PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH FILING NO. 5

Prepared For:

Classic SRJ Land, LLC 2138 Flying Horse Club Drive Colorado Springs, CO 80921 (719) 785-3270

> March 2023 Project No. 25188.16

Prepared By: JR Engineering, LLC 5475 Tech Center Drive, Suite 235 Colorado Springs, CO 80919 719-593-2593



PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH FILING NO. 5 MAR 2023

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. 32314 For and On Behalf of JR Engineering, LLC

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

Classic SRJ Land, LLC

By:

Title: Address:

2138 Flying Horse Club Drive Colorado Springs, CO 80921

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Joshua Palmer, P.E. County Engineer/ ECM Administrator Date

Conditions:



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PURPOSE

This document is the Preliminary Drainage Report for Sterling Ranch Filing Number 5. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert, inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

GENERAL SITE DESCRIPTION

GENERAL LOCATION

Sterling Filing Number 5 (hereby referred to as the "site") is a proposed development within the Sterling Ranch master planned community with a total area of approximately 11.6 acres. The site is currently being designed to accommodate approximately 72 urban lots.

The site is located in a portion of the Southeast Quarter (SE ¹/₄) Of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridian County Of El Paso, State Of Colorado. The site is surrounded by Barbarick Subdivision and Branding Iron at Sterling Ranch Filing No. 1 to the north, Sterling Ranch Filing No. 4 to the west, Sterling Ranch Road to the south, and Dines Boulevard to the east.

DESCRIPTION OF PROPERTY

The property will be primarily single-family residential development (approximately 11.6 acres), open space and drainage tracts. The site is comprised of variable sloping grasslands that generally slope(s) downward to the southwest at 1 to 3% towards Sterling Ranch Road and Hazlett Dr.

Soil characteristics are comprised of Type A and B hydrologic soil groups. Refer to the soil survey map in Appendix A for additional information.

There are no major drainage ways running through the site, Sand Creek lies to the east of the site. Currently, JR Engineering, LLC is performing studies and plans to address Sand Creek stabilization. There are no known irrigation facilities located on the project site.

FLOODPLAIN STATEMENT

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, the proposed development lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. FIRM Map is presented in Appendix A.



EXISTING DRAINAGE CONDITIONS

MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into major subbasins. The site is within the Upper Sand Creek sub-basin as shown in Appendix C.

The Sand Creek DBPS assumed the Sterling Ranch Filing No. 5 property to have a "large lot residential" use for the majority of the site however, the proposed Sterling Ranch master plan is a mix of; school, multi-family, single-family, and commercial land uses, resulting in higher runoff. The "Master Development Drainage Plan for Sterling Ranch"; (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018 assumed a mix of a school site and single family residential lots ranging in size from 0.1 to 0.33 acres for the Sterling Ranch Filing No. 5 site.

Any additional runoff has been provided for with the extended detention basin, "Pond W-5", located at the southern edge of the Sterling Ranch boundary. The site generally drains from northeast to southwest. The site currently has drainage infrastructure built with prior Sterling Ranch subdivisions filings in the site's southwest corner that collects and conveys the Sterling Ranch Filing 5 runoff to Pond W-5. Currently, the site is undeveloped vacant land. Sand Creek is located approximately 500 feet east of the site running north to south. Currently, JR engineering is performing studies and plans to address Sand Creek stabilization adjacent to the site. Provide project number

The proposed drainage on the site closely follows the approved "Master Development Drainage Plan for Sterling Ranch"; (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018. The site is tributary to Pond W-5 and full-spectrum detention for the site was previously analyzed and can be found in the Final Drainage Report for Sterling Ranch Filing 2 as shown in Appendix C.

EXISTING SUB-BASIN DRAINAGE

The existing condition of the site was broken into four onsite basins, as well as three offsite basins. The basin and sub-basin delineation is shown in the existing drainage map in Appendix D and is described as follows:

Remove assumed (same for following basin descriptions)

Basin A1 ($Q_5=1.0$ cfs, $Q_{100}=7.6$ cfs) is 5.09 acres and 0 percent impervious consists of the northern portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the assumed existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP 3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to pond W-5 built with Filing 2.



Basin A2 ($Q_5=0.8$ cfs, $Q_{100}=5.9$ cfs) is 2.89 acres and 0 percent impervious consists of the south western portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the assumed existing storm sewer built with Filing 5 just north of Sterling Ranch Road located at DP 3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to pond W-5 built with Filing 2.

Basin A3 ($Q_5=0.5$ cfs, $Q_{100}=3.7$ cfs) is 1.94 acres and 0 percent impervious consists of the southern portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the assumed existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP 3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to pond W-5 built with Filing 2.

Basin A4 ($Q_5=6.8$ cfs, $Q_{100}=16.0$ cfs) is 4.83 acres and 47 percent impervious consists of the southeastern portion of the proposed Sterling Filing No. 5 site as well as the norther portion of Sterling Ranch Road. Runoff from this basin drains via overland flow to Sterling Ranch Road, then west to the existing 15' Type R inlet located at DP 5. Collected runoff is piped via existing storm infrastructure south to pond W-5 built with Filing 2.

Basin OS1 (Q_5 = 1.5 cfs, Q_{100} =3.2 cfs) is 0.79 acres and 65 percent impervious, consists of the southern portion of the proposed Branding Iron at Sterling Ranch Filing No.1. Runoff from this basin drains to the south into the proposed Sterling Filing No.5 northern site sub-basin A1. Runoff is collected into the assumed existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to pond W-5 built with Filing 2.

State what pond

Indicate what project and/or report the detained flows for the pond were obtained from

Basin OS2 (Q_5 =14.6 cfs, Q_{100} =52.8 cfs) is 33.07 acres and 19 percent impervious and is located directly north of the site in the Barbarick subdivision. Historic runoff from this site drains south onto the Sterling Ranch Filing 4 site at DP 2. Detained flow from this basin will be piped through the Sterling Ranch Filing 4 site to the detention pond and will outfall to Sand Creek. The emergency overflow path for this pond is routed east around the Sterling ranch Filing 4 lots and onto the northwest corner of Sterling Ranch Filing 5. The emergency overflow path is conveyed south via a concrete line swale and grass swale to DP3. Show and label overflow path and swales on drainage map

Basin OS3 ($Q_5=19.4$ cfs, $Q_{100}=46.3$ cfs) is 13.90 acres and 49 percent impervious, consists of the Sterling Ranch Filing No.4. Runoff from this basin drains to the southwest into the storm sewer built with Sterling Ranch Filing 4 and DP 4. Collected runoff is piped south to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.

PROPOSED DRAINAGE CONDITIONS

PROPOSED SUB-BASIN DRAINAGE

The proposed site was broken into ten onsite basins and one offsite basin that lead into the existing storm structures on Sterling Ranch Road and Sterling Ranch Filing 4. The proposed basin (and subbasin) delineation is shown on the proposed drainage basin map within Appendix D and is described as follows.

Basin A1 ($Q_5=0.6$ cfs, $Q_{100}=2.0$ cfs) is 0.70 acres and 30 percent impervious, consists of single-family residential lots, open space, lawns, and part of an existing concrete channel. Runoff from this basin drains via sheet flow to the swale at DP2 where runoff is collected in an area inlet. Collected runoff is piped south to the proposed sump inlet and DP5.1. The overall runoff is piped south to Sterling Ranch Road storm structures which eventually conveys runoff to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A2 ($Q_5=0.8$ cfs, $Q_{100}=2.3$ cfs) is 0.68 acres and 41 percent impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP1 where it is conveyed west via swale to DP 2 and collected in an area inlet. Collected runoff is piped to DP2.1 and then south to DP5.1. The overall runoff is piped south to Sterling Ranch Road storm structures which eventually conveys runoff to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A3 ($Q_5=0.9$ cfs, $Q_{100}=2.5$ cfs) is 0.75 acres and 43 percent impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP3 where it is conveyed to the street and sump inlet at DP5.1. The overall runoff is piped south to Sterling Ranch Road storm structures which eventually conveys runoff to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A4 ($Q_5=3.1$ cfs, $Q_{100}=6.3$ cfs) is 1.00 acres and 85 percent impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to DP4, then flows to a sump inlet at DP5.1. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A5 ($Q_5=5.1$ cfs, $Q_{100}=12.3$ cfs) is 2.85 acres and 62 percent impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to DP5, then flows to a sump inlet at DP5.1. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.



Basin A6 ($Q_5=1.3$ cfs, $Q_{100}=3.3$ cfs) is 0.74 acres and 55 percent impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter offsite to the curb and gutter in Dines Boulevard. The flows collect in an existing sump inlet at DP6 and are piped via an existing 24" storm pipe to and existing water quality and detention pond (W-8) on the east side of Dines and eventually outfalls to Sand Creek. Pond W-8 was analyzed with the Sterling Ranch Filing 1, Branding Iron Filing 1 and Branding Iron Filing 2 subdivisions and has a total tributary area of approximately 29 acres. The addition of the Basin A6 flows are assumed to be immaterial but will be further analyzed with the Final Drainage Report for SR Filing 5 to confirm this Preliminary Drainage Report assumption. Also include that the existing inlet will be checked for capacity with the additional flow.

Basin A7 ($Q_5=3.8 \text{ cfs}$, $Q_{100}=9.2 \text{ cfs}$) is 2.03 acres and 58 percent impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to an on-grade inlet at DP7. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek. Runoff that is not collected by the inlet at DP7 continues west to an existing sump inlet at DP11 built with Sterling Ranch Filing 4. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing inlet will be checked for capacity with the by-pass flow in the FDR.

Basin A8 ($Q_5=3.9 \text{ cfs}$, $Q_{100}=8.6 \text{ cfs}$) is 1.55 acres and 71 percent impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to an on-grade inlet at DP 8. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek. Runoff that is not collected by the inlet at DP8 continues west to an existing sump inlet at DP12 built with Sterling Ranch Filing 4. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing inlet will be checked for capacity with the by-pass flow in the FDR.

Basin A9 ($Q_5=0.3 \text{ cfs}$, $Q_{100}=0.8 \text{ cfs}$) is 0.21 acres and 50 percent impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via overland and sheet flow to the curb and gutter on Dines Boulevard. The flows collect at DP9 and run along the curb and gutter along Sterling Ranch Road to an existing on-grade inlet at DP13 built with Sterling Ranch Filing 2. The overall runoff is piped south to Sterling Ranch Road storm structures which eventual dentify that the existing inlet the flow to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek additional flow from this basin and the set of the set of

FDR.

Basin A10 ($Q_5=1.9$ cfs, $Q_{100}=5.1$ cfs) is 1.35 acres and 52 percent impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via overland flow and sheet flow offsite to the curb and gutter on Sterling Ranch Road at DP10 and continues west along the curb and gutter to an existing on-grade inlet at DP13 built with Sterling Ranch Filing 2. The overall runoff is



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Identify that the existing inlet (DP13) will be checked for capacity with the additional flow from this basin in the FDR and the next downstream inlet will be checked with additional bypass flow from DP13. piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin OS1 ($Q_5=1.5$ cfs, $Q_{100}=3.5$ cfs) is 0.79 acres and 65 percent impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP1 where it is conveyed west via swale to DP2.1 and collected in an area inlet. Collected runoff is piped south to DP5.1. The overall runoff is piped south to Sterling Ranch Road storm structures which eventually conveys runoff to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek. Include discussion on overall flows exiting site and indicate if there is an increase or decrease to amount

of flows entering existing storm system from Filing 5

DRAINAGE DESIGN CRITERIA

DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.

HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Table 2 - 1-m Tomt Kaman Data						
Storm	Rainfall (in.)					
5-year	1.50					
100-year	2.52					

Table 2	2 -	1-hr	Point	Rainfall	Data
I unic A	-		I UIIIU	I (u) III (u) I	Duu

HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Sump and on-grade inlets will be sized using UDFCD UD-Inlet v5.02. StormCAD will be used to model the proposed storm sewer system within the interim area and



interim area? Is there phases planned?

to analyze the proposed HGL calculations for the Construction Drawings. Autodesk Hydraflow express will be used to size any channels or swales. Manhole and pipe losses for the model will be obtained from the <u>Modeling Hydraulic and Energy Gradients in Storm Sewers: A Comparison of Computation</u> <u>Methods</u>, by AMEC Earth & Environmental, Inc. The manhole loss coefficients used in the model can be seen in Table 3 (below) this method is accurate for pipes 42" and smaller for larger pipes the Standard head-loss coefficients as recommended by Bentley were used as shown in Table 4. All hydraulic calculations will be found in the Final Drainage Report Appendices.

	StormCA	D Conversion Tal	ble
	Bend Angle	K coefficient (Conversion
so	0	0.0	5
	22.5	0.1	
en	45	0.4	8
	60	0.64	1
	90	1.32	2
	1 Latera	al K coefficient Co	nversion
	Bend Angle	Non Surcharged	Surcharged
S	45	0.27	0.47
2	60	0.52	0.9
al	90	1.02	1.77
ate	2 Latera	Is K coefficient Co	onversion
_	45	0.96	6
	60	1.10	6
	90	1.52	2

Table 3 Storm Head-loss Coefficients

Table 4 Storm Head-loss Coefficients



Type of Manhole	Diagram	Headloss Coefficient
Trunkline only with no bend at the junction		0.5
Trunkline only with 45° bend at the junction	5-0	0.6
Trunkline only with 90° bend at the junction	J-C	0.8
Trunkline with one lateral	8-0-6	Small 0.6 Large 0.7
Two roughly equivalent entrance lines with angle $<$ 90° between lines	A Contraction	0.8
Two roughly equivalent entrance lines with angle > 90° between lines	E Contraction	0.9
Three or more entrance lines	E 5	1.0

DRAINAGE FACILITY DESIGN

GENERAL CONCEPT

The proposed stormwater conveyance system was designed to convey the developed Sterling Ranch Filing No. 5 runoff to an existing (Filing 2) full spectrum water quality and detention pond W-5 via existing and proposed storm sewer. The existing pond was designed to release at less than historic rates to minimize adverse impacts downstream. Treated water will outfall directly into the Sand Creek Drainageway, where it will eventually outfall into Fountain Creek. A proposed drainage map is presented in Appendix D showing locations of the pond.

FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The Sterling Ranch Filing No. 5 development project consists of single-family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.



Step 2 – Stabilize Drainage ways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the channel stabilization being designed by JR Engineering adjacent to the site and on future projects within the basin to stabilize drainage ways. The site does not discharge directly into the open drainage way of Sand Creek, therefore no downstream stabilization will be accomplished with this project

& W-8 (Basin A6 now releases into this existing pond)

Step 3 – Treat the WQCV: Water Quality treatment for this site is provided in an existing full spectrum water quality detention pond (W-5). The runoff from this site will be collected within inlets and conveyed to the proposed pond via storm sewer. Upon entrance to the pond, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the pond to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the pond will be reduced to less than historic rates.

Step 4 –BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. The Filing No. 5 site is residential. There is no proposed commercial or industrial use for the site. The permanent erosion control BMPs include asphalt drives, storm inlets and storm pipe, the full spectrum detention pond W-5 and permanent vegetation. Maintenance responsibilities and plans will be defined at the time of final platting.

WATER QUALITY

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention are provided for all developed basins. This site will drain into an existing Full Spectrum Drainage Pond W-5 developed during the Sterling Ranch Filing No. 2 Project. Further details as well as all pond volume, water quality, and outfall calculations are included in the Sterling Ranch Filing 2 Final Drainage Report. Pond W-5 corresponds to pond FSD6 from the Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018 and is releasing less than the MDDP values in the proposed design. A summary of Pond W-5 has been included below for reference. From the Filing No.2 drainage report, Pond W-5 accounted for Sterling Ranch Filing 5 area to have 65% imperviousness. The total imperviousness for the Filing 5 development is 59% imperviousness, and the total runoff is less than what was anticipated; therefore the existing pond W-5 will function as intended.

	REQUIRED VOLUME	VOLUME PROVIDED	WQCV	EURV	5-YEAR RELEASE	100-YEAR RELEASE
	(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)	(CFS)	(CFS)
POND W-5	18.217	18.441	3.29	11.71	2.7	137.1

Table 3. Pond	Volumes &	& Release	Rates
---------------	-----------	-----------	-------

Engineer must confirm in the Drainage Report that the existing offsite PBMP that the site is tributary to are functioning as intended.



EROSION CONTROL PLAN

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

OPERATION & MAINTENANCE

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The district shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. A maintenance road was provided for the existing pond W-5 and information on the road can be found in the Final Drainage Report for Sterling Ranch Filing No. 2. The maintenance road access is off Marksheffel Road and wraps around the top of the pond providing access to the inflow pipe wing walls and outlet structure for the pond. As flows are now also reaching existing

As flows are now also reaching existing Pond W-8, it will also need to be included in the discussion.

DRAINAGE AND BRIDGE FEES

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees will be defined within the Final Drainage Report and will be due at time of platting (depending on date of plat submittal).

SUMMARY

The proposed Sterling Ranch Filing No. 5 drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainage-ways or surrounding development. The existing pond W-5 is to release less than 90% of the predeveloped runoff study associated with the subject site. The site is in continuity with the Sterling Ranch Filing No. 2 Drainage Report. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.

and Filing No. 4

Include statement that proposed site does not impact any downstream facility or property.



REFERENCES

- 1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2. Sand Creek Channel Design Report, prepared by JR Engineering, May 19, 2021 (not yet approved)
- 3. "Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018.
- 4. <u>Sand Creek Drainage Basin Planning Study</u>, prepared Kiowa Engineering Corporation, January 1993, revised March 1996.
- 5. "Sterling Ranch Filing 2 Final Drainage Report", prepared by JR Engineering, dated May 2021
- 6. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- Sand Creek Stabilization at Aspen Meadows Subdivision Filing No. 1 100% Design Plans, April 2020
- 8. <u>Final Drainage Report For Barbarick Subdivision Portion Of Lots 1,2 And Lots 3 and 4</u>, Prepared by Matrix Design Group, June 2016
- 9. Preliminary Drainage Report And MDDP Addendum For Homestead North At Sterling Ranch Preliminary Plan", prepared by JR Engineering, dated January 2022
- 10. Sand Creek Drainage Basin Planning Study, Stantec, January 2021
- 12. Final Drainage Report for Aspen Meadows, Matrix Design, January 2019* pending approval



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Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map





N.T.S.

VICINITY MAP HOMESTEAD FILING NO. 5 JOB NO. 25188.16 8/26/22 SHEET 1 OF 1



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
9	Blakeland-Fluvaquentic Haplaquolls	A	0.8	3.3%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	12.0	49.0%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	11.7	47.7%
Totals for Area of Intere	est		24.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



NOTES TO USERS

This map is for use in administring the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage curces of small size. The community map repository should be consulted for ossible updated or additional flood hazard information.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0° North American Vortical Datum of 1889 (N4/V089). Users of this FIRM Hould be aware that coastal flood deviators are aired provided in the Summary of Sillware Elevators table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Sillware Elevators table should be used for construction and/or floodpian management purposes when they are higher than the deviations

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway width and other partinent floodway data are provided in the Flood Insurance Study report for this jurisdicture.

Certain areas not in Special Flood Hazard Areas may be protected by **flood contrn** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insuranc Study report for information on flood control structures for this jurisdiction.

The projection used in the properties of this may was Universel Transverse Meanser (UTM) are 13. The hotherabil attain was NABO, GR585 spheroid. Differences in datum, spheroid, projection or UTM screes zones used in the production of FRMNs for adjacent juncticions may require uit, in slight positional differences in mag features across jurisdiction boundaries. These differences do not affect the accuracy of this FRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD68), Thesis flood elevations must be compared to structure are compared to structure and the structure of the structure and conversion between the National Geodelic Vertical Datum of 1528 and the North American Vertical Datum of 1988, visit the National Geodelic Survey at the Holm/ American Service and Service and Service and the Islaming Service and Service and

NGS Information Services NOAA, NINGS12 National Geodetic Survey SSMC-3, #9202 1315 East-Weast Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Seodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gow/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Ublities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map infects more detailed and up-to-date stream channel configurations and modplain delineations than those shown on the previous FRM for this jurisdice, this way to be adjudged to confirm to these more stream channel configurations. As sets the besing disudded to confirm to these more stream channel configurations. As a sets the besing disudded chain may reflect them channel disarces that offer from what is shown on the integr. The profit baselines diplated disarces that offer from what is shown on the integr. The profit baselines diplated disarces that offer from what is shown on the integr. The profit baselines diplated baselines that offer from what is shown on the integration and Frodowy Data habes is spirated in the FIS report. As a result, the profit baselines digited of the foroignan.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, may users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a siting of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is conted.

Contact FEMA Map Service Center (MSC) via tha FEMA Map information eXchange FMX) 1677-038227 for information on available products associated with the FRM. Available products may include prevauly issued Letters of Map Change, a food insurance Study Report, and/or diplail versions of his map. The MSC may also be reached by Fax at 1-800-358-8620 and its websile at try/invow.msc.fema.gov/.

f you have questions about this map or questions concerning the National Flood nsurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or isit the FEMA website at http://www.fema.gov/business/nfip.





This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Water Conservation Board

tional Flood Hazaro Information and resource lable from local communities and the Col-



3235000 FT JOINS PANEL 0535 1047 307 33 607 104" 41" 15.00" 381 581 7 501 38" 58' 7 50" Sand Creek ZONEAE Ø EL PASO COUNTY UNINCORPORATED AREAS 080059 -424-2000mai (DC) VOLLMER F 33 32 34 ZONE (C) (cx) 4312000mN 1410000 F T. 12 S T. 13 S MOJAVE DR T. 12 S. T. 13 S. EL PASO COUNTY UNINCORPORATED AREAS 080059 ZONEA 070 CIR SITE LOCATION in. ZONE AE KENOSHA DR EL PASO COUNTY CITY OF COLORADO SPRINGS PONCA RD 3 4 5 EL PASO COUNTY NINCORPORATED AREAS 080059 CITY OF COLORADO SPRINGS 1405000 F 6886 WOODMEN FRONTAGE RD E WOODMEN RD Bridge E WOODMEN D co AREAS (000159 10 ZONE AE 8 43-10.000mN Sand Creek 381 561 15 00 381 561 15.001 104° 41' 15.00" JOINS PANEL 0545 104" 39' 22.50' \$-000mp NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.



Appendix B Hydrologic Calcs



COMPOSITE % IMPERVIOUS & COMPOSITE EXISTING RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location: Sterling Ranch Subdivision- Existing El Paso County

 Project Name:
 Sterling Ranch Filing 5

 Project No.:
 25188.16

 Calculated By:
 DIG

 Checked By:
 RAB

 Date:
 11/21/22

	Total	Str	eets (10	10% Impe	rvious)	Re	Residential (65% Impervious)				Light Industrial (80% Impervious)				Lawns (0% Impervious)					Basins Total Weighted %
Basin ID	Al ea (ac)	C ₅	C ₁₀₀	Area	Weighted	C ₅	C ₁₀₀	Area	Weighted %	C ₅	C ₁₀₀	Area	Weighted	C ₅	C ₁₀₀	Area	Weighted %	vai		Imp.
				(ac)	% imp.			(dl)	imp.			(ac)	70 IIIIp.			(dt)	imp.	U5	U ₁₀₀	
A1	5.09	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	5.09	0.0%	0.08	0.35	0.0%
A2	2.89	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	2.89	0.0%	0.08	0.35	0.0%
A3	1.94	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.94	0.0%	0.08	0.35	0.0%
A4	4.83	0.90	0.96	1.75	36.2%	0.45	0.59	0.80	10.8%	0.59	0.70	0.00	0.0%	0.08	0.35	2.28	0.0%	0.44	0.61	47.0%
OS1	0.79	0.90	0.96	0.00	0.0%	0.45	0.59	0.79	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
OS2	33.07	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	7.91	19.1%	0.08	0.35	25.16	0.0%	0.20	0.43	19.1%
OS3	13.90	0.90	0.96	2.35	16.9%	0.45	0.59	6.86	32.1%	0.59	0.70	0.00	0.0%	0.08	0.35	4.69	0.0%	0.40	0.57	49.0%
TOTAL (A1-A4)	14.75																			0.0%
TOTAL (OS1-OS3)	47.76																			28.6%
TOTAL	62.51																			25.5%

EXISTING STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Subdivision- Existing

Location: El Paso County

Project Name: <u>Sterling Ranch Filing 5</u> Project No.: 25188.16

Equation 6-3

Equation 6-5

Calculated By: DIG

Checked By: RAB

Date: 11/21/22

		SUB-I	BASIN			INITI	AL/OVERI	AND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T _i)				(T _t)			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t i	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	5.09	В	0%	0.08	0.35	180	1.4%	22.1	497	1.6%	10.0	1.3	6.5	28.7	677.0	33.3	28.7
A2	2.89	А	0%	0.08	0.35	125	4.6%	12.4	385	5.2%	10.0	2.3	2.8	15.3	510.0	29.1	15.3
A3	1.94	А	0%	0.08	0.35	80	1.7%	13.8	385	2.5%	10.0	1.6	4.1	17.9	465.0	30.5	17.9
A4	4.83	А	47%	0.44	0.61	100	3.0%	8.3	1466	1.5%	20.0	2.4	10.0	18.3	1566.0	30.8	18.3
OS1	0.79	А	65%	0.45	0.59	88	2.0%	8.8	122	2.0%	10.0	1.4	1.4	10.2	210.0	15.7	10.2
OS2	33.07	А	19%	0.20	0.43	298	3.0%	19.5	1664	2.7%	10.0	1.6	16.9	36.4	1962.0	37.2	36.4
OS3	13.90	А	49%	0.40	0.57	100	1.8%	10.4	796	1.7%	20.0	2.6	5.1	15.5	896.0	24.1	15.5

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$

t_i = overland (initial) flow time (minutes)

 $L_i =$ length of overland flow (ft)

 $C_5 = \text{runoff coefficient for 5-year frequency (from Table 6-4)}$

 S_0 = average slope along the overland flow path (ft/ft).

NOTES:

 $t_c = t_i + t_t$

-020 - 50

Where:

te = computed time of concentration (minutes)

 t_i = overland (initial) flow time (minutes)

 t_t = channelized flow time (minutes).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

 $\begin{array}{l} t_t = \text{channelized flow time (travel time, min)} \\ L_t = \text{waterway length (ft)} \\ S_o = \text{waterway slope (ft/ft)} \\ V_t = \text{travel time velocity (ft/sec)} = K \sqrt{S_o} \\ K = \text{NRCS conveyance factor (see Table 6-2).} \end{array}$

Equation 6-4
$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

Where:

Equation 6-2

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1. t_r = length of channelized flow path (ft) i = imperviousness (expressed as a decimal) S_r = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

STANDARD FORM SF-3 - EXISTING STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision:	Sterling Ranch Subdivision- Existing
Location:	El Paso County

Design Storm: 5-Year

Project Name: Sterling Ranch Filing 5 Project No.: 25188.16 Calculated By: DIG Checked By: RAB Date: 11/21/22

	_																						
				DIRE	CT RUI	NOFF			TC) tal f	RUNOF	FF	STRE	ET/SW	/ALE		PI	PE		TRAV	'EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	OS1	0.79	0.45	10.2	0.36	4.10	1.5															
	2	OS2	33.07	0.20	36.4	6.68	2.19	14.6															Offsite Barbarick Pond Release Piped to DP4
	3	A1	5.09	0.08	28.7	0.41	2.55	1.0															
	3	A2	2.89	0.08	15.3	0.23	3.50	0.8															
	3	A3	1.94	0.08	17.9	0.16	3.26	0.5															
	3								28.7	1.16	2.55	3.0											Sum of basins A1-A3 and OS1, drain to Ex storm Piped west and south to Ex. Pond W-5
	4	OS3	13.90	0.40	15.5	5.58	3.47	19.4															
	5	A4	4.83	0.44	18.3	2.12	3.22	6.8															Runoff to Ex. Inlet in Sterling Ranch Road Piped south to Ex. Pond W-5

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - EXISTING STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision:	Sterling Ranch Subdivision- Existing
Location:	El Paso County
Design Storm:	100-Year

Project Name:	Sterling Ranch Filing 5
Project No.:	25188.16
Calculated By:	DIG
Checked By:	RAB

Date: 11/21/22

				DIR	ECT RL	JNOFF			Т	OTAL F	RUNO	F	STRE	ET/SW	'ALE		PIP	E		TRAV	EL TIN	ЛE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	OS1	0.79	0.59	10.2	0.47	6.88	3.2															
	2	OS2	33.07	0.43	36.4	14.34	3.68	52.8															Offsite Barbarick Pond Release Piped to DP4
	3	A1	5.09	0.35	28.7	1.78	4.28	7.6															
	3	A2	2.89	0.35	15.3	1.01	5.87	5.9															
	3	A3	1.94	0.35	17.9	0.68	5.47	3.7															
	3								28.7	3.94	4.28	16.9											Sum of basins A1-A3 and OS1, drain to Ex storm Piped west and south to Ex. Pond W-5
	4	OS3	13.90	0.57	15.5	7.94	5.83	46.3															
	5	A4	4.83	0.61	18.3	2.95	5.41	16.0															Runoff to Ex. Inlet in Sterling Ranch Road Piped south to Ex. Pond W-5

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location:

Sterling Ranch Subdivision - Proposed El Paso County

Project Name: Sterling Ranch Filing 5

Project No.:	25
Calculated By:	DI

% impervious is good for detached lots, but what about attached lots? Those areas would be closer to 70% impervious

5188.16 IG Checked By: RAB Date: 3/20/23

	Total	Paved	/Streets	s (100% Ir	mpervious)	Re	sidentia	l (65% lm	npervious)	Light I	ndustria	l (80% In	npervious)	I	awns (0	% Imper	vious)	Basin: Weigl	s Total nted C	Basins Total Weighted %
Basin ID	Area (ac)	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	Val C ₅	ues C ₁₀₀	Imp.
A1	0.70	0.90	0.96	0.01	1.4%	0.45	0.59	0.31	28.8%	0.59	0.70	0.00	0.0%	0.08	0.35	0.38	0.0%	0.26	0.47	30.2%
A2	0.68	0.90	0.96	0.00	0.0%	0.45	0.59	0.43	41.1%	0.59	0.70	0.00	0.0%	0.08	0.35	0.25	0.0%	0.31	0.50	41.1%
A3	0.75	0.90	0.96	0.00	0.0%	0.45	0.59	0.50	43.3%	0.59	0.70	0.00	0.0%	0.08	0.35	0.25	0.0%	0.33	0.51	43.3%
A4	1.00	0.90	0.96	0.64	64.0%	0.45	0.59	0.32	20.8%	0.59	0.70	0.00	0.0%	0.08	0.35	0.04	0.0%	0.72	0.82	84.8%
A5	2.85	0.90	0.96	0.74	26.0%	0.45	0.59	1.56	35.6%	0.59	0.70	0.00	0.0%	0.08	0.35	0.55	0.0%	0.50	0.64	61.5%
A6	0.74	0.90	0.96	0.10	13.5%	0.45	0.59	0.47	41.3%	0.59	0.70	0.00	0.0%	0.08	0.35	0.17	0.0%	0.43	0.58	54.8%
A7	2.03	0.90	0.96	0.69	34.0%	0.45	0.59	0.76	24.3%	0.59	0.70	0.00	0.0%	0.08	0.35	0.58	0.0%	0.50	0.65	58.3%
A8	1.55	0.90	0.96	0.76	49.0%	0.45	0.59	0.52	21.8%	0.59	0.70	0.00	0.0%	0.08	0.35	0.27	0.0%	0.61	0.73	70.8%
A9	0.21	0.90	0.96	0.00	0.0%	0.45	0.59	0.16	49.5%	0.59	0.70	0.00	0.0%	0.08	0.35	0.05	0.0%	0.36	0.53	49.5%
A10	1.35	0.90	0.96	0.00	0.0%	0.45	0.59	1.08	52.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.27	0.0%	0.38	0.54	52.0%
OS1	0.79	0.90	0.96	0.00	0.0%	0.45	0.59	0.79	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
TOTAL (A1-A10)	11.86																			58.3%
TOTAL	12.65																			58.7%

PROPOSED **STANDARD FORM SF-2** TIME OF CONCENTRATION

Subdivision: Sterling Ranch Subdivision - Proposed

Location: El Paso County

Project Name: Sterling Ranch Filing 5 Project No.: 25188.16

Calculated By: DIG

Checked By: RAB

Date: 3/20/23

		SUB-	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME		_	tc CHECK		
		DA	ATA				(T _i)				(T _t)			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t i	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t _c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	0.70	В	30%	0.26	0.47	70	2.2%	9.8	335	0.7%	7.0	0.6	9.3	19.2	405.0	25.8	19.2
A2	0.68	В	41%	0.31	0.50	70	2.0%	9.4	210	1.0%	7.0	0.7	5.0	14.4	280.0	21.4	14.4
A3	0.75	А	43%	0.33	0.51	80	3.6%	8.2	345	1.5%	7.0	0.9	6.7	14.9	425.0	21.7	14.9
A4	1.00	А	85%	0.72	0.82	30	2.0%	3.0	931	1.6%	20.0	2.5	6.2	9.2	961.0	17.6	9.2
A5	2.85	А	62%	0.50	0.64	95	2.0%	8.5	900	1.6%	20.0	2.5	5.9	14.4	995.0	22.3	14.4
A6	0.74	А	55%	0.43	0.58	93	2.6%	8.6	231	1.9%	20.0	2.8	1.4	9.9	324.0	18.3	9.9
A7	2.03	А	58%	0.50	0.65	91	2.0%	8.3	702	1.6%	20.0	2.6	4.6	12.8	793.0	21.4	12.8
A8	1.55	А	71%	0.61	0.73	38	2.0%	4.4	830	1.6%	20.0	2.5	5.5	9.8	868.0	19.7	9.8
A9	0.21	А	50%	0.36	0.53	100	3.5%	8.8	598	1.5%	20.0	2.4	4.1	12.9	698.0	22.7	12.9
A10	1.35	А	52%	0.38	0.54	100	3.5%	8.6	599	1.5%	20.0	2.4	4.1	12.7	699.0	22.2	12.7
OS1	0.79	А	65%	0.45	0.59	88	2.0%	8.8	122	2.0%	10.0	1.4	1.4	10.2	210.0	15.7	10.2
				1													

NOTES:

 $t_c = t_i + t_t$

Where:

te = computed time of concentration (minutes)

ti = overland (initial) flow time (minutes)

 t_t = channelized flow time (minutes).

 $t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$

Where:

 t_t = channelized flow time (travel time, min) $L_t =$ waterway length (ft) So = waterway slope (ft/ft) V_t = travel time velocity (ft/sec) = K $\sqrt{S_o}$ K = NRCS conveyance factor (see Table 6-2).

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$

Where:

Equation 6-2

Equation 6-4

 t_i = overland (initial) flow time (minutes) C_5 = runoff coefficient for 5-year frequency (from Table 6-4) L_i = length of overland flow (ff) S_0 = average slope along the overland flow path (ft/ft).

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1. $L_t =$ length of channelized flow path (ft)

Equation 6-3

i = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

X:\2510000.all\2518816\Excel\Drainage\2518816_ Proposed Conditions.xlsm

Table 6-2. NRCS Conveyance factors, K

Conveyance Factor, K

2.5

5

7

10

15

20

Type of Land Surface

Heavy meadow

Tillage/field

Short pasture and lawns

Nearly bare ground

Grassed waterway

Paved areas and shallow paved swales

Equation 6-5

STANDARD FORM SF-3 - PROPOSED STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

	Subdivision	: Sterli	ng Ranc	h Subd	ivision	-Propc	sed										Pro	ject N Projec	ame: t No.:	2518	ng Rai 8.16	nch Filir	ng 5	
	Location Design Storm	: El Pas : 5-Yea	ir Ir	ty													Cal C	culate hecke	d By: d By:	RAB				
F																		l	Date:	3/20/	/23			
•					DIRE	CT RUI	NOFF	1		T	OTAL R	UNOFF	-	STRE	ET/SW	ALE		PIF	PE		TRAV	/EL TIM	IE	
	STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (CfS)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
			OS1	0.79	0.45	10.2	0.36	4.10	1.5															FLOWS IN SWALE TO DP 1 CONVEY VIA SWALE TO DP2.1
			A2	0.68	0.31	14.4	0.21	3.58	0.8															FLOWS IN SWALE TO DP 1 CONVEY VIA SWALE TO DP2.1
		1								14.4	0.57	3.58	2.0											TOTAL FLOW AT DP1 BASINS OS1 AND A2
		2	A1	0.70	0.26	19.2	0.18	3.15	0.6															FLOWS IN SWALE TO DP 2 CAPTURED IN AREA INLET
		2.1								19.2	0.75	3.15	2.4											AREA INLET PIPED TO DP 5.1
		3	A3	0.75	0.33	14.9	0.25	3.53	0.9															FLOWS IN SWALE TO DP 3 CONVEYED TO DP5
		4	A4	1.00	0.72	9.2	0.72	4.25	3.1															FLOWS IN SWALE TO DP 2 THEN FLOWS TO CURB AND GUTTER TO INLET AT DP 5
										14.9	0.97	3.53	3.4											BASINS A3 AND A4 CONVEYED TO INLET DP5
		5	A5	2.85	0.50	14.4	1.41	3.58	5.1															FLOWS IN CURB AND GUTTER TO DP 5
		1								14.9	2.38	3.53	8.4											BASINS A3-A5
Should this be	•	5.1								19.2	3.13	3.15	9.9											PIPED FROM INLET AT DP 5 TO EX STORM BASINS A1-A5 AND OS1
labeled as DP	25 ,	6	A6	0.74	0.43	9.9	0.32	4.14	1.3															FLOWS INTO DINES BLVD CURB AND GUTTER TO EXISTING INLET
SINCE It'S		7	A7	2.03	0.50	12.8	1.01	3.75	3.8															FLOWS IN CURB AND GUTTER TO ON-GRADE INLET AT DP 7 ON SCHOOLHOUSE ROAD COLLECTED RUNOFF PIPED TO DP8.1. BYPASS RUNOFF TO EX. INLET AT DP11
from other		8	A8	1.55	0.61	9.8	0.94	4.15	3.9															FLOWS IN CURB AND GUTTER TO ON-GRADE INLET AT DP 8 ON SCHOOLHOUSE ROAD COLLECTED RUNOFF PIPED TO DP8.1, BYPASS RUNOFF TO EX. INLET AT DP12
basins at the		8.1								12.8	1.95	3.75	7.3											TOTAL RUNOFF PIPED TO EXISTING STORM SEWER FROM FILING 4
inlet & DP5.1	is	9	A9	0.21	0.36	12.9	0.08	3.75	0.3															FLOWS INTO DINES BLVD AND STERLING RANCH ROAD ULTIMATELY TO EX. ON-GRADE INLET AT DP 13
the ning/intercent	od	10	A10	1.35	0.38	12.7	0.51	3.77	1.9															FLOWS INTO STERLING RANCH ROAD ULTIMATELY TO EX. ON-GRADE INLET AT DP 13
flow?	eu									12.9	0.59	3.75	2.2											BASINS A9-A10 CONVEYED TO EX. INLET AT DP13
		11	RUNO	FF FROM	1 FILING	G 4 DP5			12.0				12.0											TOTAL RUNOFF TO EX. 15' TYPE R INLET PIPED TO DP 14
		12	RUNO	FF FROM	1 FILING	6 4 DP6	.2		2.0				2.0	,	Do	esn	't							TOTAL RUNOFF TO EX. TO: TYPE R INLET PIPED TO DP 14
		13	RUNOF	FF FROM	1 FILING	G 4 DP8			6.1	\leftarrow			8.3	N	ma	tch								PIPED TO DP 14
Ĺ		14	~										29.6											TOTAL RUNOFF PIPED TO EX. POND W-5 List all DP's/Basins
Should this be	e																							contributing
labeled as DF since it's colle flow from othe basins at the	P10, pec ecting er inlet?	S*A val	ies are d	letermir	clude	2/i usin	^{g1} Sr is DP 1	now an ii that	total ncrea	flow ase	v to E or de	DP1: ecreated to D	3, in ase)P1(dica fron	nte ir n Fili m	n rep ing	port No.	if th 4 re	nere epoi	e rt				
X:\2	2510000.all\2518816\Exe	cel\Draina;	ge\2518816	the the the	e ⊢ili ere i	ing l s ar	no. n inc	4 re reas	port. se/de	indi ecrea	cate ase i	n flo	epo ws	rt If										Page 1 of 1 3/21/20

													S	TANE Stof (F	DARD RM DI RATION	FOR RAINA	M SF- AGE SYS THOD P	3 - PI stem rocei	ROP DESI DURE)	OSE GN	D		
Subdivision: Location: Design Storm:	Sterlir El Pas 100-Y	ng Rand o Coun ear	h Subdivi: ty	sion	-Propo	osed										Pi C	roject N Projec alculate Checke	ame: t No.: d By: d By: Date:	Sterlii 25188 DIG RAB 3/20/	ng Ra 8.16 '23	nch Fi	ling 5	
				DIR	ECT RL	JNOFF			Ţ	OTAL F	UNOF	F	STRE	ET/SW	ALE		PIP	E		TRA∖	EL TI	ME	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
		OS1	0.79 (0.59	10.2	0.47	7.51	3.5															FLOWS IN SWALE TO DP 1 CONVEY VIA SWALE TO DP2.1
		A2	0.68	0.50	14.4	0.34	6.73	2.3															FLOWS IN SWALE TO DP 1 CONVEY VIA SWALE TO DP2.1
	1								14.4	0.81	6.73	5.4											TOTAL FLOW AT DP1 BASINS OS1 AND A2
	2	A1	0.70	0.47	19.2	0.33	6.09	2.0															FLOWS IN SWALE TO DP 2 CAPTURED IN AREA INLET
	2.1								19.2	1.14	6.09	6.9											AREA INLE I PIPED TO DP 5.1
	3	A3	0.75	0.51	14.9	0.38	6.66	2.5															FLOWS IN SWALE TO DP 3 CONVEYED TO DP5
	4	A4	1.00 (0.82	9.2	0.82	7.74	6.3															FLOWS IN SWALE TO DP 2 THEN FLOWS TO CURB AND GUTTER TO INLET AT DP 5
									14.9	1.20	6.66	8.0											BASINS A3 AND A4 CONVEYED TO INLET DP5
	5	A5	2.85	0.64	14.4	1.82	6.73	12.3															FLOWS IN CURB AND GUTTER TO DP 5
									14.9	3.02	6.66	20.1											INLET AT DP5 BASINS A3-A5
	5.1								19.2	4.16	6.09	25.3											PIPED FROM INLET AT DP 5 TO EX STORM BASINS A1-A5 AND OS1
	6	A6	0.74	0.58	9.9	0.43	7.57	3.3															FLOWS INTO DINES BLVD CURB AND GUTTER TO EXISTING INLET
	7	A7	2.03	0.65	12.8	1.31	6.99	9.2															FLOWS IN CURB AND GUTTER TO ON-GRADE INLET AT DP 7 ON SCHOOLHOUSE ROAD COLLECTED RUNOFF PIPED TO DP8.1, BYPASS RUNOFF TO EX. INLET AT DP11
	8	A8	1.55 (0.73	9.8	1.13	7.59	8.6															FLOWS IN CURB AND GUTTER TO ON-GRADE INLET AT DP 8 ON SCHOOLHOUSE ROAD COLLECTED RUNOFF PIPED TO DP8.1, BYPASS RUNOFF TO EX. INLET AT DP12
	<u>8</u> 1								12.8	2 11	6 00	17 1											
	0.1								12.0	2.94	0.77	17.1											FLOWS INTO DIRES BLVD AND STERLING RANCH ROAD ULTIMATELY TO EX. ON-GRADE
	9 10	A9 A10	1.35 (0.53 0.54	12.9	0.11	6.98 7.01	0.8															INLEL AL DP 13 FLOWS INTO STERLING RANCH ROAD ULTIMATELY TO EX. ON-GRADE INLET AT DP 13
									12.9	0.84	6.98	5.9											BASINS A9-A10 CONVEYED TO EX. INLET AT DP13
	11	RUNOF	F FROM F	ILING	6 4 DP5			25.9				25.9											TOTAL RUNOFF TO EX. 15' TYPE R INLET PIPED TO DP 14
	12	RUNOF	F FROM F	ILING	4 DP6	.2		6.4				6.4											TOTAL RUNOFF TO EX. 10' TYPE R INLET PIPED TO DP 14
	13	RUNOF	F FROM F	ILING	6 4 DP8			12.9				18.8	4										TOTAL RUNOFF TO EX. 15' TYPE R INLET PIPED TO DP 14
	14											68.1	1										TOTAL RUNOFF PIPED TO EX. POND W-5
es: et and Pipe C	*A valu	ies are o	determined	d by C	⊇∕i usin	ig the ca	atchment	's intens	ity valu	e. –						\mathbf{b}							

Flows do not match with Filing No. 4 report

Appendix C Reference Material



MASTER DEVELOPMENT DRAINAGE PLAN FOR STERLING RANCH

OCTOBER 2018

Prepared for:

Morley-Bentley Investments, LLC 20 Boulder Crescent, 2nd Floor Colorado Springs, CO 80903 (719) 471-1742

Prepared by:



20 Boulder Crescent, Suite 110 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-002 SKP-18-003 SF-17-024

HW/D ratio of ~ 1.3 . The peak detained volume has been estimated at 78.2 ac-ft. A low point in Sterling Ranch Road will be designed adjacent to the facility to provide a safe overflow route. An exhibit showing the concept design and its various elements is included in the appendix of this report.

As previously discussed a Condition Letter of Map Revision and Letter of Map Revision (CLOMR/LOMR) will need to be processed through the Federal Emergency Management Agency (FEMA) to revise the hydrology to the Sand Creek Channel and allow for the remapping of the revised floodplains. It should be noted that the DBPS flow rates for Reach SC-8 (Reach 163) adjacent to this location were estimate to be 2,630 cfs and that the effective FEMA 100 year flow rate is 2,600cfs. A comparison table of the various flow rates is provided later in this text and on the accompanying drainage maps.

The final design of the culvert crossing and final determination of approved rates as well as the final pond design will be discussed within the future Sterling Ranch Channel Design Report and Sand Creek CLOMR/LOMR documents. No deviations for this pond and accompanying outlet structure are anticipated at this time.

It is important to note that the planned discharge outlet pipe for the FSD pond located to the west of the pond W3 will need to be extended to the downstream outlet side of the culvert to ensure that the 100 year water surface elevation with W3 does not affect the functionality of the adjacent FSD and its storm sewer systems.

In regards to timing, the need to construction this facility can be tied to the Sand Creek Channel improvements which is discussed within this report and also within the Subdivision Improvements Agreement. In no case should runoff from the East Fork of Sand Creek be diverted to the Main Branch of the Sand Creek Channel prior to the construction and of this facility.

Basin SC3-11A (Q5 = 7.8 cfs, Q100 = 24.3 cfs) consists of a 10.7 acre area located within of Sterling. Ranch, that is south of Sterling Ranch Road, west of Sand Creek. This portion of Sterling Ranch consists of single family residential for lots ranging in size from 0.2 to 0.3 acres in size and open space associated with the Sand Creek Channel. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems to a full spectrum detention pond FSD11A. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 0.9 cfs and 12.3 cfs in the 5 and 100 year events respectively just upstream of DP-63. It should be noted that this detention facility may not be necessary if grading can be oriented to force surface runoff to the west.

Basin SC3-11B (Q5 = 81.3 cfs, Q100 = 213.7 cfs) consists of a 76.6 acre area located within of Sterling. Ranch, that is south of Sterling Ranch Road, east of Sand Creek. This portion of Sterling Ranch consists of single family residential planned for lots ranging in size from 0.2 to 0.3 acres in size and a portion of a park site and collector roadways. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems westward to a full spectrum detention pond FSD11B. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 4.5 cfs and 69.5 cfs in the 5 and 100 year events respectively. The runoff from DP68 and from FSD ponds 11A and 11B combine at DP63 at peak flow rates of Q5 = 201.0 cfs, Q100 = 1385.1, which is less than the anticipated existing modeled flow rates of Q5 = 430.7 cfs, Q100 = 1911.5 at DP63. Runoff from DP63 continues south within the Sand Creek Channel toward DP61.

Basin SC3-7 (Q5 = 69.9 cfs, Q100 = 157.2 cfs) consists of a 45.7 acre industrial zoned area, referred to as the Barbarick Subdivision, located outside of Sterling Ranch. Per the Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3 and 4 the filing consists of four lots which upon which development will be constructed which will include adding a proposed Extended Detention Basin within Lot 4. This detention basin will provide water quality treatment for portions of Lots 1 & 2, and Lots 3 & 4. The EBD will structure will outfall at the south end of Lot 4 at the Barbarick Subdivision/Sterling Ranch property line. Per the report the proposed total outflow from the EDB pond will be Q5 = 0.3 cfs, Q100 = 45.9** cfs(**which includes pass through flows of 29.4 cfs). A second Sand Filter Basin water quality detention catchment will be provided at the southeast/downstream end of Lot 2. The SFB will outfall at the southeast corner of the Lot 2 at the Barbarick Subdivision/Sterling Ranch property line. Per the report the proposed total outflow the SFB pond will be Q5 = 0.1 cfs, Q100 = 3.6 cfs. At the initial writing of this report, neither EDB nor SFB structure has been fully constructed, and thus the assumption was made to utilize the full un-detained untreated runoff from the offsite development for onsite drainage planning purposes. Thus the downstream facilities planned within Sterling Ranch will account for the total un-detained runoff from the parcel of Q5 = 69.9 cfs, Q100 = 157.2 cfs and will plan to treat the total runoff onsite facilities. This provides a conservative approach for master planning. Runoff discharged from the property will be collected by proposed storm sewer within Sterling Ranch and routed to DP64. These facilities and their effects on drainage will be re-reviewed with subsequent drainage report and shall be implemented into final design and construction.

Basin SC3-6B (Q5=43.4 cfs, Q100=102.7 cfs) consists of a 30.9 acre area located within of Sterling Ranch, that is north of Sterling

Ranch Road and west of Sand Creek. This portion of Sterling Ranch will consist of single family residential planned for lots ranging in size from 0.1 to 0.33 acres in size, a school site and portion of the local collector roadways. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems where it combines with flows from Basin SC3-7 at DP64 (Q5 = 112.1 cfs, Q100 = 258.0 cfs). The combined runoff continues south toward Pond FSD6.

Basin SC3-6A (Q5=79.3 cfs, Q100=177.1 cfs) consists of a 49.3 acre area located within of Sterling Ranch, that is north and east of Marksheffel Road and of Sterling Ranch Road and west of Sand Creek. This portion of Sterling Ranch is planned for a commercial site and single family residential lots ranging in size from 0.2 to 0.3 acres lots as well as portions of major and local collector roadways. Developed runoff from the basin shall be conveyed within street sections and storm sewer systems and directed to FSD Pond 6.

Basin SC3-6C (Q5=72.5 cfs, Q100=181.5 cfs) consists of a 58.0 acre area located mostly within the confines of Sterling Ranch, near the south boundary of the site, west of the Sand Creek Channel. This portion of Sterling Ranch is planned for a commercial site and single family residential lots ranging in size from 0.2 to 0.3 acres lots as well as portions of major and local collector roadways. A small segment of the existing Pawnee Rancheros subdivision (5 acres lots) also falls within the basin. Where not sheet flowing into the creek, the developed runoff from the basin shall be conveyed within street sections and storm sewer systems and directed to FSD Pond 6. Runoff from DP64 and from Basins SC3-6B and 6C will combine in FSD6. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 7.5 cfs and 149.6 cfs in the 5 and 100 year events respectively. Flows from FSD6 outfall into the Sand Creek Channel at DP61.

Basin SC3-8 (Q5 = 42.1 cfs, Q100 = 166.2 cfs) consists of 143.4 acres located outside of Sterling Ranch and to the west of Basin SC3-15A. In the developed condition, it is assumed that the remaining large parcel are fully developed into 5 acres lots. Runoff from the basin is conveyed as surface flows to Basin SC3-9.

Basin SC3-9 (Q5 = 71.5 cfs, Q100 = 254.0 cfs) consists of 217.4 acres located to northwest of Vollmer Road and south of Basin SC3-8. In the current condition, much of the large parcel has been developed into 2.5-5 acres lots. The calculated runoff will assume that that Vollmer Road is widened as a part of this project. Runoff from Basins SC3-8 and SC3-9 combine within the roadside ditches and natural drainage ways within the development before combining within an upgraded roadside swale located along the west side of Vollmer Road which discharges into a full spectrum detention pond (FSD9) located at the south end of the basin. The treated detained flows from the pond are conveyed under Vollmer and along Marksheffel Road within a storm drain or stabilized channel to Sand Creek at peak flow rates of 24.9 cfs and 289.9 cfs in the 5 and 100 year events respectively just downstream of DP-61.

Basin SC3-10 (Q5 = 12.3 cfs, Q100 = 47.7 cfs) consists of 36.0 acres (located outside of Sterling Ranch), of the existing Pawnee Rancheros Filing No 2 (5 acre lots), that is located to the east of Basin SC3-6. Runoff from the basin is conveyed as surface drainage to the Sand Creek Channel, where it combines with flows discharged from FSD Ponds 6 and 9 and from DP 63 at the County/City Boundary (DP-61) at peak flow rates of 223.9 cfs and 1620.1 cfs in the 5 and 100 year events respectively. It is anticipated that easements from the owner of the property located to the south of the Sterling Ranch will be required to outfall the storm sewer from FSD6 and FSD9 as well as provide an emergency overflow route. Runoff from DP61 continues south within the Sand Creek Channel toward DP60A.

Basin SC3-5A (Q5 = 53.7 cfs, Q100 = 129.1 cfs) is a 39.1 acres offsite area located to the south of Sterling Ranch, west of the Sand Creek Channel. In the developed condition, it is assumed that this area will be developed into 0.1 acre residential lots, portions of Marksheffel Road and stabilized segments of the Sand Creek Channel. Runoff produced from within the basin shall be directed to a proposed full spectrum detention facility (FSD5) located at the southeast corner of the basin upstream of DP-60A. Released flows from the pond will discharge into Sand Creek at peak flow rates of 1.4 cfs and 30.1 cfs in the 5 and 100 year events.

Basin SC3-61 (Q5 = 22.0 cfs, Q100 = 84.8 cfs) is a 65.5 acres offsite area located to the south of Sterling Ranch east of Basin SC3-5B, that is made up of 5 acre lots. With the development of filing SC3-5B, a storm sewer bypass line will be constructed to safely convey the upstream runoff thru the development to the channel just upstream of DP-60A.

Basin SC3-5B (Q5 = 73.0 cfs, Q100 = 187.0 cfs) is a 63.0 acres offsite area located to the south of Sterling Ranch east of Basin SC3-5A. In the developed condition, it is assumed that the majority of the area will be subdivided into 0.1 acre residential lots. Water quality treatment only is anticipated for this area and thus a FSD pond has not been included in the modeling. Runoff produced from within the basin shall be directed to Sand Creek just upstream of DP-60A. The runoff from DP61, FSD5 and from Basins SC3-5B and SC3-61 combine at DP60A at peak flow rates of Q5 = 224.8 cfs, Q100 = 1661.8, which is less than the anticipated existing modeled flow rates of Q5 = 430.2 cfs, Q100 = 1913.5 at DP60A. Runoff from DP60A continues south within the Sand Creek Channel toward



| ROAD STAR \$40. |
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(CFS)
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(CFS)
33.0
 | Q 25
(CFS)
45.8 | Q50
(CFS)
57.1
 | Q100
(CFS)
68.9 | |
| J. C. | SC3-5A
SC3-5B
SC3-6A
 | 84
81
88 | <u> </u>
 | 0.061
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61.4 | 53.7
73.0
79.3
 | 71.0
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130.1 | 110.6
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 | 129.1
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| SS JAS VE | SC3-6B
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 | 85
82
88 | 30.9
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45.7
 | 0.048
0.091
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53.9
54.0 | 43.4
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 | 57.0
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| 555. 2120 | SC3-8
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 | 62
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63 | 143.4
217.4
.36.0
 | 0.224
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 | 66.7
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29.1 | 132.3
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38.0
 | 166.2
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| 3-79 | SC3-11A
SC3-11B
 | 70
80
81 | 10.7
76.6
 | 0.017 | 5.3
59.4 | 7.8
81.3
 | 11.3
110.8
 | 15.9
148.1 | 20.0
180.5
 | 24.3
213.7 | |
| | SC3-13
SC3-14A
 | 85
79 | 41.0
164.9
 | 0.138 | 43.9
127.6 | 57.8
175.4
 | 76.0
239.8
 | 98.5
321.9 | 117.6
393.2
 | 136.9
466.3 | |
| | SC3-14B
SC3-15A
SC3-15B
 | 77
62
87 | 34.7
139.7
7.9
 | 0.054
0.218
0.012 | 24.6
21.3
10.8 | 34.3
35.5
14.0
 | 47.4
56.3
18.2
 | 64.2
85.3
23.3 | 79.0
112.1
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 | 94.1
141.0
31.9 | |
| | SC3-16A
SC3-16B
SC3-17
 | 74
78
73 | 168.1
50.7
70.6
 | 0.263
0.079
0.110 | 84.4
39.0
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53.7
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 | 351.8
143.8
180.6 | |
| PAD 7245 | SC3-18
SC3-19
 | 81
62 | 53.8
184.0
 | 0.084 | 49.3
28.8 | 67.1
47.7
 | 91.0
75.7
23.8
 | 121.2
114.4
35.1 | 147.3
150.2
 | 174.0
188.8 | |
| | SC3-20
SC3-21
SC3-22
 | 66
65 | 23.3
 | 0.036 | 9.9
7.0
9.4 | 10.8
14.8
 | 16.3
22.5
 | 23.7 | 40.0
30.4
42.5
 | 37.5
52.6 | |
| | SC3-23
SC3-24A
SC3-24B
 | 67
65
65 | 14.5
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| | SC3-25
SC3-26
SC3-27
 | 66
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71 | 19.0
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 | 31.0
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| 7359 | SC3-61
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 | 63
64
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 | 0.102
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 | 34.4
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41.3
 | 51.6
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81.3
 | 84.8
76.0 | |
| | SC3-74
SC3-75
 | 63
63 | 119.7
79.3
 | 0.187 | 22.3 | 36.5
21.5
 | 57.3
33.7
 | 85.9
50.5 | 112.3
66.1
 | 140.7
82.8 | |
| | SC3-76
SC3-77
SC3-78
 | 63
62
63 | 86.4
106.9
155.6
 | 0.135
0.167
0.243 | 14.2
16.6
28.1 | 23.1
27.6
45.3
 | 36.4
43.8
70.6
 | 54.6
66.2
106.2 | 71.4
87.0
139.1
 | 89.6
109.4
174.5 | |
| WG I I I I I I I I I I I I I I I I I I I | SC3-79
SC3-80
SC3-81
 | 63
63
62 | 189.0
147.7
262.9
 | 0.295
0.231
0.411 | 34.9
27.3
42.6 | 57.0
44.3
70.2
 | 89.5
69.6
111.0
 | 134.3
104.5
167.4 | 175.6
136.8
219.6
 | 220.1
171.4
275.7 | |
| | SC3-82
SC3-88
SC3-89
 | 62
62
62 | 117.8
60.2
27.5
 | 0.184
0.094
0.043 | 20.0
10.5
6.1 | 33.2
17.4
10
 | 52.8
27.6
15.7
 | 80.0
41.8
23.6 | 105.1
54.9
30.8
 | 132.3
69.0
38.6 | |
| | SCE-1
SCE-2
 | 65
64
70 | 64.4
15.0
 | 0.101 | 23.3 | 35.9
7.0
 | 53.8
10.8
 | 79.1 | 102.4
20.7
 | 127.4
25.7 | |
| | SCE-5
SCE-5
 | 70 70 87 | 29.5
85.5
 | 0.046 | 13.3
100.4 | 43.2
19.6
130.6
 | 28.6
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 | 40.6
217.4 | 257.8
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 | 62.6
298.4 | |
| SCE-13 | SCE-6
SCE-7
SCE-8
 | 64
89
92 | 3.8
44.9
25.5
 | 0.006
0.070
0.040 | 1.6
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38.6 | 2.5
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48.4
 | 3.7
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 | 5.4
122.2
75.4 | 7.0
143.7
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 | 8.6
165.2
99.9 | |
| | SCE-9
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 | 64
83
64 | 4.0
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 | 0.006
0.272
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7.6
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 | 3.6
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 | 5.3
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8.0 | 6.8
398.9
10.3
 | 8.5
467.5
12.8 | |
| SCE-2 | SCE-13
 | 63 | 78.6
 | 0.123 | 19.6 | 31.3
 | 48.7
 | 73.1 | 95.7
 | 120.0 | |
| | SCE = 14
 | 63
51 | 52.5
 | 0.082 | 13.2 | 21.2
 | 33.3
 | 49.9 | 65.2
 | 81.7
33.4 | |
| 1 1E
RT-1E | SCE-14
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 | 51 | 52.5
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 | 33.3
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33.4 | |
| OLD SETTLERS TRAIL | DESIGN
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DP-74
 | 65
51
AREA
(sq MI)
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Q ₂
(CF5)
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 | 0.082
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N POIN
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T SUM
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 | 49.9
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LOCA | TION |
| OLD SETTLERS TRAIL | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78
 | 6.5
51
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33.4
LOCA
RROYA LA | TION |
| DLD SETTLERS TRAIL | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-72 DP-71
 | 65 51 AREA (s0 MI) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 | 52.5
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A
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LOCA
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S RANCH 1 | ANE X-ING
AD X-ING
NORTHERN BNDRY |
| DLD SETTLERS TRAIL | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-73 DP-72 DP-71 DP-70 DP-70 DP-70
 | 6.3 51 AREA
(so MI) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 | 52.5
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LOCA
RROYA LA
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RANCH I
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AD X-ING
NORTHERN BNDRY
RKWAY X-ING |
| DLD SETTLERS TRAIL | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-72 DP-71 DP-70 DP-69 DP-87 DP-68 DP-64 DP-63
 | 65 51 AREA
(so MI) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 |
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LOCA
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ANE X-ING
AD X-ING
NORTHERN BNDRY
RKWAY X-ING
DF POND W3
SOUTHERN BNDRY |
| DLD SETTLERS TRAIL | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-73 DP-72 DP-71 DP-70 DP-69 DP-68 DP-64 DP-63 DP-60A
 | 6.3 51 AREA
(so MI) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 5.356 5.617 |
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A
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LOCA
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AD X-ING
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RKWAY X-ING
DF POND W3
SOUTHERN BNDRY
S/EL PASO BNDRY
FEL X-ING
AND DOND 3 |
| 1 IE OLD SETTLERS TRAIL
RT-IE
SCE-14
SCE-14
SCE-14
SCE-4
SCE-4
FSD-E2
SCE-4
SCE-4
SCE-4
SCE-4
SCE-6 | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-73 DP-74 DP-78 DP-70 DP-60 DP-61 DP-60A DP-53A DP-2E DP-2E
 | 6.3 51 AREA
(sq M) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 5.356 5.617 5.661 0.247 0.486 | 52.5
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LOCA
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STREAM C
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S RANCH 1
C SPRINGS
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ANE X-ING
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RKWAY X-ING
OF POND W3
SOUTHERN BNDRY
S/EL PASO BNDRY
FEL X-ING
AND POND 3 |
| CLD SETTLERS TRAIL | SCE-14 SCE-15 SCE-15 DP-71 DP-77 DP-78 DP-73 DP-74 DP-78 DP-70 DP-71 DP-70 DP-70 DP-71 DP-70 DP-71 DP-72 DP-73 DP-74 DP-75 DP-69 DP-61 DP-61 DP-63 DP-53A DP-1E DP-2E DP-3E DP-4E DP-56
 | 6.3 51 AREA
(so MI) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 5.356 5.617 5.661 0.247 0.486 0.626 0.745 1.017 | 52.5
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 | 33.3 10.1 Q.59 209.1 750.9 1168.4 306.2 1187.2 1195.3 1226.9 1260.6 1364.1 1471.5 1674.9 222.6 1112.1 1287.3 1320.5 1326.0 173.0 319.7 387.1 407.3 152.1
 | 49.9
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MARY
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LOCA
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OF POND W3
SOUTHERN BNDRY
S/EL PASO BNDRY
FEL X-ING
AND POND 3
SOUTHERN BNDRY
FEL X-ING
AND POND 3 |
| DLD SETTLERS TRAIL | SCE-14 SCE-15 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-73 DP-70 DP-71 DP-70 DP-70 DP-69 DP-64 DP-63 DP-64 DP-63 DP-61 DP-53A DP-1E DP-2E DP-3E DP-4E DP-56 DP-3E DP-22
 | 6.3 51 AREA
(so M) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 5.356 5.617 5.661 0.247 0.486 0.626 0.745 1.017 1.079 0.396 0.342 | 52.5 39.7 39.3 141.2 209.9 59.7 207.5 206.2 205.3
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I SUM
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33.4
LOCA
RROYA LA
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RANCH I
RGATE PA
STREAM C
STREAM STREAM | ANE X-ING
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AD X-ING
NORTHERN BNDRY
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OF POND W3
SOUTHERN BNDRY
S/EL PASO BNDRY
FEL X-ING
AND POND 3
COP CORNER
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 | 6.3 51 AREA
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STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (C STORED VOLUME (AC-FSD5 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (C STORED VOLUME (AC-FSD6 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD9 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD11A STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (C STORED VOLUME (AC-FSD11B STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD12 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD13 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD14A TORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (C STORED VOLUME (AC-FSD14B STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (CF STORED VOLUME (AC-FSD15B STORM EVENT (YR) DRY PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (CF STORED VOLUME (AC-

FSD1

STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (CI STORED VOLUME (AC-

FSD16A

DBPS DESIGN POINT DP-50 P-51 (BASIN 86) DP-52 DP-56

Values reported from SCDE DBPS Reach 85(Basin91)=



WATER QUAL	TY & [DETEN	TION PO	ND SUN	MARY	, ,		TY&D	ETENTI	ION PO	ND SUI	MMARY	
EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR) PEAK INFLOW (CFS)	2 39.0	5	10 73.6	25 99.0	50	100
NFLOW (CFS) ABLE RELEASE (CFS)	16.3 0.1	23.3 1.7	33.0 3.3	45.8 10.9	57.1 17.5	68.9 25.5	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.0	0.4	0.7 0.7	8.3 7.9	17.2 17.2	28.2 28.1
ED RELEASE (CFS) D VOLUME (AC-FT)	0.1	1.6 2.6	3.2	10.9 3.6	17.4 1.9	25.4 2.2	STORED VOLUME (AC-FT)	3.0	3.9	5.1	5.1	5.3	5.8
EVENT (YR)	2	5	10	25	50	100	FSD17 STORM EVENT (YR)	2	5	10	25	50	100
NFLOW (CFS)	40.6	53.7	71.0	92.4	110.6 19.8	129.1	ALLOWABLE RELEASE (CFS)	41.8 0.7	<u> </u>	85.2 22.5	52.0	67.2	86.3
ED RELEASE (CFS) D VOLUME (AC-FT)	0.1	1.4	2.6	11.2 4.1	<u>19.8</u> <u>19.7</u> 4.7	30.1 5.2	STORED VOLUME (AC-FT)	0.7 2.6	8.4 2.6	22.4	52.0 3.4	67.2 4.0	4.7
							FSD18 STORM EVENT (YR)	2	5	10	25	50	100
EVENT (YR) NFLOW (CFS)	2 196.5	5 258.5	10 5 339.1	25 438.7	50 523.3	100 608.6	PEAK INFLOW (CFS)	49.3	67.1 9.2	91.0 18.4	121.2 42.2	147.3	174.0
ABLE RELEASE (CFS) ED RELEASE (CFS)	0.5 0.5	7.6	14.6 14.5	58.4 58.2	99.6 99.6	149.7 149.6	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.6	6.3 3.2	18.4	42.2	54.6 4.7	<u>69.6</u> 5.3
D VOLUME (AC-FT)	15.5	16.4	18.7	20.8	23.3	26.0	FSD20						
event (yr)	2	5	10	25	50	100	STORM EVENT (YR) PEAK INFLOW (CFS)	2 9.9	5 15.5	10 23.8	25 35.1	50 45.5	100 56.6
NFLOW (CFS) Able release (CFS)	64.6 1.7	105.6 24.9	169.5 49.8	252.3 141.1	327.1 207.2	410.1 290.0	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.4	5.5 2.8	11.1 10.9	25.7 25.7	33.2 33.0	42.5
ED RELEASE (CFS) D VOLUME (AC-FT)	1.7 8.7	24.9 8.7	49.8 9.6	141.1 10.8	207.0 12.3	289.9 13.8	STORED VOLUME (AC-FT)	0.7	0.8	0.8	0.9	1.0	1.2
EVENT (YR)	2	5	10	25	50	100	FSD21 STORM EVENT (YR)	2	5	10	25	50	100
NFLOW (CFS) Able release (CFS)	5.3 0.1	7.8	11.3 3.2	15.9 7.5	20.0 9.7	24.3 12.4	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	7.0 0.3	10.8 4.0	16.3 8.0	23.7 18.3	30.4 23.7	37.5 30.3
ED RELEASE (CFS) D VOLUME (AC-FT)	0.2	0.9	3.0 0.4	7.5 0.4	9.7 0.5	12.3 0.6	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.3	3.3 0.5	8.0 0.5	18.3 0.6	23.7 0.7	30.1 0.8
3	1						FSD22						
EVENT (YR) NFLOW (CFS)	2 59.4	5 81.3	10 110.8	25 148.1	50 180.5	100 213.7	STORM EVENT (YR) PEAK INFLOW (CFS)	2 9.4	5	10 22.5	25 32.9	50 42.5	100 52.6
ABLE RELEASE (CFS) ED RELEASE (CFS)	0.3	4.5	8.7	29.6 29.5	47.7	69.6 69.5	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.4	5.8	11.5	26.5 26.5	34.3	43.9
D VOLUME (AC-FT)	4.8	4.9	5.5	6.4	7.3	8.2	STORED VOLUME (AC-FT)	0.6	0.6	0.7	0.8	0.9	1.0
EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100
ABLE RELEASE (CFS)	0.9	105.6	26.7	189.1 62.0	80.2	270.0	ALLOWABLE RELEASE (CFS)	0.2	0.3 2.4	4.9	11.2	14.5	20.4 18.6
ed Release (CFS) D Volume (AC-FT)	0.9	<u>9.0</u> 5.5	5.8	61.9 6.7	7.8	103.1 8.9	STORED VOLUME (AC-FT)	0.2	0.3	4.9 0.4	0.4	0.5	0.6
		5	10	25	50	100	FSD27	0	_	10	25	50	100
NFLOW (CFS)	43.9	57.8	76.0	25 98.5	117.6	136.9	PEAK INFLOW (CFS)	38.8	57.6	84.1	25 119.7	159.2	206.3
ED RELEASE (CFS)	0.4	4.2	12.3	28.6	36.9	47.0	MODELED RELEASE (CFS)	1.4	18.4 2.8	42.4	97.0	126.2	161.9
	0.1	0.1	0.0	5.0	+.+	0.0	FSD72	2.1	2.0	2.5	J.Z	0.7	<u>+.</u> ∠
EVENT (YR) NELOW (CES)	2	5	10	25 321.9	50 393.2	100	STORM EVENT (YR) PEAK INFLOW (CES)	2	5	10	25 46 7	50 60.9	100 76.0
ABLE RELEASE (CFS) ED RELEASE (CFS)	0.5	7.5	14.4	56.2 56.2	95.2 95.1	142.4	ALLOWABLE RELEASE (CFS)	0.6	9.6	19.3 19.2	44.4	57.4	73.4
D VOLUME (AC-FT)	9.9	10.6	11.9	13.5	15.3	17.3	STORED VOLUME (AC-FT)	1.0	1.0	1.1	1.1	1.2	1.3
B Event (yr)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100
NFLOW (CFS) Able release (CFS)	24.6 0.0	34.3 0.3	47.4 0.5	64.2 5.7	79.0 11.8	94.1 19.3	MODELED RELEASE (CFS)	214.0 154.3	200.3	366.8	799.9	1074.9	1350.6
ED RELEASE (CFS) D VOLUME (AC-FT)	0.0	0.3	0.5	4.5 3.5	11.8 3.5	19.3 3.8	FSD-E1	2.0	5.5	20.0	-1.2	57.2	/0.2
3							PEAK INFLOW (CFS)	2 23.3	5 35.9	10 53.8	25 79.1	50 102.4	100
EVENT (YR) NFLOW (CFS)	2 10.8	5 14.0	10 18.2	25 23.3	50 27.6	100 31.9	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.7	5.4	19.9	50.9 48.9	65.7	84.1
ABLE RELEASE (CFS) ED RELEASE (CFS)	0.1	1.6	3.2 3.2	7.3 7.3	9.5 9.5	12.0 12.0	FSD-E2	1.5	1.3	1.5	1.8	I	2.5
) VOLUME (AC-FI)	0.6	0.6	0.7	0.8	0.9	1.0	STORM EVENT (YR) PEAK INFLOW (CFS)	2 30.6	5 45.2	10 65.9	25 93.3	50 118.0	100 143.9
EVENT (YR)	2	5	10	25	50	100	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.6	9.5 3.2	19.2 18.5	45.5	59.8 58.5	77.6
ABLE RELEASE (CFS)	84.4 0.6	8.8	170.0	234.8 56.2	88.4	351.8 128.3	FSD-E3	2.1	2.3	2.4	2.8	3.3	3.8
D RELEASE (CFS) D VOLUME (AC-FT)	7.6	7.7	8.9	56.2 10.4	12.1	128.3	STORM EVENT (YR) PEAK INFLOW (CFS)	2 100.4	5 130.6	10 169.6	25 217.4	50 257.8	100 298.4
	SAN	D CRE	EK FLOW	I	7		ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.9 1.0	13.2 6.8	26.5 25.7	61.6 56.0	79.8 79.8	102.6 101.3
DESIGN	COMF		DN CHAR		_		STORED VOLUME (AC-FT)	7.0	7.2	7.7	8.9	10.1	11.4
POINT DP-77	(sq мі) 2.343	(cFs) 1468	PROPOSED (CONDITION			STORM EVENT (YR) PEAK INFLOW (CES)	2	5	10	25 122.2	50 143.7	100
	2.91	2262 2600	SAND CREE	ek dbps A			ALLOWABLE RELEASE (CFS)	0.3	4.4	8.8 8.7	23.0	32.2	43.7
DP-71	2.757	1612 2260	PROPOSED (SAND CREE	CONDITION EK DBPS			STORED VOLUME (AC-FT)	4.2	4.3	4.7	5.4	6.2	6.9
DP-63	4.449	1385	PROPOSED (CONDITION			STORM EVENT (YR)	2	5	10	25	50	100
	4.33	2630 2600	SAND CREE	ek dbps A			ALLOWABLE RELEASE (CFS)	0.0	40.4 0.2	0.4	4.2	8.7 5 1	99.9 14.3
DP-60A	5.661 5.38	1662 3295	PROPOSED (SAND CREE	CONDITION EK DBPS			STORED VOLUME (AC-FT)	3.0	3.7	0.5 4.4	4.8	5.0	5.3
							FSD-E6 STORM EVENT (YR)	2	5	10	25	50	100
SL	JMMAF	S DES RY (PE	AK FLOW	() ()			PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	141.6 0.2	189.4 1.9	252.5 3.2	331.4 37.4	398.9 77.3	467.5
DBPS DESIGN AR POINT (SO	EA (Q10 CFS) EXIST)	Q100 ARI (CFS) (SQ (EXIST) (SQ	A Q1 (CFS (CFS) (PRO	0 Q1)) (CF P) (PR	100 FS) OP)	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.2	0.9	3.2 21.9	18.3 22.2	64.1 22.6	123.3 23.7
DP-50 0. -51 (BASIN 86) 0.	32 4 33 1	7.0 1 7.7	95.7 0.3 74.1 0.3	32 146 33 110	.7 <u>37</u> (.0 23.	0.3 3.5	PND-E7 STORM EVENT (YR)	2	5	10	25	50	100
DP-52 1.6 DP-56 0.7	67 8 79 6	0.5 4 3.6 2	56.5 1.6 265.0 0.7	57 120 79 513	7.9 212 .0 908	3.0 8.2	PEAK INFLOW (CFS) MODELED RELEASE (CFS)	46.5 23.1	75.4 35.3	121.2 71.5	285.2 108.3	402.4 152.1	548.0 196.4
ies reported from SCDBPS, ([S Reach 85(Basin91)=Q10=2	0P 50, 51, 5 8.8cfs Q10 (EXISTING	2 Not analyz 0=115.2cfs /)	ed as a part of t Q10=345.7cfs (PROPC)	nis study) Q100=588.9cfs (SED)	3		STORED VOLUME (AC-FT)	1.0	1.8	4.6	10.5	17.9	28.0
				,			2018 5	TFRII	NG R	ANCH	MDL)P	
						NT, SUITE 110							
				PHONE: 7	19.955.5485		DEVELOPED H	HYDR	ULUG	IC CO	NDITI	UNS	MAP

CIVIL CONSULTANTS, INC.

SCALE DESIGNED BY: JD DRAWN BY: JD HORIZ: 1"=2400' CHECKED BY: VAS

VERT: 1"=2400'

PROJECT NO. 09-002 | FILE: \dwg\Eng Exhibits\2018-MDDP-PROPCOND.dwg DATE: 10-21-2018

DM2

SAND CREEK DRAINAGE BASIN PLANNING STUDY

PRELIMINARY DESIGN REPORT

CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO



PREPARED FOR:

City of Colorado Springs Department of Comprehensive Planning, Development and Finance Engineering Division 30 S. Nevada Colorado Springs, Colorado 80903

PREPARED BY:

Kiowa Engineering Corporation 1011 North Weber Colorado Springs, CO 80903



Land Use Classification	Percent Impervious	Land Use Density
Multi-Family Residential	65-80	10-24 DU/AC
Single-Family Residential	45-65	6-10 DU/AC
Low Density Residential	30-45	1-6 DU/AC
Large Lot Residential/ Agricultural	5-20	1 DU/AC
Office/Commercial	80-90	
Industrial	85-95	
Institutional	50-75	
Dedicated Open Space/Park	5-10	
Rangeland - Poor to Good Condition	5-20	

NOTE: The above data was used in the preparation of the hydrologic analysis for the Sand Creek Drainage Basin Planning Study. These data are not intended to reflect future land use planning within the City or the County.

Table III-1. Percent Impervious Values.

Table III	I-2:	Summary 24-hour D Baseline Hy	of P Durati drolo
Design Point	Location	Area s.m.	100 Ex:
	SAND CREEK (1)		
1	@ Fountain Creek	54.1	
12	Hancock Blvd.	53.1	
19	Fountain Blvd.	50.7	
27	C D L & D D D	23.0	
99 20	U.K.I. & F. KK	10.0	
20	Statson Hills Blvd	10.0	
60	Woodmen Road	5.4	
75	Black Forest Road	1.4	
	WEST FORK SAND CR	EEK	
27	@ Sand Creek	5.0	
52	U.S. 24	4.8	
59	Constitution Ave.	2.1	
69	South Carefree	1.0	
	CENTER TRIBUTARY	SAND CRE	EK
42	Airport Road	1.6	
43	Powers Blvd.	1.3	
44	U.S.24	1.1	
45	Galley Road	0.8	
	EAST FORK SAND CRE	EEK	
1	@ Center Tributary	24.3	
9	@ East Fork Sub. Tributary	19.8	
29	@ W. Bierstadt Creek	10.6	
40	@ Tamlin Road	4.6	
52	@ Woodmen Road	1.7	
	EAST FORK SUB-TRIB	UTARY SA	ND
11	@ Constitution Avenue	5.9	
15	@ Chicago & Rock Island RR	5.2	
26	@ Confluence w/Toy Ranch	1.0	
47	@ Proposed Dublin Blvd.	0.4	
	WEST BIERSTADT CRI	EEK	
31	@ Confluence w/ East Fork	1.8	
39	@ Tamlin Road	0.8	
54	@ Woodmen Road	0.5	
	EAST BIERSTADT CRE	EK	
32	@ Conf. w/W Bierstadt	2.4	
38	@ Chicago & Rock Island RR	0.4	

(1) Future baseline condition discharges for Sand Creek compiled with the assumption that the discharges from the East Fork Sand Creek basin are maintained at existing rates as shown on this Table.

Peak Discharges ration Storm, AMC-II plogic Conditions

100-year (cfs) Existing	Future	10-year (cfs) Existing	Future
16900	25800	7470	11800
16100	25000	7250	11600
13600	22100	6230	10800
11300	18900	5920	8790
5820	14530	2360	7400
4030	10260	1520	4810
3230	6690	840	3060
2630	3300	760	950
1000	1030	320	350
(940	(840	2000	2000
6840	6840	3200	3200
0860	0800	3230	3230
3430	3430	1680	1680
1650	1650	810	810
K			
1530	2010	650	1200
1300	1710	590	980
1200	1680	580	960
1180	1340	530	650
3970	15600	700	6530
3730	13990	650	6050
2080	7460	400	3330
950	3570	210	1820
460	2120	80	1210
D CREEK			
1330	4100	240	1630
1250	3540	240	1370
220	820	230 50	370
100	300	20	140
100	500	20	140
100	1500	90	(00
480	1390 200	80 50	200
270	060 120	JU 57	290
230	420	cc	150
520	1520	۵n	580
120	350	15	120
120	550	15	150



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Worksheet for FSD Outlet Orifice Plate

Project Description	a.			
Solve For	Diameter			
Input Data				
Discharge		45.90	ft³/s	(16.5 His+29.4 Asc)
Headwater Elevation		4.70	ft	
Centroid Elevation		0.00	ft	
Tailwater Elevation		0.00	ft	
Discharge Coefficient		0.60		
Results				
Diameter		2.37	ft	
Headwater Height Above Centroid		4.70	ft	
Tailwater Height Above Centroid		0.00	ft	
Flow Area		4.40	ft²	
Velocity		10.43	ft/s	

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Worksheet for FSD Overflow - Pass

Discharge			
	0.90	ft	
	0.00	ft	
	0.00	ft	
Gravel			
	12.00	ft	
:	36.00	ft	
1	86.22	ft³/s	(55Dul+29.4) pres = 44.4 2)
	0.90	ft	1
	0.00	ft	
	2.80	US	
	1.00		
	2.80	US	
1	32.40	ft²	
	2.66	ft/s	
	37.80	ft	
	36.00	ft	
	Discharge Gravel	Discharge 0.90 0.00 Gravel 12.00 36.00 86.22 0.90 0.00 2.80 0.00 2.80 1.00 2.80 32.40	Discharge 0.90 ft 0.00 ft 0.00 ft 0.00 ft 0.00 ft 36.00 ft 36.00 ft 0.00 ft 0.

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Worksheet for FSD Overflow - Pass

Discharge			
	0.90	ft	
	0.00	ft	
	0.00	ft	
Gravel			
	12.00	ft	
:	36.00	ft	
1	86.22	ft³/s	(55Dul+29.4) pres = 44.4 2)
	0.90	ft	1
	0.00	ft	
	2.80	US	
	1.00		
	2.80	US	
1	32.40	ft²	
	2.66	ft/s	
	37.80	ft	
	36.00	ft	
	Discharge Gravel	Discharge 0.90 0.00 Gravel 12.00 36.00 86.22 0.90 0.00 2.80 0.00 2.80 1.00 2.80 32.40	Discharge 0.90 ft 0.00 ft 0.00 ft 0.00 ft 0.00 ft 36.00 ft 36.00 ft 0.00 ft 0.

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	Worksheet for SF	B Overflo	w Develop	ed
Project Description		yaa		
Solve For	Discharge			
Input Data		r sister som		
Headwater Elevation		0.45	ft	
Crest Elevation		0.00	ft	
Tailwater Elevation		0.00	ft	*
Crest Surface Type	Gravel			
Crest Breadth		6.00	ft	
Crest Length		10.00	ft	
Results			Mas - Mary	
Discharge		8.08	ft'/s	
Headwater Height Above Cres	it	0.45	ft	
Tailwater Height Above Crest		0.00	ft	
Weir Coefficient		2.68	US	
Submergence Factor		1.00		
Adjusted Weir Coefficient		2.68	US	

4.50 ft²

1.80 ft/s

10.90 ft

10.00 ft

141 OFD A.

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Flow Area Velocity

Top Width

.

Wetted Perimeter

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Appendix D Drainage Maps





STERLING RANCH FILING 5



Label project boundary

Label all existing easements

Include another map with larger scale of project area

LEGEND



EXISTING



BASIN SUMMARY TABLE

Tributary	Area	Percent			t _c	Q₅	Q ₁₀₀
Sub-basin	(acres)	Impervious	C ₅	C ₁₀₀	(min)	(cfs)	(cfs)
A 1	5.09	0%	0.08	0.35	28.7	1.0	7.6
A2	2.89	0%	0.08	0.35	15.3	0.8	5.9
A3	1.94	0%	0.08	0.35	17.9	0.5	3.7
A4	4.83	47%	0.44	<mark>0.61</mark>	18.3	6.8	16.0
OS1	0.79	<mark>65%</mark>	0.45	0.59	10.2	1.5	3.2
OS2	33.07	19%	0.20	0.43	36.4	14.6	52.8
OS3	13.90	49%	0.40	0.57	15.5	19.4	46.3

ESIGN POINT				
	Q5	Q100		
	Total	Total		
	1.5	3.2		
	14.6	<mark>52.8</mark>		
	1.0	7.6		
	19.4	46.3		
	6.8	16.0		



STERLING RANCH FILING 5 EXISTING DRAINAGE MAP JOB NO. 25188.16 11/27/22 SHEET 1 OF 1



J·R ENGINEERING A Westrian Company

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HOMESTEAD FILING 5

LEGEND BASIN ID A A: BASIN LABEL B C D B: AREA C: C –100 YR D: C–5 YR DESIGN POINT /#\ PROPOSED FLOW DIRECTION EXISTING FLOW DIRECTION BASIN DRAINAGE AREA EXISTING STORM SEWER STORM SEWER PROPOSED PROPOSED R.O.W ____ PROPOSED PROPERTY LIN PROPOSED SIDEWALK EXISTING PROPERTY LINE ROW EXISTING _____ FL EXISTING _____ SIDEWALK EXISTING ------DRAINAGE ACCESS & MAINTENANCE ---- ---- ----EASEMENT

EXISTING

_____ 6100_____

PROPOSED - 6100-

_	-	\sim	-	

Tributary	Area	Percent			t _c	Q ₅	Q ₁₀₀
Sub-basin	(acres)	Impervious	C ₅	C ₁₀₀	(min)	(cfs)	(cfs)
A1	0.70	30%	0.26	0.47	19.2	0.6	2.0
A2	0.68	41%	0.31	0.50	14.4	0.8	2.3
A3	0.75	43%	0.33	0.51	14.9	0.9	2.5
A4	1.00	85%	0.72	0.82	9.2	3.1	6.3
A5	2.85	62%	0.50	0.64	14.4	5.1	12.3
A6	0.74	55%	0.43	0.58	9.9	1.3	3.3
A7	2.03	58%	0.50	0.65	12.8	3.8	9.2
A8	1.55	<mark>71</mark> %	0.61	0.73	9.8	3.9	<mark>8.6</mark>
A9	0.21	50%	0.36	0.53	12.9	0.3	0.8
A10	1.35	52%	0.38	0.54	12.7	1.9	5.1
OS1	0.79	65%	0.45	0.59	10.2	1.5	3.5

BASIN SUMMARY TABLE

DES	IGN PO	DINT	Label all easements
DD	Q5	Q100	
DP	Total	Total	Label all storm as public or private
1	2.0	5.4	
2	0.6	2.0	Label Streets, lots and tracts
2.1	2.4	6.9	
3	0.9	2.5	
4	3.1	6.3	
5	5.1	12.3	
5.1	9.9	25.3	
6	1.3	3.3	
7	3.8	9.2	
8	3.9	<mark>8.6</mark>	
8.1	7.3	17.1	
9	0.3	0.8	
10	1.9	5.1	
11	12.0	25.9	
12	2.0	<mark>6.4</mark>	
13	8.3	18.8	
14	29.6	68.1	*
	60	30	0 60 120
		ORI	IGINAL SCALE: 1" = 60'
		HOME	STEAD FILING 5
		PROP	OSED DRAINAGE MAP
		JOB	NO. 25188.16
		<u></u>	8/23

08/08/23 SHEET 1 OF 1



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V1_ drainage.pdf Markup Summary



	Subject: Callout Page Label: 1 Author: CDurham Date: 10/2/2023 4:07:45 PM Status: Color: Layer: Space:	Should this be labeled as DP5, since it's collecting flow from other basins at the inlet & DP5.1 is the pipe/intercepted flow?
	Subject: Callout Page Label: 1 Author: CDurham Date: 10/2/2023 4:07:36 PM Status: Color: Layer: Space:	Should this be labeled as DP10, since it's collecting flow from other basins at the inlet?
	Subject: Callout Page Label: 1 Author: CDurham Date: 10/2/2023 4:08:41 PM Status: Color: Layer: Space:	Doesn't match
	Subject: Callout Page Label: 1 Author: CDurham Date: 10/2/2023 4:11:55 PM Status: Color: Layer: Space:	Include a DP that corresponds to DP10 from the Filing No. 4 report. Indicate in report if there is an increase/decrease in flows
	Subject: Callout Page Label: 1 Author: CDurham Date: 10/2/2023 4:11:25 PM Status: Color: Layer: Space:	Show total flow to DP13, indicate in report if there is an increase or decrease from Filing No. 4 report
Fire do not much with Fire No. 4 report	Subject: Callout Page Label: 1 Author: CDurham Date: 10/2/2023 4:12:40 PM Status: Color: Layer: Space:	Flows do not match with Filing No. 4 report

	Subject: Callout Page Label: 46 Author: CDurham Date: 10/2/2023 4:14:38 PM Status: Color: Layer: Space:	Show overflow path and swales discussed in report under Basin OS2
	Subject: Callout Page Label: 46 Author: CDurham Date: 10/2/2023 4:14:57 PM Status: Color: Layer: Space:	Label existing pond W-8
Low poor and neese floor neese. Indices where how one instance	Subject: Callout Page Label: 46 Author: CDurham Date: 10/2/2023 4:15:33 PM Status: Color: Layer: Space:	Label pond and release flow rates. Indicate where flows were obtained.
SEE S FILING	Subject: Callout Page Label: 46 Author: CDurham Date: 10/2/2023 4:16:42 PM Status: Color: Layer: Space:	Include project #
	Subject: Callout Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:18:24 PM Status: Color: Layer: Space:	Inlets are missing
	Subject: Callout Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:21:25 PM Status: Color: Layer: Space:	Compare with DP2.5 from Filing No. 2 report & DP10 in Filing No. 4 report

	Subject: Callout Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:20:30 PM Status: Color: Layer: Space:	Compare with DP2.2 from Filing No. 2 report
	Subject: Callout Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:22:45 PM Status: Color: Layer: Space:	Show and label proposed wall along Dines and Sterling Ranch. Will it impede drainage, is a swale or weep holes needed?
Highlight (3)		
6.4	Subject: Highlight Page Label: 1 Author: CDurham Date: 10/2/2023 4:12:23 PM Status: Color: Layer: Space:	6.4
18.8	Subject: Highlight Page Label: 1 Author: CDurham Date: 10/2/2023 4:12:24 PM Status: Color: Layer: Space:	18.8
60 30 0 60 12 ORIGNAL SCALE: 1" = 60" HOMESTEAD FUING 5 PROPOSED DRAINAGE MAP JOB NO. 25188.16 08/08/23 SHEET 1 OF 1	Subject: Highlight Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:23:23 PM Status: Color: Layer: Space:	

SW - Textbox (1)

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Subject: SW - Textbox Page Label: 12 Author: Glenn Reese - EPC Stormwater Date: 9/22/2023 8:55:14 AM Status: Color: ■ Layer: Space:

Engineer must confirm in the Drainage Report that the existing offsite PBMP that the site is tributary to are functioning as intended.

Text Box (21)

and conveys the Sterling Ranch nt land. Sand Creek is located a ily, JR engineering is performing site.Provide project number the approved "Master Developm ivil Consultants, Inc., dated Octo	Subject: Text Box Page Label: 5 Author: CDurham Date: 10/2/2023 3:12:27 PM Status: Color: Layer: Space:	Provide project number
were improving, sensitive of the seathers of No.1. Result from this basis during the star basisma AL. Bandli 's calculated in this of the basis grant and the located at DN to the search of the search of the search of the search of the search of the search of the search of the the search of the s	Subject: Text Box Page Label: 6 Author: CDurham Date: 10/2/2023 3:22:19 PM Status: Color: Layer: Space:	Indicate what project and/or report the detained flows for the pond were obtained from
(* Ane an DA _, Dotament How How to the strict to the detention pond and will outfind is routed estarrout the Storing ranch. Filing 5. The emergency overflow path in DP. Show and label overflow path in DP. Show and DP detention to the s g 4 and DP 4. Collected runoff is piped :	Subject: Text Box Page Label: 6 Author: CDurham Date: 10/2/2023 3:22:57 PM Status: Color: Layer: Space:	Show and label overflow path and swales on drainage map
ully outfalls to Sand Creek. Filing 1 and Branding Iron ares. The addition of the area in the addition of the area in the addition of the plant and the addition of the same of the addi	Subject: Text Box Page Label: 8 Author: CDurham Date: 10/2/2023 3:32:24 PM Status: Color: Layer: Space:	Also include that the existing inlet will be checked for capacity with the additional flow.
ow to the existing detention not collected by the inlet at lands Pding 4. The collected natually convex the flow to use with the perspective processing of the pro- tected for capacity with the perspective processing of the pro- lected name in the FOR. Recent processing of the perspective detected name in the proof south detected name in the proof south detected name in the proof south	Subject: Text Box Page Label: 8 Author: CDurham Date: 10/2/2023 3:33:35 PM Status: Color: Layer: Space:	Identify that the existing inlet will be checked for capacity with the by-pass flow in the FDR.
low to the existing detention not collected by the inlet a Rand-Filing 4. The collected entually coverse the flow to reach. Monthly that the constant problem by and the one in the FDR. Box, constitut of single-family a overland and sheet flow to un along the curb and gutter with Sterling Ranch Filing 2.	Subject: Text Box Page Label: 8 Author: CDurham Date: 10/2/2023 3:34:01 PM Status: Color: Layer: Space:	Identify that the existing inlet will be checked for capacity with the by-pass flow in the FDR.

et is sugger seamery and sheet flow to be carb and gatter generating a seamer of the seamer of the sea years, Heing 2. years, these of carcary with the production flow flow flow the basis in the to single-family over and desc flow though the carb and meansfl memory is	Subject: Text Box Page Label: 8 Author: CDurham Date: 10/2/2023 3:37:30 PM Status: Color: Layer: Space:	Identify that the existing inlet will be checked for capacity with the additional flow from this basin in the FDR.
see, and lawns. Remoff from this basin drains vta uter on Sterling Ranch Road at DP10 and coart grade intel at DP13 balk with Sterling Ranch Lidentify that use sensing with (CP1) additional flow from the basin in the DP FOR and the mice downstream intel the sterling sterling sterling sterling sterling hypean flow from DP13.	Subject: Text Box Page Label: 8 Author: CDurham Date: 10/2/2023 3:38:29 PM Status: Color: Layer: Space:	Identify that the existing inlet (DP13) will be checked for capacity with the additional flow from this basin in the FDR and the next downstream inlet will be checked with additional bypass flow from DP13
Antenny on a strategy of a strategy of an electron strategy of a strateg	Subject: Text Box Page Label: 9 Author: CDurham Date: 10/2/2023 3:43:55 PM Status: Color: Layer: Space:	Include discussion on overall flows exiting site and indicate if there is an increase or decrease to amount of flows entering existing storm system from Filing 5
report information located offsite A maintenant disformation on the road can be focust in the Fi -The maintenance mod access is of MatchArdfelf and excess to the allow proving walk and other at Article and the state of the sta	Subject: Text Box Page Label: 13 Author: CDurham Date: 10/2/2023 3:45:36 PM Status: Color: Layer: Space:	As flows are now also reaching existing Pond W-8, it will also need to be included in the discussion.
ange impersionals van derignet in som er ensamt de ningener wit en asknensky diet in de die ensite gener 2000 K is in statue in de Antor, in de die statue gener 2000 K is in statue in de die statue in de in statue in de die statue in de die statue in de die statue in de die statue in de die statue in de die statue in de die statue in de die statue in de die statue in de die statue in die sta	Subject: Text Box Page Label: 13 Author: CDurham Date: 10/2/2023 3:51:57 PM Status: Color: Layer: Space:	Include statement that proposed site does not impact any downstream facility or property.
ut us contributing	Subject: Text Box Page Label: 1 Author: CDurham Date: 10/2/2023 4:09:36 PM Status: Color: Layer: Space:	List all DP's/Basins contributing

0.01 0.02 <th0.02< th=""> 0.02 0.02 <th0< th=""><th>Subject: Text Box Page Label: 22 Author: CDurham Date: 10/2/2023 4:13:47 PM Status: Color: Layer: Space:</th><th>Highlight basins and design points being referenced within report.</th></th0<></th0.02<>	Subject: Text Box Page Label: 22 Author: CDurham Date: 10/2/2023 4:13:47 PM Status: Color: Layer: Space:	Highlight basins and design points being referenced within report.
Label project boundary	Subject: Text Box Page Label: 46 Author: CDurham Date: 10/2/2023 4:15:54 PM Status: Color: Layer: Space:	Label project boundary
Label all existing easements	Subject: Text Box Page Label: 46 Author: CDurham Date: 10/2/2023 4:16:06 PM Status: Color: Layer: Space:	Label all existing easements
Include another map with larger scale of project area	Subject: Text Box Page Label: 46 Author: CDurham Date: 10/2/2023 4:16:24 PM Status: Color: Layer: Space:	Include another map with larger scale of project area
Label all drainage infrastructure (Existing & proposed)	Subject: Text Box Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:17:14 PM Status: Color: Layer: Space:	Label all drainage infrastructure (Existing & proposed)
j 0.45 0.59 10.2	Subject: Text Box Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:17:53 PM Status: Color: Layer: Space:	Label all easements

Label Pond W-8	Subject: Text Box Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:18:04 PM Status: Color: Layer: Space:	Label Pond W-8
Label all storm as public or private	Subject: Text Box Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:21:46 PM Status: Color: Layer: Space:	Label all storm as public or private
Label Streets, lots and tracts	Subject: Text Box Page Label: [1] DRO1 Author: CDurham Date: 10/2/2023 4:23:15 PM Status: Color: Layer: Space:	Label Streets, lots and tracts