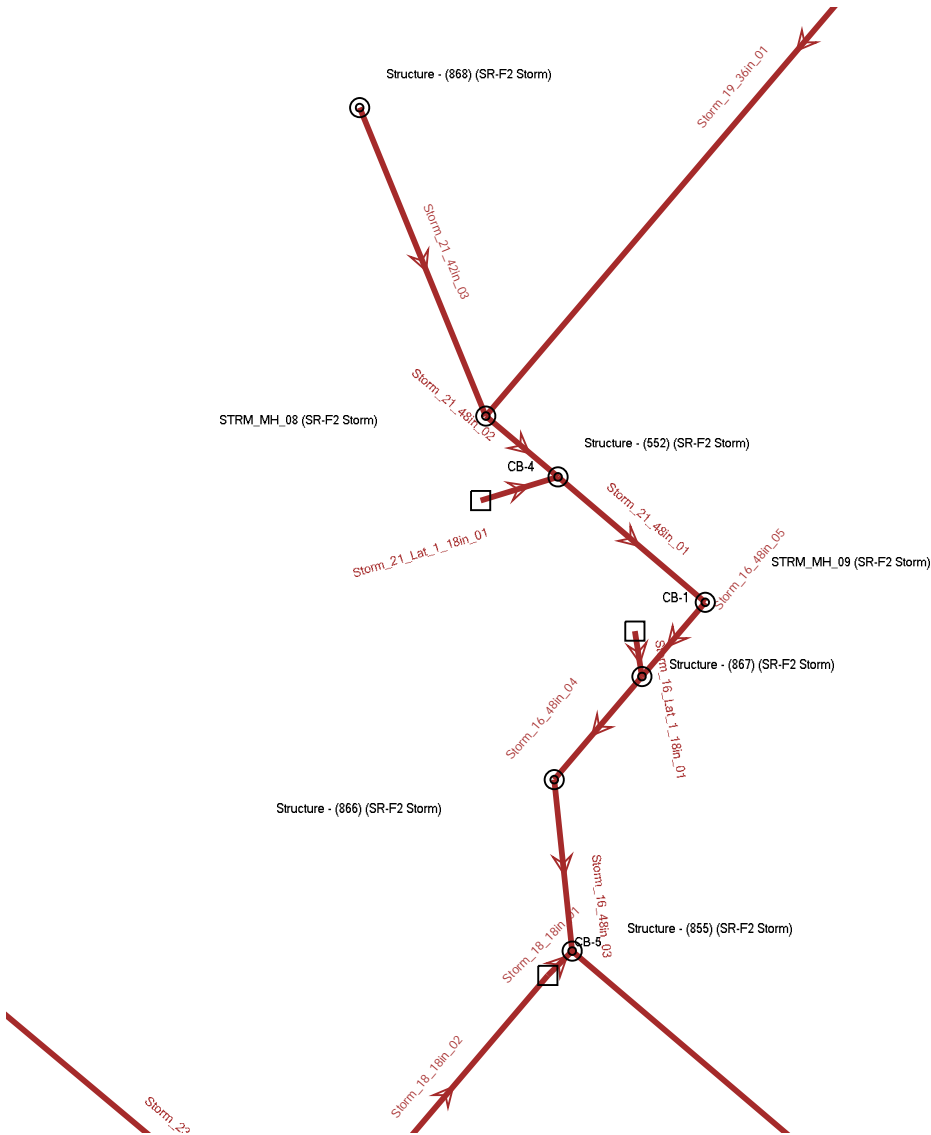
Sterling Ranch 5yr



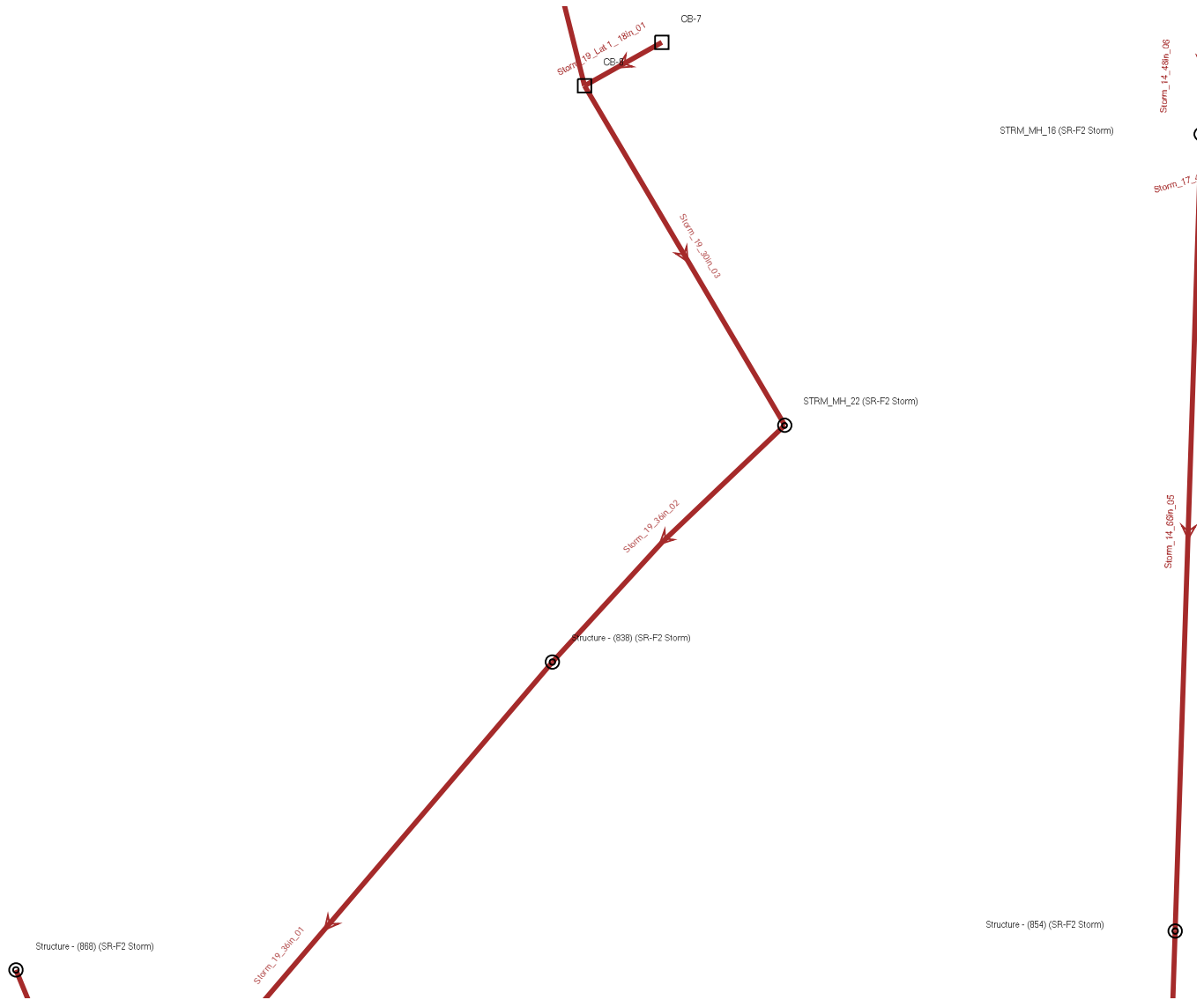
Sterling Ranch 5yr



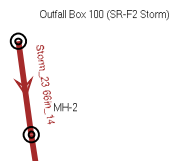
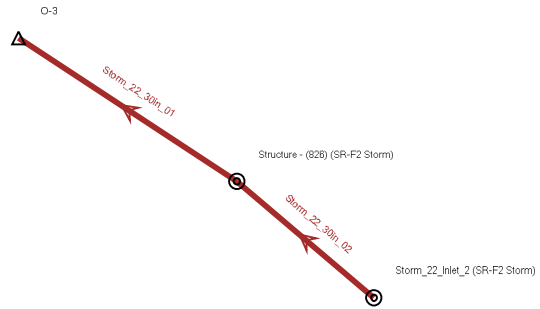
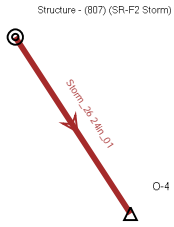
Sterling Ranch 5yr



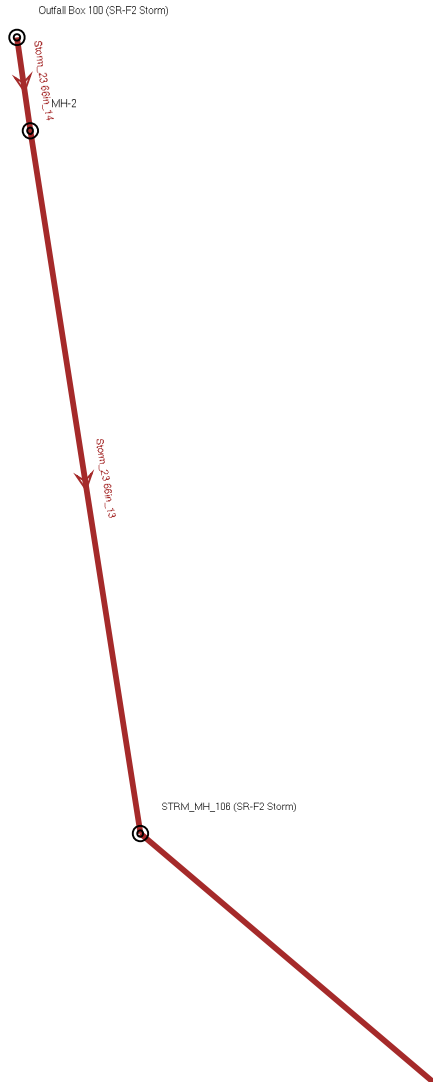
Sterling Ranch 5yr



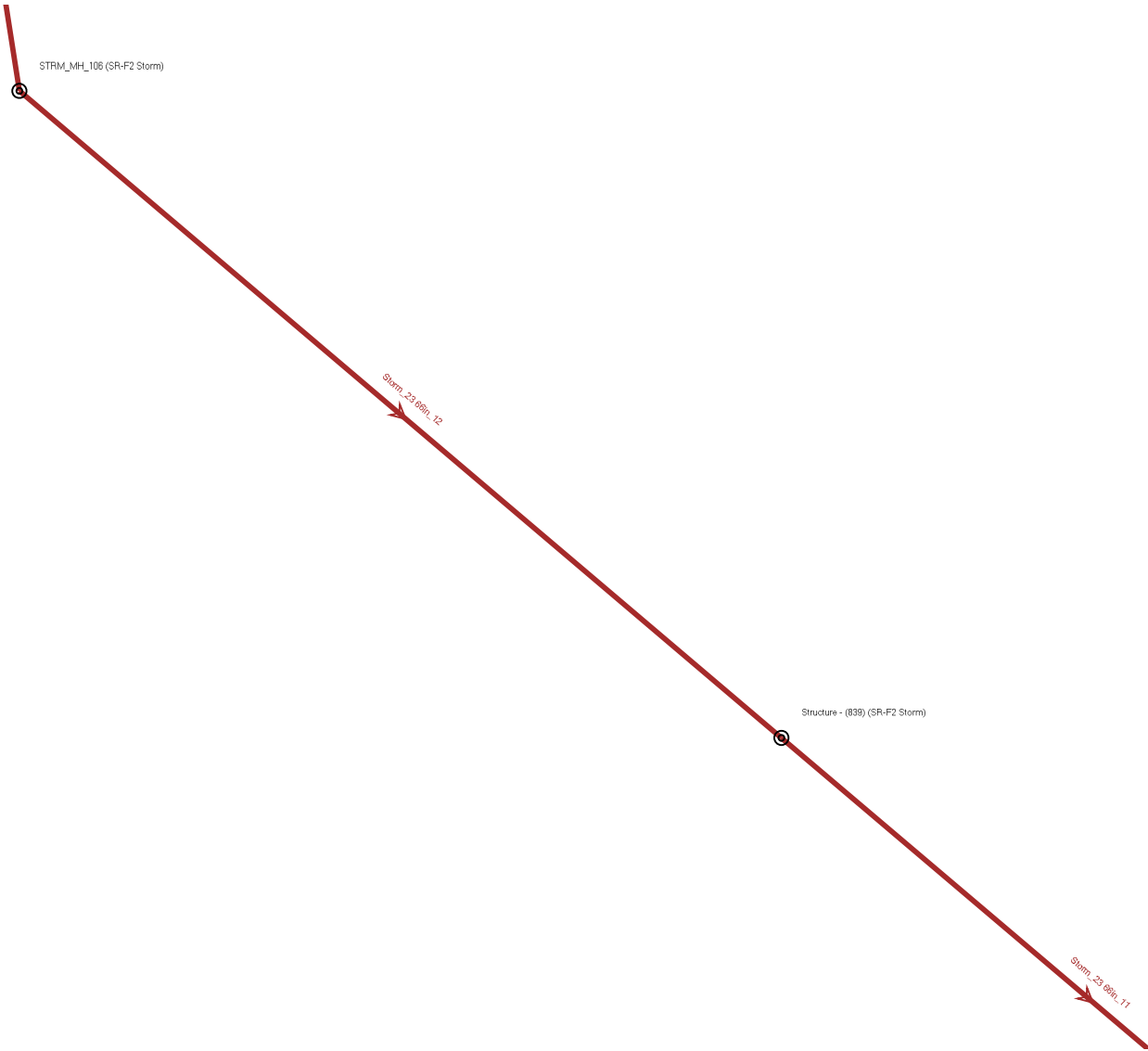
Sterling Ranch 5yr



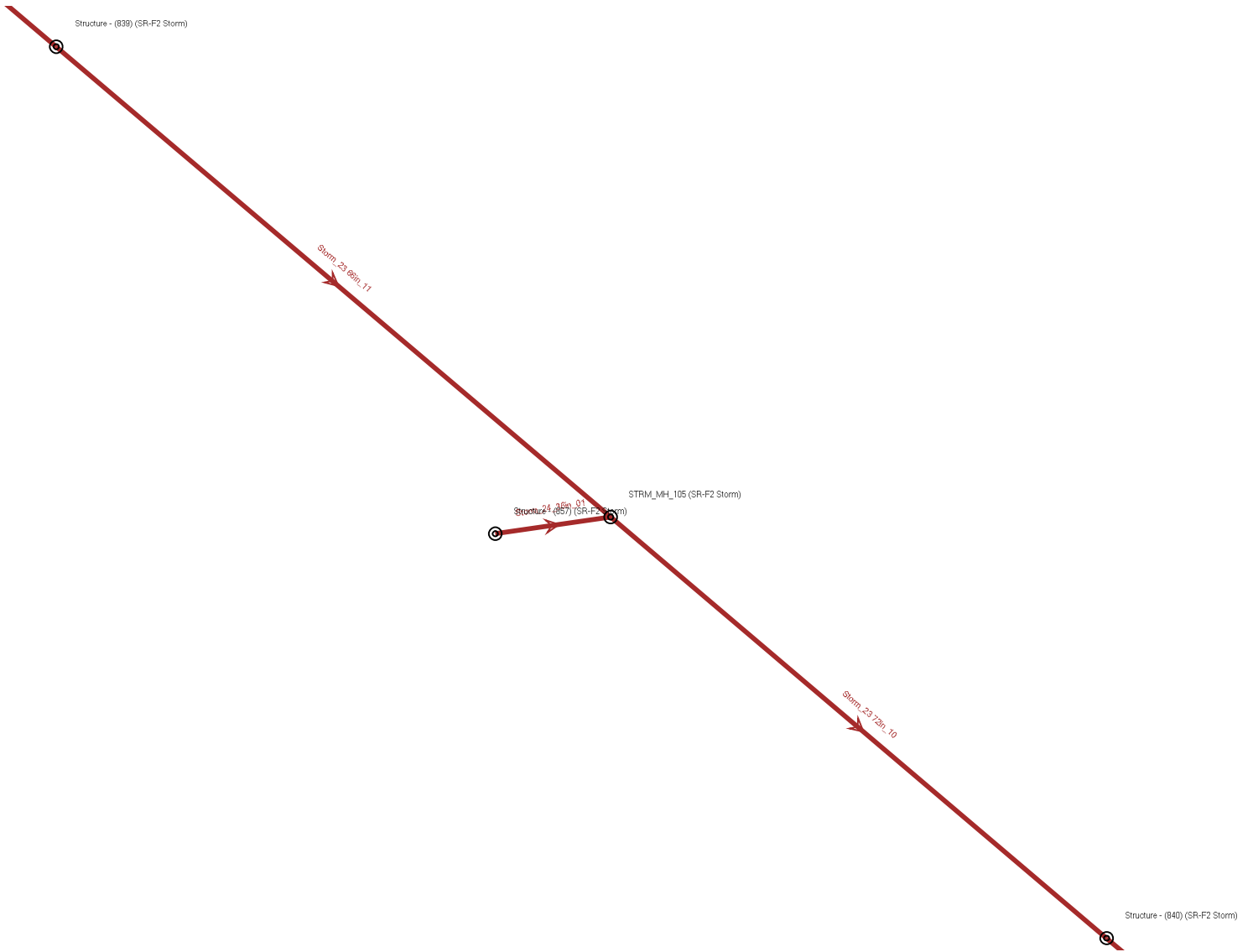
Sterling Ranch 5yr



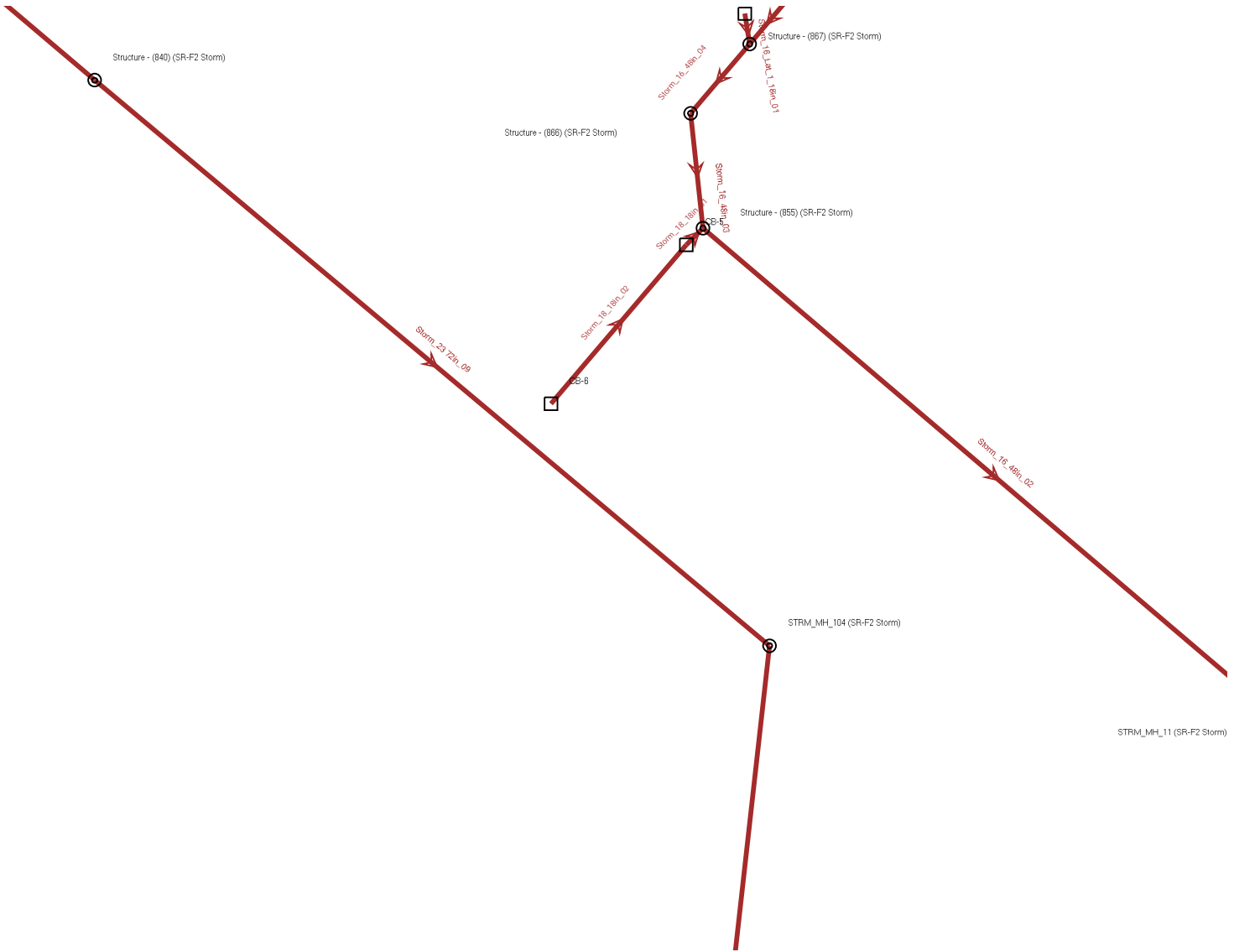
Sterling Ranch 5yr



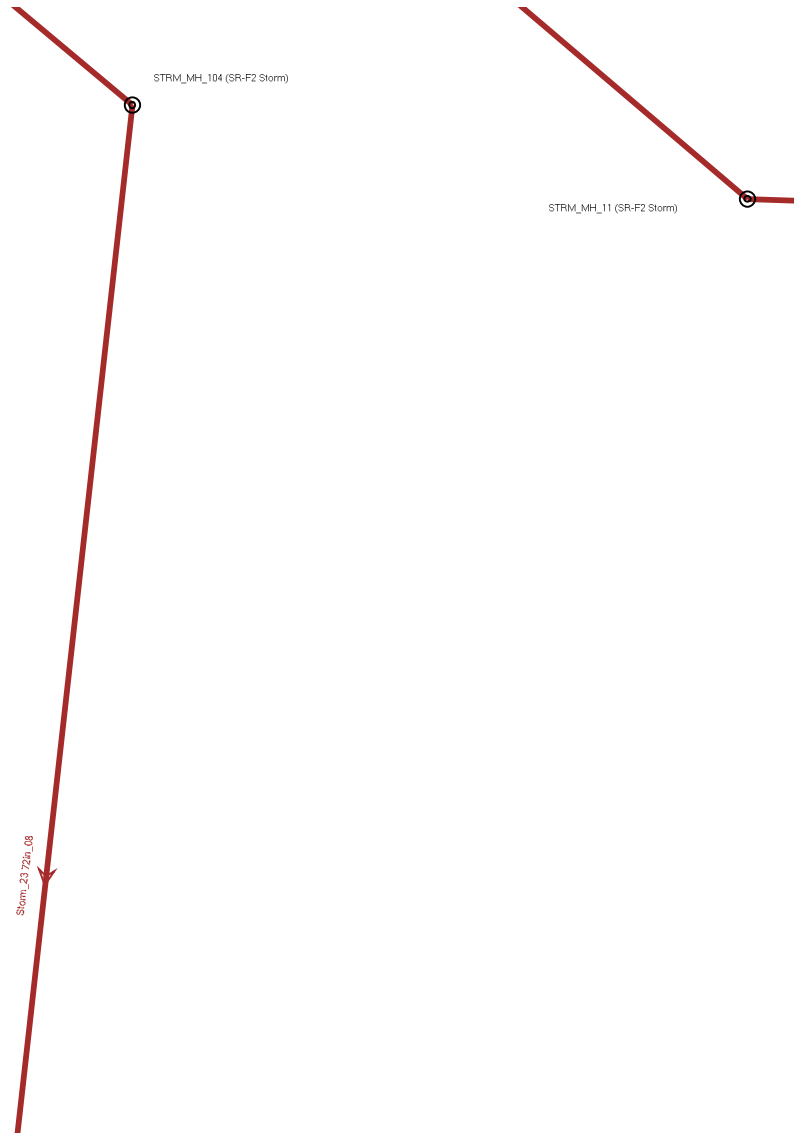
Sterling Ranch 5yr



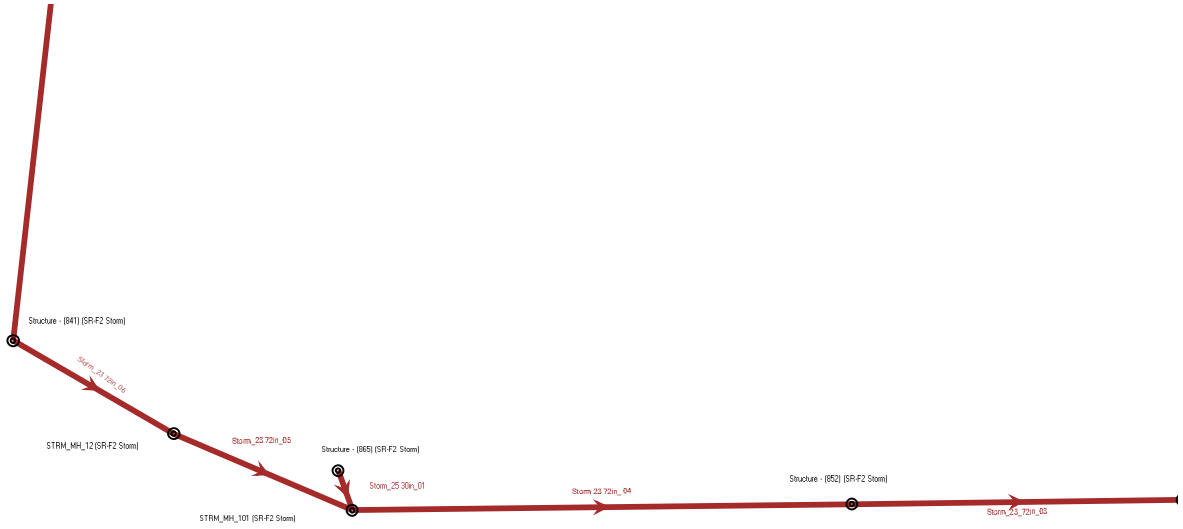
Sterling Ranch 5yr



Sterling Ranch 5yr



Sterling Ranch 5yr



Sterling Ranch 5yr



Sterling Ranch 5yr



Scenario: 5-YEAR
Current Time Step: 0.000 h
FlexTable: Conduit Table

ID	Label	Start Node	Set Invert to Start?	Invert (Start) (ft)	Stop Node	Set Invert to Stop?	Invert (Stop) (ft)	Has User Defined Length?	Length (User Defined) (ft)	Length (Scaled) (ft)	Slope (Calculated) (ft/ft)	Section Type	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Depth (Normal) / Rise (%)	Notes
109	Storm_28_30in_01	O-5	False	7,042.60	VT2_Inlet_3 (SR-F2 Storm)	False	7,042.47	True	35.4	36.9	0.004	Circle	30.0	0.013	18.40	3.75	1.45	24.92	73.8	(N/A)	30' RCP
115	Storm_26_24in_01	O-4	False	7,016.00	Structure - (807) (SR-F2 Storm)	False	7,016.81	True	80.7	82.6	-0.010	Circle	24.0	0.013	2.10	4.50	0.41	22.61	9.3	20.6	24' RCP
116	Storm_22_30in_02	Storm_22_Inlet_2 (SR-F2 Storm)	False	7,015.99	Structure - (826) (SR-F2 Storm)	False	7,015.30	True	68.8	70.3	0.010	Circle	30.0	0.013	8.30	6.55	1.41	41.01	20.2	30.5	30' RCP
117	Storm_22_30in_01	O-3	False	7,014.17	Structure - (826) (SR-F2 Storm)	False	7,015.09	True	100.7	102.2	-0.009	Circle	30.0	0.013	16.00	7.56	1.11	39.07	40.9	44.6	30' RCP
118	Storm_19_Lat_3_18in_02	STRM_MH_24 (SR-F2 Storm)	False	7,015.25	CB-12	False	7,015.84	True	29.3	30.8	-0.020	Circle	18.0	0.013	1.90	5.79	1.15	14.90	12.8	24.1	18' RCP
119	Storm_19_Lat_3_18in_01	CB-13	False	7,015.37	STRM_MH_24 (SR-F2 Storm)	False	7,015.25	True	6.0	7.5	0.020	Circle	18.0	0.013	4.20	7.22	1.15	14.84	28.3	36.4	18' RCP
120	Storm_19_18in_06	STRM_MH_23 (SR-F2 Storm)	False	7,001.54	STRM_MH_24 (SR-F2 Storm)	False	7,015.05	True	339.5	339.4	-0.040	Circle	18.0	0.013	6.00	10.23	1.38	20.95	28.6	36.6	18' RCP
122	Storm_23_66in_12	Structure - (839) (SR-F2 Storm)	False	6,994.77	STRM_MH_106 (SR-F2 Storm)	False	7,000.50	True	409.4	421.7	-0.014	Circle	66.0	0.013	37.80	10.54	1.15	397.26	9.5	20.8	66' RCP
123	Storm_17_48in_06	Structure - (862) (SR-F2 Storm)	False	6,998.16	STRM_MH_FUTR_02 (SR-F2 Storm)	False	6,998.61	True	22.6	25.0	-0.020	Circle	48.0	0.013	56.90	13.86	2.73	202.98	28.0	36.2	48' RCP
124	Storm_17_36in_07	STRM_MH_FUTR_02 (SR-F2 Storm)	False	6,999.61	Structure - (861) (SR-F2 Storm)	False	6,999.81	True	9.8	15.0	-0.020	Circle	36.0	0.013	17.60	10.21	1.73	94.31	18.7	29.3	36' RCP
125	Storm_19_Lat_2_18in_01	STRM_MH_23 (SR-F2 Storm)	False	7,001.54	CB-11	False	7,005.27	True	76.7	81.4	-0.049	Circle	18.0	0.013	12.60	13.29	1.38	23.16	54.4	52.6	18' RCP
126	Storm_19_24in_05	Structure - (842) (SR-F2 Storm)	False	6,995.73	STRM_MH_23 (SR-F2 Storm)	False	7,001.04	True	177.0	176.9	-0.030	Circle	24.0	0.013	17.60	12.14	0.94	39.18	44.9	47.0	24' RCP
127	Storm_23_66in_11	STRM_MH_105 (SR-F2 Storm)	False	6,987.91	Structure - (839) (SR-F2 Storm)	False	6,992.57	True	333.0	339.2	-0.014	Circle	66.0	0.013	37.80	10.54	1.15	397.25	9.5	20.8	66' RCP
128	Storm_17_48in_05	STRM_MH_20 (SR-F2 Storm)	False	6,992.31	STRM_MH_20 (SR-F2 Storm)	False	6,998.16	True	292.3	294.4	-0.020	Circle	48.0	0.013	56.90	13.87	2.31	203.11	28.0	36.2	48' RCP
129	Storm_17_48in_04	Structure - (863) (SR-F2 Storm)	False	6,990.79	STRM_MH_20 (SR-F2 Storm)	False	6,992.12	True	82.9	85.2	-0.016	Circle	48.0	0.013	56.90	12.80	2.50	181.90	31.3	38.4	48' RCP
130	Storm_24_36in_01	STRM_MH_105 (SR-F2 Storm)	False	6,990.41	Structure - (857) (SR-F2 Storm)	False	6,991.42	True	50.2	54.3	-0.020	Circle	36.0	0.013	2.00	5.39	0.30	94.58	2.1	10.1	36' RCP
131	Storm_23_72in_10	Structure - (840) (SR-F2 Storm)	False	6,981.00	STRM_MH_105 (SR-F2 Storm)	False	6,985.13	True	295.1	303.6	-0.014	Circle	72.0	0.013	43.30	10.86	1.19	501.04	8.6	19.9	72' RCP
132	Storm_19_Lat_1_18in_01	CB-8	False	6,991.89	CB-7	False	6,992.98	True	36.4	39.4	-0.030	Circle	18.0	0.013	5.00	8.78	1.13	18.18	27.5	35.8	18' RCP
134	Storm_19_24in_04	CB-8	False	6,991.39	Structure - (842) (SR-F2 Storm)	False	6,995.73	True	144.7	151.8	-0.030	Circle	24.0	0.013	0.50	4.31	1.63	39.18	1.3	7.9	24' RCP
135	Storm_19_30in_03	STRM_MH_22 (SR-F2 Storm)	False	6,986.85	CB-8	False	6,990.89	True	165.0	175.2	-0.024	Circle	30.0	0.013	25.90	12.37	1.81	64.17	40.4	44.2	30' RCP
136	Storm_17_48in_03	Structure - (864) (SR-F2 Storm)	False	6,988.37	Structure - (863) (SR-F2 Storm)	False	6,990.79	True	150.3	150.2	-0.016	Circle	48.0	0.013	56.90	12.82	2.50	182.25	31.2	38.4	48' RCP
137	Storm_17_48in_02	Structure - (856) (SR-F2 Storm)	False	6,986.77	Structure - (864) (SR-F2 Storm)	False	6,988.37	True	102.0	102.8	-0.016	Circle	48.0	0.013	56.90	12.70	2.46	179.90	31.6	38.6	48' RCP
138	Storm_17_48in_01	STRM_MH_16 (SR-F2 Storm)	False	6,986.46	Structure - (856) (SR-F2 Storm)	False	6,986.57	True	23.0	27.1	-0.005	Circle	48.0	0.013	63.70	8.38	2.34	99.25	64.2	58.3	48' RCP
139	Storm_17_Lat_1_24in_01	Structure - (856) (SR-F2 Storm)	False	6,988.57	CB-3	False	6,988.62	True	8.8	11.0	-0.006	Circle	24.0	0.013	9.60	5.58	1.08	17.03	56.4	53.7	24' RCP
140	Storm_17_Lat_1_24in_02	CB-3	False	6,988.62	CB-2	False	6,988.97	True	53.4	56.3	-0.007	Circle	24.0	0.013	4.30	4.76	1.22	18.29	23.5	33.0	24' RCP
141	Storm_14_48in_06	STRM_MH_16 (SR-F2 Storm)	False	6,986.46	Structure - (820) (SR-F2 Storm)	False	6,987.48	True	59.3	63.6	-0.017	Circle	48.0	0.013	38.10	11.72	1.33	187.87	20.3	30.5	48' RCP
142	Storm_14_66in_05	Structure - (854) (SR-F2 Storm)	False	6,976.45	STRM_MH_16 (SR-F2 Storm)	False	6,981.41	True	354.4	354.4	-0.014	Circle	66.0	0.013	96.60	13.79	1.85	397.24	24.3	33.6	66' RCP
143	Storm_19_36in_02	Structure - (838) (SR-F2 Storm)	False	6,985.50	STRM_MH_22 (SR-F2 Storm)	False	6,986.35	True	144.5	147.2	-0.006	Circle	36.0	0.013	25.90	7.26	1.98	51.15	50.6	50.4	36' RCP
144	Storm_14_36in_07	Structure - (820) (SR-F2 Storm)	False	6,988.48	Structure - (858) (SR-F2 Storm)	False	6,990.00	True	76.3	79.6	-0.020	Circle	36.0	0.013	15.70	9.89	0.85	94.31	16.6	27.6	36' RCP
145	Storm_23_72in_09	STRM_MH_104 (SR-F2 Storm)	False	6,971.95	Structure - (840) (SR-F2 Storm)	False	6,977.58	True	402.6	410.7	-0.014	Circle	72.0	0.013	43.30	10.85	1.19	500.84	8.6	19.9	72' RCP
146	Storm_21_48in_01	STRM_MH_09 (SR-F2 Storm)	False	6,980.28	Structure - (552) (SR-F2 Storm)	False	6,982.00	True	57.3	60.5	-0.030	Circle	48.0	0.013	55.10	15.91	1.47	248.76	22.1	32.0	48' RCP
147	Storm_16_48in_05	Structure - (867) (SR-F2 Storm)	False	6,978.77	STRM_MH_09 (SR-F2 Storm)	False	6,979.31	True	26.8	30.5	-0.020	Circle	48.0	0.013	55.10	13.74	2.72	203.11	27.1	35.6	48' RCP
148	Storm_21_42in_03	STRM_MH_08 (SR-F2 Storm)	False	6,983.49	Structure - (868) (SR-F2 Storm)	False	6,984.00	True	101.2	104.4	-0.005	Circle	42.0	0.013	27.50	6.92	2.33	71.15	38.6	43.1	42' RCP
149	Storm_19_36in_01	STRM_MH_08 (SR-F2 Storm)	False	6,983.73	Structure - (838) (SR-F2 Storm)	False	6,985.50	True	302.2	306.4	-0.006	Circle	36.0	0.013	25.90	7.25	2.10	51.04	50.7	50.4	36' RCP
150	Storm_21_48in_02	Structure - (552) (SR-F2 Storm)	False	6,982.00	STRM_MH_08 (SR-F2 Storm)	False	6,982.77	True	25.8	29.5	-0.030	Circle	48.0	0.013	52.50	15.69	2.69	248.66	21.1	31.2	48' RCP
151	Storm_21_Lat_1_18in_01	Structure - (552) (SR-F2 Storm)	False	6,984.49	CB-4	False	6,984.58	True	19.4	25.2	-0.005	Circle	18.0	0.013	3.00	3.87	0.66	7.16	41.9	45.1	18' RCP
152	Storm_16_Lat_1_18in_01	Structure - (867) (SR-F2 Storm)	False	6,981.26	CB-1	False	6,981.53	True	13.2	14.3	-0.020	Circle	18.0	0.013	2.10	5.99	0.41	15.01	14.0	25.3	18' RCP
153	Storm_16_48in_02	STRM_MH_11 (SR-F2 Storm)	False	6,968.32	Structure - (855) (SR-F2 Storm)	False	6,976.52	True	348.6	357.0	-0.024	Circle	48.0	0.013	68.80	15.49	4.07	220.31	31.2	38.4	48' RCP
154	Storm_16_48in_03	Structure - (855) (SR-F2 Storm)	False	6,976.91	Structure - (866) (SR-F2 Storm)	False	6,977.92	True	50.4	53.9	-0.020	Circle	48.0	0.013	56.40	13.85	2.65	203.42	27.7	36.0	48' RCP
155	Storm_18_18in_02	CB-5	False	6,980.25	CB-6	False	6,984.78	True	94.4	97.3	-0.048	Circle	18.0	0.013	8.70	12.12	0.64	23.01	37.8	42.6	18' RCP
156	Storm_14_66in_04	STRM_MH_15 (SR-F2 Storm)	False	6,968.14	Structure - (854) (SR-F2 Storm)	False	6,974.25	True	512.4	518.6	-0.012	Circle	66.0	0.013	96.60	13.02	3.96	366.67	26.3	35.0	66' RCP
157	Storm_23_72in_08	Structure - (841) (SR-F2 Storm)	False	6,961.25	STRM_MH_104 (SR-F2 Storm)	False	6,969.23	True	602.8	608.9	-0.013	Circle	72.0	0.013	43.30	10.64	1.21	487.25	8.9	20.1	72' RCP
159	Storm_16_42in_01	STRM_MH_11 (SR-F2 Storm)	False	6,967.89	STRM_MH_15 (SR-F2 Storm)	False	6,967.57	True	158.3	158.9	0.002	Circle	42.0	0.013	68.80	3.58	4.53	90.47	76.0	65.3	42' RCP
160	Storm_16_48in_04	Structure - (866) (SR-F2 Storm)	False	6,977.92	Structure - (867) (SR-F2 Storm)	False	6,978.77	True	42.5	42.5	-0.020	Circle	48.0	0.013	56.40	13.83	2.72	203.12	27.8	36.0	48' RCP
161	Storm_14_72in_03	STRM_MH_14 (SR-F2 Storm)	False	6,967.18	STRM_MH_15 (SR-F2 Storm)	False	6,967.57	True	74.5	94.3	-0.005	Circle	72.0	0.013	162.00	10.99	3.82	306.40	52.9	51.7	72' RCP
162	Storm_14_72in_02	STRM_MH_13 (SR-F2 Storm)	False	6,966.54	STRM_MH_14 (SR-F2 Storm)	False	6,967.18	True	127.9	123.3	-0.005	Circle	72.0	0.013	162.00	10.80	3.94	299.58	54.1	52.4	72' RCP
163	Storm_15_18in_02-W	STRM_MH_13 (SR-F2 Storm)	False	6,971.54	Structure - (860) (SR-F2 Storm)	False	6,972.80	True	25.5	30.0	-0.049	Circle	18.0	0.013	4.30	10.08	0.47	23.36	18.4	29.1	18' RCP
164	Storm_14_84in_01	O-1	False	6,966.00	STRM_MH_13 (SR-F2 Storm)	False	6,966.54	True	107.3	110.6	-0.005	Circle	84.0	0.013	189.80	11.25	3.23	453.09	41.9	45.1	84' RCP
165	Storm_20_48in_01	Structure - (793) (SR-F2 Storm)	False	6,948.88	Storm_20_Outfall (SR-F2 Storm)	False	6,949.67	True	57.9	64.1	-0.014	Circle	48.0	0.013	0.00	0.00	0.00	167.45	0.0	(N/A)	48' RCP
166	Storm_23_84in_01	O-2	False	6,945.31	Structure - (793) (SR-F2 Storm)	False	6,945.97	True	222.1	226.6	-0.003	Circle	84.0	0.013	46.50	6.31	1.73	349.27	13.3	24.6	84' RCP
167	Storm_23_72in_02	Structure - (793) (SR-F2 Storm)	False	6,946.97	STRM_MH_102 (SR-F2 Storm)	False	6,948.62	True	549.0	560.5	-0.003	Circle	72.0	0.013	45.20	6.36	1.78	232.16	19.5	29.9	72' RCP
169	Storm_23_72in_05	STRM_MH_101 (SR-F2 Storm)	False	6,954.29	STRM_MH_12 (SR-F2 Storm)	False	6,956.09	True	120.0	104.1	-0.015	Circle	72.0	0.013	43.30	11.13	1.21	518.77	8.3	19.5	72' RCP
170	Storm_25_30in_01	Structure - (865) (SR-F2 Storm)	False	6,955.17	STRM_MH_101 (SR-F2 Storm)	False	6,952.68	True	23.6	22.6	0.105	Circle	30.0	0.013	1.40	8.85	0.18	133.22	1.1	7.2	30' RCP
172	Storm_23_72in_03	STRM_MH_102 (SR-F2 Storm)	False	6,948																	

Scenario: 100-YEAR
Current Time Step: 0.000 h
FlexTable: Conduit Table

ID	Label	Start Node	Set Invert to Start?	Invert (Start) (ft)	Stop Node	Set Invert to Stop?	Invert (Stop) (ft)	Has User Defined Length?	Length (User Defined) (ft)	Length (Scaled) (ft)	Slope (Calculated) (ft/ft)	Section Type	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Depth (Normal) / Rise (%)	Notes
109	Storm_28_30in_01	O-5	False	7,042.60	VT2_Inlet_3 (SR-F2 Storm)	False	7,042.47	True	35.4	36.9	0.004	Circle	30.0	0.013	26.10	5.32	1.74	24.92	104.8	(N/A)	30' RCP
115	Storm_26_24in_01	O-4	False	7,016.00	Structure - (807) (SR-F2 Storm)	False	7,016.81	True	80.7	82.6	-0.010	Circle	24.0	0.013	14.50	4.62	5.67	22.61	64.1	58.2	24' RCP
116	Storm_22_30in_02	Storm_22_Inlet_2 (SR-F2 Storm)	False	7,015.99	Structure - (826) (SR-F2 Storm)	False	7,015.30	True	68.8	70.3	0.010	Circle	30.0	0.013	14.40	2.93	7.25	41.01	35.1	40.9	30' RCP
117	Storm_22_30in_01	O-3	False	7,014.17	Structure - (826) (SR-F2 Storm)	False	7,015.09	True	100.7	102.2	-0.009	Circle	30.0	0.013	31.00	6.32	7.50	39.07	79.3	67.2	30' RCP
118	Storm_19_Lat_3_18in_02	STRM_MH_24 (SR-F2 Storm)	False	7,015.25	CB-12	False	7,015.84	True	29.3	30.8	-0.020	Circle	18.0	0.013	3.80	7.05	1.72	14.90	25.5	34.4	18' RCP
119	Storm_19_Lat_3_18in_01	CB-13	False	7,015.37	STRM_MH_24 (SR-F2 Storm)	False	7,015.25	True	6.0	7.5	0.020	Circle	18.0	0.013	6.60	3.73	1.72	14.84	44.5	46.7	18' RCP
120	Storm_19_18in_06	STRM_MH_23 (SR-F2 Storm)	False	7,001.54	STRM_MH_24 (SR-F2 Storm)	False	7,015.05	True	339.5	339.4	-0.040	Circle	18.0	0.013	10.30	11.81	2.12	20.95	49.2	49.5	18' RCP
122	Storm_23_66in_12	Structure - (839) (SR-F2 Storm)	False	6,994.77	STRM_MH_106 (SR-F2 Storm)	False	7,000.50	True	409.4	421.7	-0.014	Circle	66.0	0.013	270.70	17.99	3.38	397.26	68.1	60.6	66' RCP
123	Storm_17_48in_06	Structure - (862) (SR-F2 Storm)	False	6,998.16	STRM_MH_FUTR_02 (SR-F2 Storm)	False	6,998.61	True	22.6	25.0	-0.020	Circle	48.0	0.013	138.70	11.04	4.60	202.98	68.3	60.7	48' RCP
124	Storm_17_36in_07	STRM_MH_FUTR_02 (SR-F2 Storm)	False	6,999.61	Structure - (861) (SR-F2 Storm)	False	6,999.81	True	9.8	15.0	-0.020	Circle	36.0	0.013	48.90	6.92	4.30	94.31	51.8	51.1	36' RCP
125	Storm_19_Lat_2_18in_01	STRM_MH_23 (SR-F2 Storm)	False	7,001.54	CB-11	False	7,005.27	True	76.7	81.4	-0.049	Circle	18.0	0.013	19.70	14.72	2.12	23.16	85.0	70.8	18' RCP
126	Storm_19_24in_05	Structure - (842) (SR-F2 Storm)	False	6,995.73	STRM_MH_23 (SR-F2 Storm)	False	7,001.04	True	177.0	176.9	-0.030	Circle	24.0	0.013	30.00	13.74	1.31	39.18	76.6	65.6	24' RCP
127	Storm_23_66in_11	STRM_MH_105 (SR-F2 Storm)	False	6,987.91	Structure - (839) (SR-F2 Storm)	False	6,992.57	True	333.0	339.2	-0.014	Circle	66.0	0.013	270.70	17.99	3.42	397.25	68.1	60.6	66' RCP
128	Storm_17_48in_05	STRM_MH_20 (SR-F2 Storm)	False	6,992.31	Structure - (862) (SR-F2 Storm)	False	6,998.16	True	292.3	294.4	-0.020	Circle	48.0	0.013	138.70	17.39	3.85	203.11	68.3	60.6	48' RCP
129	Storm_17_48in_04	Structure - (863) (SR-F2 Storm)	False	6,990.79	STRM_MH_20 (SR-F2 Storm)	False	6,992.12	True	82.9	85.2	-0.016	Circle	48.0	0.013	138.70	15.94	4.05	181.90	76.3	65.4	48' RCP
130	Storm_24_36in_01	STRM_MH_105 (SR-F2 Storm)	False	6,990.41	Structure - (857) (SR-F2 Storm)	False	6,991.42	True	50.2	54.3	-0.020	Circle	36.0	0.013	15.00	9.78	0.86	94.58	15.9	26.9	36' RCP
131	Storm_23_72in_10	Structure - (840) (SR-F2 Storm)	False	6,981.00	STRM_MH_105 (SR-F2 Storm)	False	6,985.13	True	295.1	303.6	-0.014	Circle	72.0	0.013	242.40	17.57	3.04	501.04	48.4	49.0	72' RCP
132	Storm_19_Lat_1_18in_01	CB-8	False	6,991.89	CB-7	False	6,992.98	True	36.4	39.4	-0.030	Circle	18.0	0.013	8.70	10.18	2.25	18.18	47.9	48.7	18' RCP
134	Storm_19_24in_04	CB-8	False	6,991.39	Structure - (842) (SR-F2 Storm)	False	6,995.73	True	144.7	151.8	-0.030	Circle	24.0	0.013	30.00	13.74	2.75	39.18	76.6	65.6	24' RCP
135	Storm_19_30in_03	STRM_MH_22 (SR-F2 Storm)	False	6,986.85	CB-8	False	6,990.89	True	165.0	175.2	-0.024	Circle	30.0	0.013	46.90	9.55	4.43	64.17	73.1	63.5	30' RCP
136	Storm_17_48in_03	Structure - (864) (SR-F2 Storm)	False	6,988.37	Structure - (863) (SR-F2 Storm)	False	6,990.79	True	150.3	150.2	-0.016	Circle	48.0	0.013	138.70	15.96	4.05	182.25	76.1	65.3	48' RCP
137	Storm_17_48in_02	Structure - (856) (SR-F2 Storm)	False	6,986.77	Structure - (864) (SR-F2 Storm)	False	6,988.37	True	102.0	102.8	-0.016	Circle	48.0	0.013	138.70	15.79	4.34	179.90	77.1	65.9	48' RCP
138	Storm_17_48in_01	STRM_MH_16 (SR-F2 Storm)	False	6,986.46	Structure - (856) (SR-F2 Storm)	False	6,986.57	True	23.0	27.1	-0.005	Circle	48.0	0.013	151.90	12.09	3.61	99.25	153.1	(N/A)	48' RCP
139	Storm_17_Lat_1_24in_01	Structure - (856) (SR-F2 Storm)	False	6,988.57	CB-3	False	6,988.62	True	8.8	11.0	-0.006	Circle	24.0	0.013	17.20	5.47	2.54	17.03	101.0	82.9	24' RCP
140	Storm_17_Lat_1_24in_02	CB-3	False	6,988.62	CB-2	False	6,988.97	True	53.4	56.3	-0.007	Circle	24.0	0.013	7.00	2.23	2.66	18.29	38.3	42.9	24' RCP
141	Storm_14_48in_06	STRM_MH_16 (SR-F2 Storm)	False	6,986.46	Structure - (820) (SR-F2 Storm)	False	6,987.48	True	59.3	63.6	-0.017	Circle	48.0	0.013	106.60	15.42	2.45	187.87	56.7	53.9	48' RCP
142	Storm_14_66in_05	Structure - (854) (SR-F2 Storm)	False	6,976.45	STRM_MH_16 (SR-F2 Storm)	False	6,981.41	True	354.4	354.4	-0.014	Circle	66.0	0.013	250.70	17.68	5.59	397.24	63.1	57.6	66' RCP
143	Storm_19_36in_02	Structure - (838) (SR-F2 Storm)	False	6,985.50	STRM_MH_22 (SR-F2 Storm)	False	6,986.35	True	144.5	147.2	-0.006	Circle	36.0	0.013	46.90	6.63	4.38	51.15	91.7	75.4	36' RCP
144	Storm_14_36in_07	Structure - (820) (SR-F2 Storm)	False	6,988.48	Structure - (858) (SR-F2 Storm)	False	6,990.00	True	76.3	79.6	-0.020	Circle	36.0	0.013	34.60	12.31	2.92	94.31	36.7	41.9	36' RCP
145	Storm_23_72in_09	STRM_MH_104 (SR-F2 Storm)	False	6,971.95	Structure - (840) (SR-F2 Storm)	False	6,977.58	True	402.6	410.7	-0.014	Circle	72.0	0.013	242.40	17.57	2.99	500.84	48.4	49.1	72' RCP
146	Storm_21_48in_01	STRM_MH_09 (SR-F2 Storm)	False	6,980.28	Structure - (552) (SR-F2 Storm)	False	6,982.00	True	57.3	60.5	-0.030	Circle	48.0	0.013	103.90	8.27	5.68	248.76	41.8	45.1	48' RCP
147	Storm_16_48in_05	Structure - (867) (SR-F2 Storm)	False	6,978.77	STRM_MH_09 (SR-F2 Storm)	False	6,979.31	True	26.8	30.5	-0.020	Circle	48.0	0.013	103.90	8.27	5.99	203.11	51.2	50.7	48' RCP
148	Storm_21_42in_03	STRM_MH_08 (SR-F2 Storm)	False	6,983.49	Structure - (868) (SR-F2 Storm)	False	6,984.00	True	101.2	104.4	-0.005	Circle	42.0	0.013	60.60	6.30	4.55	71.15	85.2	70.9	42' RCP
149	Storm_19_36in_01	STRM_MH_08 (SR-F2 Storm)	False	6,983.73	Structure - (838) (SR-F2 Storm)	False	6,985.50	True	302.2	306.4	-0.006	Circle	36.0	0.013	46.90	6.63	4.31	51.04	91.9	75.5	36' RCP
150	Storm_21_48in_02	Structure - (552) (SR-F2 Storm)	False	6,982.00	STRM_MH_08 (SR-F2 Storm)	False	6,982.77	True	25.8	29.5	-0.030	Circle	48.0	0.013	105.90	8.43	4.80	248.66	42.6	45.6	48' RCP
151	Storm_21_Lat_1_18in_01	Structure - (552) (SR-F2 Storm)	False	6,984.49	CB-4	False	6,984.58	True	19.4	25.2	-0.005	Circle	18.0	0.013	10.60	6.00	2.31	7.16	148.0	(N/A)	18' RCP
152	Storm_16_Lat_1_18in_01	Structure - (867) (SR-F2 Storm)	False	6,981.26	CB-1	False	6,981.53	True	13.2	14.3	-0.020	Circle	18.0	0.013	4.50	2.55	3.50	15.01	30.0	37.6	18' RCP
153	Storm_16_48in_02	STRM_MH_11 (SR-F2 Storm)	False	6,968.32	Structure - (855) (SR-F2 Storm)	False	6,976.52	True	348.6	357.0	-0.024	Circle	48.0	0.013	125.00	9.95	11.37	220.31	56.7	53.9	48' RCP
154	Storm_16_48in_03	Structure - (856) (SR-F2 Storm)	False	6,976.91	Structure - (866) (SR-F2 Storm)	False	6,977.92	True	50.4	53.9	-0.020	Circle	48.0	0.013	107.70	8.57	6.19	203.42	52.9	51.7	48' RCP
155	Storm_18_18in_02	CB-5	False	6,980.25	CB-6	False	6,984.78	True	94.4	97.3	-0.048	Circle	18.0	0.013	12.80	7.24	5.07	23.01	55.6	53.3	18' RCP
156	Storm_14_66in_04	STRM_MH_15 (SR-F2 Storm)	False	6,968.14	Structure - (854) (SR-F2 Storm)	False	6,974.25	True	512.4	518.6	-0.012	Circle	66.0	0.013	250.70	10.55	10.61	366.67	68.4	60.7	66' RCP
157	Storm_23_72in_08	Structure - (841) (SR-F2 Storm)	False	6,961.25	STRM_MH_104 (SR-F2 Storm)	False	6,969.23	True	602.8	608.9	-0.013	Circle	72.0	0.013	242.40	17.21	2.99	487.25	49.7	49.9	72' RCP
159	Storm_16_42in_01	STRM_MH_11 (SR-F2 Storm)	False	6,967.89	STRM_MH_15 (SR-F2 Storm)	False	6,967.57	True	158.3	158.9	0.002	Circle	42.0	0.013	125.00	6.50	11.18	90.47	138.2	(N/A)	42' RCP
160	Storm_16_48in_04	Structure - (866) (SR-F2 Storm)	False	6,977.92	Structure - (867) (SR-F2 Storm)	False	6,978.77	True	42.5	42.5	-0.020	Circle	48.0	0.013	107.70	8.57	6.03	203.12	53.0	51.8	48' RCP
161	Storm_14_72in_03	STRM_MH_14 (SR-F2 Storm)	False	6,967.18	STRM_MH_15 (SR-F2 Storm)	False	6,967.57	True	74.5	94.3	-0.005	Circle	72.0	0.013	336.80	11.91	9.45	306.40	109.9	(N/A)	72' RCP
162	Storm_14_72in_02	STRM_MH_13 (SR-F2 Storm)	False	6,966.54	STRM_MH_14 (SR-F2 Storm)	False	6,967.18	True	127.9	123.3	-0.005	Circle	72.0	0.013	336.80	11.91	8.73	299.58	112.4	(N/A)	72' RCP
163	Storm_15_18in_02-W	STRM_MH_13 (SR-F2 Storm)	False	6,971.54	Structure - (860) (SR-F2 Storm)	False	6,972.80	True	25.5	30.0	-0.049	Circle	18.0	0.013	14.00	7.92	3.73	23.36	59.9	55.8	18' RCP
164	Storm_14_84in_01	O-1	False	6,966.00	STRM_MH_13 (SR-F2 Storm)	False	6,966.54	True	107.3	110.6	-0.005	Circle	84.0	0.013	424.40	11.03	8.32	453.09	93.7	76.8	84' RCP
165	Storm_20_48in_01	Structure - (793) (SR-F2 Storm)	False	6,948.88	Storm_20_Outfall (SR-F2 Storm)	False	6,949.67	True	57.9	64.1	-0.014	Circle	48.0	0.013	149.20	15.06	3.17	167.45	89.1	73.5	48' RCP
166	Storm_23_84in_01	O-2	False	6,945.31	Structure - (793) (SR-F2 Storm)	False	6,945.97	True	222.1	226.6	-0.003	Circle	84.0	0.013	315.80	10.28	4.68	349.27	90.4	74.5	84' RCP
167	Storm_23_72in_02	Structure - (793) (SR-F2 Storm)	False	6,946.97	STRM_MH_102 (SR-F2 Storm)	False	6,948.62	True	549.0	560.5	-0.003	Circle	72.0	0.013	245.10	9.28	4.97	232.16	105.6	88.2	72' RCP
169	Storm_23_72in_05	STRM_MH_101 (SR-F2 Storm)	False	6,954.29	STRM_MH_12 (SR-F2 Storm)	False	6,956.09	True	120.0	104.1	-0.015	Circle	72.0	0.013	242.40	18.04	3.21	518.77	46.7	48.1	72' RCP
170	Storm_25_30in_01	Structure - (865) (SR-F2 Storm)	False	6,955.17	STRM_MH_101 (SR-F2 Storm)	False	6,952.68	True	23.6	22.6	0.105	Circle	30.0	0.013	10.00	15.95	3.04	133.22	7.5	18.5	30' RCP
17																					

Channel Report

Vollmer Roadside Swale

Trapezoidal

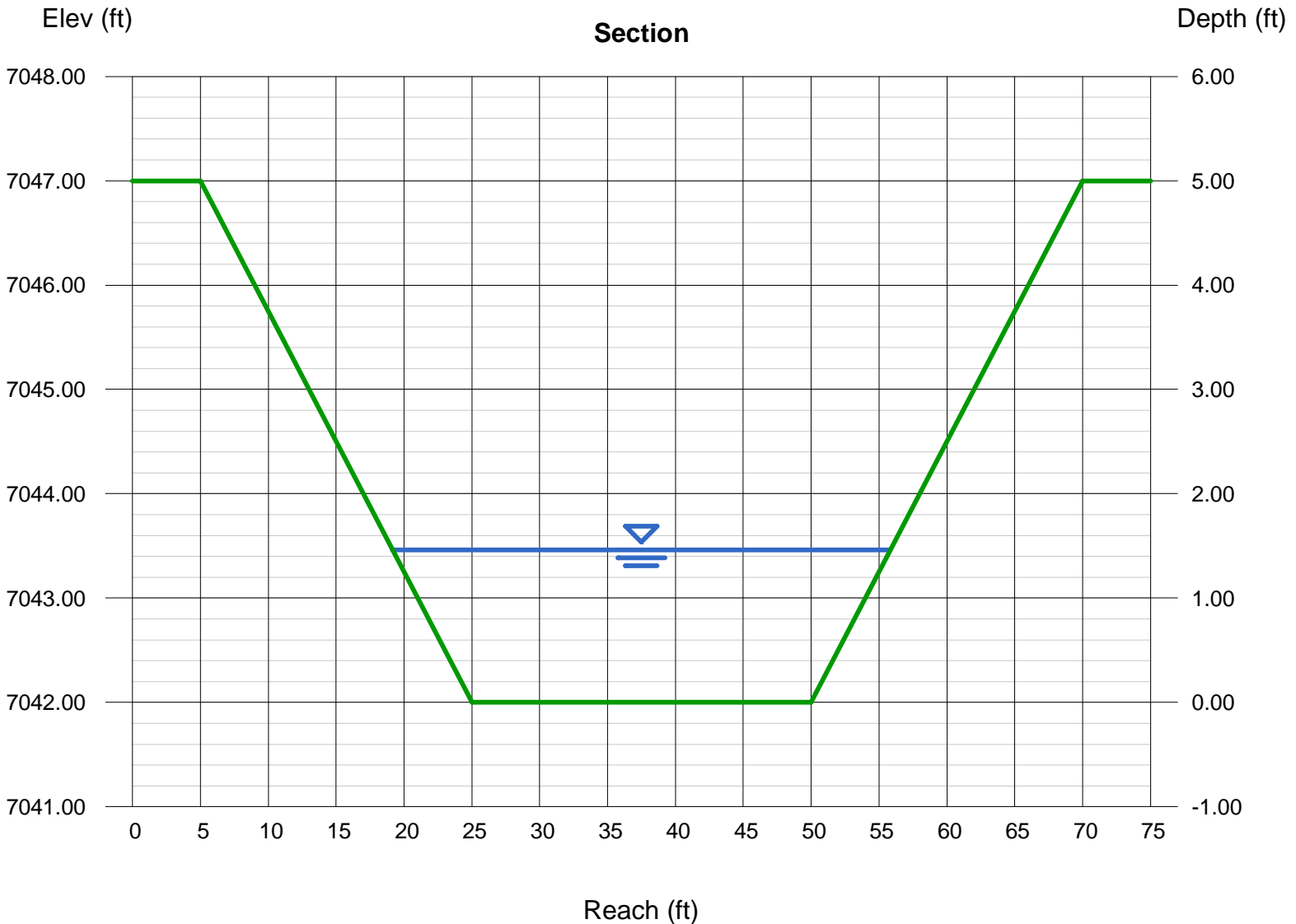
Bottom Width (ft)	= 25.00
Side Slopes (z:1)	= 4.00, 4.00
Total Depth (ft)	= 5.00
Invert Elev (ft)	= 7042.00
Slope (%)	= 1.50
N-Value	= 0.030

Highlighted

Depth (ft)	= 1.46
Q (cfs)	= 310.00
Area (sqft)	= 45.03
Velocity (ft/s)	= 6.88
Wetted Perim (ft)	= 37.04
Crit Depth, Yc (ft)	= 1.55
Top Width (ft)	= 36.68
EGL (ft)	= 2.20
Froude No.	= 1.12

Calculations

Compute by:	Known Q
Known Q (cfs)	= 310.00



Culvert Report

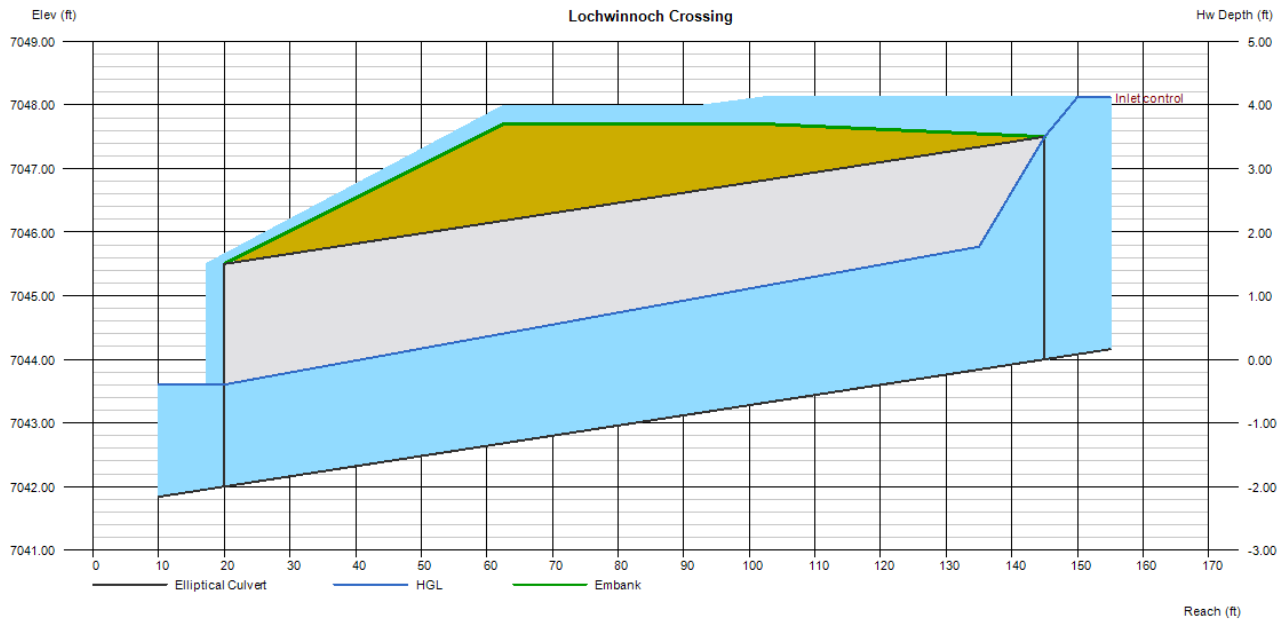
Lochwinnoch Crossing

Invert Elev Dn (ft)	= 7042.00
Pipe Length (ft)	= 125.00
Slope (%)	= 1.60
Invert Elev Up (ft)	= 7044.00
Rise (in)	= 42.0
Shape	= Elliptical
Span (in)	= 66.0
No. Barrels	= 1
n-Value	= 0.012
Culvert Type	= Horizontal Ellipse Concrete
Culvert Entrance	= Groove end projecting (H)
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2

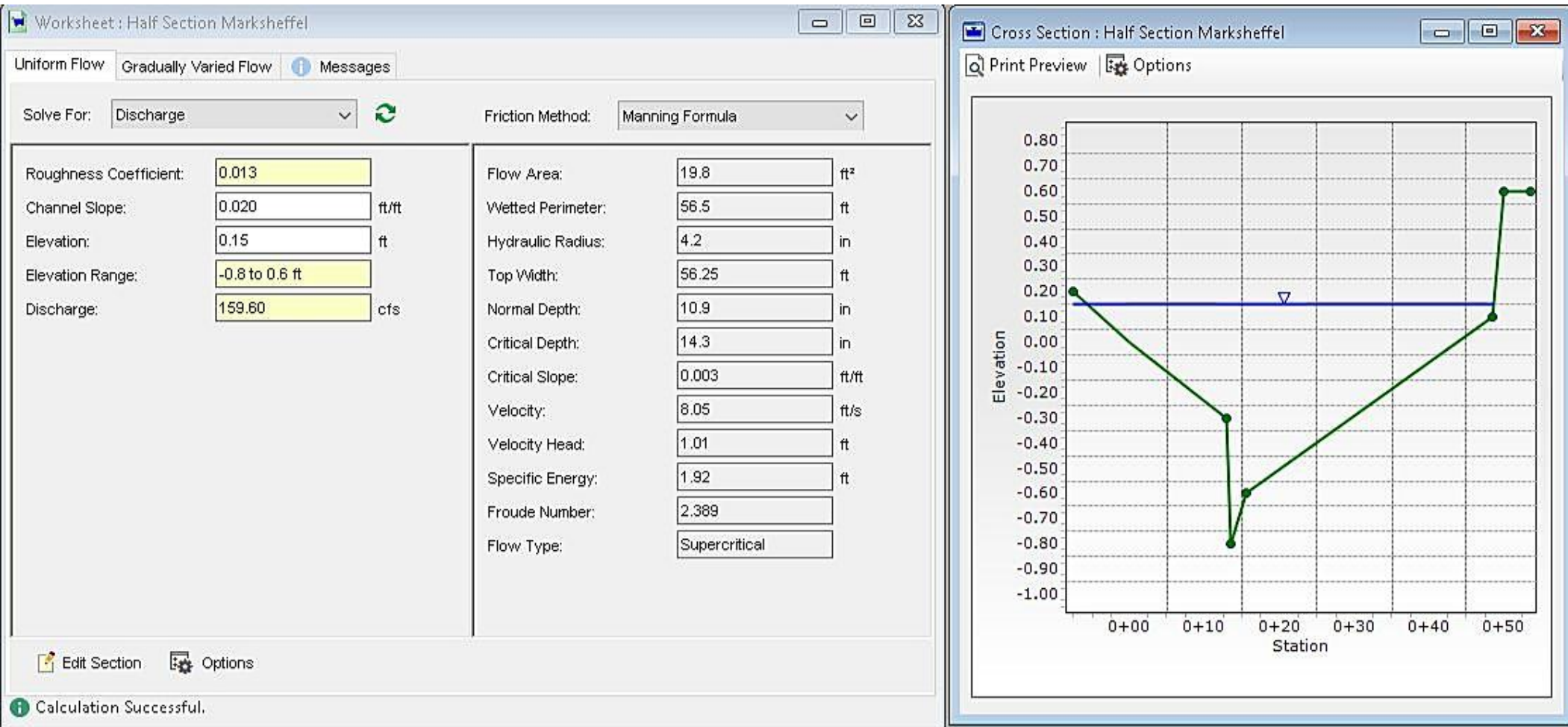
Embankment	
Top Elevation (ft)	= 7047.70
Top Width (ft)	= 40.00
Crest Width (ft)	= 150.00

Calculations	
Qmin (cfs)	= 235.90
Qmax (cfs)	= 235.90
Tailwater Elev (ft)	= Normal

Highlighted	
Qtotal (cfs)	= 235.90
Qpipe (cfs)	= 105.79
Qovertop (cfs)	= 130.11
Veloc Dn (ft/s)	= 14.58
Veloc Up (ft/s)	= 11.96
HGL Dn (ft)	= 7043.60
HGL Up (ft)	= 7045.96
Hw Elev (ft)	= 7048.12
Hw/D (ft)	= 1.18
Flow Regime	= Inlet Control



MARKSHEFFEL HALF SECTION EMERGENCY OVERFLOW CAPACITY



IF AN EMERGENCY OVERFLOW SITUATION WERE TO OCCUR, UPSTREAM BASIN'S (A6A, A7, A8, A9 A11, A15, A16, AND A21) 100 YEAR RUNOFF WOULD TRAVEL DOWN MARKSHEFFEL ROAD AND SHEET FLOW INTO SAND CREEK. THE TOTAL 100 YEAR RUNOFF OF THESE BASINS IS 126.7 CFS.

Channel Report

Pond W4 Spillway

Trapezoidal

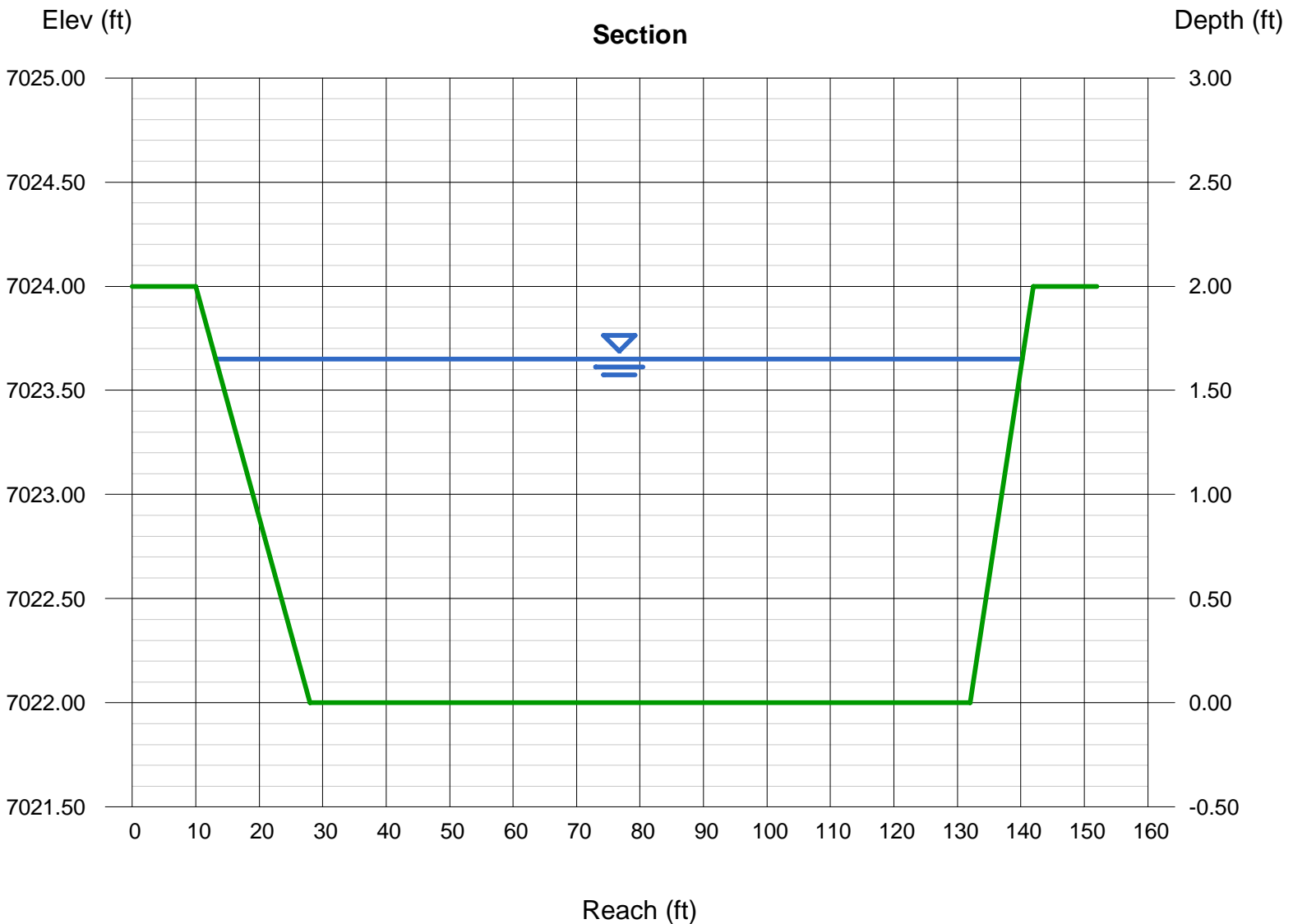
Bottom Width (ft) = 104.00
Side Slopes (z:1) = 9.00, 5.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7022.00
Slope (%) = 0.01
N-Value = 0.012

Highlighted

Depth (ft) = 1.65
Q (cfs) = 308.10
Area (sqft) = 190.66
Velocity (ft/s) = 1.62
Wetted Perim (ft) = 127.35
Crit Depth, Y_c (ft) = 0.64
Top Width (ft) = 127.10
EGL (ft) = 1.69

Calculations

Compute by: Known Q
Known Q (cfs) = 308.10



PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Sterling Ranch Filing No. 2
 Location: El Paso County

Project Name: Sterling Ranch Subdivision
 Project No.: 25188.01
 Calculated By: AJH
 Checked By: _____
 Date: 8/31/20

Pond W4 Release - Outfall release to DP 4.6

	STORM DRAIN SYSTEM			Notes
	DESIGN POINT	DESIGN POINT	DESIGN POINT	
Q ₁₀₀ (cfs):	232.5			Flows are the greater of proposed vs. future
Conduit	Pipe			
D _c , Pipe Diameter (in):	66			
W, Box Width (ft):	N/A			
H, Box Height (ft):	N/A			
Y _t , Tailwater Depth (ft):	2.20			If unknown, use Y _t /D _c (or H)=0.4
Y _t /D _c or Y _t /H	0.40			
Q/D ^{2.5} or Q/(WH ^{3/2})	3.28			
Supercritical?	No			
Y _n , Normal Depth (ft) [Supercritical]:	N/A			
D _a , H _a (in) [Supercritical]:	N/A			D _a =(D _c +Y _n)/2
Riprap d ₅₀ (in) [Supercritical]:	N/A			
Riprap d ₅₀ (in) [Subcritical]:	14.94			
Required Riprap Size:	H			Fig. 9-38 or Fig. 9-36
d₅₀ (in):	15			
Expansion Factor, 1/(2 tan θ):	4.20			Read from Fig. 9-35 or 9-36
θ:	0.12			
Erosive Soils?	No			
Area of Flow, A _t (ft ²):	33.21			A _t =Q/V
Length of Protection, L _p (ft):	40.3			L=(1/(2 tan θ))(A _t /Y _t - D)
Min Length (ft)	16.5			Min L=3D or 3H
Max Length (ft)	55.0			Max L=10D or 10H
Min Bottom Width, T (ft):	15.1			T=2*(L _p *tanθ)+W
Design Length (ft)	41.0			
Design Width (ft)	15.1			
Riprap Depth (in)	30			Depth=2(d ₅₀)
Type II Bedding Depth (in)*	8			*Not used if Soil Riprap
Cutoff Wall	No			
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

Note: No Type II Base to be used if Soil Riprap is specified within the plans

* For use when the flow in the culvert is supercritical (and less than full).

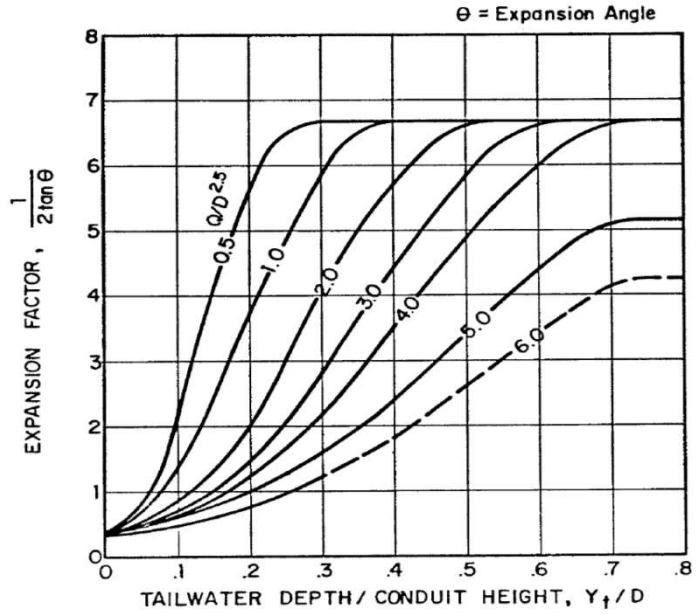


Figure 9-35. Expansion factor for circular conduits

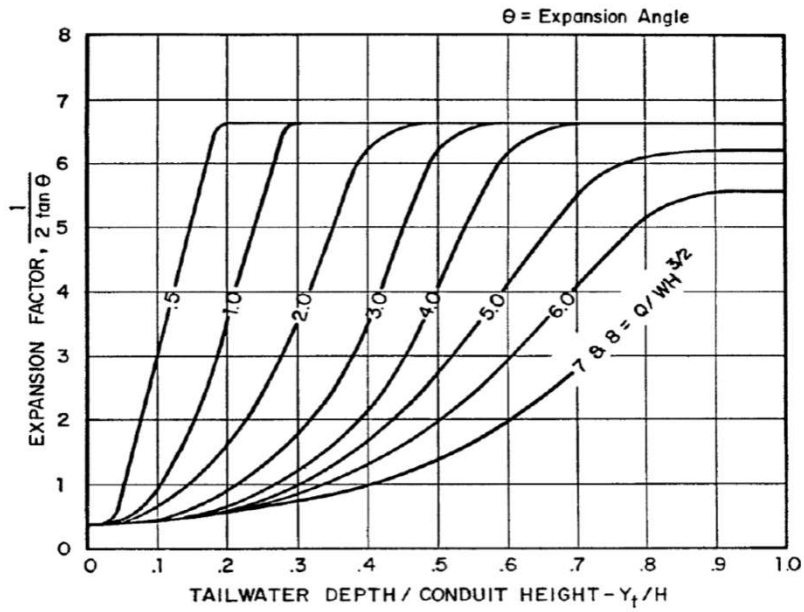


Figure 9-36. Expansion factor for rectangular conduits

Worksheet: Temporary Roadside Ditch Section A

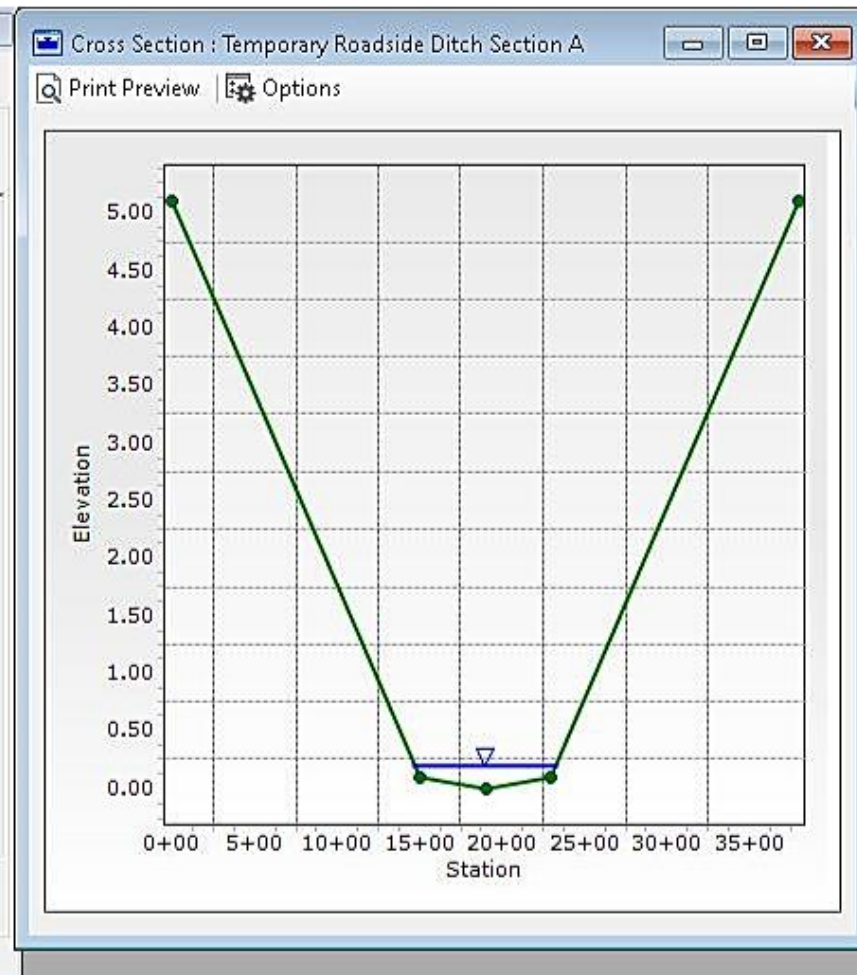
Uniform Flow | Gradually Varied Flow | Messages

Solve For: Normal Depth | Friction Method: Manning Formula

Roughness Coefficient:	0.030	Flow Area:	134.3	ft ²	
Channel Slope:	0.017	ft/ft	Wetted Perimeter:	873.3	ft
Elevation:	0.20	ft	Hydraulic Radius:	1.8	in
Elevation Range:	0.0 to 5.1	ft	Top Width:	873.33	ft
Discharge:	245.10	cfs	Normal Depth:	2.4	in
			Critical Depth:	2.2	in
			Critical Slope:	0.026	ft/ft
			Velocity:	1.83	ft/s
			Velocity Head:	0.05	ft
			Specific Energy:	0.25	ft
			Froude Number:	0.821	
			Flow Type:	Subcritical	

Edit Section | Options

Calculation Successful.

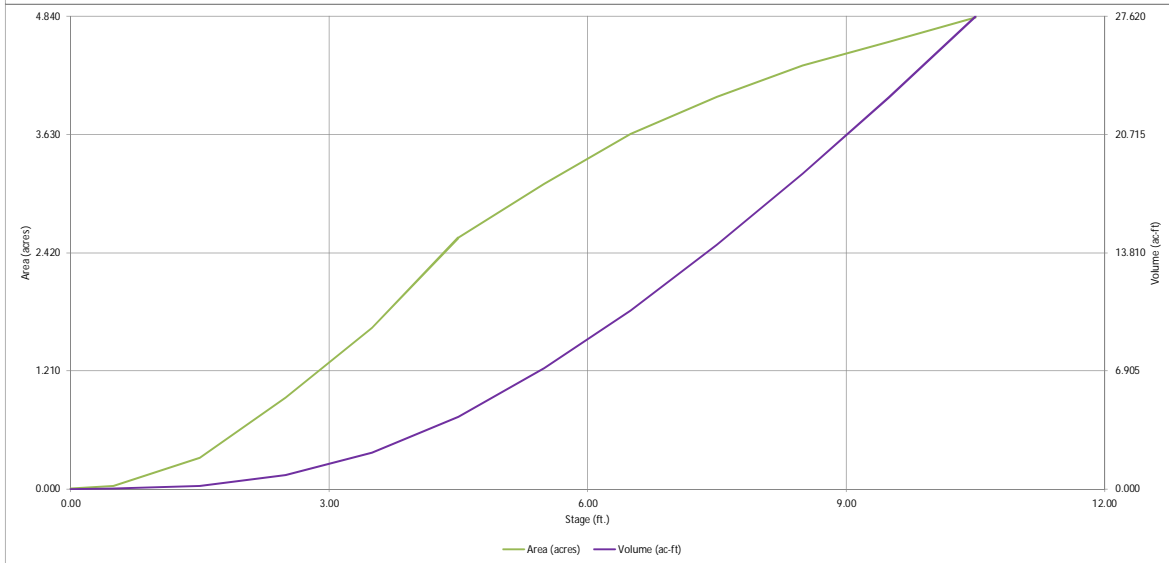
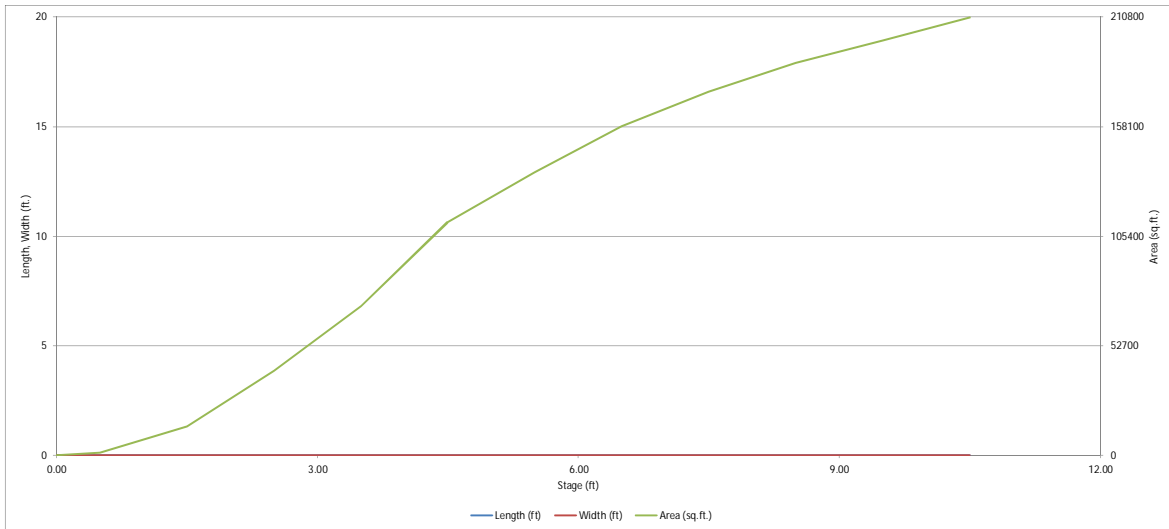


APPENDIX C

WATER QUALITY AND DETENTION CALCULATIONS

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

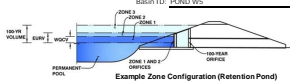


DETENTION BASIN OUTLET STRUCTURE DESIGN

MFD Detention, Version 4.03 (May 2020)

Project: STERLING RANCH FILLING NO. 2

Basin ID: POND WS



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WOCV)	4.13	3.311	Orifice Plate
Zone 2 (EURV)	6.88	8.532	Rectangular Orifice
Zone 3 (100-year)	8.49	6.532	Weir/Pipe (Restrict)
Total (all zones)		18.376	

User Input - Orifice at Underdrain Outlet (Typically used to drain WOCV in a Filtration BMP)

Underdrain Orifice Invert Depth	N/A	ft (relative to the filtration media surface)
Underdrain Orifice Diameter	N/A	inches

Underdrain Orifice Area	N/A	ft ²
Underdrain Orifice Centroid	N/A	feet

User Input - Orifice Plate with one or more orifices or Elliptical Slot Weir (Typically used to drain WOCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate	6.88	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing	N/A	inches
Orifice Plate: Orifice Area per Row	N/A	inches

WQ Orifice Area per Row	N/A	ft ²
Elliptical Half-Width	N/A	feet
Elliptical Slot Centroid	N/A	feet
Elliptical Slot Area	N/A	ft ²

User Input - Stage and Total Area of Each Orifice Row (Numbered from lowest to highest)

Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Control (ft)	0.00	2.35	4.00				
Orifice Area (sq. inches)	12.5%	12.5%	25.00				
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)
Stage of Orifice Control (ft)							
Orifice Area (sq. inches)							

User Input - Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected	
Invert of Vertical Orifice	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Height	N/A	N/A	inches
Vertical Orifice Width	N/A	N/A	inches

Vertical Orifice Area	N/A	ft ²
Vertical Orifice Centroid	N/A	feet

User Input - Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe, NB Rectangular/Trapezoidal Weir, Dard, No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o	7.30	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length	20.00	N/A	feet
Overflow Weir Grate Slope	0.00	N/A	H:V
Horiz. Length of Weir Sides	6.00	N/A	feet
Overflow Grate Open Area %	70%	N/A	%, grate open area/total area
Debris Chocking %	50%	N/A	%

Height of Grate Upper Edge, H _u	7.30	N/A	feet
Overflow Weir Slope Length	6.00	N/A	feet
Grate Open Area / 100-y Orifice Area	6.48	N/A	ft ²
Overflow Grate Open Area w/o Debris	84.00	N/A	ft ²
Overflow Grate Open Area / Debris	42.00	N/A	ft ²

User Input - Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe	2.25	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter	54.00	N/A	inches
Restrictor Plate Height Above Pipe Invert	41.00	N/A	inches

Outlet Orifice Area	12.96	N/A	ft ²
Outlet Orifice Centroid	1.88	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe	2.12	N/A	radians

User Input - Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage	8.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length	48.00	feet
Spillway End Slopes	10.00	H:V
Freebord above Max Water Surface	2.00	feet

Spillway Design Flow Depth - Stage at Top of Freeboard	1.74	feet
Basin Area at Top of Freeboard	12.24	feet
Basin Area at Top of Freeboard	4.83	acres
Basin Volume at Top of Freeboard	27.61	acre-ft

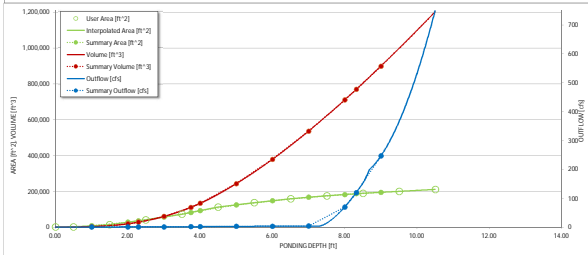
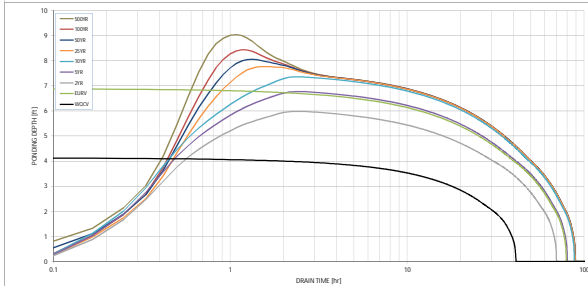
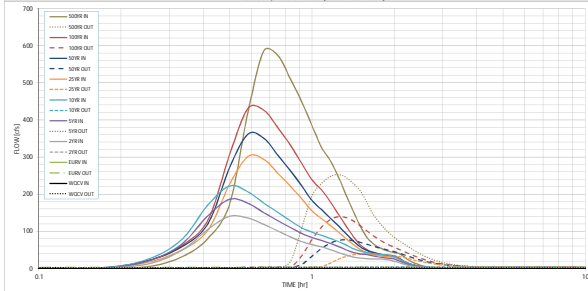
Basin Hydrograph Results

The user can override the default CRRP hydrographs and outfall volumes by entering new values in the Inflow Hydrographs table. (Columns 19 through 22)

	WOCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period	N/A	N/A							
One-Hour Rainfall Depth (in)	3.311	11.843	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CRRP Runoff Volume (ac-ft)	N/A	N/A	9.121	11.991	14.334	18.244	21.510	25.732	34.734
Inflow Hydrograph Volume (ac-ft)	N/A	N/A	9.121	11.991	14.334	18.244	21.510	25.732	34.734
CRRP Revolvement Peak Q (cfs)	N/A	N/A	1.6	2.9	5.1	54.6	85.6	128.5	217.8
OPTIONAL Override Pradevolvement Peak Q (cfs)	N/A	N/A							
Pradevolvement Unit Peak Flow, q (cfs/acre)	N/A	N/A	0.01	0.02	0.03	0.31	0.49	0.74	1.25
Pradevolvement Unit Peak Inflow Q (cfs)	N/A	N/A	140.5	186.5	222.1	301.6	361.5	431.2	586.0
Peak Outflow Q (cfs)	1.7	3.4	3.0	3.4	5.1	38.8	77.3	139.3	252.7
Ratio Peak Outflow to Pradevolvement Q	N/A	N/A	N/A	1.2	1.0	0.7	0.9	1.1	1.2
Structure Controlling Flow	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps)	N/A	N/A	N/A	N/A	N/A	0.0	0.4	0.9	1.6
Max Velocity through Grate 2 (fps)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hour)	38	70	63	67	78	76	75	73	90
Time to Drain 99% of Inflow Volume (hour)	40	78	67	77	84	84	83	82	81
Maximum Ponding Depth (ft)	4.13	6.88	5.98	6.77	7.35	7.76	8.05	8.43	9.04
Area at Maximum Ponding Depth (ac-ft)	2.23	3.78	3.37	3.73	3.96	4.10	4.19	4.31	4.47
Maximum Volume Stored (ac-ft)	3.320	11.847	8.616	11.396	13.666	15.319	16.522	18.138	20.774

DETENTION BASIN OUTLET STRUCTURE DESIGN

MMFD- Detention, Version 4.00 (December 2019)



S-S-V-D Chart 1 Axis Overlaid: X-axis Left Y-Axis Right Y-Axis
 minimum bound maximum bound

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

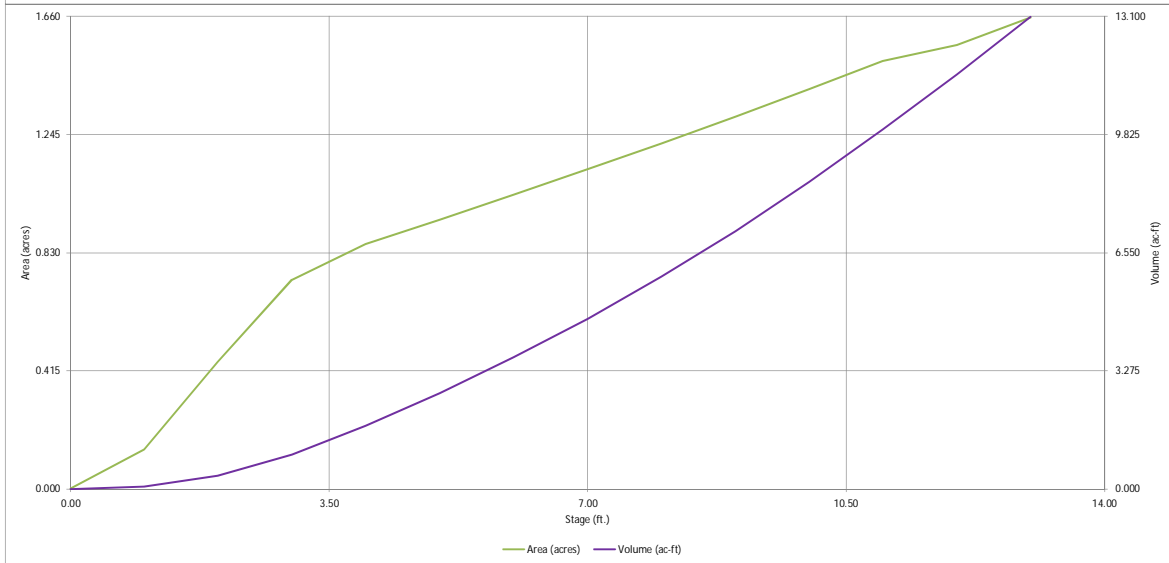
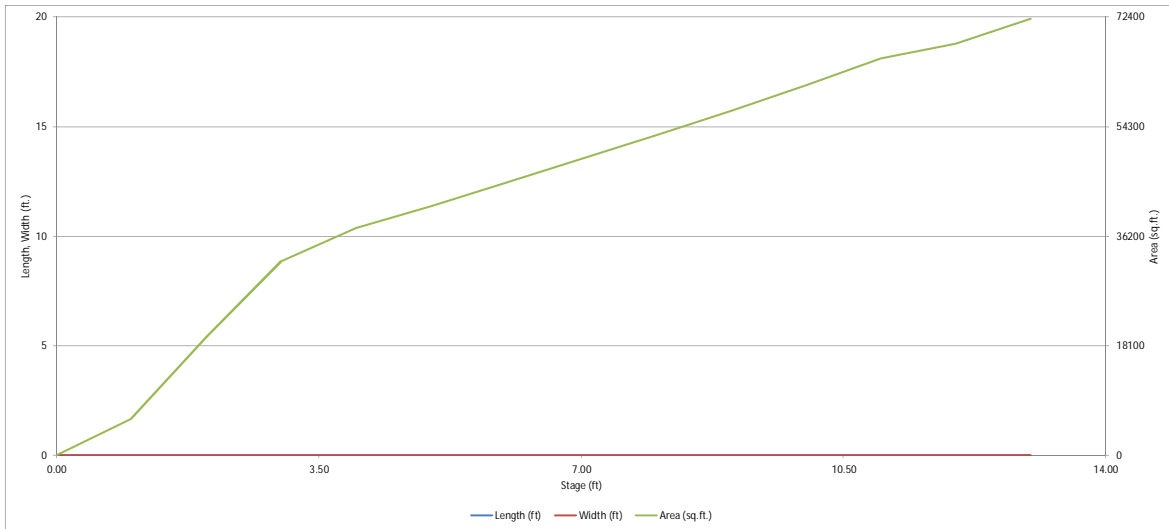
Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCC [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	1.37	0.14	4.42
	0:15:00	0.00	0.00	12.01	19.62	24.38	16.41	21.13	20.11	30.88
	0:20:00	0.00	0.00	48.30	65.31	77.56	49.45	58.16	61.60	81.16
	0:25:00	0.00	0.00	105.72	142.84	171.74	104.01	121.39	131.21	174.25
	0:30:00	0.00	0.00	140.48	186.46	222.11	127.64	172.85	188.13	250.01
	0:35:00	0.00	0.00	135.46	175.22	206.02	109.41	161.54	171.24	255.96
	0:40:00	0.00	0.00	118.36	150.07	175.48	290.61	350.26	425.82	573.28
	0:45:00	0.00	0.00	100.92	128.44	150.65	256.40	304.92	376.98	510.45
0:50:00	0.00	0.00	84.87	110.40	128.43	222.14	263.81	332.30	449.36	
0:55:00	0.00	0.00	72.36	94.33	109.32	187.66	222.42	282.99	384.40	
1:00:00	0.00	0.00	64.06	83.13	97.59	154.96	182.98	238.59	325.88	
1:05:00	0.00	0.00	58.14	75.08	88.94	134.19	158.26	211.50	280.49	
1:10:00	0.00	0.00	50.72	67.68	80.67	115.60	135.72	179.70	246.12	
1:15:00	0.00	0.00	42.71	59.28	72.45	97.95	114.20	145.50	197.60	
1:20:00	0.00	0.00	35.76	50.04	63.10	80.42	93.20	113.95	153.88	
1:25:00	0.00	0.00	30.54	42.87	53.10	64.63	74.31	85.95	114.90	
1:30:00	0.00	0.00	27.71	39.21	46.68	51.11	58.33	64.24	85.13	
1:35:00	0.00	0.00	26.36	37.32	42.89	49.74	48.57	51.51	67.73	
1:40:00	0.00	0.00	25.40	34.28	40.22	37.77	42.78	44.23	57.57	
1:45:00	0.00	0.00	25.13	31.06	38.26	34.61	39.11	39.26	50.51	
1:50:00	0.00	0.00	24.76	28.74	36.93	32.45	36.59	36.99	45.78	
1:55:00	0.00	0.00	22.48	27.05	35.35	31.03	34.94	33.68	42.43	
2:00:00	0.00	0.00	19.58	25.23	32.57	30.00	33.77	32.06	40.11	
2:05:00	0.00	0.00	15.52	20.27	25.90	24.54	22.57	26.26	32.38	
2:10:00	0.00	0.00	11.36	14.69	18.66	17.66	19.83	18.68	23.23	
2:15:00	0.00	0.00	8.25	10.65	13.46	12.75	14.30	13.52	16.79	
2:20:00	0.00	0.00	5.94	7.66	9.70	9.23	10.34	9.85	12.22	
2:25:00	0.00	0.00	4.23	5.34	6.86	6.50	7.28	6.96	8.63	
2:30:00	0.00	0.00	2.91	3.63	4.77	4.51	5.04	4.82	5.97	
2:35:00	0.00	0.00	1.96	2.50	3.30	3.19	3.57	3.40	4.20	
2:40:00	0.00	0.00	1.21	1.65	2.12	2.10	2.34	2.23	2.75	
2:45:00	0.00	0.00	0.68	0.97	1.20	1.24	1.38	1.31	1.60	
2:50:00	0.00	0.00	0.28	0.47	0.55	0.60	0.66	0.61	0.76	
2:55:00	0.00	0.00	0.09	0.15	0.16	0.19	0.20	0.19	0.22	
3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
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4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
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5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

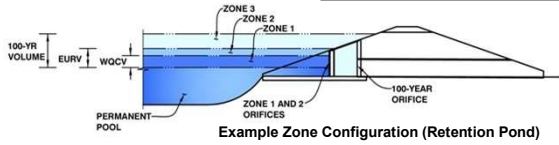


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: STERLING RANCH FILING NO. 2

Basin ID: POND W4 Interim



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	4.61	2.281	Orifice Plate
Zone 2 (EURV)	6.07	1.429	Orifice Plate
Zone 3 (100-year)	12.46	8.500	Weir&Pipe (Restrict)
Total (all zones)		12.211	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
 Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = 4.99 ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = N/A inches
 Orifice Plate: Orifice Area per Row = 6.80 sq. inches (use rectangular openings)

Calculated Parameters for Plate
 WQ Orifice Area per Row = 4.722E-02 ft²
 Elliptical Half-Width = N/A feet
 Elliptical Slot Centroid = N/A feet
 Elliptical Slot Area = N/A ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.66	3.33					
Orifice Area (sq. inches)	6.80	6.80	6.80					
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = Not Selected Not Selected ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft)
 Vertical Orifice Diameter = N/A N/A inches

Calculated Parameters for Vertical Orifice
 Vertical Orifice Area = Not Selected Not Selected ft²
 Vertical Orifice Centroid = N/A N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, Ho = Zone 3 Weir 6.07 Not Selected N/A ft (relative to basin bottom at Stage = 0 ft)
 Overflow Weir Front Edge Length = 20.00 N/A feet
 Overflow Weir Grate Slope = 4.00 N/A H:V
 Horiz. Length of Weir Sides = 10.00 N/A feet
 Overflow Grate Open Area % = 70% N/A %, grate open area/total area
 Debris Clogging % = 50% N/A %

Calculated Parameters for Overflow Weir
 Height of Grate Upper Edge, H_u = Zone 3 Weir 8.57 Not Selected N/A feet
 Overflow Weir Slope Length = 10.31 N/A feet
 Grate Open Area / 100-yr Orifice Area = 6.46 N/A
 Overflow Grate Open Area w/o Debris = 144.31 N/A ft²
 Overflow Grate Open Area w/ Debris = 72.15 N/A ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = Zone 3 Restrictor 0.58 Not Selected N/A ft (distance below basin bottom at Stage = 0 ft)
 Outlet Pipe Diameter = 66.00 N/A inches
 Restrictor Plate Height Above Pipe Invert = 58.80 N/A inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
 Outlet Orifice Area = Zone 3 Restrictor 22.35 Not Selected N/A ft²
 Outlet Orifice Centroid = 2.60 N/A feet
 Half-Central Angle of Restrictor Plate on Pipe = 2.47 N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 9.50 ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = 74.00 feet
 Spillway End Slopes = 4.00 H:V
 Freeboard above Max Water Surface = 1.50 feet

Calculated Parameters for Spillway
 Spillway Design Flow Depth = 1.20 feet
 Stage at Top of Freeboard = 12.20 feet
 Basin Area at Top of Freeboard = 1.58 acres
 Basin Volume at Top of Freeboard = 11.80 acre-ft

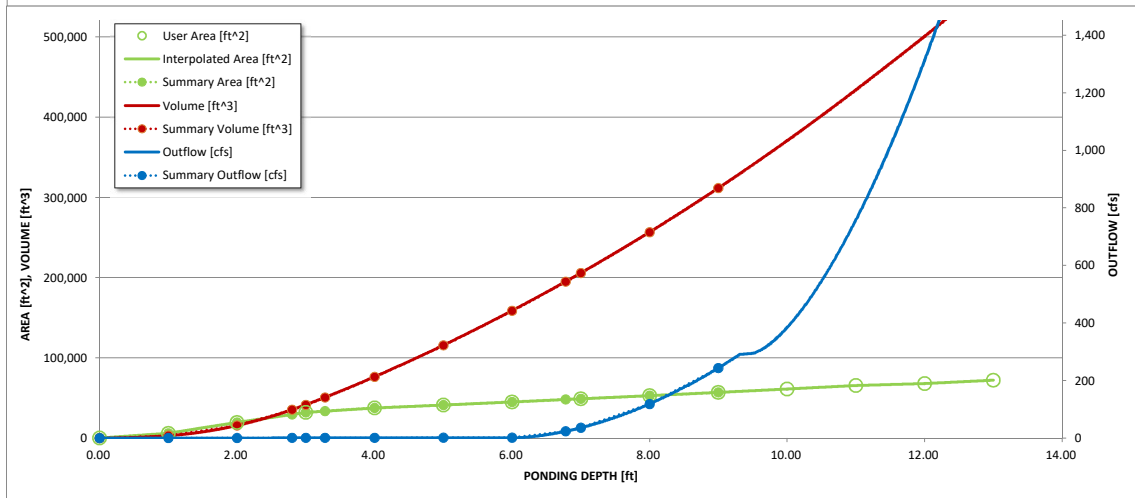
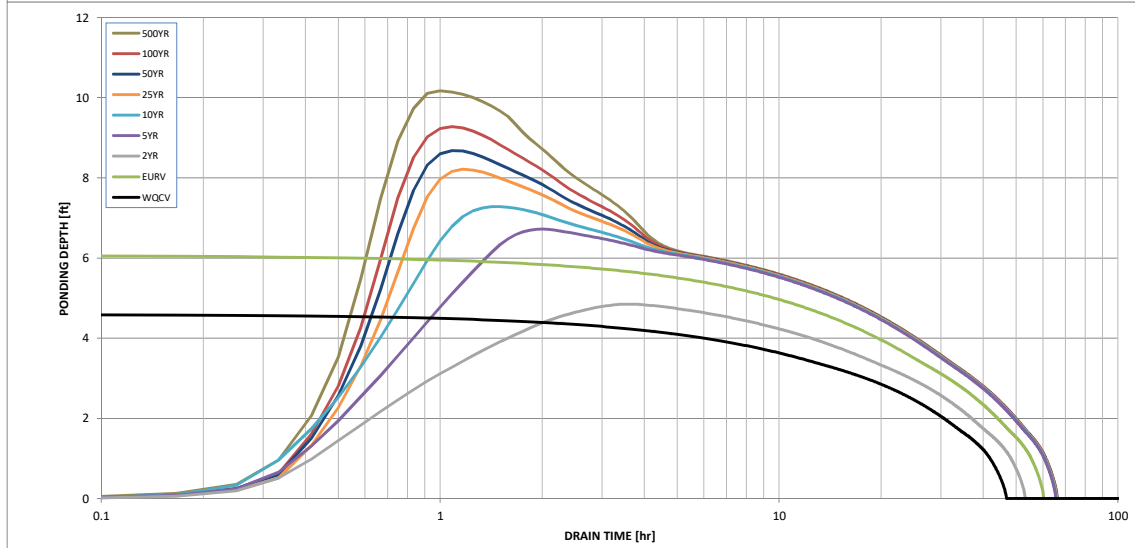
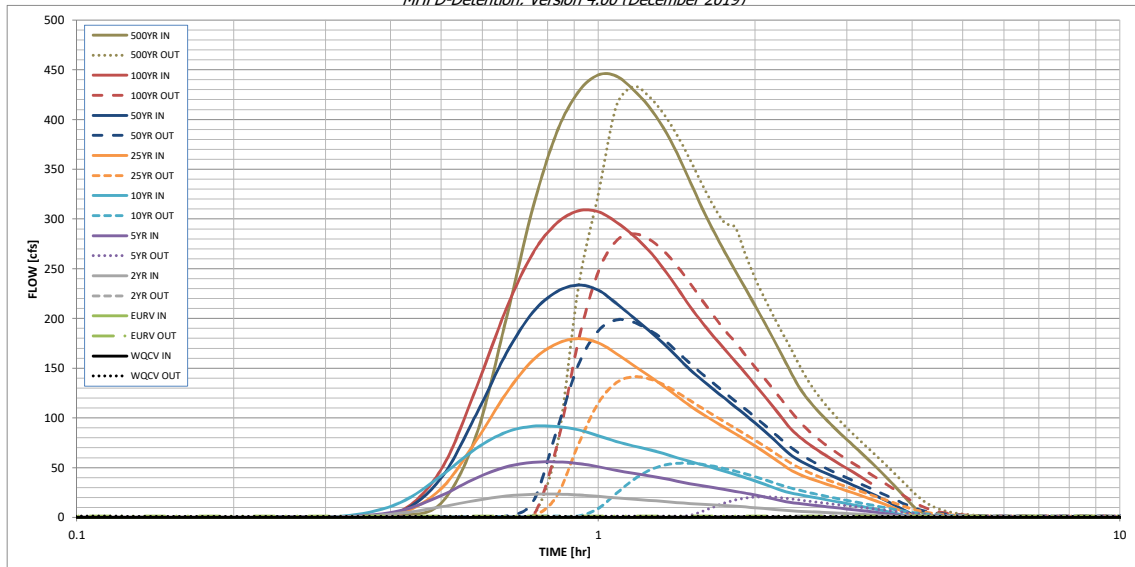
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
One-Hour Rainfall Depth (in)	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft)	2.281	3.710	2.802	6.573	10.859	20.281	26.707	36.815	54.041
Inflow Hydrograph Volume (acre-ft)	N/A	N/A	2.802	6.573	10.859	20.281	26.707	36.815	54.041
CUHP Predevelopment Peak Q (cfs)	N/A	N/A	3.7	30.4	64.6	150.7	203.5	280.5	416.0
OPTIONAL Override Predevelopment Peak Q (cfs)	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre)	N/A	N/A	0.01	0.09	0.18	0.43	0.58	0.80	1.19
Peak Inflow Q (cfs)	N/A	N/A	23.4	55.7	91.6	179.7	233.5	308.1	444.7
Peak Outflow Q (cfs)	1.1	1.4	1.2	20.7	54.4	141.3	198.4	285.0	433.1
Ratio Peak Outflow to Predevelopment Q	N/A	N/A	N/A	0.7	0.8	0.9	1.0	1.0	1.0
Structure Controlling Flow	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Gate 1 (fps)	N/A	N/A	N/A	0.1	0.4	1.0	1.4	2.0	2.1
Max Velocity through Gate 2 (fps)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours)	42	53	48	55	51	44	40	35	27
Time to Drain 99% of Inflow Volume (hours)	45	57	51	61	59	55	53	50	46
Maximum Ponding Depth (ft)	4.61	6.07	4.85	6.72	7.28	8.21	8.68	9.28	10.17
Area at Maximum Ponding Depth (acres)	0.91	1.04	0.93	1.10	1.15	1.23	1.28	1.33	1.42
Maximum Volume Stored (acre-ft)	2.290	3.714	2.511	4.398	5.039	6.146	6.736	7.506	8.745

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.00 (December 2019)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.05
	0:15:00	0.00	0.00	0.13	0.22	0.27	0.19	0.26	0.23	0.41
	0:20:00	0.00	0.00	0.70	1.03	1.91	0.80	0.98	0.99	1.99
	0:25:00	0.00	0.00	4.05	6.62	14.64	3.93	5.22	5.86	14.30
	0:30:00	0.00	0.00	10.59	21.88	41.83	28.88	39.54	48.08	81.91
	0:35:00	0.00	0.00	17.09	39.51	69.21	76.76	103.22	129.56	199.96
	0:40:00	0.00	0.00	21.42	50.84	85.74	124.91	164.83	209.85	311.38
	0:45:00	0.00	0.00	23.26	55.39	91.58	158.09	206.35	265.79	387.19
	0:50:00	0.00	0.00	23.43	55.73	91.37	174.59	226.89	295.75	427.74
	0:55:00	0.00	0.00	22.60	54.20	87.99	179.69	233.50	308.15	444.73
	1:00:00	0.00	0.00	21.09	50.99	82.12	175.52	228.49	307.36	443.68
	1:05:00	0.00	0.00	19.58	47.22	76.30	164.74	215.25	296.89	430.21
	1:10:00	0.00	0.00	18.33	44.40	71.93	153.13	201.32	283.81	413.28
	1:15:00	0.00	0.00	17.16	41.96	68.16	142.50	188.13	268.44	391.95
	1:20:00	0.00	0.00	16.00	39.30	64.26	132.29	174.98	250.51	366.18
	1:25:00	0.00	0.00	14.87	36.45	60.01	122.00	161.53	231.17	338.13
	1:30:00	0.00	0.00	13.96	33.90	56.25	112.10	148.57	212.08	310.76
	1:35:00	0.00	0.00	13.21	31.96	52.94	104.00	137.94	195.94	287.45
	1:40:00	0.00	0.00	12.50	30.03	49.64	96.86	128.39	181.69	266.65
	1:45:00	0.00	0.00	11.83	28.10	46.33	90.29	119.57	168.78	247.80
	1:50:00	0.00	0.00	11.16	26.19	43.06	83.95	111.08	156.61	230.01
	1:55:00	0.00	0.00	10.46	24.30	39.85	77.88	102.92	144.90	212.87
	2:00:00	0.00	0.00	9.73	22.42	36.66	71.85	94.85	133.46	196.17
	2:05:00	0.00	0.00	8.94	20.50	33.43	65.81	86.82	122.23	179.75
	2:10:00	0.00	0.00	8.12	18.55	30.15	59.74	78.80	111.18	163.53
	2:15:00	0.00	0.00	7.29	16.62	27.00	53.67	70.78	100.15	147.40
	2:20:00	0.00	0.00	6.67	15.07	24.72	47.94	63.30	89.82	132.66
	2:25:00	0.00	0.00	6.21	14.10	23.11	43.84	58.01	82.20	121.64
	2:30:00	0.00	0.00	5.79	13.19	21.64	40.65	53.80	76.06	112.54
	2:35:00	0.00	0.00	5.42	12.32	20.22	37.96	50.19	70.67	104.47
	2:40:00	0.00	0.00	5.06	11.50	18.86	35.48	46.87	65.80	97.17
	2:45:00	0.00	0.00	4.71	10.71	17.53	33.22	43.83	61.30	90.40
	2:50:00	0.00	0.00	4.37	9.94	16.25	31.01	40.87	57.03	84.03
	2:55:00	0.00	0.00	4.04	9.19	15.00	28.84	37.99	53.02	78.06
	3:00:00	0.00	0.00	3.72	8.47	13.79	26.71	35.19	49.23	72.44
	3:05:00	0.00	0.00	3.41	7.76	12.62	24.62	32.42	45.47	66.87
	3:10:00	0.00	0.00	3.10	7.07	11.48	22.54	29.69	41.74	61.34
	3:15:00	0.00	0.00	2.80	6.38	10.35	20.48	26.97	38.01	55.82
	3:20:00	0.00	0.00	2.50	5.70	9.23	18.42	24.26	34.28	50.31
	3:25:00	0.00	0.00	2.20	5.03	8.12	16.37	21.55	30.56	44.81
	3:30:00	0.00	0.00	1.91	4.36	7.01	14.32	18.86	26.85	39.32
	3:35:00	0.00	0.00	1.62	3.69	5.91	12.27	16.16	23.14	33.84
	3:40:00	0.00	0.00	1.34	3.02	4.81	10.23	13.47	19.43	28.38
	3:45:00	0.00	0.00	1.06	2.36	3.72	8.20	10.79	15.74	22.93
	3:50:00	0.00	0.00	0.78	1.72	2.65	6.18	8.13	12.05	17.51
	3:55:00	0.00	0.00	0.52	1.11	1.69	4.19	5.51	8.43	12.27
	4:00:00	0.00	0.00	0.38	0.70	1.15	2.44	3.26	5.30	7.97
	4:05:00	0.00	0.00	0.30	0.56	0.93	1.47	2.05	3.46	5.40
	4:10:00	0.00	0.00	0.25	0.46	0.76	0.94	1.34	2.31	3.71
	4:15:00	0.00	0.00	0.22	0.37	0.62	0.64	0.91	1.52	2.50
	4:20:00	0.00	0.00	0.18	0.30	0.50	0.44	0.62	0.97	1.64
	4:25:00	0.00	0.00	0.15	0.24	0.39	0.33	0.45	0.58	1.03
	4:30:00	0.00	0.00	0.13	0.19	0.30	0.25	0.32	0.32	0.61
	4:35:00	0.00	0.00	0.11	0.14	0.22	0.18	0.22	0.18	0.38
	4:40:00	0.00	0.00	0.09	0.11	0.16	0.14	0.16	0.13	0.30
	4:45:00	0.00	0.00	0.07	0.09	0.12	0.10	0.12	0.10	0.23
	4:50:00	0.00	0.00	0.05	0.07	0.09	0.08	0.09	0.08	0.19
	4:55:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.06	0.14
	5:00:00	0.00	0.00	0.03	0.04	0.05	0.04	0.05	0.05	0.11
	5:05:00	0.00	0.00	0.02	0.03	0.03	0.03	0.04	0.03	0.07
	5:10:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.05
	5:15:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.03
	5:20:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

FOREBAY VOLUME REQUIREMENTS

Equation 3-1 $WQCV = a(0.91I^3 - 1.19I^2 + 0.781I)$
 $a=1$ (40 hour drain time)

Forebay @ DP 3.0	I= .549	WQCV= 0.22013
Future Forebay @ DP 3.1	I= .894	WQCV= 0.39644
Forebay @ DP 4.3	I= .066	WQCV= 0.046558

Equation 3-3 $V = (WQCV/12)A$

Forebay @ DP 3.0	A= 170.21 Acres	V= 3.122
Future Forebay @ DP 3.1	A= 3.76 Acres	V= 0.124
Forebay @ DP 4.3	A= 355.10 Acres	V= 1.378

3% OF WQCV
 FOREBAY TOTAL VOLUME= .03(V)

Volume Required for Forebay @ DP 3.0 =	0.094	AC-FT	4080 CF
Volume Required for Future Forebay @ DP 3.1 =	0.004	AC-FT	162 CF
Volume Required for Forebay @ DP 4.3 =	0.041	AC-FT	1801 CF

Q ₁₀₀ Discharges	2% OF Q ₁₀₀
Q ₁₀₀ Forebay @ DP 3.0=	.02*424.4 CFS= 8.49 CFS
Q ₁₀₀ Future Forebay @ DP 3.1 =	.02*22.5 CFS= 0.45 CFS
Q ₁₀₀ Forebay @ DP 4.3=	.02*262.3 CFS= 5.25 CFS

Weir Report

Forebay @ DP 3.0 Notch

Rectangular Weir

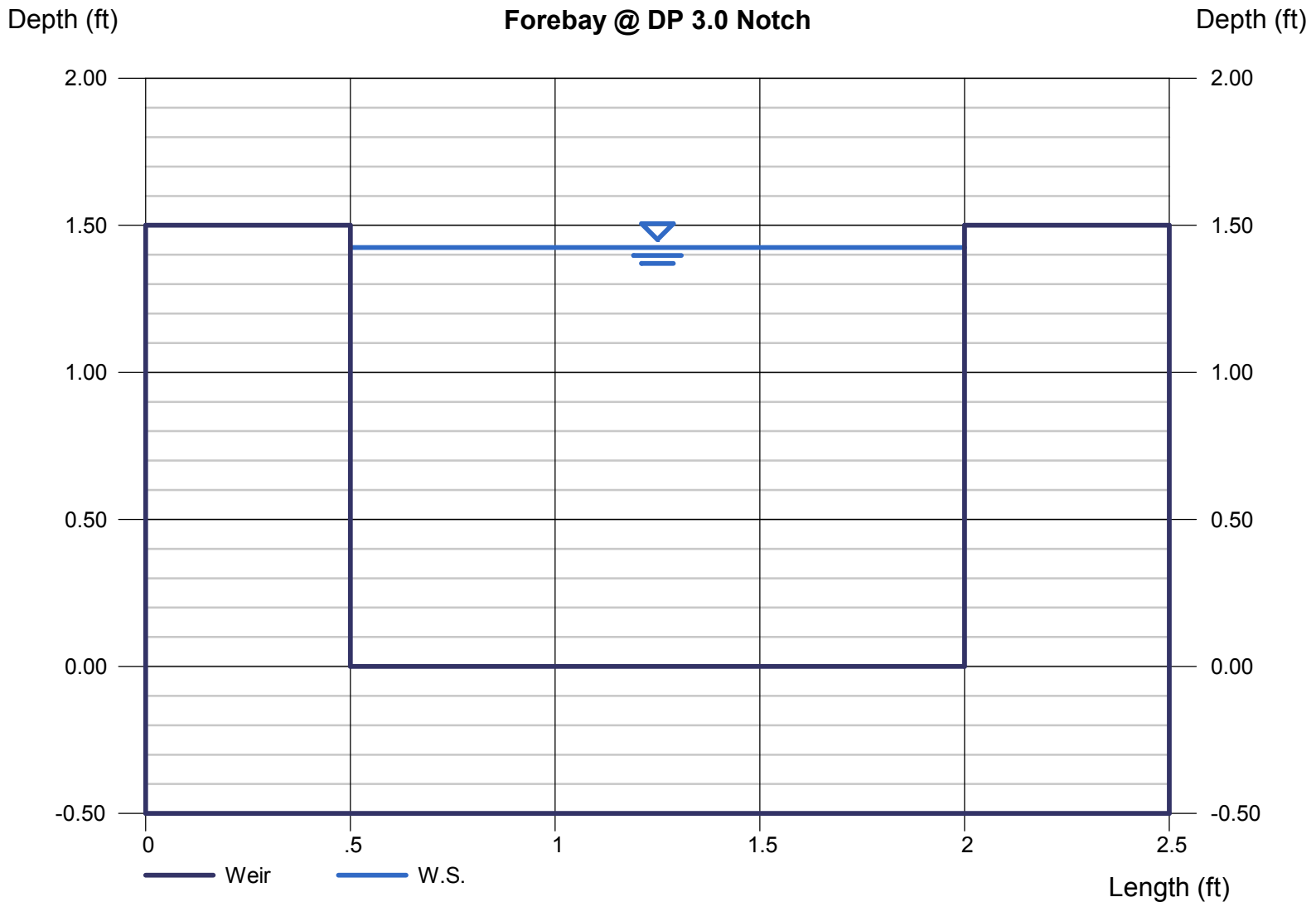
Crest = Sharp
Bottom Length (ft) = 1.50
Total Depth (ft) = 1.50

Highlighted

Depth (ft) = 1.42
Q (cfs) = 8.490
Area (sqft) = 2.14
Velocity (ft/s) = 3.97
Top Width (ft) = 1.50

Calculations

Weir Coeff. Cw = 3.33
Compute by: Known Q
Known Q (cfs) = 8.49



Weir Report

Future Forebay @ DP 3.1

Rectangular Weir

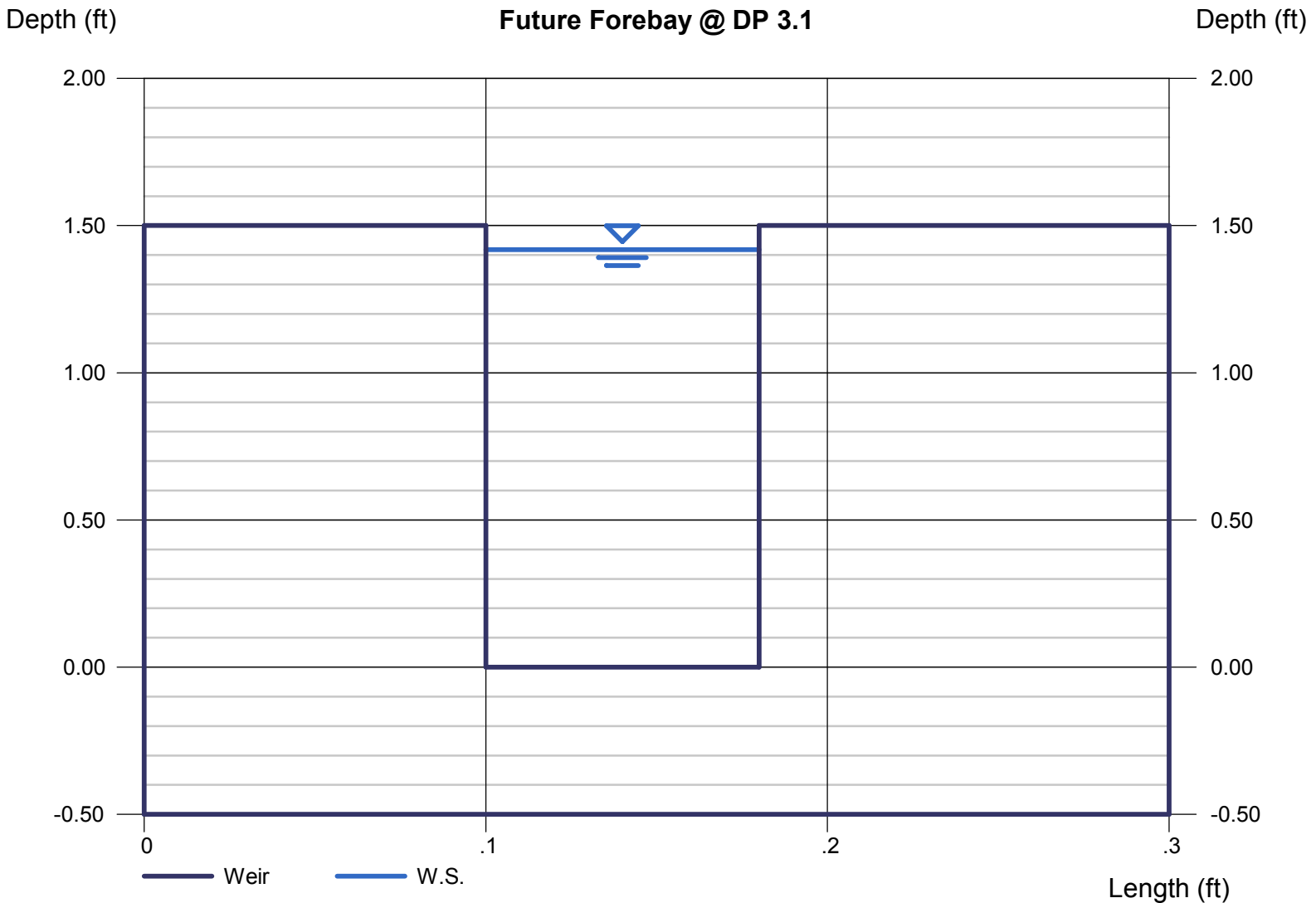
Crest = Sharp
Bottom Length (ft) = 0.08
Total Depth (ft) = 1.50

Highlighted

Depth (ft) = 1.42
Q (cfs) = 0.450
Area (sqft) = 0.11
Velocity (ft/s) = 3.97
Top Width (ft) = 0.08

Calculations

Weir Coeff. Cw = 3.33
Compute by: Known Q
Known Q (cfs) = 0.45



Weir Report

Forebay @ DP 4.3 Notch

Rectangular Weir

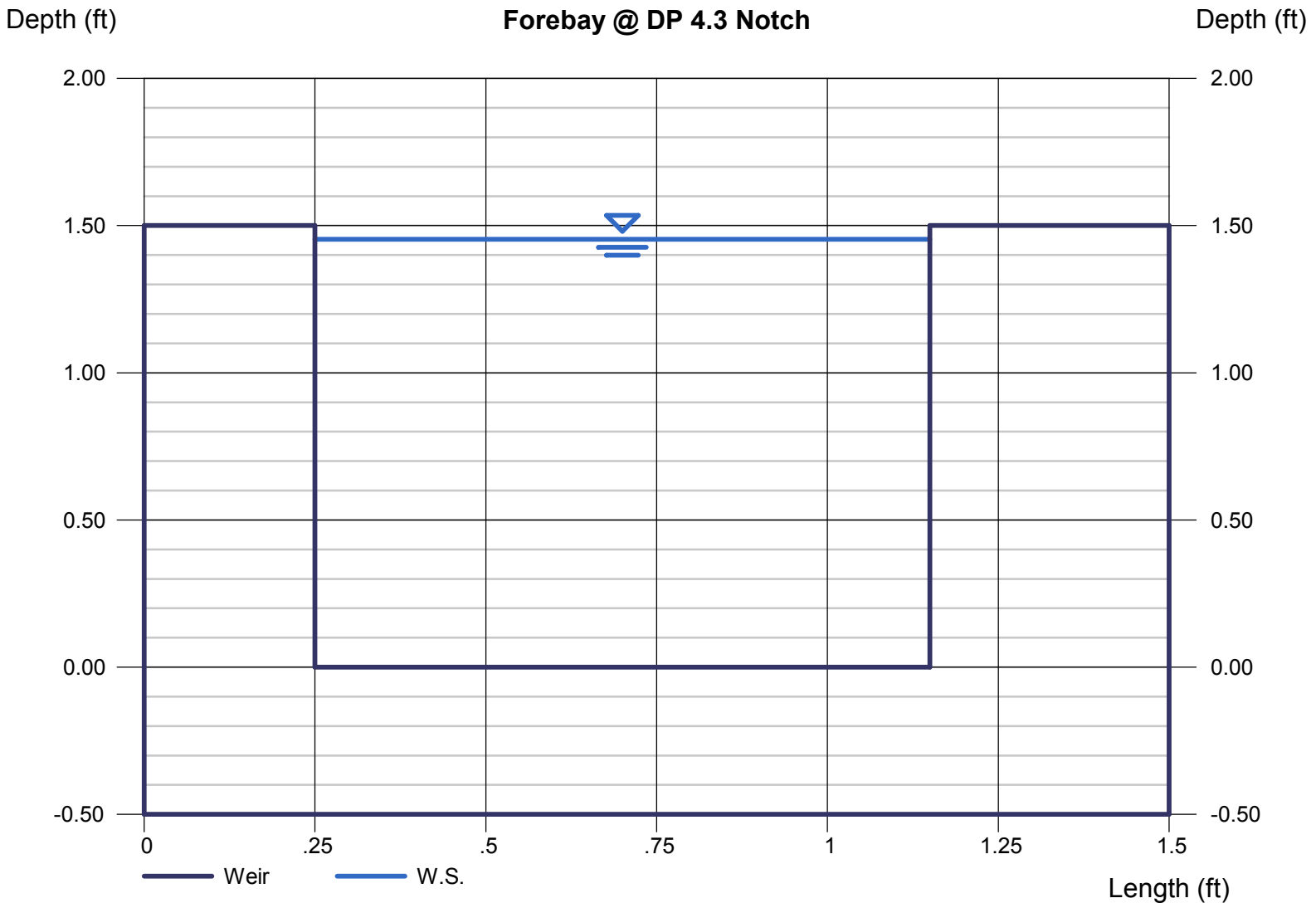
Crest = Sharp
Bottom Length (ft) = 0.90
Total Depth (ft) = 1.50

Highlighted

Depth (ft) = 1.45
Q (cfs) = 5.250
Area (sqft) = 1.31
Velocity (ft/s) = 4.01
Top Width (ft) = 0.90

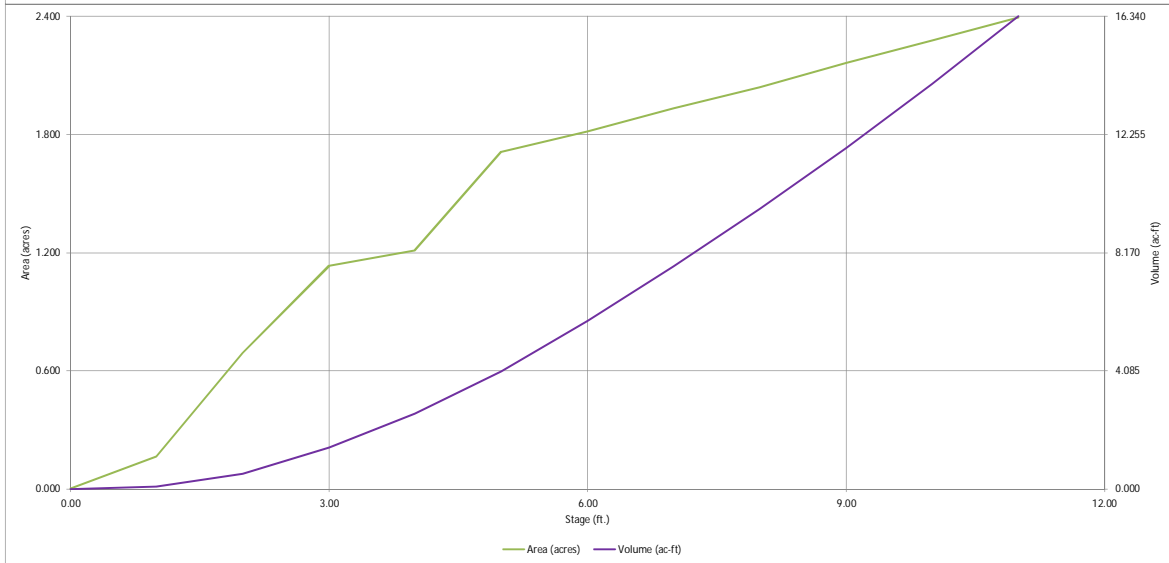
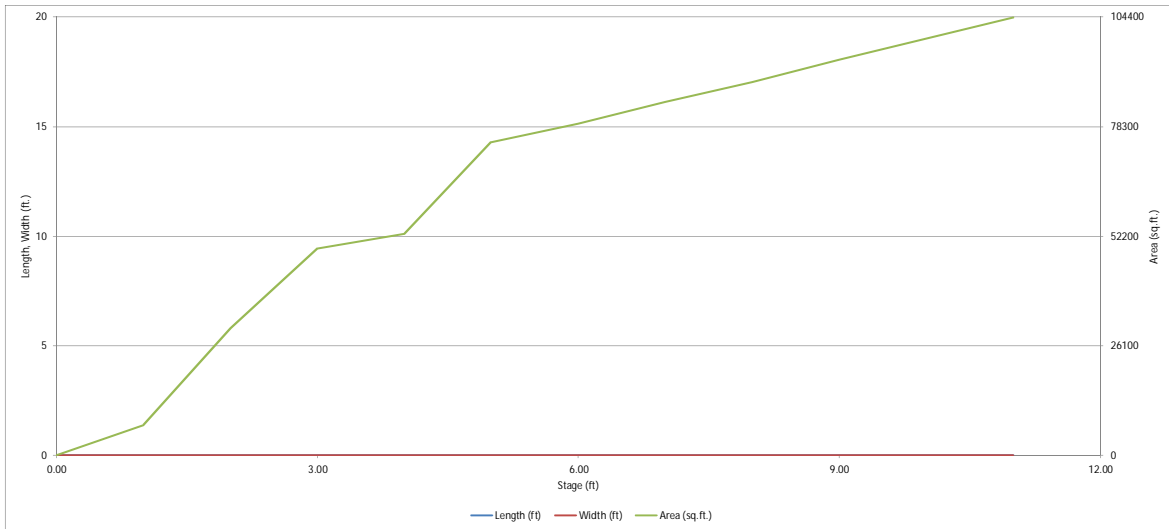
Calculations

Weir Coeff. Cw = 3.33
Compute by: Known Q
Known Q (cfs) = 5.25



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)





El Paso County MS4 Post Construction Detention / Water Quality Facility Documentation Form

This document **must be completed and submitted** with required attachments to the County for projects requiring a detention and/or a water quality facility. A separate completed form must be submitted for each facility.

Project name:

Owner name:

Location Address:

Latitude and Longitude:

Assessor's Parcel #: Section: Township: Range:

Expected Completion date:

Project acreage: Design Ponding Acres: Design Storm:

Design Engineer Email Address:

To ensure compliance with C.R.S. 37-92-602(8), the completed Stormwater Detention and Infiltration Design Data Sheet **must be attached**. The form can be found here: <https://maperture.digitaldataservices.com/gvh/?viewer=cswdiff#> (click on Download SDI Design Data Sheet)

List all permanent water quality control measure(s) (EDBs, rain gardens, etc):

For all projects for which the constrained redevelopment sites standard is applied, provide an explanation of why it is not practicable to meet the full design standards.

Attach Operations and Maintenance (O&M) Plan describing the operation and maintenance procedures that ensure the long-term observation, maintenance, and operation of control measure(s), including routine inspection frequencies and maintenance activities. If multiple, different water quality control measures are used at the same location, a separate O & M Plan must be provided for each facility.

Attach Private Detention Basin / Stormwater Quality Best Management Practice Maintenance Agreement and Easement addressing maintenance of BMPs that shall be binding on all subsequent owners of the permanent BMPs.

- Attachments:**
- Stormwater Detention and Infiltration Design Data Sheet
 - O & M Plan
 - Maintenance and Access Agreement

Review Engineer
EPC Project File No.



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Owner name:

Location Address:

Latitude and Longitude:

Assessor's Parcel #: Section: Township: Range:

Expected Completion date:

Project acreage: Design Ponding Acres: Design Storm:

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Attachments:

- Stormwater Detention and Infiltration Design Data Sheet
- O & M Plan
- Maintenance and Access Agreement

Review Engineer

EPC Project File No.

Worksheet for Pond W5 Emergency Outfall

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.078
Channel Slope	0.100 ft/ft
Left Side Slope	3.000 H:V
Right Side Slope	3.000 H:V
Bottom Width	20.00 ft
Discharge	427.10 cfs
Results	
Normal Depth	24.0 in
Flow Area	52.0 ft ²
Wetted Perimeter	32.6 ft
Hydraulic Radius	19.1 in
Top Width	32.00 ft
Critical Depth	25.9 in
Critical Slope	0.076 ft/ft
Velocity	8.21 ft/s
Velocity Head	1.05 ft
Specific Energy	3.05 ft
Froude Number	1.136
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	24.0 in
Critical Depth	25.9 in
Channel Slope	0.100 ft/ft
Critical Slope	0.076 ft/ft

Worksheet for Pond W5 Emergency Outfall with Stilling Basin

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Channel Slope	0.005 ft/ft
Discharge	742.90 cfs

Section Definitions

Station (ft)	Elevation (ft)
0+00	6,956.50
0+01	6,946.00
0+19	6,944.00
0+26	6,944.00
0+35	6,946.50
0+40	6,945.98
0+60	6,945.98
0+82	6,952.00

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 6,956.50)	(0+82, 6,952.00)	0.078

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	62.7 in
Roughness Coefficient	0.078
Elevation	6,949.22 ft
Elevation Range	6,944.0 to 6,956.5 ft
Flow Area	248.3 ft ²
Wetted Perimeter	75.0 ft
Hydraulic Radius	39.7 in
Top Width	71.16 ft
Normal Depth	62.7 in
Critical Depth	36.6 in
Critical Slope	0.078 ft/ft
Velocity	2.99 ft/s
Velocity Head	0.14 ft

Worksheet for Pond W5 Emergency Outfall with Stilling Basin

Results

Specific Energy	5.36 ft
Froude Number	0.282
Flow Type	Subcritical

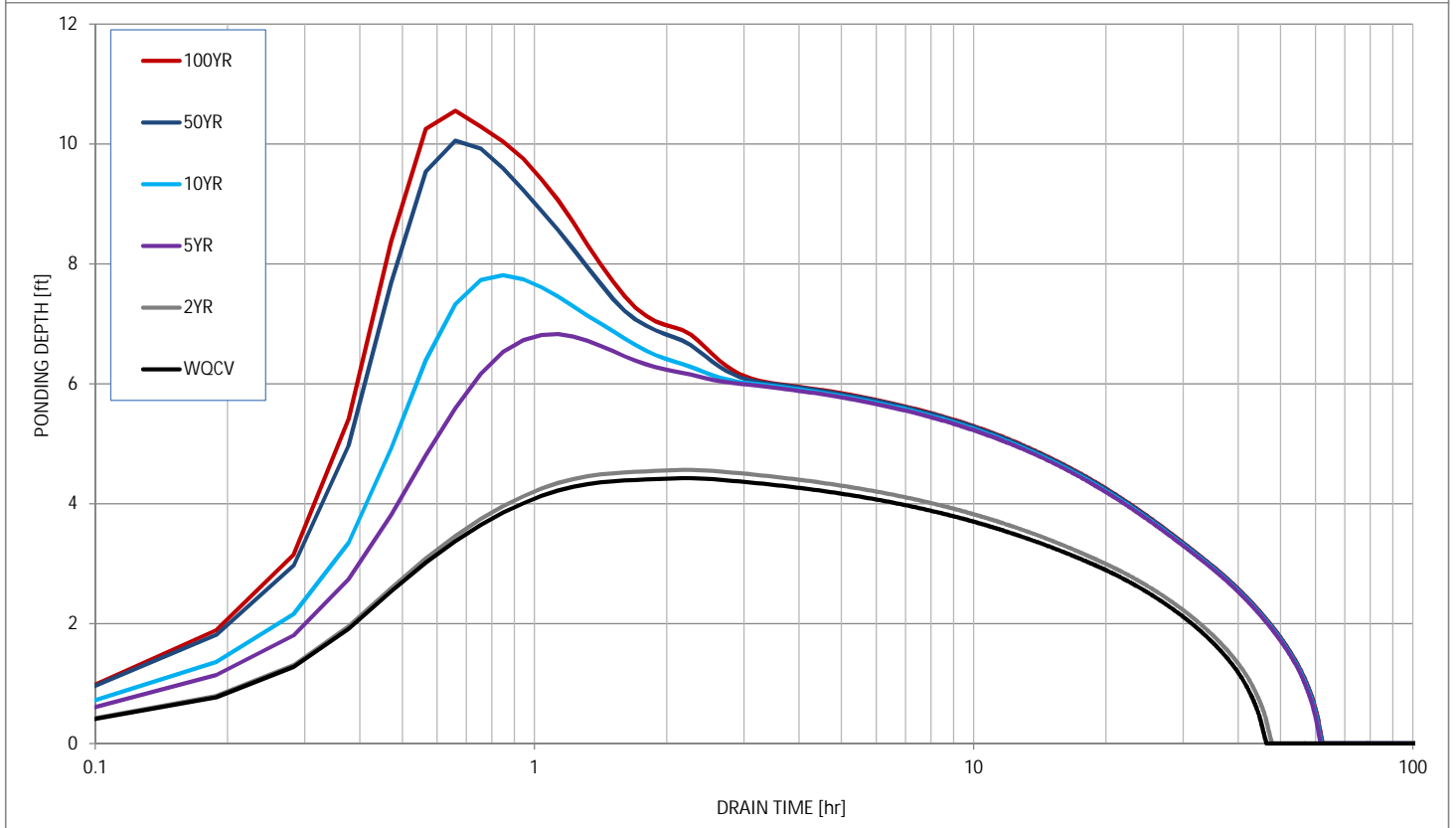
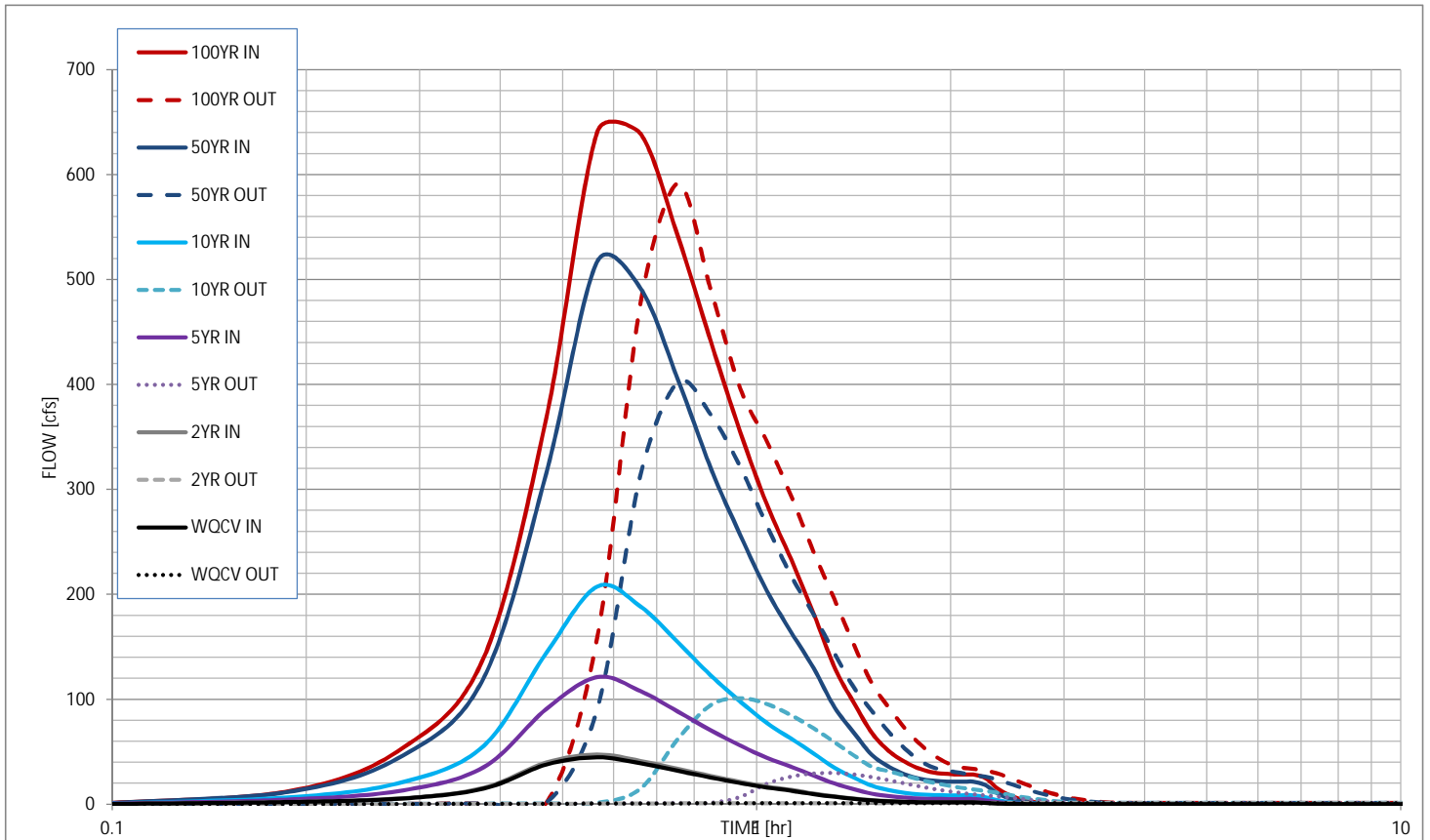
GVF Input Data

Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

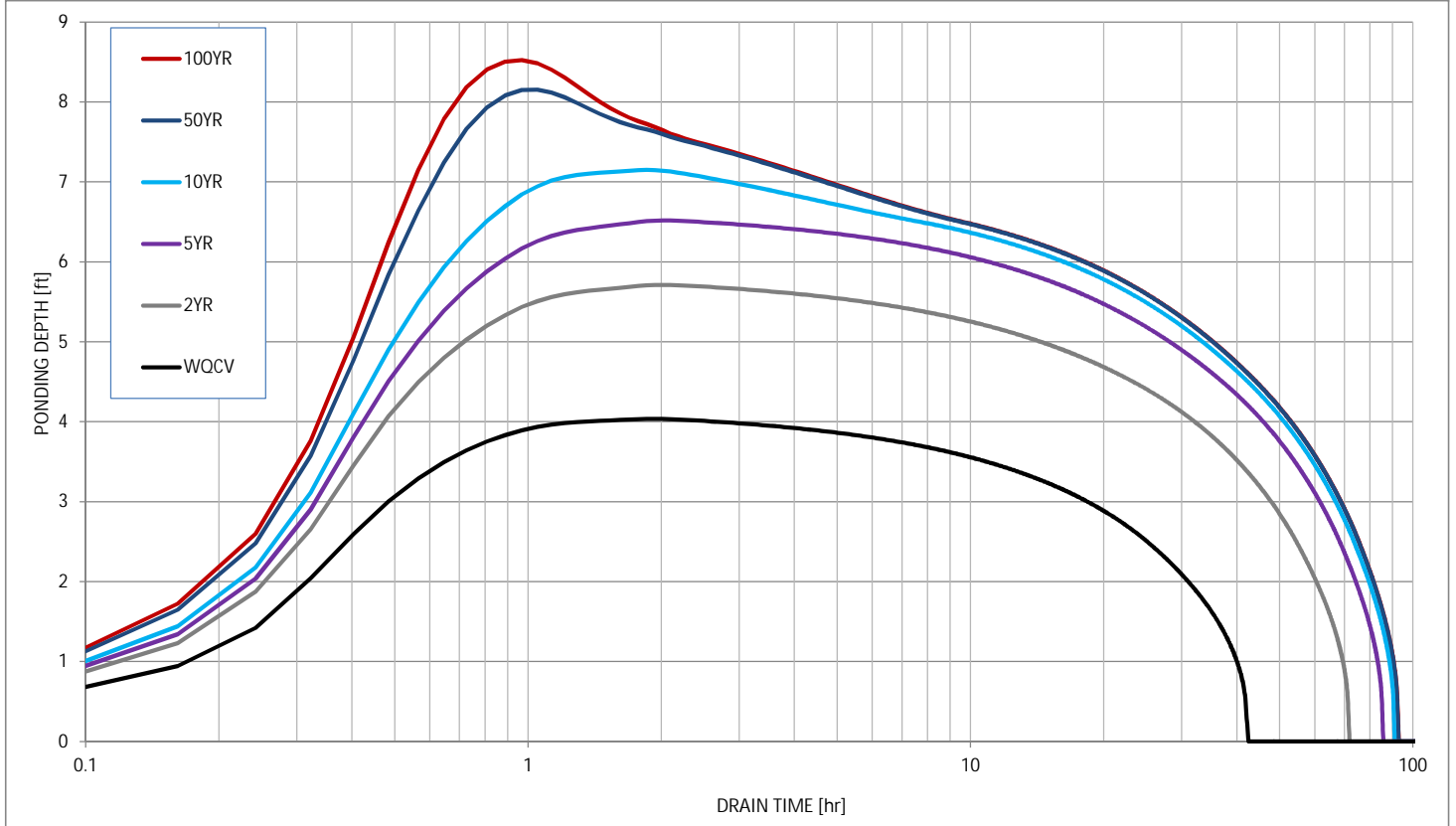
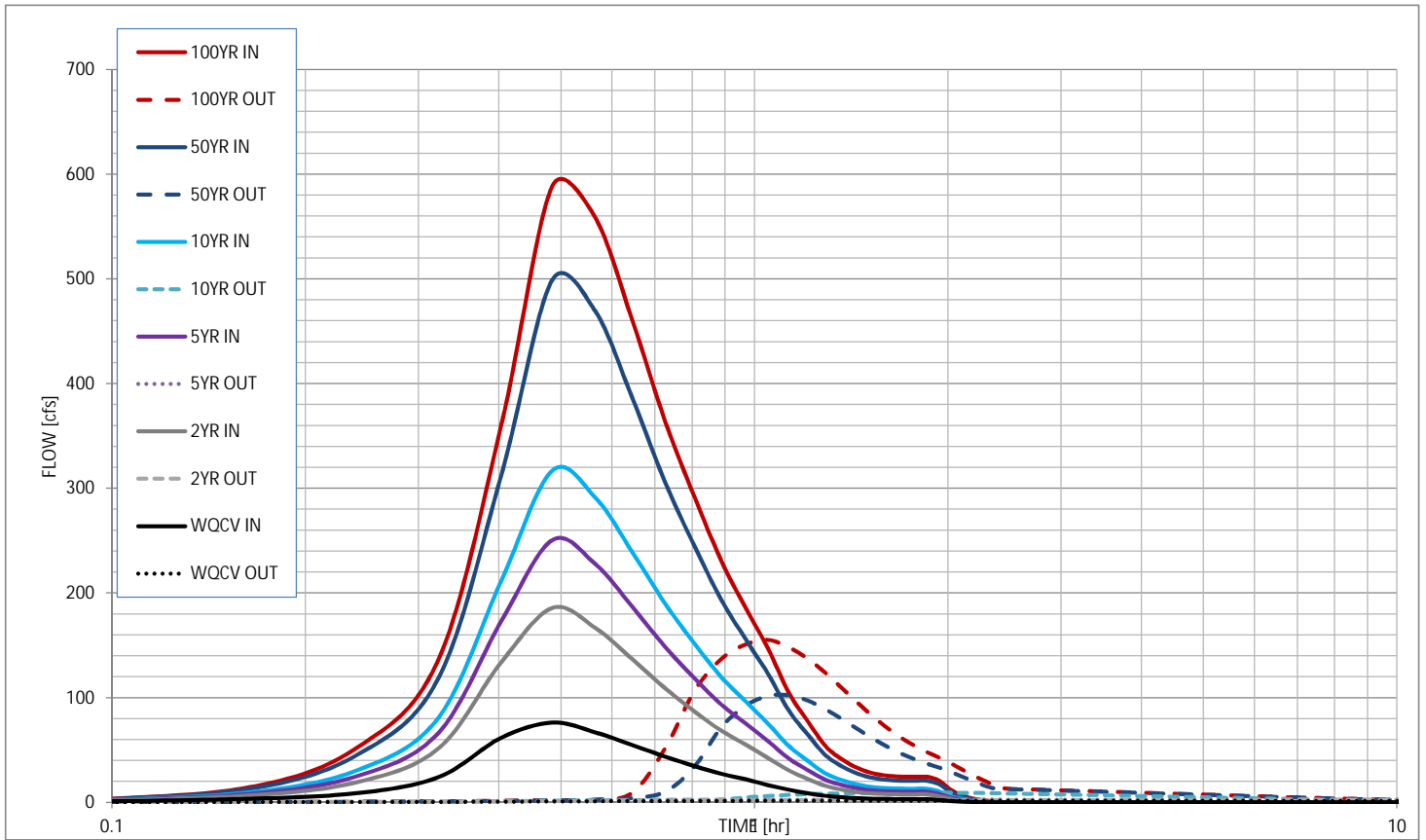
GVF Output Data

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	62.7 in
Critical Depth	36.6 in
Channel Slope	0.005 ft/ft
Critical Slope	0.078 ft/ft

Stormwater Detention and Infiltration Design Data Sheet

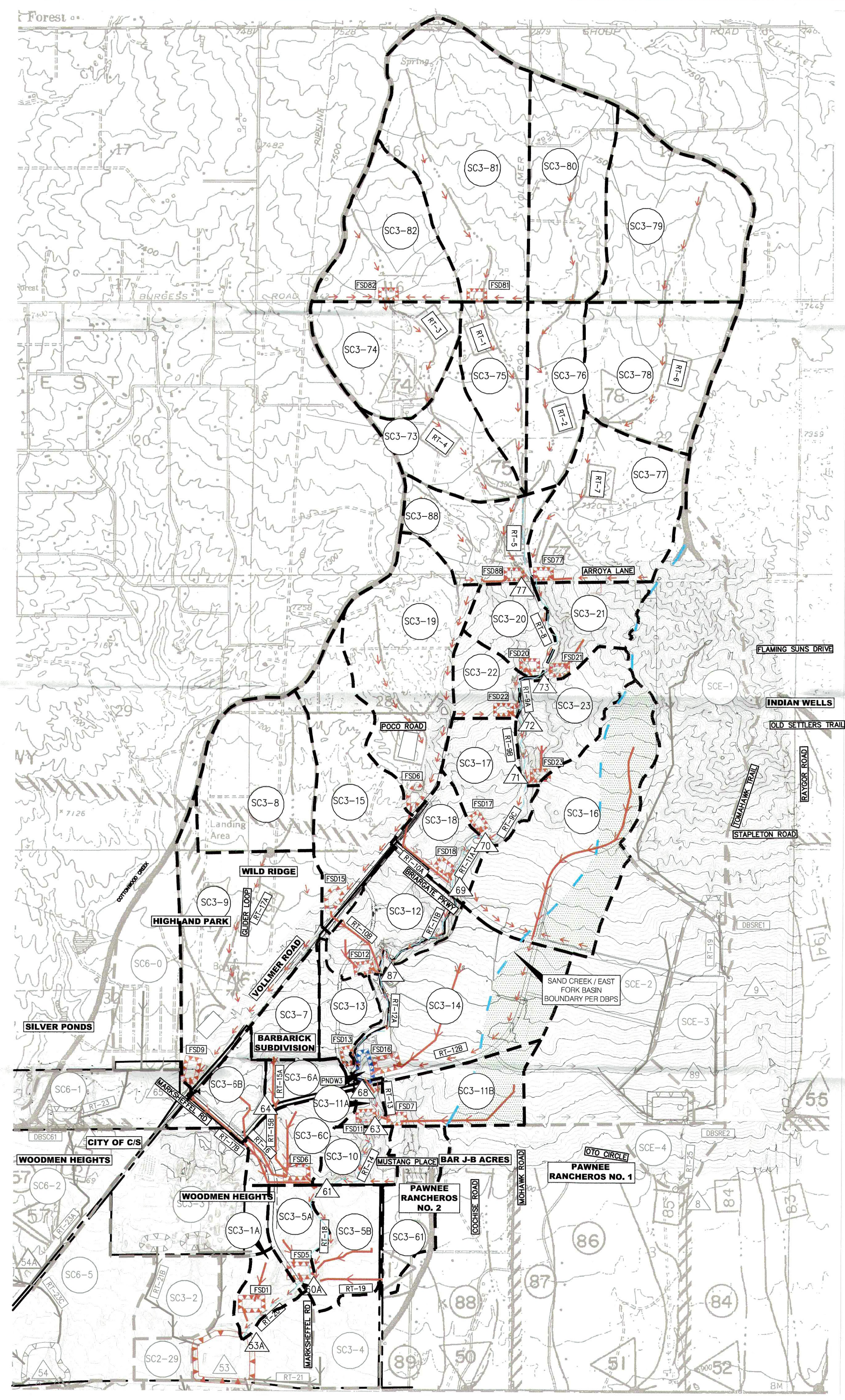


Stormwater Detention and Infiltration Design Data Sheet



APPENDIX D
REFERENCE MATERIALS

File: D:\08035A\Sand Creek Study\Long\Eng Exhibits\Proposed Conditions Watershed Work Map.dwg Plotstamp: 10/21/2016 2:46 PM

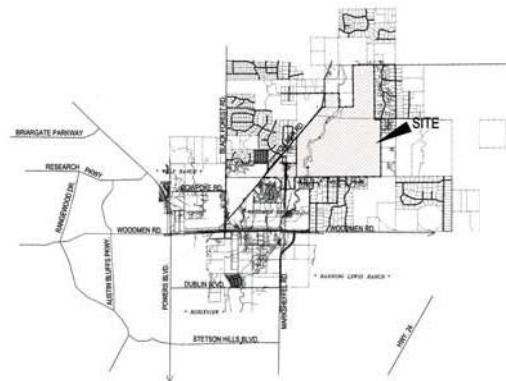


BASIN SUMMARY									
BASIN	CN	AREA (ac)	AREA (sq mi)	Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₂₅ (cfs)	Q ₅₀ (cfs)	Q ₁₀₀ (cfs)
SC3-1A	73	27.8	0.085	31.4	45.0	63.8	88.5	110.3	133.1
SC3-5A	84	39.1	0.061	40.6	53.7	71.0	92.4	110.6	129.1
SC3-5B	81	63.0	0.098	53.8	73.0	98.5	130.8	158.6	187.0
SC3-6A	88	49.3	0.077	61.4	79.3	102.2	130.1	153.6	177.1
SC3-6B	85	30.9	0.048	32.9	43.4	57.0	73.9	88.2	102.7
SC3-6C	82	58.0	0.091	53.9	72.5	97.1	128.0	154.5	181.5
SC3-7	88	45.7	0.071	54.0	69.9	90.3	115.2	136.2	157.2
SC3-8	63	143.4	0.224	28.0	45.5	71.1	106.4	138.9	173.8
SC3-9	66	217.4	0.340	49.2	76.2	115.0	168.1	217.1	269.5
SC3-10	63	36.0	0.056	7.6	12.3	19.4	29.1	38.0	47.7
SC3-11A	70	10.7	0.017	5.3	7.8	11.3	15.9	20.0	24.3
SC3-11B	80	76.6	0.120	59.4	81.3	110.8	148.1	180.5	213.7
SC3-12	81	88.2	0.138	77.8	105.6	142.5	189.1	229.1	270.0
SC3-13	85	41.0	0.064	43.9	57.8	76.0	98.5	117.6	136.9
SC3-14	80	199.4	0.311	162.1	221.4	300.7	401.5	488.6	577.7
SC3-15	65	147.6	0.231	32.8	51.8	79.4	117.0	151.5	188.3
SC3-16	79	224.1	0.350	150.7	208.5	286.6	386.6	473.7	563.4
SC3-17	71	70.6	0.110	37.2	53.9	77.7	109.9	138.8	169.2
SC3-18	81	53.7	0.084	49.3	67.1	91.0	121.2	147.3	174.0
SC3-19	63	191.5	0.299	37.2	60.5	94.6	141.6	184.9	231.4
SC3-20	63	50.3	0.079	12.2	19.6	30.4	45.2	58.9	73.5
SC3-21	63	62.6	0.098	14.3	23.1	36.1	53.9	70.3	87.9
SC3-22	63	40.6	0.063	9.2	14.9	23.2	34.6	45.2	56.5
SC3-23	64	81.3	0.127	19.5	31.2	48.2	71.6	93.0	116.0
SC3-61	63	65.6	0.102	13.7	22.0	34.4	51.6	67.6	84.8
SC3-73	63	90.0	0.141	16.4	26.4	41.3	62.1	81.3	102.0
SC3-74	63	119.7	0.187	22.3	36.5	57.3	85.9	112.3	140.7
SC3-75	63	79.3	0.124	13.6	22.1	34.6	51.9	67.8	84.9
SC3-76	63	86.4	0.135	14.2	23.1	36.4	54.6	71.4	89.6
SC3-77	63	163.8	0.256	33.0	53.4	83.2	124.1	161.9	202.4
SC3-78	63	155.6	0.243	28.1	45.3	70.6	106.2	139.1	174.5
SC3-79	63	189.0	0.295	34.9	57.0	89.5	134.3	175.6	220.1
SC3-80	63	147.7	0.231	27.3	44.3	69.6	104.5	136.8	171.4
SC3-81	63	262.9	0.411	48.3	78.3	123.1	184.9	242.0	303.4
SC3-82	63	117.8	0.184	25.0	40.6	63.7	95.5	125.0	156.6
SC3-88	63	87.2	0.136	18.3	29.4	46.2	69.4	90.9	113.9

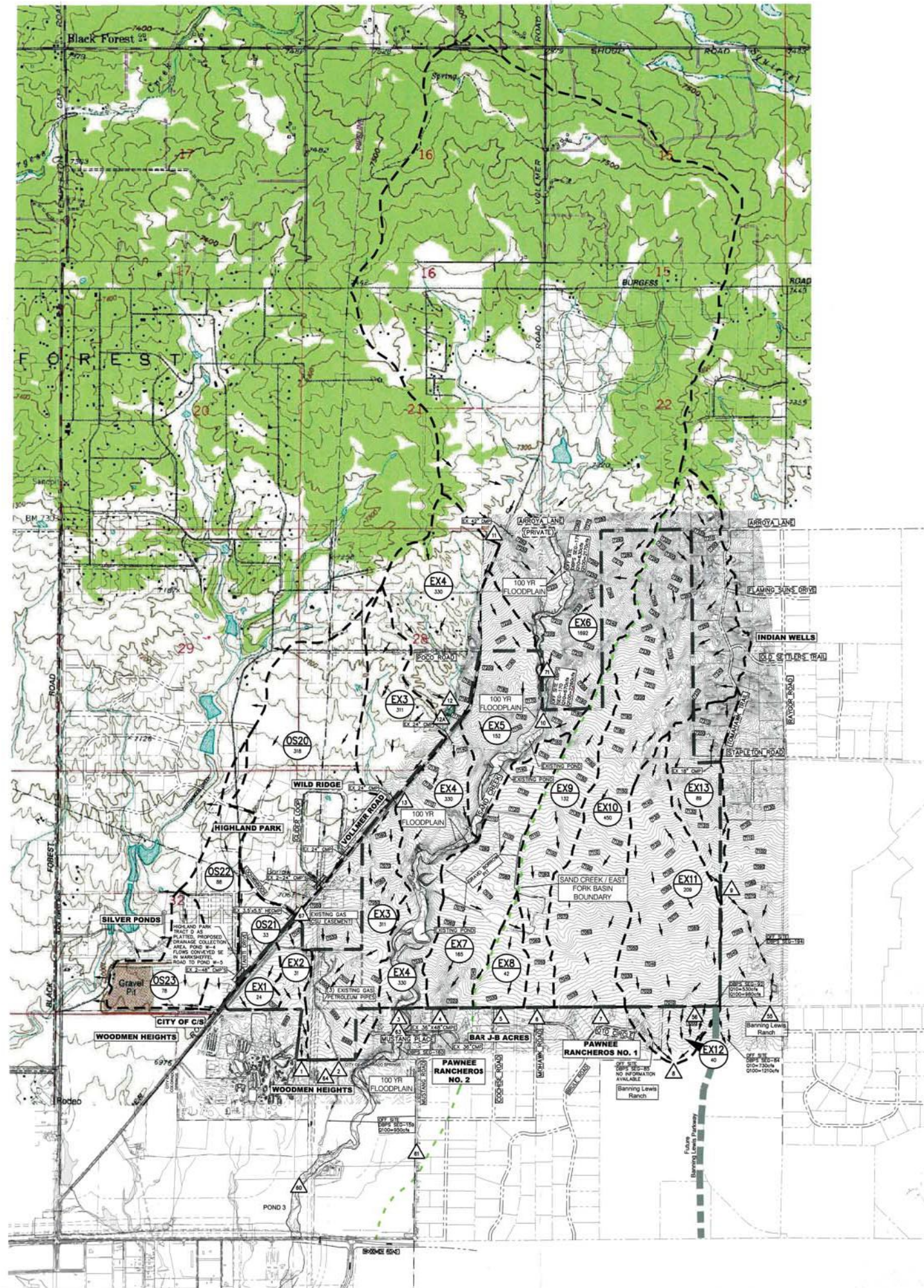
DESIGN POINT SUMMARY									
DESIGN POINT	AREA (ac)	Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₂₅ (cfs)	Q ₅₀ (cfs)	Q ₁₀₀ (cfs)	LOCATION	
DP-74	0.371	22.3	36.5	61.8	136.5	192.8	249.7		
DP-75	1.413	82.4	139.5	230.2	521.6	724.3	928.7		
DP-77	2.343	139.3	231.4	430.3	793.5	1118.3	1486.8	ARROYA LANE X-ING	
DP-78	0.538	59.7	98.4	154.0	232.6	306.2	385.3		
DP-73	2.520	137.4	236.9	446.0	806.4	1145.0	1521.9		
DP-72	2.583	134.9	236.2	443.8	793.7	1156.5	1501.6	POCO ROAD X-ING	
DP-71	2.710	135.1	242.0	452.4	803.1	1154.4	1523.3	STERLING RANCH NORTHERN BNDRY	
DP-70	2.820	134.4	246.1	462.4	808.9	1177.6	1543.2		
DP-69	3.203	134.3	256.6	499.1	864.2	1262.7	1673.2	BRIARGATE PARKWAY X-ING	
DP-87	3.572	133.9	255.6	541.2	922.7	1371.3	1836.4		
DP-68	4.297	105.0	202.9	462.9	914.3	1302.7	1653.2	STERLING RANCH ROAD X-ING	
DP-64	0.148	114.5	148.0	191.1	243.7	288.0	332.4		
DP-63	4.434	105.1	203.2	471.7	932.6	1323.3	1955.5	COLORADO SPRINGS/EL PASO BNDRY	
DP-61	5.341	106.6	206.3	531.1	1051.2	1524.3	2093.4	MARKSHEFFEL X-ING	
DP-60A	5.602	111.0	212.4	543.2	1073.9	1558.5	2001.4		
DP-53A	5.687	110.4	212.3	546.2	1078.2	1567.6	2017.3	SAND CREEK AND POND 3	

WATER QUALITY & DETENTION POND SUMMARY									
FSD#	STORM EVENT (YR)	2	5	10	25	50	100		
FSD1									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		31.4	45.0	63.8	88.5	110.3	133.1		
ALLOWABLE RELEASE (CFS)		0.1	1.7	3.3	10.9	17.5	25.5		
MODELED RELEASE (CFS)		0.2	1.7	3.3	10.9	17.5	25.5		
STORED VOLUME (AC-FT)		2.4	2.6	3.0	3.6	4.2	4.9		
FSD5									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		40.6	53.7	71.0	92.4	110.6	129.1		
ALLOWABLE RELEASE (CFS)		0.1	1.4	2.6	11.3	19.8	30.2		
MODELED RELEASE (CFS)		0.1	1.4	2.6	11.2	19.7	30.1		
STORED VOLUME (AC-FT)		3.0	3.2	3.8	4.1	4.7	5.2		
FSD6									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		196.6	258.6	339.2	438.9	523.4	608.8		
ALLOWABLE RELEASE (CFS)		0.6	8.3	15.9	60.5	101.7	151.7		
MODELED RELEASE (CFS)		0.6	8.3	15.9	60.4	101.4	151.6		
STORED VOLUME (AC-FT)		15.4	16.1	18.3	20.6	23.2	26.2		
FSD9									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		67.9	112.8	174.2	259.1	342.0	429.4		
ALLOWABLE RELEASE (CFS)		1.7	24.9	49.8	141.1	207.2	290.0		
MODELED RELEASE (CFS)		1.7	20.8	49.4	141.2	206.9	289.4		
STORED VOLUME (AC-FT)		9.0	9.0	10.0	11.3	13.0	14.5		
FSD11A									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		5.3	7.8	11.3	15.9	20.0	24.3		
ALLOWABLE RELEASE (CFS)		0.1	1.5	3.2	7.5	9.7	12.4		
MODELED RELEASE (CFS)		0.2	0.9	3.0	7.6	9.6	12.2		
STORED VOLUME (AC-FT)		0.3	0.3	0.4	0.4	0.5	0.6		
FSD11B									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		59.4	81.3	110.8	148.1	180.5	213.7		
ALLOWABLE RELEASE (CFS)		0.3	4.5	8.7	29.6	47.7	69.6		
MODELED RELEASE (CFS)		0.3	4.5	8.6	29.5	47.7	69.0		
STORED VOLUME (AC-FT)		4.8	4.9	5.5	6.4	7.3	8.2		
FSD12									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		77.8	105.6	142.5	189.1	229.1	270.0		
ALLOWABLE RELEASE (CFS)		0.9	13.2	26.7	62.0	80.2	103.2		
MODELED RELEASE (CFS)		0.9	9.0	26.7	61.9	80.1	103.1		
STORED VOLUME (AC-FT)		5.2	5.5	5.8	6.7	7.8	8.9		

WATER QUALITY & DETENTION POND SUMMARY									
FSD#	STORM EVENT (YR)	2	5	10	25	50	100		
FSD13									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		43.9	57.8	76.0	98.5	117.6	136.9		
ALLOWABLE RELEASE (CFS)		0.4	6.1	12.3	28.6	37.0	47.6		
MODELED RELEASE (CFS)		0.4	4.2	12.3	28.6	36.9	47.2		
STORED VOLUME (AC-FT)		3.1	3.1	3.3	3.8	4.4	5.0		
FSD15									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		32.8	51.8	79.4	117.0	151.5	188.3		
ALLOWABLE RELEASE (CFS)		1.2	17.5	35.7	85.4	111.7	145.8		
MODELED RELEASE (CFS)		1.2	13.1	35.7	85.4	111.7	145.7		
STORED VOLUME (AC-FT)		3.3	3.3	3.6	4.0	4.5	5.0		
FSD16									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		248.6	362.6	503.9	692.0	852.3	1016.5		
ALLOWABLE RELEASE (CFS)		1.5	21.5	41.9	143.4	231.0	338.7		
MODELED RELEASE (CFS)		1.5	21.5	41.8	143.2	230.8	338.7		
STORED VOLUME (AC-FT)		25.5	26.0	29.7	34.2	39.0	43.9		
FSD17									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		37.2	53.9	77.7	109.9	138.8	169.2		
ALLOWABLE RELEASE (CFS)		0.7	11.1	22.5	52.0	67.2	86.3		
MODELED RELEASE (CFS)		0.7	7.3	22.4	52.0	67.3	86.3		
STORED VOLUME (AC-FT)		2.3	2.3	2.5	3.0	3.6	4.2		
FSD18									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		49.3	67.1	91.0	121.2	147.3	174.0		
ALLOWABLE RELEASE (CFS)		0.6	9.2	18.4	42.2	54.6	69.9		
MODELED RELEASE (CFS)		0.6	6.6	18.4	42.2	54.6	69.6		
STORED VOLUME (AC-FT)		3.2	3.2	3.4	4.0	4.7	5.3		
FSD19									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		37.2	60.5	94.6	141.6	184.9	231.4		
ALLOWABLE RELEASE (CFS)		1.7	24.6	50.3	118.4	153.3	198.4		
MODELED RELEASE (CFS)		1.7	18.6	50.3	118.1	153.2	198.2		
STORED VOLUME (AC-FT)		3.4	3.4	3.7	4.1	4.5	5.1		
FSD20									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		12.2	19.6	30.4	45.2	58.9	73.5		
ALLOWABLE RELEASE (CFS)		0.6	8.4	16.8	38.8	50.1	64.2		
MODELED RELEASE (CFS)		0.6	8.4	16.6	38.8	50.0	63.8		
STORED VOLUME (AC-FT)		0.8	0.8	0.9	1.0	1.1	1.3		
FSD21									
STORM EVENT (YR)		2	5	10	25	50	100		
PEAK INFLOW (CFS)		14.3	23.1	36.1	53.9	70.3	8		



STERLING RANCH
N.T.S.



HISTORIC CONDITION

BASIN SUMMARY			
BASIN	AREA (ACRES)	Q ₁ (CFS)	Q ₁₀₀ (CFS)
EX-1	24	3	40
EX-2	31	3	45
EX-3	311	49	341
EX-4	330	71	353
EX-5	152	14	209
EX-6	1692	118	2168
EX-7	165	12	197
EX-8	42	4	64
EX-9	132	11	149
EX-10	450	48	474
EX-11	209	17	261
EX-12	40	5	65
EX-13	89	6	114
OS-20	318	61	310
OS-21	33	8	38
OS-22	88	18	91
OS-23	78	34	84

* NOTE: BASINS OS-22 & OS-23 NOT PART OF THIS REPORT. FLOWS FOLLOW HISTORIC PATTERNS ON THE WESTSIDE OF VOLLMER ROAD.

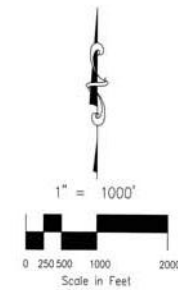
HISTORIC CONDITION

DESIGN POINTS						
DESIGN POINT	SQ. MI.	Q ₁ (CFS)	Q ₁₀₀ (CFS)	SQ. MI.	DBPS Q ₁₀₀	DBPS DP/D
1	0.09	5	84			
2	0.49	55	465	0.74	465	64
3	0.52	139	2610	4.33	2552	63
4	0.26	12	197			
5	0.07	4	64			
6	0.21	11	149			
7	0.70	48	474			
8	0.39	18	305			
9	0.14	6	114			
10	2.64	122	2245	3.27	2245	71
11	0.09	5	83			
12A	0.01	3	16			
12	0.27	10	200			
13	0.17	6	126			

* NOTE: SQ. MI. ARE NOT CONSTANT AT EACH DESIGN POINT DP-DBPS

* NOTE: DBPS FLOWS ARE FOR THE EXISTING CONDITION

NO DATA GIVEN IN DBPS



LEGEND

- EXISTING MDDP BASIN ACREAGE
- EXISTING FLOW RELEASE POINT
- FLOW DIRECTION
- BASIN BOUNDARY
- PROPERTY BOUNDARY
- EXISTING CONTOUR
- CULVERT PIPE



CIVIL CONSULTANTS, INC.
102 E. PIKES PEAK AVE. STE 306
COLORADO SPRINGS, CO 80903
(719) 955-5465, FAX (719) 444-8427

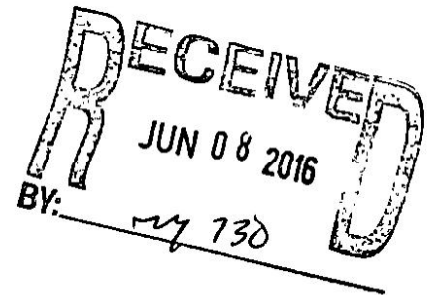
STERLING RANCH MDDP			
HISTORIC - DRAINAGE MAP			
PROJECT NO. 09-001	FILE: \\dwg\Dev\Plan\09001-MDDP HISTORIC	SCALE	DATE: 03/16/15
DESIGNED BY: VAS	CHECKED BY: VAS	HORIZ: 1"=500'	VERT: N/A
SHEET 1 OF 1			D1

**FINAL DRAINAGE REPORT**

For

**BARBARICK SUBDIVISION,
PORTIONS OF LOTS 1, 2 and LOTS 3 & 4
El Paso County, Colorado****Sand Creek Drainage Basin**

Prepared for:
**El Paso County Development Services
Engineering Division**



On Behalf of:
Wykota Construction
430 Beacon Light Road, Suite 130
Monument, CO 80132

Prepared by:

Matrix 
DESIGN GROUP

2435 Research Parkway, Suite 300
Colorado Springs, CO 80920
(719) 575-0100
Fax (719) 572-0208

June 6, 2016

15.789.001

Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin.

Gregory G. Shaner
Registered Professional Engineer
State of Colorado, No. 036307



SEAL

Developer's Statement:

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Wykota Construction

Business Name

By: _____

Justin Ballard
Justin Ballard

Title: _____
President

Address: _____
430 Beacon Light Road, Suite 130

Monument, CO 80132

El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Print Name — ~~FORE TENUKLE TRUMB~~
County Engineer / ECM Administrator

9 JUNE 2016

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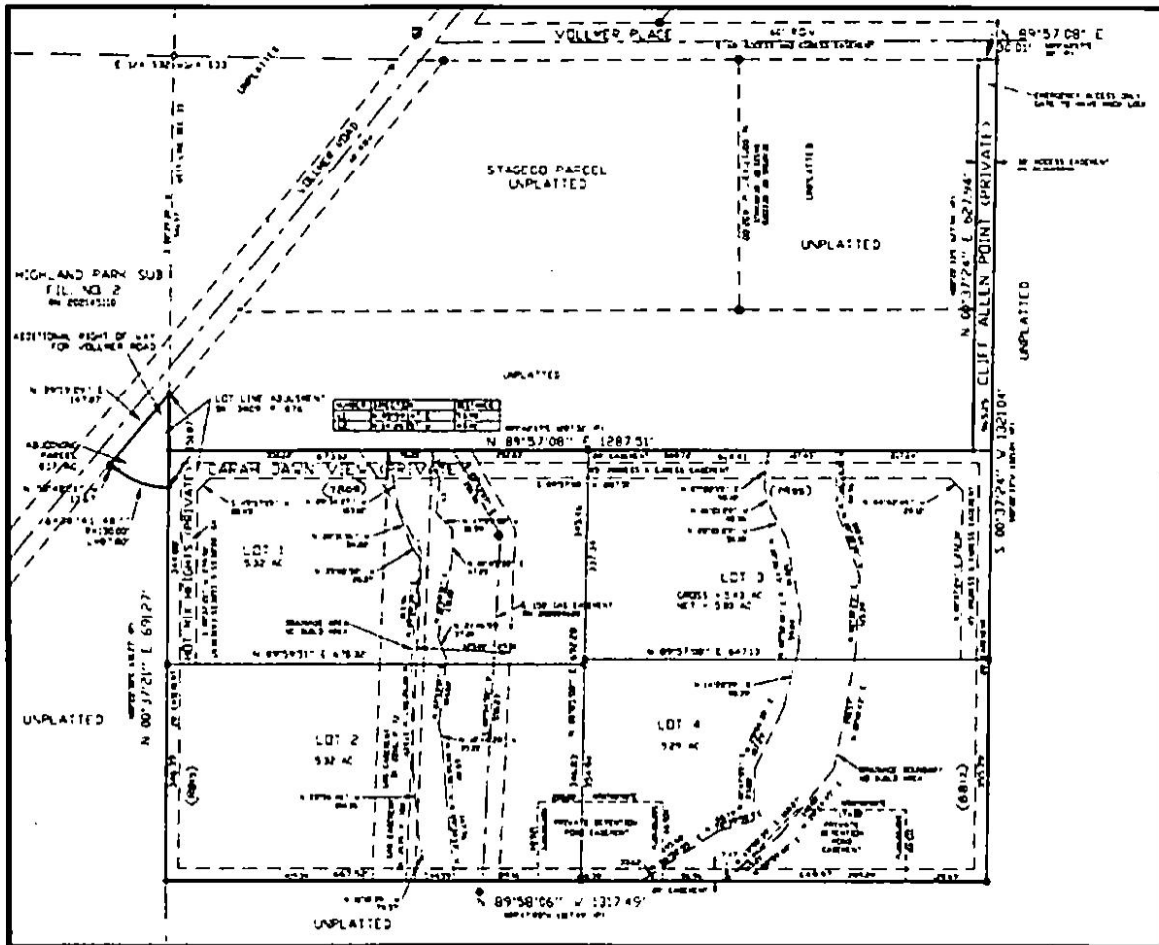
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Surrounding Developments. The following are the existing or planned general land uses adjacent to the property.

North: Un-platted parcels that contain commercial/industrial uses. Carah Dawn View is on the north side of the property.

East and South: Although this adjacent area is currently undeveloped, the Sterling Ranch Master Planned area is in the process of developing this area (future single family development).

West: This is an undeveloped, un-platted lot. Across Vollmer Road is a low density single family development (Highland Park, Fil 2).

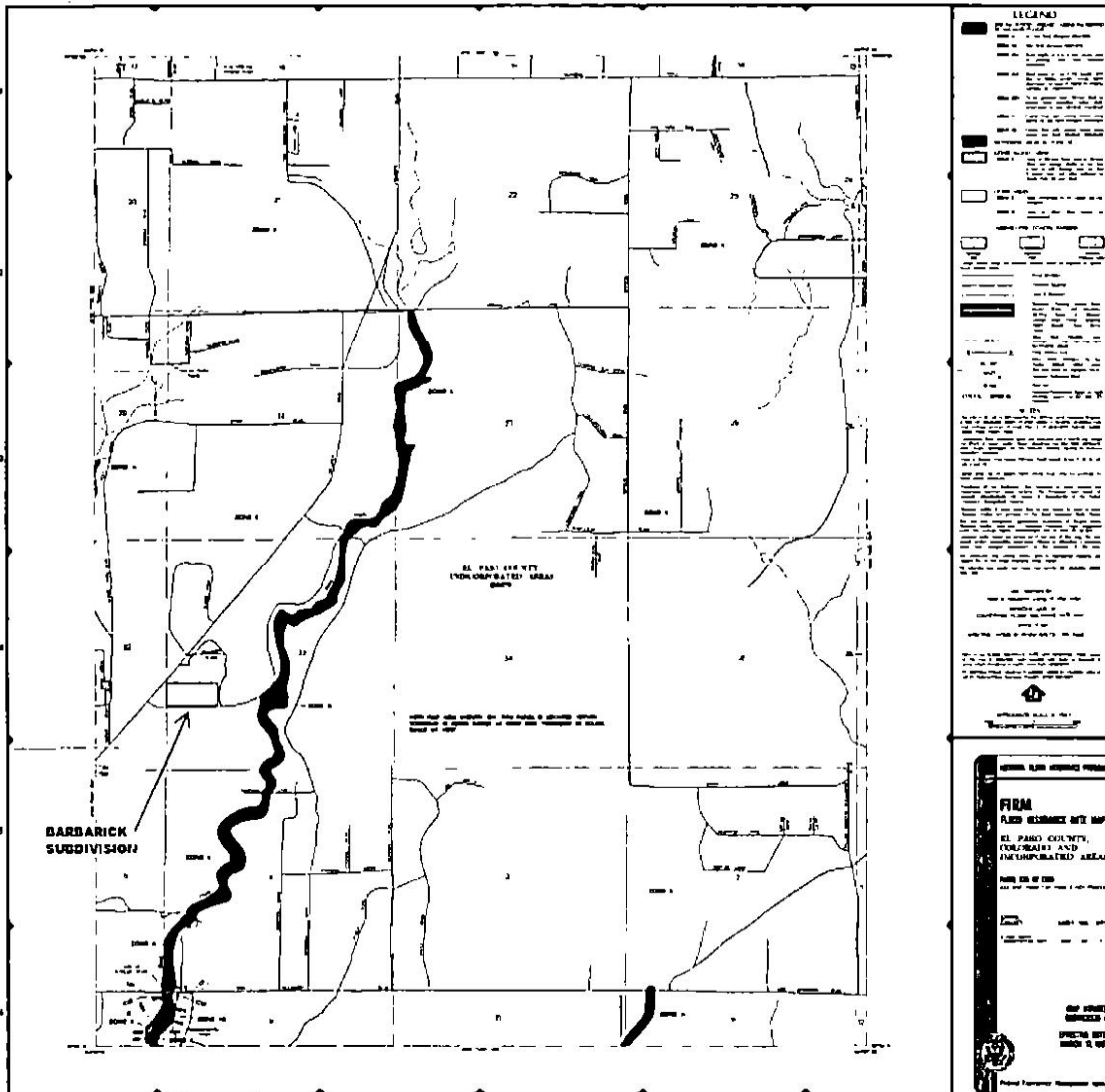


Barbarick Subdivision Plat

Property Description

1. **Major Drainage Way:** The entire site is located within the Sand Creek Drainage Basin. The Main Fork of Sand Creek is located about 1500 feet to the east. The site currently drains to the south into natural drainage ways that direct runoff to Sand Creek. The Sand Creek Drainage Basin is located in the northeastern portion of the City of Colorado Springs and El Paso County. The general drainage pattern of this larger basin flows to the southwest and ultimately feeds into Fountain Creek.
2. **Project Site Area:** This site is approximately 21.37 acres in area.
3. **Ground Cover:** This site is covered with native grasses.
4. **General Topography:** The site drains from north to the south with average grades ranging from 1% to 5%. There are two natural drainage ways that drain through these lots.
5. **Irrigation Facilities:** No known functioning irrigation facilities are located on the site. A small detention pond does exist to the northeast of the property; however, the outfall of this pond will be re-routed in order to direct runoff around the perimeter of the proposed development.
6. **Utilities:** Utilities in the project area include; but are not limited to, telephone, high pressure gas/petroleum and electrical lines. Water & wastewater service is provided through wells & individual septic systems. These utilities will be examined on a case-by-case basis and avoided where feasible, or they will be relocated. Any relocation of these utilities will be coordinated with the respective utility contact. Utility services will be extended into the site as necessary. There are large gas easements that run north-south through these lots. These easements contain one 6 inch and two 20 inch high pressure gas/petroleum pipelines. These Utility Easements will be no-build zones and grading will be fill only.
7. **On-Site Drainage Ways:** The plat shows two “Drainage Boundary – No Build Area(s)” draining through the subdivision. These are not regulated FEMA floodplains. The site development will include the installation of pass through culverts for offsite flows, and regraded. An amended plat has been completed for the removal of the no build areas, identification of new drainage easements, and relocation of water quality ponds.

8. **Floodplain Statement:** Review of the Flood Insurance Rate Map (FIRM) 535 (08041CO535 F), effective date March 17, 1997, published by the Federal Emergency Management Agency (FEMA) reveals that no portion of Barbaric Subdivision lie within any designated 100-year floodplain.



FEMA - Flood Insurance Rate Map (FIRM)

HYDROLOGIC AND HYDRAULIC ANALYSIS

Basin Description

The Barbarick Subdivision is located within the Sand Creek Drainage Basin. The tributary area that drains through the Barbarick Subdivision is developed, which includes large lot single-family parcels and some commercial/industrial land uses. Sub-basins were delineated using surveyed information, proposed contours and field observations. See the Drainage Basin Maps in the Appendix.

This study is in conformance with the following two approved Drainage Reports:

1. **Preliminary Drainage Report for Sterling Ranch-Phase 1, Sand Creek Drainage Basin**, M & S Civil Consultants, Inc., May 2015 AKA: "SR-PDR"
2. **Woodmen Storage Final Drainage Report, El Paso County**, Calibre Engineering, Inc., July 2004; Revised February, 2010; Revised May, 2010; Revised July, 2010 AKA: "WS-FDR"

This study is *not* in conformance with the following approved Drainage Report due to changes from the approved recent reports cited above that supercede the original report:

1. **Preliminary and Final Drainage Plan and Report, Barbarick Subdivision a Replat of Lot "D", McClintock Subdivision, El Paso County**, Oliver E. Watts, Consulting Engineer, Inc., August 15, 2007 AKA: "BS-FDR"

Design Criteria

This report has been prepared in accordance to the criteria set forth in the **City of Colorado Springs & El Paso County Drainage Criteria Manual, Volumes I and II**, dated November 1991 including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the **City of Colorado Springs & El Paso County Drainage Criteria Manual, Volumes I and II**, dated May 2014 (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the ECM, the **Urban Storm Drainage Criteria Manuals, Volumes 1-3**, published by the Urban Drainage and Flood Control District, (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 with some sections update November 2015), has also been used to supplement the ECM.

Hydrologic Criteria

Hydrologic analyses for the site have been completed using the Rational Method for on-site basins. The SCS Method was used in the referenced studies for the larger off-site basins (greater than 100 acres). The design storms for each method are:

- Initial Storm = 5-Year Storm
- Major Storm = 100-Year Storm

Rational Method: The Rational Method will be utilized to evaluate smaller basins (under 100 acres). This methodology is used for the design of localized facilities such as inlets, storm drain, drainage swales and detention:

Rational Method peak flow rate equation (cfs): $Q=C*I*A$

- Where: Q = Maximum runoff rate in cubic feet per second (cfs)
- C = Runoff coefficient
- I = Average rainfall intensity in inches per hour
- A = Area of drainage sub-basin in acres

Runoff Coefficient

Rational Method coefficients are derived from UDFCD Vol 1 (Chapter 6 – Runoff, 2016-01 Rev) for the various land uses, including parking areas, drives, walks, roofs, lawns and open space areas. The Runoff Coefficients associated with these land uses also have a corresponding impervious value that is used in the detention calculations. The Rational Method Coefficients used in this study include:

<u>Land Use or Surface Type</u>	<u>% Impervious</u>	<u>Runoff Coefficient (B Soils)</u>	
		<u>(5-Year)</u>	<u>(100-Year)</u>
Greenbelts/Agricultural	2%	.03	.46
Gravel (packed)	40%	.37	.65
Drives & Walks	90%	.84	.90

Table 6-3. Recommended percentage imperviousness values

Land Use or Surface Characteristics	Percentage Imperviousness (%)
Business:	
Downtown Areas	95
Suburban Areas	75
Residential:	
Single-family	
2.5 acres or larger	12
0.75 – 2.5 acres	20
0.25 – 0.75 acres	30
0.25 acres or less	45
Apartments	75
Industrial:	
Light areas	80
Heavy areas	90
Parks, cemeteries	10
Playgrounds	25
Schools	55
Railroad yard areas	50
Undeveloped Areas:	
Historic flow analysis	2
Greenbelts, agricultural	2
Off-site flow analysis (when land use not defined)	45
Streets:	
Paved	100
Gravel (packed)	40
Drive and walks	90
Roofs	90
Lawns, sandy soil	2
Lawns, clayey soil	2

Table 6-5. Runoff coefficients, c

Total or Effective % Imperviousness	NRCS Hydrologic Soil Group A					
	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
2%	0.02	0.02	0.02	0.02	0.02	0.17
5%	0.04	0.05	0.05	0.05	0.05	0.19
10%	0.09	0.09	0.09	0.09	0.1	0.23
15%	0.13	0.14	0.14	0.14	0.14	0.28
20%	0.18	0.19	0.19	0.19	0.19	0.32
25%	0.22	0.23	0.24	0.24	0.24	0.36
30%	0.27	0.28	0.28	0.28	0.29	0.4
35%	0.31	0.33	0.33	0.33	0.33	0.44
40%	0.36	0.37	0.38	0.38	0.38	0.48
45%	0.4	0.42	0.42	0.42	0.43	0.52
50%	0.45	0.47	0.47	0.47	0.48	0.56
55%	0.49	0.51	0.52	0.52	0.52	0.6
60%	0.53	0.56	0.56	0.57	0.57	0.64
65%	0.58	0.6	0.61	0.61	0.62	0.68
70%	0.62	0.65	0.66	0.66	0.67	0.72
75%	0.67	0.7	0.71	0.71	0.71	0.76
80%	0.71	0.74	0.75	0.76	0.76	0.8
85%	0.76	0.79	0.8	0.8	0.81	0.84
90%	0.8	0.84	0.85	0.85	0.86	0.88
95%	0.85	0.88	0.89	0.9	0.9	0.92
100%	0.89	0.93	0.94	0.94	0.95	0.96
Total or Effective % Imperviousness	NRCS Hydrologic Soil Group B					
2%	0.02	0.02	0.14	0.24	0.38	0.46
5%	0.04	0.05	0.17	0.27	0.39	0.48
10%	0.09	0.09	0.21	0.3	0.42	0.5
15%	0.13	0.14	0.25	0.34	0.45	0.53
20%	0.18	0.19	0.29	0.37	0.48	0.55
25%	0.22	0.23	0.33	0.41	0.51	0.58
30%	0.27	0.28	0.37	0.44	0.54	0.6
35%	0.31	0.33	0.41	0.48	0.57	0.63
40%	0.36	0.37	0.45	0.51	0.6	0.65
45%	0.4	0.42	0.49	0.55	0.63	0.67
50%	0.45	0.47	0.53	0.58	0.66	0.7
55%	0.49	0.51	0.57	0.62	0.69	0.72
60%	0.53	0.56	0.61	0.65	0.72	0.75
65%	0.58	0.6	0.65	0.69	0.75	0.77
70%	0.62	0.65	0.69	0.72	0.78	0.8
75%	0.67	0.7	0.73	0.76	0.81	0.82
80%	0.71	0.74	0.77	0.79	0.84	0.85
85%	0.76	0.79	0.81	0.83	0.87	0.87
90%	0.8	0.84	0.85	0.86	0.89	0.9
95%	0.85	0.88	0.89	0.9	0.92	0.92
100%	0.89	0.93	0.94	0.94	0.95	0.94

Time of Concentration

The time of concentration (T_c) for the Rational Method was calculated by methods derived from the UDFCD. The time of concentration consists of an initial time or overland flow time (t_i) plus the travel time (t_t) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an initial time or overland flow time (t_i)

plus the time of travel (t_t) in concentrated form, such as a swale or drainageway. A minimum T_c of 5 minutes and 10 minutes were used for the final calculations in developed and undeveloped conditions, respectively.

Storm Drain Systems

All proposed storm drain infrastructure will be located within private property and will be owned and maintained by the property owner.

The storm drain hydraulics is analyzed using *Bentley's FlowMaster*, *CulvertMaster* & *StormCAD* design software. Colorado Department of Transportation (CDOT) type inlets will be used where necessary.

The designated outfall locations for the proposed on-site storm drains are the natural drainage ways at the south end of the property. The proposed storm drain infrastructure will be discussed in more detail below.

EXISTING DRAINAGE REPORT DISCUSSION

The approved Barbarick Subdivision Final Drainage Report (BS-FDR) and the approved Woodmen Storage Final Drainage Report (WS-FDR) both apply to the existing general drainage conditions for this site. The off-site basins and general flow patterns in the BS-FDR and WS-FDR still apply. Excerpts from these reports are provided below for reference.

On-site and Off-Site Basin Descriptions from the BS-FDR and WS-FDR:

The following summary is taken from the Barbarick Subdivision Final Drainage Report (BS-FDR):

Off-site:

Off-site Basin O3 This basin encompasses approximately 7.03 acres and represents the area north and northwest of Lot 1. This basin drains into Lot 1 through a series of (2) 24" CMP pipes which control the flow of 14/36 cfs in the 5/100 year storm events.

Lots 1 & 2 – these lots are considered fully developed lots and drain north to south collecting at the existing concrete settling pond on Lot 2. This developed flow (20.8 cfs /57.2 cfs) combines with Off-site Basin O3 to total 30.5 cfs / 80.8 cfs in the greenbelt offsite south of Lot 2. At the time of development permit for these developed lots, a detention pond for water quality will be required, probably in the area of the existing concrete settling pond, that will accommodate Lots 1 and 2 west of the gas easement and flood plain area.

On-site:

On-site Basins A1 and B1 (for portions of Lots 1 and 2, and Lots 3 & 4)

These basins encompass approximately 5.3 & 3.8 acres and represent the buildable portions of the property as described in the BS-FDR (see Basin Map from BS-FDR below). These basins were slated (in the BS-FDR) to drain into small detention ponds that would release to historic rates. These discharge rates were calculated to be 2.9/7.3 and 2.2/5.4 cfs (5/100 year). The BS-FDR does not include the drainage ways in any hydrology calculations due to the fact that this no-build drainage area was not planned on being developed. This drainage way allowed off-site flows from O1+O2 to pass-through Lots 3 & 4. The drainage way to the west of A1 passes through flows from offsite O3. Since the approval of this report, offsite tributary basins O1+O2 have been changed, and the development of the property encompasses the whole property, including the previously determined no-build area.

The following summary is taken from the Woodmen Storage Final Drainage Report (WS-FDR):

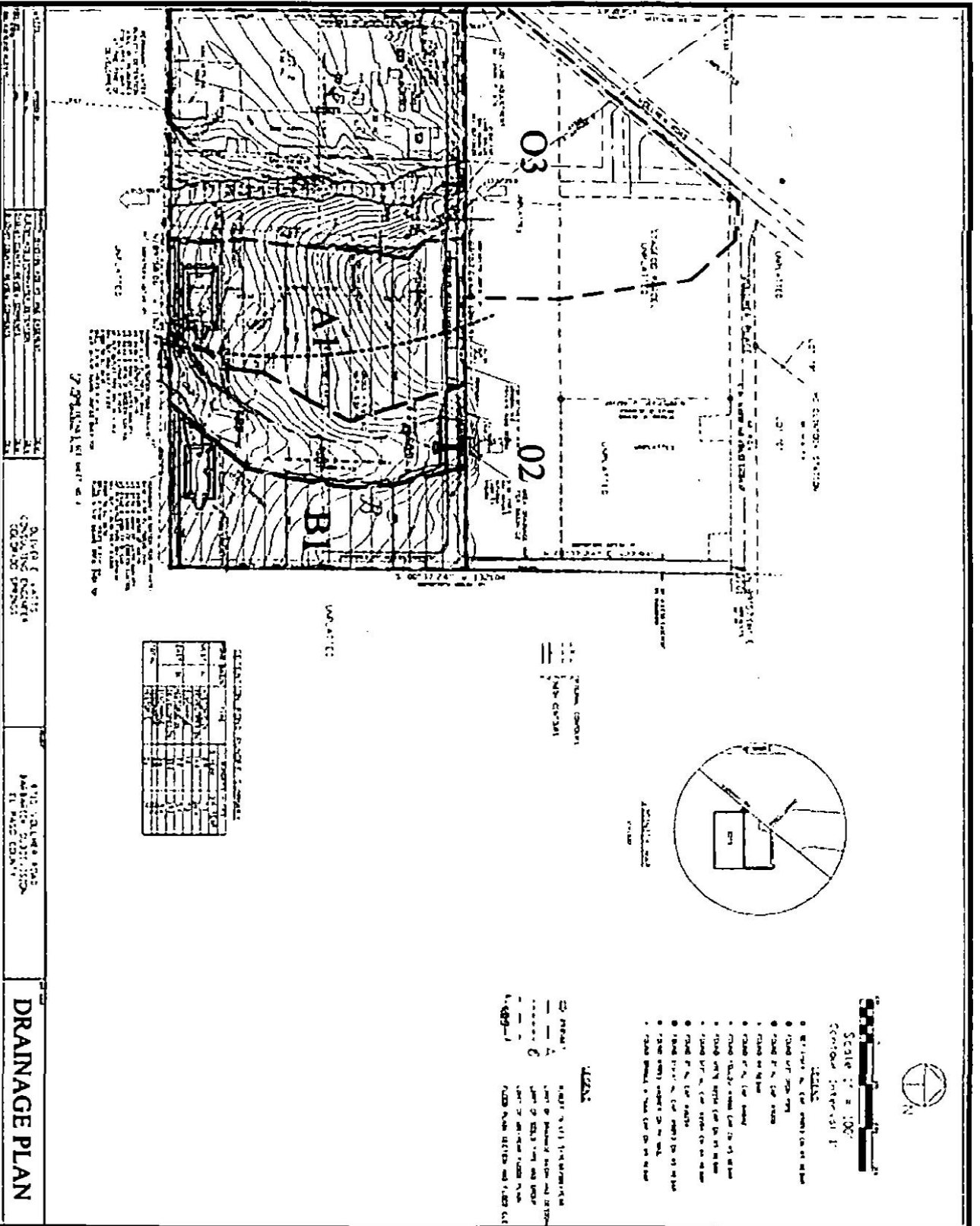
Off-site:

Design Point 5 - This design point encompasses approximately 19.69 acres and represents the tributary area north of the project site. This basin drains into a proposed detention pond near the northeast corner of the property and generates 57.4/92.7 cfs in the 10/100 year storm events, historic flows are 16.7/30.3 cfs. The releases rates from this pond are lower than historic 16.1 cfs/29.4 cfs in the 10/100-year storm events. These flows are conveyed along the east property line of the site and into the eastern natural drainage way that leaves the property to the south.

Review of the Sterling Ranch Preliminary Drainage Report (SR-PDR):

The Barbarick Subdivision is surrounded on three sides by the planned Sterling Ranch Development. The approved Sterling Ranch PDR was prepared by M&S Civil Consultants in May of 2015. This Sterling Ranch PDR re-analyzes runoff from Barbarick Subdivision and plans for storm drain improvements to convey this runoff to a full spectrum detention and water quality pond to be located down stream of Barbarick Subdivision as part of Sterling Ranch Phase One.

In summary; the Sterling Ranch PDR is planning on receiving 73.3/139.2 cfs (5/100 year) from Basin OS3. A 54" RCP is planned to convey this flow through Sterling Ranch. The Sterling Ranch PDR is planning on receiving 45/86 cfs (5/100 year) from OS2, encompasses Lots 1 & 2 and OS3 encompasses Lots 3 & 4 and the Basin north of Lot 3. A 48" RCP is planned to convey this flow through Sterling Ranch. The cumulative runoff from the northerly property and Lots 1 through 4 does not exceed the anticipated rates in the SR-PDR.

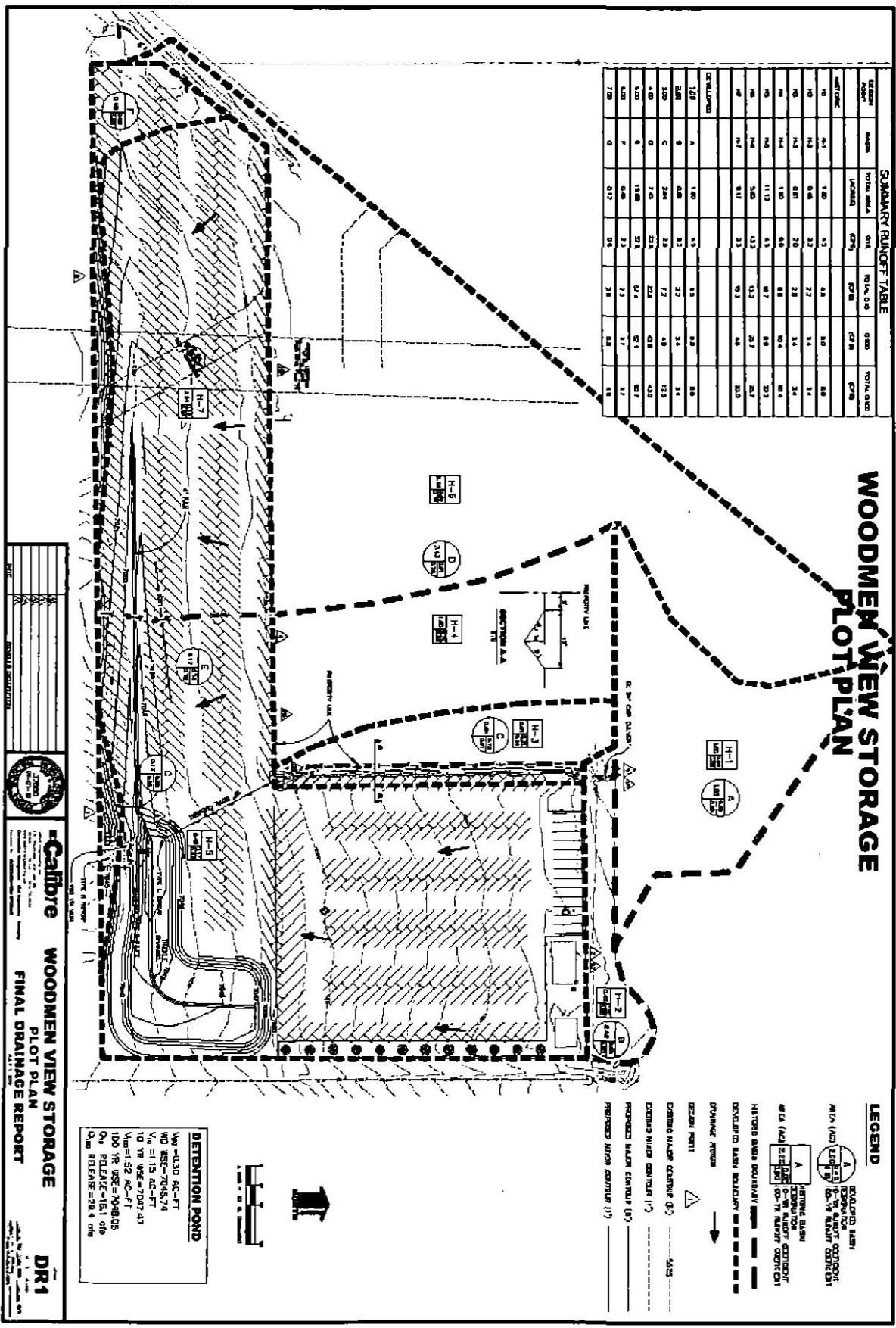


Basin Map - from the Barbarick Subdivision FDR


WOODMEN VIEW STORAGE PLOT PLAN

SUMMARY RUNOFF TABLE

STATION NUMBER	AREA (AC)	TOTAL AREA (AC)	Q10	Q5	Q2	Q1	Q0.5	TOTAL Q10
10	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
20	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
30	1.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
40	1.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00
50	1.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
60	1.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00
70	1.00	7.00	7.00	7.00	7.00	7.00	7.00	7.00
80	1.00	8.00	8.00	8.00	8.00	8.00	8.00	8.00
90	1.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
100	1.00	10.00	10.00	10.00	10.00	10.00	10.00	10.00
110	1.00	11.00	11.00	11.00	11.00	11.00	11.00	11.00
120	1.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00
130	1.00	13.00	13.00	13.00	13.00	13.00	13.00	13.00
140	1.00	14.00	14.00	14.00	14.00	14.00	14.00	14.00
150	1.00	15.00	15.00	15.00	15.00	15.00	15.00	15.00
160	1.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00
170	1.00	17.00	17.00	17.00	17.00	17.00	17.00	17.00
180	1.00	18.00	18.00	18.00	18.00	18.00	18.00	18.00
190	1.00	19.00	19.00	19.00	19.00	19.00	19.00	19.00
200	1.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00
210	1.00	21.00	21.00	21.00	21.00	21.00	21.00	21.00
220	1.00	22.00	22.00	22.00	22.00	22.00	22.00	22.00
230	1.00	23.00	23.00	23.00	23.00	23.00	23.00	23.00
240	1.00	24.00	24.00	24.00	24.00	24.00	24.00	24.00
250	1.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00
260	1.00	26.00	26.00	26.00	26.00	26.00	26.00	26.00
270	1.00	27.00	27.00	27.00	27.00	27.00	27.00	27.00
280	1.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00
290	1.00	29.00	29.00	29.00	29.00	29.00	29.00	29.00
300	1.00	30.00	30.00	30.00	30.00	30.00	30.00	30.00
310	1.00	31.00	31.00	31.00	31.00	31.00	31.00	31.00
320	1.00	32.00	32.00	32.00	32.00	32.00	32.00	32.00
330	1.00	33.00	33.00	33.00	33.00	33.00	33.00	33.00
340	1.00	34.00	34.00	34.00	34.00	34.00	34.00	34.00
350	1.00	35.00	35.00	35.00	35.00	35.00	35.00	35.00
360	1.00	36.00	36.00	36.00	36.00	36.00	36.00	36.00
370	1.00	37.00	37.00	37.00	37.00	37.00	37.00	37.00
380	1.00	38.00	38.00	38.00	38.00	38.00	38.00	38.00
390	1.00	39.00	39.00	39.00	39.00	39.00	39.00	39.00
400	1.00	40.00	40.00	40.00	40.00	40.00	40.00	40.00
410	1.00	41.00	41.00	41.00	41.00	41.00	41.00	41.00
420	1.00	42.00	42.00	42.00	42.00	42.00	42.00	42.00
430	1.00	43.00	43.00	43.00	43.00	43.00	43.00	43.00
440	1.00	44.00	44.00	44.00	44.00	44.00	44.00	44.00
450	1.00	45.00	45.00	45.00	45.00	45.00	45.00	45.00
460	1.00	46.00	46.00	46.00	46.00	46.00	46.00	46.00
470	1.00	47.00	47.00	47.00	47.00	47.00	47.00	47.00
480	1.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00
490	1.00	49.00	49.00	49.00	49.00	49.00	49.00	49.00
500	1.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00



Basin Map - from the FDR

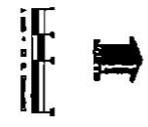



Calibre
WOODMEN VIEW STORAGE
PLOT PLAN
FINAL DRAINAGE REPORT

DR1

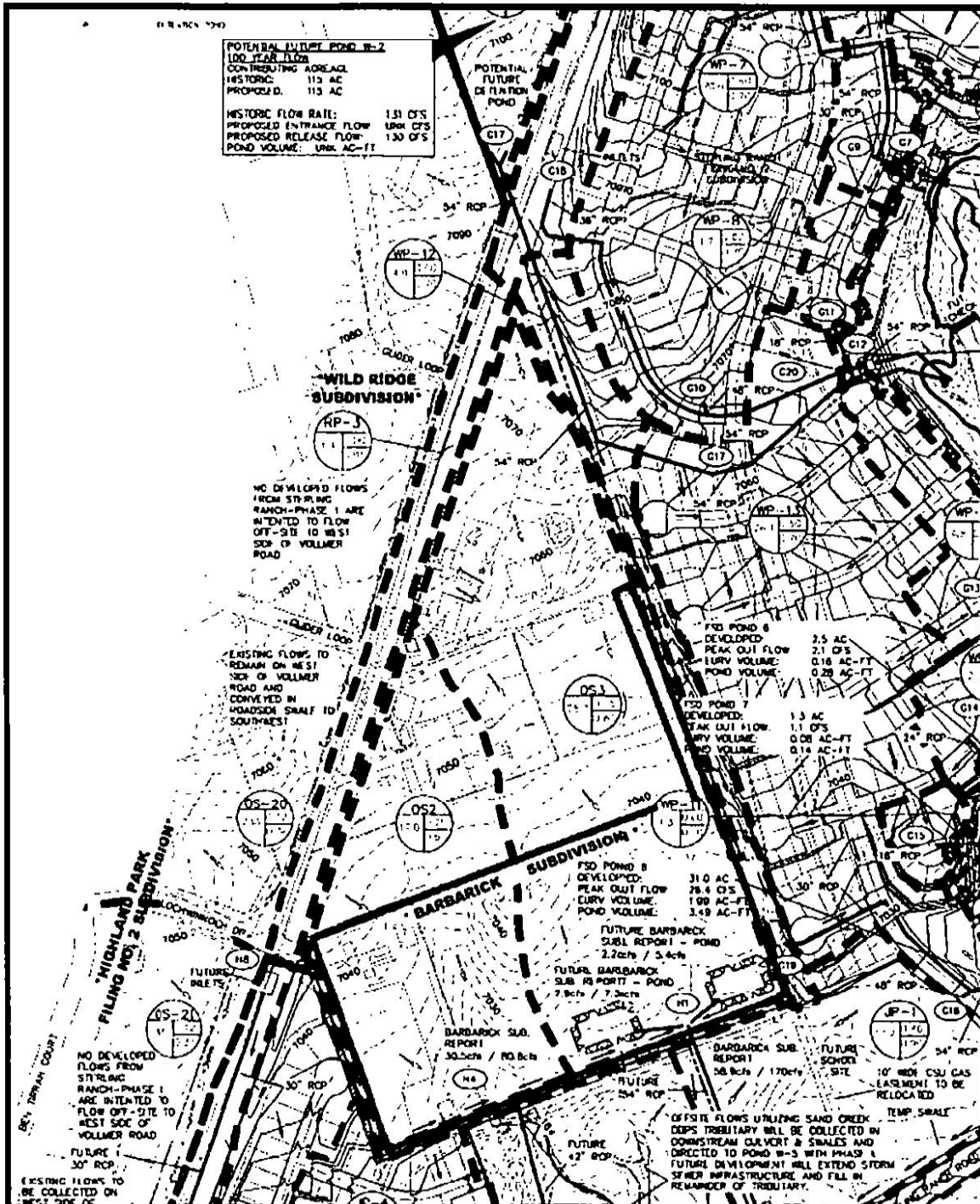
DETENTION POND

V₁₀ = 13.30 AC-FT
 V₅ = 11.15 AC-FT
 V₂ = 11.15 AC-FT
 V₁ = 11.15 AC-FT
 V_{0.5} = 11.15 AC-FT
 100 YR USE = 100% BCS
 ON RELEASE = 100% OF BCS
 ON RELEASE = 100% OF BCS



 <p>CIVIL CONSULTANTS, INC. 102 E. Pikes Peak Ave. Ste 306 Colorado Springs, CO 80903 (719) 955-5485, FAX (719) 448-8427</p>	STERLING RANCH PHASE 1		
	PROPOSED - DRAINAGE MAP (OVERALL)		
PROJECT NO. 09-001	SCALE	DATE: 5/2015	
DESIGNED BY: DLM	HORIZ: 1"=200'		
DRAWN BY: DLM	VERT: N/A		
CHECKED BY: VAS		SHEET 1 of 1	D2

Basin Map from the Sterling Ranch PDR



STORM SEWER ROUTING SUMMARY			
DF SIGN POINT	Q _s (cfs)	Q ₁₀₀ (cfs)	
G4A	640	1584	
G5	78	146	
G6	32	66	
G7	82	157	
G8	20	42	
G9	14	29	
G10	47	97	
G11	4	9	
G12	72	144	
G13	12	25	
G14	7	14	
G15	3	7	
G16	60	125	
G17	80	130	
G18	29	54	
G19	11	23	
G20	69	138	
G21	1044	1767	
G22	5	10	
G23	64	133	
G25	1056	1795	
H1	73	139	
H2	46	92	
H3	103	200	
H4	45	86	
H5	30	61	
H6	68	134	
H8	16	29	
H11	22	45	
H12	31	62	
H13	57	118	
H14	196	382	
H16	31	65	
H17	26	54	
H18	224	441	

BASIN SUMMARY			
BASIN	AREA (ACRES)	Q _s (cfs)	Q ₁₀₀ (cfs)
OS1	110.1	68	167
OS2	17.0	45	86
OS3	28.7	73	139
OS4	5.0	5	11

Flow Summary from the Sterling Ranch PDR

EXISTING SITE DRAINAGE DISCUSSION:

On-Site (Existing Conditions):

On-site Basin H1 This basin covers approximately 10.7 acres and represents the majority of Lots 3 & 4. This basin is modeled as good condition undeveloped rangeland. This drains to the south and generates 2.6/23.7 cfs in the 5/100 year storm events.

On-site Basin H2 This existing basin covers approximately 3.70 acres and represents the eastern half of Lots 1 & 2. This basin is modeled as good condition rangeland and generates 0.9/8.2 cfs in the 5/100 year storm events.

On-site Basin H3 This existing basin covers 1.1 acres and represents the a small portion of lots 3 & 4 that drains south easterly. This basin is modeled as good

condition rangeland and generates 0.3/2.7 cfs in the 5/100 year storm events. This basin sheet flows offsite where it is captured in a small swale between the site and existing roadway and conveyed westerly to the low point south of the outfall of Basin H1.

These existing basins encompass the previously unmodelled drainage area from the BS-FDR. The total historic flow from the site is 3.8/34.6 cfs in the 5/100 year storm events. The following design point table is for combined allowable discharge rates from the property at respective locations including historic flows from the tributary upstream basins:

<u>Design Point</u>	<u>5/100 Release</u>	<u>Comments</u>
DP H1	16.7*/30.3 cfs	DP H5 WS-FDR - * is 10year
DP H2	13.7/35.5 cfs	O3 BS-FDR
DP H3	56.7 cfs	DPH1+H1+H3 (100-year)
DP H4	14.6/43.7 cfs	DPH2 + H2

Design Point H3 will release a flow lower than previously anticipated within the BS-FDR (52.9/170 cfs). It is the introduction of development within the Sterling Ranch site that has eliminated offsite flows from BS-FDR Basin O1 that significantly changed the drainage pattern. The historic release is now contained solely to the historic flows from WS-FDR design point H5 and the proposed onsite historic flows.

Design Point H4 will combine with the western half of Lots 1&2. Per the BS-FDR the combined portions of Lots 1&2 and O3 to release a combined flow of 30.5/80.8 cfs downstream. The flow anticipated in the BS-FDR appears consistent with the smaller basin analysis of this report and should be used for downstream analysis.

PROPOSED DRAINAGE DISCUSSION

Introduction

The proposed site will be developed differently than anticipated in the previous BS-FDR. The previous plan for this site maintained the existing native drainage way down the middle of Lots 1 & 2 and 3 & 4, thereby splitting the buildable area into the outer thirds of these lots. The native drainage way and "Drainage Boundary – No Build Area" (as shown on the Plat & FDR) will be eliminated with the proposed development. The proposed site and proposed drainage improvements will allow this native drainage way to be eliminated while maintaining the pass through of major flows. These modifications to the site and to the drainage patterns will allow a larger buildable area.

The existing retention pond, located just north of Lot 3, will be modified by others to become a water quality/detention pond pursuant to the WS-FDR. A new outlet works and a storm drain pipe will convey runoff from this detention pond (16.1/29.4 cfs in the 10/100 year storm events) discharging at the property line. This development is proposing a CDOT Type D inlet to capture the discharged flow and pipe it downstream along the east side of Lots 3 & 4 to discharge into the proposed Full Spectrum Extended

Detention Basin (EDB) in Lot 4. The EDB is designed to pass through, and not treat or detain, these offsite flows.

A new EDB will be provided in Lot 4. This detention basin will provide water quality treatment for portions of Lots 1 & 2, and Lots 3 & 4. In the approved Barbarick FDR there were to be two separate ponds. The new site development has been planned for a single pond to treat the developed flows. Tributary water sheet flow across the site to shallow swales that will direct runoff to the proposed EDB. The EDB will have a forebay at the confluence of the two pipe outfalls, a concrete trickle channel that terminates at a micropool structure, and is designed to treat the WQCV, EURV and 100-year detention.

A second SFB water quality with detention catchment basin will be provided at the south east/downstream end of Lot 2. This SFB will not have an outlet structure to release flows due to requirements from the gas main utility ownership of no structure to be built within the existing easements. There will be a small spillway to allow the release of large storm events. Runoff will be directed to the proposed SFB where possible.

Flow from the area north of Lot 1 (Basin O3) will pass through the site via two 24" culverts and will be discharged at the southern boundary of Lot 2, as historically done. An earthen channel will run north-south along the east side of the existing Lot 1 and Lot 2 developments. The channel is approximately 1-ft deep with 4:1 side slopes and will capture and convey any westerly flowing nuisance runoff from the proposed improvements to the sand filter detention pond as discussed in the original Barbarick Subdivision FDR, instead of the existing Lot 1 and 2 improved areas.

Runoff from the property is at historic flows and will not exceed the anticipated runoff as determined in the Sterling Ranch PDR. This is described in more detail below. The Sterling Ranch PDR includes an analysis of future drainage conditions and includes recommended infrastructure to convey this runoff. Since the Sterling Ranch surrounds the Barbarick Subdivision, it is appropriate to include the recommendations from the SR-PDR in this Proposed Drainage Discussion.

Proposed On-Site Basin Descriptions: (See Basin Map in the pocket)

On-site Basin D1 (D for Developed condition) - This developed basin encompasses approximately 11.4 acres - the majority of Lots 3 & 4 and small portions of Lots 1 & 2. This basin generates 19.7/56.0 cfs in the 5/100 year storm events and sheet flows into shallow swales that direct the runoff into the proposed EDB to be located in Lot 4. Lot 3 is based on Owner provided information for a gravel parking/vehicle storage area, and Lot 4 has been based on proposed building site improvements as identified in the rezoning application. Any changes to the land use will require an update to the Final Drainage Report; much like the original Barbarick Subdivision Final Drainage Report is being updated with the grading and Lot 4 development application.

On-site Basin D2 This undeveloped basin encompasses 1.2 acres and represents the south portion of Lot 4, below and south of the two detention ponds. This basin is historic in nature and generates 0.8/3.0 cfs and drains directly into a road side ditch within the Sterling Ranch development.

On-site Basin D3 This developed basin encompasses approximately 3.13 acres - the remaining proposed infill portions of Lots 1 and 2 (east of the currently built out Lots 1&2). As discussed in the original Barbarick Subdivision FDR, development of these areas will require a detention water quality pond. This basin generates 4.1/11.6 cfs in the 5/100 year storm events and sheet flows southerly to the proposed SFB located at the southern-most portion of Lot 2.

The following design point table is for combined allowable discharge rates from the property at respective locations including historic flows from the tributary upstream basins:

<u>Design Point</u>	<u>5/100 Year</u>	<u>Comments</u>
DP D1	85.4 cfs (100)	D1+O2 Pass Through
DP D2	48.9 cfs (100)	Pond Release+D2
DP D3	4.1/11.6 cfs	D3
DP D4	13.8/39.1 cfs	Pond Release +O3 Pass Through

All release flows downstream are at or below historic levels.

RECOMMENDED DESIGN

Off-site Detention Facility:

This shallow pond will be modified for the proposed development to the north as part of the WS-FDR. This will eliminate the retention properties in this pond, will provide detention for off-site flows, will provide a suitable outlet structure, and will remove accumulated sediment. The modified pond will store up to 1.52 acft (66,211 cuft) to the principal spillway (elevation = 7048.05). A summary of flows into and out of this pond:

<u>Off-site Pond Flow Summary (cfs)</u>	<u>5 year</u>	<u>100 year</u>
Proposed Flow into offsite pond (Basin G/DP 5)	<u>57.4</u>	<u>92.7</u>
Increase in peak flow due to development	46.2	51.3
Proposed flow out of modified pond	<u>16.1</u>	<u>29.4</u>
Reduction in peak flow	41.3	63.3

For complete pond design, refer to the WS-FDR.

Proposed 30” HDPE Storm Drain from Modified Off-site Detention Pond:

This storm drain will capture flows from the discharged offsite pond and route them along the perimeter of the property daylighting into the EDB in Lot 4. 4’ precast concrete manholes will be used for maintenance access at all bends and grade breaks. A grouted riprap forebay will help dissipate energy at the outlet of the pipe, and allow for settling prior to entering the pond. See the Appendix for the hydraulic analysis of this storm drain (StormCAD).

In the event of an emergency and the offsite pond fails, developed flow (Q100=93.0 cfs) will overtop the pond and be collected between the proposed roadway and pond berm.. Flow not captured by the proposed inlet will bypass easterly to the proposed offsite swale between this property and the Sterling Ranch property and conveyed southerly.

Proposed 18” HDPE Storm Drain Culvert:

A 18” HDPE culvert will convey collected runoff from Lot 3 (Developed Q100 = 15.90cfs) through Lot 4 to the FSD Pond and join sheet flow from Lot 4 and the 30” piped bypass flow from basin O2. This culvert will be privately owned and maintained by the property owners. See the Appendix for open channel calculations.

On-site FSD - EDB Pond in Lot 4 (Basin D1):

This On-site Full Spectrum Extended Detention Basin Pond provides water quality, EURV and 100-year detention. Onsite flows will combine with the 30-inch bypass flows from the north and pass through the EDB. The pond has been sized for the release of historic flows from Basin D1, as well as provides capacity for pass through conveyance of historic flows from the north.

The following table outlines the onsite existing and developed flow, required detention, and modifications to required detention utilizing the upstream over detention.

<u>On-site Basin Flow Summary (cfs)</u>	<u>5 year</u>	<u>100 year</u>
Existing On-site Flow at Pond	2.2	16.5
Developed On-site Flow (Basin D1)	<u>19.7</u>	<u>56.0</u>
Increase in peak flow due to development	17.5	39.5
Proposed Pass Through Flow from Off-Site Pond	<u>16.1*</u>	<u>29.4</u>
Proposed total flow out of EDB pond	<u>0.3</u>	<u>45.9**</u>

*Includes 10 year from WS-FDR

**Includes Pass Through flow of 29.4 cfs

Water Quality Benefits:

Stormwater from Lots 3 & 4, and portions of 1 & 2 will drain directly to the proposed Full Spectrum Extended Detention Pond. This pond will be privately maintained and provide water quality treatment to approximately 11.4 acres of developed land.

The proposed Water Quality facility is sized using the methods derived from the UDFCD Stormwater FSD Design Workbook (UD-FSD 1.11) (see Appendix). The Water Quality Capture Volume (WQCV) will be provided in this EDB, where the “initial flush” of storm water will be drained over a 40-hour time period.

The impervious area ratio is used in the UDFCD workbook to calculate the WQCV. An adjusted impervious ratio of 57% to correlate with the land use charts and Runoff Coefficients (provided above) is being utilized for the sizing of the facility.

The EDB Pond will have a forebay, concrete trickle channel and micro-pool within the outlet structure (per UDFCD). This outlet structure will have a bar screen and an orifice plate containing 3 rows outlets (1.55 sq in orifices for the first two, and 3.8 sq in for the last row). The EURV has been designed to an elevation of 7021.50. The top of the inlet will have a grate to allow flows that exceed the WQCV and EURV to drain through the outlet works without overtopping the spillway, with an internal orifice plate of 2.37-ft diameter constricting flows to historic release rates ($Q_{100 \text{ Onsite}} = 16.5 \text{ cfs} + Q_{100 \text{ bypass}} = 29.4$ Total Release = 45.9 cfs) .

The EDB pond can store up to 64,904 cuft (1.49 acft) to the principal spillway (7023.20). The pond bottom elevation will be at 7018.50 and the top of the embankment will be at elevation 7025.10. Should the outlet works become fully blocked; the 36' spillway will have the capacity to pass the combined 100 year peak developed runoff and northerly bypass with a flow depth = 0.90' ($55.0 + 29.4 = 84.4 \text{ cfs}$) maintaining 1-ft of freeboard. .

Summary results include:

- WQCV Volume = 0.203 ac-ft depth 1.53-ft (40 hour release)
- EURV Volume Stored = 0.677 ac-ft at depth 2.98 ft (72 hour release)
- 5 Year Volume Stored = 0.673 ac-ft at depth 2.98 ft (72 hour release)
- 100 Year Volume Stored = 1.261 ac-ft depth 4.26-ft (77 hour release)
- Emergency Spillway Volume at Crest = 1.49 ac-ft at depth 4.7ft.

A 30" HDPE pipe will drain this outlet structure. A Low-Tailwater basin will be provided at the outlet for energy dissipation. This storm drain will daylight into the open channel just south of Lot 4 near the entrance of an existing 12" CMP. This existing 12" CMP drains under a dirt road. This dirt road will be eliminated upon development of the Sterling Ranch. Due to the limited capacity of this existing 12" CMP, runoff in excess of 5.7 cfs will overtop this dirt road, creating tail water to 7018.0. See the Appendix for the calculation results (CulvertMaster).

On-site Sand Filter Basin w/ Detention in Lot 2 (Basin D3):

A sand filter basin detention pond is being proposed to treat runoff from the proposed gravel parking portions of Lots 1 and 2 prior to discharging from the site. Due to the high pressure gas mains within this basin, grading is limited to fill only and no structures are allowed within the gas easement, so this pond will have underdrain design with partial infiltration and a controlled overflow design for the 100-year event.

The following table outlines the onsite existing and developed flow, required detention, and modifications to required detention utilizing the upstream over detention.

<u>On-site Basin Flow Summary (cfs)</u>	<u>5 year</u>	<u>100 year</u>
Existing On-site Flow at Pond	0.5	4.2
Developed On-site Flow (Basin D3)	4.1	11.6
Increase in peak flow due to development	3.6	7.4
Proposed total flow out of Sand Filter pond	<u>0.1</u>	<u>3.6</u>

Water Quality Benefits:

Stormwater from portions of 1 & 2 will drain directly to the proposed Sand Filter Pond. This pond will be privately maintained and provide water quality treatment to approximately 3.13 acres of developed land.

The proposed Water Quality facility is sized using the methods derived from the UDFCD Stormwater Detention Design Workbook (UD-Detention 3.04) (see Appendix). The Water Quality Capture Volume (WQCV) will be provided in this SFB, where the "initial flush" of storm water will be drained over a 12-hour time period.

The impervious area ratio is used in the UDFCD workbook to calculate the WQCV. An adjusted impervious ratio of 57% to correlate with the land use charts and Runoff Coefficients (provided above) is being utilized for the sizing of the facility.

The sand filter will contain a 4" underdrain beneath 18" of CDOT Class C material. The underdrain will contain a 1.27" diameter orifice to control the outflow time in accordance with UDFCD.

The SFB pond can store up to 16,247 cu ft (0.373 acft) to the principal spillway (7025.50). The pond bottom elevation will be at 7023.00 and the top of the embankment will be at elevation 7027.37. Because the spillway acts as the 100-year control structure and notched weir design is proposed. The spillway is 5-ft wide for a depth of 10-inches for the release of the 100-year flow (3.6 cfs which is less than the 4.2 historic) then the spillway widens to 10ft for a depth of 18-inches which will have the capacity to pass the combined 100 year peak developed runoff (11.6cfs) with a flow depth = 0.5' maintaining 1-ft of freeboard.

Summary results include:

- WQCV Volume = 0.039 ac-ft depth 0.37-ft (12 hour release)
- EURV Volume Stored = 0.181 ac-ft at depth 1.52 ft (42 hour release)
- 5 Year Volume Stored = 0.181 ac-ft at depth 1.52 ft (42 hour release)
- 100 Year Volume Stored = 0.394 ac-ft depth 2.83-ft (68 hour release)

Proposed (2) 24" HDPE Storm Drain Culvert:

Two 24" pipes will convey offsite flows through Lots 1 and 2 discharging to the south. The culverts will connect to a pair of existing 24" culverts entering the property and will discharge to a riprap settling basing prior to the released downstream. These culverts will be privately owned and maintained by the property owners. See the Appendix for the hydraulic analysis of this storm drain (CulvertMaster). Flow from these pipes will join the flow from the Sand Filter and discharge at Design Point 4 (combined 39.4 cfs in the 100-year event). Per the BS-FDR this flow combines with the westerly portions of Lots 1 & 2 offsite for a total release of 30.5/80.8 cfs in the 5/100 year events.

As stated above in the summary from the Sterling Ranch PDR, the anticipated runoff from this proposed discharge point (aka: SR-PDR Basin H4) is 30.5/80.8 cfs (5/100 year) due to the large pass through flow. A 42" RCP is planned to convey this flow through Sterling Ranch.

DRAINAGE, BRIDGE, AND POND FEES

This subdivision has already been platted. No additional Drainage, Bridge or Pond fees are required.

MAINTENANCE

All proposed storm drain infrastructure will be located within private property and will be owned and maintained by the property owner. The detention pond will be owned and maintained by the property owner and will require maintenance consisting of routine inspections, removal of debris from the detention area, and bi-annual inspections for hydraulic performance of the basin. Refer to the DCM for exact maintenance criteria and for other Best Management Practices (BMP).

EROSION CONTROL

Best Management Practices (BMPs) will be utilized to minimize erosion during construction and will be shown on the construction drawings. These will be in accordance with will be utilized as deemed necessary by the contractor and/or engineer. The contractor shall minimize the amount of area disturbed during all construction activities.

In general, the following shall be applied in developing the sequence of major activities;

1. Install down slope and side slope perimeter BMPs before the land disturbing activity occurs.
2. Do not disturb area until it is necessary for the construction activity to proceed.
3. Cover or stabilize exposed areas as soon as possible.
4. Time the construction activities to reduce the impacts from seasonal climatic changes or weather events.
5. The construction of permanent filtration BMPs should wait until the end of the construction project when drainage areas have been stabilized.
6. Do not remove the temporary erosion controls until after all areas are stabilized.

Slopes

Erosion control soil retention blankets shall be installed where noted on slopes 3:1 or steeper. At a minimum, coconut/straw blend fiber material blankets should be used. The silt fence or erosion logs shall be installed at the toe of fill slopes where noted on a level contour. Erosion logs shall also be installed on slopes greater than ten feet in height where noted to reduce runoff length. The erosion logs shall be installed on a level contour. Disturbed surfaces shall be left in a roughened condition at all times when horizontal depressions approximately 2" to 4" deep, spaced 4" to 6" apart. Silt fence and erosion logs shall remain in place until all construction is complete and/or "finally stabilized", after which the silt fence and erosion logs shall be removed from the slopes. All material shall be installed per manufacturer's installation instructions.

Stockpiles/Mobilization/Winter Shutdown

Soils stockpiled for more than 30 days shall be mulched with mulch tackifier and native seeding within 14 days of stockpile construction. After mobilization and prior to winter shutdown, all disturbed slopes not completed shall be mulched with mulch tackifier and native seeding.

Inlet and Outlet Protection

Storm Drain Inlet Protection shall be provided at all storm inlets. Outlet protection shall be provided at all pipe outlet and runoff / rundown treatment locations. All materials shall be installed per manufacturer's installation instructions.

Concrete Washout

Concrete washout structures shall be installed for cleaning concrete trucks. The concrete washout structure shall be constructed such that water can only evaporate or infiltrate from the structure. Residue and concrete from the washout structure shall be periodically cleaned out and properly disposed.

Erosion Control Supervisor and Maintenance

The erosion control supervisor shall be a person other than the superintendent. The erosion control supervisor shall inspect at least every 14 days and after any precipitation or snowmelt event that causes surface erosion. At sites where construction has been completed but a vegetative cover has not been established, these inspections must occur at least once per month.

All erosion control measures shall remain in place until all construction is complete and final stabilization has been achieved. "Final stabilization" is where all disturbed areas

have been built on, paved, or germinated with a uniform vegetative cover with a density of at least 70% of pre-disturbance levels. Equivalent permanent, physical erosion reduction methods may also be employed. Any areas not meeting this standard shall be repaired according to the BMP guidelines. Accumulated sediment and debris shall be removed when the sediment level reaches one half the height of the BMP or when the sediment/debris adversely impacts the functionality of the BMP. The Contractor shall remove all sediment, mud, and construction debris that may accumulate in public right of ways not designated before-hand as a result of this construction project. All repairs, removals, and replacements stated above shall be conducted in a timely manner.

Cost Estimate

The proposed drainage system to be constructed will be privately owned and maintained. The developer will be responsible for constructing the proposed improvements.

An engineer's estimate of probable construction costs has been provided for the proposed improvements. The storm sewer systems will be located in the Sand Creek Drainage Basin. The construction cost for the improvements are not eligible for reimbursement.

**Engineer's Estimate of Probable Construction Costs
Tri-Lakes Construction - Sand Creek Drainage Basin
Non-Reimbursable Private Improvements**

Item	Unit	Quantity	Unit Cost	Total Cost
Precast Manhole	EA	4	\$2,500	\$10,000
18" HDPE Pipe	LF	231	\$45	\$10,395
24" HDPE Pipe	LF	1212	\$60	\$72,720
30" HDPE Pipe	LF	1128	\$72	\$81,216
18" Flared End	EA	2	\$225	\$450
24" Flared End	EA	2	\$250	\$500
24" CMP-HDPE	EA	2	\$200	\$400
30" Flared End	EA	1	\$350	\$350
CDOT Type D Inlet	EA	1	\$4,000	\$4,000
EDB Pond Outlet	EA	1	\$35,000	\$35,000
			SubTotal	\$215,031.00
			15% Contingency	\$32,254.65
			Total Estimate	\$247,285.65

REFERENCES

1. **City of Colorado Springs & El Paso County Drainage Criteria Manual, Volumes I and II**, dated May 2014 including subsequent updates
2. **City of Colorado Springs & El Paso County Drainage Criteria Manual, Volumes I and II**, dated November 1991 including subsequent updates
3. **Appendix I of the El Paso County's Engineering Criteria Manual (ECM)**, (2008).
4. **Urban Storm Drainage Criteria Manuals, Volumes 1-3**, published by the Urban Drainage and Flood Control District, (Volumes 1 & 2 dated 2016, Volume 3 dated 2015)
5. **Preliminary Drainage Report for Sterling Ranch-Phase 1, Sand Creek Drainage Basin**, M & S Civil Consultants, Inc., May 2015
6. **Woodmen Storage Final Drainage Report, El Paso County**, Calibre Engineering, Inc., July 2004; Revised February, 2010; Revised May, 2010; Revised July, 2010
7. **Preliminary and Final Drainage Plan and Report for Barbarick Subdivision, El Paso County**, Oliver E. Watts Consulting Engineer Inc., January 2005; Revised October 2005; Revised December 2006; Revised May 2007; Revised August 15, 2007
8. **NOAA Atlas 14, Volume 8 Version 2** U.S. Department of Commerce, National Oceanic and Atmospheric Administration, National Weather Service, Hydrometeorological Design Studies Center.
9. FEMA Map Service Center: <http://msc.fema.gov>
10. NRCS Web Soil Survey. <http://websoilsurvey.nrcs.usda.gov>

APPENDIX A

HYDROLOGIC AND HYDRAULIC CALCULATIONS

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: H-1 5 Year

I. Catchment Hydrologic Data

Catchment ID = H1
 Area = 10.70 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

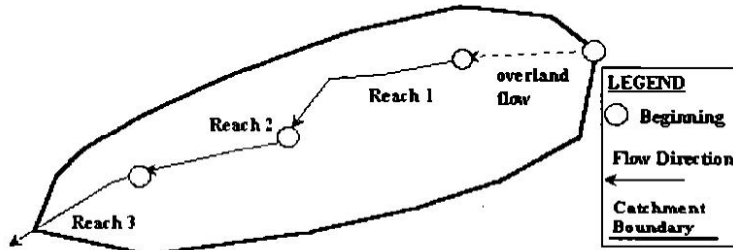
II. Rainfall Information I (inch/hr) = $C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 5 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 1.23 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.08
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, C = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Convey- ance input	Flow Velocity V fps output	Flow Time Tf minutes output
1	0.0300	338		10.00	1.73	3.25
2						
3						
4						
5						
Sum		638				

Computed T_c = 25.42
 Regional T_c = 13.54
 User-Entered T_c = 13.54

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c , I = 2.12 inch/hr
 Rainfall Intensity at Regional T_c , I = 2.93 inch/hr
 Rainfall Intensity at User-Defined T_c , I = 2.93 inch/hr

Peak Flowrate, Q_p = 1.85 cfs
 Peak Flowrate, Q_p = 2.56 cfs
 Peak Flowrate, Q_p = 2.56 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: H-1 100 Year

I. Catchment Hydrologic Data

Catchment ID = H1
 Area = 10.70 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

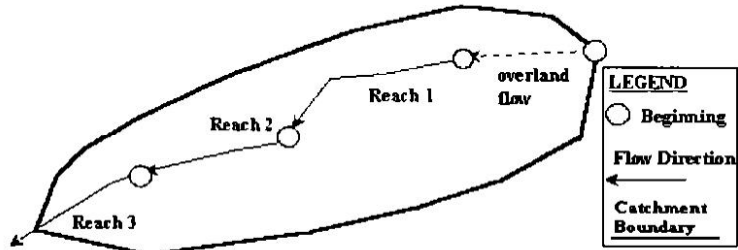
II. Rainfall Information I (inch/hr) = $C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 100 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 2.57 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.36
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, $C-5$ = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff		NRCS Conveyance input	Flow Velocity V		Flow Time T _f minutes output
			C-5 output			fps output		
Overland	0.0300	300		0.08	N/A	0.23		22.16
1	0.0300	338			10.00	1.73		3.25
2								
3								
4								
5								
Sum		638						

Computed T_c = 25.42
 Regional T_c = 13.54
 User-Entered T_c = 13.54

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c, I = 4.44 inch/hr
 Rainfall Intensity at Regional T_c, I = 6.12 inch/hr
 Rainfall Intensity at User-Defined T_c, I = 6.12 inch/hr

Peak Flowrate, Q_p = 17.20 cfs
 Peak Flowrate, Q_p = 23.71 cfs
 Peak Flowrate, Q_p = 23.71 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: H-2 5 Year

I. Catchment Hydrologic Data

Catchment ID = H2
 Area = 3.70 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

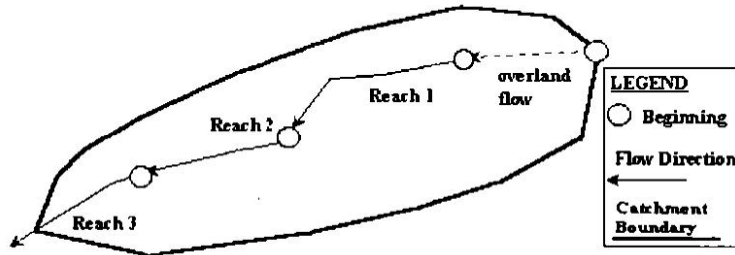
II. Rainfall Information I (inch/hr) = $C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 5 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 1.23 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.08
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, C = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/ Field	Short Pasture/ Lawns	Nearly Bare Ground	Grassed Swales/ Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Convey- ance input	Flow Velocity V fps output	Flow Time Tf minutes output
1	0.0350	515		10.00	1.87	4.59
2						
3						
4						
5						
Sum		670				

Computed T_c = 19.32
 Regional T_c = 13.72
 User-Entered T_c = 13.72

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c , I = 2.46 inch/hr
 Rainfall Intensity at Regional T_c , I = 2.91 inch/hr
 Rainfall Intensity at User-Defined T_c , I = 2.91 inch/hr

Peak Flowrate, Q_p = 0.74 cfs
 Peak Flowrate, Q_p = 0.88 cfs
 Peak Flowrate, Q_p = 0.88 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: H-2 100 Year

I. Catchment Hydrologic Data

Catchment ID = H2
 Area = 3.70 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

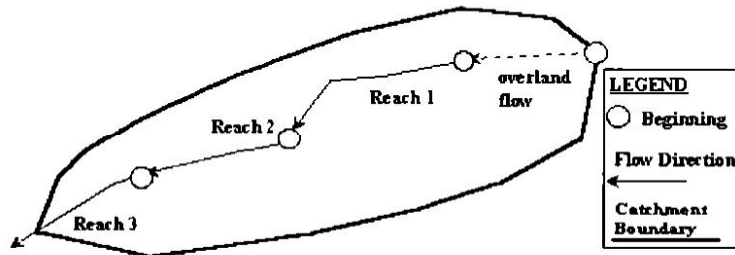
II. Rainfall Information $I (\text{inch/hr}) = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 100 years (input return period for design storm)
 $C1$ = 28.50 (input the value of C1)
 $C2$ = 10.00 (input the value of C2)
 $C3$ = 0.786 (input the value of C3)
 $P1$ = 2.57 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.36
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C.)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, C = _____ (enter an override C-5 value if desired, or leave blank to accept calculated C-5.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S	Length L	5-yr Runoff Coeff C-5	NRCS Conveyance	Flow Velocity V	Flow Time Tf	
	ft/ft input	ft input	output	input	fps output	minutes output	
Overland	0.0380	155	0.08	N/A	0.18	14.74	
1	0.0350	515		10.00	1.87	4.59	
2							
3							
4							
5							
Sum		670					
						Computed Tc =	19.32
						Regional Tc =	13.72
						User-Entered Tc =	13.72

IV. Peak Runoff Prediction

Rainfall Intensity at Computed Tc, I = 5.15 inch/hr
 Rainfall Intensity at Regional Tc, I = 6.08 inch/hr
 Rainfall Intensity at User-Defined Tc, I = 6.08 inch/hr

Peak Flowrate, Q_p = 6.90 cfs
 Peak Flowrate, Q_p = 8.15 cfs
 Peak Flowrate, Q_p = 8.15 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: H-3 5 year

I. Catchment Hydrologic Data

Catchment ID = H3
 Area = 1.11 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

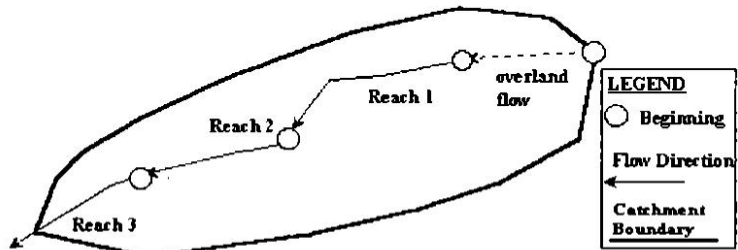
II. Rainfall Information I (inch/hr) = $C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 5 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 1.23 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.08
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, $C-5$ = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Convey- ance input	Flow Velocity V fps output	Flow Time Tf minutes output	
							Overland
1							
2							
3							
4							
5							
Sum		338					
						Computed Tc =	24.98
						Regional Tc =	11.88
						User-Entered Tc =	11.88

IV. Peak Runoff Prediction

Rainfall Intensity at Computed Tc, I = 2.14 inch/hr
 Rainfall Intensity at Regional Tc, I = 3.10 inch/hr
 Rainfall Intensity at User-Defined Tc, I = 3.10 inch/hr

Peak Flowrate, Q_p = 0.19 cfs
 Peak Flowrate, Q_p = 0.28 cfs
 Peak Flowrate, Q_p = 0.28 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: H-3 100 year

I. Catchment Hydrologic Data

Catchment ID = H3
 Area = 1.11 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

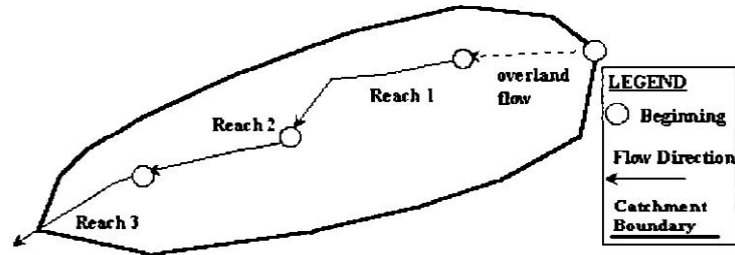
II. Rainfall Information $I \text{ (inch/hr)} = C1 \cdot P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 100 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 2.67 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.36
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, $C-5$ = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S	Length L	5-yr Runoff Coeff C-5	NRCS Conveyance	Flow Velocity V	Flow Time T _f
	ft/ft	ft	input		input	output
Overland	0.0250	338	0.08	N/A	0.23	24.98
1						
2						
3						
4						
5						
Sum		338				

Computed T_c = 24.98
 Regional T_c = 11.88
 User-Entered T_c = 11.88

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c, I = 4.65 inch/hr
 Rainfall Intensity at Regional T_c, I = 6.73 inch/hr
 Rainfall Intensity at User-Defined T_c, I = 6.73 inch/hr

Peak Flowrate, Q_p = 1.87 cfs
 Peak Flowrate, Q_p = 2.71 cfs
 Peak Flowrate, Q_p = 2.71 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: D-2 5 Year

I. Catchment Hydrologic Data

Catchment ID = D2
 Area = 1.20 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

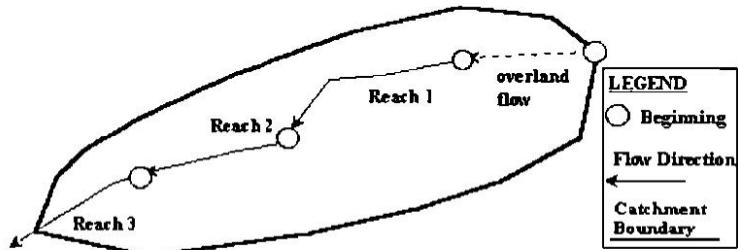
II. Rainfall Information $I(\text{inch/hr}) = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 5 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 1.23 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.08
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, C = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S	Length L	5-yr Runoff Coeff C-5	NRCS Conveyance	Flow Velocity V	Flow Time T _f
	ft/ft input	ft input	output		fps output	minutes output
Overland	0.0200	155	0.08	N/A	0.14	18.21
1						
2						
3						
4						
5						
Sum		155				

Computed T_c = 18.21
 Regional T_c = 10.86
 User-Entered T_c = 10.86

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c, I = 2.54 inch/hr
 Rainfall Intensity at Regional T_c, I = 3.22 inch/hr
 Rainfall Intensity at User-Defined T_c, I = 3.22 inch/hr

Peak Flowrate, Q_p = 0.25 cfs
 Peak Flowrate, Q_p = 0.32 cfs
 Peak Flowrate, Q_p = 0.32 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: D2 - 100yr

I. Catchment Hydrologic Data

Catchment ID = D2
 Area = 1.20 Acres
 Percent Imperviousness = 2.00 %
 NRCS Soil Type = B A, B, C, or D

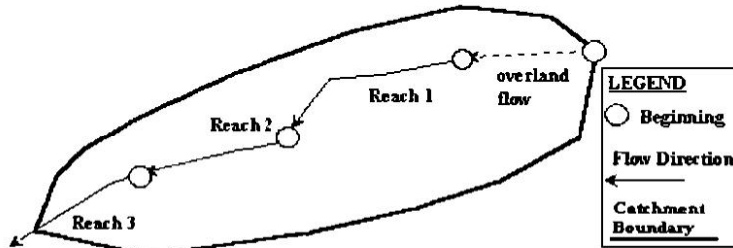
II. Rainfall Information I (inch/hr) = $C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 100 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 2.57 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.36
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.08
 Override 5-yr. Runoff Coefficient, C = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S	Length L	5-yr Runoff Coeff C-5	NRCS Conveyance	Flow Velocity V	Flow Time T _f
	ft/ft input	ft input	output		fps output	minutes output
Overland	0.0200	85	0.08	N/A	0.11	13.49
1						
2						
3						
4						
5						
	Sum	85				

Computed T_c = 13.49
 Regional T_c = 10.47
 User-Entered T_c = 10.47

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c, I = 6.13 inch/hr
 Rainfall Intensity at Regional T_c, I = 6.83 inch/hr
 Rainfall Intensity at User-Defined T_c, I = 6.83 inch/hr

Peak Flowrate, Q_p = 2.66 cfs
 Peak Flowrate, Q_p = 2.97 cfs
 Peak Flowrate, Q_p = 2.97 cfs

CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Barbarick Subdivision
 Catchment ID: Lot3-Culvert 100yr

I. Catchment Hydrologic Data

Catchment ID = Lot 3
 Area = 4.86 Acres
 Percent Imperviousness = 57.00 %
 NRCS Soil Type = B A, B, C, or D

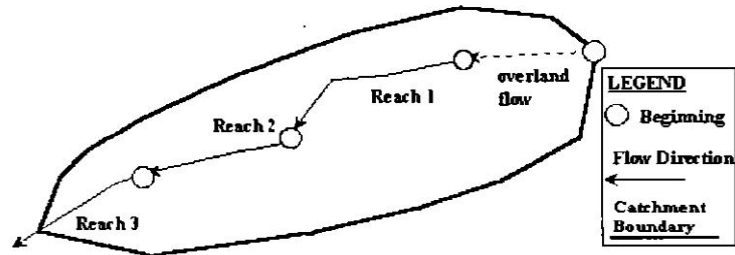
II. Rainfall Information $I (\text{inch/hr}) = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period, T_r = 100 years (input return period for design storm)
 $C1$ = 28.50 (input the value of $C1$)
 $C2$ = 10.00 (input the value of $C2$)
 $C3$ = 0.786 (input the value of $C3$)
 $P1$ = 2.57 inches (input one-hr precipitation--see Sheet "Design Info")

III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient, C = 0.55
 Override Runoff Coefficient, C = _____ (enter an override C value if desired, or leave blank to accept calculated C .)
 5-yr. Runoff Coefficient, $C-5$ = 0.39
 Override 5-yr. Runoff Coefficient, $C-5$ = _____ (enter an override $C-5$ value if desired, or leave blank to accept calculated $C-5$.)

Illustration



NRCS Land Type	Heavy Meadow	Tillage/ Field	Short Pasture/ Lawns	Nearly Bare Ground	Grassed Swales/ Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S	Length L	5-yr Runoff Coeff C-5	NRCS Conveyance	Flow Velocity V	Flow Time T _f
	ft/ft input	ft input	output	input	fps output	minutes output
Overland	0.0300	300	0.39	N/A	0.32	15.41
1	0.0100	500		10.00	1.00	8.33
2						
3						
4						
5						
Sum		800				

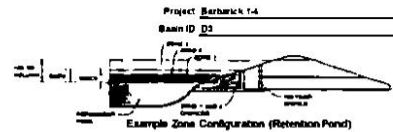
Computed T_c = 23.74
 Regional T_c = 14.44
 User-Entered T_c = 14.44

IV. Peak Runoff Prediction

Rainfall Intensity at Computed T_c, I = 4.61 inch/hr
 Rainfall Intensity at Regional T_c, I = 5.94 inch/hr
 Rainfall Intensity at User-Defined T_c, I = 5.94 inch/hr

Peak Flowrate, Q_p = 12.34 cfs
 Peak Flowrate, Q_p = 15.90 cfs
 Peak Flowrate, Q_p = 15.90 cfs

DETENTION BASIN STAGE-STORAGE TABLE BUILDER



Required Volume Calculation

Selected BMP Type	BF	
Watershed Area	3.12	acres
Watershed Length	648	ft
Watershed Slope	0.020	ft/ft
Water shed Imperviousness	57.00%	percent
Percentage Hydrologic Soil Group A	5.0%	percent
Percentage Hydrologic Soil Group B	95.0%	percent
Percentage Hydrologic Soil Group C/D	0.0%	percent
Desired WQCV Drain Time	12.0	hours
Location for 1-hr Rainfall Depth	Use Input	
Water Quality Capture Volume (WQCV)	0.947	acre-feet
Excess Linear Runoff Volume (ELRV)	0.184	acre-feet
2-yr Runoff Volume (P1 = 0.95 in)	0.128	acre-feet
5-yr Runoff Volume (P1 = 1.23 in)	0.194	acre-feet
10-yr Runoff Volume (P1 = 1.48 in)	0.253	acre-feet
25-yr Runoff Volume (P1 = 1.88 in)	0.363	acre-feet
50-yr Runoff Volume (P1 = 2.21 in)	0.452	acre-feet
100-yr Runoff Volume (P1 = 2.57 in)	0.554	acre-feet
500-yr Runoff Volume (P1 = 3.0 in)	0.660	acre-feet
Approximate 2-yr Detention Volume	0.122	acre-feet
Approximate 5-yr Detention Volume	0.178	acre-feet
Approximate 10-yr Detention Volume	0.204	acre-feet
Approximate 25-yr Detention Volume	0.237	acre-feet
Approximate 50-yr Detention Volume	0.273	acre-feet
Approximate 100-yr Detention Volume	0.336	acre-feet

Optional Linear Input 1-hr Precipitation	0.95	inches
	1.23	inches
	1.48	inches
	1.88	inches
	2.21	inches
	2.57	inches

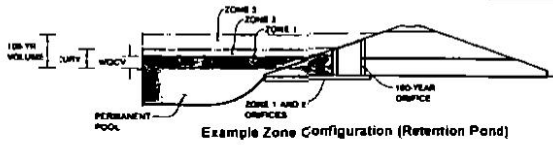
Stage-Storage Calculation

Zone 1 Volume (WQCV)	0.947	acre-feet
Zone 2 Volume (100-yr - Zone 1)	0.289	acre-feet
Select Zone 3 Storage Volume (Optional)		acre-feet
Total Detention Basin Volume	0.336	acre-feet
Initial Surcharge Volume (SV)	NA	ft ³
Initial Surcharge Depth (ISD)	NA	ft
Total Available Detention Depth (H _{total})	2.50	ft
Depth of Trickle Channel (H _{tc})	NA	ft
Slope of Trickle Channel (S _{tc})	NA	ft/ft
Slope of Main Basin Sides (S _{mb})	4:1	ft/ft
Basin Length-to-Width Ratio (L _{mb} /W _{mb})	1.5	
Initial Surcharge Area (A _{sv})	0	ft ²
Surcharge Volume Length (L _{sv})	0.0	ft
Surcharge Volume Width (W _{sv})	0.0	ft
Depth of Basin Floor (H _{floor})	0.00	ft
Length of Basin Floor (L _{floor})	81.0	ft
Width of Basin Floor (W _{floor})	94.0	ft
Area of Basin Floor (A _{floor})	4370	ft ²
Volume of Basin Floor (V _{floor})	0	ft ³
Depth of Main Basin (H _{mb})	2.50	ft
Length of Main Basin (L _{mb})	101.0	ft
Width of Main Basin (W _{mb})	74.0	ft
Area of Main Basin (A _{mb})	7488	ft ²
Volume of Main Basin (V _{mb})	14876	ft ³
Calculated Total Basin Volume (V _{total})	0.336	acre-feet

Depth Increment	0.1								
Stage - Storage Description	Stage (ft)	Optional Overide Stage (ft)	Length (ft)	Width (ft)	Area (sq-ft)	Optional Overide Area (sq-ft)	Area (acres)	Volume (ft ³)	Volume (ac-ft)
Media Surface	0.00	81.0	84.0	4.370	0.100	0.100	0.000	0.000	0.000
	0.10	81.6	84.9	4.478	0.103	0.103	0.001	0.010	0.001
	0.20	82.5	86.5	4.577	0.105	0.105	0.001	0.020	0.002
	0.30	83.3	88.3	4.668	0.106	0.106	0.001	0.030	0.003
	0.40	84.1	90.1	4.751	0.107	0.107	0.001	0.040	0.004
	0.50	84.9	91.9	4.828	0.108	0.108	0.001	0.050	0.005
	0.60	85.7	93.7	4.900	0.109	0.109	0.001	0.060	0.006
	0.70	86.5	95.5	4.967	0.110	0.110	0.001	0.070	0.007
	0.80	87.3	97.3	5.030	0.111	0.111	0.001	0.080	0.008
	0.90	88.1	99.1	5.089	0.112	0.112	0.001	0.090	0.009
Zone 1 (WQCV)	1.00	88.9	100.9	5.144	0.113	0.113	0.001	0.100	0.010
	1.10	89.7	102.7	5.197	0.114	0.114	0.001	0.110	0.011
	1.20	90.5	104.5	5.248	0.115	0.115	0.001	0.120	0.012
	1.30	91.3	106.3	5.297	0.116	0.116	0.001	0.130	0.013
	1.40	92.1	108.1	5.344	0.117	0.117	0.001	0.140	0.014
	1.50	92.9	109.9	5.389	0.118	0.118	0.001	0.150	0.015
	1.60	93.7	111.7	5.433	0.119	0.119	0.001	0.160	0.016
	1.70	94.5	113.5	5.475	0.120	0.120	0.001	0.170	0.017
	1.80	95.3	115.3	5.516	0.121	0.121	0.001	0.180	0.018
	1.90	96.1	117.1	5.555	0.122	0.122	0.001	0.190	0.019
Zone 2 (100-yr)	2.00	96.9	118.9	5.593	0.123	0.123	0.001	0.200	0.020
	2.10	97.7	120.7	5.630	0.124	0.124	0.001	0.210	0.021
	2.20	98.5	122.5	5.666	0.125	0.125	0.001	0.220	0.022
	2.30	99.3	124.3	5.701	0.126	0.126	0.001	0.230	0.023
	2.40	100.1	126.1	5.735	0.127	0.127	0.001	0.240	0.024
	2.50	100.9	127.9	5.768	0.128	0.128	0.001	0.250	0.025
	2.60	101.7	129.7	5.800	0.129	0.129	0.001	0.260	0.026
	2.70	102.5	131.5	5.831	0.130	0.130	0.001	0.270	0.027
	2.80	103.3	133.3	5.862	0.131	0.131	0.001	0.280	0.028
	2.90	104.1	135.1	5.892	0.132	0.132	0.001	0.290	0.029

Detention Basin Outlet Structure Design

Project: **Barbakc Subdivision**
Basin ID: **D3**



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.45	0.047	Filtration Media
Zone 2 (100-year)	2.50	0.289	Not Utilized
Zone 3			
		0.336	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate Orifice Vertical Spacing = inches
Orifice Plate Orifice Area per Row = inches

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Overflow Weir Front Edge Height, H_o = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Slope = H:V (enter zero for flat grate)
Horiz. Length of Weir Sides = feet
Overflow Grate Open Area % = % grate open area/total area
Debris Clogging % = %

Calculated Parameters for Overflow Weir

Height of Grate Upper Edge, H_g = feet
Over Flow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area = should be ≥ 4
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	0.95	1.23	1.48	1.88	2.21	2.57	0.00
Calculated Runoff Volume (acre-ft) =	0.047	0.194	0.128	0.194	0.253	0.363	0.452	0.554	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.047	0.194	0.127	0.194	0.253	0.363	0.451	0.553	#N/A
Pradevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.17	0.34	0.80	1.04	1.33	1.89
Pradevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.5	1.1	2.5	3.2	4.2	5.9
Peak Inflow Q (cfs) =	1.0	4.1	2.7	4.1	5.3	7.6	9.4	11.6	#N/A
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	0.1	0.2	1.7	3.6	#N/A
Ratio Peak Outflow to Pradevelopment Q =	N/A	N/A	N/A	0.1	0.1	0.1	0.5	0.9	#N/A
Structure Controlling Flow =	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Spillway	Spillway	Spillway	#N/A
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	41	29	41	51	66	65	65	#N/A
Time to Drain 89% of Inflow Volume (hours) =	13	42	30	42	52	68	68	68	#N/A
Maximum Ponding Depth (ft) =	0.37	1.52	1.04	1.52	1.91	2.55	2.71	2.83	#N/A
Area at Maximum Ponding Depth (acres) =	0.11	0.14	0.13	0.14	0.15	0.17	0.18	0.18	#N/A
Maximum Volume Stored (acre-ft) =	0.039	0.181	0.117	0.181	0.240	0.343	0.371	0.394	#N/A

APPENDIX B

STORMCAD INFORMATION

Culvert Calculator Report Twin 24" Culvert

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	2.00 ft	Headwater Depth/Height	1.32
Computed Headwater Elev.	7,038.15 ft	Discharge	35.50 cfs
Inlet Control HW Elev.	7,038.10 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	7,038.15 ft	Control Type	Entrance Control
Grades			
Upstream Invert	7,035.51 ft	Downstream Invert	7,020.00 ft
Length	606.00 ft	Constructed Slope	0.025594 ft/ft
Hydraulic Profile			
Profile	S2	Depth, Downstream	0.94 ft
Slope Type	Steep	Normal Depth	0.94 ft
Flow Regime	Supercritical	Critical Depth	1.52 ft
Velocity Downstream	12.17 ft/s	Critical Slope	0.006140 ft/ft
Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	Concrete	Span	2.00 ft
Section Size	24 inch	Rise	2.00 ft
Number Sections	2		
Outlet Control Properties			
Outlet Control HW Elev.	7,038.15 ft	Upstream Velocity Head	0.75 ft
Ke	0.50	Entrance Loss	0.37 ft
Inlet Control Properties			
Inlet Control HW Elev.	7,038.10 ft	Flow Control	Transition
Inlet Type	Square edge w/headwall	Area Full	6.3 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report Outlet Pipe

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	7,023.10 ft	Headwater Depth/Height	2.07
Computed Headwater Elev:	7,023.10 ft	Discharge	55.60 cfs
Inlet Control HW Elev.	7,023.10 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	7,022.97 ft	Control Type	Inlet Control
Grades			
Upstream Invert	7,017.92 ft	Downstream Invert	7,017.52 ft
Length	40.00 ft	Constructed Slope	0.010000 ft/ft
Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	2.36 ft
Slope Type	Mild	Normal Depth	N/A ft
Flow Regime	Subcritical	Critical Depth	2.36 ft
Velocity Downstream	11.58 ft/s	Critical Slope	0.013538 ft/ft
Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	Concrete	Span	2.50 ft
Section Size	30 inch	Rise	2.50 ft
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	7,022.97 ft	Upstream Velocity Head	1.99 ft
Ke	0.20	Entrance Loss	0.40 ft
Inlet Control Properties			
Inlet Control HW Elev.	7,023.10 ft	Flow Control	Submerged
Inlet Type	Beveled ring, 33.7° bevels	Area Full	4.9 ft ²
K	0.00180	HDS 5 Chart	3
M	2.50000	HDS 5 Scale	B
C	0.02430	Equation Form	1
Y	0.83000		

O2-Overflow Channel

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient	0.050	
Channel Slope	0.02000	ft/ft
Normal Depth	2.00	ft
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Bottom Width	4.00	ft

Results

Discharge	94.99	ft ³ /s
Flow Area	20.00	ft ²
Wetted Perimeter	16.65	ft
Hydraulic Radius	1.20	ft
Top Width	16.00	ft
Critical Depth	1.73	ft
Critical Slope	0.03707	ft/ft
Velocity	4.75	ft/s
Velocity Head	0.35	ft
Specific Energy	2.35	ft
Froude Number	0.75	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.00	ft
Critical Depth	1.73	ft
Channel Slope	0.02000	ft/ft

O2-Overflow Channel

GVF: Output Data

Critical Slope

0.03707 ft/ft

Worksheet for Open Channel Culvert Lot 3

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.012	
Channel Slope	0.03000	ft/ft
Diameter	1.50	ft
Discharge	15.90	ft ³ /s

Results

Normal Depth	1.02	ft
Flow Area	1.28	ft ²
Wetted Perimeter	2.91	ft
Hydraulic Radius	0.44	ft
Top Width	1.40	ft
Critical Depth	1.42	ft
Percent Full	68.1	%
Critical Slope	0.01690	ft/ft
Velocity	12.41	ft/s
Velocity Head	2.39	ft
Specific Energy	3.41	ft
Froude Number	2.29	
Maximum Discharge	21.20	ft ³ /s
Discharge Full	19.71	ft ³ /s
Slope Full	0.01952	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	68.08	%
Downstream Velocity	Infinity	ft/s

Worksheet for Open Channel Culvert Lot 3

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.02	ft
Critical Depth	1.42	ft
Channel Slope	0.03000	ft/ft
Critical Slope	0.01690	ft/ft

Worksheet for Outlet with Passthrough-Weir

Project Description

Solve For Discharge

Input Data

Headwater Elevation	1.40	ft
Crest Elevation	0.00	ft
Tailwater Elevation	0.00	ft
Weir Coefficient	3.00	US
Crest Length	32.00	ft
Number Of Contractions	0	

Results

Discharge	159.02	ft ³ /s
Headwater Height Above Crest	1.40	ft
Tailwater Height Above Crest	0.00	ft
Flow Area	44.80	ft ²
Velocity	3.55	ft/s
Wetted Perimeter	34.80	ft
Top Width	32.00	ft

Weir is more restrictive than Orifice.
159.02 cfs
70% Gate Opening
50% Closing
= 55.66 cfs > 45.9 tributary
→ Install orifice Restrictor on outlet pipe.

Worksheet for Outlet wPass - Orifice

Project Description

Solve For Discharge

Input Data

Headwater Elevation	1.40	ft
Centroid Elevation	0.00	ft
Tailwater Elevation	0.00	ft
Discharge Coefficient	0.60	
Opening Width	4.00	ft
Opening Height	12.00	ft

Results

Discharge	273.35	ft ³ /s
Headwater Height Above Centroid	1.40	ft
Tailwater Height Above Centroid	0.00	ft
Flow Area	48.00	ft ²
Velocity	5.69	ft/s

*Top Box Weir is more Restrictive
USE Weir Calculations.*

Worksheet for FSD Outlet Orifice Plate

Project Description

Solve For Diameter

Input Data

Discharge	45.90	ft ³ /s	(16.5 H ₁₅ + 29.4 P ₁₀₀)
Headwater Elevation	4.70	ft	
Centroid Elevation	0.00	ft	
Tailwater Elevation	0.00	ft	
Discharge Coefficient	0.60		

Results

Diameter	2.37	ft
Headwater Height Above Centroid	4.70	ft
Tailwater Height Above Centroid	0.00	ft
Flow Area	4.40	ft ²
Velocity	10.43	ft/s

Worksheet for FSD Overflow - Pass

Project Description

Solve For Discharge

Input Data

Headwater Elevation		0.90	ft
Crest Elevation		0.00	ft
Tailwater Elevation		0.00	ft
Crest Surface Type	Gravel		
Crest Breadth		12.00	ft
Crest Length		36.00	ft

Results

Discharge	86.22	ft ³ /s	(55 DVI + 29.4 pucc = 84.4 cfs)
Headwater Height Above Crest	0.90	ft	
Tailwater Height Above Crest	0.00	ft	
Weir Coefficient	2.80	US	
Submergence Factor	1.00		
Adjusted Weir Coefficient	2.80	US	
Flow Area	32.40	ft ²	
Velocity	2.66	ft/s	
Wetted Perimeter	37.80	ft	
Top Width	36.00	ft	

Worksheet for Type D Inlet - Weir

Project Description

Solve For Discharge

Input Data

Headwater Elevation	1.50	ft
Crest Elevation	0.00	ft
Weir Coefficient	3.00	US
Crest Length	17.17	ft

Results

Discharge	94.61	ft ³ /s
Headwater Height Above Crest	1.50	ft
Flow Area	25.75	ft ²
Velocity	3.67	ft/s
Wetted Perimeter	20.17	ft
Top Width	17.17	ft

Type D Weir is most restrictive

94.61 cfs

70% Grate Opening

50% Clogging

= 33.11 cfs > 29.4 cfs tributary

Worksheet for Western Channel Capacity

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.02000	ft/ft
Normal Depth	1.00	ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)

Results

Discharge	17.30	ft ³ /s
Flow Area	4.00	ft ²
Wetted Perimeter	8.25	ft
Hydraulic Radius	0.49	ft
Top Width	8.00	ft
Critical Depth	1.03	ft
Critical Slope	0.01703	ft/ft
Velocity	4.32	ft/s
Velocity Head	0.29	ft
Specific Energy	1.29	ft
Froude Number	1.08	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	1.00	ft
Critical Depth	1.03	ft
Channel Slope	0.02000	ft/ft
Critical Slope	0.01703	ft/ft

Label	Start Node	Stop Node	Branch ID	Branch		Length (ft)	Upstream Inlet C	Upstream		System Intensity (in/h)
				Element ID	(Unified)			Intensity (in/h)	Area (acres)	
CO-1	CB-1	MH-1	1	1	255.4 (N/A)		8 (N/A)		8	
CO-2	MH-1	MH-2	1	2	295.1 (N/A)		8 (N/A)		8	
CO-3	MH-2	MH-3	1	3	295.1 (N/A)		8 (N/A)		8	
CO-4	MH-3	MH-4	1	4	44.9 (N/A)		8 (N/A)		8	
CO-5	MH-4	OF-1	1	5	198.3 (N/A)		8 (N/A)		8	

System	Rational Flow (ft ³ /s)	Total Flow (ft ³ /s)	Rise		Capacity (Full Flow) (ft ³ /s)	Velocity (Average) (ft/s)	Invert (Upstream) (m) (ft)	Invert (Downstream) (ft)	Slope (ft/ft)
			(in)	(Unified)					
CO-1	0	29.4	30		44.49	9.68	7032.21	7029.65	0.01
CO-2	0	29.4	30		44.43	9.67	7029.35	7026.4	0.01
CO-3	0	29.4	30		38.97	8.72	7026.2	7023.93	0.008
CO-4	0	29.4	30		57.43	11.77	7023.63	7022.88	0.017
CO-5	0	29.4	30		44.4	9.67	7022.88	7020.9	0.01

APPENDIX C

STANDARD DESIGN CHARTS AND TABLES



NOAA Atlas 14, Volume 8, Version 2
Location name: Colorado Springs, Colorado, US*
Latitude: 38.9514°, Longitude: -104.6905°
Elevation: 6984 ft*
 * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Penca, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk,
 Dale Unruh, Michael Yekta, Geoffrey Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.237 (0.195-0.290)	0.289 (0.238-0.355)	0.380 (0.311-0.467)	0.460 (0.374-0.568)	0.577 (0.456-0.746)	0.674 (0.517-0.880)	0.775 (0.573-1.04)	0.883 (0.625-1.21)	1.03 (0.701-1.46)	1.15 (0.759-1.65)
10-min	0.347 (0.285-0.425)	0.424 (0.348-0.520)	0.556 (0.455-0.684)	0.673 (0.548-0.832)	0.846 (0.667-1.09)	0.987 (0.757-1.29)	1.14 (0.839-1.52)	1.29 (0.914-1.78)	1.51 (1.03-2.14)	1.69 (1.11-2.41)
15-min	0.423 (0.348-0.519)	0.516 (0.424-0.634)	0.678 (0.555-0.834)	0.821 (0.668-1.01)	1.03 (0.814-1.33)	1.20 (0.924-1.57)	1.38 (1.02-1.85)	1.58 (1.11-2.17)	1.84 (1.25-2.61)	2.06 (1.35-2.94)
30-min	0.613 (0.504-0.751)	0.747 (0.614-0.917)	0.980 (0.802-1.21)	1.19 (0.965-1.47)	1.49 (1.17-1.92)	1.74 (1.33-2.27)	2.00 (1.48-2.67)	2.27 (1.61-3.13)	2.66 (1.80-3.76)	2.97 (1.95-4.24)
60-min	0.795 (0.654-0.974)	0.948 (0.779-1.16)	1.23 (1.00-1.51)	1.48 (1.21-1.83)	1.88 (1.49-2.44)	2.21 (1.70-2.90)	2.57 (1.91-3.46)	2.96 (2.10-4.09)	3.52 (2.39-4.99)	3.97 (2.61-5.67)
2-hr	0.977 (0.809-1.19)	1.15 (0.951-1.40)	1.47 (1.22-1.80)	1.78 (1.46-2.19)	2.27 (1.82-2.94)	2.68 (2.09-3.51)	3.14 (2.35-4.21)	3.65 (2.61-5.02)	4.38 (3.00-6.18)	4.98 (3.30-7.06)
3-hr	1.08 (0.897-1.31)	1.25 (1.04-1.51)	1.58 (1.31-1.93)	1.92 (1.57-2.34)	2.45 (1.98-3.19)	2.92 (2.29-3.83)	3.45 (2.60-4.62)	4.04 (2.91-5.55)	4.90 (3.39-6.92)	5.62 (3.75-7.95)
6-hr	1.26 (1.05-1.51)	1.44 (1.20-1.73)	1.81 (1.51-2.18)	2.19 (1.81-2.65)	2.81 (2.30-3.64)	3.37 (2.66-4.39)	4.00 (3.04-5.34)	4.71 (3.43-6.45)	5.77 (4.02-8.09)	6.65 (4.46-9.33)
12-hr	1.45 (1.23-1.74)	1.68 (1.41-2.00)	2.12 (1.78-2.54)	2.55 (2.13-3.07)	3.26 (2.68-4.19)	3.89 (3.10-5.03)	4.59 (3.52-6.08)	5.38 (3.94-7.31)	6.54 (4.59-9.11)	7.51 (5.08-10.5)
24-hr	1.68 (1.43-1.99)	1.97 (1.67-2.33)	2.50 (2.12-2.98)	3.01 (2.53-3.60)	3.80 (3.13-4.80)	4.48 (3.58-5.72)	5.23 (4.02-6.83)	6.04 (4.45-8.11)	7.23 (5.09-9.96)	8.20 (5.58-11.4)
2-day	1.95 (1.67-2.29)	2.31 (1.97-2.72)	2.95 (2.51-3.48)	3.53 (2.99-4.18)	4.39 (3.62-5.46)	5.11 (4.10-6.44)	5.88 (4.55-7.59)	6.71 (4.96-8.91)	7.89 (5.59-10.8)	8.83 (6.07-12.2)
3-day	2.15 (1.85-2.51)	2.54 (2.18-2.97)	3.22 (2.75-3.78)	3.83 (3.26-4.52)	4.74 (3.92-5.87)	5.50 (4.42-6.88)	6.30 (4.89-8.09)	7.16 (5.31-9.45)	8.37 (5.96-11.4)	9.34 (6.45-12.8)
4-day	2.31 (2.00-2.70)	2.72 (2.34-3.17)	3.42 (2.94-4.01)	4.06 (3.46-4.78)	5.00 (4.15-6.16)	5.78 (4.67-7.21)	6.61 (5.14-8.46)	7.50 (5.58-9.87)	8.75 (6.25-11.8)	9.76 (6.75-13.3)
7-day	2.74 (2.38-3.18)	3.17 (2.75-3.68)	3.92 (3.39-4.57)	4.60 (3.95-5.38)	5.60 (4.67-6.86)	6.43 (5.23-7.97)	7.32 (5.73-9.30)	8.27 (6.19-10.8)	9.60 (6.90-12.9)	10.7 (7.44-14.5)
10-day	3.11 (2.71-3.60)	3.58 (3.11-4.14)	4.39 (3.80-5.09)	5.11 (4.40-5.95)	6.17 (5.17-7.51)	7.05 (5.75-8.69)	7.98 (6.27-10.1)	8.97 (6.75-11.7)	10.4 (7.47-13.9)	11.5 (8.03-15.5)
20-day	4.18 (3.67-4.79)	4.79 (4.20-5.50)	5.83 (5.09-6.71)	6.72 (5.84-7.77)	7.99 (6.71-9.59)	9.01 (7.38-11.0)	10.0 (7.94-12.6)	11.1 (8.42-14.3)	12.6 (9.17-16.7)	13.8 (9.73-18.6)
30-day	5.05 (4.46-5.77)	5.80 (5.11-6.63)	7.04 (6.18-8.07)	8.08 (7.05-9.30)	9.51 (8.01-11.3)	10.6 (8.73-12.8)	11.8 (9.32-14.6)	12.9 (9.79-16.5)	14.4 (10.5-19.0)	15.6 (11.1-20.9)
45-day	6.14 (5.44-6.98)	7.06 (6.25-8.03)	8.54 (7.53-9.74)	9.75 (8.55-11.2)	11.4 (9.60-13.4)	12.6 (10.4-15.1)	13.8 (11.0-17.0)	15.0 (11.4-19.1)	16.6 (12.1-21.7)	17.7 (12.6-23.7)
60-day	7.05 (6.27-7.99)	8.12 (7.20-9.20)	9.80 (8.66-11.1)	11.1 (9.80-12.7)	12.9 (10.9-15.2)	14.2 (11.8-17.0)	15.5 (12.4-19.0)	16.7 (12.8-21.1)	18.3 (13.4-23.8)	19.4 (13.9-25.8)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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Map Unit Legend

El Paso County Area, Colorado (CO625)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
9	Blakeland-Fluvaquentic Haplaquolls	12.5	76.4%
71	Pring coarse sandy loam, 3 to 8 percent slopes	3.9	23.6%
Totals for Area of Interest		16.4	100.0%

El Paso County Area, Colorado

9—Blakeland-Fluvaquentic Haplaquolls

Map Unit Setting

National map unit symbol: 36b6
Elevation: 3,500 to 5,800 feet
Mean annual precipitation: 13 to 17 inches
Mean annual air temperature: 46 to 55 degrees F
Frost-free period: 110 to 165 days
Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 60 percent
Fluvaquentic haplaquolls and similar soils: 30 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Flats, hills
Landform position (three-dimensional): Side slope, talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Sandy alluvium derived from arkose and/or eolian deposits derived from arkose

Typical profile

A - 0 to 11 inches: loamy sand
AC - 11 to 27 inches: loamy sand
C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 5 percent
Available water storage in profile: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Ecological site: Sandy Foothill (R049BY210CO)

Description of Fluvaquentic Haplaquolls

Setting

Landform: Swales
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium

Typical profile

H1 - 0 to 12 inches: variable

Properties and qualities

Slope: 1 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat):
Moderately high to high (0.20 to 6.00 in/hr)
Depth to water table: About 0 to 24 inches
Frequency of flooding: Occasional
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)

Interpretive groups

Land capability classification (irrigated): 6w
Land capability classification (nonirrigated): 6w
Hydrologic Soil Group: D

Minor Components

Other soils

Percent of map unit:

Pleasant

Percent of map unit:
Landform: Depressions

Data Source Information

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 13, Sep 22, 2015

El Paso County Area, Colorado

71—Pring coarse sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 369k
Elevation: 6,800 to 7,600 feet
Farmland classification: Not prime farmland

Map Unit Composition

Pring and similar soils: 85 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pring

Setting

Landform: Hills
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Arkosic alluvium derived from sedimentary rock

Typical profile

A - 0 to 14 inches: coarse sandy loam
C - 14 to 60 inches: gravelly sandy loam

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 6.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: B
Ecological site: Loamy Park (R048AY222CO)

Minor Components

Other soils

Percent of map unit:

Pleasant

Percent of map unit:

Landform: Depressions

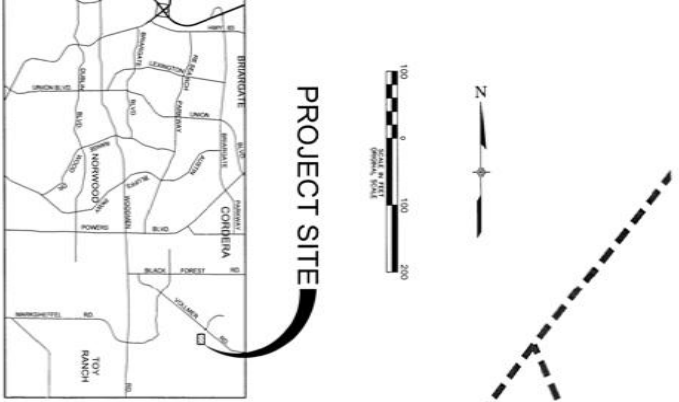
Data Source Information

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 13, Sep 22, 2015

APPENDIX D

MAPS

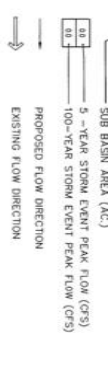


VICINITY MAP

BARBARICK DRAINAGE SUMMARY TABLE

BASIN	AREA (AC.)	Q/6 (CFS)	Q/100 (CFS)	%IMP	COMMENT
D1	11.40	25.7	56.0	57%	
D2	1.21	0.8	3.0	2%	
D3	3.13	4.1	11.6	57%	HISTORIC
D2	11.12	16.7	30.3		REF: WOODMAN STORAGE FOR 2010
03	7.03	13.7	35.5		REF: BARBARICK FOR 2005

DESIGN POINT	AREA (AC.)	Q/(100) (CFS)	COMMENT
D1	11.40	85.4	D1 BASIN TO FSD +02; PASS THROUGH
D2	22.52	48.9	POND RELEASE + D2
D3	3.13	11.6	D3 BASIN TO SFB
D4	10.16	39.1	POND RELEASE + 03 PIPE PASS THROUGH



VERTICAL BENCHMARK

THE BENCHMARK IS A CONCRETE PILE 12 INCHES IN DIAMETER AND 12 FEET LONG, SET IN A 24 INCH DIAMETER HOLE. THE BENCHMARK IS LOCATED ON THE WEST SIDE OF THE LOT AND IS 12 FEET FROM THE EAST PROPERTY LINE. THE BENCHMARK IS 12 FEET FROM THE SOUTH PROPERTY LINE AND 12 FEET FROM THE WEST PROPERTY LINE.

PREPARED UNDER A PROFESSIONAL ENGINEERING CONTRACT FOR DIRECT SUPERVISION FOR DESIGN GROUP, INC.

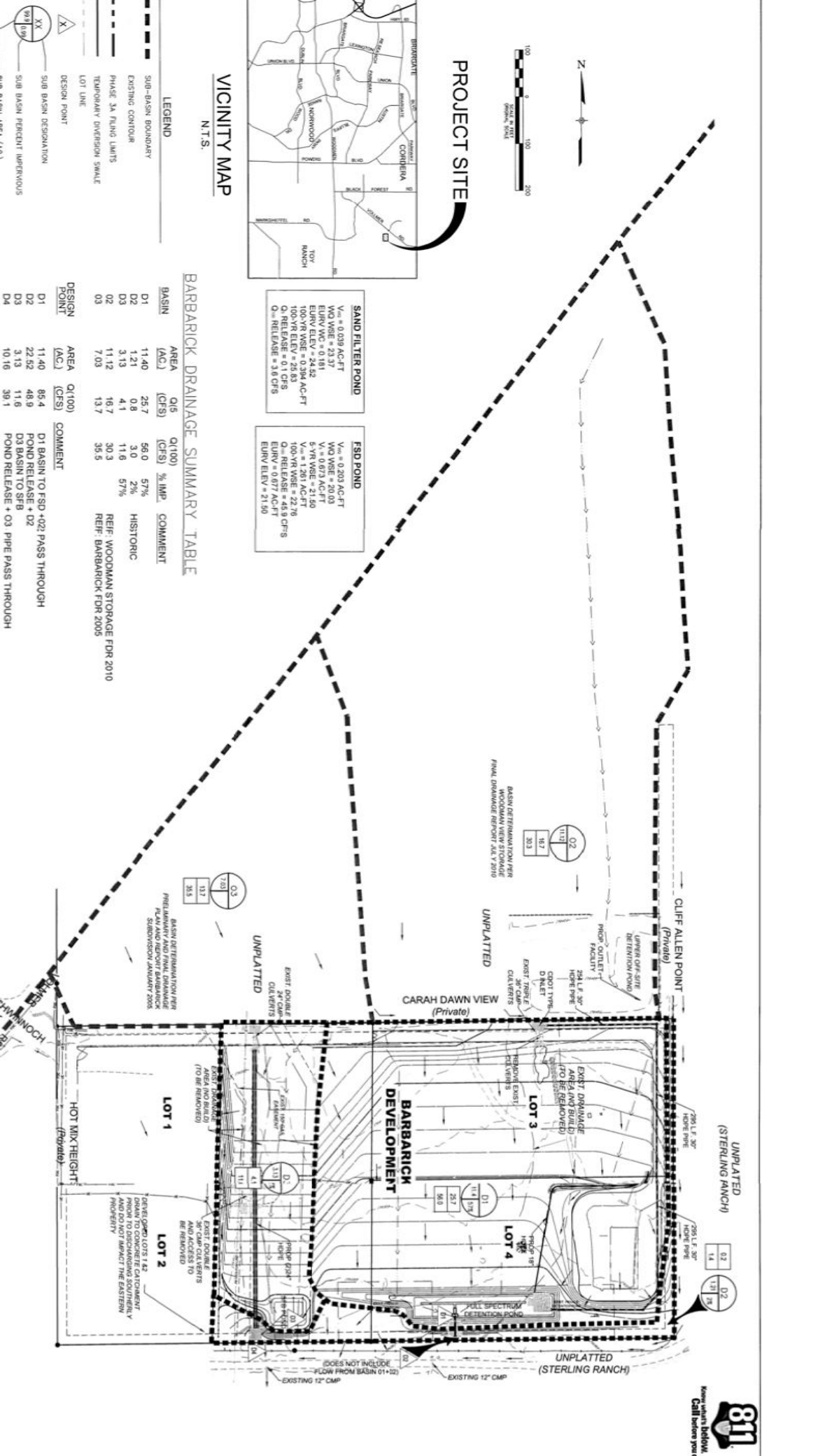
Matrix DESIGN GROUP
2435 Research Parkway, Suite 300
Colorado Springs, CO 80902
Phone: 719.572.0100
Fax: 719.572.0008

BARBARICK SUBDIVISION LOTS 1-4

PROPOSED DRAINAGE PLAN

DESIGNED BY: [Name] SCALE: 1"=100' DATE DRAINED: April 2011
DRAWN BY: [Name] SCALE: 1"=100' SHEET NO. 1 OF 2 SHEETS
CHECKED BY: [Name]

DP02

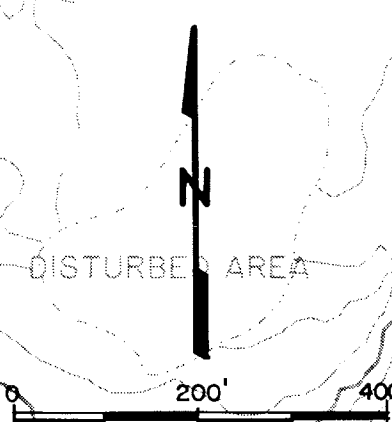


THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

MATCH STA 760+30 SHT 48

MATCH STA 47A

MATCH SHT 47B



DISTURBED AREA

IMPROVED RIPRAP CHANNEL
 BW = 40', d = 3', S = 1.0%
 3' DROPS @ 250' INTERVALS
 Q100 = 950 cfs

CHANNEL IMPROVEMENTS		
SEGMENT NO.	BOTTOM WIDTH (FT)	CHANNEL TYPE
151	N/A	SELECTIVE RIPRAP LININGS AND GRADE CONTROL
160		

FOR PROFILE SEE SHEET P-13

PROPOSED MARKSHEFFEL ROAD

EX EMBANKMENTS TO BE REMOVED

PRESERVE EX. VEGETATION & FLOODPLAIN

STA 758+00 CHECK

STA 748+00 CHECK

STA 738+00 CHECK

SAND CREEK REACH SC-B

TRIPLE 10' x 10' CBC

Kiowa Engineering Corporation
 419 W. Bijou Street
 Colorado Springs, Colorado
 80905-1308

SAND CREEK DRAINAGE BASIN PLANNING STUDY
 PRELIMINARY DESIGN PLANS

Project No	90-04-09
Date:	9-92
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	

MATCH SHT 48A

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

IMPROVED RIPRAP CHANNEL
BW = 25', d = 3', S = 1.19%
3' DROPS @ 200' INTERVALS
Q100 = 660 cfs

TEMPLETON GAP ROAD

REMOVE EX.
30' CMPs

NEW 2'-6" H x 10' W CBC

FOR CHANNEL DATA
SEE SHEET 46A

157

154



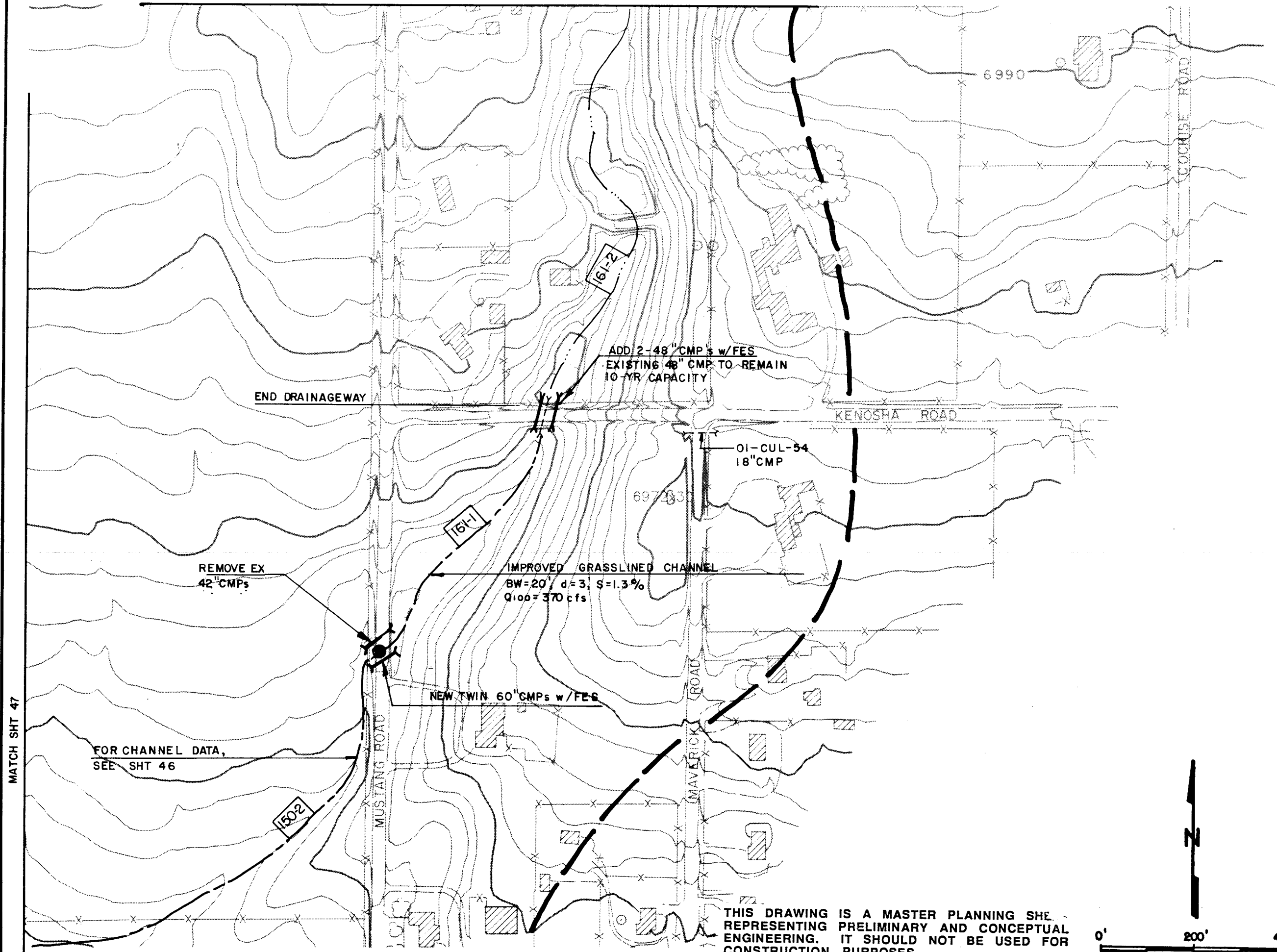
MATCH SHT 46A

MATCH SHT 47

Kiowa Engineering Corporation
419 W. Bijou Street
Colorado Springs, Colorado
80905-1308

SAND CREEK DRAINAGE
BASIN PLANNING STUDY
PRELIMINARY DESIGN PLANS

Project No:	04-09
Date:	12 / 92
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	



MATCH SHT 47

FOR CHANNEL DATA,
SEE SHT 46

END DRAINAGEWAY

ADD 2-48" CMP's w/FES
EXISTING 48" CMP TO REMAIN
10-YR CAPACITY

KENOSHA ROAD

01-CUL-54
18" CMP

IMPROVED GRASSLINED CHANNEL
BW=20', d=3', S=1.3%
Q₁₀₀=370 cfs

REMOVE EX
42" CMPs

NEW TWIN 60" CMPs w/FES

MUSTANG ROAD

MAVERICK ROAD



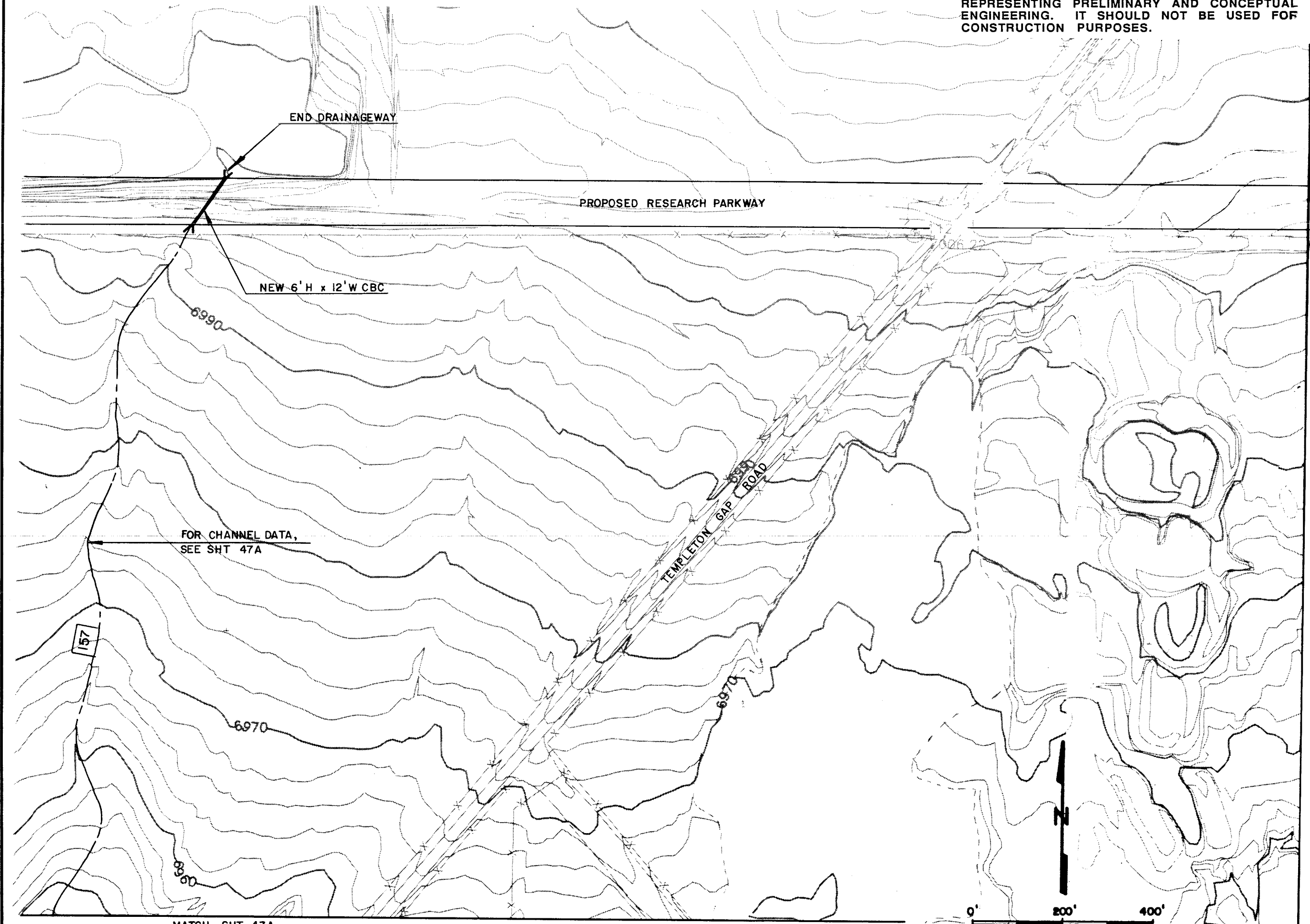
THIS DRAWING IS A MASTER PLANNING SHEET
REPRESENTING PRELIMINARY AND CONCEPTUAL
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CONSTRUCTION PURPOSES.

Kiowa Engineering Corporation
419 W. Bijou Street
Colorado Springs, Colorado
80905-1308

SAND CREEK DRAINAGE
BASIN PLANNING STUDY
PRELIMINARY DESIGN PLANS

Project No	90-04-09
Date:	12/92
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	

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SAND CREEK DRAINAGE
BASIN PLANNING STUDY
PRELIMINARY DESIGN PLANS

Project No	90-04-09
Date:	12/92
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Check:	RNW
Revisions:	

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

IMPROVED RIPRAP CHANNEL
BW = 25', d=3', S=1.2%
3' DROPS @ 270' INTERVALS
Q₁₀₀ = 600 cfs

PROPOSED RESEARCH PARKWAY

NEW 2-6' H x 9' W CBC
100-YR CAPACITY

FOR CHANNEL DATA,
SEE SHT 47

END FLOODPLAIN
DELINEATION

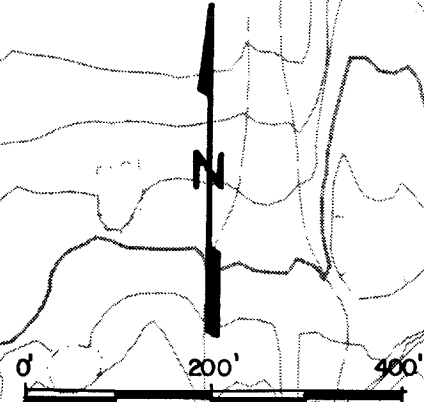
STA 768+00 CHECK

PRESERVE X VEGETATION
& FLOODPLAIN

MATCH STA 760+30 SHT 47

MATCH STA 768+80 SHT 49

MATCH SHT 48 A



CHANNEL IMPROVEMENTS

SEGMENT NO.	BOTTOM WIDTH (FT)	CHANNEL TYPE
100	NA	SELECTIVE RIPRAP LININGS AND GRADE CONTROL

FOR PROFILE SEE SHEETS P-13 AND P-14

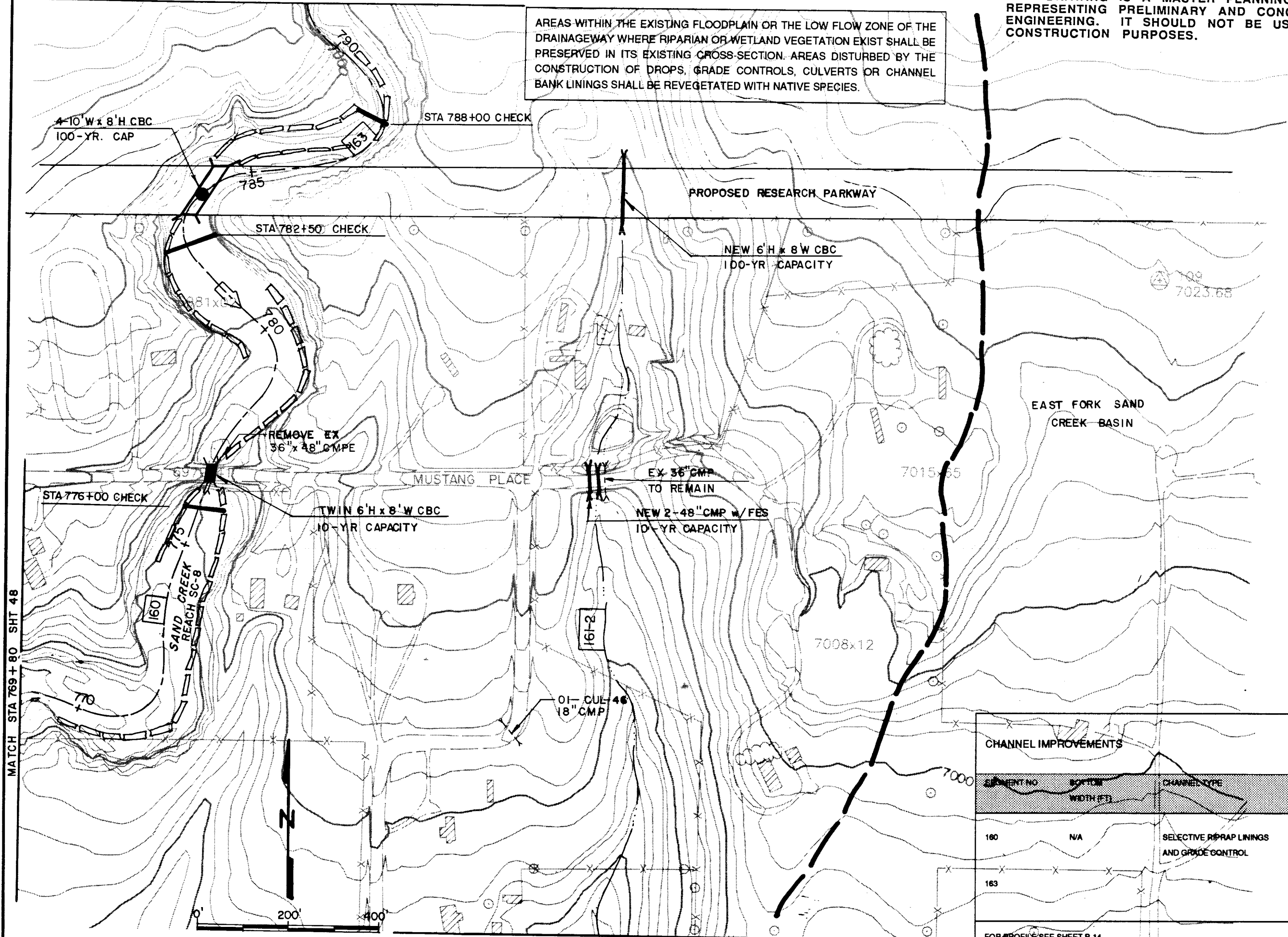
Kiowa Engineering Corporation
419 W. Bijou Street
Colorado Springs, Colorado
80905-1308

SAND CREEK DRAINAGE
BASIN PLANNING STUDY
PRELIMINARY DESIGN PLANS

Project No	90-04-08
Date:	9-92
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

AREAS WITHIN THE EXISTING FLOODPLAIN OR THE LOW FLOW ZONE OF THE DRAINAGEWAY WHERE RIPARIAN OR WETLAND VEGETATION EXIST SHALL BE PRESERVED IN ITS EXISTING CROSS-SECTION. AREAS DISTURBED BY THE CONSTRUCTION OF DROPS, GRADE CONTROLS, CULVERTS OR CHANNEL BANK LININGS SHALL BE REVEGETATED WITH NATIVE SPECIES.



CHANNEL IMPROVEMENTS		
ELEMENT NO.	BOTTOM WIDTH (FT)	CHANNEL TYPE
160	N/A	SELECTIVE RIPRAP LININGS AND GRADE CONTROL
163		

FOR PROFILE SEE SHEET P-14

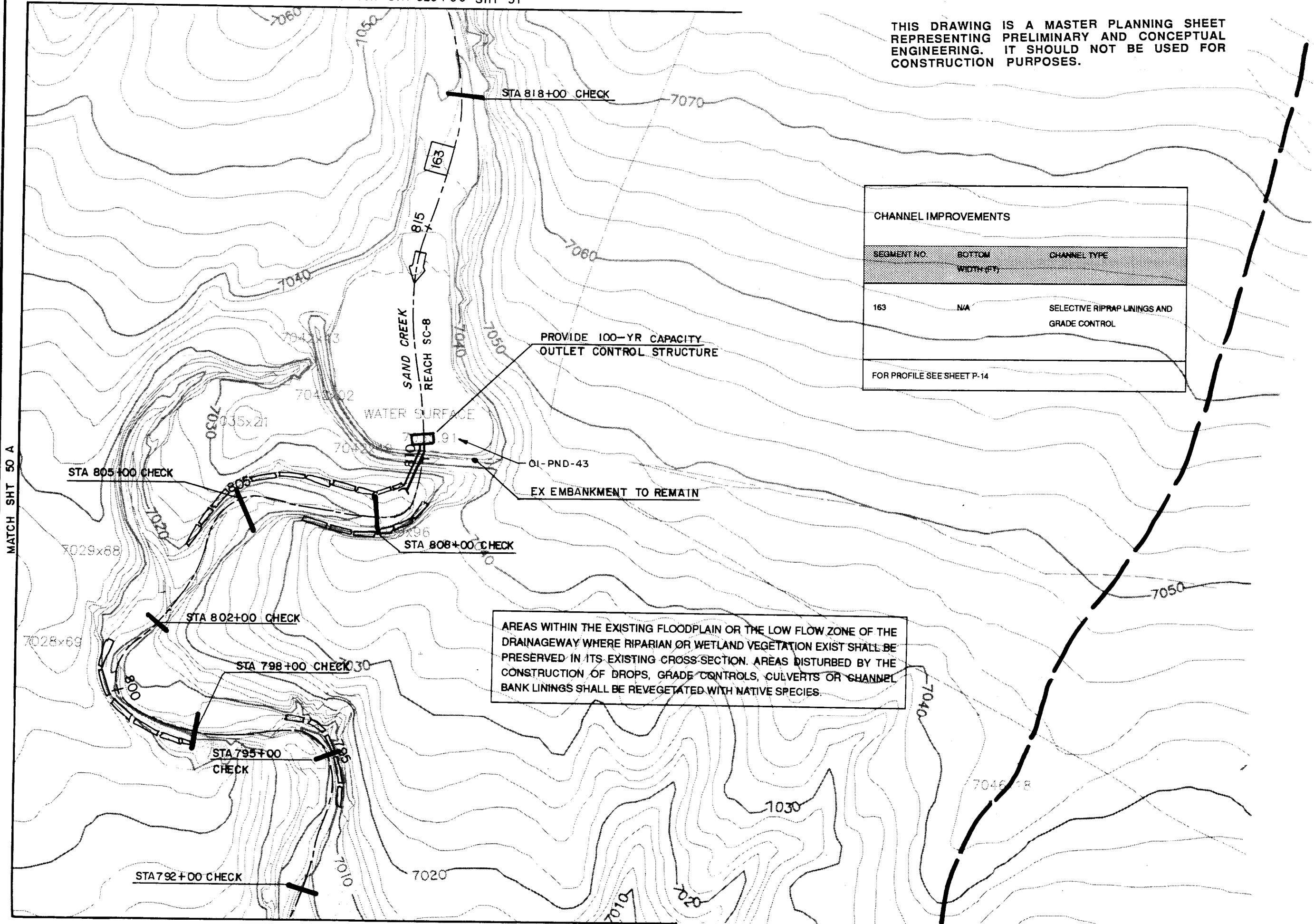
Kiowa Engineering Corporation
 419 W. Bijou Street
 Colorado Springs, Colorado
 80905-1308

SAND CREEK DRAINAGE BASIN PLANNING STUDY
 PRELIMINARY DESIGN PLANS

Project No 90-04-09
 Date: 9-92
 Design: RNW
 Drawn: EAK
 Check: RNW
 Revisions:

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

CHANNEL IMPROVEMENTS		
SEGMENT NO	BOTTOM WIDTH (FT)	CHANNEL TYPE
163	N/A	SELECTIVE RIPRAP LININGS AND GRADE CONTROL
FOR PROFILE SEE SHEET P-14		



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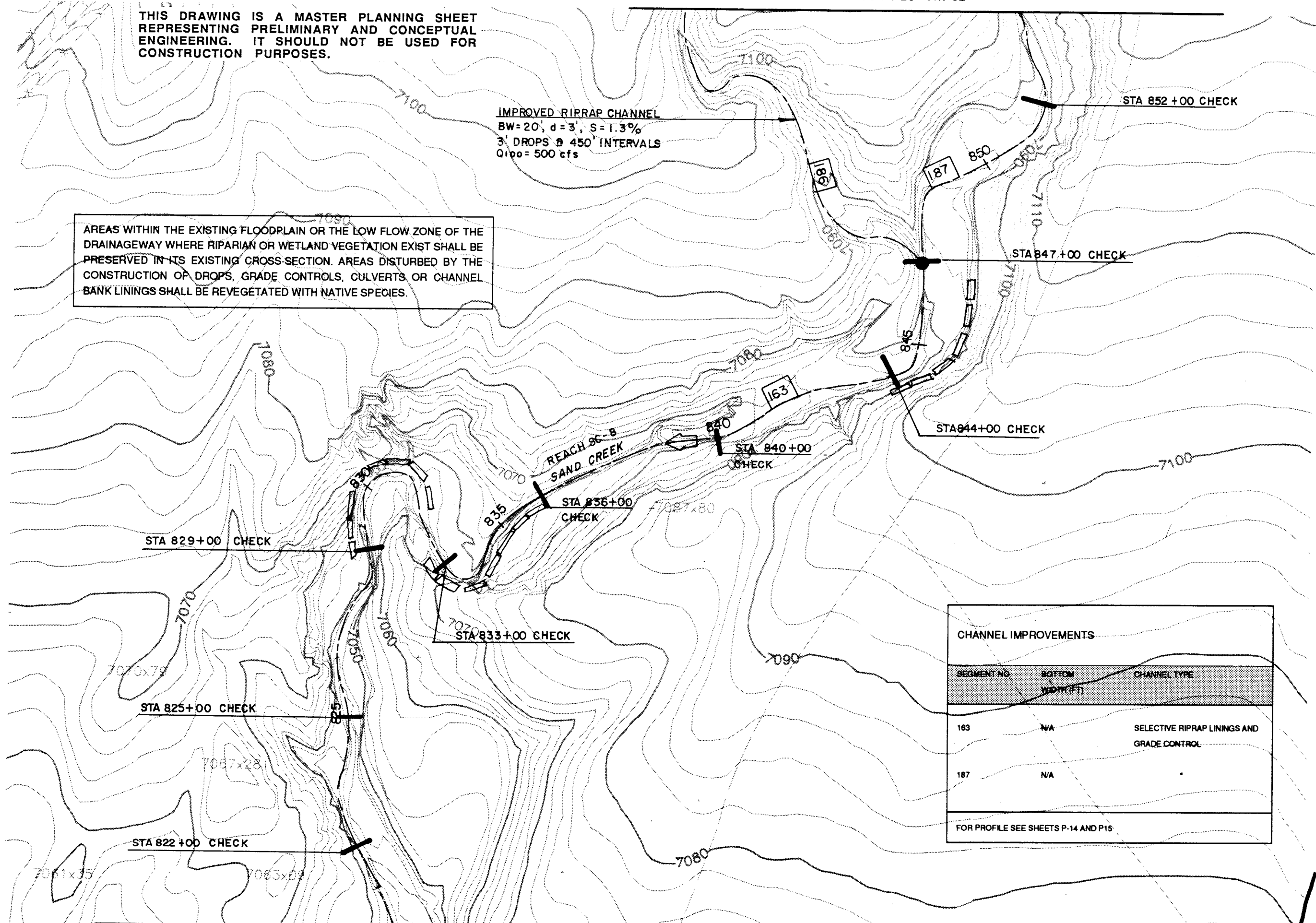
SAND CREEK DRAINAGE
 BASIN PLANNING STUDY
 PRELIMINARY DESIGN PLANS

Project No	90-04-09
Date	11/92
Design	RNW
Drawn	EAK
Check	RNW
Revisions	

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

AREAS WITHIN THE EXISTING FLOODPLAIN OR THE LOW FLOW ZONE OF THE DRAINAGEWAY WHERE RIPARIAN OR WETLAND VEGETATION EXIST SHALL BE PRESERVED IN ITS EXISTING CROSS-SECTION. AREAS DISTURBED BY THE CONSTRUCTION OF DROPS, GRADE CONTROLS, CULVERTS OR CHANNEL BANK LININGS SHALL BE REVEGETATED WITH NATIVE SPECIES.

IMPROVED RIPRAP CHANNEL
 BW=20', d=3', S=1.3%
 3' DROPS @ 450' INTERVALS
 Q₁₀₀=500 cfs



CHANNEL IMPROVEMENTS		
SEGMENT NO	BOTTOM WIDTH (FT)	CHANNEL TYPE
163	N/A	SELECTIVE RIPRAP LININGS AND GRADE CONTROL
187	N/A	

FOR PROFILE SEE SHEETS P-14 AND P15

Kiowa Engineering Corporation
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 Colorado Springs, Colorado
 80905-1308

SAND CREEK DRAINAGE BASIN PLANNING STUDY
 PRELIMINARY DESIGN PLANS

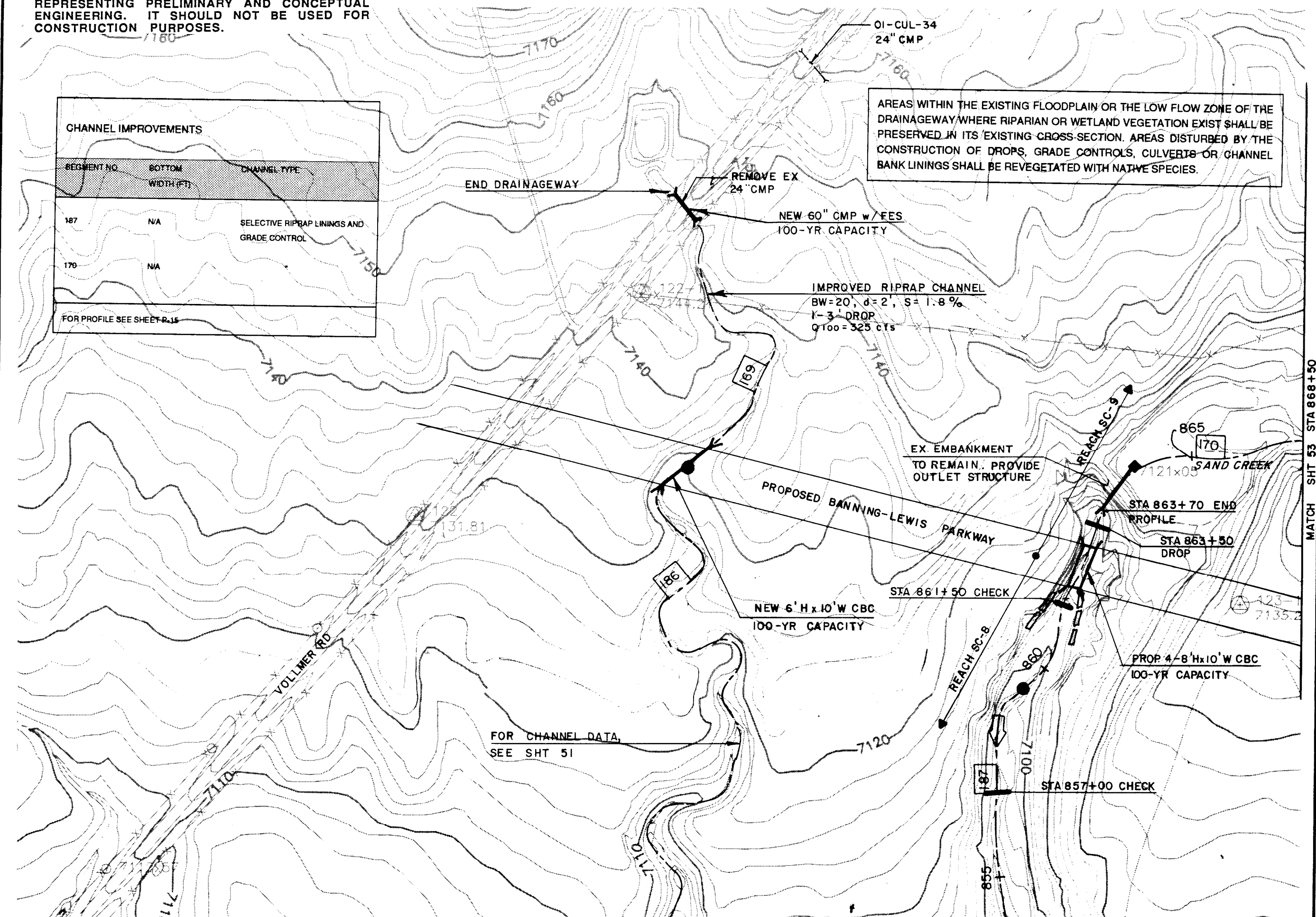
Project No 90-04-09
 Date: 11/92
 Design: RNW
 Drawn: EAK
 Check: RNW
 Revisions:

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

CHANNEL IMPROVEMENTS		
REACHMENT NO.	BOTTOM WIDTH (FT)	CHANNEL TYPE
187	N/A	SELECTIVE RIPRAP LININGS AND GRADE CONTROL
170	N/A	

FOR PROFILE SEE SHEET P-15

AREAS WITHIN THE EXISTING FLOODPLAIN OR THE LOW FLOW ZONE OF THE DRAINAGEWAY WHERE RIPARIAN OR WETLAND VEGETATION EXIST SHALL BE PRESERVED IN ITS EXISTING CROSS-SECTION. AREAS DISTURBED BY THE CONSTRUCTION OF DROPS, GRADE CONTROLS, CULVERTS OR CHANNEL BANK LININGS SHALL BE REVEGETATED WITH NATIVE SPECIES.

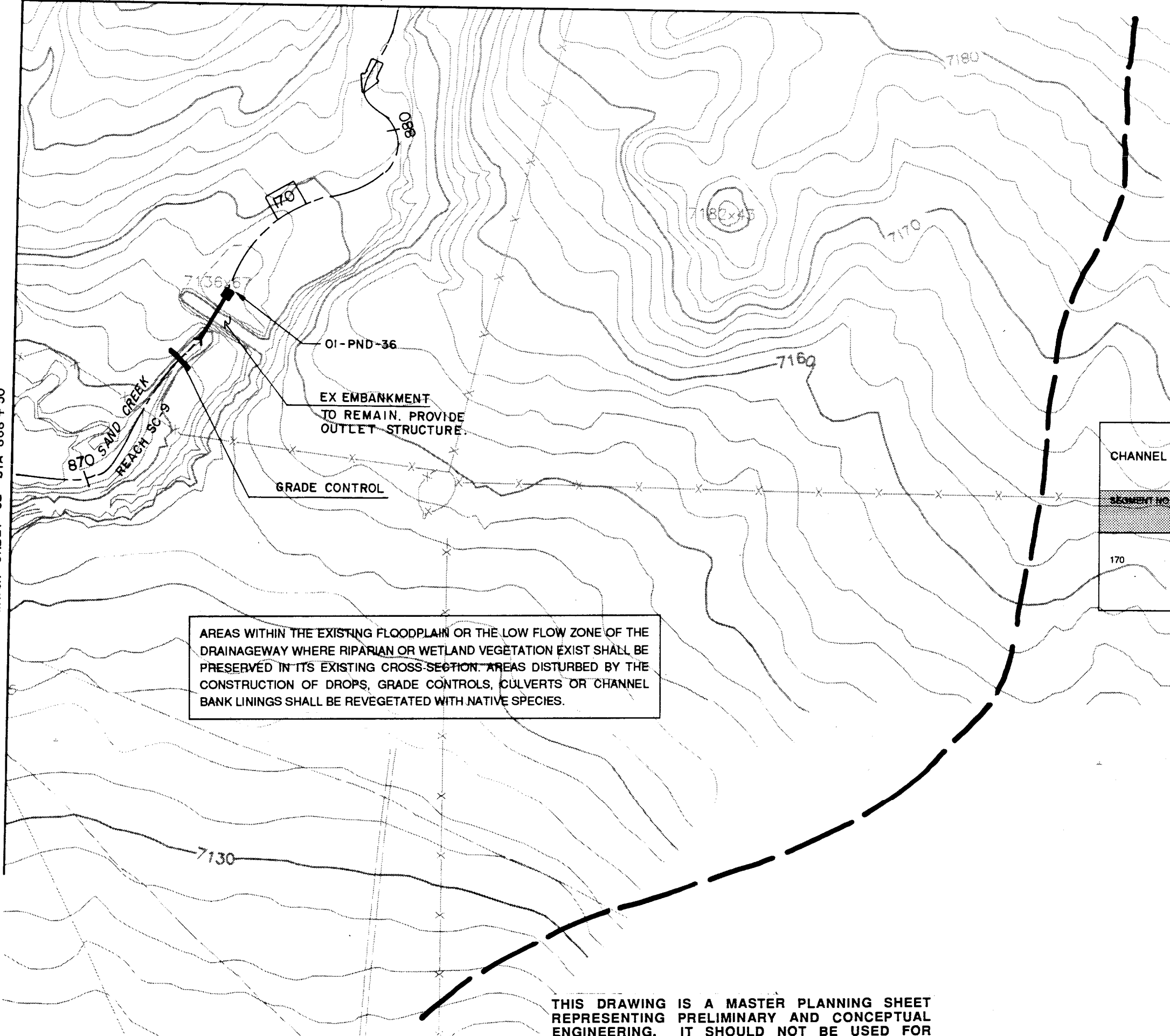


MATCH SHT 53 STA 868+50

**SAND CREEK DRAINAGE BASIN PLANNING STUDY
PRELIMINARY DESIGN PLANS**

Project No	90-04-09
Date	11/92
Design	RNW
Drawn	EAK
Check	RNW
Revisions	

Kiowa Engineering Corporation
 419 W. Bijou Street
 Colorado Springs, Colorado
 80905-1308



AREAS WITHIN THE EXISTING FLOODPLAIN OR THE LOW FLOW ZONE OF THE DRAINAGEWAY WHERE RIPARIAN OR WETLAND VEGETATION EXIST SHALL BE PRESERVED IN ITS EXISTING CROSS-SECTION. AREAS DISTURBED BY THE CONSTRUCTION OF DROPS, GRADE CONTROLS, CULVERTS OR CHANNEL BANK LININGS SHALL BE REVEGETATED WITH NATIVE SPECIES.

THIS DRAWING IS A MASTER PLANNING SHEET REPRESENTING PRELIMINARY AND CONCEPTUAL ENGINEERING. IT SHOULD NOT BE USED FOR CONSTRUCTION PURPOSES.

CHANNEL IMPROVEMENTS		
SEGMENT NO.	Q TO	CHANNEL TYPE
170	670 2260	SELECTIVE RIPRAP LININGS AND GRADE CONTROL

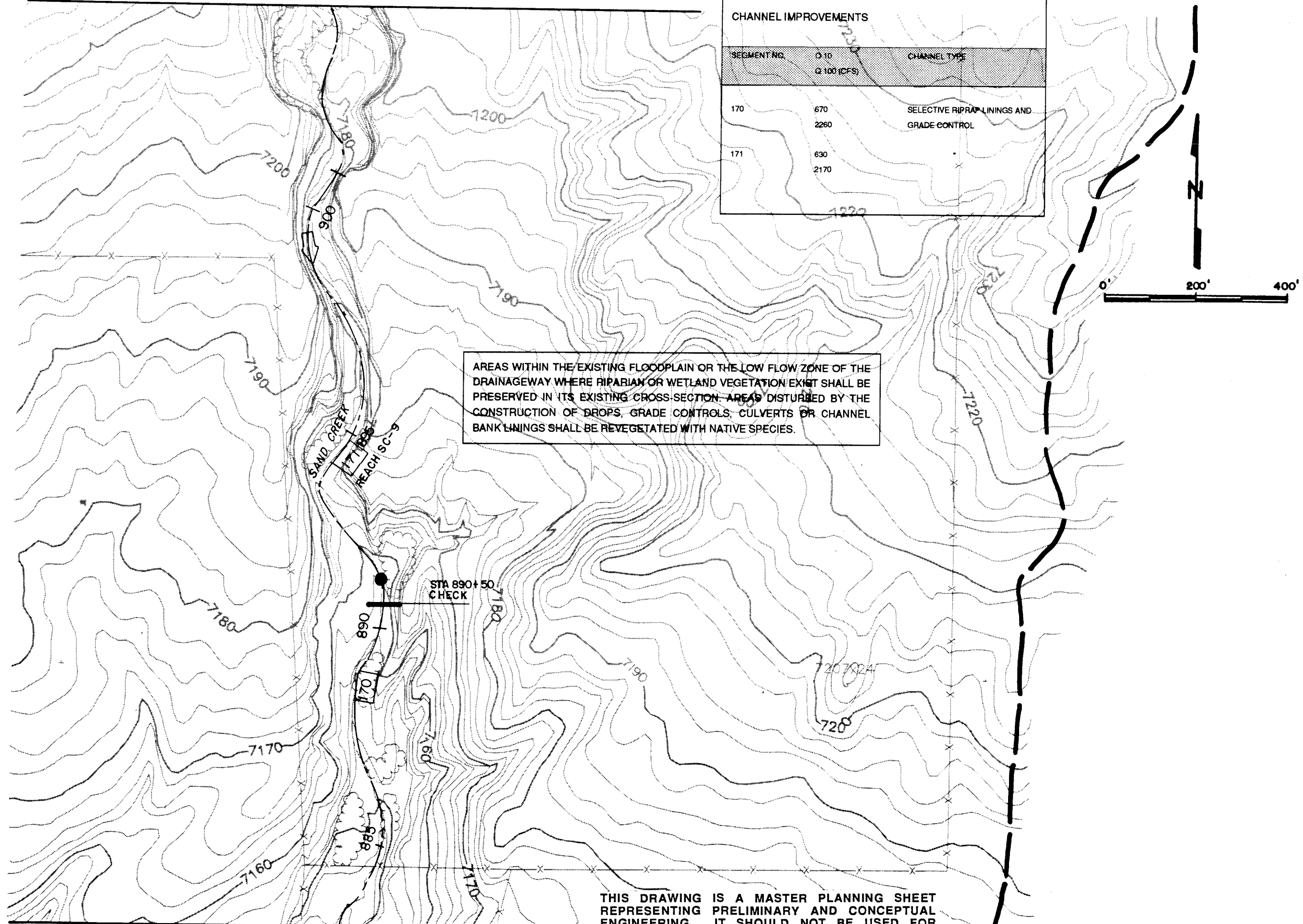
Kiowa Engineering Corporation
 419 W. Bijou Street
 Colorado Springs, Colorado
 80905-1308

SAND CREEK DRAINAGE
 BASIN PLANNING STUDY
 PRELIMINARY DESIGN PLANS

Project No 90-04-09
 Date: 9-92
 Design: RNW
 Drawn: EAK
 Check: RNW
 Revisions:

MATCH SHT 55 STA 905+00

CHANNEL IMPROVEMENTS		
SEGMENT NO.	Q 10	CHANNEL TYPE
170	670 2260	SELECTIVE RIPRAP LININGS AND GRADE CONTROL
171	630 2170	



AREAS WITHIN THE EXISTING FLOODPLAIN OR THE LOW FLOW ZONE OF THE DRAINAGEWAY WHERE RIPARIAN OR WETLAND VEGETATION EXIST SHALL BE PRESERVED IN ITS EXISTING CROSS-SECTION. AREAS DISTURBED BY THE CONSTRUCTION OF DROPS, GRADE CONTROLS, CULVERTS OR CHANNEL BANK LININGS SHALL BE REVEGETATED WITH NATIVE SPECIES.

STA 890+50
CHECK

MATCH SHT 53 STA 883+00

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Kiowa Engineering Corporation
419 W. Bijou Street
Colorado Springs, Colorado
80905-1308

SAND CREEK DRAINAGE
BASIN PLANNING STUDY
PRELIMINARY DESIGN PLANS

Project No	90-04-09
Date:	9/92
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	

STERLING RANCH FILING NO. 2 - TRACTS AND RIGHT-OF-WAY - DRAINAGE & BRIDGE FEES (2020)

TRACT/ROW	SIZE/ACRE	USE	MAINTENANCE	OWNERSHIP	% Impervious	DRAINAGE FEE	FEE	BRIDGE FEE	FEE
A	0.391	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	29.0%	\$ 19,698	\$ 2,233.56	\$ 8,057	\$ 913.58
B	0.658	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	29.0%	\$ 19,698	\$ 3,758.77	\$ 8,057	\$ 1,537.44
C	0.845	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	24.0%	\$ 19,698	\$ 3,994.75	\$ 8,057	\$ 1,633.96
D	2.159	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	13.0%	\$ 19,698	\$ 5,528.64	\$ 8,057	\$ 2,261.36
E	19.674	ZERO LOT LINE FUTURE SINGLE FAMILY RESIDENTIAL LOTS	SR LAND, LLC	SR LAND, LLC	70.0%	\$ 19,698	\$ 271,276.92	\$ 8,057	\$ 110,959.39
F	1.231	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	4.0%	\$ 19,698	\$ 969.93	\$ 8,057	\$ 396.73
G	0.249	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	2.0%	\$ 19,698	\$ 98.10	\$ 8,057	\$ 40.12
H	0.062	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	2.0%	\$ 19,698	\$ 24.43	\$ 8,057	\$ 9.99
I	0.5	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY/MAIL KIOSK	SRMD #1	SRMD #1	15.0%	\$ 19,698	\$ 1,477.35	\$ 8,057	\$ 604.28
J	0.379	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	30.0%	\$ 19,698	\$ 2,239.66	\$ 8,057	\$ 916.08
K	0.387	LANDSCAPE/PUBLIC IMPROVEMENTS/PUBLIC UTILITY	SRMD #1	SRMD #1	30.0%	\$ 19,698	\$ 2,286.94	\$ 8,057	\$ 935.42
49 LOTS	11.871	SINGLE FAMILY RESIDENTIAL LOTS	SRMD #1	SRMD #1	70.0%	\$ 19,698	\$ 163,684.47	\$ 8,057	\$ 66,951.25
ROW	4.734	ROAD RIGHTS OF WAY (STERLING RANCH ROAD)	EPC	EPC	95.0%	\$ 19,698	\$ 88,587.82	\$ 8,057	\$ 36,234.75
ROW	3.525	ROAD RIGHTS OF WAY (MARKSHEFFEL ROAD)	EPC	EPC	95.0%	\$ 19,698	\$ 65,963.68	\$ 8,057	\$ 26,980.88
ROW	2.979	ROAD RIGHTS OF WAY (VOLLMER ROAD, ULTIMATE)	EPC	EPC	95.0%	\$ 19,698	\$ 55,746.32	\$ 8,057	\$ 22,801.71
							DRAINAGE FEE		BRIDGE FEE
	49.644	TOTAL AREA				TOTAL FEES	\$ 667,871.33		\$ 273,176.94

*SRMD#1 = STERLING RANCH METROPOLITAN DISTRICT NO. 1



Know what's below.
Call before you dig.

SAND CREEK STABILIZATION AT ASPEN MEADOWS

SUBDIVISION FILING NO. 1

COLORADO LAND ACQUISITION

100% DESIGN PLANS

APRIL 2020

MATRIX PROJECT No. 19.886.017

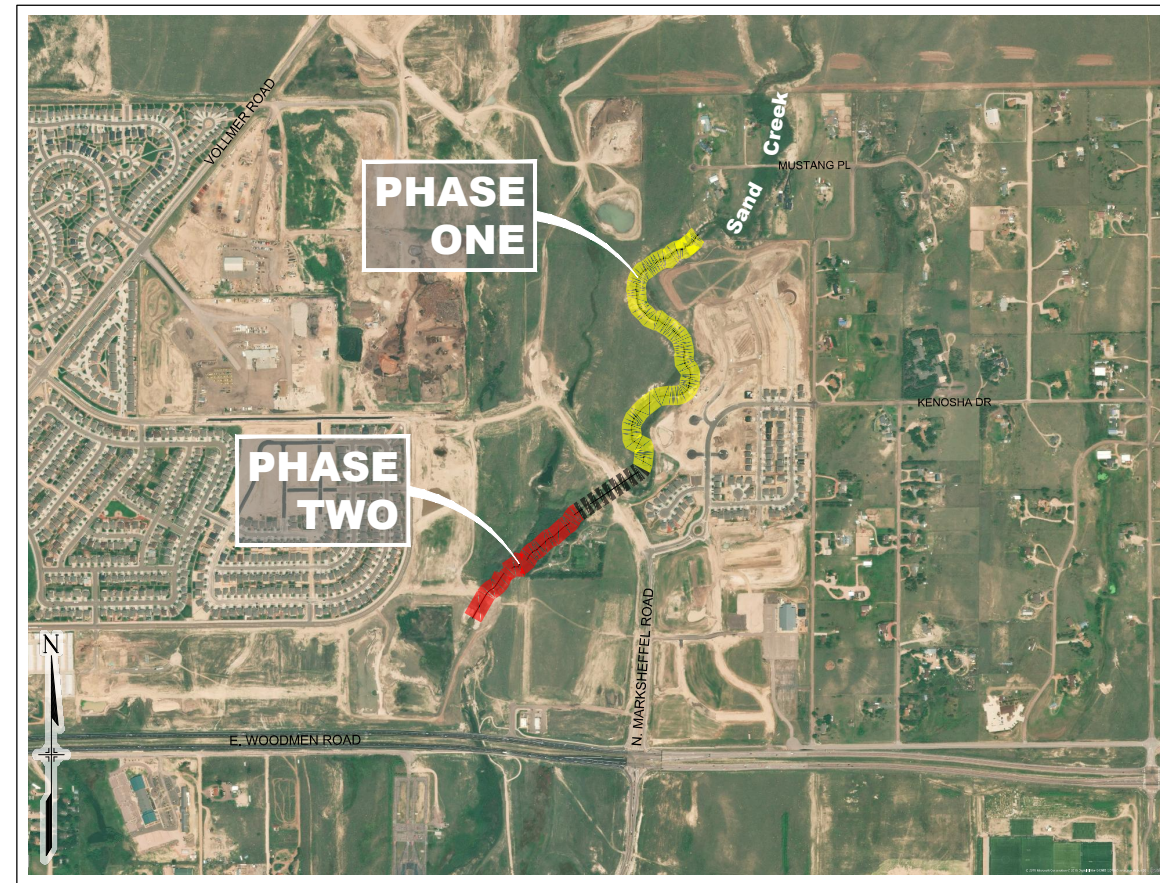


VICINITY MAP
N.T.S.

ENGINEER'S STATEMENT:

THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID DETAILED PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE ESTABLISHED CRITERIA FOR DETAILED DRAINAGE PLANS AND SPECIFICATIONS, AND SAID DETAILED PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH THE MASTER PLAN OF THE DRAINAGE BASIN. SAID DETAILED DRAINAGE PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR DRAINAGE FACILITY(S) IS DESIGNED. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THE DETAILED DRAINAGE PLANS AND SPECIFICATIONS.

SIGNED: _____ DATE: _____



LOCATION MAP
SCALE: 1" = 1500'

PLAN REVIEW BY CITY OF COLORADO SPRINGS IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH DESIGN CRITERIA. THE CITY OF COLORADO SPRINGS IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE CITY OF COLORADO SPRINGS, THROUGH THE APPROVAL OF THIS DOCUMENT, ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

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DT21	SHEET PILE DETAILS	34
DT22-24	TYPICAL GRADE CONTROL DETAILS	35-37
DT25	EROSION CONTROL FABRIC DETAILS	38

VERTICAL DATUM: THE ELEVATIONS ON THIS PROJECT ARE REFERENCED TO THE NATIONAL GEODETIC VERTICAL DATUM OF 1929.

AERIAL PHOTO: PROVIDED BY AERIAL MAPPING SERVICES.

BENCHMARK STATEMENT: BENCHMARK: THE BENCHMARK USED FOR THIS SURVEY IS A FACILITIES INFORMATION MANAGEMENT SYSTEM (FIMS) SURVEY CONTROL MONUMENT NUMBER "F_69" BEING A FOUND 3-1/4" ALUMINUM CAP IN A RANGE BOX, LOCATED ON THE WEST SIDE OF BLACK FOREST ROAD, JUST SOUTH OF THE SCHMIDT CONSTRUCTION COMPANY DRIVEWAY. THE VERTICAL CONTROL VALUES ARE BASED ON NATIONAL GEODETIC VERTICAL DATUM (NGVD 29), 1929 AND THE 1960 SUPPLEMENTARY ADJUSTMENT. 6975.62 U.S. SURVEY FEET.

OWNER / DEVELOPER:

DATE:

COLORADO LAND ACQUISITION, LLC
TIM BUSCHAR
7910 GATEWAY BOULEVARD, STE 102
EL PASO, TX 79915

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
X-886-MDG22x34				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-TS01.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 3:13 PM				
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.				

CITY OF COLORADO SPRINGS ONLY:
FILED IN ACCORDANCE WITH SECTION 7.7.906 OF THE CODE OF THE CITY OF COLORADO SPRINGS, 2001, AS AMENDED.

FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



PRELIMINARY THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND IS SUBJECT TO CHANGE	COLORADO LAND ACQUISITION SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS
TITLE SHEET	
FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 19.886.017	DESIGNED BY: JAB DRAWN BY: RAF CHECKED BY: AJS
SCALE: HORIZ N/A VERT. N/A	DATE ISSUED: February 2020 SHEET 01 OF 38
	DRAWING No. TS01



Know what's below.
Call before you dig.

GENERAL NOTES:

1. THE LOCATIONS OF EXISTING ABOVE GROUND AND UNDERGROUND UTILITIES ARE SHOWN IN THEIR APPROXIMATE LOCATIONS ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. CONTRACTOR TO CALL FOR UTILITY LOCATOR AT LEAST 3 CALENDAR DAYS BEFORE EARTHWORK. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY THEIR FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL ABOVE GROUND AND UNDERGROUND UTILITIES. IN THE EVENT THAT THE CONTRACTOR UTILITY VERIFICATION RESULTS IN EXISTING STRUCTURES OR UTILITIES BEING IN CONFLICT WITH THE PROPOSED WORK OF THIS CONTRACT, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY UTILITIES AND COORDINATE ANY NEEDED MODIFICATIONS TO THE PROPOSED WORK AS DIRECTED BY AFFECTED AGENCY OR UTILITY.
2. THE CONTRACTOR SHALL COORDINATE WITH ALL AFFECTED UTILITY OWNERS TO ESTABLISH THE REQUIREMENTS AND METHODS TO ACCOMMODATE THE PROTECTION, TEMPORARY SUPPORT, ADJUSTMENT OR RELOCATION OF UTILITIES PRIOR TO THE START OF CONSTRUCTION.
3. OVERHEAD UTILITIES ARE NOT INDICATED ON PROFILE OR SECTION DRAWINGS.
4. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING AND MAINTAINING IN CONTINUOUS OPERATION, ALL EXISTING STRUCTURES. NOT ALL POTENTIALLY IMPACTED STRUCTURES MAY BE SHOWN ON THE DRAWINGS AND IT IS THE CONTRACTOR'S RESPONSIBILITY TO IDENTIFY AND PROTECT ALL STRUCTURES INCLUDING BUT NOT LIMITED TO STREETS, CURB AND GUTTER, BRIDGE PIERS AND ABUTMENTS, CREEK BANK PROTECTION OF VARIOUS TYPES, CREEK DROP STRUCTURES, SIGNS, PEDESTRIAN WALKS, RETAINING WALLS AND FENCING. IN THE EVENT THAT A STRUCTURE OR UTILITY IS DAMAGED DURING CONSTRUCTION THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE OWNER OF THE FACILITY IN WRITING AND COORDINATE AND COOPERATE WITH NEEDED REPAIRS PER THE APPROPRIATE SPECIFICATIONS ACCORDING TO THE OWNER'S DIRECTION.
5. THE CONTRACTOR SHALL CONFIRM THE RECEIPT OF ALL NECESSARY PERMITS AND APPROVALS BEFORE THE START OF CONSTRUCTION.
6. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE STANDARDS OF THE CITY OF COLORADO SPRINGS UNLESS SPECIFICALLY DETAILED OTHERWISE ON THESE PLANS AND ASSOCIATED SPECIFICATIONS.
7. THE CONTRACTOR SHALL MAINTAIN AT THE SITE AT ALL TIMES ONE SIGNED COPY OF THE PROJECT DRAWINGS AND SPECIFICATIONS, ONE COPY OF THE STORMWATER MANAGEMENT PLAN AND ONE COPY OF ALL REQUIRED PERMITS.
8. THE CONTRACTOR SHALL CONDUCT THEIR OPERATIONS IN SUCH A WAY THAT THE AREA OF DISTURBANCE IS MINIMIZED. ALL EXISTING TREES, SHRUBS AND VEGETATION SHALL BE PROTECTED UNLESS OTHERWISE NOTED ON THE DRAWINGS. NO TREES SHALL BE REMOVED WITHOUT APPROVAL. DESIGNATED ACCESS SHALL BE MINIMAL AND AGREED UPON WITH THE ENGINEER PRIOR TO CONSTRUCTION ACTIVITIES.
9. FOR ALL SITE GRADING, SMOOTH, PARABOLIC TRANSITIONS SHALL BE MADE BETWEEN CHANGES IN SLOPE.
10. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR PROVIDING STABLE EXCAVATIONS AND TEMPORARY SLOPES AND FOR SATISFYING ALL APPLICABLE FEDERAL, STATE AND LOCAL REGULATIONS.
11. CONSTRUCTION OF THE PROPOSED WORK WILL TAKE PLACE WITHIN THE CHANNEL AND WATER CONTROL MEASURES WILL BE REQUIRED. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE ACCEPTANCE AND CONTROL OF DRAINAGE WATER FROM AREAS ADJACENT TO SAND CREEK AND FOR FLOW WITHIN SAND CREEK AND ITS TRIBUTARIES INCLUDING STORMWATER OUTFALLS. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR ESTABLISHING MEANS AND METHODS OF GROUND AND SURFACE WATER CONTROL APPROPRIATE FOR CONSTRUCTION IN ACCORDANCE WITH THE REQUIREMENTS OF THE PROJECT DRAWINGS AND SPECIFICATIONS AND ALL APPLICABLE FEDERAL, STATE AND LOCAL REGULATIONS AND PERMITS.
12. THE CONTRACTOR SHALL PREPARE AND MAINTAIN THE STORMWATER MANAGEMENT PLAN AND OBTAIN THE NATIONAL POLLUTION DISCHARGE ELIMINATION SYSTEM (NPDES) PERMIT THROUGH THE COLORADO DEPARTMENT OF PUBLIC HEALTH (CDPHE) AND ALL OTHER APPROPRIATE FEDERAL, STATE AND LOCAL PERMITS.
13. CONTRACTOR SHALL BE RESPONSIBLE FOR AS-BUILT DRAWINGS TO BE MAINTAINED AND SUBMITTED TO THE CITY OF COLORADO SPRINGS.
14. THE CONTRACTOR SHALL PROVIDE AND MAINTAIN ON-SITE SURVEY CONTROL AND CONSTRUCTION STAKING.
15. CONTRACTOR SHALL FENCE OFF CRITICAL AREAS TO BE PROTECTED AT THE DISCRETION OF THE CITY OF COLORADO SPRINGS.
16. THE CONTRACTOR SHALL DEVELOP A TRAFFIC CONTROL PLAN FOR PLANNED ACCESS TO THE SITE AND FOR EXITING AND ENTERING PUBLIC ROADS.
17. THE CONTRACTOR SHALL BE RESPONSIBLE FOR IDENTIFYING AND MAINTAINING PHYSICAL AND LEGAL ACCESS TO THE PROJECT SITE AND SHALL LIMIT TRANSPORTATION TO AND FROM THE SITE TO THOSE APPROVED BY THE CITY OF COLORADO SPRINGS.
18. THE CONTRACTOR SHALL TAKE MEASURES TO PREVENT AND MANAGE SPILLS OF TOXIC MATERIALS, SUCH AS EQUIPMENT FUELS
19. ALL MATERIALS USED SHALL BE NEW AND WITHOUT FLAWS OR DEFECTS OF ANY TYPE AND SHALL BE THE BEST OF THEIR CLASS AND KIND.
20. WORK INCLUDES FURNISHING OF LABOR, MATERIALS, TOOLS, AND EQUIPMENT TO COMPLETE THE CONSTRUCTION OF ALL ELEMENTS OF THE DESIGN PLANS.

ABBREVIATIONS

CL	CENTER LINE	APPROX.	APPROXIMATE
HCL	HORIZONTAL CONTROL LINE	MIN.	MINIMUM
DIA	DIAMETER	MAX.	MAXIMUM
EX/EXIST	EXISTING	HORIZ	HORIZONTAL
EL./ELEV	ELEVATION	VERT.	VERTICAL
FT.	FEET	DIST.	DISTANCE
INV.	INVERT	NTS	NOT TO SCALE
LF	LINEAR FEET	TYP	TYPICAL
LT	LEFT	O.C.	ON CENTER
N,S,E,W	NORTH, SOUTH, EAST, WEST	L.O.C.	LIMITS OF CONSTRUCTION
PL	PROPERTY LINE	RR	RAILROAD
ROW	RIGHT-OF-WAY	BCL	BANKFULL CONTROL LINE
RT	RIGHT	TCL	THALWEG CONTROL LINE
SF	SQUARE FEET		
STA.	STATION		

STANDARD SYMBOLS

	CENTER LINE
	EXISTING CONTOURS
	PROPOSED CONTOURS
	L.O.C.
	CONSTRUCTION ACCESS
	ROW
	RAILROAD ROW
	PROTECT EXISTING VEGETATION

LEGEND

	PROPOSED GROUDED BOULDER DROP STRUCTURE
	PROPOSED GROUDED BOULDER DROP STRUCTURE BURIED WITH TOPSOIL & REVEGETATION
	PROPOSED SOIL RIPRAP
	PROPOSED SOIL RIPRAP - BURIED WITH TOPSOIL & REVEGETATION

REFERENCE DRAWINGS				
X-886-MDG22x34				
No.	DATE	DESCRIPTION	BY	
		REVISIONS		
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CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 3:29 PM				
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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



PREPARED BY:
Matrix
Excellence by Design

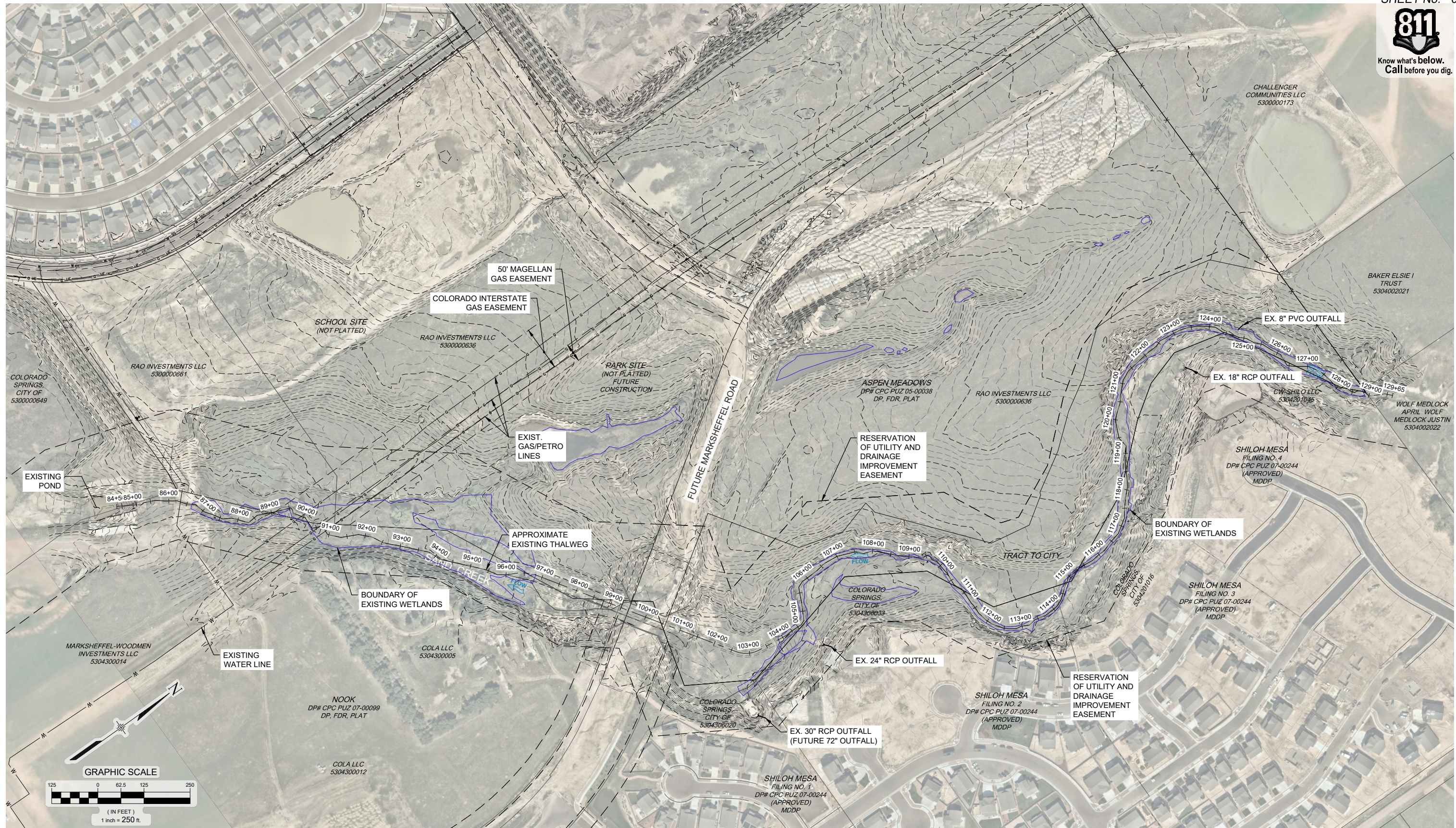
SEAL
PRELIMINARY
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION				
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS				
LEGEND AND GENERAL NOTES				
DESIGNED BY:	JAB	SCALE:	DATE ISSUED:	February 2020
DRAWN BY:	RAF	HORIZ:	N/A	
CHECKED BY:	AJS	VERT:	N/A	SHEET
				02 OF 38
				DRAWING No. GN01



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COMPUTER FILE MANAGEMENT			
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PLOT DATE: 5/20/2020 3:56 PM			
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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



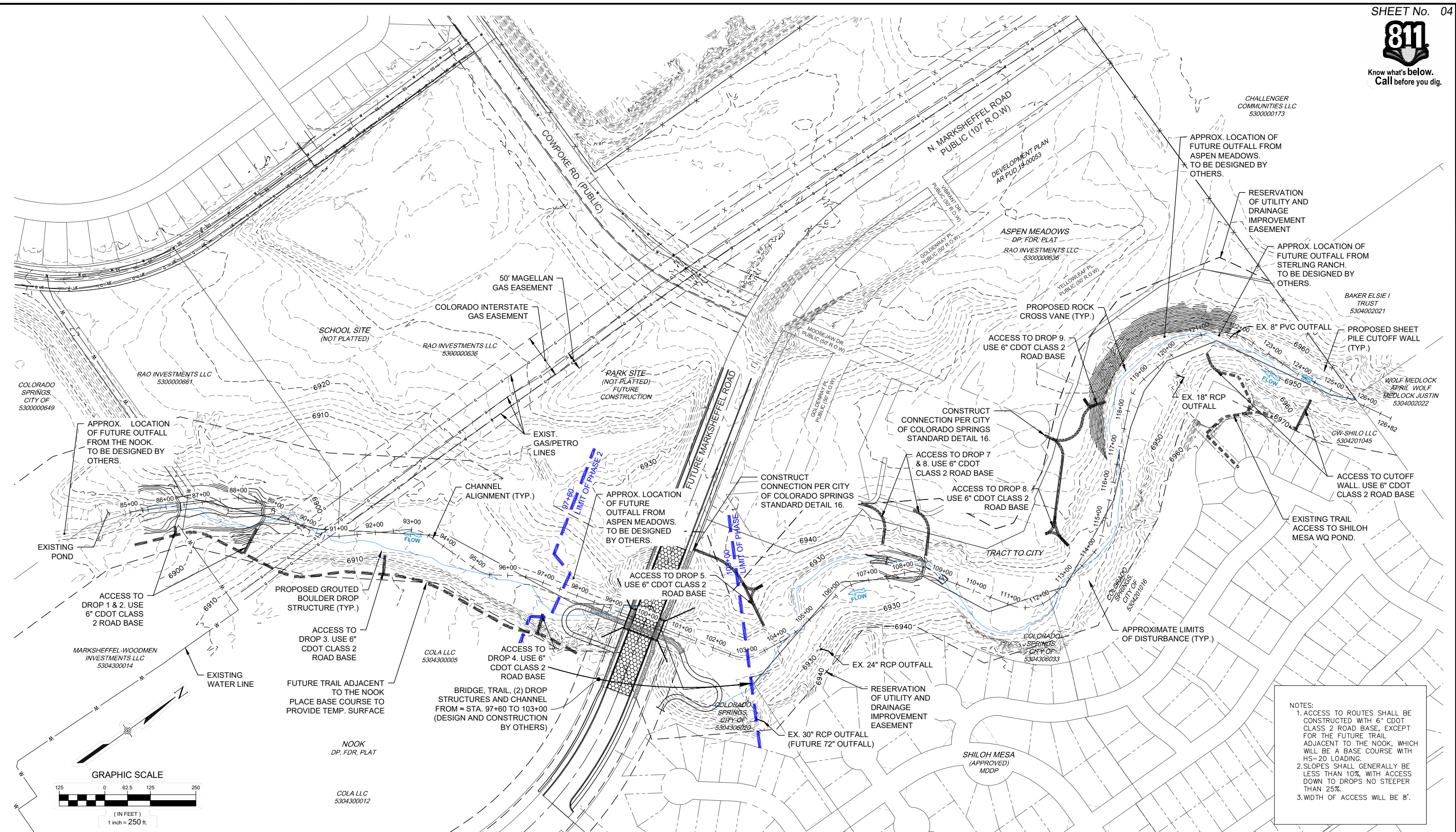
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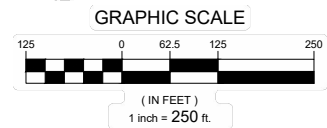
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
EXISTING CONDITIONS MAP			
DESIGNED BY: JAB	SCALE: HORIZ. 1" = 250'	DATE ISSUED: MAY 2020	DRAWING No. EX01
CHECKED BY: AJS	VERT. N/A	SHEET 03 OF 38	



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NOTES:
 1. ACCESS TO ROUTES SHALL BE CONSTRUCTED WITH 6" CDOT CLASS 2 ROAD BASE, EXCEPT FOR THE FUTURE TRAIL ADJACENT TO THE NOOK, WHICH WILL BE A BASE COURSE WITH HS-20 LOADING.
 2. SLOPES SHALL GENERALLY BE LESS THAN 10% WITH ACCESS DOWN TO DROPS NO STEEPER THAN 25%.
 3. WIDTH OF ACCESS WILL BE 8'.



REFERENCE DRAWINGS			
X-886-EX-IMAGE			
X-886-EX-MAP			
X-886-EX-TOPO			
X-886-MD-022-04			
No.	DATE	DESCRIPTION	BY
		REVISIONS	
COMPUTER FILE MANAGEMENT			
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CONDITIONS:



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Matrix
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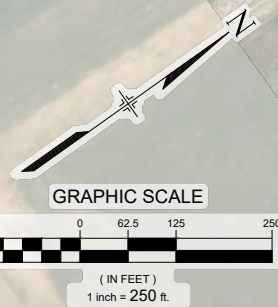
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FOR AND ON BEHALF OF
 MATRIX DESIGN GROUP, INC.
 PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
OVERALL DRAINAGE PLAN			
DESIGNED BY: JAB	SCALE: HORIZ. 1" = 125'	DATE ISSUED: February 2020	DRAWING No. DR01
CHECKED BY: AJS	VERT. N/A	SHEET 04 OF 38	



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No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19 886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-HZ01.dwg			
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FOR CITY ENGINEER _____

DATE _____

CONDITIONS:



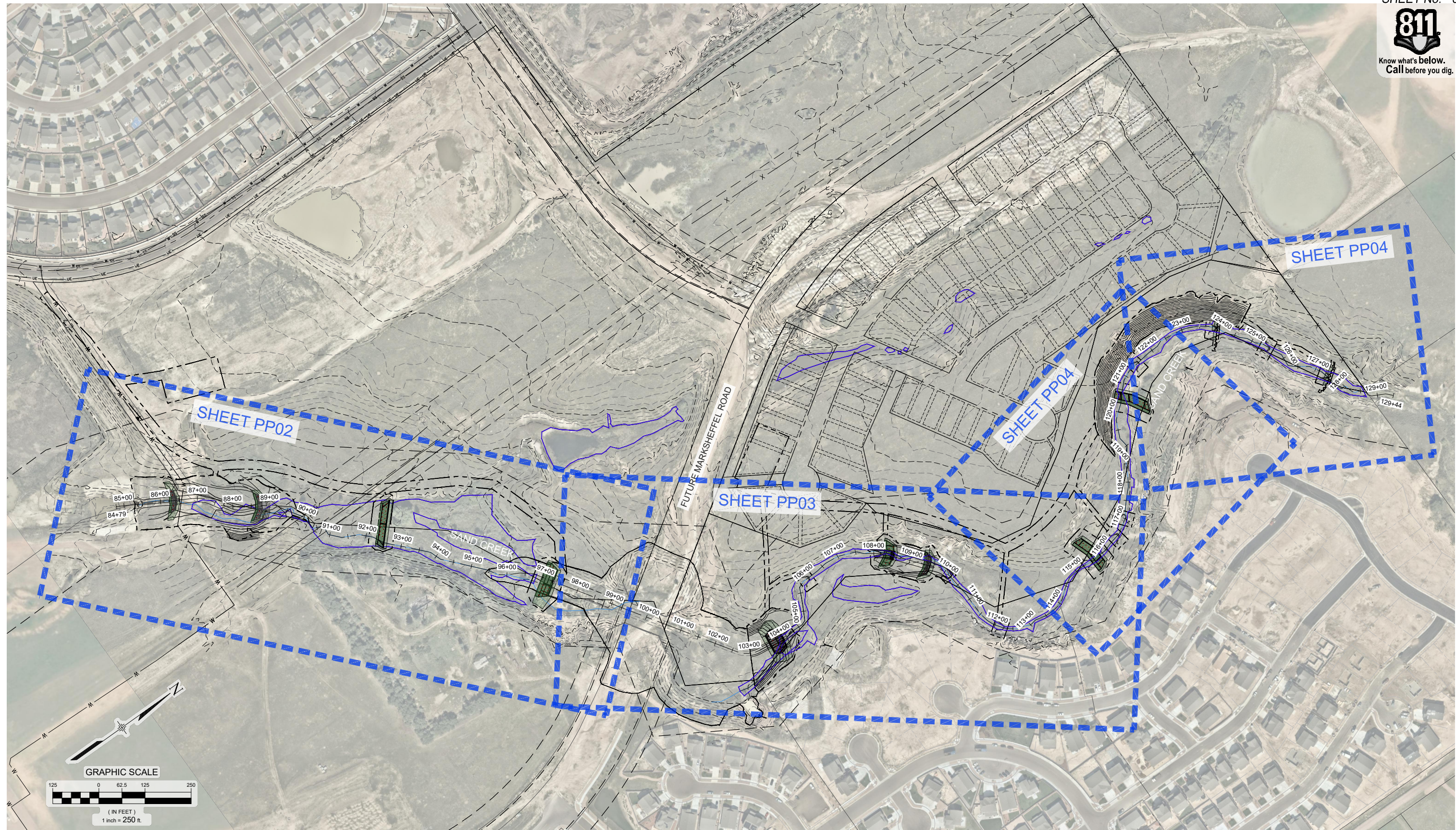
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COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
HORIZONTAL CONTROL PLAN			
DESIGNED BY: JAB	SCALE: 1" = 250'	DATE ISSUED: MAY 2020	DRAWING No. HZ01
CHECKED BY: AJS	HORIZ: 1" = 250'	SHEET 05 OF 38	
	VERT: N/A		



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DATE _____
CONDITIONS:



PREPARED BY:
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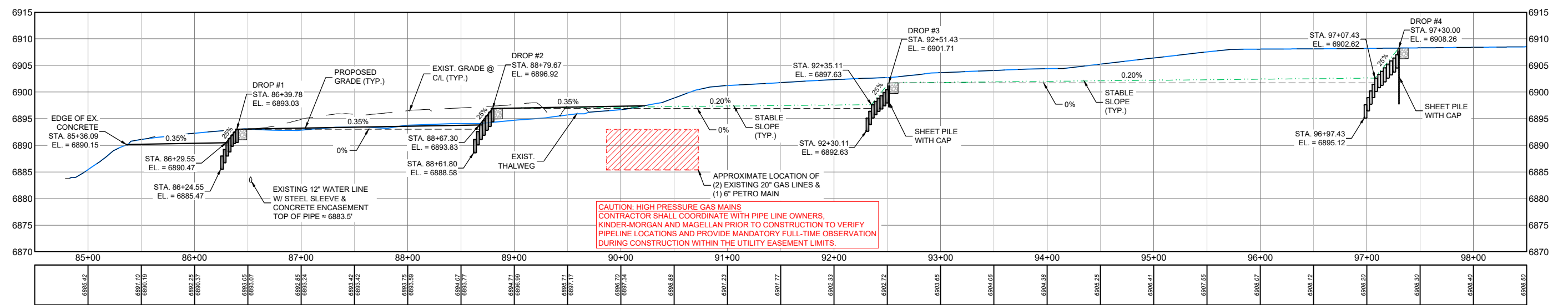
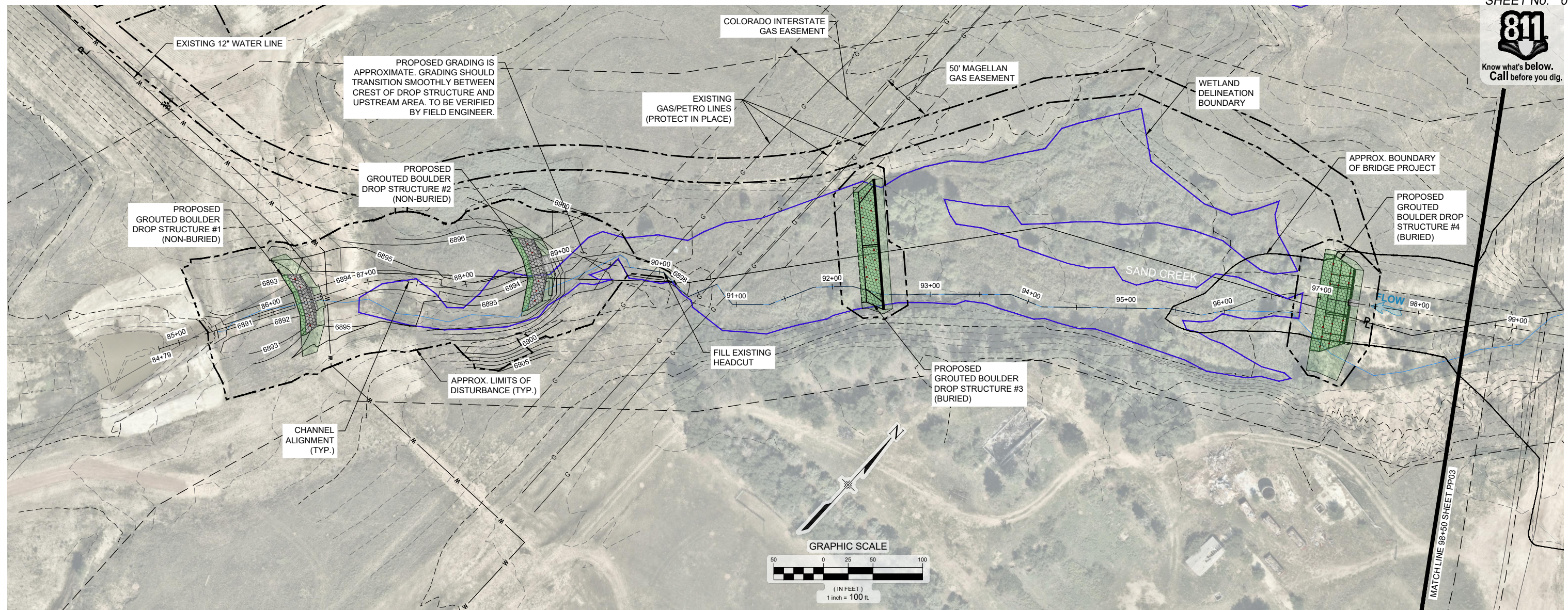
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COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
PLAN AND PROFILE OVERVIEW MAP			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 250'	DATE ISSUED: MAY 2020	DRAWING No. PP01
CHECKED BY: RAF	VERT. N/A	SHEET 06 OF 38	

FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 19.886.017



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FILE NAME: S:\119.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\1886-PP01-04.dwg			
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FOR CITY ENGINEER _____

DATE _____

CONDITIONS:

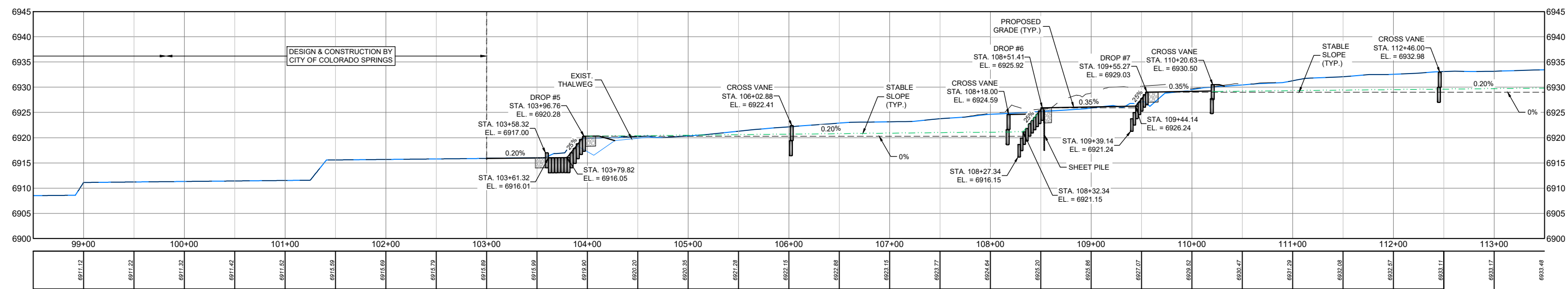
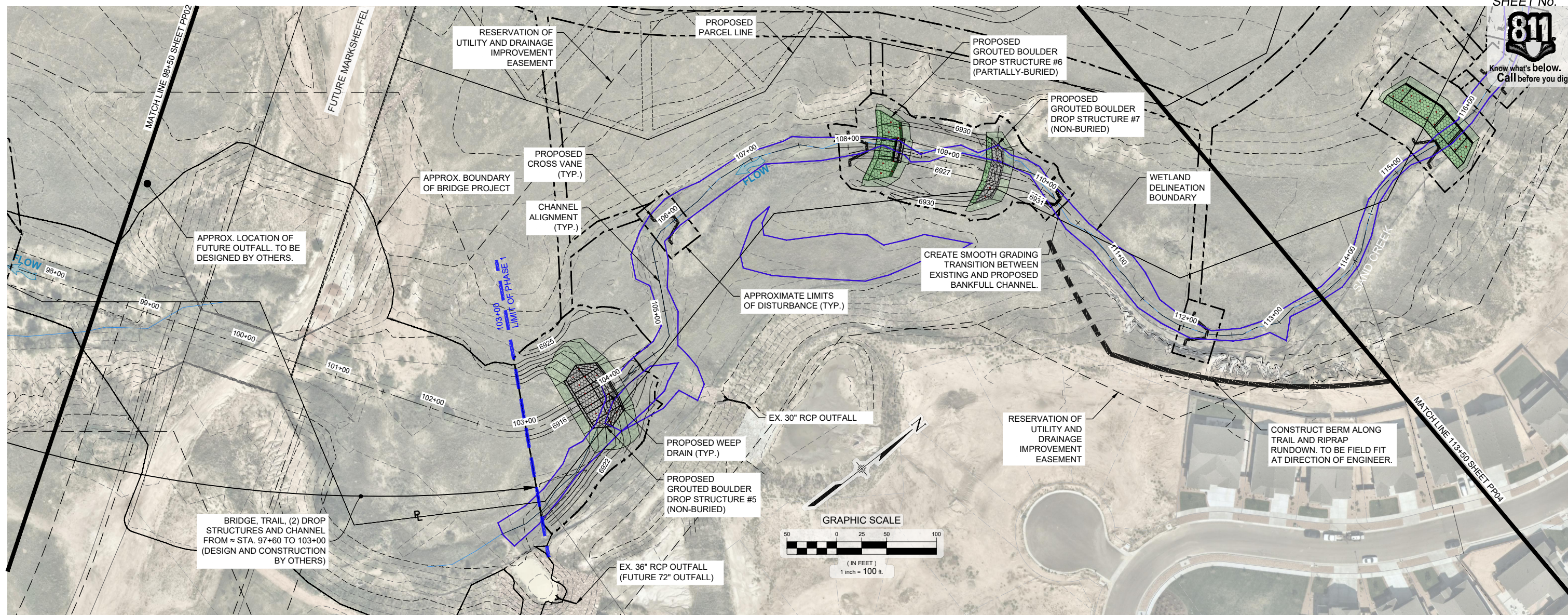
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MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
PLAN AND PROFILE			
STA.: 84+79 TO 98+50			
DESIGNED BY: JAB	SCALE: 1" = 100'	DATE ISSUED: MAY 2020	DRAWING No. PP02
CHECKED BY: AJS	HORIZ. 1" = 100'	SHEET 07 OF 38	
	VERT. 1" = 20'		



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COMPUTER FILE MANAGEMENT			
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MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

DESIGNED BY: JAB
CHECKED BY: AJS

SCALE
HORIZ 1" = 100'
VERT. 1" = 20'

DATE ISSUED: MAY 2020

DRAWING No. PP03

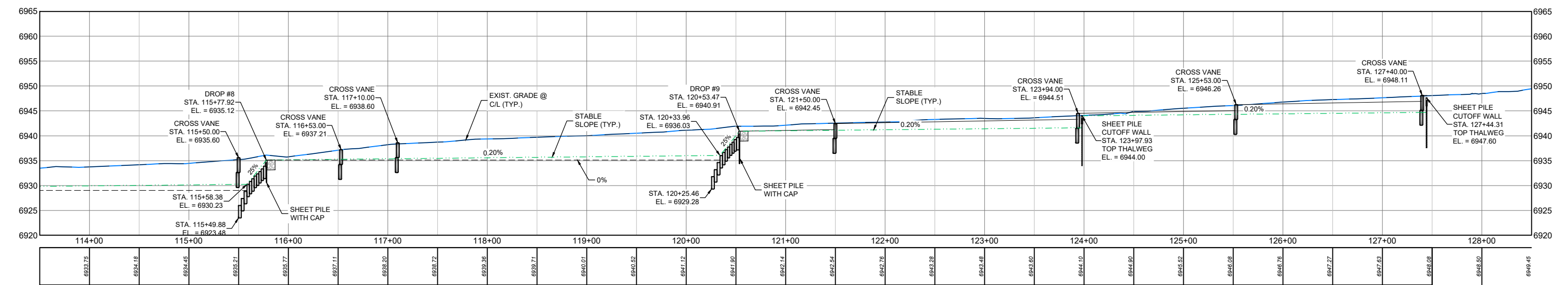
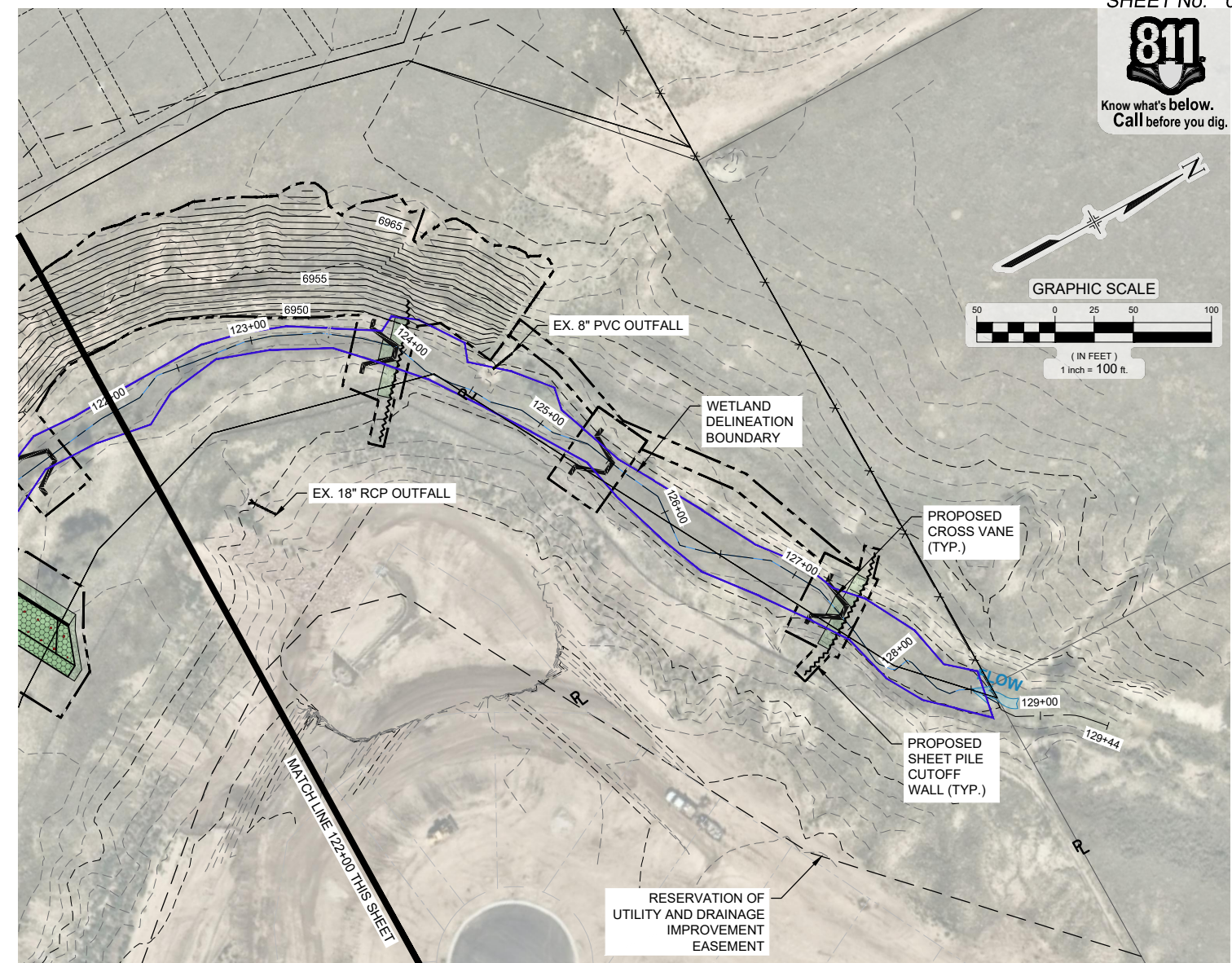
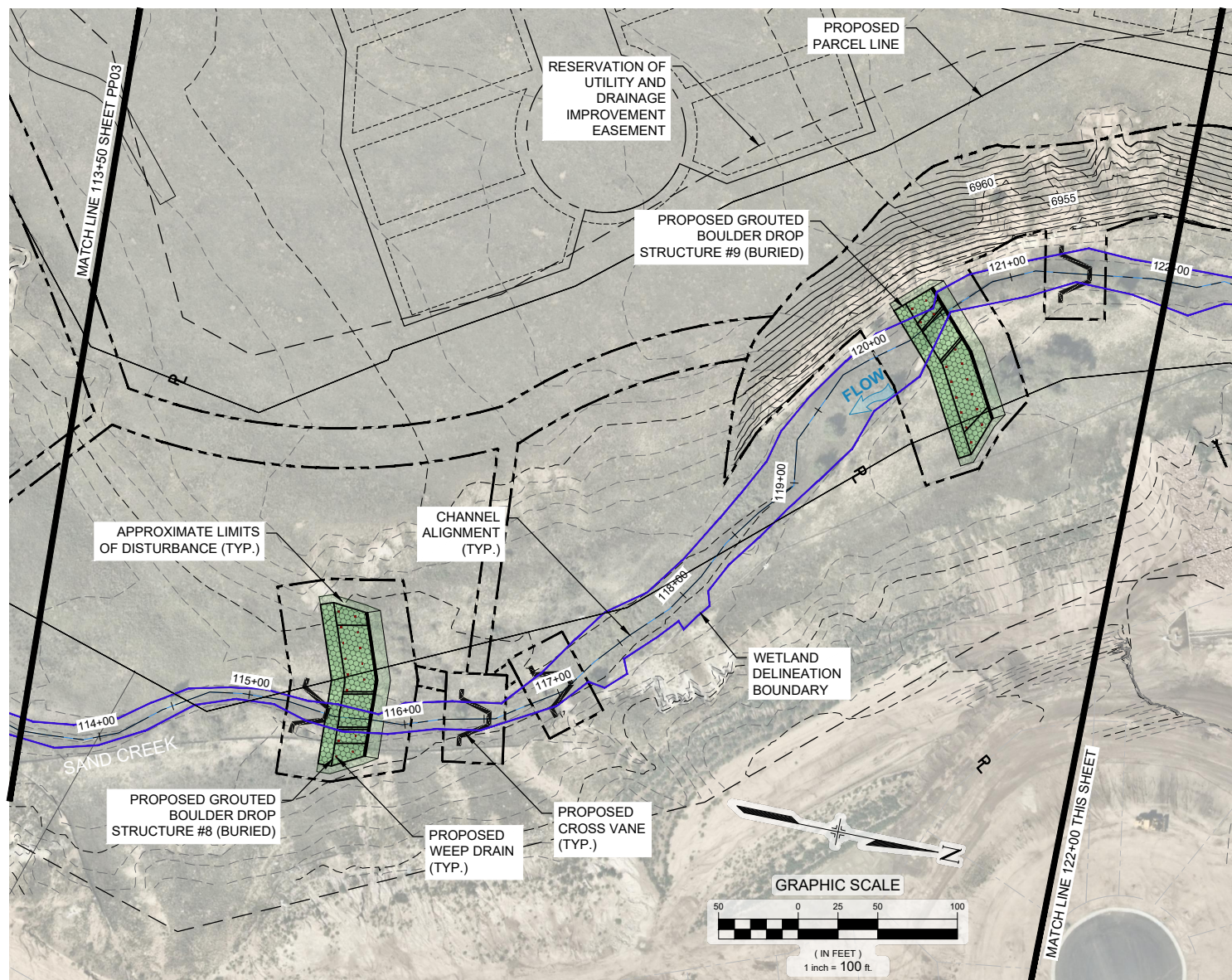
COLORADO LAND ACQUISITION

SAND CREEK STABILIZATION AT ASPEN MEADOWS
SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS

PLAN AND PROFILE
STA.: 98+50 TO 113+50



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COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\1886-PP01-04.dwg			
CTB FILE: Matrix(black).ctb			
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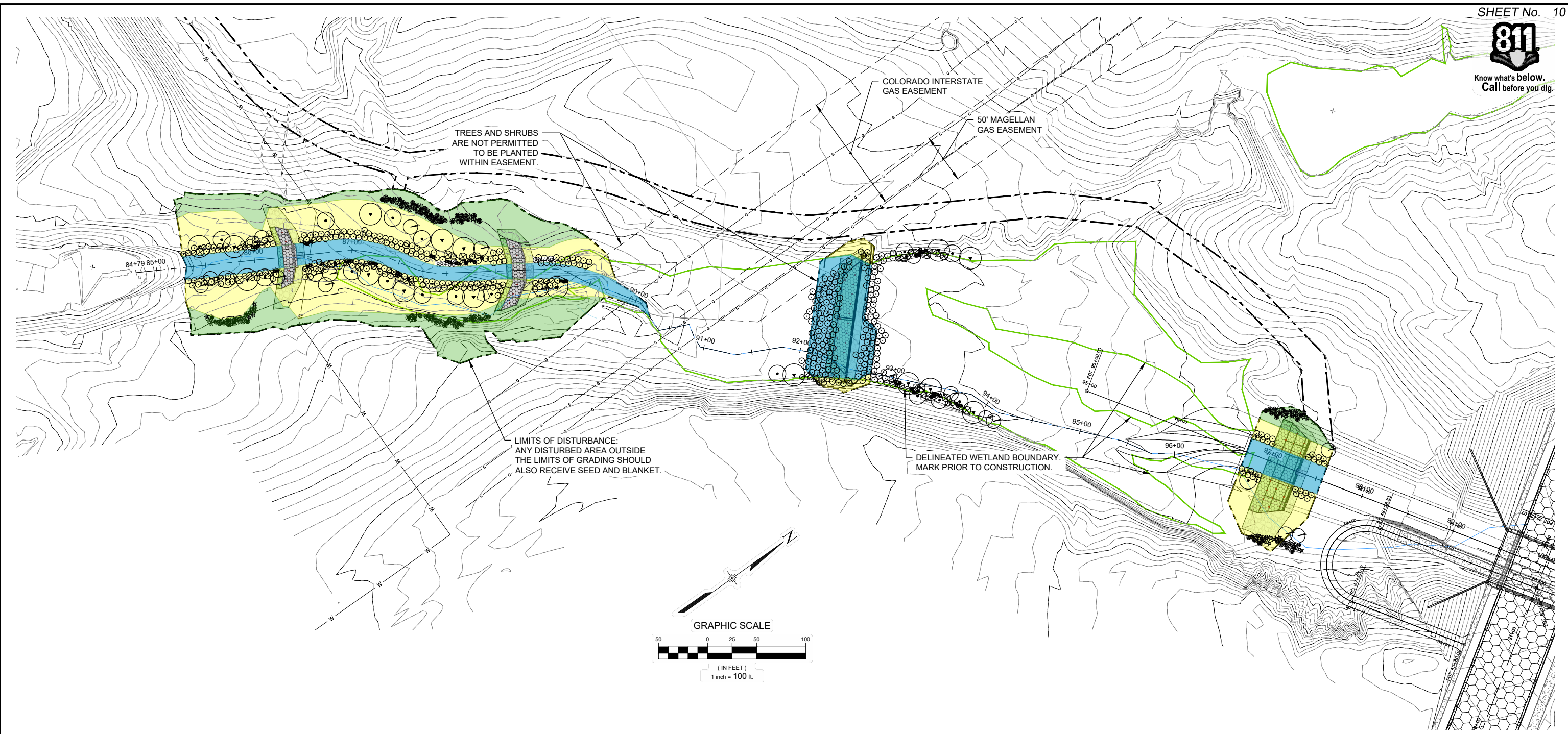
COLORADO LAND ACQUISITION
 SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS

PLAN AND PROFILE
 STA.: 113+50 TO 128+50

DESIGNED BY: JAB	SCALE: HORIZ. 1" = 100'	DATE ISSUED: MAY 2020	DRAWING No. 09 OF 38
CHECKED BY: RAJ	VERT. 1" = 20'	SHEET	PP04



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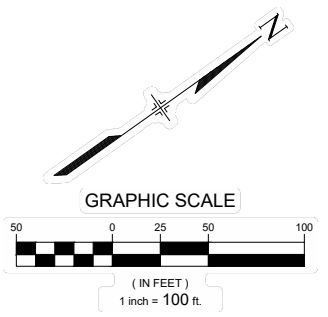


TREES AND SHRUBS ARE NOT PERMITTED TO BE PLANTED WITHIN EASEMENT.

COLORADO INTERSTATE GAS EASEMENT
50' MAGELLAN GAS EASEMENT

LIMITS OF DISTURBANCE: ANY DISTURBED AREA OUTSIDE THE LIMITS OF GRADING SHOULD ALSO RECEIVE SEED AND BLANKET.

DELINEATED WETLAND BOUNDARY. MARK PRIOR TO CONSTRUCTION.



SYMBOL KEY- DECIDUOUS TREES

- ◀ Alnus tenuifolia (ATE) - Native Thin-Leaf Alder
- ▶ Populus sargentii (PSA) - Plains Cottonwood
- Salix amygdaloides (SAM) - Peach-leaf Willow

SYMBOL KEY- DECIDUOUS SHRUBS

- ◐ Amorpha fruticosa (AFR) - Desert False Indigo
- ◑ Cornus sericea 'Bailey' (CSB) - Bailey Redtwig Dogwood
- ◒ Dasiphora fruticosa (DFR) - Shrubby Cinquefoil
- ◓ Ribes aureum (RAU) - Golden Currant
- ◔ Rosa woodsii (RWO) - Woods Rose
- ◕ Salix exigua (SEX) - Sandbar Willow
- ◖ Symphoricarpos occidentalis (SOC) - Western Snowberry

SYMBOL KEY- SEED MIXES - THE NOOK

- WETLAND SEED MIX
17,969 SF (0.41 Ac)
- RIPARIAN SEED MIX
35,815 SF (0.82 Ac)
- UPLAND SEED MIX
20,667 SF (0.47 Ac)

NOTE: AS AVAILABLE, HARVEST HEALTHY SODMATS ONSITE IN AREAS TO BE DISTURBED, AND USE FOR REVEGETATION IN LIEU OF SEED AND FABRIC. SEE NOTES ON RV04 FOR SODMAT INSTRUCTIONS.

REVEGETATION PLANTING SCHEDULE SAND CREEK AT FOREST MEADOWS - THE NOOK

DECIDUOUS TREES									
Quantity	Abbr.	Genus	Species	Common Name	Min. Size	Spacing	Notes		
19	ATE	Alnus	incana tenuifolia	Native Thin-Leaf Alder	1" cal., B&B	as shown	FACU		
16	PDE	Populus	deltoides	Plains Cottonwood	poles	as shown	FAC		
18	SAM	Salix	amygdaloides	Peach-leaf Willow	1" cal., B&B	as shown	FAC		
DECIDUOUS SHRUBS									
Quantity	Abbr.	Genus	Species	Common Name	Min. Size	Spacing	Notes		
51	AFR	Amorpha	fruticosa	False Indigo Bush	1 gal.	5'-as shown	FACW		
12	CSB	Cornus	sericea 'Bailey'	Bailey Redtwig Dogwood	1 gal.	6'-as shown	FACW		
56	DFR	Dasiphora	fruticosa	Golden Hardhack	1 gal.	3'-as shown	FACW		
39	RAU	Ribes	aureum	Golden Currant	1 gal.	5'-as shown	FACU		
70	RWO	Rosa	woodsii	Woods Rose	1 gal.	4'-as shown	FACU		
401	SEX	Salix	exigua	Sandbar Willow	stakes	18-30' o.c.	FACW		
61	SOC	Symphoricarpos	occidentalis	Western Snowberry	1 gal.	4'-as shown	FACU		

REFERENCE DRAWINGS			
X-886-EX-IMAGE			
X-886-EX-TOPO			
X-886-EX-MAP			
X-886-EX-22-34			
X-886-PR-GRADE			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
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CONDITIONS:

PREPARED BY:

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COLORADO LAND ACQUISITION

SAND CREEK STABILIZATION AT ASPEN MEADOWS
100% DESIGN PLANS

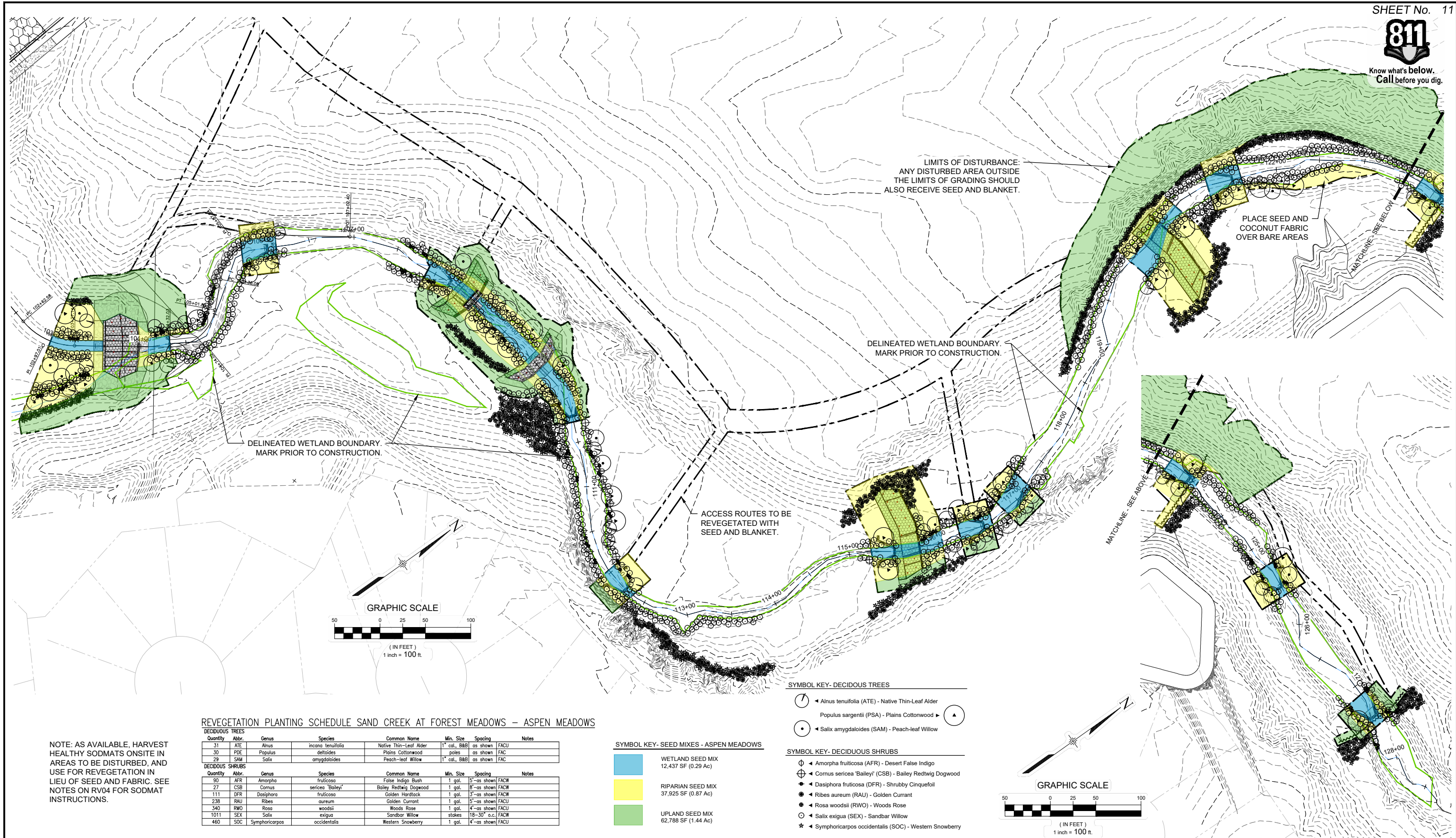
REVEGETATION PLAN

DESIGNED BY: JAB	SCALE: HORIZ 1" = 100'	DATE ISSUED: MAY 2020	DRAWING No. RV01
DRAWN BY: RAF	VERT. N/A	SHEET 10 OF 38	
CHECKED BY: AJS			

FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 19.886.017



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REVEGETATION PLANTING SCHEDULE SAND CREEK AT FOREST MEADOWS – ASPEN MEADOWS

DECIDUOUS TREES							
Quantity	Abbr.	Genus	Species	Common Name	Min. Size	Spacing	Notes
31	ATE	Alnus	incana tenuifolia	Native Thin-Leaf Alder	1" cal., B&B	as shown	FACU
30	PDE	Populus	deltoides	Plains Cottonwood	poles	as shown	FAC
29	SAM	Salix	amygdaloides	Peach-leaf Willow	1" cal., B&B	as shown	FAC

DECIDUOUS SHRUBS							
Quantity	Abbr.	Genus	Species	Common Name	Min. Size	Spacing	Notes
90	AFR	Amorpha	fruticosa	False Indigo Bush	1 gal.	5'-0" as shown	FACU
27	CSB	Cornus	sericea 'Bailey'	Bailey Redtwig Dogwood	1 gal.	8'-0" as shown	FACU
111	DFR	Dasiphora	fruticosa	Golden Hartsack	1 gal.	5'-0" as shown	FACU
238	RAU	Ribes	aurum	Golden Currant	1 gal.	5'-0" as shown	FACU
340	RWO	Rosa	woodsii	Woods Rose	1 gal.	4'-0" as shown	FACU
1011	SEX	Salix	exigua	Sandbar Willow	18-30" o.c.	as shown	FACU
460	SOC	Symphoricarpos	occidentalis	Western Snowberry	1 gal.	4'-0" as shown	FACU

SYMBOL KEY - SEED MIXES - ASPEN MEADOWS

- WETLAND SEED MIX
12,437 SF (0.29 Ac)
- RIPARIAN SEED MIX
37,925 SF (0.87 Ac)
- UPLAND SEED MIX
62,788 SF (1.44 Ac)

SYMBOL KEY - DECIDUOUS TREES

- ◀ Alnus tenuifolia (ATE) - Native Thin-Leaf Alder
- ▶ Populus sargentii (PSA) - Plains Cottonwood
- ◀ Salix amygdaloides (SAM) - Peach-leaf Willow

SYMBOL KEY - DECIDUOUS SHRUBS

- ◐ Amorpha fruticosa (AFR) - Desert False Indigo
- ◐ Cornus sericea 'Bailey' (CSB) - Bailey Redtwig Dogwood
- ◐ Dasiphora fruticosa (DFR) - Shrubby Cinquefoil
- ◐ Ribes aureum (RAU) - Golden Currant
- ◐ Rosa woodsii (RWO) - Woods Rose
- ◐ Salix exigua (SEX) - Sandbar Willow
- ★ Symphoricarpos occidentalis (SOC) - Western Snowberry

NOTE: AS AVAILABLE, HARVEST HEALTHY SODMATS ONSITE IN AREAS TO BE DISTURBED, AND USE FOR REVEGETATION IN LIEU OF SEED AND FABRIC. SEE NOTES ON RV04 FOR SODMAT INSTRUCTIONS.

No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\1886-RV01-04.dwg			
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COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS 100% DESIGN PLANS			
REVEGETATION PLAN			
DESIGNED BY:	JAB	SCALE:	DATE ISSUED:
DRAWN BY:	RAF	HORIZ: 1" = 100'	MAY 2020
CHECKED BY:	AJS	VERT: N/A	SHEET
FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 19.886.017			DRAWING No. RV02



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REVEGETATION NOTES:

- MATERIALS PLANTED PRIOR TO INSPECTION AND ACCEPTANCE OF PLANTS DELIVERED TO THE SITE ARE SUBJECT TO REJECTION.
- CONTRACTOR IS RESPONSIBLE FOR DETERMINING SOURCE LOCATIONS (ON- OR OFF-SITE) FOR ALL HARVESTED MATERIALS. OFF-SITE PLANT MATERIALS SHALL ONLY BE USED UPON APPROVAL.
- SEEDING OR PLANTING SHALL NOT OCCUR WHEN THE GROUND IS FROZEN, WHEN FREEZING TEMPERATURES ARE FORECASTED WITHIN 24 HOURS, OR WHEN CONDITIONS ARE OTHERWISE UNSUITABLE.
- CONTRACTOR SHALL CONDUCT A SOIL TEST FOR TOP SOIL STOCKPILED ON THE SITE PRIOR TO APPLICATION OF SOIL CONDITIONER, SEEDING OR PLANTING. SOIL TEST SAMPLES SHALL ALSO BE TAKEN APPROXIMATELY EVERY 1,000 FEET ALONG THE GRADED CHANNEL FOR THE SUBGRADE SOILS AND TESTED. A RECOMMENDED SOIL CONDITIONING AMENDMENT AND APPLICATION RATE SHALL BE DETERMINED BASED ON THE SOIL TEST RESULTS. NO SOIL CONDITIONING, SEEDING, OR PLANTING SHALL OCCUR PRIOR TO SOIL TEST AND UNTIL A SOIL CONDITIONING AMENDMENT IS ACCEPTED.
- CONTRACTOR SHALL BE REQUIRED TO SUBMIT SIGNED STATEMENTS OF GUARANTEE AND/OR CERTIFICATIONS FROM VENDORS WHO SUPPLY SEED AND SOIL CONDITIONER STATING THAT THE SEED FURNISHED IS FROM A LOT THAT HAS BEEN TESTED BY A RECOGNIZED LABORATORY FOR SEED TESTING WITHIN TWELVE (12) MONTHS PRIOR TO THE DATE OF SEEDING.
- CONTRACTOR SHALL SUBMIT A LAB TEST OF COMPOST SAMPLE TO BE USED FOR APPROVAL. LAB TEST OF COMPOST SHALL BE TAKEN FROM THE SAME SOURCE THAT IS TO BE USED ON THIS PROJECT. LAB TEST SHALL BE TAKEN A MAXIMUM OF SIX (6) MONTHS PRIOR TO APPLICATION. THE COMPOST SHALL BE TESTED IN ACCORDANCE WITH THE U.S. COMPOSTING COUNCIL'S TEST METHODS FOR EXAMINING OF COMPOSTING AND COMPOST (TMECC) MANUAL.
- ALL MATERIALS SHALL BE FURNISHED IN ORIGINAL MANUFACTURER'S SHIPPING BAGS OR CONTAINERS AND REMAIN IN THESE BAGS OR CONTAINERS UNTIL THEY ARE USED. ALL MATERIALS SHALL BE STORED IN A MANNER THAT WILL PREVENT THEM FROM COMING INTO CONTACT WITH PRECIPITATION, SURFACE WATER, OR ANY OTHER CONTAMINATING SUBSTANCE. ANY MATERIALS THAT HAVE BECOME WET, MOLDY, OR OTHERWISE DAMAGED IN TRANSIT OR IN STORAGE SHALL NOT BE USED.
- ALL MATERIALS AND EQUIPMENT FURNISHED SHALL BE FREE OF NOXIOUS WEEDS INCLUDING BUT NOT LIMITED TO RUSSIAN KNAWWEED, DIFFUSE KNAWWEED, CANADA THISTLE, FIELD BINDWEED, JOHNSONGRASS, LEAFY SPURGE, KOCHIA, OR ANY STATE OR DISTRICT CRITERIA MANUAL-LISTED NOXIOUS WEED SPECIES.

SOIL AMENDMENTS

- COMPOST: COMPOST SHALL BE CLASS A AS DEFINED BY CFR TITLE 40, PART 503 OR CLASS 1 AS DESCRIBED IN THE TABLE BELOW. THE AMOUNT OF COMPOST ADDED TO THE SOIL MAY VARY DEPENDING ON SOIL TEST RESULTS.

Compost Parameters	Reported As	Requirements	Test Method
pH	pH units	6.0 - 8.4	TMECC 04.11-A
Soluble Salts (Electrical Conductivity)	dS m ⁻¹ or mmhos cm ⁻¹	0-5 mmhos/cm	TMECC 04.11-A
Moisture Content	%, wet weight basis	35 - 60%	TMECC 03.09-A
Organic Matter Content	%, dry weight basis	30 - 70%	TMECC 05.07-A
Particle Size (Sieve Sizes)	%, dry weight basis for each sieve fraction	Passing 1 inch - 100% 1/2 inch - 95%	TMECC 02.02-B
Man-made Inert Contamination	%, dry weight basis	< 1%	TMECC 03.08-A
Stability (Respirometry)	mg CO ₂ - C per g TS per day mg CO ₂ - C per g OM per day	8 or below	TMECC 05.08-B
Select Pathogens	(PASS/FAIL) Limits: Salmonella < 3 MPN/4grams of TS, or Coliform Bacteria <1000 MPN/gram	Pass	TMECC 07.01-B Fecal Coliforms, or 07.02 Samonella
Trace Metals	(PASS/FAIL) Limits (mg kg ⁻¹ dw basis): As 41, Cd 39, Cu 1500, Pb 300, Hg 17, Ni 420, Se 100, Zn 2800	Pass	TMECC 04.06
Maturity (Bioassay) Percent	%, (average)	> 80%	
Emergency Relative Seedling Vigor	%, (average)	> 80%	TMECC 05.05-A

Notes: The Contractor shall provide a CTR in accordance with subsection 106.13 of CDOT standard specifications confirming that the material has been tested in accordance with TMECC.

- OTHER SOIL AMENDMENTS
 - BIOSOL ORGANIC SLOW-RELEASE FERTILIZER AND HUMATE SOIL CONDITIONERS CAN BE SUBSTITUTED FOR COMPOST AMENDMENTS IF APPROVED AFTER REVIEW OF SOIL TEST RESULTS.
 - BIOSOL ORGANIC FERTILIZER SHOULD HAVE THE FOLLOWING CHARACTERISTICS:
 - 6% N, 1% P AS P2O5, 1% K AS K2O
 - 95% FUNGAL BIOMASS
 - APPLICATION RATE IS 1200 LBS/ACRE IN A UNIFORM MANNER, PRIOR TO TILLING SOILS FOR SEED, AND MUST BE THOROUGHLY MIXED INTO SOIL TO INCREASE NUTRIENTS. PLANT SPECIES SHOULD ALSO BE TAKEN INTO CONSIDERATION WHEN CONSIDERING THEIR USE.
 - HUMATE SOIL CONDITIONER, NATURAL MINERAL, CARBON AND HUMIC ACID-BASED SOIL CONDITIONER SHOULD HAVE THE FOLLOWING CHARACTERISTICS:
 - HUMIC ACIDS >50%
 - ORGANIC MATTER >85%
 - 1%N, <0.1% AS P2O5, <0.10%K AS K2O
 - PH 3.4
 - APPLICATION RATE IS BETWEEN 250-500 LBS/ACRE DEPENDENT ON SOIL TEST RESULTS. HUMATE WORKS BEST WHEN MINIMUM DAILY SOIL TEMPERATURES REACH 55DEGREES F. HUMATE CONDITIONERS MUST BE THOROUGHLY MIXED INTO SOIL.
- SEEDING:
 - ALL SEED SHALL BE FURNISHED IN BAGS OR CONTAINERS CLEARLY AND PROPERLY LABELED TO SHOW THE NAME AND ADDRESS OF THE SUPPLIER, THE SEED NAME, THE LOT NUMBER, NET WEIGHT, ORIGIN, THE PERCENT OF WEED SEED CONTENT, THE GUARANTEED PERCENTAGE OF PURITY AND GERMINATION, POUNDS OF PURE LIVE SEED (PLS) OF EACH SEED SPECIES, AND THE TOTAL POUNDS OF PLS IN THE CONTAINER. ALL SEED SHALL BE GUARANTEED FOR PURITY AND GERMINATION, FREE OF NOXIOUS WEED SEED AND SUPPLIED ON A PURE LIVE SEED (PLS) BASIS.
 - ANY SUBSTITUTIONS OF SEED SPECIES MUST BE APPROVED PRIOR TO DELIVERY OF SEED TO CONSTRUCTION SITE.
 - MYCORRHIZAE, ENDO AND ECTO, GRANULAR INOCULUM IS TO BE INCORPORATED INTO ALL SOIL PRIOR TO SEEDING. MYCORRHIZAE SHALL HAVE THE FOLLOWING CHARACTERISTICS:
 - 16 SPECIES OF ENDO- AND ECTO-MYCORRHIZAE FUNGI SPORES COMPATIBLE WITH 90% OF THE WORLD'S PLANT SPECIES
 - 5 BACTERIAL SPECIES
 - GRANULAR FORM
 - APPLICATION RATE IS 60LBS/ACRE FOR BROADCAST APPLICATION
- EROSION CONTROL FABRIC: CONTRACTOR SHALL SUBMIT SAMPLES OF THE LAYERED COIR MAT, GROUND ANCHORING DEVICES, AND METHOD OF ANCHORING TWO (2) WEEKS PRIOR TO INSTALLATION FOR APPROVAL.
- SITE PREPARATION:
 - ALL DISTURBED AREAS SHALL BE RIPPED TO A MINIMUM DEPTH OF EIGHT (8) INCHES, WITH NO MORE THAN A TEN (10) INCH INTERVAL BETWEEN FURROWS. SLOPES FLATTER THAN 2:1 SHALL HAVE A WELL SETTLED SEEDBED EIGHT (8) INCHES DEEP. SLOPES 2:1 OR STEEPER SHALL BE LEFT IN A ROUGHENED CONDITION.
 - SLOPES SHALL BE FREE OF SOIL CLOUDS, STICKS, STONES, AND DEBRIS IN EXCESS OF FOUR (4) INCHES IN ANY DIMENSION, AND BE BROUGHT TO THE DESIRED GRADE AND LINE. SOIL PREPARATION FOR SEEDING SHALL NOT OCCUR WHEN SOIL IS FROZEN OR IN AN EXTREME WET OR DRY CONDITION.
- SEEDING:
 - SEEDING SHALL BE RESTRICTED TO BETWEEN SPRING THAW AND JUNE 1 AND BETWEEN SEPTEMBER 1 UNTIL CONSISTENT GROUND FREEZE AND SHALL NOT BE APPLIED DURING INCLEMENT WEATHER INCLUDING RAIN AND HIGH WINDS, OR WHEN SOIL MOISTURE IS TOO HIGH TO EVENLY DISTRIBUTE SEED.
 - SEEDING SHALL BE ACCOMPLISHED WITHIN 24 HOURS OF PREPARING THE SEEDING SURFACE.
 - DRILL SEEDING OR BROADCAST SEEDING SHALL BE USED FOR REVEGETATION. AS OUTLINED BELOW, THE SIZE AND SLOPE OF THE DISTURBED AREA SHALL DETERMINE WHICH SEEDING METHOD(S) IS APPROPRIATE AND ACCEPTABLE. WHERE FEASIBLE, DRILL SEEDING IS THE REQUIRED METHOD. IF BROADCAST SEEDING IS EMPLOYED, EITHER BY HAND, SPREADER, OR OTHER APPROVED MEANS, THE SEEDING RATE (PLS LBS/ACRE) SHALL BE DOUBLED AS SHOWN ON THE DESIGN PLAN. HYDROMULCHING, HYDRAULIC SEEDING AND STRAW MULCHING WILL NOT BE ACCEPTED.
 - FOR SLOPES EQUAL TO OR LESS THAN 3:1, SEED SHALL BE PLANTED USING A RANGELAND DRILL WITH A SMALL SEED/LEGUME BOX AND AN AGITATOR BOX FOR FLUFFY OR BULKY SEED. SEED ROWS SHALL BE SPACED SEVEN (7) TO TEN (10) INCHES APART, AND PLANTED ½ INCH TO ¾ INCH DEEP. THE DRILL SHALL HAVE DOUBLE-DISK FURROW OPENERS WITH DEPTH BANDS AND PACKER WHEELS. SEEDING SHALL BE ACCOMPLISHED USING BI-DIRECTIONAL DRILLING AND WITH THE SECOND DIRECTION FOLLOWING THE SLOPE CONTOUR. THE DRILL EQUIPMENT SHALL BE CALIBRATED EACH DAY OR WHENEVER THERE IS A CHANGE IN THE SEED MIX TO ENSURE PROPER SEED DISTRIBUTION AND RATE.
 - FOR SLOPES GREATER THAN 3:1, SEED SHALL BE BROADCAST BY HAND OR MECHANICAL SPREADER. ALL SEED SOWN BY BROADCAST-TYPE SEEDERS SHALL BE "RAKED IN" OR COVERED WITH SOIL TO A DEPTH OF AT LEAST ¼ INCH. BROADCAST SEEDING SHALL PROCEED ON FRESHLY DISTURBED (RAKED OR HARROWED) SOIL SURFACE AND BROADCAST SEED SHALL BE IMMEDIATELY RAKED OR HARROWED INTO THE SURFACE. RAKING SHALL BE ACCOMPLISHED USING METAL-TINED GARDEN OR LANDSCAPE RAKES; NO PLASTIC LEAF RAKES SHALL BE ALLOWED. IF HARROWING IS USED, AN ENGLISH HARROW OR ITS EQUIVALENT SHALL BE REQUIRED. BROADCAST SEEDING SHALL BE AVOIDED WHEN WIND SPEED EXCEEDS 15 MILES-PER-HOUR.
 - FOLLOWING SEEDING, ALL SEEDED AREAS SHALL BE WATERED SUFFICIENTLY AS TO SATURATE THE SOILS.

- WILLOW CUTTINGS: WILLOW CUTTINGS SHALL BE COLLECTED IN AREAS WITHIN 1,000 VERTICAL FEET OF ELEVATION AND OF SIMILAR HYDROLOGY TO THOSE EXISTING AT THE PLANTING SITE. IF A SUFFICIENT NUMBER OF WILLOW CUTTINGS ARE NOT AVAILABLE AT OR NEAR THE PLANTING SITE, THE CONTRACTOR WILL COLLECT THE REQUIRED WILLOW CUTTINGS AT AN ACCEPTABLE SITE WITH APPROVAL OF THE PROPERTY OWNER (AS APPLICABLE) AND TRANSPORT THEM TO THE PLANTING SITE.
 - WILLOW COLLECTION SITES SHALL BE A MINIMUM OF ONE-QUARTER ACRE IN SIZE, WITH MATURE WILLOW STANDS. NO MORE THAN TWENTY (20) PERCENT OF MIDDLE AGE PLANT MATERIAL SHALL BE TAKEN FROM THE SITE UNLESS THE PLANT WILL BE REMOVED OR TRANSPLANTED DURING EXCAVATION AND GRADING. WRITTEN CONSENT FROM THE PROPERTY OWNER MUST BE RECEIVED IN AREAS WHERE HARVESTING WILL OCCUR, AND WILL SPECIFY IF IT IS BENEFICIAL TO TAKE MORE THAN TWENTY (20) PERCENT OF THE PLANT MATERIAL.
 - CUTTINGS SHALL BE MAINTAINED IN A SHADED, MOIST, AND COOL CONDITION FROM THE TIME OF HARVEST THROUGH THE TIME OF INSTALLATION, INCLUDING DURING TRANSPORTATION AND UPON DELIVERY TO THE SITE. THE CUTTINGS WILL BE KEPT WET UNTIL PLACED INTO THE GROUND AND WILL NOT BE ALLOWED OUT OF WATER FOR MORE THAN TEN MINUTES DURING PLANTING.
 - WILLOW CUTTINGS SHALL BE PLANTED IN AREAS SHOWN ON THE DESIGN PLAN. FINAL LOCATIONS AND ELEVATIONS FOR WILLOW CUTTINGS SHALL BE APPROVED PRIOR TO INSTALLATION.
- COTTONWOOD POLES: COTTONWOOD POLES SHALL BE COLLECTED WITHIN 1,000 VERTICAL FEET OF ELEVATION AND OF SIMILAR HYDROLOGY TO THOSE EXISTING AT THE PLANTING SITE. POLES THAT ARE COLLECTED SHALL BE HARVESTED IN A MANNER CONFORMING TO LOCAL, STATE, AND FEDERAL LAW. COTTONWOOD POLES MAY BE COLLECTED FROM THE SAME LOCATION AS WILLOW CUTTINGS AND AT THE SAME TIME WITH APPROPRIATE PROPERTY OWNER APPROVAL.
 - COTTONWOOD POLES SHALL BE COLLECTED AND TRANSPORTED IN A MANNER CONSISTENT WITH WILLOW CUTTINGS.
 - LOCATIONS DESIGNATED ON DESIGN PLAN SHALL BE PLANTED WITH COTTONWOOD POLES.
 - ALL COTTONWOOD PLANTINGS WILL BE PERFORMED USING *POPULUS ANGUSTIFOLIA* (NARROWLEAF COTTONWOOD) OR *POPULUS DELTOIDES* (PLAINS COTTONWOOD) POLES WITH ONE-HALF OF THE REQUIRED POLES FROM EACH SPECIES.
 - COTTONWOOD POLES SHALL BE STORED IN WATER, FLAT CUTS UP. AT LEAST 2/3 OF THE TOTAL CUTTING LENGTH SHALL BE COVERED WITH WATER. POLES SHALL BE TREATED WITH ROOTONE F ROOTING HORMONE OR AN APPROVED EQUAL AT THE RATE OF ONE (1) POUND PER 35 GALLONS OF WATER. ROOTING HORMONE SHALL BE APPLIED, HANDLED, STORED AND CLEANED IN ACCORDANCE WITH MANUFACTURER RECOMMENDATIONS. COTTONWOOD POLES SHALL BE SOAKED FOR A MINIMUM OF 48 HOURS AND A MAXIMUM OF 14 DAYS. ROOTONE F SHALL NOT BE PAID FOR SEPARATELY, BUT SHALL BE INCLUDED IN THE PRICE OF THE WORK. ROOTONE F (OR APPROVED EQUAL) SHALL CONTAIN UP TO 5% ACTIVE INGREDIENTS OF NAPHTHALENEACETAMIDE AND THIRAM
 - CONTRACTOR IS RESPONSIBLE FOR ENSURING THAT COTTONWOOD POLES ARE IN CONTACT WITH THE WATER TABLE AT TIME OF PLANTING.
 - COTTONWOOD POLES SHALL BE WATERED SO THAT THE GROUND IS THOROUGHLY SATURATED IMMEDIATELY FOLLOWING PLANTING.
- ACCESS ROUTES SHALL BE REVEGATED AFTER CONSTRUCTION. SEED AND BLANKET ALONG ACCESS SHOULD MATCH HYDROLOGIC ZONES AS SHOWN IN REVEGETATION PLANS AND AS DIRECTED BY THE ENGINEER.

TOPSOIL NOTES:

- WITHIN THE PROJECT AREA, ANY AREAS WITH ADEQUATE TOPSOIL (IN PLACES WHERE NOT HARVESTING SOD) SHALL BE STRIPPED AND STOCKPILED FOR REUSE.
- ALL AREAS OF SEEDING WILL RECEIVE 4" OF TOPSOIL.
- IF ONSITE CONDITIONS DO NOT YIELD ADEQUATE TOPSOIL, SOIL CONDITIONER SHALL BE APPLIED.
- IMPORTED SOIL CONDITIONER WILL BE AT A RATE OF 5 CUBIC YARDS PER 1,000 SQUARE FEET. SOIL CONDITIONER SHALL BE EVENLY DISTRIBUTED AND TILLED TO A DEPTH OF 8" MINIMUM.

FABRIC NOTES:

- USE COIR FABRIC WITHIN THE BANKFULL CHANNEL AS SHOWN ON DT01. AT DROP #3, COIR FABRIC SHOULD EXTEND TO LIMITS OF WETLAND SEEDING. COIR FABRIC SHALL BE NEDIA KOIRWRAP 1200. AN EQUIVALENT FABRIC MAY BE USED IF APPROVED BY THE ENGINEER.
- AREAS OUTSIDE THE BANKFULL CHANNEL SHALL RECEIVE COCONUT FABRIC. COCONUT FABRIC SHALL BE NEDIA C400B. AN EQUIVALENT FABRIC MAY BE USED IF APPROVED BY THE ENGINEER.
- SEE DT25 FOR DETAILS ON TRENCHING AND STAKING.
- FABRIC AND SEEDING ARE NOT REQUIRED WHERE SOD MATS ARE PLACED.

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
X-886-EX-IMAGE X-886-EX-TOPO X-886-EX-MAP X-886-EX-22-34 X-886-PR-GRADE				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:\119.886.017 Sand Creek Stabilization at Forest Meadows P2\1Dwg\Design Plans\886-RV01-04.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 4:46 PM				
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.				

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PREPARED BY:

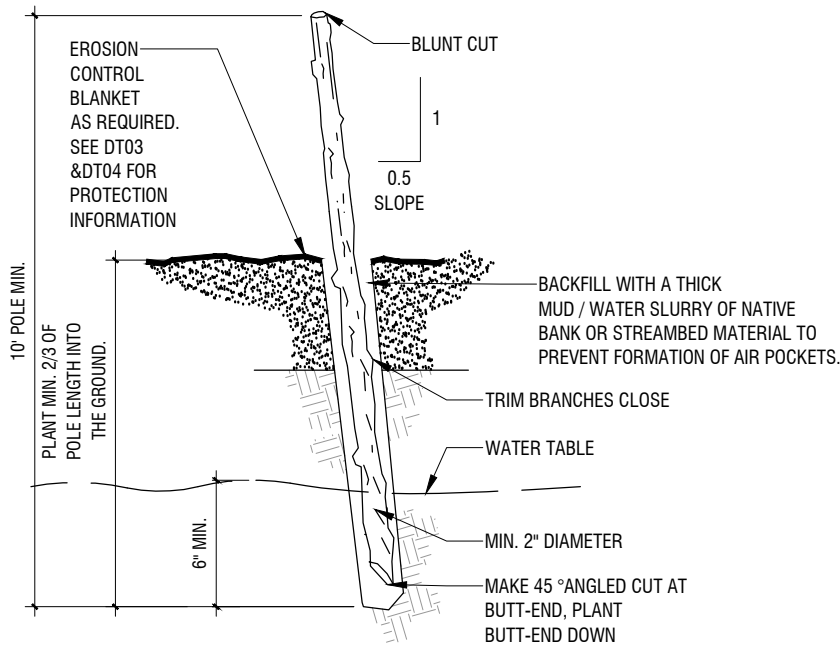
SEAL
PRELIMINARY
THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND IS SUBJECT TO CHANGE

COLORADO LAND ACQUISITION				
SAND CREEK STABILIZATION AT ASPEN MEADOWS 100% DESIGN PLANS				
REVEGETATION NOTES				
DESIGNED BY:	JAB	SCALE	DATE ISSUED:	MAY 2020
DRAWN BY:	RAF	HORIZ N/A	DRAWING No.	RV03
CHECKED BY:	AJS	VERT. N/A	SHEET	12 OF 38



Know what's below.
Call before you dig.

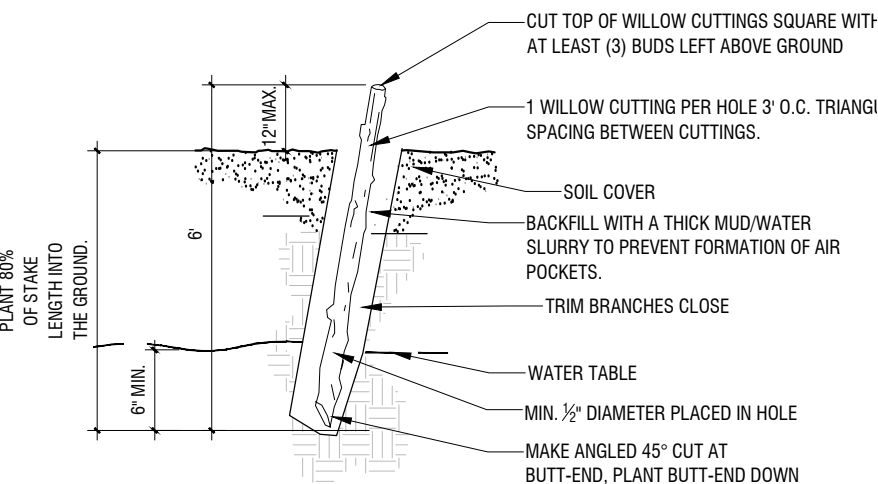
1. HARVEST AND PLANT POLES DURING THE DORMANT SEASON FROM LIVE SAPLINGS.
2. USE HEALTHY, STRAIGHT AND LIVE WOOD AT LEAST ONE YEAR OLD.
3. MAKE CLEAN CUTS WHEN HARVESTED. DO NOT DAMAGE POLES OR SPLIT ENDS DURING INSTALLATION.
4. BARK MUST NOT BE SEPARATED FROM THE CAMBIUM LAYER WITH AT LEAST (3) LIVE BUDS LEFT ABOVE GROUND.



COTTONWOOD POLES

SCALE: N.T.S.

1. HARVEST AND PLANT CUTTINGS DURING THE DORMANT SEASON BEFORE BUDS APPEAR.
2. USE HEALTHY, STRAIGHT AND LIVE WOOD AT LEAST ONE YEAR OLD.
3. MAKE CLEAN CUTS BY HAND AND DO NOT DAMAGE CUTTINGS OR SPLIT ENDS DURING INSTALLATION. USE A PILOT BAR IN FIRM SOILS.
4. TOTALLY SUBMERGE CUTTINGS WITHIN ONE HOUR OF CUTTING AT A DEPTH OF ONE FOOT FOR 7-14 DAYS PRIOR TO INSTALLATION. BARK MUST NOT BE SEPARATED FROM CAMBIUM LAYER.
5. TAMP THE SOIL AROUND THE CUTTINGS OR BACKFILL WITH MUD SLURRY.

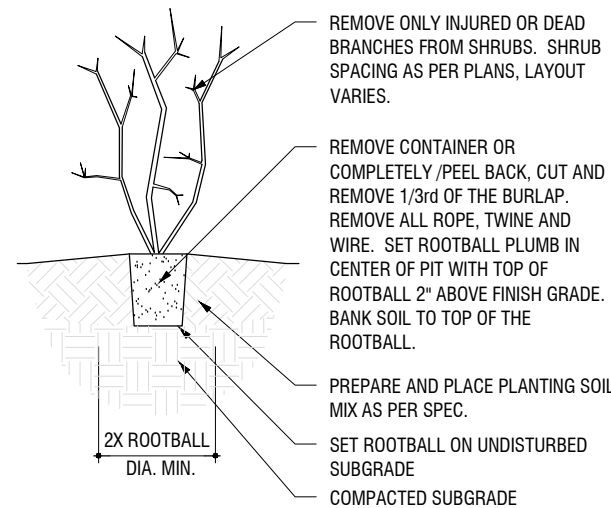


WILLOW CUTTING

SCALE: N.T.S.

ON-SITE SALVAGE OF WETLAND SODMATS

1. WETLAND SODMATS ARE LARGE PIECES OF INTACT WETLAND SOIL AND VEGETATION REMOVED FROM THE DONOR SITE WHERE DISTURBANCE IS EXPECTED TO OCCUR.
2. IDENTIFY AREAS WHERE WETLAND SODMATS MIGHT BE SALVAGED FROM WITHIN THE CONSTRUCTION SITE. TAKE NOTE OF THE HYDROLOGICAL ZONE AND CONDITIONS FROM WITH THE SODMATS ARE HARVESTED. THE LARGER AREAS OF DISTURBANCE SHOULD RECEIVE SALVAGED SODMATS AS A PRIORITY.
3. SEQUENCING CONSTRUCTION TO ALLOW IMMEDIATE TRANSPLANT OF SOD MATS IS PREFERABLE.
4. HARVEST SODMATS WITH SHOVELS, BACKHOE OR FRONT-END LOADER MODIFIED WITH A SHARP-EDGED STEEL PLATE THAT UNDERCUTS THE SOD FOR REMOVAL. THE FRONT-END LOADER HARVEST UNIFORM SOD SQUARES. THE BACKHOE WITH A LARGE BUCKET AND THUMB CAN BE USED FOR QUICK REMOVAL.
5. SODMATS CAN BE UP TO 8 FEET SQUARE DEPENDING ON THE EQUIPMENT USED TO HARVEST. HARVESTED MATERIAL SHOULD BE 6-8\"/>



SHRUB PLANTING

SCALE: N.T.S.

Sand Creek at Aspen Meadows						
Wetland Seed Mix		lb/ac (PLS)	% PLS/ac	seeds/lb	seeds/ac	seeds/ft ²
<i>Beckmannia syzigachne</i>	American Sloughgrass	0.4	3.08	1,150,000	460,000	10.56
<i>Carex nebrakensis</i>	Nebraska Sedge	1	7.69	534,100	534,100	12.26
<i>Dechampsia cespitosa</i>	Tufted Hairgrass	0.4	3.08	1,500,000	600,000	13.77
<i>Eleocharis palustris</i>	Creeping Spikenush	0.8	6.15	620,000	496,000	11.39
<i>Panicum virgatum 'Blackwell'</i>	Switchgrass, Blackwell	2	15.38	259,000	518,000	11.89
<i>Pascopyrum smithii 'Arriba'</i>	Western Wheatgrass, Arriba	2.5	19.23	115,000	287,500	6.60
<i>Schoenoplectus acutus</i>	Hardstem Bulrush	1.3	10.00	377,600	490,880	11.27
<i>Scirpus maritimus</i>	Alkali Bulrush	2	15.38	230,000	460,000	10.56
<i>Spartina pectinata</i>	Prairie Cordgrass	2.6	20.00	197,000	512,200	11.76
		13	100.00	4,982,700	4,358,680	100.06
Riparian Seed Mix		lb/ac (PLS)	% PLS/ac	seeds/lb	seeds/ac	seeds/ft ²
<i>Andropogon hallii</i>	Sand Bluestem	3.3	16.41	96,640	318,912	7.32
<i>Calamagrostis canadensis</i>	Blue-joint Reedgrass	0.16	0.80	2,270,000	363,200	8.34
<i>Dechampsia cespitosa</i>	Tufted Hairgrass	0.25	1.24	1,500,000	375,000	8.61
<i>Elymus canadensis</i>	Canada Wildrye	2.6	12.93	114,000	296,400	6.80
<i>Elymus lanceolatus</i> spp. <i>psammophilus</i>	Streambank wheatgrass, Sodar	2.4	11.93	156,000	374,400	8.60
<i>Glyceria striata</i>	Fowl Mammagrass	1.7	8.45	180,000	306,000	7.02
<i>Nassella viridula 'Cucharas'</i>	Green Needlegrass, Cucharas	2	9.95	167,840	335,680	7.71
<i>Panicum virgatum 'Blackwell'</i>	Switchgrass, Blackwell	1.4	6.96	259,000	362,600	8.32
<i>Pascopyrum smithii 'Arriba'</i>	Western wheatgrass, Arriba	3.5	17.40	115,000	402,500	9.24
<i>Spartina pectinata</i>	Prairie cordgrass	2.5	12.43	197,000	492,500	11.31
<i>Sporobolus airoides 'Salado'</i>	Alkali sacaton, Salado	0.3	1.49	1,750,000	525,000	12.05
		20.11	100.00	6,805,480	4,152,192	95.32
Forbes and Shrubs						
<i>Asclepias incarnata</i>	Swamp Milkweed	2	20.30	68,100	136,200	3.13
<i>Asclepias speciosa</i>	Showy Milkweed	2	20.30	58,000	116,000	2.66
<i>Careopsis tinctoria</i>	Plains Coreopsis	0.1	1.02	3,200,000	320,000	7.35
<i>Ahus incana tenuifolia</i>	Thinleaf Aker	0.25	2.54	675,000	168,750	3.87
<i>Rosa woodsii</i>	Wood's Rose	3	30.46	49,000	147,000	3.37
<i>Sambucus racemosa</i>	Red Elderberry	0.5	5.08	286,000	143,000	3.28
<i>Symphoricarpos albus</i>	Common Snowberry	2	20.30	76,000	152,000	3.49
		9.85	100.00	4,412,100	1,182,950	27.16
Upland Seed Mix		lb/ac (PLS)	% PLS/ac	seeds/lb	seeds/ac	seeds/ft ²
<i>Achnatherum hymenoides</i>	Indian Ricegrass	2	6.87	161,920	323,840	7.43
<i>Bouteloua curtipendula 'Vaughn'</i>	Sideoats Grama, Vaughn	2	6.87	191,000	382,000	8.77
<i>Bouteloua gracilis 'Bad River'</i>	Blue Grama, Bad River	0.4	1.37	825,000	330,000	7.58
<i>Buchloe dactyloides 'Texoka'</i>	Buffalograss, Texoka	6	20.62	45,000	270,000	6.20
<i>Hesperostipa comata</i> ssp. <i>Comata</i>	Needle and Thread	2.5	8.59	115,000	287,500	6.60
<i>Koeleria macrantha</i>	Prairie Junegrass	0.15	0.52	2,310,000	346,500	7.95
<i>Nassella viridula 'Cucharas'</i>	Green Needlegrass, Cucharas	1.7	5.84	167,840	285,328	6.55
<i>Pascopyrum smithii 'Arriba'</i>	Western Wheatgrass, Arriba	3	10.31	115,000	345,000	7.92
<i>Schizachyrium scoparium 'Pastura'</i>	Little Bluestem, Pastura	1.3	4.47	240,670	312,871	7.18
<i>Sporobolus cryptandrus</i>	Sand Dropseed	0.05	0.17	5,600,000	280,000	6.43
<i>Avena sativa 'Monida'</i>	Oats-Monida	10	34.36	14,000	140,000	3.21
		29.1	100.00	9,785,430	3,303,039	75.83
Forbes and Shrubs						
<i>Achillea millefolium</i>	White Yarrow	0.05	0.76	2,700,000	135,000	3.10
<i>Antennaria parvifolia</i>	Pussytoes	0.12	1.82	1,135,000	136,200	3.13
<i>Artemisia frigida</i>	Fringed Sage	0.03	0.46	4,500,000	135,000	3.10
<i>Astragalus adsurgens</i>	Upright Milkvetch	2	30.40	70,000	140,000	3.21
<i>Cleome serrulata</i>	Rocky Mountain Bee Plant	1.4	21.28	113,500	158,900	3.65
<i>Fallugia paradoxa</i>	Apache Plume	0.35	5.32	420,000	147,000	3.37
<i>Philadelphus microphyllus</i>	Littleleaf Mock Orange	0.03	0.46	5,400,000	162,000	3.72
<i>Ptelea trifoliata</i>	Western Hop Tree	1.5	22.80	9,000	13,500	0.31
<i>Prunella tridentata</i>	Bitterbrush	1.1	16.72	13,400	14,740	0.34
		6.58	100.00	14,360,900	1,042,340	23.93

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
X-886-EX-IMAGE				
X-886-EX-TOPO				
X-886-EX-MAP				
X-886-EX-22-34				
X-886-PR-GRADE				

COMPUTER FILE MANAGEMENT			
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THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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DATE _____

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PREPARED BY:

SEAL

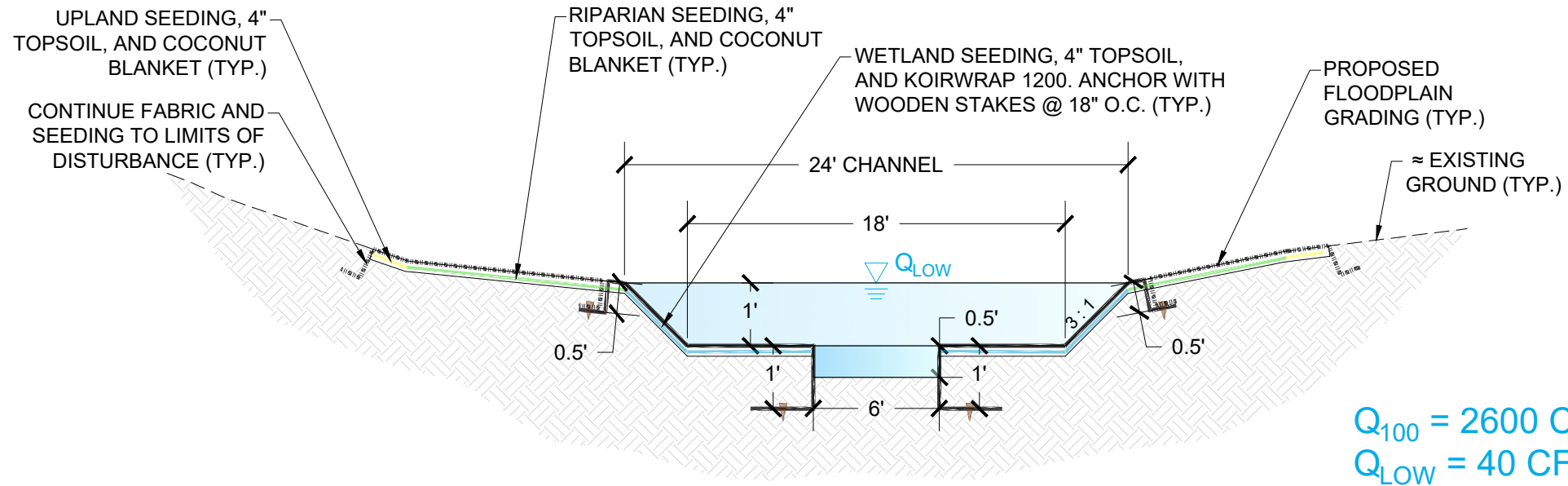
PRELIMINARY
THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND IS SUBJECT TO CHANGE

FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION					
SAND CREEK STABILIZATION AT ASPEN MEADOWS 100% DESIGN PLANS					
REVEGETATION DETAILS					
DESIGNED BY:	JAB	SCALE	DATE ISSUED:	MAY 2020	DRAWING No.
DRAWN BY:	RAF	HORIZ	N/A		
CHECKED BY:	AJS	VERT.	N/A	SHEET	13 OF 38
					RV04



Know what's below.
Call before you dig.

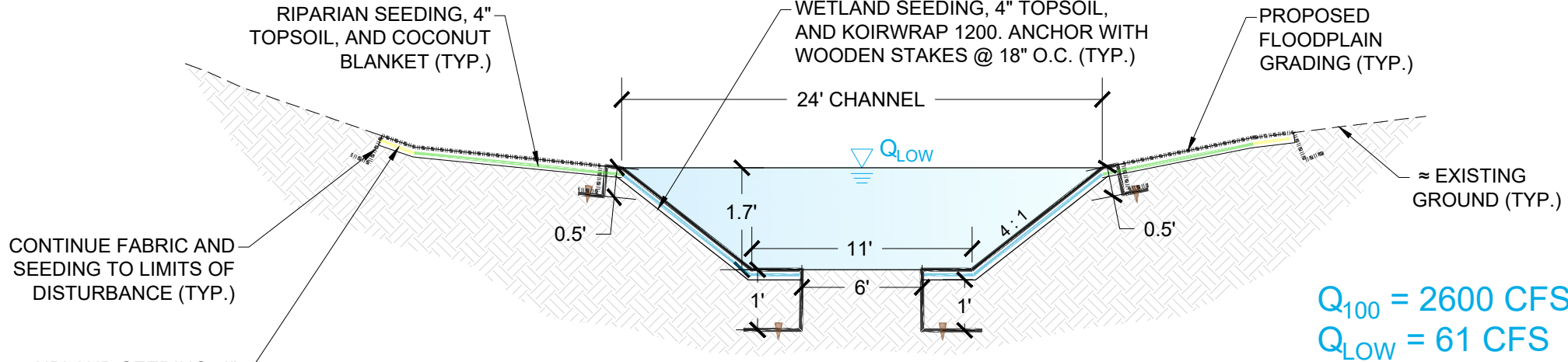


$Q_{100} = 2600 \text{ CFS}$
 $Q_{LOW} = 40 \text{ CFS}$

TYPICAL DESIGN CHANNEL SECTION 1

NOT TO SCALE NOTE: 3:1 VERTICAL EXAGGERATION

- NOTES:
1. TYPICAL SECTION 1 APPLIES FROM APPROXIMATELY STATION 85+52 TO 88+67 AND 108+20 TO 110+20, EXCLUDING THE DROP STRUCTURES.
 2. TYPICAL SECTION 2 CONNECTS THE DOWNSTREAM END OF DROP 5 TO THE BRIDGE PROJECT (APPROXIMATELY STATION 103+00 TO 103+58).
 3. BASED UPON ONSITE AVAILABILITY, SOD MATS SHOULD BE HARVESTED AND PLACED IN LIEU OF SEEDING AND BLANKET. SEE REVEGETATION DETAILS FOR FURTHER INSTRUCTIONS.



$Q_{100} = 2600 \text{ CFS}$
 $Q_{LOW} = 61 \text{ CFS}$

TYPICAL DESIGN CHANNEL SECTION 2

NOT TO SCALE NOTE: 3:1 VERTICAL EXAGGERATION

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34 Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:41 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

CITY OF COLORADO SPRINGS ONLY:
FILED IN ACCORDANCE WITH SECTION 7.7.906 OF THE CODE OF THE CITY OF COLORADO SPRINGS, 2001, AS AMENDED.

FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



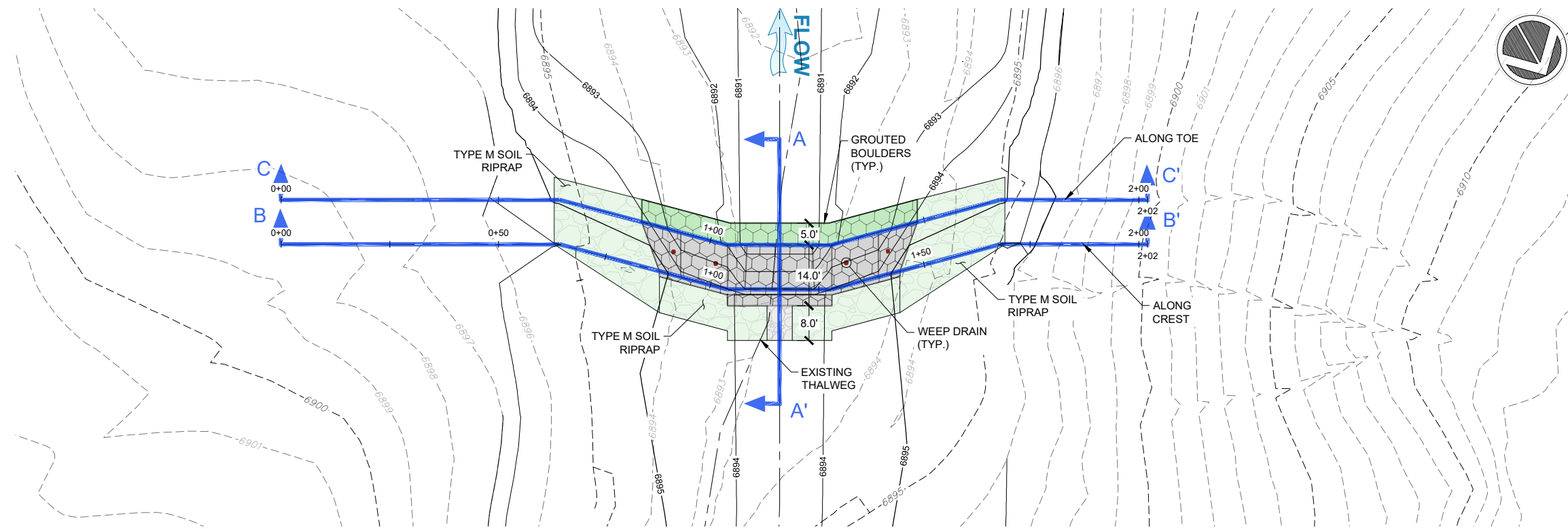
PREPARED BY:
Matrix
Excellence by Design

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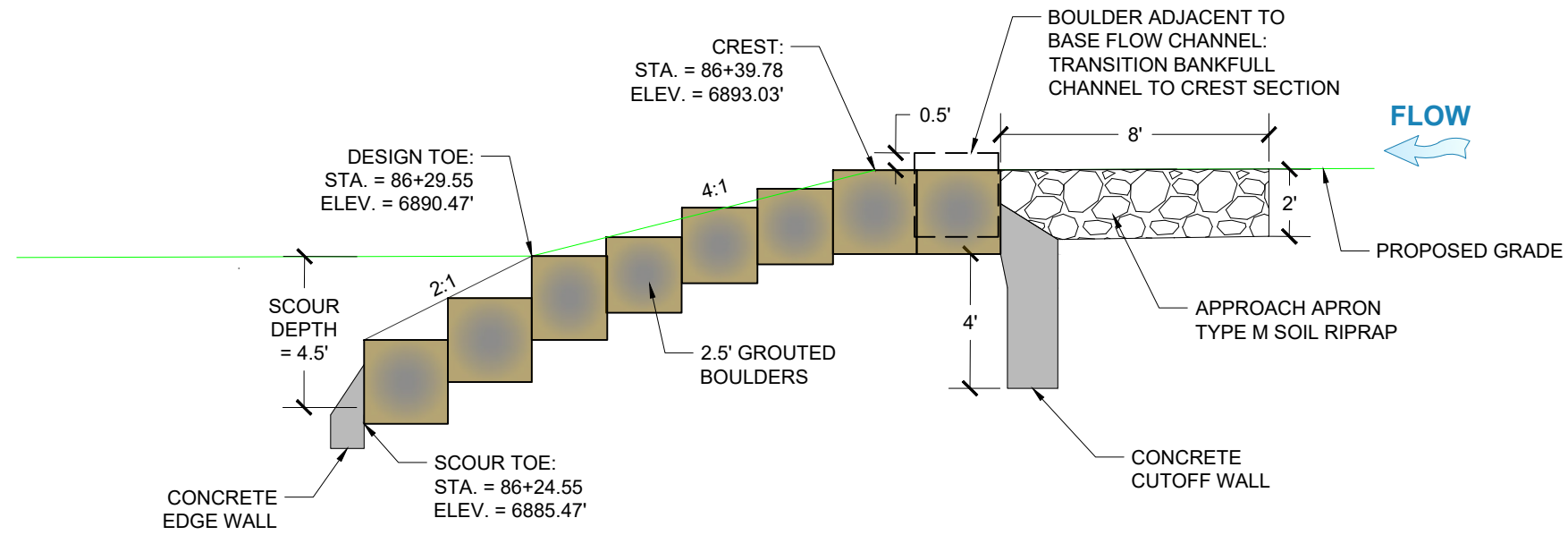
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
TYPICAL SECTIONS			
DESIGNED BY: JAB	SCALE: HORIZ N/A	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. N/A	SHEET 14 OF 38	DT01
CHECKED BY: AJS			



Know what's below.
Call before you dig.



PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #1 (NON-BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach			
X-886-PR-GRADE			
X-886-MD022x34			
Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
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DATE _____
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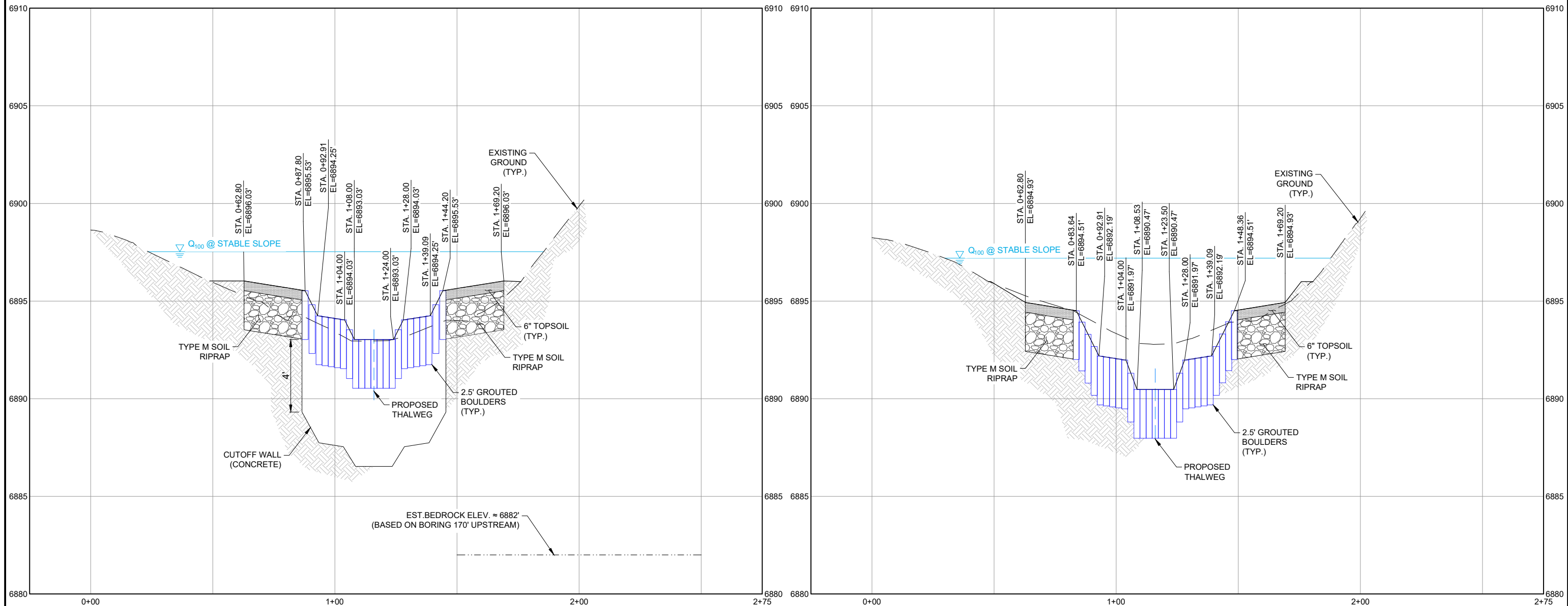
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #1 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. N/A	SHEET 15 OF 38	DT02
CHECKED BY: AJS			



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)

CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #1 (NON-BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:41 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



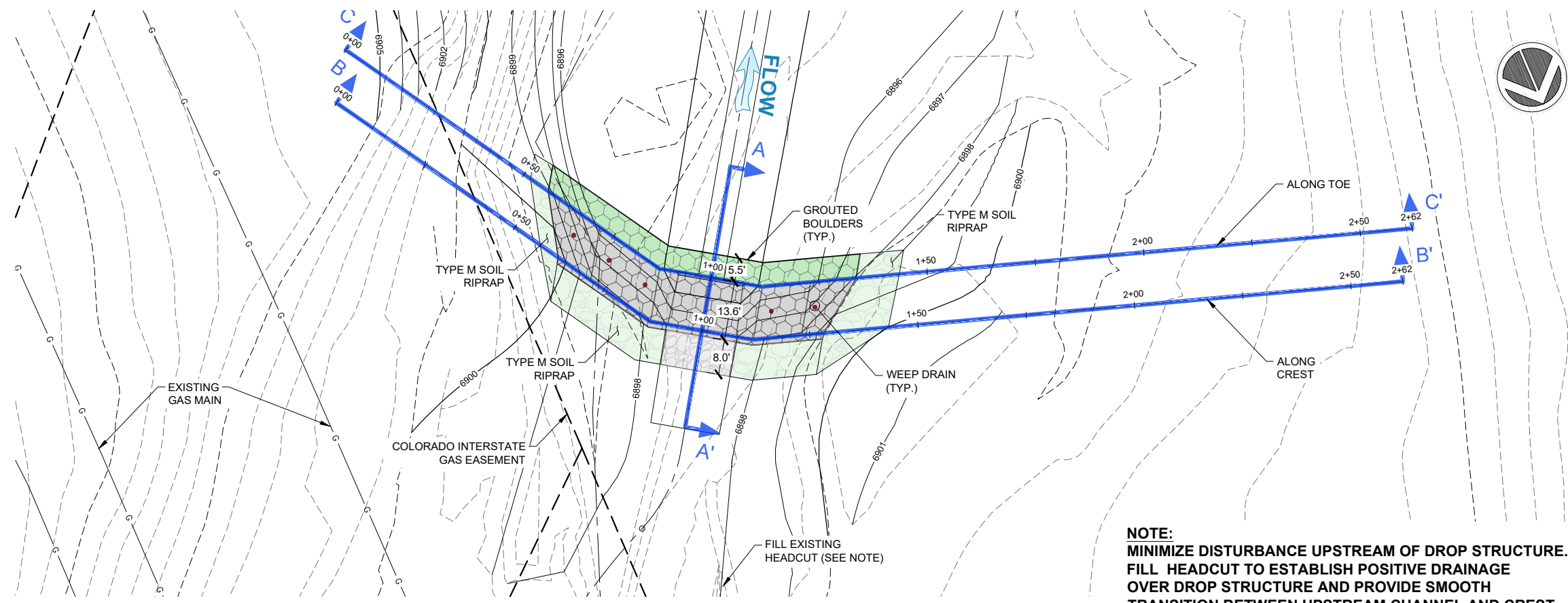
PREPARED BY:
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PRELIMINARY
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COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #1 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No. DT03
CHECKED BY: RAF	VERT. 1" = 5'	SHEET 16 OF 38	

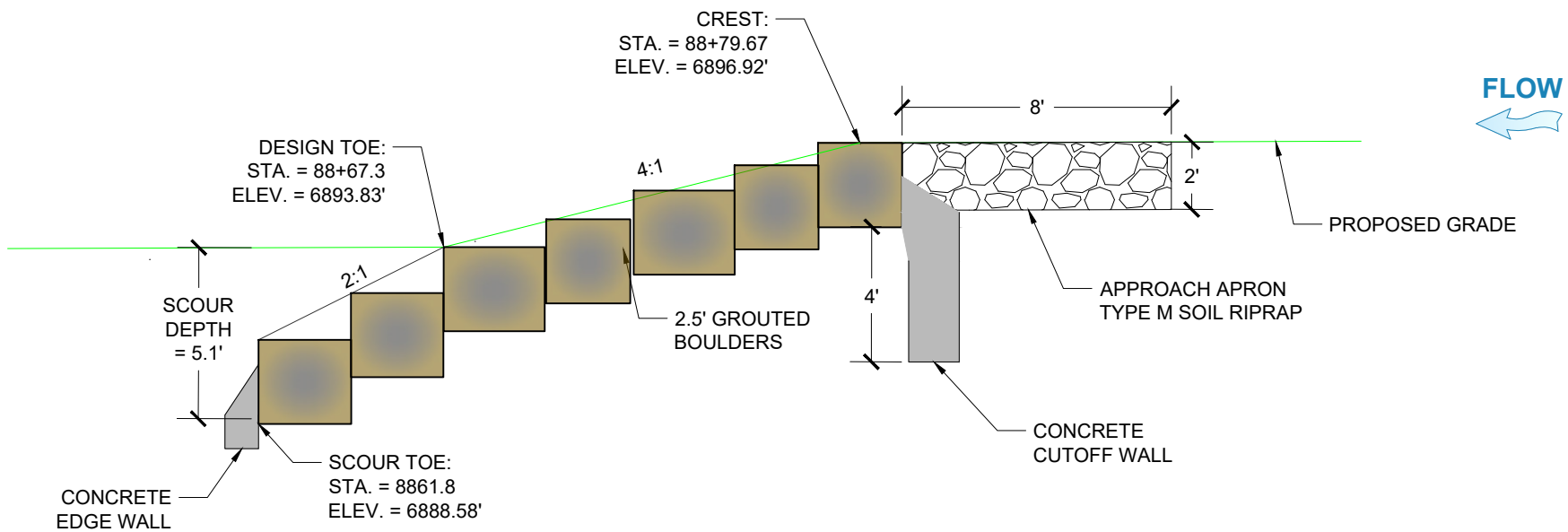


Know what's below.
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NOTE:
MINIMIZE DISTURBANCE UPSTREAM OF DROP STRUCTURE.
FILL HEADCUT TO ESTABLISH POSITIVE DRAINAGE
OVER DROP STRUCTURE AND PROVIDE SMOOTH
TRANSITION BETWEEN UPSTREAM CHANNEL AND CREST
SECTION. REVEGETATE ANY IMPACT.

PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #2 (NON-BURIED)

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
Drop Modeling - Lower Reach				
X-886-PR-GRADE				
X-886-MDQ22x34				
Drop Modeling - Upper Reach				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 4:42 PM				
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CONDITIONS:



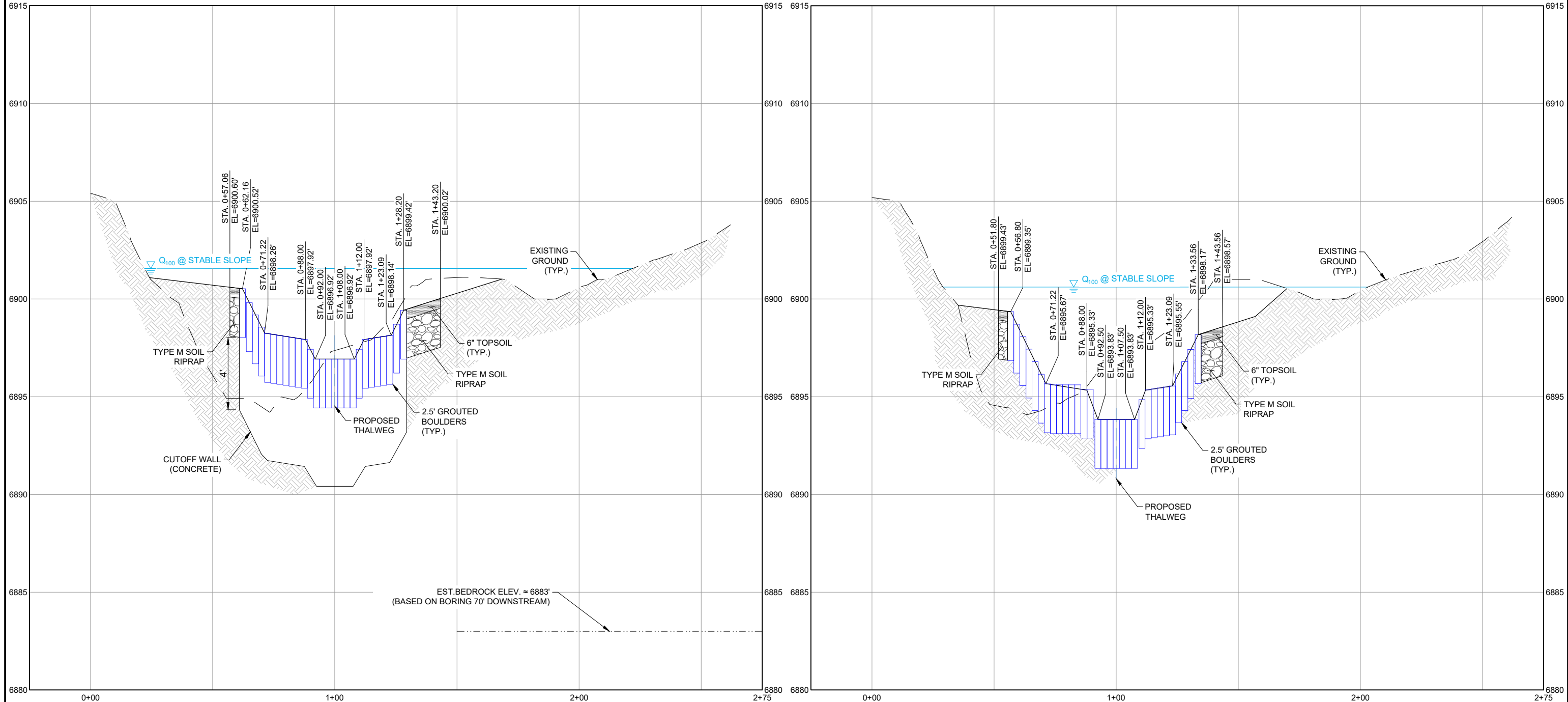
PREPARED BY:
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Excellence by Design

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COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #2 DETAILS			
DESIGNED BY: JAB	SCALE: 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No. DT04
DRAWN BY: RAF	HORIZ: N/A	SHEET 17 OF 38	
CHECKED BY: AJS	VERT: N/A		



Know what's below.
Call before you dig.



DROP STRUCTURE #2 (NON-BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:42 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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CONDITIONS:

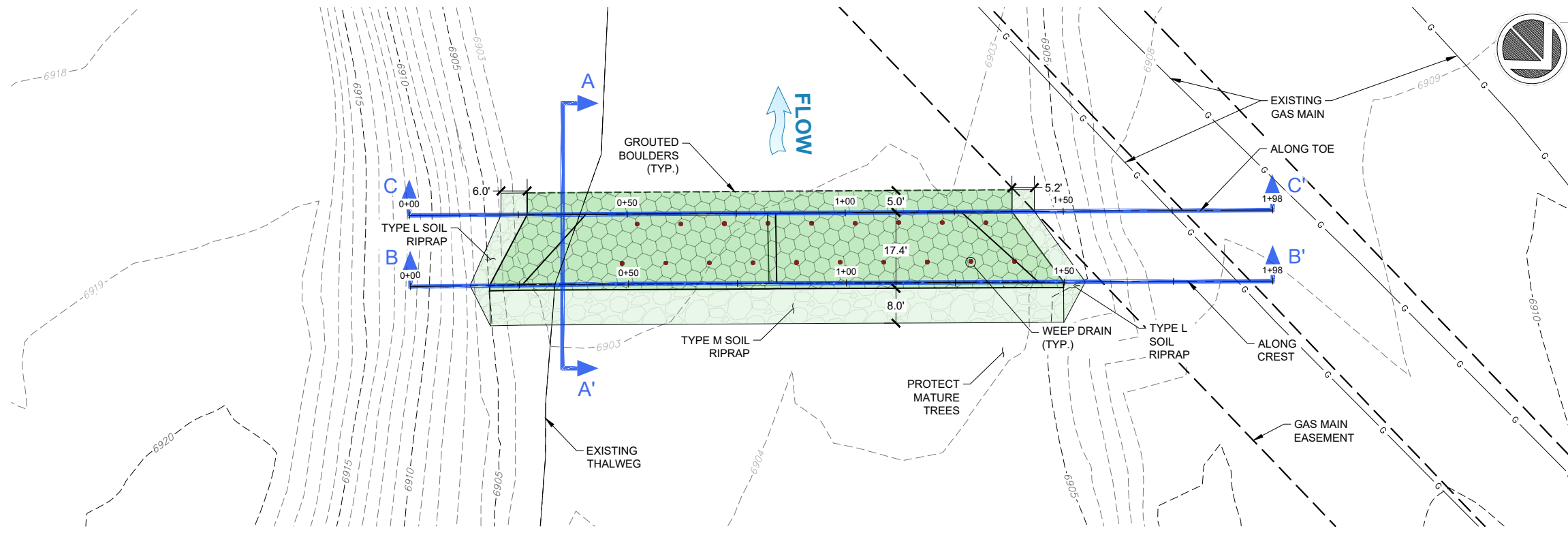


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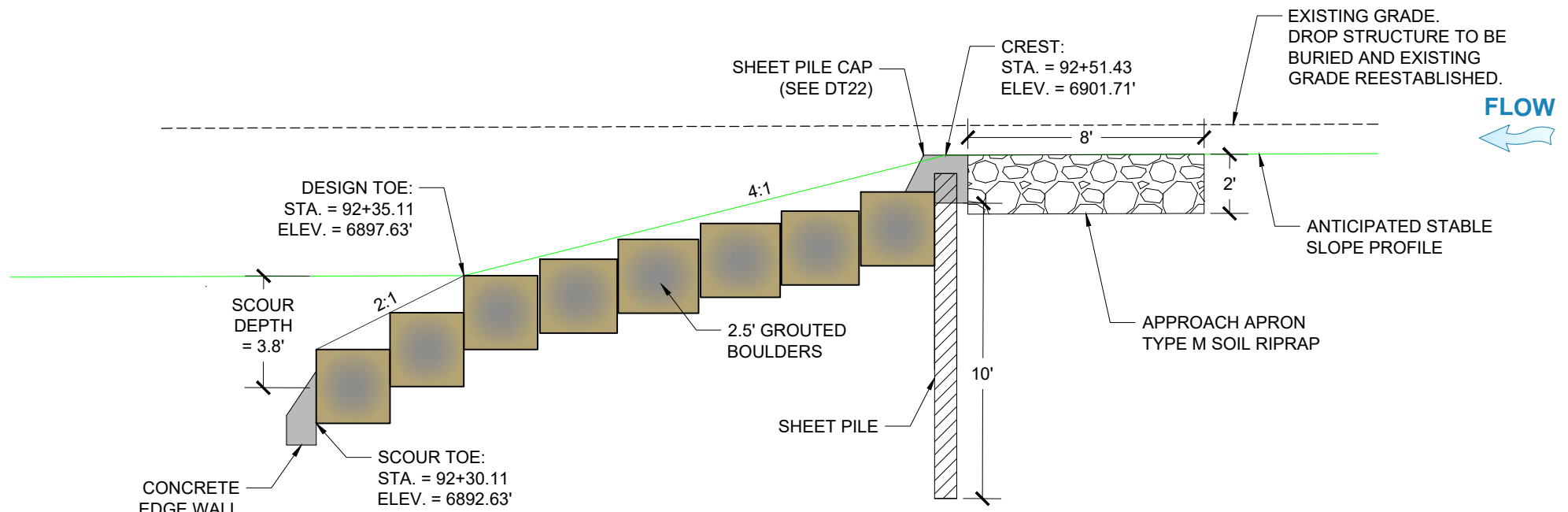
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #2 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. 1" = 5'	SHEET 18 OF 38	DT05
CHECKED BY: AJS			



Know what's below.
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PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #3 (BURIED)

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34 Drop Modeling - Upper Reach				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\886-DT01-26.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 4:42 PM				
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.				

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DATE _____
CONDITIONS:



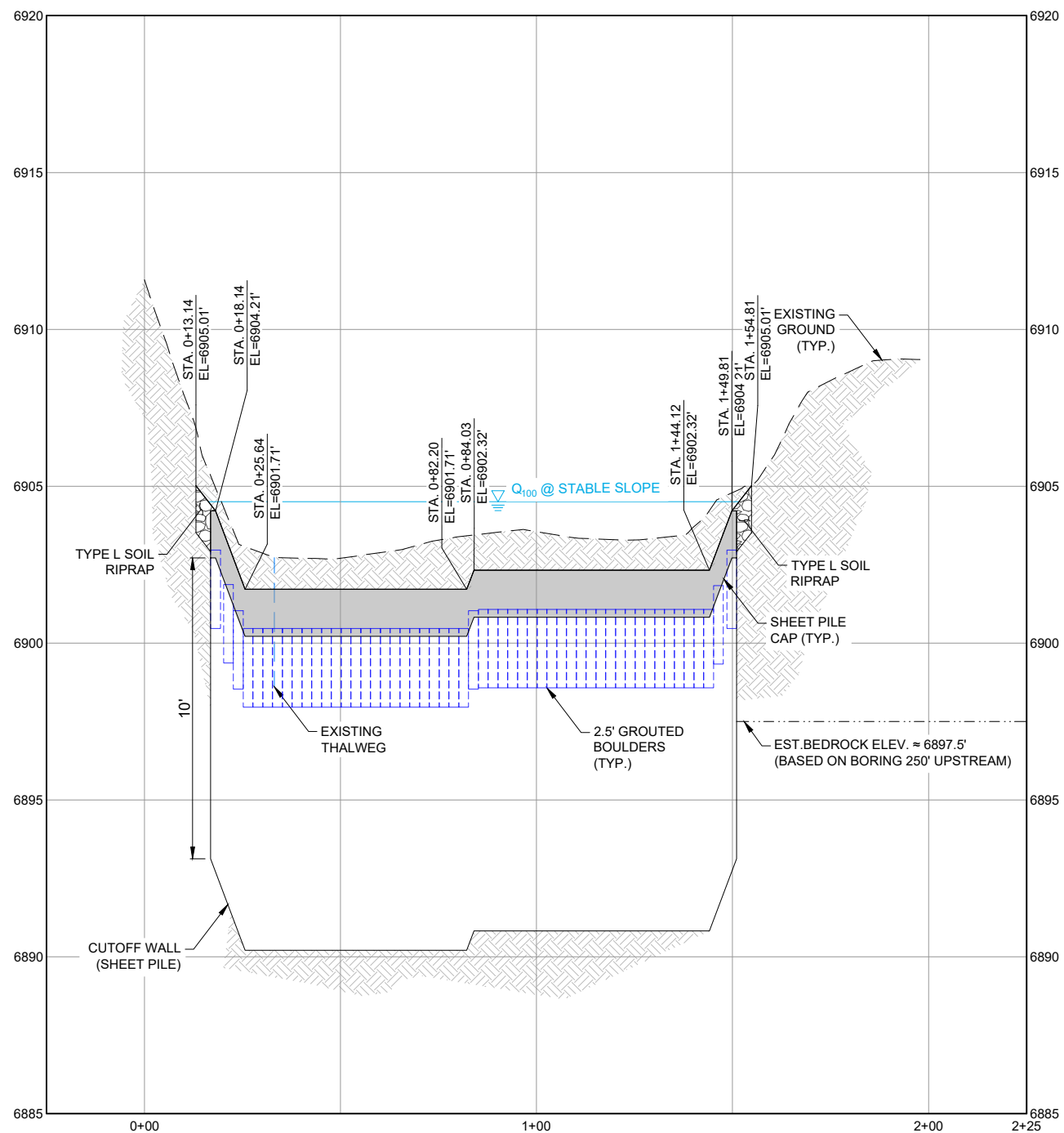
PREPARED BY:
Matrix
Excellence by Design

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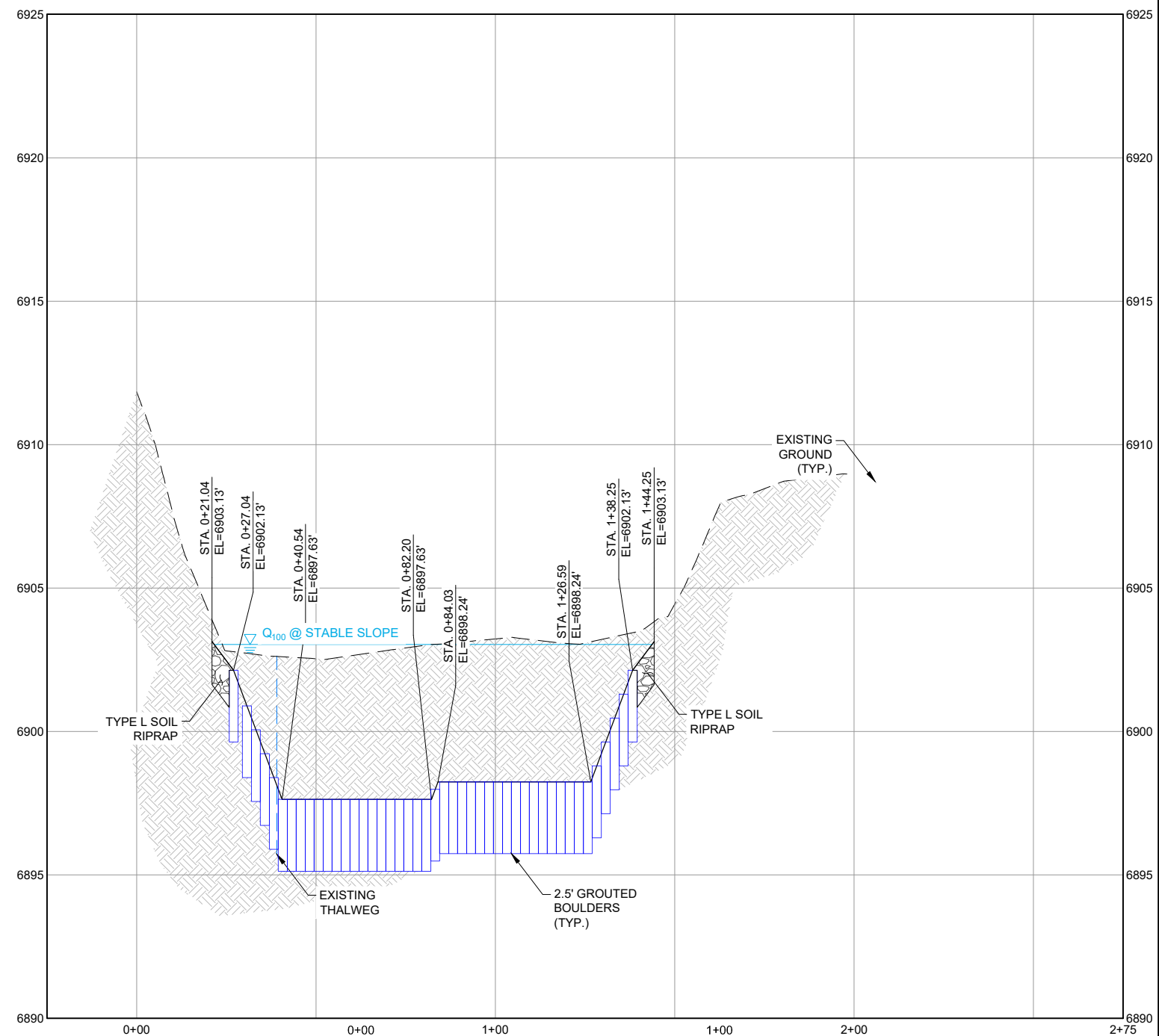
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #3 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. N/A	SHEET	19 OF 38
CHECKED BY: AJS			DT06



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)



CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #3 (BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34 Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:43 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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FOR CITY ENGINEER _____

DATE _____

CONDITIONS:



SEAL

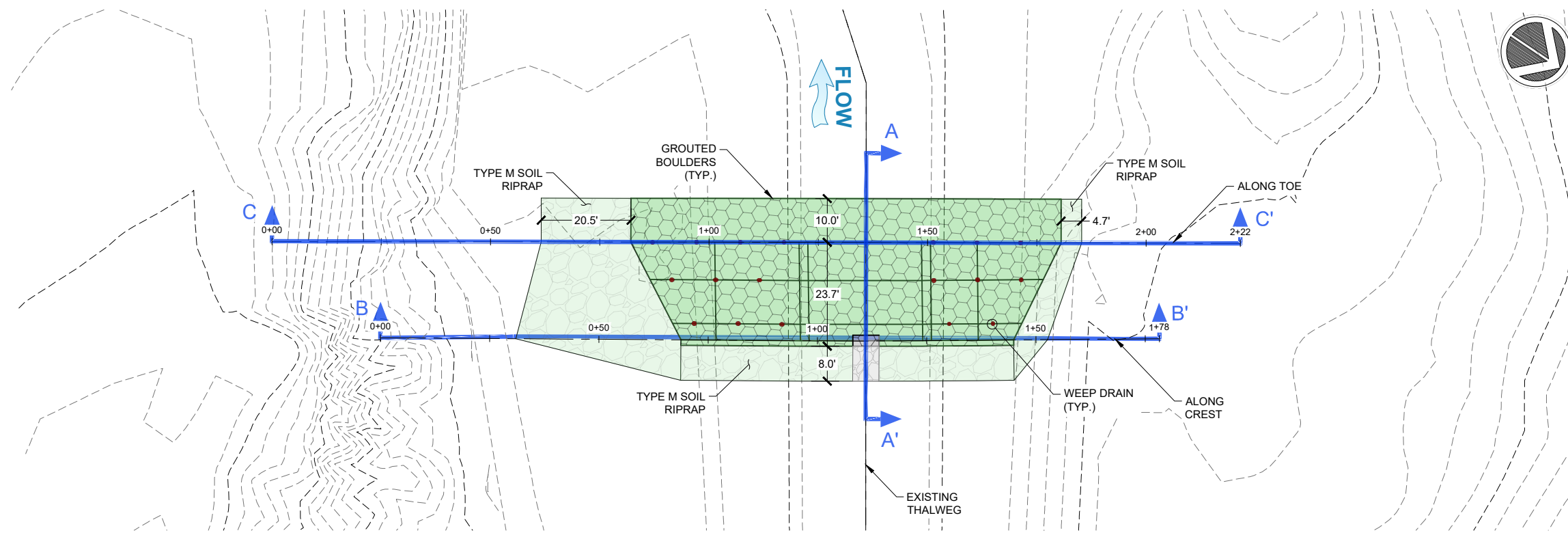
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

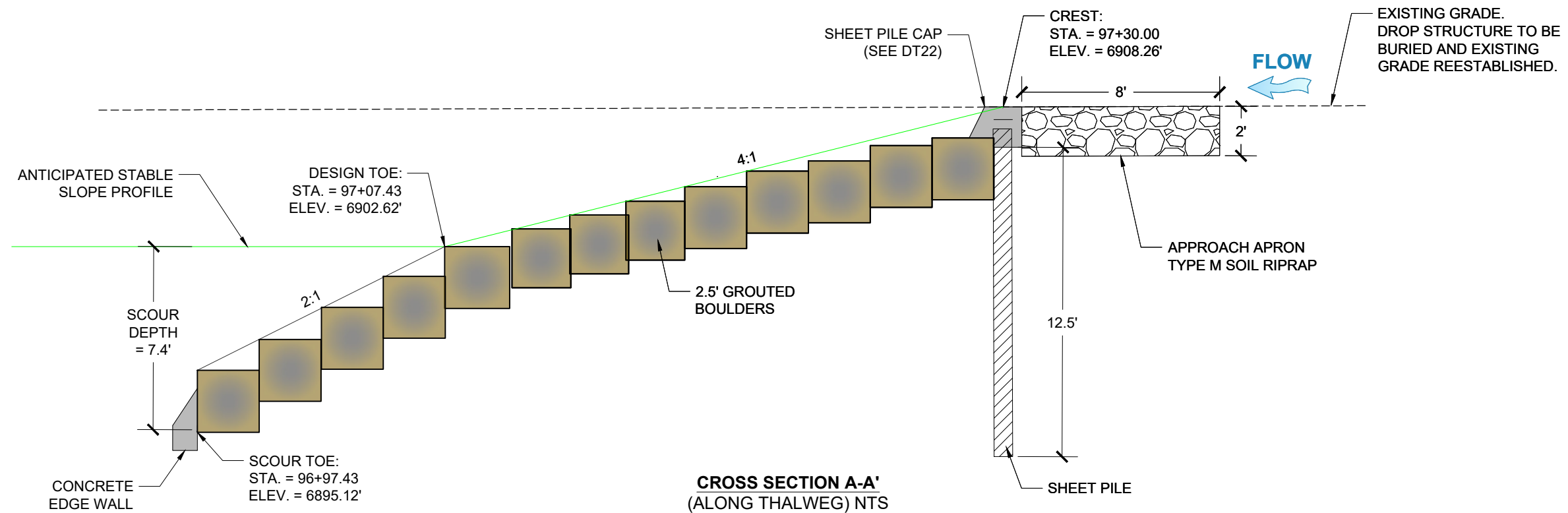
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #3 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No.
CHECKED BY: RAF	VERT. 1" = 5'	SHEET 20 OF 38	DT07



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PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #4 (BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach			
X-886-PR-GRADE			
X-886-MD-G22x34			
Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:44 PM			
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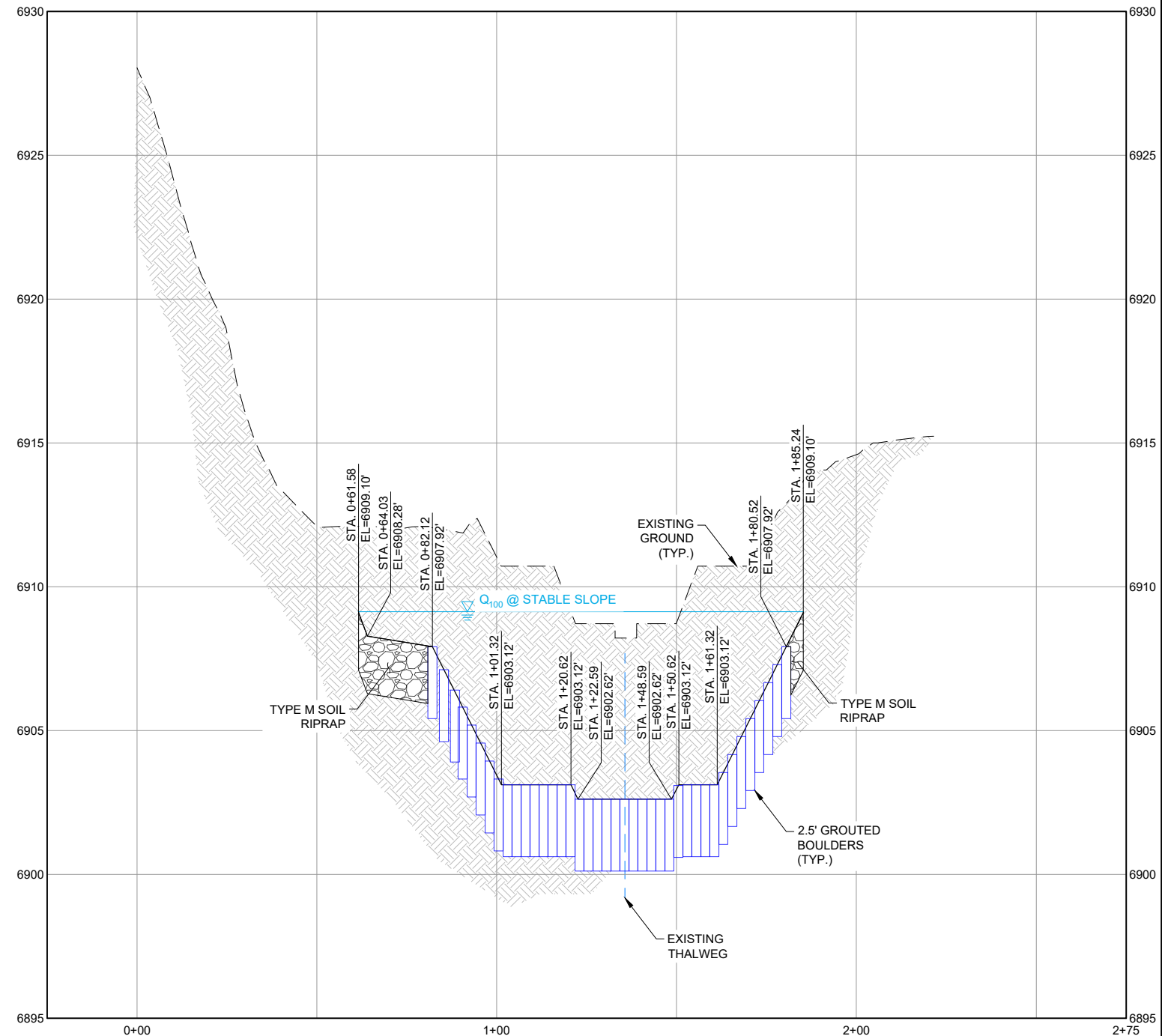
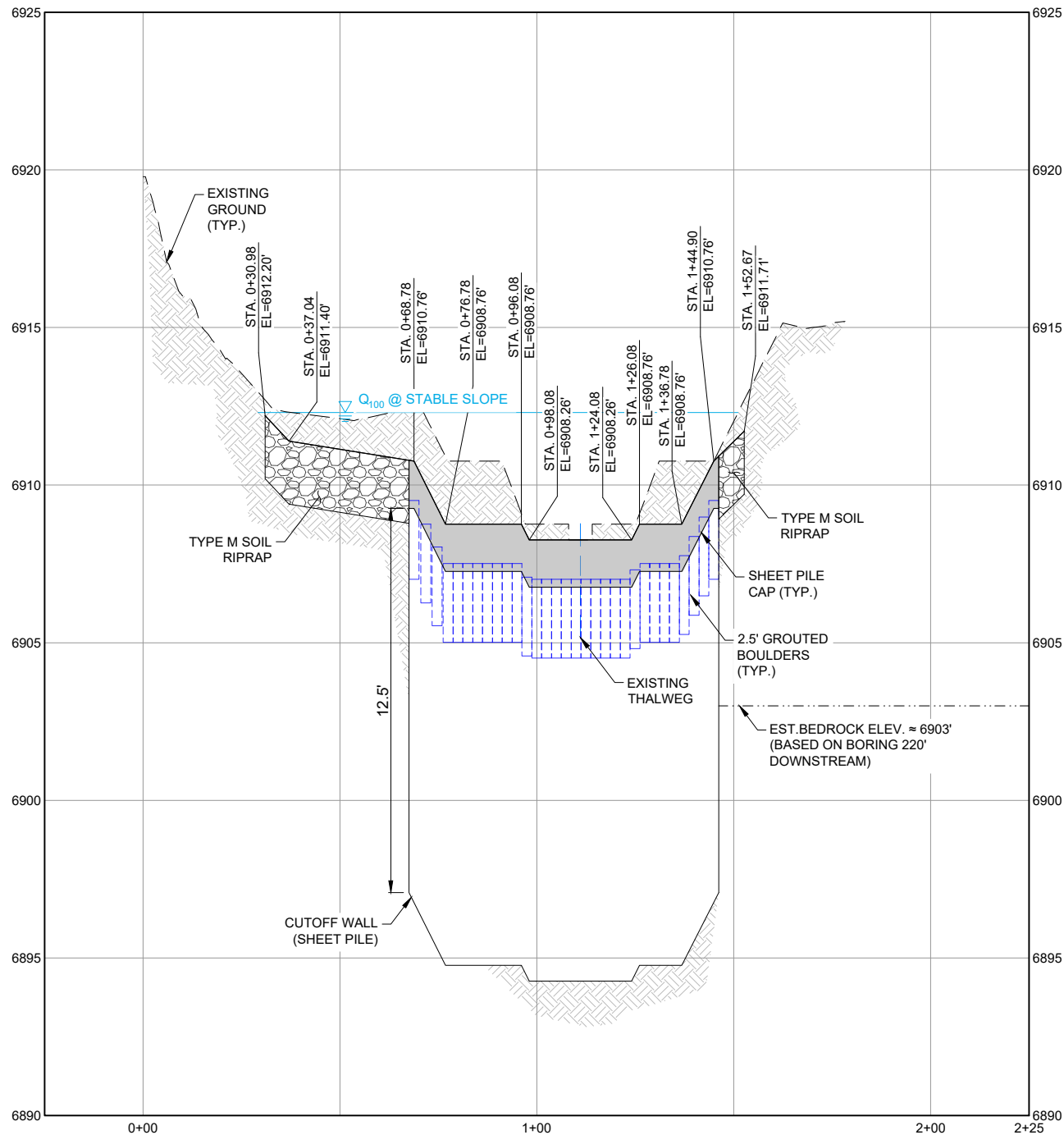
PREPARED BY:
Matrix
Excellence by Design

FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

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COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #4 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. N/A	SHEET 21 OF 38	DT08
CHECKED BY: AJS			



Know what's below.
Call before you dig.



CROSS SECTION B-B' (ALONG CREST)

CROSS SECTION C-C' (ALONG TOE)

DROP STRUCTURE #4 (BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:44 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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PREPARED BY:
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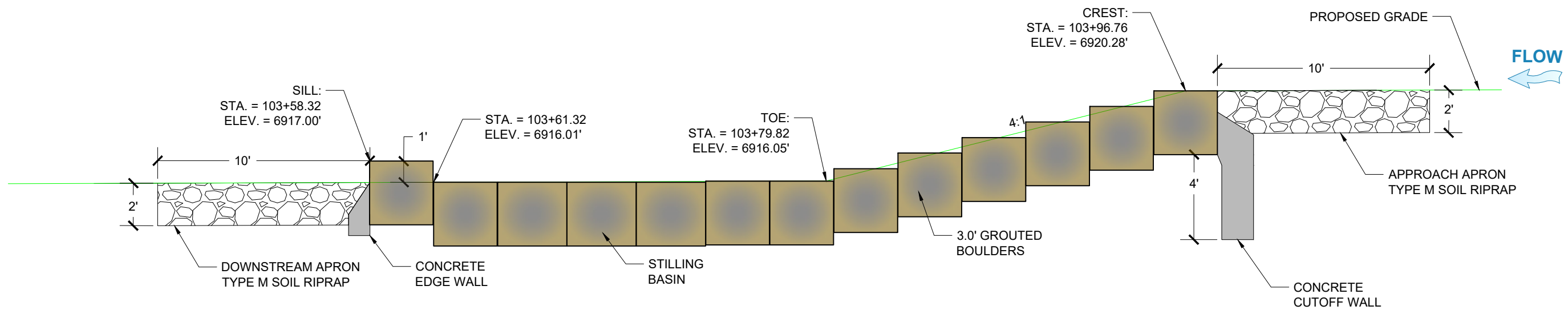
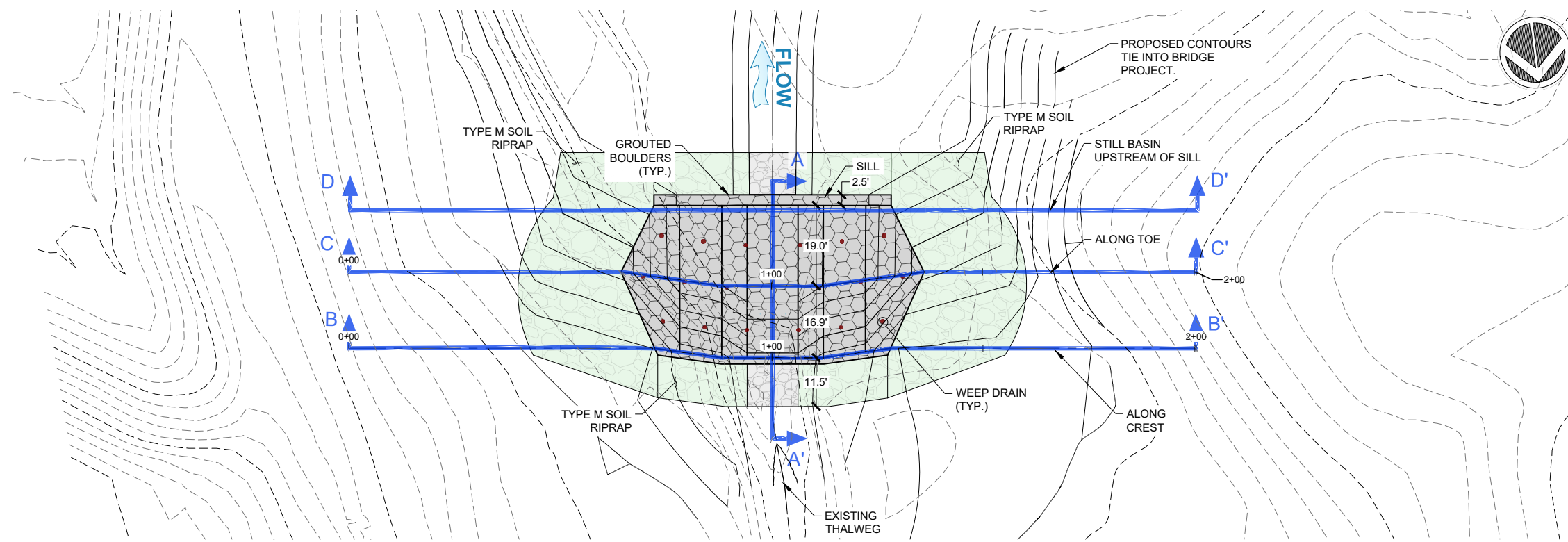
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #4 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No. DT09
CHECKED BY: AJS	VERT. 1" = 5'	SHEET 22 OF 38	



Know what's below.
Call before you dig.



DROP STRUCTURE #5 (NON-BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach			
X-886-PR-GRADE			
X-886-MD-G22x34			
Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:44 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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DATE _____
CONDITIONS:



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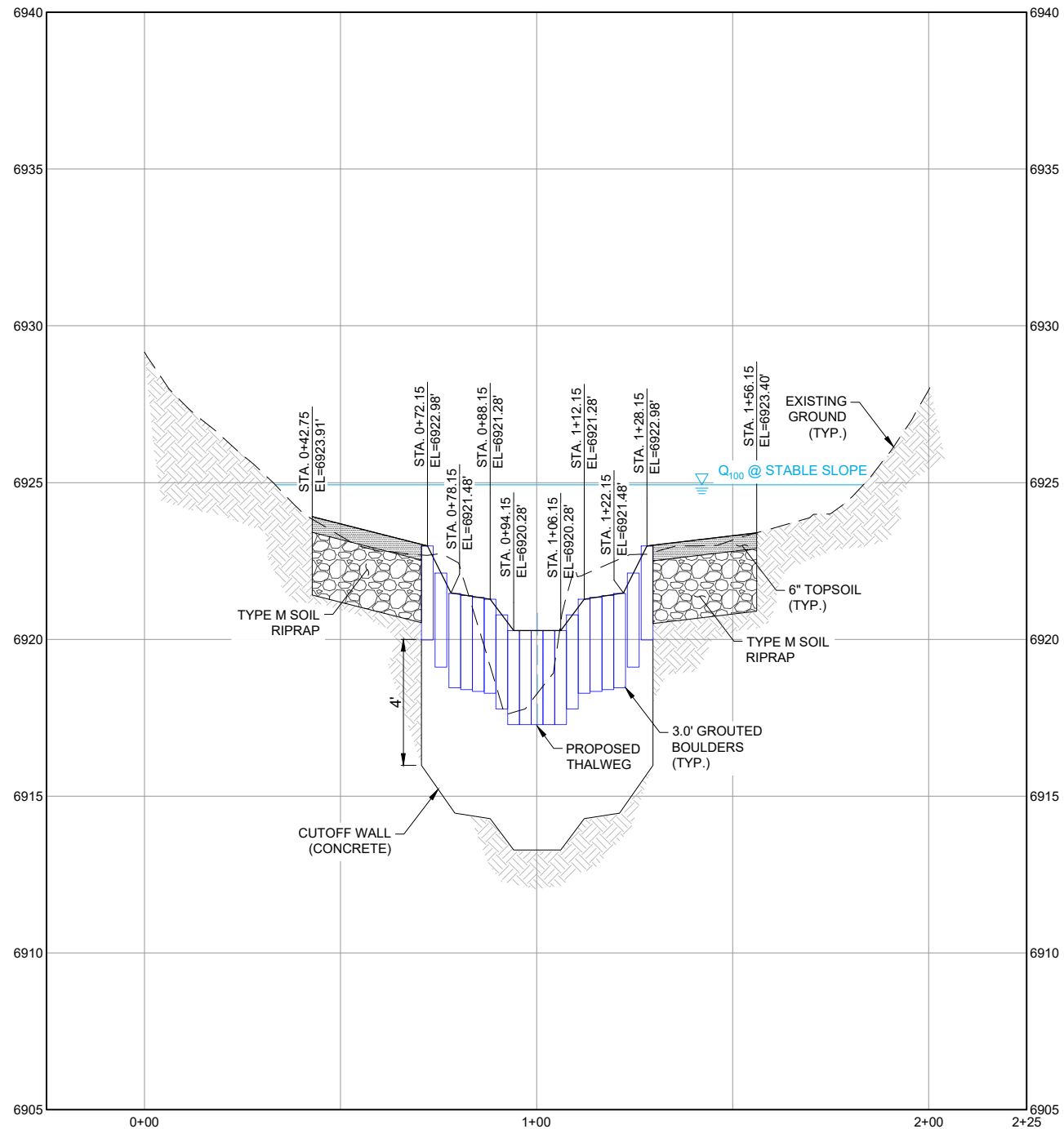
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PROJECT No. 19.886.017

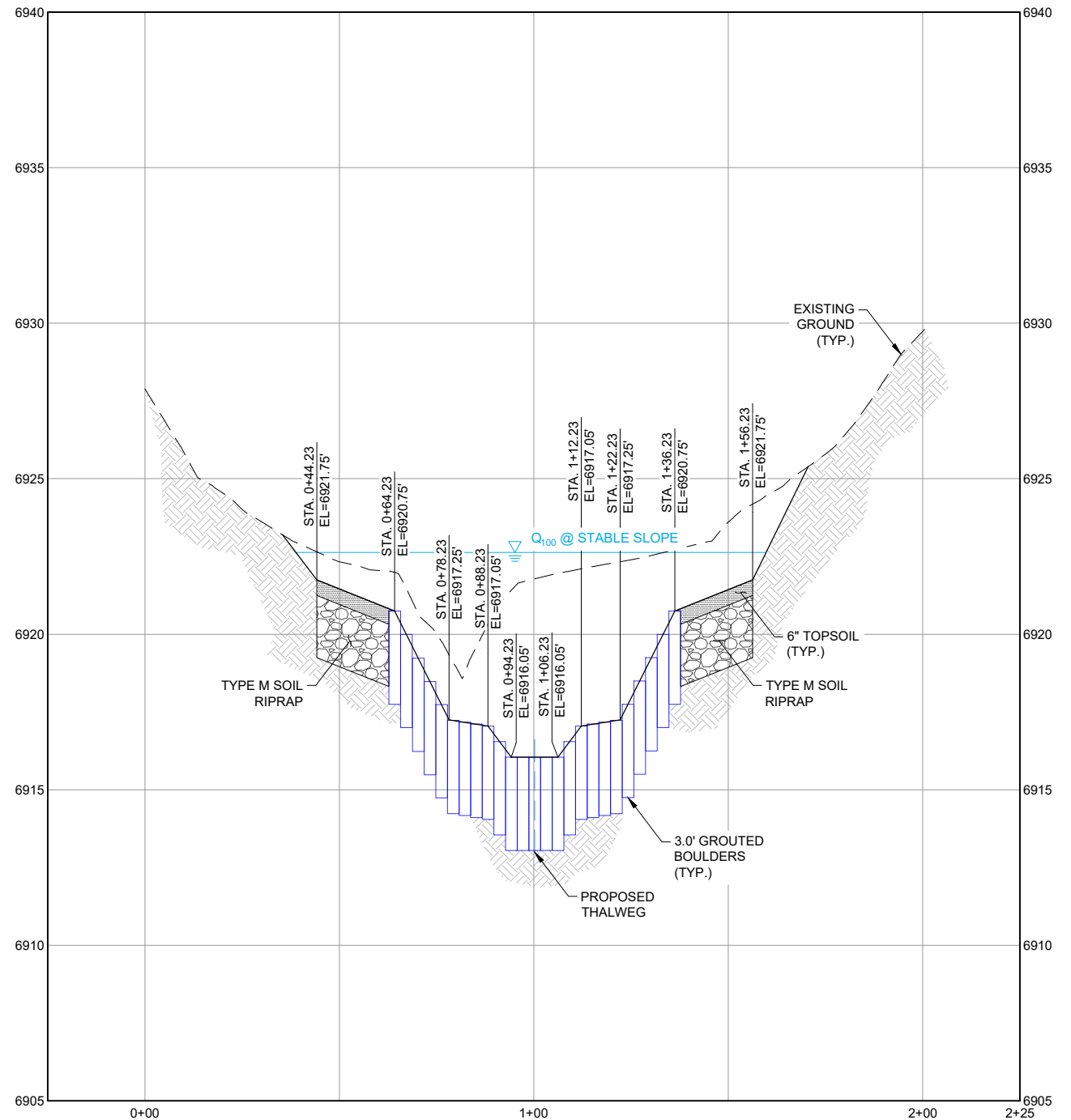
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #5 DETAILS			
DESIGNED BY: JAB	SCALE: 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	HORIZ. N/A	SHEET 23 OF 38	DT10
CHECKED BY: AJS	VERT. N/A		



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)



CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #5 (NON-BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:45 PM			
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DATE _____
CONDITIONS:



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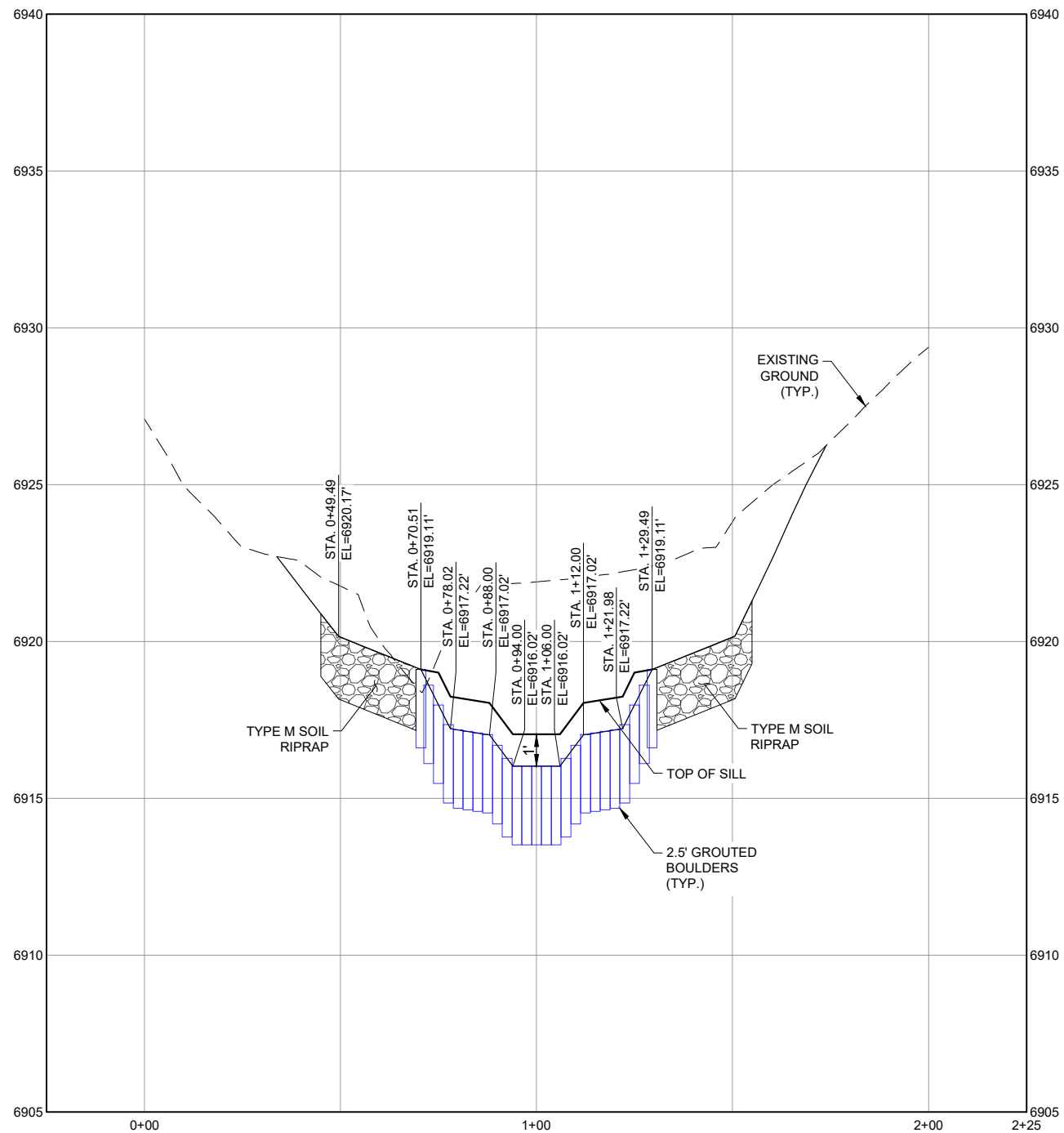
PRELIMINARY
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MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

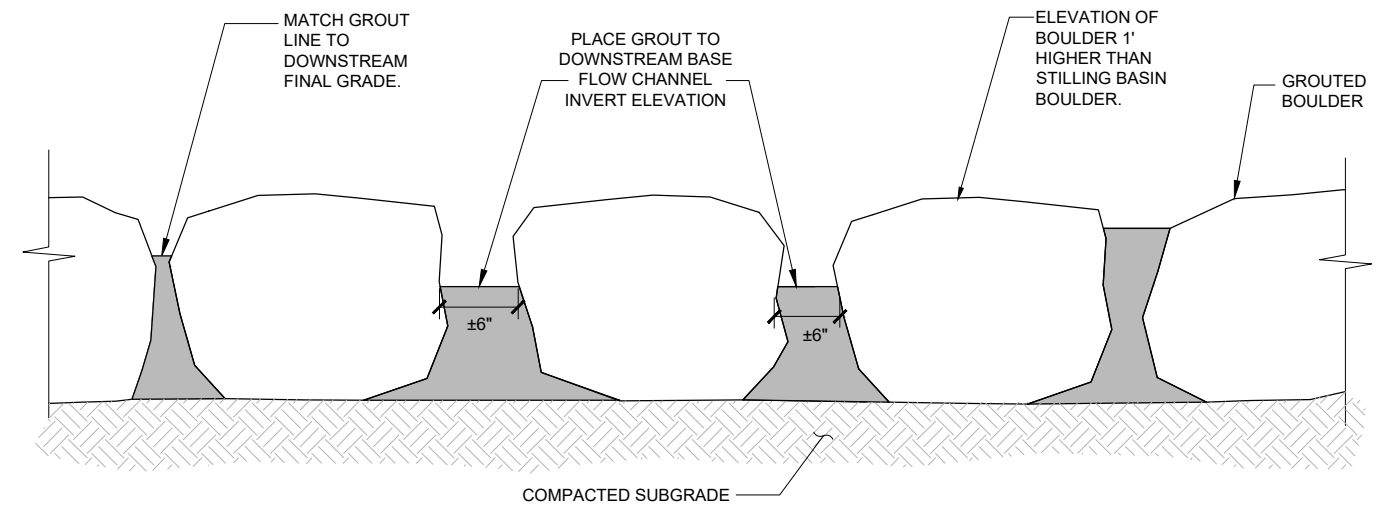
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #5 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No.
CHECKED BY: AJS	VERT. 1" = 5'	SHEET 24 OF 38	DT11



Know what's below.
Call before you dig.



CROSS SECTION D-D'
(STILLING BASIN UPSTREAM OF SILL)



NOTE: ALONG THE END SILL, CORRESPONDING TO THE BASE FLOW CHANNEL, WIDEN GAP BETWEEN BOULDERS TO 6" AND MATCH TOP OF GROUT TO DOWNSTREAM INVERT AND STILLING BASIN INVERT (STILLING BASIN SHOULD BE FREE DRAINING).

SECTION F - END SILL DETAIL

NOT TO SCALE

DROP STRUCTURE #5 (NON-BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:46 PM			
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DATE _____
CONDITIONS:



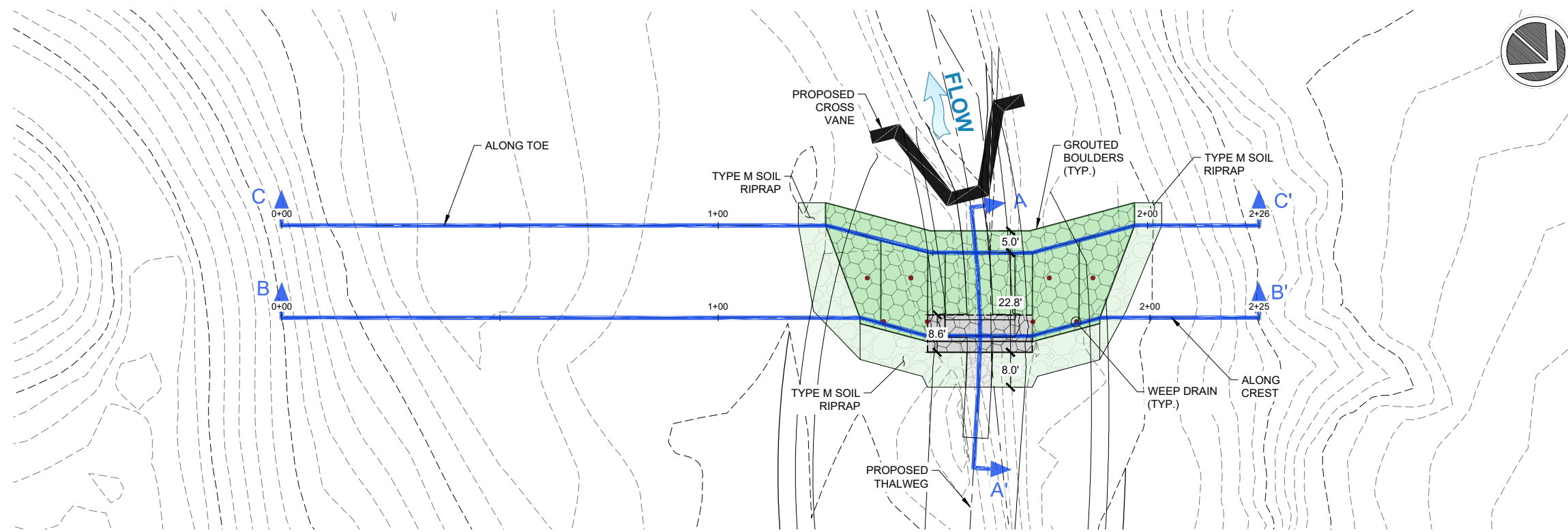
SEAL
PRELIMINARY
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FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

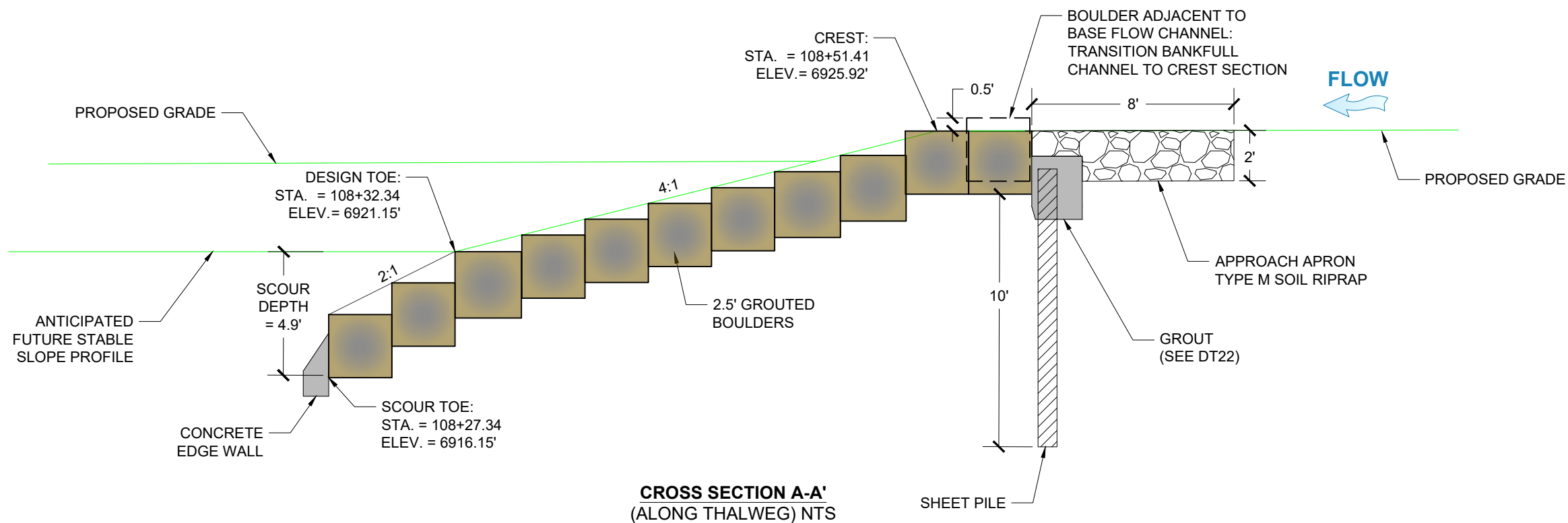
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #5 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. 1" = 5'	SHEET 25 OF 38	DT12
CHECKED BY: AJS			



Know what's below.
Call before you dig.



PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #6 (PARTIALLY BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MDQ22x34 Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:46 PM			
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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



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Excellence by Design

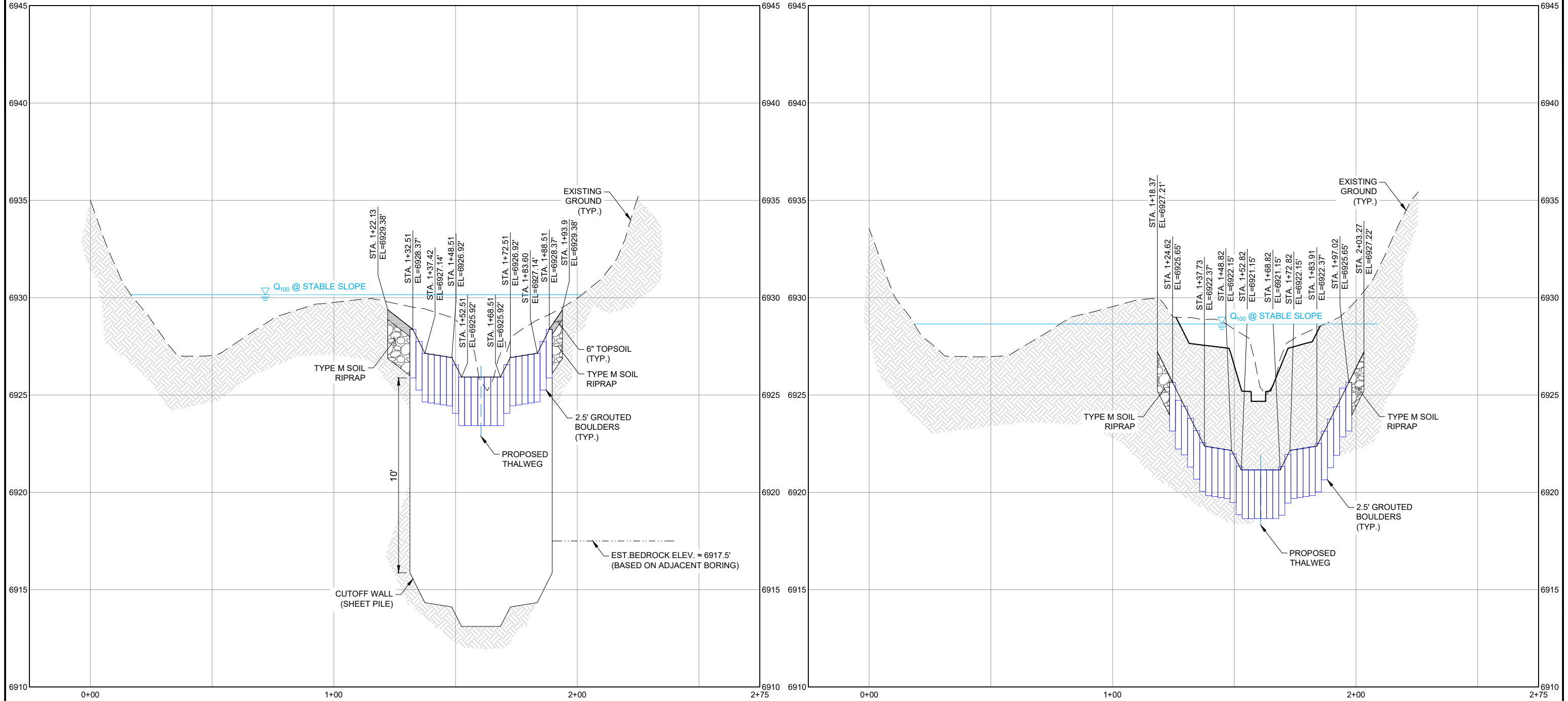
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GOVERNING AGENCIES AND
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #6 DETAILS			
DESIGNED BY:	JAB	SCALE:	DATE ISSUED:
DRAWN BY:	RAF	HORIZ 1" = 30'	MAY 2020
CHECKED BY:	AJS	VERT. N/A	26 OF 38
			DRAWING No. DT13



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)

CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #6 (PARTIALLY BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34 Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:47 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



PREPARED BY:
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Excellence by Design

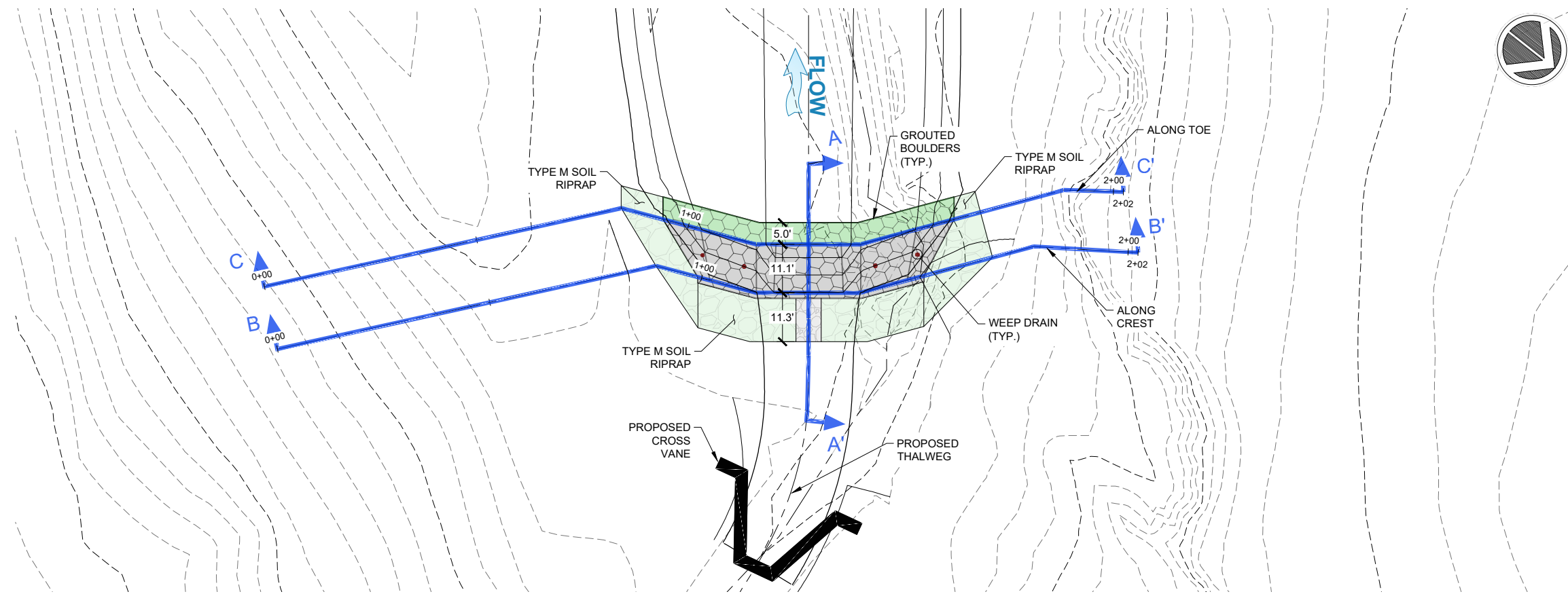
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PRELIMINARY
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

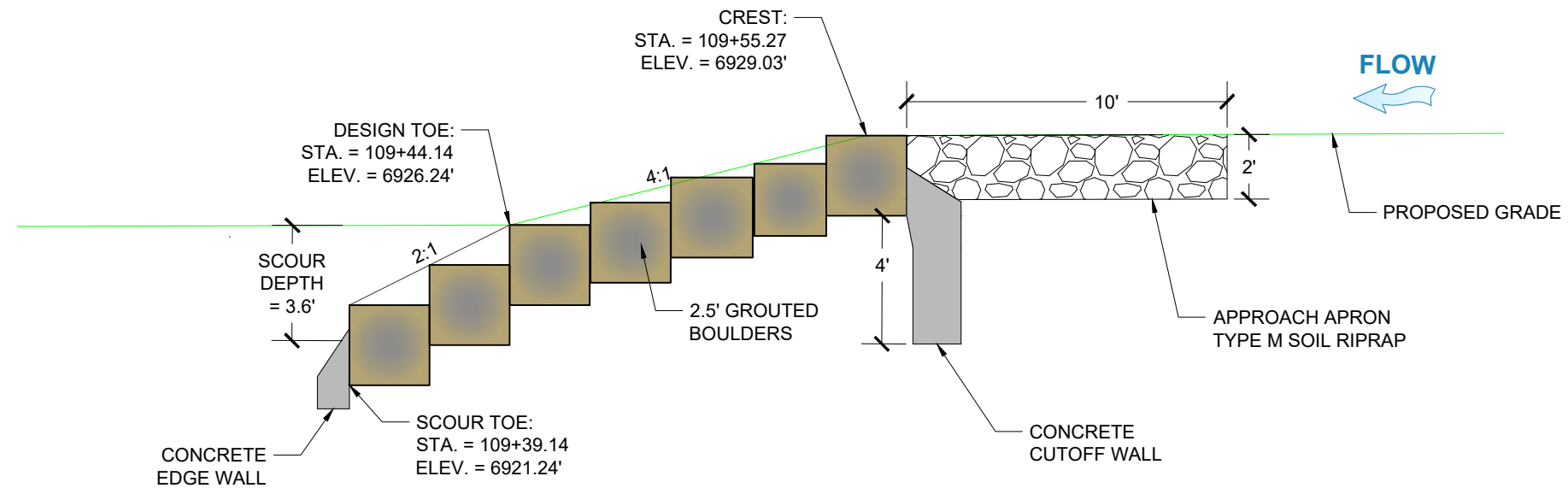
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #6 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No.
CHECKED BY: AJS	VERT. 1" = 5'	SHEET 27 OF 38	DT14



Know what's below.
Call before you dig.



PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #7 (NON-BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach			
X-886-PR-GRADE			
X-886-MD022x34			
Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:47 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



PREPARED BY:
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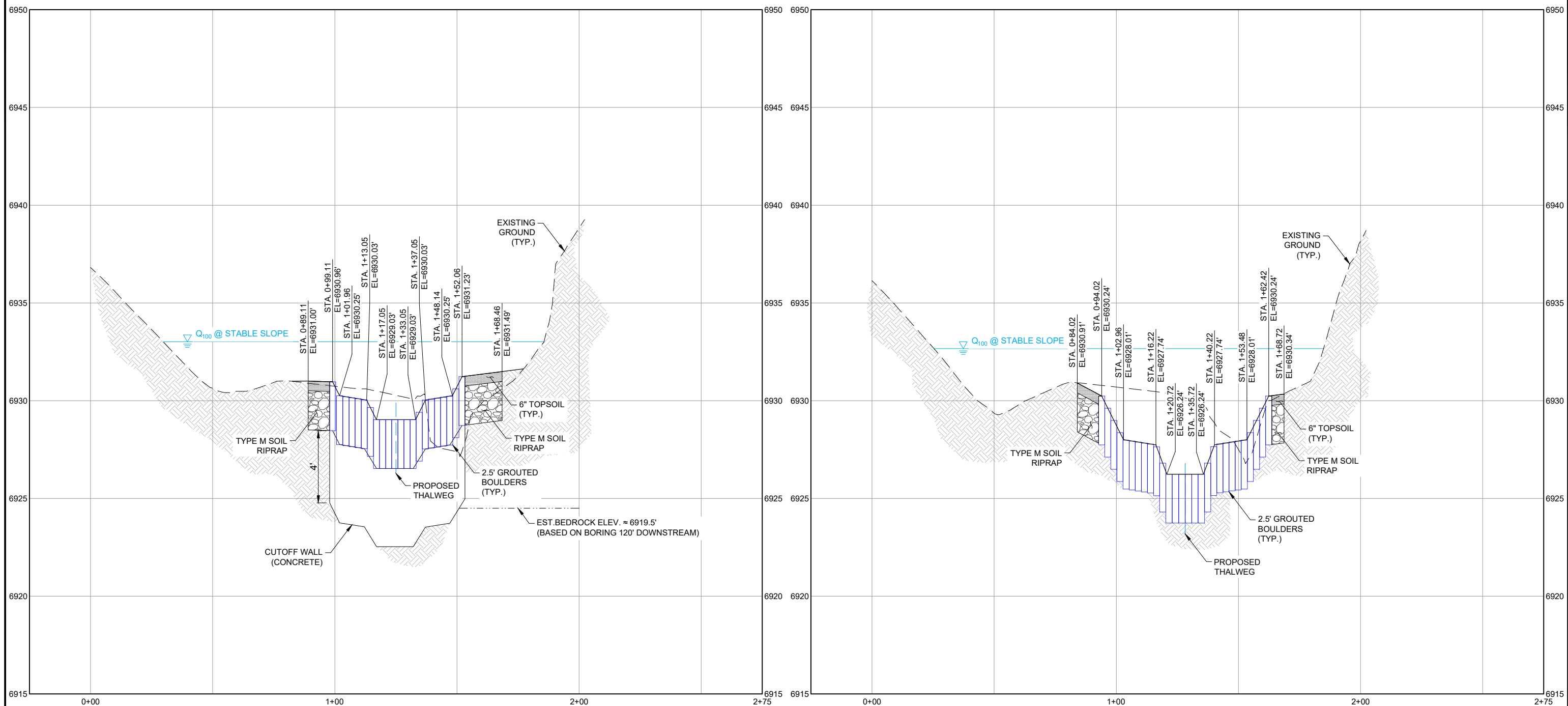
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #7 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
CHECKED BY: AJS	VERT. N/A	SHEET 28 OF 38	DT15



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)

CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #7 (NON-BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:48 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



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Excellence by Design

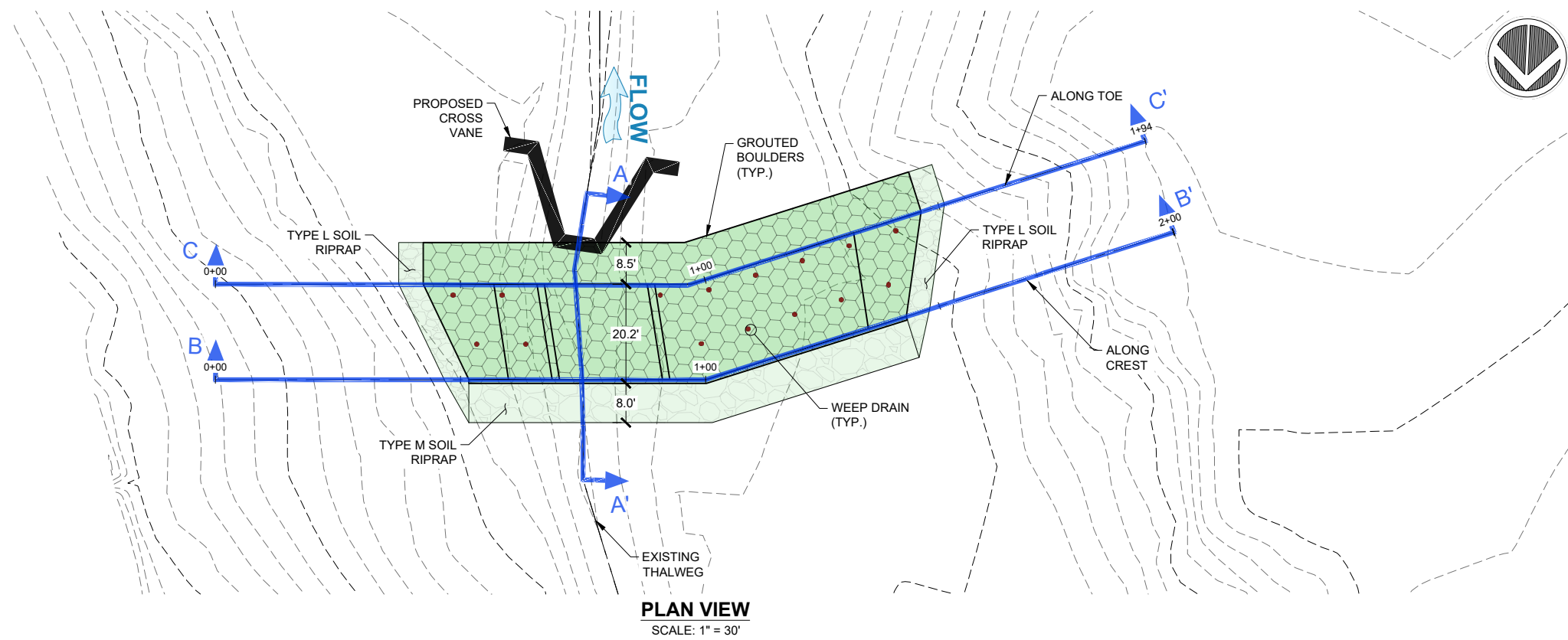
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MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

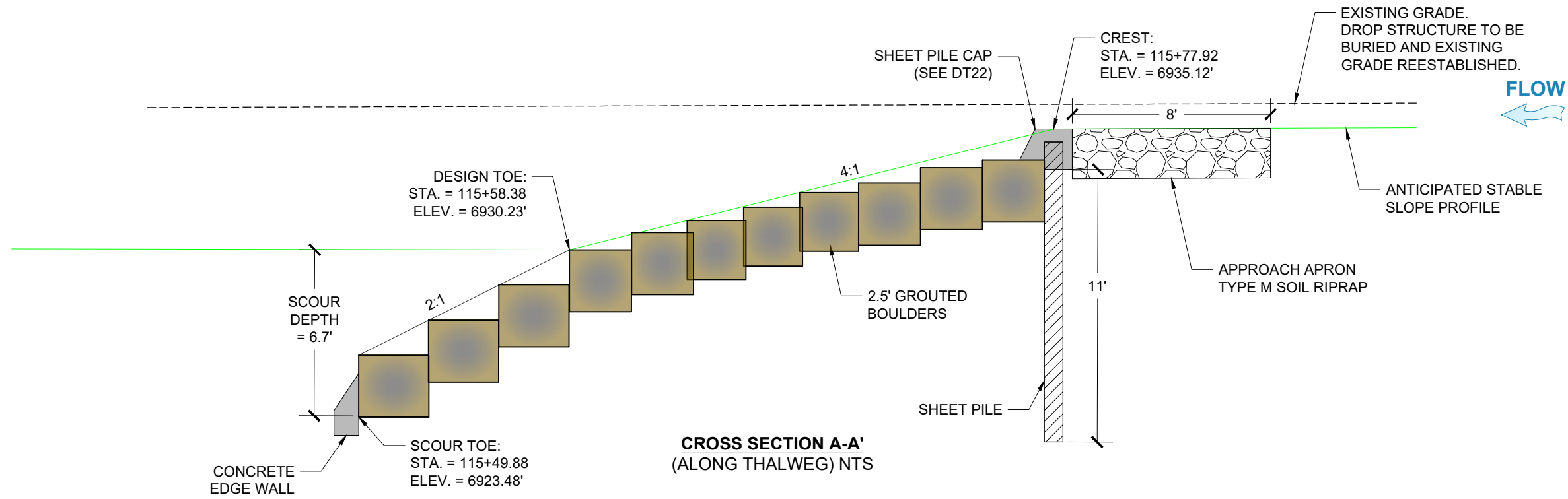
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #7 DETAILS			
DESIGNED BY:	JAB	SCALE	DATE ISSUED:
DRAWN BY:	RAF	HORIZ 1" = 40'	MAY 2020
CHECKED BY:	AJS	VERT 1" = 5'	29 OF 38
			DRAWING No. DT16



Know what's below.
Call before you dig.



PLAN VIEW
SCALE: 1" = 30'



CROSS SECTION A-A'
(ALONG THALWEG) NTS

DROP STRUCTURE #8 (BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach			
X-886-PR-GRADE			
X-886-MD022x34			
Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawings\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:48 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



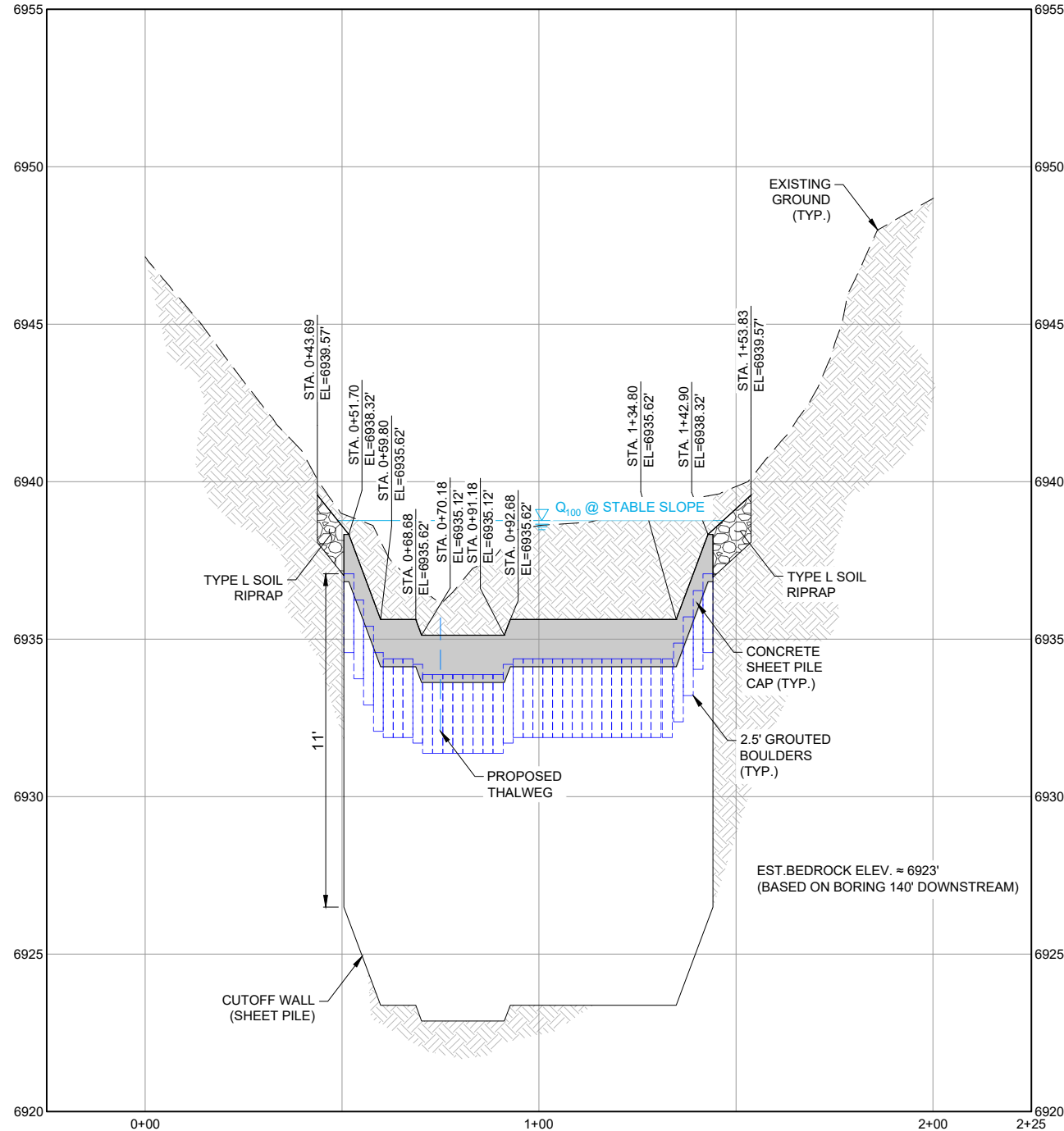
PREPARED BY:
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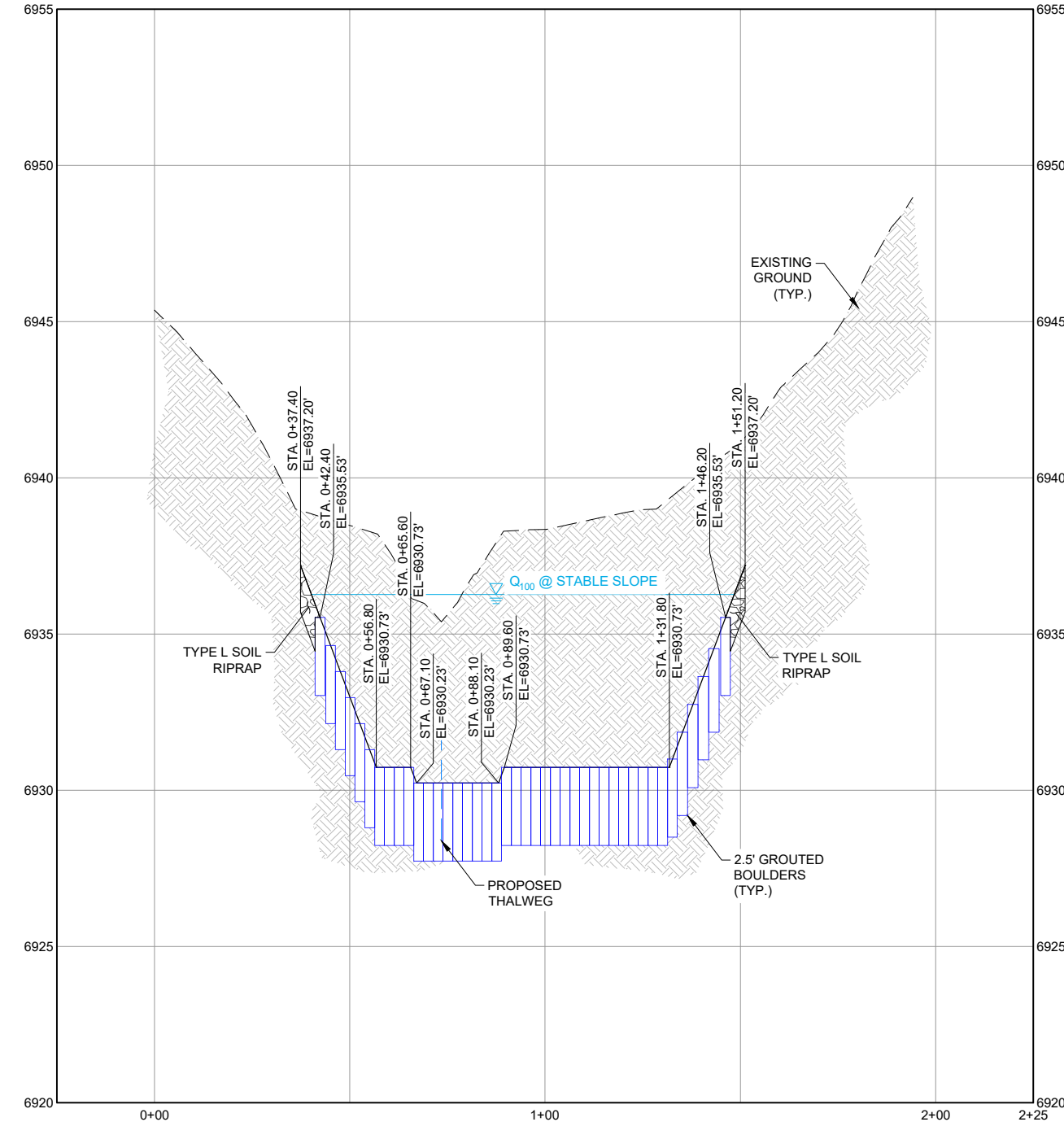
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #8 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. N/A	SHEET 30 OF 38	DT17
CHECKED BY: AJS			



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)



CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #8 (BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34 Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
REVISIONS			
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:49 PM			
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DATE _____
CONDITIONS:



PREPARED BY:

SEAL

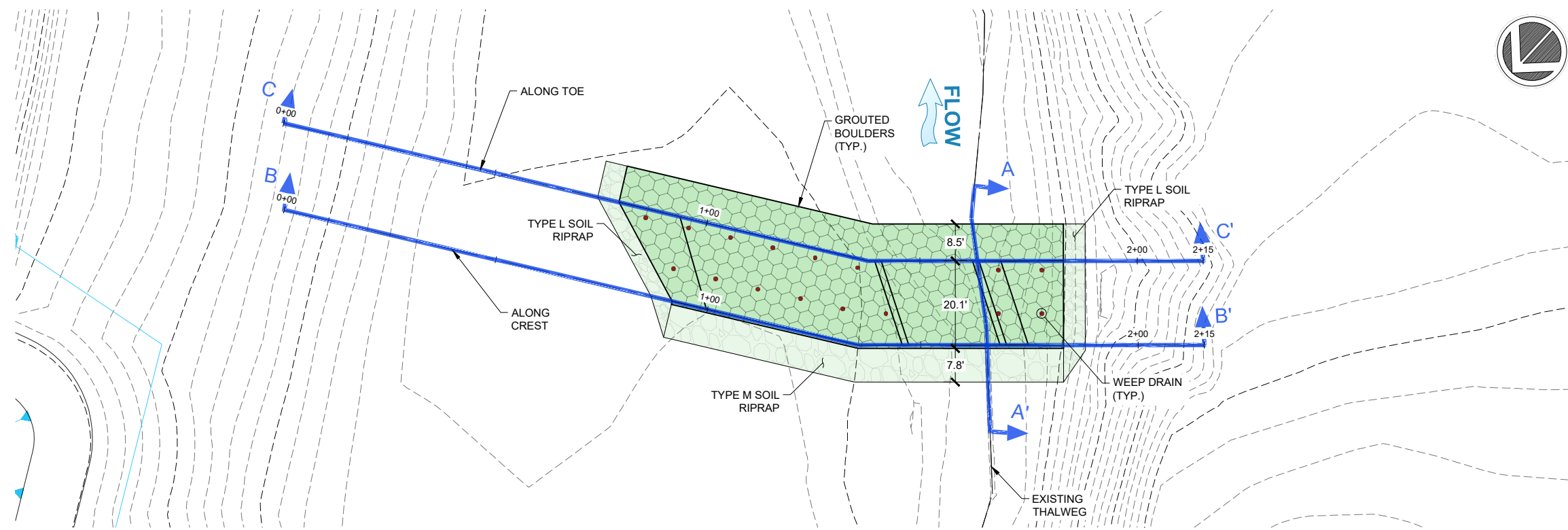
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FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

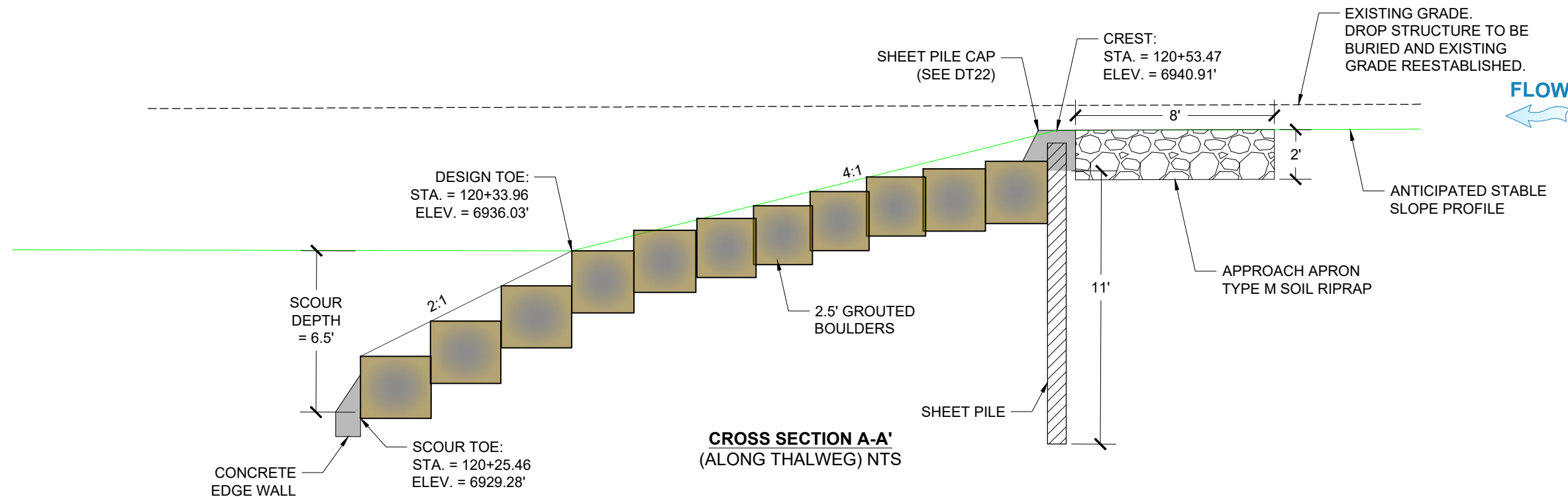
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #8 DETAILS			
DESIGNED BY:	JAB	SCALE	DATE ISSUED:
DRAWN BY:	RAF	HORIZ 1" = 40'	MAY 2020
CHECKED BY:	AJS	VERT 1" = 5'	31 OF 38
			DRAWING No. DT18



Know what's below.
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PLAN VIEW
SCALE: 1" = 30'



DROP STRUCTURE #9 (BURIED)

REFERENCE DRAWINGS			
Drop Modeling - Lower Reach			
X-886-PR-GRADE			
X-886-MD022x34			
Drop Modeling - Upper Reach			
No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:49 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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DATE _____
CONDITIONS:



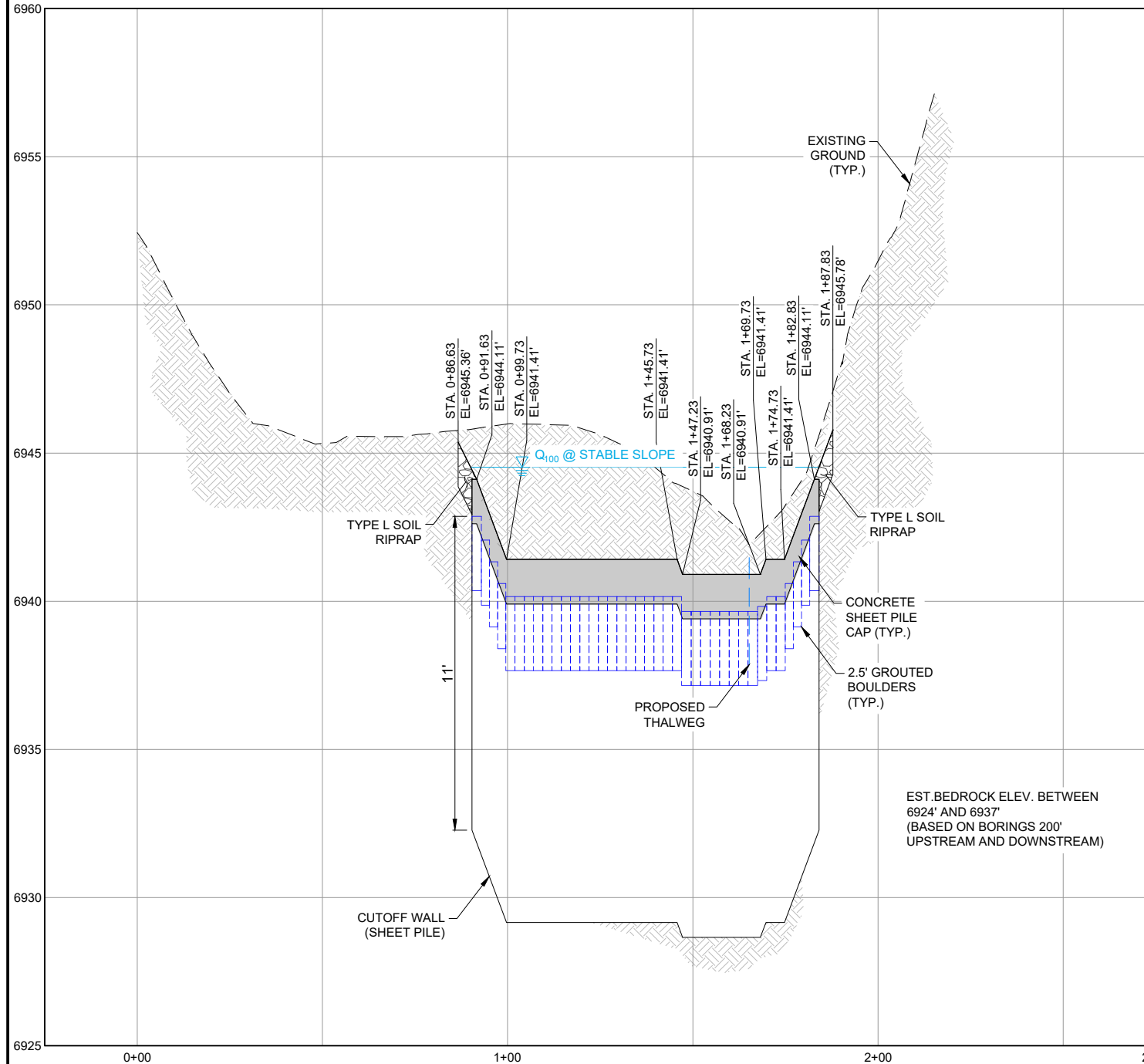
PREPARED BY:
Matrix
Excellence by Design

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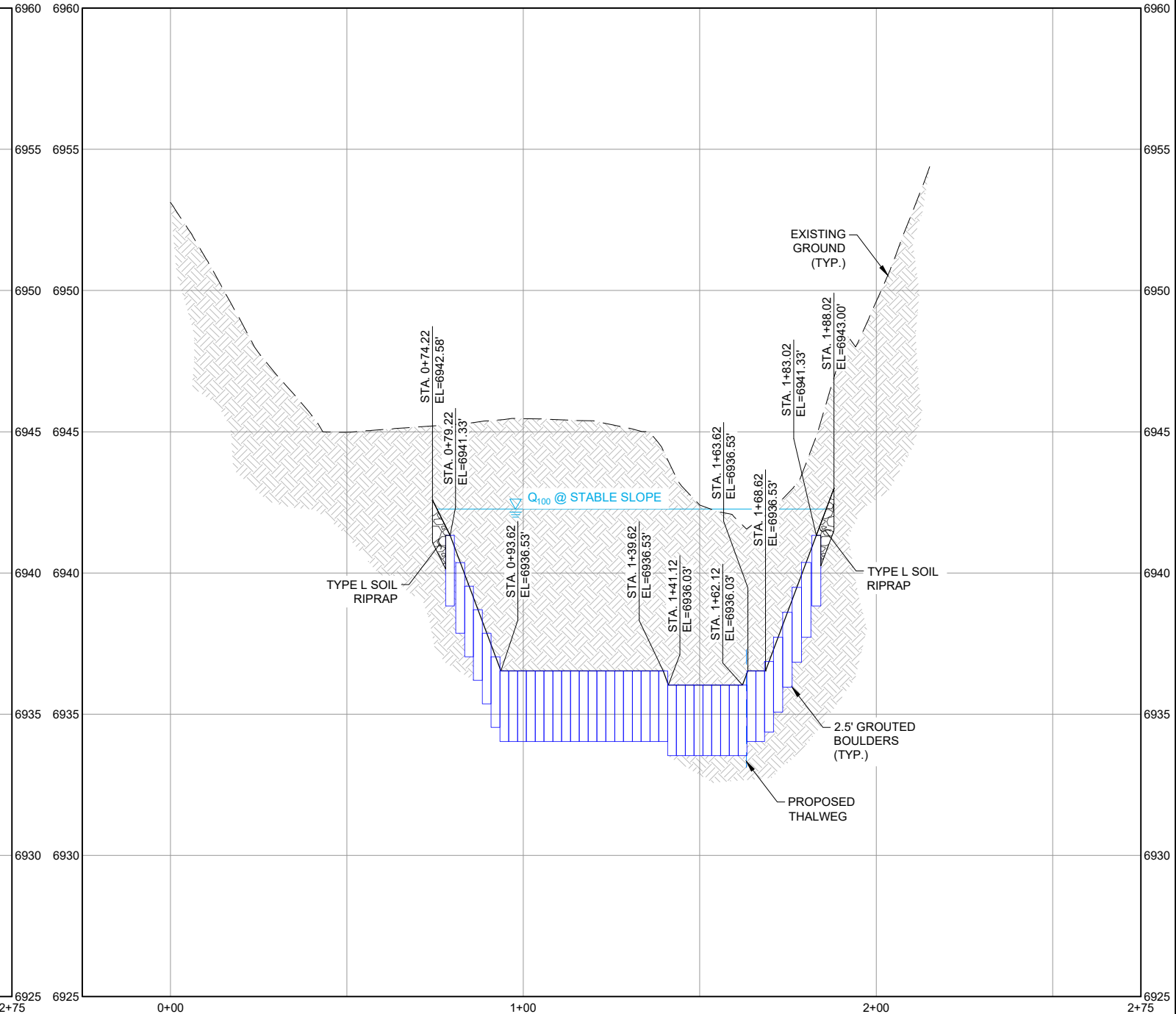
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #9 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 30'	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	VERT. N/A	SHEET 32 OF 38	DT19
CHECKED BY: AJS			



Know what's below.
Call before you dig.



CROSS SECTION B-B'
(ALONG CREST)



CROSS SECTION C-C'
(ALONG TOE)

DROP STRUCTURE #9 (BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:50 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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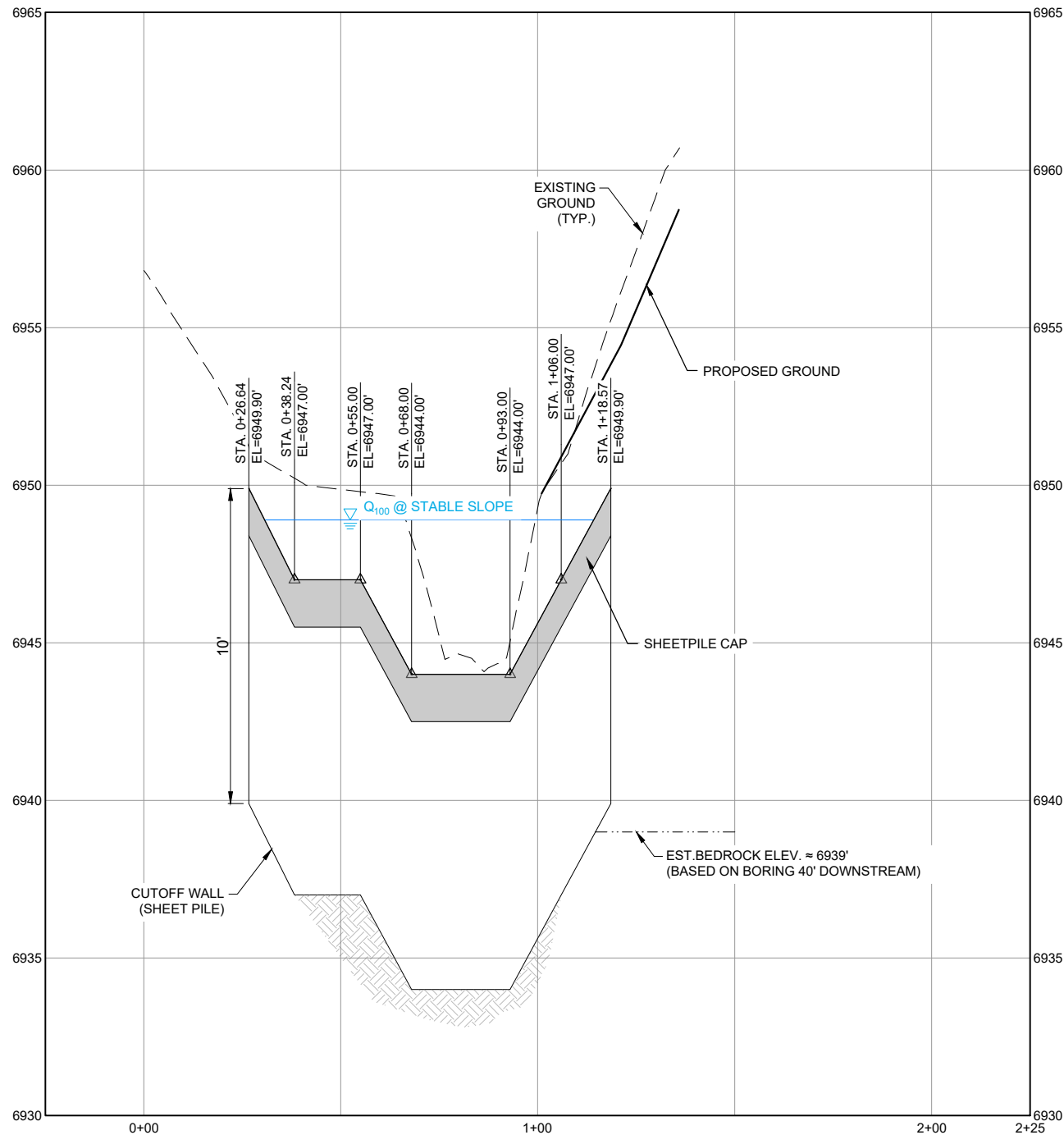
FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
DROP STRUCTURE #9 DETAILS			
DESIGNED BY: JAB	SCALE: HORIZ 1" = 40'	DATE ISSUED: MAY 2020	DRAWING No. DT20
CHECKED BY: AJS	VERT. 1" = 5'	SHEET 33 OF 38	

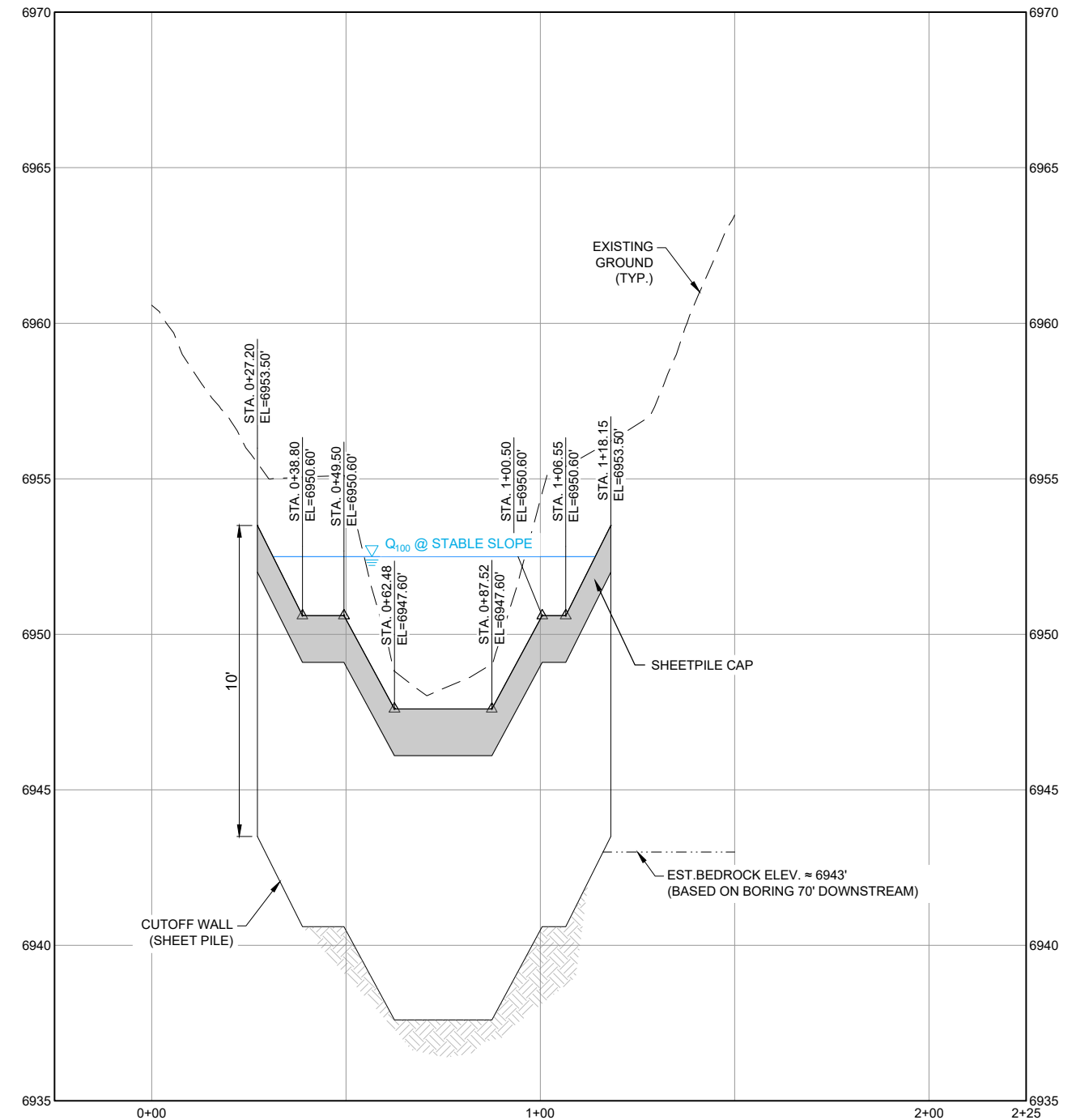


Know what's below.
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NOTE: REESTABLISH EXISTING GRADE AFTER INSTALLATION OF SHEETPILE, EXCEPT AT RIGHT BANK ON SHEET PILE #1, AS NOTED



SHEET PILE #1



SHEET PILE #2

SHEET PILE (BURIED)

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:50 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

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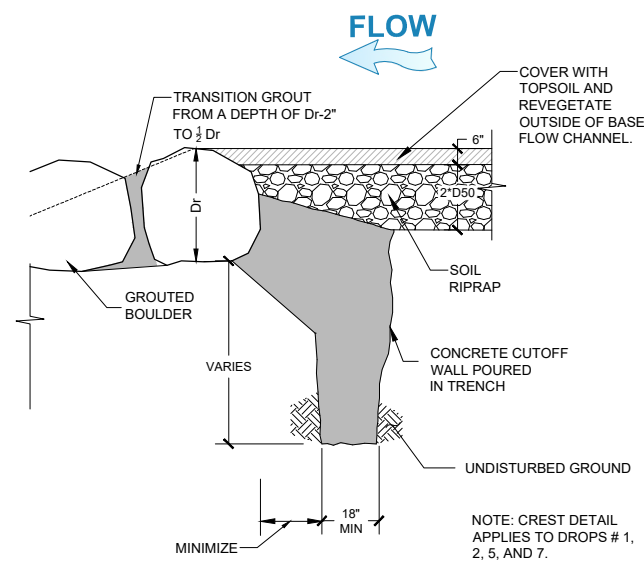
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PROJECT No. 19.886.017

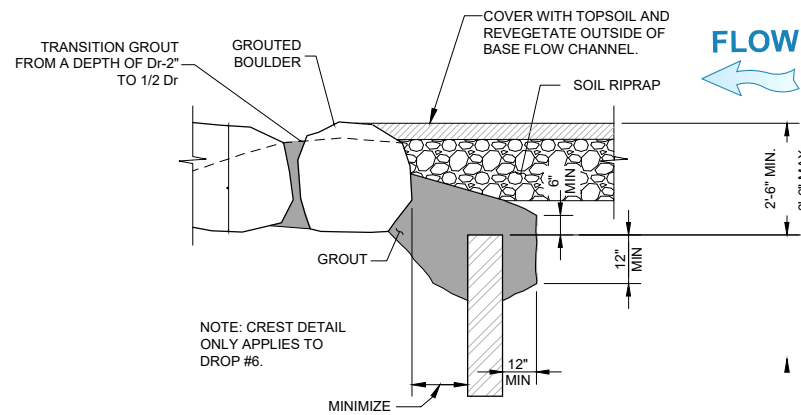
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
SHEET PILE DETAILS			
DESIGNED BY: JAB	SCALE: N/A	DATE ISSUED: MAY 2020	DRAWING No. DT21
CHECKED BY: AJS	HORIZ: N/A	SHEET: 34 OF 38	



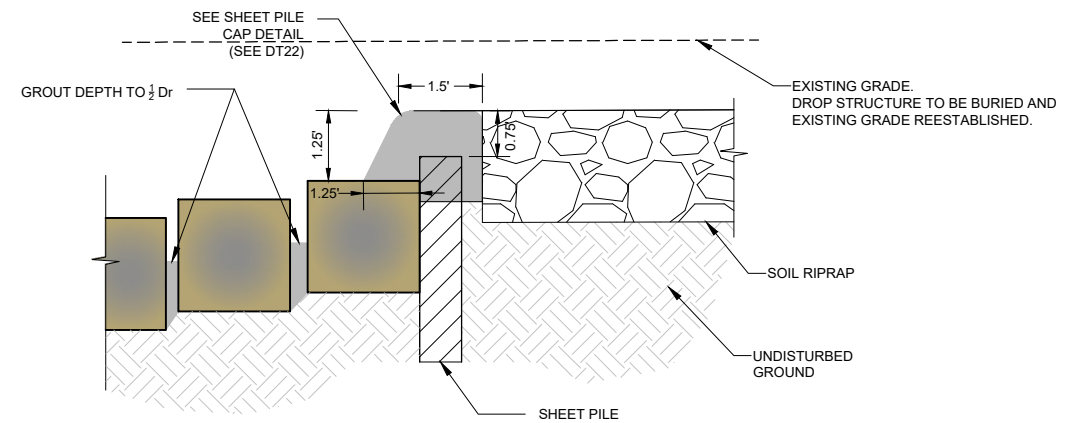
Know what's below.
Call before you dig.



CONCRETE CUTOFF WALL
NOT TO SCALE



SHEET PILE CUTOFF WALL
NOT TO SCALE

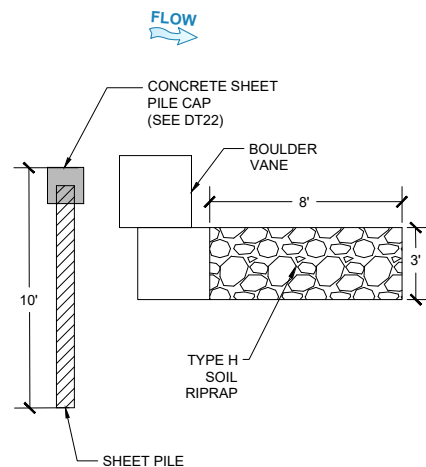
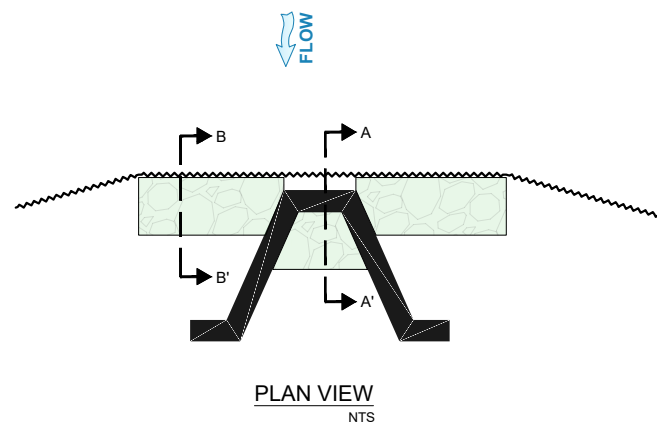


- NOTES:
1. TROWEL FINISH CAP TO CREATE SMOOTH CREST WITH ROUND TOP.
 2. WORK GROUT TO FILL ALL VOID SPACE BETWEEN SHEET PILE AND TOP BOULDER.
 3. SEE SHEET PILE CAP DETAIL FOR FURTHER DIMENSIONS AND INSTRUCTIONS ON REBAR.
 4. CREST DETAIL APPLIES TO DROPS # 3, 4, 8, AND 9.

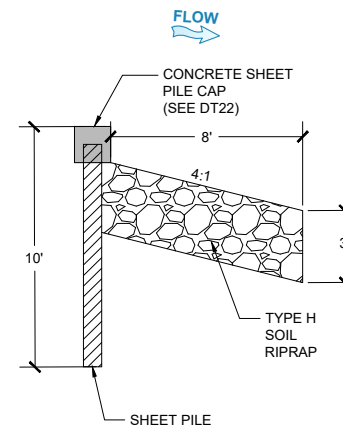
CREST WITH SHEET PILE CAP AND CUTOFF WALL
NOT TO SCALE

NOTE:
ALL SHEET PILE TO BE DRIVEN TO DESIGN DEPTH OR INTO BEDROCK, WHICHEVER COMES FIRST.

TYPICAL CREST AND CUTOFF WALL DETAILS
NOT TO SCALE



SECTION A-A'
NTS



SECTION B-B'
NTS

- NOTES:
1. CONSTRUCT VANES BEFORE PLACING RIPRAP.
 2. RIPRAP ON UPSTREAM SIDE OF VANE SHOULD BE PLACED BEHIND THE GEOTEXTILE FABRIC.
 3. REESTABLISH EXISTING GRADE AFTER CONSTRUCTION.

TYPICAL SHEET PILE RIPRAP APRON DETAILS
NOT TO SCALE

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION REVISIONS	BY
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022304 Drop Modeling - Upper Reach				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 4:51 PM				
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DATE _____
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PREPARED BY:
Matrix
Excellence by Design

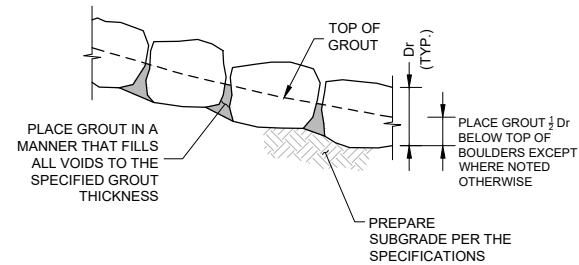
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MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

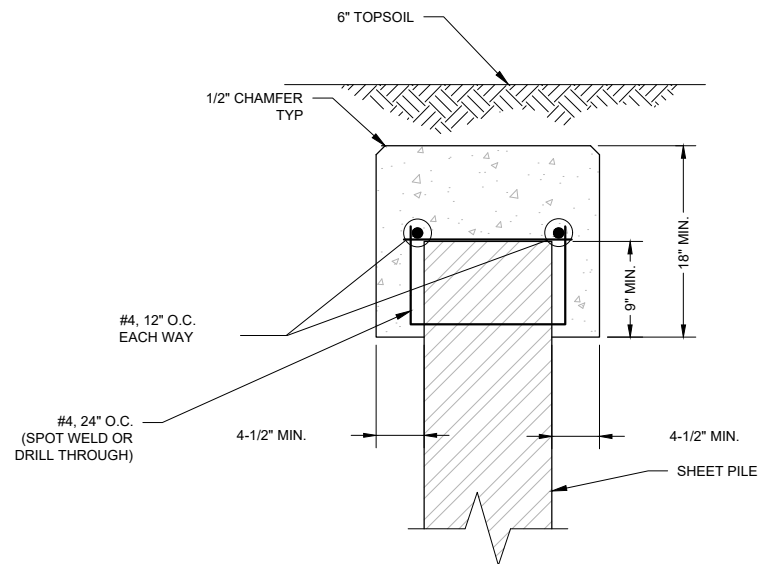
COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
TYP. GROUTED BOULDER DROP STRUCTURE & SHEET PILE RIPRAP APRON DETAILS			
DESIGNED BY: JAB	SCALE: N/A	DATE ISSUED: MAY 2020	DRAWING No.
DRAWN BY: RAF	HORIZ. N/A		
CHECKED BY: AJS	VERT. N/A	SHEET 35 OF 38	DT22



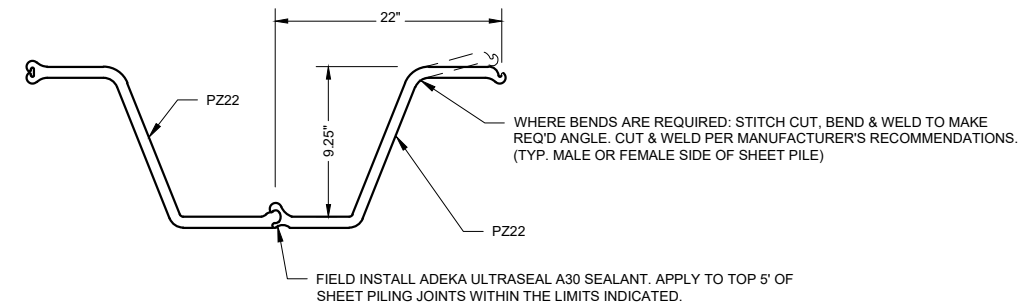
Know what's below.
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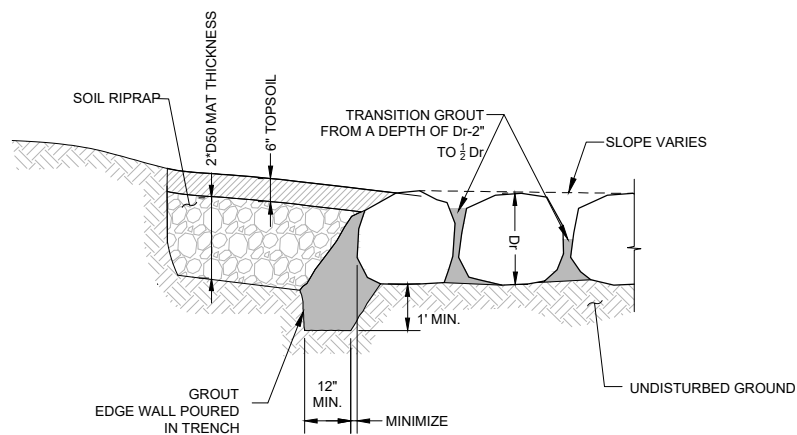
GRouted BOULDER PLACEMENT DETAIL
NOT TO SCALE



CONCRETE SHEET PILE CAP
NOT TO SCALE

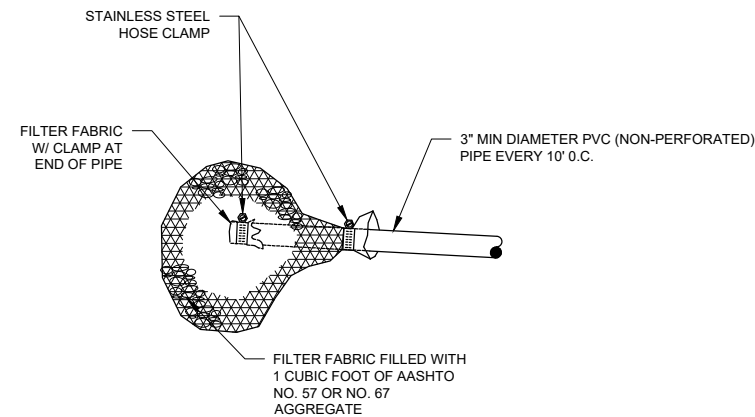


PZ22 SHEET PILE DETAIL
NOT TO SCALE

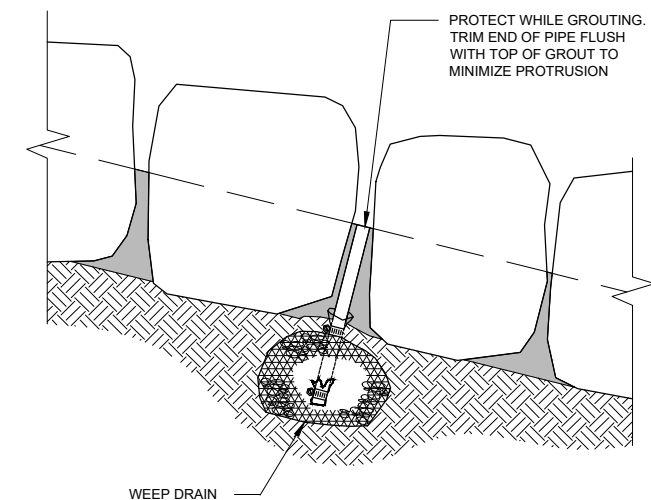


- NOTES:
1. EDGE WALL TO BE PLACED ON LEFT, RIGHT, AND DOWNSTREAM SIDE OF STRUCTURE. SEE DT21 FOR UPSTREAM CUTOFF WALL DETAILS.
 2. THE TOPSOIL DETAIL APPLIES TO ANY STRUCTURE EDGE THAT MATCHES FINISHED GRADE. WHERE THE STRUCTURE IS BURIED, THE RIPRAP MAT WILL BE 6\"/>

EDGE WALL DETAIL
NOT TO SCALE



WEEP DRAIN DETAILS
NOT TO SCALE



REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34				
Drop Modeling - Upper Reach				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:119.886.017 Sand Creek Stabilization at Forest Meadows P2(Dwg)Design Plans\886-DT01-26.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 4:51 PM				
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FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION				
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS				
TYPICAL GROUTED BOULDER DROP STRUCTURE DETAILS				
DESIGNED BY: JAB	SCALE: MAY 2020	DATE ISSUED: MAY 2020	DRAWING No. DT23	
DRAWN BY: RAF	HORIZ: N/A	SHEET: 36 OF 38		
CHECKED BY: AJS	VERT: N/A			



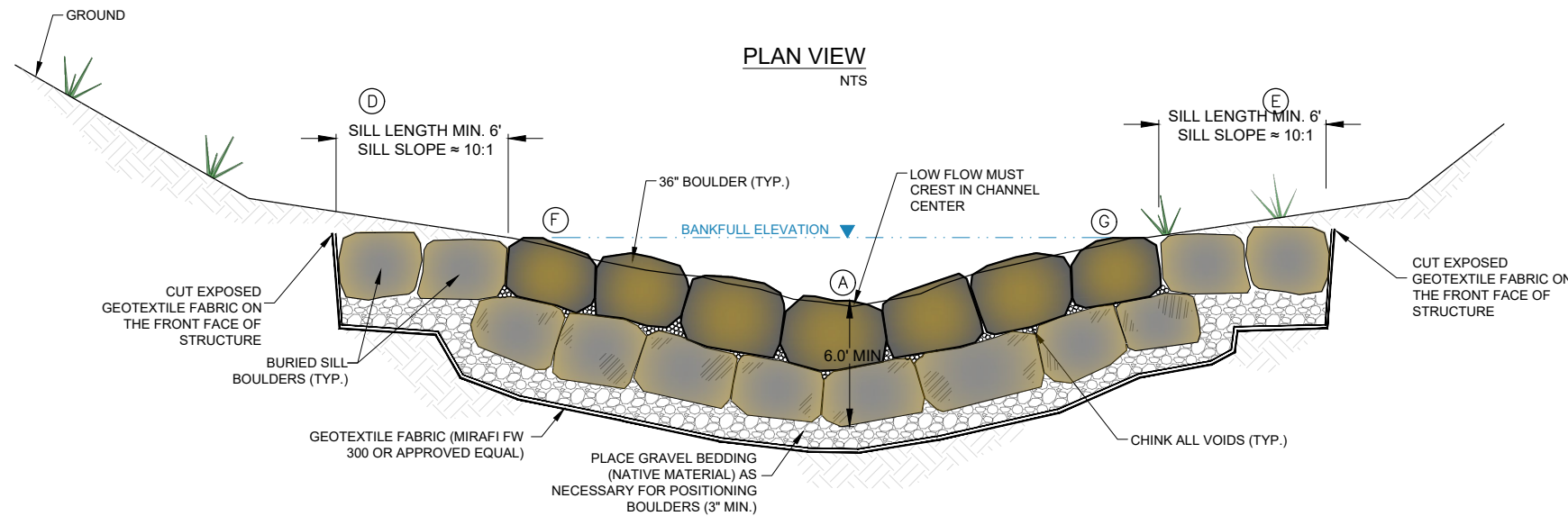
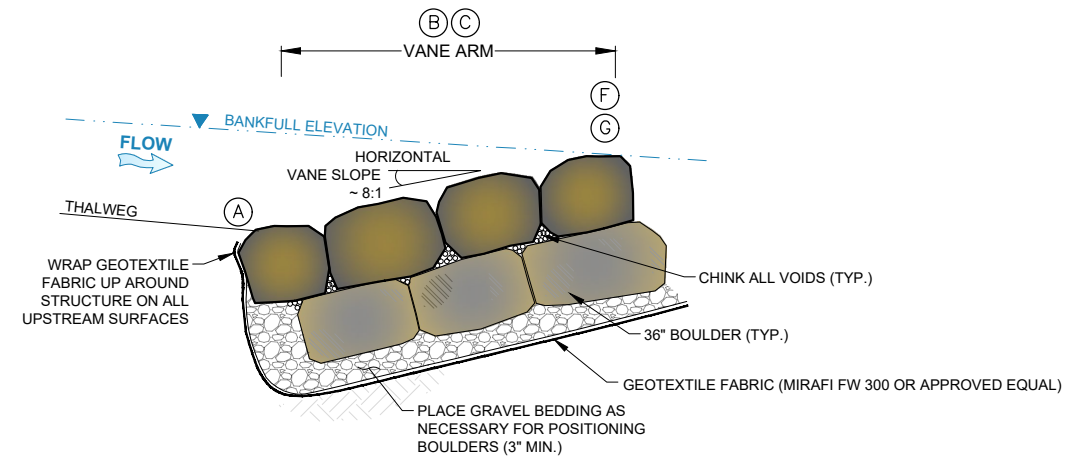
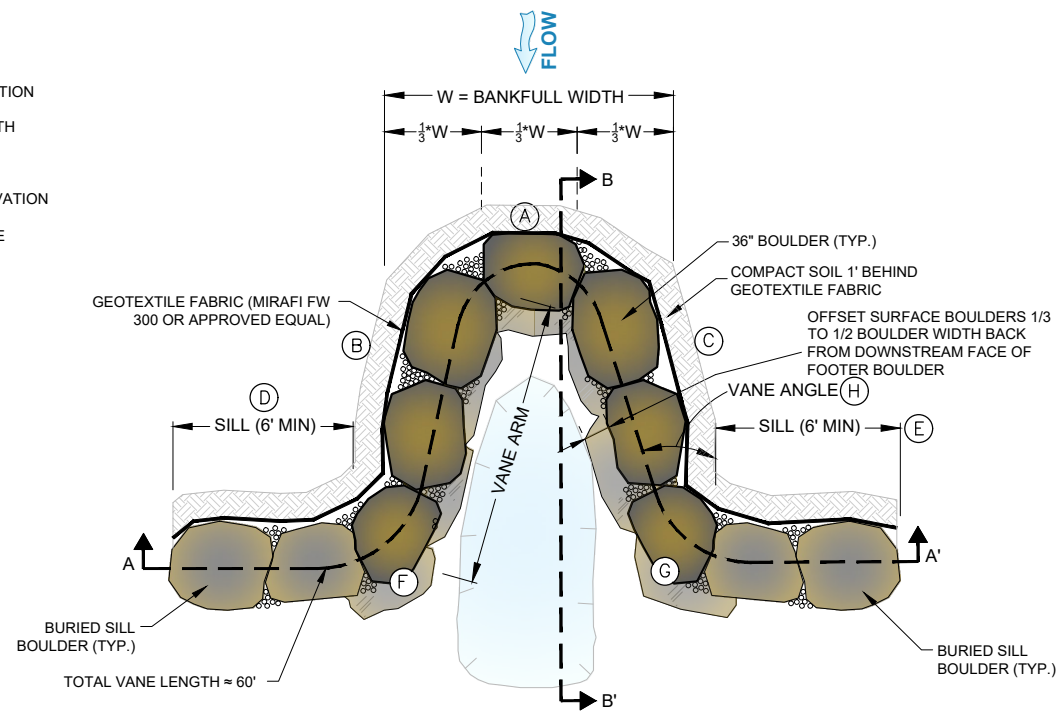
Know what's below.
Call before you dig.

NOTE:

- (A) DENOTE THALWEG ELEVATION
- (B) AND (C) DENOTE VANE ARM LENGTH
- (D) AND (E) DENOTE SILL LENGTH
- (F) AND (G) DENOTE BANK TIE-IN ELEVATION
- (H) DENOTE VANE ARM ANGLE

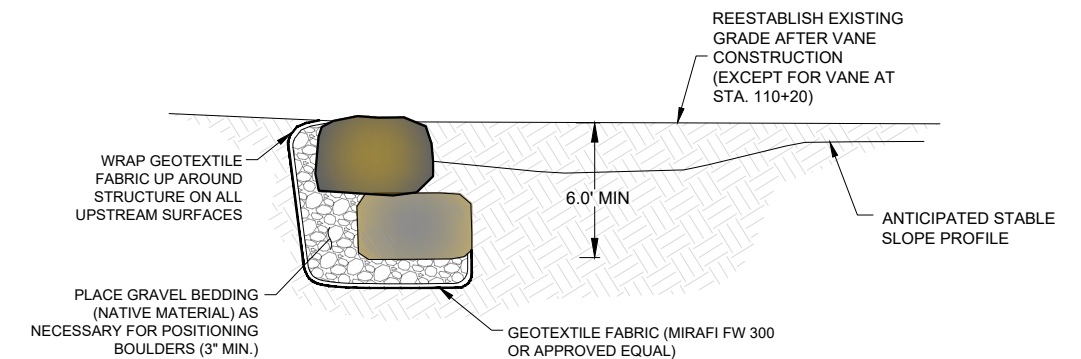
NOTES:

1. CROSS VANES TO BE PLACED TO FIT EXISTING BANKFULL CHANNEL.
2. BANKFULL TYPICAL WIDTH IS 24', THOUGH ACTUAL WIDTH MAY VARY. THE WIDTH WILL BE VERIFIED IN THE FIELD BY THE ENGINEER.
3. POINT "A" TO BE SET IN CENTER OF CHANNEL AT STATION AND ELEVATION SHOWN ON THE PROFILE SHEETS (PP03-PP04).
4. POINTS "F" AND "G" SHOULD BE LOCATED AT TOP OF BANK OF THE BANKFULL CHANNEL (TO BE VERIFIED IN THE FIELD BY THE ENGINEER).
5. THE ELEVATIONS OF "F" AND "G" SHOULD BE AT MINIMUM 0.6' HIGHER THAN THE ELEVATION AT POINT "A".
6. THE VANE ARM ANGLE ("H") SHOULD BE BETWEEN 20 AND 30 DEGREES.
7. AFTER VANE CONSTRUCTION, REESTABLISH EXISTING GRADE. BOULDERS ALONG CREST AND ARM SHOULD BE AT GRADE. BURY SILL BOULDERS WHERE EXISTING GRADE OFFERS SUFFICIENT COVER FOR REVEGETATION.
8. AS AN EXCEPTION TO THE ABOVE, THE VANE AT STATION 110+20 WILL BE INSTALLED WITH THE PROPOSED GRADING AND BANKFULL CHANNEL.
9. THERE SHOULD BE VERTICAL 6" MINIMUM BETWEEN BOTTOM OF FOOTER AND TOP OF HEADER BOULDERS IN ORDER TO PROVIDE ADEQUATE SCORE PROTECTION



CROSS VANE LONGITUDINAL PROFILE ALONG VANE
NTS

CROSS VANE SECTION A-A'
LOOKING UPSTREAM
NTS



CROSS VANE PROFILE B-B'
NTS

TYPICAL ROCK CROSS VANE DETAILS

NOT TO SCALE

No.	DATE	DESCRIPTION	BY
COMPUTER FILE MANAGEMENT			
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\Drawg\Design Plans\886-DT01-26.dwg			
CTB FILE: Matrix(black).ctb			
PLOT DATE: 5/21/2020 4:52 PM			
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.			

CITY OF COLORADO SPRINGS ONLY:
FILED IN ACCORDANCE WITH SECTION 7.7.906 OF THE CODE OF THE CITY OF COLORADO SPRINGS, 2001, AS AMENDED.

FOR CITY ENGINEER _____
DATE _____
CONDITIONS:



SEAL

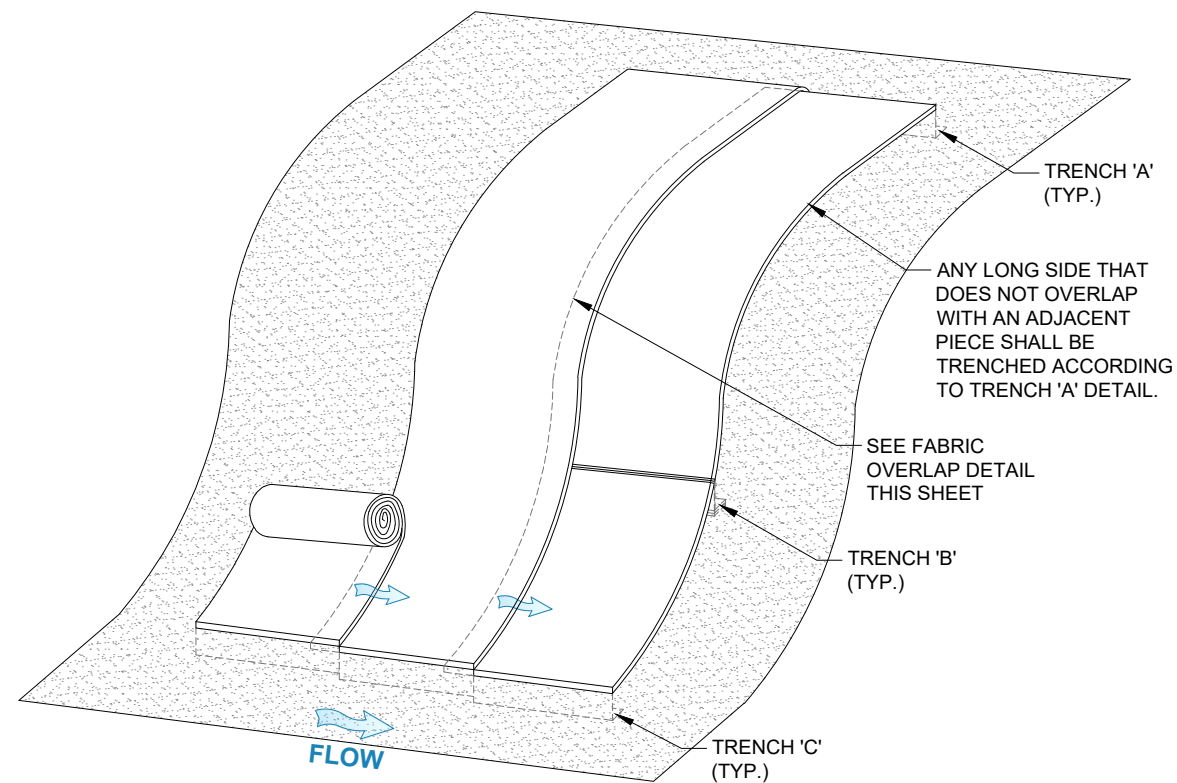
PRELIMINARY
THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND IS SUBJECT TO CHANGE

FOR AND ON BEHALF OF
MATRIX DESIGN GROUP, INC.
PROJECT No. 19.886.017

COLORADO LAND ACQUISITION			
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS			
TYPICAL GRADE CONTROL DETAILS ROCK CROSS VANE			
DESIGNED BY: JAB	SCALE: N/A	DATE ISSUED: MAY 2020	DRAWING No. DT24
CHECKED BY: AJS	HORIZ: N/A	SHEET: 37 OF 38	



Know what's below.
Call before you dig.



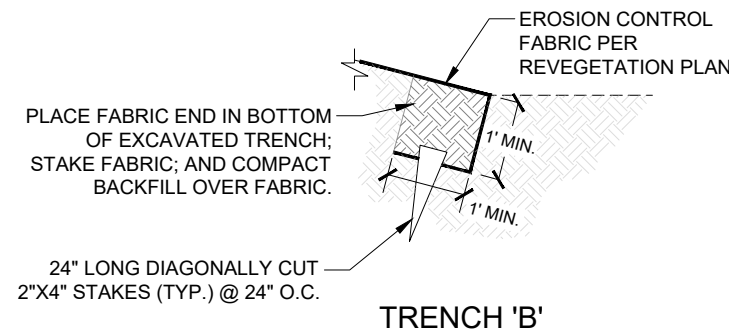
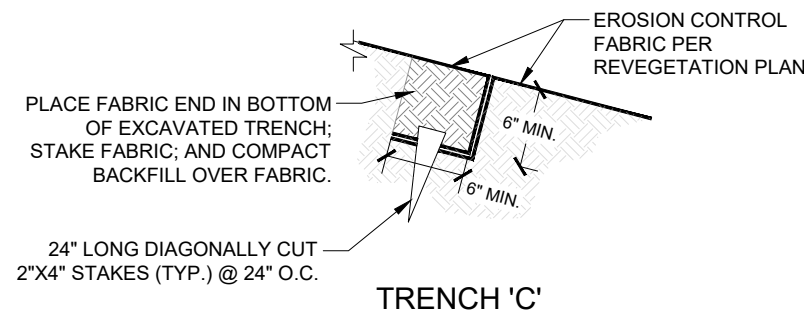
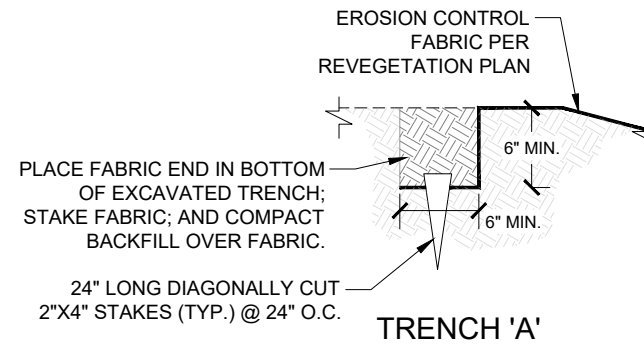
NOTE: STAKE @24" O.C. AND ALL SEAMS @18" O.C.

EROSION CONTROL FABRIC SLOPE INSTALLATION DETAIL

NTS

NOTES:

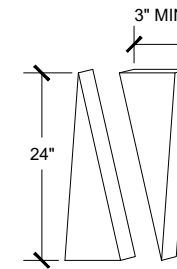
1. USE KOIRWRAP 1200 FROM TOE OF BASE FLOW UP TO TOP OF BANK OF BANKFULL CHANNEL, AS SHOWN ON DT01.
2. IN AREAS WHERE EXISTING GRADE IS TO BE REESTABLISHED, TOE OF BASE FLOW AND TOP OF BANKFULL WILL NEED TO BE IDENTIFIED BY ENGINEER.
3. USE NEDIA C400B COCONUT BLANKET IN REMAINING AREAS OUTSIDE OF BANKFULL CHANNEL.
4. FOR COCONUT BLANKET, USE 12" ECO-STAKES.
5. THE 24" STAKES FOR THE COIR FABRIC SHOULD BE DRIVEN TO LEAVE 2-3" ABOVE GROUND.



FABRIC TRENCH DETAILS

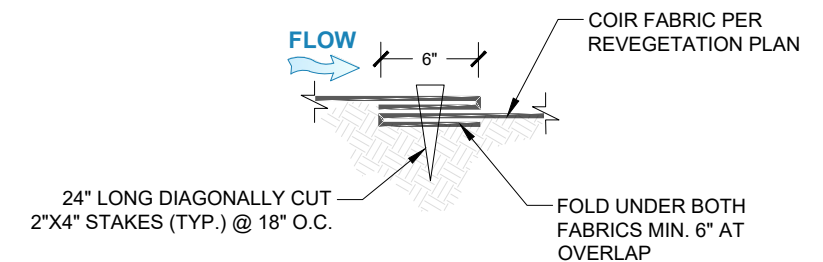
NTS

SAW 2"X4" LUMBER ON DIAGONAL



COIR FABRIC WOOD STAKE DETAIL

NTS



OVERLAP DETAIL

NTS

EROSION CONTROL FABRIC DETAILS

NOT TO SCALE

REFERENCE DRAWINGS	No.	DATE	DESCRIPTION	BY
Drop Modeling - Lower Reach X-886-PR-GRADE X-886-MD022x34				
Drop Modeling - Upper Reach				
COMPUTER FILE MANAGEMENT				
FILE NAME: S:\19.886.017 Sand Creek Stabilization at Forest Meadows P2\DWG\Design Plans\886-DT01-26.dwg				
CTB FILE: Matrix(black).ctb				
PLOT DATE: 5/21/2020 7:16 PM				
THIS DRAWING IS CURRENT AS OF PLOT DATE AND MAY BE SUBJECT TO CHANGE.				

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FOR CITY ENGINEER _____

DATE _____

CONDITIONS:



PREPARED BY:

Matrix
Excellence by Design

SEAL

PRELIMINARY
THIS DRAWING HAS NOT BEEN APPROVED BY GOVERNING AGENCIES AND IS SUBJECT TO CHANGE

FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. PROJECT No. 19.886.017

COLORADO LAND ACQUISITION				
SAND CREEK STABILIZATION AT ASPEN MEADOWS SUBDIVISION FILING NO. 1 - 100% DESIGN PLANS				
EROSION CONTROL FABRIC DETAILS				
DESIGNED BY: JAB	SCALE: _____	DATE ISSUED: MAY 2020	DRAWING No. DT25	
DRAWN BY: RAF	HORIZ. N/A	SHEET 38 OF 38		
CHECKED BY: AJS	VERT. N/A			

SAND CREEK DBPS IMPROVEMENTS

LEGEND

REACH IDENTIFIER

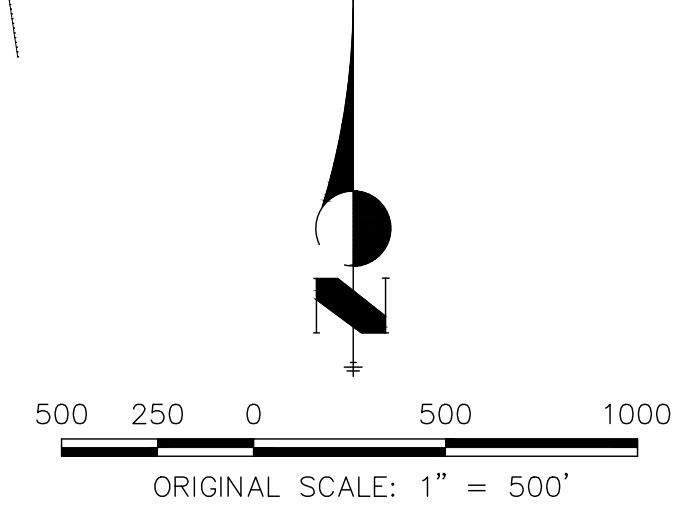
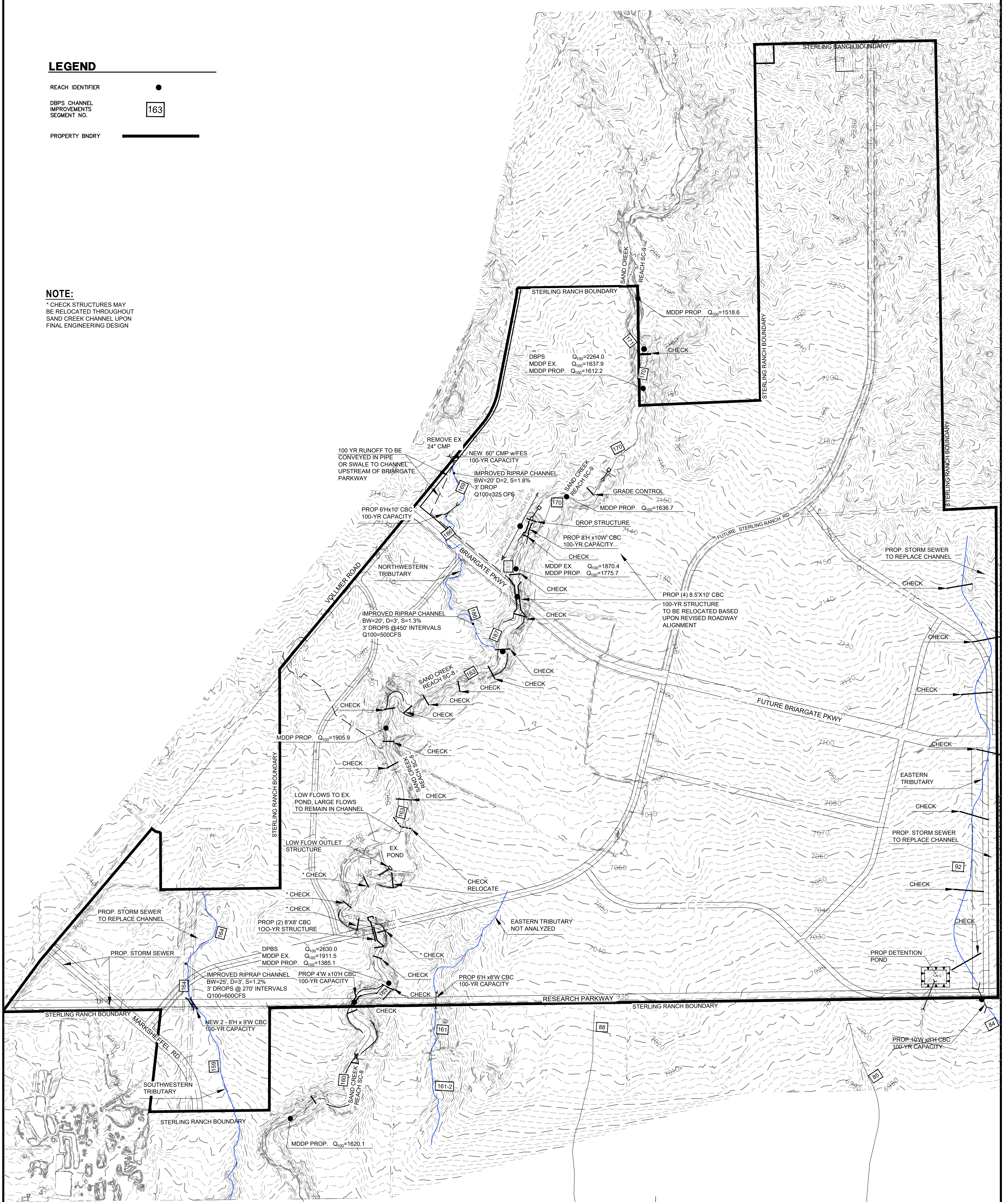
163

DBPS CHANNEL IMPROVEMENTS SEGMENT NO.

PROPERTY BNDRY

NOTE:

* CHECK STRUCTURES MAY BE RELOCATED THROUGHOUT SAND CREEK CHANNEL UPON FINAL ENGINEERING DESIGN



DBPS MAP OVERLAY
STERLING RANCH
JOB NO. 25188.00
1-08-2021
SHEET 1 OF 1

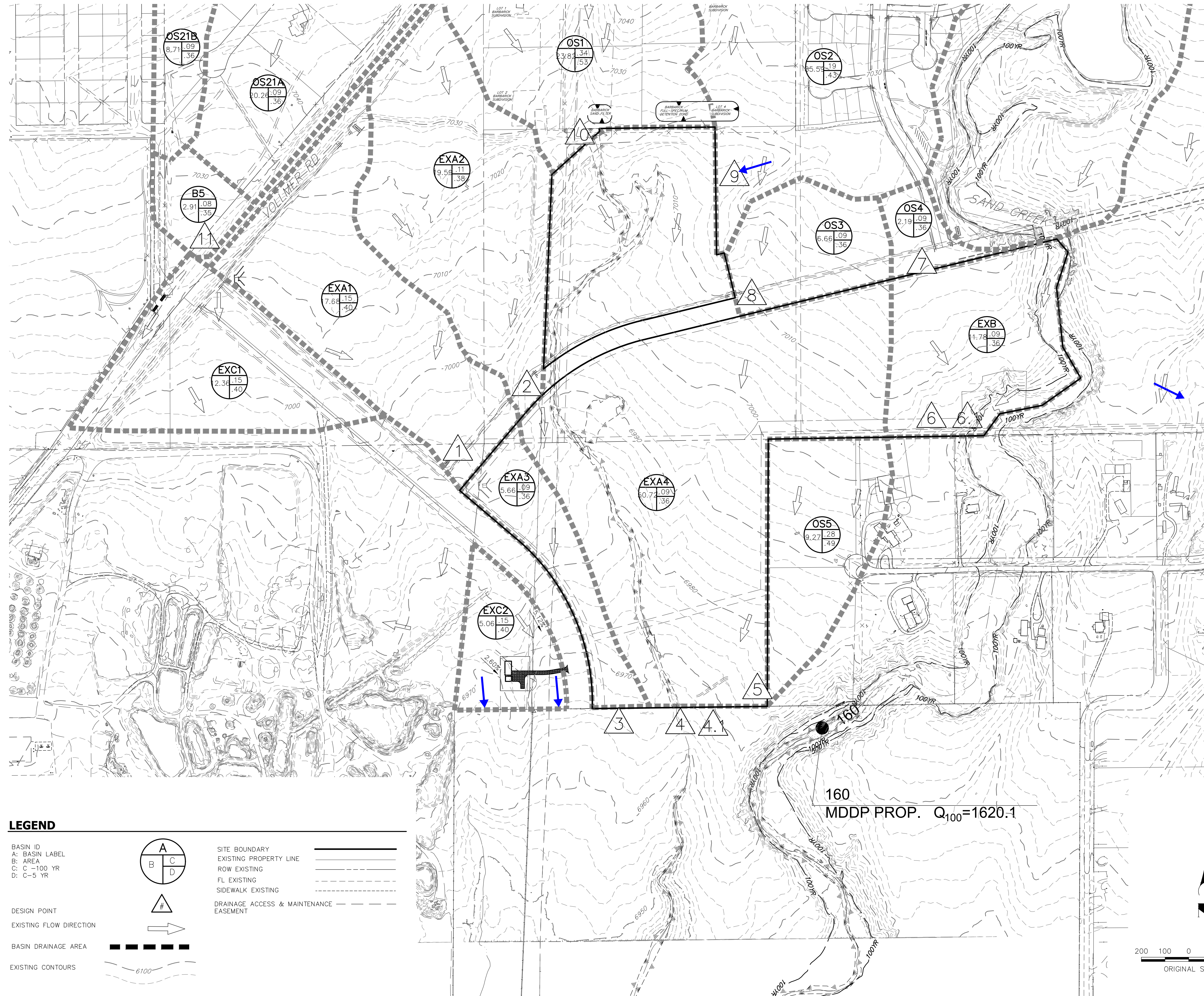
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X:\25188\000\25188\000\Drawings\Cleaned_Digital\2020-12-29\DBPS Overlay.dwg, 24x36 Plot Format, 1/8/2021 12:41:32 PM, FC

APPENDIX E
DRAINAGE MAPS & PLANS

STERLING RANCH EXISTING DRAINAGE MAP

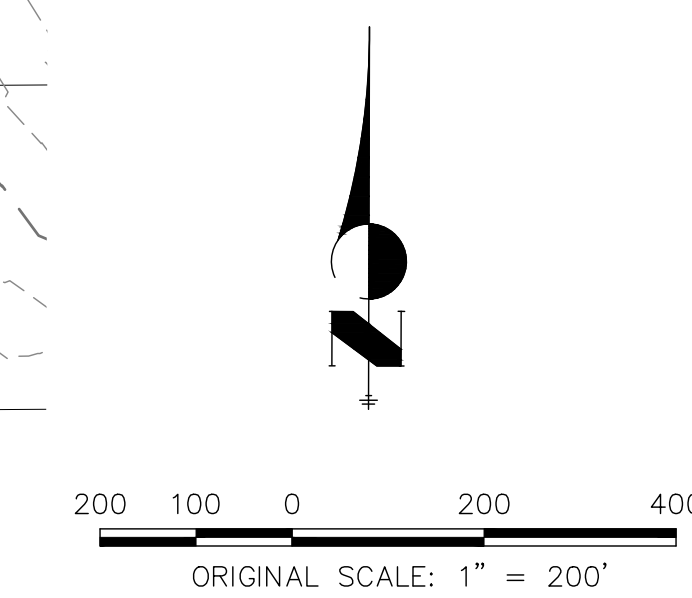


DESIGN POINT		
DP	Q5	Q100
1	7.2	12.1
2	5.4	9.0
3	1.4	2.3
4	10.6	17.8
5	7.5	23.4
6	3.0	5.0
7	0.5	0.9
8	1.8	3.1
9	37.3	62.6
10	23.9	40.1
4.1	45.6	76.5
6.1	3.0	5.1
11	11.8	19.9

BASIN SUMMARY TABLE							
Tributary Sub-basin	Area (acres)	Percent Impervious	C _s	C ₁₀₀	t _c (min)	Q _s (cfs)	Q ₁₀₀ (cfs)
EXA1	17.68	9%	0.15	0.40	25.4	7.2	12.1
EXA2	19.59	5%	0.11	0.38	31.5	5.4	9.0
EXA3	5.66	2%	0.09	0.36	26.4	1.4	2.3
EXA4	50.72	2%	0.09	0.36	33.2	10.6	17.8
EXC1	12.36	2%	0.09	0.36	22.0	3.3	5.5
EXC2	5.06	2%	0.09	0.36	20.6	1.4	2.3
EXB	11.78	2%	0.09	0.36	23.8	3.0	5.0
OS1	23.82	45%	0.34	0.53	22.4	23.9	40.1
OS2	85.59	18%	0.19	0.43	34.1	37.3	62.6
OS3	6.66	2%	0.09	0.36	20.3	1.8	3.1
OS4	2.19	2%	0.09	0.36	26.6	0.5	0.9
OS5	9.27	9%	0.28	0.49	22.8	7.5	23.4
B5	2.91	26%	0.79	1.19	5.0	11.8	19.9

LEGEND

- BASIN ID
 - A: BASIN LABEL
 - B: AREA
 - C: C -100 YR
 - D: C -5 YR
-
- DESIGN POINT
 - EXISTING FLOW DIRECTION
 - BASIN DRAINAGE AREA
 - EXISTING CONTOURS
-
-
-
-
- SITE BOUNDARY
 - EXISTING PROPERTY LINE
 - ROW EXISTING
 - FL EXISTING
 - SIDEWALK EXISTING
 - DRAINAGE ACCESS & MAINTENANCE EASEMENT
-
-
-
-
-
-



STERLING RANCH FILING 2
EXISTING DRAINAGE MAP
JOB NO. 25188.00
1/15/21
SHEET 1 OF 1



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DESIGN POINT	Q5		Q100	
	Total	Total	Total	Total
1	4.4	9.4		
2	1.9	3.9		
3	11.1	24.7		
4	3.7	7.4		
5	4.1	19.6		
6	3.3	6.7		
6A	2.2	4.1		
7	27.5	60.6		
8	3.0	12.5		
9	1.9	4.8		
10	9.2	17.3		
11	9.5	19.9		
12	1.9	9.5		
13	15.7	34.6		
14	16.0	37.9		
15	5.4	11.7		
16	4.4	9.6		
17	1.4	4.7		
18	4.3	14.0		
19	38.8	85.4		
20	7.1	13.4		
21	7.4	15.2		
22	2.7	15.4		
23	8.8	15.8		
24	11.5	20.6		
25	49.4	310.0		
26	4.2	21.9		
27	8.3	14.4		
28	8.4	16.7		
29	3.1	16.3		
30	0.9	6.4		
31	2.0	15.0		
32	1.4	10.0		
1.0	6.0	10.3		
1.1	12.6	19.7		
1.2	17.6	28.2		
1.3	25.9	46.9		
1.3A	5.0	8.7		
1.4	52.5	105.9		
1.5	55.1	103.9		
1.6	56.4	107.7		
1.7	17.3	25.3		
1.8	68.8	125.0		
2.0	23.2	74.5		
2.1	38.1	106.6		
2.2	56.9	138.7		
2.3	9.6	17.2		
2.4	63.7	151.9		
2.5	96.6	250.7		
2.6	97.8	250.4		
2.7	162.0	336.8		
2.8	189.8	424.4		
2.9	14.2	22.5		
3.0	189.8	424.4		
3.1	14.2	22.5		
3.2	187.5	428.2		
4.0	18.4	26.1		
4.1	56.2	264.7		
4.2	16.0	31.0		
4.3	49.9	293.1		
4.4	3.1	3.1		
4.5	51.2	51.2		
4.6	56.7	245.8		
4.7	58.5	248.6		
4.8	59.9	320.3		
OS2	13.8	39.1		
OS3	17.6	48.9		
OS4	2.6	8.5		

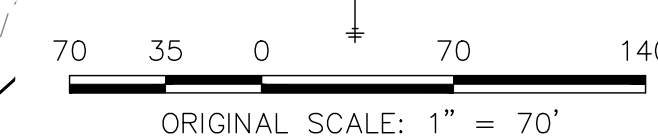
BASIN SUMMARY TABLE									
Tributary	Area	Percent	C _s	C ₁₀₀	t _c	Q ₅	Q ₁₀₀		
Sub-basin	(acres)	Impervious			(min)	(cfs)	(cfs)		
A1	2.06	66%	0.51	0.65	9.7	4.4	9.4		
A2	0.82	69%	0.53	0.66	9.1	1.9	3.9		
A3	6.76	60%	0.47	0.62	15.0	11.1	24.7		
A4	1.51	77%	0.60	0.71	10.2	3.7	7.4		
A5	1.70	76%	0.59	0.70	9.9	4.1	8.3		
A6	1.37	75%	0.58	0.70	10.0	3.3	6.6		
A6A	0.53	95%	0.81	0.88	5.0	2.2	4.1		
A7	19.00	65%	0.45	0.59	18.3	27.5	60.6		
A8	1.48	63%	0.56	0.70	13.9	3.0	6.3		
A9	0.61	79%	0.73	0.83	8.7	1.9	3.7		
A10	2.61	86%	0.79	0.88	7.9	9.2	17.3		
A11	2.89	83%	0.76	0.86	8.7	9.5	18.1		
A12	3.87	8%	0.13	0.38	11.9	1.9	9.5		
A13	9.65	65%	0.45	0.59	14.0	15.7	34.6		
A14	11.76	55%	0.39	0.55	15.3	16.0	37.9		
A15	2.91	54%	0.52	0.68	14.9	5.4	11.7		
A16	2.34	56%	0.54	0.69	14.7	4.4	9.6		
A17	1.76	24%	0.21	0.44	13.7	1.4	4.7		
A18	5.27	21%	0.24	0.47	16.4	4.3	14.0		
A19	31.85	67%	0.45	0.59	25.8	38.8	85.4		
A20	1.83	89%	0.81	0.89	8.0	6.6	12.2		
A21	1.93	90%	0.82	0.90	8.7	6.8	12.6		
A22	8.68	5%	0.11	0.37	23.3	2.7	15.4		
B1	2.98	100%	0.90	0.96	17.6	8.8	15.8		
B2	3.89	100%	0.90	0.96	17.6	11.5	20.6		
B3	2.05	100%	0.90	0.96	9.4	7.8	14.0		
B4	1.94	100%	0.90	0.96	9.4	7.4	13.2		
B5	2.91	5%	0.08	0.35	13.1	0.9	6.4		
C1	8.01	95%	0.81	0.88	9.9	2.0	15.0		
C2	5.06	95%	0.81	0.88	7.9	1.4	10.0		
OS20	308.00	9%	0.13	0.40	68.9	49.4	310.0		
OS21A	20.26	12%	0.13	0.40	53.5	4.2	21.9		
OS21B	8.71	12%	0.13	0.40	24.5	3.1	16.3		
OS2	17.00	70%	0.49	0.62	36.0	13.8	39.1		
OS3	28.70	70%	0.49	0.62	52.6	17.6	48.9		
OS4	5.08	15%	0.20	0.40	29.5	2.6	8.5		

- LEGEND:**
- PROPOSED STORM SEWER
 - 5000— PROPOSED MAJOR CONTOUR
 - PROPOSED MINOR CONTOUR
 - 5000— EXISTING MAJOR CONTOUR
 - EXISTING MINOR CONTOUR
 - ▬ DRAINAGE BASIN
 - ⊙ A
⊙ B
⊙ C
⊙ D
 - ⊙ A = BASIN DESIGNATION
 - ⊙ B = AREA IN ACRES
 - ⊙ C = 5-YR RUNOFF COEFFICIENT
 - ⊙ D = 100-YR RUNOFF COEFFICIENT
 - ⊙ DESIGN POINT
 - HP HIGH POINT
 - LP LOW POINT
 - DRAINAGE ARROW
 - ← EXISTING DRAINAGE ARROW
 - PROPOSED DRAINAGE SWALE

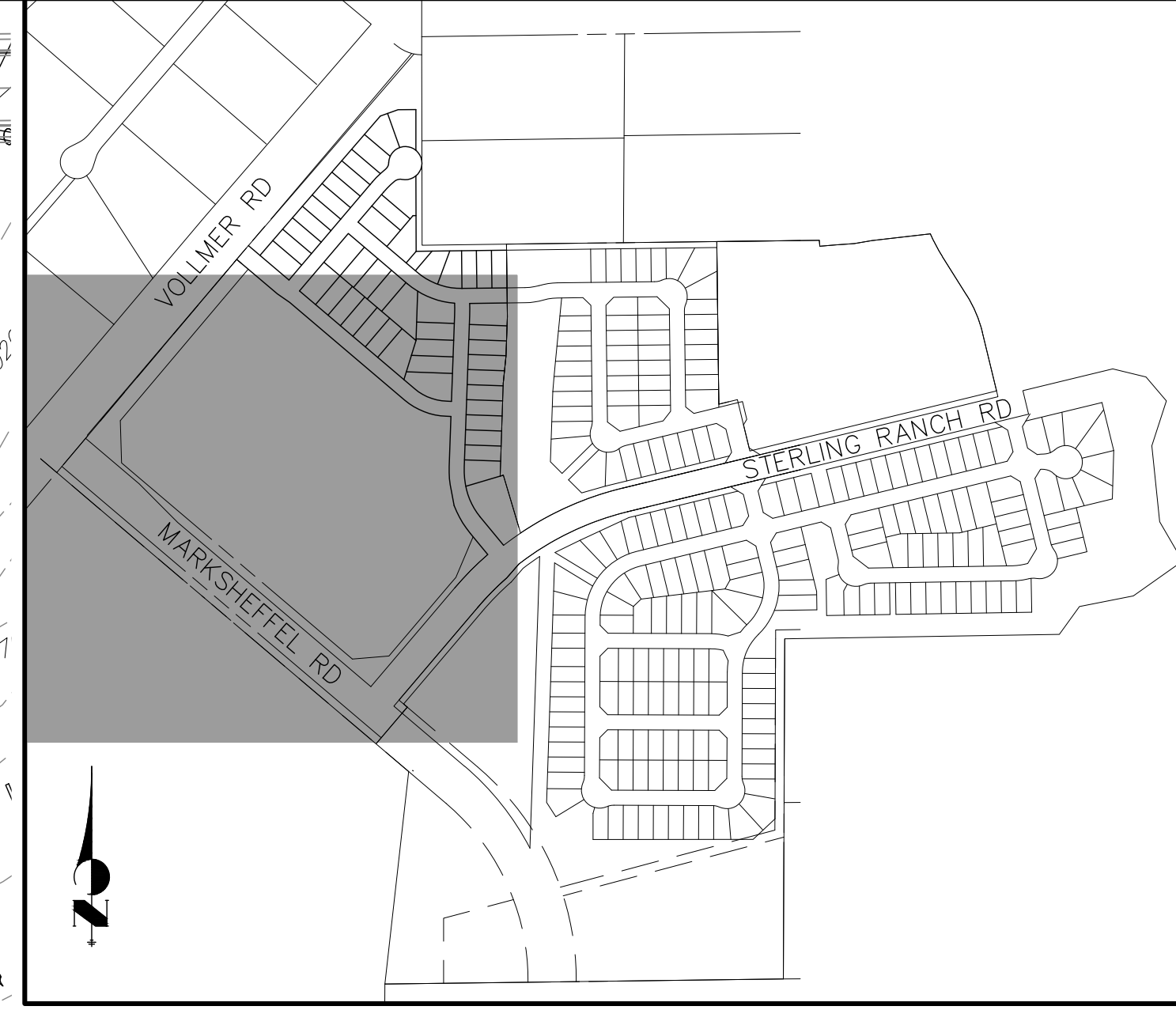
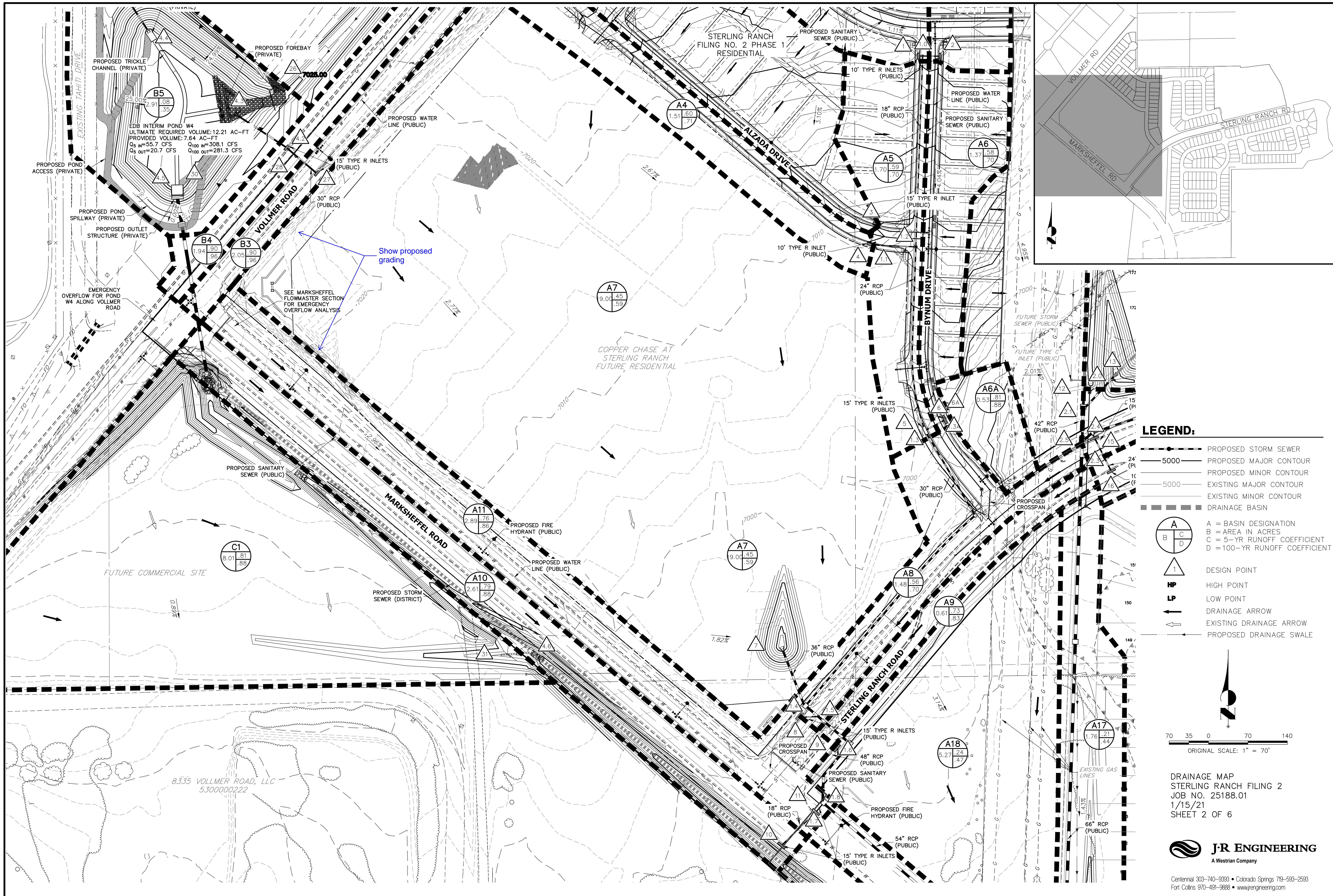
DRAINAGE MAP
STERLING RANCH FILING 2
JOB NO. 25188.01
1/15/21
SHEET 1 OF 6



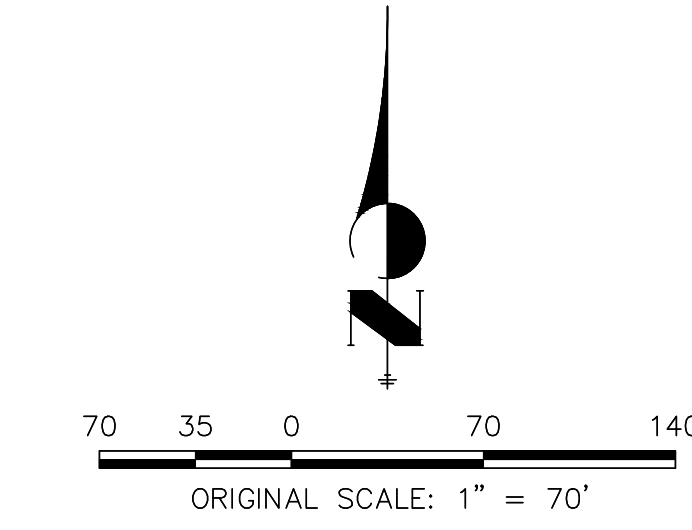
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RAO INVESTMENTS, LLC
 5300000709



- LEGEND:**
- PROPOSED STORM SEWER
 - 5000 PROPOSED MAJOR CONTOUR
 - PROPOSED MINOR CONTOUR
 - 5000 EXISTING MAJOR CONTOUR
 - EXISTING MINOR CONTOUR
 - DRAINAGE BASIN
 - A = BASIN DESIGNATION
B = AREA IN ACRES
C = 5-YR RUNOFF COEFFICIENT
D = 100-YR RUNOFF COEFFICIENT
 - DESIGN POINT
 - HIGH POINT
 - LOW POINT
 - DRAINAGE ARROW
 - EXISTING DRAINAGE ARROW
 - PROPOSED DRAINAGE SWALE



DRAINAGE MAP
 STERLING RANCH FILING 2
 JOB NO. 25188.01
 1/15/21
 SHEET 2 OF 6

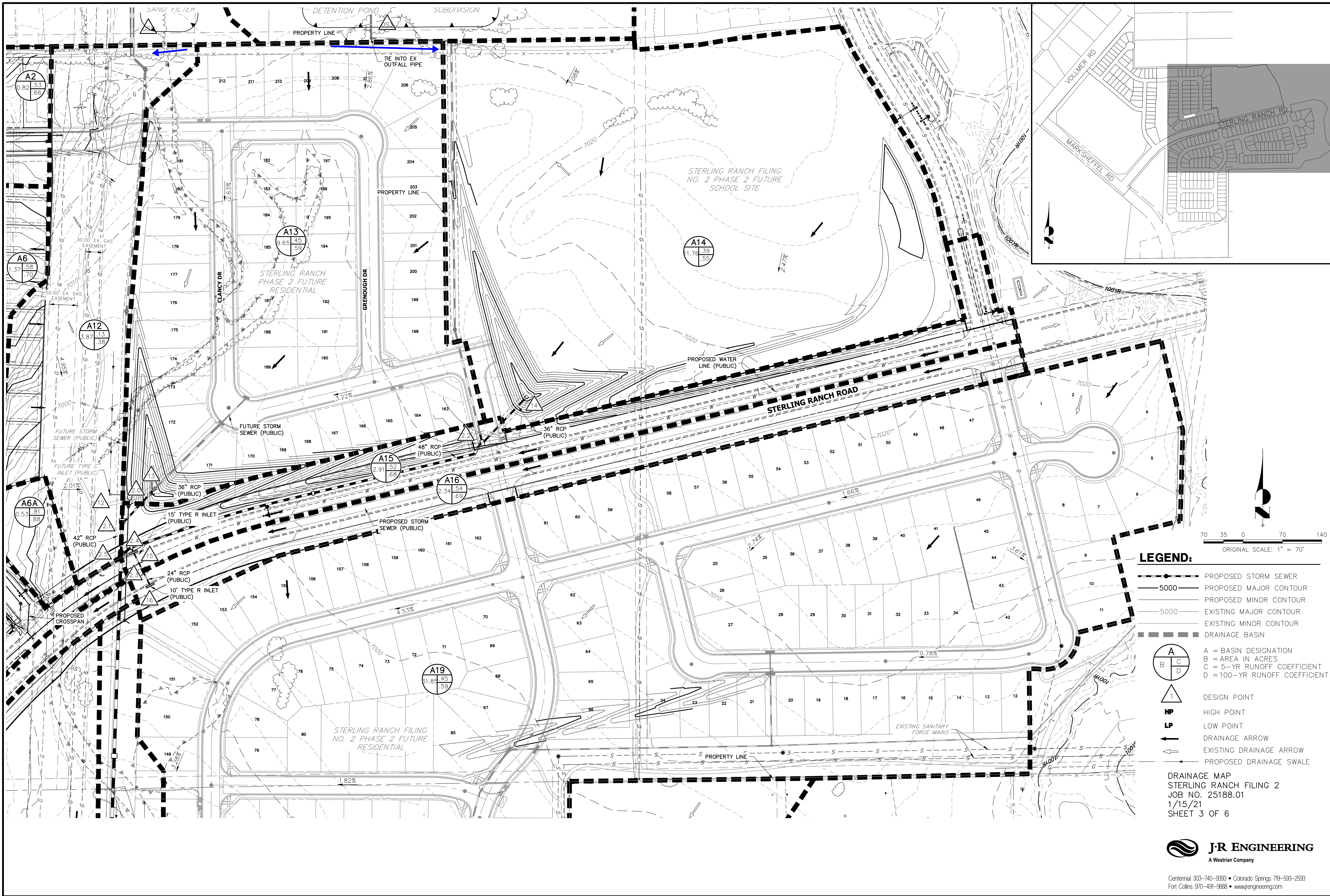
EDB INTERIM POND W4
 ULTIMATE REQUIRED VOLUME: 12.21 AC-FT
 PROVIDED VOLUME: 7.64 AC-FT
 Q_{s in} = 55.7 CFS Q_{100 in} = 308.1 CFS
 Q_{s out} = 20.7 CFS Q_{100 out} = 281.3 CFS

Show proposed grading

SEE MARKSHEFFEL FLOWMASTER SECTION FOR EMERGENCY OVERFLOW ANALYSIS

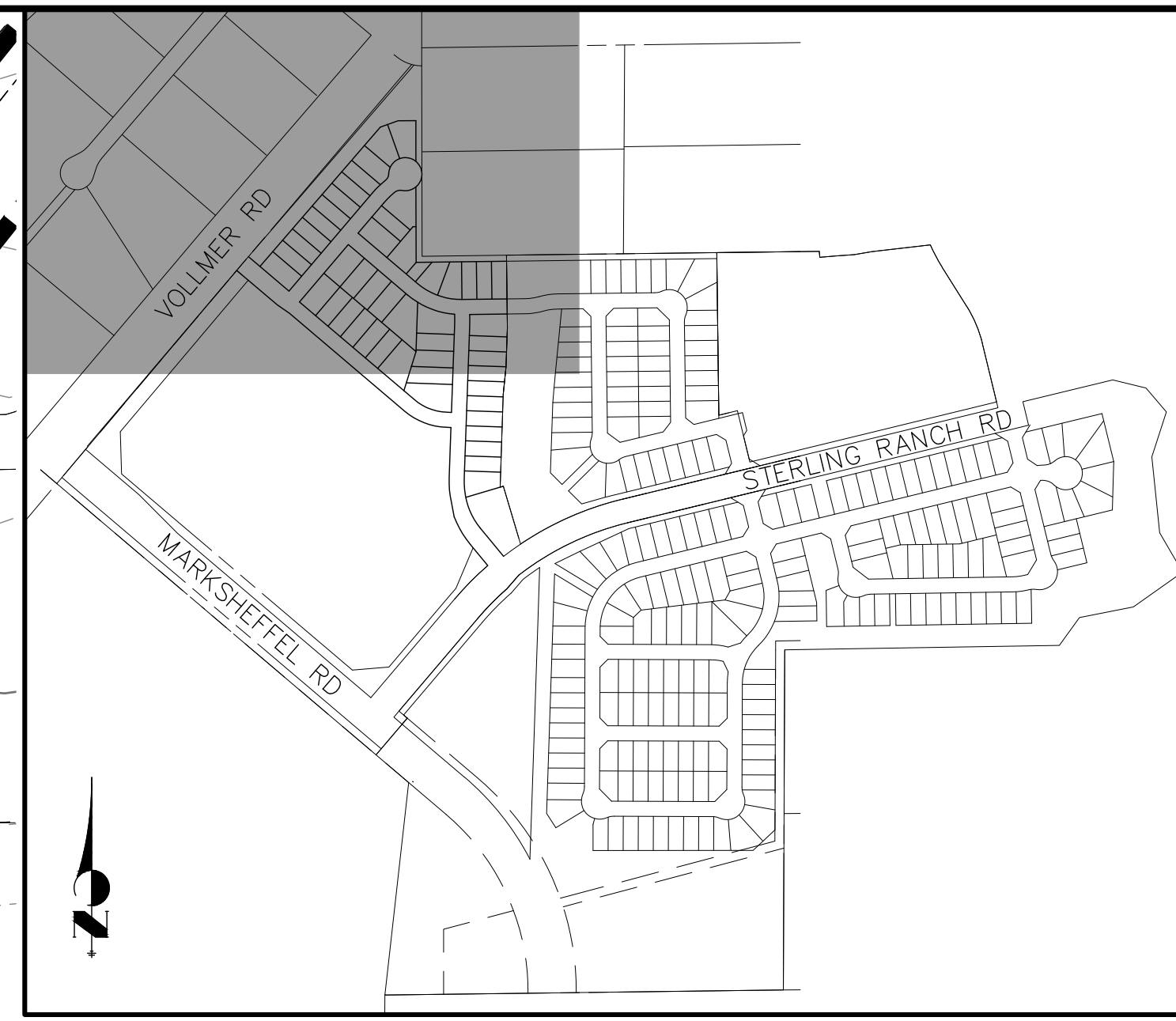
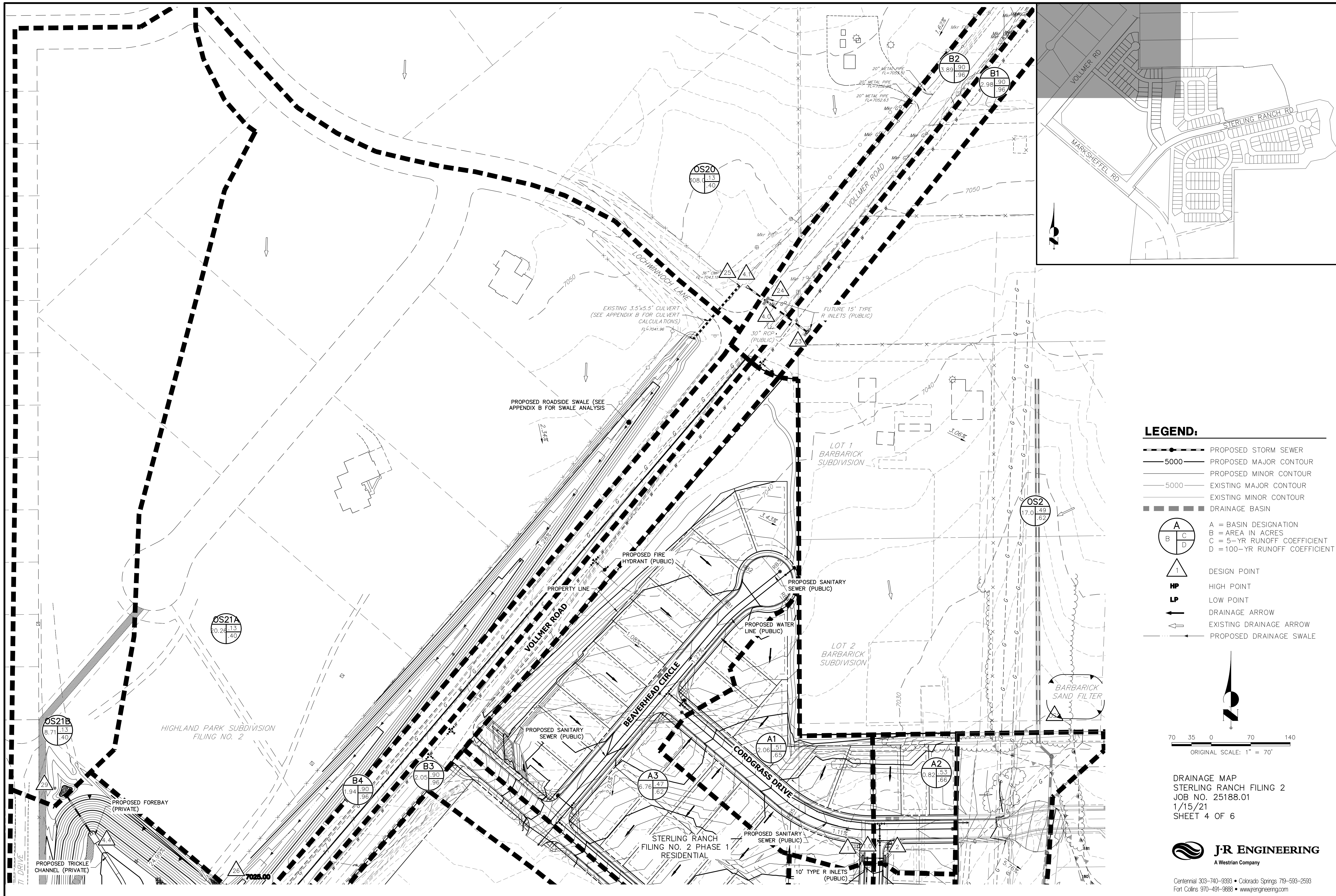
COPPER CHASE AT STERLING RANCH FUTURE RESIDENTIAL

8335 VOLLMER ROAD, LLC
 5300000222

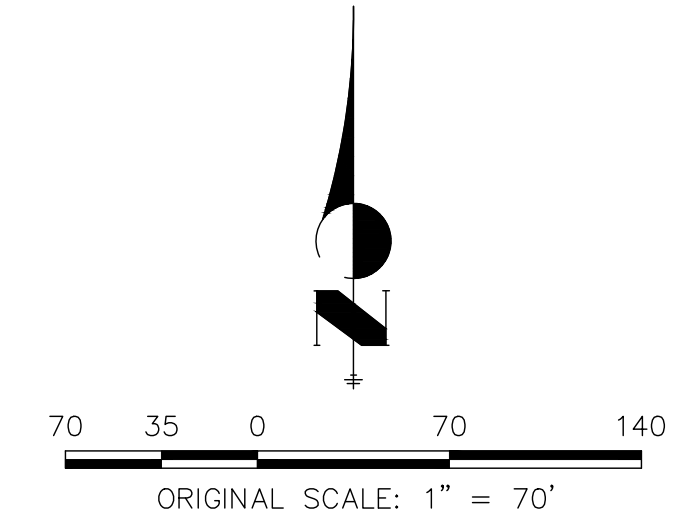


- LEGEND:**
- PROPOSED STORM SEWER
 - 5000 PROPOSED MAJOR CONTOUR
 - PROPOSED MINOR CONTOUR
 - 5000 EXISTING MAJOR CONTOUR
 - EXISTING MINOR CONTOUR
 - DRAINAGE BASIN
 - A = BASIN DESIGNATION
B = AREA IN ACRES
C = 5-YR RUNOFF COEFFICIENT
D = 100-YR RUNOFF COEFFICIENT
 - DESIGN POINT
 - HIGH POINT
 - LOW POINT
 - DRAINAGE ARROW
 - EXISTING DRAINAGE ARROW
 - PROPOSED DRAINAGE SWALE

DRAINAGE MAP
 STERLING RANCH FILING 2
 JOB NO. 25188.01
 1/15/21
 SHEET 3 OF 6



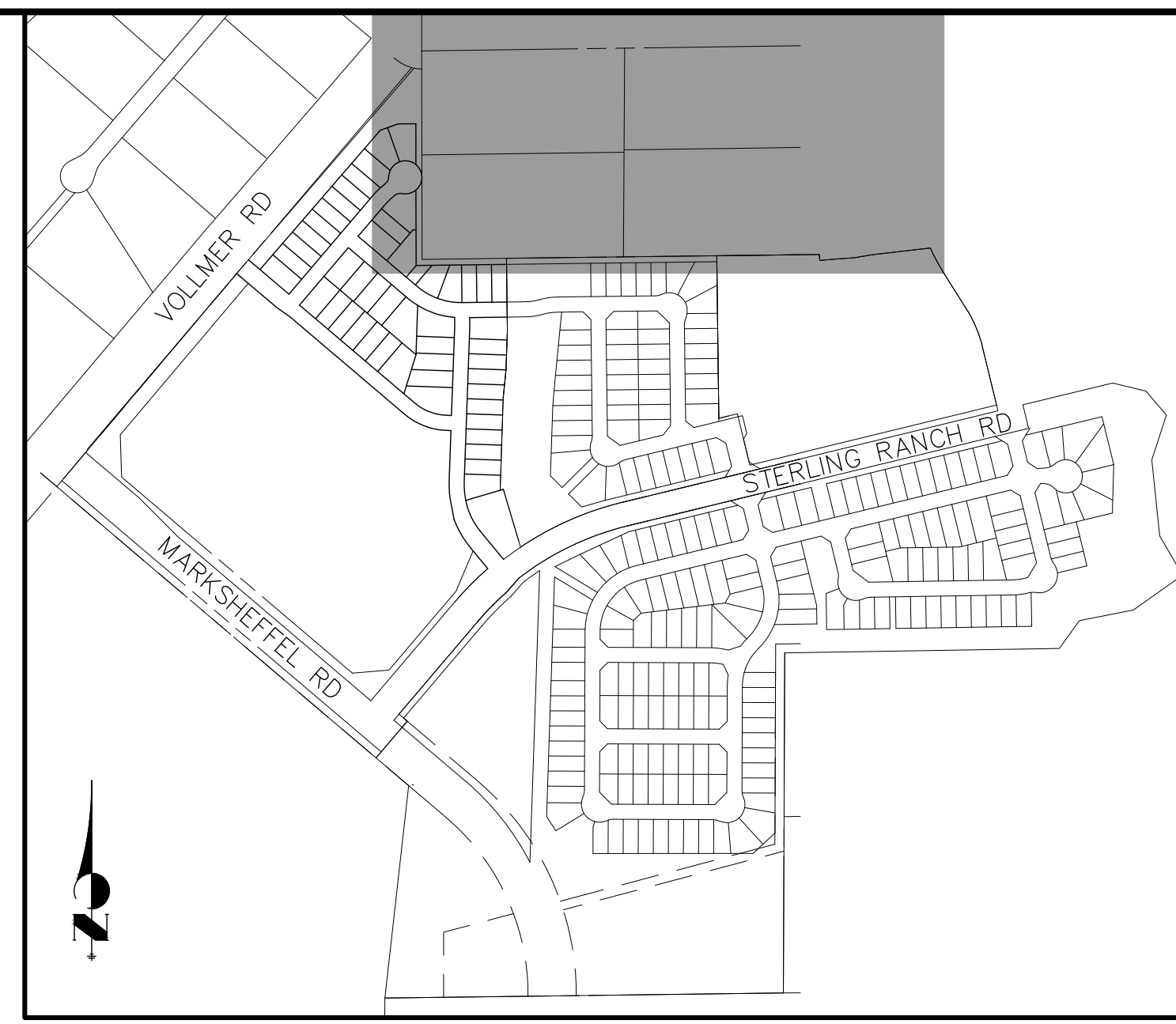
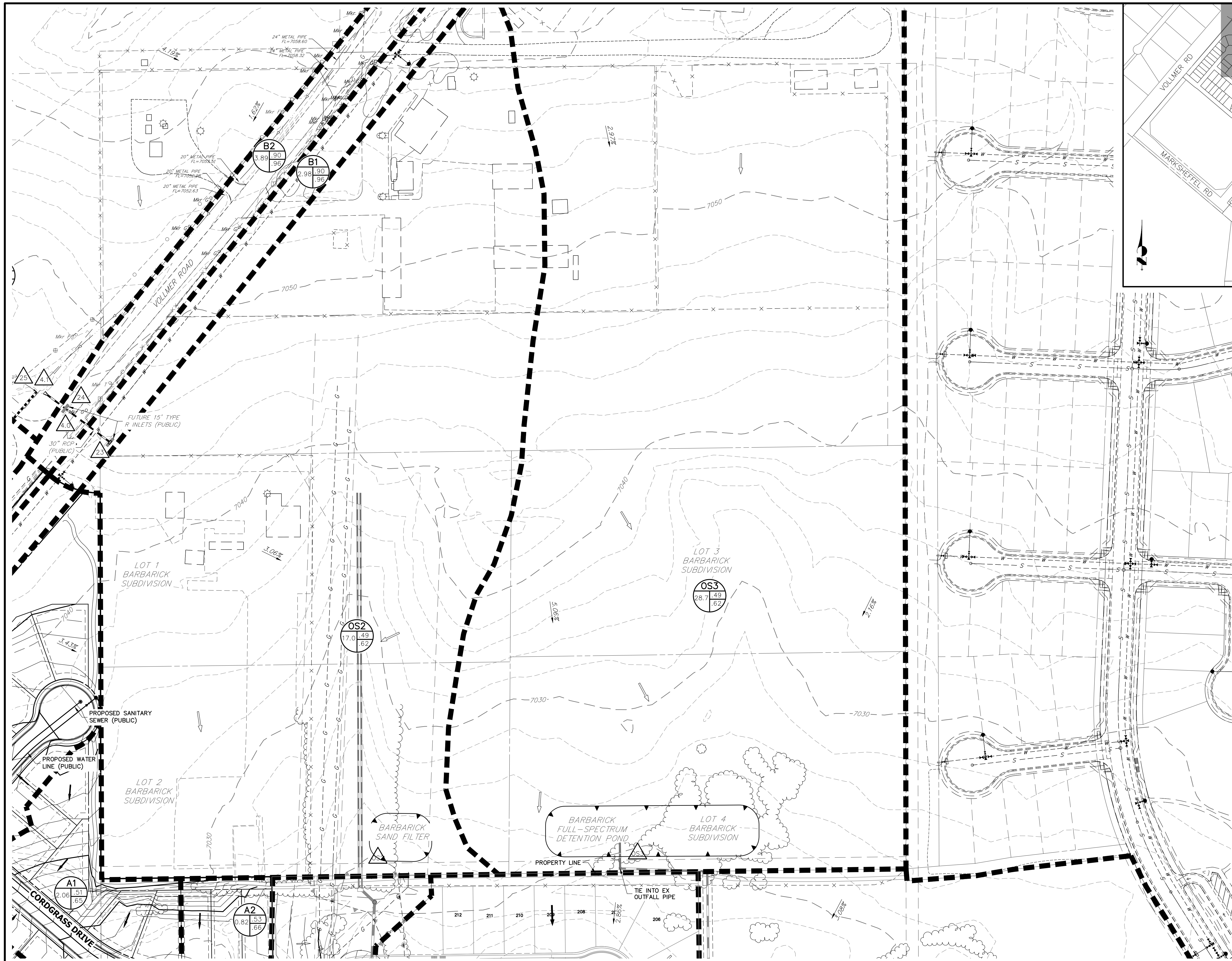
- LEGEND:**
- PROPOSED STORM SEWER
 - 5000 PROPOSED MAJOR CONTOUR
 - PROPOSED MINOR CONTOUR
 - 5000 EXISTING MAJOR CONTOUR
 - EXISTING MINOR CONTOUR
 - DRAINAGE BASIN
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 - DESIGN POINT
 - HIGH POINT
 - LOW POINT
 - DRAINAGE ARROW
 - EXISTING DRAINAGE ARROW
 - PROPOSED DRAINAGE SWALE



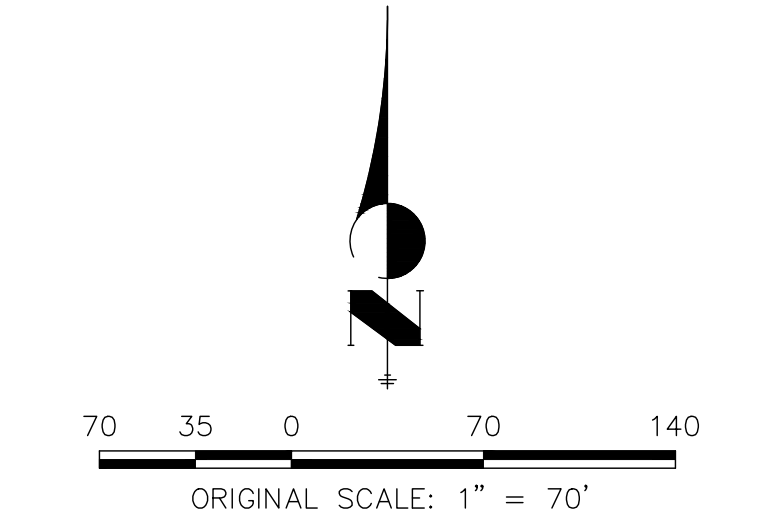
DRAINAGE MAP
 STERLING RANCH FILING 2
 JOB NO. 25188.01
 1/15/21
 SHEET 4 OF 6

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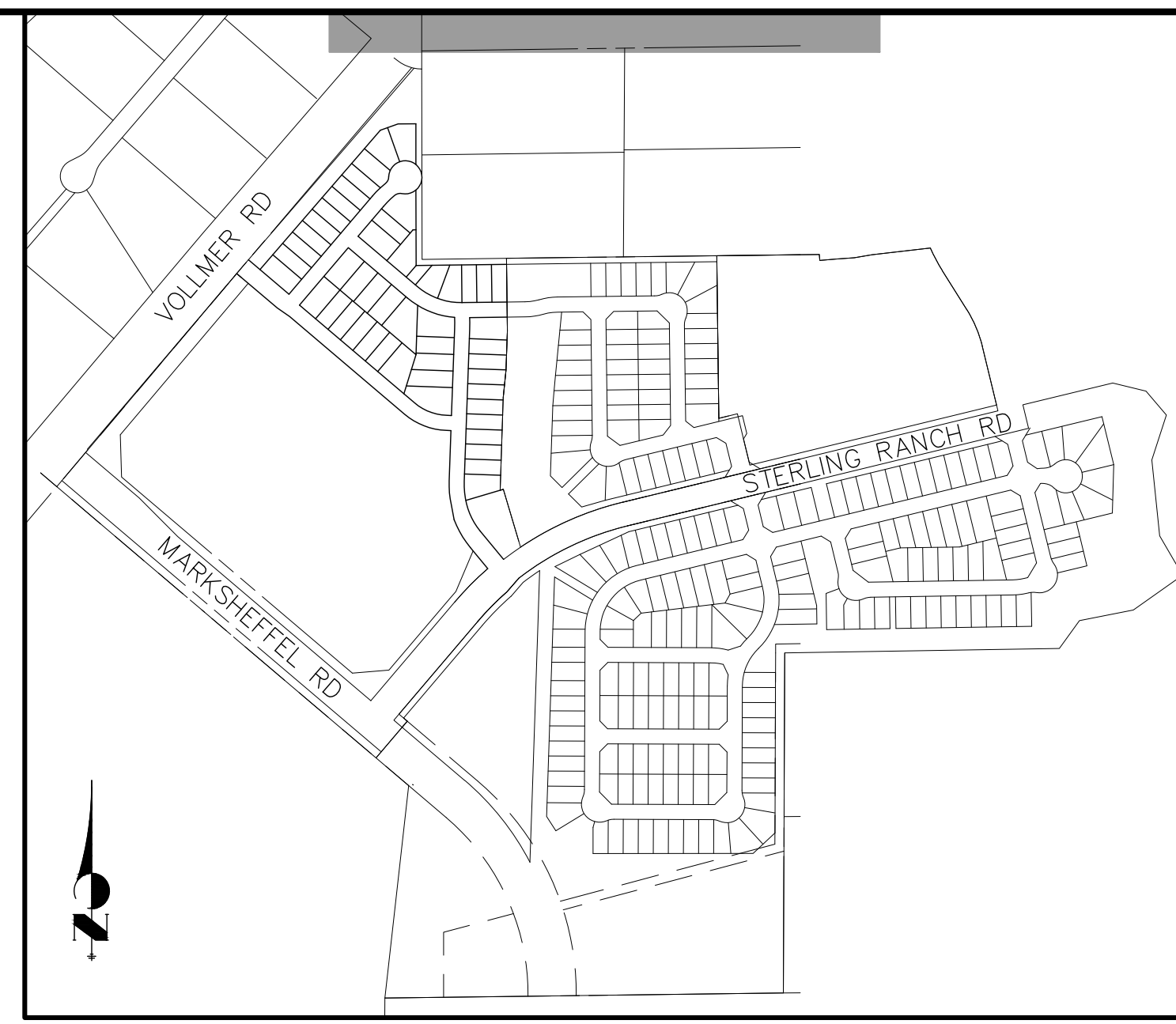
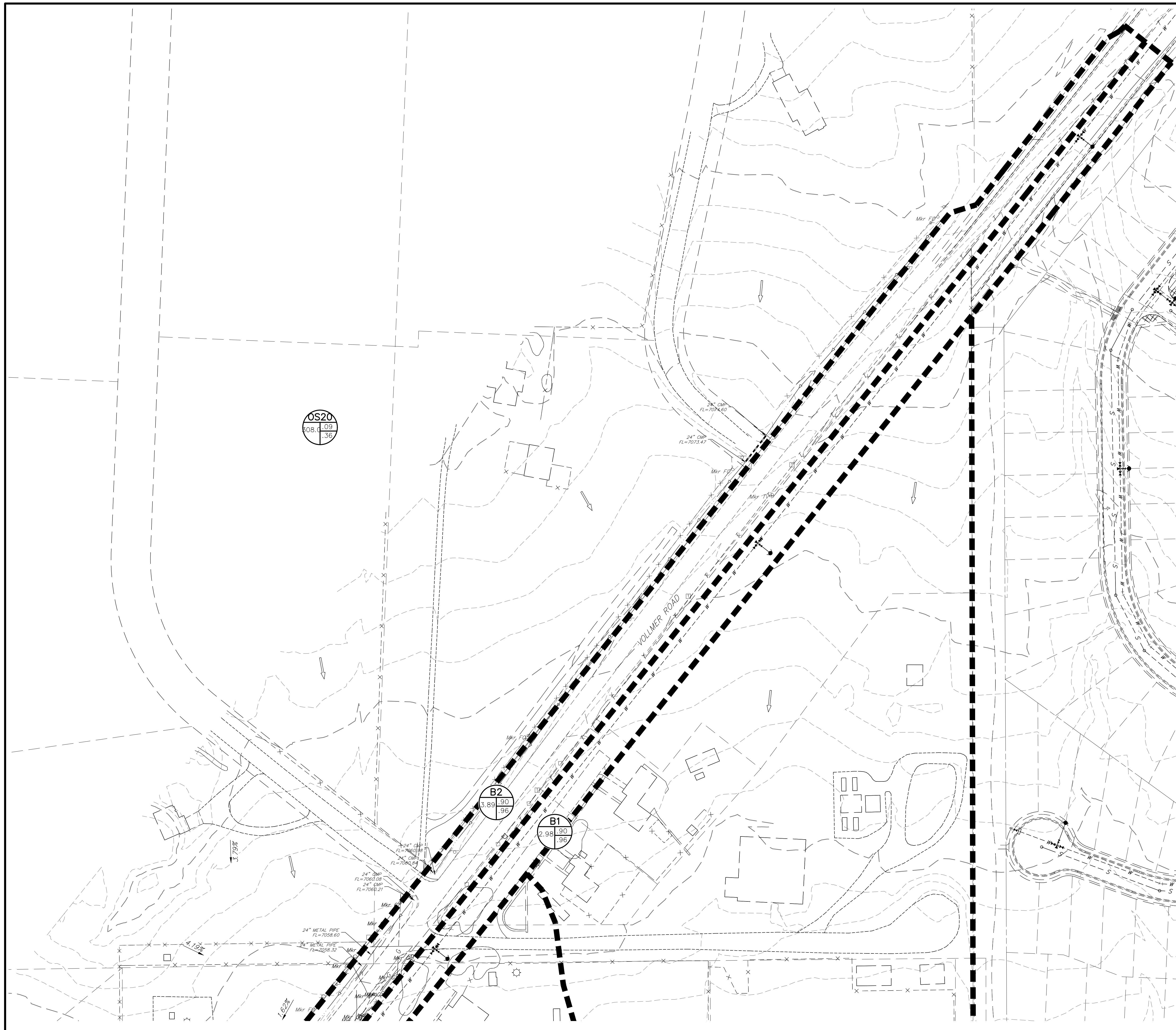
- LEGEND:**
- PROPOSED STORM SEWER
 - 5000 PROPOSED MAJOR CONTOUR
 - PROPOSED MINOR CONTOUR
 - 5000 EXISTING MAJOR CONTOUR
 - EXISTING MINOR CONTOUR
 - DRAINAGE BASIN
 - A = BASIN DESIGNATION
B = AREA IN ACRES
C = 5-YR RUNOFF COEFFICIENT
D = 100-YR RUNOFF COEFFICIENT
 - DESIGN POINT
 - HIGH POINT
 - LOW POINT
 - DRAINAGE ARROW
 - EXISTING DRAINAGE ARROW
 - PROPOSED DRAINAGE SWALE



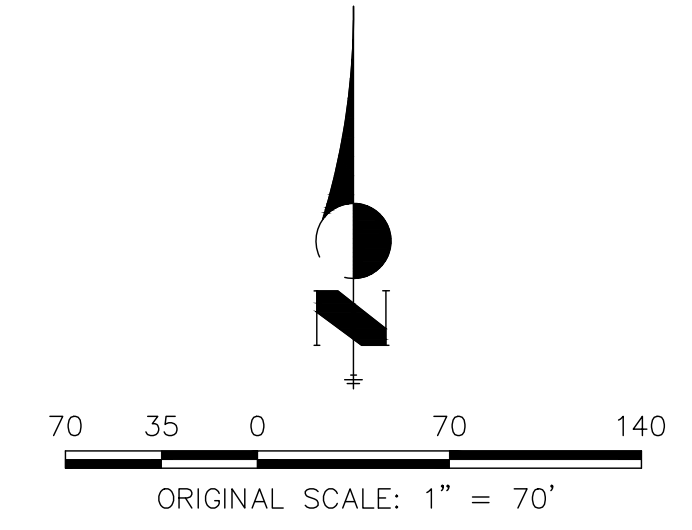
DRAINAGE MAP
 STERLING RANCH FILING 2
 JOB NO. 25188.01
 1/15/21
 SHEET 5 OF 6

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- LEGEND:**
- PROPOSED STORM SEWER
 - 5000 PROPOSED MAJOR CONTOUR
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 - EXISTING MINOR CONTOUR
 - DRAINAGE BASIN
- | | |
|-----------|--|
| | A = BASIN DESIGNATION
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D = 100-YR RUNOFF COEFFICIENT |
| | DESIGN POINT |
| HP | HIGH POINT |
| LP | LOW POINT |
| | DRAINAGE ARROW |
| | EXISTING DRAINAGE ARROW |
| | PROPOSED DRAINAGE SWALE |



DRAINAGE MAP
 STERLING RANCH FILING 2
 JOB NO. 25188.01
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 SHEET 6 OF 6



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