PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH FILING NO. 5

Prepared For:

Classic SRJ Land, LLC 2138 Flying Horse Club Drive Colorado Springs, CO 80921 (719) 785-3270

> November 2023 Project No. 25188.16

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PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH FILING NO. 5 NOV 2023

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. 32314 For and On Behalf of JR Engineering, LLC

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

Classic SRJ Land, LLC

By:

Title: Address:

2138 Flying Horse Club Drive Colorado Springs, CO 80921

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Joshua Palmer, P.E. County Engineer/ ECM Administrator Date

Conditions:



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- Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map
- Appendix B Hydrologic Calcs
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PURPOSE

This document is the Preliminary Drainage Report for Sterling Ranch Filing Number 5. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert, inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

GENERAL SITE DESCRIPTION

GENERAL LOCATION

Sterling Ranch Filing Number 5 (hereby referred to as the "site") is a proposed development within the Sterling Ranch master planned community with a total area of approximately 11.6 acres. The site is currently being designed to accommodate approximately 72 urban lots.

The site is located in a portion of the Southeast Quarter (SE ¹/₄) Of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridian County Of El Paso, State Of Colorado. The site is surrounded by Barbarick Subdivision and Branding Iron at Sterling Ranch Filing No. 1 to the north, Sterling Ranch Filing No. 4 to the west, Sterling Ranch Road to the south, and Dines Boulevard to the east.

DESCRIPTION OF PROPERTY

The property will be primarily single-family residential development (approximately 11.6 acres), open space and drainage tracts. The site is comprised of variable sloping grasslands that generally slope(s) downward to the southwest at 1 to 3% towards Sterling Ranch Road and Hazlett Dr.

Soil characteristics are comprised of Type A and B hydrologic soil groups. Refer to the soil survey map in Appendix A for additional information.

There are no major drainage ways running through the site, Sand Creek lies to the east of the site. Currently, JR Engineering, LLC is performing studies and plans to address Sand Creek stabilization. There are no known irrigation facilities located on the project site.

FLOODPLAIN STATEMENT

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, the proposed development lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. FIRM Map is presented in Appendix A.



EXISTING DRAINAGE CONDITIONS

MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into major subbasins. The site is within the Upper Sand Creek sub-basin as shown in Appendix C.

The Sand Creek DBPS assumed the Sterling Ranch Filing No. 5 property to have a "large lot residential" use for the majority of the site however, the proposed Sterling Ranch master plan is a mix of; school, multi-family, single-family, and commercial land uses, resulting in higher runoff. The "Master Development Drainage Plan for Sterling Ranch"; (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018 assumed a mix of a school site and single family residential lots ranging in size from 0.1 to 0.33 acres for the Sterling Ranch Filing No. 5 site.

Any additional runoff has been provided for with the extended detention basin, "Pond W-5", located at the southern edge of the Sterling Ranch boundary. The site generally drains from northeast to southwest. The site currently has drainage infrastructure built with prior Sterling Ranch subdivisions filings in the site's southwest corner that collects and conveys the Sterling Ranch Filing 5 runoff to Pond W-5. Currently, the site is undeveloped vacant land. Sand Creek is located approximately 500 feet east of the site running north to south. Currently, JR engineering is performing studies and plans to address Sand Creek stabilization adjacent to the site under PCD project number CDR-20-004 and is undergoing review.

The proposed drainage on the site closely follows the approved "Master Development Drainage Plan for Sterling Ranch"; (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018. The site is tributary to Pond W-5 and full-spectrum detention for the site was previously analyzed and can be found in the Final Drainage Report for Sterling Ranch Filing 2 as shown in Appendix C.

EXISTING SUB-BASIN DRAINAGE

The existing condition of the site was broken into four on-site basins, as well as three off-site basins. The basin and sub-basin delineation is shown in the existing drainage map in Appendix D and is described as follows:

Basin A1 ($Q_5=1.0$ cfs, $Q_{100}=7.6$ cfs) is 5.09 acres and 0 percent impervious consists of the northern portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP 3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.



Basin A2 ($Q_5=0.8$ cfs, $Q_{100}=5.9$ cfs) is 2.89 acres and 0 percent impervious consists of the south western portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the existing storm sewer built with Filing 5 just north of Sterling Ranch Road located at DP 3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin A3 ($Q_5=0.5$ cfs, $Q_{100}=3.7$ cfs) is 1.94 acres and 0 percent impervious consists of the southern portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP 3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin A4 ($Q_5=6.8$ cfs, $Q_{100}=16.0$ cfs) is 4.83 acres and 47 percent impervious consists of the southeastern portion of the proposed Sterling Filing No. 5 site as well as the norther portion of Sterling Ranch Road. Runoff from this basin drains via overland flow to Sterling Ranch Road, then west to the existing 15' Type R inlet located at DP 5. Collected runoff is piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin OS1 (Q_5 = 1.4 cfs, Q_{100} =3.1 cfs) is 0.77 acres and 65 percent impervious, consists of the southern portion of the proposed Branding Iron at Sterling Ranch Filing No.1. Runoff from this basin drains to the south into the proposed Sterling Filing No.5 northern site sub-basin A1. Runoff is collected into the existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin OS2 ($Q_5=14.6$ cfs, $Q_{100}=52.8$ cfs) is 33.07 acres and 19 percent impervious and is located directly north of the site in the Barbarick subdivision per the "Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3&4" prepared by Matrix Design Group dated June 6, 2016. Historic runoff from this site drains south onto the Sterling Ranch Filing 4 site at DP 2. Detained flow from this basin will be piped through the Sterling Ranch Filing 4 site to the detention Pond W-5 and will outfall to Sand Creek. The emergency overflow path for this pond is routed east around the Sterling ranch Filing 4 lots and onto the northwest corner of Sterling Ranch Filing 5. The emergency overflow path is conveyed south via a concrete line swale and grass swale to DP3.

Basin OS3 ($Q_5=19.4$ cfs, $Q_{100}=46.3$ cfs) is 13.90 acres and 49 percent impervious, consists of the Sterling Ranch Filing No.4. Runoff from this basin drains to the southwest into the storm sewer built with Sterling Ranch Filing 4 and DP 4. Collected runoff is piped south to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.



PROPOSED DRAINAGE CONDITIONS

PROPOSED SUB-BASIN DRAINAGE

The proposed site was broken into ten on-site basins and two off-site basin that lead into the existing storm structures on Sterling Ranch Road and Sterling Ranch Filing 4. The proposed basin (and subbasin) delineation is shown on the proposed drainage basin map within Appendix D and is described as follows.

Basin A1 ($Q_5=0.7$ cfs, $Q_{100}=2.0$ cfs) is 0.65 acres and 37% impervious, consists of single-family residential lots, open space, lawns, concrete trail, and part of an existing concrete channel. Runoff from this basin drains via sheet flow to the swale at DP2 where runoff is collected in an area inlet. The emergency overflow path of the inlet is to the south to the proposed swale. Collected runoff is piped south to the proposed sump inlet at DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A2 ($Q_5=0.9$ cfs, $Q_{100}=2.6$ cfs) is 0.78 acres and 46% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP1 where it is conveyed west via swale to DP2 and collected in an area inlet. Collected runoff is piped to DP2.1 and then south to DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A3 ($Q_5=0.8$ cfs, $Q_{100}=2.5$ cfs) is 0.79 acres and 44% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP3 where it is conveyed to the street and sump inlet at DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A4 ($Q_5=2.8$ cfs, $Q_{100}=6.0$ cfs) is 1.00 acres and 80% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to DP4, then flows to a sump inlet at DP5.1. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A5 ($Q_5=5.5$ cfs, $Q_{100}=13.2$ cfs) is 2.84 acres and 62% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to DP5, then flows to a sump inlet at DP5.1. The emergency



overflow path of this inlet is to the south to School House Drive. Flows combine with DP.8.1 at DP8.2. The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A6 ($Q_5=1.4$ cfs, $Q_{100}=3.3$ cfs) is 0.66 acres and 58% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter offsite to the curb and gutter in Dines Boulevard. The flows collect in an existing sump inlet at DP6 and are piped via an existing 24" storm pipe to and existing water quality and detention Pond W-8 on the east side of Dines and eventually outfalls to Sand Creek. Pond W-8 was analyzed with the Sterling Ranch Filing 1, Branding Iron Filing 1 and Branding Iron Filing 2 subdivisions and has a total tributary area of approximately 29 acres. The addition of the Basin A6 flows are assumed to be immaterial but will be further analyzed with the Final Drainage Report for SR Filing 5 to confirm this Preliminary Drainage Report assumption. The existing inlet shall also be checked for capacity with the additional flow to ensure no impacts to existing infrastructure.

Basin A7 ($Q_5=3.8$ cfs, $Q_{100}=9.2$ cfs) is 2.04 acres and 59% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to an on-grade inlet at DP7. Flows combine with DP8 at DP8.1. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek. Runoff that is not collected by the inlet at DP7 continues west to an existing sump inlet at DP11 built with Sterling Ranch Filing 4. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing infrastructure. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A8 ($Q_5=3.0$ cfs, $Q_{100}=6.4$ cfs) is 1.10 acres and 77% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to an on-grade inlet at DP8. Flows combine with flows of DP7 at DP8.1 ($Q_5=6.4$ cfs, $Q_{100}=14.9$ cfs). Then flows combine with DP5.1 at DP8.2 ($Q_5=15.5$ cfs, $Q_{100}=38.8$ cfs). The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek. Runoff that is not collected by the inlet at DP8 continues west to an existing sump inlet at DP12 built with Sterling Ranch Filing 4. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention POR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention POR.

Basin A9 ($Q_5=0.3$ cfs, $Q_{100}=0.8$ cfs) is 0.20 acres and 52% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via overland and sheet flow to the curb and gutter on Dines Boulevard. The flows collect at DP9 and run along the curb and gutter



along Sterling Ranch Road to an existing on-grade inlet at DP15 built with Sterling Ranch Filing 2. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A10 ($Q_5=1.9$ cfs, $Q_{100}=5.1$ cfs) is 1.32 acres and 52% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via overland flow and sheet flow to the proposed swale and continues west to the proposed area inlet at DP10. The emergency overflow path is to the west to Hazlett Drive. Flows then combine with DP8.2 flows at DP10.1 ($Q_5=17.1$ cfs, $Q_{100}=43.1$ cfs).The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin OS1 ($Q_5=1.4$ cfs, $Q_{100}=3.4$ cfs) is 0.77 acres and 65% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP1 where it is conveyed west via swale to DP2.1 and collected in an area inlet. Collected runoff is piped south to DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin C4 ($Q_5=5.4$ cfs, $Q_{100}=13.5$ cfs) is 3.67 acres and 62% impervious, consists of a portion of Sterling Ranch Road, a portion of Dines Blvd, Filing 4 single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the existing curb and gutter where it is conveyed west to the existing on-grade inlet at DP15 built with Sterling Ranch Filing 2. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

There are several locations where proposed Filing 5 storm sewer connects to existing storm sewer built with previous Sterling Ranch Filings 2 and 4. The proposed Filing 5 flows at DP5.1 ($Q_5=10.0$ cfs, $Q_{100}=25.7$ cfs) are located at the same location as Filing 4 DP2.i ($Q_5=11.6$ cfs, $Q_{100}=25.7$ cfs) and have less than or equal to the anticipated flow at the existing 24" RCP. The proposed Filing 5 flows at DP8.1 ($Q_5=6.4$ cfs, $Q_{100}=14.9$ cfs) are located at the same location as Filing 4 DP3.i ($Q_5=7.1$ cfs, $Q_{100}=19.4$ cfs) and have less than the anticipated flow at the existing 18" RCP. The proposed Filing 5 flows at DP8.2 ($Q_5=15.5$ cfs, $Q_{100}=38.8$ cfs) are located at the same location as Filing 4 DP3.2 ($Q_5=16.9$ cfs, $Q_{100}=40.2$ cfs) and have less than the anticipated flow at the existing storm manhole. The proposed Filing 5 flows at DP10.1 ($Q_5=17.1$ cfs, $Q_{100}=43.1$ cfs) are located at the same location as Filing 4 DP3.2 ($Q_5=56.9$ cfs, $Q_{100}=138.7$ cfs) and have less than the anticipated flow at the existing storm manhole. The proposed Filing 5 flows at DP11, DP12, DP13, DP14, and DP16.1 are the same flows the inlets at



Filing 4 DP5, DP6.1, DP6.2, DP9, and DP7.1 capture. The proposed Filing 5 flows at DP15 ($Q_5=5.6$ cfs, $Q_{100}=14.1$ cfs) are located the same location as Filing 4 DP8 ($Q_5=6.1$ cfs, $Q_{100}=12.9$ cfs). The series of inlets along Sterling Ranch Road and Marksheffel Road to the Aspen Meadows Filing 1 development have the additional capacity to handle the change in bypass flows past this inlet. The proposed Filing 5 flows at DP17.1 ($Q_5=83.1$ cfs, $Q_{100}=194.0$ cfs) is located at the same location as Filing 4 DP10 ($Q_5=55.8$ cfs, $Q_{100}=149.7$ cfs) and Filing 2 DP2.5 ($Q_5=96.6$ cfs, $Q_{100}=250.7$ cfs). The downstream storm infrastructure from this design point was built in Filing 2 and the proposed flows are less than was anticipated in the existing storm manhole.

DRAINAGE DESIGN CRITERIA

DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.

HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

	Int Kunnun Dutu
Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

Table 1: 1-hr Point Rainfall Data

HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Sump and on-grade inlets will be sized using UDFCD UD-Inlet v5.02. StormCAD will be used to model the proposed storm sewer system within the site to analyze the proposed HGL calculations for the Construction Drawings. Autodesk Hydraflow express will be



used to size any channels or swales. Manhole and pipe losses for the model will be obtained from the <u>Modeling Hydraulic and Energy Gradients in Storm Sewers: A Comparison of Computation Methods</u>, by AMEC Earth & Environmental, Inc. The manhole loss coefficients used in the model can be seen in Table 2 (below) this method is accurate for pipes 42" and smaller for larger pipes the Standard head-loss coefficients as recommended by Bentley were used as shown in Table 3. All hydraulic calculations will be found in the Final Drainage Report Appendices.

	StormCA	D Conversion Ta	ble						
	Bend Angle	K coefficient (Conversion						
ose	0	0.0	5						
L L	22.5	0.1							
Bend Loss	45	0.4	8						
-	60	0.64	1						
	90	1.32	2						
	1 Latera	I K coefficient Co	nversion						
	Bend Angle	Non Surcharged	Surcharged						
SS	45	0.27	0.47						
۲ ۲	60	0.52	0.9						
la	90	1.02	1.77						
-ateral Loss	2 Lateral	Is K coefficient Co	onversion						
_	45	0.96	6						
	60	1.10	6						
		1.52							

 Table 2: Storm Head-loss Coefficients

Table 3:	Storm	Head-loss	Coefficients
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Type of Manhole	Diagram	Headloss Coefficient
Trunkline only with no bend at the junction	<u><u></u></u>	0.5
Trunkline only with 45° bend at the junction	5-Q2	0.6
Trunkline only with 90° bend at the junction	J.	0.8
Trunkline with one lateral	8	Small 0.6 Large 0.7
Two roughly equivalent entrance lines with angle < 90° between lines	A A A A A A A A A A A A A A A A A A A	0.8
Two roughly equivalent entrance lines with angle > 90° between lines	E Contraction	0.9
Three or more entrance lines	ET T	1.0

DRAINAGE FACILITY DESIGN

GENERAL CONCEPT

The proposed stormwater conveyance system was designed to convey the developed Sterling Ranch Filing No. 5 runoff to an existing (Filing 2) full spectrum water quality and detention Pond W-5 via existing and proposed storm sewer. The existing pond was designed to release at less than historic rates to minimize adverse impacts downstream. Treated water will outfall directly into the Sand Creek Drainageway, where it will eventually outfall into Fountain Creek. A proposed drainage map is presented in Appendix D showing locations of the pond.

FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The Sterling Ranch Filing No. 5 development project consists of single-family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.



Step 2 – Stabilize Drainage ways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the channel stabilization being designed by JR Engineering adjacent to the site and on future projects within the basin to stabilize drainage ways. The site does not discharge directly into the open drainage way of Sand Creek, therefore no downstream stabilization will be accomplished with this project

Step 3 – Treat the WQCV: Water Quality treatment for this site is provided in the existing full spectrum water quality detention Pond W-5 and Pond W-8. The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structures have been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the pond will be reduced to less than historic rates.

Step 4 –BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. The Filing No. 5 site is residential. There is no proposed commercial or industrial use for the site. The permanent erosion control BMPs include asphalt drives, storm inlets and storm pipe, the full spectrum detention Pond W-5 and permanent vegetation. Maintenance responsibilities and plans will be defined at the time of final platting.

WATER QUALITY

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full-spectrum water quality and detention are provided for all developed basins. This site will drain into an existing Full-Spectrum Drainage Pond W-5 developed during the Sterling Ranch Filing Project. Further details as well as all pond volume, water quality, and outfall calculations are included in the Sterling Ranch Filing 2 Final Drainage Report. Pond W-5 corresponds to pond FSD6 from the Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018 and is releasing less than the MDDP values in the proposed design. A summary of Pond W-5 has been included below for reference. From the Filing No.2 drainage report, Pond W-5 accounted for Sterling Ranch Filing 5 area to have 65% imperviousness. The total imperviousness for the Filing 5 development is 59% imperviousness, and the total runoff is less than what was anticipated; therefore the existing Pond W-5 will function as intended. The FDR will analyze and determine if the existing off-site pond is functioning as intended.

	REQUIRED	VOLUME PROVIDED	WQCV	EURV	5-YEAR RELEASE	100-YEAR RELEASE
	VOLUME (AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)	(CFS)	(CFS)
POND W-5	18.217	18.441	3.29	11.71	2.7	137.1

Table 4: Pond Volumes & Release Rates



EROSION CONTROL PLAN

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

OPERATION & MAINTENANCE

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The district shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. A maintenance road was provided for the existing Pond W-5 and information on the road can be found in the Final Drainage Report for Sterling Ranch Filing No. 2. The maintenance road access is off Marksheffel Road and wraps around the top of the pond providing access to the inflow pipe wing walls and outlet structure for the pond. A maintenance road was provided for the existing Pond W-5 for the existing Pond W-8 and information on the road can be found in the road can be found in the approved Sterling Ranch Filing No. 1 Storm Sewer Plans. The maintenance road access is off Dines Boulevard and provides access to the inflow pipe forebay and outlet structure for the pond.

DRAINAGE AND BRIDGE FEES

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees will be defined within the Final Drainage Report and will be due at time of platting (depending on date of plat submittal).

SUMMARY

The proposed Sterling Ranch Filing No. 5 drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainage-ways or surrounding development. The existing Ponds W-5 and W-8 are to release less than 90% of the predeveloped runoff study associated with the subject site. The site is in continuity with the Sterling Ranch Filing No. 2 Drainage Report and the Sterling Ranch Filing No. 4 Drainage Report. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site. The proposed site does not impact any downstream facility or property.



REFERENCES

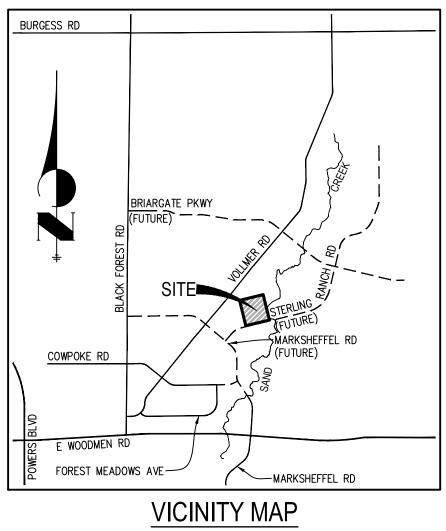
- 1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2. Sand Creek Channel Design Report, prepared by JR Engineering, May 19, 2021 (not yet approved)
- 3. "Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018.
- 4. <u>Sand Creek Drainage Basin Planning Study</u>, prepared Kiowa Engineering Corporation, January 1993, revised March 1996.
- 5. "Sterling Ranch Filing 2 Final Drainage Report", prepared by JR Engineering, dated May 2021
- 6. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- Sand Creek Stabilization at Aspen Meadows Subdivision Filing No. 1 100% Design Plans, April 2020
- 8. <u>Final Drainage Report For Barbarick Subdivision Portion Of Lots 1,2 And Lots 3 and 4</u>, Prepared by Matrix Design Group, June 2016
- 9. Preliminary Drainage Report And MDDP Addendum For Homestead North At Sterling Ranch Preliminary Plan", prepared by JR Engineering, dated January 2022
- 10. Sand Creek Drainage Basin Planning Study, Stantec, January 2021
- 12. Final Drainage Report for Aspen Meadows, Matrix Design, January 2019* pending approval



J·R ENGINEERING

Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map



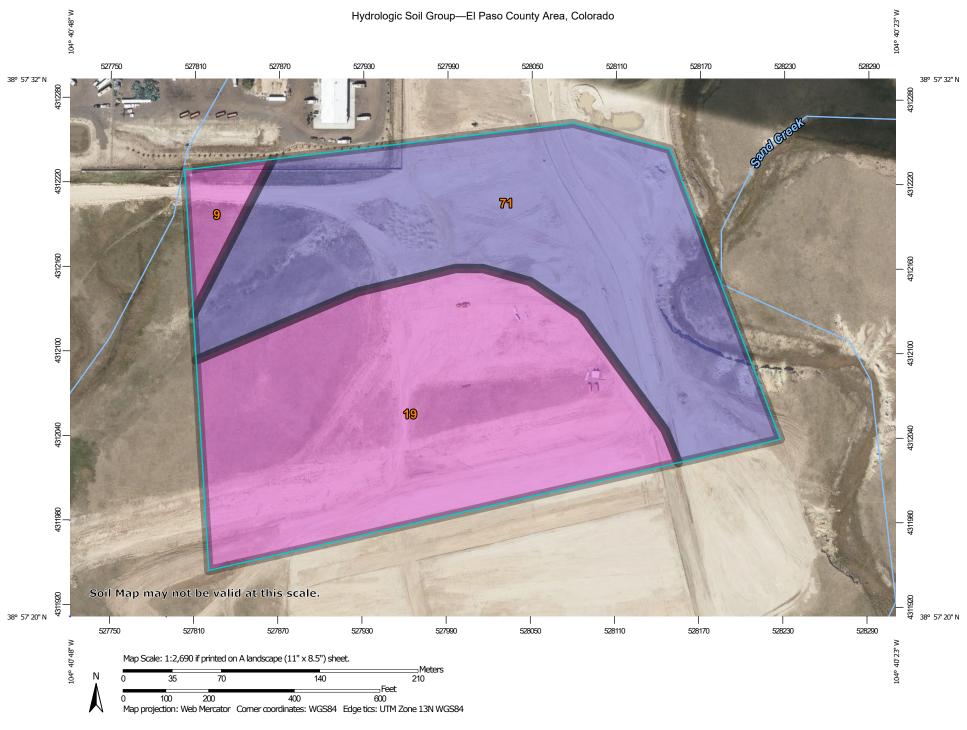


N.T.S.

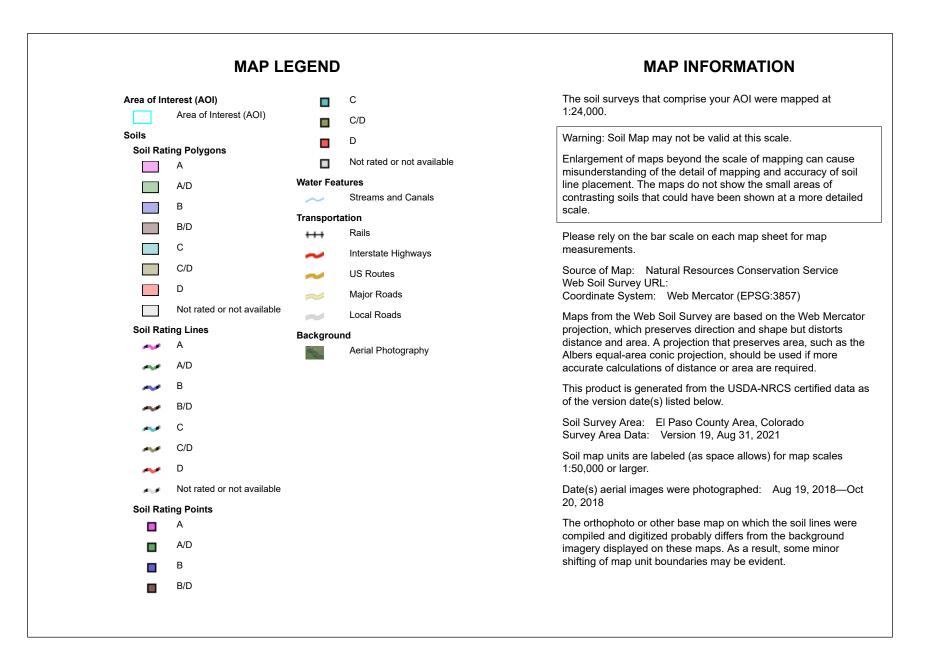
VICINITY MAP HOMESTEAD FILING NO. 5 JOB NO. 25188.16 8/26/22 SHEET 1 OF 1



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
9	Blakeland-Fluvaquentic Haplaquolls	A	0.8	3.3%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	12.0	49.0%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	11.7	47.7%
Totals for Area of Inter	est	1	24.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



NOTES TO USERS

This map is for use in administring the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

Location or detailed information in answer them taken the action flowed based information in answer the take Flood Elevations (RFEs) action flowed based and the flowed action of the flowed within the Flood traverse based (RFEs) within the Flood traverse based (RFE) provide the account and the same that BFEs allows on the FIRM traverse traverse whole bod that and the same that BFEs allows on the FIRM traverse traverse whole bod that and the RFE and the same traverse the same traverse that and the result of the same traverse the same traverse that and the RFE and the same traverse the same traverse that and the RFE and the same traverse that the RFE and the same of construction and the FIRM traverse of construction of construction and the RFE and the same traverse the RFE and the RFE and the same traverse the RFE and the RFE and the same traverse the RFE and the RFE and the RFE and the traverse the RFE and the RFE

Coastal Base Flood Elevations shown on this map apply only landward of 0.0° North American Vortical Datum of 1889 (NAVOB6). Users of this FIRM Hould be aware that coastal flood deviators are aired provided in the Summary of Sillware Elevators table in the Flood Insurance Study report for this unitadicion. Elevations shown in the Summar of Sillware Elevators table should be used for construction and/or floodpian management purposes when they are higher than the deviations

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway width and other partinent floodway data are provided in the Flood Insurance Study report for this jurisdicture.

Certain areas not in Special Flood Hazard Areas may be protected by **flood contrn** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insuranc Study report for information on flood control structures for this jurisdiction.

The projection used in the properties of this may was Universel Transverse Meanser (UTM) are 13. The hothcast attain was NARDS, GR585 spheroid. Differences in datum, spheroid, projection or UTM screes zones used in the production of FRMNs for adjacent juncticions may require uit, in slight positional differences in mag features across jurisdiction boundaries. These differences do not affect the accuracy of this FRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD68), Thesis flood elevations must be compared to structure are compared to structure and the structure of the structure and conversion between the National Geodelic Vertical Datum of 1528 and the North American Vertical Datum of 1988, visit the National Geodelic Survey at the Holm/ American Service and Service and Service and the Islaming Service and Service and

NGS Information Services NOAA, NINGS12 National Geodetic Survey SSMC-3, #9202 1315 East-Weast Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map infects more detailed and up-to-date stream channel configurations and modplain delineations than those shown on the previous FRM for this jurisdice, this way to be adjudged to confirm to these more stream channel configurations. As sets the besing disudder to confirm to these more stream channel configurations. As a sets the besing disudder to confirm to these more stream channel configurations. As a sets the besing disudder the stream channel configuration and disarces that offer from what is shown on the map. The profit baselines diplated disarces that offer from what is shown on the map. The profit baselines diplated baselines that offer from what is shown on the map. The profit baselines diplated baselines and the stream configuration that the FIS report. As a result, the profit baselines significantly from the new base map channel representation and may appear contact of the fore forem.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, may users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a siting of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is conted.

Contact ERUA Mag Service Center (MSC) via the FEMA Mag information at/change FHMV 1 5477-032827 for information on savalable products associated with the FIRM. Available products may include previously issued Latters of Map Change, a FiRM. Available product organization of the MSC may also be reached by Fax at 1-800-358-8620 and its websile at http://www.msc.fema.gov/.

f you have **questions about this map** or questions concerning the National Flood nsurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

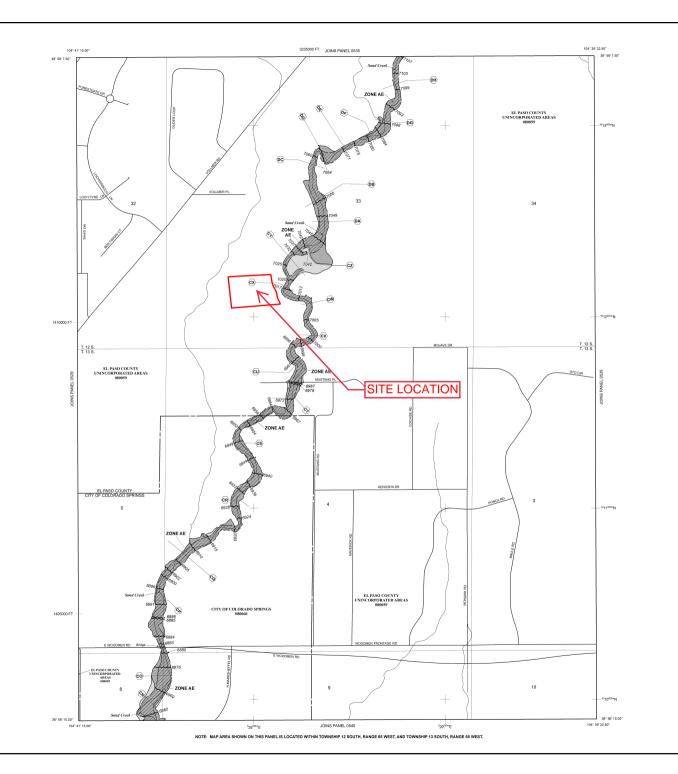




This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Water Conservation Board

tional Flood Hazaro Information and resource lable from local communities and the Col-





Appendix B Hydrologic Calcs



COMPOSITE % IMPERVIOUS & COMPOSITE EXISTING RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location: Sterling Ranch Subdivision- Existing El Paso County Project Name: <u>Sterling Ranch Filing 5</u> Project No.: 25188.16 Calculated By: DIG

Checked By: RAB

Date: 11/3/23

	Total	Str	eets (10	0% Impe	rvious)	Re	sidentia	l (65% Im	npervious)	Light I	ndustria	ıl (80% In	npervious)		Lawns (0% Impe	rvious)	Weigl	s Total nted C ues	Basins Total Weighted %
Basin ID	Area (ac)	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	ues C ₁₀₀	İmp.
A1	5.09	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	5.09	0.0%	0.08	0.35	0.0%
A2	2.89	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	2.89	0.0%	0.08	0.35	0.0%
A3	1.94	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.94	0.0%	0.08	0.35	0.0%
A4	4.83	0.90	0.96	1.75	36.2%	0.45	0.59	0.80	10.8%	0.59	0.70	0.00	0.0%	0.08	0.35	2.28	0.0%	0.44	0.61	47.0%
OS1	0.77	0.90	0.96	0.00	0.0%	0.45	0.59	0.77	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
OS2	33.07	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	7.91	19.1%	0.08	0.35	25.16	0.0%	0.20	0.43	19.1%
OS3	13.90	0.90	0.96	2.35	16.9%	0.45	0.59	6.86	32.1%	0.59	0.70	0.00	0.0%	0.08	0.35	4.69	0.0%	0.40	0.57	49.0%
TOTAL (A1-A4)	14.75																			0.0%
TOTAL (OS1-OS3)	47.74																			28.6%
TOTAL	62.49																			25.5%

EXISTING STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Subdivision- Existing

Location: El Paso County

 Project Name:
 Sterling Ranch Filing 5

 Project No.:
 25188.16

 Calculated By:
 DIG

 Checked By:
 RAB

Date: 11/3/23

		SUB-	BASIN			INITL	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T _i)				(T _t)			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t i	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	5.09	В	0%	0.08	0.35	180	1.4%	22.1	497	1.6%	10.0	1.3	6.5	28.7	677.0	33.3	28.7
A2	2.89	А	0%	0.08	0.35	125	4.6%	12.4	385	5.2%	10.0	2.3	2.8	15.3	510.0	29.1	15.3
A3	1.94	А	0%	0.08	0.35	80	1.7%	13.8	385	2.5%	10.0	1.6	4.1	17.9	465.0	30.5	17.9
A4	4.83	А	47%	0.44	0.61	100	3.0%	8.3	1466	1.5%	20.0	2.4	10.0	18.3	1566.0	30.8	18.3
OS1	0.77	А	65%	0.45	0.59	88	2.0%	8.8	122	2.0%	10.0	1.4	1.4	10.2	210.0	15.7	10.2
OS2	33.07	А	19%	0.20	0.43	298	3.0%	19.5	1664	2.7%	10.0	1.6	16.9	36.4	1962.0	37.2	36.4
OS3	13.90	А	49%	0.40	0.57	100	1.8%	10.4	796	1.7%	20.0	2.6	5.1	15.5	896.0	24.1	15.5

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$

ti = overland (initial) flow time (minutes)

 $L_i =$ length of overland flow (ft)

 $C_5 =$ runoff coefficient for 5-year frequency (from Table 6-4)

Where:

NOTES:

 $t_c = t_i + t_t$

Where:

 t_c = computed time of concentration (minutes)

 $t_i = \text{overland (initial) flow time (minutes)}$

 t_t = channelized flow time (minutes).

 S_{σ} = average slope along the overland flow path (ft/ft). Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of

concentration.

$$t_{t} = \frac{L_{t}}{60K\sqrt{S_{o}}} = \frac{L_{t}}{60V_{r}}$$

Equation 6-4 $t_{c} = (26 - 17i) + \frac{L_{t}}{60(14i + 9)\sqrt{S_{t}}}$

Where:

Equation 6-2

Equation 6-5

Equation 6-3

Where:

 $\begin{array}{l} t_{t} = \text{channelized flow time (travel time, min)} \\ L_{i} = \text{waterway length (ft)} \\ S_{o} = \text{waterway slope (ft/ft)} \\ V_{i} = \text{travel time velocity (ft/sec)} = K \sqrt{S_{o}} \\ K = \text{NRCS conveyance factor (see Table 6-2).} \end{array}$

 $t_c = \min$ imum time of concentration for first design point when less than t_c from Equation 6-1. $L_t = \text{length of channelized flow path (ft)}$ $i = \operatorname{imperviousness}(expressed as a decimal)$ $S_t = \text{slope of the channelized flow path (ft/ft)}.$

Table 6-2. NRCS Conveyance factors, K Type of Land Surface Conveyance Factor, K Heavy meadow 2.5 Tillage/field 5 Short pasture and lawns 7 Nearly bare ground 10 Grassed waterway 15 Paved areas and shallow paved swales 20

STANDARD FORM SF-3 - EXISTING STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Subdivision- Existing Location: El Paso County

Design Storm: 5-Year

Project Name: Project No.: Calculated By: Checked By: Date: Sterling Ranch Filing 5 25188.16 DIG RAB 11/3/23

				DIRE	CT RUI	NOFF			TC	DTAL R	UNOF	F	STRE	et/sw	/ALE		PII	PE		TRAV	'EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	OS1	0.77	0.45	10.2	0.35	4.10	1.4															
	2	OS2	33.07	0.20	36.4	6.68	2.19	14.6															Offsite Barbarick Pond Release Piped to DP4
	3	A1	5.09	0.08	28.7	0.41	2.55	1.0															
	3	A2	2.89	0.08	15.3	0.23	3.50	0.8															
	3	A3	1.94	0.08	17.9	0.16	3.26	0.5															
	3								28.7	1.15	2.55	2.9											Sum of basins A1-A3 and OS1, drain to Ex storm Piped west and south to Ex. Pond W-5
	4	OS3	13.90	0.40	15.5	5.58	3.47	19.4															
	5	A4	4.83	0.44	18.3	2.12	3.22	6.8															Runoff to Ex. Inlet in Sterling Ranch Road Piped south to Ex. Pond W-5
		7.4	1.00	0.77	10.5	2.12	0.22	0.0															

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - EXISTING STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name: Project No.: Calculated By: Checked By: Date: Sterling Ranch Filing 5 25188.16 DIG RAB 11/3/23

Subdivision: Sterling Ranch Subdivision- Existing Location: El Paso County

Design Storm: 100-Year

				DIR	ECT RI	JNOFF			Т	OTAL RU	INOF	F	STRE	ET/SW	ALE		PIP	-		TRAV	'EL TIN	ЛE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	OS1	0.77	0.59	10.2	0.45	6.88	3.1															
	2	OS2	33.07	0.43	36.4	14.34	3.68	52.8															Offsite Barbarick Pond Release Piped to DP4
	3	A1	5.09	0.35	28.7	1.78	4.28	7.6															
	3	A2	2.89	0.35	15.3	1.01	5.87	5.9															
	3	A3	1.94	0.35	17.9	0.68	5.47	3.7															
	3								28.7	3.92	4.28	16.8											Sum of basins A1-A3 and OS1, drain to Ex storm Piped west and south to Ex. Pond W-5
	4	OS3	13.90	0.57	15.5	7.94	5.83	46.3															
	5	A4	4.83	0.61	18.3	2.95	5.41	16.0															Runoff to Ex. Inlet in Sterling Ranch Road Piped south to Ex. Pond W-5

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Location:

Sterling Ranch Subdivision - Proposed

El Paso County

Project Name: Sterling Ranch Filing 5

Project No.: 25188.16

Calculated By: GAG

Checked By:

Date: 11/3/23

	Total	Paved	/Streets	(100% Ir	npervious)	Re	sidentia	(65% Im	ipervious)	L	awns (09	% Imper∖	vious)	Weigh	s Total nted C	Basins Total
Basin ID	Area (ac)	C_5	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	Val C₅	ues C ₁₀₀	Weighted % Imp.
A1	0.65	0.90	0.96	0.07	10.8%	0.45	0.59	0.26	26.0%	0.08	0.35	0.32	0.0%	0.32	0.51	36.8%
A2	0.78	0.90	0.96	0.03	3.8%	0.45	0.59	0.50	41.7%	0.08	0.35	0.25	0.0%	0.35	0.53	45.5%
A3	0.79	0.90	0.96	0.00	0.0%	0.45	0.59	0.54	44.4%	0.08	0.35	0.25	0.0%	0.33	0.51	44.4%
A4	1.00	0.90	0.96	0.59	59.0%	0.45	0.59	0.32	20.8%	0.08	0.35	0.09	0.0%	0.68	0.79	79.8%
A5	2.84	0.90	0.96	0.74	26.1%	0.45	0.59	1.55	35.5%	0.08	0.35	0.55	0.0%	0.50	0.64	61.5%
A6	0.66	0.90	0.96	0.10	15.2%	0.45	0.59	0.43	42.3%	0.08	0.35	0.13	0.0%	0.45	0.60	57.5%
A7	2.04	0.90	0.96	0.71	34.8%	0.45	0.59	0.76	24.2%	0.08	0.35	0.57	0.0%	0.50	0.65	59.0%
A8	1.10	0.90	0.96	0.51	46.4%	0.45	0.59	0.52	30.7%	0.08	0.35	0.07	0.0%	0.64	0.75	77.1%
A9	0.20	0.90	0.96	0.00	0.0%	0.45	0.59	0.16	52.0%	0.08	0.35	0.04	0.0%	0.38	0.54	52.0%
A10	1.32	0.90	0.96	0.01	0.8%	0.45	0.59	1.05	51.7%	0.08	0.35	0.26	0.0%	0.38	0.55	52.5%
OS1	0.77	0.90	0.96	0.00	0.0%	0.45	0.59	0.77	65.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
C4	3.67	0.90	0.96	1.75	47.7%	0.45	0.59	0.83	14.7%	0.08	0.35	1.09	0.0%	0.55	0.70	62.4%
TOTAL (A1-A10)	11.38															59.0%
TOTAL	15.82															60.1%

PROPOSED STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Subdivision - Proposed

Location: El Paso County

Project Name: Sterling Ranch Filing 5

Project No.: 25188.16

Calculated By: GAG

Checked By:

Date: 11/3/23

		SUB-	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		DA	ATA				(T _i)				(T _t)			(U	IRBANIZED BA	(SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t i	L _t	S _t	K	VEL.	t _t	COMP. t _c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	0.65	В	37%	0.32	0.51	70	2.2%	9.1	335	0.7%	7.0	0.6	9.3	18.5	405.0	24.4	18.5
A2	0.78	В	46%	0.35	0.53	70	2.0%	9.0	345	1.0%	7.0	0.7	8.2	17.2	415.0	22.0	17.2
A3	0.79	А	44%	0.33	0.51	115	2.5%	11.0	420	1.5%	7.0	0.9	8.2	19.1	535.0	22.2	19.1
A4	1.00	А	80%	0.68	0.79	30	2.0%	3.3	950	1.6%	20.0	2.5	6.4	9.6	980.0	18.7	9.6
A5	2.84	А	62%	0.50	0.64	30	2.0%	4.8	1035	1.6%	20.0	2.5	6.8	11.6	1065.0	23.3	11.6
A6	0.66	А	58%	0.45	0.60	30	2.0%	5.2	300	1.9%	20.0	2.8	1.8	7.0	330.0	18.3	7.0
A7	2.04	А	59%	0.50	0.65	95	2.0%	8.4	750	1.6%	20.0	2.6	4.9	13.2	845.0	21.6	13.2
A8	1.10	А	77%	0.64	0.75	30	2.0%	3.7	830	1.6%	20.0	2.5	5.5	9.1	860.0	18.4	9.1
A9	0.20	А	52%	0.38	0.54	85	2.3%	9.2	170	1.5%	20.0	2.4	1.2	10.3	255.0	18.6	10.3
A10	1.32	А	52%	0.38	0.55	75	3.5%	7.4	665	1.0%	20.0	2.0	5.5	13.0	740.0	23.9	13.0
OS1	0.77	А	65%	0.45	0.59	90	2.0%	8.9	125	2.0%	10.0	1.4	1.5	10.3	215.0	15.8	10.3
C4	3.67	А	62%	0.55	0.70	20	2.0%	3.5	1745	1.5%	10.0	1.2	23.7	27.2	1765.0	28.8	27.2

NOTES:

Where:

Where

 $t_c = t_i + t_t$

Equation 6-2

Equation 6-4

$$=\frac{0.395(1.1-C_5)\sqrt{L_i}}{S_o^{0.033}}$$

Where:

Where:

 t_i

t_i = overland (initial) flow time (minutes) $C_5 = \text{runoff coefficient for 5-year frequency (from Table 6-4)}$ $L_i =$ length of overland flow (ft) S_0 = average slope along the overland flow path (ft/ft).

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S}}$$

$$60(14i+9)\sqrt{S_t}$$

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

Equation 6-3

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

 L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$

te = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

 $t_t =$ channelized flow time (travel time, min)

K = NRCS conveyance factor (see Table 6-2).

 t_t = channelized flow time (minutes).

 $t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$

 $L_t =$ waterway length (ft) S_0 = waterway slope (ft/ft) V_t = travel time velocity (ft/sec) = K $\sqrt{S_0}$

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

.

Equation 6-5

														TORN	/I DR/	AINA	VI SF- Ge sy:	STEM	DES	IGN)		
														(RA	TIONA	l Met	THOD F	PROCE	DURE))			
Subdivision	Storlin	na Pana	sh Subd	ivision	Prop	have										Pro	oject N Projec	lame:	Sterli 2518	ing Rai 8 16	nch Fil	ling 5	
Location				IVISION	-гтор	useu											lculate						
Design Storm:	-		ity .														Checke						
																		Date:		/23			
				DIRE	CT RU	NOFF			T	OTAL R	UNOF	F	STRE	et/sw	/ALE		PI	PE		TRAV	/EL TIN	ИE	
STREET	Jesign Point	Basin ID	Area (Ac)	kunoff Coeff.	(min)	*A (Ac)	(in/hr)	Q (cfs)	(min)	:*A (ac)	(in/hr)	Q (cfs)	Qstreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	oipe Size (inches)	-ength (ft)	/elocity (fps)	(min)	REMARKS
	De	Bas	Are	Rui	t _c (ć*	I (i	0 0	tc	C*	i) l	o o	Ost	C*	Slo	Q _{pi}	C*	Slo	Pip	Ler	Vel	t, (
		OS1	0.77	0.45	10.3	0.35	4.08	1.4															Off-site flows overland into Basin A2 Combines flow in swale at DP1
		031	0.77	0.43	10.3	0.30	4.00	1.4															Flows overland into swale at DP1
		A2	0.78	0.35	17.2	0.27	3.31	0.9															Combines flow in swale at DP1
																							Combined flow of Basin OS1 and Basin A2 within swale
	1								17.2	0.62	3.31	2.1				-							Flows continue in swale to DP2 Flows overland into swale at DP2
	2	A1	0.65	0.32	18.5	0.21	3.21	0.7															Combines flow in area inlet at DP2.1
	-		0.00	0.02	10.0	. 0.21	0.21	0.7															Combined flow of DP1 and DP2 within area inlet
	2.1								18.5	0.83	3.21	2.7											Flows piped to sump inlet at DP5.1
			0.70		10.1		0.47																Flows overland into swale at DP3
	3	A3	0.79	0.33	19.1	0.26	3.16	0.8															Combines flow at sump inlet at DP5 Flows along c&g at DP4
	4	A4	1.00	0.68	9.6	0.68	4.18	2.8															Combines flow at sump inlet at DP5
																							Flows along c&g at within Basin A5
		A5	2.84	0.50	11.6	1.41	3.91	5.5															Combines flow at sump inlet at DP5
	5								19.1	2.25	3.16	7 4											Combined flow of DP3, DP4, and Basin A5 within sump inlet Flows piped to sump inlet at DP5.1
-	5								19.1	2.30	3.10	7.4											Combined flow of DP2.1 and DP5 within pipe
	5.1								19.1	3 18	3.16	10.0											Flows piped to manhole at DP8.2
	0.1								17.1	0.10	5.10	10.0											
	6	A6	0.66	0.45	7.0	0.29	4.67	1.4															Flows off-site along ex. Dines Blvd. c&g to ex. sump inlet at DP6 Flows piped to ex. Pond W-8
						-												-					Flows along c&g to the on-grade inlet at DP7
	7	A7	2.04	0.50	13.2	1.03	3.71	3.8															Captured flows piped to manhole at DP8.1, bypass runoff to ex. sump inlet at DP11
																				1			Flows along c&g to the on-grade inlet at DP8
	8	A8	1.10	0.64	9.1	0.70	4.27	3.0									<u> </u>			<u> </u>		<u> </u>	Captured flows piped to manhole at DP8.1
	8.1								13.2	1.73	3.71	6.4											Combined flow of DP7 and DP8 at manhole Flows piped to manhole at DP8.2 Combined flow of DP5.1 and DP8.1 at manhole
	8.2								19.1	4.91	3.16	15.5											Flows piped to ex. manhole at DP10.1
					1	1	1										1			1		1	Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g
L	9	A9	0.20	0.38	10.3	0.08	4.08	0.3												L		L	Flows to ex. inlet at DP15
	10	A10	1.32	0.38	13.0	0.50	3.74	1.9															Flows into swale to area inlet at DP10 Piped to manhole at DP10.1
	10	AIU	1.32	0.30	13.0	0.30	3.74	1.9			-			-			-			-			Combined flow of DP8.2 and DP10 at manhole
	10.1								19.1	5.41	3.16	17.1						1		1			Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1

	STANDARD FORM SF-3 - PROPOSED STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)																					
Location	Subdivision: Sterling Ranch Subdivision -Proposed Project Name: Sterling Ranch Filing 5 Location: El Paso County Project Name: 25188.16 Design Storm: 5-Year Calculated By: GAG DIRECT RUNOFF TOTAL RUNOFF STREET/SWALE PIPE TRAVEL TIME																					
	1	1	DIRE		NOFE		1	т			F	STRE	ET/S/M	/ΔI F		PI	ÞF		TRAV	/FL TIN	/F	
STREET	Design Point	Basin ID Area (Ac) Area (Ac) Runoff Coeff. t, (min) T I															REMARKS					
		EX F4 DP5 EX F4 DP6.1					12.0 3.9															Captured runoff to ex. sump inlet at Filing 4 DP5 Piped to sump inlet at DP13 Captured runoff to ex. sump inlet at Filing 4 DP6.1 Piped to sump inlet at DP13 Captured runoff to ex. sump inlet at Filing 4 DP6.2
		EX F4 DP6.2 EX F4 DP6.3					2.0 16.9															Piped to sump inlet at DP13 Combined captured flow DP11, DP12, and DP13 Piped to manhole at DP17.1 Combined flow of DP9 and Basin C4
	14	EX F4 DP9 C4 3.67	7 0.55	27.2	2.04	2.63	3.8 5.4															Piped to ex. Filing 4 storm sever and combines at manhole at DP17.1 Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g Flows to ex. Inlet at DP15 Combined flow of DP9 and Basin C4
	15 16.1	EX F4 DP7.1					39.8	27.2	2.12	2.63	5.6											Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1 Total runoff to ex. manhole at Filing 4 DP7.1 Piped to DP15 and combines at manhole at DP17.1 Combined flow of DP10.1, DP13.1, DP14, DP15 and DP16.1. Filing 4 DP10.
	17.1		\bigwedge								83.1											Total runoff piped to ex. Pond W-5
Notes: Street and Pipe C Values in BLUE in										Filing	No. 4" (lated Au	igust 1	4, 2023	3 by JR	Engine	ering					
		Is t	this n	neai	nt to	be [OP7.	2?	\sim	\sim	\sim	\sim	\sim	\sim	\sim	\sim	\sim	\sim	\sim	\sim	\sim	、

Flow matches flow in report for DP7.2. Revise DP label or flow as needed. Same for 100-year spreadsheet

JR Response: Revised this flow to be the Filing 4 DP7.1. 100-year was correct.

														ORM I	DRAII	VAGE	SF-3 - F SYSTEN d proce	/ DES	SIGN	D			
																Р	roject N	ame:	Sterl	ing Ra	anch Fi	iling 5	
Subdivision:	Sterlin	ig Rancl	h Subdi	ivision	-Propo	osed											Projec	t No.:	2518	8.16		5	
Location:			ty														alculate						
Design Storm:	100-Ye	ear															Checke						
																		Date:	11/3	/23			
	1			DIE	ECT D				т	OTAL			STDI	ET /\$\A/		1	PIP	c		TDAY		ME	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (CfS)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
		001		0.50	40.0	0.45	7.40																Off-site flows overland into Basin A2
		OS1	0.77	0.59	10.3	0.45	7.48	3.4													-		Combines flow in swale at DP1 Flows overland into swale at DP1
		A2	0.78	0.53	17.2	0.41	6.33	2.6															Combines flow in swale at DP1
																					1		Combined flow of Basin OS1 and Basin A2 within swale
	1								17.2	0.86	6.33	5.4											Flows continue in swale to DP2
	2	A1	0.45	0.51	18.5	0.33	6.17	2.0															Flows overland into swale at DP2 Combines flow in area inlet at DP2.1
	2	AT	0.05	0.51	10.0	0.33	0.17	2.0															Combined flow of DP1 and DP2 within area inlet
	2.1								18.5	1.19	6.17	7.3											Flows piped to sump inlet at DP5.1
	_																						Flows overland into swale at DP3
	3	A3	0.79	0.51	19.1	0.41	6.09	2.5															Combines flow at sump inlet at DP5 Flows along c&g at DP4
	4	A4	1 00	0.79	9.6	0.79	7.64	6.0															Combines flow at sump inlet at DP5
	·		1.00	0.77	7.0	0.77	7.01	0.0															Flows along c&g at within Basin A5
		A5	2.84	0.64	11.6	1.82	7.23	13.2															Combines flow at sump inlet at DP5
	5								19.1	2.02	6.09	10 /											Combined flow of DP3, DP4, and Basin A5 within sump inlet Flows piped to sump inlet at DP5.1
	5								19.1	3.02	0.09	10.4											Combined flow of DP2.1 and DP5 within pipe
	5.1								19.1	4.21	6.09	25.7											Flows piped to manhole at DP8.2
																							Flows off-site along ex. Dines Blvd. c&g to ex. sump inlet at DP6
	6	A6	0.66	0.60	7.0	0.40	8.37	3.3															Flows piped to ex. Pond W-8
																					_		Flows along c&g to the on-grade inlet at DP7
	7	A7	2.04	0.65	13.2	1.33	6.92	9.2															Flows along cwg to the on-grade inter at DP7 Cantured flows nined to manbole at DP8.1, bypass runoff to ex, sump inlet at DP11
-	,	111	2.01	0.00	10.2	1.55	0.72	7.2															Captured flows piped to manhole at DP8.1, bypass runoff to ex. sump inlet at DP11 Flows along c&g to the on-grade inlet at DP8
	8	A8	1.10	0.75	9.1	0.82	7.76	6.4															Captured flows piped to manhole at DP8.1
									ľ														Combined flow of DP7 and DP8 at manhole
	8.1			-					13.2	2.15	6.92	14.9											Flows piped to manhole at DP8.2
1																				I			Combined flow of DP5.1 and DP8.1 at manhole
	8.2								19.1	6.36	6.09	38.8								<u> </u>	<u> </u>		Flows piped to ex. manhole at DP10.1
1				0.5																I			Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g
	9	A9	0.20	0.54	10.3	0.11	7.49	0.8															Flows to ex. inlet at DP15
	10	A10	1 22	0 55	12.0	0.70	(07	EO												I			Flows into swale to area inlet at DP10 Bired to methods at DP10 1
	10	A10	1.32	0.55	13.0	0.72	6.97	5.0															Piped to manhole at DP10.1 Combined flow of DP8.2 and DP10 at manhole
	10.1								19.1	7.08	6.09	43.1											Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1

														ORM [DRAI	NAGE :	SF-3 - F SYSTEN D PROC	/ DES	IGN	D						
Location:	Subdivision: Sterling Ranch Subdivision -Proposed Location: El Paso County esign Storm: 100-Year DIRECT RUNOFF TOTAL RUNOFF STE															Project Name: Sterling Ranch Filing 5 Project No.: 25188.16 Calculated By: GAG Checked By: 11/3/23										
	DIRECT RUNOFF TOTAL RUNOFF																PIP	E		TRAV	EL TIN	ЛE				
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS			
		EX F4 D EX F4 D						<mark>13.5</mark> 8.3			F F T	lighl natcl	ighte h rep	ed flo oort. I	ws (Plea	do no ase u	ot ipdat	e _					Captured runoff to ex. sump inlet at Filing 4 DP5 Piped to sump inlet at DP13 Captured runoff to ex. sump inlet at Filing 4 DP6.1 Piped to sump inlet at DP13			
	13.1	EX F4 D EX F4 D EX F4 D	DP6.3					14.2 35.6			E	∽ JR	Res		ہے ise		e b	\frown	~	}			Captured runoff to ex. sump inlet at Filing 4 DP6.2 Piped to sump inlet at DP13 Combined captured flow DP11, DP12, and DP13 Piped to manhole at DP17.1 Combined flow of DP9 and Basin C4 Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1			
		C4		0.70	27.2	2.55	5.30	13.5				\sim						×)			Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g Flows to ex. inlet at DP15 Combined flow of DP9 and Basin C4			
	15 16.1	EX F4 C)P7.1					93.5	27.2	2.66	5.30	14.1											Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1 Total runoff to ex. manhole at Filing 4 DP7.1 Piped to DP15 and combines at manhole at DP17.1			
	17.1											194.0											Combined flow of DP10.1, DP13.1, DP14, DP15 and DP16.1. Filing 4 DP10. Total runoff piped to ex. Pond W-5			
Notes: Street and Pipe C Values in BLUE in											iling N	o. 4" da	ted Aug	ust 14, 2	023 by	JR Engi	ineering	<u> </u>	<u> </u>	L	<u> </u>					

JR Response:

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• DP11 (Ex. F4 DP5) = Correct value from the 100-year inlet capacity in highlighted inlet calculation in the excerpts. Included total values from the existing design points and captured flow values in the pipe column.

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• DP12 (Ex. F4 DP6.1) = Revised value from the 100-year inlet capacity in highlighted inlet calculation in the excerpts. Included total values from the existing design points and captured flow values in the pipe column.

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- DP13 (Ex. F4 DP6.2) = Revised value from the 100-year inlet flow in highlighted inlet calculation in the excerpts. Included total values from the existing design points and captured flow values in the pipe column.
- DP14 (Ex. F4 DP9) = Correct value from the 100-year inlet capacity in highlighted inlet calculation in the excerpts. Included total values from the existing design points and captured flow values in the pipe column.

Appendix C Reference Material



MASTER DEVELOPMENT DRAINAGE PLAN FOR STERLING RANCH

OCTOBER 2018

Prepared for:

Morley-Bentley Investments, LLC 20 Boulder Crescent, 2nd Floor Colorado Springs, CO 80903 (719) 471-1742

Prepared by:



20 Boulder Crescent, Suite 110 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-002 SKP-18-003 SF-17-024

HW/D ratio of ~ 1.3 . The peak detained volume has been estimated at 78.2 ac-ft. A low point in Sterling Ranch Road will be designed adjacent to the facility to provide a safe overflow route. An exhibit showing the concept design and its various elements is included in the appendix of this report.

As previously discussed a Condition Letter of Map Revision and Letter of Map Revision (CLOMR/LOMR) will need to be processed through the Federal Emergency Management Agency (FEMA) to revise the hydrology to the Sand Creek Channel and allow for the remapping of the revised floodplains. It should be noted that the DBPS flow rates for Reach SC-8 (Reach 163) adjacent to this location were estimate to be 2,630 cfs and that the effective FEMA 100 year flow rate is 2,600cfs. A comparison table of the various flow rates is provided later in this text and on the accompanying drainage maps.

The final design of the culvert crossing and final determination of approved rates as well as the final pond design will be discussed within the future Sterling Ranch Channel Design Report and Sand Creek CLOMR/LOMR documents. No deviations for this pond and accompanying outlet structure are anticipated at this time.

It is important to note that the planned discharge outlet pipe for the FSD pond located to the west of the pond W3 will need to be extended to the downstream outlet side of the culvert to ensure that the 100 year water surface elevation with W3 does not affect the functionality of the adjacent FSD and its storm sewer systems.

In regards to timing, the need to construction this facility can be tied to the Sand Creek Channel improvements which is discussed within this report and also within the Subdivision Improvements Agreement. In no case should runoff from the East Fork of Sand Creek be diverted to the Main Branch of the Sand Creek Channel prior to the construction and of this facility.

Basin SC3-11A (Q5 = 7.8 cfs, Q100 = 24.3 cfs) consists of a 10.7 acre area located within of Sterling. Ranch, that is south of Sterling Ranch Road, west of Sand Creek. This portion of Sterling Ranch consists of single family residential for lots ranging in size from 0.2 to 0.3 acres in size and open space associated with the Sand Creek Channel. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems to a full spectrum detention pond FSD11A. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 0.9 cfs and 12.3 cfs in the 5 and 100 year events respectively just upstream of DP-63. It should be noted that this detention facility may not be necessary if grading can be oriented to force surface runoff to the west.

Basin SC3-11B (Q5 = 81.3 cfs, Q100 = 213.7 cfs) consists of a 76.6 acre area located within of Sterling. Ranch, that is south of Sterling Ranch Road, east of Sand Creek. This portion of Sterling Ranch consists of single family residential planned for lots ranging in size from 0.2 to 0.3 acres in size and a portion of a park site and collector roadways. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems westward to a full spectrum detention pond FSD11B. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 4.5 cfs and 69.5 cfs in the 5 and 100 year events respectively. The runoff from DP68 and from FSD ponds 11A and 11B combine at DP63 at peak flow rates of Q5 = 201.0 cfs, Q100 = 1385.1, which is less than the anticipated existing modeled flow rates of Q5 = 430.7 cfs, Q100 = 1911.5 at DP63. Runoff from DP63 continues south within the Sand Creek Channel toward DP61.

Basin SC3-7 (Q5 = 69.9 cfs, Q100 = 157.2 cfs) consists of a 45.7 acre industrial zoned area, referred to as the Barbarick Subdivision, located outside of Sterling Ranch. Per the Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3 and 4 the filing consists of four lots which upon which development will be constructed which will include adding a proposed Extended Detention Basin within Lot 4. This detention basin will provide water quality treatment for portions of Lots 1 & 2, and Lots 3 & 4. The EBD will structure will outfall at the south end of Lot 4 at the Barbarick Subdivision/Sterling Ranch property line. Per the report the proposed total outflow from the EDB pond will be Q5 = 0.3 cfs, Q100 = 45.9** cfs(**which includes pass through flows of 29.4 cfs). A second Sand Filter Basin water quality detention catchment will be provided at the southeast/downstream end of Lot 2. The SFB will outfall at the southeast corner of the Lot 2 at the Barbarick Subdivision/Sterling Ranch property line. Per the report the proposed total outflow the SFB pond will be Q5 = 0.1 cfs, Q100 = 3.6 cfs. At the initial writing of this report, neither EDB nor SFB structure has been fully constructed, and thus the assumption was made to utilize the full un-detained untreated runoff from the offsite development for onsite drainage planning purposes. Thus the downstream facilities planned within Sterling Ranch will account for the total un-detained runoff from the parcel of Q5 = 69.9 cfs, Q100 = 157.2 cfs and will plan to treat the total runoff onsite facilities. This provides a conservative approach for master planning. Runoff discharged from the property will be collected by proposed storm sewer within Sterling Ranch and routed to DP64. These facilities and their effects on drainage will be re-reviewed with subsequent drainage report and shall be implemented into final design and construction.

Basin SC3-6B (Q5=43.4 cfs, Q100=102.7 cfs) consists of a 30.9 acre area located within of Sterling Ranch, that is north of Sterling

Ranch Road and west of Sand Creek. This portion of Sterling Ranch will consist of single family residential planned for lots ranging in size from 0.1 to 0.33 acres in size, a school site and portion of the local collector roadways. Runoff from the developed portion of the basin shall be collected and conveyed within street and storm sewer systems where it combines with flows from Basin SC3-7 at DP64 (Q5 = 112.1 cfs, Q100 = 258.0 cfs). The combined runoff continues south toward Pond FSD6.

Basin SC3-6A (Q5=79.3 cfs, Q100=177.1 cfs) consists of a 49.3 acre area located within of Sterling Ranch, that is north and east of Marksheffel Road and of Sterling Ranch Road and west of Sand Creek. This portion of Sterling Ranch is planned for a commercial site and single family residential lots ranging in size from 0.2 to 0.3 acres lots as well as portions of major and local collector roadways. Developed runoff from the basin shall be conveyed within street sections and storm sewer systems and directed to FSD Pond 6.

Basin SC3-6C (Q5=72.5 cfs, Q100=181.5 cfs) consists of a 58.0 acre area located mostly within the confines of Sterling Ranch, near the south boundary of the site, west of the Sand Creek Channel. This portion of Sterling Ranch is planned for a commercial site and single family residential lots ranging in size from 0.2 to 0.3 acres lots as well as portions of major and local collector roadways. A small segment of the existing Pawnee Rancheros subdivision (5 acres lots) also falls within the basin. Where not sheet flowing into the creek, the developed runoff from the basin shall be conveyed within street sections and storm sewer systems and directed to FSD Pond 6. Runoff from DP64 and from Basins SC3-6B and 6C will combine in FSD6. The treated detained flows from the pond will discharge into Sand Creek at peak flow rates of 7.5 cfs and 149.6 cfs in the 5 and 100 year events respectively. Flows from FSD6 outfall into the Sand Creek Channel at DP61.

Basin SC3-8 (Q5 = 42.1 cfs, Q100 = 166.2 cfs) consists of 143.4 acres located outside of Sterling Ranch and to the west of Basin SC3-15A. In the developed condition, it is assumed that the remaining large parcel are fully developed into 5 acres lots. Runoff from the basin is conveyed as surface flows to Basin SC3-9.

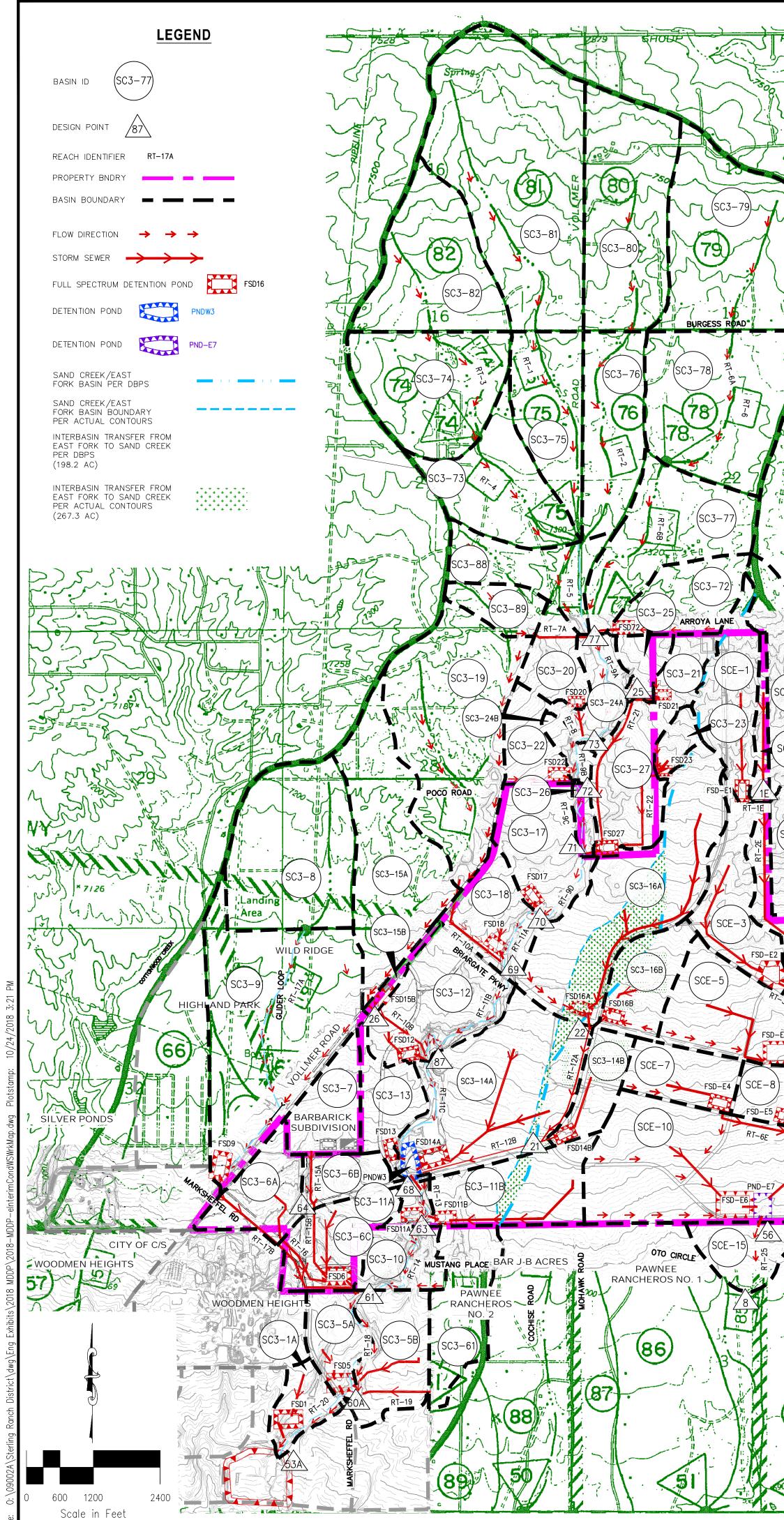
Basin SC3-9 (Q5 = 71.5 cfs, Q100 = 254.0 cfs) consists of 217.4 acres located to northwest of Vollmer Road and south of Basin SC3-8. In the current condition, much of the large parcel has been developed into 2.5-5 acres lots. The calculated runoff will assume that that Vollmer Road is widened as a part of this project. Runoff from Basins SC3-8 and SC3-9 combine within the roadside ditches and natural drainage ways within the development before combining within an upgraded roadside swale located along the west side of Vollmer Road which discharges into a full spectrum detention pond (FSD9) located at the south end of the basin. The treated detained flows from the pond are conveyed under Vollmer and along Marksheffel Road within a storm drain or stabilized channel to Sand Creek at peak flow rates of 24.9 cfs and 289.9 cfs in the 5 and 100 year events respectively just downstream of DP-61.

Basin SC3-10 (Q5 = 12.3 cfs, Q100 = 47.7 cfs) consists of 36.0 acres (located outside of Sterling Ranch), of the existing Pawnee Rancheros Filing No 2 (5 acre lots), that is located to the east of Basin SC3-6. Runoff from the basin is conveyed as surface drainage to the Sand Creek Channel, where it combines with flows discharged from FSD Ponds 6 and 9 and from DP 63 at the County/City Boundary (DP-61) at peak flow rates of 223.9 cfs and 1620.1 cfs in the 5 and 100 year events respectively. It is anticipated that easements from the owner of the property located to the south of the Sterling Ranch will be required to outfall the storm sewer from FSD6 and FSD9 as well as provide an emergency overflow route. Runoff from DP61 continues south within the Sand Creek Channel toward DP60A.

Basin SC3-5A (Q5 = 53.7 cfs, Q100 = 129.1 cfs) is a 39.1 acres offsite area located to the south of Sterling Ranch, west of the Sand Creek Channel. In the developed condition, it is assumed that this area will be developed into 0.1 acre residential lots, portions of Marksheffel Road and stabilized segments of the Sand Creek Channel. Runoff produced from within the basin shall be directed to a proposed full spectrum detention facility (FSD5) located at the southeast corner of the basin upstream of DP-60A. Released flows from the pond will discharge into Sand Creek at peak flow rates of 1.4 cfs and 30.1 cfs in the 5 and 100 year events.

Basin SC3-61 (Q5 = 22.0 cfs, Q100 = 84.8 cfs) is a 65.5 acres offsite area located to the south of Sterling Ranch east of Basin SC3-5B, that is made up of 5 acre lots. With the development of filing SC3-5B, a storm sewer bypass line will be constructed to safely convey the upstream runoff thru the development to the channel just upstream of DP-60A.

Basin SC3-5B (Q5 = 73.0 cfs, Q100 = 187.0 cfs) is a 63.0 acres offsite area located to the south of Sterling Ranch east of Basin SC3-5A. In the developed condition, it is assumed that the majority of the area will be subdivided into 0.1 acre residential lots. Water quality treatment only is anticipated for this area and thus a FSD pond has not been included in the modeling. Runoff produced from within the basin shall be directed to Sand Creek just upstream of DP-60A. The runoff from DP61, FSD5 and from Basins SC3-5B and SC3-61 combine at DP60A at peak flow rates of Q5 = 224.8 cfs, Q100 = 1661.8, which is less than the anticipated existing modeled flow rates of Q5 = 430.2 cfs, Q100 = 1913.5 at DP60A. Runoff from DP60A continues south within the Sand Creek Channel toward



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AND FREE AND	340.	BASIN SC3-1A SC3-5A SC3-5B	CN 73 84 81	AREA (ACRES) 27.8 39.1 63.0	AREA (so m) 0.044 0.061 0.098	Q2 (crs) 16.3 40.6 53.8	(crs) 23.3 53.7 73.0	Q10 (CFS) 33.0 71.0 98.5	Q25 (CFS) 45.8 92.4 130.8	Q 55 57.1 110.6 158.6	0,100 (cFS) 68.9 129.1 187.0	
223/3 <	Dr	SC3-6A SC3-6B SC3-6C	88 85 82	49.3 30.9 58.0	0.077 0.048 0.091	61.4 32.9 53.9	79.3 43.4 72.5	102.2 57.0 97.1	130.1 73.9 128.0	153.6 88.2 154.5	177.1 102.7 181.5	
States.	Sai	SC3-7 SC3-8 SC3-9	88 62 66	45.7 143.4 217.4	0.071 0.224 0.340	54.0 25.4 45.8	69.9 42.1 71.5	90.3 66.7 108.6	115.2 100.7 158.9	136.2 132.3 204.9	157.2 166.2 254.0	
	۶.	SC3-10 SC3-11A SC3-11B	63 70 80	36.0 10.7 76.6	0.056 0.017 0.120	7.6 5.3 59.4	12.3 7.8 81.3	19.4 11.3 110.8	29.1 15.9 148.1	38.0 20.0 180.5	47.7 24.3 213.7	
C3-79		SC3-12 SC3-13 SC3-14A	81 85 79	88.2 41.0 164.9	0.138 0.064 0.258	77.8 43.9 127.6	105.6 57.8 175.4	142.5 76.0 239.8	189.1 98.5 321.9	229.1 117.6 393.2	270.0 136.9 466.3	
		SC3–14B SC3–15A SC3–15B	77 62 87	34.7 139.7 7.9	0.054 0.218 0.012	24.6 21.3 10.8	34.3 35.5 14.0	47.4 56.3 18.2	64.2 85.3 23.3	79.0 112.1 27.6	94.1 141.0 31.9	
		SC3-16A SC3-16B SC3-17	74 78 73	168.1 50.7 70.6	0.263 0.079 0.110	84.4 39.0 41.8	120.4 53.7 59.6	170.0 73.6 85.2	234.8 99.0 119.0	292.2 121.1 149.1	351.8 143.8 180.6	
ROAD	17449	SC3-18 SC3-19 SC3-20	81 62 65	53.8 184.0 34.2	0.084 0.287 0.053	49.3 28.8 9.9	67.1 47.7 15.5	91.0 75.7 23.8	121.2 114.4 35.1	147.3 150.2 45.5	174.0 188.8 56.6	
RTORY	$\langle \langle \rangle$	SC3-21 SC3-22 SC3-23	66 65 67	23.3 33.9 14.5	0.036 0.053 0.023	7.0 9.4 5.5	10.8 14.8 8.3	16.3 22.5 12.4	23.7 32.9 18.0	30.4 42.5 23.0	37.5 52.6 28.4	
Tank S		SC3–24A SC3–24B	65 65	35.7 12.2	0.056 0.019	13.0 3.4	20.4 5.3 8.9	31.1 8.1 13.4	45.7 11.8	59.0 15.2	73.2 18.9	
in the second states in the se		SC3-25 SC3-26 SC3-27	66 63 71	19.0 10.0 70.0	0.030 0.016 0.109	5.8 2.5 35.1	4.0 51.2	6.2 73.8	19.5 9.2 103.7	25.1 12.1 130.3	31.0 15.1 158.3	
2 3 3	7359	SC3-61 SC3-72 SC3-73	63 64 63	65.5 56.2 90.0	0.102 0.088 0.141	13.7 12.8 16.4	22.0 20.2 26.4	34.4 31.4 41.3	51.6 46.7 62.1	67.6 60.9 81.3	84.8 76.0 102.0	
	لیم - کړ الله ا	SC3-74 SC3-75 SC3-76	63 63 63	119.7 79.3 86.4	0.187 0.124 0.135	22.3 13.1 14.2	36.5 21.5 23.1	57.3 33.7 36.4	85.9 50.5 54.6	112.3 66.1 71.4	140.7 82.8 89.6	
		SC3-77 SC3-78 SC3-79	62 63 63	106.9 155.6 189.0	0.167 0.243 0.295	16.6 28.1 34.9	27.6 45.3 57.0	43.8 70.6 89.5	66.2 106.2 134.3	87.0 139.1 175.6	109.4 174.5 220.1	
	2.25	SC3-80 SC3-81 SC3-82	63 62 62	147.7 262.9 117.8	0.231 0.411 0.184	27.3 42.6 20.0	44.3 70.2 33.2	69.6 111.0 52.8	104.5 167.4 80.0	136.8 219.6 105.1	171.4 275.7 132.3	
	5	SC3-88 SC3-89 SCE-1	62 62 65	60.2 27.5 64.4	0.094 0.043 0.101	10.5 6.1 23.3	17.4 10 35.9	27.6 15.7 53.8	41.8 23.6 79.1	54.9 30.8 102.4	69.0 38.6 127.4	
		SCE-2 SCE-3 SCE-4	64 70 70	15.0 67.5 29.5	0.023 0.105 0.046	4.4 30.6 13.3	7.0 45.2 19.6	10.8 65.9 28.6	15.9 93.3 40.6	20.7 118.0 257.8	25.7 143.9 62.6	
CE-1) (SCE-13) (SCE-13)		SCE-5 SCE-6 SCE-7	87 64 89	85.5 3.8 44.9	0.134 0.006 0.070	100.4 1.6 58.9	130.6 2.5 75.5	169.6 3.7 96.6	217.4 5.4 122.2	257.8 7.0 143.7	298.4 8.6 165.2	
5-23	UNS DRIVE	SCE-8 SCE-9 SCE-10	92 64 83	25.5 4.0 174.3	0.040 0.006 0.272	38.6 1.5 7.6	48.4 2.4 189.4	60.7 3.6 19.4	75.4 5.3 29.1	87.7 6.8 398.9	99.9 8.5 467.5	
SCE-2	ر ۲ WELLS	SCE 10 SCE-11 SCE-13 SCE-14	64 63 63	5.8 78.6 52.5	0.009 0.123 0.082	2.3 19.6 13.2	3.6 31.3 21.2	5.5 48.7 33.3	8.0 73.1 49.9	10.3 95.7 65.2	12.8 120.0 81.7	
	TTLERS TRAIL	SCE-15	51	39.7	0.062	2.2	5.1	10.1	17.7	25.1	33.4	
RT-1E SCE-14	ROAD	DESIGN POINT DP-74	AREA (sq mi) 0.371	Q2 (CFS) 39.3	Q5 (crs) 65.3	Q10 (cFS) 104.8	Q25 (CFS) 158.9	Q50 (CFS) 209.1	Q100 (CFS) 262.8		LOCATI	ON
HI-IN AND AND AND AND AND AND AND AND AND AN	RAYGOR	DP-75 DP-77 DP-78	1.413 2.343 0.538	141.2 209.9 59.7	235.1 351.9 98.4	376.6 580.6 154.0	566.6 886.6 232.6	750.9 1168.4 306.2	950.5 1467.7 385.3	A	RROYA LAN	IE X-ING
STAPLETON ROAD		DP-73 DP-72 DP-71	2.471 2.543 2.757	207.5 206.2 205.9	354.3 352.5 349.3	588.5 586.7 610.5	897.1 897.2 932.4	1187.2 1195.3 1226.9	1506.7 1518.6 1612.2		POCO ROAD ; RANCH NO) X—ING DRTHERN BNDRY
CE-3 SCE-4		DP-70 DP-69 DP-87	2.867 3.238 3.594	205.3 212.7 216.9	349.8 366.6 374.6	614.0 653.7 681.9	940.1 1010.6 1072.1	1260.6 1364.1 1471.5	1636.7 1775.7 1905.9	BRIAF	rgate pari	KWAY X-ING
FSD-E2		DP-68 DP-64 DP-63	4.312 0.119 4.449	214.6 85.9 154.4	374.5 112.1 201.0	714.9 145.9 375.7	1187.6 187.5 815.9	1674.9 222.6 1112.1	2204.1 258.0 1385.1		STREAM OF	POND W3 DUTHERN BNDRY
RT-3E		DP-61 DP-60A	5.356 5.617	156.6 161.6 161.6	223.9 224.8	428.0 439.1	928.2 950.4	1287.3 1320.5 1326.0	1620.1 1661.8	COLORADO N) SPRINGS/ IARKSHEFFE	EL PASO BNDRY
FSD-E3	A	DP-53A DP-1E DP-2E	5.661 0.247 0.486	23.9 48.9	225.7 38.3 76.8 75.7	441.8 70.1 123.0	951.1 132.8 228.7	173.0 319.7	1668.9 220.9 419.4	JAN	U UNLEN A	
		DP-3E DP-4E	0.626 0.745 1.017	48.5 48.1 23.1	75.7 76.2 35.3	122.2 122.4 71.5	271.1 286.9 108.3	387.1 407.3 152.1	500.1 534.8 196.4		AR SE PRO	
JE JE	Τ,	DP-56	1 0 7 0	<u> </u>	770				200.7	I BFT	OW SE PRO	OP CORNER
4 SCE-8 ₩ FSD-E5 ₩ SCE-9		DP-8 DP-21 DP-22	1.079 0.396 0.342	24.1 0.6 0.6	37.2 8.8 8.8	73.5 17.8 17.6	111.3 57.1 56.8	155.4 116.8 105.1	174.9 156.4			
		DP-8 DP-21	0.396	0.6	8.8	17.8	57.1	116.8	174.9			
RT-6E		DP-8 DP-21 DP-22 DP-25 DP-26	0.396 0.342 0.066 0.012 AREA	0.6 0.6 5.9 0.1	8.8 8.8 9.1 1.1 DES	17.8 17.6 16.3 3.2	57.1 56.8 35.1 7.3	116.8 105.1 46.4 9.5	174.9 156.4 58.2 12.0	UME)		10N
RT-6E PND-E7	55	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-76 DESIGN POINT DP-74 DP-75	0.396 0.342 0.066 0.012 AREA (sq MI) 0.371 1.413	0.6 0.6 5.9 0.1 V ₂ (AC-FT) 5.9 22.7	8.8 9.1 1.1 DESI (AC-FT) 9.0 34.5	17.8 17.6 16.3 3.2 GN PO V10 (AC-FT) 13.6 51.7	57.1 56.8 35.1 7.3 INT SU (AC-FT) 19.8 75.4	116.8 105.1 46.4 9.5 MMAR) (AC-FT) 25.5 97.1	174.9 156.4 58.2 12.0 (VI00 (AC-FT) 31.6 120.5		LOCAT	
FSD-E5 RT-6E V-2 SD-E6 SCE-9 SCE-9 SCE-9 SCE-11 SCE-11 SCE-11 SCE-11 SCE-11 SCE-11 SCE-9	55	DP-8 DP-21 DP-22 DP-25 DP-26 DESIGN POINT DP-74 DP-75 DP-77 DP-78 DP-73	0.396 0.342 0.066 0.012 AREA (so MI) 0.371 1.413 2.343 0.538 2.471	0.6 0.6 5.9 0.1 V2 (AC-FT) 5.9 22.7 37.7 8.9 40.0	8.8 9.1 1.1 DES (AC-FT) 9.0 34.5 57.4 13.5 60.8	17.8 17.6 16.3 3.2 GN PO (AC-FT) 13.6 51.7 85.9 20.1 91.0	57.1 56.8 35.1 7.3 INT SU (AC-FT) 19.8 75.4 125.1 29.3 132.5	116.8 105.1 46.4 9.5 MMAR √₅ (AC-FT) 25.5 97.1 161.1 37.7 170.7	174.9 156.4 58.2 12.0 (VIC) (VIC) (ко-гл) 31.6 120.5 199.9 46.7 211.7		ARROYA LAN	NE X—ING
FSD-E5 FSD-E5 RT-6E RT-6E SCE-9 SCE-9 SCE-11 SCE-11 PND-E7 SD-E6 SCE-11 SCE-11 SCE-11 SCE-11 SCE-11 SCE-9 SCE-11 SCE-9	55	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-76 DP-77 DP-74 DP-77 DP-77	0.396 0.342 0.066 0.012 AREA (so m) 0.371 1.413 2.343 0.538	0.6 0.6 5.9 0.1 Vz (AC-FT) 5.9 22.7 37.7 8.9	8.8 9.1 1.1 DES Vs (AC-FT) 9.0 34.5 57.4 13.5	17.8 17.6 16.3 3.2 GN РО (дс-гг) 13.6 51.7 85.9 20.1	57.1 56.8 35.1 7.3 INT SU V25 (AC-FT) 19.8 75.4 125.1 29.3	116.8 105.1 46.4 9.5 MMAR ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ 161.1 37.7	174.9 156.4 58.2 12.0 (VOL) V100 (AC-FT) 31.6 120.5 199.9 46.7		ARROYA LAN Poco roai	NE X—ING
FSD-E5 <i>RT-6E</i> <i>AE</i> SCE-9 <i>RT-6E</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i> <i>SCE-11</i>	1	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-75 DP-74 DP-74 DP-75 DP-77 DP-78 DP-73 DP-72 DP-71	0.396 0.342 0.066 0.012 AREA (so m) 0.371 1.413 2.343 0.538 2.471 2.543 2.757	0.6 0.6 5.9 0.1 <u>V2</u> (AC-FT) 5.9 22.7 37.7 8.9 40.0 41.3 46.3	8.8 9.1 1.1 DESI V₅ (xc-FT) 9.0 34.5 57.4 13.5 60.8 62.9 70.0	17.8 17.6 16.3 3.2 GN PO (xc-Fr) 13.6 51.7 85.9 20.1 91.0 94.0 104.3 110.6 127.4 145.6	57.1 56.8 35.1 7.3 INT SU (AC-FT) 19.8 75.4 125.1 29.3 132.5 136.8 151.3	116.8 105.1 46.4 9.5 MMAR 25.5 97.1 161.1 37.7 170.7 176.2 194.5	174.9 156.4 58.2 12.0 (VOL) V100 (AC-FT) 31.6 120.5 199.9 46.7 211.7 218.5 240.8	STERLING	ARROYA LAN Poco Roai G Ranch N	NE X-ING D X-ING ORTHERN BNDRY KWAY X-ING
FSD-E5 RT-6E $4E$ $SCE-9$ $RT-6E$ $4E$ $SCE-11$ $PND-E7$ $SD-E6$ 56 $E-15$ 56 $E-15$ 56 56 56 56 56 56 56 5	1	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-76 DP-77 DP-74 DP-77 DP-77 DP-77 DP-78 DP-73 DP-72 DP-71 DP-70 DP-70 DP-69 DP-64 DP-64 DP-63	0.396 0.342 0.066 0.012 AREA (so MI) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449	0.6 0.6 5.9 0.1 5.9 22.7 37.7 8.9 40.0 41.3 46.3 49.5 57.5 66.5 81.8 7.0 85.6	8.8 9.1 1.1 DES 9.0 34.5 57.4 13.5 60.8 62.9 70.0 74.5 86.1 98.9 123.7 9.1 129.5	17.8 17.6 16.3 3.2 GN PO (AC-FT) 13.6 51.7 85.9 20.1 91.0 94.0 104.3 110.6 127.4 145.6 183.9 11.8 192.3	57.1 56.8 35.1 7.3 NT SU V25 (AC-FT) 19.8 75.4 125.1 29.3 132.5 136.8 151.3 160.1 183.8 209.1 264.9 15.2 276.7	116.8 105.1 46.4 9.5 MMAR 25.5 97.1 161.1 37.7 170.7 176.2 194.5 205.4 235.3 267.1 338.0 18.1 352.8	174.9 156.4 58.2 12.0 (VOL) V100 (x0-FT) 31.6 120.5 199.9 46.7 211.7 218.5 240.8 254.0 290.6 329.1 415.8 21.1 433.5	STERLING STERLING BRIA	ARROYA LAN POCO ROAL G RANCH N RGATE PAR PSTREAM OF G RANCH S	NE X-ING D X-ING ORTHERN BNDRY KWAY X-ING F POND W3 OUTHERN BNDRY
FSD-E5 RT-6E $4E$ $SCE-9$ $RT-6E$ $4E$ $SCE-11$ $PND-E7$ $SD-E6$ 56 $E-15$ 56 $E-15$ 56 56 56 56 56 56 56 5	1	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-76 DP-77 DP-74 DP-77 DP-78 DP-77 DP-78 DP-72 DP-72 DP-72 DP-71 DP-70 DP-69 DP-69 DP-64 DP-64 DP-63 DP-61 DP-60A DP-63A	0.396 0.342 0.066 0.012 AREA (so M) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 5.356 5.617 5.661	0.6 0.6 5.9 0.1 vz (xc-rn) 5.9 22.7 37.7 8.9 40.0 41.3 46.3 49.5 57.5 66.5 81.8 7.0 85.6 103.7 111.0 112.0	8.8 9.1 1.1 DES 9.0 34.5 57.4 13.5 60.8 62.9 70.0 74.5 86.1 98.9 123.7 9.1 129.5 157.8 168.6 170.0	17.8 17.6 16.3 3.2 GN PO (,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	57.1 56.8 35.1 7.3 INT SU 19.8 75.4 125.1 29.3 132.5 136.8 151.3 160.1 183.8 209.1 264.9 15.2 276.7 338.4 359.5 362.6	116.8 105.1 46.4 9.5 MMAR 25.5 97.1 161.1 37.7 170.7 176.2 194.5 205.4 235.3 267.1 338.0 18.1 352.8 431.3 457.7 461.7	174.9 156.4 58.2 12.0 (VOL 12.0 12.0 12.0 12.0 120.5 199.9 46.7 211.7 218.5 240.8 254.0 290.6 329.1 415.8 21.1 433.5 529.8 561.5 566.5	STERLING STERLING BRIA UP STERLING COLORAD	ARROYA LAN POCO ROAL G RANCH N RGATE PAR 2STREAM OF G RANCH SI O SPRINGS, MARKSHEFFE	NE X-ING O X-ING ORTHERN BNDRY KWAY X-ING F POND W3 OUTHERN BNDRY /EL PASO BNDRY
FSD-E5 FSD-E5 RT-6E $4E$ $SCE-9$ $RT-6E$ $4E$ $SCE-11$ $PND-E7$ $SD-E6$ 56 $E-15$ 56 $E-15$ 56 56 $E-15$ 56 56 56 56 56 56 56 5	1	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-76 DP-74 DP-74 DP-75 DP-77 DP-78 DP-73 DP-73 DP-72 DP-73 DP-72 DP-71 DP-70 DP-69 DP-69 DP-69 DP-69 DP-64 DP-63 DP-64 DP-63 DP-61 DP-63 DP-61 DP-63 A DP-53A DP-1E DP-2E DP-3E	0.396 0.342 0.066 0.012 AREA (so mi) 0.371 1.413 2.343 0.538 2.471 2.543 2.757 2.867 3.238 3.594 4.312 0.119 4.449 5.356 5.617 5.661 0.247 0.480 0.620	0.6 0.6 5.9 0.1 vr (xc-rn) 5.9 22.7 37.7 8.9 40.0 41.3 46.3 40.0 41.3 46.3 49.5 57.5 66.5 81.8 7.0 85.6 103.7 111.0 112.0 3.1 6.1 7.0	8.8 9.1 1.1 DES 0 0 0 0 0 0 0 0 0 0	17.8 17.6 16.3 3.2 GN PO (кс-гл) 13.6 51.7 85.9 20.1 91.0 94.0 104.3 110.6 127.4 145.6 183.9 11.8 192.3 235.1 250.4 252.6 8.4 16.9 23.4	57.1 56.8 35.1 7.3 NT SU 19.8 75.4 125.1 29.3 132.5 136.8 151.3 160.1 183.8 209.1 264.9 15.2 276.7 338.4 359.5 362.6 12.7 25.7 36.1	116.8 105.1 46.4 9.5 MMAR 25.5 97.1 161.1 37.7 170.7 176.2 194.5 205.4 235.3 267.1 338.0 18.1 352.8 431.3 457.7 461.7 16.6 33.7 47.4	174.9 156.4 58.2 12.0 (VOL V100, 31.6 120.5 199.9 46.7 211.7 218.5 240.8 254.0 290.6 329.1 415.8 21.1 433.5 529.8 561.5 566.5 20.9 42.2 59.3	STERLING STERLING BRIA UP STERLING COLORAD	ARROYA LAN POCO ROAL G RANCH N RGATE PAR 2STREAM OF G RANCH SI O SPRINGS, MARKSHEFFE	NE X-ING O X-ING ORTHERN BNDRY KWAY X-ING F POND W3 OUTHERN BNDRY /EL PASO BNDRY EL X-ING
FSD-E5 FSD-E5 FSD-E5 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E6 FSD-E7 FSD-E7 FSD-E6 FSD-E7 FSD-FSD-FSD FSD FSD-FSD-FSD FSD-FSD FSD-FSD-FSD FSD-FSD-FSD FSD-FSD-FSD-FSD-FSD-FSD-FSD-FSD-FSD-FSD-	1	DP-8 DP-21 DP-22 DP-25 DP-26 DP-26 DP-76 DP-77 DP-74 DP-77 DP-78 DP-77 DP-78 DP-73 DP-72 DP-71 DP-70 DP-70 DP-69 DP-69 DP-69 DP-64 DP-63 DP-64 DP-63 DP-61 DP-60A DP-61 DP-53A DP-1E DP-2E	0.396 0.342 0.066 0.012	0.6 0.6 5.9 0.1	8.8 9.1 1.1 DESI V₅ (xc-FT) 9.0 34.5 57.4 13.5 60.8 62.9 70.0 74.5 86.1 98.9 123.7 9.1 129.5 157.8 168.6 170.0 5.2 10.4	17.8 17.6 16.3 3.2 GN PO (xc-fr) 13.6 51.7 85.9 20.1 91.0 94.0 104.3 110.6 127.4 145.6 183.9 11.8 192.3 235.1 250.4 252.6 8.4 16.9	57.1 56.8 35.1 7.3 NT SU ($(2-F)$) 19.8 75.4 125.1 29.3 132.5 136.8 151.3 160.1 183.8 209.1 264.9 15.2 276.7 338.4 359.5 362.6 12.7 25.7	116.8 105.1 46.4 9.5 MMAR 25.5 97.1 161.1 37.7 170.7 176.2 194.5 205.4 235.3 267.1 338.0 18.1 352.8 431.3 457.7 461.7 16.6 33.7	174.9 156.4 58.2 12.0 (VOL V100 (AC-FT) 31.6 120.5 199.9 46.7 211.7 218.5 240.8 254.0 290.6 329.1 415.8 21.1 433.5 529.8 561.5 566.5 20.9 42.2	STERLING STERLING STERLING COLORAD N SAN	ARROYA LAN POCO ROAL G RANCH N RGATE PAR PSTREAM OF G RANCH SI O SPRINGS, MARKSHEFFE ID CREEK A CREEK A	NE X-ING O X-ING ORTHERN BNDRY KWAY X-ING F POND W3 OUTHERN BNDRY /EL PASO BNDRY EL X-ING ND POND 3

WATER QU FSD1 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (C STORED VOLUME (AC-FSD5 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD6 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD9 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD11A STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (C STORED VOLUME (AC-FSD11B STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD12 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD13 STORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE (MODELED RELEASE (CI STORED VOLUME (AC-FSD14A TORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (C STORED VOLUME (AC-FSD14B TORM EVENT (YR) PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (CF STORED VOLUME (AC-FSD15B STORM EVENT (YR) DRY PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (CF STORED VOLUME (AC-FSD16A RY STORM EVENT (YR) DRY PEAK INFLOW (CFS) ALLOWABLE RELEASE MODELED RELEASE (CA STORED VOLUME (AC-

DP-DP-

DP-6

DBPS DESIGN POINT DP-50 P-51 (BASIN 86) DP-52 DP-56

Values reported from SCDE DBPS Reach 85(Basin91)=



	 TY &	DETENT	ION PO			,	WATER QUALI	TY & D	ETENTI	ON PO	ND SUI	MMARY	
T		1			1		STORM EVENT (YR)	2	5	10	25	50	100
	2 16.3	5 23.3	10 33.0	25 45.8	50 57.1	100 68.9	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	39.0 0.0	53.7 0.4	73.6	99.0 8.3	121.1 17.2	143.8 28.2
(CFS)	0.1	1.7	3.3	10.9	17.5	25.5	MODELED RELEASE (CFS)	0.0	0.4	0.7	7.9	17.2	28.1
CFS) —FT)	0.1	1.6	3.2	10.9 3.6	17.4 1.9	25.4 2.2	STORED VOLUME (AC-FT)	3.0	3.9	5.1	5.1	5.3	5.8
					1.0		FSD17						
	2	5	10	25	50	100	STORM EVENT (YR) PEAK INFLOW (CFS)	2 41.8	5 59.6	10 85.2	25 119.0	50 149.1	100 180.6
·>	40.6	53.7	71.0	92.4	110.6	129.1	ALLOWABLE RELEASE (CFS)	0.7	11.1	22.5	52.0	67.2	86.3
(CFS) CFS)	0.1	1.4	2.6	11.3	19.8 19.7	30.2 30.1	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.7 2.6	8.4 2.6	22.4 2.8	52.0 3.4	67.2 4.0	86.1 4.7
-FT)	3.0	3.2	3.8	4.1	4.7	5.2		2.0	2.0	Ζ.υ	J.+	4.0	4./
							FSD18 STORM EVENT (YR)	2	5	10	25	50	100
	2	5	10	25	50	100	PEAK INFLOW (CFS)	49.3	67.1	91.0	121.2	147.3	174.0
(CFS)	196.5 0.5	258.5	339.1 14.6	438.7 58.4	523.3 99.6	608.6 149.7	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.6 0.6	9.2 6.3	18.4 18.4	42.2	54.6 54.6	69.9 69.6
CFS) —FT)	0.5 15.5	7.5	14.5 18.7	58.2	99.6	149.6	STORED VOLUME (AC-FT)	3.2	3.2	3.4	4.0	4.7	5.3
<u></u>	10.0	10.4	10.7	20.8	23.3	26.0	FSD20						
	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100
	64.6	105.6	169.5	252.3	327.1	410.1	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	9.9 0.4	15.5 5.5	23.8 11.1	35.1 25.7	45.5 33.2	56.6 42.5
(CFS) CFS)	1.7 1.7	24.9 24.9	49.8 49.8	141.1	207.2 207.0	290.0 289.9	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.4	2.8 0.8	10.9	25.7	33.0 1.0	42.4
–FT)	8.7	8.7	9.6	10.8	12.3	13.8		U. /	0.0	0.8	0.9	1.0	1.2
			- 10			100	FSD21 STORM EVENT (YR)	2	5	10	25	50	100
	2 5.3	5	10 11.3	25 15.9	50 20.0	100 24.3	PEAK INFLOW (CFS)	7.0	10.8	16.3	23.7	30.4	37.5
(CFS)	0.1	1.6	3.2	7.5	9.7	12.4	ALLOWABLE RELEASE (CFS)	0.3 0.3	4.0 3.3	8.0 8.0	18.3 18.3	23.7 23.7	30.3 30.1
CFS) —FT)	0.2	0.9	3.0 0.4	7.5 0.4	9.7 0.5	12.3 0.6	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.3	0.5	8.0 0.5	0.6	0.7	0.8
			<u> </u>]	FSD22						
	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100
(250)	59.4	81.3	110.8	148.1	180.5	213.7	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	9.4 0.4	14.8 5.8	22.5 11.5	32.9 26.5	42.5 34.3	52.6 43.9
(CFS) CFS)	0.3	4.5	8.7 8.6	29.6 29.5	47.7 47.7	69.6 69.5	MODELED RELEASE (CFS)	0.4	5.8	11.4	26.5	34.3	43.8
-FT)	4.8	4.9	5.5	6.4	7.3	8.2	STORED VOLUME (AC-FT)	0.6	0.6	0.7	0.8	0.9	1.0
							FSD23						
	2 77.8	5	10 142.5	25 189.1	50 229.1	100 270.0	STORM EVENT (YR) PEAK INFLOW (CFS)	2 5.5	5 8.3	10 12.4	25 18.0	50 23.0	100 28.4
(CFS)	0.9	105.6	26.7	62.0	80.2	103.2	ALLOWABLE RELEASE (CFS)	0.2	2.4	4.9	11.2	14.5	18.6
CFS) —FT)	0.9 5.2	9.0 5.5	26.7 5.8	61.9 6.7	80.1 7.8	103.1 8.9	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.2 0.3	2.0 0.3	4.9 0.4	11.2 0.4	14.5 0.5	18.6 0.6
<u></u>	J.Z		ງ.ບ	0./	/.0	0.3		0.0	0.0	U. 1	0. 1	0.0	0.0
	2	5	10	25	50	100	FSD27 Storm event (yr)	2	5	10	25	50	100
	43.9	57.8	76.0	98.5	117.6	136.9	PEAK INFLOW (CFS)	38.8	57.6	84.1	119.7	159.2	206.3
(CFS) CFS)	0.4	6.1 4.2	12.3 12.3	28.6 28.6	37.0 36.9	47.6 47.2	ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	1.4 1.4	21 <i>.</i> 1 18.4	42.4 42.3	97.8 97.7	126.4 126.2	161.9 161.9
_F3) _FT)	3.1	3.1	3.3	3.8	4.4	47.2 5.0	STORED VOLUME (AC-FT)	2.7	2.8	42.3	3.2	3.7	4.2
						ļ	FSD72						
	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100
(CFS)	127.6 0.5	175.4 7.5	239.8	321.9 56.2	393.2 95.2	466.3	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	12.8 0.6	20.2 9.6	31.4 19.3	46.7 44.4	60.9 57.4	76.0
CFS)	0.5	7.5	14.4	56.2	95.1	142.2	MODELED RELEASE (CFS)	0.6	9.3	19.2	44.4	57.4	73.4
-FT)	9.9	10.6	11.9	13.5	15.3	17.3	STORED VOLUME (AC-FT)	1.0	1.0	1.1	1.1	1.2	1.3
			1 10	1 05		1 100	STORM EVENT (YR)	2	5	10	25	50	100
	2 24.6	5 34.3	10 47.4	25 64.2	50 79.0	100 94.1	PEAK INFLOW (CFS) MODELED RELEASE (CFS)	214.6 154.3	374.5 200.3	714.9 366.8	1187.6 799.9	1674.9 1085.6	2204.1 1350.6
(CFS)	0.0	0.3	0.5	5.7	11.8	19.3	STORED VOLUME (AC-FT)	154.3 2.8	200.3 9.5	366.8 26.3	799.9 41.2	1085.6 57.2	1350.6 78.2
CFS) —FT)	0.0 1.9	0.3	0.5	4.5 3.5	11.8 3.5	19.3 3.8	FSD-E1				·	·	
							STORM EVENT (YR) PEAK INFLOW (CFS)	2 23.3	5 35.9	10 53.8	25 79.1	50 102.4	100 127.4
	2	5	10	25	50	100	ALLOWABLE RELEASE (CFS)	0.7	11.0	22.1	50.9	65.7	84.1
(CFS)	10.8 0.1	14.0	18.2 3.2	23.3	27.6 9.5	31.9 12.0	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.7 1.3	5.4 1.3	19.9 1.5	48.9 1.8	62.8 2.1	84.0 2.5
CFS)	0.1	1.1	3.2	7.3	9.5	12.0	FSD-E2						
-FT)	0.6	0.6	0.7	0.8	0.9	1.0	STORM EVENT (YR) PEAK INFLOW (CFS)	2 30.6	5 45.2	10 65.9	25 93.3	50 118.0	100 143.9
			.	·			ALLOWABLE RELEASE (CFS)	0.6	9.5	19.2	45.5	59.8	77.6
	2 84.4	5 120.4	10	25 234.8	50 292.2	100 351.8	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.6	3.2 2.3	18.5 2.4	41.3 2.8	58.5 3.3	74.7 3.8
(CFS)	0.6	8.8	17.3	56.2	88.4	128.3	FSD-E3	<u> </u>	2.0	۷.۰۱	۷.۵	0.0	
CFS) —FT)	0.6 7.6	8.8	17.3 8.9	56.2	88.3 12.1	128.3 13.8	STORM EVENT (YR)	2	5	10	25	50	100
				1	<u> </u>	10.0	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	100.4 0.9	130.6 13.2	169.6 26.5	217.4 61.6	257.8 79.8	298.4 102.6
							MODELED RELEASE (CFS)	1.0	6.8	25.7	56.0	79.8	101.3
SIGN	AREA	PARISO			_		STORED VOLUME (AC-FT)	7.0	7.2	7.7	8.9	10.1	11.4
OINT	(SQ MI)	Q100 (CFS)	DESCRI		_		STORM EVENT (YR)	2	5	10	25	50	100
<u>-77</u>	2.343 2.91		SAND CREE	CONDITION EK DBPS	-		PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	58.9 0.3	75.5 4.4	96.6 8.8	122.2 23.0	143.7 32.2	165.2 43.7
	0 75 7	2600	FEM				MODELED RELEASE (CFS)	0.9	2.8	8.7	23.0	32.2	43.6
<u>P-71</u>	2.757		ROPOSED (_		STORED VOLUME (AC-FT)	4.2	4.3	4.7	5.4	6.2	6.9
°−63	4.440	1705 D		CONDITION	$\overline{}$		FSD-E5 STORM EVENT (YR)	2	5	10	25	50	100
-03	4.449 4.33		SAND CREE		_		PEAK INFLOW (CFS)	38.6	48.4	60.7	75.4	87.7	99.9
-60A	5.661	2600 1662 Pf	FEM	AA CONDITION	_		ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.0	0.2	0.4	4.2	8.7 5.1	14.3 10.0
	5.38		SAND CREE		_		STORED VOLUME (AC-FT)	3.0	3.7	4.4	4.8	5.0	5.3
		<u> </u>					FSD-E6 Storm event (yr)	2	5	10	25	50	100
-	-	PS DESI					PEAK INFLOW (CFS)	141.6	189.4	252.5	331.4	398.9	467.5
		RY (PEA		/			ALLOWABLE RELEASE (CFS) MODELED RELEASE (CFS)	0.2	1.9 0.9	3.2 3.2	37.4 18.3	77.3 64.1	125.6 123.3
ARE (SQ M	ÍA MI)	Q10 Q (CFS) (C (EXIST) (EX		REA Q10 (CFS) (PROF	10 Q1 S) (CF XP) (PRC	00 (S) (OP)	STORED VOLUME (AC-FT)	13.0	17.0	21.9	22.2	22.6	23.7
0.3			95.7 0.3 4.1 0.3			0.3 3.5	PND-E7						
1.6			4.1 0.2 56.5 1.6				STORM EVENT (YR) PEAK INFLOW (CFS)	2 46.5	5 75.4	10 121.2	25 285.2	50 402.4	100 548.0
		63.6 26 52 Not analyzed	65.0 0.7		.0 908	8.2	MODELED RELEASE (CFS)	23.1	35.3	71.5	108.3	152.1	196.4
1)=Q10=28	8cfs Q10 EXISTINC	00=115.2cfs / Q	10=345.7cfs ((PROP(Q100=588.9cfs QSED)	3		STORED VOLUME (AC-FT)	1.0	1.8	4.6	10.5	17.9	28.0
(<u>,</u>	(11010				0.010 0						
						ENT, SUITE 110	2018 S	IEKLI	NG R.	ANCH	MDL	P	
						S, CO 80903							
				PHONE: 71	19.955.5485)							
							PROJECT NO 09-002 F	- II (-	ı∖Fna Fxhihit			10.1	

CIVIL CONSULTANTS, INC.

SCALE DESIGNED BY: JD DRAWN BY: JD HORIZ: 1"=2400' CHECKED BY: VAS

VERT: 1"=2400'

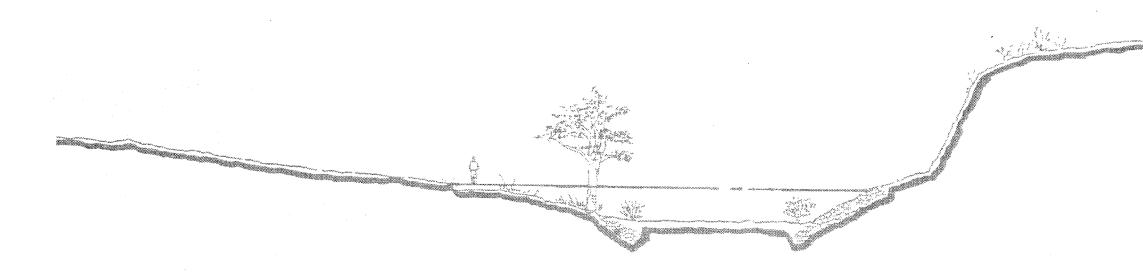
PROJECT NO. 09-002 | FILE: \dwg\Eng Exhibits\2018-MDDP-PROPCOND.dwg DATE: 10-21-2018

DM2

SAND CREEK DRAINAGE BASIN PLANNING STUDY

PRELIMINARY DESIGN REPORT

CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO

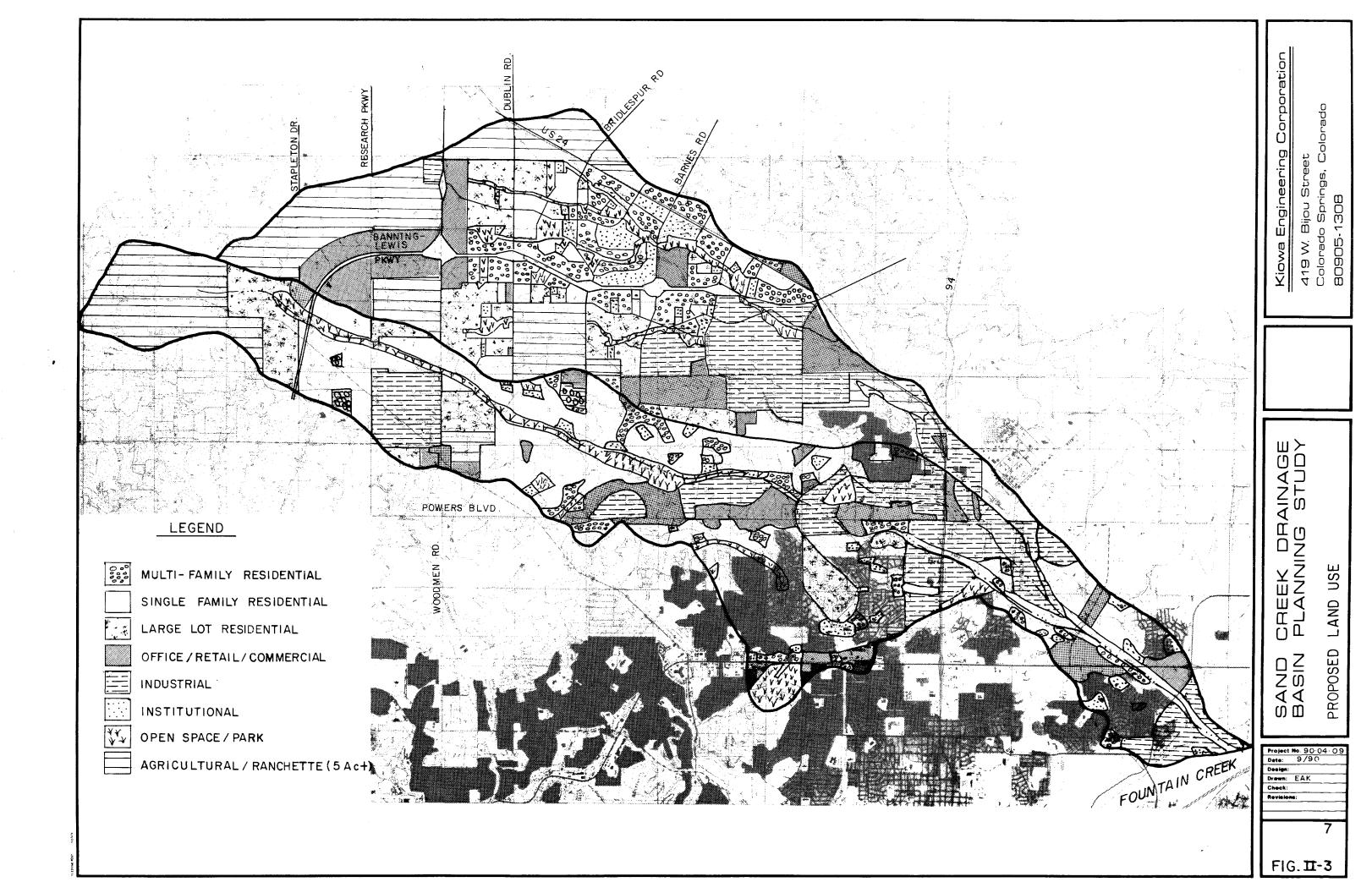


PREPARED FOR:

City of Colorado Springs Department of Comprehensive Planning, Development and Finance Engineering Division 30 S. Nevada Colorado Springs, Colorado 80903

PREPARED BY:

Kiowa Engineering Corporation 1011 North Weber Colorado Springs, CO 80903



Land Use Classification	Percent Impervious	Land Use Density
Multi-Family Residential	65-80	10-24 DU/AC
Single-Family Residential	45-65	6-10 DU/AC
Low Density Residential	30-45	1-6 DU/AC
Large Lot Residential/ Agricultural	5-20	1 DU/AC
Office/Commercial	80-90	
Industrial	85-95	
Institutional	50-75	
Dedicated Open Space/Park	5-10	
Rangeland - Poor to Good Condition	5-20	

NOTE: The above data was used in the preparation of the hydrologic analysis for the Sand Creek Drainage Basin Planning Study. These data are not intended to reflect future land use planning within the City or the County.

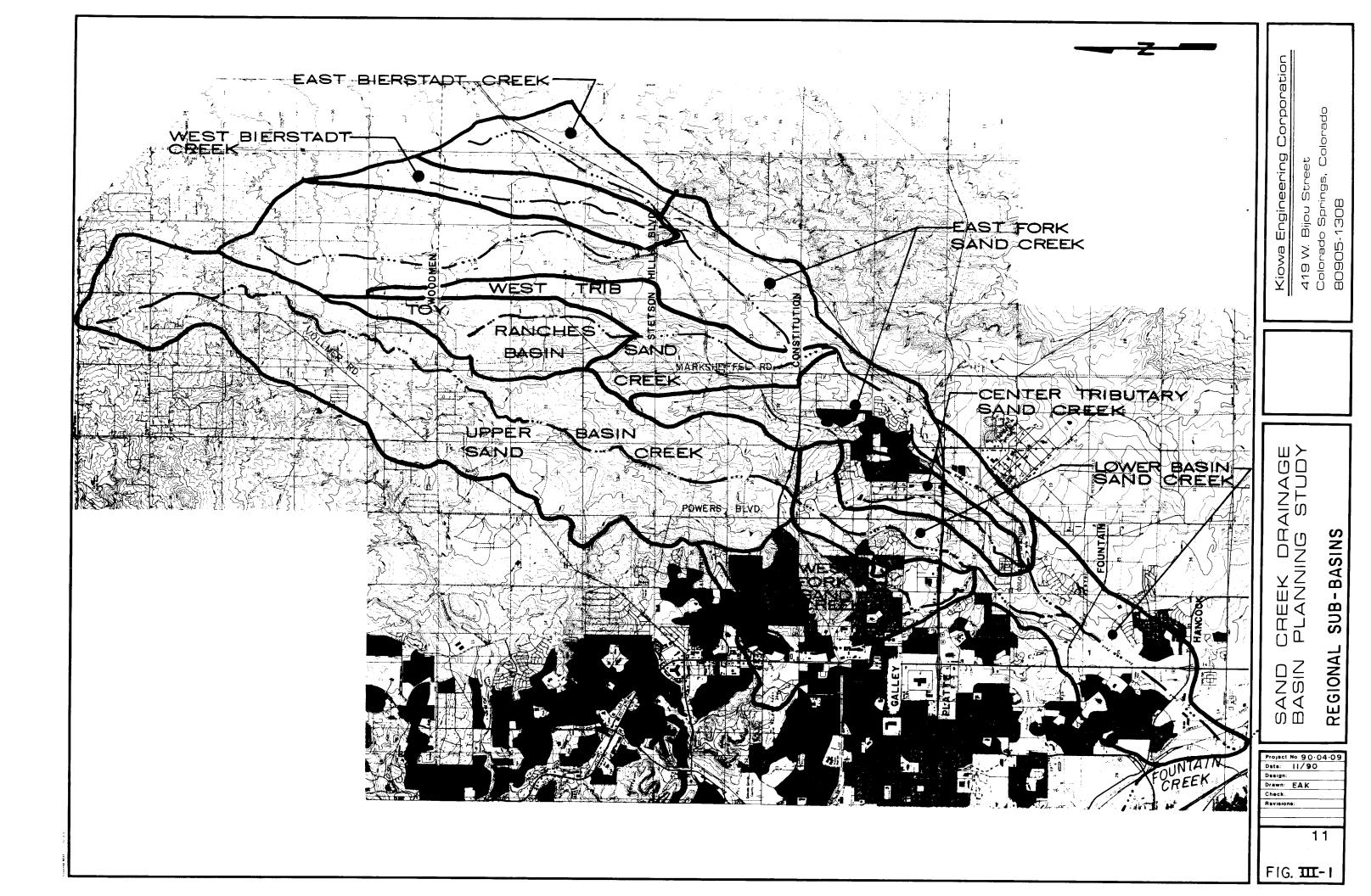
Table III-1. Percent Impervious Values.

Table III	I-2:	Summary 24-hour D Baseline Hy	Durati
Design Point	Location	Area s.m.	100 Ex:
	SAND CREEK (1)		
1	@ Fountain Creek	54.1	
12	Hancock Blvd.	53.1	
19	Fountain Blvd.	50.7	
27	West Fork Sand Creek C.R.I. & P. RR	23.0 16.0	
99 20	North Carefree	13.5	
20 37	Stetson Hills Blvd.	10.0	
60	Woodmen Road	5.4	
75	Black Forest Road	1.4	
	WEST FORK SAND CR	EEK	
27	@ Sand Creek	5.0	
52	U. S. 24	4.8	
59	Constitution Ave.	2.1	
69	South Carefree	1.0	
	CENTER TRIBUTARY	SAND CRE	EK
42	Airport Road	1.6	
43	Powers Blvd.	1.3	
44	U.S.24	1.1	
45	Galley Road	0.8	
	EAST FORK SAND CRE	EEK	
1	@ Center Tributary	24.3	
9	@ East Fork Sub. Tributary	19.8	
29	@ W. Bierstadt Creek	10.6	
40	@ Tamlin Road	4.6	
52	@ Woodmen Road	1.7	
	EAST FORK SUB-TRIB	UTARY SA	ND
11	@ Constitution Avenue	5.9	
15	@ Chicago & Rock Island RR	5.2	
26	@ Confluence w/Toy Ranch	1.0	
47	@ Proposed Dublin Blvd.	0.4	
	WEST BIERSTADT CRI	EEK	
31	@ Confluence w/ East Fork	1.8	
39	@ Tamlin Road	0.8	
54	@ Woodmen Road	0.5	
	EAST BIERSTADT CRE	EK	
32	@ Conf. w/W Bierstadt	2.4	
38	@ Chicago & Rock Island RR	0.4	

(1) Future baseline condition discharges for Sand Creek compiled with the assumption that the discharges from the East Fork Sand Creek basin are maintained at existing rates as shown on this Table.

Peak Discharges ration Storm, AMC-II plogic Conditions

100-year (cfs) Existing	Future	10-year (cfs) Existing	Future
16900	25800	7470	11800
16100	25000	7250	11600
13600	22100	6230	10800
11300	18900	5920	8790
5820	14530	2360	7400
4030	10260	1520	4810
3230	6690	840	3060
2630	3300	760	950
1000	1030	320	350
6840	6840	3200	3200
6860	6860	3230	3230
3450	3450	1680	1680
1630	1630	810	810
K			
1530	2010	650	1200
1300	1710	590	980
1200	1680	580	960
1180	1340	530	650
3970	15600	700	6530
3730	13990	650	6050
2080	7460	400	3330
950	3570	210	1820
460	2120	80	1210
ID CREEK			
1330	4100	240	1630
1250	3540	230	1370
220	820	50	370
100	300	20	140
480	1 59 0	80	600
270	680	50	290
230	420	55	150
520	1520	90	580
120	350	15	130



FINAL DRAINAGE REPORT

BARBARICK SUBDIVISION, PORTIONS OF LOTS 1, 2 and LOTS 3 & 4 El Paso County, Colorado

Sand Creek Drainage Basin

Prepared for: El Paso County Development Services Engineering Division



On Behalf of: Wykota Construction 430 Beacon Light Road, Suite 130 Monument, CO 80132



435 Research Parkway, Suite 300 Colorado Springs, CO 80920 (719) 575-0100 Fax (719) 572-0208

June 6, 2016

15.789.001

(CDO	PREL T Type Urban	R In	ARY DRAI	FILING NO. 1 NAGE REPORT ions - Sump Condit averment-6" Vertical Curb A3") & MAJOR (0.66") storm	tion)
Iniet Length	Storm	Depth		Eqn. 7-32	Eqn. 7-29
			Qw=CwNwLeD^3/2	Qo=CoNo(LeHc)(2g(D-0.5Hc))^1/2	Qm=Cm(QwQo)^1/2
5	Q5	0.43	5,1	5.7	5.0
5	Q100	0.66	9.7	8.6	8.5
G	Q5	0.43	6.1	6.8	6.0
15	Q100	0.66	11.6	10.3	10.2
8	Q5	0.43	8.1	9.1	8,0
8	Q100	0.68	15,4	13.8	13.6
10	Q5	0.43	10.2	11.4	10.0
10	Q100	0.66	19.3	17.2	17.0
12	Q5	0.43	12.2	13.7	12.0
12	Q100	0.66	23.2	20.7	20.3
14	Q5	0.43	14.2	16.0	14.0
14	Q100	0.66	27.0	24.1	23.7
15	Qs	0.43	15.2	17.1	15.0
15	Q100	0.66	29.0	25.8	25.4
16	Q5	0.43	16.2	18.2	16.0
18	Q100	0.68	30.9	27.5	27.1

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Inlet Type	Nw	Cw	No	Co	Cm
CDOT Type 13 Grate	0.7	3.3	0.43	0.6	0.93
Denver No. 16 Grate	0.73	3.6	0.31	0.6	0.9
Curb Opening for Type					
13/Nu. 18 Combination	1	3.7	1	0.66	0.86
CDOT Type R Curb					
Opening	1	3.6	1	0.67	0.93

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Worksheet for FSD Outlet Orifice Plate

Project Description				
Solve For	Diameter			
Input Data	<i>r</i> .			
Discharge		45.90	ft³/s	(16.5 His+29.4 Asc)
Headwater Elevation		4.70	ft	
Centroid Elevation		0.00	ft	
Tailwater Elevation		0.00	ft	
Discharge Coefficient		0.60		
Results				
Diameter		2.37	ft	
Headwater Height Above Centroid		4.70	ft	
Tailwater Height Above Centroid		0.00	ft	
Flow Area		4.40	ft²	
Velocity		10.43	ft/s	

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Worksheet for FSD Overflow - Pass

Project Description				
Solve For	Discharge			
Input Data				
Headwater Elevation		0.90	ft	
Crest Elevation		0.00	ft	
Tailwater Elevation		0.00	ft	
Crest Surface Type	Gravel			
Crest Breadth		12.00	ft	
Crest Length		36.00	ft	
Results				
Discharge		86.22	ft³/s	(55D)+29.4 prec = 44.4 2)
Headwater Height Above Crest		0.90	ft	/
Tailwater Height Above Crest		0.00	ft	
Weir Coefficient		2.80	US	
Submergence Factor		1.00		
Adjusted Weir Coefficient		2.80	US	
Flow Area		32.40	ft²	
Flow Area Velocity		32.40 2.66	ft/s	
and the second sec				
Velocity		2.66	ft/s	

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	Worksheet for SF	B Overflo	w Deve	loped
Project Description	NEF KERK KA	y see se		(6 .2 2) (142) (3)
Solve For	Discharge			
Input Data		n standel		
Headwater Elevation		0.45	ft	-
Crest Elevation		0.00	ft	
Tailwater Elevation		0.00	ft	×
Crest Surface Type	Gravel			
Crest Breadth		6.00	ft	
Crest Length		10.00	ft	
Results				
Discharge		8.08	ft³/s	
Headwater Height Above Cre	est	0.45	ft	
Tailwater Height Above Crest	i i i i i i i i i i i i i i i i i i i	0.00	ft	
Weir Coefficient		2.68	US	
Submergence Factor		1.00		
Adjusted Weir Coefficient		2.68	US	

4.50 ft²

1.80 ft/s

10.90 ft

10.00 ft

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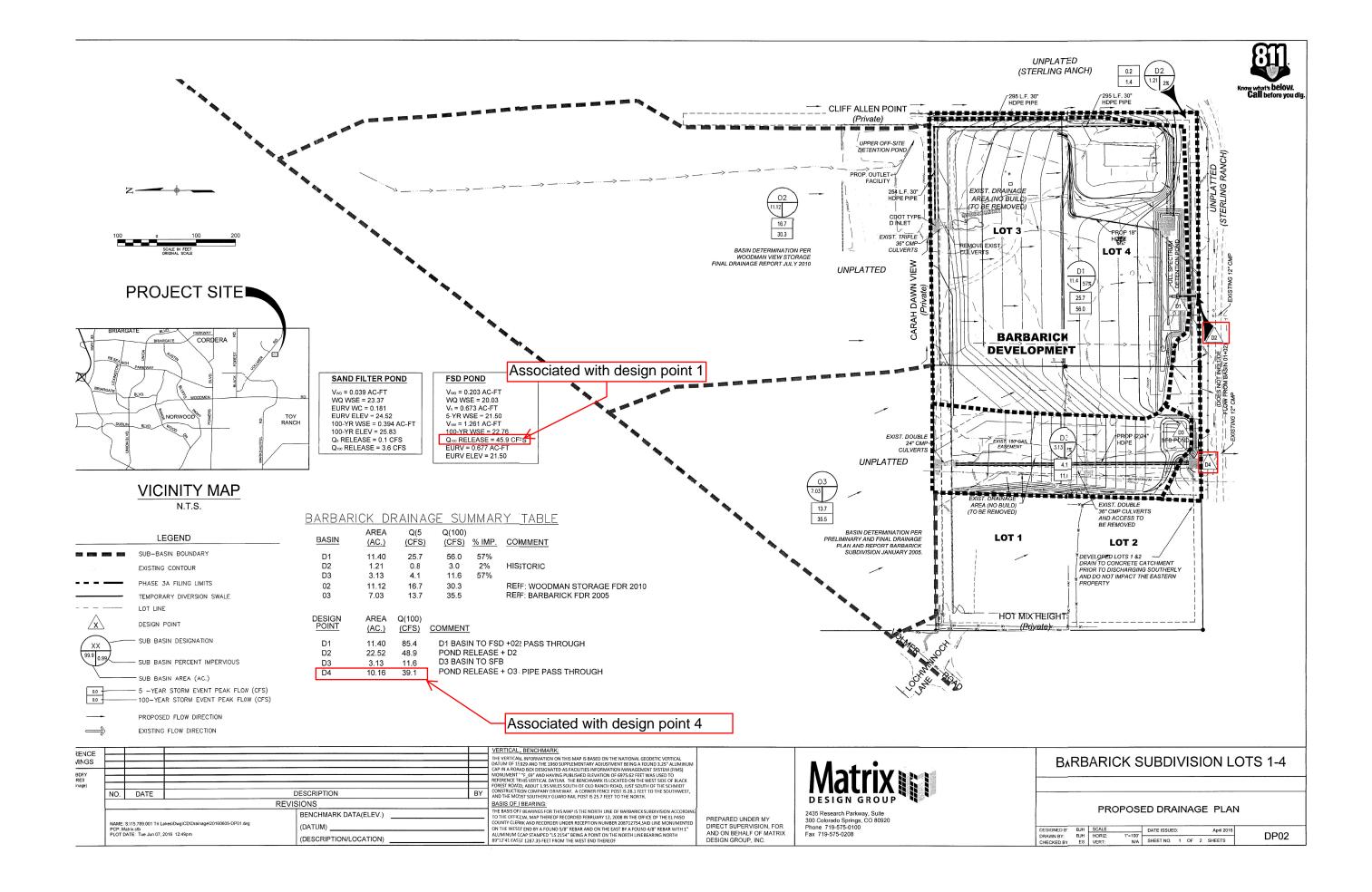
Flow Area Velocity

Top Width

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Wetted Perimeter

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FINAL DRAINAGE REPORT FOR STERLING RANCH FILING NO. 2

Prepared For: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

August 2021 Project No. 25188.01

Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

PCD File No. SF-20-015

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Sterling Ranch Filing No. 2 Location: El Paso County Design Storm: 5-Year

Project Name: Sterling Ranch Subdivision Project No.: 25188.01 Calculated By: AAM Checked By: Date: 8/16/21

	Date: 8/16/21																						
				DIRE	CT RUI	NOFF			т	DTAL P	RUNOF	F	STRE	et/sw	ALE		PIF	PE	1	TRAV	EL TIN	VIE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t_t (min)	REMARKS
	1	A1	2.06	0.51	9.7	1.05	4.17	4.4					0.2	0.04	3.3	4.2	1.01		18	652 5		3.0	On-grade inlet, carryover flow to DP 5 Piped to DP 1.0
	2	A2	0.82					1.9								1.9	0.44						Piped to DP 1.0
	1.0	7.2	UIUL	0100				1.0	9.7	1.45	4 17	6.0				6.0							Sum of DP 1 & DP 2, piped to DP 1.2
	3	A3	6.76	0.47	15.0	3.16	2 5 2	11.1	9.7	1.45	4.17	6.0	1.6	0.47	2.9	9.5				426		2.1	On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
	4	A3	1.51					3.7					0.1	0.03	2.9	3.6	0.88			395	3.4	1.9	Piped to DP 1.1 On-grade inlet, carryover flow to DP 5 Piped to DP 1.1
		A4	1.51	0.60	10.2	0.91	4.10	5.7															
	1.1									3.57						12.6	3.57				7.4		Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.2	5.02	3.50	17.6				17.6	5.02	3.3	24	319	12.5		Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53				5.17																Overland Flow to DP1.3A On-grade inlet
	6	A6	1.37	0.58	10.0	0.79	4.14	3.3								3.3	0.79						Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
	1.3A									1.22						5.0							Sum of DP 6 & DP 6A, piped to DP 1.3 On-grade inlet
	5	A5	1.70	0.59	9.9	0.99	4.14	4.1	17.0	1.53	3.33	5.1				5.1	1.53	2.0			7.6		Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	7.77	3.33	25.9				25.9	7.77	1.1	36	620	9.2		Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4 Future storm infrastructure from Copper Chase Subdivision
	7	A7	19.00	0.45	18.3	8.55	3.22	27.5								27.5	8.55	1.5	42	20	10.3	0.0	Piped to DP 1.4
	1.4								18.4	16.32	3.22	52.5				52.5	16.32	0.5	48	26	8.2		Sum of DP 1.3 & DP 7, piped to DP 1.5 On-grade inlet, carryover flow to DP 11
	8	A8	1.48	0.56	13.9	0.83	3.63	3.0								3.0	0.83	2.0	18	20	6.6		Piped to DP 1.5
	1.5								18.4	17.15	3.21	55.1				55.1	17.15	0.5	48	91	8.3		Sum of DP 1.4 & DP 8, piped to DP 1.6 On-grade inlet
	9	A9	0.61	0.73	8.7	0.44	4.34	1.9	8.7	0.48	4.34	2.1				2.1	0.48	2.0	18	13	5.8		Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								18.6	17.63	3.20	56.4				56.4	17.63	0.5	48				Sum of DP 1.5 & DP 9, piped to DP 1.8
	10	A10	2.61	0.79	7.9	2.05	4.49	9.2						0.11		8.7	1.94	2.5	18		9.5	0.2	On-grade inlet, carryover flow to DP 20 Piped to DP 1.7
	11	A11	2.89	0.76	8.7	2.20	4.34	9.5					0.6	0.15	1.5	8.9	2.05	2.5	18	1049 0			On-grade inlet, carryover flow to DP 21 Piped to DP 1.7
	1.7								8.7	3.99	4.34	17.3				17.3	3.99	1.0	24	8	7.9	0.0	Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								18.8	21.63	3.18	68.8				68.8	21.63	2.0	54	517	14.4		Sum of DP 1.6 & DP 1.7, piped to DP 2.7
	OS2	OS2	17.00	0.49	14.0	6.25	2.20	13.8								13.8	6.25	1.0	30	787	7.5	1.7	Future flow released from Barbarick Subdivision Piped to DP 2.0
	12	A12	3.87	0.13	11.9	0.49	3.86	1.9								1.9	0.49	2.0	18	17	5.6		Type C inlet Piped to DP 2.0
	2.0								15.7	6.74	3.45	23.2				23.2	6.74	1.0	48	52	8.4		Sum of DP OS2 & DP 12, Piped to DP 2.1
	13	A13	9.65	0.45	14.0	4.34	3.62	15.7								15.7	4.34	1.5	30	200	9.1		Future storm infrastructure from Sterling Ranch Phase 2 Piped to DP 2.1

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Project Name: Sterling Ranch Subdivision Project No.: 25188.01 Subdivision: Sterling Ranch Filing No. 2 Location: El Paso County Calculated By: AAM Design Storm: 5-Year Checked By: Date: 8/16/21 DIRECT RUNOFF TOTAL RUNOFF STREET/SWALE PIPE TRAVEL TIME ipe Size (inches) (cfs) /elocity (fps) Runoff Coeff. Point ength (ft) STREET REMARKS Area (Ac) lope (%) Q_{pipe} (cfs) iope (%) C*A (ac) *A (Ac) C*A (ac) (in/hr) C*A (ac) ≙ (in/hr) (min) (min) (min) Design I Q (cfs) Q (cfs) asin Ų, . 44 15.9 11.08 3.44 38.3 65 11.4 0.1 Sum of DP 2.0 & DP 13, piped to DP 2.5 2.1 38.1 11.08 1.6 48 Future flow released from Barbarick Subdivision 0.49 19.0 14.06 OS3 OS3 28.70 1.25 17.6 17.6 14.06 1.0 719 8.0 1.5 Piped to DP 2.2 30 Future flow released from School Site 14 A14 11.76 0.39 15.3 4.59 3.49 16.0 16.0 4.59 1.0 20 7.8 0.0 Piped to DP 2.2 30 2.2 20.5 18.65 3.05 56.9 56.9 18.65 1.5 48 773 12.4 1.0 Sum of DP OS3 & DP 14, piped to DP 2.3 On-grade inlet 2.91 0.52 14.9 1.52 3.53 35 0.1 Piped to DP 2.3 15 A15 5.4 5.4 1.52 1.3 18 6.5 6.5 On-grade inlet, carryover flow to DP 9 0.1 0.04 697 1.8 0.8 0.54 14.7 3.55 12 16 A16 2.34 1.25 2.0 7.2 0.0 Piped to DP 2.3 Δ. 4.3 1.21 18 2.3 15.0 2.73 3.52 96 9.6 2.73 1.6 48 51 7.6 0.1 Sum of DP 15 & DP 16, piped to DP 2.4 0.0 Sum of DP 2.2 & DP 2.3, piped to DP 2.5 2.4 21.5 21.38 2.98 63.7 63.7 21.38 1.6 48 19 13.1 21.6 32.46 2.98 96.6 96.6 32.46 2.0 839 15.8 0.9 Sum of DP 2.1 & DP 2.4 piped to DP 2.6 2.5 60 Type C inlet 17 A17 1.76 0.21 13.7 0.38 3.66 0.38 1.0 24 4.1 0.1 Piped to DP 2.6 1.4 18 2.6 21.6 32.84 2.98 97.8 97.8 32.84 2.0 60 32 15.8 0.0 Sum of DP 2.5 & DP 17, piped to DP 2.7 21.6 54.47 2.97 162.0 2.7 162.0 54.47 0.6 0.3 Sum of DP1.8 & DP 2.6, piped to DP 2.8 78 220 11.5 Area inlet 5.27 0.24 16.4 1.28 3.38 18 A18 24 5.6 0.1 Piped to DP 2.6 Δ: 43 1.28 1.0 18 Area inlet 19 A19 31.85 0.45 25.8 14.33 2.71 38.8 38.8 14.33 1.0 24 22.0 0.0 Piped to DP 2.6 18 2.8 25.8 70.08 2.71 189.8 89.8 70.08 0.6 78 145 12.1 0.2 Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0. 189.8 70.08 0.5 584 1.4 6.9 Detention Pond 3.0 25.8 70.08 2.71 189.8 Trickle channel conveyance to DP 3.2 On-grade inlet 8.0 1.48 20 A20 1.83 0.81 4.47 1.59 4.47 1.59 Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0 6.6 8.0 7.1 7.1 1.0 24 105 6.4 0.3 On-grade inlet 0.1 0.03 1.5 A21 1.93 0.82 8.7 1.57 4.33 1.72 4.33 7.3 1.68 2.5 9.0 0.0 Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9 21 6.8 8.7 7.4 18 0 8.7 3.27 4.33 14.2 3.27 2.0 24 58 9.8 0.1 Sum of DP 20 & DP 21,piped to DP 3.1 2.9 14.2 14.2 3.27 0.5 568 6.7 Detention Pond 1.4 3.27 4.33 Trickle channel conveyance to DP 3.2 3.1 8.7 14.2 Detention Pond A22 8.68 0.11 23.3 0.95 2.86 Overland flow to DP 3.2 22 27 2.6 1.02 13.0 113 5.4 0.3 Existing topography OS4 OS4 5.08 0.20 29.5 1.02 2.51 2. Overland flow to DP 4.1 Outlet Structure 3.2 29.8 75.32 2.49 187.5 Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8 29.8 1.45 2.49 1.45 3.6 2.0 58 6.2 0.2 Outlet structure release to DP 4.8 Pond W5 3.6 48 0.4 0.12 2.0 1399 2.0 12.0 On-grade inlet 5.1 0.3 Piped to DP 4.0 23 B1 2.98 0.90 17.6 2.68 3.29 8.8 2.56 0.5 88 84 30

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

 Subdivision: Sterling Ranch Filing No. 2
 Project Name: Sterling Ranch Subdivision

 Location: El Paso County
 Project Name: 25188.01

 ssign Storm: 100-Year
 Calculated By:

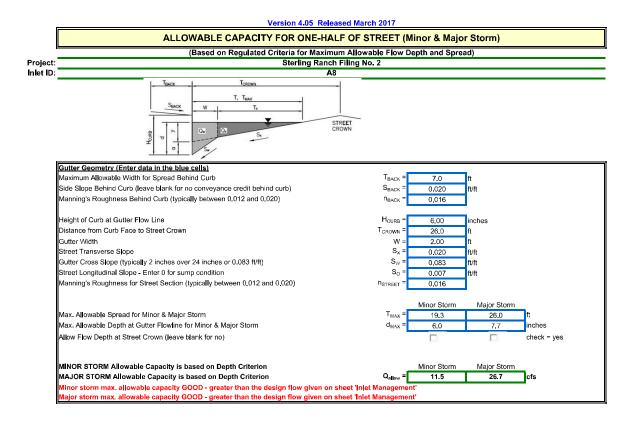
 Date:
 B/16/21

		DIRECT RUNOFF TOTAL RUNOFF S												ET/SW	ALE.		PIPE	-		TRAV	VEL TI	ME	
				UIK		JNOFF				UTAL		r	JIKE		~LC		riri		0	IKAN	V E L I		
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q _{street/swale} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
						_							2.8		3.3					652	3.6	3.0	D On-grade inlet, carryover flow to DP 5
	1	A1	2.06	0.65	9.7	1.34	7.01	9.4					0.1	0.01	3.3	6.6	0.94	2.0	18	639			Piped to DP 1.0 On-grade inlet, carryover flow to DP 6
	2	A2	0.82	0.66	9.1	0.54	7.17	3.9								3.8	0.53	2.0	18		7.0	0.1	1 Piped to DP 1.0
	1.0								9.7	1.47	7.00	10.3				10.3	1.47	3.0	18	335	10.6	0.5	5 Sum of DP 1 & DP 2, piped to DP 1.2
													10.0	1.69	2.9					426	5 3.4	2.1	1 On-grade inlet, carryover flow to DP 5
	3	A3	6.76	0.62	15.0	4.17	5.92	24.7					1.6	0.24	2.9	14.7	2.48	4.7	18	36	13.6 3.4	0.0	Piped to DP 1.1 On-grade inlet, carryover flow to DP 5
	4	A4	1.51	0.71	10.2	1.08	6.88	7.4								5.8	0.84	4.7	18	0	10.7	0.0	Piped to DP 1.1
	1.1								15.0	3.33	5.91	19.7				19.7	3.33	1.0	24	74	8.1	0.2	2 Sum of DP 3 & DP 4, piped to DP 1.2
	1.2								15.1	4.80	5.89	28.2				28.2	4.80	3.3	24	319	13.9	0.4	4 Sum of DP 1.0 & DP 1.1, piped to DP 1.3
	6A	A6A	0.53	0.88	5.0	0.47	8.68	4.1															Overland Flow to DP1.3A
	6	A6	1 37	0.70	10.0	0.95	6.94	6.6	10.0	0.96	6.94	6.7	1.3	0.18	0.7	5.4	0.78	2.0	18				DOn-grade inlet, carryover flow to DP 8 D Sum of Sub-basin A6 & Carryover flow from DP 2, Piped to DP 1.3A
		7.0	2107	0170	2010	0.00	010 1	010															
	1.3A								10.0	1.25	6.94	8.7	65	1.17	0.7	8.7	1.25	1.0	24		6.7	0.1	1 Sum of DP 6 & DP 6A, piped to DP 1.3 6 On-grade inlet, carryover flow to DP 8
	5	A5	1.70	0.70	9.9	1.19	6.95	8.3	17.0	3.51	5.59	19.6	0.5	1.17	0.7	13.1	2.34	2.0	18				D Sum of Sub-basin A5 & Carryover flows from DP 1, P 3 & DP 4. Piped to DP 1.3
	1.3								17.0	8 30	5.59	46.9				46.9	8 30	1.1	36	620	10.7	10	D Sum of DP 1.2, 1.3A & DP 5, piped to DP 1.4
										0.55	5.55	40.5											Future storm infrastructure from Copper Chase Subdivision
	7	A7	19.00	0.59	18.3	11.21	5.41	60.6								60.6	11.21	1.5	42	20	12.7	0.0	D Piped to DP 1.4
	1.4								18.4	19.60	5.40	105.9				105.9	19.60	0.5	48				D Sum of DP 1.3 & DP 7, piped to DP 1.5
	8	A8	1 49	0.70	12.0	1.04	6.10	6.2	23.7	7 62	4.76	12 5	1.9	0.41	0.7	10.6	2.23	2.0	18				P On-grade inlet, carryover flow to DP 11 D Sum of Sub-basin A8 & Carryover flows from DP5, DP 6 & DP 15, Piped to DP 1.5
	0	70	1.40	0.70	13.5	1.04	0.10	0.5												20			
	1.5								23.7	21.83	4.76	103.9	0.2	0.05	0.7	103.9	21.83	0.5	48		9.2	0.2	2 Sum of DP 1.4 & DP 8, piped to DP 1.6 4 On-grade inlet, carryover flow to DP 11
	9	A9	0.61	0.83	8.7	0.51	7.29	3.7	21.2	0.95	5.04	4.8	0.5	0.05	0.7	4.5	0.89	2.0	18				D Sum of Sub-basin A9 & carryover flows from DP 16, piped to DP 1.6
	1.6								22.0	22.72	4.74	107.7				107.7	22.72	0.5	48	0.5	0.1	0.2	Sum of DD 1.5.9. DD 0, pixed to DD 1.9
	1.0								23.9	22.12	4.74	107.7	4.5	0.59	1.5	107.7				955	2.4	6.5	2 Sum of DP 1.5 & DP 9, piped to DP 1.8 On-grade inlet, carryover flow to DP 20
	10	A10	2.61	0.88	7.9	2.29	7.53	17.3					6.1	0.90	1 5	12.8	1.70	2.5	18	118	10.3	0.2	2 Piped to DP 1.7 1 On-grade inlet, carryover flow to DP 21
	11	A11	2.89	0.86	8.7	2.48	7.28	18.1	10.6	2.94	6.77	19.9	6.1	0.90	1.5	13.8	2.04	2.5	18				Don-grade inlet, carryover flow to DP 21 D Sum of Sub-basin A11 & carryover flows from DP 8 & DP 9, piped to DP 1.7
	17								10.0	0.74	c 77	25.0				25.2	2.74	1.0	2.4				
	1.7								10.6	3.74	6.77	25.3				25.3	3./4	1.0	24	8	8.1	0.0	D Sum of DP 10 & DP 11, piped to DP 1.8
	1.8								24.0	26.45	4.72	125.0				125.0	26.45	2.0	54	517	17.0	0.5	5 Sum of DP 1.6 & DP 1.7, piped to DP 2.7
	OS2	OS2	17.00	0.62	12.0	10.54	3.71	39.1								39.1	10.54	1.0	30	787	9.5	1.4	Future flow released from Barbarick Subdivision 4 Piped to DP 2.0
																							Type C inlet
	12	A12	3.87	0.38	11.9	1.47	6.49	9.5			$\left \right $					9.5	1.47	2.0	18	17	8.9	0.0	D Piped to DP 2.0
	2.0								13.4	12.01	6.20	74.5				74.5	12.01	1.0	48	52	11.6	0.1	1 Sum of DP OS2 & DP 12, Piped to DP 2.1
	13	A13		0.50		5.69	6.08	34.6								34.6	F (0	1 5	20	200	110	0.2	Future storm infrastructure from Sterling Ranch Phase 2 3 Piped to DP 2.1

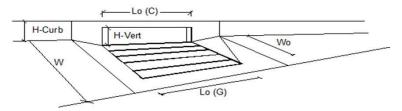
STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

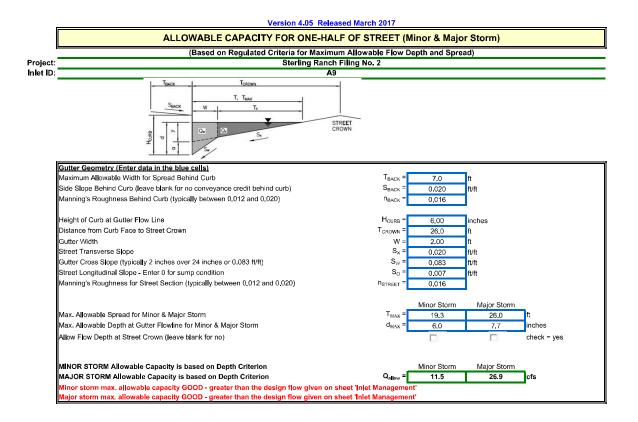
Project Name: Sterling Ranch Subdivision Subdivision: Sterling Ranch Filing No. 2 Project No.: 25188.01 Location: El Paso County Calculated By: AAM sign Storm: 100-Year Checked By: Date: 8/16/21 DIRECT RUNOFF TOTAL RUNOFF STREET/SWALE PIPE TRAVEL TIME Size (inches) (cfs) unoff Coeff. /elocity (fps) Point -ength (ft) REMARKS Description ilope (%) Q_{pipe} (cfs) Slope (%) Area (ac) C*A (ac) ≙ C*A (ac) (in/hr) (min) C*A (ac) (in/hr) C*A (ac) (min) (min) Q (cfs) Q (cfs) В asin ipe . 0 Q, 14.3 17.70 6.02 106. 2.1 106.6 17.70 1.6 48 65 15.1 0.1 Sum of DP 2.0 & DP 13, piped to DP 2.5 Future flow released from Barbarick Subdivision OS3 28.70 0.62 15.0 17.79 2.75 48.9 48.9 17.79 719 10.0 1.2 Piped to DP 2.2 053 10 30 Future flow released from School Site 0.0 Piped to DP 2.2 14 A14 11.76 0.55 15.3 6.47 5.86 37. 37.9 6.47 1.0 20 9.5 2.2 16.2 24.26 5.72 138. 138.7 24.26 15 773 15.5 0.8 Sum of DP OS3 & DP 14, piped to DP 2.3 724 1.7 7.2 On-grade inlet, carryover flow to DP 8 1.4 0.24 0. A15 2.91 5.93 15 0.68 14.9 1.98 11. 10.3 1.74 1.3 35 7.6 0.1 Piped to DP 2.3 1.8 6.5 On-grade inlet, carryover flow to DP 9 0 44 697 2.6 0 0.69 14.7 A16 2.34 1.61 7.0 2.0 12 8.2 0.0 Piped to DP 2.3 16 5 96 q 1.17 2.91 5.91 17. 15.0 17.2 2.91 15 0.0 Sum of DP 15 & DP 16, piped to DP 2.4 23 16 48 9.0 17.0 27.17 5.59 151. 151.9 27.17 1.6 48 19 16.2 0.0 Sum of DP 2.2 & DP 2.3, piped to DP 2.5 2.4 17.1 44.87 5.59 250.7 250.7 44.87 2.0 839 20.1 0.7 Sum of DP 2.1 & DP 2.4 piped to DP 2.6 2.5 60 Type C inlet 17 A17 1.76 0.44 13.7 0.77 6.14 4. 0.77 1.0 24 0.1 Piped to DP 2.6 4 5.7 18 2.6 17.7 45.64 5.49 250.4 250.4 45.64 2.0 60 32 20.2 0.0 Sum of DP 2.5 & DP 17, piped to DP 2.7 24.5 72.10 4.67 336. 2.7 336.8 72.10 0.6 78 220 13.7 0.3 Sum of DP1.8 & DP 2.6, piped to DP 2.8 Area inlet 5.27 0.47 16.4 7.9 0.1 Piped to DP 2.6 18 A18 2.47 5.68 14. 14.0 2.47 1.0 18 24 Area inlet A19 31.85 0.59 25.8 18.79 4.55 85.4 85.4 18.79 1.0 24 48.4 0.0 Piped to DP 2.6 19 18 2.8 25.8 93.36 4.55 424. 424.4 93.36 0.6 78 145 13.9 0.2 Sum of DP 2.7, DP 18 & DP 19, piped to DP 3.0. 424.4 93.36 0.5 564 1.4 6.6 Detention Pond 3.0 25.8 93.36 4.55 424.4 Trickle channel conveyance to DP 3.2 On-grade inlet 2.3 0.38 1 A20 0.89 8.0 1.63 7.50 1.0 0.2 Sum of Sub-basin A20 & carryover flow from DP 10, piped to DP 3.0 20 1.83 12.2 14.4 2.22 6.02 13 11.: 1.84 24 105 7.2 On-grade inlet 33 0.57 1 5 A21 1.93 0.90 8.7 1.73 7.28 15.8 2.63 5.77 15.2 11.9 2.5 0 10.2 0.0 Sum of Sub-basin A21 & carryover flow from DP 11, piped to DP 2.9 21 12.6 2.06 18 3.91 5.77 22. 22.5 3.91 2.0 58 11.0 0.1 Sum of DP 20 & DP 21, piped to DP 3.1 2.9 15.8 24 568 1.4 6.7 Detention Pond 22.5 3.91 0.5 Trickle channel conveyance to DP 3.2 15.8 3.91 5.77 3.1 22. Detention Pond A22 8.68 0.37 23.3 3.21 4.80 15.4 Overland flow to DP 3.2 22 8.5 2.03 13.0 113 5.4 0.3 Existing topography OS4 OS4 5.08 0.40 29.5 2.03 4.21 8 Overland flow to DP 3.2 Outlet Structure 29.8 102.50 4.18 428.2 3.2 Sum of DP 3.0, DP 3.1, DP 22 & DP OS4, outlet structure release to DP 4.8 29.8 34.84 4.18 145. 58 17.5 0.1 Outlet structure release to DP 4.8 2.0 Pond W5 145.5 34.84 48 1394 2.1 11.0 On-grade inlet 3.6 0.65 2.0 B1 2.98 0.96 17.6 2.86 5.51 15.8 0.5 88 5.7 0.3 Piped to DP 4.0 23 12.2 2.21 30 6.5 1.17 1394 2.1 11.0 On-grade inlet 2. 24 B2 3.89 0.96 17.6 3.73 5.51 20.6 14.1 2.56 2.0 0 9.7 0.0 Piped to DP 4.0



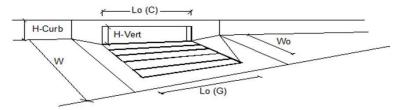
Version 4.05 Released March 2017



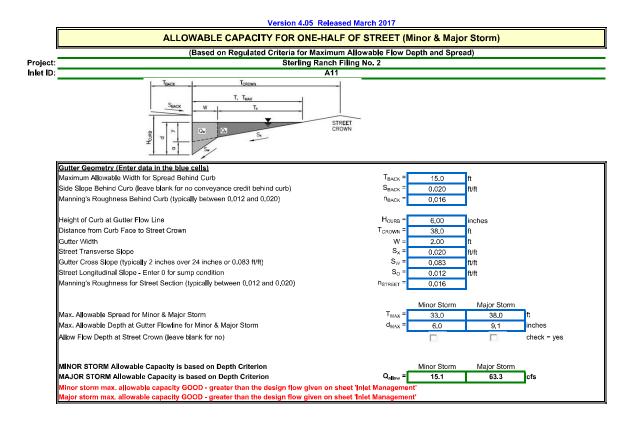
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C ₁ -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MNOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.0	10.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	85	%



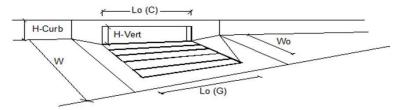
Version 4.05 Released March 2017



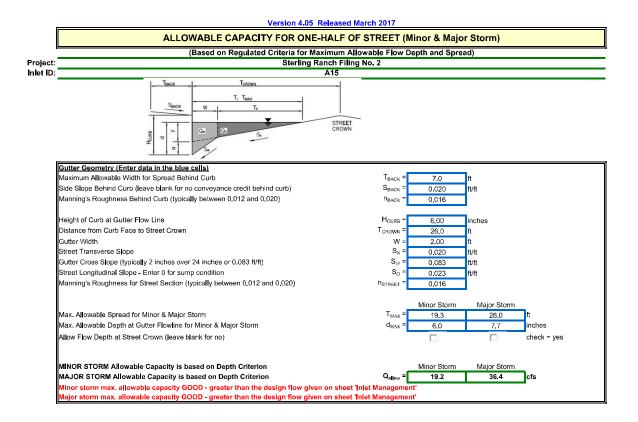
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _r -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MNOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.1	4.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	94	%



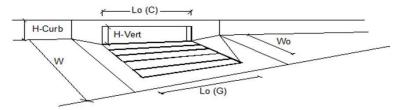
Version 4.05 Released March 2017



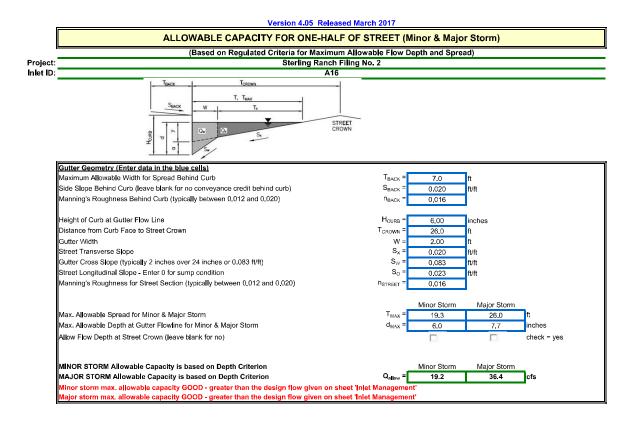
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _r -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MNOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.9	13.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.6	6.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	93	69	%



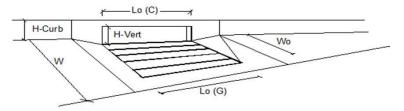
Version 4.05 Released March 2017



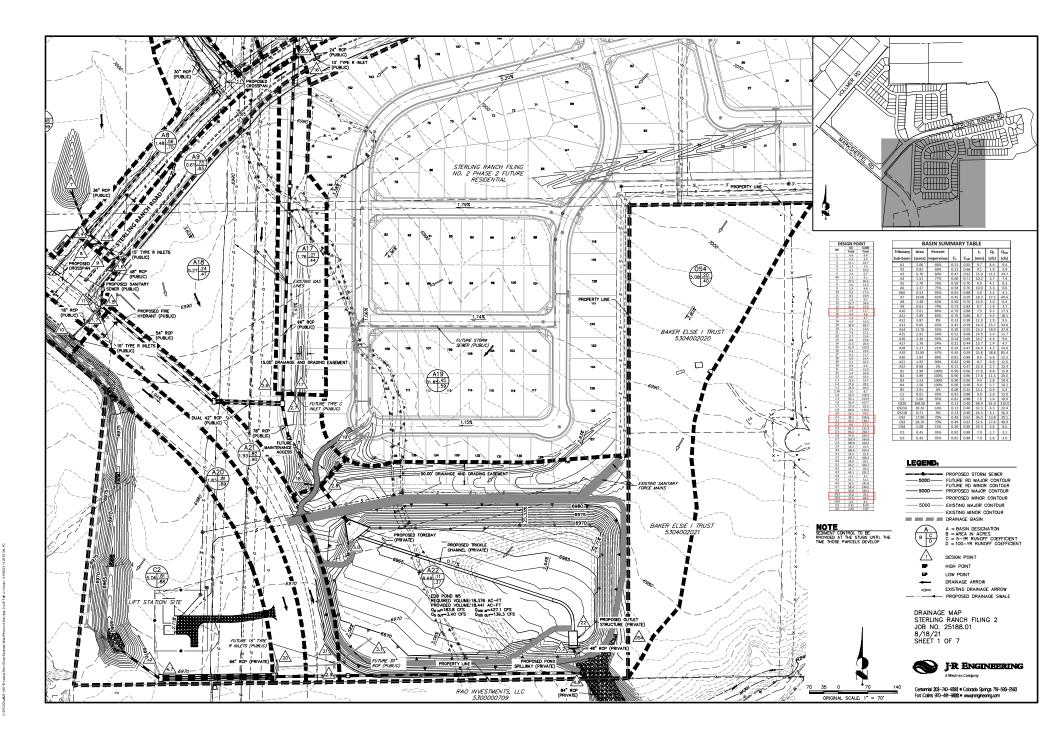
Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MNOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.4	10.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	88	%

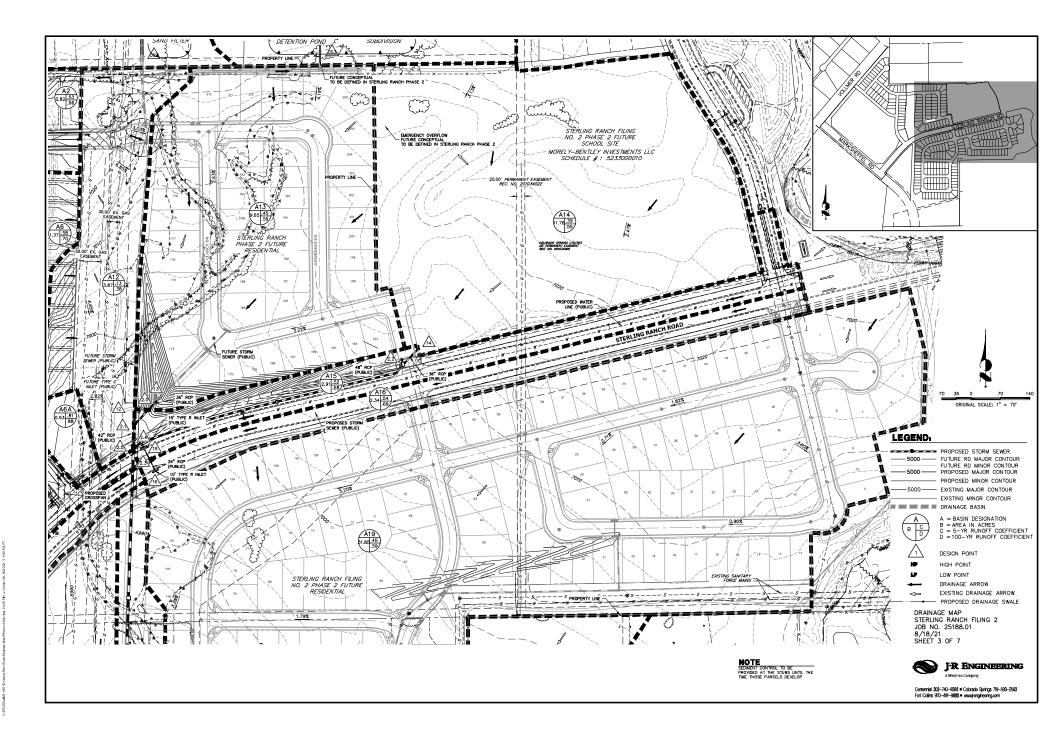


Version 4.05 Released March 2017



Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.3	7.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	2.6	cfs
Capture Percentage = Q_a/Q_o =	C% =	97	73	%





FINAL DRAINAGE REPORT FOR STERLING RANCH FILING NO. 4

Prepared For:

SR Land, LLC 20 Boulder Crescent, Suite 200 Colorado Springs, CO 80903 (719) 491-3024

> August 14, 2023 Project No. 25188.11

Prepared By: JR Engineering, LLC 5475 Tech Center Drive, Suite 235 Colorado Springs, CO 80919 719-593-2593

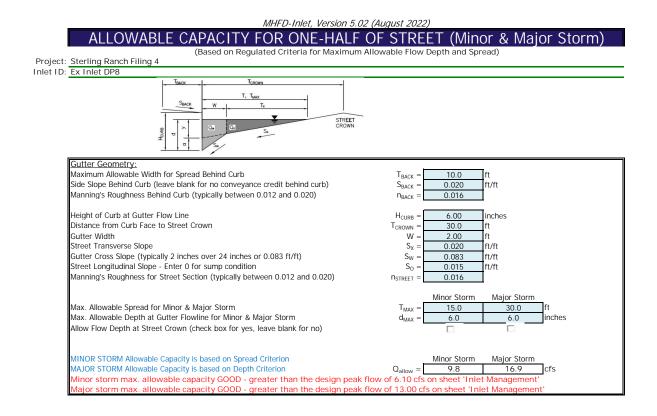
> PCD Filing No.: SF-22-030



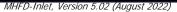
STANDARD FORM SF-3 - PROPOSED STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

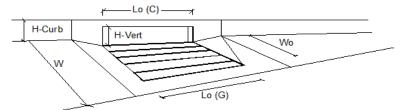
Location	ubdivision: Sterling Ranch Subdivision -Proposed Location: El Paso County sign Storm: 5-Year														Ca	Project Iculate Checke	t No.: d By:	25188 ARJ APL	3.11	ich Fil	ing No. 4	4	
				DIRE	CT RUI	NOFF			T	OTAL R	UNOFI	F	STRE	et/SW	/ALE		PIF	PE		TRAV	EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	(in/hr)	Q (cfs)	Qstreet/swale (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1 OS7 33.07 0.20 36.4 6.68 2.19 14.6													14.6	6.68		36	427	7.5		Offsite Barbarick Subdivision pond release Piped to DP 4.1		
	4	OS6	18.38				3.29	22.3								22.3				162	8.4		Offsite subdivision pond release 3 Confluenced at DP 4.1
	4.1	000	10.00	0.07	17.0	0.77	0.27	22.0	37.3	13.45	2 15	29.0					13.45				9.0		Offsite undetained flow confluenced from basins OS7 and OS6 w/ bypass flows
	5	C2	6 75	0.40	14.2	2 2 2	3.61	12.0	57.5	10.40	2.10	27.0				12.0							Sump Inlet Piped to DP 6.3
																							Sump Inlet
	6.1	C1.1	1.78			0.92		3.9								3.9	0.92	1.0	18	9	5.5	0.0	DPiped to DP 6.3 Sump Inlet
	6.2	C1.2	0.81	0.57	8.3	0.46	4.42	2.0															Piped to DP 6.3
	6.3								14.3	4.70	3.59	16.9				16.9	4.70	1.0	36	245	7.9	0.5	Piped to DP 7.2 Area Inlet
	7	C3	4.18	0.20	9.3	0.82	4.24	3.5															Piped to DP 7.1
	7.1								38.6	14.27	2.10	30.0				30.0	14.27	1.0	36	40	9.2	0.1	1 Structure piped to 7.2
	7.2								38.7	18.97	2.10	39.8											Piped to existing storm sewer in Sterling Ranch Road Offsite flow to existing inlet in Sterling Ranch Road
	8	C4	4.41	0.54	28.3	2.37	2.57	6.1															Piped to existing storm sewer in Sterling Ranch Road
	9	В3	2.38	0.58	25.5	1.39	2.73	3.8															Offsite flow to existing inlet in Sterling Ranch Road Piped to existing storm sewer in Sterling Ranch Road
	1.i	11	5.88	0.44	20.8	2.58	3.03	7.8															Runoff drains into into swale
	3.i	13	2.94	0.60	10.8	1.77	4.01	7.1															Runoff drains into swale
	2.i	12	2.18	0.58	11.9	1.26	3.87	4.9	20.8	3.84	3.03	11.6				11.6	3.84	2.0	24	113	9.3	0.2	2
	3.2								21.0	5.61	3.02	16.9											DP2.i and DP3.i combine at DP3.2
	10									26.57													Sum of flows from DP7.2, 8, 9, and 2.1
	15							8.2					0.4	0.11	1.6	7.8							Existing runoff piped from Sterling Ranch Filing 3 subdivision by-passed to DP17 curb and gutter flow to DP17
	15.1								19.5	6.71	3.13	21.0				21.0	6.71	1.0	24	45	8.2	0.1	On-grade Inlet from overland flow on Filing 3 subdivision I Captured Flows piped to DP 16.1
	16	A5	0.45	0.63	5.0	0.28	5.17	1.4					0.0	0	2.9	1.4							Existing On-grade Inlet from Sterling Ranch Filing 3 Captured Flows piped to DP 16.1, by pass flow to DP12
	16.1								19.6	6.88	3.12	21.5				21.5	6.88	1.0	36	280	8.4	0.6	Piped to DP 18.1
	17	A2	1.38	0.30	10.3	0.42	4.08	1.7	20.1		3.08	1.6	0.0	0		1.6					4.3		On-grade Inlet, includes by pass flow from DP15/ Sterling Ranch Filing 3 Piped to DP 18.1
	17.1															1.6							Captured runoff from on Grade inlet at DP 17, FLOWS TO DP 18.1
	18.1								20.3	7 / 1	3.07	22.8				22.8		1.0	36	600	8.5	1.3	2 Piped to DP18.2
		A.4 1	4 7 2	0.55	10.1	2 50	2 05	10.0	20.3	7.41	3.07	22.0	0.9	0.23	1.0								On-grade Inlet, includes by pass flow from DP16 2 Captured Flows piped to DP 18.2, Bypass flow to DP 19
	12	A6.1	4./3	U.55	12.1	2.59	3.85	10.0								9.1	2.36	1.0	24	100	6.8	0.2	2 Captureu Fiows pipeu to DP 18.2, Bypass now to DP 19

	STANDARD FORM SF-3 - PROPOSED STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE) Project Name: <u>Sterling Ranch Filing No. 4</u>																						
Subdivision:	Sterlir	na Ranc	h Subdi	vision	-Prop	osed										Pro	oject N Projec	ame: t No.:	Sterli 2518	ng Rar 8 11	nch Fili	ng No	. 4
Location: Design Storm:	El Pas	o Coun														Ca	lculate	d By: d By:	ARJ				
Bosignotorini	100 1	our																Date:		23			
DIRECT RUNOFF TOTAL RUNOFF																		1E					
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	OS7	33.07	0.43	36.4	14.34	3.68	52.8								52.8	14.34	1.0	36	427	10.5	0.7	Offsite Barbarick Subdivision pond release Piped to DP 4.1
	4	OS6	18.38	0.55	17.5	10.07	5.52	55.6								55.6	10.07	1.0	36	162	10.6	0.3	Offsite subdivision pond release Confluenced at DP 4.1
	4.1								37.0	24.41	3.63	88.7				88.7	24.41	1.0	36	704	12.6	0.9	Offsite undetained flow confluenced from basins OS7 and OS6 w/ bypass flows Piped to DP 7.1
	5	C2	6.75	0.63	14.2	4.28	6.06	25.9					12.4	2.05	2.0	13.5	2.23		24	42 63	2.8 7.5	0.2	Sump Inlet, Over flows 12.4 cfs to DP 6.1 Piped to DP 6.3
	6.1	C1.1	1.78	0.65			7.16	8.3	14.4	3.21	6.01	19.3	3.1	0.52	0.1	16.2	0.97		18	16	0.6	0.4	Sump Inlet, Overflows 3.1 cfs to DP6.2 Piped to DP 6.3
	6.2	C1.2	0.81	0.69			7.41	4.2	14.8														Sump Inlet Piped to DP 6.3
	6.3	0112	0.01	0.07	0.0	0.00	7.11		14.8							35.6	6.00	1.0	36	245	9.6	0.4	Piped to DP 7.2
	7	C3	4.18	0.43	9.3	1.79	7.12	12.8															Area Inlet Piped to DP 7.1
	7.1								38.0	26.20	3.57	93.5				93.5	26.20	1.0	36	40	13.2	0.1	structure piped to 7.2
	7.2								38.0	32.20	3.57	114.9											Piped to existing storm sewer in Sterling Ranch Road
	8	C4	4.41	0.69	28.3	3.00	4.31	12.9															Offsite flow to existing inlet in Sterling Ranch Road Piped to existing storm sewer in Sterling Ranch Road
	9	B3	2.38	0.00			4.58	7.9															Piped to existing storm sever in Sterling Ranch Road Piped to existing storm sever in Sterling Ranch Road
	- 7 1.i	11	5.88	0.60			5.09	17.9															Runoff drains into into swale
	3.i	13	2.94	0.98			6.74	19.4															Runoff drains into swale
	2.i	12	2.18	0.70			6.50	9.9	20.8	5.05	5.09	25.7				25.7	5.05	2.0	24	113	11.3	0.2	
	3.2								21.0		5.07												Flows from DP2.i and DP3.1 combine in proposed storm sewer
	10									41.97	1												Sum of flows from DP7.2, 8, 9, and 2.1
	15							17.7					4.7	0.817	1.5	12.5							Existing runoff piped from Sterling Ranch Filing 3 subdivision by-passed to DP 17 curb and gutter flow to DP17
	15.1								19.2	8.18	5.28	43.2				43.2	8.18	1.0	24	45	13.8	0.1	On-grade Inlet from overland flow on Filing 3 subdivision Captured Flows piped to DP 16.1
	16	A5	0.45	0.73	5.0	0.33	8.68	2.9					0.0	0	2.9	2.9							Existing On-grade Inlet from Sterling Ranch Filing 3 Captured Flows piped to DP 16.1, by pass flow to DP12
	16.1								19.3	8.51	5.28	44.9				44.9	8.51	1.0	36	280	10.1	0.5	Piped to DP 18.1
	17	A2	1.38	0.51	10.3	0.70	6.85	4.8	19.8	1.52	5.22	7.9	0.2	0.029	1.5	7.7	1.49	1.0	18	27	6.5	0.1	On-grade Inlet, includes by pass flow from DP15/ Sterling Ranch Filing 3 Piped to DP 18.1
	17.1															7.7							Captured runoff from on Grade inlet at DP 17, FLOWS TO DP 18.1
	18.1								19.8	10.03	5.21	52.2				52.2	10.03	1.0	36	600	10.4	1.0	Piped to DP18.2
	12	A6.1	4.73	0.67	12.1	3.17	6.46	20.5					6.6	1.022	1.0	13.9	2.15	1.0	24	100	7.6	0.2	On-grade Inlet, includes by pass flow from DP16 Captured Flows piped to DP 18.2, Bypass flow to DP 19
	12.1															13.9							Captured flow into on grade inlet at DP12.1

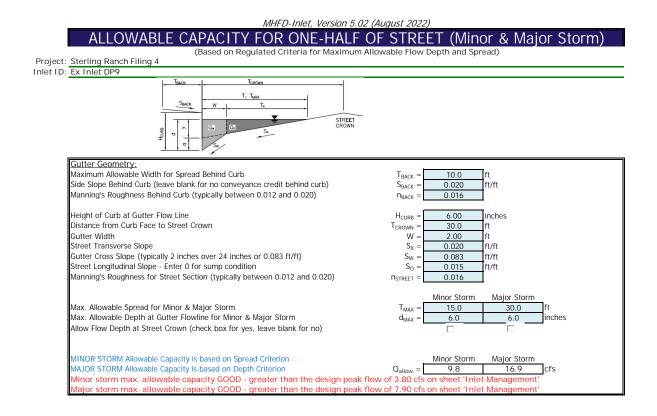


INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)

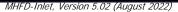


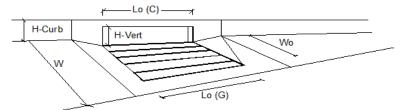


Design Information (Input) CDOT Type R Curb Opening	Type =	MINOR CDOT Type R	MAJOR Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.1	10.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	2.2	cfs
Capture Percentage = Q_a/Q_o	C% =	100	83	%

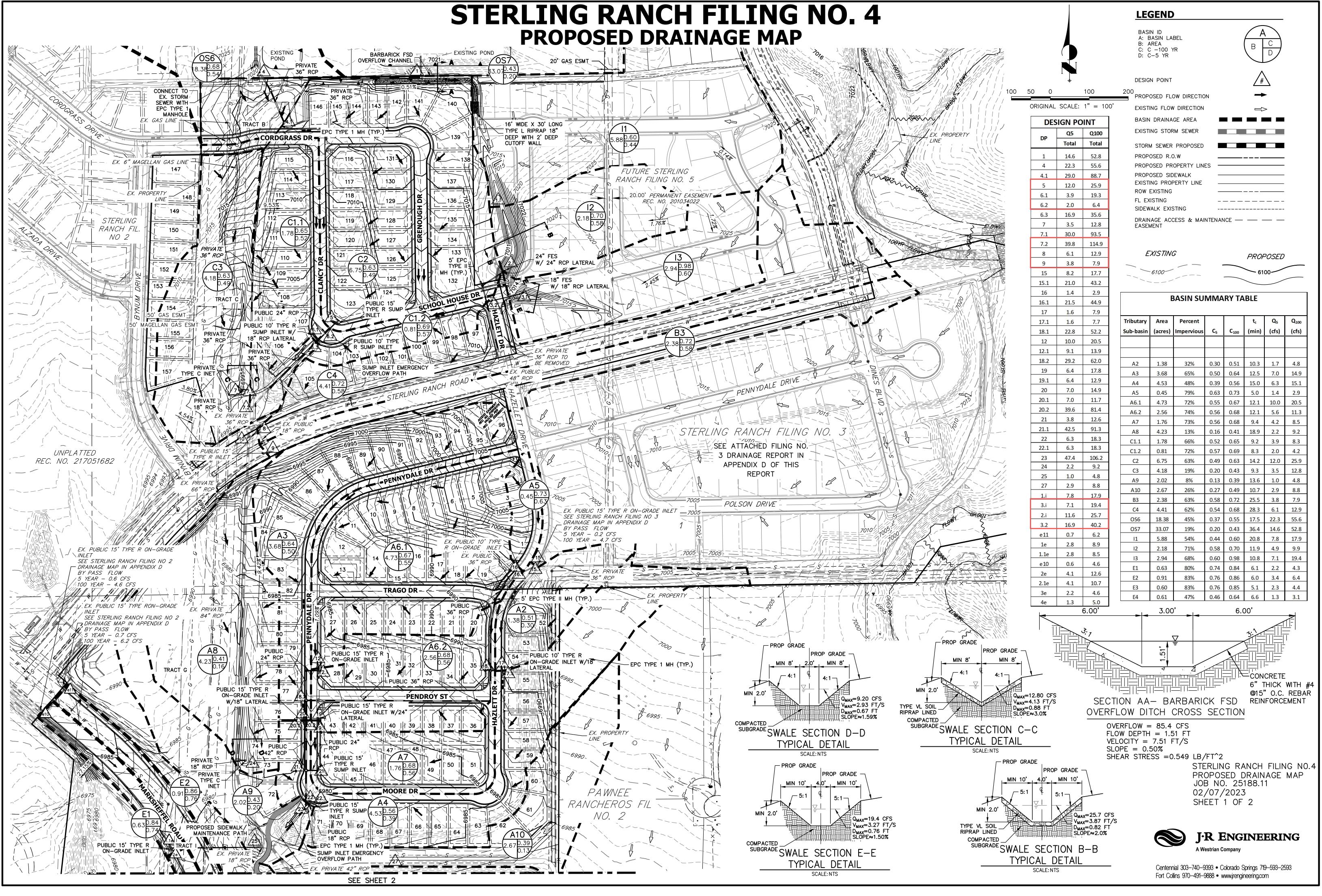


INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)





Design Information (Input) Type of Inlet	Type =	MINOR CDOT Type R	MAJOR Curb Opening	1
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.8	7.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.2	cfs
Capture Percentage = Q_a/Q_o	C% =	100	98	%



FINAL DRAINAGE REPORT FOR BRANDING IRON AT STERLING RANCH FILING NO. 1

EL PASO COUNTY, COLORADO

October 2018

Prepared for: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

Prepared by:



CIVIL CONSULTANTS, INC. 20 Boulder Crescent, Suite 110 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-006 DSD Project # SF-17-024

Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 (henceforth referred to as "Sterling Ranch Filing Nos. 1 & 2 MDDP") and the Sterling Ranch MDDP revised April 2018. Please refer to the Sterling Ranch Filing Nos. 1 & 2 MDDP by MS Civil Consultants for detailed information regarding the historic conditions of the area and discussion regarding early overlot grading which altered the existing drainage patterns prior to the issuance of this report.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

As the Hydrologic calculations performed as a part of this analysis matched the hydraulic analysis conducted with the Sterling Ranch Filing Nos. 1 & 2 MDDP, there is no need to reproduce in duplicate the hydraulic calculations provided within the aforementioned study. As such, please refer to the hydraulic calculations located in the appendix of the Master Development Drainage Report for Sterling Ranch Filing Nos. 1 & 2, and Final Drainage Report for Sterling Ranch Filing No.1 prepared by MS Civil Consultants, dated April 2017 for the relevant data sheets detailing the hydraulic analysis.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0535 F, effective date March 17, 1997 and revised to reflect LOMR, 08-08-0541P, dated July 23, 2009. An annotated FIRM Panel is included in the Appendix.

DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the aforementioned ECMs, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates) have been utilized to aid in design of the Full Spectrum Detention Facilities when required.

EXISTING DRAINAGE CONDITIONS

The Branding Iron at Sterling Ranch Filing No. 1 site consists of 10.545 acres. According to the Sterling Ranch MDDP (Existing Condition Map), historically runoff from the site drained to the southern boundary of the Sterling Ranch property (portion of Basin EX-3A) before combining with offsite runoff prior to reaching Sand Creek Channel. With the approval of the Sterling Ranch Onsite Early Grading Plan,

will be treated as WQCV and Full Spectrum Detention. As such the proposed develop shall not adversely affect the downstream infrastructure.

Water Quality/Full Spectrum Detention Facilities

With the exception of the outer permeable western and southern edges of the development the majority of the developed runoff from Branding Iron at Sterling Ranch Filing No. 1 is collected within the internal streets and conveyed via existing storm sewer systems to the existing Full Spectrum Detention Facility Pond 8 that was approved for construction as a portion of the Sterling Ranch Filing No.1 improvements. Pond 8 will provide 0.46 acre feet of water quality and 2.90 acres of full spectrum detention for approximately 29 acres of Sterling Ranch development of which the Branding Iron at Sterling Ranch Filing No.1 is a portion. The pond initially sized and designed within Sterling Ranch Filing Nos. 1&2 MDDP using the Detention Design UD-Detention v3.05 workbook. It should be noted that this drainage report and the SR Filing 1 and 2 MDDP were developed concurrently. Thus the larger scale concept planning was very finite and thus allowed for the developed flow rates to align between the two documents and thereby not requiring modifications to facility which is often common between conceptual and final design. Refer to the approved Sterling Ranch Filing No. 1 Storm Sewer Plans for additional details of FSD Pond 8.

The flows generated by Basin OS13 will be routed south via overlot grading and vegetated swales to a temporary sediment basin (future Pond W-5), at the south end of the Sterling Ranch Development. Upon development of the Sterling Ranch Filing No. 2 infrastructure Pond W-5 will be constructed and flows from Basin OS13 will be treated as WQCV (see WQCV deviation request) and Full Spectrum Detention. As such the proposed develop shall not adversely affect the downstream infrastructure.

EROSION CONTROL

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. EPC approved "Early Grading Plan for Sterling Ranch Phase I <u>Onsite</u> Grading & Erosion Control", November 18, 2015. And "Early Grading Plan for Sterling Ranch Phase I <u>Offsite</u> Grading & Erosion Control", December 3, 2015. Grading and Erosion control operations are currently underway (August 2016). Grading and Erosion Control will cease with the final development of the site in the next 12-36 months.

CONSTRUCTION COST OPINION – BRANDING IRON AT STERLING RANCH FIL. NO. 1

Drainage Facilities:

There are no planned improvements with the development of Branding Iron at Sterling Ranch Filing No. 1. Construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1 &2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Please see Drainage and Bridge Fees below.

DRAINAGE & BRIDGE FEES – BRANDING IRON AT STERLING RANCH FIL. NO. 1

This site is within the Sand Creek Drainage Basin. The 2017 Drainage and Bridge Fees per El Paso County for the BRANDING IRON AT STERLING RANCH FILING NO. 1 site are as follows:

DP5, (Aka DP19*), 11.86 acres, consists of planned residential lots and streets (Basin OS-7 (Aka Basin HH*)) that have been assigned runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year, and a portion of the east half of existing Dines Boulevard (Basin OS8 (Aka Basin JJ*)), with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year as well as flow-by from DP3. Developed runoff of Q5=20.5 cfs and Q100=52.0 cfs has been calculated to reach DP5 as shallow overland and as street flows. An existing 15' CDOT type R at-grade inlet at DP5 will intercept flows of Q5=15.0 cfs and Q100=23.2 cfs and allow for flow-by of Q5=5.5 cfs and Q100=28.8 cfs. The collected runoff combines with flows from DP4, prior to being discharged into existing FSD Pond 8.

DP6, (Aka DP20*), 2.19 acres, consists of proposed residential lots and streets (Basin E (Aka Basin KK*)) that have been assigned runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year, and the west half of a portion of existing Dines Boulevard (Basin OS10 (Aka Basin MM)), with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year as well as flow-by from DP4. Developed runoff of Q5=5.2 cfs and Q100=27.9 cfs has been calculated for to reach DP6 as shallow overland and as street flows. An existing 15' CDOT type R at-grade inlet at DP6 will intercept flows of Q5=5.2 cfs and Q100=17.6 cfs and allow flow-by of Q5=0.0 cfs and Q100=10.3 cfs. Runoff collected by the inlet is conveyed under Dines where it will combine with flows intercepted at DP7, while the flow by continues downgradient in the west half of existing Dines Boulevard.

DP7, (Aka DP21*), 0.43 acres, consists of planned residential backyard lots (Basin OS11 (Aka Basin LL*)) that have been assigned runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, and a portion of the east half of existing Dines Boulevard (Basin OS12 (Aka Basin NN*)), with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year as well as flow-by from DP5. Developed runoff of Q5=6.4 cfs and Q100=30.7 cfs has been calculated to reach DP7 as shallow overland and as street flows. An existing 15' CDOT type R at-grade inlet at DP7 will intercept flows of Q5=6.4 cfs and Q100=18.6 cfs and will allow for flow-by of Q5=0.0 cfs and Q100=12.1 cfs. The collected runoff combines with flows from DP6, prior to being discharged into existing FSD Pond 8, while the flow by continues south within the east half of Existing Dines Boulevard.

DP8, (Aka DP22*), 0.67 acres, consists of proposed rear half of residential lots (Basin G (Aka Basin OO*)) that have been assigned runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, and the west half of a portion of existing Dines Boulevard (Basin OS14 (Aka Basin PP)), with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year as well as flow-by from DP6. Developed runoff of Q5=5.2 cfs and Q100=27.9 cfs has been calculated for to reach DP8 as shallow overland and as street flows. An existing 10' CDOT type R sump inlet at DP8 will intercept flows of Q5=1.4 cfs and Q100=13.2 cfs. Runoff collected by the inlet is conveyed under Dines where it will combine with flows intercepted at DP9.

DP9, (Aka DP23*), 0.59 acres, consists a portion of the east half of existing Dines Boulevard and mail kiosk and parking lot (Basin OS15 (Aka Basin QQ*)), with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year as well as flow-by from DP7. Developed runoff of Q5=2.0 cfs and Q100=15.9 cfs has been calculated to reach DP9 as shallow overland and as street flows. An existing 10' CDOT type R sump inlet at DP9 will intercept flows of Q5=2.0 cfs and Q100=15.9 cfs. The collected runoff combines with flows from DP8, prior to being discharged into existing FSD Pond 8.

BRANDING IRON AT STERLING RANCH FILING NO. 1 FINAL DRAINAGE REPORT (Basin Routing Summary)

					1			0			57						
From Area Runoff Coefficient Summary				OVERLAND			PIPE / CHANNEL FLOW		Time of Travel (T_t) INTENSITY **		SITY **	TOTAL FLOWS					
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA100	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q5	Q ₁₀₀	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
		PRO	OPOSEI) DR/	4INAG	E BASI	IN ROU	U TING S	SUMM	ARY							
1	083	2.34	3.39									16.3	3.4	5.7	8.0	19.3	36" FES/TSB
2	OS4, OS5, Sterling Ranch Filing Nos. 1&2 MDDP* Flowby DP4	1.07	3.02									11.7	3.9	6.5	4.2	19.7	EX 15' AT-GRADE INLET
3	OS6, Sterling Ranch Filing Nos. 1&2 MDDP* Basins I, J, K	3.50	3.97									10.8	4.0	6.7	14.1	26.7	EX 15' AT-GRADE INLET
4	A, B, C, OS2, OS9, Flowby DP2	4.14	7.30									16.3	3.4	5.7	14.1	41.6	EX 15' AT-GRADE INLET
5	OS7, OS8 FLOWBY DP 3	5.53	8.34									13.2	3.7	6.2	20.5	52.0	EX 15' AT-GRADE INLET
6	E, OS10 FLOWBY DP 4	1.53	4.89									16.3	3.4	5.7	5.2	27.9	EX 15' AT-GRADE INLET
7	OS11, OS12 FLOWBY DP 5	1.72	4.92									13.2	3.7	6.2	6.4	30.7	EX 15' AT-GRADE INLET
8	G, OS14, FLOWBY DP 6	0.40	2.31									16.3	3.4	5.7	1.4	13.2	EX 10' SUMP INLET
9	OS15, FLOWBY DP 7	0.53	2.54									13.2	3.7	6.2	2.0	15.9	EX 10' SUMP INLET

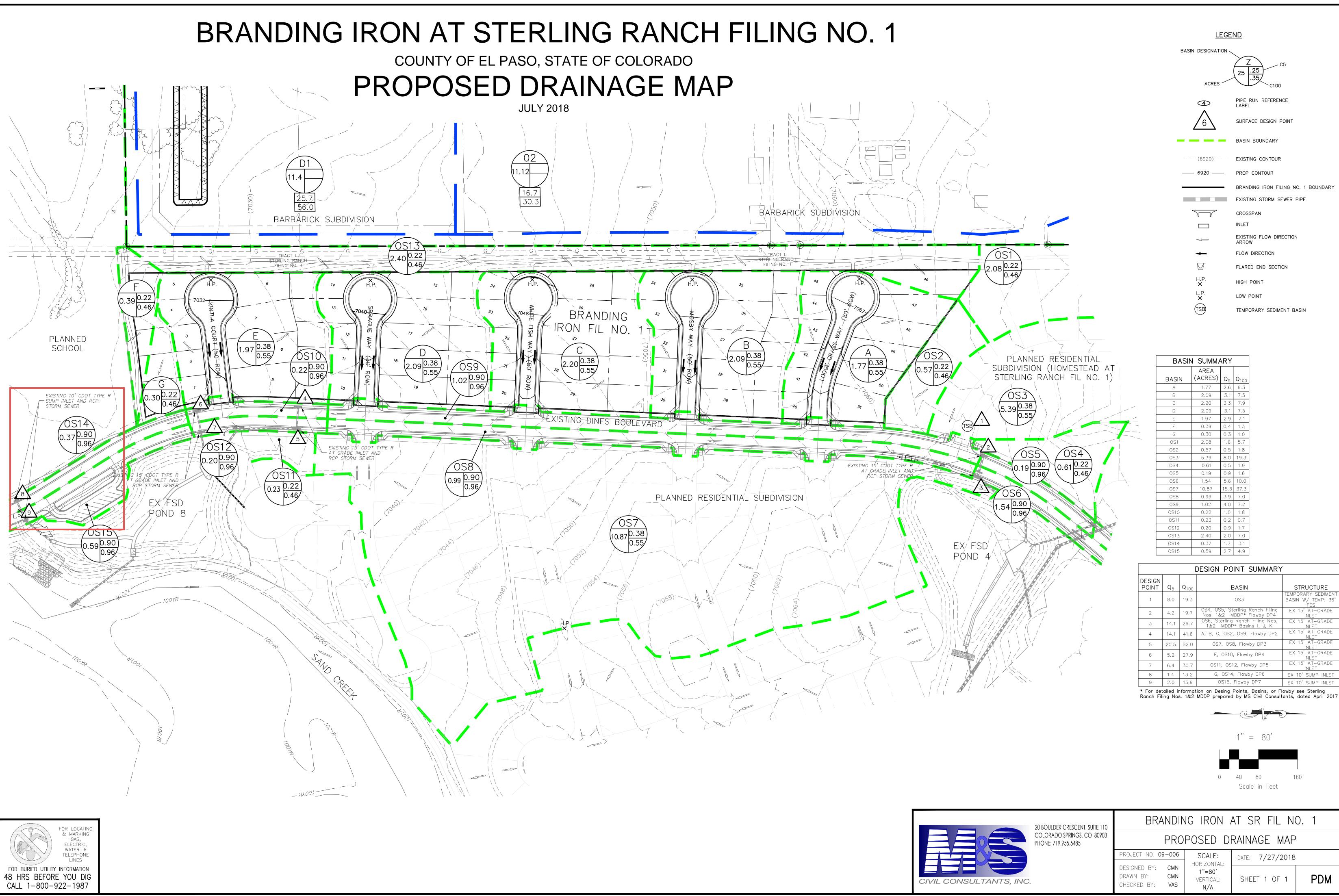
* For detailed information on Design Points, Basins, or Flowby see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

** Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: <u>ET</u> Date: 4/10/2017

Checked by: VAS

MS CIVIL, INC.

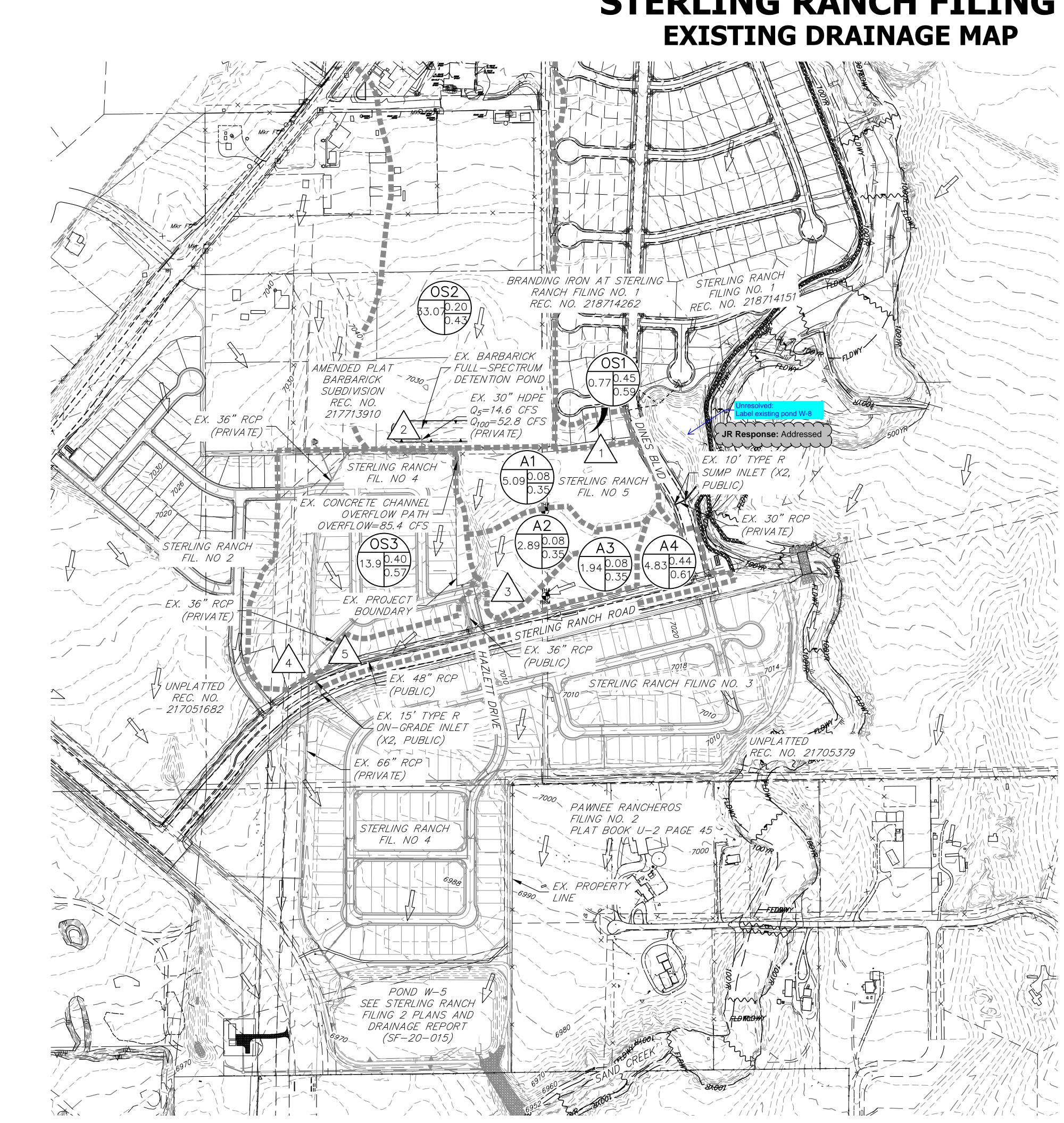


BASIN	BASIN SUMMARY					
BASIN	AREA (ACRES)	Q ₅	Q ₁₀₀			
A	1.77	2.6	6.3			
В	2.09	3.1	7.5			
С	2.20	3.3	7.9			
D	2.09	3.1	7.5			
E	1.97	2.9	7.1			
F	0.39	0.4	1.3			
G	0.30	0.3	1.0			
OS1	2.08	1.6	5.7			
OS2	0.57	0.5	1.8			
OS3	5.39	8.0	19.3			
OS4	0.61	0.5	1.9			
OS5	0.19	0.9	1.6			
OS6	1.54	5.6	10.0			
0S7	10.87	15.3	37.3			
OS8	0.99	3.9	7.0			
OS9	1.02	4.0	7.2			
0S10	0.22	1.0	1.8			
0S11	0.23	0.2	0.7			
0S12	0.20	0.9	1.7			
OS13	2.40	2.0	7.0			
OS14	0.37	1.7	3.1			
0S15	0.59	2.7	4.9			

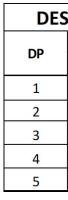
DESIGN POINT SUMMARY							
DESIGN POINT	Q ₅	Q ₁₀₀	BASIN	STRUCTURE			
1	8.0	19.3	OS3	TEMPORARY SEDIMENT BASIN W/ TEMP. 36" FES			
2	4.2	19.7	OS4, OS5, Sterling Ranch Filing Nos. 1&2 MDDP* Flowby DP4	EX 15'AT-GRADE INLET			
3	14.1	26.7	OS6, Sterling Ranch Filing Nos. 1&2 MDDP* Basins I, J, K	EX 15' AT-GRADE INLET			
4	14.1	41.6	A, B, C, OS2, OS9, Flowby DP2	EX 15'AT-GRADE INLET			
5	20.5	52.0	OS7, OS8, Flowby DP3	EX 15'AT-GRADE INLET			
6	5.2	27.9	E, OS10, Flowby DP4	EX 15'AT-GRADE INLET			
7	6.4	30.7	OS11, OS12, Flowby DP5	EX 15'AT-GRADE INLET			
8	1.4	13.2	G, OS14, Flowby DP6	EX 10' SUMP INLET			
9	2.0	15.9	OS15, Flowby DP7	EX 10' SUMP INLET			

Appendix D Drainage Maps

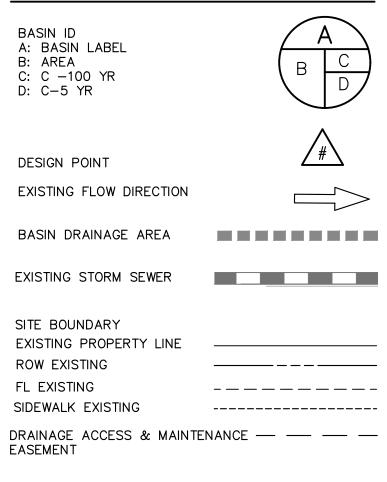




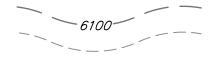
STERLING RANCH FILING 5



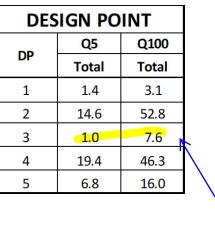
LEGEND

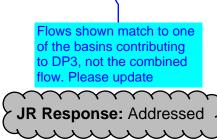


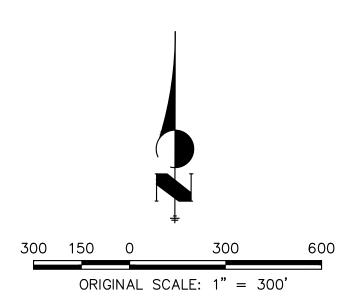
EXISTING



BASIN SUMMARY TABLE							
Tributary	Area	Percent			t _c	Q₅	Q ₁₀₀
Sub-basin	(acres)	Impervious	C ₅	C ₁₀₀	(min)	(cfs)	(cfs)
<mark>A</mark> 1	5. <mark>0</mark> 9	0%	0.08	0.35	28.7	1.0	7.6
A2	2.89	0%	0.08	0.35	15.3	0.8	<mark>5.</mark> 9
A 3	1.94	0%	0.08	0.35	17.9	0.5	3.7
A4	4.83	47%	0.44	0.61	18.3	<mark>6.8</mark>	16.0
OS1	0.77	<mark>65%</mark>	0.45	0.59	10.2	1.4	3.1
OS2	33.07	19%	0.20	0.43	36.4	14.6	52.8
OS3	13.90	49%	0.40	0.57	15.5	19.4	46.3
083	13.90	49%	0.40	0.57	15.5	19.4	46.3





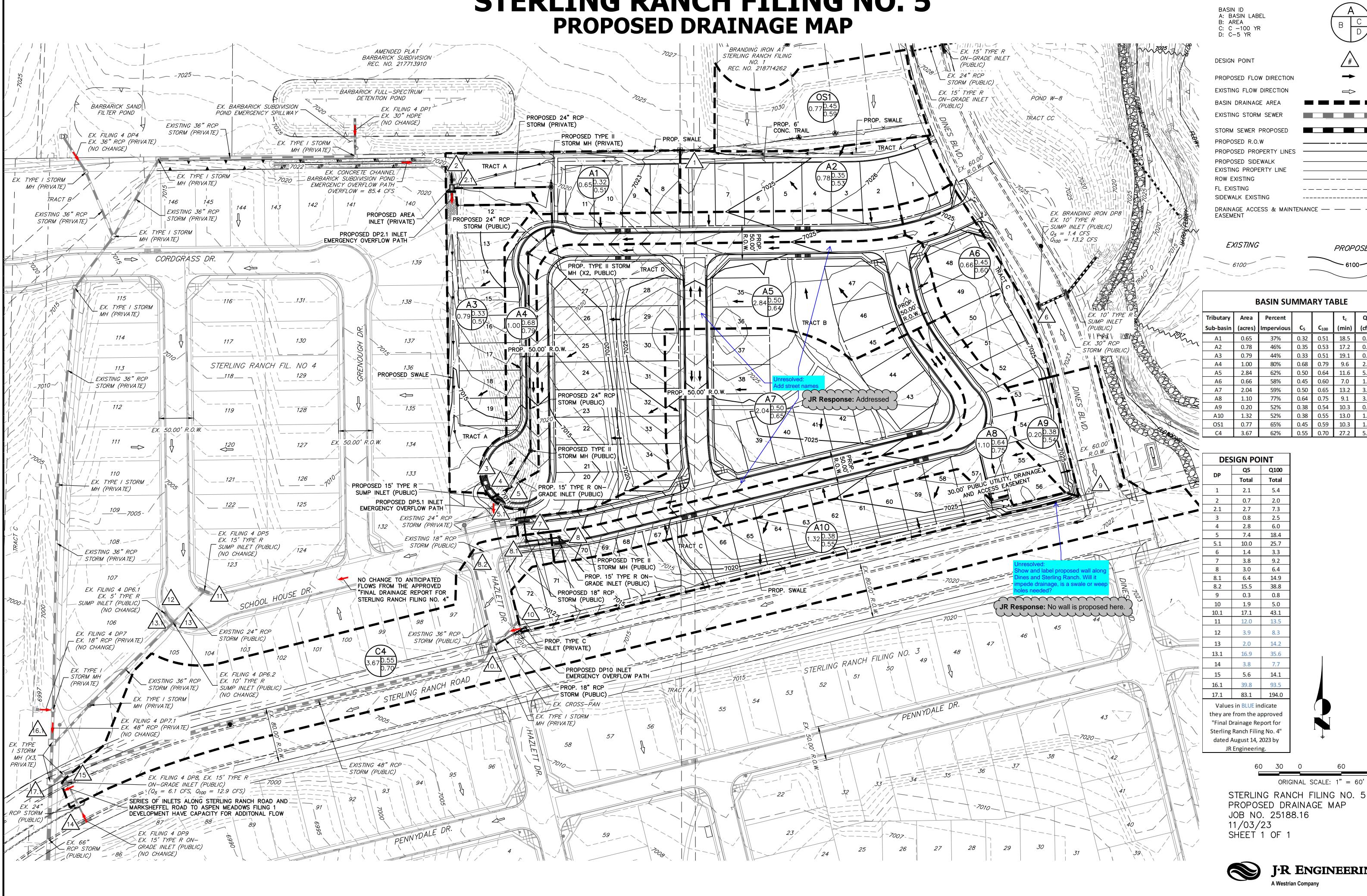


STERLING RANCH FILING 5 EXISTING DRAINAGE MAP JOB NO. 25188.16 11/03/23 SHEET 1 OF 1



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STERLING RANCH FILING NO. 5

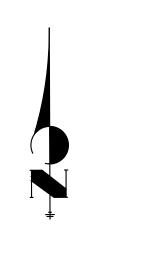
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BASIN ID A: BASIN LABEL B: AREA C: C –100 YR D: C–5 YR	A B C D
DESIGN POINT	<u>/</u> #
PROPOSED FLOW DIRECTION	→
EXISTING FLOW DIRECTION	\Rightarrow
BASIN DRAINAGE AREA	
EXISTING STORM SEWER	
STORM SEWER PROPOSED PROPOSED R.O.W PROPOSED PROPERTY LINES PROPOSED SIDEWALK EXISTING PROPERTY LINE ROW EXISTING FL EXISTING SIDEWALK EXISTING DRAINAGE ACCESS & MAINTER EASEMENT	

- 6100-

PROPOSED

BASIN SUMMARY TABLE

Tributary	Area	Percent			t _c	Q ₅	Q ₁₀₀
Sub-basin	(acres)	Impervious	C ₅	C ₁₀₀	(min)	(cfs)	(cfs)
A1	0.65	37%	0.32	0.51	18.5	0.7	2.0
A2	0.78	46%	0.35	0.53	17.2	0.9	2.6
A3	0.79	44%	0.33	0.51	19.1	0.8	2.5
A4	1.00	80%	0.68	0.79	9.6	2.8	6.0
A5	2.84	62%	0.50	0.64	11.6	5.5	13.2
A6	0.66	<mark>58%</mark>	0.45	0.60	7.0	1.4	3.3
A7	2.04	59%	0.50	0.65	13.2	3.8	9.2
A8	1.10	77%	0.64	0.75	9.1	3.0	6.4
A9	0.20	52%	0.38	0.54	10.3	0.3	0.8
A10	1.32	52%	0.38	0.55	13.0	1.9	5.0
OS1	0.77	65%	0.45	0.59	10.3	1.4	3.4
C4	3.67	<mark>62%</mark>	0.55	0.70	27.2	5.4	13.5



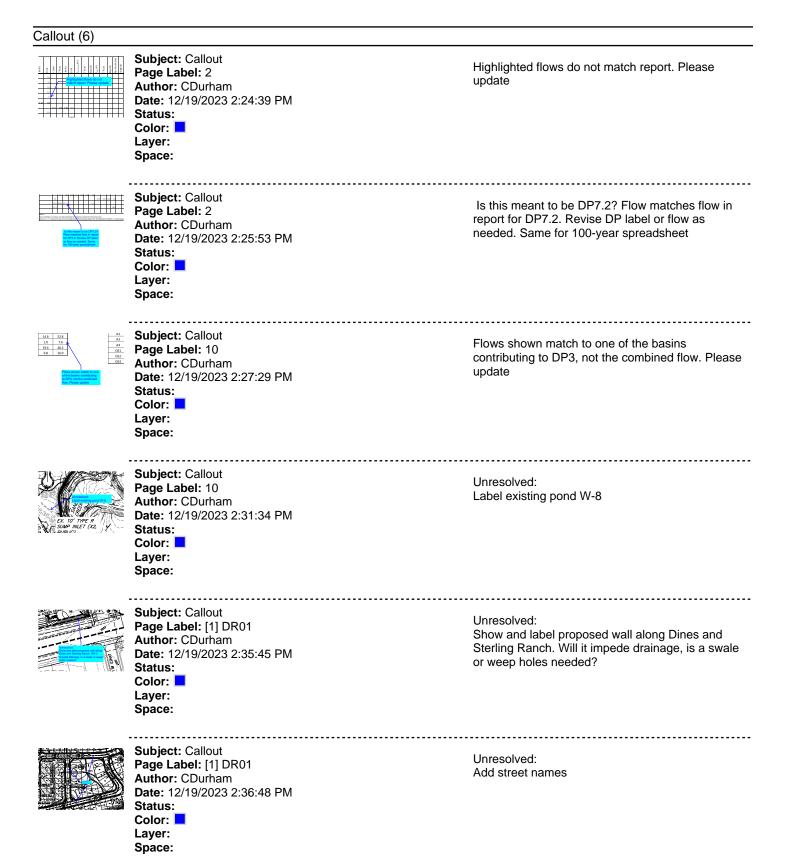
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STERLING RANCH FILING NO. 5 PROPOSED DRAINAGE MAP JOB NO. 25188.16

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V2_ Drainage Report.pdf Markup Summary



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