PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH FILING NO. 5

Prepared For:

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> November 2023 Project No. 25188.16

Prepared By:
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PRELIMINARY DRAINAGE REPORT FOR STERLING RANCH FILING NO. 5 NOV 2023

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by earlinegligent acts, errors, or omissions on my part in preparing this report.

Ryan Burns, Colorado P.E. 0054412

For and On Behalf of JR Engineering, LLC



DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

Classic SRJ Land, LLC

By:

ICE PRESIDENT Title:

Address:

2138 Flying Horse Club Drive

Colorado Springs, CO 80921

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Joshua Palmer, P.E.

County Engineer/ ECM Adminis

By: Gilbert LaForce, P.E. **Engineering Manager** On behalf of the **ECM Administrator**

Date: 01/18/2024 9:20:19 AM

El Paso County Department of Public Works

Conditions:



Table of Contents

Purpose	1
General Site Description	1
General Location	1
Description of Property	1
Floodplain Statement	1
Existing Drainage Conditions	2
Major Basin Descriptions	2
Existing Sub-basin Drainage	2
Proposed Drainage Conditions	4
Proposed Sub-basin Drainage	4
Orainage Design Criteria	7
Development Criteria Reference	7
Hydrologic Criteria	7
Hydraulic Criteria	7
Orainage Facility Design	9
General Concept	9
Four Step Process to Minimize Adverse Impacts of Urbanization	9
Water Quality	10
Erosion Control Plan	10
Operation & Maintenance	10
Drainage and Bridge Fees	10
Summary	11
References	12

APPENDIX

Appendix A – Vicinity Map, Soil Descriptions, FEMA Floodplain Map

Appendix B - Hydrologic Calcs

Appendix C - Reference Material

Appendix D - Drainage Maps



PURPOSE

This document is the Preliminary Drainage Report for Sterling Ranch Filing Number 5. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert, inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

GENERAL SITE DESCRIPTION

GENERAL LOCATION

Sterling Ranch Filing Number 5 (hereby referred to as the "site") is a proposed development within the Sterling Ranch master planned community with a total area of approximately 11.6 acres. The site is currently being designed to accommodate approximately 72 urban lots.

The site is located in a portion of the Southeast Quarter (SE ¼) Of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridian County Of El Paso, State Of Colorado. The site is surrounded by Barbarick Subdivision and Branding Iron at Sterling Ranch Filing No. 1 to the north, Sterling Ranch Filing No. 4 to the west, Sterling Ranch Road to the south, and Dines Boulevard to the east.

DESCRIPTION OF PROPERTY

The property will be primarily single-family residential development (approximately 11.6 acres), open space and drainage tracts. The site is comprised of variable sloping grasslands that generally slope(s) downward to the southwest at 1 to 3% towards Sterling Ranch Road and Hazlett Dr.

Soil characteristics are comprised of Type A and B hydrologic soil groups. Refer to the soil survey map in Appendix A for additional information.

There are no major drainage ways running through the site, Sand Creek lies to the east of the site. Currently, JR Engineering, LLC is performing studies and plans to address Sand Creek stabilization. There are no known irrigation facilities located on the project site.

FLOODPLAIN STATEMENT

Based on the FEMA FIRM Maps number 08041C0533G, dated December 7, 2018, the proposed development lies within Zone X. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. FIRM Map is presented in Appendix A.



EXISTING DRAINAGE CONDITIONS

MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" (DBPS) completed by Kiowa Engineering Corporation in January 1993, revised March 1996. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into major subbasins. The site is within the Upper Sand Creek sub-basin as shown in Appendix C.

The Sand Creek DBPS assumed the Sterling Ranch Filing No. 5 property to have a "large lot residential" use for the majority of the site however, the proposed Sterling Ranch master plan is a mix of; school, multi-family, single-family, and commercial land uses, resulting in higher runoff. The "Master Development Drainage Plan for Sterling Ranch"; (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018 assumed a mix of a school site and single family residential lots ranging in size from 0.1 to 0.33 acres for the Sterling Ranch Filing No. 5 site.

Any additional runoff has been provided for with the extended detention basin, "Pond W-5", located at the southern edge of the Sterling Ranch boundary. The site generally drains from northeast to southwest. The site currently has drainage infrastructure built with prior Sterling Ranch subdivisions filings in the site's southwest corner that collects and conveys the Sterling Ranch Filing 5 runoff to Pond W-5. Currently, the site is undeveloped vacant land. Sand Creek is located approximately 500 feet east of the site running north to south. Currently, JR engineering is performing studies and plans to address Sand Creek stabilization adjacent to the site under PCD project number CDR-20-004 and is undergoing review.

The proposed drainage on the site closely follows the approved "Master Development Drainage Plan for Sterling Ranch"; (MDDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018. The site is tributary to Pond W-5 and full-spectrum detention for the site was previously analyzed and can be found in the Final Drainage Report for Sterling Ranch Filing 2 as shown in Appendix C.

EXISTING SUB-BASIN DRAINAGE

The existing condition of the site was broken into four on-site basins, as well as three off-site basins. The basin and sub-basin delineation is shown in the existing drainage map in Appendix D and is described as follows:

Basin A1 (Q_5 =1.0 cfs, Q_{100} =7.6 cfs) is 5.09 acres and 0 percent impervious consists of the northern portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP 3 (Q_5 =2.9 cfs, Q_{100} =16.8 cfs). Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.



Basin A2 (Q_5 =0.8 cfs, Q_{100} =5.9 cfs) is 2.89 acres and 0 percent impervious consists of the south western portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the existing storm sewer built with Filing 5 just north of Sterling Ranch Road located at DP 3 (Q_5 =2.9 cfs, Q_{100} =16.8 cfs). Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin A3 (Q_5 =0.5 cfs, Q_{100} =3.7 cfs) is 1.94 acres and 0 percent impervious consists of the southern portion of the proposed Sterling Filing No. 5 site. Runoff from this basin drains via overland flow to the south west into the existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP 3 (Q_5 =2.9 cfs, Q_{100} =16.8 cfs). Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin A4 (Q_5 =6.8 cfs, Q_{100} =16.0 cfs) is 4.83 acres and 47 percent impervious consists of the southeastern portion of the proposed Sterling Filing No. 5 site as well as the norther portion of Sterling Ranch Road. Runoff from this basin drains via overland flow to Sterling Ranch Road, then west to the existing 15' Type R inlet located at DP 5. Collected runoff is piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin OS1 (Q_5 = 1.4 cfs, Q_{100} =3.1 cfs) is 0.77 acres and 65 percent impervious, consists of the southern portion of the proposed Branding Iron at Sterling Ranch Filing No.1. Runoff from this basin drains to the south into the proposed Sterling Filing No.5 northern site sub-basin A1. Runoff is collected into the existing storm sewer built with Filing 4 just north of Sterling Ranch Road located at DP3. Collected runoff is piped west to the DP 5 and then piped via existing storm infrastructure south to Pond W-5 built with Filing 2.

Basin OS2 (Q₅=14.6 cfs, Q₁₀₀=52.8 cfs) is 33.07 acres and 19 percent impervious and is located directly north of the site in the Barbarick subdivision per the "Final Drainage Report for Barbarick Subdivision, Portions of Lots 1, 2 and Lots 3&4" prepared by Matrix Design Group dated June 6, 2016. Historic runoff from this site drains south onto the Sterling Ranch Filing 4 site at DP 2. Detained flow from this basin will be piped through the Sterling Ranch Filing 4 site to the detention Pond W-5 and will outfall to Sand Creek. The emergency overflow path for this pond is routed east around the Sterling ranch Filing 4 lots and onto the northwest corner of Sterling Ranch Filing 5. The emergency overflow path is conveyed south via a concrete line swale and grass swale to DP3.

Basin OS3 (Q_5 =19.4 cfs, Q_{100} =46.3 cfs) is 13.90 acres and 49 percent impervious, consists of the Sterling Ranch Filing No.4. Runoff from this basin drains to the southwest into the storm sewer built with Sterling Ranch Filing 4 and DP 4. Collected runoff is piped south to the existing detention pond W-5 built with Filing 2 and outfalls to Sand Creek.



PROPOSED DRAINAGE CONDITIONS

PROPOSED SUB-BASIN DRAINAGE

The proposed site was broken into ten on-site basins and two off-site basin that lead into the existing storm structures on Sterling Ranch Road and Sterling Ranch Filing 4. The proposed basin (and subbasin) delineation is shown on the proposed drainage basin map within Appendix D and is described as follows.

Basin A1 (Q_5 =0.7 cfs, Q_{100} =2.0 cfs) is 0.65 acres and 37% impervious, consists of single-family residential lots, open space, lawns, concrete trail, and part of an existing concrete channel. Runoff from this basin drains via sheet flow to the swale at DP2 where runoff is collected in an area inlet. The emergency overflow path of the inlet is to the south to the proposed swale. Collected runoff is piped south to the proposed sump inlet at DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A2 (Q_5 =0.9 cfs, Q_{100} =2.6 cfs) is 0.78 acres and 46% impervious, consists of single-family residential lots, open space, a sound wall, and lawns. Runoff from this basin drains via sheet flow to the swale at DP1 where it is conveyed west via swale to DP2 and collected in an area inlet. Collected runoff is piped to DP2.1 and then south to DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A3 (Q_5 =0.8 cfs, Q_{100} =2.5 cfs) is 0.79 acres and 44% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP3 where it is conveyed to the street and sump inlet at DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A4 (Q_5 =2.8 cfs, Q_{100} =6.0 cfs) is 1.00 acres and 80% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to DP4, then flows to a sump inlet at DP5.1. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A5 (Q_5 =5.5 cfs, Q_{100} =13.2 cfs) is 2.84 acres and 62% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to DP5, then flows to a sump inlet at DP5.1. The emergency overflow path of this inlet is to the south to School House Drive. Flows combine with DP.8.1 at DP8.2.



The collected runoff is piped south to Sterling Ranch Road storm structures which eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A6 (Q_5 =1.4 cfs, Q_{100} =3.3 cfs) is 0.66 acres and 58% impervious, consists of single-family residential lots, a sound wall, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter offsite to the curb and gutter in Dines Boulevard. Flows will pass under the proposed sound wall and will not impact drainage patterns. The flows collect in an existing sump inlet at DP6 and are piped via an existing 24" storm pipe to and existing water quality and detention Pond W-8 on the east side of Dines and eventually outfalls to Sand Creek. Pond W-8 was analyzed with the Sterling Ranch Filing 1, Branding Iron Filing 1 and Branding Iron Filing 2 subdivisions and has a total tributary area of approximately 29 acres. The addition of the Basin A6 flows are assumed to be immaterial but will be further analyzed with the Final Drainage Report for SR Filing 5 to confirm this Preliminary Drainage Report assumption. The existing inlet shall also be checked for capacity with the additional flow to ensure no impacts to existing infrastructure.

Basin A7 (Q_5 =3.8 cfs, Q_{100} =9.2 cfs) is 2.04 acres and 59% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to an on-grade inlet at DP7. Flows combine with DP8 at DP8.1. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek. Runoff that is not collected by the inlet at DP7 continues west to an existing sump inlet at DP11 built with Sterling Ranch Filing 4. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A8 (Q_5 =3.0 cfs, Q_{100} =6.4 cfs) is 1.10 acres and 77% impervious, consists of single-family residential lots, open space, lawns, sidewalks and streets. Runoff from this basin drains via overland flow, sheet flow, and curb and gutter to an on-grade inlet at DP8. Flows combine with flows of DP7 at DP8.1 (Q_5 =6.4 cfs, Q_{100} =14.9 cfs). Then flows combine with DP5.1 at DP8.2 (Q_5 =15.5 cfs, Q_{100} =38.8 cfs). The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek. Runoff that is not collected by the inlet at DP8 continues west to an existing sump inlet at DP12 built with Sterling Ranch Filing 4. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The collected runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A9 (Q_5 =0.3 cfs, Q_{100} =0.8 cfs) is 0.20 acres and 52% impervious, consists of single-family residential lots, a sound wall, open space, and lawns. Runoff from this basin drains via overland and sheet flow to the curb and gutter on Dines Boulevard. Flows will pass under the proposed sound wall



and will not impact drainage patterns. The flows collect at DP9 and run along the curb and gutter along Sterling Ranch Road to an existing on-grade inlet at DP15 built with Sterling Ranch Filing 2. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin A10 ($Q_5=1.9$ cfs, $Q_{100}=5.1$ cfs) is 1.32 acres and 52% impervious, consists of single-family residential lots, sound walls, open space, and lawns. Runoff from this basin drains via overland flow and sheet flow to the proposed swale and continues west to the proposed area inlet at DP10. The emergency overflow path is to the west to Hazlett Drive. Flows will pass under the proposed sound wall and will not impact drainage patterns. Flows then combine with DP8.2 flows at DP10.1 ($Q_5=17.1$ cfs, $Q_{100}=43.1$ cfs). The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin OS1 (Q_5 =1.4 cfs, Q_{100} =3.4 cfs) is 0.77 acres and 65% impervious, consists of single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the swale at DP1 where it is conveyed west via swale to DP2.1 and collected in an area inlet. Collected runoff is piped south to DP5.1. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys runoff to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

Basin C4 (Q₅=5.4 cfs, Q₁₀₀=13.5 cfs) is 3.67 acres and 62% impervious, consists of a portion of Sterling Ranch Road, a portion of Dines Blvd, Filing 4 single-family residential lots, open space, and lawns. Runoff from this basin drains via sheet flow to the existing curb and gutter where it is conveyed west to the existing on-grade inlet at DP15 built with Sterling Ranch Filing 2. In the FDR, the existing inlet shall be checked for capacity with the additional flow to ensure no impacts to existing infrastructure. The overall runoff is piped south to Sterling Ranch Road storm infrastructure that eventually conveys the flow to the existing detention Pond W-5 built with Filing 2 and outfalls to Sand Creek.

There are several locations where proposed Filing 5 storm sewer connects to existing storm sewer built with previous Sterling Ranch Filings 2 and 4. The proposed Filing 5 flows at DP5.1 (Q_5 =10.0 cfs, Q_{100} =25.7 cfs) are located at the same location as Filing 4 DP2.i (Q_5 =11.6 cfs, Q_{100} =25.7 cfs) and have less than or equal to the anticipated flow at the existing 24" RCP. The proposed Filing 5 flows at DP8.1 (Q_5 =6.4 cfs, Q_{100} =14.9 cfs) are located at the same location as Filing 4 DP3.i (Q_5 =7.1 cfs, Q_{100} =19.4 cfs) and have less than the anticipated flow at the existing 18" RCP. The proposed Filing 5 flows at DP8.2 (Q_5 =15.5 cfs, Q_{100} =38.8 cfs) are located at the same location as Filing 4 DP3.2 (Q_5 =16.9 cfs, Q_{100} =40.2 cfs) and have less than the anticipated flow at the existing storm manhole. The proposed Filing 5 flows at DP10.1 (Q_5 =17.1 cfs, Q_{100} =43.1 cfs) are located at the same location as Filing 2 DP2.2



 $(Q_5=56.9 \text{ cfs}, Q_{100}=138.7 \text{ cfs})$ and have less than the anticipated flow at the existing storm manhole. The proposed Filing 5 flows at DP11, DP12, DP13, DP14, and DP16.1 are the same flows the inlets at Filing 4 DP5, DP6.1, DP6.2, DP9, and DP7.1 capture. The proposed Filing 5 flows at DP15 $(Q_5=5.6 \text{ cfs}, Q_{100}=14.1 \text{ cfs})$ are located the same location as Filing 4 DP8 $(Q_5=6.1 \text{ cfs}, Q_{100}=12.9 \text{ cfs})$. The series of inlets along Sterling Ranch Road and Marksheffel Road to the Aspen Meadows Filing 1 development have the additional capacity to handle the change in bypass flows past this inlet. The proposed Filing 5 flows at DP17.1 $(Q_5=73.3 \text{ cfs}, Q_{100}=194.0 \text{ cfs})$ is located at the same location as Filing 4 DP10 $(Q_5=55.8 \text{ cfs}, Q_{100}=149.7 \text{ cfs})$ and Filing 2 DP2.5 $(Q_5=96.6 \text{ cfs}, Q_{100}=250.7 \text{ cfs})$. The downstream storm infrastructure from this design point was built in Filing 2 and the proposed flows are less than was anticipated in the existing storm manhole.

DRAINAGE DESIGN CRITERIA

DEVELOPMENT CRITERIA REFERENCE

Storm drainage analysis and design criteria for this project were taken from the "City of Colorado Springs/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual" (CSDCM), dated May 2014, as adopted by El Paso County.

HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Table 1: 1-hr Point Rainfall Data

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Sump and on-grade inlets will be sized using UDFCD UD-Inlet



v5.02. StormCAD will be used to model the proposed storm sewer system within the site to analyze the proposed HGL calculations for the Construction Drawings. Autodesk Hydraflow express will be used to size any channels or swales. Manhole and pipe losses for the model will be obtained from the *Modeling Hydraulic and Energy Gradients in Storm Sewers: A Comparison of Computation Methods*, by AMEC Earth & Environmental, Inc. The manhole loss coefficients used in the model can be seen in Table 2 (below) this method is accurate for pipes 42" and smaller for larger pipes the Standard headloss coefficients as recommended by Bentley were used as shown in Table 3. All hydraulic calculations will be found in the Final Drainage Report Appendices.

Table 2: Storm Head-loss Coefficients

	StormCA	D Conversion Ta	ble									
(0	Bend Angle	K coefficient (Conversion									
So	0	0.08	5									
٦ ا	22.5	0.1										
Bend Loss	45	0.4	.2									
	60	0.64										
	90	1.32	2									
	1 Lateral K coefficient Conversion											
	Bend Angle	Non Surcharged	Surcharged									
SS	45	0.27	0.47									
2	60	0.52	0.9									
<u>a</u>	90	1.02	1.77									
Lateral Loss	2 Latera	Is K coefficient Co	onversion									
	45	0.96	6									
	60	1.16	6									
	90	1.52										

Table 3: Storm Head-loss Coefficients

Type of Manhole	Diagram	Headloss Coefficient
Trunkline only with no bend at the junction	∑ → (0.5
Trunkline only with 45° bend at the junction	€-7-6	0.6
Trunkline only with 90° bend at the junction		0.8
Trunkline with one lateral	F	Small 0.6 Large 0.7
Two roughly equivalent entrance lines with angle < 90° between lines		0.8
Two roughly equivalent entrance lines with angle > 90° between lines		0.9
Three or more entrance lines		1.0



DRAINAGE FACILITY DESIGN

GENERAL CONCEPT

The proposed stormwater conveyance system was designed to convey the developed Sterling Ranch Filing No. 5 runoff to an existing (Filing 2) full spectrum water quality and detention Pond W-5 via existing and proposed storm sewer. The existing pond was designed to release at less than historic rates to minimize adverse impacts downstream. Treated water will outfall directly into the Sand Creek Drainageway, where it will eventually outfall into Fountain Creek. A proposed drainage map is presented in Appendix D showing locations of the pond.

FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The Sterling Ranch Filing No. 5 development project consists of single-family homes with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

Step 2 – Stabilize Drainage ways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be due at time of platting. These funds will be used for the channel stabilization being designed by JR Engineering adjacent to the site and on future projects within the basin to stabilize drainage ways. The site does not discharge directly into the open drainage way of Sand Creek, therefore no downstream stabilization will be accomplished with this project

Step 3 – Treat the WQCV: Water Quality treatment for this site is provided in the existing full spectrum water quality detention Pond W-5 and Pond W-8. The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structures have been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the pond will be reduced to less than historic rates.

Step 4 –BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. The Filing No. 5 site is residential. There is no proposed commercial or industrial use for the site. The permanent erosion control BMPs include asphalt drives, storm inlets and storm pipe, the full spectrum detention Pond W-5 and permanent vegetation. Maintenance responsibilities and plans will be defined at the time of final platting.



WATER QUALITY

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full-spectrum water quality and detention are provided for all developed basins. This site will drain into an existing Full-Spectrum Drainage Pond W-5 developed during the Sterling Ranch Filing Project. Further details as well as all pond volume, water quality, and outfall calculations are included in the Sterling Ranch Filing 2 Final Drainage Report. Pond W-5 corresponds to pond FSD6 from the Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018 and is releasing less than the MDDP values in the proposed design. A summary of Pond W-5 has been included below for reference. From the Filing No.2 drainage report, Pond W-5 accounted for Sterling Ranch Filing 5 area to have 65% imperviousness. The total imperviousness for the Filing 5 development is 59% imperviousness, and the total runoff is less than what was anticipated; therefore the existing Pond W-5 will function as intended. The FDR will analyze and determine if the existing off-site pond is functioning as intended.

EURV REQUIRED VOLUME PROVIDED WOCV 5-YEAR RELEASE 100-YEAR RELEASE VOLUME (AC-FT) (AC-FT) (AC-FT) (AC-FT) (CFS) (CFS) 137.1 POND W-5 18.217 18.441 3.29 11.71 2.7

Table 4: Pond Volumes & Release Rates

EROSION CONTROL PLAN

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit.

OPERATION & MAINTENANCE

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The district shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. A maintenance road was provided for the existing Pond W-5 and information on the road can be found in the Final Drainage Report for Sterling Ranch Filing No. 2. The maintenance road access is off Marksheffel Road and wraps around the top of the pond providing access to the inflow pipe wing walls and outlet structure for the pond. A maintenance road was provided for the existing Pond W-8 and information on the road can be found in the approved Sterling Ranch Filing No. 1 Storm Sewer Plans. The maintenance road access is off Dines Boulevard and provides access to the inflow pipe forebay and outlet structure for the pond.

DRAINAGE AND BRIDGE FEES

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees will be



defined within the Final Drainage Report and will be due at time of platting (depending on date of plat submittal).

SUMMARY

The proposed Sterling Ranch Filing No. 5 drainage improvements were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainage-ways or surrounding development. The existing Ponds W-5 and W-8 are to release less than 90% of the predeveloped runoff study associated with the subject site. The site is in continuity with the Sterling Ranch Filing No. 2 Drainage Report and the Sterling Ranch Filing No. 4 Drainage Report. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site. The proposed site does not impact any downstream facility or property.



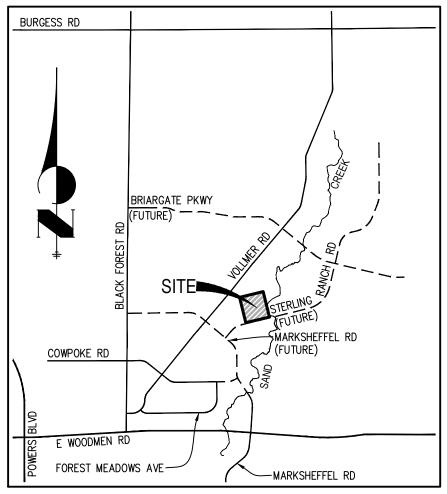
REFERENCES

- 1. "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), prepared by Mile High Flood District, Revised August 2018, September 2017, and January 2021.
- 3. "Master Development Drainage Plan for Sterling Ranch", (MMDP) prepared by M&S Civil Consultants, Inc., dated October 24, 2018.
- 4. <u>Sand Creek Drainage Basin Planning Study.</u> prepared Kiowa Engineering Corporation, January 1993, revised March 1996.
- 5. <u>Final Drainage Report For Barbarick Subdivision Portion Of Lots 1,2 And Lots 3 and 4,</u> prepared by Matrix Design Group, dated June 2016
- 6. "Final Drainage Report for Sterling Ranch Filing No. 2", prepared by JR Engineering, dated August 2021
- 7. "Final Drainage Report for Sterling Ranch Filing No. 4", prepared by JR Engineering, dated August 14, 2023
- 8. "Final Drainage Report for Branding Iron at Sterling Ranch Filing No. 1", prepared by M&S Civil Consultants, Inc., dated October 2018



Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map



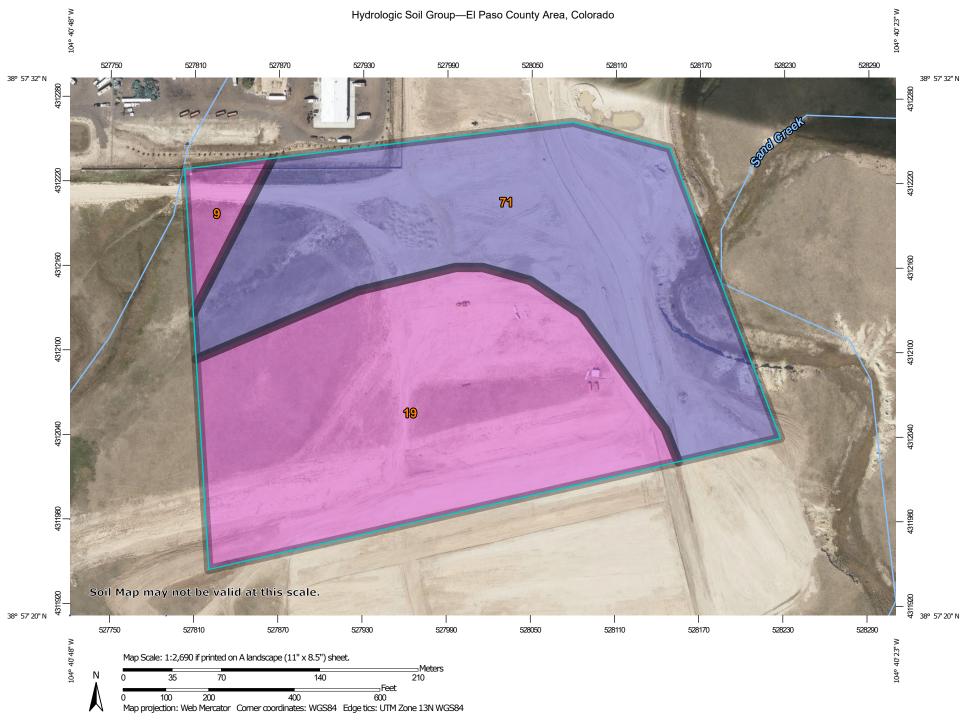


VICINITY MAP

VICINITY MAP HOMESTEAD FILING NO. 5 JOB NO. 25188.16 8/26/22 SHEET 1 OF 1



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Aug 19, 2018—Oct 20. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

	_			
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
9	Blakeland-Fluvaquentic Haplaquolls	А	0.8	3.3%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	12.0	49.0%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	11.7	47.7%
Totals for Area of Inter	rest	24.5	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

his map is for use in administering the National Flood Insurance Program. It does ot necessarily identify all areas subject to flooding, particularly from local drainage curces of small size. The community map repository should be consulted for sestile updated or additional flood heazerd information.

To class more dealers of included in contract measurements and the contract measurement of the contract measuremen

coastal Base Flood Elevations shown on this map apply only landward of 0.0 horn American Vertical Datum of 1989 (NAVDBS). Users of this FRM should be level from the level the level from the level level the level the level level the level level the level level level the level level level level the level level

Boundaries of the floodways were computed at cross sections and interpolate between cross sections. The floodways were based on hydraulic considerations will regard to requirements of the National Flood Insurance Program. Floodways width and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood contri** tructures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance study report for information on flood control structures for this jurisdiction.

The projection used in the presentation of this map was Universal Transverse decision UTIA1 year 13. The hosticontal datam was MADSIA GR899 sphesoid Differences in datum, spheroid, prejection or UTM zones zones used in the conduction of FIRINA for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not refer the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and of 1988 (NAVD88). These flood elevations must be compared to structure and conversion between the National Geodesic Vertical Datum of 1929 and the North American Vertical Datum of 1988, with the National Geodesic Survey website at the National Geodesic Survey website at the National Geodesic Survey and the North American Vertical Datum of 1988, visit the National Geodesic Survey are the National Geodesic Survey and the National Geodesic Survey are the National Geodesic Survey at the National Geodesic Survey are the National Geodesic Survey at the National Geodesic Survey

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

This map reflects more detailed and up-to-date stream channel configurations and loopighin delineations than those shown on the previous FRM for this principlion was been adjusted to contrion these are stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Instrumed SNU, Separative of the SNU of the S

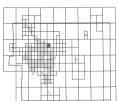
lease refer to the separately printed Map Index for an overview map of the count nowing the layout of map panels; community map repository addresses; and sting of Communities table containing National Flood insurance Program dates for sch community as well as a listing of the panels on which each community is

ontact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange MIX) 1-877-336-2627 for information on available products associated with this M. Available products may include previously issued Letters of Map Change, a lood Insurance Study Report, and/or digital versions of this map. The MSC may be be reached by Fax at 1-800-336-8020 and its website at

you have questions about this map or questions concerning the National Flossurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) sit the FEMA website at http://www.fema.gow/business/nflp.

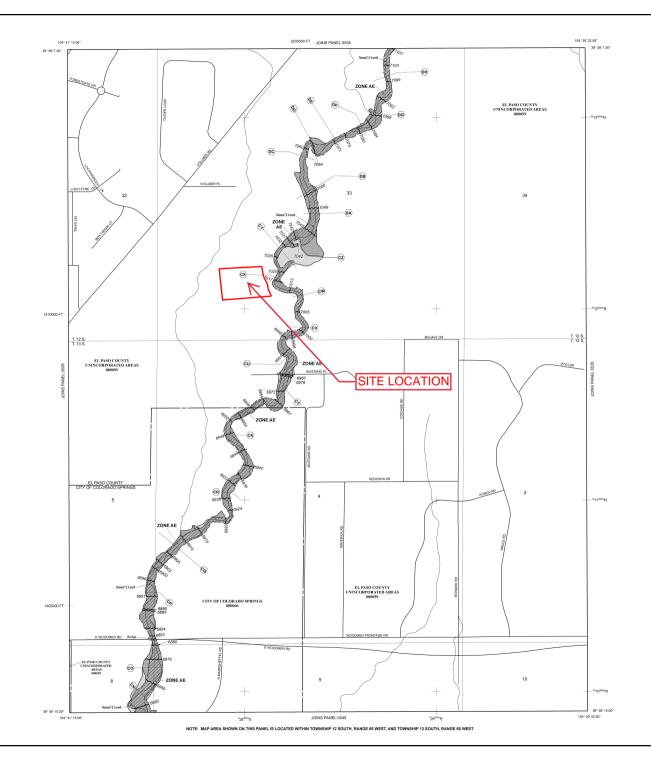
El Paso County Vertical Datum Offset Table

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



Digital Flood Insurance Rate Map (DFIRM) was produced through a serating Technical Partner (CTP) agreement between the State of Colorado or Conservation Board (CWCB) and the Federal Emergency Management





LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

ZONE A No Base Flood Elevations determined.

ZONE AE Base Flood Elevations determined.

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

determined.

Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the Former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Bevations

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encreachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodolain.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

Roodolain boundary Zone D Boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. Base Flood Elevation line and value; elevation in feet* (EL 987)

Base Flood Elevation value where uniform within zone; * Referenced to the North American Vertical Datum of 1988 (NAVD 88)

 $\begin{picture}(100,0) \put(0,0){\line} \put(0,0){\li$

23-----23 97° 07' 30.00° 32° 22' 30.00° Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

4274(000mg) 1000-meter Universal Transverse Mercator grid ticks, zone 13

• M1.5

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
DECEMBER 7, 2016 - to update corporate limits, to change Base Flood
Special Flood Hazard Areas, to update map format, to add crads and no

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-930-638-6630.

MAP SCALE 1" = 500"

250 0 500 1000 H H H FEET

FIRM

FLOOD INSURANCE RATE MAP

PANEL 0533G

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 533 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS COMMUNITY NUMBER PANEL SUFFIX

MAP NUMBER 08041C0533G

MAP REVISED **DECEMBER 7. 2018**

Federal Emergency Management Agency

Appendix B Hydrologic Calcs



COMPOSITE % IMPERVIOUS & COMPOSITE EXISTING RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Subdivision- Existing
Location: El Paso County

Project Name: Sterling Ranch Filing 5

Project No.: 25188.16

Calculated By: DIG
Checked By: RAB

Date: 11/3/23

	Total Area (ac)	Str	eets (10	0% Impe	rvious)	Re	sidentia	l (65% lm	pervious)	Light I	ndustria	l (80% In	npervious)		Lawns (0% Impe	Weigl	s Total nted C ues	Basins Total Weighted %	
Basin ID	Ai ea (ac)	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	Imp.	
A1	5.09	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	5.09	0.0%	0.08	0.35	0.0%
A2	2.89	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	2.89	0.0%	0.08	0.35	0.0%
A3	1.94	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	0.00	0.0%	0.08	0.35	1.94	0.0%	0.08	0.35	0.0%
A4	4.83	0.90	0.96	1.75	36.2%	0.45	0.59	0.80	10.8%	0.59	0.70	0.00	0.0%	0.08	0.35	2.28	0.0%	0.44	0.61	47.0%
OS1	0.77	0.90	0.96	0.00	0.0%	0.45	0.59	0.77	65.0%	0.59	0.70	0.00	0.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%
OS2	33.07	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.59	0.70	7.91	19.1%	0.08	0.35	25.16	0.0%	0.20	0.43	19.1%
OS3	13.90	0.90	0.96	2.35	16.9%	0.45	0.59	6.86	32.1%	0.59	0.70	0.00	0.0%	0.08	0.35	4.69	0.0%	0.40	0.57	49.0%
TOTAL (A1-A4)	14.75																			0.0%
TOTAL (OS1-OS3)	47.74																			28.6%
TOTAL	62.49																			25.5%

EXISTING STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Sterling Ranch Subdivision- Existing

Location: El Paso County

Project Name: Sterling Ranch Filing 5

Project No.: 25188.16

Calculated By: DIG Checked By: RAB

Date: 11/3/23

		SUB-I	BASIN			INITI	AL/OVER	_AND			TRAVEL TI	ME					
		DA	·ΤΑ				(T _i)				(T _t)			(L	FINAL		
BASIN	D.A.	Hydrologic	Impervious	C_5	C ₁₀₀	L	S_o	t_i	L _t	S_t	К	VEL.	t_t	COMP. t_c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	5.09	В	0%	0.08	0.35	180	1.4%	22.1	497	1.6%	10.0	1.3	6.5	28.7	677.0	33.3	28.7
A2	2.89	Α	0%	0.08	0.35	125	4.6%	12.4	385	5.2%	10.0	2.3	2.8	15.3	510.0	29.1	15.3
A3	1.94	Α	0%	0.08	0.35	80	1.7%	13.8	385	2.5%	10.0	1.6	4.1	17.9	465.0	30.5	17.9
A4	4.83	А	47%	0.44	0.61	100	3.0%	8.3	1466	1.5%	20.0	2.4	10.0	18.3	1566.0	30.8	18.3
OS1	0.77	Α	65%	0.45	0.59	88	2.0%	8.8	122	2.0%	10.0	1.4	1.4	10.2	210.0	15.7	10.2
OS2	33.07	А	19%	0.20	0.43	298	3.0%	19.5	1664	2.7%	10.0	1.6	16.9	36.4	1962.0	37.2	36.4
OS3	13.90	А	49%	0.40	0.57	100	1.8%	10.4	796	1.7%	20.0	2.6	5.1	15.5	896.0	24.1	15.5

NOTES:

 $t_c = t_i + t_t$

Equation 6-2

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$

Equation 6-3

Where:

 t_c = computed time of concentration (minutes)

 t_i = overland (initial) flow time (minutes)

 t_t = channelized flow time (minutes).

Where:

 t_i = overland (initial) flow time (minutes)

 C_5 = runoff coefficient for 5-year frequency (from Table 6-4)

 L_i = length of overland flow (ft)

 S_0 = average slope along the overland flow path (ft/ft).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where: t_t = channelized flow time (travel time, min) $L_t = \text{waterway length (ft)}$

 S_o = waterway slope (ft/ft) V_t = travel time velocity (ft/sec) = $K \lor S_o$ K = NRCS conveyance factor (see Table 6-2). Equation 6-4 $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$

Equation 6-5

Where:

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

 L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal) S_t = slope of the channelized flow path (ft/ft)

Table 6-2. NRCS Conveyance factors, K

E 61 16 6	C. T. T. T.	_
Type of Land Surface	Conveyance Factor, K	
Heavy meadow	2.5	
Tillage/field	5	
Short pasture and lawns	7	
Nearly bare ground	10	
Grassed waterway	15	
Paved areas and shallow paved swales	20	

STANDARD FORM SF-3 - EXISTING

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Sterling Ranch Filing 5
Subdivision: Sterling Ranch Subdivision- Existing	Project No.: 25188.16
Location: El Paso County	Calculated By: DIG
Design Storm: 5-Year	Checked By: RAB
	Date: 11/3/23

				DIREC	CT RUI	NOFF			TC	OTAL R	RUNOF	F	STRE	ET/SW	'ALE		PIPE TRA			TRAV	EL TIM	E
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	REMARKS
	1	OS1	0.77	0.45	10.2	0.35	4.10	1.4														
	2	OS2	33.07	0.20	36.4	6.68	2.19	14.6														Offsite Barbarick Pond Release Piped to DP4
		A1	5.09	0.08	28.7	0.41	2.55	1.0														
		A2	2.89	0.08	15.3	0.23	3.50	0.8														
		А3	1.94	0.08	17.9	0.16	3.26	0.5														
	3								28.7	1.15	2.55	2.9										Sum of basins A1-A3 and OS1, drain to Ex storm Piped west and south to Ex. Pond W-5
	4	OS3	13.90	0.40	15.5	5.58	3.47	19.4														
	5	A4	4.83	0.44	18.3	2.12	3.22	6.8														Runoff to Ex. Inlet in Sterling Ranch Road Piped south to Ex. Pond W-5

Motos

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

STANDARD FORM SF-3 - EXISTING

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Sterling Ranch Filing 5
Subdivision: Sterling Ranch Subdivision- Existing	Project No.: 25188.16
Location: El Paso County	Calculated By: DIG
Design Storm: 100-Year	Checked By: RAB
	Date: 11/3/23

				DIR	ECT RU	JNOFF			T	OTAL F	RUNOF	F	STRE	ET/SW	ALE	PIPE			TRAV	/EL TIN	ΛE		
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	O _{street/swale} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	OS1	0.77	0.59	10.2	0.45	6.88	3.1															
	2	OS2			36.4			52.8															Offsite Barbarick Pond Release Piped to DP4
		A1	5.09	0.35	28.7	1.78	4.28	7.6															
		A2	2.89	0.35	15.3	1.01	5.87	5.9															
		А3	1.94	0.35	17.9	0.68	5.47	3.7															
	3								28.7	3.92	4.28	16.8											Sum of basins A1-A3 and OS1, drain to Ex storm Piped west and south to Ex. Pond W-5
	4	OS3	13.90	0.57	15.5	7.94	5.83	46.3															
	5	A4	4.83	0.61	18.3	2.95	5.41	16.0				_											Runoff to Ex. Inlet in Sterling Ranch Road Piped south to Ex. Pond W-5

Notes:

Street and Pipe C^*A values are determined by Q/i using the catchment's intensity value.

COMPOSITE % IMPERVIOUS & COMPOSITE PROPOSED RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Sterling Ranch Subdivision -Proposed

Location: El Paso County

Project Name: Sterling Ranch Filing 5

Project No.: 25188.16

Calculated By: GAG

Checked By:

Date: 11/3/23

	Total	Paved	/Streets	(100% Ir	mpervious)	Res	sidential	(65% Im	pervious)	L	awns (0º	% Imperv	rious)	Weigh	s Total nted C	Basins Total	
Basin ID	Area (ac)	rea (ac) C_5 C_{100} Area Weighted C_5 C_{100} Area Weighted C_5 C_{100} Area Weighted C_5 C_5		C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	Val C ₅	ues C ₁₀₀	Weighted % Imp.							
A1	0.65	0.90	0.96	0.07	10.8%	0.45	0.59	0.26	26.0%	0.08	0.35	0.32	0.0%	0.32	0.51	36.8%	
A2	0.78	0.90	0.96	0.03	3.8%	0.45	0.59	0.50	41.7%	0.08	0.35	0.25	0.0%	0.35	0.53	45.5%	
А3	0.79	0.90	0.96	0.00	0.0%	0.45	0.59	0.54	44.4%	0.08	0.35	0.25	0.0%	0.33	0.51	44.4%	
A4	1.00	0.90	0.96	0.59	59.0%	0.45	0.59	0.32	20.8%	0.08	0.35	0.09	0.0%	0.68	0.79	79.8%	
A 5	2.84	0.90	0.96	0.74	26.1%	0.45	0.59	1.55	35.5%	0.08	0.35	0.55	0.0%	0.50	0.64	61.5%	
A6	0.66	0.90	0.96	0.10	15.2%	0.45	0.59	0.43	42.3%	0.08	0.35	0.13	0.0%	0.45	0.60	57.5%	
A7	2.04	0.90	0.96	0.71	34.8%	0.45	0.59	0.76	24.2%	0.08	0.35	0.57	0.0%	0.50	0.65	59.0%	
A8	1.10	0.90	0.96	0.51	46.4%	0.45	0.59	0.52	30.7%	0.08	0.35	0.07	0.0%	0.64	0.75	77.1%	
A9	0.20	0.90	0.96	0.00	0.0%	0.45	0.59	0.16	52.0%	0.08	0.35	0.04	0.0%	0.38	0.54	52.0%	
A10	1.32	0.90	0.96	0.01	0.8%	0.45	0.59	1.05	51.7%	0.08	0.35	0.26	0.0%	0.38	0.55	52.5%	
OS1	0.77	0.90	0.96	0.00	0.0%	0.45	0.59	0.77	65.0%	0.08	0.35	0.00	0.0%	0.45	0.59	65.0%	
C4	3.67	0.90	0.96	1.75	47.7%	0.45	0.59	0.83	14.7%	0.08	0.35	1.09	0.0%	0.55	0.70	62.4%	
TOTAL (A1-A10)	11.38															59.0%	
TOTAL	15.82															60.1%	

PROPOSED STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision:	Sterling Ranch Subdivision -Proposed
Location:	El Paso County

Project Name: Sterling Ranch Filing 5
Project No.: 25188.16

Calculated By: GAG

Checked By:

Date: 11/3/23

		SUB-E	BASIN			INITI	AL/OVER	LAND			TRAVEL TI	ME					
		DA	ATA				(T_i)				(T_t)			(U	FINAL		
BASIN	D.A.	Hydrologic	Impervious	C_5	C ₁₀₀	L	S_o	t _i	L_t	S_t	K	VEL.	t _t	COMP. t_c	TOTAL	Urbanized t_c	t_c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	0.65	В	37%	0.32	0.51	70	2.2%	9.1	335	0.7%	7.0	0.6	9.3	18.5	405.0	24.4	18.5
A2	0.78	В	46%	0.35	0.53	70	2.0%	9.0	345	1.0%	7.0	0.7	8.2	17.2	415.0	22.0	17.2
A3	0.79	А	44%	0.33	0.51	115	2.5%	11.0	420	1.5%	7.0	0.9	8.2	19.1	535.0	22.2	19.1
A4	1.00	А	80%	0.68	0.79	30	2.0%	3.3	950	1.6%	20.0	2.5	6.4	9.6	980.0	18.7	9.6
A 5	2.84	А	62%	0.50	0.64	30	2.0%	4.8	1035	1.6%	20.0	2.5	6.8	11.6	1065.0	23.3	11.6
A6	0.66	А	58%	0.45	0.60	30	2.0%	5.2	300	1.9%	20.0	2.8	1.8	7.0	330.0	18.3	7.0
A7	2.04	А	59%	0.50	0.65	95	2.0%	8.4	750	1.6%	20.0	2.6	4.9	13.2	845.0	21.6	13.2
A8	1.10	А	77%	0.64	0.75	30	2.0%	3.7	830	1.6%	20.0	2.5	5.5	9.1	860.0	18.4	9.1
A9	0.20	А	52%	0.38	0.54	85	2.3%	9.2	170	1.5%	20.0	2.4	1.2	10.3	255.0	18.6	10.3
A10	1.32	А	52%	0.38	0.55	75	3.5%	7.4	665	1.0%	20.0	2.0	5.5	13.0	740.0	23.9	13.0
OS1	0.77	А	65%	0.45	0.59	90	2.0%	8.9	125	2.0%	10.0	1.4	1.5	10.3	215.0	15.8	10.3
C4	3.67	А	62%	0.55	0.70	20	2.0%	3.5	1745	1.5%	10.0	1.2	23.7	27.2	1765.0	28.8	27.2

NOTES:

 $t_c = t_i + t_t$

Equation 6-2

Where:

 t_c = computed time of concentration (minutes)

 t_i = overland (initial) flow time (minutes)

 t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Equation 6-4

 $s_0 = \frac{0.395(1.1 - C_5)\sqrt{L}}{S_0^{0.33}}$

Where:

 t_i = overland (initial) flow time (minutes)

 C_5 = runoff coefficient for 5-year frequency (from Table 6-4)

 L_i = length of overland flow (ft)

 S_0 = average slope along the overland flow path (ft/ft).

 $t_c = (26-17i) + \frac{L_t}{60(14i+9)\sqrt{S_t}}$

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Where

 t_t = channelized flow time (travel time, min)

 $L_t = \text{waterway length (ft)}$

 S_0 = waterway slope (ft/ft) V_t = travel time velocity (ft/sec) = $K\sqrt{S_0}$

K = NRCS conveyance factor (see Table 6-2).

Where:

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

Equation 6-3

Equation 6-5

 L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal) S_t = slope of the channelized flow path (ft/ft).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name	Sterling Ranch Filing 5

Subdivision: Sterling Ranch Subdivision - Proposed

Location: El Paso County
Design Storm: 5-Year

Project No.: 25188.16 Calculated By: GAG

Checked By:
Date: 11/3/23

	I			DIREC	T RUN	NOFF			T	OTAL R	UNOF	F	STRF	ET/SW	/AI F	1	PII	PF		TRA\	/EL TII	MF	1
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	(in/hr)	(cfs)	(min)	C*A (ac)	(in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	ipe Size (inches)	ength (ft)	Velocity (fps)	(min)	REMARKS
	۵	Ba	Ar	R	t _c	<u>ڻ</u>	_	O	tc	Č	_	0	Ő	*ు	SIC	ď	ڻ	SIC	- Bi	Le	Ve	<u>+</u>	Off-site flows overland into Basin A2
		OS1	0.77	0.45	10.3	0.35	4.08	1.4															Combines flow in swale at DP1
		A2	0.78	0.35	17 2	0.27	3 31	0.9															Flows overland into swale at DP1 Combines flow in swale at DP1
		AZ	0.70	0.33	17.2	0.27	3.31	0.7															Combined flow of Basin OS1 and Basin A2 within swale
	1								17.2	0.62	3.31	2.1											Flows continue in swale to DP2
			, ,	0.00	10	0.04	0.04	0.7															Flows overland into swale at DP2
	2	A1	0.65	0.32	18.5	0.21	3.21	0.7															Combines flow in area inlet at DP2.1 Combined flow of DP1 and DP2 within area inlet
	2.1								18.5	0.83	3.21	2.7											Flows piped to sump inlet at DP5.1
																							Flows overland into swale at DP3
	3	A3	0.79	0.33	19.1	0.26	3.16	0.8															Combines flow at sump inlet at DP5
	4	A4	1.00	0.68	0.6	0.69	4.18	2.8															Flows along c&g at DP4 Combines flow at sump inlet at DP5
	+	74	1.00	0.00	7.0	0.00	4.10	2.0												1			Flows along c&g at within Basin A5
		A5	2.84	0.50	11.6	1.41	3.91	5.5															Combines flow at sump inlet at DP5
																							Combined flow of DP3, DP4, and Basin A5 within sump inlet
	5								19.1	2.35	3.16	7.4											Flows piped to sump inlet at DP5.1
																							Combined flow of DP2.1 and DP5 within pipe
	5.1								19.1	3.18	3.16	10.0											Flows piped to manhole at DP8.2
	1																						Flows off-site along ex. Dines Blvd. c&g to ex. sump inlet at DP6
	6	A6	0.66	0.45	7.0	0.29	4.67	1.4															Flows piped to ex. Pond W-8
																							Flows along c&g to the on-grade inlet at DP7
	7	A7	2.04	0.50	13.2	1.03	3.71	3.8															Captured flows piped to manhole at DP8.1, bypass runoff to ex. sump inlet at DP11
																							Flows along c&g to the on-grade inlet at DP8
	8	8A	1.10	0.64	9.1	0.70	4.27	3.0												ļ			Captured flows piped to manhole at DP8.1 Combined flow of DP7 and DP8 at manhole
	8.1								13.2	1 73	3.71	6.4											Flows piped to manhole at DP8.2
	0.1								10.2	1.75	5.71	0.1								1			Combined flow of DP5.1 and DP8.1 at manhole
	8.2								19.1	4.91	3.16	15.5											Flows piped to ex. manhole at DP10.1
																							Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g
	9	A9	0.20	0.38	10.3	0.08	4.08	0.3						-				ļ			-		Flows to ex. inlet at DP15 Flows into swale to area inlet at DP10
	10	A10	1.32	0.38	13.0	0.50	3.74	1.9															Piped to manhole at DP10.1
	T.	75		0.00		0.00	5	/													+		Combined flow of DP8.2 and DP10 at manhole
	10.1								19.1	5.41	3.16	17.1											Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

	Project Name: Sterling Ranch Filing 5
Subdivision: Sterling Ranch Subdivision -Proposed	Project No.: 25188.16
Location: El Paso County	Calculated By: GAG
Design Storm: 5-Year	Checked By:

Checked By:

Date:	11/3/23

				DIRE	CT RUI	NOFF			T	OTAL R	UNOF	F	STRE	ET/SW	/ALE		PII	PE		TRAV	/EL TIN	ИE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	C*A (Ac)	l (in/hr)	O (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	11	EX F4 I	DP5					12.0								12.0							Captured runoff to ex. sump inlet at Filing 4 DP5 Piped to sump inlet at DP13
		EX F4 I						3.9								3.9							Captured runoff to ex. sump inlet at Filing 4 DP6.1 Piped to sump inlet at DP13
	13	EX F4 I	DP6.2					2.0								2.0							Captured runoff to ex. sump inlet at Filing 4 DP6.2 Piped to sump inlet at DP13
		EX F4 I						16.9															Combined captured flow DP11, DP12, and DP13 at Filing 4 DP6.3 Piped to manhole at DP17.1
	14	EX F4 I	DP9					3.8								3.8							Combined flow of DP9 and Basin C4 Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1
		C4	3.67	0.55	27.2	2.04	2.63	5.4															Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g Flows to ex. inlet at DP15
	15								27.2	2.12	2.63	5.6											Combined flow of DP9 and Basin C4 Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1
	16.1	EX F4 I	DP7.1					30.0															Total runoff to ex. manhole at Filing 4 DP7.1 Piped to DP15 and combines at manhole at DP17.1
	17.1											73.3											Combined flow of DP10.1, DP13.1, DP14, DP15 and DP16.1. Filing 4 DP10. Total runoff piped to ex. Pond W-5

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

Values in BLUE indicate they are from the approved "Final Drainage Report for Sterling Ranch Filing No. 4" dated August 14, 2023 by JR Engineering

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision:	Sterling Ranch Subdivision -Proposed
Location:	El Paso County
Design Storm:	100-Year

Project Name: Sterling Ranch Filing 5
Project No.: 25188.16
Calculated By: GAG

Checked By:

Date: 11/3/23

				DIR	ECT R	UNOFF			T	OTAL F	RUNOI	FF	STRI	ET/SW	'ALE		PIF	PΕ		TRA\	/EL TIN	ИE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	(in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
		OS1	0.77	0.59	10.3	0.45	7.48	3.4															Off-site flows overland into Basin A2 Combines flow in swale at DP1
		A2	0.78				6.33	2.6															Flows overland into swale at DP1 Combines flow in swale at DP1
		nz.	0.70	0.55	17.2	0.41	0.33	2.0	47.0	0.01													Combined flow of Basin OS1 and Basin A2 within swale
	-								17.2	0.86	6.33	5.4											Flows continue in swale to DP2 Flows overland into swale at DP2
	2	A1	0.65	0.51	18.5	0.33	6.17	2.0															Combines flow in area inlet at DP2.1 Combined flow of DP1 and DP2 within area inlet
	2.1								18.5	1.19	6.17	7.3											Flows piped to sump inlet at DP5.1 Flows overland into swale at DP3
	3	А3	0.79	0.51	19.1	0.41	6.09	2.5															Combines flow at sump inlet at DP5
	4	A4	1.00	0.79	9.6	0.79	7.64	6.0															Flows along c&g at DP4 Combines flow at sump inlet at DP5
		A5	2.84	0.64	11.6	1.82	7.23	13.2															Flows along c&g at within Basin A5 Combines flow at sump inlet at DP5
	5								19.1	3 02	6.09	18.4											Combined flow of DP3, DP4, and Basin A5 within sump inlet Flows piped to sump inlet at DP5.1
	5.1								19.1		6.09												Combined flow of DP2.1 and DP5 within pipe Flows piped to manhole at DP8.2
	5.1								19.1	4.21	0.09	25.7											riows piped to marmole at DP8.2
	6	A6	0.66	0.60	7.0	0.40	8.37	3.3															Flows off-site along ex. Dines Blvd. c&g to ex. sump inlet at DP6 Flows piped to ex. Pond W-8
	7	A7	2.04	0.65	13.2	1.33	6.92	9.2															Flows along c&g to the on-grade inlet at DP7
	, ·																						Captured flows piped to manhole at DP8.1, bypass runoff to ex. sump inlet at DP11 Flows along c&g to the on-grade inlet at DP8
	8	A8	1.10	0.75	9.1	0.82	7.76	6.4															Captured flows piped to manhole at DP8.1 Combined flow of DP7 and DP8 at manhole
	8.1								13.2	2.15	6.92	14.9											Flows piped to manhole at DP8.2
	8.2								19.1	6.36	6.09	38.8											Combined flow of DP5.1 and DP8.1 at manhole Flows piped to ex. manhole at DP10.1
	9	40	0.20	0.54	10.3	0.11	7.40	0.0															Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g Flows to ex. inlet at DP15
	9	A9	0.20	0.54	10.3	0.11	7.49	0.8															Flows not ex. inject at DP15 Flows into swale to area inject at DP10
	10	A10	1.32	0.55	13.0	0.72	6.97	5.0															Piped to manhole at DP10.1 Combined flow of DP8.2 and DP10 at manhole
	10.1								19.1	7.08	6.09	43.1											Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1

STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision:	Sterling Ranch Subdivision -Proposed
Location:	El Paso County
Design Storm:	100-Year

Project Name: Sterling Ranch Filing 5

Project No.: 25188.16
Calculated By: GAG Checked By:

Date: 11/3/23

		DIRECT RUNOFF			1	OTAL F	RUNOF	F	STRE	ET/SWA	ALE		PIP	E		TRA	VEL TI	ME					
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet/swale (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	11	EX F4 C	DE.					25.9								13.5							Captured runoff to ex. sump inlet at Filing 4 DP5 Piped to sump inlet at DP13
		EX F4 C						19.3								16.2							Captured runoff to ex. sump inlet at Filing 4 DP6.1 Piped to sump inlet at DP13
	13	EX F4 C	P6.2					7.3								7.3							Captured runoff to ex. sump inlet at Filing 4 DP6.2 Piped to sump inlet at DP13
	13.1	EX F4 C	P6.3					35.6															Combined captured flow DP11, DP12, and DP13 at Filing 4 DP6.3 Piped to manhole at DP17.1
	14	EX F4 C)P9					7.9								7.7							Combined flow of DP9 and Basin C4 Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1
		C4	3.67	0.70	27.2	2.55	5.30	13.5															Flows off-site along ex. Dines Blvd. c&g to ex. Sterling Ranch Road c&g Flows to ex. inlet at DP15
	15								27.2	2.66	5.30	14.1											Combined flow of DP9 and Basin C4 Piped to ex. Filing 4 storm sewer and combines at manhole at DP17.1
	16.1	EX F4 C	P7.1					93.5															Total runoff to ex. manhole at Filing 4 DP7.1 Piped to DP15 and combines at manhole at DP17.1
	17.1											194.0											Combined flow of DP10.1, DP13.1, DP14, DP15 and DP16.1. Filing 4 DP10. Total runoff piped to ex. Pond W-5

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
Values in BLUE indicate they are from the approved "Final Drainage Report for Sterling Ranch Filing No. 4" dated August 14, 2023 by JR Engineering

Appendix C Reference Material



MASTER DEVELOPMENT DRAINAGE PLAN FOR STERLING RANCH

OCTOBER 2018

Prepared for:

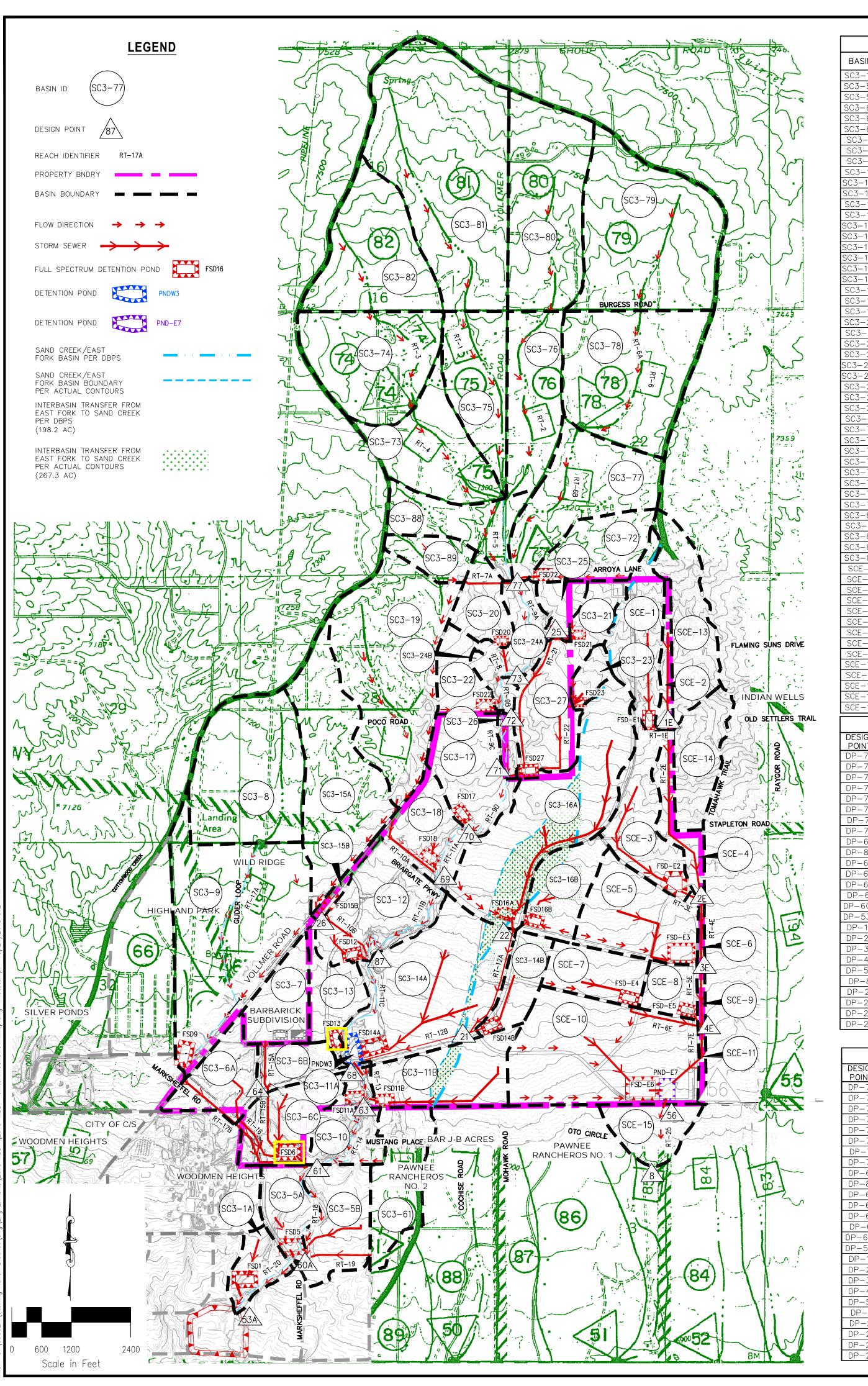
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Prepared by:



20 Boulder Crescent, Suite 110 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-002 SKP-18-003 SF-17-024



BASIN SUMMARY													
BASIN	CN	AREA (ACRES)	AREA (sq mi)	Q ₂ (CFS)	Q5 (OFS)	Q ₁₀ (cfs)	Q ₂₅ (CFS)	Q 50 (CFS)	Q ₁₀₀ (cFs)				
SC3-1A	73	27.8	0.044	16.3	23.3	33.0	45.8	57.1	68.9				
SC3-5A	84	39.1	0.061	40.6	53.7	71.0	92.4	110.6	129.1				
SC3-5B	81	63.0	0.098	53.8	73.0	98.5	130.8	158.6	187.0				
SC3-6A	88	49.3	0.077	61.4	79.3	102.2	130.1	153.6	177.1				
SC3-6B	85	30.9	0.048	32.9	43.4	57.0	73.9	88.2	102.7				
SC3-6C	82	58.0	0.091	53.9	72.5	97.1	128.0	154.5	181.5				
SC3-7	88	45.7	0.071	54.0	69.9	90.3	115.2	136.2	157.2				
SC3-8	62	143.4	0.224	25.4	42.1	66.7	100.7	132.3	166.2				
SC3-9	66	217.4	0.340	45.8	71.5	108.6	158.9	204.9	254.0				
SC3-10	63	36.0	0.056	7.6	12.3	19.4	29.1	38.0	47.7				
SC3-11A	70	10.7	0.017	5.3	7.8	11.3	15.9	20.0	24.3				
SC3-11B	80	76.6	0.120	59.4	81.3	110.8	148.1	180.5	213.7				
SC3-12	81	88.2	0.138	77.8	105.6	142.5	189.1	229.1	270.0				
SC3-13	85	41.0	0.064	43.9	57.8	76.0	98.5	117.6	136.9				
SC3-14A	79	164.9	0.258	127.6	175.4	239.8	321.9	393.2	466.3				
SC3-14B	77	34.7	0.054	24.6	34.3	47.4	64.2	79.0	94.1				
SC3-15A	62	139.7	0.218	21.3	35.5	56.3	85.3	112.1	141.0				
SC3-15B	87	7.9	0.012	10.8	14.0	18.2	23.3	27.6	31.9				
SC3-16A	74	168.1	0.263	84.4	120.4	170.0	234.8	292.2	351.8				
SC3-16B	78	50.7	0.079	39.0	53.7	73.6	99.0	121.1	143.8				
SC3-17	73	70.6	0.110	41.8	59.6	85.2	119.0	149.1	180.6				
SC3-18	81	53.8	0.084	49.3	67.1	91.0	121.2	147.3	174.0				
SC3-19	62	184.0	0.287	28.8	47.7	75.7	114.4	150.2	188.8				
SC3-20	65	34.2	0.053	9.9	15.5	23.8	35.1	45.5	56.6				
SC3-21	66	23.3	0.036	7.0	10.8	16.3	23.7	30.4	37.5				
SC3-22	65	33.9	0.053	9.4	14.8	22.5	32.9	42.5	52.6				
SC3-23	67	14.5	0.023	5.5	8.3	12.4	18.0	23.0	28.4				
SC3-24A	65	35.7	0.056	13.0	20.4	31.1	45.7	59.0	73.2				
SC3-24B	65	12.2	0.019	3.4	5.3	8.1	11.8	15.2	18.9				
SC3-25	66	19.0	0.030	5.8	8.9	13.4	19.5	25.1	31.0				
SC3-26	63	10.0	0.016	2.5	4.0	6.2	9.2	12.1	15.1				
SC3-27	71	70.0	0.109	35.1	51.2	73.8	103.7	130.3	158.3				
SC3-61	63	65.5	0.102	13.7	22.0	34.4	51.6	67.6	84.8				
SC3-72	64	56.2	0.088	12.8	20.2	31.4	46.7	60.9	76.0				
SC3-73	63	90.0	0.141	16.4	26.4	41.3	62.1	81.3	102.0				
SC3-74	63	119.7	0.187	22.3	36.5	57.3	85.9	112.3	140.7				
SC3-75	63	79.3	0.124	13.1	21.5	33.7	50.5	66.1	82.8				
SC3-76	63	86.4	0.135	14.2	23.1	36.4	54.6	71.4	89.6				
SC3-77	62	106.9	0.167	16.6	27.6	43.8	66.2	87.0	109.4				
SC3-78	63	155.6	0.243	28.1	45.3	70.6	106.2	139.1	174.5				
SC3-79	63	189.0	0.295	34.9	57.0	89.5	134.3	175.6	220.1				
SC3-80 SC3-81	63 62	147.7 262.9	0.231	27.3 42.6	44.3 70.2	69.6 111.0	104.5 167.4	136.8 219.6	171.4 275.7				
SC3-82	62	117.8	0.411	20.0	33.2	52.8	80.0	105.1	132.3				
SC3-88	62	60.2	0.184	10.5	17.4	27.6	41.8	54.9	69.0				
SC3-89	62	27.5	0.094	6.1	10	15.7	23.6	30.8	38.6				
SCE-1	65	64.4	0.043	23.3	35.9	53.8	79.1	102.4	127.4				
SCE-2	64	15.0	0.101	4.4	7.0	10.8	15.9	20.7	25.7				
SCE-3	70	67.5	0.023	30.6	45.2	65.9	93.3	118.0	143.9				
SCE-4	70	29.5	0.105	13.3	19.6	28.6	40.6	257.8	62.6				
SCE-5	87	85.5	0.134	100.4	130.6	169.6	217.4	257.8	298.4				
SCE-6	64	3.8	0.006	1.6	2.5	3.7	5.4	7.0	8.6				
SCE-7	89	44.9	0.070	58.9	75.5	96.6	122.2	143.7	165.2				
SCE-8	92	25.5	0.040	38.6	48.4	60.7	75.4	87.7	99.9				
SCE-9	64	4.0	0.006	1.5	2.4	3.6	5.3	6.8	8.5				
SCE-10	83	174.3	0.272	7.6	189.4	19.4	29.1	398.9	467.5				
SCE-11	64	5.8	0.009	2.3	3.6	5.5	8.0	10.3	12.8				
	63	78.6	0.123	19.6	31.3	48.7	73.1	95.7	120.0				
SCE-13 I	00												
SCE-14	63	52.5	0.082	13.2	21.2	33.3	49.9	65.2	81.7				

				DESIG	N POIN	IT SUM	MARY	
DESIGN POINT	AREA (sq mi)	Q ₂ (CFS)	Q ₅ (CFS)	Q ₁₀ (cfs)	Q ₂₅ (CFS)	Q ₅₀ (cFs)	Q100 (CFS)	LOCATION
DP-74	0.371	39.3	65.3	104.8	158.9	209.1	262.8	
DP-75	1.413	141.2	235.1	376.6	566.6	750.9	950.5	
DP-77	2.343	209.9	351.9	580.6	886.6	1168.4	1467.7	ARROYA LANE X-ING
DP-78	0.538	59.7	98.4	154.0	232.6	306.2	385.3	
DP-73	2.471	207.5	354.3	588.5	897.1	1187.2	1506.7	
DP-72	2.543	206.2	352.5	586.7	897.2	1195.3	1518.6	POCO ROAD X-ING
DP-71	2.757	205.9	349.3	610.5	932.4	1226.9	1612.2	STERLING RANCH NORTHERN BNDRY
DP-70	2.867	205.3	349.8	614.0	940.1	1260.6	1636.7	
DP-69	3.238	212.7	366.6	653.7	1010.6	1364.1	1775.7	BRIARGATE PARKWAY X-ING
DP-87	3.594	216.9	374.6	681.9	1072.1	1471.5	1905.9	
DP-68	4.312	214.6	374.5	714.9	1187.6	1674.9	2204.1	UPSTREAM OF POND W3
DP-64	0.119	85.9	112.1	145.9	187.5	222.6	258.0	
DP-63	4.449	154.4	201.0	375.7	815.9	1112.1	1385.1	STERLING RANCH SOUTHERN BNDRY
DP-61	5.356	156.6	223.9	428.0	928.2	1287.3	1620.1	COLORADO SPRINGS/EL PASO BNDRY
DP-60A	5.617	161.6	224.8	439.1	950.4	1320.5	1661.8	MARKSHEFFEL X-ING
DP-53A	5.661	161.6	225.7	441.8	951.1	1326.0	1668.9	SAND CREEK AND POND 3
DP-1E	0.247	23.9	38.3	70.1	132.8	173.0	220.9	
DP-2E	0.486	48.9	76.8	123.0	228.7	319.7	419.4	
DP-3E	0.626	48.5	75.7	122.2	271.1	387.1	500.1	
DP-4E	0.745	48.1	76.2	122.4	286.9	407.3	534.8	
DP-56	1.017	23.1	35.3	71.5	108.3	152.1	196.4	NEAR SE PROP CORNER
DP-8	1.079	24.1	37.2	73.5	111.3	155.4	200.7	BELOW SE PROP CORNER
DP-21	0.396	0.6	8.8	17.8	57.1	116.8	174.9	
DP-22	0.342	0.6	8.8	17.6	56.8	105.1	156.4	
DP-25	0.066	5.9	9.1	16.3	35.1	46.4	58.2	
DP-26	0.012	0.1	1.1	3.2	7.3	9.5	12.0	

	DESIGN POINT SUMMARY (VOLUME)													
DESIGN POINT	AREA (sq mi)	V ₂ (AC-FT)	V ₅ (AC-FT)	V10 (AC-FT)	V25 (AC-FT)	V ₅₀ (AC-FT)	V ₁₀₀ (AC-FT)	LOCATION						
DP-74	0.371	5.9	9.0	13.6	19.8	25.5	31.6							
DP-75	1.413	22.7	34.5	51.7	75.4	97.1	120.5							
DP-77	2.343	37.7	57.4	85.9	125.1	161.1	199.9	ARROYA LANE X-ING						
DP-78	0.538	8.9	13.5	20.1	29.3	37.7	46.7							
DP-73	2.471	40.0	60.8	91.0	132.5	170.7	211.7							
DP-72	2.543	41.3	62.9	94.0	136.8	176.2	218.5	POCO ROAD X-ING						
DP-71	2.757	46.3	70.0	104.3	151.3	194.5	240.8	STERLING RANCH NORTHERN BNDRY						
DP-70	2.867	49.5	74.5	110.6	160.1	205.4	254.0							
DP-69	3.238	57.5	86.1	127.4	183.8	235.3	290.6	BRIARGATE PARKWAY X—ING						
DP-87	3.594	66.5	98.9	145.6	209.1	267.1	329.1							
DP-68	4.312	81.8	123.7	183.9	264.9	338.0	415.8	UPSTREAM OF POND W3						
DP-64	0.119	7.0	9.1	11.8	15.2	18.1	21.1							
DP-63	4.449	85.6	129.5	192.3	276.7	352.8	433.5	STERLING RANCH SOUTHERN BNDRY						
DP-61	5.356	103.7	157.8	235.1	338.4	431.3	529.8	COLORADO SPRINGS/EL PASO BNDRY						
DP-60A	5.617	111.0	168.6	250.4	359.5	457.7	561.5	MARKSHEFFEL X-ING						
DP-53A	5.661	112.0	170.0	252.6	362.6	461.7	566.5	SAND CREEK AND POND 3						
DP-1E	0.247	3.1	5.2	8.4	12.7	16.6	20.9							
DP-2E	0.480	6.1	10.4	16.9	25.7	33.7	42.2							
DP-3E	0.620	7.0	13.7	23.4	36.1	47.4	59.3							
DP-4E	0.736	7.6	15.6	27.2	43.0	57.2	72.0							
DP-56	1.017	7.7	16.1	28.6	51.3	71.7	92.9	NEAR SE PROP CORNER						
DP-8	1.079	8.0	16.7	26.6	53.0	74.0	95.9	BELOW SE PROP CORNER						
DP-21	0.396	6.3	11.3	18.3	27.5	35.6	44.0							
DP-22	0.736	6.3	10.7	16.7	24.6	31.5	38.7							
DP-25	1.017	1.3	1.9	2.8	4.1	5.2	6.4							
DP-26	1.079	0.7	0.9	1.2	1.5	1.8	2.1							

WATER QUALI	TV & D	FTENTI	ON PO	ND SIII	ΙΜΔΡΥ	,	WATER QUALITY & DETENTION POND SUMMARY							
FSD1	11 & D			140 001	MINITALY I		FSD16B							
STORM EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100	
PEAK INFLOW (CFS)	16.3	23.3	33.0	45.8	57.1	68.9	PEAK INFLOW (CFS)	39.0	53.7	73.6	99.0	121.1	143.8	
ALLOWABLE RELEASE (CFS)	0.1	1.7	3.3	10.9	17.5	25.5	ALLOWABLE RELEASE (CFS)	0.0	0.4	0.7	8.3 7.9	17.2 17.2	28.2	
MODELED RELEASE (CFS)	0.1	1.6	3.2	10.9	17.4	25.4	MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.0 3.0	0.4 3.9	5.1	5.1	5.3	28.1 5.8	
STORED VOLUME (AC-FT)	2.4	2.6	3.0	3.6	1.9	2.2	STORED VOLUME (AC-FT)	3.0	J.9	3.1	J.1	3.3	3.0	
				1			FSD17							
FSD5							STORM EVENT (YR)	2	5	10	25	50	100	
STORM EVENT (YR)	2	5	10	25	50	100	PEAK INFLOW (CFS)	41.8	59.6	85.2	119.0	149.1	180.6	
PEAK INFLOW (CFS)	40.6	53.7	71.0	92.4	110.6	129.1	ALLOWABLE RELEASE (CFS)	0.7	11.1	22.5	52.0	67.2	86.3	
ALLOWABLE RELEASE (CFS)	0.1	1.4	2.6	11.3	19.8	30.2	MODELED RELEASE (CFS)	0.7	8.4	22.4	52.0	67.2	86.1	
MODELED RELEASE (CFS)	0.1	1.4	2.6	11.2	19.7	30.1	STORED VOLUME (AC-FT)	2.6	2.6	2.8	3.4	4.0	4.7	
STORED VOLUME (AC-FT)	3.0	3.2	3.8	4.1	4.7	5.2								
FODG							FSD18							
FSD6 STORM EVENT (YR)			10) o =	E0	100	STORM EVENT (YR)	2	5	10	25	50	100	
PEAK INFLOW (CFS)	2 196.5	5 258.5	10 339.1	25 438.7	50 523.3	100 608.6	PEAK INFLOW (CFS)	49.3	67.1	91.0	121.2	147.3	174.0	
ALLOWABLE RELEASE (CFS)	0.5	7.6	14.6	58.4	99.6	149.7	ALLOWABLE RELEASE (CFS)	0.6	9.2	18.4	42.2	54.6	69.9	
MODELED RELEASE (CFS)	0.5	7.5	14.5	58.2	99.6	149.6	MODELED RELEASE (CFS)	0.6	6.3	18.4	42.2	54.6	69.6	
STORED VOLUME (AC-FT)	15.5	16.4	18.7	20.8	23.3	26.0	STORED VOLUME (AC-FT)	3.2	3.2	3.4	4.0	4.7	5.3	
		1	1				FSD20							
FSD9							STORM EVENT (YR)	2	5	10	25	50	100	
STORM EVENT (YR)	2	5	10	25	50	100	PEAK INFLOW (CFS)	9.9	15.5	23.8	35.1	45.5	56.6	
PEAK INFLOW (CFS)	64.6	105.6	169.5	252.3	327.1	410.1	ALLOWABLE RELEASE (CFS)	0.4	5.5	11.1	25.7	33.2	42.5	
ALLOWABLE RELEASE (CFS)	1.7	24.9	49.8	141.1	207.2	290.0	MODELED RELEASE (CFS)	0.4	2.8	10.9	25.7	33.0	42.4	
MODELED RELEASE (CFS)	1.7	24.9	49.8	141.1	207.0	289.9	STORED VOLUME (AC-FT)	0.7	0.8	0.8	0.9	1.0	1.2	
STORED VOLUME (AC-FT)	8.7	8.7	9.6	10.8	12.3	13.8	, , ,		,	•	,		,	
FSD11A							FSD21							
STORM EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100	
PEAK INFLOW (CFS)	5.3	7.8	11.3	15.9	20.0	24.3	PEAK INFLOW (CFS)	7.0	10.8	16.3	23.7	30.4	37.5	
ALLOWABLE RELEASE (CFS)	0.1	1.6	3.2	7.5	9.7	12.4	ALLOWABLE RELEASE (CFS)	0.3	4.0	8.0	18.3	23.7	30.3	
MODELED RELEASE (CFS)	0.2	0.9	3.0	7.5	9.7	12.3	MODELED RELEASE (CFS)	0.3	3.3	8.0	18.3	23.7	30.1	
STORED VOLUME (AC-FT)	0.3	0.3	0.4	0.4	0.5	0.6	STORED VOLUME (AC-FT)	0.5	0.5	0.5	0.6	0.7	0.8	
500440														
FSD11B		I -	10	T 05		400	FSD22 STORM EVENT (YR)	2	5	10	25	50	100	
STORM EVENT (YR)	2	5	10	25	50	100	PEAK INFLOW (CFS)	9.4	14.8	22.5	32.9	42.5	52.6	
PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	59.4 0.3	81.3 4.5	110.8 8.7	148.1 29.6	180.5 47.7	213.7 69.6	ALLOWABLE RELEASE (CFS)	0.4	5.8	11.5	26.5	34.3	43.9	
MODELED RELEASE (CFS)	0.3	4.5	8.6	29.5	47.7	69.5	MODELED RELEASE (CFS)	0.4	5.8	11.4	26.5	34.3	43.8	
STORED VOLUME (AC-FT)	4.8	4.9	5.5	6.4	7.3	8.2	STORED VOLUME (AC-FT)	0.6	0.6	0.7	0.8	0.9	1.0	
STORED VOLOME (NO 11)	7.0	1 +.5	0.0	0.7	7.5	0.2		0,0	1 0.0		0.0	1 0,0	1,,,	
FSD12							FSD23							
STORM EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100	
PEAK INFLOW (CFS)	77.8	105.6	142.5	189.1	229.1	270.0	PEAK INFLOW (CFS)	5.5	8.3	12.4	18.0	23.0	28.4	
ALLOWABLE RELEASE (CFS)	0.9	13.2	26.7	62.0	80.2	103.2	ALLOWABLE RELEASE (CFS)	0.2	2.4	4.9	11.2	14.5	18.6	
MODELED RELEASE (CFS)	0.9	9.0	26.7	61.9	80.1	103.1	MODELED RELEASE (CFS)	0.2	2.0	4.9	11.2	14.5	18.6	
STORED VOLUME (AC-FT)	5.2	5.5	5.8	6.7	7.8	8.9	STORED VOLUME (AC-FT)	0.3	0.3	0.4	0.4	0.5	0.6	
500.47														
FSD13			1.0		F.0	100	FSD27		T -	1 40	0.5	T 50	100	
STORM EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100	
PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	43.9 0.4	57.8 6.1	76.0 12.3	98.5 28.6	117.6 37.0	136.9 47.6	PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	38.8 1.4	57.6 21.1	84.1 42.4	119.7 97.8	159.2 126.4	206.3 161.9	
MODELED RELEASE (CFS)	0.4	4.2	12.3	28.6	36.9	47.0	MODELED RELEASE (CFS)	1.4	18.4	42.4	97.6	126.4	161.9	
STORED VOLUME (AC-FT)	3.1	3.1	3.3	3.8	4.4	5.0	STORED VOLUME (AC-FT)	2.7	2.8	2.9	3.2	3.7	4.2	
STORED VOLONIE (NO 11)	1 0.1	J 0.1	L 3.3	1 0.0	1.7		STORED VOLUME (AU II)	<u> </u>					I +. Z	
FSD14A							FSD72							
STORM EVENT (YR)	2	5	10	25	50	100	STORM EVENT (YR)	2	5	10	25	50	100	
PEAK INFLOW (CFS)	127.6	175.4	239.8	321.9	393.2	466.3	PEAK INFLOW (CFS)	12.8	20.2	31.4	46.7	60.9	76.0	
ALLOWABLE RELEASE (CFS)	0.5	7.5	14.4	56.2	95.2	142.4	ALLOWABLE RELEASE (CFS)	0.6	9.6	19.3	44.4	57.4	73.4	
MODELED RELEASE (CFS)	0.5	7.5	14.4	56.2	95.1	142.2	MODELED RELEASE (CFS)	0.6	9.3	19.2	44.4	57.4	73.4	
STORED VOLUME (AC-FT)	9.9	10.6	11.9	13.5	15.3	17.3	STORED VOLUME (AC-FT)	1.0	1.0	1.1	1.1	1.2	1.3	
50045							PNDW3							
FSD14B		_	4.0	^-	 ^	100	STORM EVENT (YR)	2	5	10	25	50	100	
STORM EVENT (YR)	2	5	10	25	50	100	PEAK INFLOW (CFS)	214.6	374.5	714.9	1187.6	1674.9	2204.1	
PEAK INFLOW (CFS) ALLOWABLE RELEASE (CFS)	24.6	34.3	47.4	64.2	79.0	94.1	MODELED RELEASE (CFS)	154.3	200.3	366.8	799.9	1085.6	1350.6	
MODELED RELEASE (CFS)	0.0	0.3	0.5 0.5	5.7 4.5	11.8 11.8	19.3 19.3	STORED VOLUME (AC-FT)	2.8	9.5	26.3	41.2	57.2	78.2	
STORED VOLUME (AC-FT)	1.9	2.5	3.3	3.5	3.5	3.8	FSD-E1							
STORED VOLUME (AU-IT)	1.3	۷. ک	L 0.0	J. J. J	J. J.	J. U	STORM EVENT (YR)	2	5	10	25	50	100	
FSD15B							PEAK INFLOW (CFS)	23.3	35.9	53.8	79.1	102.4	127.4	
STORM EVENT (YR)	2	5	10	25	50	100	ALLOWABLE RELEASE (CFS)	0.7	11.0	22.1	50.9	65.7	84.1	
PEAK INFLOW (CFS)	10.8	14.0	18.2	23.3	27.6	31.9	MODELED RELEASE (CFS)	0.7	5.4	19.9	48.9	62.8	84.0	
ALLOWABLE RELEASE (CFS)	0.1	1.6	3.2	7.3	9.5	12.0	STORED VOLUME (AC-FT)	1.3	1.3	1.5	1.8	2.1	2.5	
MODELED RELEASE (CFS)	0.1	1.1	3.2	7.3	9.5	12.0	FSD-E2							
STORED VOLUME (AC-FT)	0.6	0.6	0.7	0.8	0.9	1.0	STORM EVENT (YR)	2	5	10	25	50	100	
							PEAK INFLOW (CFS)	30.6	45.2	65.9	93.3	118.0	143.9	
FSD16A	_	· · · · · · · · · · · · · · · · · · ·	_	· · · · · · · · · · · · · · · · · · ·			ALLOWABLE RELEASE (CFS)	0.6	9.5	19.2	45.5	59.8	77.6	
STORM EVENT (YR)	2	5	10	25	50	100	MODELED RELEASE (CFS)	0.6	3.2	18.5	41.3	58.5	74.7	
PEAK INFLOW (CFS)	84.4	120.4	170.0	234.8	292.2	351.8	STORED VOLUME (AC-FT)	2.1	2.3	2.4	2.8	3.3	3.8	
ALLOWABLE RELEASE (CFS)	0.6	8.8	17.3	56.2	88.4	128.3	FSD-E3							
MODELED RELEASE (CFS) STORED VOLUME (AC-FT)	0.6 7.6	8.8 7.7	17.3 8.9	56.2 10.4	88.3 12.1	128.3 13.8	STORM EVENT (YR)	2	5	10	25	50	100	
STONED VOLUME (ACTI)	/.0	/·/ 	J 0.9	10,4		10.0	PEAK INFLOW (CFS)	100.4	130.6	169.6	217.4	257.8	298.4	
	SAND	CREEK	√ FI ∩W	,			ALLOWABLE RELEASE (CFS)	0.9	13.2	26.5	61.6	79.8	102.6	
		A DISON					MODELED RELEASE (CFS)	1.0	6.8	25.7	56.0	79.8	101.3	
I	1-13NAD	ベロにいい					I CTARER VALUE (AC ET)	7.0	7 2	7 7	വ	I 1∩1		

			EEK FLOW ON CHART
DESIGN POINT	AREA (sq mi)	Q100 (CFS)	DESCRIPTION
DP-77	2.343	1468	PROPOSED CONDITION
	2.91	2262	SAND CREEK DBPS
		2600	FEMA
DP-71	2.757	1612	PROPOSED CONDITION
		2260	SAND CREEK DBPS
DP-63	4.449	1385	PROPOSED CONDITION
	4.33	2630	SAND CREEK DBPS
		2600	FEMA
DP-60A	5.661	1662	PROPOSED CONDITION
	5.38	3295	SAND CREEK DBPS

EFSC DBPS DESIGN POINT SUMMARY (PEAK FLOW)											
DBPS DESIGN POINT	AREA (sq mi)	Q10 (CFS) (EXIST)	Q100 (CFS) (EXIST)	AREA (sq mi)	Q10 (CFS) (PROP)	Q100 (CFS) (PROP)					
DP-50	0.32	47.0	195.7	0.32	146.7	370.3					
DP-51 (BASIN 86)	0.33	17.7	74.1	0.33	110.0	233.5					
DP-52	1.67	80.5	456.5	1.67	1207.9	2123.0					
DP-56	0.79	63.6	265.0	0.79	513.0	908.2					

Values reported from SCDBPS, (DP 50, 51, 52 Not analyzed as a part of this study) DBPS Reach 85(Basin91)=Q10=28.8cfs Q100=115.2cfs / Q10=345.7cfs Q100=588.9cfs (EXISTING) (PROPOSED)



20 BOULDER CRESCEN COLORADO SPRINGS PHONE: 719.955.5485

	STORED VOLUME (AC-FT)	3.0	3.7	4.4	4.8	5.0	5.3								
	FSD-E6	SD-E6													
	STORM EVENT (YR)	2	5	10	25	50	100								
	PEAK INFLOW (CFS)	141.6	189.4	252.5	331.4	398.9	467.5								
	ALLOWABLE RELEASE (CFS)	0.2	1.9	3.2	37.4	77.3	125.6								
100	MODELED RELEASE (CFS)	0.2	0.9	3.2	18.3	64.1	123.3								
100 FS) (OP)	STORED VOLUME (AC-FT)	13.0	17.0	21.9	22.2	22.6	23.7								
0.3	PND-E7														
3.5	STORM EVENT (YR)	2	5	10	25	50	100								
23.0 8.2	PEAK INFLOW (CFS)	46.5	75.4	121.2	285.2	402.4	548.0								
8.2	MODELED RELEASE (CFS)	23.1	35.3	71.5	108.3	152.1	196.4								
	STORED VOLUME (AC-FT)	1.0	1.8	4.6	10.5	17.9	28.0								
•															
	2019 0	TEDI I	NIC D	${\Lambda}$ NICH	MDD										
NT, SUITE 110	2010 3	2018 STERLING RANCH MDDP													
S, CO 80903		1) (D D	01 001	0 00	NIDIT!	<u> </u>									
5, 00 00/00	I DEVELOPED H	$TYDR^{I}$	OLOGI	C	וועמי	UNS	MAP								

ALLOWABLE RELEASE (CFS) | 0.0 | 0.2 | 0.4 | 4.2 MODELED RELEASE (CFS) 0.0 0.2 0.5 2.2

S) 0.3 4.4 8.8 23.0 MODELED RELEASE (CFS) | 0.9 | 2.8 | 8.7 | 21.9 | 32.2 | 43.6 STORED VOLUME (AC-FT) 4.2 4.3 4.7 5.4 6.2 6.9

DELED RELEASE (CFS) | 1.0 | 6.8 | 25.7 | 56.0 | 79.8 | STORED VOLUME (AC-FT) 7.0 7.2 7.7 8.9 10.1

TORM EVENT (YR)

FSD-E5

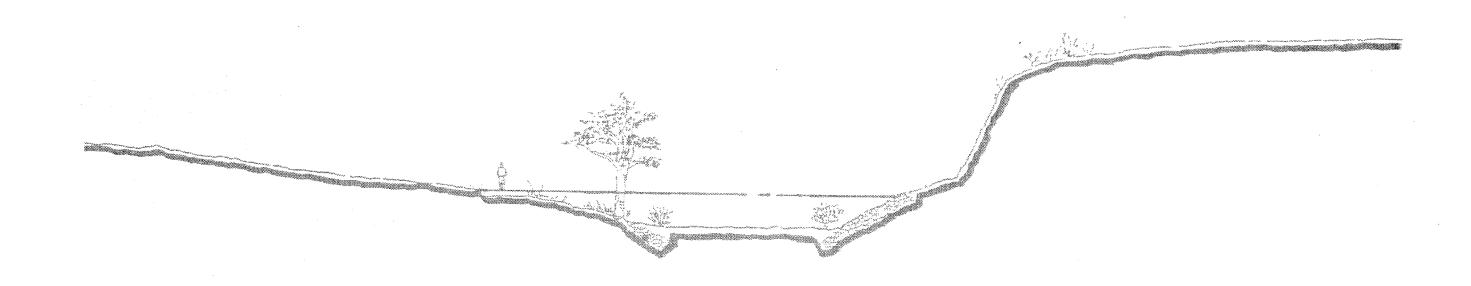
DEVELOTED THENCEOUS CONDITIONS WAT

PROJECT NO. 09-002 | FILE: \dwg\Eng Exhibits\2018-MDDP-PROPCOND.dwg DATE: 10-21-2018 DESIGNED BY: JD DRAWN BY: HORIZ: 1"=2400' DM2 CHECKED BY: VAS VERT: 1"=2400"

SAND CREEK DRAINAGE BASIN PLANNING STUDY

PRELIMINARY DESIGN REPORT

CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO

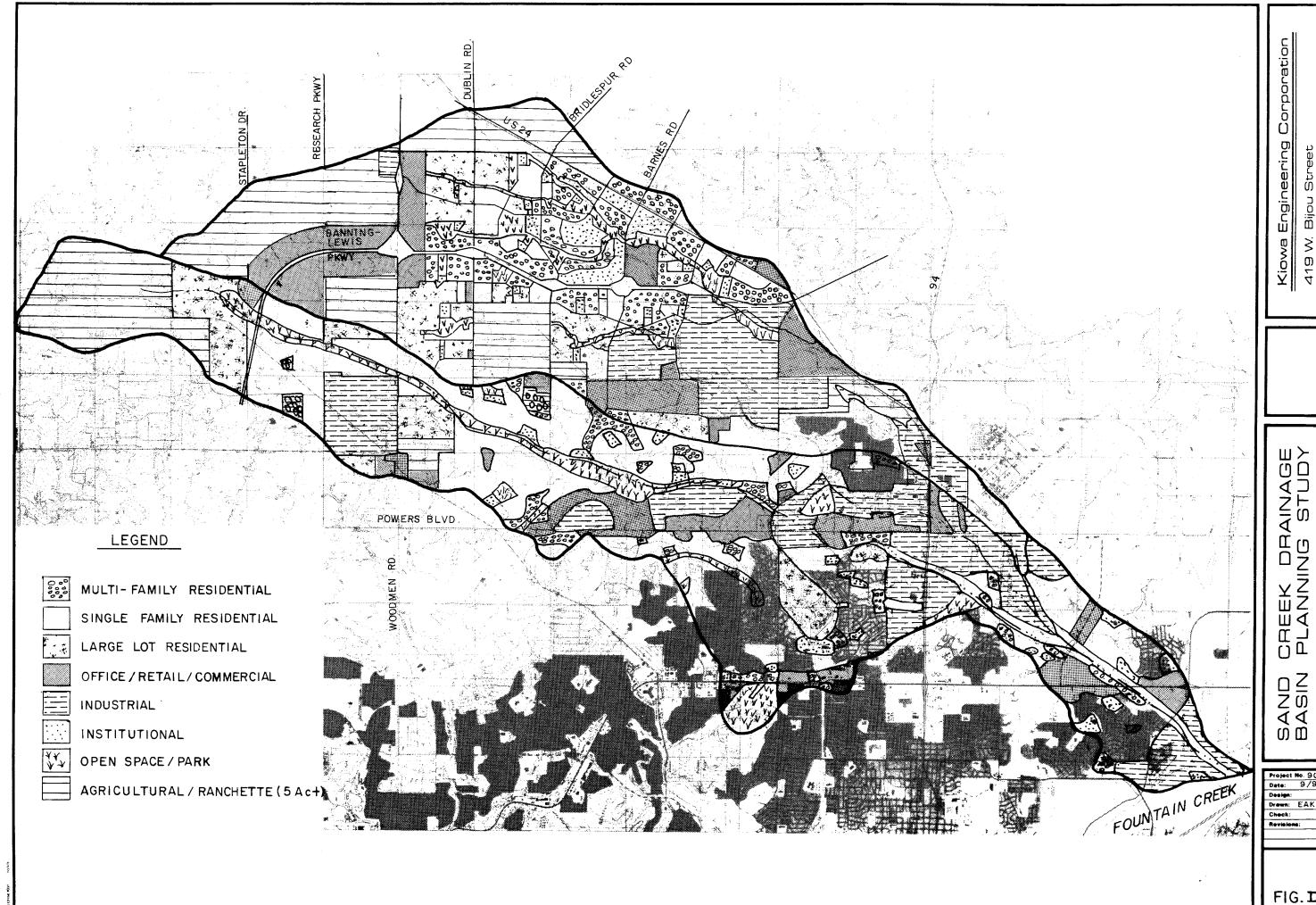


PREPARED FOR:

City of Colorado Springs
Department of Comprehensive Planning, Development and Finance
Engineering Division
30 S. Nevada
Colorado Springs, Colorado 80903

PREPARED BY:

Kiowa Engineering Corporation 1011 North Weber Colorado Springs, CO 80903



Bijou Street do Springs, Co 419 W. Bijou S Colorado Sprin 80905-1308

PROPOSED SAND BASIN

FIG. **II-3**

Table III-1. Percent Impervious Values.

Land Use Classification	Percent Impervious	Land Use Density
Multi-Family Residential	65-80	10-24 DU/AC
Single-Family Residential	45-65	6-10 DU/AC
Low Density Residential	30-45	1-6 DU/AC
Large Lot Residential/ Agricultural	5-20	1 DU/AC
Office/Commercial	80-90	
Industrial	85-95	
Institutional	50-75	
Dedicated Open Space/Park	5-10	
Rangeland - Poor to Good Condition	5- 20	

NOTE: The above data was used in the preparation of the hydrologic analysis for the Sand Creek Drainage Basin Planning Study. These data are not intended to reflect future land use planning within the City or the County.

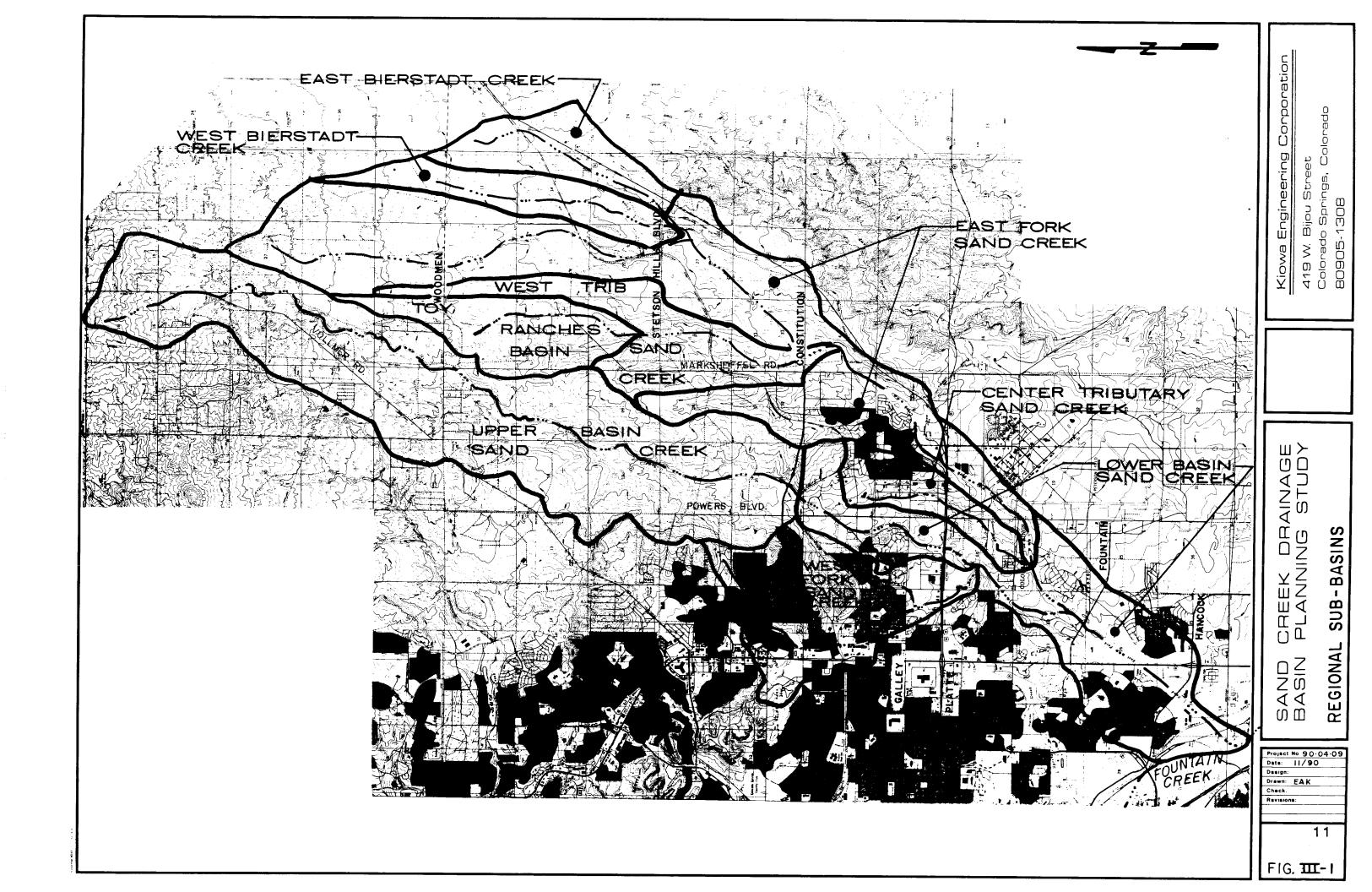
Table III-2:

Summary of Peak Discharges 24-hour Duration Storm, AMC-II Baseline Hydrologic Conditions

Design Point	Location	Area s.m.	100-year (cfs) Existing	Future	10-year (cfs) Existing	Future
	SAND CREEK (1)					
1	@ Fountain Creek	54.1	16900	25800	7470	11800
12	Hancock Blvd.	53.1	16100	25000	7250	11600
19	Fountain Blvd.	50.7	13600	22100	6230	10800
27	West Fork Sand Creek	23.0	11300	18900	5920	8790
99	C.R.I. & P. RR	16.0	5820	14530	2360	7400
20	North Carefree	13.5	4030	10260	1520	4810
37	Stetson Hills Blvd.	10.0	3230	6690	840	3060
60	Woodmen Road	5.4	2630	3300	760	950
75	Black Forest Road	1.4	1000	1030	320	350
	WEST FORK SAND CRE	EK				
27	@ Sand Creek	5.0	6840	6840	3200	3200
52	U. S. 24	4.8	6860	6860	3230	3230
59	Constitution Ave.	2.1	3450	3450	1680	1680
69	South Carefree	1.0	1630	1630	810	810
	CENTER TRIBUTARY S.	AND CRE	EK			
42	Airport Road	1.6	1530	2010	650	1200
43	Powers Blvd.	1.3	1300	1710	590	980
44	U. S. 24	1.1	1200	1680	580	960
45	Galley Road	0.8	1180	1340	530	650
	EAST FORK SAND CREA	EK				
1	@ Center Tributary	24.3	3970	15600	700	6530
9	@ East Fork Sub. Tributary	19.8	3730	13990	650	6050
29	@ W. Bierstadt Creek	10.6	2080	7460	400	3330
40	@ Tamlin Road	4.6	950	3570	210	1820
52	@ Woodmen Road	1.7	460	2120	80	1210
	EAST FORK SUB-TRIBU	TARY SA	ND CREEK			
11	@ Constitution Avenue	5.9	1330	4100	240	1630
15	@ Chicago & Rock Island RR	5.2	1250	3540	230	1370
26	@ Confluence w/Toy Ranch	1.0	220	820	50 50	370
47	@ Proposed Dublin Blvd.	0.4	100	300	20	140
	WEST BIERSTADT CREI	EK				
31	@ Confluence w/ East Fork	1.8	480	1590	80	600
39	@ Tamlin Road	0,8	270	680	50	290
54	@ Woodmen Road	0.5	230	420	55	150
	EAST BIERSTADT CREE	EK				
32	@ Conf. w/W Bierstadt	2.4	520	1520	90	580
38	@ Chicago & Rock Island RR	0.4	120	350	15	130

⁽¹⁾ Future baseline condition discharges for Sand Creek compiled with the assumption that the discharges from the East Fork Sand Creek basin are maintained at existing rates as shown on this Table.

10



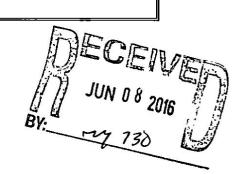


FINAL DRAINAGE REPORT

BARBARICK SUBDIVISION, PORTIONS OF LOTS 1, 2 and LOTS 3 & 4 El Paso County, Colorado

Sand Creek Drainage Basin

Prepared for: El Paso County Development Services Engineering Division



On Behalf of:
Wykota Construction
430 Beacon Light Road, Suite 130
Monument, CO 80132

Prepared by:

2435 Research Parkway, Suite 300 Colorado Springs, CO 80920 (719) 575-0100 Fax (719) 572-0208

June 6, 2016

15.789.001

STERLING RANCH FILING NO. 1 PRELIMINARY DRAINAGE REPORT

(CDOT Type R Inlet Calculations - Sump Condition)

Urban Local Roadway-50' ROW-30' Pavement-6" Vertical Curb Maximum allowable depth for MINOR (0.43') & MAJOR (0.66') storm

iniet Length	Storm	Depth	Eqn. 7-31	Eqn. 7-32	Eqn. 7-29
			Qw=CwNwLeD^3/2	Qo=CoNo(LeHc)(2g(D-0.5Hc))^1/2	Qm=Cm(QwQo)^1/2
5	Q5	0.43	5.1	5.7	5.0
5	Q100	0.66	9.7	8.6	8.5
G	Q5	0.43	6.1	8.8	6.0
8	Q100	0.66	11.6	10.3	10.2
8	Q6	0.43	8.1	9.1	8,0
8	Q100	0.68	15,4	13.8	13.6
10	Q5	0.43	10.2	11.4	10.0
10	Q100	0.68	19.3	17.2	17.0
12	Q5	0.43	12.2	13.7	12.0
12	Q100	0.66	23.2	20.7	20,3
14	Qs	0.43	14.2	16.0	14.0
14	Q100	0.66	27.0	24.1	23.7
15	Q ₅	0.43	15.2	17.1	15.0
15	Q100	0.66	29.0	25.8	25.4
16	Q5	0.43	16.2	18.2	16.0
18	Q100	0.68	30.9	27.5	27.1

Table 7-7. Coefficients for various inlets in sumps								
inlet Type	Nw	Cw	140	<u> </u>	Cm			
CDOT Type 13 Grate	0.7	3.3	0.43	0.6	0.93			
Denver No. 16 Grate	0.73	3.6	0.31	0,6	0.9			
Curb Opening for Type								
13/No. 16 Combination	1	3.7	1	0.66	0.86			
CDOT Type R Curb								
Opening	1	3.6	1 1	0.67	0.93			

Woi	rksheet for	FSD Ou	tlet	Orifice Plate
Project Description				
Solve For	Diameter			
Input Data				
Discharge			45.90	11/5 (16.5 His + 29.4 Pec)
Headwater Elevation		÷	4.70	ft
Centroid Elevation			0.00	ft ·
Tailwater Elevation			0.00	ft .
Discharge Coefficient			0.60	
Results				
Diameter			2.37	ft
Headwater Height Above Centroid			4.70	ft
Tailwater Height Above Centroid			0.00	ft .

4.40 ft²

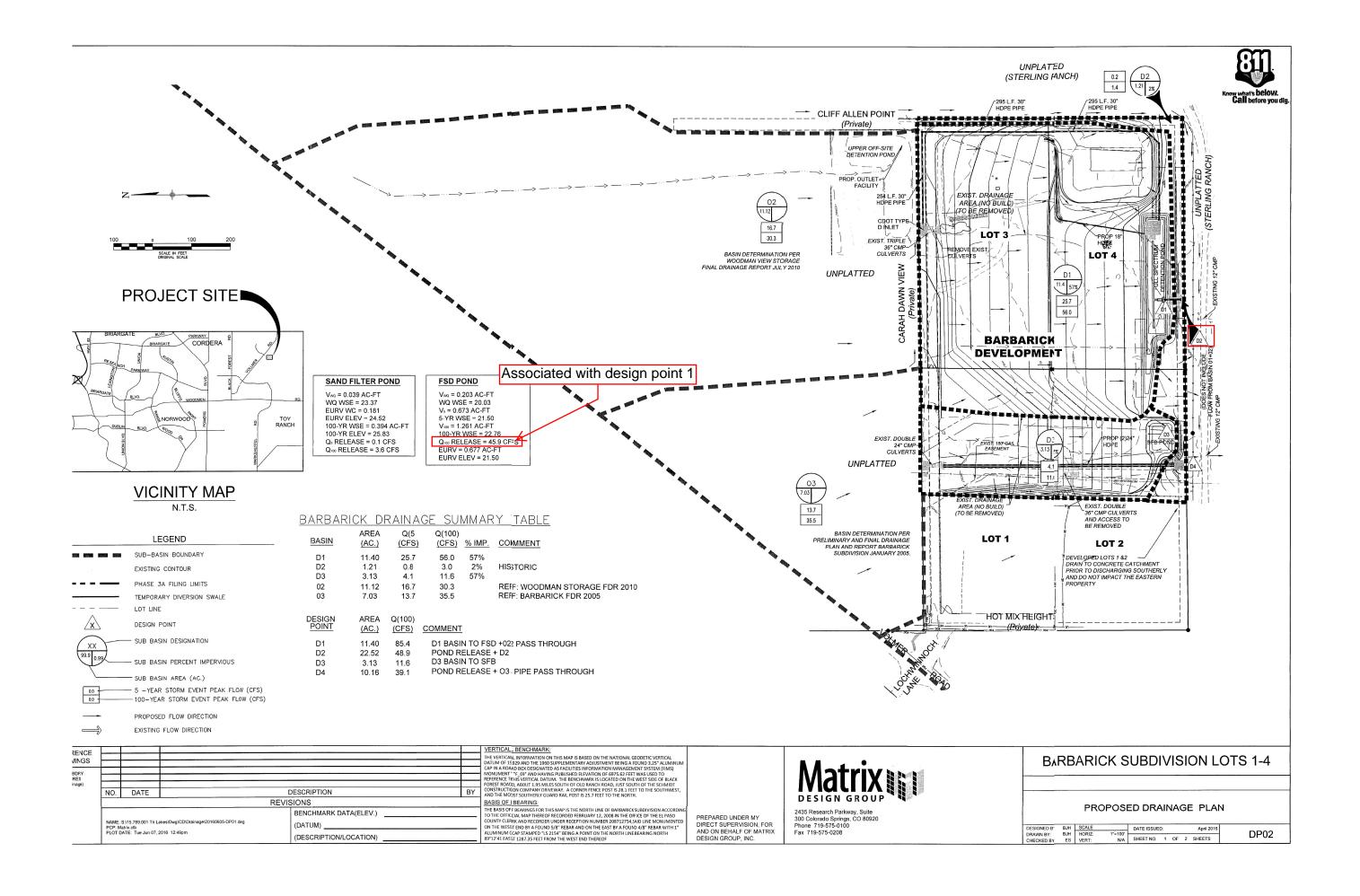
10.43 ft/s

Flow Area

Velocity

	Worksheet for	FSD Over	flow	v - Pass
Project Description				
olve For	Discharge			
nput Data				
leadwater Elevation		0.90	ft	
rest Elevation		0.00	ft	
ailwater Elevation		0.00	ft	
rest Surface Type	Gravel			
rest Breadth		12.00	ft	
rest Length		36.00	ft	
Results	*			
ischarge		86.22	ft³/s	(5510)+29.4 piec = 64.48
eadwater Height Above Crest		0.90	ft	,
ailwater Height Above Crest		0.00	ft	
Veir Coefficient		2.80	US	
ubmergence Factor		1.00		
djusted Weir Coefficient		2.80	US	
low Area		32.40	ft²	
elocity		2.66	ft/s	
Vetted Perimeter		37.80	ft	
op Width		36.00	ft	

Wo	ksheet for SFB (Overflo	w Developed
Project Description			
Solve For	Discharge		
Input Data			
Headwater Elevation		0.45	ft
Crest Elevation		0.00	ft
Tailwater Elevation		0.00	ft .
Crest Surface Type	Gravel		
Crest Breadth		6.00	ft
Crest Length		10.00	ft
Results			Res William Ade Color
Discharge		8.08	ft³/s
Headwater Height Above Crest		0.45	ft
Tailwater Height Above Crest		0.00	ft
Weir Coefficient		2.68	US
Submergence Factor		1.00	
Adjusted Weir Coefficient		2.68	US
Flow Area		4.50	€3
Velocity		1.80	ft/s
Wetted Perimeter		10.90	ft
Top Width		10.00	ft



FINAL DRAINAGE REPORT FOR STERLING RANCH FILING NO. 2

Prepared For: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

August 2021 Project No. 25188.01

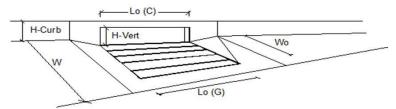
Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Sterling Ranch Filing No. 2 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.016 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 26.0 Gutter Width 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) \textbf{S}_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.007 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 19.3 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm 26.7 cfs Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

UD-Inlet_v4.05.xlsm, A8 5/15/2020, 9:24 AM

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input) CDOT Type R Curb Opening ▼	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.0	10.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	85	%

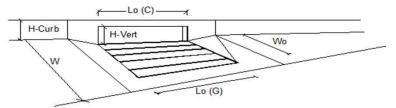
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Sterling Ranch Filing No. 2 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.016 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 26.0 Gutter Width 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) \textbf{S}_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.007 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 19.3 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm 26.9 cfs Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

UD-Inlet_v4.05.xlsm, A9 5/15/2020, 9:24 AM

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet CDOT Type R Curb Opening ▼	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.1	4.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	94	%

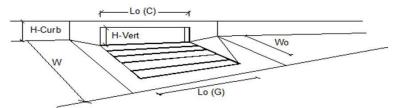
UD-Inlet_v4.05.xlsm, A9 5/15/2020, 9:24 AM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Sterling Ranch Filing No. 2 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) ft/ft 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.016 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 38.0 Gutter Width 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) \textbf{S}_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.012 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 33.0 38.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm d_{MAX} 6.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm 15.1 63.3 cfs Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

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INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet CDOT Type R Curb Opening ▼	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.9	13.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.6	6.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	93	69	%

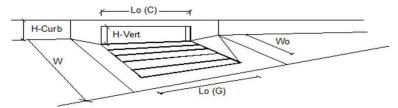
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Sterling Ranch Filling No. 2 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.016 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 26.0 Gutter Width 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) \textbf{S}_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.023 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 19.3 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Major Storm 36.4 Minor Storm 19.2 cfs Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

UD-Inlet_v4.05.xlsm, A15 5/15/2020, 9:24 AM

INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)	_	MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.4	10.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	88	%

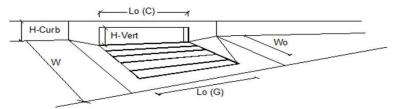
UD-Inlet_v4.05.xlsm, A15 5/15/2020, 9:24 AM

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Sterling Ranch Filing No. 2 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.016 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 26.0 Gutter Width 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) \textbf{S}_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.023 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 19.3 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Major Storm 36.4 Minor Storm 19.2 cfs Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

UD-Inlet_v4.05.xlsm, A16 5/15/2020, 9:24 AM

INLET ON A CONTINUOUS GRADE

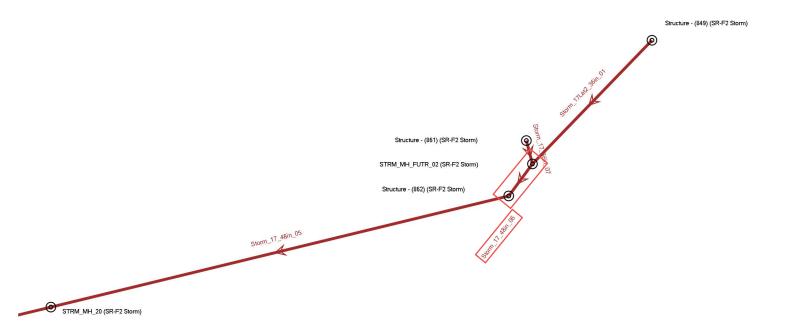
Version 4.05 Released March 2017



Design Information (Input)	_	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.3	7.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	2.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	97	73	%

UD-Inlet_v4.05.xlsm, A16 5/15/2020, 9:24 AM

Sterling Ranch 5yr



Scenario: 5-YEAR

Current Time Step: 0.000 h FlexTable: Conduit Table

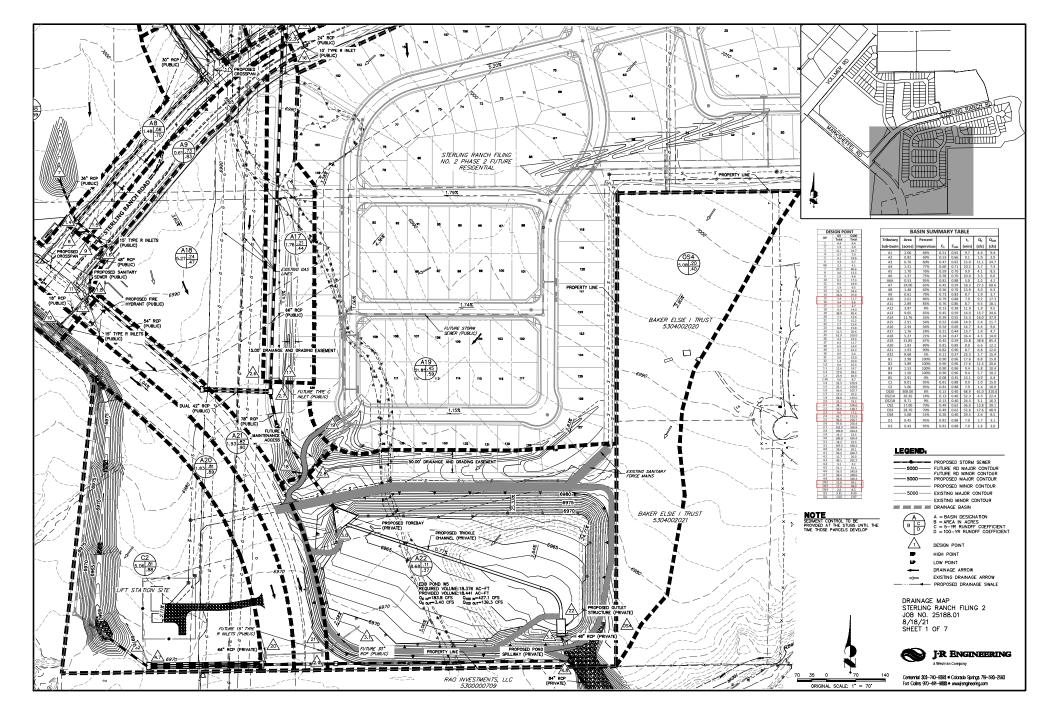
			Length	Olema			Capacity	Hydraulic	Hydraulic
Labal	Flow	Diameter	(User	Slope	Manning's	Velocity	(Full	Grade	Grade
Label	(cfs)	(in)	Defined)	(Calculated)	n	(ft/s) ´	Flow)	Line (ln)	Line
	, ,	` ′	(ft)	(ft/ft)			(cfs)	(ft)	(Out) (ft)
Storm 21 48in 01	55.10	48.0	57.3	-0.030	0.013	15.91	248.76	6,984,23	6,981.75
Storm 21 48in 02	52.50	48.0	25.8	-0.030	0.013	15.69	248.66	6,984.95	6,984.69
Storm 16 48in 02	68.80	48.0	348.6	-0.024	0.013	15.49	220,31	6,979.03	6,972.39
Storm_17_48in_01	63.70	48.0	15.6	-0.020	0.013	14.28	202.74	6,989.18	6,988.44
Storm_17_48in_05	56.90	48.0	292.3	-0.020	0.013	13.87	203.11	7,000.43	6,994.63
Storm_16_48in_03	56.40	48.0	50.4	-0.020	0.013	13.85	203.42	6,980.18	6,979.56
Storm 16 48in 04	56.40	48.0	42.5	-0.020	0.013	13.83	203.12	6,981.03	6,980.64
Storm_17_48in_06	56.90	48.0	22.6	-0.020	0.013	13.82	202.28	7,000.88	7,000.89
Storm_14_66in_05	96.60	66.0	354.4	-0.014	0.013	13.79	397.24	6,984.12	6,978.30 6,981.49
Storm_16_48in_05 Storm 19 Lat 2 18in 01	55.10 12.60	48.0 18.0	26.8 76.7	-0.020 -0.049	0.013 0.013	13.74 13.39	203.11 23.16	6,981.54 7,006.61	7,002.92
Storm 14 66in 04	96.60	66.0	512.4	-0.049	0.013	13.02	366.67	6,976.96	6,972.10
Storm 17Lat2 36in 01	16.00	36.0	110.1	-0.040	0.013	12.71	133.20	7,005.28	7,001.34
Storm 19 30in 03	25.90	30.0	165.0	-0.024	0.013	12.37	64.17	6,992.63	6,988.66
Storm 18 18in 02	8.70	18.0	82.7	-0.050	0.013	12.29	23.47	6,985.92	6,983.18
Storm 17 48in 04	56.90	48.0	82.9	-0.014	0.013	12,29	172.06	6,994.40	6,993.44
Storm 17 48in 03	56.90	48.0	150.3	-0.014	0.013	12.28	171.79	6,993.21	6,991.28
Storm 17 48in 02	56.90	48.0	102.0	-0.014	0.013	12.19	170.08	6,991.05	6,989.03
Storm_19_24in_05	17.60	24.0	177.0	-0.030	0.013	12.14	39.18	7,002.55	6,996.67
Storm_14_48in_06	38.10	48.0	59.3	-0.017	0.013	11.72	187.87	6,989 . 32	6,987.79
Storm_14_84in_01	189.80	84.0	107.3	-0.005	0.013	11.25	453.09	6,970.13	6,969.23
Storm_14_72in_03	162.00	72.0	74.5	-0.005	0.013	10.99	306.40	6,971.03	6,971.00
CO-6	23.20	48.0	9.5	-0.021	0.013	10.94	208.41	6,989.62	6,989.67
Storm_14_72in_02	162.00	72.0	127.9	-0.005	0.013	10.80	299.58	6,970.64	6,970.48
Storm_23 54in_05	30.70	54.0	120.0	-0.015	0.013	10.39	240.88 240.88	6,957.68	6,955.40 6.971.61
Storm_23 54in_09 Storm 23 54in 08	30.70 30.70	54.0 54.0	402.5 567.0	-0.015 -0.015	0.013 0.013	10.39 10.39	240.88	6,978.16 6,969.87	6,960.87
Storm 23 54in 06	30.70	54.0	93.0	-0.015	0.013	10.39	240.76	6.959.07	6,957.97
Storm 19 18in 06	6.00	18.0	339.5	-0.040	0.013	10.23	20.95	7.016.00	7.002.92
Storm_17_36in_07	17.60	36.0	9.8	-0.020	0.013	10.21	94.31	7,001.15	7,001.34
Storm 23 54in 10	30.70	54.0	298.5	-0.014	0.013	10.14	232.69	6,982.73	6,978.06
Storm 23 54in 11	30.70	54.0	333.6	-0.014	0.013	10.14	232.65	6,993.98	6,988.82
Storm_23 54in_12	30.70	54.0	412.3	-0.014	0.013	10.14	232.63	7,002.09	6,995.83
Storm_15_18in_02-W	4.30	18.0	25.5	-0.049	0.013	10.08	23.36	6,973.60	6,972.01
Storm_14_36in_07	15.70	36.0	76.3	-0.020	0.013	9.89	94.31	6,991.27	6,989.33
Storm_18_18in_01	17.30	18.0	22.4	-0.059	0.013	9.79	25.59	6,982.43	6,981.79
Storm_19_Lat 1_ 18in_01	5.00	18.0	36.4	-0.030	0.013	8.78	18.18	6,993.84	6,993.02
Storm_19_Lat 2_18in_02	9.50	18.0	35.3	-0.015	0.013	7.97	12.86	7,007.49	7,007.05
Storm_19_36in_02	25.90	36.0	144.5	-0.006	0.013	7.26	51.15	6,987.99	6,987.48
Storm_19_36in_01	25.90	36.0 18.0	302.2	-0.006 -0.020	0.013 0.013	7.25	51.04 14.84	6,987.14 7,016.37	6,985.83
Storm_19_Lat 3_18in_01 Storm 15 42in 01-E	4.20 38.80	42.0	6.0 63.9	-0.020	0.013	7.22 7.09	65.41	6,971.94	7,016.40 6,971.67
Storm 23 54in 13	30.70	54.0	265.9	-0.005	0.013	6.98	138.03	7,010.66	7,009.20
Storm_21_42in_03	27,50	42.0	101.2	-0.005	0.013	6.92	71.15	6,985.78	6,985,83
Storm 23 54in 14	27.40	54.0	43.7	-0.005	0.013	6.70	136.36	7,011.10	7,011.18
Storm 22 30in 02	8.30	30.0	79.4	-0.009	0.013	6.22	38.24	7,016.69	7,016.15
Storm 23 three 42in 04	32.10	42.0	258.8	-0.008	0.013	6.19	264.00	6,954.49	6,952.34
STRM_29_02	1.60	18.0	79.6	-0.027	0.013	6.11	17.27	7,015.72	7,013.40
Storm_20_48in_01	3.40	48.0	57.9	-0.020	0.013	6.07	203.30	6,961.20	6,959.87
Storm_22_30in_01	16.00	30.0	113.0	-0.005	0.013	6.06	29.03	7,016.09	7,015.50
Storm_16_Lat_1_18in_01	2.10	18.0	13.2	-0.020	0.013	5.99	15.01	6,982.08	6,981.67
Storm_23_84in_02	35.50	84.0	27.0	-0.003	0.013	5.81	347.91	6,947.59	6,947.51
Storm_28 30in_01	8.40	30.0	90.0	-0.007	0.013	5.81	34.60	7,044.20	7,044.15
Storm_19_Lat 3_18in_02	1.90	18.0	29.3	-0.020	0.013	5.79	14.90	7,016.36	7,016.40
Storm_28 30in_01	18.40	30.0	35.4	-0.004	0.013	5.71	25.78	7,044.15	7,043.91
Storm_17_Lat_1_24in_01	9.60	24.0	8.8	-0.006	0.013	5.58	17.03	6,989.73	6,989.65
Storm_23_84in_01 STRM 29 01	35.50	84.0	200.4	-0.003	0.013	5.55 4.85	325.38	6,948.26	6,947.85
STRM 29 01 Storm 23 66in 03	3.30 32.10	18.0 66.0	66.2 167.7	-0.008 -0.002	0.013 0.013	4.85 4.77	9.40 139.63	7,013.34 6,951.31	7,012.73 6,951.02
Storm_23_66in_03 Storm 17 Lat 1 24in 02	32.10 4.30	24.0	53.4	-0.002	0.013	4.77	18.29	6.989.80	6,989.84
Storm 23 66in 02	32.10	66.0	549.0	-0.007	0.013	4.75	138.58	6,950.94	6,949.73
Storm 26 24in 01	2.10	24.0	80.7	-0.002	0.013	4.73	22.68	7,017.31	7,016.41
Storm 19 24in 04	0.50	24.0	144.7	-0.030	0.013	4.31	39.18	6,995.97	6,993.02
Storm 21 Lat 1 18in 01	3.00	18.0	19.4	-0.005	0.013	3.87	7.16	6,985.26	6,985.15
Storm_16_42in_01	68.80	42.0	158.3	-0.002	0.013	3.58	90.47	6,972.29	6,972.10

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Scenario: 100-YEAR Current Time Step: 0.000 h FlexTable: Conduit Table

Label Flow Diameter (rish) Diameter (rish) Clear Cle										
Label				Lenath				Canacity	Hydraulic	Hydraulic
Library Cefs		Flow	Diameter			Manning's	Velocity			
Storm 17,48in 01	Label					_				
Storm 17 48m 01 151,90 48.0 15.6 -0.020 -0.013 17.70 -0.0274 6.590.38 6.589.68 Storm 20 48m 05 139,30 48.0 57.9 -0.020 -0.013 17.42 203,30 6.594.17 6.590.18 Storm 23 54m 05 139,70 48.0 57.9 -0.020 -0.013 17.42 203,30 6.594.17 6.590.18 Storm 23 54m 05 139,70 48.0 57.9 -0.020 -0.013 17.42 203,30 6.594.17 6.599.18 Storm 23 54m 05 139,70 48.0 33.5 -0.014 -0.013 16.67 232,53 6.596.80 6.599.18 Storm 25 54m 04 139,70 48.0 410,13 4		(6,5)	("'')	,	(ft/ft)		(103)			
Storm 1-6 Storm 1-6 Storm 2-6 Stor	47 48'- 04	454.00	400		0.000	0.040	47.70	, ,	. ,	
Storm 2-6 sin 01 39,30 48,0 57,9 -0,020 -0,013 17,42 20,30 6,984,77 6,982,31 Storm 2-3 sin 15 233,40 54,0 333,6 -0,014 -0,013 16,67 232,85 6,986,66 6,986,66 58,000 58,										
Storm 17.48ln OS										
Storm 3 Alm 1										
Storm 73.64m 72 233.40 54.0 412.3 -0.014 0.013 16.67 232.63 7.004.71 6.996.49 Storm 71.42, 36in_0 1 33.70 36.0 110.1 -0.040 0.013 16.24 133.20 17.006.00 7.006.00 7.006.00 Storm 77.48in_0 3 138.70 48.0 85.3 -0.017 0.013 15.23 172.06 6.996.81 6.996.89 Storm 77.48in_0 3 138.70 48.0 85.3 -0.014 0.013 15.21 171.79 6.996.44 6.992.83 Storm 77.48in_0 3 138.70 48.0 85.3 -0.014 0.013 15.21 171.79 6.996.44 6.992.83 Storm 78.48in_0 2 23.40 46.0 6.003 -0.024 0.013 16.21 171.79 6.996.44 6.992.84 Storm 79.48in_0 2 23.40 46.0 6.005 -0.004 0.013 14.22 12.16 7.006.74 7.003.64 Storm 23.44in_0 9 233.40 54.0 206.5 -0.014 0.013 14.68 24.088 6.981.49 6.975.82 Storm 23.44in_0 8 233.40 54.0 206.5 -0.014 0.013 14.68 24.088 6.981.49 6.975.82 Storm 23.44in_0 8 233.40 54.0 266.5 -0.014 0.013 14.68 24.088 6.981.49 6.975.82 Storm 23.44in_0 8 233.40 54.0 567.0 -0.015 0.013 14.68 24.088 6.981.49 6.975.82 Storm 23.54in_0 8 233.40 54.0 250.0 -0.015 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 233.40 54.0 250.0 -0.015 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 233.40 54.0 250.0 -0.015 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 233.40 54.0 250.0 -0.015 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 233.40 54.0 250.0 -0.015 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 233.40 54.0 250.0 -0.015 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 23.00 -0.005 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 23.00 -0.005 0.013 14.68 24.088 6.962.34 6.960.84 Storm 23.54in_0 8 23.00 -0.005 0.013 14.68 24.088 6.960.84 6.960.84 6.960										
Storm T, Halp 36Hn 01 37,90 36.0 110.1 -0.040 0.013 16.24 133.20 7,006.00 7,003.91 Storm 17,48hn 04 138,70 48.0 85.3 -0.017 0.013 15.23 172.06 6,996.06 6,996.80 5,996.8										
Storm 14 48										
Simm_17_48ln_04										
Simm 7,48h 03 138,70 48,0 150,3 0.014 0.013 15,21 208,44 6,992,84 6,992,84 5,991,40 Simm 7,48h 0.9 17,760 48,0 102,0 0.014 0.013 15,00 170,06 6,992,28 6,991,40 Simm 7,48h 0.9 17,00 18,00 17,00 18,00 17,00 18,00 17,00 18,00										
COLOR T. 4810 D2 138,70 48.0 9.5 -0.021 0.013 15,20 208,41 6,991,39 6,991,01 Storm 19_Lat Z_18n 01 19,70 18.0 76.7 -0.049 0.013 14,72 23,16 7,002,74 7,003,66 5,992,28 5,991,01 5										
Storm 17_48in_02										
Storm 19_Lat Z_18h										
Storm 23 64n 70										
Storm 23 54in 08										
Storm 23 54in 08 233.40 54.0 567.0 -0.015 0.013 14.68 240.76 6,974.99 6,967.00										
Storm 23 54in 05										
Storm 23 54in 16 233,40 54.0 265.9 -0.005 -0.013 14.68 138.03 7,011.69 7,011.96 Storm 18 18in 01 25.30 18.0 22.4 -0.059 -0.013 14.22 25.59 6,984.40 6,983.10 Storm 19 24in 05 30.00 24.0 177.0 -0.005 -0.013 13.74 39.18 7,002.90 6,997.04 Storm 19 24in 05 30.00 24.0 177.0 -0.030 -0.013 13.74 39.18 7,002.90 6,997.04 Storm 19 24in 05 30.00 24.0 147.7 -0.030 -0.013 13.74 39.18 7,002.90 6,997.04 Storm 14.72in 03 336.80 77.0 74.5 -0.005 -0.013 12.31 94.31 6,991.91 6,991.40 Storm 14.72in 03 336.80 72.0 74.5 -0.005 -0.013 11.23 94.31 6,991.91 6,991.40 Storm 14.72in 03 336.80 72.0 74.5 -0.005 -0.013 11.91 299.58 6,976.00 6,975.27 Storm 19 18in 06 138.70 48.0 22.6 -0.020 -0.013 11.91 299.58 6,976.00 6,975.27 Storm 17 48in 06 138.70 48.0 22.6 -0.020 -0.013 11.04 202.28 7,002.97 7,002.76 Storm 14 68in 04 250.70 66.0 512.4 -0.012 -0.013 10.55 366.67 6,981.61 6,978.75 Storm 23 68in 03 243.40 66.0 512.4 -0.012 -0.013 10.55 366.67 6,981.61 6,978.75 Storm 23 68in 03 243.40 66.0 549.0 -0.002 -0.013 10.24 139.63 6,956.28 6,957.40 Storm 16 48in 02 125.00 48.0 348.6 -0.024 -0.013 10.24 139.63 6,958.28 6,957.40 Storm 16 48in 02 125.00 48.0 348.6 -0.024 -0.013 9.95 220.31 6,982.33 6,979.89 Storm 15 48in 02 125.00 48.0 348.6 -0.024 -0.013 9.95 220.31 6,982.33 6,975.85 Storm 16 48in 02 125.00 48.0 346.6 -0.024 -0.013 9.95 220.31 6,982.33 6,976.89 Storm 15 48in 02 125.00 48.0 346.6 -0.024 -0.013 9.95 220.31 6,982.33 6,976.89 Storm 16 48in 03 48.0 42.0 63.9 -0.004 -0.013 8.87 -0.044 -0.013 -0.004 -0.003 -0.013 -0.004 -0.003 -0.013 -0.004 -0.003 -0.013 -0.004 -0.003 -0.013 -0.004 -0.005 -0.004 -0.005 -0.005 -0.005 -0.005 -0.005 -										
Storm 23 54in 06										
Storm 18 18in O1										
Storm 12 3 54in_14										
Storm 19 24 10										
Storm_19_24in_04 30.00 24.0 144.7 -0.030 0.013 13.74 39.18 6.997.59 6.994.14										
Storm_14_36in_07										
Storm_14_72in_02 336,80 72,0 74,5 -0,005 0,013 11,91 295,86 6,976,66 6,975,62 5,007 1,91 295,86 6,976,86 6,976,86 5,007 6,976,63 5,007 1,91 295,86 6,976,86 6,976,86 5,007 6,976,83 5,004 6,075,27 7,003,86 5,004 6,075,27 7,003,86 5,004 6,075,27 7,003,86 5,004 7,002,76 7,003,86 7,002,76 7,003,86 7,002,76 7,003,86 7,002,76 7,003,86 7,002,76 7,003,86 7,002,76 7,										
Storm 14 72ln 02 336.80 72.0 127.9 -0.005 0.013 11.91 299.88 6.976.08 6.975.27 1.95										
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Storm_19_30in_O3	Storm_23_84in_02									
Storm_16_48in_03	Storm_23_84in_01									6,952.64
Storm_16_48in_03										
Storm_16_48in_04	Storm_15_42in_01-E	85.40					8.88		6,975.73	6,975.27
Storm 23 three 42in 04	Storm_16_48in_03		48.0			0.013	8.57			6,983.10
Storm 21 48in 02							8.57			6,983.95
Storm_19_Lat \(\bar{2}\) 18in \(02 \) 14.70 18.0 35.3 -0.015 0.013 8.32 12.86 7,008.40 7,007.71 Storm_21_48in_01 103.90 48.0 57.3 -0.030 0.013 8.27 248.76 6,986.27 6,985.97 Storm_16_48in_05 103.90 48.0 26.8 -0.020 0.013 8.27 203.11 6,984.90 6,984.76 Storm_15_18in_02 14.00 18.0 25.5 -0.049 0.013 7.92 23.36 6,975.72 6,975.27 Storm_18_18in_02 12.80 18.0 82.7 -0.050 0.013 7.24 23.47 6,987.22 6,985.99 Storm_19_Lat \(\bar{3}\) 18in_02 3.80 18.0 29.3 -0.020 0.013 7.05 14.90 7,016.96 7,016.97 Storm_17_36in_07 48.90 36.0 9.8 -0.020 0.013 6.63 9.431 7,003.97 7,03.91 STRM_29_01 11.80 18.0 66.2 -0.008 0.013 6.68 9.40 7,019.74 7,018.90 Storm_19_36in_02 46.90 36.0 144.5 -0.006 0.013 6.63 51.15 6,990.59 6,988.84 Storm_19_36in_01 46.90 36.0 144.5 -0.006 0.013 6.63 51.15 6,990.59 6,988.84 Storm_19_36in_01 125.00 42.0 158.3 -0.002 0.013 6.63 51.04 6,989.53 6,988.04 Storm_28_30in_01 12.20 30.0 90.0 -0.007 0.013 6.44 34.60 7,044.41 7,044.53 Storm_21_42in_03 60.60 42.0 101.2 -0.005 0.013 6.30 71.15 6,988.41 6,986.80 Storm_21_42in_03 60.60 42.0 101.2 -0.005 0.013 6.30 71.15 6,988.41 6,986.80 Storm_28_30in_01 26.10 30.0 35.4 -0.004 0.013 5.93 29.03 7,022.08 7,021.51 Storm_19_Lat_1_18in_01 17.20 24.0 8.8 -0.006 0.013 5.93 29.03 7,022.08 7,021.51 Storm_19_Lat_3_18in_01 6.60 18.0 6.0 -0.020 0.013 2.79 38.24 7,022.22 7,022.13 Storm_16_Lat_1_18in_01 4.50 24.0 80.7 -0.010 0.013 2.55 15.01 6,984.79 6,991.23 6,991.23 5,991.23 18.29 6,991.23	Storm 23 three 42in_ 04				-0.008	0.013	8.43		6,960.38	6,958.69
Storm_21_48in_01										
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FINAL DRAINAGE REPORT FOR STERLING RANCH FILING NO. 4

Prepared For:

SR Land, LLC 20 Boulder Crescent, Suite 200 Colorado Springs, CO 80903 (719) 491-3024

> August 14, 2023 Project No. 25188.11

Prepared By:
JR Engineering, LLC
5475 Tech Center Drive, Suite 235
Colorado Springs, CO 80919
719-593-2593

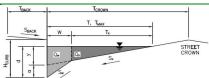
PCD Filing No.: SF-22-030



ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

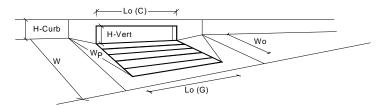
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing 4
Inlet ID: Inlet DP5



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) T_{BACK} 8.0 ft/ft $\mathsf{S}_{\mathsf{BACK}}$ 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} 0.016 Height of Curb at Gutter Flow Line $\mathsf{H}_{\mathsf{CURB}}$ 6.00 inches Distance from Curb Face to Street Crown $\mathsf{T}_{\mathsf{CROWN}}$ 17.0 Gutter Width W 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm $d_{\text{MAX}} \\$ inches 6.0 7.0 Check boxes are not applicable in SUMP conditions Major Storm SUMP MINOR STORM Allowable Capacity is not applicable to Sump Condition Minor Storm MAJOR STORM Allowable Capacity is not applicable to Sump Condition SUMP

INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.02 (August 2022)



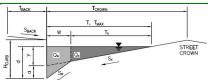
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	-
Type of Inlet	Type =	CDOT Type R		4
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	11	_11	<u>.</u> .
Water Depth at Flowline (outside of local depression)	Ponding Depth =	7.1	7.4	inches
<u>Grate Information</u>		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
<u>Curb Opening Information</u>	-	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.43	0.45	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.85	0.86	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	1
	· ·· combination L	120.2		-
	_	MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	12.2	13.5	cfs
WARNING: Inlet Capacity < Q Peak for Major Storm	Q _{PEAK REQUIRED} =	12.0	25.9	cfs

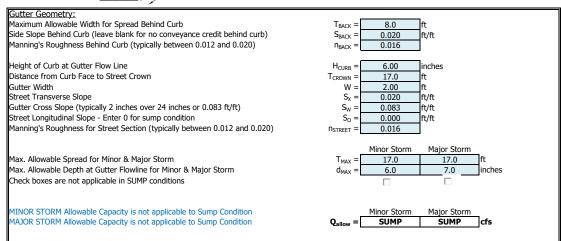
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

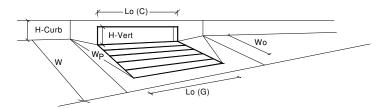
Project: Sterling Ranch Filing 4

Inlet ID: Inlet DP6.1





INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.02 (August 2022)



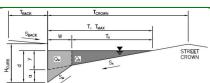
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	8.0	inches
Grate Information	, <u>.</u>	MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.50	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
		MINOR	MAJOR	1
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.9	16.2	cfs
WARNING: Inlet Capacity < Q Peak for Major Storm	Q PEAK REQUIRED =	3.9	19.3	cfs

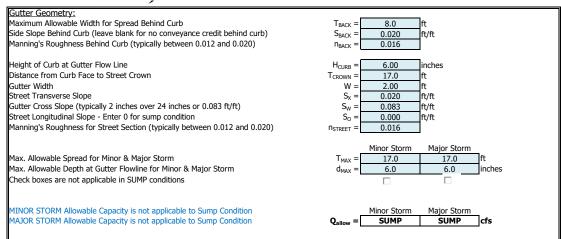
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

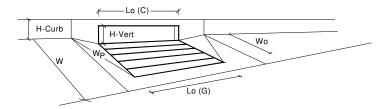
Project: Sterling Ranch Filing 4

Inlet ID: Inlet DP6.2





INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.02 (August 2022)

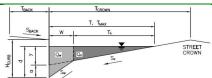


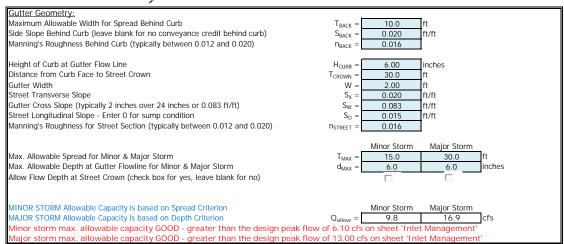
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.50	ft
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	6.9	16.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	2.0	7.3	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

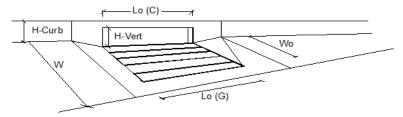
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing 4
Inlet ID: Ex Inlet DP8





INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)

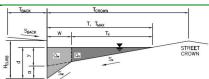


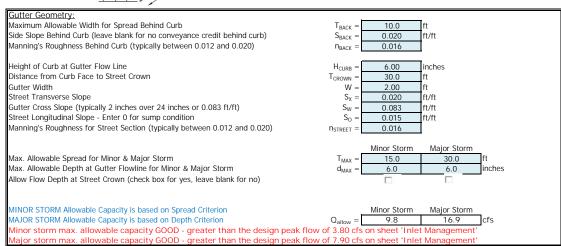
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	$a_{LOCAL} =$	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.1	10.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	2.2	cfs
Capture Percentage = Q _a /Q _o	C% =	100	83	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

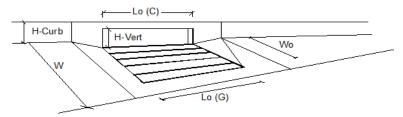
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing 4
Inlet ID: Ex Inlet DP9





INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)

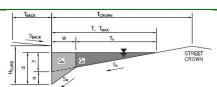


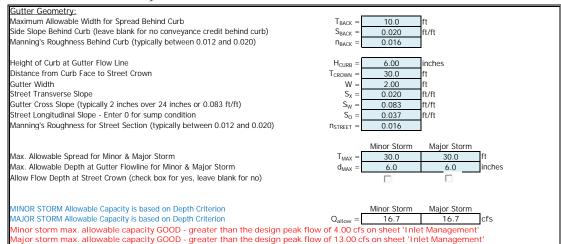
Design Information (Input) CDOT Type R Curb Opening	Tuna	MINOR	MAJOR Curb Opening	1
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.8	7.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.2	cfs
Capture Percentage = Q _a /Q _o	C% =	100	98	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

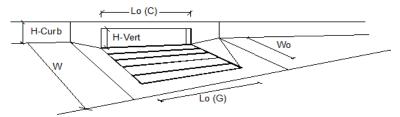
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Sterling Ranch Filing 4
Inlet ID: Inlet DP2e





INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.02 (August 2022)



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	$a_{LOCAL} =$	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_f(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.0	10.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	2.1	cfs
Capture Percentage = Q _a /Q _o	C% =	100	84	%

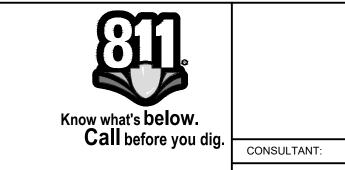
						Design Pa	oint Summ	ary Tahlo		
Design	Up	strea	n			Inlet	Jiiit Juliiiii	ary rable	Downstream	Receiving
Design Point	Area (Acres)			Subbasins Included	Name	Туре	Size (ft)	Outlet Pipe Size/Type	Design Point	Emergency Overflow
DP1	4.35	5.0	14.4	A2	A2	D 10 R	12	24" RCP/HP	DP6	DP6 / Street Overtop
DP2	5.15	5.8	16.5	A1	A1	D 10 R	10	24" RCP/HP	DP3	DP3 / Street Overtop
DP3	5.53	6.2	17.7	DP2,A4	A4	D 10 R	6	18" RCP/HP	DP6	DP6 / C & G, Street Overtop
DP4	4.06	3.4	11.4	A6	D4	D 10 R	8	36" RCP/HP	DP5	DP5 / Street Overtop
DP5	5.23	4.8	15.2	DP5, A7	D5	MH	6	36" RCP/HP	DP6	DP1 / C & G
DP6	16.22	16.7	49.3	DP1,DP3,DP5,A9	D6	D 10 R	6	42" RCP/HP	DP POND	DP POND / Overtop Curb, Swale
DP7	2.00	2.8	8.0	A5	A5	D 10 R	6	24" RCP/HP	DP POND	DP POND / Overtop Curb, Swale
DP Pond	21.57	19.9	61.2	A1,A2,A4,A5, A6,A7,A9,	A9	Detention Outlet	Overflow	ate: 1.02 Sq. In. (Stage 0', .9' & 1.06') Weir/Grate: L=2', W=2' w/ slope: 0 Weir/Grate: (Stage: 4' to 6')	-	-
Detention Discharge	-	0.4	3.7	A10	Að	Structure		Outlet Pipe: 18" RCP/HP (10.5" Orifice	Sand Creek	Sand Creek
DP8	1.95	5.9	13.2		A12	D 10 R	16	24" RCP/HP	DP9	DP10 / C & G
DP9	1.87	5.8	13.0	DP8,RP-7D,A13	A13	D 10 R	16	24" RCP/HP	DP11	DP11 / C & G
DP10	0.71	2.7	6.0	A14	A14	D 10 R	16	18" RCP/HP	DP11	DP12 / C & G
DP11	0.71	2.6	5.9	DP9,DP10,A15	A15	D 10 R	16	30" RCP/HP	DP13	DP13 / C & G
DP12	1.90	4.8	11.6	A16	A16	D 10 R	20	24" RCP/HP	DP13	Sand Creek Bridge
DP13	3.55	8.6	20.3		A17	D 10 R	16	42" RCP/HP	WQ POND/ Sand Creek	Sand Creek Bridge

Q5= 1.2 Q100=4.3

ASPEN MEADOWS

COLORADO SPRINGS, CO

PROPOSED CONDITIONS MAP



CIVIL ENGINEER/ LANDSCAPE ARCHITECT: **Matrix**

Excellence by Design

Fax (719) 575-0208

2435 Research Parkway, Suite 300 Colorado Springs, CO 80920 Contact: Greg Shaner, Civil Engineer Contact: Jason Alwine, Landscape Architect Phone (719) 575-0100

ASPEN MEADOWS FILING NO.1 PUD DEVELOPMENT PLAN CITY OF COLORADO SPRINGS

JANUARY 2020

COLA, LLC 555 MIDDLE PARKWAY COLORADO SPRINGS, CO 80921 (719)459-0807

DEVELOPER:

(719)459-0807

COLA, LLC 555 MIDDLE PARKWAY COLORADO SPRINGS, CO 80921

CITY PLANNING FILE NO: AR PUD 19-00053 ISSUE: MARCH, 2020

MAP

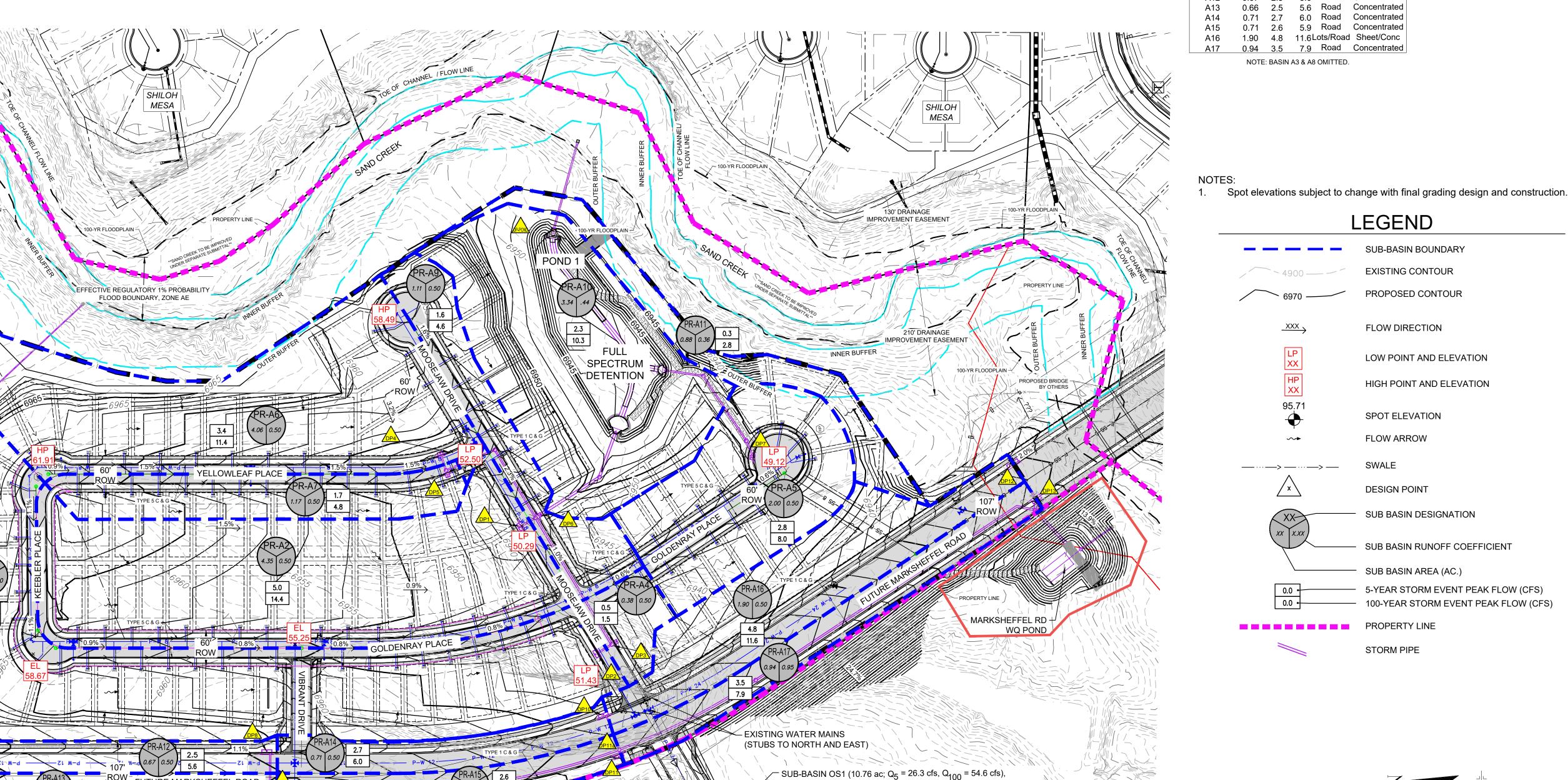
APPROVED BY:

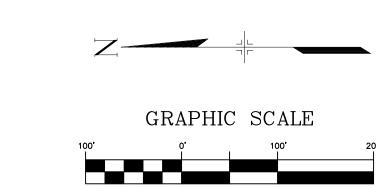
DRAWING INFORMATION: PROJECT NO: 17.886.004.000 DRAWN BY: CRAIG DOLD CHECKED BY: JEFF ODOR

JEFF ODOR

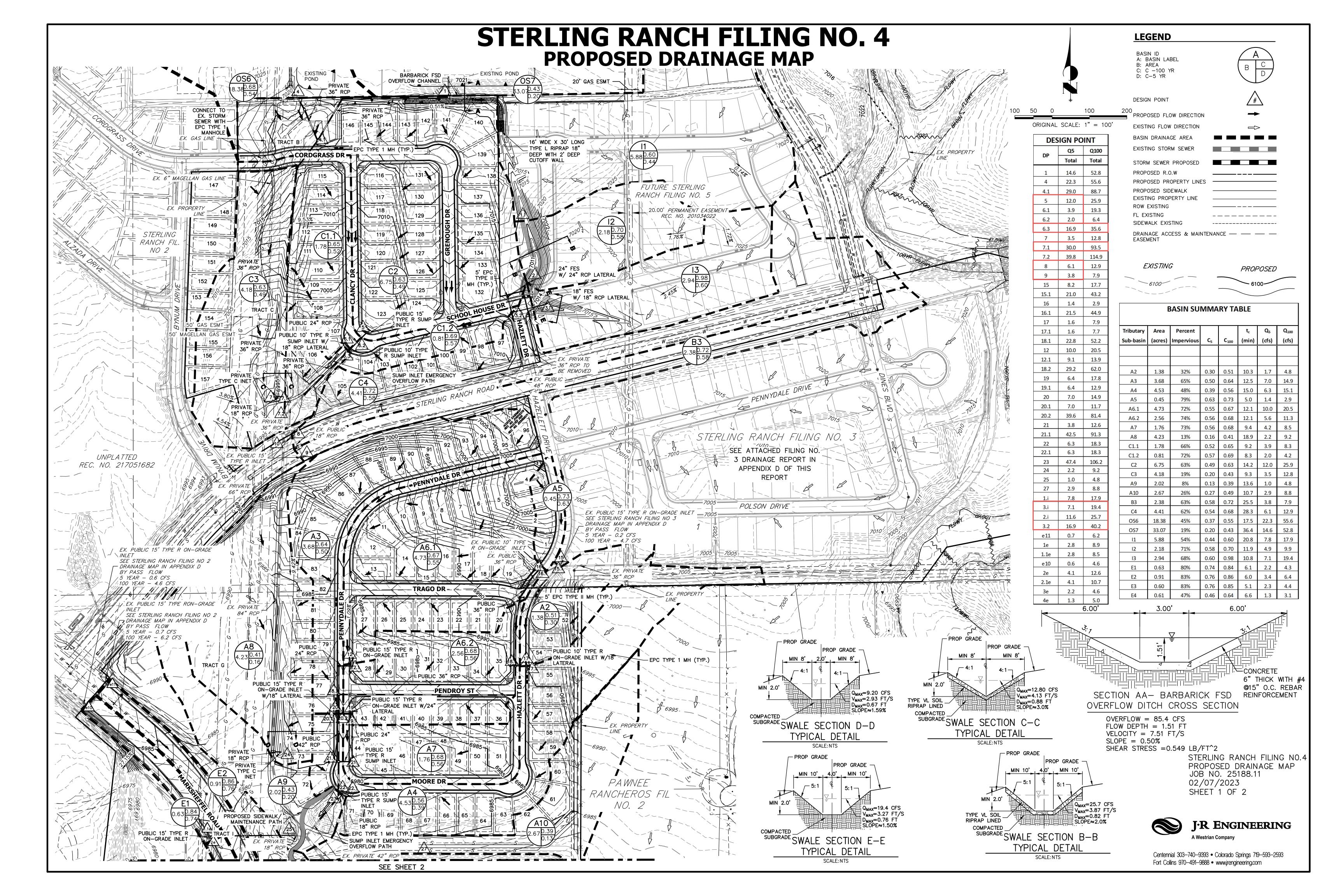
DRAINAGE **REPORT**

Area	Area	Q5	Q100	Runoff	Runoff
ID	(Acres)	(cfs)	(cfs)	Source	Type
RP-7C	1.28	2.8	6.4	Road	Concentrated
RP-7D	1.21	2.9	6.5	Road	Concentrated
A1	5.15	5.8	16.5l	_ots/Road	Sheet/Conc
A2	4.35	5.0	14.4l	_ots/Road	Sheet/Conc
A4	0.38	0.5	1.5 l	_ots/Road	Sheet/Conc
A5	2.00	2.8	8.01	_ots/Road	Sheet/Conc
A6	4.06	3.4	11.4l	_ots/Road	Sheet/Conc
A7	1.17	1.7	4.8l	_ots/Road	Sheet/Conc
A9	1.11	1.6	4.6l	_ots/Road	Sheet/Conc
A10	3.34	2.3	10.3	Pond	Sheet
A11	0.88	0.3	2.8	Channel	Concentrated
A12	0.67	2.5	5.6	Road	Concentrated
A13	0.66	2.5	5.6	Road	Concentrated
A14	0.71	2.7	6.0	Road	Concentrated
A15	0.71	2.6	5.9	Road	Concentrated
A16	1.90	4.8	11.6l	_ots/Road	Sheet/Conc
A17	0.94	3.5	7.9	Road	Concentrated
	NOTE	BASIN	1 A3 & A8	3 OMITTED.	



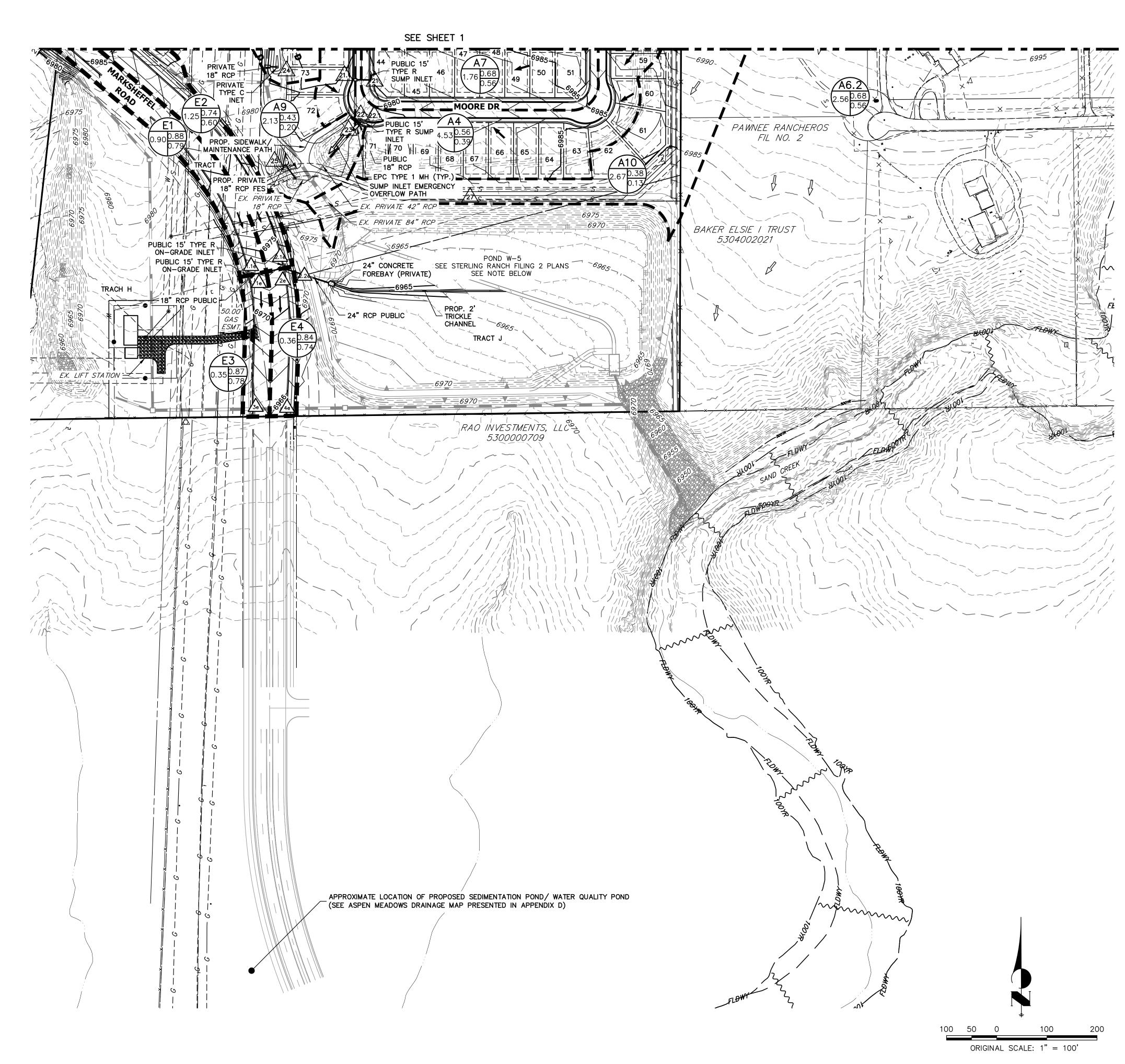


(IN FEET) 1 inch = 100 ft.



X:\2510000.all\2518811\Drawings\Sheet Dwgs\Drainage Maps\2518811 DR01_F4.dwg, DR

STERLING RANCH FILING NO. 4 PROPOSED DRAINAGE MAP



DESIGN POINT						
Q5 Q100						
DP	Total	Total				
1	14.6	52.8				
4	22.3	55.6				
4.1	29.0	88.7				
5	12.0	25.9				
6.1	3.9	19.3				
6.2	2.0	13.2				
6.3	16.9	35.6				
7	3.5	12.8				
7.1	30.0	93.5				
7.2	39.8	114.9				
8	6.1	12.9				
9	3.8	7.9				
15	8.2	17.7				
15.1	21.0	43.2				
16	1.4	2.9				
16.1	21.5	44.9				
17	1.6	7.9				
17.1	1.6	7.7				
18.1	22.8	52.2				
12	10.0	20.5				
12.1	9.1	13.9				
18.2	29.2	62.0				
	6.4					
19		17.8				
19.1	6.4	12.9				
20	7.0	14.9				
20.1	7.0	11.7				
20.2	39.6	81.4				
21	3.8	12.6				
21.1	42.5	91.3				
22	6.3	18.3				
22.1	6.3	18.3				
23 24	47.4	106.2				
	2.2	9.2				
25	1.0	5.0 8.8				
27	2.9					
1.i	7.8	17.9				
3.i	7.1	19.4				
2.i	11.6	25.7				
3.2	16.9	40.2				
e11	0.7	6.2				
1e	4.0	10.9				
1.1e	4.0	9.8				
e10	0.6	4.6				
2e	4.0	13.0				
2.1e	4.0	10.9				
2 20	0 0	20.7				

2.2e 8.0 20.7

3e 1.3 3.6 4e 1.2 4.3

	BASIN ID A: BASIN LABEL B: AREA C: C -100 YR D: C-5 YR	A B C D
С	DESIGN POINT	_#
F	PROPOSED FLOW DIRECTION	-
E	EXISTING FLOW DIRECTION	
E	BASIN DRAINAGE AREA	
E	EXISTING STORM SEWER	
5	STORM SEWER PROPOSED	
F	PROPOSED R.O.W	
F	PROPOSED PROPERTY LINES	
F	PROPOSED SIDEWALK	
E	EXISTING PROPERTY LINE	

LEGEND

ROW EXISTING

FL EXISTING

EASEMENT

SIDEWALK EXISTING

6100

DRAINAGE ACCESS & MAINTENANCE — — —

PROPOSED

ributary ub-basin Area (acres) Percent Impervious C s C 100 t c (min) Qs (cfs) Q100 (cfs) A2 1.38 32% 0.30 0.51 10.3 1.7 4.8 A3 3.68 65% 0.50 0.64 12.5 7.0 14.9 A4 4.53 48% 0.39 0.56 15.0 6.3 15.1 A5 0.45 79% 0.63 0.73 5.0 1.4 2.9 A6.1 4.73 72% 0.55 0.67 12.1 10.0 20.5 A6.2 2.56 74% 0.56 0.68 12.1 5.6 11.3 A7 1.76 73% 0.56 0.68 9.4 4.2 8.5 A8 4.23 13% 0.16 0.41 18.9 2.2 9.2 C1.1 1.78 66% 0.52 0.65 9.2 3.9 8.3 C1.2 0.81 72% 0.57

STERLING RANCH FILING NO. 4
PROPOSED DRAINAGE MAP
JOB NO. 25188.11
08/10/2023
SHEET 2 OF 2

NOTE:

FOR ADDITIONAL INFORMATION REGARDING DESIGN POINTS, ROUTING, AND RUNOFF VALUES ASSOCIATED WITH POND W-5. REFER TO THE FILING 2 DRAINAGE MAP, AS SHOWN IN APPENDIX D OF THIS REPORT.



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com

FINAL DRAINAGE REPORT FOR BRANDING IRON AT STERLING RANCH FILING NO. 1

EL PASO COUNTY, COLORADO

October 2018

Prepared for: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

Prepared by:



Project #09-006 DSD Project # SF-17-024 Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 (henceforth referred to as "Sterling Ranch Filing Nos. 1 & 2 MDDP") and the Sterling Ranch MDDP revised April 2018. Please refer to the Sterling Ranch Filing Nos. 1 & 2 MDDP by MS Civil Consultants for detailed information regarding the historic conditions of the area and discussion regarding early overlot grading which altered the existing drainage patterns prior to the issuance of this report.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

As the Hydrologic calculations performed as a part of this analysis matched the hydraulic analysis conducted with the Sterling Ranch Filing Nos. 1 & 2 MDDP, there is no need to reproduce in duplicate the hydraulic calculations provided within the aforementioned study. As such, please refer to the hydraulic calculations located in the appendix of the Master Development Drainage Report for Sterling Ranch Filing Nos. 1 & 2, and Final Drainage Report for Sterling Ranch Filing No.1 prepared by MS Civil Consultants, dated April 2017 for the relevant data sheets detailing the hydraulic analysis.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0535 F, effective date March 17, 1997 and revised to reflect LOMR, 08-08-O541P, dated July 23, 2009. An annotated FIRM Panel is included in the Appendix.

DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the aforementioned ECMs, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates) have been utilized to aid in design of the Full Spectrum Detention Facilities when required.

EXISTING DRAINAGE CONDITIONS

The Branding Iron at Sterling Ranch Filing No. 1 site consists of 10.545 acres. According to the Sterling Ranch MDDP (Existing Condition Map), historically runoff from the site drained to the southern boundary of the Sterling Ranch property (portion of Basin EX-3A) before combining with offsite runoff prior to reaching Sand Creek Channel. With the approval of the Sterling Ranch Onsite Early Grading Plan,

will be treated as WQCV and Full Spectrum Detention. As such the proposed develop shall not adversely affect the downstream infrastructure.

Water Quality/Full Spectrum Detention Facilities

With the exception of the outer permeable western and southern edges of the development the majority of the developed runoff from Branding Iron at Sterling Ranch Filing No. 1 is collected within the internal streets and conveyed via existing storm sewer systems to the existing Full Spectrum Detention Facility Pond 8 that was approved for construction as a portion of the Sterling Ranch Filing No.1 improvements. Pond 8 will provide 0.46 acre feet of water quality and 2.90 acres of full spectrum detention for approximately 29 acres of Sterling Ranch development of which the Branding Iron at Sterling Ranch Filing No.1 is a portion. The pond initially sized and designed within Sterling Ranch Filing Nos. 1&2 MDDP using the Detention Design UD-Detention v3.05 workbook. It should be noted that this drainage report and the SR Filing 1 and 2 MDDP were developed concurrently. Thus the larger scale concept planning was very finite and thus allowed for the developed flow rates to align between the two documents and thereby not requiring modifications to facility which is often common between conceptual and final design. Refer to the approved Sterling Ranch Filing No. 1 Storm Sewer Plans for additional details of FSD Pond 8.

The flows generated by Basin OS13 will be routed south via overlot grading and vegetated swales to a temporary sediment basin (future Pond W-5), at the south end of the Sterling Ranch Development. Upon development of the Sterling Ranch Filing No. 2 infrastructure Pond W-5 will be constructed and flows from Basin OS13 will be treated as WQCV (see WQCV deviation request) and Full Spectrum Detention. As such the proposed develop shall not adversely affect the downstream infrastructure.

EROSION CONTROL

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. EPC approved "Early Grading Plan for Sterling Ranch Phase I <u>Onsite</u> Grading & Erosion Control", November 18, 2015. And "Early Grading Plan for Sterling Ranch Phase I <u>Offsite</u> Grading & Erosion Control", December 3, 2015. Grading and Erosion control operations are currently underway (August 2016). Grading and Erosion Control will cease with the final development of the site in the next 12-36 months.

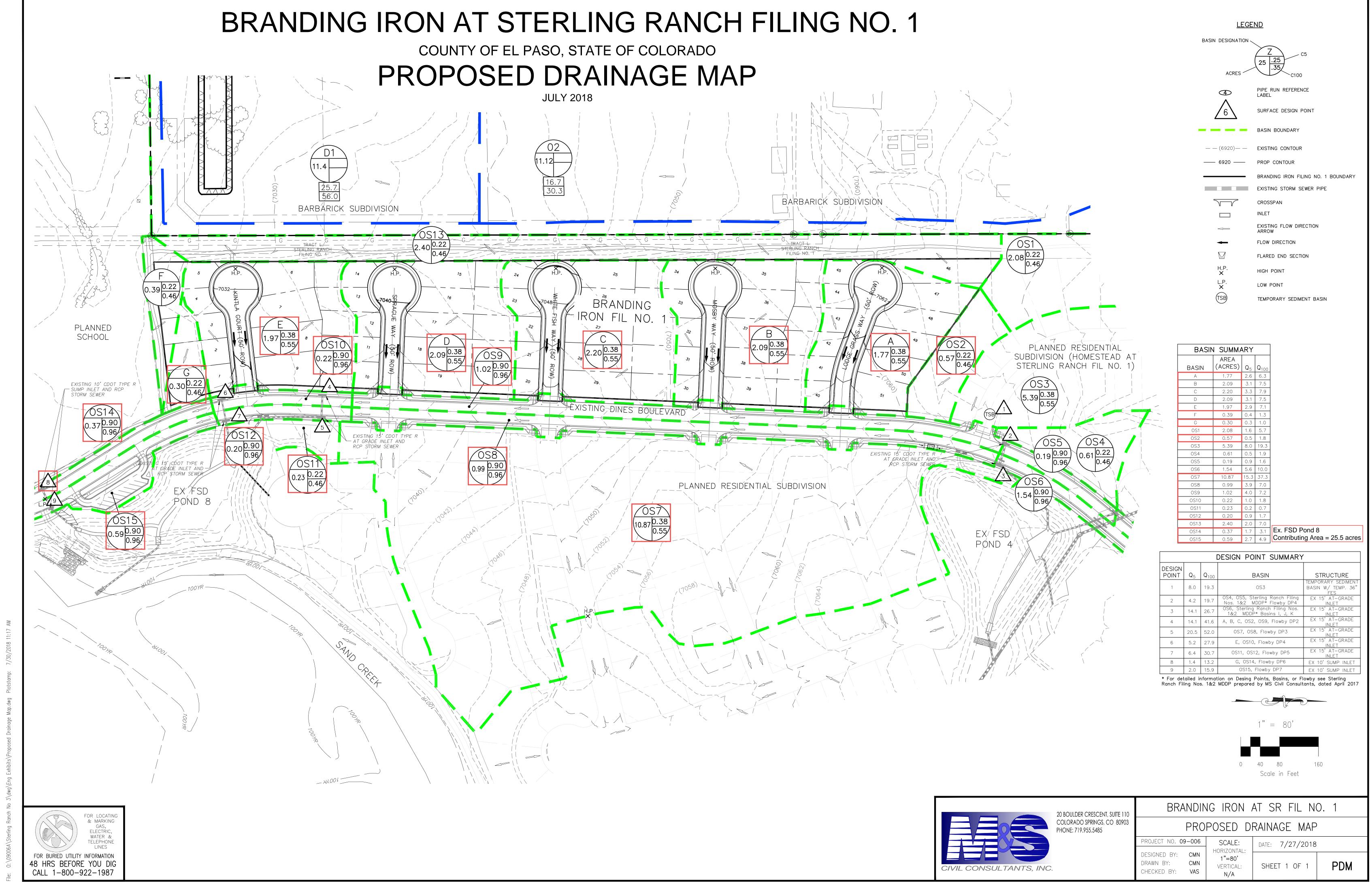
CONSTRUCTION COST OPINION – BRANDING IRON AT STERLING RANCH FIL. NO. 1

Drainage Facilities:

There are no planned improvements with the development of Branding Iron at Sterling Ranch Filing No. 1. Construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1 &2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Please see Drainage and Bridge Fees below.

DRAINAGE & BRIDGE FEES - BRANDING IRON AT STERLING RANCH FIL. NO. 1

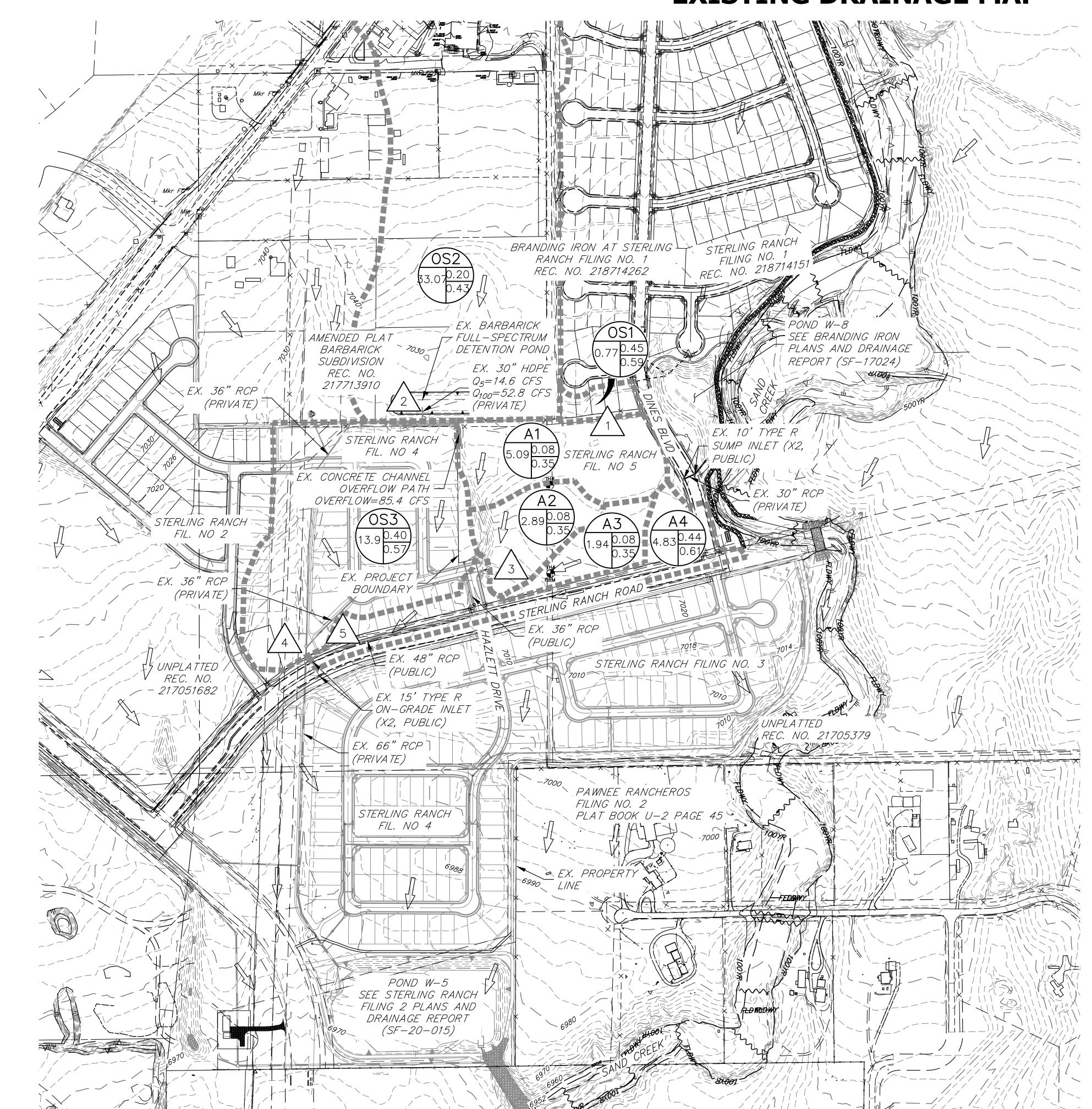
This site is within the Sand Creek Drainage Basin. The 2017 Drainage and Bridge Fees per El Paso County for the BRANDING IRON AT STERLING RANCH FILING NO. 1 site are as follows:



Appendix D Drainage Maps

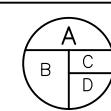


STERLING RANCH FILING 5 **EXISTING DRAINAGE MAP**



LEGEND

BASIN ID A: BASIN LABEL B: AREA C: C -100 YR D: C-5 YR



DESIGN POINT EXISTING FLOW DIRECTION

BASIN DRAINAGE AREA

EXISTING STORM SEWER

FL EXISTING

SIDEWALK EXISTING

SITE BOUNDARY EXISTING PROPERTY LINE ROW EXISTING

DRAINAGE ACCESS & MAINTENANCE — — — — EASEMENT

EXISTING

DESIGN POINT						
DD	Q5	Q100				
DP	Total	Total				
1	1.4	3.1				
2	14.6	52.8				
3	2.9	16.8				
4	19.4	46.3				
5	6.8	16.0				

BASIN SUMMARY TABLE							
Tributary Sub-basin	Area	Percent	C ₅		t _c	Q ₅	Q ₁₀₀
Sub-pasin	(acres)	Impervious	C ₅	C ₁₀₀	(min)	(cfs)	(cfs)
			Day 2007	222 222 22	2227.00.0		
A1	5.09	0%	0.08	0.35	28.7	1.0	7.6
A2	2.89	0%	0.08	0.35	15.3	0.8	5.9
А3	1.94	0%	0.08	0.35	17.9	0.5	3.7
A4	4.83	47%	0.44	0.61	18.3	6.8	16.0
OS1	0.77	65%	0.45	0.59	10.2	1.4	3.1
OS2	33.07	19%	0.20	0.43	36.4	14.6	52.8
OS3	13.90	49%	0.40	0.57	15.5	19.4	46.3



ORIGINAL SCALE: 1" = 300'

STERLING RANCH FILING 5 EXISTING DRAINAGE MAP JOB NO. 25188.16 11/03/23 SHEET 1 OF 1



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